



STPNOC Planned License Amendment Request: Technical Specification 5.3.2, Control Rod Assemblies

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STPNOC/NRC Pre-Submittal Meeting

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Objectives

- Describe STP's path forward
- Provide a description of the Unit 1 D-6 Control Rod Drive Mechanism (CRDM) issue
- Provide overview of physical configuration changes to support future operation
- Discuss impact on Chapter 15 Safety Analyses
- Provide overview of expected License Amendment Request (LAR) content
- Discuss planned submittal date and need date
- Answer NRC questions



Current Configuration

- Rod Cluster Control Assembly (RCCA) and associated drive shaft at core location D-6 have been removed
 - Flow restrictor and thimble plug installed
- Control power to stationary, moveable, and lift coils for D-6 as well as display and alarm functions have been removed
- Approved to operate Unit 1 in this condition through current fuel cycle (Cycle 20)



STP's Path Forward

- Consequences and uncertainty associated with CRDM replacement are considered significant
 - Requires special tooling and processes that currently do not exist
 - RCS pressure boundary cutting and welding
- Analyses demonstrates that STP can design future cores with 56 control rods maintaining appropriate safety margins
- Path forward is a permanent change to the design and licensing basis of the Unit 1 reactor to operate with 56 Control Rods



Overview of Proposed Change

- Requesting proposed amendment to allow Unit 1 to operate with 56 full-length control rod assemblies
- Proposed change to TS 5.3.2 (change bar on right):

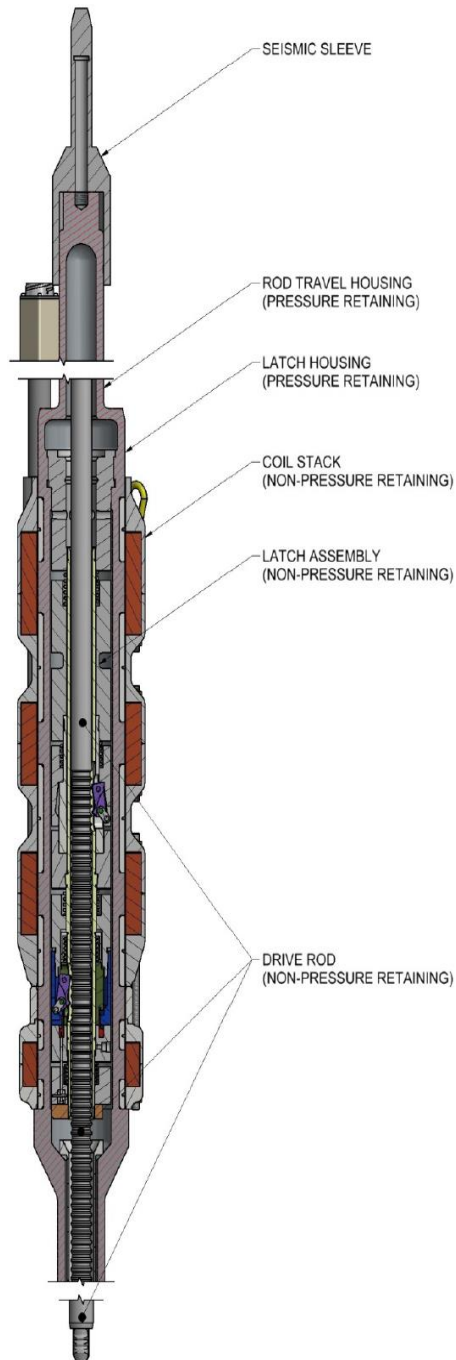
CONTROL ROD ASSEMBLIES

5.3.2 The Unit 1 core shall contain 56 full-length control rod assemblies with no full-length control rod assembly installed in core location D-6. The Unit 2 core shall contain 57 full-length control rod assemblies. The full-length control rod assemblies shall contain a nominal 158.9 inches of absorber material. The absorber material within each assembly shall be silver-indium-cadmium or hafnium. Mixtures of hafnium and silver-indium-cadmium are not permitted within a bank. All control rods shall be clad with stainless steel tubing.

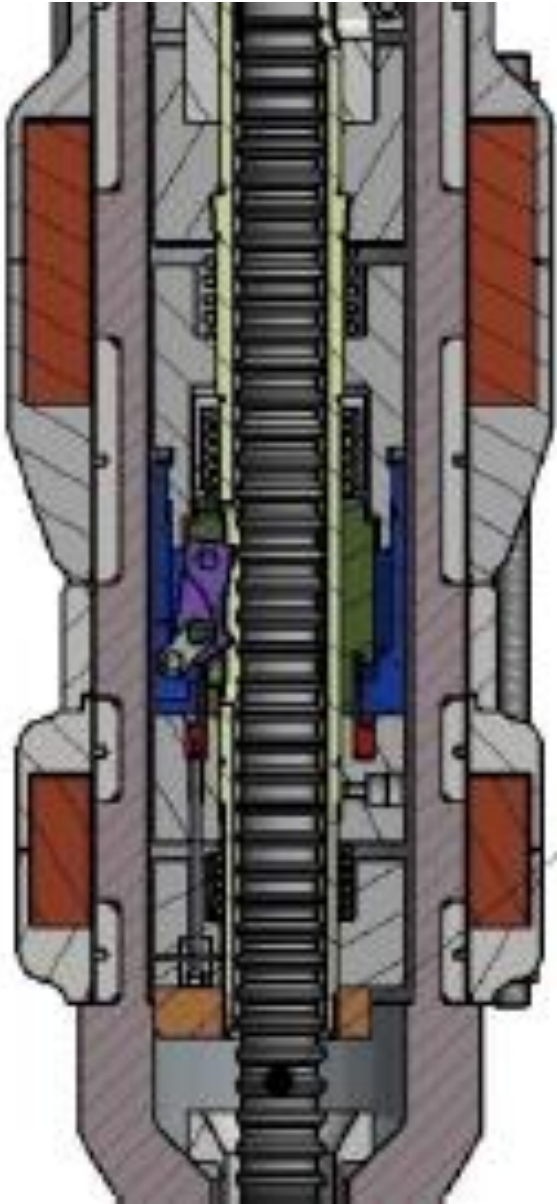


Overview of Proposed Change

- There is no methodology change involved with this change to the TS
- The proposed change would apply to Unit 1 only
- TS design description that specifies 57 control rods will remain unchanged for Unit 2



Background – CRDM Description



Background – Rod Holdout Lock Ring

- Deformation in D-6 Rod Holdout lock ring
- Initiated in 2012 during rod control sequencing while unlocking control rods
- Source of sequencing issue has been addressed with a design change



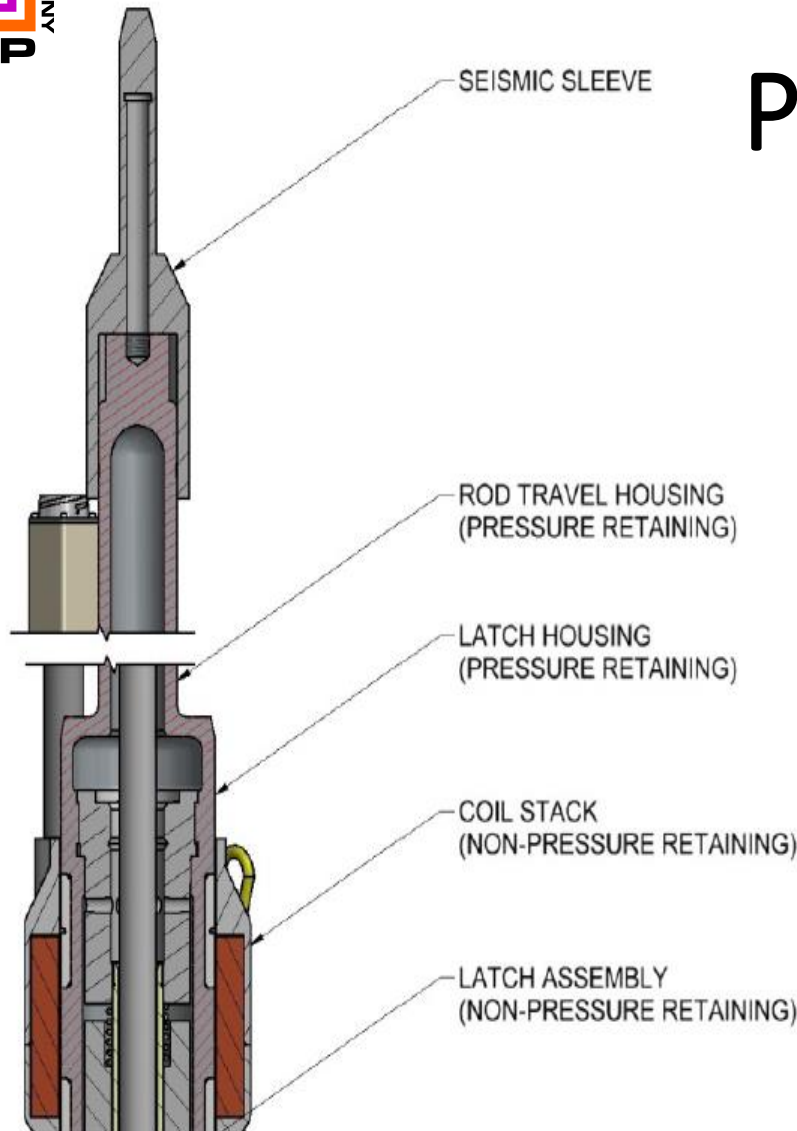
Extent of Condition

- Deformation on lockout ring is only seen on Unit 1 Rod D-6 CRDM
- Extent of condition – other 56 rods unaffected
 - Visual inspection has been performed on other 56 CRDMs
 - CRDM monitoring (coil traces) indicate other 56 CRDMs are operating reliably
- Plans for future monitoring
 - On startup: CRDM testing, rod drop timing testing
 - Periodic control rod exercise at power
 - Continue to evaluate coil traces
- Unit 2 CRDMs have been visually inspected and continue to be monitored and indicate reliable operation



Decision Inputs – Repair Evaluation

- Replacing D-6 CRDM
 - First of a kind evolution in the US (butt weld instead of canopy seal weld)
 - Post-repair maintenance testing
- Consequences and uncertainty associated with CRDM replacement are considered significant
 - Requires special tooling and processes that currently do not exist
 - RCS pressure boundary cutting and welding

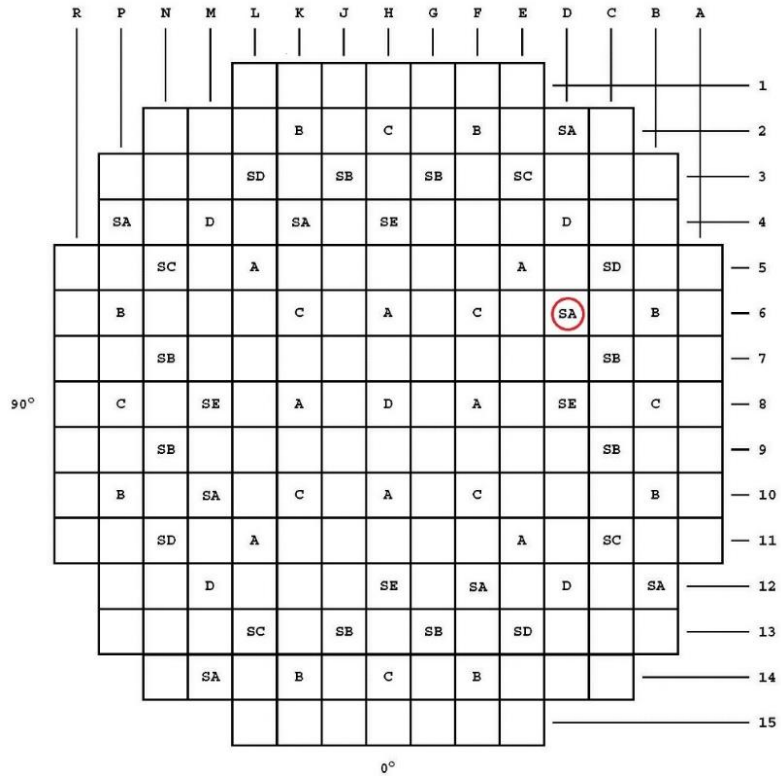


Background – Pressure Boundary

- Components being removed are internal to the RCS pressure boundary
- Pressure boundary: butt weld between CRDM latch housing and rod travel housing



Control Rod Configuration



Bank Identifier	Number of Locations	Bank Identifier	Number of Locations
A	8	SA	8
B	8	SB	8
C	8	SC	4
D	5	SD	4
		SE	4

- Rod D-6 is a Shutdown Bank rod normally positioned fully withdrawn at power
- 57 Total Control Rods
 - 29 Control Bank Rods
 - 28 Shutdown Bank Rods



Physical Configuration Changes to Support Future Operation (50.59)

- Change the plant computer rod supervision program (software) to remove input from D-6 to rod deviation alarm
- Spare in place the cabling for the D-6 CRDM, Digital Rod Position Indication (DRPI), and RHO cabling
- Existing guide tube flow restrictor remains in place to maintain flow characteristics
 - Continuing to evaluate for any potential long-term effects of the D-6 removal design change



Thermal Hydraulic Impacts

- Thimble plug will be removed to reduce fuel component handling during core refueling
 - Analysis performed to support removal
 - Causes very small increase in core bypass flow, remains bounded by safety analysis flow



Seismic and Structural Impacts

- Dynamic analysis (seismic and loss of coolant accident forces) of the CRDM that was performed using the reactor equipment system model remains valid after removal of the D-6 control rod drive shaft and RCCA
 - Drive shaft does not provide stiffening function – free motion

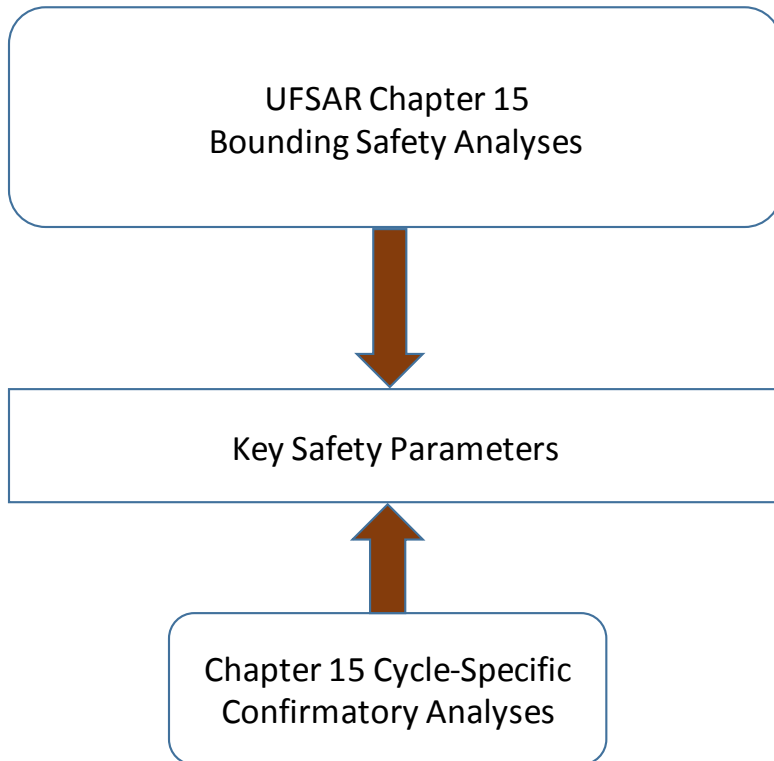


Safety Analysis – Overview

- Basis of Methodology
- Description of Methodology
- Impact of permanent removal of D-6 RCCA
 - Nuclear (Core) Design Analyses
 - Non-LOCA Transient Analyses
 - LOCA Analyses



Safety Analysis – Basis of Methodology



- STP Reload Safety Analysis uses NRC approved methodology:
 - WCAP 9272-P-A, “Westinghouse Reload Safety Evaluation Methodology”, July 1985

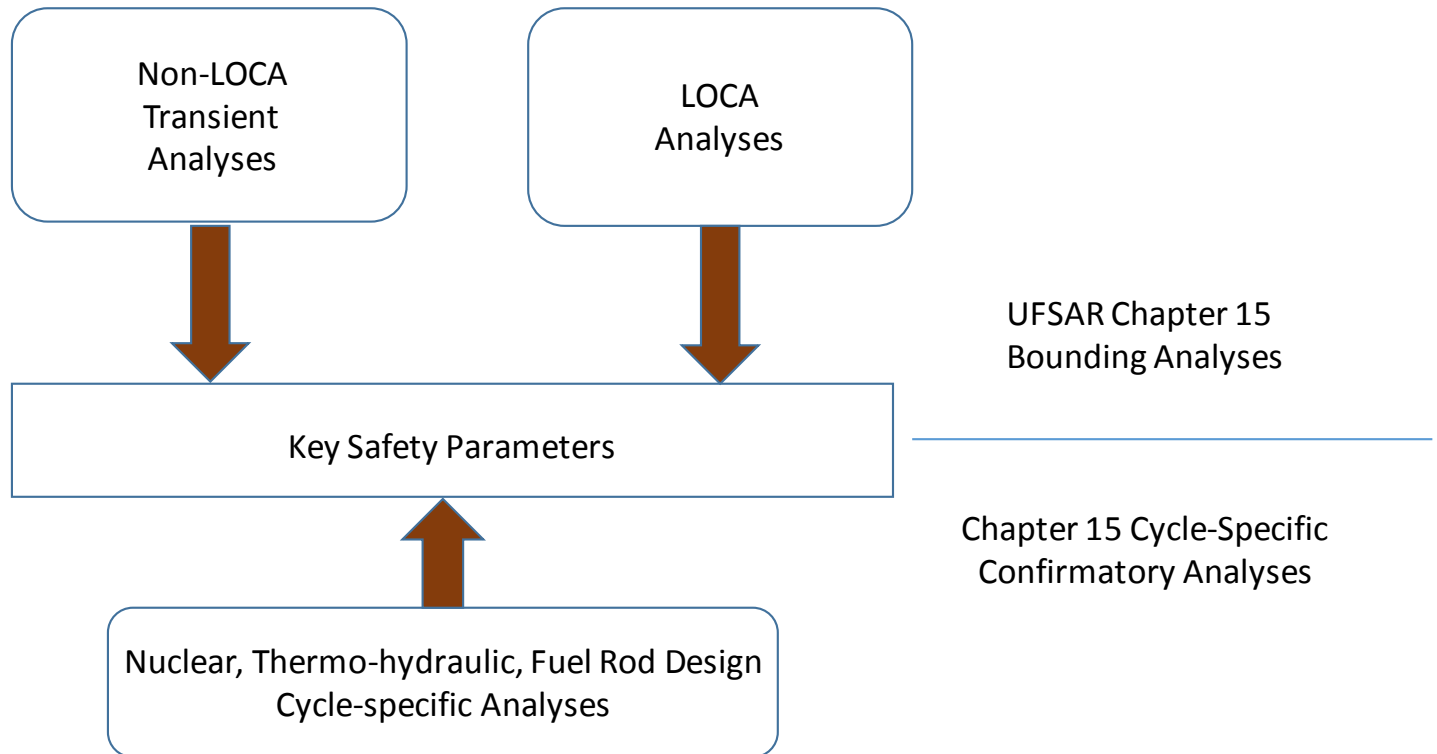


Safety Analysis – Description of Methodology

- Methodology establishes a bounding safety analysis
 - The performance and safety requirements are met through applicable acceptance limits, for example:
 - Minimum Departure from Nucleate Boiling Ratio (DNBR)
 - Maximum allowable fuel temperature
 - Maximum allowable reactor coolant system pressure
 - The bounding analyses are described in the UFSAR Chapter 15



Safety Analysis – Safety Analysis Relationships



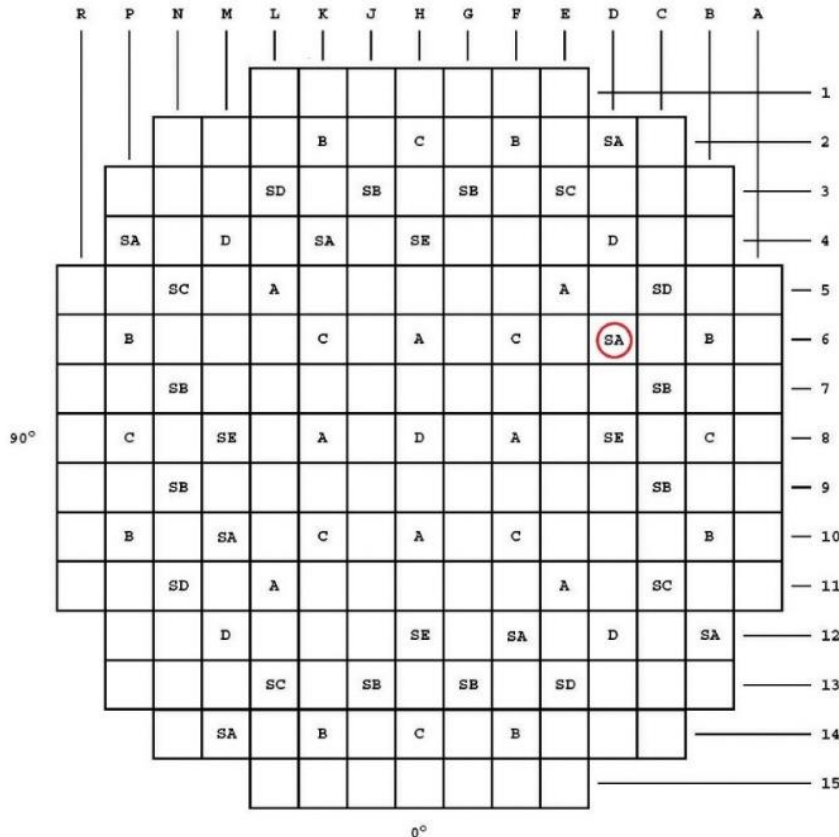


Safety Analysis – Methodology

- Chapter 15 analyses are evaluated
 - Results presented in Chapter 15 are based on bounding reference core
 - Cycle-specific information is verified against reference core to ensure Chapter 15 results remain bounded



Impact on Safety Analyses



Bank Identifier	Number of Locations	Bank Identifier	Number of Locations
A	8	SA	8
B	8	SB	8
C	8	SC	4
D	5	SD	4
		SE	4

- Power distribution within the reactor core during operation is negligibly impacted
 - Rod D-6 is a Shutdown Bank RCCA normally positioned withdrawn at power



Impact of D-6 Removal on Safety Analysis

- The removal of Control Rod D-6 could impact key safety parameters assumed in the UFSAR Chapter 15 analysis:
 - Available shutdown margin and most reactive stuck rod worth
 - Boron worth when all RCCAs are inserted
 - Rod worth of the adjacent RCCAs when all RCCAs are inserted
 - Trip reactivity as a function of time
 - Most positive moderator density coefficient (MDC)



Impact on Safety Analyses – Shutdown Margin

- Shutdown Margin used in the End-of-Life (EOL) Hot-Zero Power (HZP) Main Steam Line Break remains bounding
 - Bounding analysis for shutdown margin

Unit 1 Cycle	Burnup (MWD/MTU)	RCCA Condition	Calculated SDM (pcm)	Margin (%)
17	20400	D-6 present	2708	108
		D-6 removed	2276	75
18	19450	D-6 present	2430	87
		D-6 removed	2089	61
19	19400	D-6 present	2273	75
		D-6 removed	1968	51
20	18610	D-6 present	2432	87
		D-6 removed	2173	67



Impact on Safety Analyses – Boron Worth

- Potential impact to the chemical and volume control system (CVCS) malfunction resulting in a Reactor Coolant System (RCS) boron dilution in Modes 3, 4, and 5
- Rod removal increases boron worth for the all-rods inserted condition
- Analysis conservatively determines a boron worth with all rods out, therefore there is no impact with D-6 removed from the core



Impact on Safety Analyses – Rod Worth of Adjacent RCCAs

- Removal of Rod D-6 results in a small increase for the rod worth of the adjacent control rods with all RCCAs inserted, however
 - No impact to the fuel acceptance limits
 - Uncontrolled RCCA bank withdrawal from a subcritical or low power startup conditions and spectrum of rod ejection accidents because shutdown banks are withdrawn
 - Therefore D-6 will not add positive reactivity
 - Impacts DNBR for Main Steam Line Break, however, DNBR limit is confirmed acceptable on a cycle-specific basis



Impact on Safety Analyses – Rod Ejection Accident

- Rod Ejection N-2 Subcriticality (EOC)
 - The safety limit for subcriticality is $k_{\text{eff}} \leq 0.999$, which is met by determining N-2 rod worth is less than actual SDM + worst stuck rod worth * 0.9
 - A multi-cycle margin analysis was performed and demonstrates sufficient margin
 - Future cycles will be evaluated to ensure this limit can be met without RCCA D-6 present



Impact on Safety Analyses – Rod Ejection Accident

- Rod Ejection N-2 Subcriticality (EOC)

Unit 1 Cycle	Burnup (MWD/MTU)	RCCA Condition	N-2 Rod Worth (pcm)	Actual SDM+ WSRW * 0.9 (pcm)	Margin (%)
17	20400	D-6 present	2342	3529	34
		D-6 removed	2928	3292	11
18	19450	D-6 present	2273	3301	31
		D-6 removed	2815	3053	8
19	19400	D-6 present	2337	3187	27
		D-6 removed	2747	2937	6
20	18610	D-6 present	2175	3308	34
		D-6 removed	2659	3096	14



Impact on Safety Analyses – Trip Reactivity

- Removal of Rod D-6 reduces the total trip reactivity and the trip reactivity as a function of rod position
- A multi-cycle margin analysis was performed and demonstrates sufficient margin for total trip reactivity
- Cycle-specific analyses will be performed to ensure trip reactivity values assumed in the bounding Chapter 15 safety analyses are satisfied



Impact on Safety Analyses – Trip Reactivity (HZP)

- End-of-Cycle (EOC) HZP Trip Reactivity Following Rod Ejection
 - Safety limit is 2000 pcm for HZP

Unit 1 Cycle	Burnup (MWD/MTU)	RCCA Condition	Trip Reactivity (pcm)	Margin (%)
17	20400	D-6 present	3317	66
		D-6 removed	2605	30
18	19450	D-6 present	3145	57
		D-6 removed	2504	25
19	19400	D-6 present	2983	49
		D-6 removed	2449	22
20	18610	D-6 present	3240	62
		D-6 removed	2630	31



Impact on Safety Analyses – Trip Reactivity (HFP)

Unit 1 Cycle		RCCA Condition	Trip Reactivity (pcm)	Margin (%)
17	BOC	D-6 present	5211	30
		D-6 removed	4716	18
	EOC	D-6 present	5433	36
		D-6 removed	4854	21
18	BOC	D-6 present	5037	26
		D-6 removed	4543	14
	EOC	D-6 present	5268	32
		D-6 removed	4719	18
19	BOC	D-6 present	5071	27
		D-6 removed	4574	14
	EOC	D-6 present	5038	26
		D-6 removed	4489	12
20	BOC	D-6 present	5112	28
		D-6 removed	4625	16
	EOC	D-6 present	5256	31
		D-6 removed	4663	17

- Trip Reactivity (HFP)
 - The HFP Trip Reactivity value assumed in the Rod Ejection analysis is 4000 pcm



Impact on Safety Analyses – Moderator Density Coefficient (MDC)

- The safety limit is $0.54 \Delta k/\text{gm}/\text{cc}$
- The most positive MDC is conservatively calculated assuming all rods in the core
- Impact on the MDC calculation for removal of D-6 removal is very small
- Cycle-specific nuclear design analysis confirms the safety limit is met



Impact on Safety Analyses – LOCA Analyses

- Small Break (SB) LOCA
 - Assumptions
 - Flow restrictor in RCCA guide tube is in place
 - No explicit assumption on number of RCCAs
- Large Break (LB) LOCA and LOCA Forces
 - Assumptions
 - Flow restrictor in RCCA guide tube is in place
 - No reliance on insertion or number of RCCAs
- Operation with D-6 removed does not impact the SBLOCA, LBLOCA and LOCA Forces provided that:
 - A flow restrictor remains installed at that location
 - Adequate shutdown margin is calculated for each cycle



Impact to UFSAR Chapter 15 Accident Analyses Summary

- Bounding Chapter 15 Analyses reported in the UFSAR do not assume the number or configuration of RCCAs in the reactor core
- Cycle-specific analyses performed in accordance with WCAP-9272 will confirm bounding Chapter 15 analyses reported in the UFSAR remain satisfied
 - Effects on available shutdown margin
 - Rod worth of the adjacent control rods
 - Boron worth
 - Trip reactivity
 - Most positive MDC
- Impact on DNBR will be evaluated on a cycle-specific basis in accordance with WCAP-9272 to confirm current safety analysis limits continue to be met
- Postulated accidents dependent on core power distributions while at power are not impacted
- Therefore, the removal of RCCA D-6 does not adversely impact the results presented in Chapter 15



Regulatory Evaluation

- Requesting proposed amendment to allow Unit 1 to operate with 56 control rods
- No other changes to STP TS required
- Applicable General Design Criteria will be reviewed and are expected to be satisfied
- These items will be discussed in the proposed LAR



Proposed LAR Content – Technical Evaluation

- System description
- Current licensing basis
- Impact on the safety analysis
 - Methodology overview
 - Impact on safety parameters
 - Impact on bounding UFSAR Chapter 15 accident analyses
- Field work required to permanently remove Control Rod D-6 from service
- Evaluation of potential design impacts
 - Thermal-hydraulic
 - Seismic and structural



Overview of Proposed Change

- Proposed change to TS 5.3.2 (change bar on right):

CONTROL ROD ASSEMBLIES

5.3.2 The Unit 1 core shall contain 56 full-length control rod assemblies with no full-length control rod assembly installed in core location D-6. The Unit 2 core shall contain 57 full-length control rod assemblies. The full-length control rod assemblies shall contain a nominal 158.9 inches of absorber material. The absorber material within each assembly shall be silver-indium-cadmium or hafnium. Mixtures of hafnium and silver-indium-cadmium are not permitted within a bank. All control rods shall be clad with stainless steel tubing.



Summary Conclusions

- Utilizing current core design methodologies, future cores will be designed to remain within the criteria established in the current Chapter 15 Accident Analysis
 - Appropriate safety margins maintained with 56 control rods
- TS will be changed to describe Unit 1 as having 56 control rods
 - No other TS affected
- Instrumentation setpoints and trip settings will not be affected
- No new operator actions are proposed
- Input will be provided for No Significant Hazards Consideration determination



Proposed Schedule

- Submit LAR to NRC March 17, 2016
- Approval of the proposed amendment is requested by March 2, 2017
 - Prior to the beginning of refueling outage 1RE20
- Implementation will be prior to restart of Unit 1 Cycle 21



Additional Questions and Action Recap