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0

# **TEST PLAN 186**

# Model 880 Pipeliner Type (B) Transport Package Test Results

10 CFR 71, Packaging and Transportation of Radioactive Materials
 Subpart F – Package, Special Form, and LSA-III Tests
 Sect 71.71 Normal Conditions of Transport
 Sect 71.73 Hypothetical Accident Conditions

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### Section 1 Introduction

This document describes the mechanical test plan for the Model 880 Pipeliner Projector to meet NRC requirements for Type B(U)-96 packages as described in the Code of Federal Regulations, 10 CFR Part 71, revised as of January 1, 2009.

The test plan also covers the criteria stated in the International Atomic Energy Agency (IAEA), Safety Standards Series No. TS-R-1, Regulations for the Safe Transport of Radioactive Material, 1996 Edition, Section VI.

This document describes the test package specifications, testing equipment, testing scenario, justifies the package orientations for the different test specimens and provides test worksheets to record key steps in the testing sequence.

This series of tests is intended to evaluate any impact the Pipeliner Jacket assembly may have on the Model 880 Projector.

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### Section 2 Transport Package Description

#### Description of the Model 880 Projector Assembly

The radioactive material is sealed in a special form source capsule. The source capsule, stop and connector are swaged to a flexible steel wire to form the source wire assembly. The source wire assembly is held securely to the device by components of the rear plate assembly. One of these components, the sleeve, in conjunction with the selector ring retainer, prevents the stop ball of the source wire from being pulled through the rear of the package. Another component, the lock slide, prevents the stop ball from being pushed out of the front when in the secured position. A cover over the source wire connector prevents access to the source assembly until a keyed lock is actuated and the cover removed. This cover is in place during transport of the package.

The selector ring retainer is fastened to the rear plate with four, #10 stainless steel machine screws. The rear plate is attached to rivnuts assembled on the endplate weldment with four 5/16-18 stainless steel security screws. The endplate weldment consists of the endplate disc, a U-shaped bracket and the four rivnuts. The U-brackets are welded to the endplate disc and the endplate disc is welded to the cylindrical shell.

The shield is fastened within the device at each end by a titanium shield pin. The pin passes through the shield and the U-bracket. The shield is centered in the shell and has the source tube cast into its center. The source tube provides a cavity for the source wire assembly to travel through during use. The source capsule is positioned at the center of the ball of the shield within the source tube cavity when the source wire is in its secured position.

The model 880 uses polyurethane foam to fill the cavity around the depleted uranium shield. The foam prevents contamination to and from the depleted uranium shield.

Previous thermal tests have shown charred polyurethane foam will inhibit the flow of oxygen to the shield and prevent oxidation from occurring during a fire as long as the foam remains confined. This is shown on AEA Technology QSA Test plan number 70.

It has also been shown the charred foam will not support the shield at temperatures of 800°C. The model 880 relies on the shield pins to hold the shield in place at all times. These pins are designed to retain the shield throughout testing without the added support of the foam.

The outlet port, located at the front end, serves to block access into or out of the source tube cavity. Four stainless steel security screws fix the front plate to the endplate rivnuts.

Testing of the Model 880 Projector was performed under the following Test Plan:

• AEA Technology QSA Test Report 108 August 2000

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#### Description of the Pipeliner Jacket Assembly

The Pipeliner Jacket Assembly, Part No PL1000H, consists of:

- The Pipeliner Jacket, Part No PL1013, constructed of cast Polyurethane
  - o Pipeliner Axle Nut, Part No PL1025, constructed of Stainless Steel
- The Pipeliner Wheel Assembly, Assembly No PL1010, constructed of cast Polyurethane and:
  - o Pipeliner Wheel Hub, Part No PL1023, constructed of 6061-T6 Aluminum
  - o Pipeliner Wheel Bushing, Part No PL1024, constructed of Sintered Bronze
- The Pipeliner Wheel Axle Bolt, Part No PL1002, constructed of 303 Stainless Steel
- The Pipeliner Mounting Screws, Part No PL1030, constructed of Stainless Steel

The Pipeliner Jacket Assembly is secured to the Model 880 Projector by six #14 x <sup>3</sup>⁄<sub>4</sub> Tamperproof screws (IRSS PN PL1030) inserted through existing holes in the Projector shell. Figure 2.1 shows the Pipeliner Jacket Assembly.

Figure 2.2 shows the transport package with the Pipeliner plastic jacket assembly installed.

Figure 2.3 shows section views of the transport package with the Pipeliner plastic jacket assembly installed.

Since the jacket will be on the package during transport and its weight will add approximately 8 lbs, this series of tests will be performed with the jacket assembly installed.

In a drop, the plastic jacket may add additional protection for the transport package from further damage by absorbing energy upon impact.

The 4 foot, 30 foot and puncture orientations for these tests will be based on damage observed from orientations previously tested as part of AEA Technology QSA Test Plan 108 and speculative damaging effects the jacket may have on the safety aspects of the package.

The weight of the Model 880 transport package without a jacket installed is not greater than 46 pounds. The total weight of the package with the Pipeliner jacket installed is not greater than 55 pounds.





### FIGURE 2.2 MODEL 880 PROJECTOR WITH PIPELINER JACKET, DN 88095 Rev A

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### Section 3 Regulatory Compliance

The purpose of this plan, which was developed in accordance with QSA WI-E-1808, is to demonstrate that the Model 880 Pipeliner projector complies with the Type B(U)-96 transport package test requirements as described in the Code of Federal Regulations, 10 CFR Part 71, revised as of January 1, 2009 and the International Atomic Energy Agency (IAEA), Safety Standards Series No. TS-R-1, Regulations for the Safe Transport of Radioactive Material, 1996 Edition, Section VI.

The Model 880 Projector assembly was previously tested and approved for use as a transport package without the addition of a jacket as well as with the standard Sentinel jacket. This series of tests will evaluate the effect of adding the Pipeliner jacket to the Model 880 Projector.

The water spray preconditioning of the package will not be performed as the Model 880 Projector and the Pipeliner Jacket assemblies are constructed of waterproof materials throughout. The water spray would not contribute to any degradation in structural integrity.

The Normal Condition of Transport test to be performed is the 1.2m (Four-foot) free drop test (10 CFR 71.71 (c) (7)). (IAEA, TS-R-1, Para 722 (a)

The Hypothetical Accident Tests (10 CFR 71.73) to be performed are the 9m (30 foot) free drop test and the puncture test. (IAEA, TS-R-1, Para. 727(a) and 727(b))

The Stacking (Compression) Test TS-R-1 para 723 and 10CFR 71.71(c)(9) will not be performed as the Model 880 Projector was previously tested and the Pipeliner Jacket assembly should not adversely affect the results of this test.

The Penetration Test TS-R-1 para 724 and 10CFR 71.71(c)(10) will not be performed as the Model 880 Projector was previously tested and the Pipeliner Jacket assembly should not adversely affect the results of this test.

The Crush Test (10 CFR 71.73(c)(2)) will not be performed because the radioactive contents are qualified as Special-Form radioactive material.

The Thermal Test of (10 CFR 71.73(c)(4)) will not be performed as the Model 880 Projector has previously been evaluated for this requirement and the materials used in the Pipeliner Jacket have no different effect than the original Sentinel jacket. If damage to the 880 itself should occur during testing and there is an opening in the stainless steel shell that could expose the DU shield the waiver of thermal testing will be re-evaluated.

The melting points for the materials of the package are listed below:

TABLE 3.1	MATERIAL MELTING POINT	۲ <b>S</b>
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Material	Melting Point
Stainless steel	1390°C (2530°F)
Depleted uranium	1135°C (2075°F)
Titanium	1700°C (3100°F)
Tungsten	3410°C (6170°F)
Copper/Brass	1080°C (1980°F)
Aluminum	580°C (1080°F)
Rubber/Plastic	Less than 540°C (1000°F)

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The immersion test will not be performed. Only the source capsule (containment vessel) is sealed. The source capsule is designed and tested to withstand external pressures well in excess of 22  $lbf/in^2$ . All other assemblies are designed to allow equalization of internal and external pressure

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### Section 4 Discussion on System Failure Modes of Interest

#### <u>General</u>

The tests in this plan focus on damaging those components of the package which could cause displacement of the source from its stored position within the depleted uranium shield and which affect the integrity of the shield itself.

#### Normal and Accident Conditions of Transport

The modes of failure under normal and accident conditions that could lead to elevated dose rates include the following:

- Fracture or penetration of the projector weldment.
- Displacement of the shield within the projector weldment and distortion or fracture of the source.
- Failure of the source lock assembly and/or lock mounting screws.

The test conditions specified in this Test Plan are intended to challenge the ability of the Model 880 Pipeliner package with respect to these failure modes.

#### **Orientations to be Tested**

Based on previous testing of the 880 camera the area most subject to damage is the Rear Plate Assembly PN 88020. Damage to the Rear Plate Assembly could cause the source to become displaced or loose. Although this area passed all previous testing the Pipeliner jacket is oriented differently than the standard 880 jacket and may not offer the same protection to this assembly. This could affect the results.

Other orientations:

- Bottom Surface Impact; if an impact to the bottom surface caused the jacket to split the wheels would spread out around the body rather than impacting the shell. If the jacket did not split the jacket should absorb the impact of the wheels. In either case there is little likely hood that the shell would be significantly damaged.
- Top & Side Impacts; Impacts to the top or side surfaces might cause the plastic jacket to split, but it is highly unlikely that this would significantly damage the metal shell.

Based on the above, two orientations will be tested, both impacting the Rear Plate Assembly:

- The first orientation will be with the longitudinal axis of the camera vertical
- The second orientation will be with the Rear Plate Assembly parallel to the impact surface

### Section 5 Assessment of Package Conformance

#### **Regulatory Requirements**

#### • Normal Conditions of Transport (10 CFR 71.43(f))

There should be no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

IAEA Safety Standards Series No. TS-R-1, Para 622 (b) stipulates that the loss of shielding integrity should not result in more than a 20% increase in the radiation level at any external surface of the package.

#### • Hypothetical Accident Conditions (10 CFR 71.51(a))

There should be no escape of radioactive materials greater than  $A_2$  in one week and no external dose rate greater than 1 R/hr at 1m from the external surface with the maximum radioactive contents which the package is designed to carry.

#### **Test Package Contents**

The Model 880 Pipeliner projector is designed to carry a special form source. Containment of the radioactive source is tested at manufacture. The source capsule design has been certified in accordance with the performance requirements for special form as specified in 10 CFR Part 71 and IAEA Safety Standards Series No. TS-R-1.

A simulated source assembly, model 424-9, will be used during testing of the package. The radiation levels after testing will be measured by replacing the simulated source with an active source

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### Section 6 Construction and Condition of Test Specimens

The Model 880 transport package test specimens will be manufactured in accordance with the QSA Global, Inc. (QSA) Quality Assurance Program. The weight of each test specimen per this drawing is not greater than 46 pounds.

The Pipeliner jacket assemblies will be manufactured and supplied by IRSS in accordance with the Industrial Radiography Supplies and Services Inc. (IRSS) Quality Assurance Program, as an approved supplier to QSA. IRSS Certificates of Compliance for the supplied parts and assemblies will be included as part of the final test report.

Assembly of the Pipeliner test specimens used for these tests will be done by QSA staff qualified to perform maintenance on 880 projectors in accordance with Industrial Radiography Supplies and Services Inc. (IRSS) instructions for conversion of a standard Model 880 projector titled "Work instruction for performing Pipeliner Retro Fit" Rev 1.

Inspection of the finished assemblies will be performed by the QSA QC department in accordance with the requirements of Industrial Radiography Supplies and Services Inc. (IRSS) instructions for conversion of a standard Model 880 projector titled "Work instruction for performing Pipeliner Retro Fit" Rev 1. This represents the process QSA and IRSS intend to use for the manufacture of production units. Additionally, the test specimens will be inspected in accordance with IIR 88095 Rev

The IRSS assembly instructions include the installation of the Collimator and Shoe assemblies as required for use. These components are not part of the transport container assembly and are not included in this test plan. After the assembly and inspection of each test unit is completed the test units will be reconfigured to the transport condition as specified in IRSS Pipeliner Operations and Maintenance Manual. This involves the removal of the Pipeliner Shoe and Collimator assemblies. A copy of this manual will be included as part of the final test report.

The weight of each test specimen with the Pipeliner jacket is not greater than 55 pounds

The structural materials of the Model 880 are made of AISI Type 300 series stainless steel and titanium. The shielding materials are depleted uranium and tungsten. The non-safety related parts are made from aluminum, brass, copper, plastic, and rubber.

The Pipeliner jacket assembly is constructed of cast polyurethane, aluminum, bronze & Type 303 stainless steel.

All tests of this plan will subject the test specimen to an impact from a drop. The mechanical strength and ductility of the critical components of the package must continue to perform as expected at the ambient temperature conditions of  $-40^{\circ}$ F to  $100^{\circ}$ F.

The fracture toughness, strength and ductility, of the structural materials in the Model 880 Projector do not change significantly at or between the temperatures of  $-40^{\circ}$ F to  $100^{\circ}$ F. The shielding materials are relatively brittle throughout this entire temperature range.

The Pipeliner jacket material has a rated operating temperature range of approximately -30°F to 200°F. Because this does not meet the minimum -40°F temperature requirement of "10 CFR 71, Sect 71.73 Hypothetical Accident Conditions" this series of tests will be performed with the test units cooled to -40°F.

The primary containment is the source capsule, a special form sealed capsule welded at atmospheric pressure and pressure tested to 290 psi minimum. Except for this capsule the package is open to the atmosphere. The internal operating pressure of the containment system is considered to be in equilibrium with the outside pressure of the package. Therefore, the initial pressure of the Pipeliner system has no effect on these tests.

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Section 7 Material and Equipment List

The equipment list worksheets in Section 15 identify the equipment required, with additional space to list other necessary equipment and measuring instruments needed to perform the tests. Additional materials and equipment used to facilitate the tests will be listed as needed.

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### Section 8 Test Procedure

#### <u>General</u>

All test specimens are to be tested in the sequence presented below. Each test has been designed to check the integrity of various components of the package. An assessment of transport integrity of the package will be made based on the cumulative effect of the tests performed on the package

The test specimens will have an orientation selected to produce the most damage to the package based on the results of Test Plan 108. The justification and description for this orientation shall be documented.

The tests have the following sequence:

- 1. Test specimen preparation and inspection
- 2. 1.2m (Four-foot) free drop test (10 CFR 71.71 (c) (7))
- 3. 9m (30-foot) free drop test (10 CFR 71.73 (c) (1))
- 4. Puncture test (10 CFR 71.73 (c) (3))
- 5. Final test inspection and/or assessment.
  - a. The Pipeliner jacket assembly is to be removed prior to profiling.
  - b. Repeat the profiling procedure used to inspect QSA PN 88015 prior to testing
- 6. Test specimen storage.

#### **Roles and Responsibilities**

The responsibilities of the groups identified in this plan are:

- Engineering executes the tests according to the test plan and summarizes the test results. Engineering also provides technical input to assist Regulatory Affairs and Quality Assurance as needed.
- **Regulatory Affairs** monitors the tests and reviews test reports for compliance with regulatory requirements.
- Quality Assurance oversees test execution and test report generation to assure compliance with the QSA Global Quality Assurance Program.
- Engineering, Regulatory Affairs and Quality Assurance are jointly responsible for assessing test and specimen conditions relative to 10 CFR 71 and IAEA TS-R-1..
- Quality Control is responsible for ensuring test and specimen data is measured and recorded throughout the test cycle.

### Section 9 Test Specimen Preparation and Inspection

1. Manufacture three Model 880 projectors per QSA Global drawing number B88015, revision C. The projector is profiled per WI-Q1816 as part of this procedure.

- 2. Mount the three projectors in the Pipeliner jacket assemblies, IRSS part number PL1000H revision 1, per IRSS instructions for conversion of a standard Model 880 projector titled "Work instruction for performing Pipeliner Retro Fit" Rev 1.
- 3. Clearly and indelibly mark each specimen: "TP186(X)". Where X is an alphabetically incremented letter beginning with "A". One of the three projectors will be used as a spare and used to replace a specimen dropped onto the wrong impact point, if necessary. The spare, if used, will follow the same test sequence as the initially selected specimen.
- 4. Measure and record the weight of each specimen. This weight must not exceed the maximum specified 55 lbs
- 5. Inspect the test specimens to ensure that:
  - a. All fabrication and inspection records are documented in accordance with the QSA Global Quality Assurance Program.
  - b. The test specimens comply with the requirements of the drawings and the IRSS assembly instructions.



## Section 10 Summary of Test Schedule





### Section 11 1.2m (4-foot) Free Drop Test (10 CFR 71.71(c)(7))

The Normal Transport Conditions Test is the 1.2m (4-foot) free drop test as described in 10 CFR 71.71(c)(7). The figures of this section illustrate the orientations for the test specimens.

#### • <u>1.2m Free Drop Test Set-up</u>

To set up a package for the 1.2m (4-foot) drop test:

- 1. Measure and record the weight of the test specimen.
- 2. Cool the test specimen to  $-40^{\circ}$ F
- 3. Measure and record the test specimen and ambient temperatures.
- 4. Position the 1st specimen on the drop surface and position it according to the orientation shown in Figure 11.1.1
- 5. Raise the package so that the impact target is 1.2m (4 feet) above the drop surface. Ensure the center of gravity is over the impact point
- 6. Measure and record the ambient temperature.
- 7. Photograph the set-up.
- 8. Start the video recorder.
- 9. Drop the package.
- 10. Stop the video recorder.
- 11. Record the damage to the package and take a photographic record.
- 12. Repeat steps 3 10 with the  $2^{nd}$  specimen positioned as shown in Figure 11.1.2

#### Specimen TP186(A) Orientation for the 1.2m Drop Test

Figure 11.1.1 shows the package orientation for Specimen TP186(A).

The specimen will be dropped with its axis normal to the drop surface with the lock assembly facing down.

The object of the drop is to use the lock cover as leverage to drive the rear plate across the endplate to shear the rear plate mounting screws.



#### FIGURE 11.1.1 SPECIMEN TP186(A) ORIENTATION FOR THE 1.2M DROP TEST

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#### Specimen TP186(B) Orientation for the 1.2m Drop Test

Figure 11.1.2 shows the package orientation for Specimen TP186(B).

The specimen will be dropped with its axis at approximately 22.5 degrees to the drop surface with the lock assembly facing down.

The object of this drop is to test the integrity of the end plate and to determine the effect of the drop on the depleted uranium shield.



#### FIGURE 11.1.2 SPECIMEN TP186(B) ORIENTATION FOR THE 1.2M DROP TEST

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#### 1.2m Free Drop Test Assessment

Upon completion of each test, Engineering, Regulatory Affairs and Quality Assurance team members will jointly take the following actions:

- 1. Review the test execution to ensure that each test was performed in accordance with this test plan.
- 2. Make a preliminary evaluation of the specimens relative to the requirements of 10 CFR 71 and IAEA Safety Standards Series No. TS-R-1.
- 3. Assess the damage to each specimen to decide whether testing of that specimen is to continue.
- 4. Evaluate the condition of each specimen to determine what changes, if any, are necessary in package orientation in the 30-foot drop test to achieve maximum damage.

### Section 12 9m Free Drop Test (10 CFR 71.73(c)(1))

The first Hypothetical Accident Test is the 9m (30-foot) free drop test as described in 10 CFR 71.73(c)(1).

The figures of this section illustrate the orientations for the test specimen.

#### <u>9m Free Drop Test Set-up</u>

To set up a package for the 9m (30-foot) drop test:

- 1. Measure and record the weight of the test specimen.
- 2. Cool the test specimen to -40°F
- 3. Measure and record the test specimen and ambient temperatures.
- 4. Position the 1st specimen on the drop surface and position it according to the orientation shown in Figure 12.2.1
- 5. Raise the package so that the impact target is 9m (30 feet) above the drop surface. Ensure the center of gravity is over the impact point
- 6. Measure and record the ambient temperature.
- 7. Photograph the set-up.
- 8. Start the video recorder.
- 9. Drop the package.
- 10. Stop the video recorder.
- 11. Record the damage to the package and take a photographic record.

12. Repeat steps 3 - 10 with the  $2^{nd}$  specimen positioned as shown in Figure 12.2.2

#### Specimen TP186(A) Orientation for the 9m Drop Test

Figure 12.2.1 shows the package orientation for Specimen TP186(A).

The specimen will be dropped with its axis normal to the drop surface with the lock assembly facing down.

The object of the drop is to use the lock cover as leverage to drive the rear plate across the endplate to shear the rear plate mounting screws.



FIGURE 12.2.1 SPECIMEN TP186(A) ORIENTATION FOR THE 9M DROP TEST

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#### Specimen TP186(B) Orientation for the 9m Drop Test

Figure 12.2.2 shows the package orientation for Specimen TP186(B).

The specimen will be dropped with its axis at approximately 22.5 degrees to the drop surface with the lock assembly facing down.

The object of this drop is to test the integrity of the end plate and to determine the effect of the drop on the depleted uranium shield.



FIGURE 12.2.2 SPECIMEN TP186(B) ORIENTATION FOR THE 9M DROP TEST

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### 9m Free Drop Test Assessment

Upon completion of each test, Engineering, Regulatory Affairs and Quality Assurance team members will jointly take the following actions:

Review the test execution to ensure that each test was performed in accordance with 10 CFR 71, IAEA Safety Standards Series No. TS-R-1, and this test plan.

Make a preliminary evaluation of the specimens relative to the requirements of 10 CFR 71 and IAEA Safety Standards Series No. TS-R-1.

- 1. Assess the damage to each specimen to decide whether testing of that specimen is to continue.
- 2. Evaluate the condition of each specimen to determine what changes, if any, are necessary in package orientation in the puncture test to achieve maximum damage.

### Section 13 Puncture Test (10 CFR 71.73(c)(3))

The package is dropped from a height of 1m (40") onto the puncture billet. This test uses the 12" high puncture billet. The billet meets the minimum height (8") required in 10 CFR 71.73(c)(3). The specimen has no projections or overhanging members longer than 12" which could act as impact absorbers, allowing the billet to cause the maximum damage to the specimen. The billet is to be bolted to the drop surface used in the drop tests.

The figures of this section illustrate the orientations for each puncture test.

The justification for each puncture orientation is the same as the orientation for the 30-foot drop test. If the orientation needs to be changed, the new orientation must be documented and approved with a justification describing how it would be a worst condition than the planned orientation.

#### Puncture Test Set-up

**NOTE:** Because each test is designed to add to damage inflicted on a specific component or assembly in the preceding test, it is important that each specimen maintain its identity throughout the battery of tests and that the set-up instructions specific to the specimen are strictly followed.

To set up a package for the puncture test:

- 1. Measure and record the weight of the test specimen.
- 2. Cool the test specimen to -40°F
- 3. Measure and record the test specimen and ambient temperatures.
- 4. Position the 1st specimen on the drop surface and position it according to the orientation shown in Figure 13.3.1
- 5. Raise the package so that the impact target is 1m (40") between the impact point on the package and the top of the puncture billet. Ensure the center of gravity is over the impact point
- 6. Photograph the set-up.
- 7. Start the video recorder.
- 8. Drop the package.
- 9. Stop the video recorder.
- 10. Record the damage to the package and take a photographic record.
- 11. Repeat steps 1 9 with the 2<sup>nd</sup> specimen positioned as shown in Figure 13.3.2

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#### Specimen TP186(A) Orientation for the Puncture Test

The objective of this drop orientation (Figure 13.3.1) is to continue the damage inflicted on the specimen by the 9m-drop test.

The specimen will be dropped with its axis normal to the drop surface with the lock assembly facing down.

The specimen will be offset from the Puncture Billet as shown so that the jacket does not hit first.



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#### Specimen TP186(B) Orientation for the Puncture Test

The objective of this drop orientation (Figure 13.3.2) is to continue the damage inflicted on the specimen by the 9m-drop test.

The specimen will be dropped with its axis at approximately 22.5 degrees to the drop surface with the lock assembly facing down.



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### **Puncture Test Assessment**

Upon completion of the test, **Engineering**, **Regulatory** Affairs and **Quality** Assurance team members will jointly take the following actions:

Review the test execution to ensure that the tests were performed in accordance with 10 CFR 71, IAEA Safety Standards Series No. TS-R-1, and this test plan.

Make a preliminary evaluation of each specimen relative to the requirements of 10 CFR 71 and IAEA Safety Standards Series No. TS-R-1.

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#### Final Test Inspection and Assessment

Perform the test inspection after the puncture tests.

- 1. Measure and record the damage to each of the test specimens. Measure and record the package for signs of any permanent strain.
- 2. Measure and record the location of the source from the front plate.
- 3. Remove and assess the condition of the simulated source.
- 4. Reassemble the packages using a representative active source, making sure that the source position and the package configuration are the same as they were immediately after the puncture test.
- 5. Measure and record a radiation profile of each test specimen in accordance with QSA Work Instruction WI-Q-1806.
- 6. Assess the significance of any change in radiation at the surface and at one meter from the packages.
- 7. Determine whether it is necessary to dismantle either of the test specimens for inspection of hidden component damage or failure.
- 8. If the decision is taken to proceed with the inspection, record and photograph the process of removing any component.
- 9. Measure and record any damage or failure found in the process of dismantling the test specimens.

Engineering, Regulatory Affairs, and Quality Assurance team members will make a final assessment of each test specimen and jointly determine whether the specimens meet the requirements of 10 CFR 71 and IAEA TS-R-1.

### Section 15 Worksheets

Use the following worksheets for executing the tests of section 8. Each test shall have three worksheets; an equipment list, a procedure checklist, and a data sheet. Record the information onto copies of these worksheets for each test performed.

Attach a copy of the relevant inspection report or calibration certificate after the range and accuracy of the equipment has been verified.

### WORKSHEET 15.1 DROP & PUNCTURE TEST SPECIMEN & EQUIPMENT LIST

		Test Specime	n		
Configuration	Drawing Numb	er Serial Number	· **Attach IIR	**Attach NCR	**Attach Route Card
Pipeliner Transport	88095 Rev A	TP180A	Yes	See IIR	See TMI 279
Pipeliner Transport	88095 Rev A	TP180B	Yes	See IIR	See TMI 279
Pipeliner Transport	88095 Rev A	TP180C	Yes	See IIR	See TMI 279
** Note: Copie	es of these recor	ds are stored on th	e network in the	following	lirectory:
"K:\4 Design Hist	ory Files\Model 88	80 Pipeliner\Verificatio	on (Testing)\TP 186	\Test Specime	en Records"
Tool Descr	iption	Enter the Model a Mark NA wl	nd Serial Number Ien not used.	**Atta Report C	ch Inspection or Calibration ertificate
Drop Surlace, Drawing	, NO. 110/40	5/N	· · · · · · · · · · · · · · · · · · ·		Vos
I uncture Dinet, Diawa					Yes
Weight Scale	· · · ·				
Weight Scale Record any additional certificates.	tools used to facilit	ate the test and attach	the appropriate ins	pection repor	t or calibration
Weight Scale Record any additional certificates. Radiation Meter with F	tools used to facilit Probe	ate the test and attach 1863 Meter / S	the appropriate ins HP-270 Probe	pection repor	t or calibration Yes
Weight Scale Record any additional certificates. Radiation Meter with H	tools used to facilit Probe	ate the test and attach 1863 Meter / S Print Name	the appropriate ins HP-270 Probe	pection repor	t or calibration Yes
Weight Scale Record any additional certificates. Radiation Meter with H Signature Engineering:	tools used to facilit Probe	ate the test and attach 1863 Meter / S Print Name	the appropriate ins HP-270 Probe	pection repor	t or calibration Yes
Weight Scale Record any additional certificates. Radiation Meter with H Signature Engineering: Regulatory:	tools used to facilit Probe	ate the test and attach 1863 Meter / S Print Name	the appropriate ins HP-270 Probe	Date	t or calibration Yes

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## WORKSHEET 15.2 DROP & PUNCTURE TEST CHECKLIST

Test:		
Test Location:		
Step		Data
1. Record test specimen serial number:		
2. Record the test specimen weight:		
3. Record the ambient temperature (°C):		Instrument S/N:
3. Record the test unit temperature (°C):		Instrument S/N:
4. Identify set-up orientation figure:		I
5. Record drop height.		
6. Photograph set-up in at least two perpendicular planes.		
7. Begin video recording of the test so that impact is recorded.		
8. Release the test specimen.	<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>	
9. Stop the video recorder. Ensure the point of impact and orient	tation specified in the plan	n has been achieved.
10. Record the damage to the test specimen. Use a separate sheet	and attach, if needed.	
11. Engineering, Regulatory Affairs and Quality Assurance make Record the assessment on a separate sheet and attach.	a preliminary assessmen	t relative to 10 CFR 71.
Test witnessed by (Signature)	Print Name	Date
Engineering:		
Regulatory Affairs:	······································	
Quality Assurance:		

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### WORKSHEET 15.3 DROP & PUNCTURE TEST DATA SHEET

		1
Test Date:		Test Time:
Describe drop orientatio	n and drop height:	<b>1</b>
Describe impact (locatio	on, rotation, etc.):	
Describe on-site inspect	ion (damage, broken parts, etc.):	
On-site test assessment:		
• Was the test perform	ed in accordance with 10 CFR 71	I, IAEA TS-R-1 1996, and this test plan? Yes or No.
<ul> <li>Does the test specim</li> </ul>	en meet the requirements of 10 C	FR 71 and IAEA TS-R-1 1996 for this test? Yes or No.
• Are any changes to	subsequent drop orientations nee	ded to achieve maximum damage? Yes or No.
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> </ul>	ge occur to warrant additional dra nue with this test specimen? Yes	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> <li>Will the test specim</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or No
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> <li>Will the test specim</li> <li>Engineering:</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on <b>Regulatory:</b>	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or No QA:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test di</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection:	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or No QA:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test di</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection:	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or No QA:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing conti</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test displayers and post-test displayers</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection:	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or No QA:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing contiant</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test diant</li> <li>Describe any change in second se</li></ul>	ge occur to warrant additional dru nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection: source position (if possible):	ded to achieve maximum damage? Yes or No. op? Yes or No. or No. If yes, next test: the accumulated damage assessment? Yes or NoQA:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing contiant</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test diant</li> <li>Describe results of radio</li> <li>Completed by:</li> </ul>	ge occur to warrant additional dro nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection: source position (if possible):	ded to achieve maximum damage? Yes or No.         op? Yes or No.         or No. If yes, next test:
<ul> <li>Are any changes to If yes, then iden</li> <li>Did sufficient dama</li> <li>Should testing contiant</li> <li>Will the test specim</li> <li>Engineering: Describe any post-test diant</li> <li>Describe any change in same series</li> <li>Describe results of radio</li> <li>Completed by:</li> </ul>	ge occur to warrant additional dru nue with this test specimen? Yes en pass the thermal test based on <u>Regulatory:</u> isassembly and inspection:	ded to achieve maximum damage? Yes or No.   op? Yes or No.   or No. If yes, next test:   the accumulated damage assessment? Yes or No

1
# WORKSHEET 15.4 TEST INSPECTION DATA SHEET

-		st Test Performed:
Describe and measure (if appropriate)	any damage or broken pa	arts, etc.;
Describe and measure (if appropriate)	any signs of permanent s	train or deformation:
Describe the goodition of the simulate	d gourge wire appembly	
Describe the condition of the simulated	a source wire assembly.	
Deprese bla the sectors wine a second		close and the source position and the position
configuration is the same as they were	immediately after the las	aking sure that the source position and the package
Measure and record a radiation profile 1806.	of each test specimen in	accordance with QSA Global Work Instruction WI-Q-
Compare the pre-test dose levels with	post-test dose levels at th	e surface of the package and at 1 meter from the
surface of the package.		
Is a radiograph required to inspect for	hidden component damag	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found.	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found.	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found.	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found.	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found.	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found. Completed by:	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found. Completed by:	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found. Completed by:	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found. Completed by:	hidden component damaş	ge or failure? If radiography is performed, describe any
Is a radiograph required to inspect for damage or failures found. Completed by:	hidden component damaş	ge or failure? If radiography is performed, describe any





	1. Inspect the tools and the equipment too ensure they are in good working order, and fully functional.
	<ol> <li>With a calibrated working survey meter survey the 880 projector to ensure surface reading are below 200mr/hr</li> </ol>
	3. Perform a daily inspection on the 880 projector as required.
	<ol> <li>If the 880 projector has a source assembly, remove the source assembly to a safe storage location.</li> </ol>
	Note: performing this act can only be done by trained individuals wearing proper dosimetry
	Disassembly of standard 880 projector
	<ol> <li>Remove label by drilling out the four rivets that hold the label to the projector. (Note: rivets cannot be removed and must be carefully pushed into the housing to allow new rivets to be installed)</li> </ol>
	<ol> <li>Drill out the four-¼ inch SS rivets that hold the 880 projector to the jacket taking care not to enlarge the holes in the metal housing.</li> </ol>
	3. Remove source tag if present.
	4. Slide the 880 projector out of the original standard jacket.
	5. Remove the rear end plate from the 880 projector.
	Assembling 880 projector into the PipeLiner
	<ol> <li>Match up the correct color of PipeLiner Jacket, part# PL1000H, for Delta, Sigma, Elite or Omega.</li> </ol>
	2. With the PipeLiner Jacket, positioned on its wheels, invert the 880 projector 180° and slide the 880 projector into the PipeLiner jacket so the lock slide aligns with the lock slide access hole of the PipeLiner jacket. The 880 projector will be orientated so that the printing on the rear lock assembly will be upside down. Note: Be careful while handling projector, as it is not attached at this time. Tipping or moving the PipeLiner could cause the projector to slide out unintentionally.
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	unit	
	<ol> <li>Install shoe assembly part# PL1000S. This is accomplished with the jacket in the open position; both the whe pipe shoe feet will be flat on the work surface. Use the PL1003 to attach the lower portion of the shoe.</li> </ol>	ished by matching up the els of the Jacket and the pipe shoe pivot bolts Part#
	4. Install Collimating guide tube part # PL1017 by match male connector of the collimator with the female conne Insert the collimator and turn 90°. Turn outlet port cov and open outlet port. The collimating guide tube attach the same fashion as a standard bayonet fitting.	ing up the bayonet fitting ector of the outlet port. er 45° to lock in collimator hment is accomplished in
	5. Lift up pipe shoe to mate surface of shoe and jacket. If Once the bolt is secure, gently tilt entire assembly forw wheels are off the work surface and the Pipe shoe is fla (exposure position). The collimating guide tube will n surface of the shoe. Check alignment of lock slide hol not be perfectly aligned forward to back but should alig and at no point should the hole on the jacket cover any 880. Once the projector is in this position the projector ready for mounting.	nstall bolt part# PL1001. ward so that the PipeLiner at on the work surface ow be resting on the inside e. The lock slide hole may gned evenly top to bottom portion of the hole on the is properly aligned and
	6. With the 880 projector still in position and using an an PipeLiner jacket through the top mounting hole ½" dee and right angle drill. (Do not drill beyond ½" deep. Ta drill bit ½" from the tip to accomplish an accurate dep tamper proof screw into the top hole. (Turn screws by I doesn't strip out) Drill and screw the remaining 2 holes 880 projector.	gle drill, drill into the p using the 5/32 drill bit pe can be used to mark the th) Screw the $\#14 \times \frac{1}{4}$ hand slowly so urethane is securing the rear of the
No pro jac	nte: If a small enough drill isn't available the hole could be r ojector is in position and the holes drilled after the 880 proje .ket.	narked while the 880 ctor is removed from the
	<ol> <li>Tilt the PipeLiner back onto its wheels. Open the shoe bolt, hinge shoe forward and remove the collimating gu removing the 2 PL1003 hinge bolts.</li> </ol>	by removing the PL1001 tide tube. Remove shoe by
	8. Remove the front end plate.	
	9. Repeat step #6 on the front end of the projector.	
	8. Install QSA KIT018, Detent retrofit kit, per instruction	s included with the kit $0.210^{\circ}$
Rev	#: <u>3</u>	/* () <sup>2</sup> mice: June 15, 2009
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- DI 106	$P_{acc} = 40 \text{ of } 42$	December 2000

		······································
	<ol> <li>Replace the front and rear end plates of the 880 projector acc manufacture specifications.</li> </ol>	cording to
	11. Insert a dummy source into the device	
	12. Attach the PipeLiner collimating guide tube	
	<ol> <li>Perform a function test and cycle the dummy source several projector is functioning property.</li> </ol>	times ensuring the
	<ul> <li>14. Inspect label to ensure it is in good condition, replace if nece holes in label to match holes on projector. DO NOT DRILL THE 880 ASSEMBLY. Doing so may damage the shield and Regulatory requirements for the device. Tuck the label under PipeLiner jacket and rivet label to projector.</li> </ul>	essary. Drill new NEW HOLES IN d will violate r the edges of the
	15. The source may now be reinserted and the source tag attached designed to accommodate the source ID tag on the rear of the	ed. An area has been e projector.
		11 21 10 <sup>9</sup>
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Test

ATTACHMENT 16.2 DRAWING NO 88015 REV 0 MODEL , 880 150 CI BODY ASSEMBLY

# ATTACHMENT 16.3 IRSS PIPELINER OPERATIONS AND MAINTENANCE MANUAL, APR 4, 2007

To be attached as a separate document



# ACCESSORY FOR SENTINEL 880

DELTA SIGMA ELITE

OMEGA

**OPERATIONS AND MAINTENANCE MANUAL** 

#### 2



#### **DANGER - IMPORTANT WARNINGS**

The IRSS PipeLiner System must be operated only by trained and qualified radiographers who have read and understood this Operations Manual and the 880 Series Source Projector Operating and Maintenance Manual, or by trained assistants working under their direct supervision.

#### WARNING

# The use of radiographic exposure devices by unqualified personnel or when safety procedures are not fully met, could result in life threatening dangers.

Gamma radiography systems emit high levels of penetrating ionizing radiation during use and present a significant health risk to operators and the public including injury, sickness and/or death if appropriate safety and operational procedures are not employed.

Unshielded sources or source assemblies must never come in contact with any body parts under any circumstances.

Since gamma radiation is undetectable by the human senses, strict operating and emergency procedures must be followed. The proper use of PPE must be employed at all times during radiographic operations including calibrated survey meters, direct reading dosimeters, direct alarming dosimeters and the wearing of thermoluminecent dosimeters.

During use of this radiography system, never assume the position of the radiation source. Always conduct a thorough confirmatory survey using a calibrated survey meter to verify the location of the radiation source. Be reminded that a multitude of overexposure incidents which include injuries are directly attributed to a failure of the operator to perform or supervise an adequate confirmatory survey.

It is very important and required by regulation to prevent access by unauthorized persons to radiography equipment and to the area where radiography is performed.

Take advantage of the three basic radiation protection methods to minimize radiation exposure.

#### TIME

Spend less time near a source of radiation

#### DISTANCE

Increase your distance in a direction away from a radiation source

#### SHEILDING

Use effective shielding between you and the source of radiation

#### **DO NOT**

Perform any unauthorized modifications to the radiography exposure device or the components of this system

Use components that are not approved for use with this radiography system or after market components as this may compromise the safety designed into the system.

#### DO

Perform daily safety inspections of the radiography system for defects, wear and tear, replacing components as required. Inspections will be carried out or supervised only by trained and qualified radiographers



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- 2. DANGER—IMPORTANT WARNINGS
- 4. TECHNICAL SPECIFICATIONS
- 5. APPLICATION
- 7. DIAGRAM
- 8. RARTS LIST
- 9. WARRANTY AND LIMITATION OF LIABILITY
- *10. OPERATING INSTRUCTIONS*
- *12. OPERATION*
- 13. INSPECTION AND MANTENANCE

#### TECHNICAL SPECIFICATIONS

#### THE 880 SERIES PROJECTOR PIPELINER ACCESSORY

#### DESCRIPTION

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The PipeLiner is a rugged, easy to use attachment for the Sentinel 880 series of gamma ray radiography projectors to improve utilization and reduce dose rates to operators when performing pipeline radiography, while still maintaining the option of conventional set ups. The addition of the PipeLiner accessory essentially converts the 880 series of projectors into a dual purpose exposure device.

The PipeLiner accessory consists of four main components; the jacket, collimating guide tube, pipe shoe and swing arm assembly

#### **PIPELINER JACKET**

The PipeLiner jacket is made of polyurethane for strength, durability and weight reduction The jacket is similar to the stock 880 jacket in design and serves the same functions with a few exceptions. Wheels have been added to the jacket for easy transportation from weld to weld along pipelines. Accommodations have be made for the attachment of the "pipe shoe" and " swing arm assembly" to the front of the jacket.

A significant change, mounts the projector 180° or upside down in contrast to it's current or original jacket orientation. This new position gives a better angle to the control assembly for added durability and the collimating guide tube for ease of operation.

The PipeLiner jacket is attached to the 880 device in the same manner as the original jacket, with four stainless steel rivets.

#### PIPELINER COLLIMATING GUIDE TUBE

The collimator, guide tube and bayonet fitting are made of tungsten and manufactured as one component producing a unique design that maintains continuous shielding of the source while it is being projected to the beam port.

The beam port of the guide tube has been carefully designed to minimize the size of exclusion areas, reduce dose to operators, virtually eliminate flash dose, while still maintaining proper beam orientation. The collimating guide tube fits securely inside the "Pipe Shoe" when in use.

#### PIPE SHOE

The pipe shoe is made from similar polyurethane as the jacket and is designed to sit on the pipe during exposures. It consists of a molded bottom for positioning the exposure device along the center line of the pipe. This portion also includes the focal opening, a transverse groove that is used to align the beam port of the collimating guide tube into the position that best suits the intended geometry of the radiograph.

The top section consists of a raised area and a large indent. The raised portion will not allow the shoe to be closed unless the 880 outlet port cover is either fully closed or in the fully open position with the collimating guide tube attached. The indented area accommodates the collimating guide tube keeping it secure and protected.

The jacket accommodates the pipe shoe at the front by hinging it to the bottom portion of the jacket using two 2 3/4"x 2" socket head shoulder bolts. This hinging action is important as it allows the PipeLiner to be quickly prepared for the use of conventional guide tubes. The connection of the pipe shoe is completed by fastening the top portion of the jacket through the handle with the 3/8" x 12" socket head shoulder bolt.

#### CLAMP ASSEMBLY

The clamp assembly consists of three main sections, the right side plate including swing arm, the left side plate, and the hook plate that includes strapping, quick release latch and cam buckles.

The swing arm and right side plate is attached to the right side of the pipe shoe and the left side plate is attached to the left side using four 3/4"x 2" socket head shoulder bolts with the two rear bolts also acting to hinge the pipe shoe to the PipeLiner Jacket.

An important safety feature has been built into the Clamp assembly that will not allow the hook plate to be removed from the hook plate pin without depressing the cam buckles, releasing the strapping. This feature will not allow the PipeLiner to prematurely disengage from the pipe and fall to the ground. If the swing arm has not been engaged and the PipeLiner is accidentally allowed to fall uncontrolled it will only swing to the bottom of the pipe where it will hang until it is righted or removed.

#### APPLICATION

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The PipeLiner Accessory has been designed for the industrial applications of gamma radiography of pipeline butt welds using double wall contact and single wall viewing technique. By hinging open or removing the pipe shoe standard guide tubes can be attached to the 880 projector and conventional radiography performed. (SEE 880 OPERATION and MAINTENANCE MANUAL)

#### **880 PROJECTOR**

The PipeLiner is designed specifically for the 880 series of projectors. It is necessary that the operator has been trained and qualified in the operations of the 880 projector. Only those individuals who have received a certificate of competence for the maintenance of 880 devices should perform the jacket replacement. See your nearest Sentinel service center.

#### SOURCE ASSEMBLIES

The PipeLiner accommodates 1/4" diameter source capsules using TCI 5222 Teleflex cable style source assemblies **only**.

The following source assemblies meet the above requirements:

ISOTOPE	ASSEMBLY MODEL NO.	GAMMA ENERGY RANGE	HALF LIFE	APPROXIMATE STEEL WORK- ING THICK- NESSES
Selenium 75	A424-25W	66-612 keV	120 days	3-29mm
Iridium 192	A424-9	206-612 keV	74 days	12-63mm
Cobalt 60	A424-19	1.17-1.33 MeV	5.27 years	50-150mm

#### Activities

Authorized isotope activities are dependent on the 880 model, user license, and regulatory restrictions.

#### **OPERATING DISTANCE/POSITION**

All lengths of control assemblies can be used with the PipeLiner accessory. A 5.5 meter (18 feet) PipeLiner control assembly is available that incorporates a short .3 meter (1 foot) return. This control assembly should only be used in conjunction with the PipeLiner accessory.

It is recommended that the operator, under normal conditions, position himself to the rear of the projector and no closer than 5 meters during an exposure.

The shielding characteristics of the collimating guide tube are such that it favors the operator standing directly behind the projector. Directly forward of the projector offers the least protection while the sides as you proceed from front to back will continue to produce a reduction in dose rate until directly behind the projector.

#### ACCESSORY SPECIFICATIONS

#### Manufacturer

Industrial Radiography Supplies and Services Inc. 14705 116 Ave Edmonton, Alberta Canada T5M 3E8

Primary Application Industrial Pipeline Gamma Radiography 6



#### ACCESSORY FOR:

880 MODEL	ASSEMBLED WEIGHT	LENGTH	WIDTH	HEIGHT	SOURCE ASSEMBLIES
DELTA	65LBS	15"	7.5"	10"	A424-25W, A424-9,A424-19
SIGMA	65LBS	15"	7.5"	10"	A424-25W, A424-9,A424-19
ELITE	55LBS	15"	7.5"	10"	A424-25W,

#### MATERIALS

Polyurethane jacket and pipe shoe, aluminum and stainless steel

#### **INSPECTION REQUIRMENTS**

Daily pre-operational inspection for obvious damage to the system

#### MAINTENANCE REQUIRMENTS

Clean and dry after each days use

#### **OPERATING TEMPATURE RANGE**

-40°C to 149°C

#### NOTICE

\*The 880 PipeLiner accessory jacket has been registered as part of the Type B(U)-85 shipping container for AEA Technology QSA Inc. source assemblies and thus can remain on the projector during shipment. However all other parts of the PipeLiner accessory must be removed in their entirety before transport.

The purpose of this manual is to provide information which will assist qualified radiographers in using the PipeLiner accessory with the 880 series of projectors. The user must be thoroughly familiar with the 880 instruction manual and this instruction manual before attempting operation and use of this equipment. Prior to use of PipeLiner Jacket in conjunction with the 880 projector as a shipping container a registered user

certificate specifying the combination must be obtained from the CNSC.

It is the responsibility of the user's of this equipment to comply with local, national and international regulatory, licensing and transport rules and regulations as they apply in their respective countries.

\* to be approved



DIAGRAM



PARTS LIST

PART NUMBER	QTY	DESCRIPTION
PL101	1	3/8" x 12" SOCKET HEAD CAP BOLT
PL102	4	5/16" x 1 3/4" SOCKET HEAD CAP BOLT
PL103	4	3/4"x 2" SOCKET HEAD CAP BOLT
PL104	2	3/8" x 3/4" SOCKET HEAD CAP BOLTS
PL105	2	1/2" X 1 1/4" SOCKET HEAD CAP BOLTS
PL106	2	1/2" X 1 1/4" SOCKET HEAD CAP BOLTS
PL107	1	SWING ARM HANDLE
PL108	1	SWING ARM HANDLE NUT
PL109	1	BUNGEE CATCH
PL1010	4	WHEELS
PL1011	1	RIGHT SIDE PLATE
PL1012	1	LEFT SIDE PLATE
PL1013	1	PIPELINER JACKET
PL1014	1	HOOK PLATE PIN
PL1015	1	HOOK PLATE
PL1016	1	SWING ARM
PL1017	1	COLLIMATING GUIDE TUBE
PL1018	2	STRAPS
PL1019	1	PIPE SHOE

#### WARRANTY AND LIMITATION OF LIABILITY

Industrial Radiography Supplies and Services Inc. (IRSS, herein referred to as the manufacturer) warrants its product which it manufactures and sells to be free from defects in material and workmanship for a period of one year from the date of shipment. This warranty shall not apply to any products or parts which have been subjected to misuse, improper installation, repair, alteration, neglect, accident, abnormal conditions of operation, or use in any manner contrary to instruction or intended application.

The manufacturers liability under such warranty shall be limited to replacing or repairing at it's option, any parts found to be defective in such respects, which are returned to the manufacturer, transportation prepaid; or at it's option, to returning the purchase price thereof.

The warranty on other manufacturer's components shall be that of the original manufacturer whose warranty shall be binding.

In no event shall the manufacturer be liable for any incidental or consequential damages whether or not such damages are alleged to have resulted from the use of such product in accordance with instructions given by or referred to by the manufacturer.

IRSS assumes no liability or responsibility for the usage of any radioactive material or device generating penetrating radiation used in connection with this product.

All other warranties, except those warranties expressly stated herein, including without limitation warranties of, merchantability and implied warranties of fitness, are expressly excluded.

The warranty on this accessory is specifically limited to its use with the Sentinel 880 series of gamma ray projectors and sealed source assemblies as described on page 4 of this manual.

IRSS shall not be liable for any errors or omissions contained herein and the provision by IRSS of the information set out in this manual does not in it's self constitute acceptance of any liability on the part of IRSS.



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#### **OPERATING INSTRUCTIONS**

#### NOTE

This manual assumes that the reader has a thorough understanding of the operation and maintenance of the Sentinel 880 projector. Only personnel trained and qualified in the operation and maintenance of 880 projectors should attempt to use the PipeLiner accessory and only personnel with formal maintenance training should attempt to install an 880 projector into the PipeLiner Jacket.

#### **880 PROJECTOR CONVERSION**

#### **Tools required**

Only specially trained personnel should attempt this procedure. SEE SENTINEL 880 SERIES SOURCE PROJECTOR OPERATING AND MAINTENANCE MAN-UAL OR YOUR LOCAL DISTRIUTOR

#### **Parts Required**

IRSS PipeLiner Jacket PipeLiner Label 4 - 1/4" Stainless Steel Rivets \*Retrofitted 880 Projector

\*NOTE: 880 Projectors to be converted for use with the PipeLiner Accessory must have been retrofitted by a trained technician before conversion can be performed. See your Sentinel dealer for information on the necessary retrofits needed for your specific 880 projector.

#### Conversion

In order to use the PipeLiner accessory with the 880 projector the projector must be removed from it's original jacket and reinstalled into the PipeLiner jacket. **This can only be performed with an empty projector**. Remove the rear end plate, labels and four stainless steel rivets holding the projector to the jacket. (See Sentinel 880 Series Source Projector Operating and Maintenance Manual)

Once the projector has been removed from its original jacket it is rotated 180° and inserted into the PipeLiner jacket, making sure that the plunger lock access holes in the jacket and projector line up correctly, and then riveted into place. The rear end plate and new labels can now be re-installed and the source assembly transferred back to the device. This completes the jacket installation.

At this point the 880 projector can be operated using conventional guide tubes and controls, the only difference in operation being the upside down positioning of the device to its original orientation. Operators will soon become accustomed to this new position that provides improved support of control assemblies.

#### PIPELINER ASSEMBLY

#### **Tools Required**

3/8" T Handle Allen Key (Supplied)

#### **Parts Required**

Converted 880 Projector Pipe Shoe Right Side Plate with Swing Arm Left Side Plate Tungsten Collimating Guide Tube Hook Plate Polyurethane Straps 4 - 3/4" x 2" Socket Head Cap Bolts 1 - 3/8"x 12" Socket Head Cap Bolt

#### **Pipe Shoe Attachment**



Place the Pipe Shoe foot side down, hinge joint in front of the projector with the 880 projector on it's wheels. Approaching from the right side, plunger lock opening to your left, slide the pipe shoe back toward the projector inserting the pipe shoe hinge joint between the PipeLiner jacket hinge joints.

Align the over right side plate bolt hole, swing arm handle pointing up, with the jacket hinge joint bolt hole and insert the 3/4" x 2" socket head cap bolt and tighten loosely. Align the over right side plate bolt hole with the bolt hole in the front of the pipe shoe and insert a 3/4" x 2" socket head cap bolt through the hole and hand tighten using the T handle Allen key wrench.

Approaching the projector from the opposite side attach the left side plate in the same manner as the over right side plate using the two remaining 3/4" x 2" socket head cap bolts. With the front bolts securely fastened the rear bolts can now be securely hand tightened using the T handle Allen key wrench. The pipe shoe is now effectively hinged to the PipeLiner jacket.

#### **Attaching The Collimating Guide Tube**

The collimating guide tube has been manufactured with a bayonet connector, all as one piece. The swivel bayonet connector used with conventional guide tubes is not used with the PipeLiner accessory. Connect the collimating guide tube in the same manner a you would a conventional guide tube remembering that the 880 projector is now upside down or 180° to its original position. (See step 2 "Connecting the Source guide tube(s)" pg.2.3, in the Sentinel 880 Series Source Projector Operating and Maintenance Manual) Once the collimating guide tube is attached and the outlet port cover fully rotated clockwise until it stops, the pipe shoe can be lifted up, closing it over the collimating guide tube sealing from view, the front of the device. The 3/8" x 12" socket head cap bolt is then inserted through the carrying handle of the jacket and tightened securely using the T handle Allen key wrench.

#### **Attaching The Clamping Plate**

Select a strap length that best suits the diameter of pipe being radiographed. The proper length should leave a minimum of 6" of strapping material or tag end, projecting out of the cam buckles.

Placing the hook plate, hook side down, thread about 8" to 12" of the urethane strapping, unlooped end under the cam buckle. Reversing the direction, thread the strapping back and through the cam buckle jaw. Perform the same steps for the other cam buckle. The straps are now secured to the hook plate.

There are four horizontal posts attached to the over right side plate and swing arm. Two fixed "fulcrum" posts below and two posts that pivot as part of the swing arm. Attach the looped end of the strapping to the swing arm posts by sliding the loops over the ends. The hook plate should be positioned so that the hook points away from you and the straps should not be twisted or crossed but remain parallel.

Next lift the hook plate to create slack in the strap and force it between the gap made between the fixed fulcrum post and the over right side plate attachment bolt, positioning the strap behind the fixed fulcrum post. Repeat for the other strap.

This completes the assembly of the Sentinel 880 PipeLiner accessory.

#### Disassembly

If the operator wishes to use conventional guide tubes only the  $3/8" \ge 12"$  socket head cap bolt needs to be removed to allow the pipe shoe to hinge open. Enough space is provided to attach conventional guide tubes. If the operator wishes to remove the pipe shoe entirely, in addition to the  $3/8" \ge 12"$  socket head cap bolt, the two  $3/4" \ge 2"$  hinge bolts are all that need to be removed. This procedure will leave the swing arm assembly attached to the pipe shoe for quick reattachment later.

#### NOTE

The 880 series of projectors are not approved for transport of sealed sources while the pipe shoe remains attached to the Jacket.

#### **OPERATION**

#### Set up

Place the PipeLiner accessory, wheels first, pipe shoe forward, on the pipeline and roll it to within a few inches of the weld to be radiographed. Number belts or other identification markers can be attached to the pipe adjacent to the weld at this time. The projector is then tilted forward off it's wheels so that it is resting on the feet of the pipe shoe. The feet of the pipe shoe are designed to accommodate piping as small as 2" diameter and will automatically align the beam port along the center line of the pipe.

Position the focal opening, the apex of the transverse groove in the bottom of the pipe shoe, directly above the weld. This position can be arranged to the front or rear of the weld depending on the intended resultant radiograph.

Working from the right side of the PipeLiner with the swing arm handle in the "open" or down position, keep one hand on the PipeLiner and either reach over or under the pipeline, grasp the hook plate then hooking it onto the left side plate hook pin.

While still holding the device in place with one hand, grasp the tag ends of the straps with the your free hand and pull in a downward direction until the straps are tight. If the straps have been tightened properly it should be impossible to remove the hook plate from the hook pin without loosening the straps. In some cases, and especially with small diameter pipe, 3" and under, it is useful to give the straps one or two quick tugs to ensure the straps are sufficiently tight. Now lift the swing arm handle to lock the device securely to the pipe. It should now require a force much greater than the weight of the device to move the projector around the radius of the pipe. The larger the diameter of the pipe the greater the force required to move it, or the less tension required to hold the device in place.

The remote control assembly can now be connected to the projector and the exposure performed. (See Sentinel 880 Series Source Projector Operating and Maintenance Manual Step 3 pg.2.5).

#### 360° Rotation Around the Pipe

In order to position the PipeLiner to produce radiographs of the entire weld, it needs to be rotated into various positions around the circumference of the pipe. To accomplish this, first grasp the PipeLiner near the plunger lock opening with your left hand, curling your fingers over and around the end of the jacket. Next grasp the swing arm handle and lower it slightly to release just enough tension so that the projector can be pushed or pulled and rotated into the position required. The swing arm handle can, in this fashion, be used as a break providing the operator a high degree of control. Once you have attained the desired position, the swing arm handle is lifted locking the projector into position. This maneuver requires very little effort and can be accomplished with considerable accuracy with only a little practice.

#### Positioning of Film or Flexible Imaging Plates

Provisions for the attachment of bungee cord or similar material to the hook plate and a catch to fasten the bungee cord to, has been added to the swing arm handle so that film cassettes or imaging plates can be held firmly in place.

#### Moving to the Next Welded Joint

Once the required number of radiographs have been produced and it is time to move to the next welded joint, the PipeLiner is rotated back to the upright position on top of the pipe. If the remote control assembly is wound around the pipe it should unwound at this time and the pistol grip hung over the pipe close to and in front of the PipeLiner.

With your left hand holding firmly onto the PipeLiner, remove the hook plate from the hook pin by depressing the quick release mechanism with your right hand and allow it to fall under the pipe. Tilt the PipeLiner back onto it's wheels. Retrieve number belts and/or other identification markers and again with your right hand, reach under the pipe and retrieve the clamping plate. Position the clamping plate comfortably in your left hand while still maintaining a grip on the PipeLiner handle. This may seem awkward at first but becomes quite routine very quickly.

Pick up the pistol grip with your right hand and begin rolling the PipeLiner along the pipe to the next welded joint. The set up procedure is now repeated.

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#### **INSPECTION AND MAINTENANCE**

#### NOTE

Maintenance instructions in this manual for the PipeLiner accessory apply only to the parts listed in this manual. For maintenance instruction for the 880 projector, remote control assemblies or other Sentinel products not listed herein please refer to the Sentinel 880 Series Source Projector Operation and Maintenance Manual or the original product Operations Manual.

#### **Daily Inspection of the Radiography System**

A daily inspection of the gamma radiography system for obvious defects is essential.

The daily inspection ensures that the equipment is in a safe and proper operating condition. It is important that all radiographers perform or supervise this inspection prior to the first radiographic exposure of the shift regardless of any previous inspections that may have been performed that day. As an example, damage to a component of the system may occur during transport of the equipment to the job site. If damaged equipment were used without detection, the result may be the inability to retract the source assembly into the exposure device and secure it.

The result of a daily inspection should be recorded and include the date, name of the inspector and what specific equipment was inspected. If any defective or damaged components are discovered during daily inspection, the component must be removed from service and identified with a status indicator (tag, label, tape) to prevent inadvertent use by other radiography personnel.. Defective or damaged components must be repaired or replaced before reuse in radiography operations. The main components of the radiography system consisting of the radiographic exposure device, remote controls, source guide tubes must be inspected in addition to accessories such as lab stands, collimators, jigs, j-tubes, and pipe clamping apparatus.

Radiographers must take a proactive roll in preventing incidents, by performing or directly supervising a simple but thorough daily inspection of the radiography system. The implications that effect safety and the importance of the daily inspection must be emphasized and understood by the entire radiography staff.

#### **Daily Inspection of the PipeLiner Accessory**

**1.** Before starting any inspection, survey the surface of the exposure device to ensure that the radiation level is less than 2mSv/hr (200mR/hr). This survey provides a function test of the survey instrument, that it is responding to radiation, in addition to providing the radiographer with a reference measurement that can be compared to confirmatory surveys after terminating each radiographic exposure.

**2.** Inspect the labels on the exposure device to ensure they are legible and securely attached. The warning label containing the trefoil should be legible from a distance of 1 meter (approximately 3 feet). Inspect the legibility and attachment of the source identification tag that describes the radioactive source contained within the exposure device.

**3.** Check the PipeLiner jacket for cracks and gouges that could pinch or cut hands and fingers or wear damage that could affect the safe operation of the exposure device. Replace or repair as necessary.

It is common for the polyurethane material of the jacket to darken in color over time especially if the jacket is in direct sunlight for long periods. This is natural and will not affect the function of the jacket or the device. Inspect the wheels for smooth rotation, and the tires for wear, gouges or chunks missing. Replace as needed.

**4.** Inspect the collimating guide tube for obvious damage. Ensure the guide tube is free of dirt or debris. Check the bayonet fitting for burrs, cracks or dents. If damaged is found to the bayonet fitting the collimating guide tube should be replaced. Ensure the bayonet fitting engages and rotates smoothly into place in the outlet port by installing and removing it. A crunchy or gritty feeling indicates that dirt and/or sand has entered the outlet port mechanism and it must be serviced before use.

**5.** Inspect the pipe shoe for rough or sharp edges these should be filed smooth to prevent injury. Inspect the feet for excessive wear. The feet of the pipe shoe receives the most wear from contact with the pipe and will eventually wear to a point that the shoe will need to be replaced. Check the apex of the focal opening and of the concave between the feet for cracks. Ensure the indent that houses the collimating guide tube is free of dirt or debris and is sound with no wear through areas, allowing dirt into the collimating guide tube.

**6.** Inspect the entire swing arm assembly, right and left side plates, for obvious damage or wear and nicks or sharp edges that could cause injury. These can be filed smooth. The over swing arm should operate smoothly, the fulcrum and swing arm posts should be free of bends or burrs.

Check the straps for wear, cuts or abrasions. Check the loops, paying special attention to the inside of the loop where it rubs against the posts. If the straps show obvious fatigue or wear they need to be replaced. Inspect the operation of the cam buckles, they should open and close smoothly, firmly grasping the strapping. Check the hook plate and hook plate pin for damage and deformities.

7. During the initial set up of the days work and with the PipeLiner on the pipeline, the following exercise needs to be performed to ensure all components of the PipeLiner accessory are functioning together as intended.

Engage the hook plate onto the hook plate pin, tighten the straps and check to ensure the hook plate cannot be removed from the hook plate pin without releasing the quick release cam buckles first.

Next rotate the entire device 120° away from you and engage the swing arm. Put slight hand pressure on the PipeLiner with the intent of trying to force it further towards the bottom of the pipe. Now rotate the device from the top of the pipeline 120° in a direction towards you and engage the over centering mechanism. Again put slight hand pressure on the PipeLiner with the intent of trying to force it further towards the bottom of the pipe. Return the device to the top of the pipeline. If the device failed to hold sufficiently at any time, retighten the straps and repeat the above tests until the projector is held securly.



#### MAINTENANCE

Daily (routine) and annual (complete) maintenance requirements

Radiographic exposure devices and associated equipment must be maintained regularly by trained and qualified personnel to ensure consistent and safe operation of the radiographic system. The routine inspection and maintenance also ensures the integrity of the Type B(U)-85 transport packages are maintained in compliance with the package certification number USA/9296/B(U)-85.

Manufacturers base the recommended inspection and maintenance requirements on the system's design, application, materials, anticipated work cycles, environmental factors of use under the normal and abnormal conditions of industrial radiography and while in the transport system. A program of systematic maintenance will prolong the working life of the radiographic exposure device and associated equipment in addition to ensuring safety during use. By most national regulations, routine maintenance of the systems is required at intervals not to exceed 3 months in addition to the radiographer's daily inspections for obvious defects. The complete annual servicing ensures the integrity of the system.

Maintenance program administrators must recognize the need for maintenance intervals that are less than the required 3 month interval especially in cases where the systems are used in severe environmental conditions. Maintenance program administrators must ensure the systems are completely serviced immediately after certain jobs in severe conditions. Extreme or severe conditions may include, but is not limited to:

- Conditions where the equipment was immersed in water or mud.
- Subjected to high-concentrations of particulate such as fly ash or sand.
- Subjected to hot radiography conditions.
- Subjected to salt-water conditions, caustic or acidic materials.
- Subjected to accidental drops or falling objects.
- Whenever subjected to extreme environmental conditions.

The routine maintenance of the PipeLiner accessory performed daily requires cleaning, inspection and operational checks of the system. The complete maintenance (performed once a year) involves a complete disassembly, cleaning, inspection and operational tests of the entire system.

Equipment maintenance can be performed by trained and qualified individuals within the licensee's organization. AEA Technology QSA service engineers are available to provide maintenance on the systems at the licensee's premises or at on of he service centers.

#### Routine Daily Maintenance Requirements

At the end of each days use the PipeLiner accessory needs to be cleaned of any obvious debris, mud, dirt, or other foreign material. Use a soft wire brush or stiff bristle brush to remove dried mud and to reach tight spaces. Mild detergent and water can be used to remove dirt and grime with a damp rag. Spilled chemicals or other chemical compounds should be removed immediately using proper methods approved for the chemical involved.

NOTE: Safety glasses should be worn when using brushes to remove dirt and mud.

#### Yearly Maintenance Requirements

Once a year the entire system should be dismantled and thoroughly cleaned and inspected. (see inspection portion of this manual)

The PipeLiner uses no lubricants or does it require regular replacement of parts. Simple cleaning and a thorough inspection of all parts including bolts is all that is necessary.

#### Records

The results of the inspections, repairs and maintenance should be recorded and retained. Reports should contain the name of the person(s) involved, dates, location and should identify the specific equipment that was serviced.

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April 4, 2007

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F-Q-1806-4, rev, 2

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Page 1 of 1

Section 8.6
Equipment Certification
Records

Drop Pad - T10740

Constant	2				•:	q		10111			Sheet 1 of 1	
Inspection Instruct	tion	Originator/Date	Tom Shea	14 Aug.09		Rev. B	Part No. T	10740	Reg. Appro	/al/Date C	<u>kenthen</u>	200740
And Record	0 0 0 0 0 0	QA Approval/Da	to: []]]	Seausy	3) Avg 07	CM. NA	PIL NA	Eng. Appro	val/Date	32 14	106 09	
Item Description	8 X 8 DR	OP PAD-BU	RLINGI	<u>'ON //</u>						<del></del>		
Characteristics	Tolerance	MTE	AQL	1	REF			5			8	
General Visual	NA	Visual.	C/100%	01	15 0568							
Cracks in Concrete	NA	Note & Photograph	C/100%	01	with							
1/2-13 threaded hole, four (4) places	Gø/NaGa	Thread Gage	C/100%	10	01							
Pilch of Slab 1/2, N-S Corners	+/-1/4	Level & Scale	C/1C0%	0-1	NA							
Surface Condition of Ste- Plate	NA	Note & Photograph	C/100%	0/1	NA							
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60 days only I		Lot Qty.						*				<u> </u>
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Test Report 1 - TP186

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tem Description	Puncture	Test Billot	hane	(Jeg)	2 Sept 51	CM NA	PIL NA	Eng. Approv	alluate <u>Fi</u>	Vmm		2.607 01
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Puncture Billet – T10143

ESSCO CALIBRE DIVISION OF WALSH CALIBRATION CALIBRATIO	SATION LABORATORY ENGINEERING SERVICES, INC. OF ELECTRONIC / MECHANICAL TEST EQUIPMENT CHELMSFORD, MA 01824-4102 178) 250-0880 www.esscolab.com ISSUE DATE: 2/22/2010
CERTIFICATE	OF CALIBRATION
CUSTOMER / LOCATION OSA GLOBAL INC 40 NORTH AVENUE BURLINGTON MA 01803 DEPT:	EQUIPMENT INFORMATION MANUFACTURER: OMEGA MODEL NO: CL23A SERIAL NO: T-198776 CONTROL NO: ENG-20
PURCHASE ORDER: P32150	TYPE: CALIBRATOR
IN TOLERANCE	IN TOLERANCE
PERFORMED: IN LAB. TEMPERATURE (deg C): 23 RELATIVE HUMIDITY (%RH): 21 METHOD: OMEGA CL23A/24/25/25	CALIBRATION DATE: 2/22/2010 CALIBRATION DUE: 2/22/2011 METROLOGIST: 9-4 D. Judma
E1540 KAYE-K140-4 ICE-POINT REFERENCE E2483 FLUKE 8508A REFERENCE MULTIMETER E706: FLUKE 5700AN03 CALIBRATOR	178302 5/15/2009 5/14/2010 257701 5/27/2009 4/27/2010 276832 1/7/2010 4/7/2010
,	
The ESSCO Quality Syst or results above relate only to the item(s) califyrated. Unless otherwise dated, a minimum TUR of 4 is califias that the unit conformed to applicable appelications yone orcessful completion of the ca VIST or a National Measurement Institute. This certificate shall not be restoduced; particular of the appearance to the right signifies responsibility for the quality system. a calibration was performed in complement with the ESSCO Quality Manual, ECL 1, Rev. 26, 29 Se patient can be performed in complement with the ESSCO Quality Manual, ECL 1, Rev. 26, 29 Se patient can be performed in complement with the ESSCO Quality Manual, ECL 1, Rev. 26, 29 Se patient can be preferred in the calify a system.	em is certified to ISO 9001:2008 I was used: thout written approval of ESSCO. plember 2009, and compiles with [21, and the calibration [21, and the calibration

	ıcate #: 296477		BARCODE:	1030907	·.		Page 2 of 2
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2.00			32.5				
শ্	1 MTR IN K 0.000 mV	32.0	31.5	DEGF	31.9	31.9	37-0.5 DEG:E
2	2 MTR IN K 54 856 mV	2500.0	2502.0 2498.0	DEG F	2500.4	2500.4	+7-2.0 DEG F
3	3 MTR IN J 0.000 mV	32.0	32.5 31.5	DEG F.	31.7	31.7	+ 0.5 DEG F
4	4 MTR IN T 0.000 mV	32,0	32.5 31.5	DEG F	31.7	31.7	+/- 0.5 DEG F
÷5	5 CAL OUT K 32.0 F	0.000	0.011	'nν	0.008	0.008	+/- 0.011 mV
6	6 CAL OUT K 2500.0F	54.856	54.894 54.818	mV	54.867	54,867	+/- 0.038 mV
7	7 CAL QUT J 320 F	0.000	0.014 -0.014	mV	0.012	0.012	+/- 0.014 mV
8	8 CAL OUT T:32.0 F	0.000	0.011	mV	0:007	0.007	+/-0.011 mV
	End of Data						

Note: A = Adjusted F = Failed L = Limited

Test Report 1 - TP186

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**O'Haus Digital Scale – 0009986-6CE** 

# Hunt Metrology Service, Inc.

121 Ferry Street Lawrence, MA 01841 (978) 688-7278 (978) 794-4632 <u>Hmsi@verizon:net</u>

<u>Calibration Certificate</u> HMSCC-22922-12-P Total Pages: 15 Tech: Paul Rabs

### QSA Global 40 North Avenue Burlington, MA 01803

#### Purchase Order No: P31363-00 Date Cal: September 24, 2009 Due: September 24, 2010

The calibration performed on the following measuring and test equipment (M&TE) of this document is traceable to the National Institute of Standards and Technology (N.I.S.T.) through N.I.S.T. number 821/276493-08; Certificate number 09-69006A dated May 29, 2009 for dimensional calibration,

The M&TE have been cleaned and lubricated, as needed. Our technician(s) have calibrated, adjusted and/or reset the M&TE, affixed a calibration label to the M&TE, updated the corresponding record(s), and provided this calibration certificate. The standard(s) utilized to perform the calibration have been calibrated, certified and maintained in our laboratory which sustains a temperature of 68 degrees (+/-2ø) and less than 50% relative humidity. All records pertaining to our standards, and the masters utilized to calibrate them, are kept on file in our laboratory for a period of no less than 3 years. The services provided, traceability to the N.I.S.T., and Hunt Metrology Service's calibration system comply with the requirements of ANSI/NCSL Z540-1-1994, ISO 10012-1:1002 (E) and ISO/IEC 17025. The reported value is both "as found" and "as left" data, unless otherwise specified. A calibration uncertainty ratio of at least 4:1 is maintained unless otherwise stated. This calibration certificate cannot, in any way, be reproduced, except in full, without prior written consent from a representative of Hunt Metrology

Service, Inc.

David Dickinson, President

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2009 09:328 FR0M	HUNT METROLÓGY	19787944632	TO:17812705038	( <b>P</b> :( <b>2</b> )
	Hunt Metrolo	gy Service, Inc.	Data Sheet	:
		HMSCC-22922-12-P		ġ.
Customer: QSA Gi ID No: 411 2. ID No: Department: Deviation u: Accuracy: Temperature: 73.78 Humidity: 528 Gage Type: 0-1301b D	DEAL Manufr Sea Stand St	Cturer: 0'HAUS tal No: 0009986-60 del No: 018 lard No: 018 lard No: 057 hard No: 057 hard No: 0.00 0	P.O. No.: Date Cal: Date Due: Cel Technician Cal: 03/31/09 Due: Cal: 03/31/09 Due: Cal: Due Cal: Due Cal: Due Cal: Due Cal: 00 Cal: 00	P31363-00 09/24/09 09/24/10 PR 01 03/31/10 03/31/10
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Test Report 1 - TP186

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Safety Analysis Report for the Model 880 Series Transport Package

QSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 2-44 1

# 2.12.12 USDOT Special Form Certificate USA/0392/S-96 Rev 11



Pipeline and Hazardous Materials Safety Administration East Building, PHH-23 1200 New Jersey Avenue Southeast IAEA CERTIFICATE OF COMPETENT AUTHORITY Washington, D.C. 20590 SPECIAL FORM RADIOACTIVE MATERIALS CERTIFICATE USA/0392/S-96, REVISION 11

This certifies that the source described has been demonstrated to meet the regulatory requirements for special form radioactive material as prescribed in the regulations of the International Atomic Energy Agency<sup>1</sup> and the United States of America<sup>2</sup> for the transport of radioactive material.

- 1. <u>Source Identification</u> QSA Global, Inc. Model 875 Capsule.
- 2. <u>Source Description</u> Cylindrical single encapsulation made of Type 304 or 304L stainless steel and tungsten inert gas or laser welded. Approximate exterior dimensions are 5.2 mm (0.205 in.) in diameter and 7.84 mm (0.309 in.) in length. Inside dimensions vary, but minimum wall thickness is 0.482 mm (0.019 in.). Construction shall be in accordance with attached QSA Global, Inc. Drawing No. R875 INNER, Rev. C.
- 3. <u>Radioactive Contents</u> No more than either 8.9 TBq (240.0 Ci) of Cobalt-60 or 14.8 TBq (400.0 Ci) of Iridium-192 in the form of metallic wafers or pellets.
- 4. <u>Quality Assurance</u> Records of Quality Assurance activities required by Paragraph 310 of the IAEA regulations<sup>1</sup> shall be maintained and made available to the authorized officials for at least three years after the last shipment authorized by this certificate. Consignors in the United States exporting shipments under this certificate shall satisfy the applicable requirements of Subpart H of 10 CFR 71.
- 5. Expiration Date This certificate expires on January 31, 2018.

<sup>1</sup> "Regulations for the Safe Transport of Radioactive Material, 1996 Edition (Revised), No. TS-R-1 (ST-1, Revised)," published by the International Atomic Energy Agency(IAEA), Vienna, Austria.

<sup>2</sup> Title 49, Code of Federal Regulations, Parts 100-199, United States of America.
#### CERTIFICATE USA/0392/S-96, REVISION 11

This certificate is issued in accordance with paragraph 804 of the IAEA Regulations and Section 173.476 of Title 49 of the Code of Federal Regulations, in response to the January 07, 2013 petition by QSA Global, Inc., Burlington, MA, and in consideration of other information on file in this Office.

Certified By:

and and a start at the

Dr. Magdy El-Sibaie

Jan 24 2013 (DATE)

Associate Administrator for Hazardous Materials Safety

Revision 11 - Issued to extend the expiration date.



Safety Analysis Report for the Model 880 Series Transport Package

QSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 2-45

2.12.13 USDOT Special Form Certificate USA/0335/S-96 Rev 10



IAEA CERTIFICATE OF COMPETENT AUTHORITY 1200 New Jersey Avenue SE SPECIAL FORM RADIOACTIVE MATERIALS CERTIFICATE NUMBER USA/0335/S-96, REVISION 10

East Building, PHH-23 Washington, D.C. 20590

#### **Pipeline and Hazardous Materials** Safety Administration

This certifies that the sources described have been demonstrated to meet the regulatory requirements for special form radioactive material as prescribed in the regulations of the International Atomic Energy Agency<sup>1</sup> and United States of America<sup>2</sup> for the transport of radioactive material.

- 1. Source Identification - QSA Global, Inc. Model 875 Series.
- Source Description Cylindrical single or double encapsulations with the outer capsule made of Type 304L stainless steel and 2. tungsten inert gas or laser welded. Approximate outer dimensions are 6.35 mm (0.25 in.) in diameter and either 19.05 mm (0.75 in.) or 24.2 mm (0.954 in.) in length. Inner capsules, when present, are made of stainless steel or titanium. Construction of the outer capsule shall be in accordance with attached QSA Global, Inc. Drawing No. R875 OUTER, Rev. C. Construction of any inner capsule shall be in accordance with attached QSA Global, Inc. Drawing No. R875 INNER, Rev. C or QSA Global, Inc. Drawing No. R87527-40, Rev. Α.
- з. Radioactive Contents - No more than either 14.8 TBq (400 Ci) of <u>Radioactive contents</u> - No more than either 14.8 Eq (400 Cl) of Iridium-192 as a solid metal; 8.14 TBq (220 Ci) of Cobalt-60 as a solid metal; 5.56 TBq (150 Ci) of Selenium-75 as an encapsulated solid metal; 1.11 TBq (30 Ci) of Cesium-137 as encapsulated CsCl<sub>2</sub>; 1.85 TBq (50 Ci) of Thulium-170 as  $Tm_2O_3$ ; or 7.4 TBq (200 Ci) of Ytterbium-169 as Yb<sub>2</sub>O<sub>3</sub>.
- $\frac{Quality\ Assurance}{by\ Paragraph\ 310}\ of\ the\ IAEA\ regulations^1\ shall\ be\ maintained\ and$ 4. made available to the authorized officials for at least three years after the last shipment authorized by this certificate. Consignors in the United States exporting shipments under this certificate shall satisfy the applicable requirements of Subpart H of 10 CFR 71.
- 5, Expiration Date - This certificate expires June 30, 2017.

This certificate is issued in accordance with paragraph 804 of the IAEA Regulations and Section 173.476 of Title 49 of the Code of Federal Regulations, in response to the June 01, 2012 petition by QSA Global, Inc., Burlington, MA, and in consideration of other information on file in this Office.

Certified by WWWWWWWWW

JUN 2 6 2012

(DATE)

Dr. Magdy El-Sybaie Associate Administrator for Hazardous Materials Safety

Revision 10 - Issued to extend the expiration date.

<sup>1</sup> "Regulations for the Safe Transport of Radioactive Material, 1996 Edition (Revised), No. TS-R-1 (ST-1, Revised)," published by the International Atomic Energy Agency (IAEA), Vienna, Austria.

<sup>2</sup> Title 49, Code of Federal Regulations, Parts 100 - 199, United States of America.







Safety Analysis Report for the Model 880 Series Transport Package

QSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 2-46

2.12.14 USDOT Special Form Certificate USA/0502/S-96 Rev 8



of Transportation

Pipeline and Hazardous Materials Safety Administration 1200 New Jersey Avenue Southeast IAEA CERTIFICATE OF COMPETENT AUTHORITY Washington, D.C. 20590 SPECIAL FORM RADIOACTIVE MATERIALS CERTIFICATE USA/0502/S-96, REVISION 8

East Building, PHH-23

This certifies that the sources described have been demonstrated to meet the regulatory requirements for special form radioactive material as prescribed in the regulations of the International Atomic Energy Agency<sup>1</sup> and the United States of America<sup>2</sup> for the transport of radioactive material.

- <u>Source Identification</u> QSA Global, Inc. Model Nos. X54 (Manufactured before January 1, 1998), X540 (Manufactured on or after February 17, 1981), and X540/1 (Manufactured on or after September 27, 2000).
- 2. <u>Source Description</u> Tungsten inert gas or laser seal welded cylindrical single or double encapsulations. The outer encapsulation is made of titanium or stainless steel and the inner encapsulation, if used, is made of titanium, stainless steel, or aluminum. Approximate exterior dimensions are 5.15 mm (0.2 in.) maximum diameter and 15.15 mm (0.6 in.) in length (Model X54); and 5.16 mm (0.2 in.) in diameter and 7.65 mm (0.3 in.) in length (Models X540 and X540/1). Construction shall be in accordance with attached Amersham Drawing No. A10639, Issue C (Model X54) or QSA Global Inc. Drawing No. R87527, Rev. G (Models X540 and X540/1).
- 3. <u>Radioactive Contents</u> No more than 17.0 TBq (459.5 Ci) of Cobalt-60 (Model X54); or no more than either 20.0 TBq (540.5 Ci) of Cobalt-60, 17.0 TBq (459.5 Ci) of Iridium-192, or 5.56 TBq (150.3 Ci) of Selenium-75 (Models X540 and X540/1). The Co-60, Ir-192, and Se-75 are in the form of a metal.
- 4. <u>Quality Assurance</u> Records of Quality Assurance activities required by Paragraph 310 of the IAEA regulations<sup>1</sup> shall be maintained and made available to the authorized officials for at least three years after the last shipment authorized by this certificate. Consignors in the United States exporting shipments under this certificate shall satisfy the applicable requirements of Subpart H of 10 CFR 71.
- 5. <u>Expiration Date</u> This certificate expires on July 31, 2017.

<sup>1</sup> "Regulations for the Safe Transport of Radioactive Material, 1996 Edition (Revised), No. TS-R-1 (ST-1, Revised)," published by the International Atomic Energy Agency(IAEA), Vienna, Austria.

<sup>2</sup> Title 49, Code of Federal Regulations, Parts 100-199, United States of America.

#### CERTIFICATE USA/0502/S-96, REVISION 8

This certificate is issued in accordance with paragraph 804 of the IAEA Regulations and Section 173.476 of Title 49 of the Code of Federal Regulations, in response to the July 06, 2012 petition by QSA Global, Inc., Burlington, MA, and in consideration of other information on file in this Office.

Certified By:

Dr. Magdy El-Sibaie

Jul 10 2012

(DATE)

Associate Administrator for Hazardous Materials Safety

Revision 8 - Issued to extend the expiration date.

NO. A106	39			ltem	Description	Material	Drawing	No.	No.off
				1	BODY	STAIN.STL.	A10636	ITEM.1	1
				2	PLUG	STAIN_STL	A10638		1
			<b>\$</b>	3	ACTIVE MATERIAL				
	Secu	ritv-Relat	ed I	'nf	forma	ation Fi	gur	e	
	With	held Und	ler 1	10	CFR	2.390.	0	C	
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Safety Analysis Report for the Model 880 Series Transport Package

QSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 2-47 ł

2.12.15 Test Plan 206 (Sep 2013)



Document Number

Revision

0

**F-E-1808-1 Test Plan Cover Sheet** 

# **TEST PLAN 206**

# **MODEL 880SC TRANSPORT PACKAGE TYPE B TRANSPORT PACKAGE**

Originator	f-	Date:	9 Egyt 13	
	A	PPROVALS		
Engineering	5.6-	Date:	35KP17	
Regulatory	ab. in	Date:	2 Sep 13	
Quality Assurance	In calla	Date:	3 Sep 13	

F-E-1808-1 Rev 0

Originator

Page 1 of 1

# **TEST PLAN 206**

# MODEL 880SC SOURCE CHANGER TYPE (B) TRANSPORT PACKAGE TESTS

As of

September, 2013

SENTINEL	1	Fest Plan 206
QSA Global		August 2013
Burlington, Massachusetts		Page 2 of 45

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## Test Plan No. 206

### Section 1 Introduction

This document describes the mechanical test plan for the Model 880SC Source Changer to meet NRC requirements for Type B(U)-96 packages as described in the Code of Federal Regulations, 10 CFR Part 71, revised as of January 26, 2004. The test plan also covers the criteria stated in the IAEA TS-R-1 (1996 Edition – as Amended 2003)

This document describes the test package specifications, testing equipment, testing scenario, justifies the package orientations for the different test specimens and provides test worksheets to record key steps in the testing sequence.

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#### Section 2 Transport Package Description

Figure 2.1 describes the Model 880SC Source Changer transport package. Figure 2.2 shows the transport package schematic. Figure 2.3 shows the transport package with the plastic jacket. Fig 2.4 shows the transport package overall dimensions without the Jacket.

The radioactive material is sealed in a special form source capsule. The source capsule, stop ball and connector are swaged to a flexible steel wire to form the source wire assembly. Two source wire assemblies can be loaded into the 880SC Source Changer, one in the front and one in the rear. The source wire assemblies are held securely to the device by components of the Source Lock Assembly. There are two Source Lock Assemblies, on each end of the container assembly. The lock assembly sleeve, prevents the stop ball of the source wire from being pushed through the package. Another component, the lock slide, prevents the stop ball from being pulled out of the package when in the secured position. A keyed lock prevents the lock slide from being actuated.

The Top Lock Plate is fastened to the Bottom Lock Plate with four, 1/4-20 stainless steel machine screws. The Bottom Lock Plate is attached to rivnuts assembled on the endplate weldment with four 5/16-18 stainless steel security screws. The endplate weldment consists of the endplate disc, a U-shaped bracket and the four rivnuts. The U-brackets are welded to the endplate disc and the endplate disc is welded to the cylindrical shell.

The shield is fastened within the device at each end by a titanium shield pin. The pin passes through the shield and the U-bracket. The shield is centered in the shell and has the source tube cast into its center. The source tube provides a cavity for the source wire assemblies to travel through during use. The source capsules are positioned in the center of the ball of the shield within the source tube cavity when the source wire is in its secured position.

The model 880SC uses polyurethane foam to fill the cavity around the depleted uranium shield. The foam prevents contamination to and from the depleted uranium shield.

Previous thermal tests have shown charred polyurethane foam will inhibit the flow of oxygen to the shield and prevent oxidation from occurring during a fire as long as the foam remains confined. This is shown on QSA Global Test plan number Report 74.

It has also been shown the charred foam will not support the shield at temperatures of 800°C. The model 880SC relies on the shield pins to hold the shield in place at all times. These pins are designed to retain the shield throughout testing without the added support of the foam.

The plastic jacket is an optional part of the Type B transport package and has been demonstrated to be less damaging during transport testing on the 880D packages (ref. TP Report 108) therefore the 880SC will be tested without the jacket as the worst case condition for the type B transport testing. The absence of the jacket will present a worst case 30-foot drop and puncture test condition. In a drop, the plastic jacket protects the transport package from further damage by absorbing energy upon impact.

The weight of the Model 880SC transport package without the jacket is not greater than 46 pounds. The total weight of the package with the jacket is not greater than 52 pounds.



SOURCE LOCK ASSEMBLY DETAIL (2X)

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#### FIGURE 2.1: MODEL 880SC SOURCE CHANGER TRANSPORT PACKAGE



FIGURE 2.2: MODEL 880SC SOURCE CHANGER SCHEMATIC

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Figure 2.4: MODEL 880SC SOURCE CHANGER OVERALL DIMENSIONS

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#### Section 3 Regulatory Compliance

The main purpose of this test plan is to demonstrate that the Model 880SC transport package complies with the Type A and Type B(U)-96 transport package test requirements of 10 CFR 71 and IAEA TS-R-1.

All test specimens are first subjected to the required normal conditions of transport tests 10 CFR Part 71.71 followed by the hypothetical accident condition tests of 10 CFR Part 71.73.

#### 3.1 Normal Conditions of Transport (NCT) Tests

The *water spray test* per 10 CFR 71.71 (c) (6) and IAEA TS-R-1 Section VII, paragraph 721 of the package <u>will not be performed</u> as the Model 880SC transport package is constructed of waterproof materials throughout. Water spray will not degrade the structural integrity of the Model 880SC transport package.

The *compression or stacking test* per 10 CFR 71.71 (c) (9) and IAEA TS-R-1 Section VII, paragraph 723 <u>will not be performed</u>. This test was conducted as part of the Model 880 Transport Package Evaluation (see Test Plan Report No. 100).

The Model 880SC transport package shall be subjected to the *penetration test* of 10 CFR 71.71 (c) (10) and IAEA TS-R-1 Section VII, paragraph 724 and then the *1.2 meter free drop test* per 10 CFR 71.71 (c) (7) and IAEA TS-R-1 Section VII, paragraph 722

The Model 880SC transport package shall be tested as stated above to demonstrate its ability to withstand normal conditions of transport as identified in 10 CFR 71.71 and IAEA TS-R-1. Successfully passing the NCT tests means there is no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

IAEA TS-R-1 Section VI, paragraph 646 stipulates the same criteria except that it also requires that the loss of shielding integrity should not result in more than a 20% increase in the radiation level at any external surface of the package.

#### 3.2 Hypothetical Accident Condition (HAC) Tests

The *crush test* 10 CFR 71.73 (c) (2) and IAEA TS-R-1 Section VII, paragraph 727 (c) <u>will</u> not be performed because the Model 880SC transport package is not designed to transport radioactive contents greater than 1000  $A_2$  not as special form radioactive material.

The Model 880SC transport package shall be subjected to the *9-meter free drop test* per 10 CFR 71.73 (c) (1) and IAEA TS-R-1 Section VII, paragraph 727 (a), and then the *puncture test* per 10 CFR 71.73 (c) (3) and IAEA TS-R-1 Section VII, paragraph 727 (b).

The *thermal test* per 10 CFR 71.73 (c) (4) and IAEA TS-R-1 Section VII, paragraph 728 <u>will</u> not be performed it will be assessed.

The *immersion test – fissile material test* per 10 CFR 71.73 (c) (6) and IAEA TS-R-1 Section VII, paragraph 733. <u>will not be performed</u>. The Model 880SC transport package does not transport fissile material.

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The *immersion test – all packages test* per10 CFR 71.73 (c) (6) and IAEA TS-R-1 Section VII, paragraph 729 <u>will not be performed</u>. Only the source capsule (containment vessel) is sealed and able to pressurize as a result of 50 feet of water depth. The source capsules intended for transport in these containers are designed and tested to withstand a minimum external pressure of 290-lbf/in<sup>2</sup> (minimum ANSI HPS N43.6-1997 pressure classification of 3). This will ensure that the containment can meet the 22-lbf/in<sup>2</sup> limit specified in the regulations.

The materials used in the construction of the Model 880SC transport package are impervious to water and are not structurally affected when immersed in water of at least 15 meters (50 feet).

The Model 880SC transport package shall be subjected to the cumulative effects of the tests as stated above to demonstrate its ability to withstand the hypothetical accident conditions of transport as identified in 10 CFR 71.73 and IAEA TS-R-1. A successful pass shall indicate; there is no escape of radioactive materials greater than  $A_2$  in one week and no external dose rate greater than 1 R/hr at 1m from the external surface with the maximum radioactive contents which the package is designed to carry.

Material	Melting Point
Stainless steel	1390°C (2530°F)
Depleted uranium	1135°C (2075°F)
Titanium	1700°C (3100°F)
Tungsten	3410°C (6170°F)
Copper/Brass	1080°C (1980°F)
Aluminum	580°C (1080°F)
Rubber/Plastic	Less than 540°C (1000°F)

The melting points for the materials of the package are listed below:

#### Section 4 Discussion on System Failure Modes of Interest

#### 4.1 General

The tests in this plan focus on damaging those components of the package which could cause displacement of the source(s) from its stored position within the depleted uranium shield and which affect the integrity of the shield itself.

#### 4.2 Normal and Accident Conditions of Transport

The modes of failure under normal and accident conditions that could lead to elevated dose rates include the following:

- **4.2.1** Fracture or penetration of the Source Changer weldment.
- **4.2.2** Displacement of the shield within the Source Changer weldment and distortion or fracture of the source.
- **4.2.3** Failure of the source lock assemblies and/or lock mounting screws.
- **4.2.4** Fracture or cracking in the depleted uranium shield.

The test conditions specified in this Test Plan are intended to challenge the ability of the Model 880SC transport package with respect to these failure modes.

#### Section 5 Assessment of Package Conformance

#### 5.1 Regulatory Requirements

#### 5.1.1 Normal Conditions of Transport (71.43(f))

There should be no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

IAEA TS-R-1 para. 646 stipulates the same criteria except that it states in paragraph 646(b) that the loss of shielding integrity would not result in more than a 20% increase in the radiation level at any external surface of the package.

#### 5.1.2 Hypothetical Accident Conditions (71.51(a))

There should be no escape of radioactive materials greater than  $A_2$  in one week and no external dose rate greater than 1 R/hr at 1m from the external surface with the maximum radioactive contents which the package is designed to carry.

#### 5.2 Test Package Contents

The Model 880SC Source Changer is designed to carry either one or two special form sources. Containment of the radioactive source is tested at manufacture. The source capsule design has been certified in accordance with the performance requirements for special form as specified in 10 CFR Part 71 and IAEA TS-R-1.

This test plan therefore does <u>not</u> discuss/specify tests of the containment of the radioactive source. The purpose of the tests is to demonstrate that the sources remain shielded within the limits specified by the regulations.

Since source integrity has been demonstrated through special form testing, simulated sources will be used during testing of the package. The radiation levels after testing will be measured by replacing the simulated sources with active sources. The post-test measurements will be compared with pre-test measurements to verify the sources have not shifted within the shield.

#### 5.3 Test Orientation Assessment

The following is an assessment of all the possible test orientations for the Model 880SC transport package. Only the test orientations deemed necessary for causing failure relative to the failure modes described in section 5.1 will be used in the Penetration, 1.2 meter, 9 meter, and Puncture tests of this plan.

The Model 880SC transport package is a cylindrically shaped container. On each end of the container is an identical lock assembly. The assemblies are

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parallel to one another but at a 15 degree angle. The center of gravity is located essentially at the geometric center of the package.

The objective in every test is to cause significant damage to the extent that it would directly compromise the radiological safety of the package or adversely influence the results of subsequent tests in the test sequence. Dropping or penetrating the package just to cause damage without affecting the radiological safety consequences is not necessary.

Figure 8.5.2.1 is the first Penetration Test orientation. The penetration bar will impact the lock in its most vulnerable location potentially causing failure of the lock. The penetration bar may also produce a large enough force which could shear the lock assembly attachment screws.

Figure 8.5.3.1 is the second Penetration Test orientation. The penetration bar will impact the lock slide. This impact could shear the lock slide or cause significant damage.

Figure 8.6.2.1 is the first 1.2m Drop orientation (end drop). This orientation is based on the center of gravity of the 880SC and should cause the 880SC to impact on the cap of the lock assembly. The impact from this drop could shear the lock assembly attachment screws on the first lock assembly. This impact will also damage the cap which may shear off and allow for damage to the other components of the lock assembly. The cap may also collapse during impact and provide some level of dampening since it is constructed of relatively thin stainless steel. The collapse or damage of the cap during this test will reduce any dampening from the cap during the 9m Drop test.

Figure 8.6.3.1 is the second 1.2m Drop orientation (end drop). This orientation is based on the center of gravity of the 880SC for the opposing  $(2^{nd})$  lock assembly and should cause the 880SC to impact on the cap of the lock assembly. The impact from this drop could shear the lock assembly attachment screws on the  $2^{nd}$  lock assembly. This impact will also damage the cap which may shear off and allow for damage to the other components of the lock assembly. The cap may also collapse during impact and provide some level of dampening since it is constructed of relatively thin stainless steel. The collapse or damage of the cap during this test will reduce any dampening from the cap during the 9m Drop test.

Figure 8.6.4.1 is the third 1.2m Drop orientation (oblique drop). The object of this drop is to try and shear off the lock assembly attachment screws. This orientation is a worst case. The center of mass for the lock assembly on the right (as shown in Figure 8.6.4.1) is at a further point from the initial corner of impact on the 880SC than for the lock assembly on the left, and will therefore create a larger moment of inertia.

Neither the side drop nor the corner drop will be performed for the 1.2m Drop. Orientation 8.6.2.1 and 8.6.3.1 will create the larger shear force on the attachment screws, at the same time damaging the lock assembly.

Figure 8.7.2.1 is the first 9m Drop orientation (end drop). The object is to continue to inflict damage from the 1.2m Drop orientation (Figure 8.6.2.1). The cap may have been damaged or collapsed during the 1.2m drop and this will increase the possibility of the lock assembly attachment screws shearing

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off. The 9m drop may cause damage to the other components of the lock assembly.

Figure 8.7.3.1 is the second 9m Drop orientation (end drop). The object is to continue to inflict damage on the opposing lock assembly as shown in the 1.2m Drop orientation (Figure 8.6.2.1). The cap may have been damaged or collapsed during the 1.2m drop and this will increase the possibility of the lock assembly attachment screws shearing off. The 9m drop may cause damage to the other components of the lock assembly.

Figure 8.7.4.1 is the third 9m Drop orientation (oblique drop). The object of this drop is to try and shear off the lock assembly attachment screws. This orientation is a worst case. The center of mass for the lock assembly on the right (as shown in Figure 8.7.4.1) is at a further point from the initial corner of impact on the 880SC than for the lock assembly on the left, and will therefore create a larger moment of inertia.

Neither the side drop nor the corner drop will be performed for the 9m Drop. Orientation 8.7.2.1 and 8.7.3.1 will create the larger shear force on the attachment screws, at the same time damaging the lock assembly.

**8.8.2.1** is the first Puncture test orientation (end drop). The justification for this drop orientation is the same as for the 1.2m and 9m Drops. This test will continue to inflict damage on the lock assembly.

8.8.3.1 is the second Puncture test orientation (end drop). The justification for this drop orientation is the same as for the 1.2m and 9m Drops. This test will continue to inflict damage on the lock assembly.

**8.8.4.1** is the third Puncture test orientation (oblique). Hitting on the corner of the billet is a worst case.

Neither the side drop nor the corner drop will be performed for the 9m Drop. Orientation 8.8.2.1 and 8.8.3.1 will create the larger shear force on the attachment screws, at the same time damaging the lock assembly.

#### 5.4 Vibration Conditions

Vibration normally occurring in transport is not expected to adversely affect the structural aspects of the Model 880SC transport package. The lock assembly attachment screws and thread locking adhesive are identical to the 880D Transport package. The weight of the 880SC lock assembly is similar to the weight of the 880D Rear plate assembly.

#### Section 6 Construction and Condition of Test Specimens

The Model 880SC transport package test specimens will be constructed in accordance with QSA Global drawing 880SC-TP206 revision 2 and the QSA Global Quality Assurance Program. The weight of the test specimens per this drawing is not greater than 46 pounds.

The structural materials of the Model 880SC are made of AISI Type 300 series stainless steel and titanium. The shielding materials are depleted uranium and tungsten. The non-safety related parts are made from aluminium, brass, copper, plastic, and rubber.

With the exception of the Penetration Test all tests of this plan will subject the test specimen to an impact from a drop. The mechanical strength and ductility of the critical components of the package must continue to perform as expected at the ambient temperature conditions of  $-40^{\circ}$ F to  $100^{\circ}$ F.

The fracture toughness, strength and ductility, of the structural materials in the Model 880SC do not change significantly at or between the temperatures of  $-40^{\circ}$ F to 100°F. The shielding materials are relatively brittle throughout this entire temperature range. Therefore, any temperature within the  $-40^{\circ}$ F to 100°F range for the 4-foot, 30-foot, and puncture tests will have the same result. So, the test specimen will be dropped at ambient temperature at time of testing.

The internal operating pressure of the containment system, namely the source capsule, is considered to be in equilibrium with the outside pressure of the package. The sealed capsules are welded at atmospheric pressure and except for the capsules, the package is open to the atmosphere. Therefore, the initial internal pressure of the containment system is considered to be insignificant.

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### Section 7 Material and Equipment List

The equipment list worksheets in Section 9 identify the equipment required, with additional space to list other necessary equipment and measuring instruments needed to perform the tests. Additional materials and equipment used to facilitate the tests will be listed as needed.

#### Section 8 Test Procedure

#### 8.1 General

All test specimens are to be tested in the sequence presented below. Each test has been designed to check the integrity of various components of the package. An assessment of transport integrity of the package can be made based on the cumulative effect of the tests performed on the package.

A plastic jacket (as shown in figure 2.3) is used to carry the package and is normally present during shipping. There are instances where the jacket may not be present but the 880SC Transport package will be shipped. For this reason the jacket <u>will not</u> be used during testing since it may provide some level of impact absorption during the 1.2m Drop, 9m Drop and Puncture tests and would not provide a worst case for testing. All testing will be conducted <u>without</u> the jacket but the drop heights will be adjusted to compensate for the maximum potential weight of 52lbs vs. the actual weight of the test specimens. Drop height compensation calculations are to be included on each Drop & Puncture Test Data Sheet.

The tests have the following sequence:

- 1. Test specimen preparation and inspection (including initial profile).
- 2. Penetration test (10 CFR 71.71(c)(10)) NCT Test
- 3. 1.2m (Four-foot) free drop test (10 CFR 71.71(c)(7)) NCT Test
- 4. 9m (30-foot) free drop test (10 CFR 71.73(c)(1)) HAC Test
- 5. Puncture test (10 CFR 71.73(c)(3)) HAC Test
- 6. Test inspection.
- 7. Final test inspection and/or assessment (including post test profile).
- 8. Test specimen storage.

#### Note:

After testing, the package results will be evaluated in the Test Plan Report for impact of the reverse sequence of the 9m Drop and Puncture Testing to determine compliance with IAEA TS-R-1 #727 & #728.

#### 8.2 Roles and Responsibilities

The responsibilities of the groups identified in this plan are:

- **Engineering** executes the tests according to the test plan and summarizes the test results. Engineering also provides technical input to assist Regulatory Affairs and Quality Assurance as needed.
- **Regulatory Affairs** monitors the tests and reviews test reports for compliance with regulatory requirements.
- **Quality Assurance** oversees test execution and test report generation to assure compliance with the QSA Global Quality Assurance Program.
- Engineering, Regulatory Affairs and Quality Assurance are jointly responsible for assessing test and specimen conditions relative to 10 CFR 71 and IAEA TS-R-1.
- **Quality Control** is responsible for ensuring test and specimen data is measured and recorded throughout the test cycle.

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#### 8.3 Test Specimen Preparation and Inspection

- 1. Manufacture five Model 880SC Source Changers per QSA Global drawing number 880SC-TP206, revision 1. Clearly and indelibly mark each specimen: "TP206(X)". Where X is an alphabetically incremented letter beginning with "A". One of the five Source Changers will be used as a spare and used to replace a specimen dropped onto the wrong impact point, if necessary. The spare, if used, will follow the same test sequence as the initially selected specimen.
- 2. Measure and record the weight of each specimen.
- 3. Inspect the test specimens to ensure that:
  - All fabrication and inspection records are documented in accordance with the QSA Global Quality Assurance Program.
  - The test specimens comply with the requirements of the drawing.
- 4. Measure and record the location of the source from the front plate using the source location tool.
- 5. Perform and record the radiation profile in accordance with QSA Global Work Instruction WI-Q-1806.
- 6. Engineering, Regulatory Affairs and Quality Assurance will jointly verify that the test specimens comply with the drawings and the QSA Global Quality Assurance Program.
- 7. Prepare the test specimens for transport.

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### 8.4 Summary of Test Schedule

This section provides an overall view of the test specimen orientations for each test.

Normal Conditions of Transportation (NCT) Tests:

Penetration

NCT	Para.	Specimen	Diagram
Penetration 1	71.71(c)(10)	TP206(A)	
Penetration 2	71.71(c)(10)	TP206(B)	

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1.2m Drop			
NCT	Para.	Specimen	Diagram
1.2m Drop 1.	71.71(c)(7)	TP206(A)	100 Metric International Internati
1.2m Drop 2.	71.71(c)(7)	TP206(B)	
1.2m Drop 3.	71.71(c)(7)	TP206(C)	LUPICON LUP

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## Hypothetical Accident Condition (HAC) Tests:

## 9m Drop

HAC	Para.	Specimen	Diagram
9m Drop 1.	71.73(c)(1)	TP206(A)	DEDWARD TOP VRV JECULON DEDWARD DECWARD JECULON DECWARD JECULON DECWARD JECULON JECULO
9m Drop 2.	71.73(c)(1)	TP206(B)	
9m Drop 3.	71.73(c)(1)	TP206(C)	
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## Puncture

HAC	Para.	Specimen	Diagram
Puncture 1.	71.71(c)(3)	TP206(A)	HIGHNORT DEV NOV HIGHNORT DEV NOV HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNORT HIGHNO
Puncture 2.	71.71(c)(3)	TP206(B)	HARTINE DECEMBENT DECEMBEN
Puncture 3.	71.71(c)(3)	TP206(C)	

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## 8.5 Penetration Test (10 CFR 71.71 (c) (10))

The penetration test is a normal condition of transport test. Impact of the hemispherical end of a vertical steel cylinder of 3.2 cm (1.25 in) diameter and 6 kg (13 lbs) mass, dropped from a height of 1 m (40 in) onto the exposed surface of the package that is expected to be most vulnerable to puncture. The long axis of the cylinder must be perpendicular to the package surface.

The impact of the steel cylinder may be sufficient to damage the Lock Source assembly. There are two specific areas that are vulnerable, the Lock and the Lock Slide.

#### 8.5.1 Penetration Test Set-up

- 1. Orient each specimen according to the specimen-specific orientation shown in Figure 8.5.2.1 or Figure 8.5.3.1
- 2. Raise the penetration bar
- 3. Measure and record the ambient temperature.
- 4. Photograph the set-up.
- 5. Drop the penetration bar.
- 6. Record the damage to the package and take a photographic record.

#### 8.5.2 Specimen TP206(A) Orientation for the Penetration Test

Figure 8.5.2.1 shows the package orientation for Specimen TP206(A). The object of the drop is to puncture or damage the Lock mechanism.



Figure 8.5.2.1: Specimen TP206(A) Orientation for the Penetration Test

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#### 8.5.3 Specimen TP206(B) Orientation for the Penetration Test

Figure 8.5.3.1 shows the package orientation for Specimen TP206(B). The object of the drop is to puncture or damage the Lock Slide.





#### 8.5.4 Penetration Test Assessment

Upon completion of the test, Engineering, Regulatory Affairs and Quality Assurance team members will jointly take the following actions:

- Review the test execution to ensure that the test was performed in accordance with 10 CFR 71, IAEA TS-R-1 1996, and this test plan.
- Make a preliminary evaluation of the specimens relative to the requirements of 10 CFR 71 and IAEA TS-R-1 1996.
- Assess the damage to each specimen to decide whether testing of that specimen is to continue.

#### 8.6 1.2m (4-foot) Free Drop Test (10 CFR 71.71(c)(7))

The Normal Transport Conditions Test is the 1.2m (4-foot) free drop test as described in 10 CFR 71.71(c)(7).

The figures of section 8.6.2.1, 8.6.3.1, and 8.6.4.1 illustrate the orientations for the test specimens.

a second of

## 8.6.1 1.2m Free Drop Test Set-up

To set up a package for the 1.2m (4-foot) drop test:

- 1. Place each specimen on the drop surface and position it according to the specimen-specific orientation shown in Figure 8.6.2.1, Figure 8.6.3.1, or Figure 8.6.4.1
- 2. Raise the package so that the impact target is 1.2m (4 feet) + Weight compensated distance, above the drop surface. Ensure the center of gravity is over the impact point
- 3. Measure and record the ambient temperature.
- 4. Photograph the set-up.
- 5. Start the video recorder.
- 6. Drop the package.
- 7. Stop the video recorder.
- 8. Record the damage to the package and take a photographic record.

## 8.6.2 Specimen TP206(A) Orientation for the 1.2m Drop Test

Figure 8.6.2.1 shows the package orientation for Specimen TP206(A). The object of the drop is to damage the Lock Cap and Lock and possibly shear the attachment screws.



Figure 8.6.2.1: Specimen TP206(A) Orientation for the 1.2m Drop Test

## 8.6.3 Specimen TP206(B) Orientation for the 1.2m Drop Test

Figure 8.6.3.1 shows the package orientation for Specimen TP206(B). Since the 880SC Transport package has a Lock assembly on each end, and the ends are at different angles the object of this drop is to damage this Lock Cap and Lock or shear the attachment screws.



Figure 8.6.3.1: Specimen TP206(B) Orientation for the 1.2m Drop Test

## 8.6.4 Specimen TP206(C) Orientation for the 1.2m Drop Test

Figure 8.6.4.1 shows the package orientation for Specimen TP206(C). The object of this drop is to try and shear off the attachment screws. This orientation is a worst case. The center of mass for the Lock Slide on the right (as shown in Figure 8.6.4.1) is at a further point from the initial corner of impact on the 880SC than for the Lock Slide on the left, and will therefore create a larger moment of inertia.



Figure 8.6.4.1: Specimen TP206(C) Orientation for the 1.2m Drop Test

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#### 8.6.5 1.2m Free Drop Test Assessment

Upon completion of each test, **Engineering**, **Regulatory** Affairs and **Quality** Assurance team members will jointly take the following actions:

- Review the test execution to ensure that each test was performed in accordance with 10 CFR 71, IAEA TS-R-1, and this test plan.
- Make a preliminary evaluation of the specimens relative to the requirements of 10 CFR 71 and IAEA TS-R-1.
- Measure and record a radiation profile of each test specimen in accordance with QSA Global Work Instructions WI-Q1806.
- Assess the damage to each specimen to decide whether testing of that specimen is to continue.
- Evaluate the condition of each specimen to determine what changes, if any, are necessary in package orientation in the 30-foot drop test to achieve maximum damage.

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## 8.7 9m Free Drop Test (10 CFR 71.73(c)(1))

The first Hypothetical Accident Test is the 9m (30-foot) free drop test as described in 10 CFR 71.73(c)(1).

The figures of section 8.7.2.1, 8.7.3.1, and 8.7.4.1 illustrate the orientations for the test specimen.

## 8.7.1 9m Free Drop Test Set-up

To set up a package for the 9m (30-foot) drop test:

- 1. Measure and record the weight of each of the test specimens.
- 2. Place each specimen on the drop surface and position it according to the specimen-specific orientation as shown in Figure 8.7.2.1, Figure 8.7.3.1, or Figure 8.7.4.1.
- 3. Raise the package so that the impact target is 9m (30 feet) + Weight Compensated distance, above the drop surface. Ensure the center of gravity is over the impact point.
- 4. Measure and record the ambient temperature.
- 5. Photograph the set-up.
- 6. Start the video recorder.
- 7. Drop the package.
- 8. Stop the video recorder.
- 9. Record the damage to the package and take a photographic record.

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## 8.7.2 Specimen TP206(A) Orientation for the 9m Drop Test

Figure 8.7.2.1 shows the package orientation for Specimen TP206(A). The object of the drop is to use lock cap to drive the rear plate across the endplate to shear the rear plate mounting screws.



Figure 8.7.2.1: Specimen TP206(A) Orientation for the 9m Drop Test

## 8.7.3 Specimen TP206(B) Orientation for the 9m Drop Test

Figure 8.7.3.1 shows the package orientation for Specimen TP206(B). The object of the drop is to use lock cap to drive the rear plate across the endplate to shear the rear plate mounting screws.



Figure 8.7.3.1: Specimen TP206(B) Orientation for the 9m Drop Test

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#### 8.7.4 Specimen TP206(C) Orientation for the 9m Drop Test

Figure 8.7.4.1 shows the package orientation for Specimen TP206(C). The object of this drop is to try and shear off the attachment screws. This orientation is a worst case. The center of mass for the Lock Slide on the right (as shown in Figure 8.7.4.1) is at a further point from the initial corner of impact on the 880SC than for the Lock Slide on the left, and will therefor create a larger moment of inertia.



Figure 8.7.4.1: Specimen TP206(C) Orientation for the 9m Drop Test

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## 8.7.5 9m Free Drop Test Assessment

Upon completion of each test, Engineering, Regulatory Affairs and Quality Assurance team members will jointly take the following actions:

- Review the test execution to ensure that each test was performed in accordance with 10 CFR 71, IAEA TS-R-1, and this test plan.
- Make a preliminary evaluation of the specimens relative to the requirements of 10 CFR 71 and IAEA TS-R-1.
- Assess the damage to each specimen to decide whether testing of that specimen is to continue.
- Evaluate the condition of each specimen to determine what changes, if any, are necessary in package orientation in the puncture test to achieve maximum damage.

## 8.8 Puncture Test (10 CFR 71.73(c)(3))

The package is dropped from a height of 1m (40") onto the puncture billet. This test uses the 12" high puncture billet. The billet meets the minimum height (8") required in 10 CFR 71.73(c)(3). The specimen has no projections or overhanging members longer than 12" which could act as impact absorbers, allowing the billet to cause the maximum damage to the specimen. The billet is to be bolted to the drop surface used in the drop tests.

The figures: 8.8.2.1, 8.8.3.1 and 8.8.4.1 illustrate the orientations for each puncture test.

The justification for each puncture orientation Drop 1 and Drop 2 is the same as the orientation for the 30-foot drop test (Drop 1 and Drop 2). If the orientation needs to be changed, the new orientation must be documented and approved with a justification describing how it would be a worst condition than the planned orientation.

#### 8.8.1 Puncture Test Set-up

**NOTE:** Because each test is designed to add to damage inflicted on a specific component or assembly in the preceding test, it is important that each specimen maintain its identity throughout the battery of tests and that the set-up instructions specific to the specimen are strictly followed.

To set up a package for the puncture test:

- 1. Measure and record the weight of the test specimen.
- 2. Measure and record the ambient temperature.
- 3. Position the test package according to the specimen-specific orientation shown in figures 8.8.2.1, 8.8.3.1, or 8.8.4.1.
- 4. Raise the package so that the impact target is 1m (40") + Weight Compensated distance, between the impact point on the package and the top of the puncture billet. Ensure the center of gravity is over the impact point.
- 5. Photograph the set-up.
- 6. Start the video recorder.
- 7. Drop the package.
- 8. Stop the video recorder.
- 9. Record the damage to the package and take a photographic record.

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## 8.8.2 Specimen TP206(A) Orientation for the Puncture Test

The objective of this drop orientation (Figure 8.8.2.1) is to continue the damage inflicted on the specimen by the 9m-drop test.



Figure 8.8.2.1: Specimen TP206(A) Orientation for the Puncture Test

## 8.8.3 Specimen TP206(B) Orientation for the Puncture Test

The objective of this drop orientation (Figure 8.8.3.1) is to continue the damage inflicted on the specimen by the 9m-drop test.



Figure 8.8.3.1: Specimen TP206(B) Orientation for the Puncture Test

#### 8.8.4 Specimen TP206(C) Orientation for the Puncture Test

The objective of this drop orientation (Figure 8.8.4.1) is to puncture the shell of the 880SC.



Figure 8.8.4.1: Specimen TP206(C) Orientation for the Puncture Test

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## 8.8.5 Puncture Test Assessment

Upon completion of the test, **Engineering**, **Regulatory** Affairs and **Quality** Assurance team members will jointly take the following actions:

- Review the test execution to ensure that the tests were performed in accordance with 10 CFR 71, IAEA TS-R-1, and this test plan.
- Make a preliminary evaluation of each specimen relative to the requirements of 10 CFR 71 and IAEA TS-R-1.

#### 8.9 Test Inspection

Perform the test inspection after the puncture tests.

- 1. Measure and record the damage to each of the test specimens. Measure and record the package for signs of any permanent strain.
- 2. Measure and record the location of the source from the front plate using the source location tool.
- 3. Remove and assess the condition of the simulated source.
- 4. Reassemble the packages using a representative active source, making sure that the source position and the package configuration are the same as they were immediately after the puncture test.
- 5. Measure and record a radiation profile of each test specimen in accordance with QSA Global Work Instruction WI-Q1806.
- 6. Assess the significance of any change in radiation at the surface and at one meter from the packages.
- 7. Determine whether it is necessary to radiograph the test specimens for inspection of hidden component damage or failure.
- 8. Record any damage or failure found in radiograph of the test specimens, if performed.

## 8.10 Thermal Test (10 CFR 71.73(c)(4))

The Thermal test will be assessed.

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## 8.11 Test Specimen Storage

Place the test specimens in an appropriate container and store the container in the "low level" waste room. Dispose the test specimens only when authorized in writing by RA and QA.

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## **Section 9 Worksheets**

Use the following worksheets for executing the tests of section 8. Each test shall have three worksheets; an equipment list, a procedure checklist, and a data sheet. Record the information onto copies of these worksheets for each test performed.

Attach a copy of the relevant inspection report or calibration certificate after the range and accuracy of the equipment has been verified.

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Test Specimen Documentation Test Specimen – 880SC-TP206				
		-		
	· · · · · · · · · · · · · · · · · · ·			
Signature	 	int Name		Date
Engineering:		<u></u>	<u> </u>	<u>n i n n i konst nago trago s</u>
Regulatory:				
Quality Assurance:				

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## Drop & Puncture Test Equipment List

Test:			
Description * Mark NA when not used.	Enter the Model and Serial Number	Attach Inspection Report or Calibration	
Test Specimen, Drawing No.	and a line of the state of the	A test Continents and the	
Drop Surface, Drawing No.			
* Puncture Billet, Drawing No.			
Record any additional tools used to facilitate the test and a calibration certificates.	ttach the appropriate ins	pection report or	
	· · · · · · · · · · · · · · · · · · ·		
	· · · · · · · · · · · · · · · · · · ·		
Signature	Rrint Name	Date	
Completed by:			
Verified by:			

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## Drop & Puncture Test Checklist

Test:				
Test Location:				
Step	Data	Measuring Instrument		
1. Record test specimen serial number:				
2. Record the test specimen weight:				
3. Record the ambient temperature (°C):				
4. Record set-up orientation figure:		· · · · · · · · · · · · · · · ·		
5. Verify set-up orientation and drop height.	۱ <u>ــــــــــــــــــــــــــــــــــــ</u>			
6. Photograph set-up in at least two perpendicular planes.				
7. Begin video recording of the test so that impact is recorde	ed.			
8. Release the test specimen.				
9. Stop the video recorder. Ensure the point of impact and o	rientation specified in the p	olan has been achieved.		
10. Record the damage to the test specimen on a separate she	et and attach.			
<ol> <li>Engineering, Regulatory Affairs and Quality Assurance make a preliminary assessment relative to 10 CFR 71. Record the assessment on a separate sheet and attach.</li> </ol>				
Test witnessed by (Signature) Print Name Date				
Engineering:				
Regulatory Affairs:				
Quality Assurance:				

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Test Unit Model/Serial No.:	Test:
Test Date:	Test Time:
Describe drop orientation and drop height:	
Describe impact (location, rotation, etc.):	
Describe on-site inspection (damage, broken parts, etc	c.):
On-site test assessment:	
Engineering: Regulatory: Describe any post-test disassem bly and inspection:	QA:
Describe any change in source position:	
Describe results of radiography:	
Completed by:	Date:

## Drop & Puncture Test Data Sheet

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2.12.16 Test Plan 206 Report #1 minus Appendices D & E (Nov 2013)

	A GLOBAL	Document Number F-E-1808-2	Revision O
<u>_</u>		Test Report Cover Sheet	
	TES	T REPORT #1	
	FOR 7	<b>TEST PLAN 206</b>	
	Mode	el 880SC Transport Package	
	Normal Condit	tions of Transport (NCT) Test Results	
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,		<b>Revision: 0</b>	
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# TEST PLAN 206 – REPORT #1 MODEL 880SC TRANSPORT PACKAGE

## NORMAL CONDITIONS OF TRANSPORT (NCT) TEST

REV 0

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## Test Plan No. 206

## Section 1 Introduction

This report documents the Normal Conditions of Transport (NCT) test results described on Test Plan 206 performed on the Model 880SC transport package. The results confirm the Model 880SC transport package in its heaviest configuration tested in the most vulnerable drop orientation passes all the NCT test requirements specified in Test Plan 206, the Code of Federal Regulations, 10 CFR Part 71, revised as of January 26, 2004 and criteria stated in the IAEA Regulations for the Safe Transport of Radioactive Material, No. TS-R-1 (1996 Edition – as Amended 2003).

The Model 880SC transport package is tested to demonstrate its ability to withstand normal conditions of transport as identified in 10 CFR 71.71 and IAEA TS-R-1. Successfully passing the NCT tests means there is no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

IAEA TS-R-1 Section VI, paragraph 646 stipulates the same criteria except that it also requires that the loss of shielding integrity shall not result in more than a 20% increase in the radiation level at any external surface of the package.

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## Section 2 Construction and Condition of Test Specimens

The test specimens are constructed in accordance with QSA Global engineering drawings and Quality Assurance Program. The drawings and manufacturing documents accurately depict the intended design at the time of testing along with methods for building and verifying the finished product. There were no deviations and/or changes to the test specimen before testing.

The test specimens (4) built for this test are the Model 880SC. Figures 2.1 and 2.2 shows test specimens, specimen numbers TP206(A) through TP206D. TP206D was assembled as a spare. This unit was not required for the NCT testing. Shipping labels and nameplates were not attached for testing.

Figures 2.1 and 2.2 shows the major assemblies and common components of the Model 880SC transport package. The nomenclature used in Figures 2.1 and 2.2 are referenced throughout this report.





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#### FIGURE 2.2: MODEL 880SC SOURCE CHANGER SCHEMATIC

The primary containment system of the package is the completely seal welded source capsule assembly. The capsule assembly, tested to the ANSI/ISO class 4 or 7MPa pressure test requirements, is manufactured at atmospheric pressure and ambient temperature and therefore does not need to be adjusted for the test.

The secondary containment system, the transport package source lock assemblies and shield assembly, are open to the atmosphere and therefore in constant equilibrium with changing operating pressures.

The structural materials used in the construction of the Model 880SC transport package retain their key mechanical and physical properties between  $-40^{\circ}$ C ( $-40^{\circ}$ F) and  $+38^{\circ}$ C ( $+100^{\circ}$ F). Therefore, the temperature of the test specimens did not need to be adjusted for the tests performed in test plan 206.

## Section 3 Regulatory Compliance

The Model 880SC transport package complies with the normal transport package test requirements of 10 CFR 71.71 and IAEA TS-R-1 based on the successful completion of the tests and analysis described in this report.

The pass criteria for a successful normal transport test or analysis is identified 10 CFR part 71.43 paragraph (f). This paragraph states:

"There should be no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

IAEA TS-R-1 paragraph 646 stipulates the same criteria except that it also requires that the loss of shielding integrity not result in more than a 20% increase in the radiation level at any external surface of the package."

#### Free Drop Height Adjustment

The free drop test heights specified in 10 CFR Part 71 are adjusted higher to allow for the Model 880SC transport packages built heavier than the test specimen but less than the maximum package weight. The actual test specimens weigh less than the maximum weight specified on the top level assembly drawing. This is primarily due to the absence of the optional jacket.

Table 3.1 shows the adjusted free drop height based on the actual test specimen weight compared to the maximum transport package weight. The adjusted heights provide impact energy equal to or greater than the maximum transport package weight if dropped at the 10 CFR Part 71 specified drop height. The adjusted drop height is determined by multiplying the worst case weight ratio by the required drop test height (4 feet). The worst case weight ratio is calculated by dividing the maximum allowable weight by the actual test specimen weight.

Table 3.1. Test Specimen 1.2 Meter Free Drop Height Adjustment					
Test	Actual Test Specimen Weight	Maximum Transport Package Weight	1.2 I Adj	Meter (4-f usted Hei	oot) ght
Specimen	(Lbs)	(Lbs)	(Meters)	(Feet)	(Inches)
TP206(A)	44.80	52	1.42	4.7	:56
TP206(B)	44.85	52	1.42	4.7	56
TP206(C)	44.80	52	1.42	4.7	56

## Section 4 Test Results

#### 4.1 Water Spray Test

Per Test Plan 206 the water spray test was not performed:

"The water spray test per 10 CFR 71.71 (c) (6) and IAEA TS-R-1 Section VII, paragraph 721 of the package <u>will not be performed</u> as the Model 880SC transport package is constructed of waterproof materials throughout. Water spray will not degrade the structural integrity of the Model 880SC transport package."

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#### 4.2 Compression Test

Per Test Plan 206 the compression test was not performed:

The compression or stacking test per 10 CFR 71.71 (c) (9) and IAEA TS-R-1 Section VII, paragraph 723 <u>will not be performed</u> because the maximum weight of the 880SC transport package without the jacket is 46 lbs. and was tested as part of the 880 Transport package:

"Test Plan and Report 100 (Section 2.12) documents that Test Specimens P01 and P02 were subjected simultaneously to a compressive load of 459 lbs (209 kg) for a period of 24 hours. This exceeds five times the maximum transport package weight of 46 lbs for the heaviest version of the Model 880 (without the optional jacket). The actual compressive weight of 459 lbs (209 kg) is greater than 13 kPa (2 lb/in<sub>2</sub>) multiplied by the vertically projected area of the transport package."

#### 4.3 **Penetration Test**

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#### 4.3.1 Penetration Test Requirement

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This test drops a vertically oriented, solid steel, cylindrical bar from a height of 1 m (40 in) onto the exposed surface of the package that is most vulnerable to puncture.

The bar has a diameter of 3.2 cm (1.25 in) with a hemispherical end and a mass of 6 kg (13 lbs). The long axis of the cylinder must be perpendicular to the package surface.

For the 880SC unit it was determined the lock and lock slide would be the most vulnerable areas. Two penetration tests were performed to determine compliance to this test. Test specimens TP206(A) (s/n: D11827) and TP206(B) (s/n: D11828) were used for this test.

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## 4.3.2 Penetration Test Results – TP206(A)

Figure 4.3.2A shows the penetration bar contacting the top of the lock, figure 4.3.2B shows the drop height of the bar, and figure 4.3.2C shows the damage caused by the dropped bar.

Table 4.3.2: Penetration Bar Test Setup – T	'P206(A)	
Changes to the planned penetration target.	None	
Test Specimen Weight	44.80 Pounds	
Actual Bar Drop Height	1.0 Meter (39.4 inches)	
Temperature during test	61.2 °F/16.2 °C	
Test Specimen	TP206(A)	
Firmer 4.2.2.4. Base data firms Base Tack Scheme		
- TP206(A)	- TP206(A)	

- TP206(A)



Figure 4.3.2C: Damage from Penetration Bar Test -**TP206(A)** 

## 4.3.3 Penetration Test Results - TP206(B)

Figure 4.3.3A shows the penetration bar contacting the top of the lock slide, figure 4.3.3B shows the drop height of the bar, and figure 4.3.3C shows the damage caused by the dropped bar.

Table 4.3.3: Penetration Bar Test Setup - T	TP206(B)	
Changes to the planned penetration target.	None	
Test Specimen Weight	44.85 Pounds	
Actual Bar Drop Height	1.0 Meter (39.4 inches)	
Temperature during test	62.3 °F/16.8 °C	
Test Specimen	TP206(B)	
Figure 4.3.3A: Penetration Bar Test Setup – TP206(B)	Figure 4.3.3B: Penetration Bar height - TP206(B)	



Figure 4.3.3C: Damage from Penetration Bar Test - TP206(C)

## 4.3.4 Penetration Test Assessment

The penetration test was executed in accordance with Test plan 206, 10 CFR 71.71, and IAEA TS-R-1. An evaluation of the specimen relative to the requirements of 10 CFR 71 and IAEA TS-R-1 confirms the package meets the test requirement. The damage was not sufficient enough to prevent further testing. So, testing continued on to the 1.2 meter free drop test.

## 4.4 1.2 Meter Free Drop Test

#### 4.4.1 1.2 Meter Free Drop Test Requirement

The 1.2 meter free drop test subjects the test specimen to a free drop of at least 1.2 meters (4 feet) onto a rigid, essentially unyielding surface. The orientation of the test specimen during the drop shall be the most unfavourable relative to the failure modes identified in Test Plan 206.



## 4.4.2 1.2 Meter Free Drop Test Orientation
## 4.4.3 1.2 Meter Free Drop Test Results

## 4.4.3.1 1.2 Meter Free Drop Test - TP206(A) Results

Table 4.4.3.1A. TP206(A) Four Foot Drop	p Test Setup
Drop Orientation	Test Plan 206 Figure 8.6.2.1
Test Specimen Weight	44.80 pounds
Actual Drop Height	56 Inches
Temperature during test	17.4°C (63.4°F )

Figure 4.4.3.1A TP206(A) Orientation Figure 4.4.3.1B TP206(A) Drop Height



Figure 4.4.3.1C TP206(A) after drop Damage:

- 1. As expected there was some minor damage to the cap.
- 2. The spring plunger was damaged.
- 3. The cap remained closed.
- 4. The lock slide assembly was fully functional.

#### 4.4.3.2 1.2 Meter Free Drop Test - TP206(B) Results

Table 4.4.3.2A. TP206(B) Four Foot Dro	p Test Setup
Drop Orientation	Test Plan 206 Figure 8.6.3.1
Test Specimen Weight	44.85 pounds
Actual Drop Height	56 Inches
Temperature during test	17.7°C (63.9°F)
Figure 4.4.3.2A TP206(B) Orientation	Figure 4.4.3.2B TP206(B) Drop Height



- 2. The spring plunger was damaged.
- 3. The cap was open.
- 4. Source was secure.
- 5. The lock slide assembly was fully functional.

## 4.4.3.3 1.2 Meter Free Drop Test - TP206(C) Results

Table 4.4.3.3A. TP206(C) Four Foot Drop	p Test Setup
Drop Orientation	Test Plan 206 Figure 8.6.4.1
Test Specimen Weight	44.80 pounds
Actual Drop Height	56 Inches
Temperature during test	17.5°C (63.5°F )
to the second seco	
Figure 4.4.3.3A TP206(C) Orientation	Figure 4.4.3.3B TP206(C) Drop Height
Table 4.4.3.3B: TP206(C) Four Foot Drop	Test Damage Assessment
Figure 4.4.3.2C TP206(C) after drop	Figure 4.4.3.2D TP206(C) Close Up
Damage: 1. Shell slightly bent on both ends	

2. The lock slide assembly was fully functional.

### 4.4.4 Radiation Profile Inspection

Tables 4.4.4.1A, 4.4.4.1B and 4.4.4.1C show the surface and one-meter radiation profile measurements taken on the three test specimen (TP206(A) thru TP206(C)). All measurements are factored for a maximum package capacity of 150 curies of Iridium-192. All units were tested with source model A424-9 / source serial number 99334B. Each unit was tested first with the source in the "Front" position and then in the "Rear" position. The opposing end was loaded with the shipping plug. Comparing the measurements of the pre-tested specimen with the tested specimens proves there is no significant change in the radiation levels on the package as a result of the normal conditions of transport testing.

In some cases the dose rates after testing varied more than 25% from the original survey readings. In most cases, the dose rates involved were very low, typically < 2 mR/hr. In these cases, a variance slightly more than 0.5 mR/hr in a post test profile is sufficient to produce a dose rate change of 25% from the initial pre-test profile readings.

A review of the effect of human error introduced by obtaining manual survey measurements for dose rate surveys has demonstrated that this manual process can produce a  $\pm 25\%$  difference in measurements due to human variability alone. Factoring in the human error and comparing the results of the pre and post test survey readings and the fact that all post test surveys within the maximum allowed readings on the surface and at 1 meter from the package, it is argued that there was no significant increase in the radiation dose rate readings from the test specimens after performance of the normal condition transport tests.

	Table 4.	4.4.1A Maxi	mum Radiati	ion for	
		TP20	<u>6(A)</u>	· · · · · · · · · · · · · · · · · · ·	
	Maxin	um "Surfac	e" Measuren	aents	
Specimen	Bef	ore	Aft	er	%
Specimen	Dose mR/hr	Location	Dose mR/hr	Location	Difference
	125.9	Тор	130.1	Тор	3
TP206(A)	139.1	Right	147.3	Right	6 /
Front	119.1	Bottom	122.7	Bottom	2
Loaded	130.4	Left	132.9	Left	2
Source	154.1	Front	137.3	Front	-12
	116.6	Rear	117.1	Rear	1
	125.1	Тор	124.3	Тор	÷1
TP206(A)	134.7	Right	132.9	Right	-1
Rear	140.2	Bottom	136.8	Bottom	-2
Loaded	138.0	Left	129.8	Left	-6
Source	97.9	Front	115.4	Front	16
	148.0	Rear	150.7	Rear	2
<u>+</u>	Maxin	um "1 Mete	r" Measuren	nents	
S	Bef	ore	Aft	er	%
specimen	Dose mR/hr	Location	Dose mR/hr	Location	Difference
	.9	Тор	1.0	Тор	11
TP206(A)	.9	Right	1.1	Right	.20
Front	1.0	Bottom	1.0	Bottom	0
Loaded	1.0	Left	1.0	Left	0
Source	2.1	Front	2.0	Front	-5
	2.2	Rear	2.2	Rear	0
	.9	Тор	1.0	Тор	11
TP206(A)	1.0	Right	1.0	Right	0
Rear	1.0	Bottom	1.1	Bottom	10
Loaded	.9	Left	1.0	Left	11
Source	2,5	Front	2.9	Front	15
	1.9	Rear	2.3	Rear	19

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	Table 4	.4.4.1B Maxi TP20	mum Radiat 6(B)	ion for	
 	<u>Maxin</u>	num "Surfac	e" Measuren	nents	0/
Specimen	Dose	ore Location	Dose	Location	% Difference
· · · · · ·			mR/hr		· · · · · · · · · · · · · · · · · · ·
	145.5	lop	142.8	lop	
TP206(B)	163.5	Right	156.5	Right	4
Front	149.4	Bottom	148.7	Bottom	0
Loaded	145.9	Left	148.3	Left	2
Source	157.4	Front	170.3	Front	8
	104.0	Rear	<u>109.7</u>	Rear	5
	138.2	Top	140.7	Тор	2
TP206(B)	138.8	Right	138.6	Right	0
Rear	163.0	Bottom	164.0	Bottom	1
Loaded	149.3	Left	148.9	Left	0
Source	96	Front	138.8	Front	36
	136.9	Rear	136.9	Rear	0
· · · · ·	Maxir	num "1 Mete	r" Measure	ments	
	Bef	ore	Af	ter	%
Specimen	Dose mR/hr	Location	Dose mR/hr	Location	Difference
	.9	Тор	1.0	Тор	11
TP206(B)	1.2	Right	1.0	Right	-18
Front	1.2	Bottom	1.2	Bottom	0
Loaded	1.1	Left	1.0	Left	-10
Source	2.2	Front	1.9	Front	-15
	2.4	Rear	2.1	Rear	-13
	.8	Top	.9	Тор	10
TP206(B)	1.0	Right	1.1	Right	10
Rear	1.1	Bottom	1.1	Bottom	0
Loaded	1.0	Left	1.0	Left	0
Source	2.4	Front	2.0	Front	-18
	2.0	Rear	2.0	Rear	0

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	Table 4	.4.4.1C Maxi TP20	mum Radiat 6(C)	ion for	
-	Maxii Ref	num "Suriac	e" Measurei Af	nents	0/2
Specimen	Dose mR/hr	Location	Dose mR/hr	Location	Difference
	126.3	Тор	141.7	Top	11
TP206(C)	139.9	Right	141.6	Right	1
Front	130.3	Bottom	140.7	Bottom	8
Loaded	139.4	Left	139.9	Left	0
Source	131.0	Front	137.2	Front	5
	99.7	Rear	109.7	Rear	10
	120.9	Тор	124.7	Тор	3
TP206(C)	147.8	Right	155.9	Right	5
Rear	138.1	Bottom	143.0	Bottom	4
Loaded	135.2	Left	139.6	Left	3
Source	89.0	Front	94	Front	6
	143.4	Rear	158.5	Rear	10
	Maxi	mum "1 Mete	er" Measure	ments	
Spoolmon	Be	fore	Af	ter	%
Specimen	Dose mR/hr	Location	Dose mR/hr	Location	Difference
	.9	Тор	.9	Тор	0
TP206(C)	1.1	Right	1.0	Right	10
Front	1.0	Bottom	1.0	Bottom	0
Loaded	1.0	Left	.9	Left	-11
Source	1.9	Front	2.3	Front	19
	1.9	Rear	2.4	Rear	23
	1.0	Тор	1.1	Тор	10
TP206(C)	1.1	Right	1.1	Right	0
Rear	1.1	Bottom	1.2	Bottom	9
Loaded	1.1	Left	1.1	Left	0
Source	1.7	Front	2.3	Front	30
	2.5	Rear	2.6	Rear	4

and a second second

#### 4.4.5 1.2 Meter Free Drop Test Assessment

The 1.2 meter free drop test was performed in accordance with test plan 206, 10 CFR 71, IAEA TS-R-1.

After the 1.2 meter free drop test, all test specimens continued to successfully meet the normal transport requirements of 10 CFR 71 and IAEA TS-R-1. As a result of the testing, there was no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

## Section 5 Post Test Assessment

Los transporter and transporter a

and any set of

The test results confirm the Model 880SC transport package complies with the normal transport test requirements of 10 CFR part 71 and IAEA TS-R-1. The test resulted in no loss or dispersal of radioactive contents, no significant increase in external surface radiation levels and no substantial reduction in the effectiveness of the packaging.

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# **Appendix A: Test Specimen Documentation**

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SENTINEL QSA Global Burlindon Massachusetts		Test Plan 206 August 2013
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	Test Spec	imen Documen	itation	
	Test Spe	cimen = 880SC+T	P206	
Serial Number	Draying Number & Revision	Attach ITR's	Attach NCR	Attach TMI
D11827	880 S(- TP206 (A)	1		<u>ب</u>
D11828	8605C- TY206 (B)	1		
DI1829	880 SC-TP206(1)			
D11830	8803C-TP206(0)			· · · · · · · · · · · ·
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		- 1		·.
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Signature	Bri	nt Name		Dafe
Engineering:	= 1	PAUL BRIN		26 Sein 13
Regulatory:	P	Con Do	Nol Ale	26013
Quality Assurance		Marcine		2250720

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# **Appendix B: Radiation Profile Results**

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odel:	-DELTA BBO SC	SIVOUP	Source s/n:	99334B			
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		Pos	fNCT Test	Profile Rest	lits	<u> </u>
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	Davlan olar		1741	Course model:	404.0	· · ·
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	Shield Lot#:	1321000206		Isotope:	ir-192	· · · · · · · · · · · · · · · · · · ·
	Shield Heat #.	C1286-D07		Source activity (	Ci): 151.5	
	Ir-192 capacity (Ci)	150.00		Assay date:	12 Sep 2013	·
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		and the second	Profile Proc	cess Data		······································
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	Lepand Concept			L on the colle	eren (olova)	G.1/ I
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	· · · · · · · · · · · · · · · · · · ·		Profile Result	s - in mR/hr		
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	Right	147.3	+ y	<u> </u>	1.1	<b></b>
	Bottom	122.7	Y		1.0	Y
	Left	132.9	Ŷ		1.0	Y
1	Rear	1171	+		2.0	
	Instrument Model:	M4812	Profile Instru	ument Data Cal date:	2013-08-12	
	Instrument s/n:	291495		Cal due date:	2013-11-12	
	Right Contact a/n:	P3-1	Cal date:	2013-08-12	Cal due date	2013-11-12
	Contact-2nd s/n:	P3-2	Cal date:	2013-08-12	Cal due date	2013-11-12
	Left Contact s/n:	P3-4	Cal date:	2013-08-12	Cal due date	2013-11-12
	1-Meter Side s/n:	PR319789	Cal date:	2013-11-12	Cai due date	2013-11-12
	1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal due date	2013-11-12
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	SA GLOBAL	•	88	Auto-Profiler Data	rorm
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	880 Device Data		<del>، المحمد ال</del>	Profile Source Data	<u></u>
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Device sin:	D11827RL	97	Source model:	424-9	<u></u>
Shield Lot#	1221000206	17 NOV 17	Isotone'	89334D	<u>`</u>
Shield Heat #:	C1286-D07	<u> </u>	Source activity (C	151.5	
Ir-192 capacity	(Ci): 150.00		Assay date:	12 Sep 2013	
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Capacity Correl	ction: 1119		Surface Correct	ion (sides).	
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		Profile Resul	ts - in mR/hr		
	Surface Maximum Value	s   <= 200 mR/hr	? 1 Meter Ma	ximum Values	<= 2 mR/hr?
Тор	125.1	Y		0.9	Y
Right	134.7	Y		1.0	Y
Bottom	140.2	Y		1.0	Y
Left	138.0	<u> </u>		0.9	Y
FIOR	97.9	<u> </u>	· · · · · · · · · · · · · · · · · · ·	2.5	N .
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880 Auto-Profiler Data Form Form F-Q-1816-1           880 Device Data         Profile Source Data           Device s/n:         D11827RL           Model:         -DELTA- 8850 Sc (19 N ov 13)           Shield Lot#:         1321000206           Shield Lot#:         C1286-D07           Ir-192 capacity (Cl):         150.00
880 Auto-Profiler Data Form         880 Auto-Profiler Data Form         Form F-Q-1816-1         B80 Device Data         Device s/n:       Profile Source Data         Device s/n:       Device Data         Model:       DELTA 880 OSC 19 NOV 13         Shield Lot#:       132/1000208       Source s/n:       99334B         Shield Heat #.       C1288-D07       Ir-192       Source activity (Cl):       151.5         Ir-192 capacity (Cl):       150.00       Profile Process Data       Profile Process Data
Bill         Bill <th< th=""></th<>
880 Device Data         Device s/n:       D11827RL         Model:       DELTA- 880 CSC         Shield Lot#:       1321000206         Shield Lot#:       C1286-D07         Ir-192 capacity (Cl):       150.00         Profile Process Data       2 Sep 2013
880 Device Data         Profile Source Data           Device s/n:         D11827RL         Source model:         424-9           Model:
880 Device Data           Device s/n:         D11827RL           Model:         DELTA-         2850 Sc (17 N ov 13)           Shield Lot#:         1321000206         19 N ov 13)           Shield Lot#:         1321000206         19 N ov 13)           Shield Heat #:         C1286-D07         Source activity (Cl):         151.6           Ir-192 capacity (Cl):         150.00         Assay date:         12 Sep 2013
Device s/n:         D11827RL         Source model:         424-9           Model:         -DELTA- 8805C         19 N ov 13         Source s/n:         99334B           Shield Lot#:         1321000208         Isotope:         In-192           Shield Heat #:         C1288-D07         Source activity (Cl):         151.6           Ir-192 capacity (Cl):         150.00         Assay date:         12 Sep 2013
Model:
Shield Lot#:         1321000208         Isotope:         Ir-192           Shield Heat #:         C1288-D07         Source activity (CI):         151.5           Ir-192 capacity (CI):         150.00         Assay date:         12 Sep 2013
Shield Heat #: C1286-D07 Source activity (Cl): 151.6 Ir-192 capacity (Cl): 150.00 I Assay date: 12 Sep 2013 Profile Process Data
Profile Process Data
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Profile Process Data
Profile ID: D11827RL 9/30/2013 11:32:26 AM
Current Activity (Ci): 128.0 Surface Correction (front/rear): 1.1
Capacity Correction: 1.172 Surface Correction (sides): 1.1
Pronie Kasults - in mR/hf.
Right 132.9 Y 10 Y
Bottom 136.8 Y 1.1 Y
Left 129.8 Y 1:0 Y
Front 115.4 Y 2.9 N
Rear 150.7 Y. 2.3 N
Accent Relief
Profile Instrument Data
Instrument would. WHO 12. Cel Cate: 2013-08-12.
Right Contact s/n: P3-1 Cal date: 2013-08-12 Cal due date: 2013-11-12
Contact-zitu sini. 173-2 [ Calidate: 2013-08-12 ] Calidate: 2013-11-12.
Cel date: 2013-02-12 Cel date: 2013-02-12 Cel due dete: 2013-11-12
1-Meter Side s/n: PR319789 Cal data: 2013-11-12 Cal data: 2013-11-12
1-Meter Rear s/n: PR319787 Cal date: 2013-08-12 Cal due date: 2013-11-12
1-Meter Front s/n: PR319785 Cal date: 2013-08-12 Cal due date: 2013-11-12
Contact-Ends s/n: P3-8

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	Pr	e NCT Test	Profile Resu	lits		
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	880 Device Data	nadau arras		Profile Source Date	3.	
Device s/n:	D11828FL	Rem	Source model:	424-0		
Model:	-DELTA- BAO SC	TIS NOVIN	Source s/n:	99334B	·····	
Shield Lot#:	1321000206		Isotopa:	ir-192		
Shield Heat #:	C1286-D09		Source activity (	Ci): 151.5		
Ir-192 capacity (Ci):	150.00		Assay date:	12 Sep 2013		
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·		Profile Pro-	neep Data	<u>.</u>		
Profile Date:	25 Sep 2013	1 Joine 1 To	Profile ID: 1	011828EL 9/25/2013 1	2.09.27 PM	
Current Activity (CI	134.1		Surface Corre	ction (front/rear);	1.171	
Capacity Correction	1.118		Surface Corre	ction (sides):	1.171	
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		Profile Result	s - in mR/hr	and a standard of	and the second second	
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Instrument s/n:	291495		Cal due date:	2013-11-12		
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Contact-3rd s/n:	P3-3	Cal date:	2013-08-12	Cal due date:	2013-11-12	
Left Contact s/n:	P3-4	Cal date:	2013-08-12	Cal due date:	2013-11-12	
1-Meter Side s/n:	PR319789	Cal date:	2013-11-12	Cal due date:	2013-11-12	
1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal due date:	2013-11-12	
1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Cal due date:	2013-11-12	
Contact-Ends s/n:	P3-8	Cal date:	2013-08-12	Cal due date:	2013-11-12	
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	Post	NCT Tes	t Profile Resi	ults	<u></u>		
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Jevice s/n: Nodel:	D11828FL	No (pyl 12)	Source model:	424-9 99334B	<u></u>	-	
Shield Lot#:	13210000208		Isotope:	lr-192	· · · · · · · · · · · · · · · · · · ·		
Shield Heat #: r-192 capacity ((	C1286-D09	·	Source activity (	CI): 151.5			
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Current Activity (	Ci): 128.0		Surface Correc	ction (front/rear):	1.171		
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Pre NCT Test Profile Results	
OSA GLOBAL 880 Auto-Profiler Data Form Form F-Q-1816-1	
880 Device Data Profile Source Data	,
Device s/n: D11828RL ASSource model: 424-9	
Model:         DELTA         BB6 5C         7 ADd VI3         Source s/n:         99334B           Shield Lot#:         1321000206         Isotope:         Ir-192	
Shield Heat #: C1286-D09 Source activity (CI): 161.5	
1. 102 Capitally (CO)	
Profile Process Data	
Profile Date: 26 Sep 2013 Profile ID: D11828RL 8/25/2013 2:32:03 PM	
Capacity Correction: 1.118 Surface Correction (sides): 1.171	
Profile Results - In mR/hr	
Surface Maximum Values         <= 200 mR/hr?         1 Meter Maximum Values         <= 2 mR/hr?           Top         138.2         Y         0.8         Y	
Right 138.8. Y 1.0 Y	
Left 149.3 Y 1.0 Y	
Front 96.0. Y 2.4. N	•
Accept	
Profile Instrument Date	
Instrument Model: M4812 Cal date: 2013-08-12	
Instrument s/n: 291496 Cal due date: 2013-11-12	
Contact 2/13-11-12 Cal date: 2013-06-12 Cal due date: 2013-11-12 Cal due date: 2013-11-12	
Contact-3rd s/n: P3-3 Cal date: 2013-08-12 Cal due date: 2013-11-12	
1-Meter Side s/n: PR319789 Cal date: 2013-11-12 Cal due date: 2013-11-12	
1-Meter Rear e/n: PR319787 Cal date: 2013-08-12 Cal due date: 2013-11-12	
Contact-Ends s/n; P3-8 Cal date: 2013-08-12 Cal due date: 2013-11-12	
Inspector: Date: NCR #:	
Comments: RL = Rear Lond	
Unit 83056-TP206(B)	
Notes	
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			880	Auto-Profiler Data	Form		
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Device s/n:	D11828RL	AR	Source model:	424-9			
MODEL:	-BELTA 88050	19,21013	Source s/n:	29334B		<b>⊢</b>	
Shield Heat #	C1286-D09	·····	Source activity (CI)	151.5		- I	
Ir-192 capacity (C	): 150.00	· · · · · · · · · · · · · · · · · · ·	Assay date:	12 Sep 2013			
						-	
			And Data				
Profile Date	30 Sep 2013	FIOILE FID	Profile ID: D1	828RL 9/30/2013 1	37:03 PM		
Current Activity (C	128.0	· · · · · · · · · · · · · · · · · · ·	Surface Correction	n (front/rear):	1.171		
Capacity Correction	on: 1.172		Surface Correction	on (sides):	1.171		
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·		Class State Street St				i	
	Surface Maximum Values	Prome Result	5 IN MK/AL	mum Valuee	CE 2 mpint?		
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Right	138,6	Ŷ		1.1	Y		
Bottom	164.0	Y		1.1	Y		
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Front	138,8	<u>↓</u>		2.0		- 1	
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	Post NCT Test	Profile Results
	Q <u>SA GLOBAL</u>	880 Auto-Profiler Data Form Form F-Q-1816-1
	880 Device Data	Profile Source Data
	Device s/n: D11828FL Pla	Source model: 424-9
	Model: DELTA 8805C 19Nov13	Source s/n: 99334B
	Shield Heat #: C1285-D11	Source activity (Ci): 151.5
	Ir-192 capacity (Cl): 150.00	Assay date: 12 Sep 2013
· .	Profile Date: 30 Sep 2013	55 Data   Profile ID; D11829FL 9/30/2013 2:49:48 PM
]	Current Activity (Cl): 128.0	Surface Correction (front/rear): 1.171
	Capacity Correction: 1.172	Surface Correction (sides): 1.171
	Profile Results	
	Surface Maximum Values   <= 200 mR/hr?	1 Meter Maximum Values   <= 2 mR/hr?
1	Top 141.7 Y	0.9 Y
	Bottom 140.7 Y	<u>10</u> Υ
	Left 139.9 Y	0.9 Y
	Front         137.2         Y           Rear         109.7         Y	2.3 N 2.4 N
	Accept     reject	
	Profile Instrui	nent Data
	Instrument Model: M4612	Cal date: 2013-08-12 Cal due date: 2013-013-11-12
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	Contact-2nd s/n: P3-2 Cal date:	2013-08-12 Cal due date: 2013-11-12
	Contact-3rd s/n: P3-3 Cal date:	2013-08-12 Cel due date: 2013-11-12
	Left Contact S/n: P3-4 Cal date:	2013-11-12 Cal due date: 2013-11-12
	1-Meter Rear s/n: PR319787 Cal date:	2013-08-12 Cal due date: 2013-11-12
	1-Mater Front s/n: PR319785 Cal date: Contact-Ends s/n: P3-8 Cal date:	2013-08-12 Cal due date: 2013-11-12 2013-08-12 Cal due date: 2013-11-12
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vice s/n:	D11829RL	an-	Source model:	424-9		
odel:	-DELTA 880 SC	19NOU13	Source s/n:	99334B		
nield Lot#:	1321000206		Isotope:	lr-192		
Neid Heat#:	<u>C1286-D11</u>		Source activity (CI	) 151.5		
192 Capacity (C	<u>ni. 150.00</u>	النجيب	Assay date:	12 Sep 2013		- the second sec
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	<u> </u>	Profile Proce	ss Data			i j
ofile Date:	25 Sep 2013		Profile ID: D1	1829RL 9/25/2013 3	37:19 PM	
urrent Activity (	Ci): 134.1	,	Surface Correct	on (front/rear):		171
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Test Plan 206 – Report #1 October 2013

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Test Plan 206 – Report #1 October 2013

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# Appendix C: Test Data Worksheets

Test Plan 206 August 2013

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Description	Enter the Model and	Attach Inspectio
• Mark NA when dot used.	Serial Number	Calibration
Test Specimen, Drawing No.	8803C-TP206(A) DIL827	
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	NIA	
Record any additional tools used to facilitate the te calibration certificates.	st and attach the appropriate ins	pection report or
Penetration BAR	T10129	
Signature	Print Name	Date
Completed by:	Paul Benson	27 Sep 13
Verified by: Auth GAA	N-11 Delana	11 SEP 13

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## Drop & Puncture Test Checklist

Test Location: 40 North Dr	- Pad	
Step	P Data	Measuring Instrument
1. Record test specimen serial number: DU827	880 SC-TP206(	a
2. Record the test specimen weight:	44.80 165.	E41,110566E
3. Record the ambient temperature (°C):	61.2 °F	ENG-20
4. Record set-up orientation figure:	Fig. 8.5. 2.1	(T-198776
5. Verify set-up orientation and drop height.	40"	
6. Photograph set-up in at least two perpendicular plan	es. /	·
7. Begin video recording of the test so that impact is re	corded.	
8. Release the test specimen.	······	
9. Stop the video recorder. Ensure the point of impact a	and orientation specified in th	e plan has been achieve
10. Record the damage to the test specimen on a separat	e sheet and attach.	
<ol> <li>Engineering, Regulatory Affairs and Quality Assuration 71. Record the assessment on a separate sheet and an analysis.</li> </ol>	nce make a preliminary assess ttach.	sment relative to 10 CFI
Test witnessed by (Signature)	Print Name	Date
Engineering: MMH-CAAD MAR	Matt Btenza	27 SEP 13
Regulatory Affairs:		
1 manth	MARDAEL MILLER	20 NOV 2018

Test Plan 206 August 2013

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Drop & Puncture Test Data Sheet

Test Unit Model/Serial No .: Test: Penetration 1 - NCT 380 SC - TP206 (A) / D11827 Test Time: Test Date: 27 Sep 13 Describe drop orientation and drop height: 10:30 A Figure 8.5.2.1 of fest plan. Target impact on lock. 40" from lock. Describe impact (location, rotation, etc.): Impart an lock. Source remained in locked position Describe on-site inspection (damage, broken parts, etc.): DAMAGE to lock AREA where Key is insected On-site test assessment: TBD. Will test to see if lock is furctional Engineering: 12 27 Sep 13 Regulatory: 202 Tell 2013 QA: Al Al iboct 13 Describe and post-test disassembly and inspection: Replaced Lock. Be Key could not be inserted slide four firmal Lock was replaced AFTER Describe any change in source position: No change in source pisition Describe results of radiography: N/A. Performed 1.2 Meter dasp prior to RAdio graphy Completed by: 30 OCT 13 Date:

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Test Plan 206 August 2013

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Description * Mark NA when not used.	Enter the Model and Serial Number	Attach Inspection Report or
		Calibration Certificate
Test Specimen, Drawing No.	8805(-TP206(B)	
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	110740	
Record any additional tools used to facilitate the tes calibration certificates.	st and attach the appropriate ins	pection report or
Paus teation Bas	T10129	
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· · · · · · · · · · · · · · · · · · ·		
Signature	Print Name	Date
Completed by:		27 5 12
Varified by:	TAUL DENJON	cisepis

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Test Plan 206 August 2013

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# Drop & Puncture Test Checklist

Test Location: 40 North -	DRop PAd	<u></u>
Step	<b>Data</b>	Measuring Instrument
1. Record test specimen serial number:	8805C-TP206(B) D11828	
2. Record the test specimen weight:	44.85 lbs	E4110566 B
3. Record the ambient temperature (°C):	62.3 °F	ENG-20 (T-198776)
4. Record set-up orientation figure:	Fig. 8.5. 3.	······································
5. Verify set-up orientation and drop height.	40"	
6. Photograph set-up in at least two perpendicula	ar planes.	
7. Begin video recording of the test so that impa-	ct is recorded.	
8. Release the test specimen.		
9. Stop the video recorder. Ensure the point of ir	npact and orientation specified in the	plan has been achieved.
10. Record the damage to the test specimen on a s	eparate sheet and attach.	/
<ol> <li>Engineering, Regulatory Affairs and Quality A</li> <li>Record the assessment on a separate sheet</li> </ol>	Assurance make a preliminary assessment and attach.	ent relative to 10 CFR
	Print Name	Date
Test witnessed by (Signature)		FOR A DOMESTIC AND ADDRESS AND ADDRESS ADDR
Engineering: MAAAAAP	Matt Potenza	27 SEP 13

Test Plan 206 August 2013

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**Drop & Puncture Test Data Sheet** 

Test: Pewetration 2 - NCT Test Time: 10:40 AM Test Unit Model/Serial No.: 8805C-Tf206(B) / DU828 Test Date: drop orientation and drop height: Figure 8.5.3.1 of kst plan. TAnget impact on the lock slide. 410 from Lock slide. Describe impact (location, rotation, etc.): Pene tration ban made do rect impact on the lock slide. Describe on-site inspection (damage, broken parts, etc.): Small deart on the lock slide & shell. On-site test assessment: Lock slick Assembly was fully functional. Engineering The 275ep13 Regulatory: In Jul 20,00V Describe and post-test disassembly and inspection: None Describe any change in source position: No change in source possition Describe results of radiography: N/A. Performed 1.2 meter drop prior to RAdio graphy Completed by: Date: 30 OCT 13

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Test Plan 206 August 2013

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## **Drop & Puncture Test Equipment List**

Description * Mark NA when not used.	Enter the Model and Serial Number	Attach Inspection Report or Calibration
Test Specimen, Drawing No.	8805C-TP206(A)	<u>Certificate</u>
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	N/A	
calibration certificates.		
Signature	Print Name	Date

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Test Plan 206 August 2013

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# Drop & Puncture Test Checklist

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Test: 1.2 Meter Deop 1	-NCT-	<u></u>
Test Location: 40 North Dr.	op Pad	
Step	Data	Measuring Instrument
1. Record test specimen serial number:	880 SC- T0226 (A)	
2. Record the test specimen weight:	44 80 (b)	EXIL HASKER
3. Record the ambient temperature (°C):	124°E	EN6-70
4. Record set-up orientation figure:	F. 817	1
5. Verify set-up orientation and drop height.	<u> </u>	<u> </u>
6. Photograph set-up in at least two perpendicular planes	s. /	· · ·
7. Begin video recording of the test so that impact is reco	orded.	
8. Release the test specimen.		······································
9. Stop the video recorder. Ensure the point of impact ar	nd orientation specified in the	plan has been achieved.
10. Record the damage to the test specimen on a separate	sheet and attach.	
<ol> <li>Engineering, Regulatory Affairs and Quality Assurance</li> <li>Record the assessment on a separate sheet and attached</li> </ol>	ce make a preliminary assessm ach.	ent relative to 10 CFR
Test witnessed by (Signature)	Print Name	Date
Engineering: DR Muttally	Matt Polanza Parl Banson	27 Sep 13
Regulatory Affairs:	Marine France	20 4 01 100 10
Quality Assurance/	Dha Nillar	Mo Sent 12
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Test Plan 206 August 2013

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**Drop & Puncture Test Data Sheet** 

Test Unit Model/Serial No: 880 5C-7P206(A)/D11827 Test: 1.2 Meter Drop 1 - NCT Test Time: Test Date: 27 Sep 13 Describe drop orientation and drop height: 11:15 AN Figure 8.6.2.1 of test Plan. Height/weight Adjusted to 4'-8" Describe impact (location, rotation, etc.): Direct impact of CAP. Describe on-site inspection (damage, broken parts, etc.): Cap damaged. Spring plunger damaged. On-site test assessment: Other than cap & spring plunger there was no other visual damage Engineering: MR\_275,013 Regulatory: 3 July 20100 Describe any post-test disassembly and inspection: Backed off spring plunger & cap opened. Lock slide Assembly was fully functional. Replaced lock. Describe any change in source position: No change a source positron Describe results of radiography: See Test Plan 206 - Report #1. Section 4.4.4 Date: Completed by: 20 NOU 13

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Test Plan 206 August 2013

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1.2 Meter Deop 2 -	NCI	
Description * Mark NA when not used.	Enter the Model and - Serial Number	Attach Inspection Report or Calibration
Test Specimen, Drawing No.	8805C-TP206(B) D11828	<u>Certificate</u>
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	NIA	
Record any additional tools used to facilitate the test and a calibration certificates.	ttach the appropriate insi	ection report or
· · · · · · · · · · · · · · · · · · ·		
Signature	Print Näme	Date
Completed by:	Paul Benson	275ep 13
Verified by: Audit 6	Mart Dotostra	27 SEP 13

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## Drop & Puncture Test Checklist

Test Location: 40 North 1	Drop Pad	
Step	, Data	Measuring Instrument
1. Record test specimen serial number:	880 SC-TP26((B)	
2. Record the test specimen weight:	44.85 165	F41110566B
3. Record the ambient temperature (°C):	63.9.6	FN6-20
4. Record set-up orientation figure:	E. 8(3	(T-198776)
5. Verify set-up orientation and drop height.	1 84	2
6. Photograph set-up in at least two perpendicular plan	ies. J	
7. Begin video recording of the test so that impact is re	corded. 🖌	· · · · · · · · · · · · · · · · · · ·
8. Release the test specimen.		
9. Stop the video recorder. Ensure the point of impact	and orientation specified in the j	plan has been achieved.
10. Record the damage to the test specimen on a separat	te sheet and attach.	
<ol> <li>Engineering, Regulatory Affairs and Quality Assura 71. Record the assessment on a separate sheet and a</li> </ol>	nce make a preliminary assessm ttach.	ent relative to 10 CFR
Test witnessed by (Signature)	Print Name	Date
Engineering: Juff a fit	Matt Potenza	27 SEP 13
Regulatory Affairs:	Maculaci Finisa	201012013
- VIVTOR		

Test Plan 206 August 2013

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**Drop & Puncture Test Data Sheet** 

Test Unit Model/Serial No .: Test: 1.2 Meter Drop 2 - NCT B805C-TP206(B)/D11828 Test Date: Test Time: 11:34 27 Sep 13 Describe drop orientation and drop height: Figure 8.6.3.1 of test Plan. Height aucisht adjusted to 4'-8" Describe impact (location, rotation, etc.): Direct impact on Crip Describe on-site inspection (damage, broken parts, etc.): Cap opened. Rin damaged Spring plunger damaged. On-site test assessment: CAP can no longer be closed. Lock slide Assembly fully functional Engineering: 11 27 5 13 Regulatory: In Jul 2012 QA: UL Describe and post-test disassembly and inspection: M. # 160ct 13 NONE Describe any change in source position: No change is source location. Describe results of radiography: See Test Plan 206 - Report #1. Section 4.4.4 Completed by: Date: 20 NOV 13

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Test Plan 206 August 2013

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Description * Mark NA when not used:	Enter the Model and Serial Number	Attach Inspection Report or Calibration Certificate
Test Specimen, Drawing No.	880 SC - TP 206 (C)	
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	NIA	
Record any additional tools used to facilitate the test calibration certificates.	r and attach the appropriate ins	pection report or
15° Angle Fixture	T10835	
•		
Signature	Print Name	Date
Completed by:	PAUL BENSON	27 Seo R
Verified by: And AAA	Mart Potenza	17 SEP 13

## **Drop & Puncture Test Equipment List**

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Test Plan 206 August 2013

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# Drop & Puncture Test Checklist

	Test: 1.2 Meter Drop 3	- NCT			
· · · · · · · · · · · · · · · · · · ·	Test Location: 40 North - Dro	p Pad			
	Step	Data	Measuring Instrument		
	1. Record test specimen serial number: D11829	8505C - TP206(c)			
	2. Record the test specimen weight:	44.80 165	E4/6110566B		
	3. Record the ambient temperature (°C):	63.5°F	ENG-20		
	4. Record set-up orientation figure:	F18 8.5.4.	(T-198776)		
	<ul> <li>5. Verify set-up orientation and drop height.</li> <li>6. Photograph set-up in at least two perpendicular planes.</li> <li>7. Begin video recording of the test so that impact is recorded.</li> </ul>				
	8. Release the test specimen.				
	9. Stop the video recorder. Ensure the point of impact and orientation specified in the plan has been achieved.				
	10. Record the damage to the test specimen on a separate she	et and attach.			
	11. Engineering, Regulatory Affairs and Quality Assurance make a preliminary assessment relative to 10 CFR 71. Record the assessment on a separate sheet and attach.				
	Test witnessed by (Signature)	Print Name	Date		
	Engineering:	Matt Potenza	27 SEP 13		
	Regulatory Affairs:	Macinner Forsien	20 101/2013		
	Quality Assurance T	John Hieber	11 NOV 13		
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Test Plan 206 August 2013

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Drop & Puncture Test Data Sheet

Test Unit Model/Serial No .: Test: 1.2 meter Drup 3 - NCT Test Time: Test Date: 12:30 27 Sep 13 Describe drop orientation and drop height: Figure 8.6.4.1 of test plan. "Slap down". 1.2 meter drop. Adusted to 41' 8" for weight Describe impact (location, rotation, etc.): Impact on left side of shell. Shell bent slightly. ON impact. Right side shell also bent slightly. Describe on-site inspection (damage, broken parts, etc.): No visual damage other than shell. On-site test assessment: Minuon damage to shell. Lock slide openation A ( Engineering 275, 13 Regulatory: 20100 Describe any post-test disassembly and inspection: Very minion damage to spring plunger. Still operation Al. Lock slide operational Describe any change in source position: No change in source position Describe results of radiography: See Test PLAN 206 - Report #. Section 4.4.4 Completed by: Date: 20 Nov 13
QSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 2-49

## 2.12.17 Test Plan 206 Report #2 minus Appendices D & E (Nov 2013)



Document Number

Revision

F-E-1808-2 Test Report Cover Sheet

**TEST REPORT #2** 

FOR TEST PLAN 206

Model 880SC Transport Package

Hypothetical Accident Conditions (HAC) Transport Test Results

**Revision:** 0

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# TEST PLAN 206 – REPORT #2 MODEL 880SC TRANSPORT PACKAGE

# HYPOTHETICAL ACCIDENT CONDITIONS (HAC) TRANSPORT TEST RESULTS

As of

October, 2013

12.2.2

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# Test Plan No. 206

#### Section 1 Introduction

This report documents the hypothetical accident conditions (HAC) test results of Test Plan 206 performed on the Model 880SC transport package. The results confirm the Model 880SC transport package, identified in Section 2 passes all the hypothetical accident conditions transport test requirements specified in Test Plan 206, the Code of Federal Regulations, 10 CFR Part 71, revised as of January 26, 2004 and criteria stated in the IAEA Regulations for the Safe Transport of Radioactive Material, No. TS-R-1 1996 Edition (as amended 2003).

In order to determine the cumulative effect on the Model 880SC transport package, the HAC test evaluation is based on the sequential application of the tests specified in the order indicated in 10 CFR Part 71. Alternatively, if the test sequence had been performed in reverse order to the sequence identified in 10 CFR Part 71, with the Puncture test performed before the 30-foot free drop, an assessment is included to evaluate the effect the reverse order tests would have on the HAC test results. See section 5.3 for the reverse order assessment.

The thermal test portion of the HAC test sequence is not performed based on the condition of the test specimens after the 30-foot free drop and Puncture tests. See section 5.4 for this assessment.

The following is the pass criteria for a Type B(U) transport package after being subjected to the HAC test sequence:

- There shall be no loss or dispersal of radioactive material from the package.
- There shall be no external radiation dose rate exceeding 10-mSv/h (1-rem/h) at 1 m (40 in) from the external surface of the package.

The following HAC tests were not covered in the test plan and therefore not conducted.

- The *crush test* was not performed because is not required since the Model 880SC transport package weighs 52 lbs which is less than the 1100 lbs. minimum weight limit for the test.
- The *immersion fissile material test* is not required since the Model 880SC package does not transport fissile material.
- The *immersion all packages test* was not performed and is instead assessed since the materials of construction used in the Model 880SC transport package are impervious to water and are not structurally affected when immersed in water of at least 15 meters (50 feet).

#### Section 2 Construction and Condition of Test Specimens

#### 2.1 Test Specimen Construction

The test specimens were constructed in accordance with QSA Global engineering drawings and Quality Assurance Program. The drawings and manufacturing documents accurately depict the intended design at the time of testing along with methods for building and verifying the finished product. There were no deviations and/or changes to the test specimen before testing.

The four test specimens built for this test are the Model 880SC. Figures 2.1 and 2.2 shows test specimens, specimen numbers are TP206(A) through TP206(D). TP206(D) was assembled as a spare. This unit was not required for the HAC testing. Shipping labels and nameplates were not attached for testing.

Figures 2.1 and 2.2 shows the major assemblics and common components of the Model 880SC transport package. The nomenclature used in Figures 2.1 and 2.2 are referenced throughout this report.



FIGURE 2.1: MODEL 880SC SOURCE CHANGER TRANSPORT PACKAGE (without optional Jacket)

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# FIGURE 2.2: MODEL 880SC SOURCE CHANGER SCHEMATIC (without optional Jacket)

The primary containment system of the package is the completely seal welded source capsule assembly. The secondary containment system, the transport package source lock assemblies and shield assembly, are open to the atmosphere and therefore in constant equilibrium with changing operating pressures.

The structural materials used in the construction of the Model 880SC transport package retain their key mechanical and physical properties between  $-40^{\circ}$ C ( $-40^{\circ}$ F) and  $+38^{\circ}$ C ( $+100^{\circ}$ F). Therefore, the temperature of the test specimens did not need to be adjusted for the tests performed in test plan 206.

2.2 Test Specimen Modification

The test specimens used for the HAC were first subject to the NCT testing. Test Plan 206 - Report #1 describes damage that was caused during the testing. The penetration test on TP206(A) caused damage to the lock, specifically the key hole. This Lock was replaced prior to HAC testing.

#### Section 3 Failure Modes and Test Orientations

#### 3.1 Test Failure Modes

Each of the test orientations (Tables 3.2.1 and 3.2.2) targets a specific area on the package in an attempt to damage the package enough to cause an elevation in radiation measurements. The possible failures considered under the required test conditions potentially leading to elevated radiation measurements on and around the transport package include the following:

- 1. Fracture of the shield allowing a direct beam of radiation to transmit to the exterior of the package.
- 2. Extreme displacement of the shield within the package enough to position the source in a much less shielded location.
- 3. Any release or loss of control of the source from its shielded position within the package.

#### 3.2 Test Orientations

Table 3.2.1 shows the planned test orientation used for each test specimen in the 30-foot free drop test. These orientations attempt to exploit the failure modes discussed in section 3.1.

**Table 3.2.2** shows the planned test orientation used for each test specimen in the Puncture drop test. These orientations attempt to exploit the failure modes discussed in section 3.1.

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#### 3.3 Free Drop Height Adjustment

The drop test heights specified in 10 CFR Part 71 are adjusted higher in all the 30-foot (9 Meter) drop and 40-inch (1 Meter) Puncture tests. The adjusted drop height allows for future Model 880SC transport packages built heavier than the actual test specimens specifically for the additional weight of the jacket, but less than the maximum allowable weight specified for the transport package configuration to comply with 10 CFR Part 71.

The adjusted drop height is calculated for both the 30-foot (9 Meter) drop and 40-inch (1 Meter) Puncture tests. The adjusted drop height is determined by multiplying the worst case weight ratio by the required drop test height, 30 feet or 40 inches. The worst case weight ratio is calculated by dividing the maximum allowable weight by the actual test specimen weight. The actual weight is significantly lower given the absence of the jacket.

The maximum allowable transport package weight in the Model 880SC is 52 lbs. Table 3.3.1 shows the adjusted height for each specimen for the 30-foot (9 Meter) drop. Table 3.3.2 shows the adjusted height for each specimen for the 40-inch (1 Meter) Puncture drop.

The impact energy produced by the adjusted height in all drop tests is equal to or greater than the impact energy produced by the transport package built to its maximum weight and dropped at the required drop height specified in 10 CFR Part 71.

Table 3.3.1 Test Specimen 30-Foot (9 Meter) Free Drop Height Adjustment						
Test	Actual Test	Maximum Transport	30-Foot (9 Meter) Adjusted Height			
Specimen	(Lbs)	(Lbs)	(Meters)	(Feet)	(Feet - Inches)	
TP206(A)	44.80	52	10.6	34.82	34' 10"	
TP206(B)	44.85	52	10.6	34.82	34' 10"	
TP206(C)	44.80	52	10.6	34.82	34' 10"	

	Table 3.3.2 1	est Specimen 40-inch	(1 Meter) Puncture Dro	p Height Ad	justment	
	Test	Actual Test Specimen Weight	Maximum Transport Package Weight	40-i Adj	nch (1 Me justed Hei	ter) ght
	Specimen	(Lbs)	(Lbs)	(Meters)	(Feet)	(Inches)
	TP206(A)	44.80		1.18	3.875	46.5
	TP206(B)	44.85	52	1.18	3.875	46.5
ĺ	TP206(C)	44.80	52	1.18	3.875	46.5

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#### Section 4 Test Results

#### 4.1 Test Specimen TP206(A) Test Results

For the 30-Foot (9 Meter) test, Specimen TP206(A) was dropped from 34 feet 10 inches while oriented in its near vertical position (along the center of gravity) and with the front source lock assembly facing down toward the location of impact. The source assembly was loaded in the front source lock assembly and the shipping plug was in the rear source lock assembly. TP206(A) rotated slightly during the drop but hit the drop plate on the upper part of the source lock assembly. This impact created a shearing action on the top two bolts of the source lock assembly.

Examination of the test specimen just after the 30-Foot drop showed the top two screws of the lock source assembly had sheared off. The bottom two screws were intact. The top of the source lock assembly moved away slightly from the end plate by approximately .125". The bottom of the source lock assembly was in contact with the end plate. The end plate was slightly bent but fully intact. The source remained locked and secure. There was damage to the cap and lock. The cap was in the open position.

For the Puncture drop, test specimen TP206(A) orientation was changed from Test Plan 206. Since the top two screws were sheared / broken off during the 30-Foot drop the orientation was changed in an attempt to completely shear off the source lock assembly or try to dislodge or shear off the remaining two screws. The specimen was dropped from 46.5 inches above the puncture bar onto the side front lock source assembly. The specimen impacted per revised plan.

No additional damage was evident. The source remained locked and secure. Due to the angle of the drop the cap closed during impact.

During the post-test examination it was determined the lock needed to be replaced. The lock had sustained damage during the 30 foot drop and the key could not be inserted. To replace the lock the entire source lock assembly needed to be removed from the front plate. The "gap" created by the missing top two screws were measured prior to dis-assembly. Once the lock was replaced the source lock assembly was fully functional. The source lock assembly was then installed back onto the end plate using the original two bottom screws. These screws were bent but functional. The "gap" between the source lock assembly and the end plate was then measured to assure it was the same as prior to dis-assembly. The cap was "jammed" in the closed position and needed to be pried open.

. . . . . . . . . . . . .

Two sets of radiation profiles were taken on the package after testing. One with the source loaded in the front of the Model 880SC and one with the source loaded in the rear of the Model 880SC. Both inspections show dose levels were well below the limit of 1 R/hr at a meter from the surface of the package. See Table 5.2.1 for radiation profile data.

Table 4.1.1: 30-Foot (9 Meter) Drop Test Set	up – TP206(A)
Changes to the planned drop orientation.	None
Test Specimen Weight	44.80 pounds
Actual Drop Height	34 Feet 10 inches (10.62 Meters)
Temperature during test	68.9°F (20.5°C)
Figure 4.1.1.1: 30-Foot Drop – TP206(A) Orientation View #1	Figure 4.1.1.2: 30-Foot Drop – TP206(A) Orientation View #2
Table 4.1.2: 30-Foot Drop Test Damage Rep	ort – TP206(A)
- Top 2 bolts were missing	
<ul> <li>Minor damage to cap</li> </ul>	
<ul> <li>Cap was open</li> </ul>	
<ul> <li>Damage to top of lock</li> </ul>	1
Figure 4.1.2.1: TP206(A) immediately after 30-Foot Drop Test.	Figure 4.1.2.2: Close-up view of TP206(A) after 30-Foot Drop Test.

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Changes to the planned drop orientation.	Adjustment to angle. Trying to shear of the		
	entire source lock assembly.		
Test Specimen Weight	44.80 pounds		
Actual Drop Height	46.5 Inches (1.18 Meters)		
Temperature during test	77.5°F (25.3°C)		



Figure 4.1.3.1: Puncture Drop - TP206(A)Figure 4.1.3.2: Puncture Drop - TPOrientation View #1 - Setting AngleOrientation View #2



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Figure 4.1.5.7: Shell bent but intact.

#### 4.2 Test Specimen TP206(B) Test Results

For the 30-Foot (9 Meter) test, Specimen TP206(B) was dropped from 34 feet 10 inches while oriented in its near vertical position (along the center of gravity) and with the rear source lock assembly facing down toward the location of impact. The source assembly was loaded in the rear source lock assembly and the shipping plug was in the front source lock assembly. The cap had sustained damage during the Normal Conditions of Transport Test (see Test Plan Report #1) and therefore the cap remained open during this test. TP206(B) did not rotate during the drop and impacted per plan.

Examination of the test specimen just after the 30-Foot drop showed there was only minor additional damage to the shell and cap. The cap remained attached to the assembly. The source remained locked and secure.

For the Puncture drop, test specimen TP206(B) orientation was not changed from Test Plan 206. The specimen was dropped from 46.5 inches above the puncture bar onto the rear lock source assembly. TP206(B) impacted per plan. The cap remained open for this drop.

Examination of the test specimen just after the Puncture drop showed the cap had broken off. The bottom lock plate also appeared to be slightly bent. The source remained locked and secure.

During the post-test examination the source was secure and in the locked position but the lock slide assembly could not be opened. Due to the damage to the bottom lock plate the lock slide would not move. Upon further inspection it was discovered that the lock slide was binding on the lock slide bracket. The lock slide bracket was removed and the lock slide assembly was fully functional.

Two sets of radiation profiles were taken on the package after testing. One with the source loaded in the front of the Model 880SC and one with the source loaded in the rear of the Model 880SC. Both inspections show dose levels were well below the limit of 1 R/hr at a meter from the surface of the package. See Table 5.2.1 for radiation profile data.

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Table 4 2 3. Puncture Drop Test Setun - TP	206(B)
Changes to the planned drop orientation.	None
Test Specimen Weight	44.85 pounds
Actual Drop Height	46.5 Inches (1.18 Meters)
Temperature during test	77.2°F (25.1°C)
Figure 4.2.3.1: Puncture Drop – TP206(B)	Figure 4.2.3.2: Puncture Drop – TP206(B)
<b>Orientation View #1</b>	<b>Orientation View #2</b>

# Table 4.2.4: Puncture Drop Test Damage Report – TP206(B) • Cap broke off. • Bottom lock plate was slightly bent • Minor damage to shell. • Office of





Figure 4.2.4.1: TP206(B) immediately after the Puncture drop test.

Figure 4.2.4.2: TP206(B) immediately after the Puncture drop test – close up.

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Figure 4.2.5.1: Close-Up. Source in LockedFigure 4.2.5.2: Damage to bottom lockand secured position.plate.





Figure 4.2.5.3: Lock and lock slide still operational.

Figure 4.2.5.4: Re-assembled with lock slide bracket removed.



Figure 4.2.5.5: Close up of connector – no damage.

#### 4.3 Test Specimen TP206(C) Test Results

For the 30-Foot (9 Meter) test, Specimen TP206(C) was dropped from 34 feet 10 inches while oriented in the "slap down, 15° orientation. TP206(C) did not rotate during the drop and impacted per plan. The source assembly was loaded in the front source lock assembly and the shipping plug was in the rear source lock assembly.

Examination of the test specimen just after the 30-Foot drop showed there was only minor additional damage to the shell and rear cap. The rear cap opened but remained attached to the assembly. The source remained locked and secure.

For the Puncture drop, test specimen TP206(C) the orientation was not changed from Test Plan 206. The specimen was dropped from 46.5 inches above the puncture bar onto the bottom side of the rear source lock assembly. TP206(C) impacted per plan.

Examination of the test specimen just after the Puncture drop showed minor damage to the rear cap. The rear cap was bent but remained attached to the assembly. The front source lock assembly Cap was damaged but remained attached.

During the post-test examination the source was secure and in the locked position. Both source lock assemblies were functional.

Two sets of radiation profiles were taken on the package after testing. One with the source loaded in the front of the Model 880SC and one with the source loaded in the rear of the Model 880SC. Both inspections show dose levels were well below the limit of 1 R/hr at a meter from the surface of the package. See Table 5.2.1 for radiation profile data.

Changes to the planned drop orientation.	None
Test Specimen Weight	44.80 pounds
Actual Drop Height	34 Feet 10 inches (10.62 Meters)
Temperature during test	71.4°F (21.9°C)
Figure 4.3.1.1: 30-Foot Drop – TP206(C) Orientation View #1	Figure 4.3.1.2: 30-Foot Drop – TP206(C) Orientation View #2



Table 4.3.3: Puncture Drop Test Setup - TH	206(C)
Changes to the planned drop orientation.	None
Test Specimen Weight	44.80 pounds
Actual Drop Height	46.5 Inches (1.18 Meters)
Temperature during test	77.4°F (25.2°C)
Figure 4.3.3.1: Puncture Drop – TP206(C) Orientation View #1	Figure 4.3.3.2: Puncture Drop – TP206(C)
Orrentation Trew #1	Orientation View #2
Table 4.3.4: Puncture Drop Test Damage Re	eport – TP206(C)
<ul> <li>Table 4.3.4: Puncture Drop Test Damage Ref</li> <li>Cap opened and slightly damaged.</li> <li>Visible signs of impact but no major damage</li> <li>Minor damage to shell.</li> <li>Opposite cap was crushed.</li> </ul>	eport – TP206(C)
<ul> <li>Table 4.3.4: Puncture Drop Test Damage Ref</li> <li>Cap opened and slightly damaged.</li> <li>Visible signs of impact but no major damage</li> <li>Minor damage to shell.</li> <li>Opposite cap was crushed.</li> </ul>	eport – TP206(C) ge.
Table 4.3.4: Puncture Drop Test Damage Ref         • Cap opened and slightly damaged.         • Visible signs of impact but no major damage         • Minor damage to shell.         • Opposite cap was crushed.	eport – TP206(C) ge. Figure 4.3.4.2: TP206(C) immediately after



#### Section 5 Test Assessments

#### 5.1 30-Foot Free Drop & Puncture Test Assessment

All 30-foot free drop and Puncture tests were performed in accordance with test plan 206, 10 CFR 71, IAEA TS-R-1.

Based on the condition and position of the post Puncture test specimens, and their contents, the Model 880SC specimens tested will pass the thermal test. All Model 880SC components deemed important to safety are constructed with materials that will retain their structural integrity when exposed to temperatures at 800C for an hour.

The Model 880SC transport package satisfies the HAC test requirements of Test Plan 206, the Code of Federal Regulations, 10 CFR Part 71 and criteria stated in the IAEA Regulations for the Safe Transport of Radioactive Material, No. TS-R-1.

After the 30-foot free drop and Puncture tests, all test specimens continued to successfully meet the hypothetical accident conditions transport requirements of 10 CFR 71 and IAEA TS-R-1. After the test, there was:

- No loss or dispersal of radioactive material or contents.
- No external radiation dose rate exceeding 10-mSv/h (1-rem/h) at 1 m (40 in) from the external surface of the package.
- No escape of other radioactive material exceeding a total amount A<sub>2</sub> in 1 week.

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#### 5.2 Radiation Profile Inspection

Tables 5.2.1 shows the one-meter radiation profile measurements taken on the three test specimen (TP206(A) thru TP206(C)). All measurements are factored for a maximum package capacity of 150 curies of Iridium-192. All units were tested with source model A424-9 / source serial number 99334B. Each unit was tested first with the source in the "Front" position and then in the "Rear" position. The opposing end was loaded with the shipping plug.

Tal	ole 5.2.1 Ma	aximum 1-Me	eter Radiat	ion
	Front Load		Rear	Load
	Dose mR/hr	Location	Dose mR/hr	Location
	1.1	Тор	0.9	Тор
	1.1	Right	1.1	Right
TP206(A)	1.0	Bottom	1.1	Bottom
	1.1	Left	1.0	Left
	2.0	Front	1.5	Front
	1.6	Rear	2.3	Rear
	1.0	Тор	1.1	Top
	1.1	Right	1.1	Right
TP206(B)	1.2	Bottom	1.1	Bottom
	1.0	Left	1.0	Left
	1.6	Front	1.2	Front
	2.0	Rear	2.6	Rear
	0.9	Тор	1.1	Тор
	1.2	Right	1.1	Right
TP206(C)	1.2	Bottom	0.9	Bottom
	1.1	Left	1.0	Left
	1.3	Front	1.3	Front
	2.0	Rear	1.8	Rear

#### 5.3 Reverse Sequence 30-Foot Free Drop & Puncture Assessment

If we were to reverse the test sequence and perform the Puncture test before the 30-foot free drop, the Model 880SC transport package would continue to meet the HAC requirements of 10 CFR Part 71. The test results indicate there is no evidence the puncture billet is capable of affecting the source security of the package. It has been shown that the cap and the bottom lock plate absorb the majority of the impact with little or no effect to the source lock assembly operation and specifically the locking of the source.

This allows the Model 880SC transport package to successfully meet the hypothetical accident conditions transport test requirements of IAEA TS-R-1.

#### 5.4 Thermal Test Assessment

Review of the damage to all test specimens after the drop tests suggest the fire test would have no effect on the radiation measurements taken after the drop tests. The reasons for this can be justified based on the condition of the test specimen after the drop tests and the properties of the materials used to secure and shield the source within the specimen. See 5.4.2 for further assessment for TP206(A).

#### 5.4.1 Condition of Test Specimens before Thermal Test

- The internal structure for supporting the shield is intact and fully functional.
- The source assembly is intact, undamaged and secure in the shielded position.
- The source lock assembly continues to secure the source assemblies to the package in their shielded position.

#### 5.4.2 Additional Thermal Analysis for 880SC-TP206(A)

Significant oxidation of the depleted uranium does not occur if there is insufficient flow of oxygen available to the shield. Two major contribution factors to limiting this oxidation are the oxygen inhibitive nature of charred polyurethane foam and the packages' ability to contain the foam once charred. This has been demonstrated by thermal testing conducted by QSA Global Inc. in support of previous Type B package submissions described in the following paragraphs.

Under Test Plan 74 (Section 2.12), the Model 660 Series, Specimen D was tested successfully through normal and accidental conditions. Before thermal testing, the unit showed gaps in the outer containment (shell to endplate interface) up to  $\frac{1}{2}$  wide and 1 inch long (.5 in<sup>2</sup>). Pyrolized foam was contained within the unit. Although the shield oxidized slightly on the end nearest the largest gap, the unit passed final profile at 0.0047 R/hr at one meter.

Under Test Plan 72-S2 (Section 2.12), in support of Certificate of Compliance number USA/9035/B(U) for the Model 680-OP Series, camera s/n B198 was subjected to thermal testing. Before testing, the unit was intact and essentially undamaged with no gaps between mating surfaces. After the 30 foot and puncture drop tests,  $\frac{3}{4}$  inch long by 1/16 in wide gaps were present on both sides of the unit at the side plate / shell interface. Thermocouple readings showed temperatures of up to 1000°C on the unit and over 900°C within the depleted uranium shield. The foam was completely pyrolized but was contained within the unit. No oxidation of the shield occurred and the unit passed final profile at 0.330 R/hr at 1 meter.

Under Test Plan 80 Report (Section 2.12), in support of Certificate of Compliance number USA/9269/B(U) for the Model 650L, test specimen TP80(B) was subject to thermal testing. The drop test (30 foot and Puncture) caused the outer shell to split completely open and the inner shell to crack, creating a 3 inch long by  $\frac{1}{2}$  inch wide gap (1.5 in<sup>2</sup>). Subsequent thermal testing caused pyrolization of all the foam and vaporization in the area of the gap. Some minor oxidation of the shield was also noted. Thermocouples recorded temperatures in the shield of over 900°C and close to 1000°C at the shell. Although the shield oxidized slightly in the area of the gap, the unit passed final profile at 0.028 R/hr at one meter.

Specimen number TP206(A) sustained damage during the 30 foot drop test. The two top screws holding the source lock assembly sheared off from the end plate. The two remaining screws on the bottom were intact and securely held the source lock assembly. The top of the "bottom lock plate" moved away slightly (approx. .125") from the end plate. This gap created the potential for oxygen flow to the polyurethane foam via the .63 inch diameter foam fill hole located behind the lock plate.

As demonstrated in previous thermal testing, minor air gaps in the containment surrounding the shield are insufficient to allow oxidation of the depleted uranium shield during the thermal test.



#### 5.4.3 Material Properties at Elevated Temperatures

- The melting temperature for all materials (stainless steel, depleted uranium and tungsten) of the structure, source lock assembly and source assembly is above the thermal test temperature of 800°C.
- The thermal expansion for all materials of the structure is less than the design clearance allowed for assembly.
- The stainless steel components of the structure and source assemblies have about 30% of their room temperature strength at 800°C, respectively.

The load condition for the thermal test is for the structure to support the static weight of the shield in suspension. The dynamic impact nature of the drop tests subjects the structure to a force over 100 times the static weight of the shield. This suggests the strength of the materials used in the structure would need to decrease by two orders of magnitude or to about 1% of their strength at room temperature. The 30-minute thermal test is not long enough for significant creep deformation to occur in the structure.

## Section 6 Final Test Assessment

The Model 880SC transport package did not lose or disperse radioactive material and did not have external radiation dose rates exceeding 10-mSv/h (1-rem/h) at 1 m (40 in) from the external surface of the package after being subjected to the HAC test sequence identified in 10 CFR Part 71.

#### 6.1 Production Unit Assessment

The actual production units of the Model 880SC transport package will include a feature presenting a slight variation compared to the tested specimen. This variation and the possible effect on HAC testing is listed in Table 6.1 below.

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Table 6.1 Production Unit Feature/Change Assessment				
Feature/Change	Net Effect on Transport Package			
Thickness of the bottom lock plate. An	Add a maximum of .25 lbs. Eliminates the need			
increase of .10" will be added to the	for spacers between source lock assembly and end			
plate.	plate.			

The production feature listed in table 6.1 adds less than .25 pounds to the package and will not cause the package to exceed the maximum allowable weight for any configuration.

The results and assessments in this report confirm the Model 880SC transport package meets the hypothetical accident conditions test requirements of test plan 206, 10 CFR Part 71, and IAEA TS-R-1.

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# Appendix A: Test Specimen Documentation

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Test Specimen Documentation							
Test Specimen — 880SC-FP206							
Serial Number	Drawing Number & Revision	Attach IIR's	Attach NCR	'Attach TMI			
D11827	880 S(- TP20 6 (A)	~		~			
011828	BEOSC. TPZOG (B)	1		~			
D11829	850 SC-TP206 (c)						
DILE 30	8505C-TP266(0)	· · · · · · · · · · · · · · · · · · ·					
				· · · · · · · · · · · · · · · · · · ·			
			· · · · · · · · · · · · · · · · · · ·				
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Signature	   Pri	nt Name	]	Date			
Engineering:		PAUL BENJE	ليم	26 Sep 13			
Regulatory:	2652013						
Quality Assurance	7.75EPT 2013						

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## Appendix B: Radiation Profile Results

SSR GLOBAL         S80 Auto-Profiler Data Form Form F-Q-1815-1           Berling Jing         B80 Device Data           Herice Jn:         D1827FLF           Jing         Jing           Indel Heat K         1229-007           Jing Heat K         192 Cer 2013           Profile Process Data         1128/rLP 10/02013 31:34:345 AM           Jing Heat K         1270           Jing Heat Correction (fortheat):         1.171           Jin			Front	Load	, , , , , , , , , , , , , , , , ,	<u> </u>	مرد به در این می این این این این این این این این این ای	<u>·</u>
SPACE DEAL         Search Colspan="2">Search Colspan="2"Search Colspan="2"Search Colspan="2"Search Colspan="2"Search Cols						<u> </u>		
Biol Device Data           Profile Source Data           Device sin:         Division Data           Device Sin:         Division Data           Device Sin:         Division Data           Division Data           Division Data           Division Data           Division Data           Division Data           Profile Data:           OCC 2013           Division Data           Profile Data:           Profile Data:           Profile Data:           Profile Data:           Profile Data:           Division Data           Division Data     <	<u>QS</u>	<u>A GLOBAL</u>			880 Auto-Profiler Data Form F-Q-1815-1	Form		
Defice Stri:       D11827FLF       Surice model:       424-9         Source and:       60381       B3574       VfLoda, I. 820-5 C. 200171         Shild Lobi:       192 Source and:       603349         Source and:       12 Son 2013         Source and:       12 Son 2013         Source and:       12 Son 2013         Source and:       11 Source and:         Yurent Ackittly (D):       117.7         Source Maximum Values       <	· · · · · · · · · · · · · · · · · · ·	880 Device Data	].		Profile Source Date			
Dote:         DBERM         Profile         Description         Description           Shield Lots         13200205         Isotope:         Iriti2         Isotope:         Iriti2           Shield Lots         13200205         Isotope:         Iriti2         Isotope:         Iriti2           Shield Lots         13200205         Isotope:         Iriti2         Isotope:         Iriti2           Shield Lots:         09 Oct2013         Isotope:         Isotope:         Iriti2         Isotope:         Iriti2           Yredile Date:         09 Oct2013         IProfile ID:         D11627FLF 10/82215 3.11:34:49 AM         Iriti2           Yredile Date:         09 Oct2013         Iriti2         Surface Correction (iriti2         Iriti2           Yredile Date:         09 Oct2013         Iriti2         Iriti2         Iriti2         Iriti2           Surface Maximum Values         <= 2 mR/m?	Device s/n:	D11827FLF	Fre	Source model:	424-9	,		
Install Lots:       122100(2026)       Is (0,0)       Is (0,0)       Is (0,0)         Profile Casescity (C):       160,00       Source activity (C):       161.5         Profile Date:       09 Oct 2013       Profile Process Date         Profile Date:       09 Oct 2013       Profile Process Date         Profile Date:       09 Oct 2013       Profile Process Date         Profile Date:       09 Oct 2013       1.171         Surface Correction (formit-ear):       1.171         Surface Maximum Values       <<200 mR/hr?	Model:	DELTA Model 8:	BOSC 200013	Source s/n:	99334B	· · · · · · · · · · · · · · · · · · ·		
Profile Process Data         2 cospacity (C):       190.00         Assay date:         12 Sun 2013         Profile Process Data         Profile Process Data         During Activity (C):         117.7         Surface Correction (fronthear):         1.171         Profile Process Data         Organization (fronthear):         1.171         Surface Maximum Values         Profile Process Data         Profile Process Data         Organization (fronthear):         1.171         Surface Maximum Values         Profile Process Data         Profile Process Data         Organization:         1.171         Surface Maximum Values         Profile Process Data         Profile Process Data         Profile Process Data         Profile Instrument Data         Add data:         Profile Instrument Data         Profile Instrument Data	Shield Lot#:	1321000206		Isotope: Source activity (f		<u>·</u>		
Profile Process Date         Profile Date:       09 Oct 2013       Profile ID:       D11827FLF 109/2013 11:34:40 AM         Profile Date:       09 Oct 2013       Profile ID:       D11827FLF 109/2013 11:34:40 AM         Dependence       Surface Correction (forth/ear):       1.171         Surface Maximum Values $<= 200 \text{ mR/h?}$ 1 Mater Maximum Values $<= 2 \text{ mR/h?}^2$ Dp       Surface Maximum Values $<= 200 \text{ mR/h?}$ 1 Mater Maximum Values $<= 2 \text{ mR/h?}^2$ Dp       Surface Maximum Values $<= 200 \text{ mR/h?}^2$ 1 Mater Maximum Values $<= 2 \text{ mR/h?}^2$ Dp       Surface Maximum Values $<= 200 \text{ mR/h?}^2$ 1 Mater Maximum Values $<= 2 \text{ mR/h?}^2$ Dot $13.27 \text{ Y}$ $1.1 \text{ Y}$ <i>mater Mater Maximum Values</i> $<= 2 \text{ mR/h?}^2$ Colspan="2">Surface Maximum Values $<= 200 \text{ mR/h?}^2$ $< 1.1 \text{ Y}$ <i>mater Mater Values</i> $<= 2 \text{ mR/h?}^2$ $< mater Mater Values$ $< mater Mater Values$ <th< td=""><td>Ir-192 capacity (Ci):</td><td>150.00</td><td></td><td>Assay date:</td><td>12 Sep 2013</td><td></td><td></td><td></td></th<>	Ir-192 capacity (Ci):	150.00		Assay date:	12 Sep 2013			
Profile Process Date         Profile Date:       09 Cct 2013         Profile ID:       D11827FLF 1019/2013 11:34:49 AM         Dument Activity (C0):       117.7         Surface Correction (forthrear):       1.171         Profile Results - In mR/hr         Surface Maximum Values       <= 2 mR/hr?         Op 156.0       Y       1.1       Y         Op 156.0       Y       1.1       Y       1.1       Y         Surface Maximum Values       <= 2 mR/hr?         Surface Maximum Values       <= 2 mR/hr?         Tot       1.1       Y       1.1       Y         Surface Maximum Values       <= 2 mR/hr?         Y       1.1       Y       1.1       Y         100       Y       1.1       Y       Y       Y       N       Y       N       Y       N       Y <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
Profile Date:       09 Oct 2013       Profile ID:       D11827FLF 10/82/013 11:34:49 AM         Current Activity (Cb):       117.7       Surface Correction (fromthear):       1.171         Capacity Correction:       1.275       Surface Correction (fromthear):       1.171         Capacity Correction:       1.275       Surface Correction (sides):       1.171         Surface Maximum Values       <= 200 mR/hr?		;;	Drefle Dese					
Durrent Activity (Ci):         117.7         Surface Correction (street) And (stree) And (stree) And (street) And (street) And (stree) And (street	Profile Date:	09 Oct 2013	Profile Proce	Profile ID:	D11827ELE 10/0/2013 1	MA DA-NS		
Dapacity Correction:         1.275         Surface Correction (sides):         1.171           Profile Results - In mR/hr           Surface Maximum Values         <= 200 mR/hr?	Current Activity (Ci)	117.7		Surface Correc	tion (front/rear);	1.54.45 Pavi	171	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Capacity Correction	1.275		Surface Correc	tion (sides):	1.	171	
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Profile GenerationOpSurface Maximum Values<= 2 mR/m?	r		Destis Desuits	E-Ot-		,		
Opp          Opp <td></td> <td>Surface Maximum Values</td> <td>I &lt;= 200 mP/br/2</td> <td>In mR/nr</td> <td>wintum Values</td> <td>&lt;- 2 mB/hr2</td> <td></td> <td>1</td>		Surface Maximum Values	I <= 200 mP/br/2	In mR/nr	wintum Values	<- 2 mB/hr2		1
light       165.7       Y       1.1       Y         Gottom       132.7       Y       1.0       Y         eff       142.5       Y       1.1       Y       M&H         ront       94.8       Y       2.0       N       -/2.7       AT         Gear       102.2       Y       1.6       Y       0.06       M         Year       1.6       Y       0.06       M       METe,         Necept       Reject       N       2.0       N       -/2.7       AT         Necept       Reject       NETe,       0.06       Y       0.06       Y       0.06       Y         Necept       Reject       NETe,       0.06       Y       0.06       Y       0.06       Y       <	Тор	156.9	Y	1 110001 110	1.1	Y		1
Contom       132.7       Y       1.0       Y         aft       142.5       Y       1.1       Y       mail         ront       94.8       Y       2.0       N $-1/6.6$ AT         Rear       102.2       Y       1.8       Y       0000       AT         Rear       102.2       Y       1.8       Y       0000       AT         Accept       Reject       0012.2       Y       1.8       Y       0000         Nocept       Reject       0012.2       Y       1.8       Y       0000         Nocept       Reject       0012.2       Y       0.18       Y       0000         Nocept       Reject       0012.2       Y       0.18       Y       0013.08.12         Nocept       Reject       Cal date:       2013.08.12       Cal due date:       2013.11.12         Soltact.2nd s/n:       P3-1       Cal date:       2013.08.12       Cal due date:       2013.11.12         Soltact.2nd s/n:       P3-3       Cal date:       2013.08.12       Cal due date:       2013.11.12         Soltact.2nd s/n:       P3-4       Cal date:       2013.08.12       Cal due date:       2013.11.12	Right	165.7	Y		1.1	- Ý		
eff       142.5       Y       1.1       Y       Made         ront       94.8       Y       2.0       N       -/0.0       H         Rear       102.2       Y       1.6       Y       0.00         Naccept       Reject       0.00       N       -/0.0       H         Naccept       Reject       0.00       N       -/0.0       H       T         Naccept       Reject       0.00       Cal date:       2013-08-12       Cal due date:       2013-11-12       Cal due date:       2013-11-12 <t< td=""><td>Bottom</td><td>132.7</td><td>Y</td><td></td><td>1.0</td><td>Ŷ</td><td></td><td></td></t<>	Bottom	132.7	Y		1.0	Ŷ		
rom       94.3       Y       2.0       N       -10-0       AT         Rear       102.2       Y       1.6       Y       0ue       AT         Accept       Reject       Image: Cal date:       2013-08-12       0ue       0ue       AT         Accept       Reject       Image: Cal date:       2013-08-12       0ue date:       2013-11-12       0ue date:       2013-11-12         Instrument s/n:       291495       Cal date:       2013-08-12       Oal due date:       2013-11-12         Contact s/n:       P3-2       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact s/n:       P3-4       Cal date:       2013-08-12       Cal due date:       2013-11-12         Anter Rear s/n:       PR319789       Cal date:       2013-08-12       Cal due date:       2013-11-12         Meter Rear s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         Anter Rear s/n:       PR319785       Cal date:       2013	Left	142.5	Y		1.1	Y /	MANH	
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Instrument Sn:       291495       Cal due date:       2013-11-12         Right Contact s/n:       P3-1       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact 2nd s/n:       P3-2       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact 2nd s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         ontact s/n:       P3-4       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Meter Side s/n:       PR319789       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         -Integration s/n:       P3-8       Cal date:       2013-08-12       <	instrument Model:	M4612		Cal date:	2013-08-12			
light Contact s/n:       P3-1       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact-2nd s/n:       P3-2       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact-2nd s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact-3nd s/n:       P3-3       Cal date:       2013-08-12       Cal due date:       2013-11-12         contact-3nd s/n:       P3-4       Cal date:       2013-08-12       Cal due date:       2013-11-12         contact-sin:       PR319789       Cal date:       2013-08-12       Cal due date:       2013-11-12         i-Meter Rear s/n:       PR319787       Cal date:       2013-08-12       Cal due date:       2013-11-12         i-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         i-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         i-Meter Side s/n:       P3-8       Cal date:       2013-08-12       Cal due date:       2013-11-12         i-Meter Side s/n:       P3-8       Cal date:       2013-08-12       Cal due date:       2013-11-12         ispector:	msaument sm:	281480		Cal que daté:	2013-11-12			
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aft Contact: s/n:       P3-4       Cal date:       2013-018-12       Cal date:       2013-011-12         L=RC contact: s/n:       PR319789       Cal date:       2013-011-12       Cal date:       2013-11-12         L=Meter Side s/n:       PR319789       Cal date:       2013-011-12       Cal date:       2013-11-12         L=Meter Side s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         L=Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         L=Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         L=Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         Lontact-Ends s/n:       P3-8       Cal date:       2013-08-12       Cal due date:       2013-11-12         Ispector:	Contact-2nd s/n:	P3-3	Cal date:	2013-08-12	Cal due date:	2013-11-12		
I-Meter Side s/n:       PR319789       Cal date:       2013-11-12       Cal due date:       2013-11-12         I-Meter Rear s/n:       PR319787       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         Inspector:       Mathematical date:       Date:       9 oct f 13       NCR #:	Left Contact s/n:	P3-4	Cal date:	2013-08-12	Cal due date:	2013-11-12		1
I-Meter Rear s/n:       PR319787       Cal date:       2013-08-12       Cal due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cel due date:       2013-11-12         I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cel due date:       2013-11-12         I-Meter Front s/n:       PR3-8       Cal date:       2013-08-12       Cel due date:       2013-11-12         Ispector:       Mathematical date:       Date:       9 @CT [ 3]       NCR #:         Ispector:       FLF       FRONT       LOAD       FINAL DROP.	1-Meter Side s/n:	PR319789	Cal date:	2013-11-12	Cal due date:	2013-11-12		
I-Meter Front s/n:       PR319785       Cal date:       2013-08-12       Cal due date:       2013-11-12         Contact-Ends s/n:       P3-8       Cal date:       2013-08-12       Cal due date:       2013-11-12         Ispector: $p_{2.6}$ Date: $q_{0CT}$ $p_{3.8}$ NCR #:         ispector: $p_{2.6}$ $p_{3.6}$ $p_{3.6}$ $p_{3.6}$ $p_{3.6}$ ispector: $p_{3.6}$ $p_{3.6}$ $p_{3.6}$ $p_{3.6}$ $p_{3.6}$	1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal due date:	2013-11-12		1
$\frac{1 \text{ Cal date: } 2013 \text{ UR} $	1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Gel duo date:	2013-11-12		
ispector: pr/turn Date: 90CT 13 NCR#: iommente:FLF = FRONT LOAD FINAL DROP.	CONLICE-ENDS S/N:	<u>rs-8</u>		2013-08-12	Cai due date:	2013-11-12		
nspector: <u>fr1kkm</u> Date: <u>90cT13</u> NCR#: Nomments: <u>FLF = FRONT LOAD FINAL DROP</u> .		10	-					1
comments: <u>FLF = FRONT LOAD FINAL DROP</u> .	Inspector: h	1xm	Date:	900T13	NCR#:			
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	OS STAR	SA GLOBAL			880 Auto-Profiler Data Form F-0-1816-1	Form	
ĺ				L			
		680 Device Data			Profile Source Data		
ļ	Device s/n:	D11827RLF	Per	Source model:	424-9		
ľ	Model:	-DELTA Model 86	55C ZONOVIS	Source s/n:	99334B		
	Shield Heat #:	C1286-D07		Source activity (Ci	): 151.5		
	Ir-192 capacity (Ci)	150.00		Assay date:	12 Sep 2013	· · · · · · · · · · · · · · · · · · ·	
	r		Profile Proce	es Data			İ
	Profile Date:	09 Oct 2013	1 10/10 1 10/08	Profile ID: D	11827RLF 10/9/2013 12	2:14:30 PM	·
ļ	Current Activity (Ci	i): 117.7		Surface Correction	on (front/rear):	1	.171
	Capacity Correctio	n: 1.275		Surface Correcti	on (sides):	1	.171
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			Profile Results	- in mR/hr		·	—— I
		Surface Maximum Values	<= 200 mR/hr?	1 Meter Max	imum Values	<= 2 mR/hr?	
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	Right	133.4		-	1.1	↓ <u> </u>	
	Left	142.9			1.0		
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-	r		Profile Instrum	ent Data			
1	Instrument Model:	M4612		Cal date:	2013-08-12		
1	Instrument s/n:	291495		Cal due date:	2013-11-12		
	Right Contact s/n:	P3-1	Cal date:	2013-08-12	Cal due date:	2013-11-12	
	Contact-2nd s/n:	P3-2	Cal date:	2013-08-12	Cal due date:	2013-11-12	
1	Left Contact s/n:	P3-4	Cal date:	2013-08-12	Cal due date:	2013-11-12	
	1-Meter Side s/n:	PR319789	Cal date:	2013-11-12	Cal due date:	2013-11-12	
	1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal due date:	2013-11-12	
	1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Cal due date:	2013-11-12	
	Contact-Ends s/n:	<u> </u>		2013-08-12	Cal due date:	2013-11-12	
	-			A			
	Inspector:	man	Date:	90cT13	NCR #:		
	O among a start of the start of	ALC - ASA	A. LAAA	CTNAL DRI	P		
	Comments:	ILUT - FUERI		1015 0000	· · · · · · · · · · · · · · · · · · ·	<u> </u>	<u> </u>
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Notes and a second of the second						л	
OS OS	A GLOBAL		8	30 Auto-Profiler Data Form F-Q-1816-1	Form		
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······································	880 Device Data		<u> </u>	Profile Source Data	1	<b>-</b>	
Device s/n:	D11828FLF	Remain	Source model:	424-9			
Model:	-DELTA- Model BE	365C 20 Mar 13	Source s/n:	99334B			
Shield Heat #:	C1286-D09		Source activity (Ci):	151:5	· · · · ·		!
Ir-192 capacity (Ci):	150.00		Assay date:	12 Sep 2013			
Profile Date:	09 Oct 2013	Profile Process	Profile ID: D1	1828FLF 10/9/2013 1	2:55:49 PM		
Current Activity (Ci)	117.7		Surface Correction	n (front/rear):		1.171	
Capacity Correction	1. 1.2/5	· • •••====	Sunace Correction	1 (51085):			
		Drofile Desuite	n mD/he			1	
·	Surface Maximum Values	<= 200 mR/hr?	1 Meter Maxin	num Values	<= 2 mR/hr?		
Top	156.3	Ŷ		1.0	Y		
Bottom	146.9			1.2	Y		
Left	150,5	Y Y		1.0	Y :	men	
Rear	92,5	Y		2.0	NS	10.0 AT	1
Accept	Relect					OWEMETER	
		Profile Instrume	nt Data				
Instrument Mcdel:	291495		Cal due date:	2013-08-12	<u> </u>		Ì
Right Contact s/n:	P3-1	Cal date: 2	013-08-12	Cal due date:	2013-11-12		
Contact-2nd s/n:	P3-2 P3-3	Cal date: 2 Cal date: 2	013-08-12	Cal due date:	2013-11-12		
Left Contact s/n:	P3-4	Cal date: 2	013-08-12	Cal due date:	2013-11-12		
1-Meter Side s/n: 1-Meter Rear s/n:	PR319789 PR319787	Cal date: 2 Cal date: 2	013-11-12	Cal due date:	2013-11-12		
1-Meter Front s/n:	PR319785	Cal date: 2	013-08-12	Cal due date:	2013-11-12		
Contact-Ends s/n:	P3-8	Cal date: 2	073-08-12	Cal due date:	2013-11-12	I	
وشعر المسال	12mm	<b>D</b> (	Q1-717				
Inspector:		Date:	900113	NCR#:			
Comments:	FLF =	FRONT LO	AD FINA	- DROP.			
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Q	SA GLOBAL			880 Auto-Profiler Data Form F-Q-1816-	a Form 1		
	880 Device Data			Profile Source Data	a		
Device s/n:	D11828 RLF	Real	Source model:	424-9			
Model:	DELTA Model 881	DSC RUMOVIS	Source s/n:	99334B			
Shield Lot#:	1321000206 C1286-D09		Source activity (Ci)	Ir-192			
Ir-192 capacity (Ci	: 150.00		Assay date:	12 Sep 2013			
Pmflla Data	08 Oct 2012	Profile Proce	ss Data		40.011		
Current Activity (C	117.7		Surface Correction	1828 10/9/2013 1:28:4	42 PM 1 17		
Capacity Correction	n: 1.275	····	Surface Correction	n (sides):	1.17	71	
		Profile Results	- in mR/hr				
Top	Surface Maximum Values	<= 200 mR/hr?	1 Meter Maxi	mum Values	<= 2 mR/hr?		
Right	181.9	+ ÷		1.1	Y Y		
Bottom	157.9	Y		1.1	Y		
Left	162.5	Y		1.0	Y		
Rear	99.1	- Y		26	N Z IA	DAT	
		Profile Instrum	ient Data				
Instrument Model:	M4612	·	Cal date:	2013-08-12	· · · · · · · · · · · · · · · · · · ·		
Right Contact a fai	231403	0.144		2013-11-12			
Contact-2nd s/n:	P3-2	Cal date:	2013-08-12	Cal due date:	2013-11-12		
Contact-3rd s/n:	P3-3	Cal date:	2013-08-12	Cal due date:	2013-11-12		
Left Contact s/n:	P3-4	Cal date:	2013-08-12	Cal due date:	2013-11-12		
1-Meter Side s/h:	PR319789 PR319787	Cal date:	2013-11-12	Cal due date:	2013-11-12		
1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Cal due date:	2013-11-12		
Contact-Ends s/n:	P3-8	Cal date:	2013-08-12	Cal due date:	2013-11-12		
Inspector:	Domi	Date:	90CT13	NCR #:			
Comments:	RLF = RE	ARLOAD	FINAL	DROP		[	
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00	AGLOBAL		Γ	880 Auto-Profiler D	ata Form	7	
Si Si Ye	A OLOBAL		L	Form F-Q-181		]	
	880 Device Data			Profile Source I	Data		
Device s/n:	D11829FLF	PET	Source mo	del: 424-9			
Model:	-DELTA Model 880	SC ELMOVIO	Source s/r	: <u>99334B</u>			
Shield Heat #:	C1286-D11		Source ac	ivity (Ci): 151.5			
Ir-192 capacity (Ci)	150.00		Assay dat	e: 12 Sep 2013	<u> </u>		
Profile Date:	09 Oct 2013	Profile Proce	ess Data Profile II	D11829FLF 10/9/201	3 2:40:04 PM	<u>+</u>	
Current Activity (Ci	): 117.7	······	Surface	Correction (front/rear):		1,171	
Capacity Correctio	n: 1.275		Surface	Correction (sides):		1.171	
······	Curfuse Manderson Mathema	Profile Results	- in mR/hr	das Maximum Values		]	
Top	Surface Maximum Values	<= 200 mR/nr/		ter Maximum Values	<= 2 mR/nr/	·	
Right	147.5	+		1.1			
Bottom	136.8	Ŷ		0.9	Y		
Left	138.2	Y		1.0	Y		ĺ
Front	129.7	Y Y		1.3			
		Profile Instru	ment Data			·	
Instrument Model:	M4612		Cal date	2013-08-12			
Instrument s/n:	291495		Calidue	date: 2013-11-12			
Right Contact s/n:	P3-1	Cal date:	2013-08-12	Cal due dat	te: 2013-11-12		
Contact-2nd s/n:	P3-2	Cal date:	2013-08-12	Cal due dat	te: 2013-11-12		
Contect-3rd s/n:	P3-3	Cal date:	2013-08-12	Cal due dat	te: 2013-11-12		
Left Contact s/n:	P3-4 · · · · · · · · · · · · · · · · · · ·	Cal date:	2013-00-12	Cal due da	18: 2013-11-12 be: 2013-11-12		
1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal due dat	te: 2013-11-12		1
1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Cai due dat	te: 2013-11-12		1
Contact-Ends s/n:	P3-8	Cal date:	2013-08-12	Cal due da	te: 2013-11-12		1
Inspector:	allin-	Date:	10 oc	13 NCR#:			
Comments:	FLF = 1	FRONT COM	10 F	INBL OROP			
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QS	A GLOBAL		Γ	880 Auto-Pro Form F-	filër Data F Q-1816-1	Form	]	
	landar (1998) - 19		Ļ				1	
	880 Device Data		[	Profile So	urce Data			
Device s/n: Model:	DI1829RLF	SC POWER 13	Source mod	el: 424-9 99334B				
Shield Lot#:	1321000208		Isotope:	Ir-192				
Ir-192 capacity (Ci):			Assay date:	12 Sep 2	2013			
	<u></u>							
Profile Date:	10 Oct 2013	Profile Proce	Profile ID:	D11829RLF 10/	10/2013 7:	:53:44 AM		
Current Activity (Ci Capacity Correction	): 116.6 1: 1.287		Surface C Surface C	orrection (front/rear): orrection (sides):		1	1.171	
	· · · · · · · · · · · · · · · · · · ·			<u></u>	······		I	
	Curface Maximum Values	Profile Results	- in mR/hr			4- 2 m D 5-0		
Тор	127.6	Y	1 Met	er Maximum Values 0.9		<= 2 mR/nr? Y		
Right	153.5	Ý.		1.2		Ŷ		
Left	136.0	- <u>Y</u>		1.2		Ŷ		
Front	95.8	Y Y		1.3		Y		
	<u>149.5</u>			2,U		N A7 ~	D. ME METE	
Accept	Reject					AI 0	ive mete	<i>f</i> L.
		Profile Instrum	nent Data					
Instrument Model: Instrument s/n:	M4612 291495		Cal date: Cal due d	2013-08-1 ate: 2013-11-1	12			
Right Contact s/n:	P3-1	Cal date:	2013-08-12		le date:	2013-11-12		
Contact-2nd s/n:	P3-2	Cal date:	2013-08-12	Cal du	ie date:	2013-11-12		
Contact-3rd s/n:	P3-3	Cal date:	2013-08-12	Cal du	le date:	2013-11-12		Ì
1-Meter Side s/n:	PR319789	Cal date:	2013-08-12	Cal du	ie date:	2013-11-12		
1-Meter Rear s/n:	PR319787	Cal date:	2013-08-12	Cal du	ie date:	2013-11-12		
1-Meter Front s/n:	PR319785	Cal date:	2013-08-12	Cal du	ie date:	2013-11-12		
CONSCEPTING SIT.	<u>`````````````````````````````````````</u>	U Uai uater	2010-00-12		15 Ual(e;	.2013-11-12.		
Inspector:	Alli	Date:	10 OCT	13 NCR#				1
Comments:	RLF=	REAR LOA	0 F:	ENAL DROP	2			
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Test Plan 206 – Report #2 October 2013

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## Appendix C: Test Data Worksheets

SENTINEL QSA Global<sup>1</sup> Burlington, Massachusetts

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# Drop & Puncture Test Equipment List

Description * Mark NA when not used:	Enter the Model and Senal Number	Attach Inspection Report or Calibration Certificate
Test Specimen, Drawing No.	TP206(A)	
Drop Surface, Drawing No.	0[182]	
* Puncture Billet, Drawing No.	N/A	A//A
Record any additional tools used to facilitate the test a calibration certificates.	nd attach the appropriate h	spection/report or
	·	
	and the second	The Real State Langer, "The series and series and a series and the
Signature	Print Name	Date
Completed by:	Paul Benson	BLOCTB
Verified by: Man ( Annu )	Mars Potenza	OF OCT 13
Test Plan 206 August 2013

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#### **Drop & Puncture Test Checklist**

Test Location: 40 Nor	th Dro	p PAd	
Step		Data	Measuring Instrument
1. Record test specimen serial numbe	//////////////////////////////////////	D11827	
2. Record the test specimen weight:		44.80 165	E416110566B
3. Record the ambient temperature (°	C):	20.5	ENG-20
4. Record set-up orientation figure:		F16 8.=	72.1
5. Verify set-up orientation and drop	height.	34 PT 10	IN 34 FEIGH
6. Photograph set-up in at least two p	erpendicular planes.	V	
7. Begin video recording of the test se	o that impact is recorde	d. 🗸	
8. Release the test specimen.	····	<hr/>	
9. Stop the video recorder. Ensure the	e point of impact and o	ientation specified in the p	lan has been achieved.
10. Record the damage to the test spec	imen on a separate she	et and attach.	
<ol> <li>Engineering, Regulatory Affairs ar 71. Record the assessment on a sep</li> </ol>	d Quality Assurance m parate sheet and attach.	ake a preliminary assessm	ent relative to 10 CFR
		Print Name	Date
Test witnessed by (Signature)			24 S.
Engineering:	MMVaa	Paul Benson	20ct 13
Test witnessed by (Signature) Engineering: Regulatory Affairs	Mill nap	Poul Benson	20c7 13

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#### **Drop & Puncture Test Data Sheet**

Test Unit Model/Serial No .: Test: 9 Meter Drop 1 - HAC 8805C - TP206(A) 'DIJ827 Test Time: Test Date: 2 OCT 13 10:45 AM Describe drop orientation and drop height: 8.7.2.1 of Test Phan Fig. Describe impact (location, rotation, etc.): Slight notation onto upper edge of lock plate. Describe on-site inspection (damage, broken parts, etc.): Source lock Assy tilted Away from Endplate. Two mounting screws broken (missing. Lock was damaged. On-site test assessment: Source remains in shield & safe position but moved away from sweet spot. This impact origination was as damaging if not more damaging than the intended impact. There fore the test was not reported Engineering: 0200713 Regulatory: Brill 2013 QA: (MC) 11NOV 13 Describe any post-test disassembly and inspection: NONC Pur stoke test was performed after the 9M drop. The Describe any change in source position: broken Slight change due to SCREWS Describe results of radiography: NIA Radiography performed after the Puncture test Date: Completed by: 30 act 13

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### Drop & Puncture Test Equipment List

Description * Mark NA when not used:	Enter the Model and Serial Number	Attach Inspection Report or Calibration Certificate
Test Specimen, Drawing No.	TP206(B)	
Drop Surface, Drawing No.	T10740	
* Puncture Billet, Drawing No.	NIA	NIA
Record any additional tools used to facilitate the fest a calibration certificates.	nd attach the appropriate in	spection report or
		· ·
······································		
Signature	Print Name	Date
Completed by:	Paul Benson	02 00773
Verified by:	Nott Potenza	02 oct 13

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Test Plan 206 August 2013

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### Drop & Puncture Test Checklist

Test Location: 40 North T	Prop Pad	
Step	Data	Measuring Instrument
1. Record test specimen serial number:	D11827	
2. Record the test specimen weight:	44.85	E4/110566 B
3. Record the ambient temperature (°C):	21.1	ENG-ZO
4. Record set-up orientation figure:	EK 8	.7.3.1
5. Verify set-up orientation and drop height.	34 PT	IDIN
6. Photograph set-up in at least two perpendicular plan	nes. 🗸	
7. Begin video recording of the test so that impact is re	ecorded.	······
8. Release the test specimen.	V	
9. Stop the video recorder. Ensure the point of impact	and orientation specified in t	he plan has been achieved.
10. Record the damage to the test specimen on a separat	te sheet and attach.	
<ol> <li>Engineering, Regulatory Affairs and Quality Assura 71. Record the assessment on a separate sheet and a</li> </ol>	ance make a preliminary asses attach.	essment relative to 10 CFR
Test witnessed by (Signature)	Print Name	Date
Engineering:		
Engineering. PAR_MM usp	Paul Bausan	5 62 OCT 13

Test Plan 206 August 2013

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#### **Drop & Puncture Test Data Sheet**

Test Unit Model/Serial No .: Test: 9 M DRop 2- HAC 880 SC - TP206 (B)/D11828 Test Date: Test Time: 10:20 Am 2 OCT 13 Describe drop orientation and drop height: 8.7.3.1 of Test Plan Fig. Describe impact (location, rotation, etc.): Impact as planned. No Rotation observed. Dust cap not engaged before drop. Impact target on source connector - No damage. Describe on-site inspection (damage, broken parts, etc.): Impact print on dust cover mounting face. Bent body flarge. Lifting eye dented body. On-site test assessment: Remained secure in shielded position. Source Engineering: 10 - 07 - 07 13 Regulatory: 20 NOV Describe any post-test disassembly and inspection: IL NOV 13 Describe any post-test disassembly and inspection: NoNe The Purcture test was performed after the 9M drop. Describe any change in source position: NONE Describe results of radiography: NIA Radiography performed after the Purcture test. Completed by: Date: 30 0CT /3

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Drop & Puncture Test Equipment List

Description * Mark NA when not	used.	Enter the Model and Serial Number	Attach Inspection Report or
Test Specimen, Drawing No.		TP206(C)	Calibration Certificate
Drop Surface, Drawing No. * Puncture Billet, Drawing No.		T10740	
Record any additional tools used to fa calibration certificates.	acilitate the test and atta	//// cb the appropriate ins	pection report or
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Signature		Print Name	Date
Completed by:	-	Paul Bensin	62 AT 12
Verified by:	······································	Mart Potenza	02 OCT 13

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#### Drop & Puncture Test Checklist

Test Location: 40 North Dr	Lop PAd	1
Stêp	Data	Measuring Instrument
1. Record test specimen serial number:	D11829	
2. Record the test specimen weight:	44.80 16s	E41110566B
3. Record the ambient temperature (°C):	21.9	EN6-20
4. Record set-up orientation figure:	F16- 8.	7.4.1
5. Verify set-up orientation and drop height.	34 FT 1	DIN.
6. Photograph set-up in at least two perpendicular planes.	V	
7. Begin video recording of the test so that impact is recorded	ed. ~	
8. Release the test specimen.	~	<u>,</u>
9. Stop the video recorder. Ensure the point of impact and o	rientation specified in the	e plan has been achieved.
10. Record the damage to the test specimen on a separate she	et and attach.	· · · · · · · · · · · · · · · · · · ·
<ol> <li>Engineering, Regulatory Affairs and Quality Assurance n 71. Record the assessment on a separate sheet and attach.</li> </ol>	nake a preliminary assess	ment relative to 10 CFR
Test witnessed by (Signature)	Print Name	Date
Engineering: Nor Man use	Poul Benson	BLOCT B
Regulatory Affairs	MARWAR FILLE	2010012013
Quality Assurance:		

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**Drop & Puncture Test Data Sheet** 

Test Unit Model/Serial No .; Test: 9M Drop 3 - HAC <u>880 SC - TP206 (C)</u> <u>| DI1829</u> Test Date: Test Time: 10:30 AM 2 Oct 13 Describe drop orientation and drop height: e. englis ser i ser en Figure 8.7.4.1 of Test Phu Describe impact (location, rotation, etc.): IMPACT WEATION AS PLANNED No Rotation OBSERVED Describe on-site inspection (damage, broken parts, etc.): IMPACT PRIMUT ON BOHUM On-site test assessment: SOUNCE REMAINED SECURED AND SHIELDED. Engineering: MR 02 02 01 Regulatory: 20 Jull 2013 QA: Whe Hoto Oct 13 Describe any post-test disassembly and inspection: NONC Describe any change in source position: NONE Describe results of radiography: See Table 5.2.1 & Appendix Bot Test Plan 206 - Report #2 200 Date: 140CT 13 Completed by

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	Drop & Puncture Test E	quipment List	
	Test: PUNCture 1 -	HAC	
	Description * Mark NA when not used.	Enter the Model and Serial Number Report or Calibration	
	Test Specimen, Drawing No.	TP206(A)	
	Drop Surface, Drawing No.	D11827	-
	* Puncture Billet, Drawing No	TIDI19	
	Record any additional tools used to facilitate the test and a calibration certificates.	tach the appropriate inspection report or	
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	······································		1
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	Signature	Print Name Date	Press and House
	Completed by:	Port Benson 2007 13	_
	Verified by:	Matt Potenza 2 oct 13	

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#### Drop & Puncture Test Checklist

	PROP PAd		
Step	Data	Measuring Instrument	
1. Record test specimen serial number:	D11827		
2. Record the test specimen weight:	414.80	E41, 110566 B	1
3. Record the ambient temperature (°C):	25.3	ENG-7.0	
4. Record set-up orientation figure:	Slight ADJ	stmant to Angle	- tensi
5. Verify set-up orientation and drop height.	46,5 IN		san
6. Photograph set-up in at least two perpendicular plan	nes.		
7. Begin video recording of the test so that impact is r	ecorded.	·····	1
8. Release the test specimen.	~		1
9. Stop the video recorder. Ensure the point of impact	t and orientation specified in t	he plan has been achieved.	
10. Record the damage to the test specimen on a separa	ate sheet and attach.		
<ol> <li>Engineering, Regulatory Affairs and Quality Assur- 71. Record the assessment on a separate sheet and a</li> </ol>	ance make a preliminary asses attach.	ssment relative to 10 CFR	-
Test witnessed by (Signature)	Print Name	Date	
Engineering: PR-MMusep	Parl Banks	2 oct 13	<b>]</b> .
Regulatory Affairs:			1
m	Manage Fine	A 120 A M V 2012	1

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#### **Drop & Puncture Test Data Sheet**

Test Unit Model/Serial No .: Test: Puncture 1 - HAC <u>8805C-TP206(A)</u> D11827 Test Date: Test Time: 2:20 PM 2 OCT 13 Describe drop orientation and drop height: FIGURE 8.8.2.1 of test plan. Orientation changes to attempt to pry off two remaining bolts. Describe impact (location, rotation, etc.): Impact hit on lock plate At AN Angle with center of gravity off the tanget surface. Describe on-site inspection (damage, broken parts, etc.): only minion dents. Lock plate & source wire intact. REMAINS On-site test assessment: Source Remained in its secure & shielded position. Engineering: 10 02007 17 Regulatory: M Describe any post-test disassembly and inspection: Removed source lock assy from shell & replaced the lock. The lock was damaged during the 9m drop & needed to be replaced for Profiling. Re-Assembled using bent screws, Describe any change in source position: Gopened the CAP Slight change due to 30' deop. which was " Ammed' shat Describe results of radiography: See TAble 5.2.1 See Appendix B of Test Phin 206 Report#2 - Max. I meter reading was 2.3 m R/hr. Completed by: Date: NOV

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Drop & Puncture Test Eq	uipment List
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Test: Puncture 2 - HAC		
 Description * Mark NA when not used.	Enter the Model and Serial Number	Attach Inspection Report or Calibration
Test Specimen, Drawing No. Drop Surface, Drawing No.	TP206(B) D11828	
* Puncture Billet, Drawing No.	$\frac{10740}{1019}$	DECHORIEDOLLOT
calibration certificates.		
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	· · · · · · · · · · · · · · · · · · ·	
Signature Completed by:	Print Name Paul Benson	Date
Verified by:	Matt Potenza	02. OOT 13

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Drop & Puncture	Test	Checklist
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Test Location: 40 North Dr	op Pad			
Step	Dafa	Measuring Instrument		
1. Record test specimen serial number:	011828			
2. Record the test specimen weight:	44.85	E41110566B		
3. Record the ambient temperature (°C):	25.1	ENG-20		
4. Record set-up orientation figure:	Pen test 1	chon		
5. Verify set-up orientation and drop height.	46.5 IN	chos.		
6. Photograph set-up in at least two perpendicular planes.	<u>и</u>			
7. Begin video recording of the test so that impact is record	led.			
8. Release the test specimen.	V			
9. Stop the video recorder. Ensure the point of impact and	9. Stop the video recorder. Ensure the point of impact and orientation specified in the plan has been achieved			
10. Record the damage to the test specimen on a separate sh	eet and attach.			
<ol> <li>Engineering, Regulatory Affairs and Quality Assurance</li> <li>Record the assessment on a separate sheet and attack</li> </ol>	make a preliminary assessi 1.	nent relative to 10 CFR		
Test witnessed by (Signature)	Print-Name	Date		
Engineering:	PAUL BENSON	02 OCT 13		
102 MM HAP				
Regulatory Affairs	MTCHAGI ENLICO	20 101 2012		

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**Drop & Puncture Test Data Sheet** 

Test Unit Model/Serial No, Test: Public 2 - HAC 8805C-TP206(B)/D11828 Test Date: Test Time: 2:40 PM 200T 13 Describe drop orientation and drop height: Figure 8.8.3.1 of Test Plan Describe impact (location, rotation, etc.): IMPACT ON DUST CAP (NOT LAtches). Describe on-site inspection (damage, broken parts, etc.): Dust Cap Renoved upon import Minon DANTS ON BODY On-site test assessment: Same remains seems and in its Rilly shielded Position. Engineering Pro or city Regulatory: The 2013 OA Describe any post-test disassembly and inspection: Lock slide was sammed on lock slide bracket. Source lock Assy WAS Removed from shell & lock slide banket was removed. Surce lock Assy was then Re-Assembled to shell. Describe any change in source position: NONE Describe results of radiography: See Table 5.2.1 & Appendix B of Test Phan 206 - Report #2 MAX 1 meter Reading was 2.6 mR/hr Completed by: Date: 14 OC T

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Drop & Puncture Test E	quipment List		
Test: Puncture 3 - HA	C		
Description * Mark NA when not used.	Enter the Model and Serial Number	Attach Inspection Report or Calibration	
Test Specimen, Drawing No.	TP206(C)	Certificate	
Drop Surface, Drawing No.	D11829		
* Puncture Billet, Drawing No.	T10740		·
Record any additional tools used to facilitate the test and at calibration certificates.	tach the appropriate ins	pection report or	
·			
	* * *		
· · · · · · · · · · · · · · · · · · ·			
	· 		
Signature	Print Name	Date	
Completed by:	R.I.R.	02 ort 12	
Verified by:	Matt Btenza	of oct B	

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Drop & Pı	ncture Test	Checklist
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Test Location: 40 North T	PROP PAd					
Step	Data	Measuring Instrument				
1. Record test specimen serial number:	TP206(C) D11829					
2. Record the test specimen weight:	44.80 lbs	E41110566B				
3. Record the ambient temperature (°C):	25.2	ENG-20				
4. Record set-up orientation figure:	PER Plan	L				
5. Verify set-up orientation and drop height.	46.5 IN					
6. Photograph set-up in at least two perpendicular planes	s. V					
7. Begin video recording of the test so that impact is reco	orded.					
8. Release the test specimen.	~	······				
9. Stop the video recorder. Ensure the point of impact ar	9. Stop the video recorder. Ensure the point of impact and orientation specified in the plan has been achieved.					
10. Record the damage to the test specimen on a separate	sheet and attach.					
<ol> <li>Engineering, Regulatory Affairs and Quality Assurance</li> <li>Record the assessment on a separate sheet and attached</li> </ol>	ce make a preliminary assessm ach.	ent relative to 10 CFR				
Test witnessed by (Signature)	Print Name	Date				
Engineering: PGA MW 440	Paul Benson	62 OCTB				
Regulatory Affairs	Machan Friday	20 101 2013				

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**Drop & Puncture Test Data Sheet** Test Unit Model/Serial No.: Test: PUNCTURE 3- HAC DI1829 8805C-TP206(C)/ Test Date: Test Time: 3:05 PM 2 oct 13 Describe drop orientation and drop height: Figure 8.8.4.1 of test Plan Describe impact (location, rotation, etc.): IMPART PER PLAN Describe on-site inspection (damage, broken parts, etc.): Dust GVA UN LAtches opposite Dust Gove conshed INVARD. On-site test assessment: Source remains secures and its thidas Pose from. Engineering Min weetin Regulatory & Jul 2013 QA: fre H. [6007 (3) Describe any post-test disassembly and inspection: MONR Describe any change in source position: NONC Describe results of radiography: See TAble S.2.1 & Appendix B of Test Plan 206 - Report #2 - MAX 1 meta reading was 2.0 mR/hr Date: 14 OCT 13 Completed by;

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#### **Section 3 - THERMAL EVALUATION**

#### 3.1 Description of Thermal Design

The Model 880 Series transport packages are completely passive thermal devices having no mechanical cooling system or relief valves. The exterior surface finish of the package is light silvery stainless steel having an absorptivity of about 0.44, or a reflectivity of 0.56. Cooling of the package is through free convection and radiation. There are no specific cooling or insulating design features. Pressure relief of the container weldment is only necessary during the thermal test and is provided by the holes in both the rear and front end plates which will vent to atmosphere.

#### **3.1.1 Design Features**

The Model 880 Series transport packages are described in Section 1. The thin walls of the steel weldment exhibit almost no thermal gradient. During a fire test, the exterior steel weldment will very quickly heat to a uniform temperature, eliminating stresses induced by thermal differentials within the material. Further, the steel weldment will move and flex easily, thus relieving any thermal expansion stress without rupture.

The containers use depleted uranium shielding. The depleted uranium is fully enclosed in the welded steel structure and endplates which are attached by screws. This construction prevents oxidation by severely limiting oxygen from reaching the depleted uranium shield.

#### **3.1.2 Decay Heat of Contents**

The maximum activity for this package is 150 Ci of Ir-192. Accounting for source absorption, this equals a maximum content activity of 345 Ci of Ir-192. The corresponding decay heat generation rate for the content activity is approximately 3 Watts (See Table 1.2.B).

#### 3.1.3 Summary Tables of Temperatures

Lable 5.1.A. Summa	ry rable of reinperatures	
Temperature	Model 880 Series Package	Comments
Condition		
Insolation (38°C in full sun)	65.4°C (149.6°F)	Section 3.4.1.1
Decay Heating (38°C in shade)	47°C (117°F)	Section 3.4.1.2
Fire Test During & Maximum Post-Fire Test	800°C(1,472°F)	

Table 3.1.A: Summary Table of Temperatures

#### 3.1.4 Summary Tables of Maximum Pressures

All package components are vented to atmosphere. As such, no pressure will build up in these components under either Normal or Hypothetical Accident conditions. Normal operating conditions will generate negligible pressure differential within the package. The package has the ability to withstand elevated atmospheric pressure because all components, except the special form source, are open to the atmosphere.

OSA Global, Inc. Burlington, Massachusetts December 2015 - Revision 10 Page 3-2 Any pressure generated within the special form source is significantly below that which would be generated during the Hypothetical Accident Conditions thermal test, which is shown in Sections 2.7.4.3 and 3.4.1.4 to result in no loss of structural integrity or containment.

l	Table 5.1.B: Summary Table of Maximum Pressures						
Package Configuration	2	Normal Conditions	Fire Conditions				
	Void Volume in <sup>3</sup>	88°C (190°F)	800°C (1,472°F)	Comments			
		Pressure Developed	Pressure Developed				
880 Series	0	0 psig	0 psig				

#### Table 2.1 D. Summary Table of Maximum Drossurves

#### 3.2 **Material Properties and Component Specifications**

#### 3.2.1 Material Properties

Table 3.2.A lists the relevant thermal properties of the important materials in the transport package. The sources referred to in the last column are listed below the table.

I able 5.2.	Table 5.2.A: Thermal Properties of Principal Transport Package Materials							
Material	Density (lb/in <sup>3</sup> )	Melting/Combustion Temperature	Thermal Expansion <sup>1</sup>	Source				
Depleted Uranium	0.68	1,130°C (2,066°F)	8µin/in°F	Reference #1, p. 6- 11 and Reference #2				
Steel (nominal)	0.28	1,510°C (2,750°F)	6.3µin/in°F	Reference #1, p. 6-7 and 6-11				
Stainless Steel- Type 304L	0.29	1,400-1,450°C (2,550-2,640°F)	9.9µin/in°F	Reference #1, p. 6-11				
Tungsten	0.70	3,370°C (6,098°F)	2.4µin/in°F	Reference #1, p. 6-51				
Titanium	0.16	1,500 – 1,700°C (2,732 – 3,092°F)	11µm/m°K	Reference #4				

Table 3.2.A:	Thermal Prop	perties of Prin	cipal Trans	nort Package	e Materials

<sup>1</sup>Note that the thermal expansions of the materials in this table are temperature dependent.

#### **Resource references:**

- 1. Eugene A. Avallone and Theodore Baumeister III, Mark's Standard Handbook for Mechanical Engineers, Tenth Edition, New York: McGraw-Hill, 1996.
- 2. Lowenstein, Paul. Industrial Uses of Depleted Uranium. American Society for Metals. Metals Handbook, Volume 3, Ninth Edition.
- 3. Metals Handbook. American Society for Metals, 8th Edition.
- 4. ASM Material Properties Handbook Titanium Alloys, ed. Rodney Boyer, Gerhard Welsch, E.W. Collings, 1994.

#### 3.2.2 Component Specifications

All components are specified and described on the descriptive drawings included in Appendix 1.3.

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#### **3.3** General Considerations

#### **3.3.1** Evaluation by Analysis

Evaluations by analysis are described in the section they apply to in this Safety Analysis Report or when applicable in the Test Plans contained in Appendix 2.12.

#### **3.3.2** Evaluation by Test

Evaluations by direct testing are documented in the Test Plans contained in Appendix 2.12 or are described in the section they apply to in this Safety Analysis Report.

#### 3.4 Thermal Evaluation Under Normal Conditions of Transport

#### 3.4.1 Heat and Cold

#### 3.4.1.1 Insolation and Decay Heat

This analysis determines the maximum surface temperature produced by solar heating of the transport package surface in accordance with 10 CFR 71.71(c)(1) and Table XI of IAEA TS-R-1.

The following design analysis calculates the steady state surface temperature of a cylindrical package subjected to insolation and self-heat. The analysis is based on recognized heat transfer theory and specifically, that the total heat input due to the self-heat of the radioactive contents and the insolation energy absorbed must balance the heat loss due to convection and emitted radiation from the package surface.



Figure 3.4.A: Model of Cylindrical Package for Heat Analysis

The package is evaluated in the orientation shown in Figure 3.4a, which also defines the overall package dimensions. In order to assure conservatism, the following assumptions are made:

a. Basic Input Parameters:

Max Content Activity, A = 345 Ci of Ir-192 (150 Ci x 2.3 for self absorption) The surface finish of the package is light silvery grade 304 stainless steel

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```
Length of Package, L = 0.33 m
Diameter of Package, \phi = 0.127 m
Stefan-Boltzmann constant, \sigma = 5.669 \times 10^{-8} W/m<sup>2</sup>K<sup>4</sup>
By Kirchhoff's Law Emissivity, \epsilon = Absorptivity, \alpha = 0.44
(Ref: Heat Transmission, 3rd Edition - M<sup>e</sup>Adams)
Ambient Temperature, T<sub>A</sub> = 311<sup>o</sup>K
Area of cylinder ends, A<sub>CE</sub> = 0.025 m<sup>2</sup>
Total Area of curved surfaces, A<sub>CS</sub> = 0.132 m<sup>2</sup>
Decay Heat Input Q<sub>DT</sub> = 3 W
```

The transport package is assumed to undergo free radiative heat transfer from the top and sides.

- b. The transport package is assumed to undergo free convective heat transfer from the top, sides and bottom.
- c. To maximize the temperature of the stainless steel cylinder surface temperature, the inside transport package faces are considered perfectly insulated so there is no conduction into the transport package. In use, the inside transport package will act as a heat sink during daylight hours and a heat source during the night, but this will be ignored for this calculation.
- d. The transport package is approximated as a right cylinder with dimensions, 5 inches (0.13 m) in diameter and 13 inches (0.33m) long (approximation of the solid length of the cylinder).
- e. The surfaces of the transport package are assumed to be solid. The faces are considered to be sufficiently thin so that no temperature gradients exist in the faces.
- f. The worst case decay heat load (3 Watts) is added to the solar heat input load.

The following heat calculations are based on the steady-state equilibrium relationship between the heat gained by the package and the heat lost.

Heat Input,  $Q_{IN}$  = Heat Output,  $Q_{OUT}$  in the steady-state.  $Q_{IN}$  = Solar Heat Input + Decay Heat  $Q_{OUT}$  = Heat loss by Radiation and Convection  $Q_{IE}$  = Heat input due to insolation falling on ends  $Q_{IC}$  = Heat input due to insolation on curved surfaces,

Solar Heat Input =  $\alpha(Q_{IE} + Q_{IC})$ , where  $\alpha$  is the absorptivity

The solar heat input is the combined solar heating of the top horizontal surface and the vertical side surface. The insolation data, provided in 10 CFR 71.71(c)(1), is found in Table 3.4.A.

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Table 5.4.A. Insolution Data			
Surface	Insolation for a 12 hour period (g-cal/cm <sup>2</sup> or W/m <sup>2</sup> )		
Horizontal base	None		
Other horizontal flat surfaces	800		
Non-horizontal flat surfaces	200		
Curved surfaces	400		

#### **Table 3.4.A: Insolation Data**

Practically all solid materials used in engineering are opaque to thermal radiation (even glass is only transparent to a fairly narrow range of wavelengths), and thermal radiation is in fact either reflected or absorbed within a very shallow depth of matter. Thus for solids it is possible to neglect transmissivity and write:

reflectivity,  $\rho$  + absorptivity,  $\alpha = 1$ 

i.e., the sum of the radiation reflected and absorbed by the material is equal to the total incident energy. Since the reflected energy does not contribute to the heat energy contained within the system, or package, it is not necessary to consider it in the analysis. However, the absorptivity of the material is the fraction of the total incident energy entering the system, which in this case is the heat input due to insolation.

Heat input due to insolation falling on ends,  $Q_{IE} = 200 \text{ W/m}^2 \times A_{CE} = 5 \text{ W}$ Heat input due to insolation on curved surfaces,  $Q_{IC} = 400 \text{ W/m}^2 \times A_{CS} = 52.8 \text{ W}$ 

In the case of a cylindrical package standing on the ground, the top surface can radiate freely to the surroundings assumed to be effectively at ambient temperature. For the vertical surface, the upper 90° of azimuth can radiate freely to the surrounding air in the same way as the top surfaces. However, some radiation emitted in the lower 90° will be intercepted by the ground and vice versa. Owing to the complex nature of radiation interchange, and allowing for this asymmetrical characteristic, a geometrical factor g is assumed in the following analysis.

For curved surfaces, $g_c =$	0.5
For vertical surfaces, $g_s =$	0.5

Radiation heat transfer from curved surfaces,

$$Q_{RC} = g_{c} \sigma \epsilon A_{CS} \{ T_{W}^{4} - T_{A}^{4} \} = 1.54 \times 10^{-9} \{ T_{W}^{4} - T_{A}^{4} \}$$

Radiation heat transfer from end surface,

 $Q_{RE} = g_s \sigma \epsilon A_{CE} \{ T_W^4 - T_A^4 \} = 3.12 \times 10^{-10} \{ T_W^4 - T_A^4 \}$ 

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Heat transfer by convection is complex as it represents a dynamic process involving fluid flow. Newton introduced a quantity known as the "heat transfer coefficient" represented by the symbol, h. From Newton's Law of cooling due to heat loss by convection:

$$Q_{\rm C} = hA[T_{\rm W}-T_{\rm A}]$$

Consider the curved surface of the cylinder:

Cylindrical Surface Convection,  $Q_{CC} = H_C A_{CS}[T_W - T_A]$ 

Where the free convection coefficient,  $H_c = 1.32\{(1/\phi)^{1/4}(T_w-T_A)^{1/4}\}$  (Ref 1)

Therefore,  $Q_{CC} = 0.27 (T_W - T_A)^{5/4}$ 

Considering the vertical surfaces of the cylinder:

Vertical End Surface Convection,  $Q_{CE} = H_S A_{CE} \{T_W - T_A\}$ 

Where the free convection coefficient,  $H_s = 1.42\{(1/\phi)^{1/4}(T_w-T_A)^{1/4}\}$  (Ref. 1)

Therefore,  $Q_{CE} = 0.06 (T_W - T_A)^{1.25}$ 

Total Heat Input,  $Q_{IN} = \alpha(Q_{IE} + Q_{IC}) + Q_{DT} = 28.4 \text{ W}$ 

Total Heat Output,  $Q_{OUT} = (Q_{RC} + Q_{RE}) + (Q_{CC} + Q_{CE})$ 

28.4 W =  $1.86 \times 10^{-9} \{T_w^4 - (311)^4\} + 3.34 \times 10^{-1} (T_w - (311))^{1.25}$ 

Iteration of this relationship yields a maximum wall temperature  $(T_w)$  of 65.4°C (149.7°F). This temperature would constitute the most onerous Normal Transport thermal condition. Based on the package materials of construction, this temperature will not be sufficient to adversely affect the package containment or shielding integrity since the melting temperatures of all safety critical components are well above this temperature. It is therefore concluded that the Model 880 Series transport package will maintain its structural integrity and shielding effectiveness under the normal transport heat condition.

#### 3.4.1.2 Still Air (shaded) Decay Heating

This analysis calculates the maximum surface temperature of the Model 880 Series Transport package in the shade (i.e., no insolation effects), assuming an ambient temperature of  $38^{\circ}$ C (100°F), per 10 CFR 71.43(g).

The same assumptions from Section 3.4.1.1 are used. The following heat calculations are based on the steady-state equilibrium relationship between the heat gained by the package and the heat lost.

December 2015 - Revision 10 Page 3-7 Heat Input,  $Q_{IN}$  = Heat Output,  $Q_{OUT}$  and  $Q_{IN}$  = Decay Heat = 3 Watts

 $Q_{OUT}$  = Heat loss by Convection

Heat transfer by convection is complex as it represents a dynamic process involving fluid flow. Newton introduced a quantity known as the "heat transfer coefficient" represented by the symbol, h. From Newton's Law of cooling due to heat loss by convection:

$$Q_{\rm C} = hA[T_{\rm W}-T_{\rm A}]({\rm W})$$

Considering the curved surface of the cylinder:

Cylindrical Surface Convection,  $Q_{CC} = H_C A_{CS} [T_W - T_A]$ 

Where the free convection coefficient,  $H_C = 1.32\{(1/\phi)^{1/4}(T_W-T_A)^{1/4}\}$ (Ref. 1 Section 3.4.1.2)

Therefore, 
$$Q_{CC} = 0.27 (T_W - T_A)^{1.25}$$

Considering the vertical surfaces of the cylinder:

Vertical End Surface Convection,  $Q_{CE} = H_S A_{CE} \{T_W - T_A\}$ 

Where the free convection coefficient,  $H_s = 1.42\{(1/\phi)^{1/4}(T_w-T_A)^{1/4}\}$ (Ref. 1 Section 3.4.1.2)

Therefore, 
$$Q_{CE} = 0.06 \times (T_W - T_A)^{1.25}$$

Total Heat Input,  $Q_{IN} = Q_{DT} = 3 \text{ W}$ 

Total Heat Output,  $Q_{OUT} = (Q_{CC} + Q_{CE}) = 3.34 \times 10^{-1} (T_W - T_A)^{1.25}$ 

Since Heat Input,  $Q_{IN}$  = Heat Output,  $Q_{OUT}$ , in the steady state.

$$3 \text{ W} = 3.34 \times 10^{-1} (T_{W} - T_{A})^{1.25}$$

Solving for  $T_W$ ,  $T_W = T_A + [3/(3.34 \times 10^{-1})]^{0.8} = 320^{\circ}K$ 

Therefore, a maximum wall temperature ( $T_w$ ) of 47°C (117°F), which is less than the maximum 50°C (122°F) allowed by 10 CFR 71.43(g).

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#### 3.4.1.3 Cold Effected Materials

An ambient air temperature of -40 F in still air and shade has no effect on the safety of the package. The safety materials: stainless steel, titanium, tungsten and depleted uranium retain their mechanical properties at this temperature. Thus, it is concluded that the Model 880 transport package will withstand the normal transport cold condition.

#### 3.4.1.4 Model 880 Series Series Type B(U) Source Capsule Thermal Analysis

This analysis demonstrates that the pressure inside the Model 880 Series source capsule, when subjected to the Hypothetical Accident Conditions of Transport thermal test, does not exceed the pressure which corresponds to the minimum yield strength at the thermal test temperature.

The source capsules used in the 880 Series are all special form tested and approved. The thermal test for special form capsules involves heating the capsules at 800°C for at least 10 minutes and allowing the capsules to cool afterwards. Test capsules are tested for leak tightness after this test and must pass intact in order to achieve special form status.

Special form capsules are also brought up to the 800°C temperature and allowed to cool prior to integrity testing. The special form capsules serve as the primary containment for the radioactive material and they demonstrate their ability to retain integrity at 800°C. Therefore it is concluded that the container and contents meet the requirements of this section.

#### 3.4.2 Temperatures Resulting in Maximum Thermal Stresses

The temperature and pressure variations described in Sections 3.4.1 and 3.4.3 will not adversely affect the transport package during normal transport since the melting temperatures of all safety critical components are well above these temperatures and the package will experience no pressures sufficient to cause package failure. It its therefore concluded that the Model 880 Series transport packages will maintain their structural integrity and shielding effectiveness under the normal transport thermal stress conditions.

#### 3.4.3 Maximum Normal Operating Pressure

All 880 Series components are vented to the atmosphere. As such, pressure will not build up in the packages during Normal Transport conditions. Containers will exhibit a pressure differential of 0 psi as they are vented to the atmosphere with no means for creating a pressure differential. No other contributing gas sources are present.

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#### 3.5 Thermal Evaluation Under Hypothetical Accident Conditions

#### 3.5.1 Initial Conditions

The thermal test was not performed. Rather, an assessment was performed to demonstrate that the thermal test would not create sufficient additional damage to the package that would cause it to fail final profile criteria.

Consideration of the principle materials of manufacture and their melting points indicates that they would not fail and shielding integrity would not be significantly degraded. (See Table 2.2.A)

Damage to the outer containment, increasing the potential for oxygen ingress to the shield, by a build up of pressure within the assembly through the pyrolization of the foam, or expansion of a trapped volume of air is not possible. The package is vented to atmosphere through both the front and rear end plates. These vents will relieve any internal generation or expansion of gases created by the elevated temperatures.

Damage incurred during the drop testing (4 foot, 30 foot and puncture) was minimal, consisting of insignificant deformation of the shell, lock mounting block and dust cover, slight bowing of the end plates and loss of two lock plate bolts. None of the damage increased, or created any new, significant pathways for the ingress of oxygen. Oxygen ingress has been shown empirically to be the primary contributing factor in the oxidation of depleted uranium shields during thermal testing (see Section 2.7.4.5.b).

#### 3.5.2 Fire Test Conditions

Without the possibility of gross oxidation, and subsequent destruction of the shield, thermal failure is then predicated on mechanical degradation of the packages' support structure. The Model 880 is predominately of welded stainless steel construction. A similar type of construction was analyzed for the Model 865 (Certificate of Compliance number 9165). The thermal analysis for the Model 865 is part of the documentation referenced for that package under the USNRC Certificate of Compliance USA/9165/B(U). It showed that the thermal gradients that occur during temperature ramp-up (especially within the first 3 minutes) do not create undue stresses on the structure of the device (~4-5% strain).

In addition, the effect of structural yielding under self-weight at temperature caused by the degradation of mechanical properties of the materials of construction was insignificant. Areas examined were:

- a. Tear-out of the shield support pin from the support bracket with the device in a vertical position (see Section 2.7.4.5.c(1)).
- b. Cracking of the depleted uranium (DU) around the titanium support pin due to differential expansion (see Section 2.7.4.5.c(2)).
- c. De-attachment of the rear lock assembly due to failure of the three- (3) remaining security screws (see Section 2.7.4.5.c(3)).

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Based on the previous empirical data and analyses, we conclude that oxidation of the shield will not occur, the structural integrity of the package will remain intact and the containment of the source will not be affected. As such, the Model 880 would pass the thermal test without exceeding the final profile criteria.

#### 3.5.3 Maximum Temperatures and Pressure

See Sections 3.1.3 and 3.1.4. All 880 Series components are vented to the atmosphere. The packages are vented to atmosphere through both the front and rear end plates. These vents will relieve any internal generation or expansion of gases created by the elevated temperatures. As such, pressure will not build up in the packages during Hypothetical Accident Transport conditions. Containers will exhibit a pressure differential of 0 psi as they are vented to the atmosphere with no means for creating a pressure differential. No other contributing gas sources are present.

#### 3.5.4 Temperatures Resulting in Maximum Thermal Stresses

The temperature and pressure variations described in Sections 3.4.1 and 3.4.3 will not adversely affect the transport package during normal transport since the melting temperatures of all safety critical components are well above these temperatures and the package will experience no pressures sufficient to cause package failure. It is therefore concluded that the Model 880 Series transport package will maintain its structural integrity and shielding effectiveness under the hypothetical accident condition transport thermal stress conditions.

#### 3.5.5 Fuel/Cladding Temperatures for Spent Nuclear Fuel

Not applicable. This package is not used for transport of spent nuclear fuel.

#### 3.5.6 Accident Conditions for Fissile Material Packages for Air Transport

Not applicable. This package is not used for transport of Type B quantities of fissile material.

#### 3.6 Appendix

Not Applicable.

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#### Section 4 – CONTAINMENT

#### 4.1 Description of the Containment System

The containment system consists of the Model 880 Series transport package and the radioactive source capsule. This source capsule shall be qualified as Special Form radioactive material under 49 CFR 173 and IAEA TS-R-1.

#### 4.1.1 Special Requirements for Damaged Spent Nuclear Fuel

Not applicable. This package is not used for the transport of spent nuclear fuel.

#### 4.2 Containment Under Normal Conditions of Transport

As demonstrated in the Test Plan Reports and supported by assessments when applicable (Section 2.12), performance of the normal conditions of transport testing caused no breach of the source capsules contained in the package. The source capsules used in conjunction with the transport package have satisfied the requirements for the special form radioactive material as prescribed in 10 CFR 71.75, 49 CFR 173.469 and IAEA TS-R-1. There will be no release of radioactive material under the Normal Conditions of Transport.

The normal conditions of transport criteria listed in 10 CFR 71.71 will result in no loss of transport package containment as prescribed in 10 CFR 71.51(a)(1). This conclusion is based on information presented in Sections 2 and 3.

#### 4.3 Containment Under Hypothetical Accident Condition

The hypothetical accident conditions outlined in 10 CFR 71.73 will result in no loss of transport package containment. This conclusion is based on information presented in Section 2.7 and Section 3.5 which show that the transport package meets the containment requirements of 10 CFR 71.51(a)(2).

#### 4.4 Leakage Rate Tests for Type B Packages

The primary containment for the radioactive material in the Model 880 Series Transport Packages are the radioactive source capsules. All source capsules authorized for Type B transport in the Model 880 Series are certified as special form radioactive material under 10 CFR Part 71, 49 CFR Part 173 and IAEA TS-R-1. After manufacture, and again once every six months thereafter prior to transport, the source capsules are leak tested in accordance with ISO9978:1992(E) (or more recent editions) to ensure that containment of the source does not allow release of more than 0.005  $\mu$ Ci of radioactive material. These fabrication and periodic tests ensure that contamination release from the package does not exceed the regulatory limits.

Reference ISO9978:1992(E) – Radiation Protection – Sealed Radioactive Sources – Leakage Test Methods.

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#### 4.5 Appendix

i.

Not applicable.

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#### Section 5 - SHIELDING EVALUATION

#### 5.1 Description of Shielding Design

#### 5.1.1 Design Features

The principal shielding in the Model 880 Series transport package is the depleted uranium shield assembly. The shielding is cast as one piece and is essentially enclosed by stainless steel. Dimensional information for the individual shield containers is contained in the shield drawings (See Appendix 1.3).

#### 5.1.2 Summary Table of Maximum Radiation Levels

Tables 5.1.A and 5.1.B include worst case radiation profile data obtained from the 880 Series packages that were tested to the Normal and Hypothetical Accident Conditions of Transport under Test Plans 108 and 186 (see Section 2.12). Tables 5.1.F and 5.1.G include worst case radiation profile data obtained from the 880SC packages that were tested to the Normal and Hypothetical Accident Conditions of Transport under Test Plans 206 (see Section 2.12).

#### Table 5.1.A: Model 880 Delta sn TP186A Summary Table of External Radiation Levels Extrapolated to Capacity of 150 Ci Ir-192 (Non-Exclusive Use) and Hypothetical Accident Transport Condition Testing<sup>3</sup>

Transport Condition Tosting							
Normal Conditions of	Package Surface mSv/h (mrem/hr) <sup>2</sup>			1 Meter from Package Surface mSv/h			
Transport					(mrem/h) <sup>2</sup>		
Radiation	Тор	Side	Bottom	Тор	Side	Bottom	
Gamma	1.68 (168)	1.83 (183)	0.98 (98)	0.008 (0.8)	0.014 (0.14)	0.010 (0.10)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	1.68 (168)	1.83 (183)	0.98 (98)	0.008 (0.8)	0.014 (0.14)	0.010 (0.10)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^{1}$	$0.1(10)^{1}$	$0.1(10)^{1}$	
Paragraphs 530 and							
531 of TS-R-1 Limit							
Hypothetical Accident	Conditions						
Gamma			0.008 (0.8)	0.014 (0.14)	0.010 (0.10)		
Neutron			NA	NA	NA		
Total				0.008 (0.8)	0.014 (0.14)	0.010 (0.10)	
10 CFR 71.51(a)(2) or P	aragraph 656	(b)(ii)(I) of T	S-R-1 Limit	10 (1000)	10 (1000)	10 (1000)	

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Based on the cylindrical geometry of this package, the "top" is considered to be the front as profiled, the "bottom" is considered to be the back as profiled and all other surfaces are considered part of the "side" of the package. <sup>3</sup>Survey results after testing were obtained from the Model 880 Delta without the optional jacket. This produced dose rates which would be higher than the Model 880 Delta if it had the optional jacket attached.

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	Package (or Freight Container) Surface mSv/h				2 Meters from Outer Vehicle Surface mSv/h				
	(mrem/h)			(mrem/h)					
Normal Conditions of	Тор	Side	Bott	tom	] Te	op	Si	de	Bottom
Transport									
Gamma	1.68 (168)	1.83 (183)	0.98	(98)	0.008	(0.8)	0.014	(0.14)	0.010 (0.10)
Neutron	NA	NA	N.	A	N	A	N	A	NA
Total	1.68 (168)	1.83 (183)	0.98	(98)	0.008	(0.8)	0.014	(0.14)	0.010 (0.10)
10 CFR 71.47(b) or	$10(1000)^2$	$10(1000)^2$	10 (10	$(000)^2$	0.1	(10)	0.1	(10)	0.1 (10)
Paragraphy 572 of TS-									
R-1 Limit									
Vehicle Surface mSv/h (mrem/h)					Occupied Position mSv/h (mrem/hr)				
Gamma	< 0.008 (0.8)	< 0.014 (1.4)	< 0.010	0 (0.1)			≤ 0.02	$(2)^{3}$	
Neutron	NA	NA	N.	A			NA	A	
Total	< 0.008 (0.8)	< 0.014 (1.4)	< 0.010	0(0.1)			≤ 0.02	$(2)^{3}$	
10 CFR 71.47(b) or	2 (200)	2 (200)	2 (2	00)			0.02	(2)	
Paragraphy 572 of TS-									
R-1 Limit									
Hypothetical Accident	Conditions			1 Met	er from ]	Package	Surface	mSv/h	(mrem/hr)
Gamma			0.008	08 (0.8) 0.014 (0.14) 0.010 (0.10)		010 (0.10)			
Neutron				N	NA NA NA		NA		
Total				0.00	8 (0.8)	0.014 (	(0.14)	0.0	010 (0.10)
10 CFR 71.51(a)(2) or P	aragraph 656(b)	(ii)(I) of TS-R-1	Limit	10 (	10 (1000) 10 (1000) 10 (1000)		0 (1000)		

Table 5.1.B: Model Delta sn TP186A Summary Table of External Radia	ation Levels
Extrapolated to Capacity of 150 Ci Ir-192 (Exclusive Use) <sup>1</sup>	

<sup>1</sup>For packages transported by roadway, railway and sea.

<sup>2</sup>For packages in closed vehicles, otherwise, 2 (200).

<sup>3</sup>Confirmed at time of vehicle loading prior to shipment.

Tables 5.1.C and 5.1.D include radiation profile data used to demonstrate that the Model 880 Delta and 880 Elite package configurations will meet the external radiation level requirements for non-exclusive use transport when loaded to capacity for Se-75. Based on comparisons of radiation profiles for Ir-192 after hypothetical accident testing and relative photon energy outputs for Ir-192 and Se-75, it is assessed that radiation levels from Se-75 will be essentially unchanged after undergoing the hypothetical accident condition testing. By assessment, since the Model 880 Sigma shield has greater shielding than the Model 880 Elite shield, the Model 880 Sigma package configuration will also meet the external radiation level requirements for non-exclusive use when loaded to capacity for Se-75.

Table 5.1.E includes radiation profile data used to demonstrate that the Model 880 Elite package configuration will meet the external radiation level requirements for non-exclusive use transport when loaded to capacity for Ir-192.

Table 5.1.H includes radiation profile data used to demonstrate that the Model 880SC package configuration will meet the external radiation level requirements for non-exclusive use transport when loaded to capacity for Se-75. Based on comparisons of radiation profiles for Ir-192 after hypothetical accident testing and relative photon energy outputs for Ir-192 and Se-75, it is assessed that radiation levels from Se-75 will be essentially unchanged after undergoing the hypothetical accident condition testing.

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## Table 5.1.C: Model 880 Delta sn D2375 Summary Table of External Radiation Levels Extrapolated to Capacity of 150 Ci Se-75 (Non-Exclusive Use)<sup>2</sup>

	Package Surface mSv/h (mrem/h)			1 Meter from Package Surface mSv/h			
				(mrem/h)			
Normal Conditions of	Тор	Side	Bottom	Тор	Side	Bottom	
Transport							
Gamma	0.13 (13)	0.13 (13)	0.13 (13)	0.01 (1.0)	0.01 (1.0)	0.01 (1.0)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	0.13 (13)	0.13 (13)	0.13 (13)	0.01 (1.0)	0.01 (1.0)	0.01 (1.0)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^{1}$	$0.1(10)^{1}$	$0.1(10)^{1}$	
Paragraphs 530 and 531							
of TS-R-1 Limit				, , 			
Hypothetical Accident Conditions <sup>3</sup>							
Gamma				~0.01 (1.0)	~0.01 (1.0)	~0.01 (1.0)	
Neutron				NA	NA	NA	
Total				~0.01 (1.0)	~0.01 (1.0)	~0.01 (1.0)	
10 CFR 71.51(a)(2) or Para	agraph 656(b)(ii	)(I) of TS-R-1	Limit	10 (1000)	10 (1000)	10 (1000)	

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Normal Condition values obtained by direct measurement corrected for capacity and detector geometry.

<sup>3</sup>Based on comparisons of radiation profiles for Ir-192 after hypothetical accident testing, it is assessed that radiation levels from Se-75 will be essentially unchanged after undergoing the hypothetical accident condition testing.

## Table 5.1.D: Model 880 Elite sn E1060 Summary Table of External Radiation Levels Extrapolated to Capacity of 150 Ci Se-75 (Non-Exclusive Use)<sup>2</sup>

	Package S	urface μSv/h (	mrem/h)	1 Meter from Package Surface µSv/h			
		·		(mrem/h)			
Normal Conditions of	Тор	Side Bottom		Тор	Side	Bottom	
Transport							
Gamma	0.13 (13)	0.13 (13)	0.13 (13)	0.01 (1.0)	0.01 (1.0)	0.01 (1.0)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	0.13 (13)	0.13 (13)	0.13 (13)	0.01 (1.0)	0.01 (1.0)	0.01 (1.0)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^{1}$	$0.1(10)^{1}$	$0.1(10)^{1}$	
Paragraphs 530 and 531							
of TS-R-1 Limit							
Hypothetical Accident Co	onditions <sup>3</sup>						
Gamma	~0.01 (1.0)	~0.01 (1.0)	~0.01 (1.0)				
Neutron	NA	NA	NA				
Total	~0.01 (1.0)	~0.01 (1.0)	~0.01 (1.0)				
10 CFR 71.51(a)(2) or Par	10 (1000)	10 (1000)	10 (1000)				

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Normal Condition values obtained by direct measurement corrected for capacity and detector geometry.

<sup>3</sup>Based on comparisons of radiation profiles for Ir-192 after hypothetical accident testing, it is assessed that radiation levels from Se-75 will be essentially unchanged after undergoing the hypothetical accident condition testing.

## Table 5.1.E: Model 880 Elite sn E1060 Summary Table of External Radiation Levels Extrapolated to Capacity of 50 Ci Ir-192 (Non-Exclusive Use)<sup>2</sup>

	Package S	urface mSv/h (	(mrem/h)	1 Meter from Package Surface mSv/h (mrem/h)			
Normal Conditions of	Top Side Bottom		Тор	Side	Bottom		
Transport							
Gamma	1.35 (135)	1.64 (164)	1.43 (143)	0.008 (0.8)	0.017 (1.7)	0.009 (0.9)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	1.35 (135)	1.64 (164)	1.43 (143)	0.008 (0.8)	0.017 (1.7)	0.009 (0.9)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^{1}$	$0.1(10)^1$	$0.1(10)^1$	
Paragraphs 530 and 531							
of TS-R-1 Limit							
Hypothetical Accident Co		•	·				
Gamma	0.008 (0.8)	0.017 (1.7)	0.009 (0.9)				
Neutron	NA	NA	NA				
Total	0.008 (0.8)	0.017 (1.7)	0.009 (0.9)				
10 CFR 71.51(a)(2) or Par	10 (1000)	10 (1000)	10 (1000)				

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Normal Condition values obtained by direct measurement corrected for capacity and detector geometry.

<sup>3</sup>Based on comparisons of radiation profiles for the 880 Delta when loaded with Ir-192 after hypothetical accident testing, it is assessed that radiation levels from the 880 Elite for Ir-192 will be essentially unchanged after undergoing the hypothetical accident condition testing.

# Table 5.1.F: Model 880SC sn TP206B Summary Table of External Radiation LevelsExtrapolated to Capacity of 150 Ci Ir-192 (Non-Exclusive Use) and Hypothetical AccidentTransport Condition Testing<sup>3</sup>

Normal Conditions of Transport	Package Surface mSv/h (mrem/hr) <sup>2</sup>			1 Meter from Package Surface mSv/h (mrem/h) <sup>2</sup>			
Radiation	Тор	Side	Bottom	Тор	Side	Bottom	
Gamma	1.96 (196)	1.82 (182)	0.99 (99)	0.011 (1.1)	0.012 (1.2)	0.026 (2.6)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	1.96 (196)	1.82 (182)	0.99 (99)	0.011 (1.1)	0.012 (1.2)	0.026 (2.6)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^1$	$0.1(10)^1$	$0.1(10)^{1}$	
Paragraphs 530 and							
531 of TS-R-1 Limit							
<b>Hypothetical Accident</b>	Conditions						
Gamma				0.011 (1.1)	0.012 (1.2)	0.026 (2.6)	
Neutron	NA	NA	NA				
Total	0.011 (1.1)	0.012 (1.2)	0.026 (2.6)				
10 CFR 71.51(a)(2) or P	10 (1000)	10 (1000)	10 (1000)				

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Based on the cylindrical geometry of this package, the "top" is considered to be the front as profiled, the "bottom" is considered to be the back as profiled and all other surfaces are considered part of the "side" of the package. <sup>3</sup>Survey results after testing were obtained from the Model 880SC without the optional jacket. This produced dose rates which would be higher than the Model 880SC if it had the optional jacket attached.

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	Package (or Freight Container) Surface mSv/h				2 Meters from Outer Vehicle Surface mSv/h				
	(mrem/h)				(mrem/h)				
Normal Conditions of	Тор	Side	Bot	tom	om Top		Si	de	Bottom
Transport					-				
Gamma	1.96 (196)	1.82 (182)	0.99	(99)	< 0.01	1 (1.1)	< 0.012	2 (1.2)	<0.026 (2.6)
Neutron	NA	NA	N	A	N	A	N	A	NA
Total	1.96 (196)	1.82 (182)	0.99	(99)	< 0.01	l (1.1)	<0.012	2 (1.2)	<0.026 (2.6)
10 CFR 71.47(b) or	$10(1000)^2$	$10(1000)^2$	10 (1	$(0.1(10))^2$ $(0.1(10))$		(10)	0.1	(10)	0.1 (10)
Paragraphs 572 of TS-			l						
R-1 Limit									
	Vehicle Surface mSv/h (mrem/h)				Occupied Position mSv/h (mrem/hr)				
Gamma	< 0.011 (1.1)	$< 0.011 (1.1)   < 0.012 (1.2)   < 0.026 (2.6)   \le 0.02 (2)^3$							
Neutron	NA	NA	N	A	NA				
Total	< 0.011 (1.1)	< 0.012 (1.2)	< 0.02	5 (2.6)	$\leq 0.02 (2)^3$				
10 CFR 71.47(b) or	2 (200)	2 (200)	2 (2	00)	0.02 (2)				
Paragraph 572 of TS-									
R-1 Limit									
Hypothetical Accident Conditions				1 Met	er from Package Surface mSv/h (mrem/hr)				
Gamma	Jamma				(1.1) 0.012 (1.2) 0.026 (		026 (2.6)		
Neutron				<u> </u>	JA NA			NA	
Total				0.01	(1.1) 0.012 (1.2) 0.026 (2.6		026 (2.6)		
10 CFR 71.51(a)(2) or Paragraph 656(b)(ii)(I) of TS-R-1 Limit				10 (	1000)	000) 10 (1000) 10 (1000		0 (1000)	

## Table 5.1.G: Model 880SC sn TP206B Summary Table of External Radiation Levels Extrapolated to Capacity of 150 Ci Ir-192 (Exclusive Use)<sup>1</sup>

<sup>1</sup>For packages transported by roadway, railway and sea.

<sup>2</sup>For packages in closed vehicles, otherwise, 2 (200).

<sup>3</sup>Confirmed at time of vehicle loading prior to shipment.

## Table 5.1.H: Model 880SC Summary Table of External Radiation Levels Extrapolated to Capacity of 150 Ci Se-75 (Non-Exclusive Use)<sup>2</sup>

	Package Surface mSv/h (mrem/h)			1 Meter from Package Surface mSv/h (mrem/h)			
Normal Conditions of Transport	Тор	Side Bottom		Тор	Side	Bottom	
Gamma	<1.96 (196)	<1.82 (182)	<0.99 (99)	<0.011 (1.1)	<0.012 (1.2)	<0.026 (2.6)	
Neutron	NA	NA	NA	NA	NA	NA	
Total	<1.96 (196)	<1.82 (182)	<0.99 (99)	< 0.011 (1.1)	< 0.012 (1.2)	<0.026 (2.6)	
10 CFR 71.47(a) or	2 (200)	2 (200)	2 (200)	$0.1(10)^{1}$	$0.1(10)^{1}$	$0.1(10)^{1}$	
Paragraphs 530 and 531							
of TS-R-1 Limit							
Hypothetical Accident C							
Gamma	< 0.011 (1.1)	< 0.012 (1.2)	<0.026 (2.6)				
Neutron	NA	NA	NA				
Total	< 0.011 (1.1)	< 0.012 (1.2)	< 0.026 (2.6)				
10 CFR 71.51(a)(2) or Par	10 (1000)	10 (1000)	10 (1000)				

<sup>1</sup>Transport Index may not exceed 10.

<sup>2</sup>Normal Condition values obtained by direct measurement corrected for capacity and detector geometry.

<sup>3</sup>Based on comparisons of radiation profiles for Ir-192 after hypothetical accident testing, it is assessed that radiation levels from Se-75 will be essentially unchanged after undergoing the hypothetical accident condition testing.

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#### 5.2 Source Specification

#### 5.2.1 Gamma Source

The gamma sources allowed for transport in the Model 880 Series transport package are specified in Sections 1.2.2 and 2.10.

#### 5.2.2 Neutron Source

Not applicable. The Model 880 Series transport packages are not used for the transportation of neutron emitting sources.

#### 5.3 Shielding Model

#### 5.3.1 Configuration of Source and Shielding

A shielding model was not used as the primary justification for these packages. Shielding justification was based on direct measurement and a comparison of relative photon energy output per Ci between Ir-192 and Se-75 to justify Se-75 capacities in some cases. Since the 880 Delta and 880SC testing results showed that an insignificant change had occurred in the radiation profiles, all isotopes in all other versions of the Model 880 Series packages were considered acceptable.

#### 5.3.2 Material Properties

Not applicable. A shielding model was not used as the primary justification for these packages. Shielding justification was based on direct measurement using Ir-192 and Se-75 and comparison of relative photon shielding effectiveness between Ir-192 and Se-75. Additional package configurations were justified based on test results of the Model 880 Delta and 880SC style packages.

#### 5.4 Shielding Evaluation

#### 5.4.1 Methods

Shielding justification was based on direct measurement and assessment. Radiation profiles have not been performed for the Model 880 Sigma, however, the shield design is identical to the Model 880 Delta. This design is capable of producing shields that can adequately shield 150 Ci of Ir-192 to within the regulatory dose limits. Due to variances in the shield manufacturing process, some shields are produced with a slightly lower shielding capacity. Shields which demonstrate a capacity of 130 Ci of Ir-192, based on device profiles prior to final acceptance and shipment, are distributed as Model 880 Sigma devices.

All packages are profiled prior to final acceptance and shipment. This profile takes into account the maximum capacity and detector geometry. Any package not meeting the required dose rates is rejected.

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If the optional jacket is used, it will further reduce surface dose rates on some areas of the package. As such, the use of the jacket will have no detrimental impact on dose rates.

#### 5.4.2 Input and Output Data

Radiation measurements included in this Section were adjusted to the maximum activity capacity for the package (e.g., activity correction factor) and the surface measurements were also adjusted to correct for off-set of the survey meter probe from the true surface of the package.

Activity correction factors (CF<sub>A</sub>) were obtained by using the following relationship:

 $CF_{A} = \frac{MaximumPackageActivityCapacity(A_{C})}{Actual \operatorname{Pr}ofileActivity}(A_{P})}$ 

For Example, if  $A_p = 135 Ci$  and  $A_c = 150 Ci$ , then

$$CF_A = \frac{150Ci}{135Ci} = 1.1$$

Therefore all original surface and 1 meter profile measurements would be multiplied by a factor of 1.1 for a package profiled using 135 Ci and a package capacity of 150 Ci.

Radiation measurements at the surface of the container were also adjusted to compensate for the off-set of the survey meter probe from the true surface of the package.

Surface correction factors (SCF) were obtained by using the following relationship:

$$SCF = \sqrt{\frac{d_2^2}{d_1^2}}$$
 where  $d_1$  and  $d_2$  are determined as shown in Figure 5.4.A.

For Example, if  $d_1 = 9$  inches and  $d_2 = 10$  inches, then

$$SCF = \sqrt{\frac{(10\,inches)^2}{(9\,inches)^2}} = 1.11$$

Subsequent evaluation of the SCF revealed that the use of the inverse square law introduces an error when the material of the shield contains a heavy element such as tungsten, uranium or lead. When heavy shields are involved there is a build-up of Compton-scattered photons and X-rays which causes scattered radiation to emanate from everywhere within the shield and not just from the source in the center. Under these circumstances, the inverse square law relationship between dose rate and distance overestimates the actual dose rate on the surface of the device.
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Experimental measurement using TLDs have demonstrated that the SCF for devices using heavy element shielding varies more accurately as follows:

$$SCF = \sqrt{\frac{d_3}{d_1}}$$
 where  $d_1$  and  $d_3$  are determined as shown in Figure 5.a.

For Example, if  $d_1 = 9$  inches and  $d_3 = 10$  inches, then

$$SCF = \sqrt{\frac{(10 \text{ inches})}{(9 \text{ inches})}} = 1.05$$

Therefore in the example shown, all original surface profile measurements located along the side of the package shown in Figure 5.4.A would also be multiplied by a factor to account for surface correction of the detector to the package surface. Different SCF's would be calculated for the any dimension of the container where the minimum distance from the center of the activity to the center of the radiation probe is different.





- $d_2 =$  distance from activity center to surface of container plus radius of the survey meter probe.
- $d_3 =$  distance from activity center to back of the probe.



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The radiation profile data showed no increase in radiation dose after testing beyond normal measurement variations. All test specimens met the regulatory requirements.

## 5.4.3 Flux-to-Dose-Rate Conversion

Not applicable. Flux rates were not used to convert to dose rates in any shielding evaluations.

## 5.4.4 External Radiation Levels

Radiation surveys for all 880 Series configurations showed maximum surface and 1 meter radiation levels from the transport packages within regulatory limits. Radiation surveys of 880 Series transport packages after undergoing normal and accident condition transport testing were also well within the regulatory limits.

## 5.5 Appendix

Not Applicable.

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# Section 6 - CRITICALITY EVALUATION

All parts of this section are not applicable. The Model 880 Series transport packages are not used for shipment of Type B quantities of fissile material.

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# Section 7 – Package Operations

Operation of the Model 880 Series transport packages must be in accordance with the operating instructions supplied with the transport package, per 10 CFR 71.87 and 71.89.

## 7.1 Package Loading

## 7.1.1 Preparation for Loading

The Model 880 Series transport packages must be loaded and closed in accordance with procedures that, at a minimum, include the requirements specified in this section. Shipment of Type B quantities of radioactive material are authorized for sources specified in Section 7.1.1.1. Maintenance and inspection of these packages is in accordance with the requirements specified in Section 7.1.1.2.

## 7.1.1.1 Authorized Package Contents

The Model 880 Series transport packages are designed for use with a special form source capsules as approved under a U.S. Department of Transportation special form certification. The approved isotopes and maximum package activity limits is shown in Table 7.1.A. Details of encapsulation as well as chemical and physical form of the radioactive material will comply with specifications approved under U.S. Department of Transportation or other Competent Authority special form certifications.

Model	Nuclide	Form <sup>1</sup>	Maximum	Maximum	Maximum	Maximum	Maximum
			Capacity <sup>2</sup>	DU	Weight	Weight	Weight With
				Weight	Without	With Jacket	Jacket
					Jacket	(Version 1)	(Version 2)
880	Ir-192	Special Form	150 Ci	34.4 lbs	46 lbs	52 lbs	55 lbs
Delta	Se-75	Special Form	150 Ci	(15.6 kg)	(21 kg)	(24 kg)	(25 kg)
880	Ir-192	Special Form	130 Ci	24.4 lbs	16 lbs	52 lba	55 lba
Sigma	Se-75	Special Form	150 Ci	(15.6 kg)	(21 kg)	(24 kg)	(25 kg)
880	Ir-192	Special Form	50 Ci	25 lbs	37 lbs	42 lbs	45 lbs
Elite	Se-75	Special Form	150 Ci	(11 kg)	(17 kg)	(19 kg)	(20 kg)
8805C	Ir-192	Special Form	150 Ci	34.4 lbs	46 lbs	52 lbs	NA
000SC	Se-75	Special Form	150 Ci	(15.6 kg)	(21 kg)	(24 kg)	NA

 Table 7.1.A: Isotopes Permitted in the Model 880 Series

<sup>1</sup> Special Form is defined in 10 CFR 71, 49 CFR 173, and IAEA TS-R-1.

<sup>2</sup> Maximum Capacity Activity for Ir-192 is defined as output Curies as required in ANSI N432 and 10 CFR 34.20 and in line with TS-R-1 and Rulemaking by the USNRC and the USDOT published in the Federal Register on 26 January 2004

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#### 7.1.1.2 Packaging Maintenance and Inspection Prior to Loading

- a. Ensure all markings are legible.
- b. Inspect the container for signs of significant degradation. Ensure all welds are intact, the container is free of heavy rust and cracks/damage to the steel housing which breaches the container. If there is any evidence of bent or cracked welds contact QSA Global, Inc. prior to shipping.
- c. Assure all bolts and fasteners (hardware) required for assembly of the package and as specified on the drawings referenced on the Type B transport certificate are fit for use. Without removing the hardware by disassembly from the device, examine the visible external surfaces of the bolts/fasteners for any signs of fatigue cracking.
  - Note: A visual examination of the bolt/fastener thread condition is performed after removal from the exposure device as part of the Quarterly and Annual Maintenance inspections required for radiography devices under 10 CFR 34.31 or equivalent Agreement State regulations.

The bolts/fasteners must be replaced if they are no longer fit for use (e.g., threads stripped, unable to fully thread, signs of cracking, etc). Ensure the front port is properly secured. Ensure seal wire(s) are properly installed. Ensure any replacement hardware meets all applicable specifications listed on the drawings referenced on the Type B transport certificate.

d. If the container fails any of the inspections in steps 7.1.1.2.a-c, remove the container from use until it can be brought into compliance with the Type B certificate.

#### 7.1.2 Loading of Contents

# *NOTE:* These loading operations apply to "dry" loading only. None of the shield configurations for the Model 880 Series package are approved for wet loading.

- 7.1.2.1 Prior to transportation, ensure the package and its contents meet the following requirements:
  - a. The contents are authorized for use in the package.
  - b. The package condition has been inspected in accordance with Section 7.1.1.2.

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c. Ensure that the source is secured into place in the storage position after loading the 880 package in accordance with the applicable licensing provisions for the user's facility related to radioactive material handling.

#### 7.1.3 Preparation for Transport

- 7.1.3.1 Ensure that all conditions of the certificate of compliance are met.
- 7.1.3.2 Perform a contamination wipe of the outside surface of the package and ensure removable contamination does not exceed 0.0001  $\mu$ Ci when averaged over a wipe area of 300 cm<sup>2</sup>.
- 7.1.3.3 Survey all exterior surfaces of the package to assure that the radiation level does not exceed 200 mR/hr at the surface. Measure the radiation level at one meter from all exterior surfaces to assure that the radiation level is less than 10 mR/hr.
- 7.1.3.4 Ship the container according to the procedure for transporting radioactive material as established in 10 CFR 71.5 and 49 CFR 171-178.
- **NOTE:** The US Department of Transportation, in 49 CFR 173.22(c), requires each shipper of Type B quantities of radioactive material to provide prior notification to the consignee of the dates of shipment and expected arrival.

## 7.2 Package Unloading

#### 7.2.1 Receipt of Package from Carrier

- 7.2.1.1 The consignee of a transport package of radioactive material must make arrangements to receive the transport package when it is delivered. If the transport package is to be picked up at the carrier's terminal, 10 CFR 20.1906 requires that this be done expeditiously upon notification of its arrival.
- 7.2.1.2 Upon receipt of a transport package of radioactive material:
  - a. Survey the transport package with a survey meter as soon as possible, preferably at the time of pick-up and no more than three hours after it was received during normal working hours. Radiation levels should not exceed 200 mR/hr at the surface of the transport package, nor 10 mR/hr at a distance of 1 meter from the surface.
  - b. Record the actual radiation levels on the receiving report.
  - c. If the radiation levels exceed these limits, secure the container in a Restricted Area and notify the appropriate personnel in accordance with 10 CFR 20 or applicable Agreement State regulations.

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- d. Inspect the outer container for physical damage or leaking. If the package is damaged or leaking or it is suspected that the package may have leaked or been damaged, restrict access to the package. As soon as possible, contact the Radiation Safety Office to perform a full assessment of the package condition and take necessary follow-up actions.
- e. Record the radioisotope, activity, model number, and serial number of the source and the transport package model number and serial number.

#### 7.2.2 Receipt of Contents

- 7.2.2.1 Unload the package must be in accordance with the instructions supplied with the package per 10 CFR 71.89.
- 7.2.2.2 Unloading of the package must also be in accordance with applicable licensing provisions for the user's facility related to radioactive material handling.

#### 7.3 Preparation of Empty Package for Transport

In the following instructions, an *empty* transport package refers to a Model 880 Series transport package without an active source contained within the shielded container. To ship an empty transport package:

- **7.3.1.** For the 880 Delta, 880 Sigma or 880 Elite packages, perform the following procedure to confirm that there are no unauthorized sources within the container:
  - 7.3.1.1 Remove the authorized source assembly from the package in accordance with the instructions supplied with the package per 10 CFR 71.89.
  - **7.3.1.2** After removing the source and disconnecting the source assembly, attach the jumper (dummy connector without a serial number) to the male connector of the drive cable.
  - 7.3.1.3 Retract the jumper into the package and disconnect the controls.
  - 7.3.1.4 Insert the shipping cover, rotate the selector ring to the lock position, depress the plunger lock and remove the key.
  - 7.3.1.5 Remove the source identification tag from the package and keep it with the source.
- 7.3.2. To ship an empty 880SC package a second shipping plug assembly or dummy (inactive) A424-9 source wire DEMO assembly is required. If not available, contact QSA Global, Inc. to obtain an appropriate assembly before shipping an 880SC empty. Once the second assembly is obtained, perform the following:

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- 7.3.1.1 Remove the authorized source assembly from the package in accordance with the instructions supplied with the package per 10 CFR 71.89.
- 7.3.1.2 Insert a shipping plug assembly into one of the locking assemblies on the package until the lock engages.
- 7.3.1.3 Depress the key plunger lock and remove the key. Rotate the shipping cap to the closed position and secure in place with the spring plunger.
- **7.3.1.4** Repeat steps 7.3.1.2 and 7.3.1.3 for the other locking assembly on the package using another shipping plug assembly or a dummy (inactive) A424-9 source wire DEMO assembly.
- 7.3.1.5 Remove the source identification tag from the package and keep it with the source.
- 7.3.3 Assure that the levels of removable radioactive contamination on the outside surface of the transport package do not exceed 4 Bq/cm<sup>2</sup> (when averaged over 300 cm<sup>2</sup>).
- 7.3.4 When it is confirmed that the Model 880 Series transport package is empty, survey the device and prepare the transport package for shipment. Survey the assembled package to ensure the external surface radiation level does not exceed 5  $\mu$ Sv/hr.
- 7.3.5 Ship the container according to the procedure for transporting radioactive material as established in10 CFR 71.5.

#### 7.4 Other Operations

#### 7.4.1 Package Transportation By Consignor

Persons transporting the Model 880 Series transport package in their own conveyances should comply with the following:

- 7.4.1.1 For a conveyance and equipment used regularly for radioactive material transport, check to determine the level of contamination that may be present on these items. This contamination check is suggested if the package shows signs of damage upon receipt or during transport, or if a leak test on the special form source transported in the package exceeds the allowable limit of 185 Bq (0.005  $\mu$ Ci).
- 7.4.1.2 If contamination above 4 Bq/cm<sup>2</sup> (0.0001  $\mu$ Ci/cm<sup>2</sup>) based on wiping an area of 300 cm<sup>2</sup> is detected on any part of a conveyance or equipment used regularly for radioactive material transport, or if a radiation level exceeding 5  $\mu$ Sv/h (0.5 mR/hr) is detected on any conveyance or equipment surface, then remove the affected item from use until decontaminated or decayed to meets these limits.
- 7.4.1.3 Ensure the package is properly blocked and braced prior to transport to prevent movement within the conveyance during transport.

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#### 7.4.2 Emergency Response

In the event of a transport emergency or accident involving this package, follow the guidance contained in "2012 Emergency Response Guidebook: A Guidebook for First Responders During the Initial Phase of a Dangerous Goods/Hazardous Materials Incident", or equivalent guidance documentation.

Reference: "2012 Emergency Response Guidebook: A Guidebook for First Responders During the Initial Phase of a Dangerous Goods/Hazardous Materials Incident.

## 7.5 Appendix

Not Applicable.

# Section 8 - ACCEPTANCE TESTS AND MAINTENANCE PROGRAM

## 8.1 Acceptance Test

## 8.1.1 Visual Inspections and Measurements

- 8.1.1.1 Visually inspect each transport package component to be shipped to assure the following:
  - a. The transport package was assembled properly to the applicable drawing referenced on the Type B transport certificate.
  - b. Evaluate each shield container for shielding integrity when used in the applicable Model 880 Series assembly to ensure the transport dose rate requirements are met when the container is loaded to capacity.
  - c. All fasteners as required by the applicable drawings referenced on the Type B transport certificate are properly installed and secured.
  - d. The relevant labels are attached, contain the required information, and are marked in accordance with 10 CFR 20.1904, 10 CFR 40.13(c)(6)(i), 10 CFR 34, and 10 CFR 71 or equivalent Agreement State regulations.
- 8.1.1.2 Visual inspections and measurements will be performed in accordance with QSA Global, Inc.'s USNRC approved Quality Assurance Program No. 0040.

## 8.1.2 Weld Examinations

Weld examinations will be performed in accordance with the applicable drawings requirements and in accordance with QSA Global, Inc.'s USNRC approved Quality Assurance Program No. 0040.

## 8.1.3 Structural and Pressure Tests

Prior to first use as part of a Model 880 Series Transport Package, container structural conformance will be evaluated in accordance with the applicable drawings requirements and in accordance with QSA Global, Inc.'s USNRC approved Quality Assurance Program No. 0040. The containment system is not designed to require increased or decreased operating pressures to maintain containment during transport, therefore pressure tests of package components prior to first use are not required.

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## 8.1.4 Leakage Tests

The source capsules (primary containment) are wipe tested for leakage of radioactive contamination upon initial manufacture. The removable contamination must be less than 185 Bq (0.005  $\mu$ Ci). The source capsules will also be subjected to leak tests under ISO9978:1992(E) (or more recent editions). The source capsules are not used if they fail any of these tests.

## 8.1.5 Component and Material Tests

Component and material compliance is achieved in accordance with the requirements in QSA Global, Inc.'s USNRC approved Quality Assurance Program No. 0040.

#### 8.1.6 Shielding Tests

The radiation levels at the surface of the transport package and at 1 meter from the surface are measured upon manufacture. This survey is performed in a low background area and involves a slow scan survey of the entire surface area as well as one meter from the surface of the package. This survey is used to identify any significant void volumes or shield porosity which could prevent the finished device from complying with the dose limits in 10 CFR 71.47.

The radiation profile survey is made with the radiation detector housing in contact with the surface of the package and then also at one meter from the surface of the container. The radiation profile survey for the Model 880SC package is performed twice with the radiation source loaded into each of the locking assemblies of the package. These radiation levels, when extrapolated to the rated capacity of the transport package, must not exceed 200 mR/hr at the surface, nor 10 mR/hr at 1 meter from the surface of the transport package. Failure of this test prevented use of the package as a Type B(U) package.

Rejected packages which do not comply with the construction requirements on the applicable drawings referenced on the Type B certificate, or that do not comply with the radiation profile requirements will not distributed as approved Type B(U) packages.

#### 8.1.7 Thermal Tests

Not applicable. The source content of the Model 880 Series packages has minimal effect on the package surface temperature and therefore no additional testing is necessary to evaluate thermal properties of the packaging.

## 8.1.8 Miscellaneous Tests

Not applicable.

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#### 8.2 Maintenance Program

#### 8.2.1 Structural and Pressure Tests

Not applicable. Material certification is obtained for Safety Class A components used in the transport package prior to their initial use. Based on the construction of the design, no additional structural testing during the life of the package is necessary if the container shows no signs of defect when prepared for shipment in accordance with the requirements of Section 7 of the SAR. The 880 Series packaging is not designed to require increased or decreased operating pressures to maintain containment during transport, therefore pressure tests of package components prior to individual shipment is not required.

#### 8.2.2 Leakage Tests

As described in Section 8.1.4, "Leakage Tests," the radioactive source assembly is leaktested at manufacture. In addition, the sources are leak tested in accordance with that Section at least once every six months thereafter if being transported to ensure that removable contamination is less than 185 Bq (0.005  $\mu$ Ci). Also a contamination wipe is performed of the shield source tubes whenever the shield is returned to the manufacturer (typically the shield is shipped to a customer with new sources and may be returned directly to the manufacturer with decayed sources for disposition)

#### 8.2.3 Component and Material Tests

The transport package is inspected for tightness of fasteners, proper seal wires, general condition and fitness for use prior to each use (see Section 7.1.1). Prior to each use, a radiation survey of the transport package is made to assure that the radiation levels do not exceed 200 mR/hr at the surface, nor 10 mR/hr at 1 meter from the surface.

#### 8.2.4 Thermal Tests

Not applicable. The source content of the Model 880 Series package has no adverse effect on the package surface temperature and therefore no additional testing is necessary to evaluate thermal properties of the packaging prior to shipment.

#### 8.2.5 Miscellaneous Tests

Inspections and tests designed for secondary users of this transport package under the general license provisions of 10 CFR 71.17(b) are provided in Section 7.

#### 8.3 Appendix

Not applicable.

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# **Section 9 – Quality Assurance**

## 9.1 U.S. Quality Assurance Program Requirements

All component fabrication (including assembly) is controlled under the QSA Global, Inc. Quality Assurance program approved by the USNRC (approval number 0040) and ISO 9001.

## 9.2 Canada Quality Assurance Program Requirements

Not applicable. This package is originally submitted for certification in the United States and complies with the criteria in Section 9.1.