

Gallagher, Carol

To: Gallagher, Carol
Subject: FW: CR-6909 rev1 Draft Docket ID NRC-2014-0023
Attachments: Correction to CR-6909_rev1Draft.pdf

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From: Jerzy.Cwifeld@okg.eon.se [mailto:Jerzy.Cwifeld@okg.eon.se]
Sent: Wednesday, October 14, 2015 4:18 AM
To: Stevens, Gary
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Subject: [External_Sender] CR-6909 rev1 Draft Docket ID NRC-2014-0023

Dear Mr Stevens.
Please find attached PDF with my suggestion for correction to page C-10 in CR-6909 rev1 Draft March 2014.
Do NRC agree with my interpretation?
Do you know when the final edition of CR-6909 rev 1 will be published?

Kindly regards
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Add= *cf. Stevens (pls st)*

- v. The F_{en} was assigned to both the peak and valley for use in the CUF_{en} calculations.
- vi. The above steps were repeated for all valley-peak intervals for the entire principal stress intensity history.

B. Modified Strain Rate Approach: In this approach, the F_{en} for each peak and valley resulting from the S_{alt} calculation process was computed using the Modified Rate Approach described in Section 4.1.14, as follows:

- i. The strain rate was based on the total stress component principal stress difference, S'_{31} , which was used to compute CUF. For simplicity, K_e was conservatively not included in the calculation of strain rate.
- ii. The F_{en} integration was set up and performed between each valley and peak with increasing stress, as follows (refer to Figure 80):

$$\dot{\epsilon}_i = \frac{S'_{31i+1} - S'_{31i}}{400 \Delta t E} 100 \quad \boxed{\text{To make \% / sec}}$$

where: $\dot{\epsilon}_i$ = strain rate at any point, i, between the valley and peak (%/sec)
 S'_{31i+1} = S'_{31} stress intensity value at point i+1 (psi)
 S'_{31i} = S'_{31} stress intensity value at point i (psi)
 Δt = time increment between points i and i+1 (seconds)
 E = the Young's Modulus determined at the maximum metal temperature of points i and i+1 (psi)

- iii. To neglect compressive loading in the determination of F_{en} , the F_{en} value was set to 1.0 for any point interval where $\dot{\epsilon}$ was less than zero.
- iv. The $F_{en,i}$ was calculated between for point i and i+1 using the appropriate equation from Appendix A for the material evaluated, and using the maximum metal temperature of points i and i+1.
- v. The integrated F_{en-n} for the valley-peak load pair was calculated as:

$$F_{en-n} = \sum_{i=1}^k F_{en,i} \frac{\Delta \epsilon_i}{\epsilon_{max} - \epsilon_{min}}$$

where: F_{en-n} = integrated F_{en} for valley-peak load pair n
 k = number of integration points between valley and peak
 $\Delta \epsilon_i$ = strain at any point, i, between the valley and peak
see figure 80 Section 4.1.14 computed as S'_{31-i} divided by E evaluated at the metal temperature of point i
 ϵ_{max} = maximum strain at the peak computed as $S'_{31-peak}$ divided by E evaluated at the metal temperature of the peak
 ϵ_{min} = minimum strain at the valley computed as $S'_{31-valley}$ divided by E evaluated at the metal temperature of the valley
 E = the Young's Modulus determined at the maximum metal temperature of points i and i+1 (psi)

- vi. The F_{en} calculated in Step B(v) was assigned to both the peak and valley for use in the CUF_{en} calculations.