

Tennessee Valley Authority, 1101 Market Street, Chattanooga, Tennessee 37402

CNL-15-220

October7, 2015

10 CFR 50.36

U.S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, D.C. 20555-0001

> Watts Bar Nuclear Plant, Unit 2 Construction Permit No. CPPR-92 NRC Docket No. 50-391

Subject: Watts Bar Nuclear Plant Unit 2, Response to Request for Additional Information - Developmental Revision I Technical Specification Section 3.8 -Diesel Generator Batteries

- References: 1. Electronic Mail from J. Poole (NRC) to G. Arent (TVA), "Batteries," dated October 5, 2015
 - TVA Letter to NRC, "Watts Bar Nuclear Plant Unit 2 Submittal of Developmental Revision I of the Unit 2 Technical Specification & Technical Specification Bases and Developmental Revision D of the Unit 2 Technical Requirements Manual and Technical Requirements Manual Bases," dated June 16, 2014 [ML14169A525]

The purpose of this letter is to respond to a request for additional information (RAI) provided in Reference 1. Tennessee Valley Authority (TVA) was requested to confirm that the Diesel Generator batteries are designed to operate at 50° Fahrenheit (F). This question was identified by the Nuclear Regulatory Commission during their review of Technical Specification (TS) 3.8 provided in Development Revision I of the Watts Bar Nuclear Plant Unit 2 TSs (Reference 2).

The enclosure provides TVA's response to the Reference 1 RAI regarding batteries.

There are no new regulatory commitments associated with this letter. Please direct any questions concerning this matter to Gordon Arent at (423) 365-2004.

U.S. Nuclear Regulatory Commission CNL-15-220 Page 2 October 7, 2015

I declare under penalty of perjury that the foregoing is true and correct. Executed on the 7th day of October 2015.

Respectfully,

J. W. Shea Digitally signed by J. W. Shea DN: cn=J, W. Shea, o=Tennessee Valley Authority, ou=Nuclear Licensing, ou=Nuclear Licensing, Die 2015.10.07 19:14:15-04100'

J. W. Shea Vice President, Nuclear Licensing

Enclosure:

Response to NRC Request For Additional Information – Diesel Generator Battery Temperature

cc (Enclosure):

U.S. Nuclear Regulatory Commission, Region II NRC Senior Resident Inspector - Watts Bar Nuclear Plant, Unit 2 NRC Project Manager - Watts Bar Nuclear Plant, Unit 2

Enclosure

Response to NRC Request For Additional Information – Diesel Generator Battery Temperature

Background

By letter dated June 16, 2014, Tennessee Valley Authority (TVA) submitted the Watts Bar Nuclear Plant (WBN) Unit 2 Developmental Revision I of the Technical Specifications (TS) and TS Bases, and Developmental Revision D of the WBN Unit 2 Technical Requirements Manual (TRM) and TRM Bases to the Nuclear Regulatory Commission (NRC) (Reference 1). By electronic mail (email) dated October 5, 2015, the NRC provided a request for additional information (RAI) regarding TS Section 3.8 of Developmental Revision I (Reference 2).

The following response to the Reference 2 RAI addresses the NRC staff concerns related to the design of the Diesel Generator (DG) batteries.

NRC RAI

TS 3.8.6.3 establishes battery operability based on battery cell parameters and average electrolyte temperatures for vital and DG batteries. If the average electrolyte temperature of the representative cells is outside the lower limit (< 60° F for vital batteries and < 50° F for DG batteries), the battery is considered inoperable. The staff requested information about Station battery sizing and testing criteria for 60° F ambient temperature and DG battery at 50° F ambient temperature.

The applicant provided details on correction factors for station batteries for temperature range at and above 60°F and correction factors for DG batteries for temperature range at and above 60°F and NOT 50°F. The staff recommends that the applicant confirm that the DG batteries are designed for operating at 50°F.

TVA Response

Based on TVA's review of 125VDC Diesel Generator Battery sizing analysis calculation WBNEEBMSTI110062; the design temperature used for sizing the DG batteries is 50°F. Attachment 1 provides pages from the calculation confirming the use of 50°F The cell sizing factor for 50°F corresponds to 1.19 and is obtained from Table 1 of IEEE Standard 485, "IEEE Recommended Practice for Sizing Lead-Acid Batteries for Stationary Applications" (Attachment 2). Therefore, TVA confirms that the DG batteries are designed for operating at 50°F.

References

- 1. TVA Letter to NRC, "Watts Bar Nuclear Plant Unit 2 Submittal of Developmental Revision I of the Unit 2 Technical Specification & Technical Specification Bases and Developmental Revision D of the Unit 2 Technical Requirements Manual and Technical Requirements Manual Bases," dated June 16, 2014 [ML14169A525].
- 2. Email from J Poole (NRC) to G. Arent (TVA), "Batteries," dated October 5, 2015.

ATTACHMENT 1

TVA Calculation WBNEEBMSTI110062, "125VDC Diesel Generator (DG) Control Power System Evaluation"

Extracted Pages

							Page 1	-
REV 0 EDMS/RIM			CTS TYPE: Calculation CALC		EDMS TYPE: EDMS A		ACCESSION NO (N/A for REV. 0) 3 1 2 1 0 1 5 0 0 3	
Calc Title: 125	DC DIESE	L GENERA	TOR (DG)	CONTR	OL POWER SY			
ORG PLAN			BRANCH		NUMBER		CUR REV	NEW REV
CALC ID NUC WEN			EEB	WBNI	EBMSTI110062	027	028	
CTS UPDATE ONI (Verifier and Appro	and a second sec	Not Required)		NC (Fe	OCTS CHANGES D or calc revision, CTS	has been re	oliz//L eviewed and no (CTS changes required)
<u>UNIT</u> (check one) 0 ⊠, 1 □, 2 □, 3	D 082	IS	10 million (10 million)		UNIDS N/A	к 1		
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and Impact. <u>ABSTRACT:</u> This calculation protective device fuses and maxi and the impact 8.0 and 9.0 for The following re	of PROBLEM quacy of the n evaluate t ce sizing, sh imum voltag of its subme results and o evisions are	te adequace nort circuit are to the cont argence on the conclusions.	y of the 12 nd coordinat rol circuit co ne 125 VDC Change On	with des 5 VDC I ion, App mponen DG Con ly: 17, 2	DG Control Pow endix R, Reg. G ts. Equipment s trol Power System	er Syste luide 1.7 ubmerge n is eval	m battery si 75 - Associate d due to MEI luated in App	eview and document zing, charger sizing, ed Circuits, cascade LB event is identified endix I. See Section alculation.
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MICROFICH	E/EFICHE	Yes No	FICHE NU	JMBER(S)				
A 40532	÷		F	Page 1 of 2				NEDP-2-1 [10-31-2011]

NPG CALCULATION COVERSHEET / CTS UPDATE

WBN EEB-MS-TI11-0062

Prepared By	JAK	Date 6-22-93
Checked By	PAR	Date <u>6/22/93</u>
Page 6		

1.0 Purpose

The purpose of this calculation is to evaluate the adequacy of the 125VDCDiesel Generator Control Power System for compliance with FSAR and design criteria requirements for the following:

-battery sizing -battery charger sizing -protective device sizing -short-circuit protection and coordination -Appendix R power supply and associated circuits -Reg Guide 1.75 associated circuits -cascade fuse analysis -voltage to components

The purpose of this calculation is also to evaluate the impact of the MELB on 125V DC Diesel Generator Control Power System and demonstrate that in the event of its loss the plant's safe shutdown can be successfully achieved.

2.0 Assumptions

Refer to Section 5.0 for documentation and justification of assumptions.

3.0 References and Sources of Design Input Data

- 3.1 WBN FSAR Sections 8.3.
- 3.2 Design Criteria WB-DC-30-27, "AC and DC Control Power Systems", DIMS WB-DC-30-27-1 (B26890324040), WB-30-27-2 (B26900510078).
- 3.3 WBN Preop Test 14D R4.

3.4 TVA drawings and vendor documents listed below:

15N210-4 RF 15W814-5 RJ 1-45W727 R03 1-45W728-1 R02 1-45W760-82-1 R02, -2 R01, -3 R03, -4 R02, -5 R00, -6 R02, -11 R00, -12 R01, -13 R01, -14 R02, -15 R00, -16 R02, -20 R02, -21 R00 45W1761-1 RM 45W1762-1 RH 45W1763-1 RK 45W1763-1 RK

Date: 2-2-93 WBN EEB-MS-TI11-0062 Prepared By: m.p. _ Date: 2-2-93 Checked By:_ Page 7 45W1781-1 RN, -2 RD, -3 RG, -4 RF, -5 RC, -6 RE 45W1782-1 RE, -2 RB, -3 RD, -4 RB, -5 RB, -6 RC 45W1787-1 RG 45W2761-1 RJ 45W2763-1 RL 45W2780-1 RK, -2 RE, -3 RH, -4 RG, -5 RC, -6 RF 45W2781-1 RL, -2 RE, -3 RF, -4 RH, -5 RB, -6 RE 47E235-29 R04, -30 R03 Vendor Documents RII Contract 83090 DG Manual VOl 1 & 2, TVA IDs 979, 980 (DG 1A-A, 1B-B, 2A-A, 2B-B); DG Manual Vol 1 & 2, TVA IDs 1548, 1549 (DG C-S) 650-242, 244; 655-241 6036B11010 RD, SHEETS 1-10 6036C04501 RB C379C11501 R904 6036C11501 R901 6036C11501 R902 6036F11502 RB DS-E8.1.1 R8, "Substitution Standard for Low-Voltage 3.5 Power and Control Fuses (600 Volts or Less)". \sim \checkmark Y $\mathbf{\mathbf{v}}$ 3.6 IEEE Standard 485 (1978), IEEE Recommended Practice for Sizing Large Lead Storage Batteries for Generating Stations and Substations". لمل SQN Calculation SQN-CPS-007 R0, "Diesel Generator 3.7 Battery Capacity", B43861210901. 3.8 SQN Calculation SQN-CPS-012 R1, "Diesel Generator RII Lube Oil Pump Voltage", B87910118002. 3.9 Walkdown data for DG distribution panels included as attachment to memo from R.W. Bradford to H.B. Bounds, dated Nov. 28, 1988, "Watts Bar Nuclear Plant-Unit 1 and 2-Walkdown of Electrical Equipment -Walkdown Procedure WP-37", C24881128629. 3.10 National Electric Code, 1987, Chapter 9, Table 8 "Properties of Conductors" (dc resistance at 25° C).

This Sheet Added By Rev 11

WBN EEB-MS-TI11-0062

1hx Prepared By: Date: Date: Checked By: Page 10

- 5.0 Assumptions
 - 5.1 The minimum ambient temperature of the rooms containing the diesel batteries is 50° F. Justification: TVA drawings 47E235-29R2 and 47E235-30R0 list the average DG room temperature at 75° F and a normal minimum of 50° F. Ref. DCN M11594A.
 - 5.2 The diesel batteries shall support three start attempts; one at the beginning of its 4 hour duty cycle, one at the 29 minute mark and the other at the end of the 4 hours.

Justification: DCN S-34918-A limits the number of starting attempts to three during the 4 hour Station Blackout event. If the diesel fails to reach 200 rpm within 5 seconds of initial start, a fail to start condition exists and the diesel is locked out, requiring a manual reset for a restart attempt. Experience with the diesel has proven that if it does not start at the initial start command, the time required for response and problem correction is significant such that it is reasonable to assume that the first restart attempt will occur in the first 30 minute period. Assuming the third and final starting attempt occurs in the final minute is conservative.

RIG

5.3 It is assumed for short-circuit analysis that the DG battery system voltage is determined by the base emf of the battery at 2.06 volts-per-cell such that the battery voltage used in analysis is 119.5V (58 cells x 2.06V).

Justification: Under short-circuit conditions, the charger voltage declines as the output is currentlimited. The use of 2.06 volts per cell will provide conservative results.

This Sheet Added By Rev 19

WBN EEB-MS-TI11-0062 PAGE 15 A

PREPARED BY TAN DATE 6/28/95 CHECKED BY DATE 6/29/95

Battery Sizing Calculation IEEE 485–1983 Work Sheet DIESEL BATTERIES SIMULTANEOUS MOTOR STARTS

Period Load Section (A)	Change In Load (Amps)	Duration of Period (minutes)	Time to End of Section	Capacity At T Min	Required Section Size Pos Pl				
Section 1 - First Period On 1 A1= 108.0 A1- 108-24 108-24	$108 - 0 = \frac{108}{108}$. <i>4</i> / ≥ M1= 1	T=M1	1 72.33	1.50 1.49				
Section 2 - deleted for clari	ity		•						
Section 3 — First Three Sect 1 A1 $\frac{168}{108}$, $\frac{1}{108}$, $\frac{624}{24}$, A1- 2 A2=17.21 $\frac{16.617.04}{16.617.04}$ A2- 3 A3= $\frac{81.6}{82.04}$ A3- 82.2	$-0 = \frac{108.0}{108.0}$	M1 = 1 M2 = 28	T≓M1:M3 T=M2:M3 T=M3	30 47.33 29 47.33 1 72.33 Total	2.29 2.28 (1.93) 0.90 <u>1.25</u> 1.26 R25				
Section 4 - deleted for cla	rity				1.201-2				
2 A2=17.2) 16.81704 A2- 3 A3=82.2181.88204 4 A4=15.41 15.015.24 A4-	-0 = 108.0 -A1 = (91.2) -A2 = 65.0	$ \begin{array}{cccc} M1 = & 1 \\ M2 = & 28 \\ M3 = & 1 \\ M4 = & 209 \\ \end{array} $	T=M1:M5 T=M2:M5 T=M3:M5 T=M4:M5	240 16.00 239 16.00 211 19.00 210 19.00	6.78 6.77 				
78.64	-A4 = 03.4	M5= 1	T=M5	1 72.33 Total	0.88 1.80 1-85				
Battery Cell Size (No. Of Pos Plates) = Temp Cor Factor X Aging Factor X Design Margin $ \begin{array}{rcl} 1.86\\ & & & \\ 1.86\\ & & & \\ 1.86\\ & & \\ $									

THIS PAGE ADDED BY REVISION 19

ATTACHMENT 2

IEEE Std 485-1997(R2003)

IEEE Recommended Practice for Sizing Lead-Acid Batteries for Stationary Applications

Extracted Pages

IEEE Recommended Practice for Sizing Lead-Acid Batteries for Stationary Applications

Sponsor

IEEE Standards Coordinating Committee 29 on Stationary Batteries

Reaffirmed 11 September 2003 Approved 20 March 1997

IEEE Standards Board

Abstract: Methods for defining the dc load and for sizing a lead-acid battery to supply that load for stationary battery applications in full float operations are described. Some factors relating to cell selection are provided for consideration. Installation, maintenance, qualification, testing procedures, and consideration of battery types other than lead-acid are beyond the scope of this recommended practice. Design of the dc system and sizing of the battery charger(s) are also beyond the scope of this recommended practice.

Keywords: battery duty cycle, cell selection, dc load, full float operation, lead-acid batteries, rated capacity, sizing, stationary applications, valve-regulated lead-acid (VRLA) cell, vented battery

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Note that the "margins" required by 6.3.1.5 and 6.3.3 of IEEE Std 323-1983 are to be applied during "qualification" and are not related to "design margin."

	Electrolyte temperature		Cell size		Electroly	Cell size	
	(° F)	(° C)	correction factor		(° F)	(° C)	correction factor
25	5	-3.9	1.520	1	78	25.6	0.994
30	0	-1.1	1.430	1	79	26.1	0.987
35	5	1.7	1.350	1	80	26.7	0.980
4(0	4.4	1.300	1	81	27.2	0.976
A	5	7.2	1.250		82	27.8	0.972
50	0	10.0	1.190		83	28.3	0.968
5	, , , , , , , , , , , , , , , , , , , 	12.8	4.150	u	84	28.9	0.964
60	0	15.6	1.110		85	29.4	0.960
65	5	18.3	1.080		86	30.0	0.956
66	6	18.9	1.072		87	30.6	0.952
67	7	19.4	1.064] .	88	31.1	0.948
68	8	20.0	1.056	1	89	31.6	0.944
69	9	20.6	1.048	1	90	32.2	0.940
70	0	21.1	1.040	1	95	35.0	0.930
71	1	21.7	1.034	1	100	37.8	0.910
72	2	22.2	1.029	1	105	40.6	0.890
73	3	22.8	1.023	1	110	43.3	0.880
74	4	23.4	1.017	1	115	46.1	0.870
75	5	23.9	1.011	1	120	48.9	0.860
76	6	24.5	1.006	1	125	51.7	0.850
77	7	25.0	1.000	1			

Table 1—Cell size correction factors for temperature

NOTE—This table is based on vented lead-acid nominal 1.215 specific gravity. However, it may be used for vented cells with up to a 1.300 specific gravity. For cells of other designs, refer to the manufacturer.

6.2.3 Aging factor

As a rule, the performance of a lead-acid battery is relatively stable throughout most of its life, but begins to decline with increasing rapidity in its latter stages, with the "knee" of its life versus performance curve occurring at approximately 80% of its rated performance.

IEEE Std 450-1995 recommends that a battery be replaced when its actual performance drops to 80% of its rated performance because there is little life to be gained by allowing operation beyond this point. Therefore, to ensure that the battery is capable of meeting its design loads throughout its service life, the battery's rated capacity should be at least 125% (1.25 aging factor) of the load expected at the end of its service life.

Exceptions to this rule exist. For example, some manufacturers recommend that vented batteries with Planté, modified Planté, and round plate designs be replaced when their measured capacity drops below 100% of