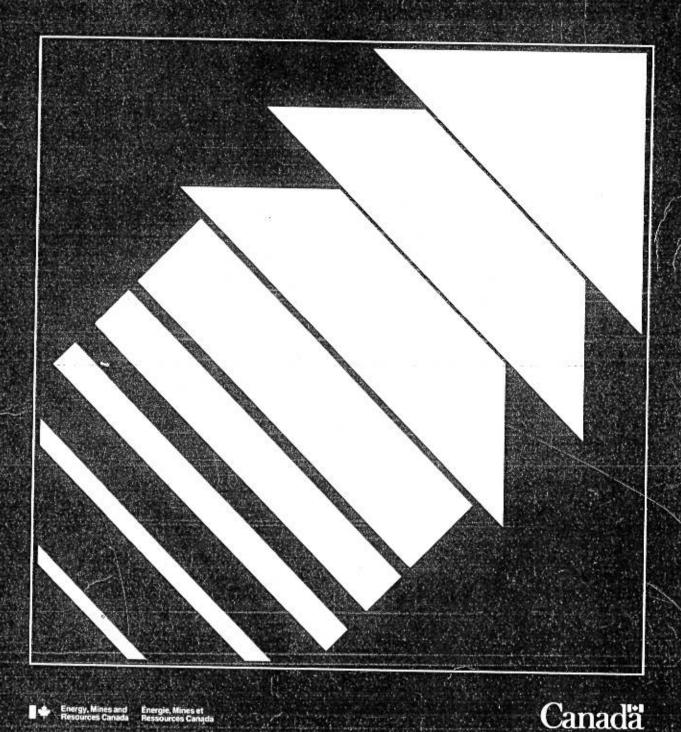
NATIONAL URANIUM TAILINGS PROGRAM

URANIUM TAILINGS REFERENCE MATERIALS

**NUTP-2E** 



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# **URANIUM TAILINGS REFERENCE MATERIALS**

C.W. Smith H.F. Steger W.S. Bowman

National Uranium Tailings Program

NUTP-2E

CANMET

Canada Centre for Mineral and Energy Technology Centre canadien de la fechnologie des minéraux et de l'énergie

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#### FOREWORD

There are currently about 130 million tonnes of mine wastes (tailings) produced from the mining and milling of uranium ore that are on, or near, the surface in Canada. At public hearings and other forums held in connection with proposals for new uranium production facilities, concern has been expressed about the impact that these wastes may have on the environment in the future. Government regulatory agencies believe that there may be long-term environmental and health consequences associated with uranium tailings that are not yet fully understood.

As a result of a year-long study, undertaken by a group of experts from government, industry, and the universities, into the possible long-term problems of uranium tailings management, the decision was taken by the Federal Government to launch an R & D program to assist in clarifying the nature and extent of problems that may arise in the future. It is anticipated that the results of such a program will be of use to the Atomic Energy Control Board and to provincial regulatory agencies in the establishment of criteria for the decommissioning and abandonment of uranium tailings. To this end, the National Uranium Tailings Program of CANMET has been funded to the extent of \$9.5 million for a period of five years.

The main objective of this Program is to provide a scientifically credible information base that will assist government regulatory agencies in making confident, knowledgeable decisions, and in establishing criteria for the long-term protection of the environment and human health. The scientific information base will, among other things, describe the chemical and physical processes that involve tailings constituents and their movement along pathways from the tailings into the biosphere.

The National Uranium Tailings Program's activities, which have been entirely contracted out, have included research into the processes involved in the behaviour and movement of contaminants from tailings, field sampling and measurements, chemical analyses, and predictive modelling. As an important part of the Program output, manuals have been prepared that incorporate the results of this work.

This manual has been prepared for the purpose of making available up-to-date information and data that will be of interest and practical use to those directly concerned with operational aspects of uranium tailings management and regulation.

W.G. Jeffery Director General Canada Centre for Mineral and Energy Technology

# **PREFACE**

Quality assurance in the production of data is indispensable to the success of the National Uranium Tailings Program. In order to provide as much assistance as possible in ensuring high quality chemical analyses for radionuclides and other constituents in a uranium tailings matrix, standard reference materials were prepared to cover the range of tailings composition encountered in Canada. These reference materials will be used to maintain a high level of quality control for all work performed by contract on behalf of the Program, and will also be available to all others that may find them useful in verifying the performance of their own equipment and procedures.

As additional reference materials, relevant to the Program are certified in the future, sup-

plements to this manual will be prepared and published.

#### **ACKNOWLEDGEMENTS**

At the beginning of the Program, Lloyd Dalton and Clint Smith of CANMET Chemical Laboratories served as Scientific Authorities on behalf of NUTP in the exchange of analyses with participating laboratories. This responsibility has subsequently been assumed by Mr. Roy John, Project Manager, Measurements, of the National Uranium Tailings Program Office. The laboratories that participated in the exchange program are listed in the body of the manual. The efforts of the following CANMET staff in organizing and operating the project in developing the reference standards are gratefully acknowledged; C.W. Smith, H.F. Steger and W.S. Bowman.

V.A. Haw Director National Uranium Tailings Program

# URANIUM TAILINGS REFERENCE MATERIALS

by

C.W. Smith\*, H.F. Steger\* and W.S. Bowman\*

### SYNOPSIS

Samples of uranium tailings from Bancroft and Elliot Lake, Ontario, and from Beaverlodge and Rabbit Lake, Saskatchewan, have been prepared as compositional reference materials at the request of the National Uranium Tailings Research Program. The four samples, UTS-1 to UTS-4, were ground to minus 104  $\mu$ m, each mixed in one lot and bottled in 200-g units for UTS-1 to UTS-3 and in 100-g units for UTS-4. The materials were tested for homogeneity with respect to uranium by neutron activation analysis and to iron by an acid-decomposition atomic absorption procedure.

In a free choice analytical program, 18 laboratories contributed results for one or more of total iron, titanium, aluminum, calcium, barium, uranium, thorium, total sulphur, and sulphate for all four samples, and for nickel and arsenic in UTS-4 only. Based on a statistical analysis of the data, recommended values were assigned to all elements/constituents, except for sulphate in UTS-3 and nickel in UTS-4.

The radioactivity of thorium-230, radium-226, lead-210, and polonium-210 in UTS-1 to UTS-4 and of thorium-232, radium-228, and thorium-228 in UTS-1 and UTS-2 was determined in a radioanalytical program composed of eight laboratories. Recommended values for the radioactivities and associated parameters were calculated by a statistical treatment of the results.

<sup>\*</sup>Research Scientists, Mineral Sciences Laboratories, CANMET, Energy, Mines and Resources Canada, Ottawa, K1A 0G1

# RÉSIDUS D'URANIUM, MATÉRIAUX DE RÉFÉRENCE

par

C.W. Smith \*, H.F. Steger \* et W.S. Bowman \*

#### SYNOPSIS

Des échantillons de résidus d'uranium provenant de Bancroft et d'Elliot Lake en Ontario et de Beaverlodge et de Rabbit Lake en Saskatchewan ont été préparés comme matériaux de référence de composition connue à la demande du Programme national de recherche sur les résidus d'uranium. Chacun des quatre échantillons, UTS-1 à UTS-4, a été broyé à une granulométrie inférieure à 104  $\mu$ m et mélangé pour former un lot. Les résidus UTS-1 à UTS-3 ont été mis dans des bouteilles de 200 g et l'UTS-4 a été mis dans des bouteilles de 100 g. On a vérifié l'homogénité des matériaux quant à l'uranium par la méthode d'activation neutronique et quant au fer total par une méthode de décomposition acide et de spectrométrie d'absorption atomique.

En vertu d'un programme analytique de *libre choix*, 18 laboratoires ont soumis des résultats pour un, ou plusieurs des éléments/constituants suivants: fer total, titane, aluminium, calcium, baryum, uranium, thorium, soufre total et sulfate pour les quatre matériaux, et nickel et arsenic pour l'UTS-4 seulement. Après une analyse statistique des données, on a assigné des valeurs recommandées à tous les éléments/constituants, sauf au sulfate pour l'UTS-3 et au nickel pour l'UTS-4.

On a déterminé la radioactivité des isotopes, thorium-230, radium-226, plomb-210, et polonium-210 pour les quatre matériaux, et thorium-232, radium-228, et thorium-228 pour l'UTS-1 et l'UTS-2, dans le cadre d'un programme radioanalytique auquel huit laboratoires ont participé. Les valeurs recommandées pour les activités des isotopes et des paramètres associés ont été calculées à l'aide d'une analyse statistique des données.

<sup>\*</sup>Chercheurs scientifiques, Laboratoires des sciences minérales, CANMET, Énergie, Mines et Ressources Canada, Ottawa, KIA 0G1.

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# INTRODUCTION

The preparation of compositional reference materials from several uranium tailings samples, typical of existing Canadian tailings sites, was initiated under the auspices of the National Uranium Tailings Research Program (NUTRP) in late 1982 (1). These were intended for use in quality-control functions for both chemical and radiochemical analytical measurements with the National Measurement Program of NUTRP. The reference materials were also to be made available through the Canadian Certified Reference Materials Project (CCRMP) for more general use by the analytical community.

CCRMP currently offers many compositional reference ores, concentrates, and related products, typical of Canadian deposits and not, in general, available from other sources for use in analytical laboratories associated with mining, metallurgy, and the earth sciences (2). Among these are uranium ores from Elliot Lake, Ontario, and Beaverlodge, Saskatchewan, of which four, DL-1a, DH-1a, BL-4a and BL-5, have been certified for radium-226 activity (3).

This report describes the preparation and characterization of the four uranium tailings samples: UTS-1, UTS-2, UTS-3 and UTS-4. The description of their nature, physical preparation, and estimation of the consensus values and related statistical parameters for use as reference materials follows.

The results of the analytical program to establish the concentration of total iron, titanium, aluminum, calcium, barium, uranium, thorium, total sulphur, sulphate, nickel and arsenic in the tailings samples are presented in "Part A" of this report.

The results of the radioanalytical program to determine the activity of thorium-230, radium-226, lead-210, and polonium for all four samples, and also for UTS-1 and UTS-2, thorium-232, radium-228 and thorium-228, are presented in "Part B".

# NATURE AND PREPARATION

#### UTS-1

The uranium tailings sample for UTS-1 was donated to NUTRP and CCRMP in October 1982 by Madawaska Mines Limited located near Bancroft, Ontario. The mine is in a belt of meta-gabbro and amphibolite. The ore is part of a zone of irregular pegmatitic granite dykes, with metasomatic phases. Uranium is present as uraninite and uranothorite with minor uranophane (4). The ore is comminuted to 50% minus  $74~\mu m$  and is leached at pH = 1.6 to 1.8 with

sulphuric acid and sodium chlorate under agitation with compressed air with a 24 h retention period. The mill tailings slurry is treated with lime to pH = 9 before disposal (5).

#### UTS-2

The tailings sample for UTS-2 was donated by Rio Algom of Elliot Lake, Ontario. The ore is a pebble conglomerate. The pebbles are mainly quartz with some chert. The matrix is a sericitic, feldsphathic quartzite containing about 10% pyrite on a whole ore basis (6). The comminuted ore is leached at 60-70°C at a concentration of 40 g/L sulphuric acid under agitation with compressed air for approximately 40 h. The mill tailings slurry is treated with limestone and lime to raise the pH to 10 before disposal (7).

#### UTS-3

The tailings sample for UTS-3 was donated by Eldorado Nuclear Limited at Beaverlodge, Saskatchewan. The orebody consists of complexes of disseminations and stringers, lenses and veins of pitchblende in reddish-brown mylonitized oligoclase saturated with dusty hematite. Pitchblende is the sole radioactive mineral present. Minor amounts of carbonates and pyrites occur along with the pitchblende (8). The pyrites are separated as a concentrate by flotation at pH 10 (sodium carbonate) using isopropyl xanthate. This concentrate is leached with 100 lb/ton (44 kg/1000 kg) of sulphuric acid and 2.5 lb/ton (1.1 kg/1000 kg) of sodium chlorate. The uranium is precipitated with magnesium hydroxide and sent to the carbonate leaching circuit.

The slurry of flotation tailings and the above precipitated uranium in 100 g/L dissolved carbonate and sulphate salts is leached for four days at 90°C. Oxidation of the uranium and residual sulphide minerals is accomplished by sparging with 99.5% oxygen. The mill tailings are disposed of directly (9).

#### UTS-4

The tailings sample for UTS-4 was provided by the Extractive Metallurgy Laboratory of CANMET which had previously prepared it from ore donated by, and using the recovery process of, Eldor Mines (formerly Gulf Minerals Canada Limited) at Rabbit Lake, Saskatchewan. The host rock for the uranium mineralization is a siliceous dolomite that has been highly altered and fractured. The ore consists of a high-grade zone of such mineralization in the centre of a brecciated zone, grading to low grade in the lesser brecciated perimeter (10). The comminuted ore is leached with sulphuric acid and sodium chlorate in

seven stages whereby pH and temperature are changed from 2.5-2.8 and 30-34°C to 1.6-1.7 and 48-52°C, respectively. The leach retention time is approximately eight hours. The mill tailings are neutralized with lime before disposal (10).

The four uranium tailings samples were dried at 80°C and dry-ground in November-December 1982 to pass a 104-µm sieve. The powdered tailings samples were each tumbled in one lot in a 570-L conical blender for 15 h and bottled. Approximately 340 kg of each of UTS-1, UTS-2 and UTS-3 were bottled in 200-g units. For UTS-4, approximately 134 kg were bottled in 100-g units. The four tailings samples were found to be sufficiently homogeneous for uranium by a neutron activation analytical technique and for total iron by an acid dissolution-atomic absorption spectrometric procedure to qualify as reference materials. Results of the confirmation of the homogeneity of UTS-1, UTS-2, UTS-3 and UTS-4 are reported in Appendix A.

The particle size analysis of the tailings samples is given in Table 1.

Table 1 - Particle size analysis of uranium tailings samples (wet screen)

Size of		UTS-1	UTS-2	UTS-3	UTS-4
fraction	(µm)		ss %		
- +	104	0.1	0.03	< 0.01	< 0.01
-104 +	74	47.8	40.9	54.8	19.7
- 74 +	55	17.6	15.6	18.5	13.1
- 55 +	37	7.0	6.9	6.3	5.7
- 37		27.5	36.6	20.4	61.5

The concentration of the elements/constituents and the activity of the selected radioisotopes in the uranium tailings samples were determined by interlaboratory programs involving eighteen and eight laboratories, respectively. All participants except one for each program performed the requested analytical work under contract to CANMET with arrangements made by Supply and Services Canada (Tables A-1 and B-1).

# ESTIMATION OF CONSENSUS VALUES AND 95% CONFIDENCE LIMITS

The estimation of the consensus value and related statistical parameters by the following procedure is performed only after outlying values are removed. The criteria for removal is peculiar to each interlaboratory program and as such is discussed in Parts A and B.

A one-way analysis of variance technique was used to estimate the consensus value and its variance. This approach considers the results of the described certification program to be only one sampling out of a universal set of results. The analytical data were assumed to fit the model (11)

$$x_{ij} = \mu + y_i + e_{ij}$$

where  $x_{ij}$  = the  $j^{th}$  result in set i,

 $\mu$  = the true consensus value,

y<sub>i</sub> = the discrepancy between the mean of the results in set i (x<sub>i</sub>) and μ, and

 $e_{ij}$  = the discrepancy between  $x_{ij}$  and  $\overline{x}_{ij}$ .

It is assumed that both  $y_i$  and  $e_{ij}$  are normally distributed with means of zero and variances of  $\omega$  and  $\sigma^2$ , respectively. The significance of  $\omega^2$  is detected by comparing the ratio of between-set mean squares and within-set mean squares with the F statistic at the 95% confidence level and with the appropriate degrees of freedom.

The consensus value of the assumed model is estimated by the overall mean  $\overline{\mathbf{x}}$ ...:

$$\overline{x}_{..} = \sum_{j=1}^{k} \sum_{i=1}^{n_{j}} x_{ij}$$

where  $n_i$  = the number of results in set i and k = the number of sets,

The value of  $\sigma^2$  is estimated by  $s_1^2$  which is given by

$$s_1^2 = \sum_{i=j}^{k} \sum_{j=1}^{n_i} (x_{ij} - \overline{x}_{i,.})^2 / \sum_{j=1}^{k} n_j - k$$

The value of  $\omega^2$  is estimated by

$$\omega^2 = (s_2^2 - s_1^2) \left/ \frac{1}{k-1} \left( \begin{matrix} k \\ \Sigma n_i - \begin{matrix} k \\ \Sigma n_i^2 / \Sigma n_i \end{matrix} \right) \right.$$

where

$$s_2^2 = \sum_{i=1}^{k} n_i (\overline{x}_i . - \overline{x}_i)^2 / k - 1$$

The variance of the overall mean is given by

$$v[\overline{x}..] = \begin{pmatrix} k & k \\ \sum_{i} n_{i} 2/(\sum_{i} n_{i})^{2} \end{pmatrix} \quad \omega^{2} + \begin{pmatrix} k \\ 1/\sum_{i} n_{i} \end{pmatrix} \quad \sigma^{2}$$

and the 95% confidence limits for X., are

It should be noted that 95% confidence limits denote that if the interlaboratory program were performed 100 times, it would be expected that the overall mean in 95 would fall within the prescribed limits.

The average within-set standard deviation,  $\sigma_A$ , is a measure of the average within-bottle precision as determined by the analytical methods used. The implication exists, therefore, that a laboratory using a method of average or better reproducibility should obtain individual results for a given certified element with a repeatability that is at least comparable to the reported value of  $\sigma_A$ .

The consensus values for the elements/constituents and the radioactive isotopes are reported in Tables 2 and 3 respectively and are given recommended value status.

Table 2 - Recommended values for elements/constituents

Element/	UTS-1	UTS-2	UTS-3	UTS-4			
constituent	mass %						
Fe (total)	4.87	3.20	3.25	2.62			
Ti	0.54	0.18	0.23	0.24			
Al	6.24	2.71	5.80	6.29			
Ca	5.24	0.42	4.03	1.75			
S (total)	1,00	3.23	0.23	1.80			
sulphate	2.64	0.84		5.21			
		μ	g/g				
barlum	324	464	212	65			
uranium	49	56	513	1010			
thorium	138	174	10.0	15.4			
arsenic				38			

Table 3 – Recommended activity values for radioactive isotopes

UTS-1	UTS-2	UTS-3	UTS-4
	Во	1/g	
3.6	4.4	11.3	22.9
3.67	5.6	13.3	38.6
3.25	4.55	12.6	32.4
3.1	4.4	11.8	30.8
0.68	0.88		
0.68	1.0		
0.71	0.92		
	3.6 3.67 3.25 3.1 0.68 0.68	3.6 4.4 3.67 5.6 3.25 4.55 3.1 4.4 0.68 0.88 0.68 1.0	Bq/g  3.6 4.4 11.3 3.67 5.6 13.3 3.25 4.55 12.6 3.1 4.4 11.8 0.68 0.88 0.68 1.0

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# CONFIRMATION OF HOMOGENEITY

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The homogeneity of the uranium tailings samples was confirmed by Chemex Laboratories Ltd., North Vancouver, British Columbia, (Contract 15SQ.23440-2-9146) by analyzing for uranium and total iron in three separate subsamples for each of 19 bottles selected from a stock of 1655 bottles for UTS-1, UTS-2 and UTS-3 and of 1280 bottles for UTS-4. The stock of UTS-1 to UTS-3 was divided into 18 lots of 87 bottles and a 19th lot of 89 bottles; the stock of UTS-4 was divided into 18 lots of 67 bottles and a 19th lot of 74 bottles. In each case. the code number of the first bottle was selected at random out of the first lot. The code numbers of the remaining 18 bottles were given by the code number of the preceding bottle plus the number of bottles in each of the first 18 lots.

Uranium was determined by an instrumental neutron activation analytical technique. Total iron was determined by atomic absorption spectrometry after multi-acid sample decomposition. The results are shown in Tables 4 to 7.

A one-way analysis of variance techniques was used to assess the homogeneity (11). Herein, the ratio of the between-bottle to within-bottle mean square is compared with the F statistic at the 95% level of probability. There was no statistical evidence for 'bottle-to-bottle inhomogeneity with respect to uranium in all four tailings samples or with respect to iron for UTS-1 and UTS-2.

The iron results for UTS-3 and UTS-4 did indicate some bottle-to-bottle inhomogeneity. This however does not imply that the inhomogeneity is physically significant particularly in view of the contradictory results observed for uranium. Moreover, a detected inhomogeneity, statistical, physical or both. does not necessarily disqualify a candidate reference material from its intended use provided that its magnitude is acceptable in comparison with the overall uncertainty in the recommended value for the element of interest. The between-bottle standard deviation for iron in UTS-3 and UTS-4 was calculated to be 0.026 and 0.015% for the overall means of 3.12 and 2.60% Fe, respectively. The detected inhomogeneity therefore gives rise to relative uncertainties of 0.83 and 0.58% for UTS-3 and UTS-4, values which CCRMP concluded would be acceptable in comparison with the between-laboratory relative uncertainty expected from the results of the interlaboratory program. The latter can be calculated to be 0.089 and 0.073% Fe for UTS-3 and UTS-4, i.e., the relative certainty is 2.74 and 2.79%, respectively, thereby demonstrating UTS-3 and UTS-4 to be sufficiently homogeneous for use as reference materials.

Table 4a - Confirmation of homogeneity of UTS-1 for uranium

Table 4b - Confirmation of homogeneity of UTS-1 for total iron

54 47 51 53	Individua! 53 49 49	48 51 50	Mean 51.7 49.0	Bottle No.	4.75	Individual	4.83	Mean 4.77
47 51 53	49 49	51					4.83	4.77
47 51 53	49 49	51						
51 53	49			127	4.93	4.75	4.88	4.85
53			50.0	214	4.80	4.80	4.76	4.79
	6.9	50	51.7	301	4.83	4.82	4.82	4.82
49	52 49	48	48.7	388	4.81	4.75	4.73	4.76
52	49	51	50.7	475	4.77	4.76	4.78	4.76
		54		565	4.83	4.83	4.77	4.81
							4.82	4.82
							4.76	4.81
							4.81	4.80
				910	4.84	4.86	4.88	4.86
				997	4.83	4.82	4.82	4.82
				1084	4.79	4.90	4.90	4.86
				1171	4.75	4.77	4.89	4.80
				1258	4.86	4.81	4.77	4.81
				1345	4.82	4.80	4.81	4.81
					4.78	4.77	4.78	4.78
					4.80	4.78	4.88	4.82
				1606	4.83	4.81	4.87	4.84
	50 50 49 52 52 52 48 48 51 50 49	50 50 51 48 50 49 49 49 52 49 52 48 52 49 48 48 48 49 51 51 50 50 49 47	50 50 54 51 48 48 50 49 51 49 49 47 52 49 49 52 48 48 52 49 45 48 48 49 48 49 52 51 51 49 50 50 50 50 50 53 49 47 51 51 49	50         50         54         51.3           51         48         48         49.0           50         49         51         50.0           49         49         47         48.3           52         49         49         50.0           52         48         48         49.3           52         49         45         48.7           48         48         49         45.3           48         49         52         49.7           51         51         49         50.3           50         50         53         51.0           49         47         51         49.0	50         50         54         51.3         565           51         48         48         49.0         649           50         49         51         50.0         736           49         49         47         48.3         823           52         49         49         50.0         910           52         48         48         49.3         997           52         49         45         48.7         1084           48         48         49         48.3         1171           48         49         52         49.7         1258           51         51         49         50.3         1345           50         50         53         51.0         1432           49         47         51         49.0         1519           51         47         49         49.0         1606	50         50         54         51.3         565         4.83           51         48         48         49.0         649         4.78           50         49         51         50.0         736         4.86           49         49         50.0         736         4.86           49         49         50.0         910         4.84           52         49         49         50.0         910         4.84           52         48         48         49.3         997         4.83           52         49         45         48.7         1084         4.79           48         48         49         48.3         1171         4.75           48         49         52         49.7         1258         4.86           51         51         49         50.3         1345         4.82           50         50         53         51.0         1432         4.78           49         47         51         49.0         1519         4.80           51         47         49         49.0         1606         4.83	50         50         54         51.3         565         4.83         4.83           51         48         48         49.0         649         4.78         4.85           50         49         51         50.0         736         4.86         4.81           49         49         47         48.3         823         4.77         4.83           52         49         49         50.0         910         4.84         4.86           52         48         48         49.3         997         4.83         4.82           52         49         45         48.7         1084         4.79         4.90           48         48         49         48.3         1171         4.75         4.77           48         49         52         49.7         1258         4.86         4.81           51         51         49         50.3         1345         4.82         4.80           50         50         53         51.0         1432         4.78         4.77           49         47         51         49.0         1519         4.80         4.78           51         47 <td>50         50         54         51.3         565         4.83         4.83         4.77           51         48         48         49.0         649         4.78         4.85         4.82           50         49         51         50.0         736         4.86         4.81         4.76           49         49         50.0         736         4.84         4.83         4.81           52         49         49         50.0         910         4.84         4.86         4.81           52         48         48         49.3         997         4.83         4.82         4.82           52         49         45         48.7         1084         4.79         4.90         4.90           48         48         49         48.3         1171         4.75         4.77         4.89           48         49         52         49.7         1258         4.86         4.81         4.77           51         51         49         50.3         1345         4.82         4.80         4.81           50         50         53         51.0         1432         4.78         4.77         4.78</td>	50         50         54         51.3         565         4.83         4.83         4.77           51         48         48         49.0         649         4.78         4.85         4.82           50         49         51         50.0         736         4.86         4.81         4.76           49         49         50.0         736         4.84         4.83         4.81           52         49         49         50.0         910         4.84         4.86         4.81           52         48         48         49.3         997         4.83         4.82         4.82           52         49         45         48.7         1084         4.79         4.90         4.90           48         48         49         48.3         1171         4.75         4.77         4.89           48         49         52         49.7         1258         4.86         4.81         4.77           51         51         49         50.3         1345         4.82         4.80         4.81           50         50         53         51.0         1432         4.78         4.77         4.78

# Analysis of variance table for uranium

Source of variation		Degrees of freedom	Mean square
Between bottles		18	3,595
Within bottles		38	3.614
Total		.56	
Calculated F statistic	c =	0.995	
F.95 (18,38)	==	1.883	
Null hypothesis of nuranium	c differen	ice between bottles is	accepted for

Source of variation	Degrees of freedom	Mean square
Between bottlas	18	2.645 × 10 <sup>-3</sup>
Within bottles	38	$1.861 \times 10^{-3}$
Total	56	
Calculated F statistic =	1,421	
F.95 (18,38) ==	1,883	
Null hypothesis of no differe	nca between bottle	s is accepted for iron

Table 5a - Confirmation of homogeneity of UTS-2 for uranium

Table 5b - Confirmation of homogeneity of UTS-2 for total iron

		Urani	um (µg/g)				Total i	ron (%)	
Bottle No.		Individual		Mean	Bottle No.		Individual		Mean
72	53	54	55	54.0	72	3.05	3.05	3.14	3.08
159	52	53	56	53.7	159	3.05	3.07	3.15	3.10
246	50	57	58	55.0	246	3.09	3.12	3.05	3.09
333	55	56	54	55.0	333	3.07	3.09	3.14	3,10
420	55	55	55	55.0	420	3.11	3.08	3.01	3.07
507	57	57	54	56.0	507	3.04	3.05	3.08	3.06
594	56	57	55	56.0	594	3.09	3.09	3.05	3.08
681	55	56	55	55.3	681	3.03	3.13	3.05	3.07
768	54	56	57	55.3	768	3.04	3.08	3.09	3.07
B55	55	55	57	55.7	855	3.09	3.03	3.04	3.05
942	57	57	55	56.3	942	3.10	3.13	3.19	3.14
1029	55	56	58	55.7	1029	3.15	3.15	3.12	3.14
1116	55	54	55	54.7	1116	3.11	3.10	3.04	3.08
1203	54	56	54	54.7	1203	3.10	3.12	3.11	3.11
1290	54	55	57	55.3	1290	3.05	3.16	3.07	3.09
1377	56	56	55	55.7	1377	3.12	3.07	3.14	3.11
1464	54	57	56	55.7	1464	3.06	3.07	3.10	3.08
1551	56	55	57	56.0	1551	3.08	3.13	3.07	3.09
1638	56	53	54	54.3	1638	3.07	3.04	3.06	3.06

# Analysis of variance table for uranium

Source of variation		Degrees of freedom	Mean square
Between bottles		18	1.558
Within bottles		38	2.368
Total		56	
Calculated F statisti	c =	0.658	
F.95 (18,38)	=	1.883	
Null hypothesis of n	a differen	ce between bottles is	accepted for

Source of variation	Degrees of freedom	Mean square
Between bottles	18	$1.888 \times 10^{-3}$
Within bottles	38	$1.349 \times 10^{-3}$
Total	58	
Calculated F statistic =	1.400	
F.95 (18,38) =	1.883	
Null hypothesis of no differe	nce between bottle	s is accepted for iron

Table 6a - Confirmation of homogeneity of UTS-3 for uranium

Table 6b - Confirmation of homogeneity of UTS-3 for total iron

	976 7 1000	Uranium (%)				Total iron (%)			
Bottle No.		Individual		Mean	Bottle No.		Individual		Mean
43	.0513	.0515	.0519	.0516	43	3.15	3.17	3.18	3.17
130	.0517	,0522	.0527	.0522	130	3.20	3.15	3.11	3.15
217	.0513	.0500	,0501	.0505	217	3.16	3.10	3.13	3.13
304	.0521	.0485	0494	.0500	304	3.07	3.10	3.11	3.09
391	.0507	,0521	.0520	.0516	391	3.13	3.07	3.14	3.11
478	.0506	.0513	0518	.0512	478	3.10	3.05	3.13	3.09
565	.0515	.0521	0497	.0511	565	3.06	3.05	3.08	3.06
652	.0516	.0521	.0513	.0517	652	3.09	3.08	3.06	3.08
739	.0517	,0510	.0524	.0517	739	3.20	3.20	3.13	3.15
826	.0517	.0502	.0497	,0505	826	3.15	3.11	3.15	3.14
913	.0511	0518	.0515	.0515	913	3 13	3.15	3.15	3.14
1000	.0505	.0518	.0507	.0510	1000	3,19	3.15	3.10	3.15
1087	.0508	.0504	.0518	.0510	1087	3.06	3.16	3.14	3.12
1174	.0517	.0510	.0511	.0513	1174	3.09	3.11	3.14	3.11
1261	.0518	.0514	.0512	.0516	1261	3.10	3.06	3.10	3.09
1348	.0531	.0613	.0510	.0518	1348	3.12	3.19	3,16	3.16
1435	.0513	.0522	.0521	.0519	1435	3.14	3.07	3.10	3.10
1522	.0513	.0497	.0497	.0502	1522	3.13	3.15	3.13	3.14
1609	.0517	,0525	.0518	.0520	1609	3,13	3.10	3.10	3.11
			(48) W						

Overall mean = .0513

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Overall mean = 3.12

# Analysis of variance table for uranium

	freedom	Mean square
	18	$1.117 \times 10^{-6}$
	38	6.628 × 10 <sup>-7</sup>
	56	
=	1.685	
=	1.883	
differ	enco between co	ttles is accepted for
	=	18 38 56 = 1.685

Source of variation	Degrees of freecom	Mean square
Between bottles	18	$2.960 \times 10^{-3}$
Within bottles	38	9.649 × 10-4
Total	56	
Calculated F statistic =	3.068	
F.95 (18,38) =	1.883	
Null hypothesis of no differ	ence between bottle	ss is rejected for iron

Table 7a - Confirmation of homogeneity of UTS-4 for uranium

Table 7b - Confirmation of homogeneity of UTS-4 for total iron

			um (%)			Total iron (%)			
Battle Na.	535000	Individual		Mean	Bottle No.	-	Individual		Mean
51	1079	.1076	.1057	.1071	51	2.64	2.61	2.63	2.63
119	1057	.1069	.1056	.1061	119	2.63	2.61	2.58	2.61
187	.1068	.1069	.1076	.1071	187	2.62	2.62	2.60	2.61
255	.1063	.1055	.1054	.1057	255	2.57	2.59	2,60	2.59
323	.1019	.1051	.1063	.1044	323	2.58	2.59	2.66	2.57
391	,1064	.1065	.1048	.1059	391	2.58	2.60	2.58	2.59
459	.1060	.1060	.1077	.1066	459	2.56	2.55	2.59	2.57
527	.1092	.1065	.1078	.1078	527	2.58	2.57	2.59	2.58
595	.1060	.1082	.1065	.1069	595	2.55	2.58	2.60	2.58
663	.1060	.1075	.1036	.1057	663	2.59	2.61	2.62	2.61
731	.1076	.1064	.1066	.1069	731	2.59	2.61	2.63	2.61
799	.1067	.1045	.1066	.1059	799	2.63	2.61	2.61	2.62
867	.1045	.1060	.1063	.1056	867	2.84	2.62	2.60	2.62
935	,1064	.1066	.1068	.1066	935	2.65	2.60	2.58	2.61
1003	.1063	.1072	.1058	.1064	1003	2.59	2.60	2.57	2.59
1071	.1075	,1051	.1078	.1068	1071	2.59	2.61	2.62	2.61
1139	.1070	.1069	.1065	.1068	1139	2.61	2.63	2.63	2.62
1207	.1071	,1056	.1065	.1064	1207	2.61	2.58	2.58	2.59
1275	.1062	.1059	.1043	.1055	1275	2.61	2.61	2.64	2.62

Analysis of variance table for uranium

Source of variation	Degrees of freedam	Mean square
Between bottles	18	$1.772 \times 10^{-8}$
Within bottles	38	$1.250 \times 10^{-6}$
Total	56	
Calculated F statistic =	1.418	
F.95 (18,38) =	1.883	
Null hypothesis of no diffe cranium	erence between bo	ttles is accepted for

Source of variation	Degrees of freedom	Mean square
Between bottles	18	1.040 × 10 <sup>-3</sup>
Within bottles	38	3.491 X 10-4
Total	56	302000001513M 750000
Calculated F statistic =	2.980	
F.95 (18,38) =	1.883	
Null hypothesis of no differe	ende between bottle	as is rejected for iron