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ION FOR PART 50 DOCKET MATERIA (TEMPORARY FORM)

CONTROL NO: 5152

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Carolina Power &	Light Company [©]					1		UTILIK	
Raleigh, N. C.	27602								
E. E. Utley	,	6-4-74	6-	10-74	x				
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Carolina Power & Light Company

June 4, 1974

File: NG-3514

Serial: NG-74-692

Mr. John F. O'Leary, Director Directorate of Licensing Office of Regulation U. S. Atomic Energy Commission 50 - 261Washington, D. C. 20545

Dear Mr. O'Leary:

U.S. ATOMIC FREBAY COMMISSION Regulatory Mail Section

5152

H. B. Robinson Unit No. 2 License DPR-23 Additional Information in Support of 2300 MWt Uprating

During the preparation of the staff evaluation report for the uprating of H. B. Robinson Unit No. 2, Carolina Power & Light Company was requested to supply additional information to allow a recalculation of the off-site population dose due to the design basis accident. By copy of this letter, the information requested is formally submitted to the Atomic Energy Commission.

The staff requested additional information concerning the operation and performance of the core spray system during the postaccident phase, as well as a calculation of containment volumes reached by the spray and an evaluation of the effectiveness of forced mixing in compartments not directly contacted by the spray droplets.

The core spray system information is presented below:

- 1. Spray system flow rate 1161 gpm (both injection and recirculation) (Page 6.4-5 FSAR)
- Spray pH 9.1 during injection
 9.0 initial during recirculation
- 3. ECCS flow 7125 gpm (Table 6.2-7 FSAR)

Length of injection phase - 42 minutes

Refueling water storage tank volume (minimum usable) - 350,000 gal. (Table 6.2-6 FSAR)

Spray additive tank volume (minimum usable) - 2505 gal. (Table 6.4-3 FSAR)



336 Fayetteville Street • P. O. Box 1551 • Raleigh, N. C. 27602

Mr. John F. O'Leary

June 4, 1974

7. Spray additive flow rate - 12 gpm (Table 6.4-2 FSAR)

8. Minimum final sump pH - 8.6

Additional information on the core spray system operation and its effectiveness in reducing iodine concentrations inside containment may be found in Section 6.4 and 14.3.4 of the FSAR.

The values of 1161 gpm recirculation spray flow rate and initial recirculation spray pH of 9.0 are inconsistent, since the value of 1161 gpm was chosen as a conservative estimate of flow rate for lack of a detailed analysis of the recirculation spray system. The flow rate will be higher due to the increased suction head on the spray pumps during recirculation. The pH value of 9.0 is based on an estimate of 1500 gpm spray flow rate and 12 gpm spray additive flow during recirculation. These assumptions provide a conservative estimate for spray system performance during the recirculation phase.

The containment volumes for each region of the containment is presented below. The corresponding letter designation for each region is obtained by reference to the attached figure. Also presented is the information concerning forced mixing in each of the regions.

Region	Volume (ft ³)	Air Changes/hour
А	5.78×10^{5}	0
В	9.94×10^{5}	7.8
С	1.35×10^{5}	5.3
D	1.28×10^{5}	1.65
E	2.64×10^{2}	27.0

The air change information is based on a study of the fan cooler system, and assumes that only two out of the four fan coolers (each rated at 65,000 cfm) are operating. Thus, forced mixing in the containment and especially in regions C, D and E, which see somewhat less than full penetration by falling spray droplets, is considered to be sufficient to allow the complete containment atmosphere to be affected by the iodine removal capabilities of the spray.

DBW:mvp Attachment

cc: Messrs. N. B. Bessac T. E. Bowman

- B. J. Furr
- W. E. Graham
- D. V. Menscer
- D. B. Waters
- R. A. Watson

Yours very truly, E./E. Utley

Vice-President Bulk Power Supply



H. B. ROBINSON - CONTAINMENT OUTLINE