



J U D I T H L . H A M I L T O N

Consulting Geologist and Engineer

GROUND - WATER AND ENGINEERING GEOLOGY

2220 Julian Street • Denver, Colorado • 80211 • (303) 455-4354

August 31, 1977

Mr. Al Stoick
Nuclear Dynamics, Inc.
200 S. Lowell
Casper, Wyoming 82601

Dear Al:

Enclosed is my report on the hydrogeologic conditions in the vicinity of your proposed in-situ leaching site near Oshoto, Wyoming. This report gives the information required by the Wyoming Department of Environmental Quality and describes the 72-hour pumping test.

A copy of Plate I is enclosed. You might want to check the ground surface elevation contour lines or the elevation of hole 797V as there appears to be a discrepancy. The hole is located between contour lines 4198 and 4200 but the ground surface elevation as given on the cross section is 4195.7. Plates II and III are your cross section of holes and your table of hole construction information.

If you have any questions or need additional information for this report, please let me know.

Sincerely,

Judith L. Hamilton

cc; Tom Melrose



J U D I T H L . H A M I L T O N

Consulting Geologist and Engineer

G R O U N D - W A T E R A N D E N G I N E E R I N G G E O L O G Y

2220 Julian Street • Denver, Colorado • 80211 • (303) 455-4354

HYDROLOGIC INFORMATION
VICINITY PROPOSED IN-SITU
URANIUM LEACHING SITE
OSHOTO, WYOMING

August 30, 1977

SUMMARY

Items 6a thru 6f of Supportive Information Handout, Wyoming DEQ, March 18, 1977:

6a. Piezometric surface (see Plate I)

Sand zone A (aquifer overlying production aquifer) - elevation 4127 to 4130 feet.

Sand zone B (production aquifer) - elev. 4082 to 4087 feet.

6b. Transmissivity - sand zone B: 126.1 to 172.1 gallons per day per foot based on 72-hour pumping test.

6c. Hydraulic conductivity (permeability) - 1.06 to 1.39 gallons per day per square foot based on 72-hour pumping test.

6d. Porosity of production zone - 19.6% to 37.8% in production zone aquifer (sand zone B); 19.6% to 28.6% in mineralized zone, based on core analyses for hole 477V (see Table 1).

6e. Water level conditions of aquifers

Sand zone A (below depth of 240-250 feet) - head approximately 160 to 185 feet above top of aquifer A (static water level 58 to 77 feet below ground surface).

Sand zone B - head 332 to 334 feet above top of aquifer (static water level 102 to 116 feet below ground surface).

Head in sand zone A approximately 45 feet above head in sand zone B.

Upper sand zone (0 to 100 feet)- water table conditions; water levels 36 to 80 feet below ground surface.

6f. Degree of hydraulic connection between aquifers - no leakage between sand zone A and sand zone B.

DESCRIPTION OF FIELD TESTS

Aquifer parameters for the vicinity of the proposed in-situ uranium leaching test site were determined from a 72-hour pumping test on a well constructed in the production zone aquifer (sand zone B) and from water level measurements in three observation holes in the same aquifer, located at distances of 53.7 to 94.0 feet from the pumped well. In addition, water level measurements were made before, during and after pumping tests, in four holes terminating above the production zone aquifer and separated from it by a clay-shale layer about ten feet thick. Water levels in a third set of 4 holes, 100 feet deep each, were also observed before, during and after pumping of the well.

Construction details of the well (hole 789V) and the observation holes are shown on Plates II and III.

The 72-hour pumping tests was begun at 11:45 A.M. Monday, August 1, 1977. A 7½ HP Flint and Walling 3-phase, 460-volt pump, type 75FF18 was used, with an intake depth of 404 feet. Static water level in the well as measured with electrical-type water level probe was 112.8 feet below ground surface and as measured with the air line was 111.9 feet below surface.

The well was pumped at an average rate of 10.04 gallons per minute (gpm), with a general range in rate from 9.9 to 10.1 gpm. Occasional short-term decreases or increases occurred. Rate of water flow was determined periodically by observation of the water flow meter rate and readings. A valve permitted adjustment to maintain the rate as close to 10 gpm as possible. Water levels in the well were measured

with both the electrical probe and the air line for 300 minutes, at which time the probe caught in the pump cable and could no longer be used. Water levels in the observation holes were measured with electrical probes.

Data on the test for the well and holes 788V, 791V and 797V are given in Appendix A-1. Water level observations for holes 3V, 5V and 9V (perforated about 250 to 450 feet and cemented above), hole 1067 (cemented to 241 feet, open hole 241 to 451 feet) and for 100-foot holes 790V, 797V, 795V, and 796V are given in Appendix A-2.

DETERMINATION OF AQUIFER PARAMETERS

Piezometric surface of production area aquifers. Water level elevations were determined by subtracting the depth of water below ground surface from the elevation of the ground at that point as determined by surveying. Contours for sand zone A (aquifer above the production zone) and sand zone B (production zone aquifer) are shown on Plate I. Since the points used in drawing the contours are close together and the differences in water level elevations are small, these contour lines may not be completely representative of regional water flow.

Transmissivity and storage coefficient. Results of the 72-hour test were analysed by the Jacob method for the well and by both the Jacob method and the Theis non-equilibrium method for the observation holes, to obtain transmissivities and storage coefficients. Plots for the well (787V) are shown on Figure 1, and for observation holes 788V on Figures 2 and 3, 791V on Figures 4 and 5 and 797V on Figures 6 and 7. A distance-drawdown curve is shown

on Figure 8. Results obtained for the different holes and methods are given below:

		Well	Observation holes			Distance-	
		789V	788V	791V	797V	DD curve	
T	gpd/ ft	Jacob Method	125.0*	172.1	162.6	140.2	169.9
		Pumping	121.6				
S		Recovery	138.1	160.6	164.6	132.5	
		Theis Method		143.8	158.9	125.9	
S		Jacob Method		.000062	.000096	.00020	.000078
		Pumping					
		Recovery		.000058	.00010	.00019	
		Theis Method		.000085	.000099	.00024	

* 300 minutes only

Parameters derived by the Theis formula were obtained by matching to the standard $W(u)$ vs. u curve for a non-leaky aquifer with a fully penetrating well and constant discharge (see Appendix A-3 for copies of these standard curves from Walton, Figure 4.2 and Table 3.1 and Todd, Figure 4.9). Graphs were plotted by Todd's method (s vs. r^2/t) rather than Walton's (s vs. t) for comparison to a $W(u)$ vs. u rather than $1/u$ standard curve.

Hydraulic conductivity (permeability). Permeabilities were obtained by dividing the transmissivity obtained in each hole by the aquifer thickness for that hole. Aquifer thickness was taken as the distance between the bottom of the shale layer above which the hole was cemented and the top of the Pierre shale. Results are shown below:

Hole No.	Transmissivity gpd/ft.	Aquifer thickness ft.	Permeability gpd/ft ²
788V	143.8 ^a	121	1.19
789V (well)	138.1 ^b	118	1.17
791V	158.9 ^a	114 ^c	1.39
797V	125.9 ^a	119	1.06

^abased on 72-hour test, using Theis method

^bbased on 72-hour test, using Jacob method (recovery)

^cbottom 10 ft. above top of Pierre shale

Porosity of the production zone. Porosity analyses were made by Core Laboratories, Inc. on cores from the production aquifer from hole 477V. This hole is located 162 feet east of the well 789V (see Plate III for location). Results of the analyses are shown on Table 1.

Artesian or non-artesian conditions of aquifers. Water level measurements indicate that water in sand zones A and B are well above the top of the aquifer, indicating artesian conditions. It is probable that water levels in the 100-foot deep holes represent local perched water tables because of the variations in depth.

Head in sand zones A and B was determined by subtracting the depth to water from the depth to the top of the aquifer. For zone B, the top of the aquifer was taken as the bottom of the shale zone above which the hole is cemented. For zone A, the top of the aquifer is taken as the bottom of the upper cement.

Degree of hydraulic connection between aquifers. The time-drawdown curves for observation holes 788V, 791V and 797V compare well in shape with the standard $W(u)$ vs. u curve for a non-leaky artesian aquifer (see Appendix A-3). It was therefore determined that the aquifer was non-leaky. Had leakage occurred, curves corresponding to those shown in Walton, Figure 4.8 or 4.11, would have been obtained (see Appendix A-3 for copies of these curves). The lack of drawdown in holes 5V and 9V, which are separated from the tested aquifer by only a ten-foot layer of clay-shale, confirm the lack of leakage. The small amount of drawdown which occurred in hole 3V

is believed to be due to downward leakage around the cement seal when the pressure from zone B was reduced, rather than leakage thru the clay layer itself.

The water levels for sand zone A are probably a composite head for various sand layers in that zone since several thick clay-shale layers exist within the perforated zone. Since zone A is not hydrologically connected to the production zone, variations in head among the different layers would not be significant to the leaching program. The piezometric surface in sand zone A is considerably higher than in sand zone B (production aquifer), on the order of 45 feet. In the unlikely event that any leakage would occur, direction of flow under natural conditions would be downward from zone A to zone B.

Respectfully submitted,

Judith L. Hamilton

Judith L. Hamilton, P.E.
Ground-water geologist

REFERENCES

Todd, David Keith, 1959. Ground Water Hydrology. John Wiley and Sons, 336 pages.

Walton, William C., 1970. Groundwater Resource Evaluation. McGraw-Hill, Inc. 664 pages

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
 DALLAS, TEXAS

Company NUCLEAR DYNAMICS Formation UNKNOWN Page 1 of 1
 Well 477Y Cores UNKNOWN File RP-4-3943
 Field UNKNOWN Drilling Fluid UNKNOWN Date Report 2-7-77
 County UNKNOWN State UNKNOWN Elevation UNKNOWN Analysts KEN BOWEN
 Location UNKNOWN Remarks _____

CORE ANALYSIS RESULTS
(Figures in parentheses refer to footnote remarks)

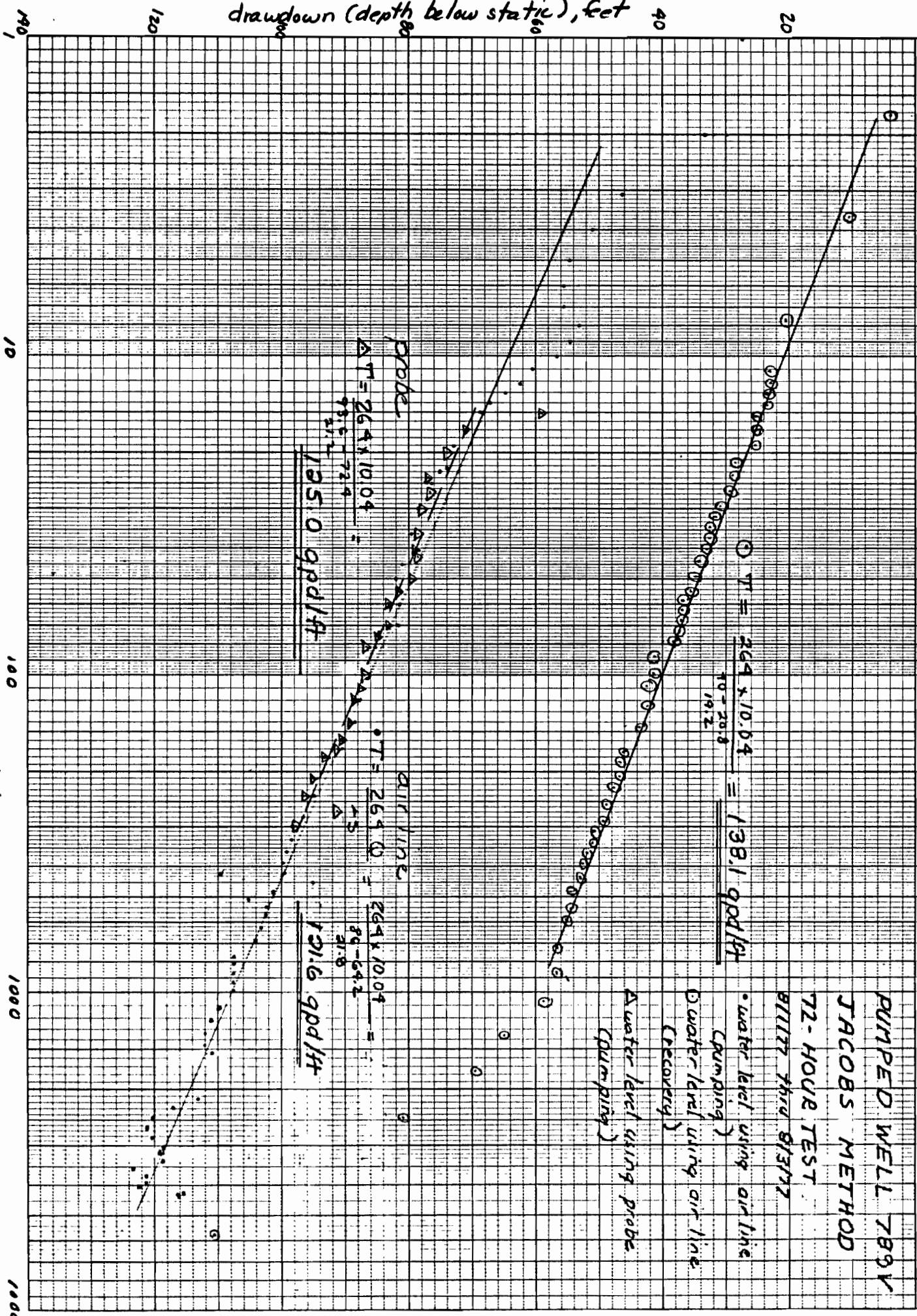
SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY		POROSITY PERCENT	RESIDUAL SATURATION		PROBABLE PRODUCTION	REMARKS
		HORIZONTAL	VERTICAL		OIL % VOLUME % PORE	TOTAL WATER % PORE		
1.	482.5	1.5	.01	24.1				
2.	490.6	38	5.0	27.8				
3.	500.0	1934	1915	34.0				
4.	506.5	2253	1239	37.8				
5.	507.0	1971	184	35.6				
6.	508.0	317	161	32.8				
7.	511.0	3380	2160	36.2				
8.	517.0	3944	2892	28.6			} Mineralized zone	
9.	524.0	51	34	19.6				
10.	531.0	254	223	27.6				
11.	543.0	2629	2291	36.4				
12.	544.0	14	.90	29.8				
13.	557.0	1606	403	32.2				
14.	573.0	8.8	.01	25.9				

TABLE 1

NOTE:
 (*) REFER TO ATTACHED LETTER.
 (1) INCOMPLETE CORE RECOVERY—INTERPRETATION RESERVED.
 (2) OFF LOCATION ANALYSES—NO INTERPRETATION OF RESULTS.

These analyses, opinions or interpretations are based on observations and materials supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc. (all errors and omissions excepted); but Core Laboratories, Inc., and its officers and employees, assume no responsibility and make no warranty or representations, as to the productivity, proper operation, or profitability of any oil, gas or other mineral well or sand in connection with which such report is used or relied upon.

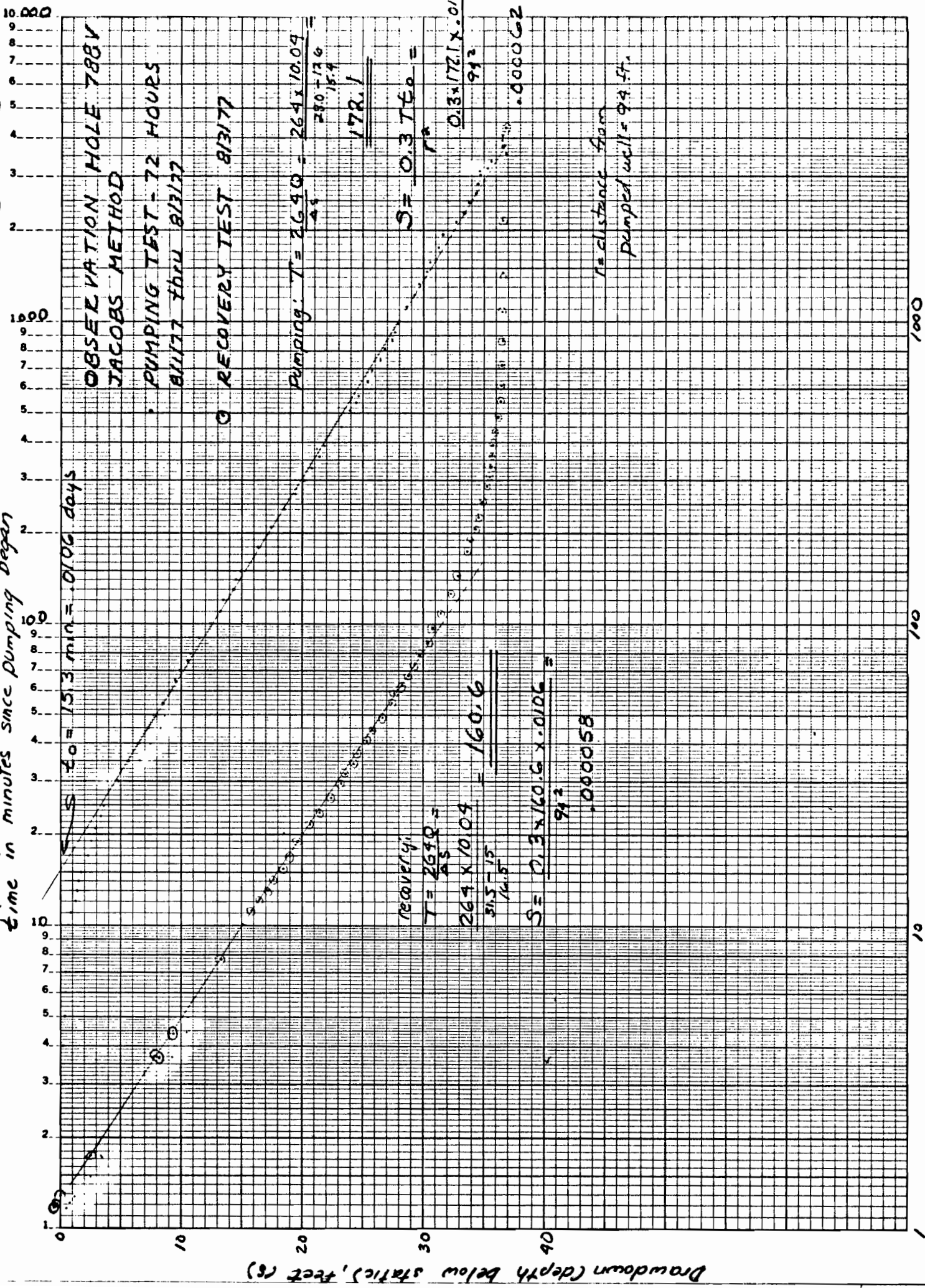
time in minutes since pumping began



Recovery 7/71

Figure 1

time in minutes since pumping began

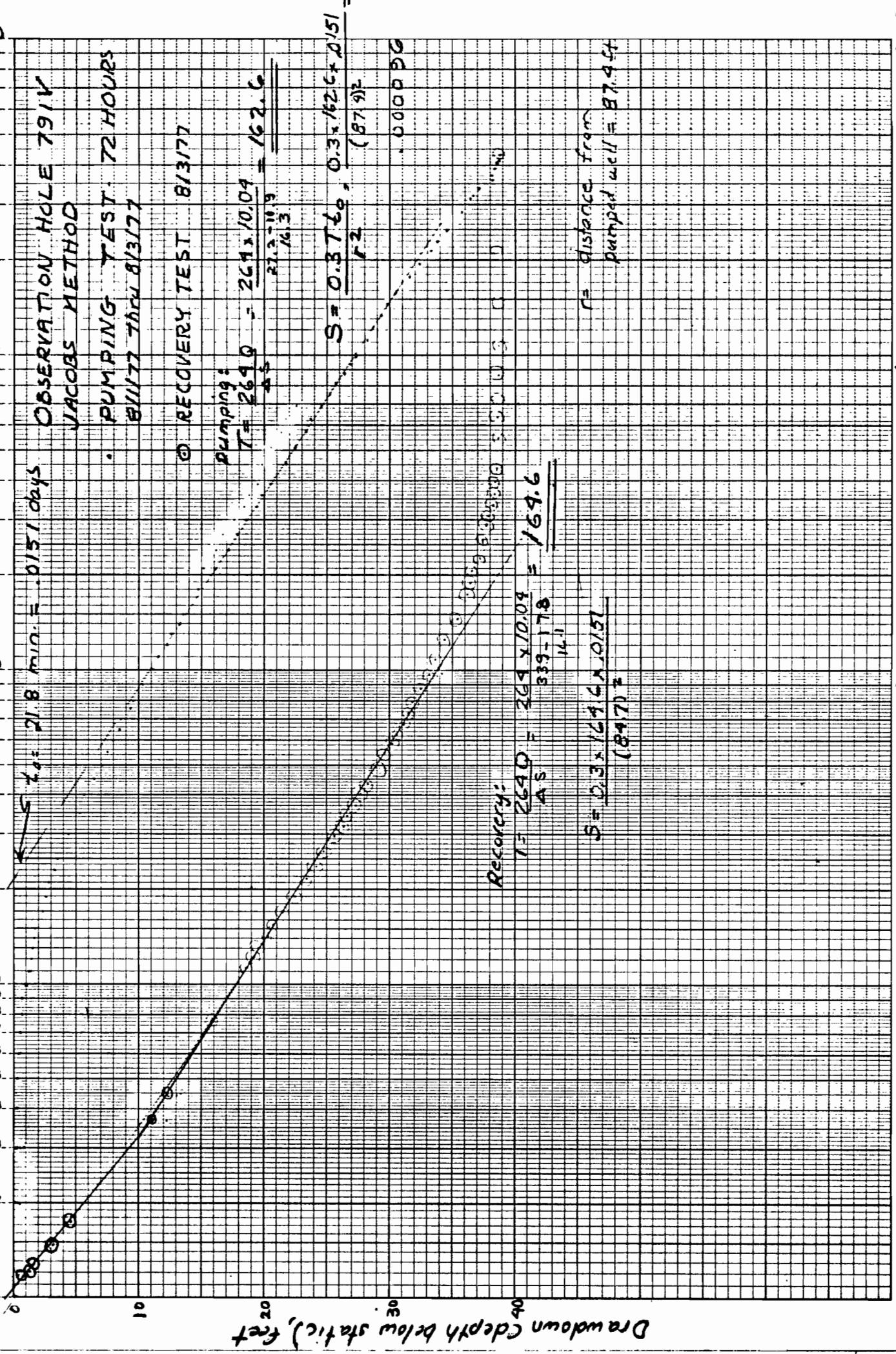


Recovery. t/t'

Figure 2

46 6010

Time in minutes since pumping began



10000

1000

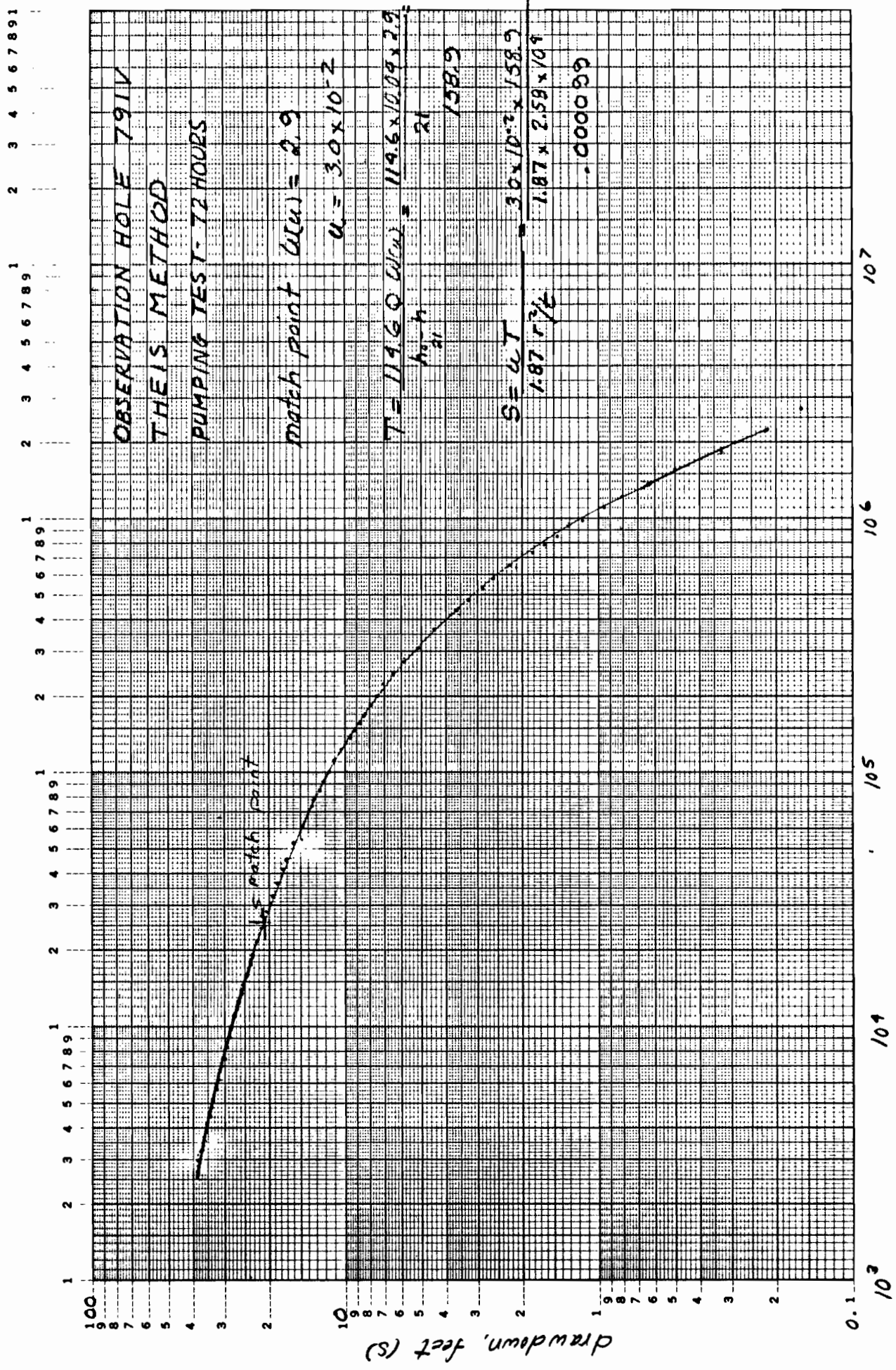
100

10

1

Recovery - t/t'

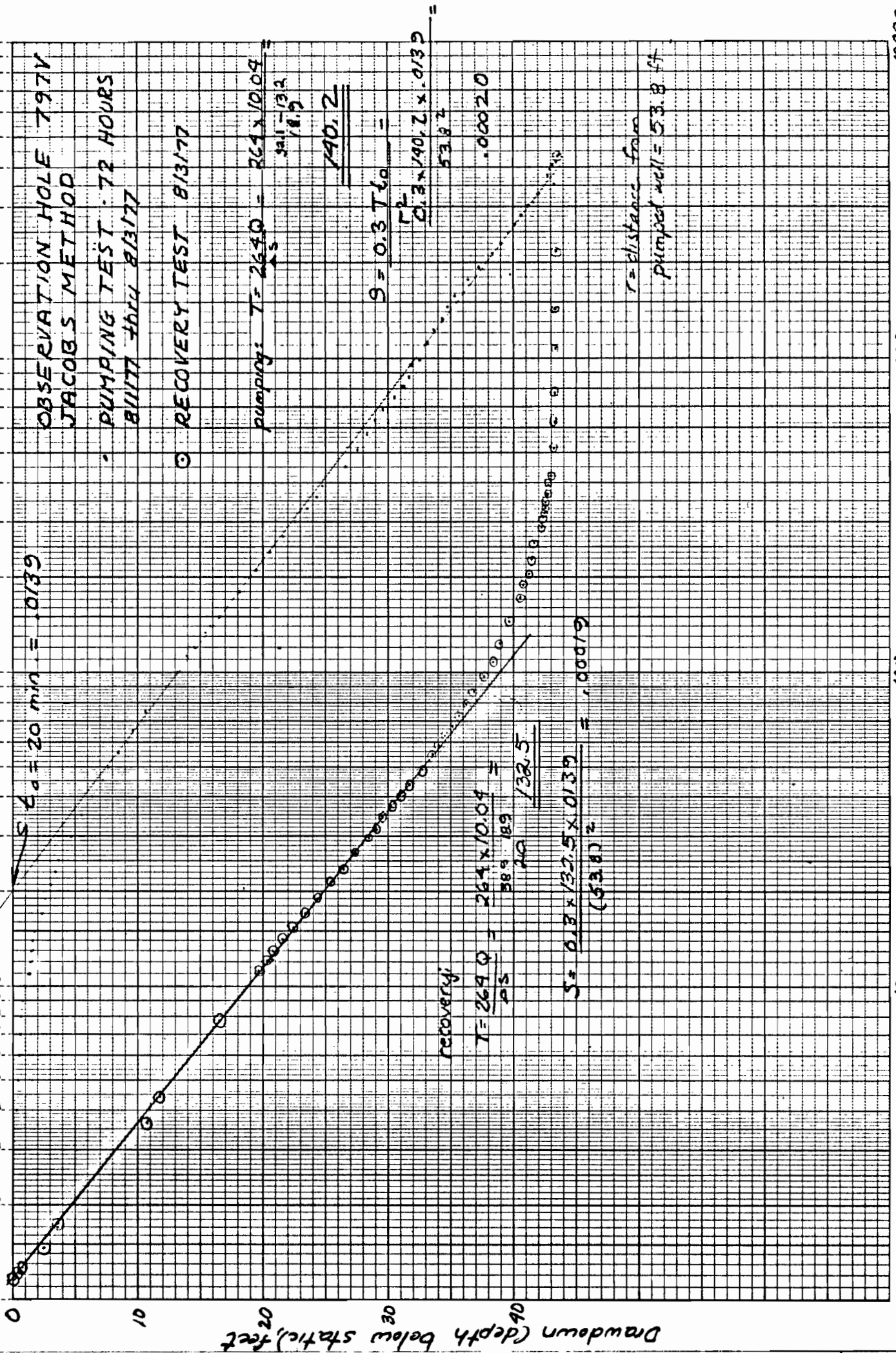
Figure 4



r^2/k

Figure 5

time in minutes since pumping began



OBSERVATION HOLE 797V
 JACOBS METHOD
 PUMPING TEST: 72 HOURS
 BUILT thru 8/13/77

RECOVERY TEST 8/31/77

pumping: $T = 264 \times 10.09$
 58.9×189

$S = 0.3 T \frac{Q}{r^2}$
 $\frac{0.13 \times 140.2 \times 0.139}{53.8^2}$

$r = \text{distance from pumped well} = 53.8 \text{ ft}$

Recovery test

OBSERVATION HOLE 797V

THEIS METHOD

PUMPING TEST - 72 HOURS

match point $W(u) = 2.9$

$u = 3.0 \times 10^{-2}$

$$T = \frac{114.6 Q W(u)}{h \cdot h} = \frac{114.6 \times 1009 \times 2.9}{86.5} = \underline{\underline{385.9}}$$

$$S = \frac{c T}{1.87 r^2} = \frac{503 \times 135.9}{1.87 \times 8.9 \times 10^3} = \underline{\underline{.000245}}$$

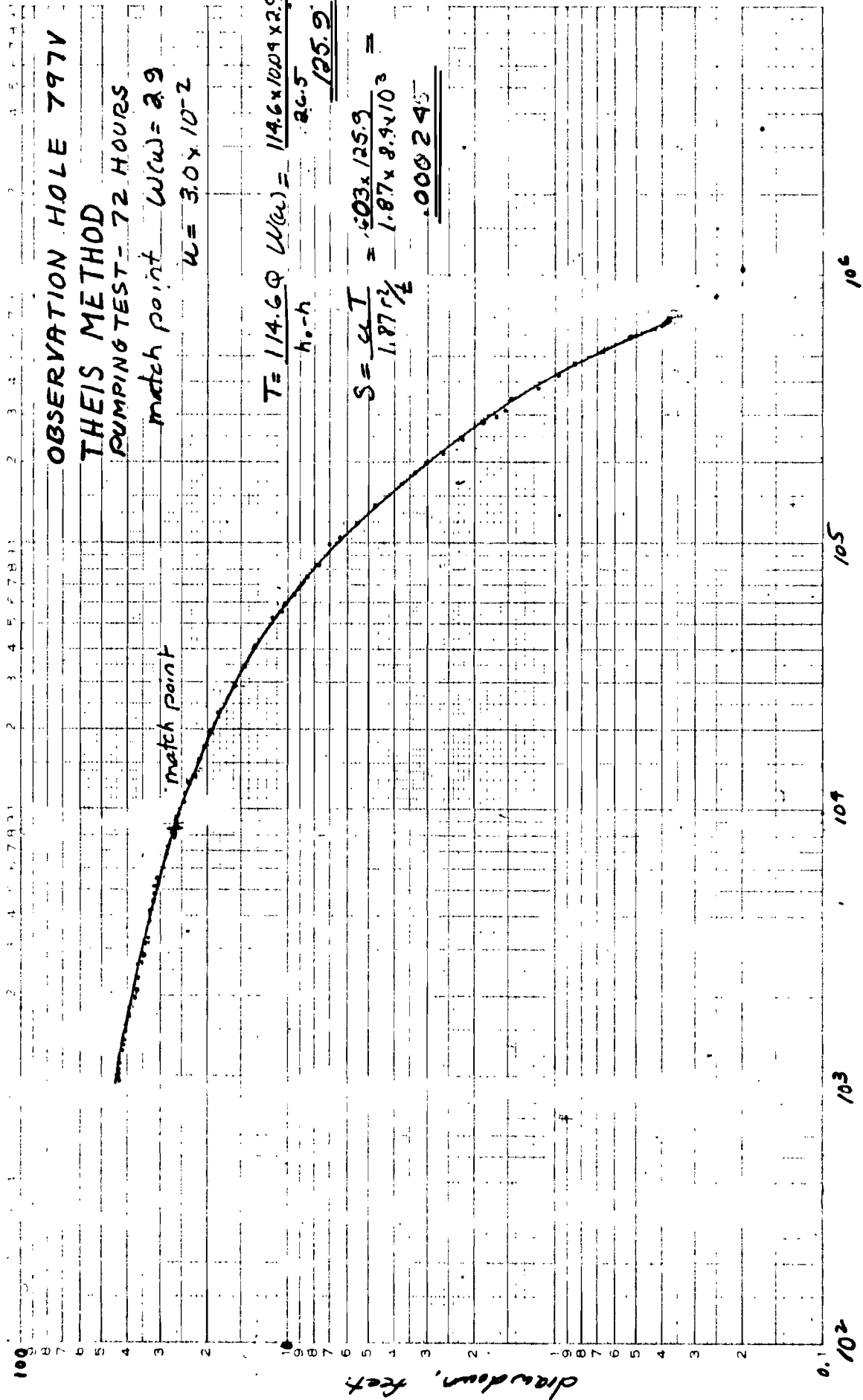
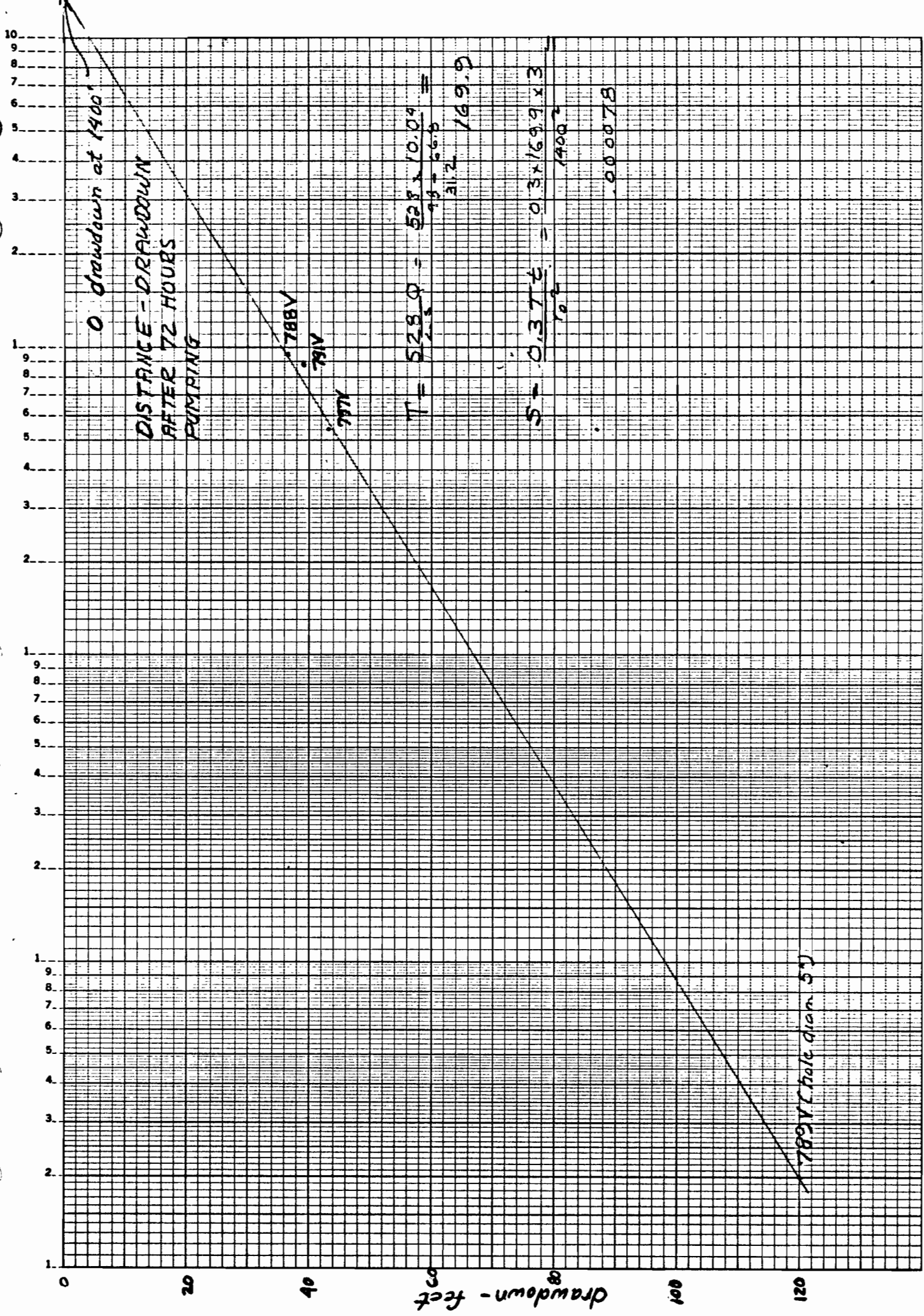


Figure 7



1000
100
10
1.0
0.1

distance from pumped well - feet

APPENDIX A-1

PUMPING TEST 8/1/77
72 hours
10 gpm

789 V

JUDITH L. HAMILTON
 Consulting Geologist and Engineer
 2220 Julian St. Denver, Colo. 80211

PUMPING TEST RESULTS

Client: NuBeth Location: Oshkoto, Wyo. Date: 8/11/77

Job No.: Hole No.: 789V T.D.: Ground elev.: ft
 Pump data: 5 h.p. 460 volt 3 phase; Make: Burks Depth Set:
 Static water level: 112.8 ft. below G.S./M.P. Meas. point: 1.0 ft. above G.S.
 Start of Test: 11:44:45 AM/PM Pumping/Recovery Air Line Depth: 999.5

Time	Time in min. from start of pumping		t/c	water depth (ft)		Air Line			pumping rate		Comments	
	to	to		below meas. pt.	below static	gauge pressure lbs	= feet	depth below M.P. ft	depth below static (ft)	sec/gal.		gpm (timed)
11:17				112.8		109	256.9	113.1				65.50 ± meter
11:43						109.5	277.6	111.9				
11:44:45												
	1	6:44:10	4			112.5	259.1	139.6	27.7			
	2	1:39:10	3			110.0	254.1	145.1	33.5			
	3:0	2:15:10	3			104.5	241.4	158.1	46.2			
	4	2:48:10	3	128' 9"		102.5	236.8	162.7	50.8	10.5		
	5	3:47:10				101	233.3	166.2	54.3			
	6	4:17:10		132' 9"		100.5	232.2	167.3	55.4			
	7	4:46:10				100.5	232.2	167.3	55.4			
	8	5:56:10				101.5	234.5	165.0	53.1	<10		
	9	6:25:10				101	233.3	166.2	54.3			
	10	7:49:10		172:20	58.4	100	231.0	168.5	56.6			
	11	7:61:10				98.5	227.5	172.0	60.1			
	12:0	8:40:10				97.5	225.2	174.3	62.4			
	13	9:03:10				96.5	222.9	176.6	64.7	10.1		
	14	9:72:10				95.5	220.6	178.9	67.0			
	15	1:04:10	2	173:4"	59.5	95	219.5	180.0	68.1			
	17	1:18:10		151:75	70.9							
	19	1:32:10				93.0	214.8	184.7	72.8			
	20	1:39:10		187:10"	74.0							
	22:0	1:56:10				92.5	213.7	185.8	73.9			
	23	1:60:10				92.0	212.5	187.0	75.1			
	24	1:67:10		190:0"	77.0					10.2		
	25	1:74:10				91.5	211.4	188.1	76.2			
	26:0	1:84:10		190:1/2"	76.3							
	30	2:03:10		191:9"	77.9	90.5	209.1	190.4	78.5	10.6		
	36	2:52:10		192:1 1/2"	78.3	90.0	207.9	191.6	79.7	10.7		
	40:4	2:83:10		192:9/2"	79.0	90.5	209.1	190.4	78.5	9.4	40	694.9 meter
	45	3:13:10		192:2 3/4"	78.4	89.5	206.7	192.8	80.9			
	47:0	3:30:10								10.1		
	50	3:47:10		193:6"	79.7	89.0	205.6	193.9	82.0	10.0		
	55	3:22:10		195:3 1/2"	81.5	89.5	206.7	192.8	80.9	10		7120 58 min.
	60	4:17:10		197:9"	83.5	89.25	206.2	193.3	81.4			
	66	4:58:10				89.25	206.2	192.7	81.4			

JUDITH L. HAMILTON
 Consulting Geologist and Engineer
 2220 Julian St. Denver, Colo. 80211

PUMPING TEST RESULTS

Client: NuBeth

Location: Oshoto, Wyo.

Date:

Job No.:

Hole No.: 789V

T.D.:

Ground elev.:

Pump data: 5 h.p.

460 volt

3 phase

Make: Burks

Depth Set:

Static water level:

ft. below G.S./M.P. Meas. point:

ft. above G.

Start of Test:

AM/PM Pumping/Recovery

Air Line Depth:

time	time in min. from		t/L	water depth (FD)		Air Line				pumping rate		Comments
	start of pumping	stopping pumping		below meas. pt.	below static	gauge pressure lbs	= feet	depth below meas. pt.	depth below static (FD)	sec./gal.	gpm (lined)	
	70	48.6	10 ⁻²	197 7/8"	83.8							
	73	5.07				88	203.3	196.2	84.3		9.9	
	75	5.21				88	203.3	196.2	84.3			
	76	5.28		198 9/16"	84.5							
	82	5.69		200 1/2"	86.3	87 5/8"	202.1	197.4	85.5			
	102	7.08		200 3/4"	86.9	87 1/4"	201.5	198.0	86.1		10	meter 760.0 107 min
	110	7.64		201 1/8"	87.3	86 3/4"	200.4	199.1	87.2		10	
	120	8.33		202.0"	88.2	86 1/2"	199.8	199.7	87.8			
	142	9.72		202.75"	88.9	86 1/4"	199.2	200.3	88.4	62/110		783 135 min
	160	1.11 x 10 ⁻¹		204 4/8"	90.5	85 1/2"	197.5	202.0	90.1		10	
	170	1.18		205 2/8"	91.4	85 1/2"	197.5	202.0	90.1		10	"836.3 @ 183 30 sec
	180	1.25		207 5/8"	93.6	89	194.0	205.5	93.6			
	210	1.46		208 8/8"	94.9	83 3/4"	193.5	206.0	94.1		10	
	240	1.67		210 0/8"	96.2	83 1/2"	192.9	206.6	94.7			
	270	1.88		205 1 1/8"	91.3	82 5/8"	191.2	208.3	96.4		10	
	300	2.08		211 9/16"	98.0	82	189.4	210.1	98.2		10	9531.2 @ 300 min
	330	2.29				82	189.4	210.1	98.2			
	360	2.50				81 1/2"	188.3	211.2	99.3		10	10155.0 @ 363 min
	390	2.71				81 1/4"	187.7	211.8	99.9			10433.0 @ 392
	420	2.92				77	177.9	221.6	109.7			trying to adjust flow up to 15 gpm pressure dropped to 76, pressure
	428	2.97				81 1/2"	188.3	211.2	99.3		9.1	lower 9
7:15 P	450	3.13				83 1/2"	198.3	206.6	94.7		9	
	456	3.17									10	
	459	3.33				80 1/2"	186.0	213.5	101.6		9.8-10.1	11355.5
7:50											10	
	510	3.54				79	182.5	217.0	105.1	61/110	10.9	11666.0 @ 513 min
	540	3.75				80 1/4"	185.9	219.1	102.2			11969.5
	570	3.96				80 1/4"	185.4	214.1	102.2		9.8, 10	12261.8
	600	4.17				-					10	
	630	4.38				79 3/4"	184.2	215.3	102.4		9.95	12861.5
11:15	630	4.79				79 1/2"	183.6	215.9	104.0		10	13461.1
12:37	772	5.36				78	180.1	219.3	107.4		10	14330.0
	810	5.63				78	180.1	219.3	↓		10	14683.0
	870	6.04 x 10 ⁻¹				78	180.1	219.2	↓		9.85	15711.5

JUDITH L. HAMILTON
 Consulting Geologist and Engineer
 2220 Julian St. Denver, Colo. 80211

PUMPING TEST RESULTS

Client:

Location:

Date: 8-2-77

Job No.:

Hole No.: 789 V

T.D.:

Ground elev.: ft.

Pump data: h.p. volt phase; Make:

ft. below G.S./M.P. Meas. point:

Depth Set: ft. above G.S.

Static water level:

Start of Test: AM/PM Pumping/Recovery Air Line Depth:

Time	Time in min. from		t/c	water depth (ft)		Air Line				pumping rate		Comments
	start of pumping	days		below meas. pt.	below static	gauge pressure lbs	depth below P.M.P. ft	depth below static (ft)	sec/gal	gpm		
	73	6.46	10 ⁻¹			78	180.2	219.3	107.4		7.4	153300
	990	6.88				78	180.2	219.3	107.4		10	164560
	1110	7.71				77	177.9	221.6	109.7		9.5	176485
	1215	8.44				76 1/2	176.7	222.8	110.9		9.9	
	1335	9.27				76	175.6	223.9	112.0		9.9	
	1455	1.01	10 ⁰			76	175.6	223.9	112.0		9.9	
	1575	1.09				76 1/2	176.7	222.8	110.9		9.9	
	1720	1.19				77	177.9	221.6	109.7		10.2, 10	4.15 pH 9.3, SO ₄ 2200
	1755	1.23				77	177.9	221.6	109.7		9.8	254 NaCl 37.5 hardness
	1935	1.34				76 1/2	176.7	222.8	110.9		9.8, 10	35 ppm H ₂ O
11:00	2115	1.47				75 1/2	174.4	225.1	113.2	27590	10	Fe 1.9 T 4.0
2:00	2275	1.59				74	170.9	228.6	116.7	29400		15.45 2320 L 5
5:00	2475	1.72				72 1/2	167.5	232.0	120.1	31200		10.2 SO ₄ 4.0 11800
7:00	2635	1.84				72	166.3	233.2	121.3		12.1	AV 1665 10.2 16200
11:00	2835	1.97				72 1/2	167.5	232.0	120.1		12.1	17.07 2922
2:00	3015	2.09				73 1/4	169.2	230.3	112.4	36740	10.0	2.13 PM 25900 2647
5:00	3195	2.22				73	168.6	230.9	119.0	38490	9.9	3:45 PM 513 pH 9.3
8:00	3375	2.34				73 1/4	169.2	230.3	118.4	40350	9.6	Hardness 37 ppm T. 48°F
11:00	3555	2.47				71	164.0	235.5	123.6		10.1	6.09 P 39167
2:00	3735	2.59				72	166.3	233.2	121.3		12.2	17.07 very strong
5:00	3915	2.72				72	166.3	233.2	121.3		12.1	wind noise - considerable
08:00	4095	2.84				71 1/2	165.2	234.3	122.4		10.0	decreased by 7.45 but
11:00	4280	2.90				71 1/2	172.1	227.4	115.5	4150	9.9	still noisy - calm
11:45	4320	3				70 1/2	171.5	228.0	116.1	49900		9.20 Wind 2.0
	4320 1/4	3 1/4	5761			71	187.1	212.4	100.5			11.40 pH 9.2-9.3
	4321 1/4	1 1/4	3957			76	192.7	208.8	88.9			hardness 32 mg/l
	4322 3/4	1 3/4	2496			77 1/2	206.9	192.8	80.9			21.00 1.275
	4322 1/2	1 1/2	1769			74 1/4	212.2	181.2	69.3			
	4323 1/4	1 1/4	1361			76 1/2	202.2	176.6	69.7			49930
	4324	1	1081			77	222.7	170.8	58.9			6550
	4325	5	865			100	231.0	168.5	56.6			43380 gal = 10.04 gpm
	4326	6	721			100	231.0	168.5	56.6			4320 min av.
	4327 1/4	7 1/4	596.9			100 1/2	233.2	167.3	55.4			
	4328	8	541			101	233.3	166.2	54.3			
	4329	9	481			101	233.3	166.2	54.3			

8D

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PUMPING TEST RESULTS

Client: _____ Location: _____ Date: _____
 Job No.: _____ Hole No.: 7014 T.D.: _____ Ground elev.: _____ ft
 Pump data: _____ h.p. _____ volt _____ phase; Make: _____ Depth Set: _____
 Static water level: _____ ft. below G.S./M.P. Meas. point: _____ ft. above G.S.
 Start of Test: _____ AM/PM Pumping/Recovery _____ Air Line Depth: _____

Time	Time in min. from		t/L	water depth (FD)		Air Line				pumping rate		Comments
	start of pumping	stopping pump		below meas. pt.	below static	Gage Pressure lbs.	ft. sec	depth below M.P.	depth below static (ft)	sec./gal.	gpm (lined)	
	4330	10	433			15 1/2	234.5	165.0	53.1			
	4331	11	393.7			15 3/4	235.0	164.5	52.6			
	4332	12	361			15 1/2	235.0	163.9	52.5			
	4333	13	333.3			15 1/2	236.8	162.7	50.5			
	4334	14	309.6			15 1/2	236.8	162.7	50.9			
	4335	15	289			16 3/4	237.0	161.6	49.7			
	4337	17	255.1			15 1/2	238.5	161.0	49.1			
	4339	19	228.4			16 3/4	239.7	159.8	47.9			
	4341	21	206.7			16 1/4	240.8	158.7	46.8			
	4343	23	188.8			15 1/2	242.2	158.7	46.8			
	4345	25	173.8			15 1/2	241.4	158.1	46.2			
	4350	30	145			15 1/2	243.7	155.8	43.9			
	4355	35	124.4			15 1/2	245.4	154.1	42.2			
	4360	40	109			15 1/4	245.4	154.1	42.2			
	4365	45	97			15 1/2	246.0	153.5	41.6			
	4370	50	87.4			16 1/2	246.0	153.5	41.6			
	4375	55	79.5			16 1/2	249.5	150.0	38.1			
	4380	60	73			16 1/2	251.1	149.4	37.5			
	4385	65	67.5			16 1/2	250.1	149.4	37.5			
	4390	70	62.7			16 1/2	250.6	148.9	37.0			
	4395	75	58.6			16 1/2	250.6	148.9	37.0			
1:05	4400	80	55			16 1/2	251.8	147.7	35.8			
1:15	4410	90	49			16 1/2	252.9	146.6	34.7			
1:25	4420	100	44.2			16 1/2	253.5	146.0	34.1			
1:35	4430	110	40.3			16 1/4	254.7	144.8	32.9			
1:45	4440	120	37			16 1/2	255.3	144.2	32.3			
1:55	4450	130	34.2			16 1/2	255.3	144.2	32.3			
2:05	4460	140	31.9			16 3/4	255.8	143.7	31.8			
2:15	4470	150	29.8			16 1/4	257.0	142.5	30.6			
2:35	4490	170	26.4			16 3/4	258.1	141.4	29.5			
2:55	4510	190	23.7			16 1/2	258.7	140.8	28.9			
3:15	4530	210	21.6			16 1/4	259.3	140.2	28.3			
3:45	4560	240	19			16 1/2	262.2	137.3	25.4			
4:15	4590	270	17			16 1/2	262.2	137.3	25.4			
4:45	4620	300	15.4			16 1/2	262.2	137.3	25.4			

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**PUMPING TEST RESULTS
 OBSERVATION HOLE**

Client: Nubetr

Location: Oshato, Wyo.

Date: 8/1/77

Job No.:

Obs. Hole No.: 788V T.D.: 570 G.S.: 4189.4

Pumped Hole No.: 789V T.D. Pumped hole: 566 Meas. pt. above G.S.: 2.8

Distance from pumped hole: 0.4 ft. pumping rate: 10 gpm

7/31
7/31
8/1

time	Time in min from start of pumping		r/z	water depth, ft.		water depth below static	Calculated recovery (S-S) ft.	time	Time in min from start of pumping		r/z	water depth (ft.)		Calculated recovery (S-S) ft.
	days	in days		below meas. pt.	below M.D.				days	in days		below meas. pt.	below M.D.	
1114				105.5	102.63			90	6.25	1.41	116.8	116.67	11.61	
				105.21				100	6.94	1.27	112.5	117.92	12.36	
				105.34	105.06	102.20	blow	110	7.64	1.16	118.14	118.13	13.07	
0				105.34	105.06	0		120	8.33	1.06	118.64	118.54	13.98	
1	6.94	1.27	1.04	105.34	105.06	.02		130	9.03	0.99	119.4	119.38	14.32	
2	1.39	10.3	6.36	105.1	105.08	.02		140	9.72	0.99	119.5	119.48	14.42	
3	2.08	4.25	4.25	105.1	105.08	.02		150	1.04	8.50	120.00	120.00	14.96	
4	2.78	3.18	3.18	105.2	105.17	.11		180	1.25	7.07	121.3	121.33	16.27	
5	3.47	2.55	2.55	105.4	105.35	.29		210	1.46	6.05	122.5	122.44	17.38	
6	4.17	2.12	2.12	105.4	105.38	.32		240	1.67	5.29	123.7	123.65	18.57	
7	4.86	1.82	1.82	105.6	105.50	.44		270	1.88	4.70	124.6	124.50	19.44	
8	5.56	1.59	1.59	105.7	105.63	.57		300	2.08	4.25	125.1	125.15	20.09	
9	6.25	1.41	1.41	105.9	105.75	.69		330	2.29	3.86	125.11	125.92	20.86	
10	6.94	1.27	1.27	105.10	105.85	.79		360	2.50	3.53	126.4	126.35	21.29	
11	7.64	1.16	1.16	105.11	105.98	.92		390	2.71	3.26	126.11	126.96	21.90	
12	8.33	1.06	1.06	106.2	106.17	1.11		450	3.13	2.82	128.3	128.26	23.20	
13	9.03	0.99	0.99	106.4	106.40	1.34		510	3.54	2.50	129.1	129.04	23.98	
14	9.72	0.99	0.99	106.6	106.54	1.48		540	3.75	2.36	129.6	129.50	24.49	
15	1.04	8.50	8.50	106.8	106.81	1.75		570	3.96	2.23	129.8	129.67	24.61	
17	1.18	7.49	7.49	107.3	107.27	2.21		630	4.38	2.02	130.4	130.33	25.27	
19	1.32	6.69	6.69	107.6	107.56	2.50		11:15	6.90	1.84	130.11	130.92	25.86	
21	1.46	6.05	6.05	108.1	108.02	2.96		750	5.21	1.70	131.5	131.42	26.36	
23	1.60	5.56	5.56	108.4	108.35	3.29		810	5.63	1.57	131.0	131.88	26.82	
25	1.74	5.08	5.08	108.9	108.77	3.71		870	6.04	1.46	132.5	132.92	27.36	
30	2.08	4.25	4.25	110.00	110.00	4.94		930	6.45	1.37	132.7	132.63	27.57	
35	2.43	3.64	3.64	110.8	110.71	5.65		990	6.88	1.28	133	133.00	27.94	
40	2.78	3.18	3.18	111.6	111.52	6.46		1010	7.71	1.15	133.2	133.63	28.57	
45	3.13	2.82	2.82	112.3	112.29	7.23		1215	9.84	1.05	134.2	134.21	29.15	
50	3.47	2.55	2.55	112.10	112.88	7.82		1235	9.27	0.93	134.9	134.75	29.69	
55	3.82	2.31	2.31	113.6	113.56	8.50		1455	1.01	8.75	135.2	135.21	30.15	
60	4.17	2.12	2.12	114.1	114.10	9.04		1575	1.09	8.11	135.7	135.58	30.52	
65	4.51	1.96	1.96	114.7	114.63	9.57		5:00pm	1755	1.22	7.24	136.2	136.21	31.15
70	4.86	1.82	1.82	115.00	115.00	9.94		8:10	1945	1.35	6.55	136.10	136.83	31.77
75	5.21	1.70	1.70	115.6	115.56	10.50		11:00	2115	1.47	6.01	137.9	137.81	32.25
80	5.56	1.59	1.59	115.4	115.42	10.81		2:00pm	2245	1.59	5.56	138.0	137.81	32.24

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**PUMPING TEST RESULTS
 OBSERVATION HOLE**

Client: NuBeth

Location: Oshoto, Wyoming

Date: 8/3/77

Job No.:

Obs. Hole No.: 788V

T.D.:

G.S.:

Pumped Hole No.:

T.D. Pumped hole:

Meas. pt. above G.S.:

Distance from pumped hole:

ft.

pumping rate:

gpm

113

time	Time in min. from		r ² 1/ft	water depth, ft.		W.L. below static	Calculated recovery (CS-S) 3-S/4
	start of pumping	stopping pump		below meas. pt.	Below M.P.		
5:00 AM	2475	1.72	5.14	135'11"	138.92	33.86	
5:00	2655	1.84	4.80	139'4 1/2"	139.38	34.32	
11:00	2935	1.97	4.49	139'6 1/2"	139.54	34.48	
2:00	3015	2.09	4.23	139'10 3/4"	139.90	34.84	
3:00	3195	2.22	3.98	140'03"	140.33	35.27	
8:00	3375	2.34	3.78	140'7 1/2"	140.72	35.66	
11:00	3555	2.47	3.58	140'0	142.00	36.94	calm
		2.59	3.41	141'0	141.50	36.44	windy
		2.72	3.25	141'0	141.50	36.44	
5:00	4095	2.84	3.11	141'5 1/2"	141.56	36.50	
11:00	4275	2.97	2.98	141'6 1/2"	141.54	36.48	
		0	2/ft	141'7 1/2"	141.65	36.59	
		1	432		141.67	36.61	
		2	216	141'8"	141.67	36.61	
		3	144	141'7 1/2"	141.63	36.57	
		4	108	141'7 1/2"	141.63	36.57	
			865	141'7 1/2"	141.63	36.57	
			72	141'6"	141.50	36.49	
			618.1	141'4 1/2"	141.38	36.32	
			541	141'4"	141.33	36.27	
			481	141'2"	141.17	36.11	
			433	141'	141.0	35.94	
			393.7	140'	140.88	35.82	
			361	140'9"	140.75	35.69	
			333.3	140'7 1/2"	140.63	35.57	
			309.6	140'5 1/2"	140.46	35.40	
			289	140'4 1/2"	140.38	35.32	
			255.1	140'0"	140.00	34.94	
			228.4	139'8"	139.67	34.61	
			206.7	139'0"	139.33	34.27	
			188.8	139'0"	139.00	33.94	
			173.8	138'8 1/2"	138.71	33.65	
			195	138'00"	138.00	32.94	
			129.4	137'2 1/2"	137.21	32.15	
			110	136'1 1/2"	136.1	31.48	

1145

time	Time in min. from		r ² 1/ft	water depth (ft.)		W.L. below static	Calculated recovery (CS-S) ft.
	start of pumping	stopping pump		below meas. pt.	Below M.P.		
			97	135'10"	135.83	30.77	
			87.4	135'4 1/2"	135.34	30.28	
			79.5	134'10"	134.83	29.77	
			73	134'4"	134.33	29.27	
			67.5	133'4 1/2"	133.94	28.88	
			62.7	133'3"	133.25	28.19	
			58.6	132'9"	132.75	27.69	
			55	132'4 1/2"	132.33	27.32	
			49	131'8 1/2"	131.71	26.65	
			44.2	130'	131.16	25.90	
			40.3	130'4"	130.33	25.27	
			37	129'8 1/2"	129.71	24.65	
			34.2	129'2"	129.17	24.11	
			31.9	128'7 1/2"	128.63	23.57	
			29.8	128'1 1/2"	128.13	23.07	
			26.4	127'4"	127.33	22.27	
			23.7	126'6 1/2"	126.46	21.46	126.52
			21.6	125'9 1/2"	125.73	20.73	125.79
			19	124'10 1/2"	124.82	19.82	124.88
			17	124'	124.00	19.00	124.04
			15.9	123'4"	123.27	18.27	123.33
			14.1	122'8"	122.61	17.61	122.67
			13	122'1"	122.02	17.02	122.08
			12.1	121'6 1/2"	121.48	16.48	121.54
			11.2	121'	121.00	15.98	121.04
			4960	140	7.75	10.21	10.27
8/5 8:30	5565	1245	4.97	115.47	109.1-1.1	9.31	
2:30	5925	1605	3.69	114.24	9.18-1.1	8.08	
8/8 1:30 P	10185	5365	1.74	108.65	3.59-1.1	2.49	
8/10 5:00 P	13275	8955	1.48	107.65	2.59-1.1	1.49	
8/15 10 A	20055	15735	1.27	106.17	1.11-1.1	0	
8/18 3:30 P	24705	20385	1.21	105.95	.89-1.1	1.22	
8/22 8:15	30450	26130	1.17	105.55	.49-1.1	1.62	

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PUMPING TEST RESULTS
OBSERVATION HOLE

Client: NuBeth

Location: Oshito, Wyo

Date: 8/1/77

Job No.:
Pumped Hole No.: 7777 T.D. Pumped hole: 566 Meas. pt. above G.S.: 2.4
Distance from pumped hole: 97.1 ft. pumping rate: 10 gpm

7/31
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8/1

time	time in min. from		r/c	water depth, ft.		below h.p. st.	Calcula- ted re- covery (S-S) ft	time	time in min. from		r/c	water depth (ft.)		below h.p. st.	Calcula- ted re- covery (S-S) ft
	start of pumping	stopping pump		below meas. pt.	below static pt.				start of pumping	stopping pump		below meas. pt.	below static		
10:00				119.30				1:15	90		1.22	29' 9"	10.36	129.69	
11:04				119.00				1:25	100		1.10	29' 4"	11.01	129.33	
11:45	0			118 3/4	115.92	118.32		1:35	110		1.00	29' 1/2"	11.61	129.93	
11:46	1		1.10	118 1/4	.01			1:45	120		9.17	30' 6"	12.20	130.52	
11:47	2		5.50	118 4/4	.03	118.35		1:55	130		8.46	131'	12.69	131.00	
11:48	3		3.67	118 4 3/4	.08	118.40		2:05	140		7.85	131' 6"	13.18	131.50	
11:49	4		2.75	118 5 3/4	.16	118.48		2:15	150		7.34	131' 11 3/4"	13.65	131.97	
11:50	5		2.20	118 6 1/4	.22	118.54		2:45	180		6.11	133' 3 1/2"	14.97	133.29	
11:51	6		1.83	118 7 3/4	.33	118.65		3:15	210		5.23	134' 4 1/2"	16.06	134.38	
11:52	7		1.57	118 9 3/8	.50	118.82		3:45	240		4.57	135' 4 1/2"	17.06	135.38	
11:53	8		1.37	118 11 1/2	.64	118.96		4:15	270		4.06	136' 2 1/2"	17.91	136.23	
11:54	9		1.22	119 1 1/2	.81	119.13		4:45	300		3.67	136' 11 1/2"	18.65	136.97	
11:55	10		1.10	119 3 3/8	.96	119.28		5:15	330		3.33	137' 7 1/2"	19.31	137.63	
11:56	11		1.00	119 5 3/8	1.15	119.47		5:45	360		3.06	138' 2 3/4"	19.91	138.23	
11:57	12		8.17	119 7 1/2	1.31	119.63		6:15	390		2.82	138' 9"	20.43	138.75	
11:58	13		8.46	119 9 3/8	1.46	119.78		7:15	450		2.44	140' 2 1/2"	21.88	140.21	
11:59	14		7.86	119 11 1/4	1.62	119.94		8:15	510		2.16	140' 9 3/4"	22.50	140.92	
12:00	15		7.35	120 1 1/2	1.81	120.13		9:15	570		1.92	141' 7"	23.26	141.58	
12:02	17		6.47	120 6 3/8	2.23	120.55		10:15	630		1.74	142' 2"	23.85	142.17	
12:04	19		5.79	120 11"	2.60	120.92		11:15	690		1.60	142' 10 1/2"	24.56	142.88	
12:06	21		5.23	121' 2 1/2"	2.89	121.21		12:15	750		1.47	143' 5 1/2"	25.14	143.46	
12:08	23		4.77	121' 7"	3.26	121.58		1:15	810		1.36	144' 3"	25.85	144.19	
12:10	25		4.39	121' 11"	3.60	121.92		2:15	870		1.27	144' 10"	26.35	144.67	
12:15	30		3.67	122' 9"	4.43	122.75		3:15	930		1.18	145' 3"	26.93	145.25	
12:20	35		3.14	123' 5 1/2"	5.14	123.46		4:15	990		1.11	145' 7"	27.35	145.67	
12:25	40		2.75	124' 2"	5.85	124.17		6:15	1110		9.91	146' 4"	28.06	146.38	
12:30	45		2.44	124' 9 1/4"	6.44	124.76		8:00	1215		9.05	147'	28.67	147.00	
12:35	50		2.20	125' 4"	7.01	125.33		10:00	1335		8.24	147'	29.18	147.50	
12:40	55		2.00	125' 10"	7.51	125.83		12:00	1455		7.56	145' 11"	29.79		
12:45	60		1.83	125' 3 3/4"	7.99	126.31		2:00	15		7.01	145' 5 1/2"	30.26		
12:50	65		1.69	126' 9"	8.43	126.75		5:00	1735		6.26	147' 8"	31.56		
12:55	70		1.57	127' 2 1/2"	8.89	127.21		8:00	1935		5.70	148'	32.15		
1:00	75		1.47	127' 6 1/2"	9.25	127.57		11:00	2115		5.20	151.49	33.17		
1:05	80		1.37	127' 11 1/2"	9.62	127.95		2:00	2295		4.80	152.20	33.88		
								5:00	2475		4.44	152' 9"	34.53		

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PUMPING TEST RESULTS
 OBSERVATION HOLE

Client: Nu Beth

Location: Oshoto, Wyo.

Date: 8/1/77

Job No.:

Obs. Hole No.: 797V T.D.: 570 G.S.: 4195.7

Pumped Hole No.: 797V

T.D. Pumped hole: 566

Meas. pt. above G.S.: 3.59

Distance from pumped hole: 53.0 ft.

28944 pumping rate: 1 gpm

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 7/31
 8/1

time	Time in min. from		r ²	water depth, ft.		dd(s) from pumping curve	Calculated recovery (s-s') ft.	time	Time in min. from		r ²	water depth (ft.)		dd(s) from pumping curve	Calculated recovery (s-s') ft.
	start of pumping	stopping pump		below meas. pt.	below static				start of pumping	days		below meas. pt.	below static		
1000				117.70				112	7.77	3.73	131.16	13.96			
1700				117.51	113.96			120		3.45	131.73	14.53			
1118				117.20	113.65			133	9.24	3.13	132.58	15.38			
1145	0							140		2.97	133.00	15.80			
	2.40							150		2.78	133.60	16.40			
	4	1.09	117.40	2				180		2.32	135.22	18.02			
	5	8.34	117.45	.25				210		1.98	136.10	19.40			
	6	6.94	117.58	.38				240		1.73	137.85	20.65			
	7	5.96	117.73	.53				270		1.54	139.00	21.80			
	8	5.20	117.88	.68				300		1.39	139.87	22.67			
	9	4.63	118.05	.85				330		1.26	140.00	23.50			
	10	4.17	118.18	.98				360		1.16	141.37	24.19			
	11	3.79	118.35	1.15				390		1.07	142.15	24.85			
	12	3.45	118.68	1.48				450		9.26	143.81	26.61			
	13	3.21	118.72	1.52				510		8.17	144.62	27.92			
	14	2.97	118.87	1.67				570		7.31	145.40	29.20			
	15	2.78	119.06	1.86				630		6.62	146.10	29.90			
	17	2.45	119.43	2.23				690		6.04	146.80	29.65			
	19	2.19	119.81	2.61				750		5.56	147.60	30.40			
	21	2.00	120.20	3.0				810		5.15	148.40	31.05			
	23	1.81	120.57	3.37				870		4.79	149.20	31.70			
	25	1.66	120.96	3.76				930		4.46	150.00	31.90			
	30	1.39	121.92	4.72				990		4.21	150.80	32.40			
	35	1.19	122.75	5.55				1050		3.76	151.60	33.10			
	40	1.09	123.56	6.36				8:00	1275	3.27	150.80	33.65			
	45	9.24	124.30	7.10					1335	3.12	151.43	34.23			
	50	8.34	124.98	7.78					1400	2.86	152.00	34.80			
	55	7.58	125.68	8.48					1575	2.65	152.45	35.25			
	60	6.94	126.30	9.10				5:00	1255	2.37	153.65	36.45			
	65	6.42	126.84	9.64				6:00	1435	1.34	154.35	37.15			
	70	5.96	127.33	10.13				11:00	2115	1.97	155.80	38.30			
	75	5.56	127.80	10.60				8:00	2295	1.82	156.20	39.00			
	80	5.20	128.40	11.20				5:00	2475	1.68	156.70	39.55			
	90	4.63	129.31	12.11				8:00	2655	1.57	157.30	40.10			
	100	4.17	130.25	13.05				11:00	2835	1.47	157.80	40.60			

APPENDIX A-2

WATER LEVEL DATA

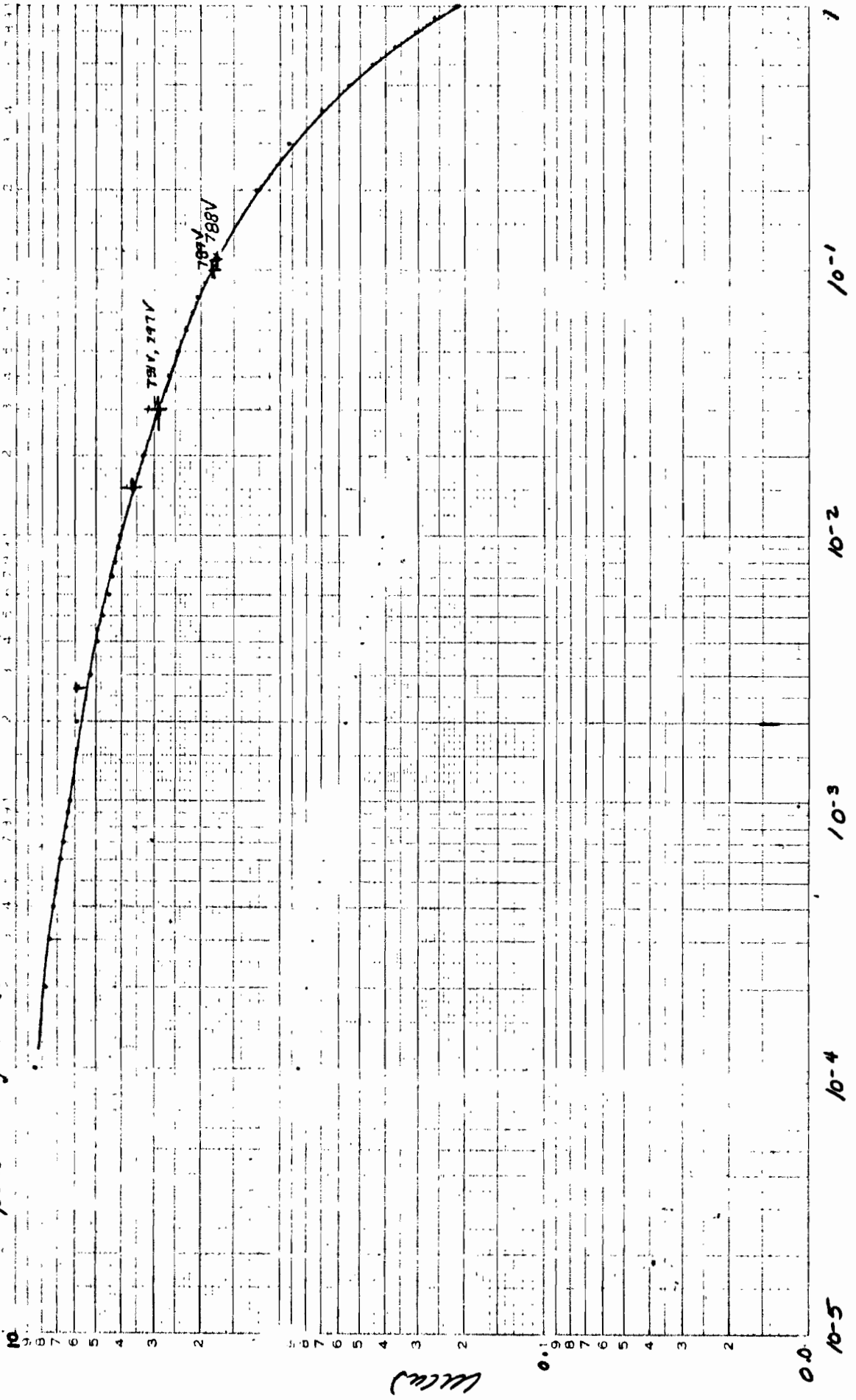
HOLES 3V, 5V, 9V, 1067V
790V, 794V, 795V, 796V

7/31/77-
8/22/77

APPENDIX A-3

STANDARD CURVES

Standard Curve for Anisotropic Non-leaky Artesian Aquifer with fully penetrating wells and constant discharge conditions



From: Walton, 1970 Groundwater Resource Evaluation

TABLE 3.1 VALUES OF $H(u)$ OR $W(u_{01})$. (After Hantush, 1942.)

N	$H(u)$															
	$N \times 10^{-15}$	$N \times 10^{-14}$	$N \times 10^{-13}$	$N \times 10^{-12}$	$N \times 10^{-11}$	$N \times 10^{-10}$	$N \times 10^{-9}$	$N \times 10^{-8}$	$N \times 10^{-7}$	$N \times 10^{-6}$	$N \times 10^{-5}$	$N \times 10^{-4}$	$N \times 10^{-3}$	$N \times 10^{-2}$	$N \times 10^{-1}$	N
1.0	33.9616	31.6590	29.3564	27.0538	24.7512	22.4486	20.1460	17.8435	15.5409	13.2383	10.9357	8.6332	6.3315	4.0289	1.8259	0.2194
1.5	33.5561	31.2535	28.9509	26.6483	24.3458	22.0432	19.7406	17.4380	15.1354	12.8328	10.5303	8.2278	5.9266	3.6254	1.5225	0.1000
2.0	33.2684	30.9658	28.6632	26.3607	24.0581	21.7555	19.4529	17.1503	14.8477	12.5451	10.2426	7.9402	5.6394	3.3457	1.2227	0.0450
2.5	33.0453	30.7427	28.4401	26.1375	23.8349	21.5323	19.2298	16.9272	14.6246	12.3220	10.0194	7.7172	5.4167	3.1365	1.0243	0.0241
3.0	32.8629	30.5604	28.2578	25.9552	23.6526	21.3500	19.0474	16.7449	14.4423	12.1397	9.8371	7.5348	5.2249	2.9591	0.9057	0.01305
3.5	32.7088	30.4062	28.1036	25.8010	23.4985	21.1959	18.8933	16.5907	14.2881	11.9855	9.6830	7.3907	5.0813	2.8059	0.7942	0.00970
4.0	32.5753	30.2727	27.9701	25.6675	23.3649	21.0623	18.7598	16.4572	14.1546	11.8520	9.5495	7.2472	4.9482	2.6813	0.7024	0.00759
4.5	32.4575	30.1549	27.8523	25.5497	23.2471	20.9446	18.6420	16.3394	14.0368	11.7342	9.4317	7.1295	4.8310	2.5624	0.6263	0.006073
5.0	32.3521	30.0495	27.7470	25.4444	23.1418	20.8392	18.5366	16.2340	13.9314	11.6280	9.3263	7.0242	4.7261	2.4699	0.5598	0.005148
5.5	32.2568	29.9542	27.6516	25.3491	23.0465	20.7439	18.4413	16.1387	13.8361	11.5330	9.2210	6.9289	4.6313	2.3775	0.5034	0.004409
6.0	32.1698	29.8672	27.5646	25.2620	22.9595	20.6569	18.3543	16.0517	13.7491	11.4465	9.1240	6.8420	4.5448	2.2931	0.4544	0.003801
6.5	32.0898	29.7872	27.4846	25.1820	22.8794	20.5768	18.2742	15.9717	13.6691	11.3665	9.0290	6.7620	4.4642	2.2101	0.4115	0.0033034
7.0	32.0156	29.7131	27.4105	25.1079	22.8053	20.5027	18.2001	15.8976	13.5950	11.2924	8.9209	6.6879	4.3916	2.1408	0.3738	0.0029145
7.5	31.9467	29.6441	27.3415	25.0389	22.7363	20.4337	18.1311	15.8280	13.5260	11.2234	8.8209	6.6150	4.3231	2.0867	0.3403	0.0025958
8.0	31.8821	29.5795	27.2769	24.9744	22.6718	20.3692	18.0666	15.7640	13.4614	11.1589	8.7563	6.5445	4.2591	2.0469	0.3106	0.0023276
8.5	31.8215	29.5189	27.2163	24.9137	22.6112	20.3086	18.0060	15.7034	13.4008	11.0982	8.6957	6.4749	4.1970	1.9711	0.2849	0.002106
9.0	31.7643	29.4618	27.1592	24.8566	22.5540	20.2514	17.9488	15.6462	13.3437	11.0411	8.6386	6.4058	4.1423	1.9187	0.2623	0.001924
9.5	31.7103	29.4077	27.1051	24.8025	22.4999	20.1973	17.8948	15.5922	13.2895	10.9870	8.5845	6.3383	4.0887	1.8695	0.2427	0.001760

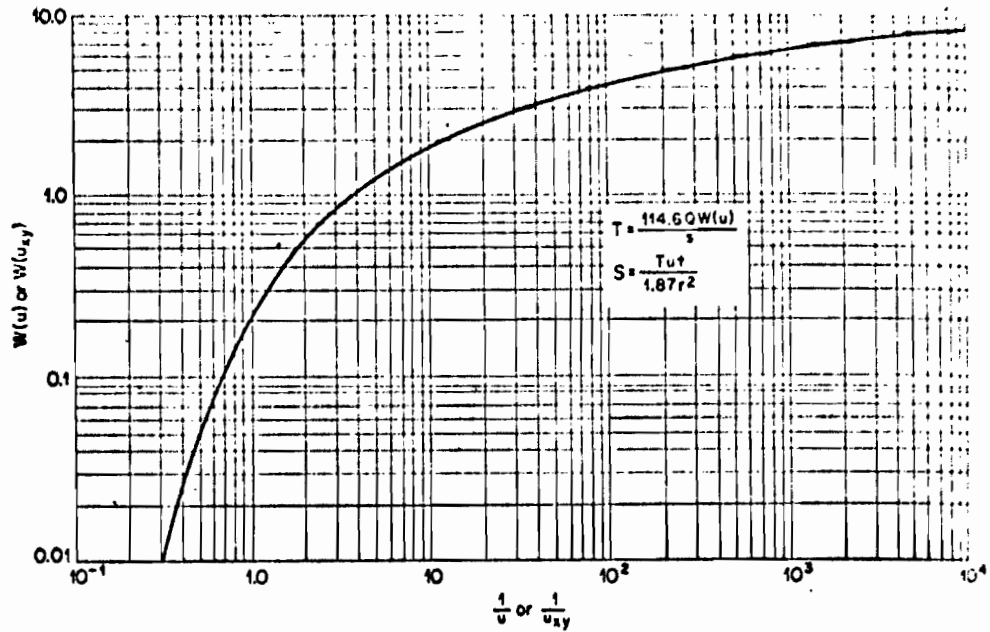
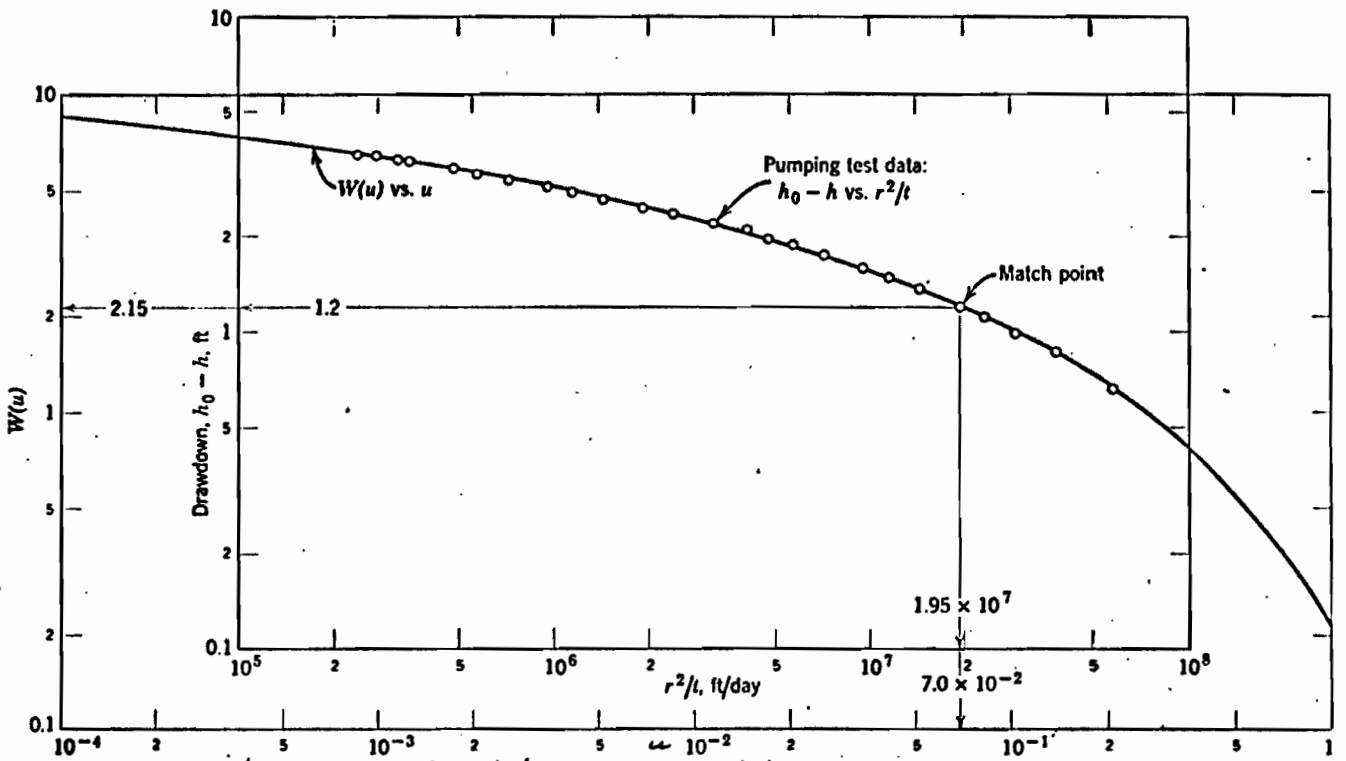


Fig. 4.2 Nonleaky artesian, fully penetrating, constant-discharge, time-drawdown type curve.
 (Drawn by W. C. Walton.)
 From: Walton, 1970, Groundwater Resource Evaluation



r = distance pumped well to observation hole
 t = time in days since pumping began
 Fig. 4.9. Theis method of superposition for solution of the nonequilibrium equation.

From: Todd, 1959, Groundwater Hydrology

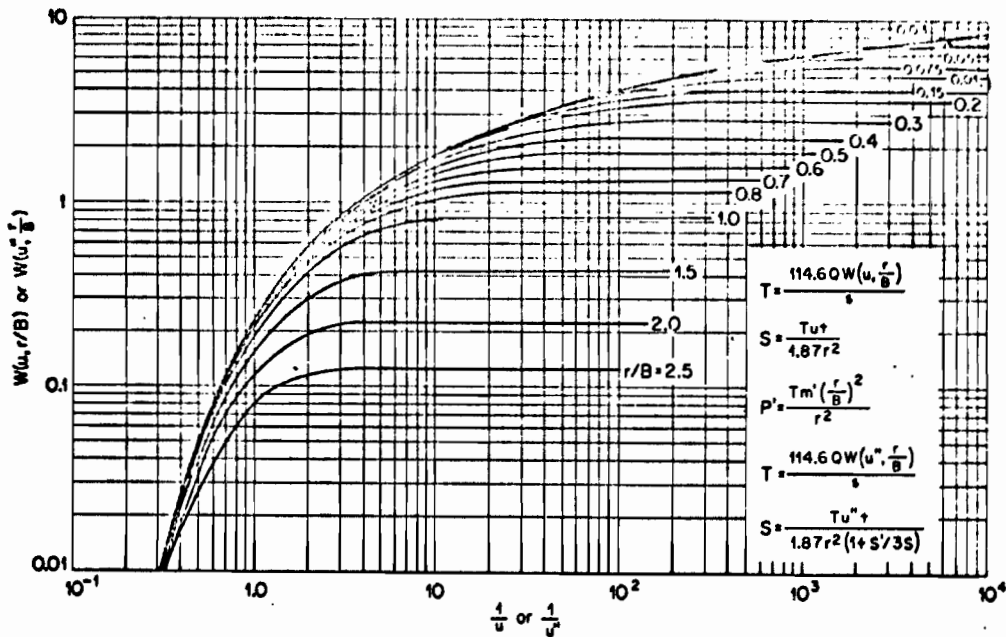


Fig. 4.8 Leaky artesian, fully penetrating, without water released from storage in aquitard, constant-discharge, time-drawdown type curves. (After Walton, 1962a.)

r = distance pumped well to observation hole.
 $B = \sqrt{T/(P'/m')}$
 P' = coef. of permeability of aquitard, cgpd/ft^2
 m' = saturated thickness of aquitard, in feet.

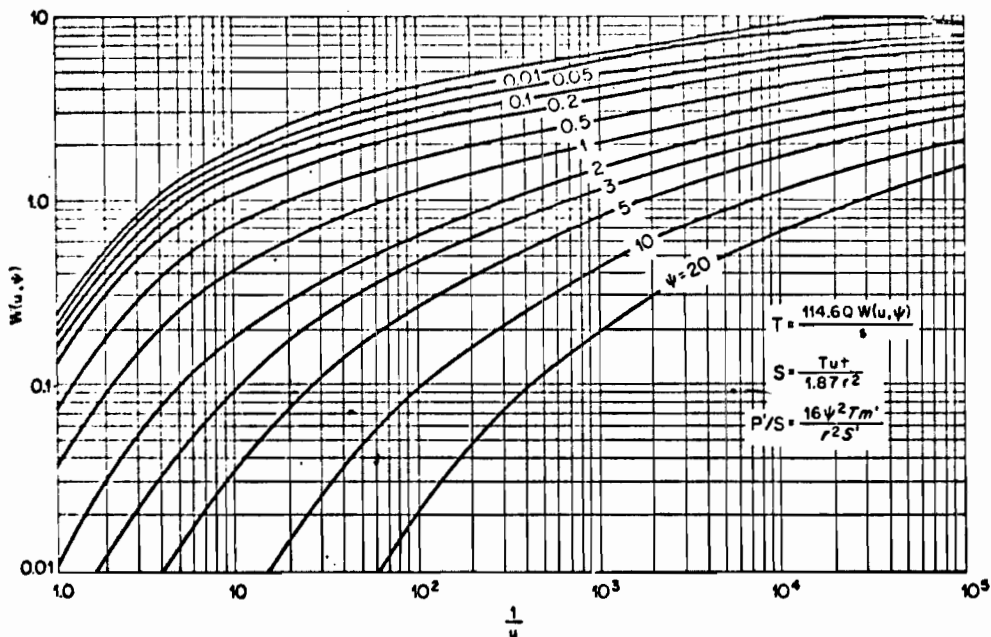
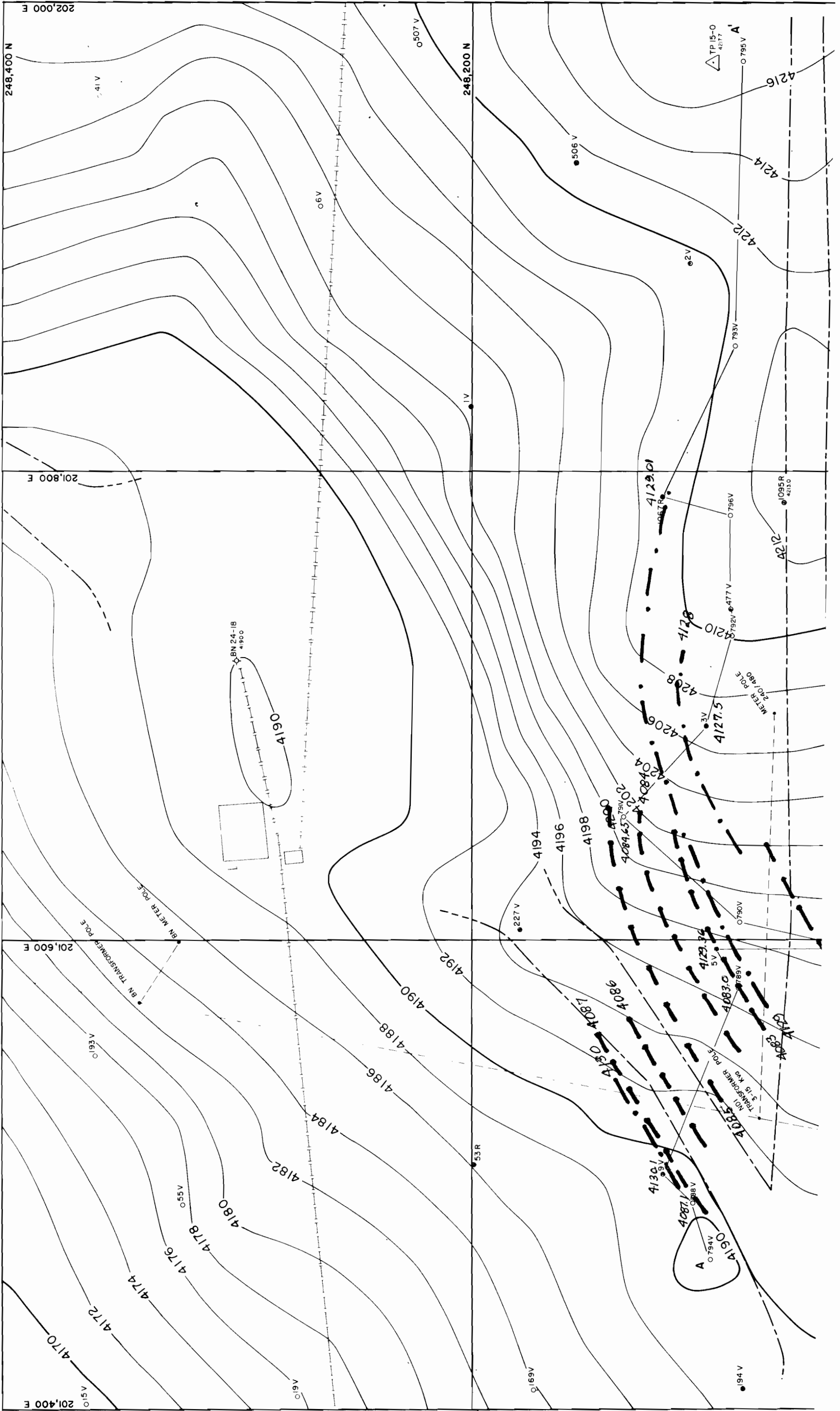


Fig. 4.11 Leaky artesian, fully penetrating, with water released from storage in aquitard, $i \leq m'S/74.8 P'$, constant-discharge, time-drawdown type curves. (Drawn by W. C. Walton.)

$\psi = \left(\frac{r}{4}\right) \sqrt{\frac{S'P'}{TSm'}}$ S' = coef. of storage of aquitard
 From: Walton, 1970. Groundwater Resource Evaluation



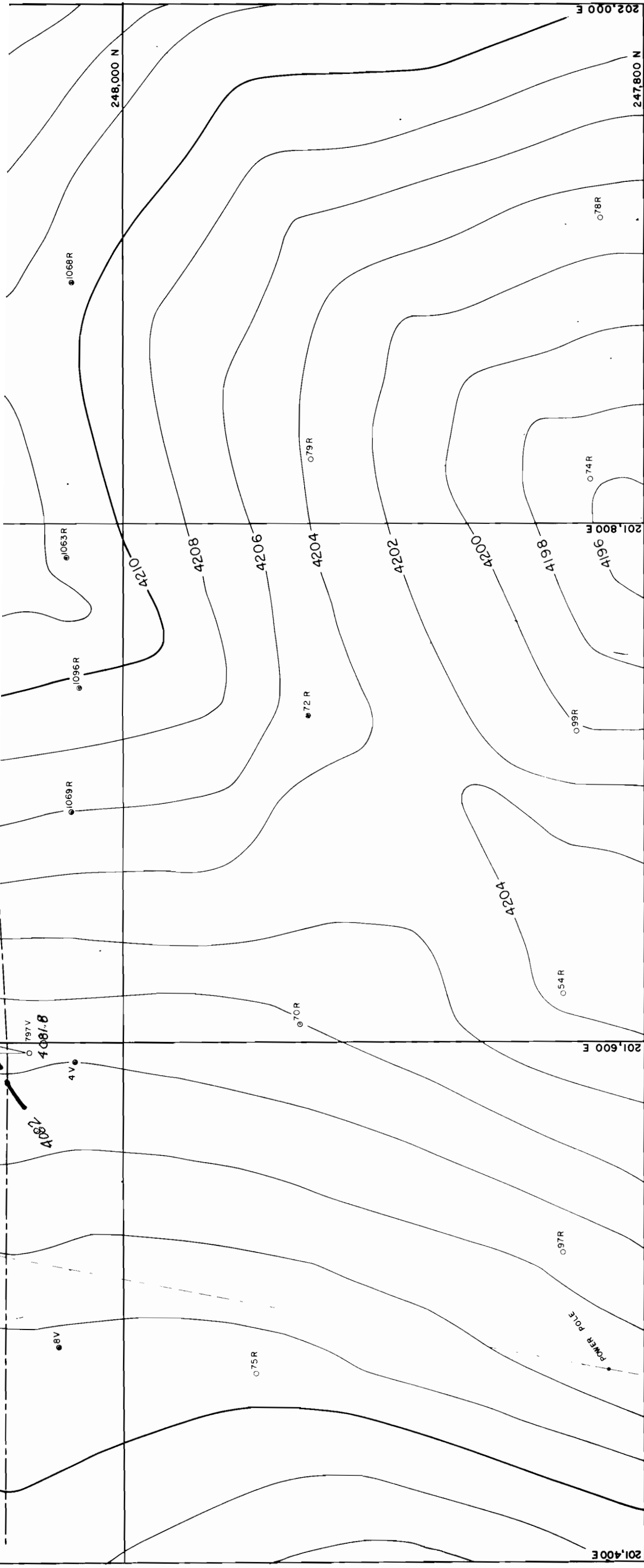


PLATE I

HYDROLOGIC TEST SITE NUCLEAR DYNAMICS AUGUST, 1977

0' 10' 20'

LEGEND

- 3V-NDI DRILL HOLE
- 4V-NDI DRILL HOLE - CEMENTED TO SURFACE
- IV-NDI DRILL HOLE - CEMENTED IN ZONE B
- ⊕ BN 24-18 OIL WELL
- POWER LINE
- BURIED PIPE LINE
- △ TP 15-O TRIANGULATION STATION
- BUILDING
- ROAD
- SURFACE CONTOUR - C1 + 2
- A—A' LINE OF SECTION

4082 ————— Piezometric surface in Sand Zone B

4129 ————— Piezometric surface in sand zone A

Water level elevation in hole, feet