| (7-77)              |   |
|---------------------|---|
|                     | CONTROL BLOCK:  |
|                     | $ \underbrace{  S   C   H   B   R   2}_{9 \text{ LICENSEE CODE} 14}   0   0   -   0   0   0   0   0   -   0   0$  |
| CON'T<br>0 1<br>7 8 | $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |
|                     | a primary to secondary leak assumed to be in excess of .35 gpm (Tech. Spec. 3.1.5.3)  |
|                     | was identified in "C" Steam Generator. An accurate determination of the leakage rate  |
| 0 5                 | could not be made due to plant conditions. Due to the stable condition of the plant   |
| 06                  | and the small leak size, there was no threat to either plant or public safety. This   |
| 07                  | event is reportable under Technical Specification 6.9.2.a.3.  |
| 08                  | ا<br>ع  |
| ۅٵ                  | $\begin{array}{c} \begin{array}{c} \text{SYSTEM} \\ \text{CODE} \end{array} \\ \begin{array}{c} \text{CAUSE} \\ \text{CODE} \end{array} \\ \begin{array}{c} \text{CAUSE} \\ \text{SUBCODE} \end{array} \\ \begin{array}{c} \text{CAUSE} \\ \text{SUBCODE} \end{array} \\ \begin{array}{c} \text{CAUSE} \\ \text{SUBCODE} \end{array} \\ \begin{array}{c} \text{COMPONENT CODE} \\ \text{COMPONENT CODE} \end{array} \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array} $ \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array}  \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \\ \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \end{array} \\ \end{array}  \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array}  \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array}  \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \\ \end{array} \\ \end{array}  \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \end{array}  \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \\ \end{array}  \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \end{array} \\ \\ \end{array}  \\ \\ \begin{array}{c} \text{SUBCODE} \end{array} \\ \\ \\ \end{array} \\ \\ \end{array}  \\ \\ \end{array}  \\ |
|                     | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   |
| 10                  | Tube sheet inspection revealed one tube leaking at an approximate rate of .25 gpm,  |
| 11                  | with the S/G full on the secondary side. The leak was repaired by explosive tube  |
| 12                  | plugging. No specific cause for the tube failure has been identified.   |
| 13                  |   |
| 14                  | 9 80  |
|                     | $ \begin{array}{c c} \hline ACILITY \\ status \\ 9 \\ \hline 10 \\ 12 \\ \hline 10 \\ 12 \\ \hline 12 \\ \hline 13 \\ \hline 13 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 13 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\ \hline 12 \\ \hline 13 \\ \hline 10 \\$  |
|                     | CTIVITY CONTENT<br>ELEASED OF RELEASE AMOUNT OF ACTIVITY $35$<br>Z 33 Z 34 NA LOCATION OF RELEASE $36NA 80$   |
| 17<br>78            | PERSONNEL EXPOSURES<br>NUMBER<br>0 0 0 37 BESCRIPTION 39<br>9 PERSONNEL INJURIES<br>80  |
| 18<br>78            | NUMBER DESCRIPTION (41)   0 0 0 (40)   9 11 12 80   |
| 19<br>7 8           | Loss of or Damage to Facility (43) 7906270176.   Type Description   2 42   10 80  |
| 20                  | PUBLICITY<br>ISSUED DESCRIPTION 45<br>NA IN 44 NA   |
| 78                  | 9 10 68 69 80 5<br>NAME OF PREPARER R. B. Starkey, Jr. PHONE: (803) 383-4524  |

**C B d B d** 

### Supplemental Information

For

#### Licensee Event Report 79-17

# 1. Cause Description & Analysis

1. 1.

At approximately 1730 hours on June 11, 1979, with the plant in the cold shutdown condition, a primary to secondary leak was identified in "C" Steam Generator. The leak was identified by analyses for gross activity and boron concentration following investigation of a high alarm on the Radiation Monitoring System. The exact rate of leakage could not be determined due to plant conditions, but was assumed to be in excess of .35 gpm.

Following identification of the leak location, results of past eddy current examinations were reviewed, and a 38-42% through wall defect in the region just above the tube sheet was indicated. However, no increase in severity of the defect over the past several years was indicated. The leak was monitored during the secondary side draining, and the location of the leak was verified as being near the tube sheet. The precise mechanism of failure is not known.

## 2. <u>Corrective Action</u>

The primary system was drained to below the generator channel head, and the secondary side was drained to the tube sheet. The tube was explosively plugged and verified as leak-tight by static head pressure test.

# 3. Corrective Action To Prevent Further Occurrence

The on-going eddy current testing program and the removal of secondary sludge deposits by lancing, which the generators are subject to, will be continued in order to minimize the development of the leaks.