



# Update on 52 Weldability

**Influence of High Si-S Stainless Steels on the Solidification Cracking Susceptibility of High Chromium Nickel-Base Metals**

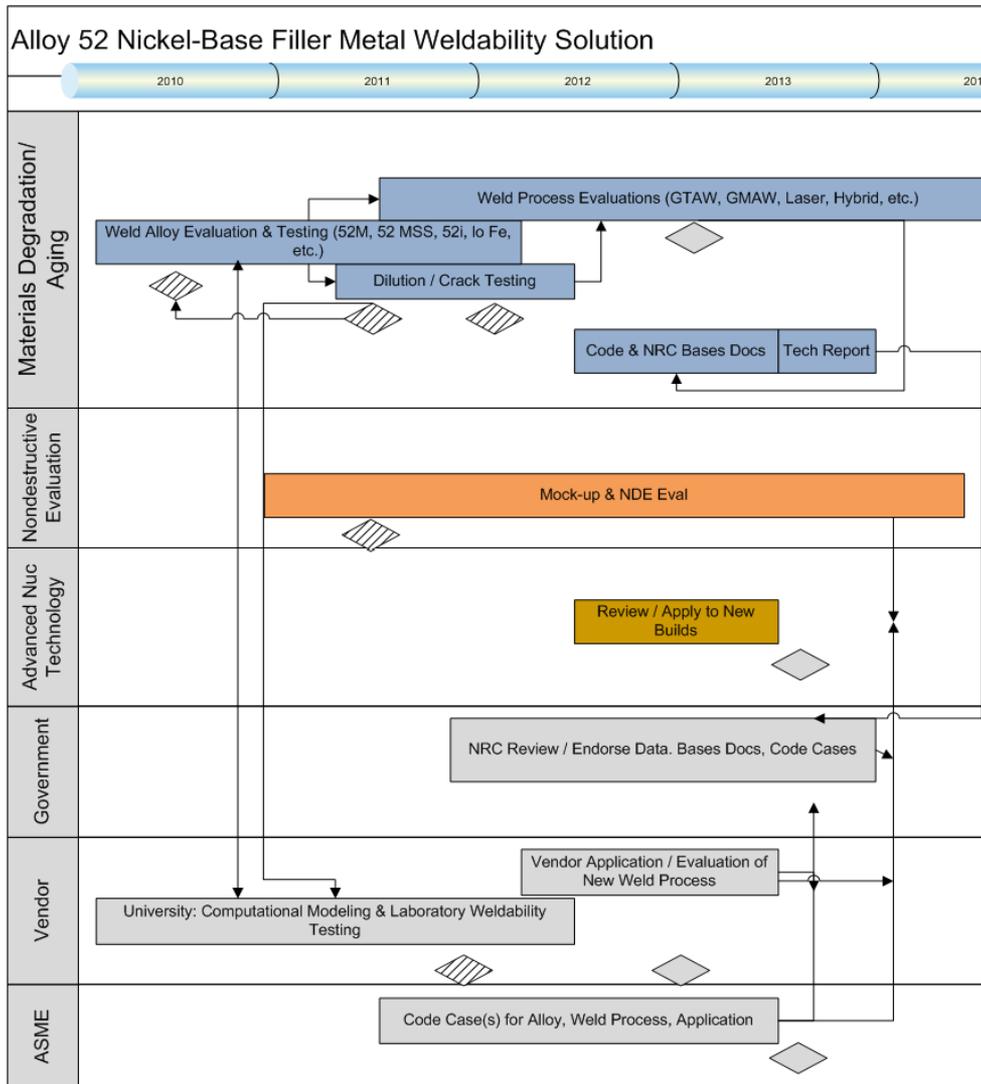
***Industry/U.S. NRC Materials Program Technical Information Exchange Meeting***

***Rockville, MD***

***Wednesday June 4, 2014***

**Steve McCracken and Jon Tatman**  
EPRI Welding & Repair Technology Center

# WRTC Roadmap: Alloy 52 Weldability Solution

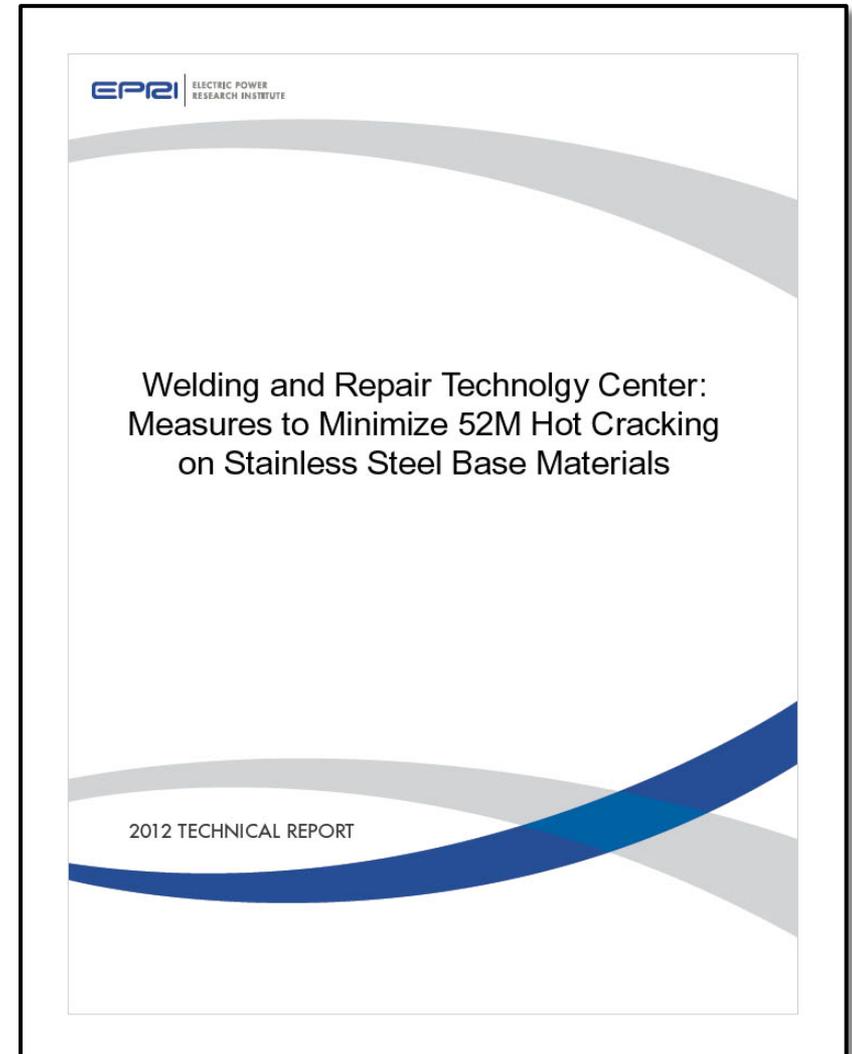


NUC\_MAT\_08\_R1 ALLOY 52 Nickel-base Filler Metal Weldability.vsd August 2012

- ✓ 52 Weldability Testing
- ✓ New High Cr Ni-Base Alloy
- ✓ ASME Code & NRC Support
- ✓ Magnetic Stir Welding
- ✓ **52M on CASS Studies**
- ✓ Low Dilution LBW
- ✓ Underwater LBW
- ✓ Friction Stir Welding
- ✓ Effective Heat Input Equation
- ✓ Effective Dilution Equation
- ✓ Inlay/Onlay Repair
- ✓ Excavate & Weld Repair
- ✓ **New Simplified DDC Test**

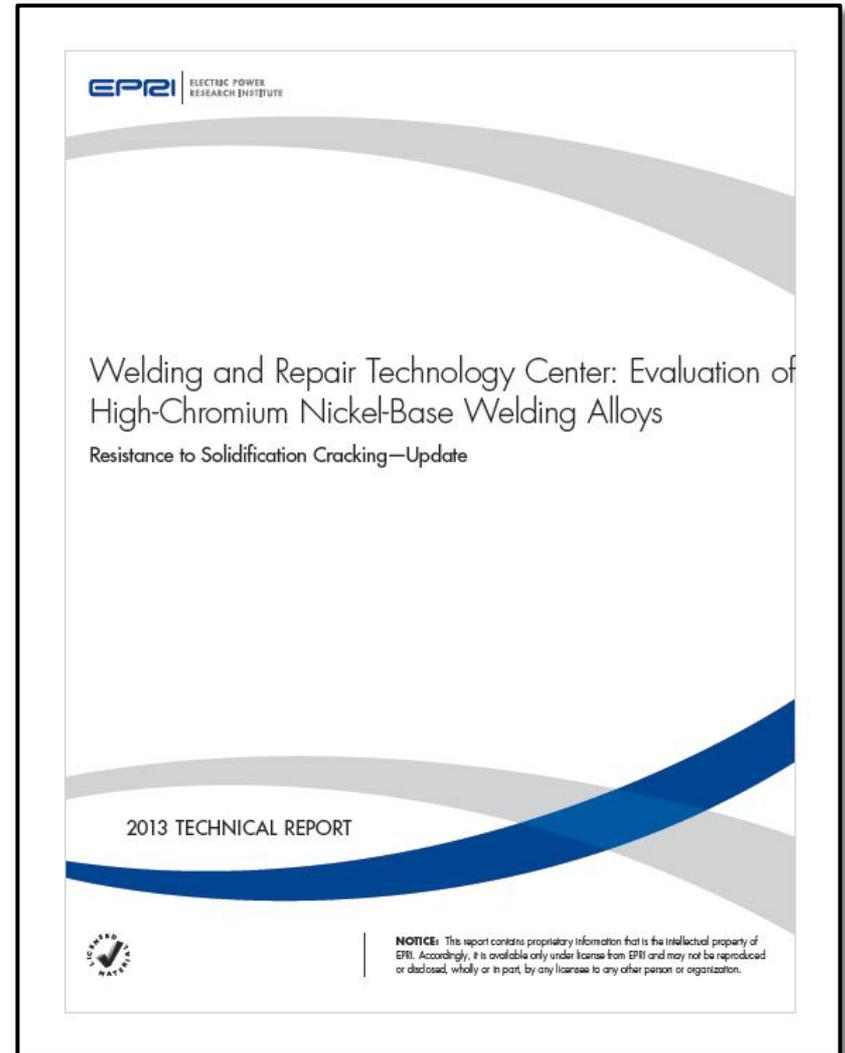
# EPRI Report 1025167

- **Measures to Minimize 52M Hot Cracking on Stainless Steel Base Materials**
- **Publication Date: December 2012**
  - Background on hot cracking experience
  - Focus on 52M
  - Hot cracking testing approach and test results
  - Discussion with measures to minimize hot cracking
  - Dilution control & buffer layer options
  - Future work



# EPRI Report 3002000641

- **Evaluation of High-Chromium Nickel-Base Welding Alloys**
- **Publication Date: August 2013**
  - Thermodynamic simulations
  - Single sensor differential thermal analysis
  - Transverse vareststraint testing
  - Cast pin tear testing
  - Strain to fracture testing
- Ranks susceptibility of filler metals to ductility-dip cracking and solidification cracking
- Discusses cracking mechanisms



# 52M Hot Cracking on Stainless Steel

## *Presentation Outline*

- Background and Motivation
- Test Design and Approach
- Test Results and Observations
  - Hot Crack Ranking of Filler Metals Tested
  - Influence of Si and S on Hot Cracking
  - Influence of Si and S on Dilution and Bead Shape
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- Conclusions and Guidelines

# Ductility-Dip and Solidification (Hot) Cracking

## Ductility-dip Temperature Range (DTR)

ductility-dip ~ 10% to 15% strain  
 ~ 950°C to 1150°C temperature range

## Brittle Temperature Range (BTR)

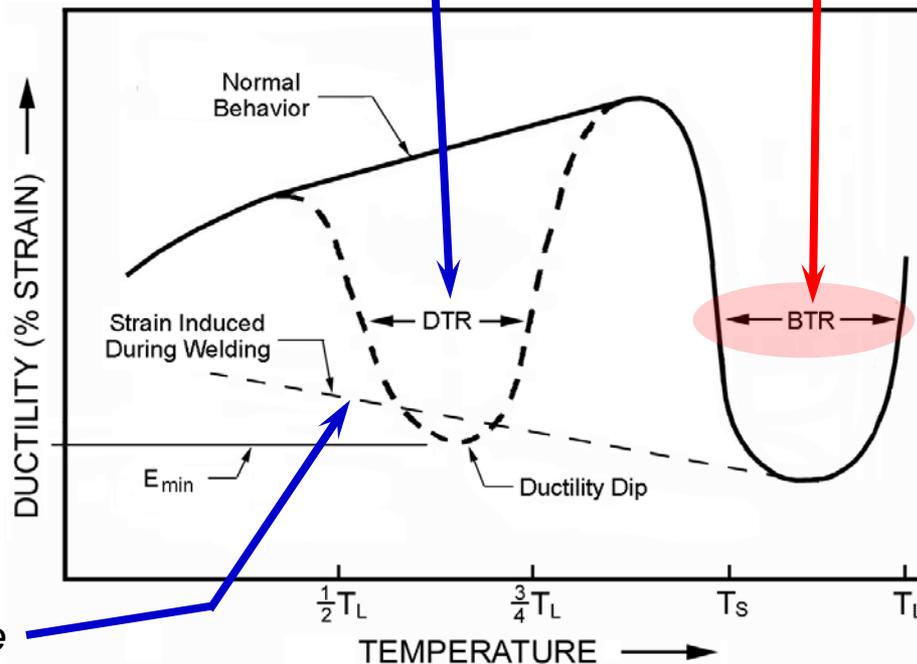
~ liquidus to terminal solidus

### Ductility-dip Cracking

Solid state cracking mechanism that occurs in the ductility-dip temperature range (reheated weld metal)

### Solidification Cracking

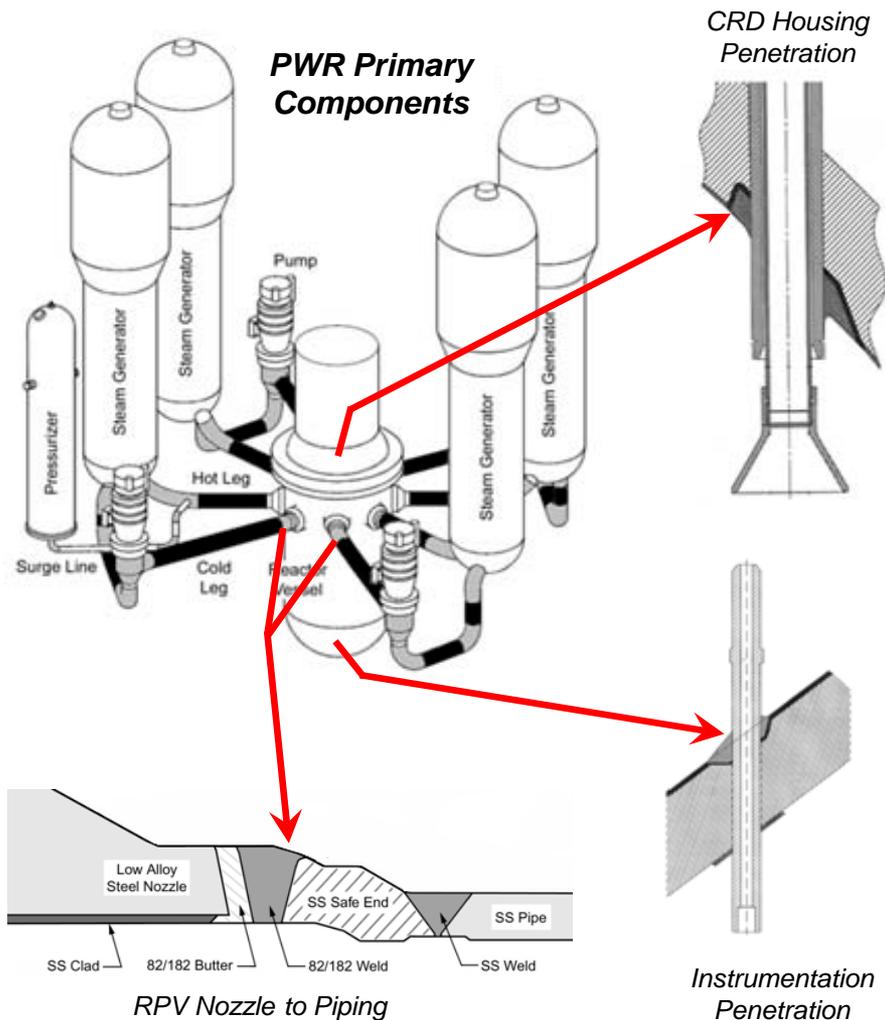
Liquation cracking mechanism that occurs during solidification in the brittle temperature range (mushy zone)



Strain applied  
 Due to weld shrinkage  
 & joint restraint

# Nuclear Power Industry Issue

## 52/152 Hot Cracking on Stainless Steel



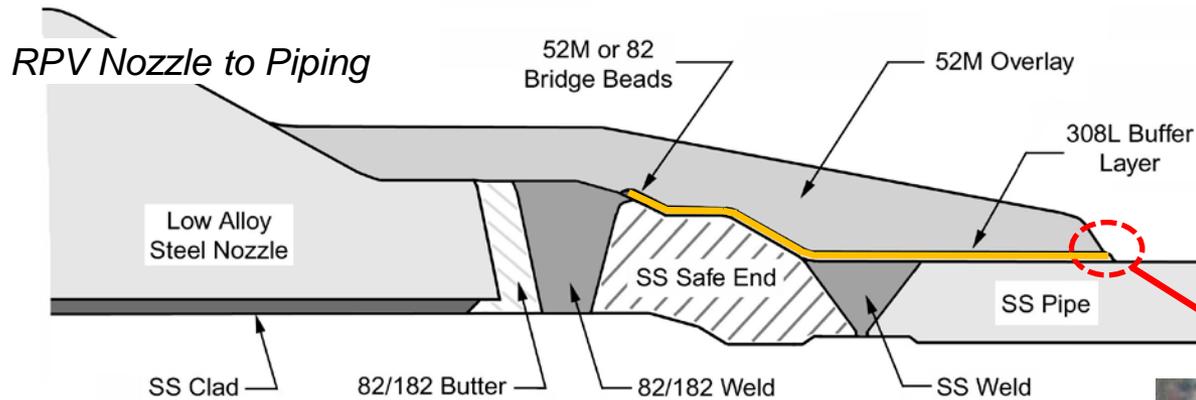
- 82/182 (Ni-18Cr alloy) was used extensively in PWR & BWR dissimilar metal welds
- 82/182 is degraded by PWSSC and IGSSC
- 52/152 (Ni-30Cr alloy) is resistant to SCC and is the weld metal of choice for repair, SCC mitigation, and new fabrication
- Experience and testing shows that Ni-30Cr weld metals are susceptible to solidification (hot) cracking when welding on some stainless steel materials

# 52M Hot Cracking



## Weld Overlay Repair on Cast Stainless Steel Reactor Coolant Pipe

- Example of 52M hot cracks on CF8A with ER308L buffer layer
- Base metal is SA-351 CF8A (0.019% S, 0.032% P, 0.72% Si)



Hot cracks in 52M on CF8A material

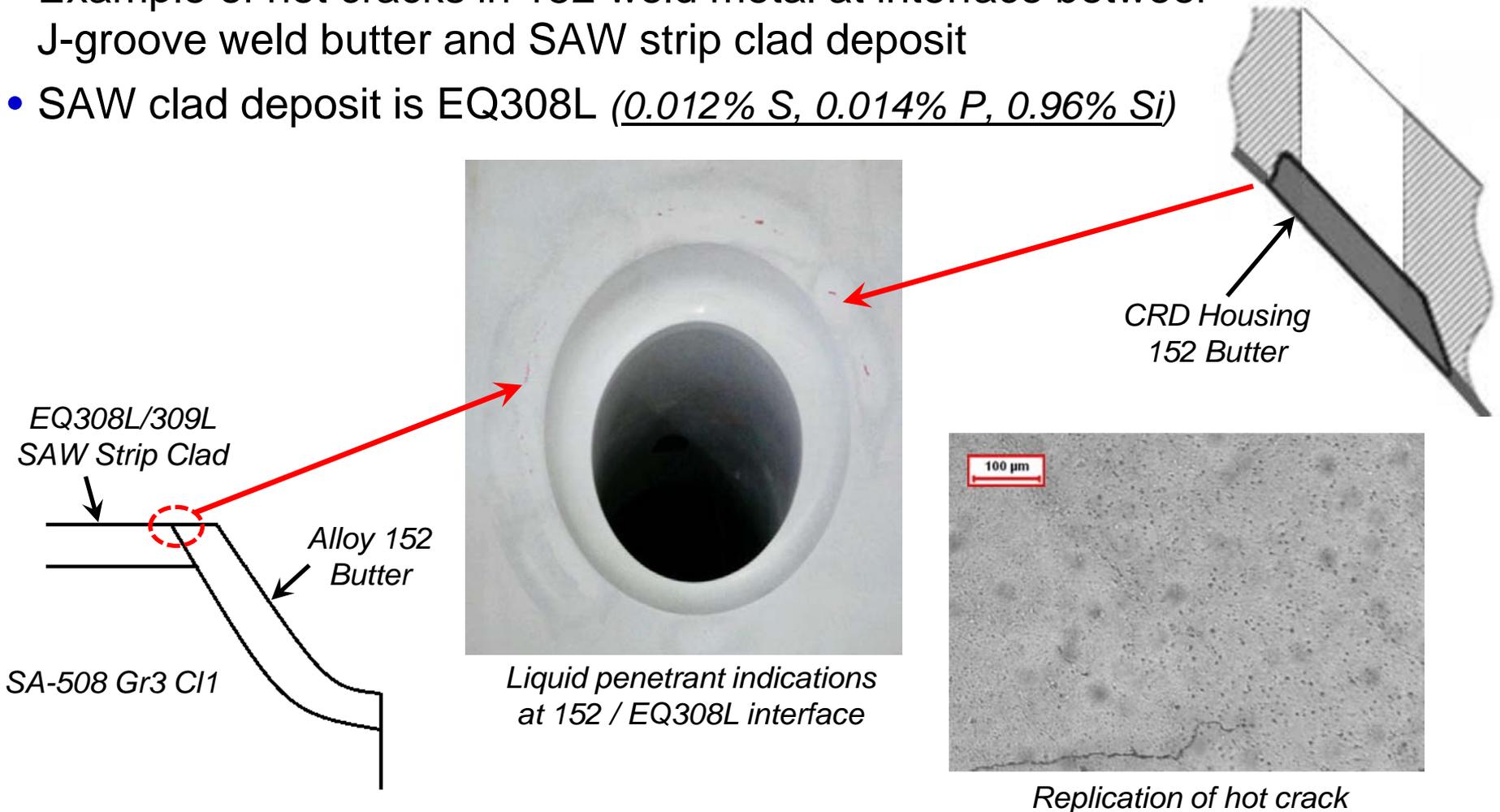


Liquid penetrant indications in 52M over ER308L buffer

# 152 Hot Cracking

## *Buttering in J-groove Pocket on Reactor Vessel Head*

- Example of hot cracks in 152 weld metal at interface between J-groove weld butter and SAW strip clad deposit
- SAW clad deposit is EQ308L (0.012% S, 0.014% P, 0.96% Si)



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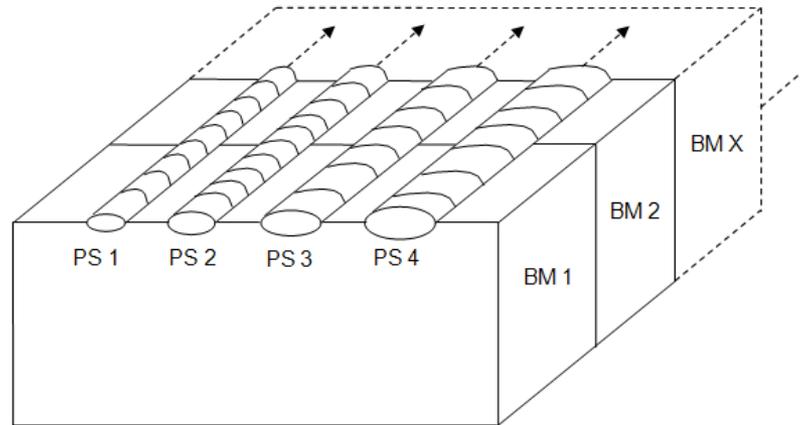
# Focus and Goal of Testing

## *Industry Requested and Needed Simple Guidelines*

- Focus of the test program
  - Understand influence of austenitic stainless steel dilution on high chromium nickel-base (Ni-30Cr) filler metal hot cracking
  - What is a safe level of Ni-30Cr dilution with high Si-S stainless steels?
  - What is influence of Si and S on dilution?
  - What are safe S+P and Si thresholds for crack free welds?
  - What is the relative potency of Si and S on Ni-Cr30 hot cracking?
  - Is one variant of Ni-30Cr weld metal more resistant to hot cracking?
- Goal of the test program
  - Develop simple industry guidelines to manage Ni-30Cr hot cracking when welding on high Si-S austenitic stainless steels

# Bead-on-plate Testing Approach

*GTAW and SMAW on Two Sets of Base Materials*



Bead-on-Plate Setup



CASS Specimen

152-152M Beads on CASS Specimens



52M Beads on CASS Specimens



Machine GTAW Setup

# Base Metal Samples & Filler Metals Tested

## *Test Matrix Overview*

- Cast SA-351 CF8A (Type 304) is base composition with min and max specified Si and S to simulate reactor coolant piping

Si & S wt% matrix compositions:

Silicon Low - Med - High

0.05 - 0.90 - 1.80

Sulfur Low - Med - High

0.001 - 0.020 - 0.040

- Weld metal matrix:

– 82 (ERNiCr-3)

– 52 (ERNiCrFe-7)

– 52M (ERNiCrFe-7A)

– 52MSS (ERNiCrFe-13)

– 52i (ErNiCrFe-15)

– 152 (ENiCrFe-7)

– 152M (ENiCrFe-7)

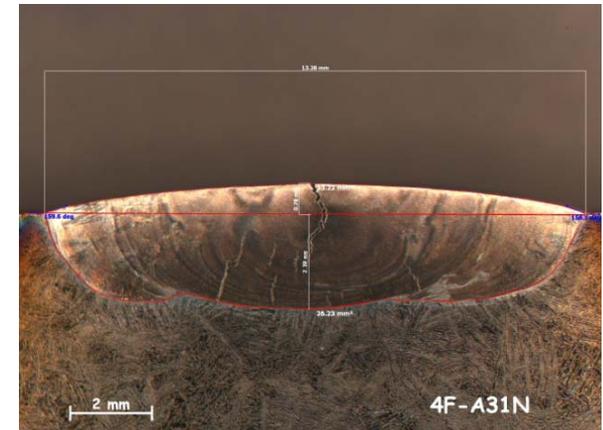
– 622 (ERNiCrMo-10)

– 625 (ERNiCrMo-3)

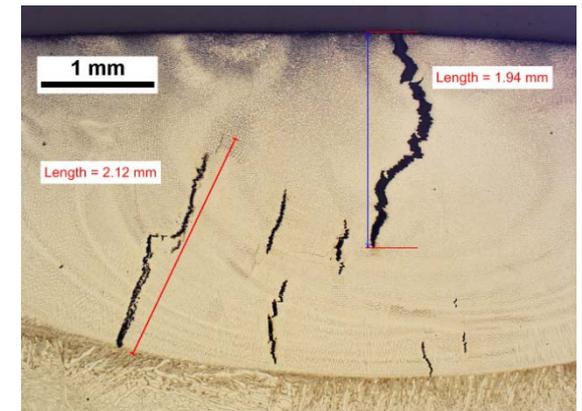
# Hot Crack Characterization

## *Specified Methodology Used for All Specimens*

- Measured and recorded the following:
  - ✓ Composite zone areas, toe angle(s), depth, width, and penetration
- Calculated dilution by area method
- Inspected for cracks at 50x
- Cracks graded as follows:
  - ✓ TNC – Total Number of Cracks > 0.2 mm
  - ✓ TCL – Total Crack Length (sum of all cracks)
  - ✓ MCL – Maximum Crack Length (single largest crack length)
  - ✓ Cracks within  $\leq 0.2$  mm proximity are counted and sized as one crack
  - ✓ Cracks categorization as:
    - Surface Crack
    - Midwall Crack
    - Fusion Line Crack
    - Evidence of backing filling was noted



*82 Bead on A31N sample*



*25x Micrograph 82 on A31N sample*

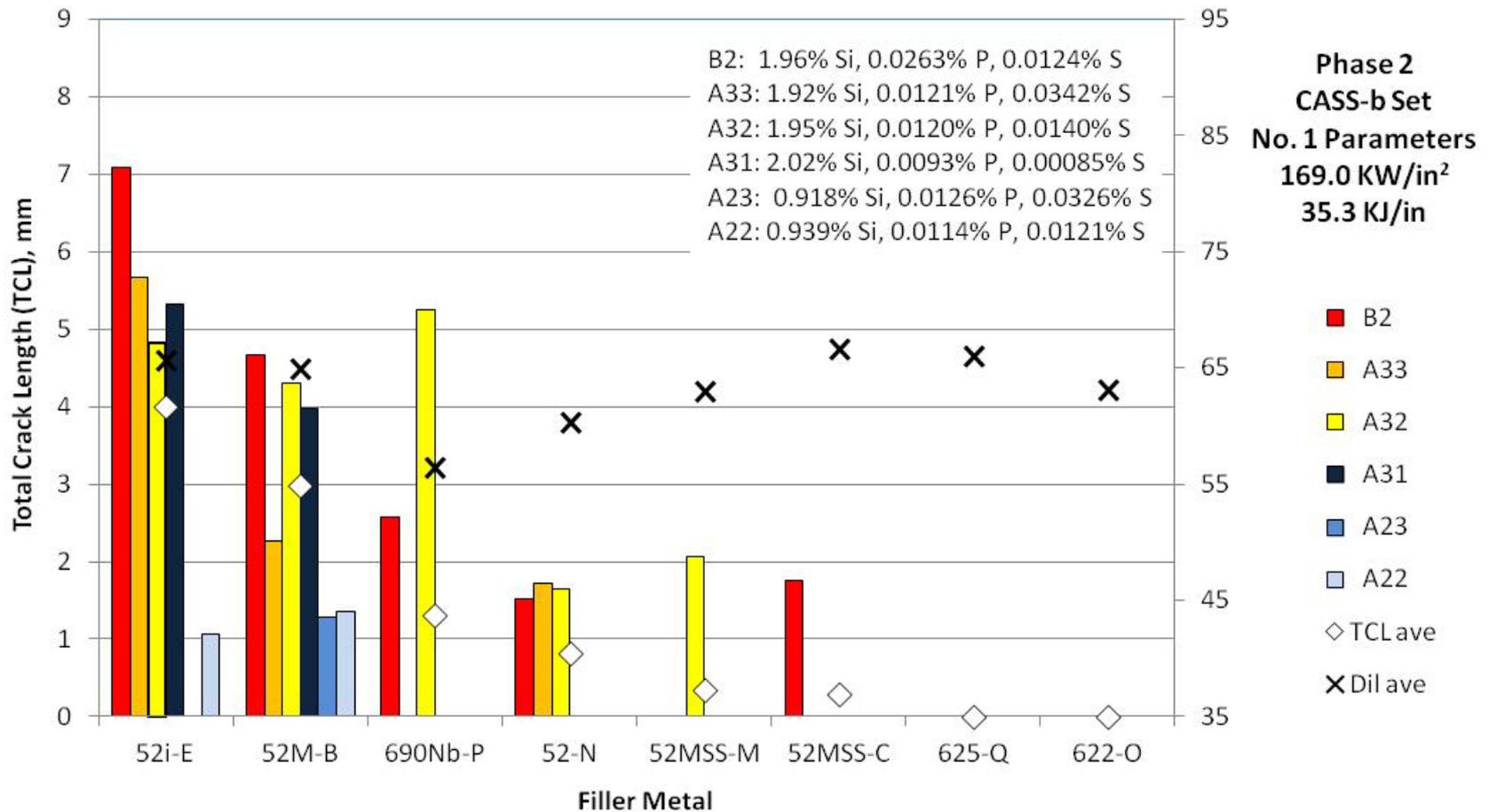
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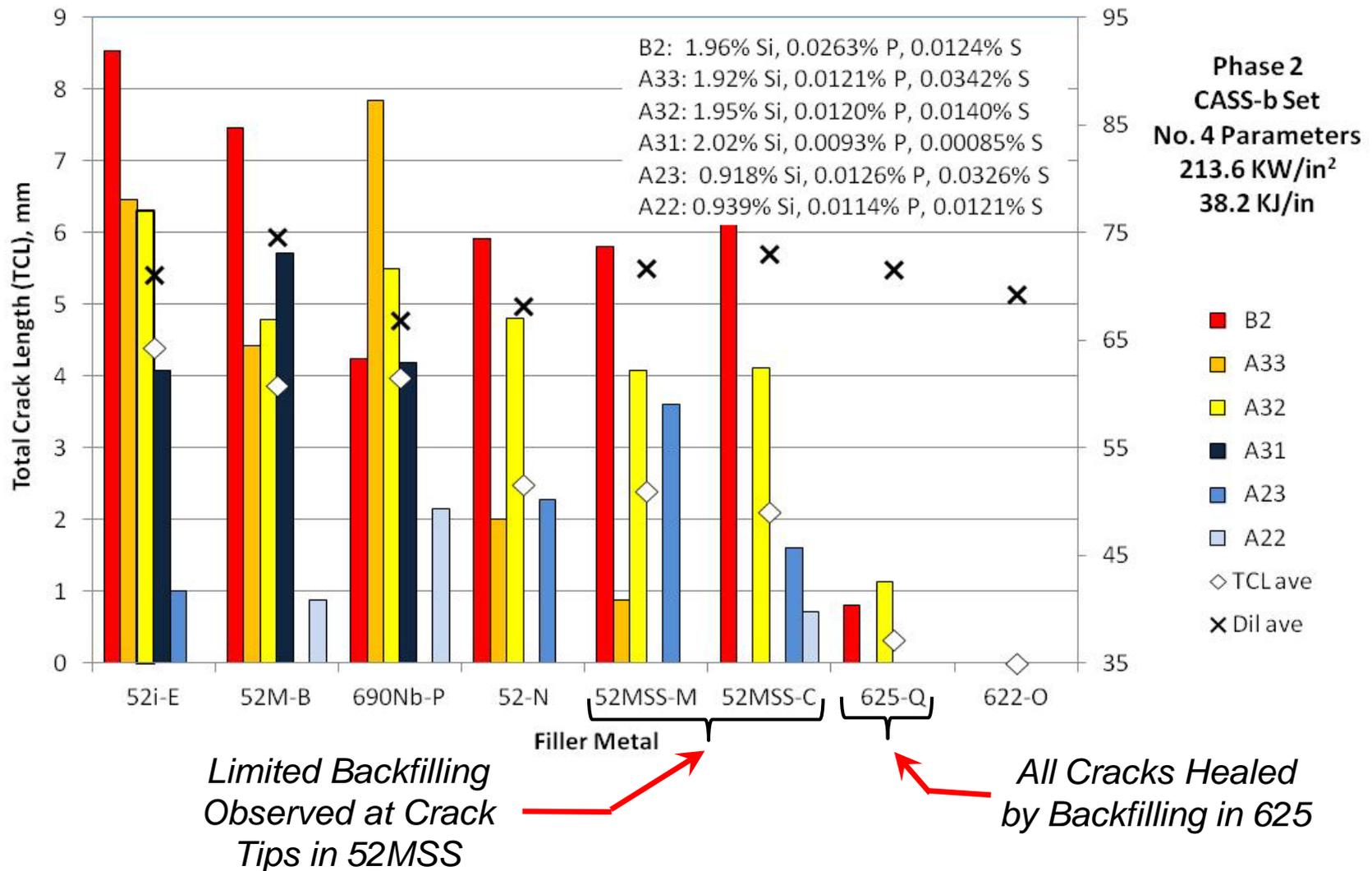
# Hot Crack Response Comparison by Filler Metal

Phase 2 CF8A CASS-b Set (169.0 KW/in<sup>2</sup>)



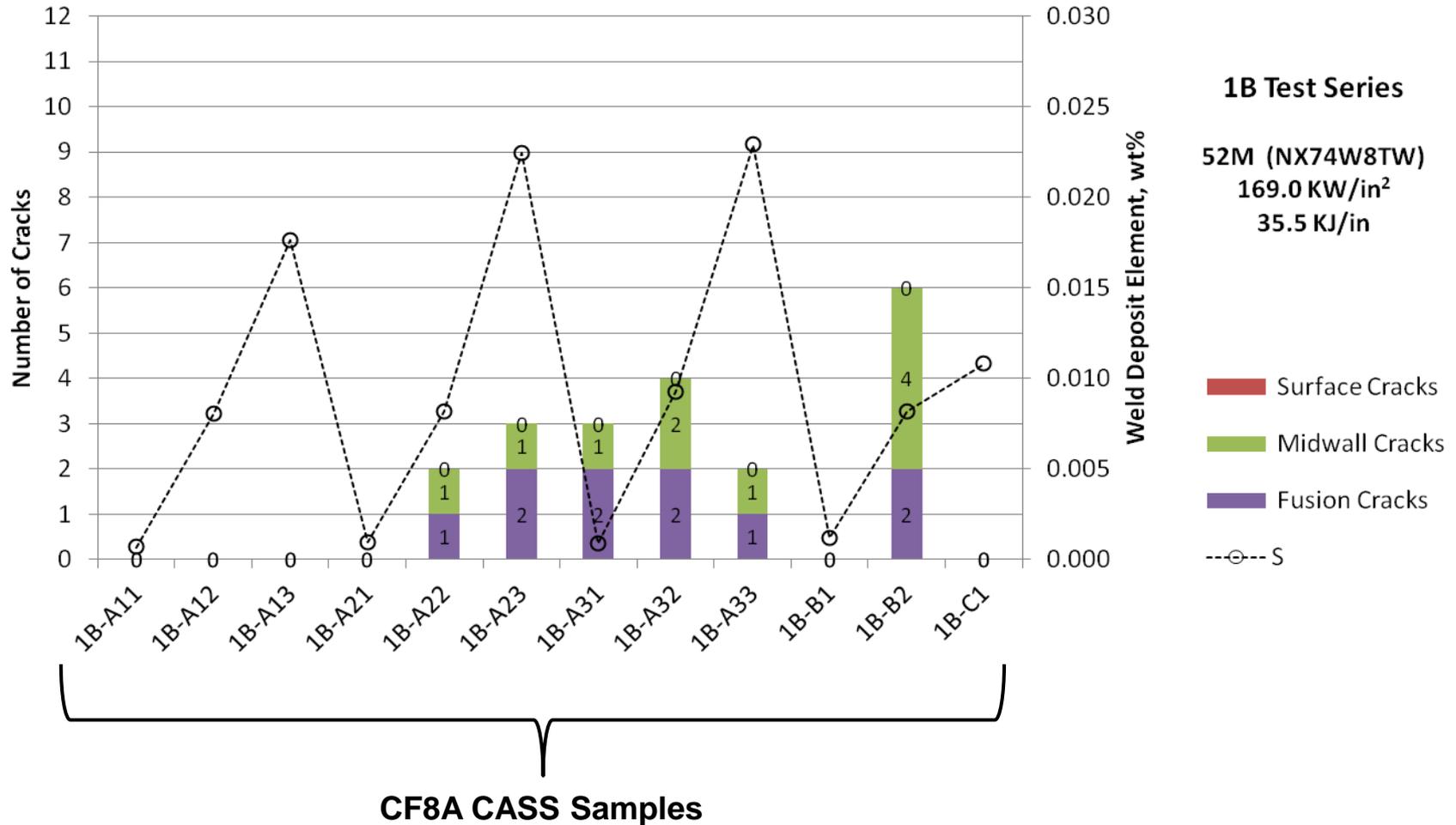
# Hot Crack Response Comparison by Filler Metal

Phase 2 CF8A CASS-b Set (213.6 KW/in<sup>2</sup>)



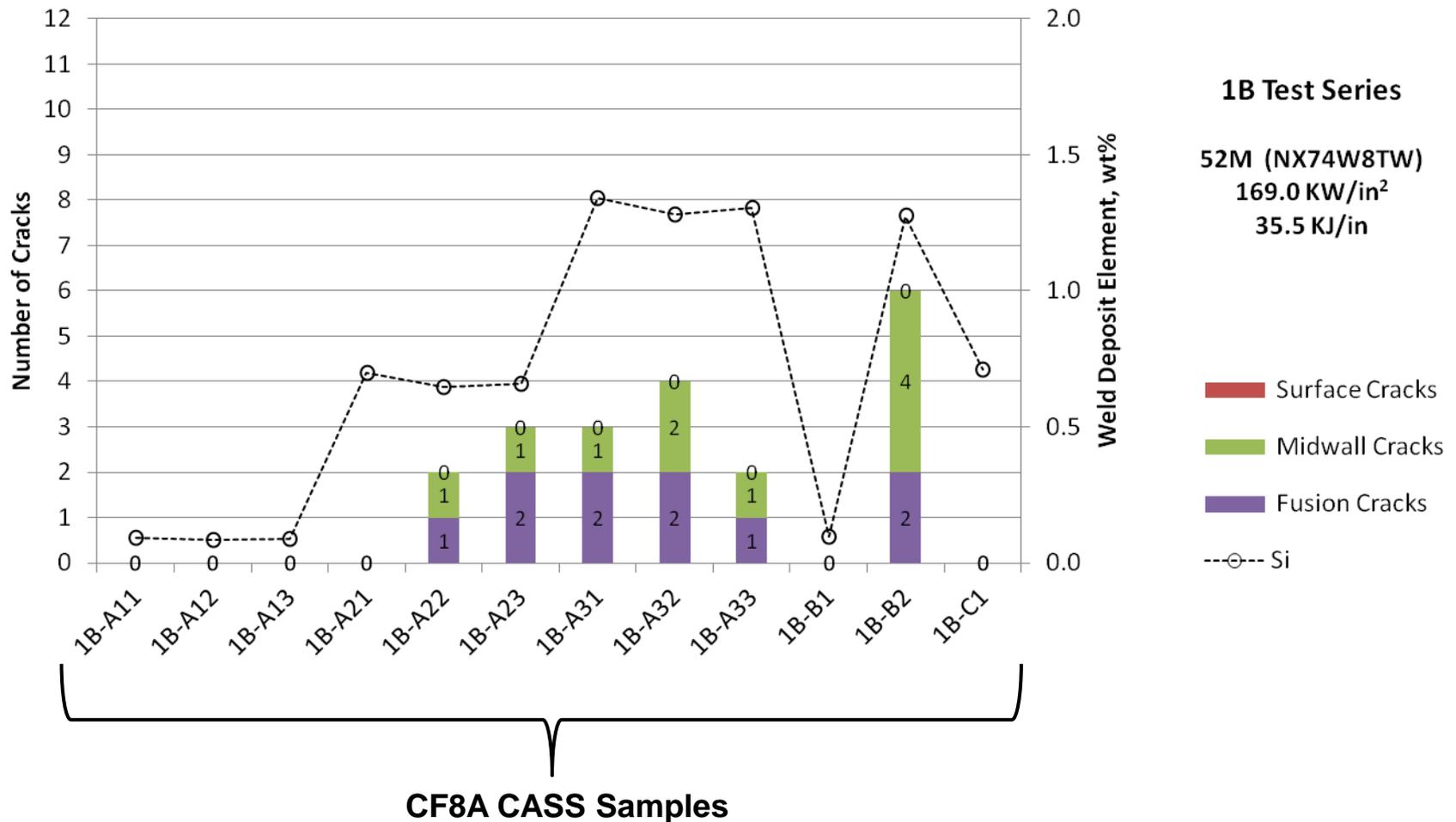
# Crack Susceptibility Plot with Sulfur (S)

*GTAW – 52M-B on CASS-b material set*



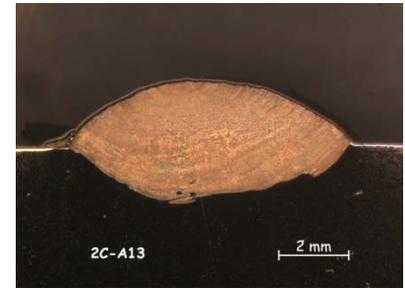
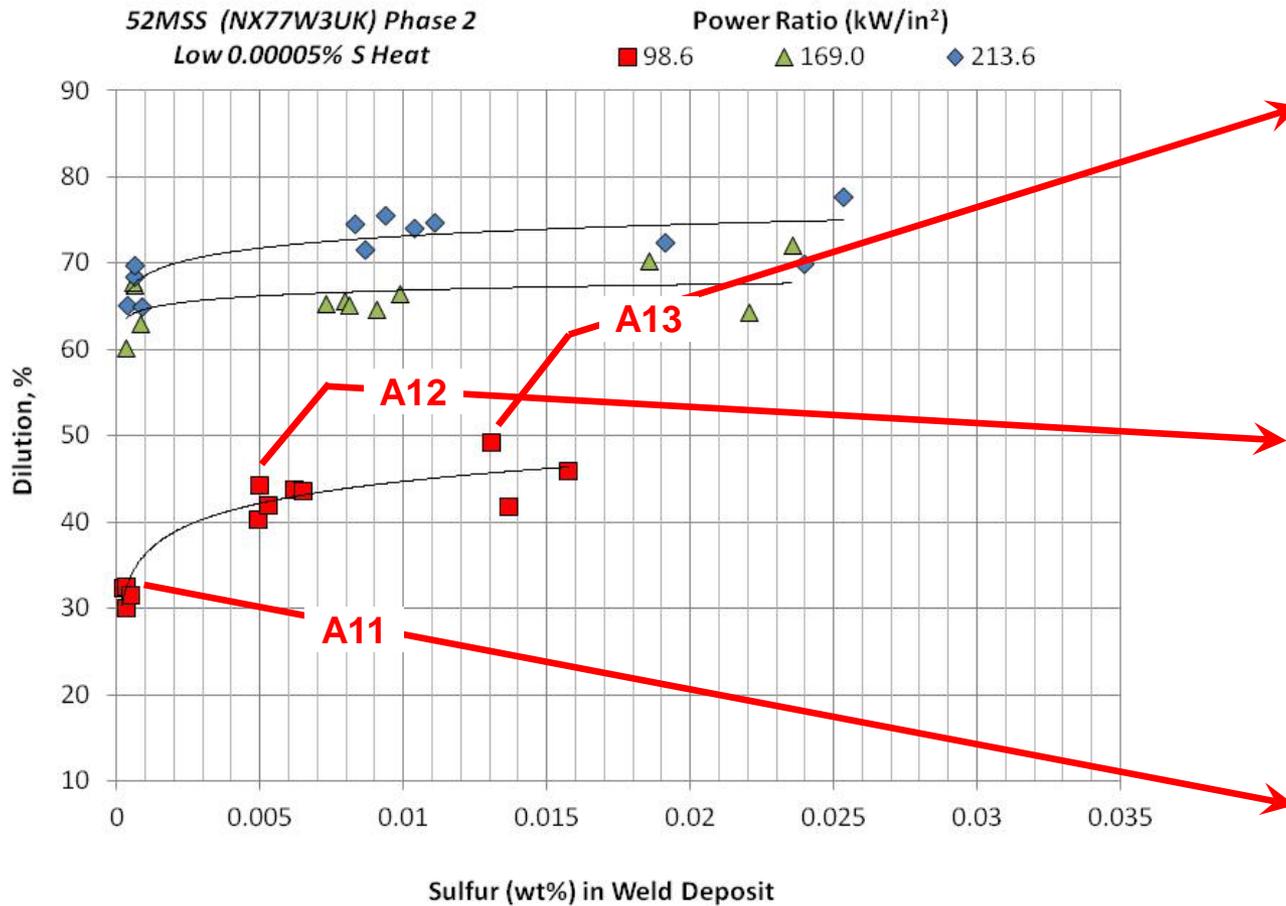
# Crack Susceptibility Plot with Silicon (Si)

*GTAW – 52M-B on CASS-b material set*

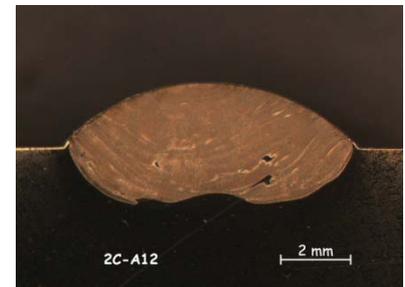


# Influence of S on Low Si Samples

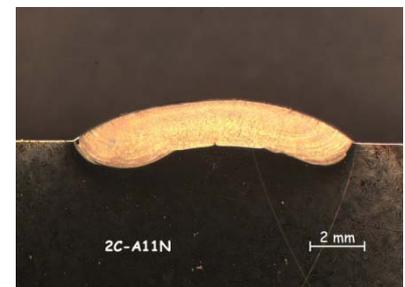
*FM 52MSS-C with Ultra Low 0.00005% S*



*0.09 Si - 0.0130 S*



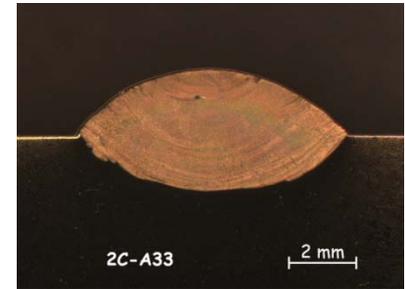
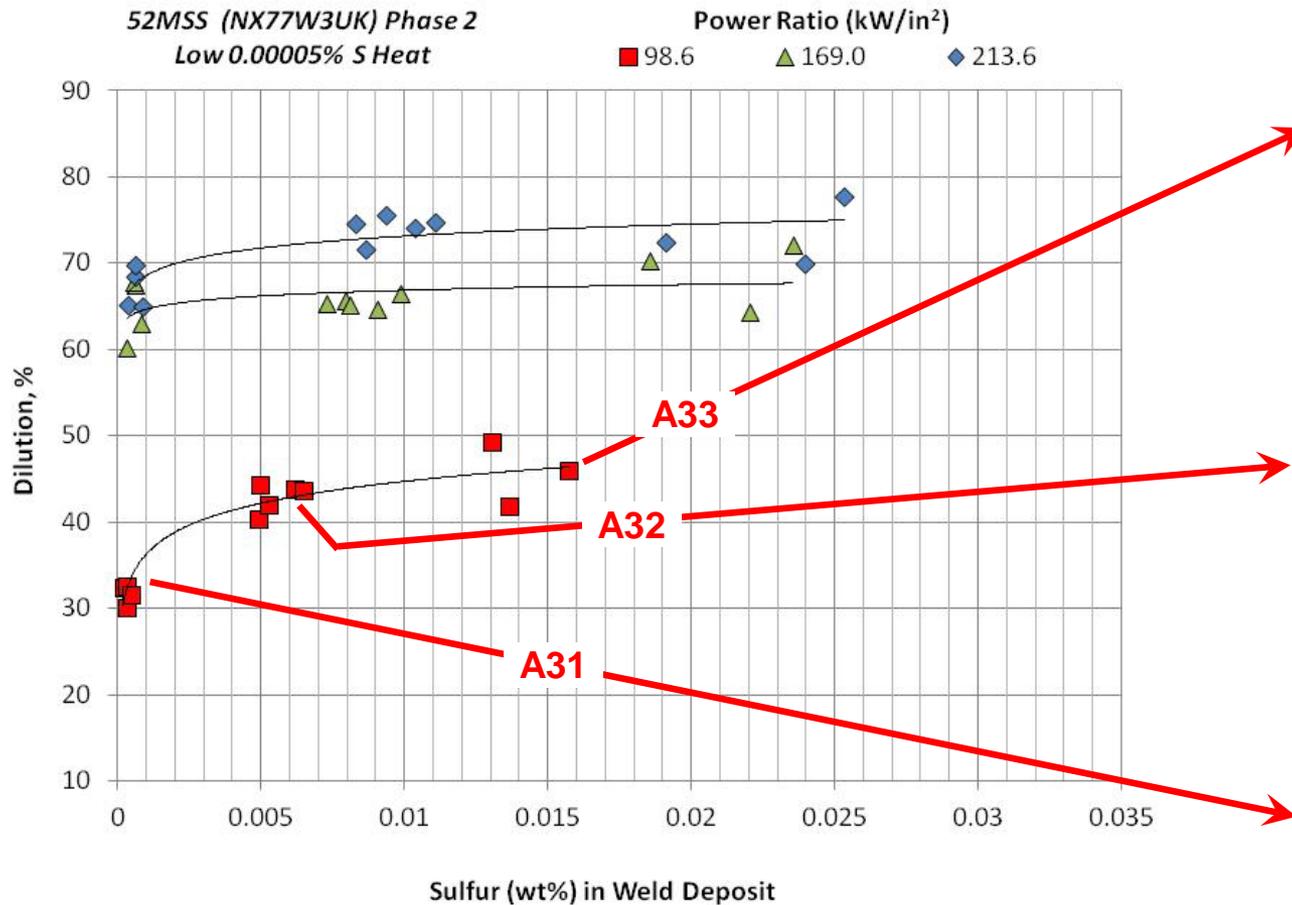
*0.09 Si - 0.0050 S*



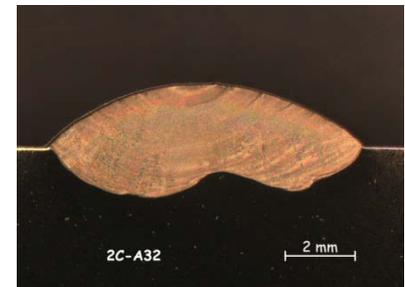
*0.10 Si - 0.0002 S*

# Influence of S on High Si Samples

*FM 52MSS-C with Ultra Low 0.00005% S*



0.94 Si - 0.0157 S



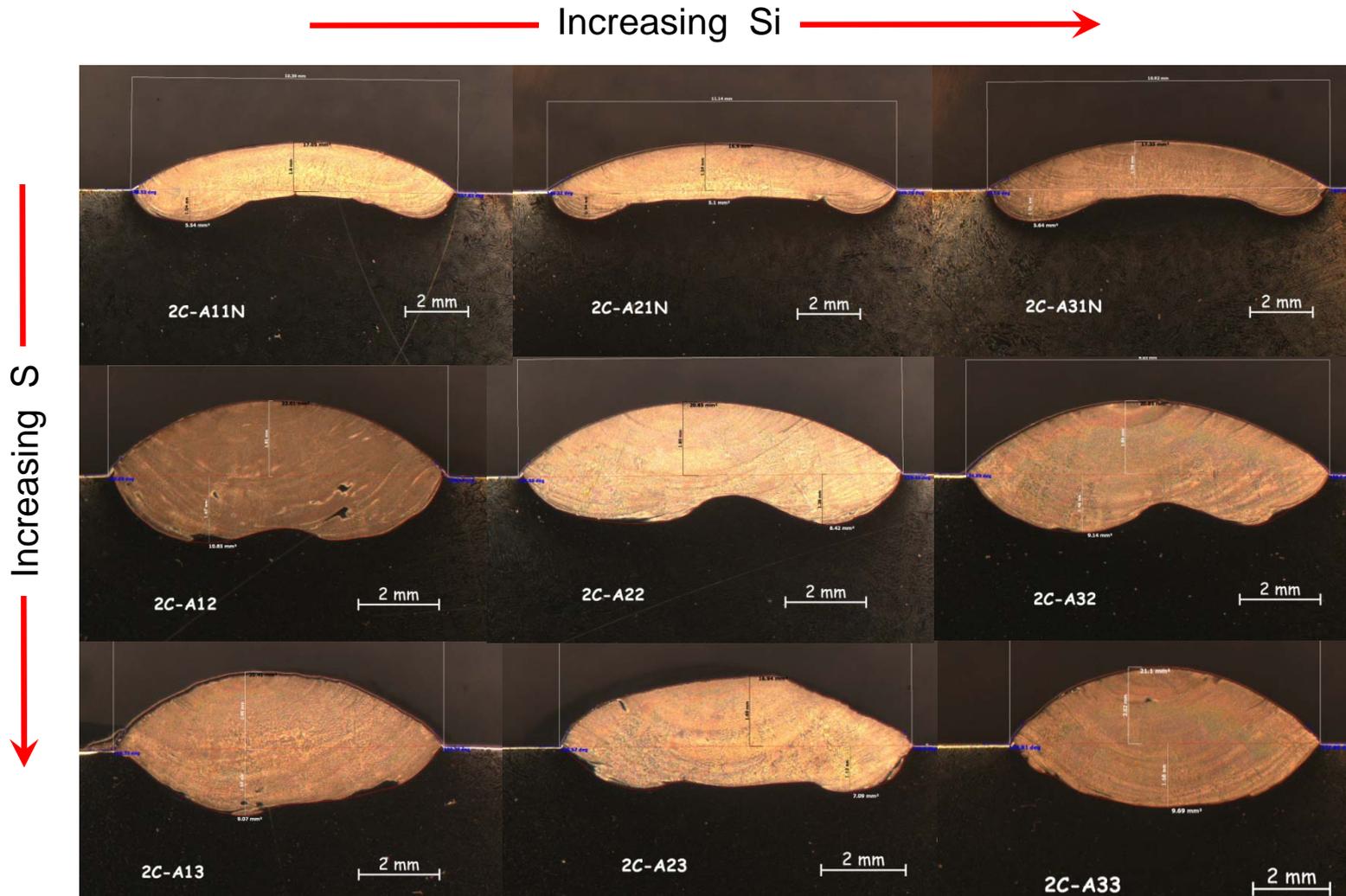
0.91 Si - 0.0062 S



0.73 Si - 0.0003 S

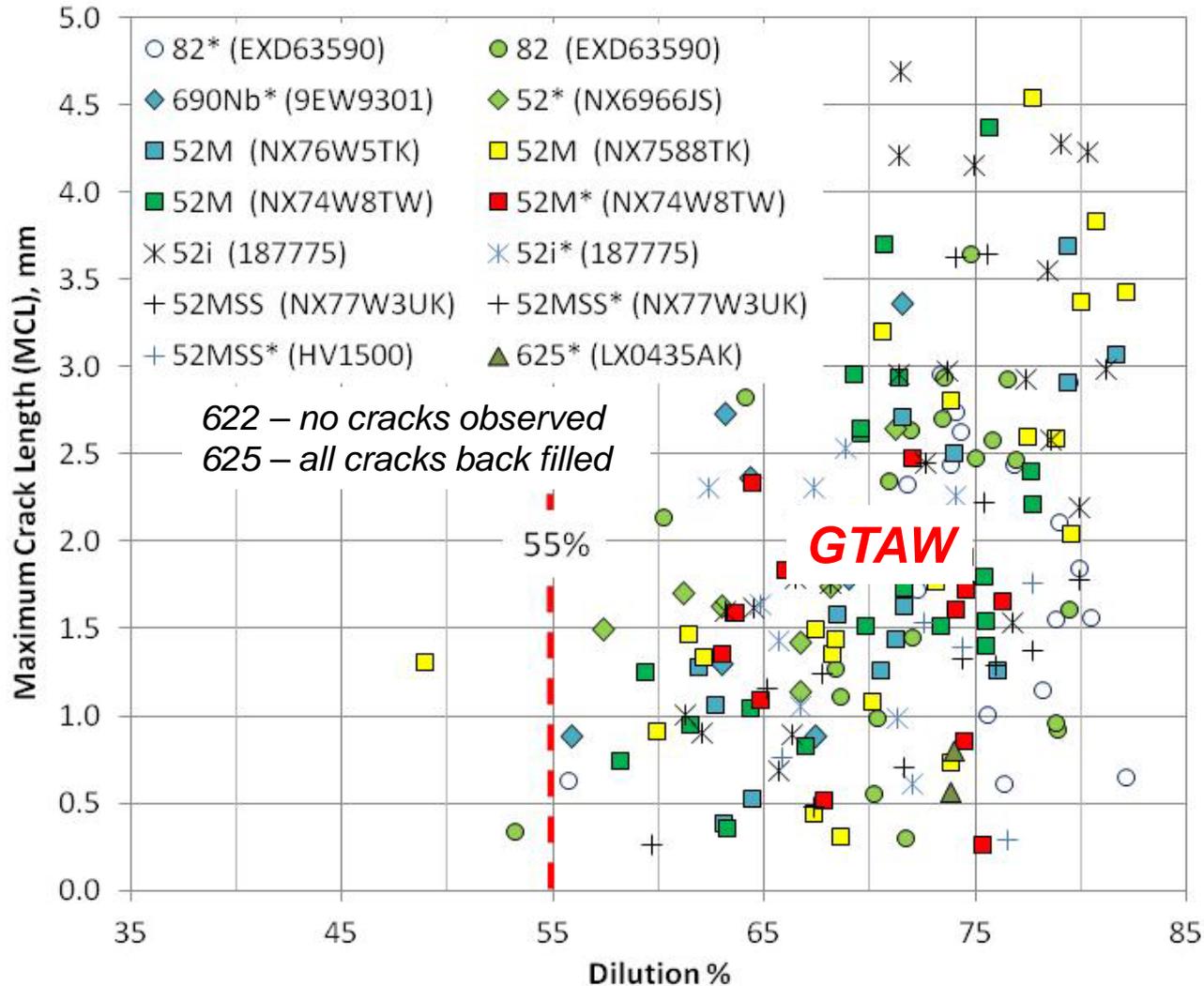
# Influence of Si and S on Bead Shape

52MSS-C (0.00005% S Wire with Power Ratio 98.6 kW/in<sup>2</sup>)



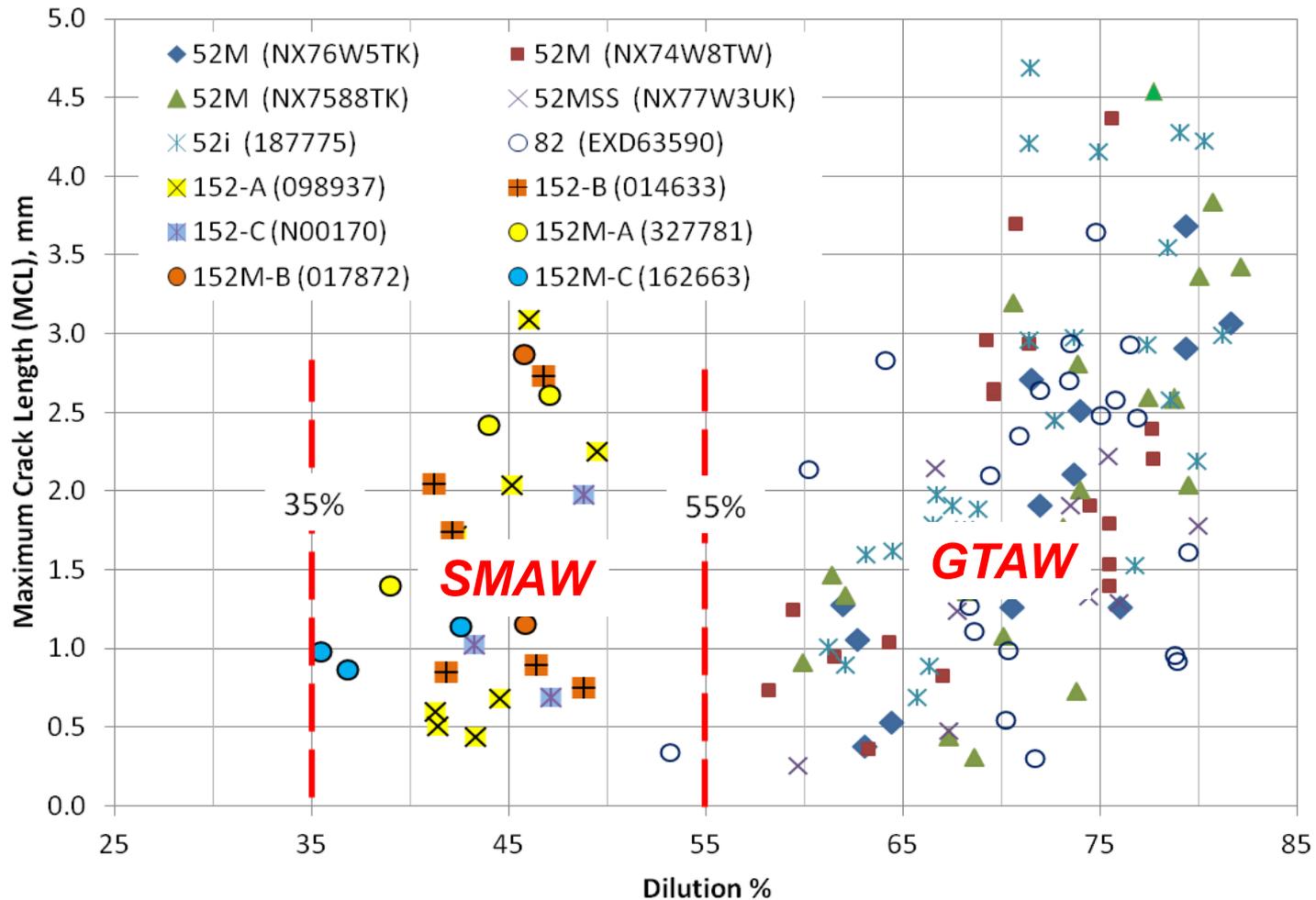
# Maximum Crack Length vs Dilution

## GTAW Phase 1 & 2



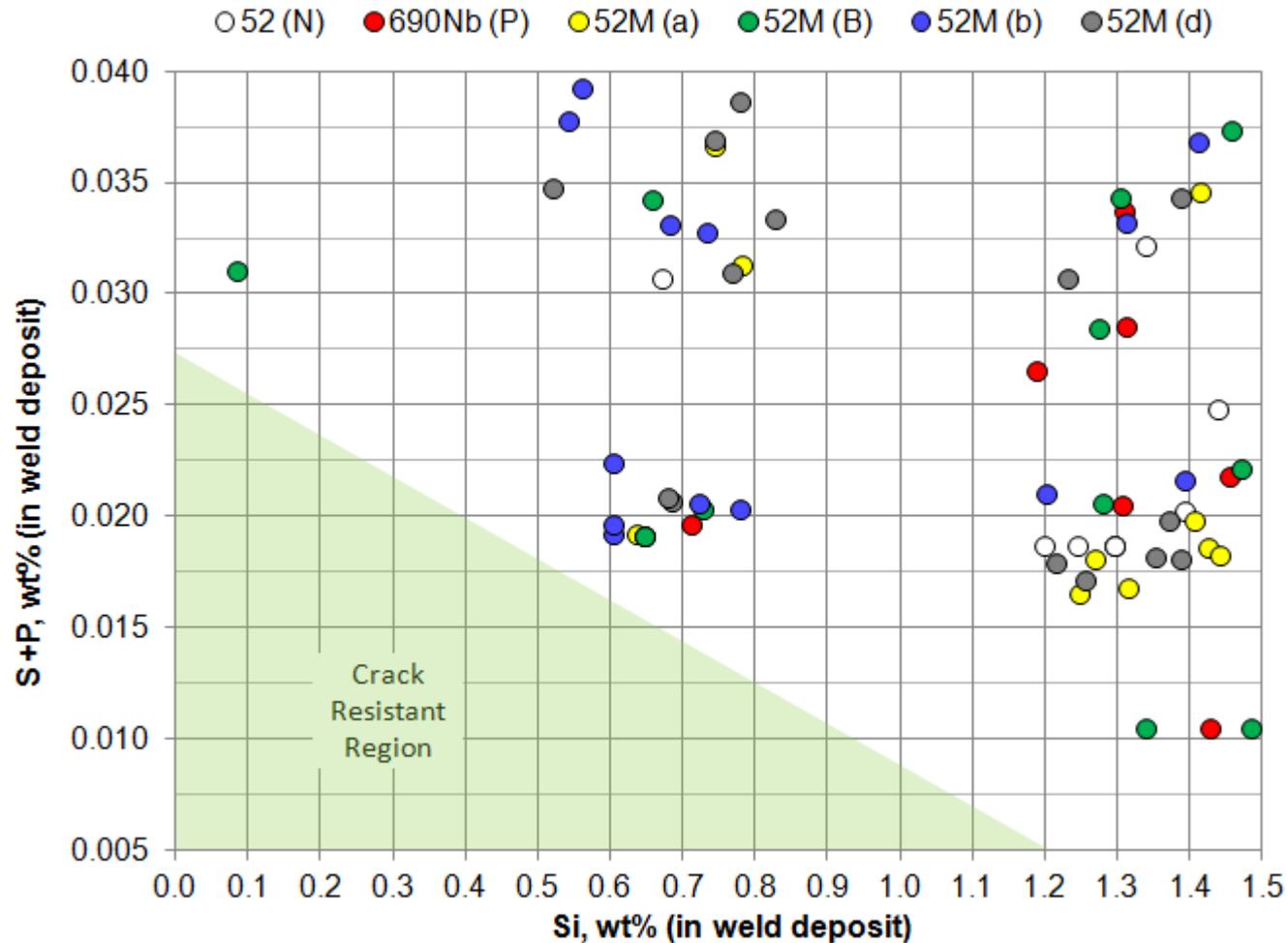
# Maximum Crack Length vs Dilution

GTAW Phase 1 & SMAW Phase 3



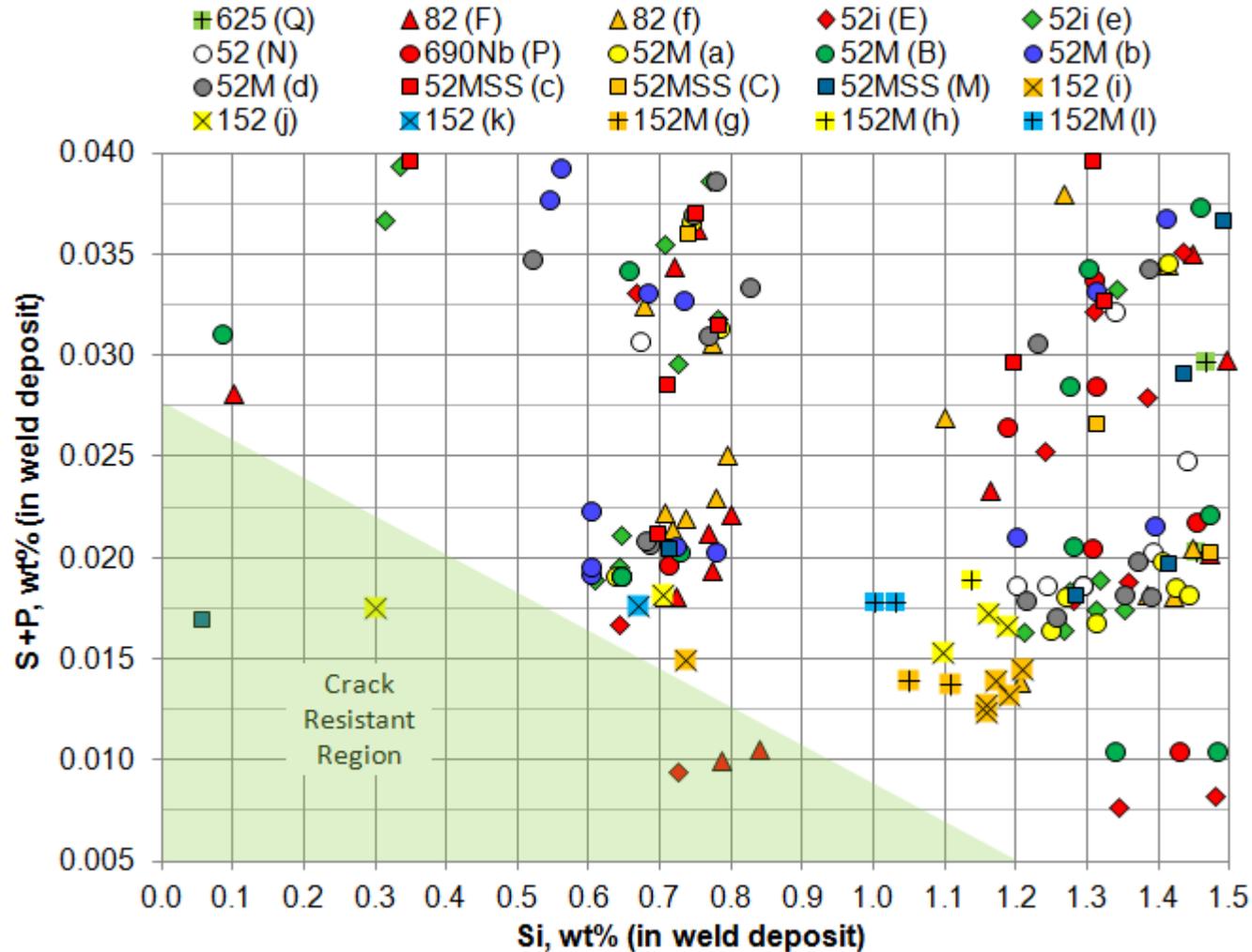
# S+P vs Si Plot with Crack Resistant Region

52 and 52M GTAW Phase 1 & 2



# S+P vs Si Plot with Crack Resistant Region

GTAW Phase 1 & 2 and SMAW Phase 3



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# Conclusions

## *Hot Cracking From Dilution with Stainless Steel*

- Ranking of filler metals tested from most to least resistant  
 $622$  (*crack free*) <  $625$  (*back filled*) <  $52MSS$  <  $52$  <  $52M$  <  $52i$
- High silicon in austenitic stainless steel promotes hot cracking in high Cr Nickel-base filler metals
- High sulfur did not strongly promote hot cracking
- Dilution can vary as much as 25% between 0.00005% and 0.034% S base materials
- Dilution control ( $\leq 55\%$  for GTAW and  $\leq 35\%$  for SMAW) is an effective tool to prevent hot cracking of Ni-30Cr weld metals when welding on high Si-S stainless steel

# Considerations to Prevent Hot Cracking

## *Guidelines for Welding with Ni-30Cr Alloys on Stainless Steel*

- **Dilution Control**

- GTAW dilution  $\leq 55\%$  (52M, 52i, 52MSS, 690Nb, or 82)
- SMAW dilution  $\leq 35\%$  (152 & 152M)

- **Composition Control**

- Use base material MTR to evaluate composition effect on welding
- Maintain following limits in diluted weld deposit  
 $S < 0.020 \text{ wt\%}; Si < 0.60 \text{ wt\%}; S+P < 0.030 \text{ wt\%}$
- Consider effect of base metal S on dilution and weld parameters
- Consider influence of joint geometry and welding position on dilution

- **Process Parameter Control**

- Develop welding parameters and techniques to appropriately control dilution
- Test weld parameters and understand potential difference of dilution on low versus high S base materials

## EPRI Contacts:

Steve McCracken – [smccracken@epri.com](mailto:smccracken@epri.com) 704-595-2627

Jon Tatman – [jtatman@epri.com](mailto:jtatman@epri.com) 704-595-2762

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