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April 23, 2014  
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U. S. Nuclear Regulatory Commission  
Attention: Document Control Desk  
Washington, DC 20555-0001

South Texas Project  
Unit 1  
Docket No. STN 50-498  
Unit 1 Cycle 19 Core Operating Limits Report

Pursuant to Technical Specification 6.9.1.6.d, STP Nuclear Operating Company submits the attached Core Operating Limits Report for Unit 1 Cycle 19. The report covers the core design changes made during the 1RE18 refueling outage.

There are no commitments included in this letter.

If there are any questions on this report, please contact Wendy Brost at (361) 972-8516 or me at (361) 972-7743.

A handwritten signature in black ink that reads 'R. F. Dunn'.

Roland F. Dunn  
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Attachment: Unit 1 Cycle 19 Core Operating Limits Report, Revision 0

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NRR

STI: 33857840

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**SOUTH TEXAS PROJECT**

**Unit 1 Cycle 19**

**CORE OPERATING LIMITS REPORT**

Revision 0

## 1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report for STPEGS Unit 1 Cycle 19 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

- 1) 2.1 SAFETY LIMITS
- 2) 2.2 LIMITING SAFETY SYSTEM SETTINGS
- 3) 3/4.1.1.1 SHUTDOWN MARGIN
- 4) 3/4.1.1.3 MODERATOR TEMPERATURE COEFFICIENT LIMITS
- 5) 3/4.1.3.5 SHUTDOWN ROD INSERTION LIMITS
- 6) 3/4.1.3.6 CONTROL ROD INSERTION LIMITS
- 7) 3/4.2.1 AFD LIMITS
- 8) 3/4.2.2 HEAT FLUX HOT CHANNEL FACTOR
- 9) 3/4.2.3 NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR
- 10) 3/4.2.5 DNB PARAMETERS

## 2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

### 2.1 SAFETY LIMITS (Specification 2.1):

- 2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature ( $T_{avg}$ ) shall not exceed the limits shown in Figure 1.

### 2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

- 2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.

2.2.2 The Over-temperature  $\Delta T$  and Over-power  $\Delta T$  setpoint parameter values are listed below:

### Over-temperature $\Delta T$ Setpoint Parameter Values

- $\tau_1$  measured reactor vessel  $\Delta T$  lead/lag time constant,  $\tau_1 = 8$  sec
- $\tau_2$  measured reactor vessel  $\Delta T$  lead/lag time constant,  $\tau_2 = 3$  sec
- $\tau_3$  measured reactor vessel  $\Delta T$  lag time constant,  $\tau_3 = 2$  sec
- $\tau_4$  measured reactor vessel average temperature lead/lag time constant,  $\tau_4 = 28$  sec
- $\tau_5$  measured reactor vessel average temperature lead/lag time constant,  $\tau_5 = 4$  sec
- $\tau_6$  measured reactor vessel average temperature lag time constant,  $\tau_6 = 2$  sec
- $K_1$  Overtemperature  $\Delta T$  reactor trip setpoint,  $K_1 = 1.14$
- $K_2$  Overtemperature  $\Delta T$  reactor trip setpoint  $T_{avg}$  coefficient,  $K_2 = 0.028/^\circ F$
- $K_3$  Overtemperature  $\Delta T$  reactor trip setpoint pressure coefficient,  $K_3 = 0.00143/\text{psi}$
- $T'$  Nominal full power  $T_{avg}$ ,  $T' \leq 592.0$   $^\circ F$
- $P'$  Nominal RCS pressure,  $P' = 2235$  psig

$f_1(\Delta I)$  is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

- (1) For  $q_t - q_b$  between  $-70\%$  and  $+8\%$ ,  $f_1(\Delta I) = 0$ , where  $q_t$  and  $q_b$  are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and  $q_t + q_b$  is total THERMAL POWER in percent of RATED THERMAL POWER;
- (2) For each percent that the magnitude of  $q_t - q_b$  exceeds  $-70\%$ , the  $\Delta T$  Trip Setpoint shall be automatically reduced by  $0.0\%$  of its value at RATED THERMAL POWER; and
- (3) For each percent that the magnitude of  $q_t - q_b$  exceeds  $+8\%$ , the  $\Delta T$  Trip Setpoint shall be automatically reduced by  $2.65\%$  of its value at RATED THERMAL POWER. (Reference 3.6 and Section 4.4.1.2 of Reference 3.7)

### Over-power $\Delta T$ Setpoint Parameter Values

- $\tau_1$  measured reactor vessel  $\Delta T$  lead/lag time constant,  $\tau_1 = 8$  sec
- $\tau_2$  measured reactor vessel  $\Delta T$  lead/lag time constant,  $\tau_2 = 3$  sec
- $\tau_3$  measured reactor vessel  $\Delta T$  lag time constant,  $\tau_3 = 2$  sec
- $\tau_6$  measured reactor vessel average temperature lag time constant,  $\tau_6 = 2$  sec
- $\tau_7$  Time constant utilized in the rate-lag compensator for  $T_{avg}$ ,  $\tau_7 = 10$  sec
- $K_4$  Overpower  $\Delta T$  reactor trip setpoint,  $K_4 = 1.08$
- $K_5$  Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  rate/lag coefficient,  $K_5 = 0.02/^\circ F$  for increasing average temperature, and  $K_5 = 0$  for decreasing average temperature
- $K_6$  Overpower  $\Delta T$  reactor trip setpoint  $T_{avg}$  heatup coefficient  $K_6 = 0.002/^\circ F$  for  $T > T''$ , and  $K_6 = 0$  for  $T \leq T''$
- $T''$  Indicated full power  $T_{avg}$ ,  $T'' \leq 592.0$   $^\circ F$
- $f_2(\Delta I) = 0$  for all  $(\Delta I)$

**2.3 SHUTDOWN MARGIN (Specification 3.1.1.1):**

The SHUTDOWN MARGIN shall be:

- 2.3.1 Greater than 1.3%  $\Delta\rho$  for MODES 1 and 2\*  
\*See Special Test Exception 3.10.1
- 2.3.2 Greater than the limits in Figure 2 for MODES 3 and 4.
- 2.3.3 Greater than the limits in Figure 3 for MODE 5.

**2.4 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):**

- 2.4.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 4.
- 2.4.2 The EOL, ARO, HFP, MTC shall be less negative than  $-62.6$  pcm/°F.
- 2.4.3 The 300 ppm, ARO, HFP, MTC shall be less negative than  $-53.6$  pcm/°F (300 ppm Surveillance Limit).

Where: BOL stands for Beginning-of-Cycle Life,  
EOL stands for End-of-Cycle Life,  
ARO stands for All Rods Out,  
HFP stands for Hot Full Power (100% RATED THERMAL POWER),  
HFP vessel average temperature is 592 °F.

- 2.4.4 The Revised Predicted near-EOL 300 ppm MTC shall be calculated using the algorithm from the document referenced by Technical Specification 6.9.1.6.b.10:

$$\text{Revised Predicted MTC} = \text{Predicted MTC} + \text{AFD Correction} - 3 \text{ pcm/°F}$$

If the Revised Predicted MTC is less negative than the COLR Section 2.4.3 limit and all of the benchmark data contained in the surveillance procedure are met, then an MTC measurement in accordance with S.R. 4.1.1.3b is not required.

**2.5 ROD INSERTION LIMITS (Specification 3.1.3.5 and 3.1.3.6):**

- 2.5.1 All banks shall have the same Full Out Position (FOP) of either 254 or 259 steps withdrawn.
- 2.5.2 The Control Banks shall be limited in physical insertion as specified in Figure 5.
- 2.5.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

**2.6 AXIAL FLUX DIFFERENCE (Specification 3.2.1):**

- 2.6.1 AFD limits as required by Technical Specification 3.2.1 are determined by Constant Axial Offset Control (CAOC) Operations with an AFD target band of +5, -10%.
- 2.6.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 6, as required by Technical Specifications.

**2.7 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):**

- 2.7.1  $F_Q^{RTP} = 2.55$ .
- 2.7.2  $K(Z)$  is provided in Figure 7.
- 2.7.3 The  $F_{xy}$  limits for RATED THERMAL POWER ( $F_{xy}^{RTP}$ ) within specific core planes shall be:
  - 2.7.3.1 Less than or equal to 2.102 for all cycle burnups for all core planes containing Bank "D" control rods, and
  - 2.7.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.
  - 2.7.3.3  $PF_{xy} = 0.2$ .

These  $F_{xy}$  limits were used to confirm that the heat flux hot channel factor  $F_Q(Z)$  will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these  $F_{xy}$  limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

- 2.7.4 Core Power Distribution Measurement Uncertainty for the Heat Flux Hot Channel Factor
  - 2.7.4.1 If the Power Distribution Monitoring System(PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty ( $U_{FQ}$ ) to be applied to the  $F_Q(Z)$  and  $F_{xy}(Z)$  using the PDMS shall be calculated by:

$$U_{FQ} = (1.0 + (U_Q/100)) * U_E$$

Where:

$U_Q$  = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced by Technical Specification 6.9.1.6.b.11

$U_E$  = Engineering uncertainty factor of 1.03.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System (PDMS).

- 2.7.4.2 If the moveable detector system is used, the core power distribution measurement uncertainty ( $U_{FQ}$ ) to be applied to the  $F_Q(Z)$  and  $F_{xy}(Z)$  shall be calculated by:

$$U_{FQ} = U_{QU} * U_E$$

Where:

$U_{QU}$  = Base  $F_Q$  measurement uncertainty of 1.05.

$U_E$  = Engineering uncertainty factor of 1.03.

## 2.8 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.8.1  $F_{\Delta H}^{RTP} = 1.62$

2.8.2  $PF_{\Delta H} = 0.3$

- 2.8.3 Core Power Distribution Measurement Uncertainty for the Enthalpy Rise Hot Channel Factor

- 2.8.3.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual Section 3.3.3.12, the core power distribution measurement uncertainty ( $U_{F\Delta H}$ ) to be applied to the  $F_{\Delta H}^N$  using the PDMS shall be the greater of:

$$U_{F\Delta H} = 1.04$$

**OR**

$$U_{F\Delta H} = 1.0 + (U_{\Delta H}/100)$$

Where:

$U_{\Delta H}$  = Uncertainty for power peaking factor as defined in Equation 5-19 from the document referenced in Technical Specification 6.9.1.6.b.11.

This uncertainty is calculated and applied automatically by the Power Distribution Monitoring System.

- 2.8.3.2 If the moveable detector system is used, the core power distribution measurement uncertainty ( $U_{F\Delta H}$ ) shall be:

$$U_{F\Delta H} = 1.04$$



## 2.9 DNB PARAMETERS (Specification 3.2.5):

- 2.9.1 The following DNB-related parameters shall be maintained within the following limits:<sup>1</sup>
- 2.9.1.1 Reactor Coolant System  $T_{avg} \leq 595 \text{ }^\circ\text{F}$ <sup>2</sup>,
  - 2.9.1.2 Pressurizer Pressure  $> 2200 \text{ psig}$ <sup>3</sup>,
  - 2.9.1.3 Minimum Measured Reactor Coolant System Flow  $> 403,000 \text{ gpm}$ <sup>4</sup>.

## 3.0 REFERENCES

- 3.1 Letter from J. M. Ralston (Westinghouse) to D. F. Hoppes (STPNOC), "South Texas Project Electric Generating Station Unit 1 Cycle 19 Final Reload Evaluation" NF-TG-14-21 (ST-UB-NOC-14003394 dated February 20, 2014.
- 3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.
- 3.3 STPNOC Calculation ZC-7035, Rev. 2, "Loop Uncertainty Calculation for RCS Tavg Instrumentation," Section 10.1.
- 3.4 STPNOC Calculation ZC-7032, Rev. 5, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," Section 2.3, Page 9.
- 3.5 5Z529ZB01025 Rev. 4, Design Basis Document, Technical Specifications /LCO, Tech Spec Section 3.2.5.c.
- 3.6 Letter from J. M. Ralston (Westinghouse) to D. F. Hoppes (STPNOC), "South Texas Project Electric Generating Station Units 1 and 2 Documentation of the  $f_1(\Delta I)$  Function in OTAT Setpoint Calculation," NF-TG-11-93 (ST-UB-NOC-11003215) dated November 10, 2011.
- 3.7 Document RSE-U1, Rev. 2, "Unit 1 Cycle 19 Reload Safety Evaluation and Core Operating Limits Report." (CR Action 13-531-9)

<sup>1</sup> A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

<sup>2</sup> Includes a 1.9 °F measurement uncertainty per Reference 3.3, Page 37.

<sup>3</sup> Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Per Technical Specification 3.2.5 Bases, this includes a 10.7 psi measurement uncertainty as read on the QDPS display, which is bounded by the 9.6 psi averaged measurement calculated in Reference 3.4.

<sup>4</sup> Includes the most limiting flow measurement uncertainty of 2.8% from Reference 3.5.

Figure 1  
Reactor Core Safety Limits - Four Loops in Operation

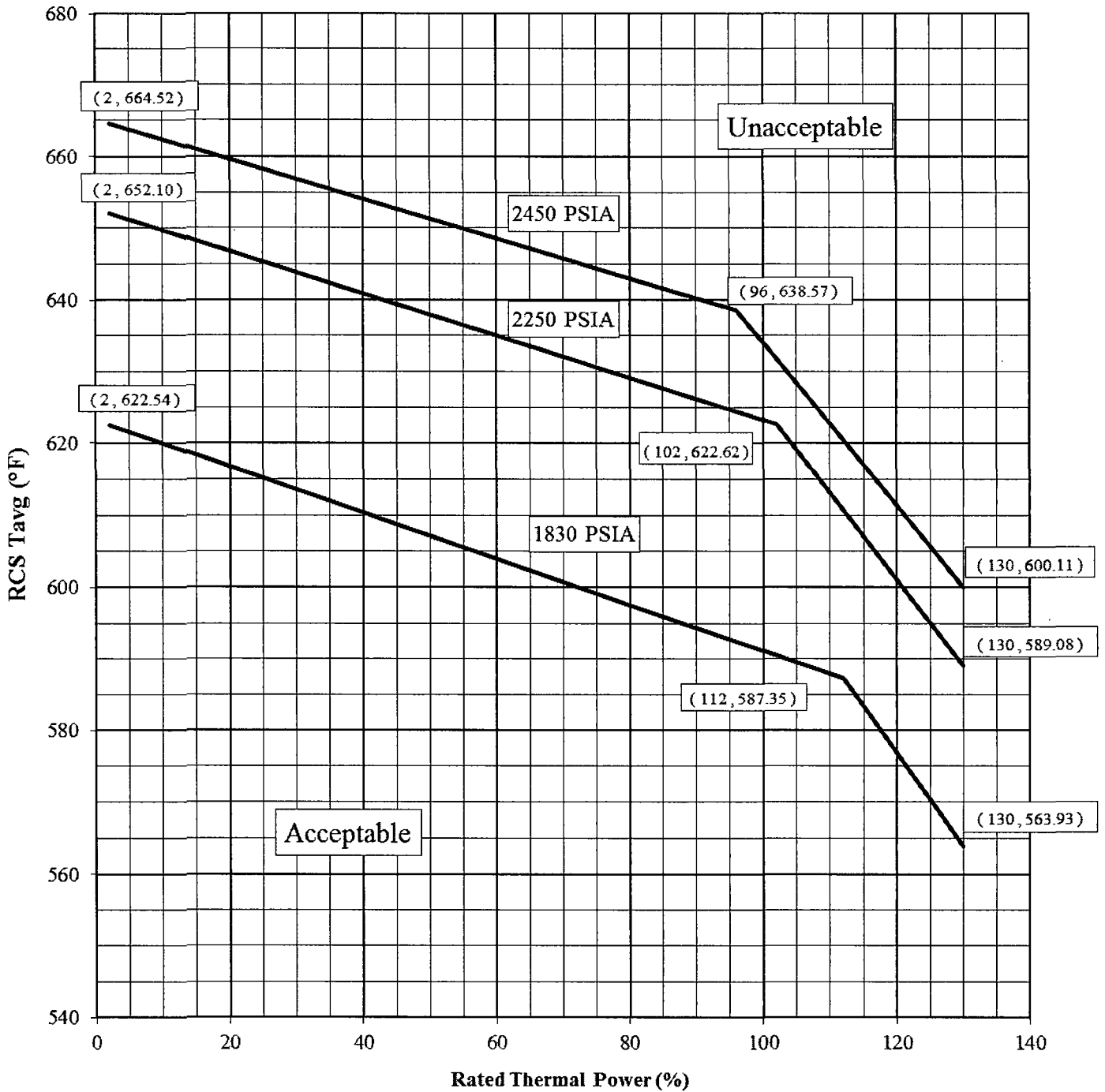


Figure 2

Required Shutdown Margin for Modes 3 & 4

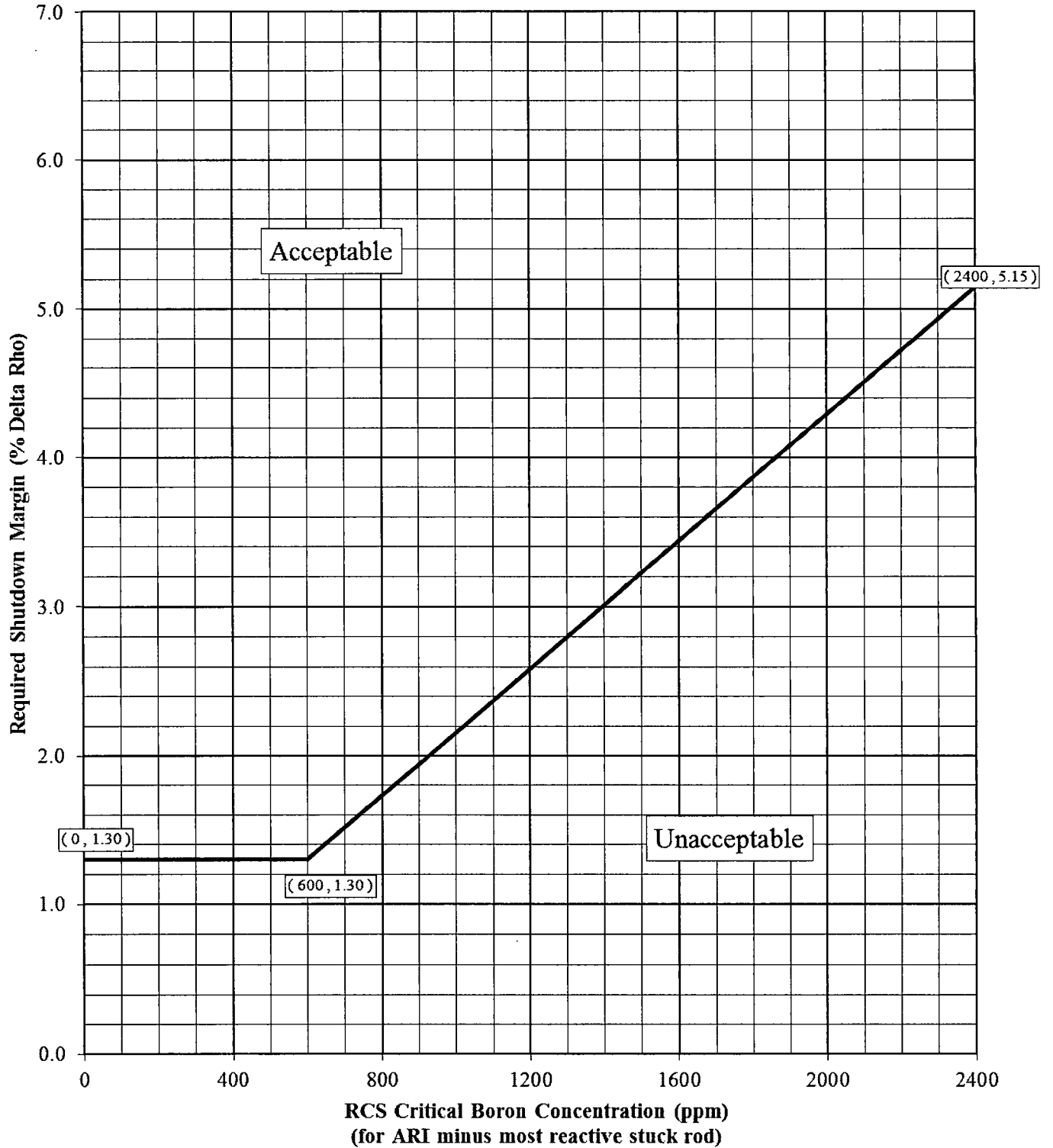


Figure 3

Required Shutdown Margin for Mode 5

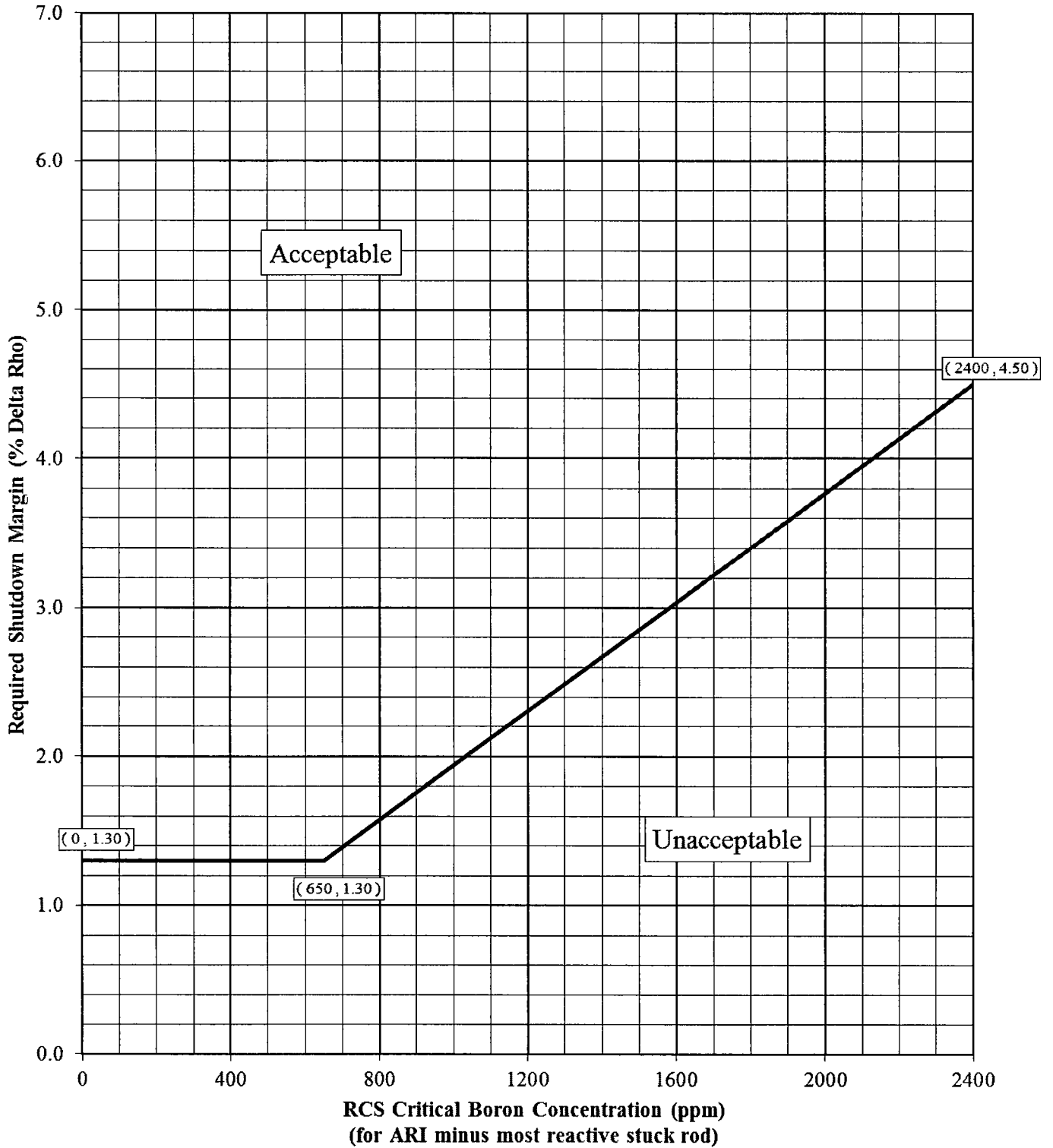


Figure 4

MTC versus Power Level

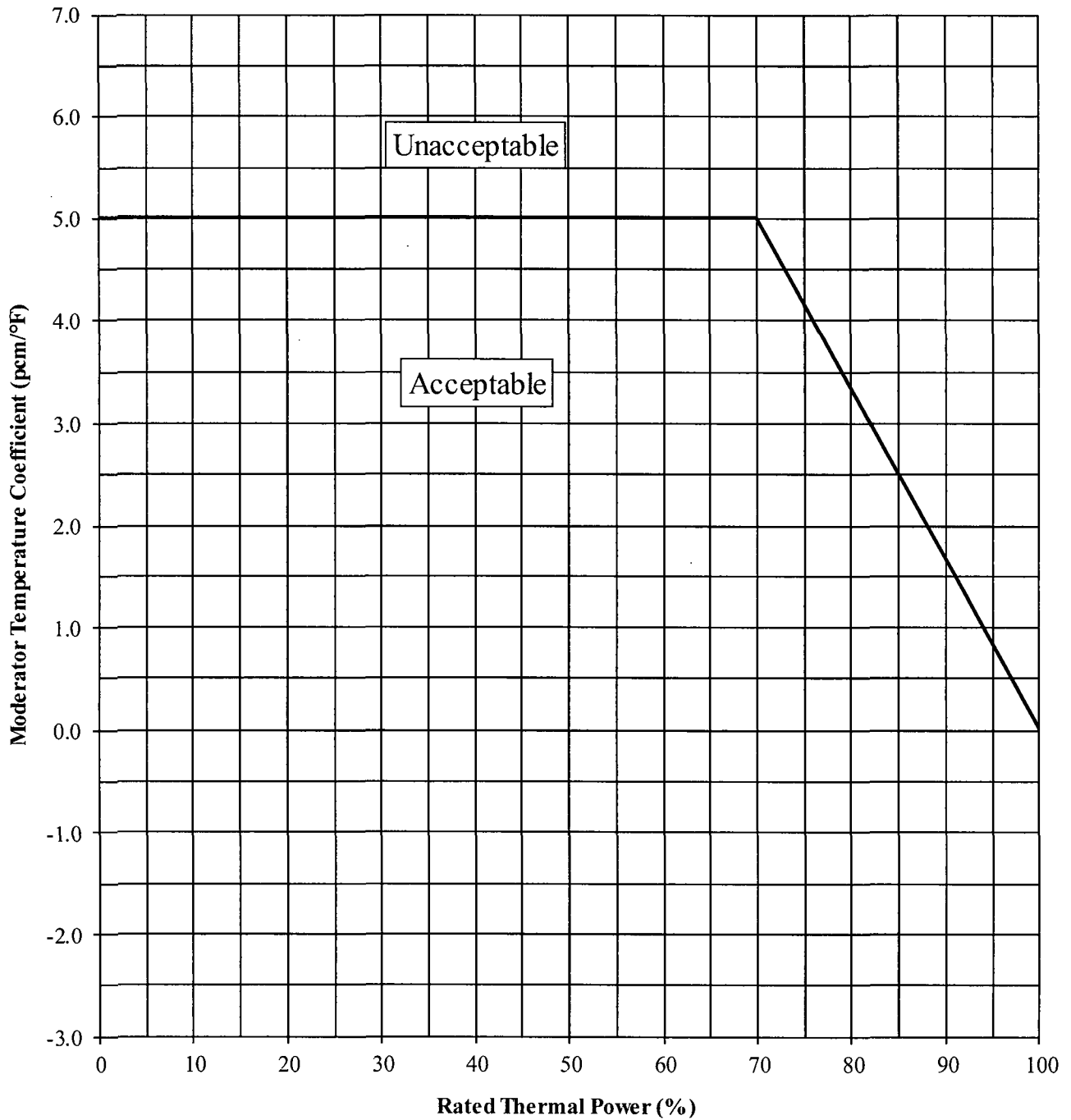


Figure 5

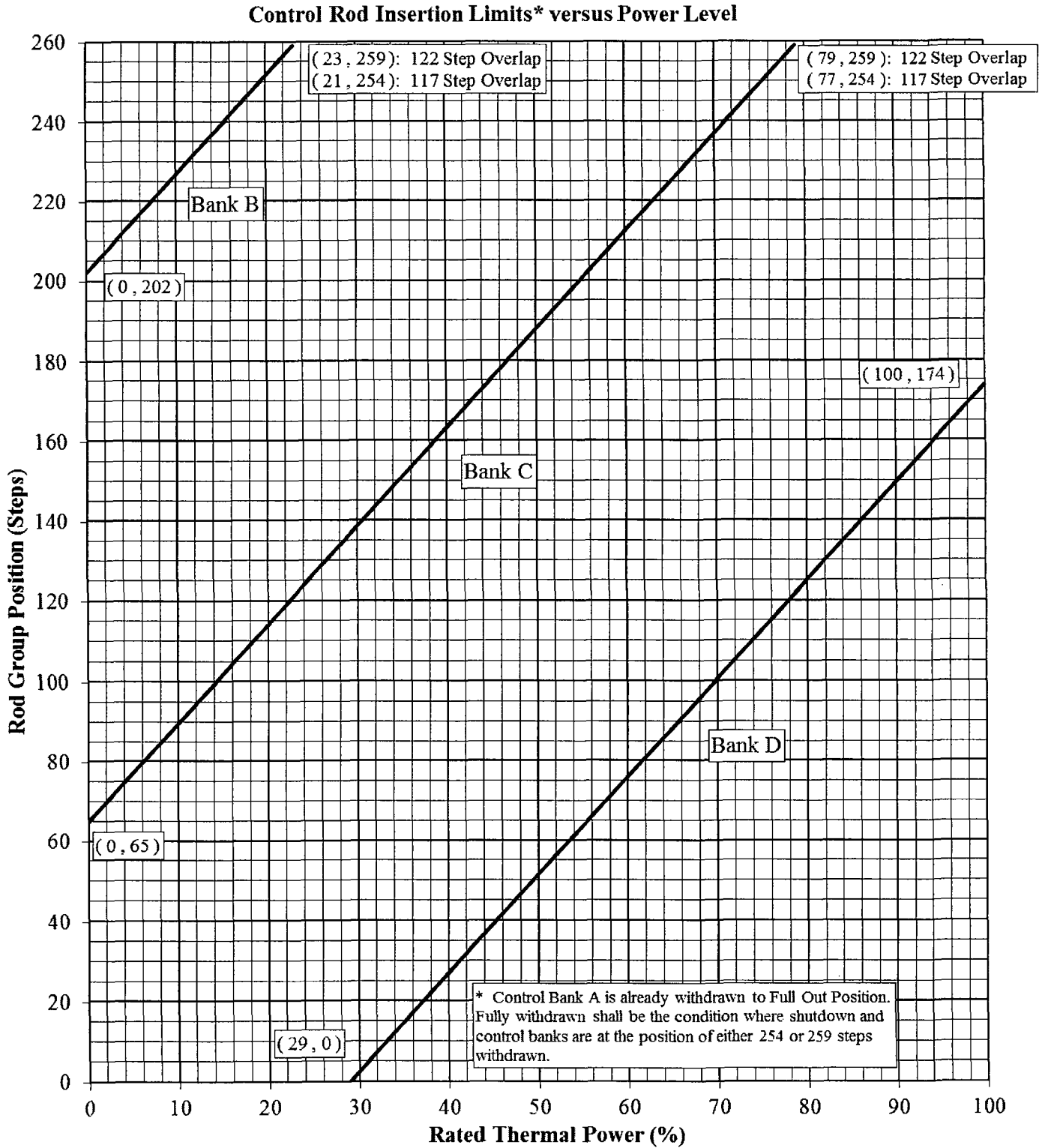


Figure 6

AFD Limits versus Power Level

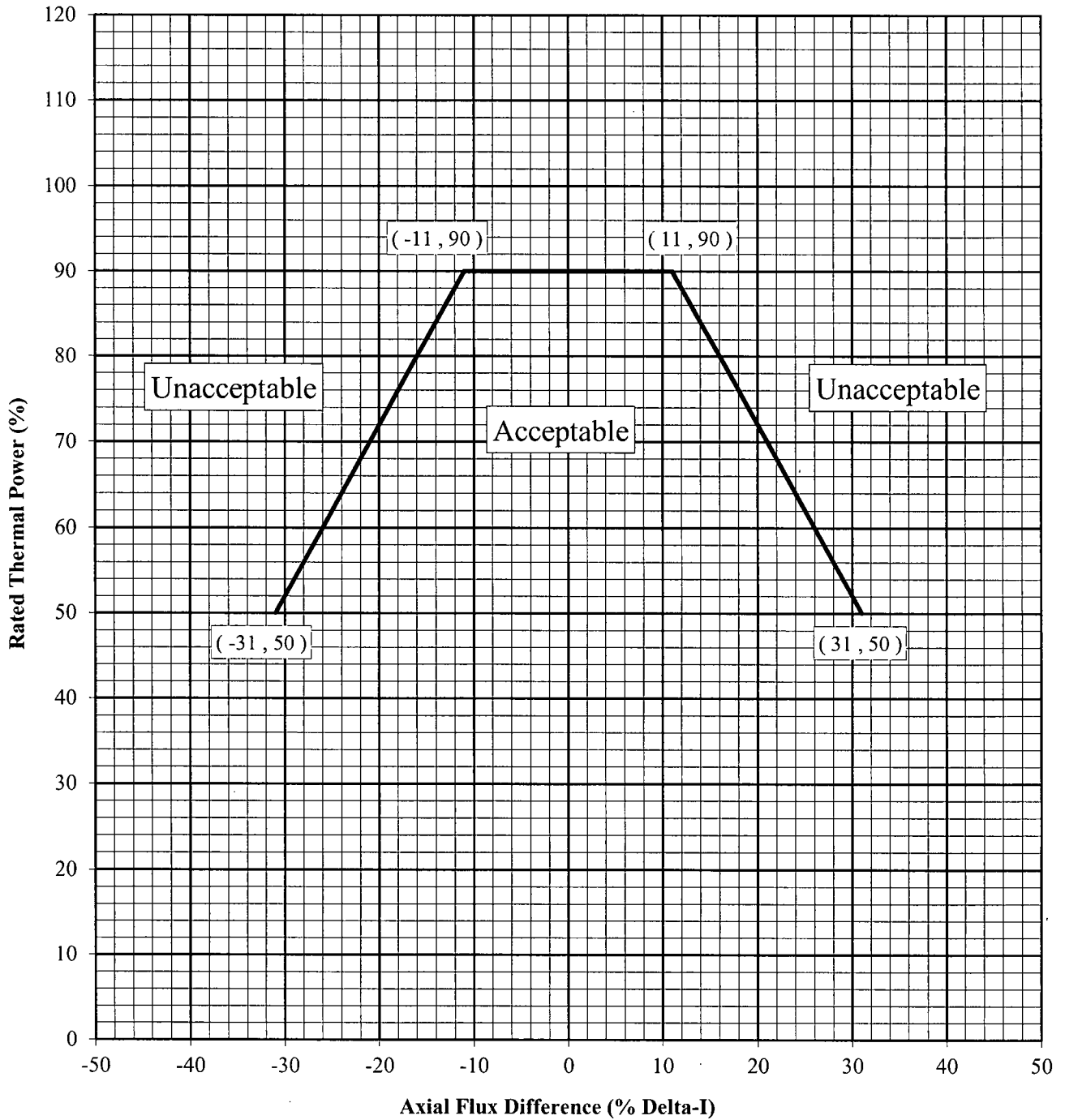
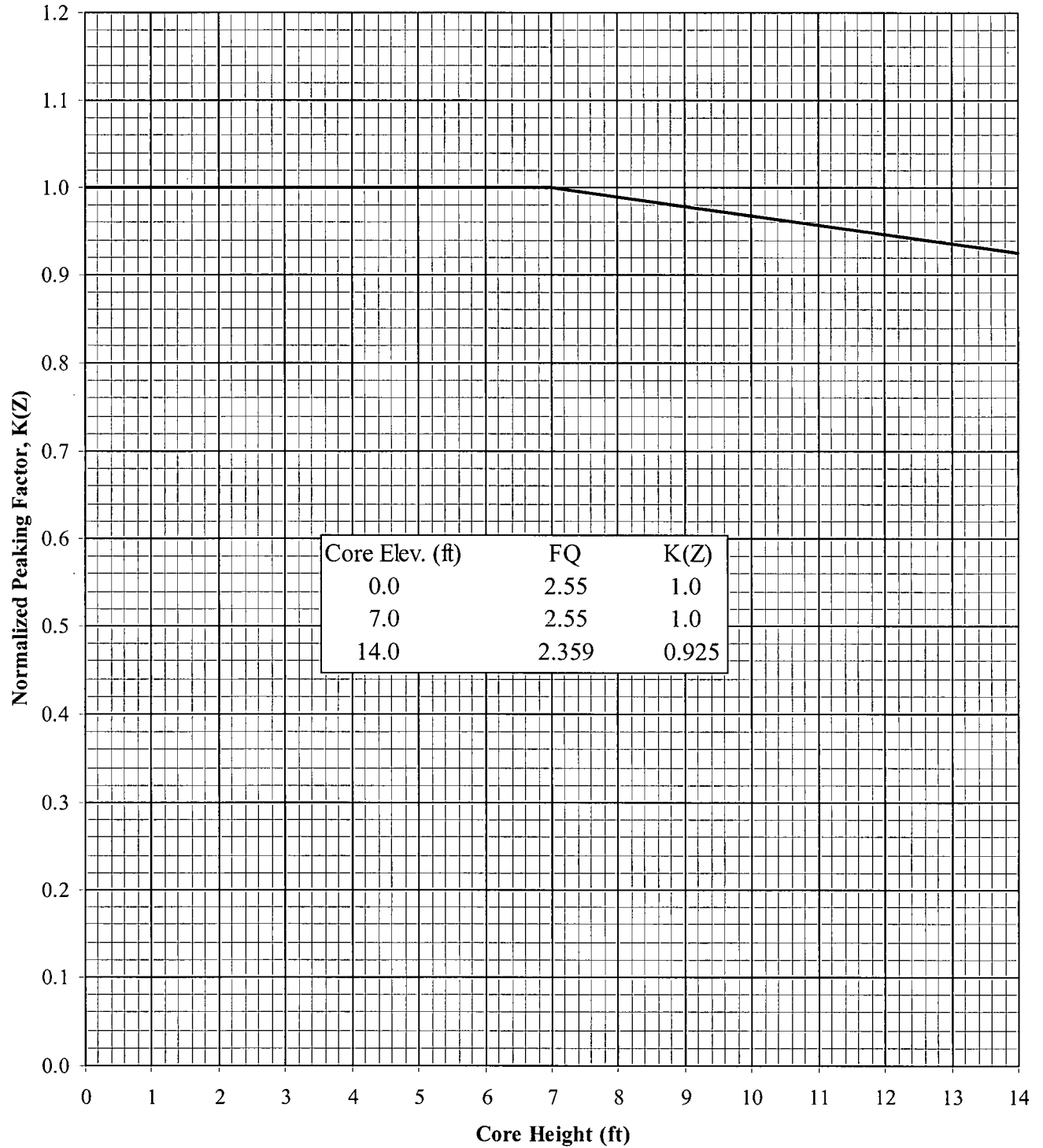


Figure 7

K(Z) - Normalized FQ(Z) versus Core Height





**Table 1 (Part 1 of 2)  
Unrodded  $F_{xy}$  for Each Core Height  
for Cycle Burnups Less Than 10000 MWD/MTU**

Core Height (Ft.)	Axial Point	Unrodded $F_{xy}$	Core Height (Ft.)	Axial Point	Unrodded $F_{xy}$
14.0	1	7.641	6.8	37	1.870
13.8	2	5.953	6.6	38	1.919
13.6	3	4.255	6.4	39	1.901
13.4	4	2.796	6.2	40	1.855
13.2	5	2.535	6.0	41	1.842
13.0	6	2.331	5.8	42	1.855
12.8	7	2.208	5.6	43	1.859
12.6	8	2.123	5.4	44	1.862
12.4	9	2.056	5.2	45	1.906
12.2	10	2.004	5.0	46	1.968
12.0	11	1.971	4.8	47	1.991
11.8	12	1.974	4.6	48	1.951
11.6	13	2.003	4.4	49	1.920
11.4	14	2.005	4.2	50	1.930
11.2	15	1.973	4.0	51	1.934
11.0	16	1.941	3.8	52	1.930
10.8	17	1.920	3.6	53	1.945
10.6	18	1.900	3.4	54	1.988
10.4	19	1.888	3.2	55	2.015
10.2	20	1.902	3.0	56	1.975
10.0	21	1.938	2.8	57	1.932
9.8	22	1.957	2.6	58	1.935
9.6	23	1.930	2.4	59	1.935
9.4	24	1.905	2.2	60	1.909
9.2	25	1.909	2.0	61	1.894
9.0	26	1.913	1.8	62	1.919
8.8	27	1.912	1.6	63	1.924
8.6	28	1.929	1.4	64	1.853
8.4	29	1.990	1.2	65	1.797
8.2	30	2.051	1.0	66	1.834
8.0	31	2.004	0.8	67	2.146
7.8	32	1.938	0.6	68	2.873
7.6	33	1.912	0.4	69	4.096
7.4	34	1.888	0.2	70	5.826
7.2	35	1.856	0.0	71	8.716
7.0	36	1.833			

**Table 1 (Part 2 of 2)  
Unrodded Fxy for Each Core Height  
for Cycle Burnups Greater Than or Equal to 10000 MWD/MTU**

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	6.466	6.80	37	2.203
13.80	2	5.154	6.60	38	2.241
13.60	3	3.840	6.40	39	2.218
13.40	4	2.707	6.20	40	2.166
13.20	5	2.517	6.00	41	2.132
13.00	6	2.322	5.80	42	2.119
12.80	7	2.165	5.60	43	2.102
12.60	8	2.080	5.40	44	2.086
12.40	9	2.036	5.20	45	2.103
12.20	10	2.012	5.00	46	2.139
12.00	11	2.008	4.80	47	2.138
11.80	12	2.021	4.60	48	2.085
11.60	13	2.053	4.40	49	2.040
11.40	14	2.058	4.20	50	2.032
11.20	15	2.040	4.00	51	2.016
11.00	16	2.030	3.80	52	1.998
10.80	17	2.033	3.60	53	1.998
10.60	18	2.033	3.40	54	2.032
10.40	19	2.036	3.20	55	2.056
10.20	20	2.063	3.00	56	2.002
10.00	21	2.109	2.80	57	1.950
9.80	22	2.137	2.60	58	1.930
9.60	23	2.119	2.40	59	1.904
9.40	24	2.100	2.20	60	1.884
9.20	25	2.106	2.00	61	1.894
9.00	26	2.110	1.80	62	1.937
8.80	27	2.112	1.60	63	1.967
8.60	28	2.124	1.40	64	1.947
8.40	29	2.163	1.20	65	1.961
8.20	30	2.203	1.00	66	2.070
8.00	31	2.179	0.80	67	2.439
7.80	32	2.151	0.60	68	3.175
7.60	33	2.150	0.40	69	4.298
7.40	34	2.155	0.20	70	5.843
7.20	35	2.160	0.00	71	8.575
7.00	36	2.168			