

#### **USNRC REGULATORY GUIDES**

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## A. INTRODUCTION

Section 20.106, "Radioactivity in Effluents to Unrestricted Areas," of the Nuclear Regulatory Commission's regulations in **10** CFR Part 20, "Standards for Protection Against Radiation," establishes limits on concentrations of radioactive material in effluents to unrestricted areas. Paragraph (c) of 5 20.1, "Purpose," of 10 CFR Part 20 states that licensees should, in addition to complying with the limits set forth in that part, make every reasonable effort to maintain releases of radioactive materials in effluents to unrestricted areas as far below the limits specified as is reasonably achievable.

Sections 50.34a, "Design Objectives for Equipment to Control Releases of Radioactive Material in Effluents -- Nuclear Power Reactors," and 50.36a, "Technical Specifications on Effluents from Nuclear Power Reactors," of **10** CFR Part 50, "Licensing of Production and Utilization Facilities," set forth design objectives and technical specifications to control releases of radioactive effluents from light-water-cooled nuclear power reactors. Section 50.36a of 10 CFR Fart 50 further provides that, in order to keep power reactor effluent releases as low as is reasonably achievable, each operating license will include technical specifications that (a) require compliance with the provisions of **§** 20.106 dealing with effluent discharge limits, (b) require that operating procedures for the control of effluents be established and followed and that eqi ipment installed in the radioactive waste system be maintained and used, and (c) establish re(  $\therefore$ -ements for reporting measured releases of radionuclides to the environment.

Appendix I, "Numerical Guides for Design Objectives and Limiting Conditions for Operation to Meet the Criterion 'As Low As Is Reasonably Achievable' for Radioactive Material in Light-Water-Cooled Nuclear Power Reactor Effluents," to **10** CFR Part 50 provides numerical guidance for radioactive effluent design objectives and technical specification requirements for limiting conditions of operation for light-water-cooled nuclear power plants.

To implement Appendix I, the NRC staff has developed a series of guides that provide methods acceptable to the staff for the calculation of preoperational estimates of effluent releases, dispersion of the effluent in the atmosphere and different water bodies, and estimation of the associated radiation doses\* to man. This guide describes basic features of these calculational models and suggests parameters for the estimation of radiation doses to man from effluent releases. The methods used herein are general approaches that the NRC staff has developed for application in lieu of specific parameters for individual sites. The use of site-specific values by the applicant is encouraged. However, the assumptions and methods used to obtain these parameters should be fully described and dncumented.

The procedures and models provided in this guide will be subject to continuing review by the-staff with the aim of providing greater flexibility to the applicant in meeting the requirements of Appendix I. As a result of such reviews, it is expected that alternative acceptable methods for calculation will be made available to applicants and that calculational procedures found to be unnecessary will be eliminated.

This guide supersedes portions of Regulatory Guide 1.42, Revision **1,** "Interim Licensing Policy on as Low as Practicable for Gaseous Radioiodine Releases from Light-Water-Cooled Nuclear Power Reactors," which is being withdrawn.

### B. DISCUSSION

Appendix I to **10** CFR Part **SO** provides guidance on the levels of exposure of the general public resulting from effluent releases that may be considered to be as low as is reasonably achievable. This guide describes basic features of the calculational models and assumptions in use by the NRC staff for the estimation of doses. These estimates can be used to implement Appendix I in lieu of site-specific phenomena actually affecting the estimation of radiation exposure.

In this guide, the term "dose," when applied to individuals, is used instead of the more precise term "dose equivalent," as defined by the International Commission on Radiological Units and Measurements (ICRU).

Appendix A of this guide describes suggested methods for calculating the estimated doses to man from discharges to the hydrosphere. Appendix B of this guide describes suggested models and assumptions for calculating submersion doses from radionuclides discharged to the atmosphere and Appendix C gives equations for estimating doses from radioiodines and other radionuclides released to the atmosphere. Appendix **D** describes the models and assumptions for calculating population dose (man-rem and man-thyroid-rem) from radionuclide releases to the atmosphere and hydrosphere.

The models and assumptions described in Appendices **A,** B, C, and D of this guide are acceptable to the NRC staff for calculating doses to individuals and populations. If other models are selected, they should include the same exposure pathways and physical mechanisms as are used in the models described in this guide.

As discussed in Section III.A.2 of Appendix I to **10** CFR Part 50, the applicant may take into account any real phenomena or actual exposure conditions that affect or modify the estimate of radiation exposure. Such conditions should include actual values for agricultural productivity, residence times, dose attenuation by structures, measured environmental transport factors (suchas bioaccumulation factors), or similar values actually determined at a specific site. The applicant should provide e pugh information on the measurements or other methods used to derive these substitute values to enable the NRC staff to evaluate their validity.

## C. REGULATORY POSITION

## 1. Radiation Doses from Liquid Effluent Pathways

The NRC staff will calculate radiation doses from potable water, aquatic food, shoreline deposits, and irrigated food pathways by using the following equations from Appendix A of this guide.

a. Potable Water

$$
R_{apj} = 1100 \frac{M_{p}U_{ap}}{F} \frac{n}{i} Q_{i}^{i} D_{aipj} exp(-\lambda_{i} t_{p})
$$
 (1)

b. Aquatic Foods

$$
R_{apj} = 1100 \frac{U_{ap}M_p}{F} \int_{i}^{n} Q_i^{\dagger}B_{ip}D_{aipj}exp(-\lambda_i t_p)
$$
 (2)

**I**

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c. Shoreline Deposits

$$
R_{\text{apj}} = 110,000 \frac{U_{\text{ap}} M_{\text{p}} W_{\text{p}}}{F} \hat{q}_{i}^{\dagger} T_{i} D_{\text{aipj}} \text{[exp(-\lambda_{i} t_{\text{p}})]} [1 - \exp(-\lambda_{i} t)] \tag{3}
$$

d. Irrigated Foods

For all radionuclides except tritium:

$$
R_{apj} = U_{ap}^{veg} \left[ d_i \exp(-\lambda_i t_h) D_{aipj} \left[ \frac{r[1 - \exp(-\lambda_{\xi i} t_e)]}{\gamma_v \lambda_{\xi i}} + \frac{B_{i\psi}[1 - \exp(-\lambda_i t_b)]}{\gamma_{\psi}} \right] + U_{ap}^{\text{animal}} \left[ S_{iA} D_{aipj} \left\{ Q_f d_i \exp(-\lambda_i t_h) \left[ \frac{r[1 - \exp(-\lambda_{\xi i} t_e)]}{\gamma_v \lambda_{\xi i}} \right] + \frac{B_{i\psi}[1 - \exp(-\lambda_i t_b)]}{\gamma_{\psi}} \right] + C_{iAw} Q_{Aw} \right\}
$$
(4)

For tritium:

$$
R_{\text{apj}} = U_{\text{ap}}^{\text{veg}} C_{\text{v}} D_{\text{apj}} + U_{\text{ap}}^{\text{animal}} D_{\text{apj}} \frac{kC_{\text{w}}}{\lambda_{m}} (w + Q_{\text{Aw}})
$$
 (5)

where

- B<sub>ip</sub> is the equilibrium bioaccumulation factor for nuclide i in pathway p, expressed as the ratio of the concentration in biota (in pCi/kg) to the radionuclide concentration in water (in pCi/lizer), in liters/kg;
- $B_{41}$  is the concentration factor for uptake of radionuclide i from soil by edible parts of crops, in pCi/kg (wet weight) per pCi/kg dry soil;
- $C_{i A w}$  is the concentration of radionuclide i in water consumed by animals, assumed to be equal to  $C_{i\omega}$  (pCi/liter);
- 
- $C_{4,1}$  is the radionuclide concentration in water, in pCi/liter;
- 

D<sub>aipi</sub> is the dose factor, specific to a given radionuclide i, pathway p, organ j, and individual's age a, which can be used to calculate the radiation dose from an intake of a radionuclide, in mrem/pCi, or from exposure to a given concentration of a radionuclide in water, expressed as a ratio of the dose rate (in mrem/hr) and the radionuclide concentration in water (in pCi/liter);

- $d_i$  is the deposition rate of nuclide i, in pCi/m<sup>2</sup> per hr;
- F is the flow rate of the liquid effluent, in  $ft^3$ /sec;
- k is the reciprocal of the body water volume  $(0.0041)$  liter<sup>-1</sup> for beef cattle and 0.0028 liter<sup>-1</sup> for dairy cattle);
- **Mp** is the mixing ratio (reciprocal of the dilution factor) at the point of exposure (or the point of withdrawal of drinking water or point of harvest of aquatic food) as described in Table **A-1** (in Appendix A of this guide), dimensionless;
- n is the number of radionuclides that are to be considered;
- P  $\,$  is the effective "surface density" for soil, in kg(dry soil)/m $^2.$  Assuming a uniform mixing of all radionuclides in a plow layer of 15 cm (6 in.) depth, P has a value of approximately 240 kg/m<sup>2</sup>;
- Q<sub>Aw</sub> is the consumption rate of contaminated water by an animal, in liters/day;
- Q<sub>F</sub> is the consumption rate of contaminated feed or forage by an animal, in kg/day (net weight);
- $Q<sub>z</sub>$  is the release rate of nuclide i, in Ci/yr;
	- r is the fraction of deposited activity retained on crops (which is 0.25 for sprinkler irrigation, 0.2 for particulates, and **1.0** for airborne deposition of radionuclides), dimensionless;
- R .is the total annual dose to organ j of individuals of age a from all of the nuclides i in pathway p, in mrem/yr; Si is the transfer coefficient for radionuclide i which relates the daily
	- is the transfer coefficient for radionuclide i which relates the daily intake rate by an animal to the concentration in an edible portion of animal product, in pCi/liter (milk) per pCi/day or pCi/kg (animal product) per pCi/day;
	- t is the period of time for which sediment is exposed to the contaminated water, nominally taken to be the mid-point of the operating lifetime of the facility, in hours;
	- $t_k$  is the mid-point of the soil exposure time (15 years for a typical power reactor), in hours;
	- $t_{\text{c}}$  is the time period that crops are exposed to contamination during the growing season, in hours;

t<sub>h</sub> is a holdup time that represents the time interval between harvest and consumption of the food, in hours;

 $T_i$  is the radioactive half life of nuclide i, in days;

t<sub>n</sub> is the average transit time required for nuclides to reach the point of exposure. For internal dose,  $t_p$  is the total time elapsed between release of the nuclides and ingestion of food or water, in hours;

 $U_{\alpha}$  is a usage factor that specifies the exposure time or intake rate for an  $\alpha$ individual of age a associated with pathway p, in hr/yr or kg/yr (as appropriate);

**w** is the water intake rate via fresh forage (28 liters/day for beef cattle and 38 liters/day for dairy cattle);

W is the shoreline width factor, dimensionless;

**Y<sub>v</sub>** is the agricultural productivity (yield), in kg(wet weight)/m<sup>2</sup>;

 $\Lambda_{\rm Fl}$  is the effective removal rate constant for radionuclide i from crops, in hr<sup>-1</sup>, provided that  $\lambda_{E1} = \lambda_1 + \lambda_w$ , where  $\lambda_1$  is the radioactive decay constant, in (hr)-I, and **Aw** is the removal rate constant for physical loss by weathering  $(\lambda_{\mu} = 0.0021 \text{ hr}^{-1})$ , which corresponds to a removal half-life of 14 days);

 $\lambda_i$  is the radioactive decay constant of nuclide i, in hr<sup>-1</sup>;

- A<sub>m</sub> is the water elimination rate constant (0.32/day for beef cattle and 0.28/day for dairy cattle);
- 1100 is the factor to convert from  $(Ci/yr)/(ft^3/sec)$  to pCi/liter; and
- 110,000 is the factor to convert from  $(Gi/yr)/(ft^3/sec)$  to pCi/liter and to account for the proportionality constant used in the sediment radioactivity model.

These equations yield the dose rate to various organs of an individual from the exposure pathways mentioned above. Appendix I of **10** CFR Part 50 requires that the annual doses or dose commitments to the total body or any organ of an individual from the sum of the exposure pathways from liquid effluents associated with each reactor should not exceed 3 mrem and **10** mrem, respectively.

## 2. Gamma and Beta Doses from Gaseous Effluents

The NRC staff will calculate radiation doses from gaseous effluents using the following equations from Appendix B of this guide. The definitions of elevated and ground-level releases are found in Regulatory Guide **1.111,** "Methods for Estimating Atmospheric Transport and Dispersion for Gaseous Effluents on Routine Releases from Light-Water-Cooled Reactors," and Appendix B to this guide.

a. Gamma Air Dose Rates for Elevated Releases

$$
D^{Y}(r, \Theta) = \frac{260}{r(\Delta \Theta)} \sum_{n} \frac{1}{u_{n}} \sum_{s}^{T} f_{ns} \sum_{k} u_{a} (E_{k}) E_{k} I(H, u, s, \sigma_{z}, E_{k}) \sum_{i} Q_{nj}^{D} A_{ki}
$$
 (6)

where

 $A_{k,i}$  is the photon yield for gamma-ray photons in energy group k from the decay of radionuclide i, in photons/disintegration;

 $D^{Y}(r,0)$  is the annual total gamma air dose at a distance r in the sector at angle  $\theta$ . in mrad/yr;

**Ek** is the energy of the kth photon energy group, in MeV/photon;

fns is the fraction of the time that stability class s and wind speed n occur for sector **0,** dimensionless;

 $I(H, u, s, \sigma_n, E_k)$  is the result of the numerical integration accounting for the distribution of radioactivity according to meteorological conditions of wind speed (u) and atmospheric stability (s) which in part determine the effective stack height (H) and the vertical plume standard deviation **(o).** In addition, I is a function of the photon energy  $E_i$  and is  $\overline{I} = \overline{I}_1 + k\overline{I}_2$  as formulated in Slade (see Reference **I** fi: Appendix B of this guide);

$$
Q_{n1}^{'D}
$$
 is the release rate of radionucide i, corrected for decay during transit to the distance r under wind speed  $u_n$ , in Ci/yr;

- r is the distance from the release point to the receptor, in meters;
- u<sub>n</sub> is the mean wind speed of wind speed class n, in m/sec;
- **AO** is the sector width over which atmospheric conditions are averaged, in radians; and

$$
\mu_{a}(\mathbf{E}_{k})
$$

is the air energy absorption coefficient for the kth photon energy group, in  $n^{-1}$ 

b. Gamma Air Dose Rates from Ground-Level Releases; Beta Air Dose Rates from Elevated and Ground-Level Releases

$$
D^{\gamma}(r, \theta)
$$
 or  $D^{\beta}(r, \theta) = 3.17 \times 10^{4} \sum_{i} Q_{i}^{T}[x/Q^{T}]^{D}(r, \theta)(DF_{i}^{T} \text{ or } DF_{i}^{\beta})$  (7)

where

- $DF_i^{\gamma}$ ,  $DF_i^{\beta}$ I' I are the gamma and beta air dose factors for radionuclide  $i$ , in mrad per yr/ pCi per **n <sup>3</sup> ;**
- $D^{\gamma}(r,0)$  or

 $Q_i$ 

 $D^B(r,0)$ are the annual gamma and beta air doses at the distance r in the sector at angle **0** from the discharge point, in mrad/yr;

is the release rate of the radionuclide i, in Ci/yr;

 $[x/Q']^D(r,0)$ is the annual average gaseous dispersion factor (corrected for radioactive decay) at the distance r in the sector at angle  $\circ$  from the release point, in sec/m3 (see Regulatory Guide **1.111,** "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light- Water-Cooled Reactors," for methods to estimate x/Q'); and

 $3.17 \times 10^{4}$ is the number of pCi per Ci divided by the number of seconds per year.

c. Total Body Dose Rates from Elevated Releases

$$
D^{T}(r,\Theta) = 1.11 S_{F} \sum_{k} D_{k}^{Y}(r,\Theta) exp[-\mu_{a}^{T}(E_{k})t]
$$
 (8)

where

 $0^{\mathsf{T}}(r,0)$ 

is the annual total body dose at the distance r in the sector at angle 0 from the discharge point, in mrem/yr;

DY(r,o) **k**

is the annual gamma air dose associated with the kth photon energy group at the distance r in the sector at angle **0** from the discharge point, in mrad/yr;  $S<sub>c</sub>$  is the attenuation factor that accounts for the dose reduction due to shielding provided by residential structures (0.7), dimensionless;

t is the product of tissue density and depth used to determine a "whole-body" exposure. This depth is 5 cm, which is equivalent to  $t = 5$  q/cm<sup>2</sup>: is the tissue energy absorption coefficient, in  $cm^2$ /g; and

 $\cdot$ <sup>T</sup>(E<sub>L</sub>)

**1.11** is the average ratio of tissue to air energy absorption coefficients.

## d. Skin Dose Rate from Elevated Releases

$$
0^{S}(r,0) = 1.11S_{F}0^{Y}(r,0) + 3.17 \times 10^{4} \int_{i}^{r} Q_{i}^{i}[x/Q^{i}]^{D}(r,0)DFS_{i}
$$
 (9)

where

 $DFS<sub>1</sub>$  is the beta skin dose factor for the radionuclide i which includes the attenuation by the outer "dead" layer of the skin, in mrem- $m^3$ /pCi-yr. This attenuation is for 70 micrometers or 7 mg/cm<sup>2</sup>  $\cdot$  f tissue; and

$$
D^{S}(r, \theta)
$$
 is the annual skin dose at the distance r in the sector at angle  $\theta$  from the discharge point, in  $mrem/yr$ .

All other parameters are as defined in preceding sections.

e. Total Body Dose Rates from Ground-Level Releases

$$
D_{\infty}^{T}(r, \Theta) = 1.11 S_{F} \sum_{i} x_{i} (r, \Theta) \text{DFB}_{i}
$$
 (10)

where

DFB<sub>2</sub> is the total body dose factor for the radionuclide i which includes the attenuation of 5  $g/cm^2$  of tissue, in mrem-m<sup>3</sup>/pCi-yr (see Table B-1 in Appendix B of this guide);

- $D_1^T(r,0)$  is the annual total body dose due to immersion in a semi-infinite cloud at the distance r in the sector at angle **0** from the discharge point, in mrem/yr; and
- $x_1(r, \theta)$  is the annual average ground-level concentration of nuclide i at the distance r in the sector at angle  $\Theta$  from the release point, in  $pC_1/m^3$ .

**All** other parameters are as defined above.

f. Skin Dose Rates from Ground-Level Releases

$$
D_{\infty}^{S}(r, \circ) = 1.11 S_{F} \frac{\sum_{i} x_{i}(r, \circ) DF_{i}^{Y} + \sum_{i} x_{i}(r, \circ) DFS_{i}
$$
 (11)

where

D5 (r,O) is the annual skin dose due to immersion in a semi-infinite cloud at the distance r in the sector at angle **0** from the discharge point, in mrem/yr.

**i**

**All** other parameters are as defined above.

3. Doses from Radioiodines and Other Radionuclides Released to the Atmosphere

The NRC staff will calculate radiation doses from radioiodines and other radlonuclides released to the atmosphere using the following equations from Appendix C of this guide.

External Irradiation from Activity Deposited onto the Ground Surface

$$
D_j^G(r, \omega) = 8760 S_F \sum_{i} C_j^G(r, \omega) DFG_{ij}
$$
 (12)

where

 $c_i^G$  is the ground plane concentration of radionuclide i, in  $pCi/m^2$ ;

- DFG<sub>i</sub>; is the open field ground plane dose conversion factor for organ j from radionuclide i, in mrem-m<sup>2</sup>/pCi-hr;
- 
- $D_{\epsilon}^{G}(r,0)$  is the annual dose to the organ j from the ground plane concentration of all radionuclides at location (r,o), in mrem/yr;
	- $S_F$  is a shielding factor that accounts for the dose reduction afforded by the shielding provided by residential structures and by occupancy, dimensionless; and
	- 8760 is the number of hours in a year.
- **Inhalation**

$$
D_{ja}^{A}(r,0) = R_a \sum_{i} x_i(r,0)DFA_{ija}
$$
 (13)

where

$$
r_{ia}^{\prime }(\mathbf{r}%
$$

 $\Omega$ , is the annual dose to organ j of an individual in the age group a at location  $(r, 0)$  due to inhalation of all radionuclides, in mrem/yr;

DFA<sub>ija</sub> is the inhalation dose factor for radionuclide i, organ j, and age group a, in mrem/pCi;

 $R_a$  is the annual air intake for individuals in the age group a, in  $\text{m}^3/\text{yr}$ ; and  $x_1(r,0)$  is the concentration of radionuclide i in air at location (r,o), in pCi/m<sup>3</sup>.

c. Ingestion

$$
D_{ja}^{D}(r,0) = \sum_{i} DFI_{ija} \left[U_{a}^{V}f_{g}C_{i}^{V}(r,0) + U_{a}^{m}C_{i}^{m}(r,0) + U_{a}^{F}C_{i}^{F}(r,0) + U_{a}^{L}f_{c}C_{i}^{L}(r,0)\right]
$$
 (14)

where

 $C_3^V(r,0)$ ,  $C_3^{\text{III}}(r,0)$ ,

- $c_i^L(r,0)$ ,  $c_i^F(r,0)$  are the concentrations of radionuclide i in produce (non-leafy-vegetables, fruits, and grains), milk, leafy vegetables, and meat, respectively, at location (r, o), in pCi/kg. These variables are determined using Equation (C-7) from Appendix C of this guide;
	- $D_{ja}^{0}(r, \omega)$  is the annual dose to the organ j of an individual in age group a from inges-<br>tion of all radionuclides at location  $(r, \omega)$ , in mrem/yr;
		- DFI<sub>1ia</sub> is the ingestion dose factor for radionuclide i, organ j, and age group a,<br>A f f this quide, in mrem/pCi; from Tables A-3 through A-6 of Appendix A of this guide, in mrem/pCi;
			- f<sub>n</sub>f<sub>o</sub> are the respective fractions of the ingestion rates of produce (vegetables fruits, and grains) and leafy vegetables which are produced in the garden of interest (Note:  $f_g$  may be taken to be 0.76 in the absence of site-specific data which would indicate that the quantity of grain produced in the garden of interest would satisfy the intake values in Table A-2 of Appendix A of this guide); and
	- U<sub>2</sub>, U<sub>n</sub>, U<sub>n</sub>, U<sub>n</sub> are the annual intake (usage) of vegetables, milk, meat, and leafy vegetables respectively, for individuals in the age group a, in kg/yr.

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## 4. Inteqrated Doses to the Population

The NRC staff will calculate integrated doses to the local population from all pathways discussed in Sections **C.1,** 2, and 3. Because of the various conditions under which the equations in Appendix D are used, they are not presented in this section. It is recommended that Appendix D be read for a detailed discussion of the staff's models.

## **5.** Summary of Staff Position

A brief summary of the staff position on methods of evaluating compliance with Appendix I is presented in Table 1.

## D. IMPLEMENTATION

The purpose of this section is to provide information to applicants and licensees regarding the NRC staff's plans for utilizing this regulatory guide.

This guide reflects current Nuclear Regulatory Commission practice. Therefore, except in those cases in which the license applicant or licensee proposes an acceptable alternative method, the method described herein for complying with specified portions of the Commission's regulations is being and will continue to be used in the evaluation of submittals for operating license or construction permit applications until the guide is revised as a result of suggestions from the public or additional staff review.

**II**

**I**





## Radioiodines and Particulates<sup>†</sup> Released to the Atmosphere



Evaluated at a location that is anticipated to be occupied during plant lifetime or evaluated with respect to such potential land and water usage and food pathways as could actually exist during the term of plant operation.

Calculated only for noble gases.

Evaluated at a location that could be occupied during the term of plant operation.

 $<sup>†</sup>$ Doses due to carbon-14 and tritium intake from terrestrial food chains are included</sup> in this category.

<sup>tt</sup> Evaluated at a location where an exposure pathway actually exists at time of licensing. However, if the applicant determines design objectives with respect to radioactive iodine on the basis of existing conditions and if potential changes in land and water usage and food pathways could result in exposures in excess of the guideline values given above, the applicant should provide reasonable assurance that a monitoring and surveillance program will be performed to determine: (1) the quantities of radioactive iodine actually released to the atmosphere and deposited relative to those estimated in the determination of design objectives; (2) whether changes in land and water usage and food pathways which would result in individual exposures greater than originally estimated have occurred; and (3) the content of radioactive iodine and foods involved in the changes, if and when they occur.

#### APPENDIX A

### METHODS FOR CALCULATING DOSES TO MAN FROM RADIONUCLIDE DISCHARGES TO THE AQUATIC ENVIRONMENT

The equations for estimating radiation exposure to man from four principal exposure pathways in the aquatic environment (potable water, aquatic foods, shoreline deposits, and irrigated foods) are listed in Section C, "Regulatory Position," of this guide. The equations can be used to calculate the annual doses to various organs of a child, **0** - **<sup>11</sup>**years; a teen, 12 - **<sup>18</sup>**years; and an adult, 18+ years.

#### **1.** Equation for Calculating Radiation Dose via Liquid Pathways

Equation (A-1) is the fundamental equation for calculating the radiation dose to man via liquid effluent pathways.

$$
R_{aipj} = C_{ip}U_{ap}D_{aipj}
$$
 (A-

where

 $c_{in}$  is the concentration of nuclide i in the media of pathway p, in pCi/kg;

- $D_{\alpha}$ ipj is the dose factor which is specific to a given radionuclide i, pathway p, organ j, and individual's age a. It represents the annual dose due to the intake of a radionuslide, in mrem/pCi, or from exposure to a given concentration of a radionuclide in water, in mrem per hr/pCi per liter;
- Raipj is the annual dose to organ j of an individual of age a from nuclide i via apip pathway p, in mrem/yr; and

U<sub>ap</sub> is the exposure time or intake rate (usage) associated with pathway p for .ge group a, in hr/yi or kg/yr (as appropriate).

The three factors making up Equation (A-1) are discussed in the following sections, most of which were taken directly from the WASA-1258 report (Ref. **1).** (An updated version of the portion of the WASH-1258 report describing models and computer programs is contained in the BNWL-1754 report (Ref. 2).)

## a. Concentration in Environmental Media (C<sub>in</sub>)

The points at which concentrations in environmental media of interest should be evaluated are shown in Table A-1. The concentrations can be estimated from the mixing ratio M<sub>n</sub>, the bioaccumulation factor B<sub>ip</sub>, the radionuclide release rate Q<sub>i</sub>, and other terms presented in the pathway equations that appear later in this discussion.

b. Usage (U<sub>ap)</sub>

The second term of Equation (A-1) is the usage term U<sub>nn</sub>. Usage is expressed as a consumption rate in kg/yr or liters/yr or as an exposure time in hr/yr, as appropriate for the pathway p and age group a under consideration.

The NRC staff encourages the use of site-specific data, whenever possible, for parameters such as those included in Table A-2. Such data should be documented. In the absence of site-specific data, however, the usage values (consumption rates and exposure times) presented in Table A-2 are recommended.\*

In selecting usage values, not only the present land and water uses should be considered, but also changes in land and water uses made possible by such activities as chemical pollution abatement. Radioactive material released into waterways may include long-lived radionuclides that have potential for accumulation in sediments and biota and may persist for many years - perhaps beyond the lifetime of the nuclear power station.

## TABLE A-I

# DEFINITION OF POINTS AT WHICH CONCENTRATIONS IN ENVIRONMENTAL MEDIA (C<sub>ip</sub>)<br>SHOULD BE CALCULATED



Point where effluent has undergone prompt dilution near the surface (about 5:1 for large receiving water bodies).

Point where effluent has undergone prompt dilution (about **10:1** in deep water and about **5:1** in shallow water).

\_\_\_\_

Fresh water sites only. over the plant lifetime, The "nearest anticipated downstream supply" is that location which, based on land use projections ing the closest point to the site where a drinking water supply exists or could exist.

AFresh water sites only. use projections over the or could exist. The "nearest anticipated point of withdrawal for irrigation" is that location which, based on land plant lifetime, is the closest point to the site where withdrawal for irrigation purposes exists

**Coo-18** 



TABLE A-2

aConsumption rate obtained from Reference 3 for average individual and age-prorated and maximized using techniques contained in Reference 4.

bconsists of the following (on a mass basis): 22% fruit, 54% vegetables (including leafy vegetables), and 24% grain.

 $c_{0n}$  additional category of maximum individual (1-yr old) should be added for these pathways. Consumption rates are the same as the child's.

 $d_{\text{Concentration}}$  rate for adult obtained by averaging data from References  $4, 6, 9$  and age-propating using techniques contained in Reference 4.

eData obtained directly from Reference 4.

fData obtained directly from Reference 15.

<sup>9</sup>Inhalation rate for infant obtained by averaging data from References 10-14.

c. Dose Factor (D<sub>aipi</sub>)

Equations for calculating internal dose factors are derived from those given by the International Commission on Radiological Protection (ICRP-Ref. 15) for body burden and maximum permissible concentration (MPC). Effective absorbed energies for the radionuclides are calculated from the ICRP model. Appendix D of Reference 16 was used as a basic source of age-dependent dose factors for ingestion. Where data are lacking, metabolic parameters for the Standard Man $^\circ$ were used for other ages as well.

The dose factors for external exposure were based on the assumption that the contaminated medium is large enough to be considered an "infinite volume" relative to the range of the emitted radiations. Under this assumption, the energy emitted per gram of medium is equivalent to the energy absorbed per gram of medium corrected for the differences in energy absorption between air or water and tissue and for the physical geometry of each specific exposure situation.

Material deposited from sedimentation in an aquatic system or from irrigation water onto the ground represents a fairly large, nearly uniform thin sheet of contamination. The factors for converting surface contamination given in  $pC_i/m^2$  to the annual gamma dose at one. meter above a uniformly contaminated plane have been described by Soldat and others (Refs. 4, 5, and 17). Dose factors for exposure to soil sediment have units of mrem/hr per pCi/m<sup>2</sup> surface.

A set of dose factors for 45 radionuclides was originally calculated for the year 2000 model (Ref. 4). These factors have since been recalculated using recent decay scheme informiation (Ref. 18) and expanded to include additional radionuclides. The revised list is given in Tables A-3 through A-7; it contains several radionuclides for which the daughter is not listed separately (e.g., Ru-Rh-106, Cs-137-Ba-137m, and Ce-Pr-144). In those instances, the daughter's decay energy has been included in the factor.

### 2. Equations for Liquid Pathways

This section develops the set of equations required for the liquid pathway model. The principal difference betveen pathways is the manner in which the radionuclide concentrations are calculated. The doses from the four pathways should be added to determine the total dose.

a. Potable Water

The annual dose from ingestion of water is calculated from Equation (A-2) below:

$$
R_{\text{apj}} = 1100 \frac{M_{\text{p}} U_{\text{ap}}}{F} \sum_{i} Q_{i}^{\dagger} \exp(-\lambda_{i} t_{\text{p}})^{0} a_{\text{ipj}}
$$
 (A-2)

Symbols for this equation were defined earlier, in Section **C.]** of this guide.

The sunmation process adds the dose contribution from each nuclide to yield the total dose for the pathway-organ combination selected. The Q<sup>1</sup>/F terms in Equation (A-2) define the concentration of nuclide i in the effluent at the point of discharge. The expression ( $Q_i^m$  $p$ /F)exp( $-A_i$ t<sub>p</sub>) yields the concentration of nuclide i at the time the water is consumed.<br>This concentration is the term C<sub>ip</sub> in Equation (A-1). As a minimum, the transit time t<sub>p</sub> may be set equal to 12 hours to allow for radionuclide transport through the water purification plant and the water distribution system. The transit time should be increased as appropriate to allow for travel from the point of effluent release to the water purification plant intake. Credit may be taken for radionuclide removal by water purification processes using techniques such as those outlined in Reference 4.

It should be noted that, depending on the hydrological dispersion model employed, the mixing ratio, M<sub>n</sub>, or dilution factor may not be explicitly defined. In those instances (e.g., buildup of activity in a cooling pond), the relative concentration in the mixed stream (compared to the effluent concentration) may be supplied as a function of the radiological decay constarnt. with any potential effluent recycling taken into account. Suggested hydrological dispersion models will be contained in another regulatory guide now under preparation on the subject of methods for estimating aquatic dispersion of liquid effluents from routine reactor releases for the purpose of implementing Appendix I.

## b. Aquatic Foods

The concentrations of radionuclides in aquatic foods are directly related to the concentrations of the nuclides in water. Equilibrium ratios between the two concentrations,





Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.

# TABLE A-3 (Continued)



# TABLE A-3 (Continued)

 $\cdot$ 



# TABLE A-3 (Continued)

 $\sim$ 



1.109-24



TABLE A-4 TEENAGER INGESTION DOSE FACTORS<br>(mrem/pCi ingested)

Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.

 $\sim$ 

 $\sim 10^7$ 

 $\sim 10^{-11}$ 

 $\mathcal{L}_{\mathrm{c}}$ 

 $\sim 10$ ÷.

 $\sim 10$ 

## TABLE A-5





Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.



 $\mathcal{L}_{\mathcal{A}}$ 





Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.



 $\epsilon_{\rm{max}}$ 

EXTERNAL DOSE FACTORS FOR STANDING ON CONTAMINATED GROUND\* (mrem/hr per pC1/m<sup>2</sup>)





 $3.70E - 09$  4.50E-09

\*The same factors apply for adult, teen, child.

Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.

 $531 - 133$ 







called bioaccumulation factors in this guide, can be found in the literature (Pnf. 19). The addition of the bioaccumulation factor B<sub>ip</sub> to Equation (A-2) yields Equation (A-3), which is suitable for calculating the internal dose for consumption of aquatic foods.

$$
R_{\alpha p j} = 1100 \frac{U_{\alpha p} M_p}{F} \sum_{i} Q_i^i B_{i p} D_{\alpha i p j} exp(-\lambda_i t_p)
$$
 (A-3)

Values of B<sub>in</sub> are given in Table A-8; the other parameters have been previously defined.

The transit time t<sub>p</sub> may be set equal to 24 hours to allow for radionuclide decay during transit through the food chain, as well as during food preparation.

#### c. Dose from Shoreline Deposits

The calculation of individual dose from shoreline deposits is complex since it involves estimation of sediment load, transport, and concentrations of radionuclides associated with suspended and deposited materials. One method of approaching this problem was presented in the Year 2000 Study (Refs. 4, 17, 20, and 21). Based on these references, an estimate of the radionuclide concentration in shoreline sediments can be obtained from the following expressions:

$$
C_{is} = K_c \frac{C_{iy}[1 - \exp(-\lambda_i t)]}{\lambda_i}
$$
 (A-4)

where

 $C_{i,s}$  is the concentration of nuclide i in sediment, in pCi/kg;

C<sub>iw</sub> is the concentration of nuclide i in water adjacent to the sediment, in pCi/liter;

K<sub>c</sub> is an assumed transfer constant from water to sediment, in liters/kg per day;

- t is the length of time the sediment is exposed to the contaminated water, nominally 15 years (approximate midpoint of facility operating life), in hours; and
- is the decay constant of nuclide i, in hours<sup>-1</sup> in the original evaluation of the equation,  $\lambda_A$  was chosen to be the radiological decay constant, but the true value should include an "environmental" removal constant.

The value of  $K_c$  was derived for several radionuclides by using data from water and

sediment samples collected over a period of several years in the Columbia River between Richiand, Washington, and the river mouth and in Tillamook Bay, Oregon, 75 km south of the river mouth (Refs. 22 and 23). Since the primary use of the equation is to facilitate estimates of the exposure rate from gamma emitters nne meter above the sediment, an effective surface contamination was estimated. This surface contamination was assumed to be contained within the top 2.5 cm (1 in.) of sediment.\*\* The dose contribution from the radionuclides at depths below 2.5 cm was ignored. The resulting equation is

$$
S_{i}^{T} = 100T_{i}C_{iw}W[1 - exp(-\lambda_{i}t)]
$$
 (A-5)

where

 $S_i^*$  is the "effective" surface contamination, in pCi/m<sup>2</sup>, that is used in subsequent calculations;

 $\frac{1}{N}$  with a mass of 40 kg/m $^2$  of surface.

If the presence of a radionuclide in water and sediment is controlled primarily by radioactive equilibrium with its parent nuclide, the water concentration and decay constant of the parent should be used in Equations (A-4) and (A-5).

## TABLE A-8

# BIOACCUMULATION FACTORS<br>(pCi/kg per pCi/liter)

 $\bar{z}$ 



1.109-31



\*ORNL - Private Communication<br>\*\*Freke, A.M., "A Model for the Approximate Calculation of Safe Rates of Discharge into<br>Marine Environments," <u>Health Physics</u>, Vol. 13, p. 749, 1967.<br>\*\*\*Derived from data in Bowen, H.J.M., <u>T</u>

 $T_i$  is the radiological half-life of nuclide i, in days; and

W is a shore-width factor that describes the geometry of the exposure.

Shore-width factors were derived from experimental data (Ref. 24) and are sunanarized in Tdble A-9. They represent the fraction of the dose from an infinite plane source that is estimated for these shoreline situations.

The combination of Equations (A-4) and (A-5) into the general Equation (A-i) leads to Equation (A-6) below for calculation of radiation dose from exposure to shoreline sediments.

$$
R_{a\bar{p}j} = U_{a\bar{p}} \sum_{i} S_{i}^{T} D_{a\bar{i}p\bar{j}} = 100 U_{a\bar{p}} W_{i}^{T} C_{i\bar{w}} T_{i} D_{a\bar{i}j}[1 - \exp(-\cdot_{i} t)] \qquad (A-6)
$$

= 110,000 
$$
\frac{U_{ap}N_{p}N}{F}
$$
  $\frac{1}{i} Q_{i}^{T}I_{i}D_{aipj}[exp(-\lambda_{i}t_{p})][1 - exp(-\lambda_{i}t)]$  (A-7)

## d. Dose from Foods Grown on Land Irrigated by Contaminated Water

The equations in the following paragiaphs can be used to calculate doses from radionuclides in irrigated crops. Separate expressions are presented for tritium because of its unique environmental behavior.

#### (1) Vegetation

The concentration of radioactive material in vegetation results from deposition onto the plant foliage and from uptake from the soil of activity deposited on the ground. The model used for estimating the transfer of radionuclides from irrigation water to crops through water deposited on leaves and uptake from soil was derived for a study of the potential doses to people from a nuclear power complex in the year 2000 (Ref. 4).

The equation for the model (for radionuclides except tritium) is presented below in slightly modified form. The first term in brackets relates to the concentration derived from direct foliar deposition during the growing season. The second term relates to uptake from soil and reflects the long-term deposition during operation of the nuclear facility. Thus for a uniform release rate, the concentration C<sub>iv</sub> of radionuclide i in the edible portion of crop species v, in units of pCi/kg, is given by:

$$
C_{iv} = d_i \left[ \frac{r[1 - \exp(-\lambda_{Ei}t_e)]}{r_v \lambda_{Ei}} + \frac{B_{iv}[1 - \exp(-\lambda_i t_b)]}{P\lambda_i} \right] \exp(-\lambda_i t_h)
$$
 (A-8)

The de; osition rate,  $d_i$ , from irrigated water is defined by the relation

$$
d_{i}^{'} = C_{i} I \text{ (water deposition)}
$$
 (A-9)

where

**I**

- $C_{iw}$  is the concentration of radionuclide i in water used for irrigation, in pCi/liter, and
	- I  $\,$  is the irrigation rate, in liters/m $^2$ /hr; i.e., volume of water (liters) sprinkled on unit area of field in **1** hour.

For tritium, the equation for estimating  $C_{ij}$  is (see Ref. 25):

$$
C_{V} = C_{VI}
$$
 (A-10)

For a cow grazing on fresh forage,  $t_{p}$  in Equation (A-8) is set equal to 720 hours (30 days), the typical time for a cow to return to a particular portion of the grazing site.



# TABLE A-9

# TABLE **A-10**

**I**

**P**

# ANIMAL CONSUMPTION RATES<sup>\*</sup>



From Reference 4, Tables **111-B** and **-10.**

i.

## (2) Animal Products

The radionuclide concentration in an animal product such as meat or milk is dependent on the amount of contaminated feed or forage eaten by the animal and its intake of contaminated water. The radionuclide concentration in animal products  $C_{iA}$  in terms of pCi/liter or pCi/kg (Ref. 4) is proportional to the animal's intake of the radionuclide in feed or forage (subscript F) and in water (subscript w):

$$
C_{iA} = F_{iA}[C_{iF}Q_F + C_{iAw}Q_{Aw}]
$$
 (A-11)

The second set of terms in the brackets in Equation (A-1l) can be omitted if the animal does not drink contaminated water. Values for Q<sub>F</sub> and Q<sub>Aw</sub> are presented in Table A-10. Values for Biv and FiA are given in Table **C-5** (see Appendix C).\*

The total dose R<sub>api</sub> from irrigated foods (excluding tritium) is given by:

$$
R_{\text{apj}} = U_{\text{ap}}^{\text{veg}} \sum_{i}^{C} C_{i\text{v}} D_{\text{aipj}} + U_{\text{ap}}^{\text{animal}} \sum_{i}^{C} C_{i\text{A}} D_{\text{aipj}}
$$
(A-12)

If values for C<sub>iv</sub> from Equation (A-8) and C<sub>iA</sub> from Equation (A-11) are substituted in Equation (A-12):

$$
R_{apj} \approx U_{ap}^{veg} \left[ d_i exp(-\lambda_i t_h) D_{aipj} \left[ \frac{r[1 - exp(-\lambda_{Ej} t_e)]}{Y_v \lambda_{Ei}} + \frac{B_{iv}[1 - exp(-\lambda_i t_b)]}{P \lambda_i} \right] + U_{ap}^{anima} \left[ \frac{F_{ja} D_{aipj} \left\{ Q_F d_i exp(-\lambda_i t_h) \left[ \frac{r[1 - exp(-\lambda_{Ej} t_e)}{Y_v \lambda_{Ei}} \right] + \frac{B_{iv}[1 - exp(-\lambda_i t_b)]}{P \lambda_i} \right\} + C_{iaw} q_{aw} \right] \tag{A-13}
$$

It should be noted that the two components of Equation (A-12) imply that contributions from the individual vegetable and animal products have already been summed. In actual use, it will be necessary to compute separately the milk and meat portions of the dose due to animal products (also applicable to Equation (A-17)).

For tritium, the concentration in animal products is given by the following equation (adapted from Reference 25):

$$
C_A = \frac{kwC_V}{\lambda_m} + \frac{kQ_{Aw}C_{Aw}}{m}
$$
 (A-14)

Since by Equation (A-10)  $C_v = C_w$ , and since for all practical purposes  $C_{Aw} = C_w$ , Equation (A-14) can be rearranged as follows:

$$
C_A = \frac{kC_W}{N_m} (w + Q_{AW})
$$
 (A-15)

Similarly, the above equations for tritium concentration can be combined with the general Equation (A-1):

$$
R_{apj} = U_{ap}^{veg}C_{v}D_{apj} + U_{ap}^{animal}C_{A}D_{apj}
$$
 (A-16)

$$
= U_{ap}^{veg}C_{v}D_{apj} + U_{ap}^{animal}D_{apj} \frac{kC_{w}}{\lambda_{m}}(w + Q_{Aw})
$$
 (A-17)

 $\sqrt{\frac{2}{\pi}}$  values for F<sub>iA</sub> appear as F<sub>m</sub> and F<sub>f</sub> in Table C-5.

## REFERENCES FOR APPENDIX A

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**1**

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### APPENDIX B

## MODELS FOR CALCULATING DOSES FROM NOBLE GASES DISCHARGED TO THE ATMOSPHERE

The following analytical models are used for calculating doses from exposure to gaseous<br>effluents. Separate models are given for air and tissue doses due to gamma and beta rays. effluents. Separate models are given for and time for allevated releases, all models assume submersion in an infinite cloud at the exposure point.

# 1. Annual Gamma Air Dose<sup>\*</sup> from Elevated<sup>\*\*</sup> Releases of Noble Gases

Slade (Ref. **1)** describes the derivation of the equations for estimating annual air doses from photon emitters dispersed in the atmosphere. The following expression can be used for calculating annual doses:

$$
D^{Y}(r,0) = \frac{260}{r(\Delta\theta)} \sum_{n} \frac{1}{u_{n}} \sum_{s} f_{ns} \sum_{k} u_{a} (E_{k}) E_{k} I(H,u,s,\sigma_{z},E_{k}) \sum_{i} Q_{ni}^{D} A_{ki}
$$
 (B-1)

Symbols for this equation were defined earlier, in Regulatory Position C.2.a of this guide.

The photons were combined into energy groups, and each photon intensity within a group was weighted by its energy and energy absorption coefficient. Thus, the effective fraction of disintegrations of the nuclide i yielding photons corresponding to the photon energy group k,  $A_{k,i}$ , was determined to be

$$
A_{ki} = \sum_{m} [A_{m}E_{m}u_{a}(E_{m})]/[E_{k}u_{a}(E_{k})]
$$
 (8-2)

where

 $A_m$  is the fraction of the disintegrations of nuclide i yielding photons of energy  $E_m$ ;

 $E_m$  is the energy of the mth photon within the kth energy group, in MeV; and

U<sub>a</sub> (E<sub>m</sub>) is the energy absorption coefficient in air associated with the photon energy  $E_m$ , in  $m^{-1}$ 

All other parameters are as previously defined. The summation is carried out over all photons within energy group k. Data for the photon energies and abundances for most of the noble gas nuclides were taken from Reference 2. For radionuclides not contained in Reference 2, data were obtained from Reference 3.

Decay during travel from the point of release to the receptor is

$$
Q_{ni}^{D} = Q_i^T \exp(-\lambda_i r/u_n)
$$
 (B-3)

The term "gamma air dose" refers to the components of the air dose associated with photons emitted during nuclear and atomic transformations, i.e., gamma and x-rays. Annihilation and bremsstrahlung photon radiations are possible contributors to this compunent of the air dose.

Elevated release conditions are assumed to occur when the point of release is higher than twice the height of adjacent solid structures. (See Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion for Gaseous Effluents in Routine Releases from Light-<br>Water-Cooled Reactors.")

where

**Qi** is the initial release rate of nuclide i, in Ci/yr, and

 $\lambda_i$  is the decay constant of nuclide i, in sec<sup>-1</sup>

All other parameters are as previously defined.

## 2. Annual Gamma Air Dose from Ground-Level<sup>\*</sup> Releases of Noble Gases and Annual Beta Air Dose

Plumes of gaseous effluents are considered semi-infinite in the case of noble gases released from vents. The concentration of the radionuclides in air at the receptor location may be determined from atmospheric dispersion model described in Regulatory Guide **1.111.** The annual average ground-level concentration of gaseous effluent species i at location  $(r,0)$  from the release point is determined from

$$
\chi_{i}(r,\theta) = 3.17 \times 10^{4} Q_{i}^{1} [\chi/Q']^{0}(r,\theta)
$$
 (B-4)

where

 $x_i(r,\theta)$  is the annual average ground-level concentration of nuclide i at the distance r in the sector at angle  $\theta$  from the release point, in pCi/m<sup>3</sup>, and  $[x/Q^i]^D(r,0)$  is the annual average gaseous dispersion factor (corrected for radioactive decay) in the sector at angle **e** at the distance r from the release point,. in sec/ $m^3$ .

The constant 3.17 x 10 $^4$  represents the number of pCi per Ci divided by the number of seconds per year. All other parameters are as previously defined.

The annual gamma or beta air dose associated with the airborne concentration of the effluent species is then **I**

$$
D^{Y}(r,\theta) \text{ or } D^{B}(r,\theta) = \sum_{i} x_{i}(r,\theta) (DF_{i}^{Y} \text{ or } DF_{i}^{B})
$$
 (B-5)

where the terms are as defined in Regulatory Position C.2.b.

Table B-1 presents a tabulation of the dose factors for the noble gases and daughters of interest.

## 3. Annual Dose to Tissue from Noble Gas Effluents

It is also necessary to determine annual doses to real individuals in unrestricted areas. The staff computes the total body dose from external radiation at a depth of 5 cm into the body and the skin dose at a depth of 7 mg/cm<sup>2</sup> of tissue.

## a. Elevated Releases

The annual total body dose is computed as follows:

$$
D^{T}(r, \theta) = 1.11 \times S_F \sum_{k} D_{k}^{Y}(r, \theta) exp[-v_{d}^{T}(E_{k})t]
$$
 (B-6)

Ground-level release conditions are assumed to exist when the release point is less than or equal to twice the height of adjacent solid structures and the vertical exit velocity is less than five times the horizontal wind speed. (See Regulatory Guide **1.111.)**

The term "beta air dose" refers to the component **of** the air dose associated with particle emissions during nuclear and atomic transformations, i.e., **0+, B-,** and conversion electrons. **I**

<b>Nuclide</b>	$\beta$ -air <sup>*</sup> (DF <sup>B</sup> )	$B-Skin$ <sup>**</sup> ( $DFS1$ )	$\gamma$ -Air <sup>*</sup> (DFB <sup><math>\gamma</math></sup> )	$y - Body$ (DFB,)
$Kr-83m$	$2.88E - 04$		$1.93E - 05$	7.56E-08
$Kr-85m$	$1.97E - 03$	$1.46E - 03$	$1.23 - 03$	$1.17E-03$
$Kr-85$	$1.95E-03$	$1.34E-03$	$1.72E-05$	$1.61E-05$
$Kr-87$	$1.03E - 02$	$9.73E - 03$	$6.17E-03$	$5.92E - 03$
$Kr-88$	$2.93E - 03$	$2.37E-03$	$1.52E - 02$	$1.47E-02$
$Kr-89$	$1.06E - 02$	$1.01E-02$	$1.73E-02$	$1.66E-02$
$Kr-90$	$7.83E - 03$	$7.29E-03$	$1.63E - 02$	$1.56E - 02$
$Xe-131m$	1.11E-03	$4.76E - 04$	$1.56E - 04$	$9.15E-05$
$Xe-133m$	$1.48E - 03$	$9.94E - 04$	$3.27E - 04$	$2.51E-04$
$Xe-133$	$1.05E-03$	$3.06E - 04$	$3.53E - 04$	$2.94E-04$
$Xe-135m$	$7.39E - 04$	$7.11E-04$	$3.36E - 03$	$3.12E - 03$
$Xe-135$	$2.46E - 03$	$1.86E-03$	$1.92E - 03$	$1.81E-03$
$Xe - 137$	$1.27E - 02$	$1.22E - 02$	$1.51E-03$	$1.42E - 03$
Xe-138	4.75E-03	$4.13E - 03$	$9.21E - 03$	8.83E-03
$Ar-41$	$3.28E - 03$	$2.69E-03$	$9.30E - 03$	8.84E-03

TABLE B-1

DOSE FACTORS FOR NOBLE GASES AND DAUGHTERS

 $\frac{\frac{1}{2} \frac{1}{\sqrt{1 - y}}}{p \cdot 1 - y \cdot r}$ 

 $\frac{r}{\frac{m \cdot m - m^3}{p(1 - y)^2}}$ 

 $\mathcal{L}_{\text{max}}$  .

\*\*\* 2.88E-04 = 2.88 x 10<sup>-4</sup>

 $1.109 - 41$ 

Symbols for this equation were defined earlier in Regulatory Position C.2.c of this guide. The constant 1.11 represents the ratio of the energy absorption coefficient for tissue to that for air.

The skin dose has two components, the ganmia and beta contributions. The skin dose rate is computed by

$$
D^{S}(r,0) = 1.11 \times S_{F}D^{Y}(r,0) + 3.17 \times 10^{4} \sum_{i=1}^{5} Q_{i}^{I}[x/Q^{T}]^{D}(r,0)DFS_{i}
$$
 (B-7)

Symbols for this equation were defined earlier in Regulatory Position C.2.d of this guide.

The skin beta dose factors **OFS** were determined using the decay scheme source documents cited above and the methods used in References 4, 5, and 6.

## b. Ground-Level Releases

The annual total body dose is computed as follows:

$$
D_{\infty}^{\mathbf{I}}(\mathbf{r},\theta) = 1.11 \times S_{\mathbf{F}} \sum_{i}^{K} x_{i}(\mathbf{r},\theta) \text{DFB}_{i}
$$
 (B-8)

Symbols for this equation were defined earlier in Regulatory Position C.2.e of this guide.

The annual skin dose is computed as follows:

$$
D_{\infty}^{S}(r, \theta) = 1.11 \times S_{\mathsf{F}} \sum_{i} \chi_{i}(r, \theta) DF_{i} + \sum_{i} \chi_{i}(r, \theta) DFS_{i}
$$
 (B-9)

where

 $D_{n}^{S}(r,\theta)$ is the annual skin dose due to immersion in a semi-infinite cloud in  $x_{\text{a}}(r,0)$  is the annual skin dose due to minersion in a semi-immunite cloud in<br>the sector at angle  $\theta$ , at the distance r from the release point, in<br> $x_{\text{i}}(r,0)$  is the airborne concentration of radionuclide i at p mrem/yr, and

$$
\chi_{z}(r, \theta)
$$
 is the airborne concentration of radionucide i at point  $(r, \varepsilon)$ , in pCi/m<sup>3</sup>.

**I**

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## APPENDIX C

# MODELS FOR CALCULATING DOSES VIA ADDITIONAL PATHWAYS FROM RADIOIODINES AND OTHER RADIONUCLIDES DISCHARGED TO THE ATMOSPHERE

## 1. Annual External Dose from Direct Exposure to Activity Deposited on the Ground Plane

The ground plane concentration of radionuclide i at the location  $(r,0)$  with respect to the release point may be determined by

$$
C_{i}^{G}(r, \epsilon) = \frac{1.1 \times 10^{B} - \epsilon_{i}(r, \epsilon) Q_{i}^{*}}{\lambda_{i}} [1 - \exp(-\lambda_{i} t)]
$$
 (C-1)

;'-here

 $C_3^G(r, \phi)$  is the ground plane concentration of the radionuclide i in the sector at angle  $\dot{\sigma}$  at the distance r from the release point, in  $pCi/m^2$ ;

 $Q'_i$  is the annual release rate of nuclide i to the atmosphere,  $\{m \in \mathbb{N}/yr\}$ 

t is the time period over which the accumulation is evaluated, which is 15 years (mid-point of plant operating life). This is a simplified method of approximating the average deposition over the operating lifetime of the facility;

$$
E_{\mathbf{i}}(r,\hat{v})
$$
 is the annual average relative deposition of effluent species i at location  $(r,\hat{v})$ , considering depletion of the plume during transport, in  $m^{-2}$ ; and

 $\mathcal{F}_{\mathbf{1}}$ is the radiological decay constant for nuclide i, in  $\mathsf{vr}^{-1}$ .

The annual dose from nuclide i resulting from direct exposure to the contaminated ground plant is then

$$
D_{ij}^{G}(r,e) = 8760 S_{F}C_{i}^{G}(r,e)DFG_{ij}
$$
 (C-2)

where

**ii**

 $\overline{G}(r)$ is the annual dose to organ j from the ground plane concentration of nuclide i at the location  $(r, \rho)$ , in mrem/yr

and other terms are as defined previously in Regulatory Position C.3.a of this guide.

The annual dose to organ j is therefore

$$
D_j^G(r, \epsilon) = 8760 S_F \sum_{i} C_i^G(r, \epsilon) DFG_{ij}
$$
 (C-3)

Values for the open field ground plane dose conversion factors for the skin and total body are given in Tables A-3 to A-7. The annual dose to all other organs is taken to be equivalent to the total body dose.

Does not include noble gases or their shurt-lived daughters; see Appendix B.

### 2. Annual Dose from Inhalation of Radionuclides in Air

The annual average airborne concentration of radionuclide i at the location  $(r,s)$  with respect to the release point may be determined as

$$
\chi_1(r,0) = 3.17 \times 10^4 Q_{\star}^1 [\chi/Q']^D(r,0)
$$
 (C-4)

where

 $Q_i^{\star}$ is the release rate of nuclide i to the atmosphere, in Ci/yr;

- $x_1(r,0)$  is the annual average ground-level concentration of nuclide i in air in the sector at angle  $\theta$  at distance r from the release point, in  $pCi/m^3$ ;
- $\left[\chi/Q^i\right]^D(r,0)$  is the annual average atmosphere dispersion factor, in sec/m<sup>3</sup> (see Requlatory Guide 1.111). This includes depletion (for radiolodines and particulates) and radioactive decay of the plume; and
	- $3.17 \times 10^4$  is the product of the number of pCi/Ci and sec/yr.

The annual dose associated with inhalation of nuclide i at the airborne concentration  $\chi_i(r, \theta)$  is then

$$
D_{ija}^{A}(r,\theta) = \chi_{i}(r,\theta)R_{a}DFA_{ija}
$$
 (C-5)

Values for DFAija are given in Tables **C-1** to C-4, and all other symbols are as defined earlier in Regulatory Position C.3.b.

The annual dose to organ j in age group a from all nuclides in the effluent is:

$$
D_{ja}^{A}(r,0) = R_a \sum_{i=1}^{N} (r,e)DFA_{ija}
$$
 (C-6)

#### 3. Concentrations of Airborne Radionuclides in Foods

The concentration of radioactive material in vegetation results from deposition onto the plant foliage and from uptake of activity initially deposited on the ground. The model used for estimating the transfer of radionuclides from the atmosphere to food products is six:ilar to the model developed for estimating the transfer of radionuclides from irrigation water given in Appendix A of this guide.

For all radioiodines and particulate radionuclides, except tritium and carbon-14, the concentration of nuclide i in and on vegetation at the location  $(r,\theta)$  is estimated using

$$
C_{i}^{V}(r,\theta) = d_{i}^{V}(r,\theta) \left[ \frac{r[1 - \exp(-\lambda_{E} t_{e})]}{Y_{v} \lambda_{E} i} + \frac{B_{i}^{V}[1 - \exp(-\lambda_{i} t_{b})]}{P_{\lambda}^{V}} \right] \exp(-\lambda_{i} t_{h})
$$
 (C-7)

See Regulatory Position C.l of tnis guide for definitions of terms.

Carbon-14 is assumed to be in oxide form (CO and  $CO<sub>2</sub>$ ). The concentration of carbon-14 in vegetation is calculated by assuming that its ratio to the natural carbon in the vegetation is the same as the ratio of carbon-14 to natural carbon in the atmosphere surrounding the vegetation (see Refs. 1 and 2).

I







Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.

# TABLE C-1 (Continued)



## TABLE C-1 (Continued)

 $\mathcal{L}$ 

 $\ddot{\phantom{a}}$ 



TABLE C-1 (Continued)









Hote: 0.0 means insufficient data or that the dose factor is <1.0E-20.

## TABLE C-3





Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.



# INFANT INHALATION DOSE FACTORS<br>(mrem/pCi inhaled)



Note: 0.0 means insufficient data or that the dose factor is <1.0E-20.

1.109-53

This yields

$$
C_{14}^{V}(r, \theta) = 3.17 \times 10^{7} Q_{14}^{V}[x/Q^{V}](r, \theta) \quad 0.11/0.16
$$
\n
$$
= 2.2 \times 10^{7} Q_{14}^{V}[x/Q^{V}](r, \theta) \qquad (C-8)
$$

where

$C_{14}^V(r,0)$	is the concentration of carbon-14 in vegetation grown at location $(r,e)$ , in $pCi/kg$ ;
$Q_{14}^1$	is the annual release rate of carbon-14, in Ci/yr;
0.11	is the fraction of total plant mass that is natural carbon, dimensionless;
0.16	is equal to the concentration of natural carbon in the atmosphere, in $g/m^3$ ;
3.17 x 10 <sup>7</sup>	is equal to $(1.0 \times 10^{12} \text{ pCi/Ci})(1.0 \times 10^3 \text{ g/kg})/(3.15 \times 10^7 \text{ sec/yr})$ .

The concentration of tritium in vegetation is calculated from its concentration in the air surrounding the vegetation. Using the method described in Reference 3, the NRC staff derived the following equation:

$$
C_{\Upsilon}^{V}(r,\theta) = 3.17 \times 10^{7} Q_{\Upsilon}^{L}(x/Q') (r,\theta) (0.75) (0.5/H)
$$
  
= 1.2 x 10<sup>7</sup> Q\_{\Upsilon}^{L}(x/Q') (r,\theta) / H (C-9)

where

 $C_{\tau}^{V}(r, \theta)$  is the concentration of tritium in vegetation grown at location  $(r, \theta)$ , pCi/kg; H is the absolute humidity of the atmosphere at location  $(r,\theta)$  in g/m<sup>3</sup>; **Qý** is the annual release rate of tritium, Ci/yr; 0.5 is the ratio of tritium concentration in atmospheric water to tritium con- centration in plant water, dimensionless; and

0.75 is the fraction of total plant mass that is water, dimensionless.

The deposition rate from the plume is defined by:

$$
d_{\frac{1}{2}}(r,\theta) = 1.1 \times 10^{8} \delta_{\frac{1}{2}}(r,\theta) Q_{\frac{1}{2}} \tag{C-10}
$$

where

 $\delta_4(r,\theta)$  is the relative deposition of nuclide 1, considering depletion and decay in transit to location (r,O), in m"2 (see Regulatory Guide **1.111)** and **1.1**  $\times$  10<sup>8</sup> is the number of pCi per Ci (10<sup>12</sup>) divided by the number of hours per year (8760).

For radioiodines the model considers only the elemental fraction of the effluent. The deposition should be computed only for that fraction of the effluent that is estimated to be elemental iodine. Measurements at operating facilities indicate that about half the radioiodine exignities is some considered nonelemental (Reference 4). With this consideration included,<br>Equation (C-10) for radioiodine becomes:<br>**I** 

$$
d_{\hat{i}}(r,\theta) = 5.5 \times 10^7 \delta_{\hat{i}}(r,\theta)Q_{\hat{i}}^{\dagger}
$$
 (C-1)

and **Q!** is the total (elemental and nonelemental) radioiodine emission rate. The retention ictor r for elemental radioiodine on vegetation should be taken as unity, since the experimental measurement (References 5, 6, and 7) techniques used to evaluate this transfer mechanism consisted of direct comparison of the gross radioiodine concentration on vegetation and the concentration in air (References 8, **9,** and **10).**

For radioiodines, the deposition model is based only on the dry deposition process. We deposition, including "washout" of the organic and non-organic iodine fractions, should be con<br>sidered at some sites depending on the meteorological conditions (see Regulatory Guide 1.111).

For particulates, the deposition model considers both wet and dry deposition. There is also a retention factor (r of Equation (C-7)) that accounts for the interception and capture of the deposited activity by the vegetative cover. A value of 0.2 is taken for this factor (References **<sup>11</sup>**and 12). All nuclides except noble gases, tritium, carbon-14, and the iodines are treated as particulates.

## a. Parameters for Calculating Nuclides Concentrations in Veqetation Consumed **by** Man

When the radionuclide concentration in vegetation directly ingested by man is estimated using Equation (C-7), the following parameters are used:



All other parameters in this equation are given in Regulatory Position C of this guide.

### b. Parameters for Calculating Nuclide Concentrations in Milk

The radionuclide concentration in milk is dependent on the amount and contamination level of the feed consumed by the animal. The radionuclide concentration in milk is estimated a<sub>5</sub>

$$
C_{i}^{m}(r, \theta) = F_{m}C_{i}^{V}(r, \theta)Q_{F} \exp(-\lambda_{i} t)
$$
 (C-12)

where

 $C_i^n(r, a)$  is the concentration in milk of nuclide i, in pCi/liter;

- $C_{\epsilon}^{V}(r, \theta)$  is the concentration of radionuclide i in the animal's feed, in pCi/kg;
	- F<sub>m</sub> is the average fraction of the animal's daily intake of radionuclide i which appears in each liter of milk, in days/liter (see Tables C-5 and C-6 for cow and goat data, respectively; for nuclides not listed in Table C-6, use the values in Table C-5);

# TABLE C-5

# STABLE ELEMENT TRANSFER DATA



 $\frac{1}{\sqrt{1}}$  Refs. 7, 8, 9, 10, 14, 15, 16, 17.

 $\overline{\text{Ref. 1.}}$  $\stackrel{\text{**}}{\text{Ref. 3.}}$ 

<sup>++</sup>Ref. 18.

\*\*\* $Ref. 13.$ 



NUCLIDE TRANSFER PARAMETERS FOR GOAT'S MILK



Computed from the data of Refs. **I** and 19.  $*_{\mathsf{p}_{\mathsf{p}}\mathsf{f}}$  13.

1.109-57

- Q<sub>F</sub> is the amount of feed consumed by the animal per day, in kg/day;
- t is the average transport time of the activity from the feed into the mil: and to the receptor (a value of 2 days is assumed); and
- $\lambda_i$  is the radiological decay constant of nuclide i, in days<sup>-1</sup>.

Milk-producing animals are assumed to be on open pasture for the following grazing periods:



where

**fp** is the fraction of the year that animals graze on pasture.

These data may be supplemented by information on site-specific dairy practices. The concentration of radionuclide i in the animal's feed is then

$$
C_{i}^{V}(r,\theta) = f_{p}f_{S}C_{i}^{P}(r,\theta) + (1 - f_{p})C_{i}^{S}(r,\theta) + f_{p}(1 - f_{S})C_{i}^{S}(r,\theta)
$$
 (C-13)

where

**P** Ci(ra) is the concentration of radionuclide i on pasture grass, in pCi/kg;  $C_3^S(r,\theta)$  is the concentration of radionuclide i in stored feeds, in pCi/kg; and f<sub>s</sub> is the fraction of daily feed that is pasture grass when the animal grazes on pasture.

The following parameters will be employed in evaluating the milk pathway, unless site-specific data is supplied.



4

## c. Parameters for Calculating Nuclide Concentration in Meat

As in the milk pathway, the radionuclide concentration in meat is dependent on the amount and contamination level of the feed consumed by the animal. The radionuclide concentration in meat is estimated as

$$
C_1^F(r,e) = F_f C_1^V(r,e) Q_F exp(-\lambda_1 t)
$$
 (C-14)

where

 $\mathsf{c}^\mathsf{r}_\ast$ 

is the concentration of nuclide i in animal flesh, in  $pCi/kg$ ;

- $F_f$  is the fraction of the animal's daily intake of nuclide i which appears in each kiloaram of flesh, in days/kg (see Table C-5 for values); and
- t is the average time from slaughter to consumption, which is assumed to be 20 days.

All the other symbols are as previously defined.

Beef cattle will be assumed to be on open pasture for the grazing periods outlined for milk cattle.

## 4. Annual Dose from Atmospherically Released Radionuclides in Foods

The annual dose resulting from ingestion of radionuclide i in the diet is given by

$$
D_{ija}^{D}(r,e) = DFI_{ija} [U_{a}^{V}f_{g}C_{i}^{V}(r,e) + U_{a}^{m}C_{i}^{m}(r,e) + U_{a}^{F}C_{i}^{F}(r,e) + U_{a}^{F}f_{i}C_{i}^{L}(r,e)]
$$
 (C-15)

where

$$
\mathsf{D}_{\mathtt{i}\mathtt{j}\mathtt{a}}^{\mathsf{U}}(\mathsf{r},\mathtt{e}
$$

) is the annual dose to organ j of an individual in age group a for nuclide i, in mrem/yr;

DFI<sub>ija</sub> is the dose conversion factor for the ingestion of nuclide i, organ j, and age group a, in mrem/pCi (from Tables A-3 through A-6 of Appendix A of this guide); and

$$
u_a^v, u_a^m, u_a^F, u
$$

 $\frac{1}{a}$  are the ingestion rates of produce (non-leafy vegetables, fruit, and grains), milk, meat, and leafy vegetables, respectively, for individuals in age group a (from Table A-2 of Appendix A of this guide).

All the other symbols are as previously defined.

The annual dose to organ j of an individual in age group a from consumption of vegetables, milk, and meat is therefore

$$
D_{ja}^{0} = \sum_{i} DF_{ija} [U_{a}^{V}f_{g}C_{i}^{V}(r,e) + U_{a}^{m}C_{i}^{m}(r,e) + U_{a}^{F}C_{i}^{F}(r,e) + U_{a}^{L}f_{\lambda}C_{i}^{L}(r,e)]
$$
 (C-16)

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## APPENDIX D

## MODELS FOR CALCULATING POPULATION DOSES FROM NUCLEAR POWER PLANT EFFLUENTS

Calculation of the annual population-integrated total body and thyroid doses should be performed for the three effluent types identified in this guide. These doses should be evaluated for the population within a 50-mile radius of the site, as specified in paragraph **D,** Section II of Appendix I to **10** CFR Part 50.

For the purpose of calculating the annual population-integrated dose, the 50-mile region should be divided into a number of subregions consistent with the nature of the region. These subregions may represent, for example, the reaches of a river or land areas over which the appropriate dispersion factor is averaged. Dispersion factors, population data, and other information describing existing or planned uses of the subregions should be developed.

#### **1.** General Expressions for Population Dose

For pathways in which the permanent and transient population of the subregion can be considered to be exposed to the average radionuclide concentrations estimated for the subregion, the annual population-integrated dose is calculated as follows:

$$
D_j^P = 0.001 \sum_{d} P_d \sum_{a} D_{jda} f_{da}
$$
 (D-1)

where

Djda is the annual dose to organ j (total body or thyroid) of an average ida and in the state of an average individual of age group a in subregion d, in mrem/yr;

D<sup>P</sup> is the annual population-integrated dose to organ j (total body or thyroid),<br>in man-rems or thyroid man-rems;

f<sub>da</sub> is the fraction of the population in subregion d that is in age group a;

P<sub>d</sub> is the population associated with subregion d; and

**0.001** is the conversion factor from millirems to rems.

The annual dose to the total body or thyroid of an average individual should be evaluated with the usage factors of Table **0-1.** Models and equations for the detailed dose calculations are presented In Appendices A, B, and C of this guide. The annual population-integrated doses from ingestion of potable water, inhalation of airborne effluents, and external exposure to airborne or deposited radionuclides should be evaluated.

For pathways that involve food products produced in the subregion, the food products may be distributed to other areas for consumption. For all the food that is produced within the 50-mile radius, the radioactivity concentrations are averaged over the entire area by weiqhting the concentrations in each subregion by the amount produced in each subregion. This average concentration is used in calculating the population doses. The 50-mile average concentration of nuclide i in food p is computed as

$$
\overline{c}_{ip} = (1/V_p) \exp(-\lambda_i t_p) \int\limits_{d}^{R} C_{dip} v_{dp}
$$
 (0-2)

The population-integrated dose is the summation of the dose received by all individuals and has units of man-rem when applied to the total body dose and units of man-thyroid-rem when applied to the summation of thyroid dose.



# TABLE **D-1**

RECOMMENDED VALUES TO BE USED FOR THE AVERAGE INDIVIDUAL

Consumption rate obtained from Reference 3 of Appendix A and in Reference 4 of Appendix A. Data obtained directly from Reference 4 of Appendix **A.** age-prorated using techniques

Data obtained directly from Reference **15** of Appendix A.  $+ +$ 

**i**

where

C<sub>dip</sub> is the average concentration over subregion d of the nuclide i in pathway p,<br>in pCi/kg or pCi/liter (see Appendices A and C of this guide for models and equations for calculation of pathway concentrations);

 $\overline{c}_{in}$  is the 50-mile average concentration of nuclide i in pathway p, in pCi/kg or pCi/liter;

 $\label{eq:2} \left\langle \mathcal{L}_{\mathcal{A}} \left( \mathcal{L}_{\mathcal{A}} \right) \right\rangle = \left\langle \mathcal{L}_{\mathcal{A}} \right\rangle = \left\langle \mathcal{L}_{\mathcal{A}} \right\rangle$ 

t<sub>o</sub> is the transport time of the food medium p through the distribution system. **p** in days (Tahle D-2 presents estimates of the transport times that may be used in lieu of site-specific data);

- **v** dp is the annual mass or volume of food medium p produced in subregion d,  $\mathbf{d} \cdot \mathbf{r}$
- V<sub>2</sub> is the mass or volume of the food medium p produced annually with the **p'** 50-mile radius about the site, in kg or liters; and
- $\lambda_i$  is the radiological decay constant for nuclide i, in days<sup>-1</sup>.

The population served by all the food produced within 50 miles of the site is estimated as

$$
p_p^* = V_p / \frac{1}{a} U_{ap} f_a
$$
 (D-3)

where

**fa** is the fraction of the population within the age group a;

 $P_{D}$  is the estimated population that can be served by the quantity of food p likely to be produced within 50 miles of the site;

**U** a is the use or consumption factor of food medium p for the average Uap individual in age group a, in kg/yr or liters/yr (taken from Table **0-1);** and

V is the annual mass or volume of food medium p likely to be produced within<br>
a 50-mile radius about the site, in kg or liters.

The annual population-integrated dose is then calculated as

 $D_j^P = 0.001 \sum_{n} P_p \sum_{i} \sum_{a} f_a \overline{C}_{ip} U_{ap} DF_{ai}$  (0-4)

where

$$
P_{p} = \begin{cases} p_{p}^{*} & \text{if } p_{p}^{*} < P_{50} \\ p_{50} & \text{if } p_{p}^{*} \ge P_{50} \end{cases}
$$

and

DF<sub>ai</sub> is the dose factor for age group a and nuclide i, in mrem/pCi (taken from Tables A-3 to A-7 and **C-1** to C-4);

## TABLE D-2

# RECOMMENDED VALUES FOR THE TRANSPORT TIMES IN THE FOOD DISTRIBUTION SYSTEM<sup>\*</sup>



To be used in lieu of site-specific data on food distribution.

4

D<sub>j</sub> is the annual population-integrated dose to organ j (total body or thyroid), in man-rem/yr or thyroid man-rem/yr;

P<sub>p</sub> is the population consuming food medium p; and

 $P_{50}$  is the total population within 50 miles.

All other factors are as defined above.

Note that the above formulation limits the evaluation of the exposed population evaluation to the population residing within 50 miles as specified in paragraph **D,** Section II of Appendix I to **10** CFR Part 50. In calculating the annual population-integrated total body and thyroid doses, the current age distribution of the population within 50 miles may be assumed to be the same as the current age distribution of the U.S. population (see Reference for Appendix **D).** Models and equations for the detailed dose calculations are presented in Appendices A, B, and C.

## 2. Use of the Models

## a. Population-Integrated Doses from Liquid Effluents

The annual total body and thyroid population-integrated doses due to exposure to liquid effluents should be evaluated for the following principal pathways: potable water, aquatic food products, external irradiation from shoreline deposits, and terrestrial food products irrigated with water that has received the liquid effluent. In addition to these pathways, other exposure pathways that arise from unique conditions at a specific site should be evaluated if they provide a significant\* contribution to the annual dose received by an exposed population group.

#### **(1)** Doses from Potable Water

The annual population-integrated total body and thyroid doses from water consumption are evaluated for all subregions that have water intakes existing or designated at the time of the license application. The products of the individual doses and the population exposed in each such subregion within 50 miles from the site are summed to obtain the total dose. The formulation expressed in Equation **(D-1)** may be used.

The total body and thyroid dose of the individuals should be evaluated using Ecuation (A-2) in Appendix A of this guide, together with the age-dependent usage factors U<sub>ap</sub> obtained from Table D-1. The dilution from the discharge point to the usage point should

be evaluated using appropriate hydrological models for the various subregions.

If the population served by a particular water supply system is not known, it can be estimated by the following:

 $P_w = v/c$  (D-5)

where

**c** is the average daily usage of individuals on the system, in gal/day per person;

P<sub>w</sub> is the estimated population served by the water system; and

v is the average'daily intake of the water supply system, in gal/day.

If the industrial usage from the water supply system is known, it can be subtracted from the average daily intake of the system before this value is entered into Equation (0-5).

For the purpose of this guide, any additional pathway is deemed to be significant if a conservative evaluation of the pathway yields an additional dose contribution equal to or greater than **10%** of the total from all the pathways described here. Any pathway so identified should then be evaluated by a model similar to that used above.

The population served by a water supply system whose intake is within the 50-mile radius may include individuals who reside outside the circle. This population may be pro-rated to include only the population within the 50-mile radius. Conversely, a water supply system with an intake beyond the 50-mile radius may serve the population within the 50-mile radius. Such exposed population should be included in the 50-mile population dose evaluation.

#### (2) Doses from Food Products

The annual population-integrated total body and thyroid doses from consumption of aquatic food products are evaluated using the production of sport and commercial harvests in the various subregions. The mixing ratio (or dilution) should be evaluated for each subregion using an appropriate hydrological model. For sport harvests, the entire edible harves is assumed to be ingested by the population within 50 miles. The formulation expressed by Equation (D-4) should be used with the population **P<sub>p</sub>** given by the results of Equation (D-3)

The age-specific ingestion factors of Table **D-I** may be used in lieu of site-specific data.

For commercial harvests, the production within 50 miles from the site is considered as part of the total U.S. harvest. Equation (D-2) should be used to compute the average concentration, with **Vp** as the total estimated U.S. commercial harvest of the aquatic food

medium p. The annual population-integrated dose is then computed using Equation (D-4) with P<sub>p</sub> = P<sub>SO</sub>. The age-specific factors of Table D-1 may be used in lieu of site-specific data

## (3) Doses from Shoreline Deposits

The annual population-integrated total body and thyroid doses from recreational activities on the shoreline of the receiving water body are evaluated by sunmming the product of the individual doses in each subregion and the population exposed therein. All subregions within the 50-mile radius should be considered where existing or designated recreational facilities exist. If available, actual recreational usage in the vicinity of each facility should be used. The formulation of Equation **(D-1)** is appropriate.

## (4) Doses from Consumption of Terrestrial Food Products Irrigated by Waters Receiving the Liquid Effluent

The annual population-integrated total body and thyroid doses from consumption of food irrigated with water from the body receiving the liquid effluent are evaluated following the procedures outlined in the development of Equation (0-4). Note that the term V<sub>p</sub> of Equations

(0-2) and (D-3) denotes the total production of food medium p within 50 miles, not just the total production of irrigated food medium p. The consumption rate data of Table **D-1** may be used in lieu of site-specific data in the evaluation of Equation (D-4).

#### b. Population-Integrated Doses from Airborne Effluents

The annual total body and thyroid population-integrated doses should be evaluated for the following principal exposure pathways: noble gas submersion, inhalation of airborne effluents, ingestion of contaminated terrestrial foods (milk, meat, and vegetation), and external irradiation from activity deposited on the ground. In addition to these pathways, other exposure pathways that arise from unique conditions at a specific site should be evaluated if they provide a significant contribution to the annual dose received by an exposed population group. (See Regulatory Position **C.1** of this guide.)

For the evaluation of exposures from atmospheric releases, the 50-mile region should be divided into 160 subregions formed by sectors centered on the 16 compass points (N, NNE, NE, etc.) and annuli at distances of **1,** 2, 3, 4, 5, **10,** 20, 30, 40, and 50 miles from the center of the facility. The atmospheric dispersion factors  $(x/Q')$  or similar factors should be evaluated at the radial midpoint for each of the subregions using appropriate atmospheric dispersion models such as those described in Regulatory Guide **1.111.**

#### (1) Doses due to Exposure to Noble Gases

The annual population-integrated total body dose due to noble gas effluents should be evaluated by summing the products of the individual doses in each subregion and the population in each subregion. Equation **(D-1)** may be used. For external exposure, the model does population in each subtegron. Equation (D-1) may be used. For external exposure, the model does<br>not differentiate between age groups. A structural shielding factor of 0.5 should be applied in<br>conjunction with the dose fact

## (2) Doses due to Inhalation of Radlolodines and Particulates

The annual population-integrated total body and thyroid doses from inhalation of airborne effluents should be evaluated by summing the products of the individual doses received in each subregion and the population in each subregion. Equation **(D-1)** may be used. The age-specific inhalation rates of Table **D-1** may be used with the data of Tables C-l to C-4.

## (3) Doses due to Ingestion of Terrestrial Food Products

The annual population-integrated total body and thyroid doses from ingestion of terrestrial food products should be evaluated using the production data for each subregion. For milk, meat, and commercial vegetables, the formulation of Equation (0-2) should be used to calculate the average concentrations in the foods. These concentrations are then used in Equation (D-4), along with the data of Tables **D-1,** D-2, and A-l to calculate population doses.

#### (4) Doses due to External Irradiation from Activity Deposited on the Ground

The annual population-integrated total body and thyroid doses from external exposure to surface deposition of the effluent should be evaluated using Equation (D-l). A household shielding and occupancy factor of 0.5 should be applied in conjunction with the dose factors of Tables A-3 to A-7.

#### REFERENCE FOR APPENDIX D

"Current Population Reports," Bureau of the Census, Series P-25, No. 541, U.S. Dept. of Commerce, **1975.**