# Southern California Edison Company

SAN ONOFRE NUCLEAR GENERATING STATION

P. O. BOX 128 SAN CLEMENTE. CALIFORNIA 92672

H. E. MORGAN STATION MANAGER

## October 18, 1989

TELEPHONE (714) 368-6241

U. S. Nuclear Regulatory Commission Document Control Desk Washington, D.C. 20555

Subject: Docket No. 50-206 Revised Report Licensee Event Report No. 89-001, Revision 1 San Onofre Nuclear Generating Station, Unit 1

Reference: Letter, H. E. Morgan (SCE) to USNRC Document Control Desk, dated January 23, 1989

The referenced letter provided Licensee Event Report (LER) No. 89-001, for an condition involving the reactor vessel thermal shield support system. Enclosed is a revision to this LER which provides additional information concerning the cause and corrective action.

If you require any additional information, please so advise.

Sincerely, HEMO

Enclosure: LER No. 89-001, Rev. 1

cc: C. W. Caldwell (USNRC Senior Resident Inspector, Units 1, 2 and 3)
J. B. Martin (Regional Administrator, USNRC Region V)
Institute of Nuclear Power Operations (INPO)

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On 1/8/89, with Unit 1 in Mode 6 for the Cycle 10 refueling outage, after performing a remote video camera inspection of the thermal shield support system, it was observed that three thermal shield support block bolts were out of tolerance. Three bolts, two on one support block and one on another support block, were protruding from the inner surface of the core barrel by an amount that exceeds normal, original assembly, tolerance. The remaining four blocks and their bolts were acceptable. The three bolts protruding from the inner surface of the core barrel are postulated to have failed. The cause of the failure is believed to be high-cycle fatigue due to flow induced vibration.

As corrective action all accessible support features have been inspected by remote video camera. The bottom of the reactor vessel has been inspected and no broken bolts were found. Engineering analysis has been performed to verify that continued operation through fuel Cycle 10 would not degrade the thermal shield support system to an extent which would lead to significant damage of core internals. Also, analysis has shown that significant loose parts, leading to flow blockage, would not be generated; and that increased vibration due to loose parts, or further bolt failure could be monitored.

License Amendment Number 127 provides for a thermal shield monitoring program which has been implemented and will be continued until the thermal shield fasteners are restored to their designed functional condition during the 10-year ASME Inservice Inspection planned for the fuel Cycle-11 refueling outage. The refueling outage is scheduled to begin no later that June 30, 1990. A conceptual design and plan for restoring the thermal shield supports was submitted on October 6, 1989.

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Plant: San Onofre Nuclear Generating Station Unit: One Reactor Vendor: Westinghouse Event Date: 1-8-89

A. CONDITIONS AT TIME OF THE EVENT:

Mode: 6, Refueling

### B. BACKGROUND INFORMATION:

The thermal shield, located between the core barrel and the reactor vessel [RV], reduces neutron induced, reactor vessel embrittlement. The thermal shield is cylindrical, approximately 10 feet in height and about 2.5 inches thick. The thermal shield is supported at the bottom by six support blocks and a system of dowel pins and bolts. The shield is supported at the top by six flexures and four displacement limiting keys. The flexures are designed to provide tangential and radial restraint of the thermal shield and the core barrel. Five of the six flexures have been known to be failed since 1978 (further historical information has been submitted by item d of Section G, subsection 4, Supportive Documentation). The four displacement limiting keys are located approximately 9.5 inches below the top of the thermal shield and initially limit the relative radial motion between the thermal shield and the core barrel.

The six lower support blocks are located every 60 degrees around the thermal shield. Each support block is fastened to the core barrel by two long bolts, three short bolts and two dowel pins. The thermal shield is fastened to the support block by the two long bolts and two additional dowel pins. The bolt holes travel continuously through the core barrel, permitting the threaded end of the bolts to protrude from the core barrel surface opposite the thermal shield.

As this condition underwent an extensive review by the NRC staff, there exists a substantial amount of documented technical information which has previously been provided to the NRC. This information may be found in the documents listed in Section G, Additional Information.

#### C. DESCRIPTION OF THE EVENT:

1. Event:

On 1/8/89, with Unit 1 in Mode 6 for the Cycle 10 refueling outage, after performing a remote video camera inspection of the thermal shield support system, it was revealed that three thermal shield support block bolts were out of tolerance. Three bolts, two on one support block and one on another support block, were protruding from the inner surface of the core barrel by an amount that exceeded the normal, original assembly, tolerance.

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	2.	Inoperable Structures, S Event:	ystems or Components	that Contributed	to the
		Five of the six upper fl since 1978. These failu resulted from the cause	exure supports are kn res may have contribu of the lower support	nown to have been ated to or may hav block bolt protro	failed ve usion.
	3.	Sequence of Events:			
		Not applicable.	,		
	4.	Method of Discovery:			
		In response to an alert fasteners at another fac (utility, nonlicensed) i supports using a remote	from the reactor vend ility had been found nspected the accessib video camera.	dor that thermal s degraded, engined ole thermal shield	shield ers 1
	5.	Personnel Actions and An	alysis of Actions:		
		Not applicable.			
	6.	Safety System Responses:			
		Not applicable.			
D.	CAUSE	OF THE EVENT:			
	1.	Immediate Cause:			
		The three bolts protrudi are postulated to have f thermal shield toward th of the failure is believ Reactor coolant flows in perpendicular to the the is directed parallel to vessel and shield, and t	ng from the inner sur ailed and traveled in the center of the react red to be high-cycle of the the reactor vesse the longitudinal axis then redirected at the	rface of the core nward, away from a tor vessel. The of flow induced vibra above and inal axis. The co s and down between a bottom of the ve	barrel the cause ation. polant n the assel

up to the core. As a result of the flow redirection and velocity, turbulence is created which is characterized by local pressure variations. The pressure variations induce vibrational displacement

forces on the thermal shield.

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## 2. Intermediate Cause:

The vibrational forces combined with differential thermal movement between the thermal shield and the core barrel caused excessive wear of the displacement limiting keys and failure of five flexures. In this degraded condition, the thermal shield natural frequency shifted to a range that is more susceptible to turbulence excitation forces. As a result, the high-cycle fatigue limit of the support block bolts was exceeded.

In support of conclusions resulting from this cause determination, similar flexures at another facility were determined to have failed early in life during hot functional testing due to flow induced high-cycle fatigue. The symptoms of the degradation were similar to those found here. However, the time to failure at San Onofre Unit 1 is much longer. Four of the six flexures were inspected in 1971 and 1972 (at approximately 4.1 EFPY) and found to be intact (two flexures could not be inspected). In 1976 (at approximately 7.3 EFPY), all six flexures were inspected; two of the flexures were found to have failed since the 1972 inspection, and two of the flexures, which could not be inspected in 1971 and 1972, were found to have failed (i.e., their failure could have occured anytime between 1967 and the 1976 inspection). In 1978 (at approximately 8 EFPY), an additional flexure was observed to have failed. The difference in the operating time to failure, between Unit 1 and the other facility, is consistent with the high-cycle fatigue analysis when several factors are considered:

- a) The displacement limiting keys at the other facility restrained less radial movement than those at Unit 1. Thus, additional radial displacement was permitted at the other facility.
- b) The flow velocity at the other facility was greater than at Unit 1. Thus, larger local pressure variations caused higher vibrational forces at the other facility.
- 3. Root Cause:

Our root cause investigation is continuing and will draw upon data obtained from the retrieval of the bolts and subsequent metallurgical analysis. At this time it is believed that the root cause of the bolt failure is inadequate appraisal of the effects that flow induced vibration have on support bolt loading.

### E. CORRECTIVE ACTIONS:

1. Corrective Actions Taken:

a. All accessible support features have been inspected by remote video camera.

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- b. The bottom of the reactor vessel has been inspected and no broken bolts or dowel pins were found.
- c. Engineering analysis has been performed to verify that continued operation through fuel Cycle 10 would not lead to catastrophic support failure and would not lead to further significant degradation of the supports. Also, analysis has shown that significant loose parts, leading to flow blockage, would not be generated; and that increased vibration due to loose parts, further key wear or bolt failure could be monitored.
- d. A conceptual design and plan for restoring the thermal shield supports was submitted to the NRC October 6, 1989.
- 2. Planned Corrective Actions:

License Amendment Number 127 provides for a thermal shield monitoring program which has been implemented. The monitoring program will be continued until the thermal shield fasteners are restored to their designed functional condition during the 10-year ASME Inservice Inspection planned for the fuel Cycle-11 refueling outage which is scheduled to begin by June 30, 1990.

F. SAFETY SIGNIFICANCE OF THE EVENT:

There is no safety significance to this occurrence since the thermal shield continues to be adequately supported and degradation of the support system has not resulted in loose parts which may obstruct cooling flow to the core.

- G. ADDITIONAL INFORMATION:
  - 1. Component Failure Information:

The three bolts which are postulated to have failed were supplied by Westinghouse Electric Corporation of ASTM A193, Type B8M (316) stainless steel. One bolt is 2.75 inches long by 0.75 inches diameter. The other two bolts were 5 inches long by 0.875 inches diameter.

2. Previous LERs for Similar Events:

None.

3. Results of NPRDS Search:

Not applicable.

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# 4. Supportive Documentation:

Significant information has been submitted to the NRC in support of the observations, analyses, conclusions, and corrective actions related to this occurrence. This LER serves as a summary of this information pursuant to regulatory reporting requirements. A list of these documents follows:

- Letter, H. E. Morgan (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, 30-Day Report, Licensee Event Report No. 89-001, San Onofre Nuclear Generating Station, Unit 1, dated January 23, 1989. Enclosure: LER 89-001, Reactor Vessel Thermal Shield Support Block Bolts Out Of Tolerance.
- b. Viewgraphs, Southern California Edison and Westinghouse Electric presented to NRC staff, Subject: Technical Presentation on Issues Related to Degraded Fasteners for Thermal Shield Support Blocks at San Onofre Unit 1, dated January 27, 1989.
- c. Letter, Charles M. Trammell (NRC) to Kenneth P. Baskin (SCE), Subject: Summary of Meeting Held on January 27, 1989, RE: Broken Bolts Found in Reactor Vessel Thermal Shield, dated February 8, 1989.
- d. Letter, Kenneth P. Baskin (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Amendment Application No. 165, San Onofre Nuclear Generating Station, Unit 1, dated February, 17 1989.
- e. Letter, F. R. Nandy (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Response on Issues Related to Degraded Fasteners for Thermal Shield Support Blocks, San Onofre Nuclear Generating Station, Unit 1, dated March 21, 1989.
- f. Letter, F. R. Nandy (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Response To Thermal Shield Questions, San Onofre Nuclear Generating Station, Unit 1, dated March 23, 1989.
- g. Letter, Kenneth P. Baskin (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Supplement 1 to Amendment Application No. 165, San Onofre Nuclear Generating Station, Unit 1, dated May, 3, 1989.
- h. Letter, Kenneth P. Baskin (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Revision to Supplement 1 to Amendment Application No. 165, San Onofre Nuclear Generating Station, Unit 1, dated May 8, 1989.

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 Letter, Charles M. Trammell (NRC) to Kenneth P. Baskin (SCE), Subject: Issuance of Amendment No. 127 to Provisional License, San Onofre Nuclear Generating Station, Unit No. 1 (TAC No. 71853), dated May 15, 1989.

j. Letter, F. R. Nandy (SCE) to U. S. Nuclear Regulatory Commission, Subject: Docket No. 50-206, Thermal Shield Conceptual Design and Repair Plan, San Onofre Nuclear Generating Station, Unit 1, dated October 6, 1989.