ADDENDUM 1 TO REPORT ON

SOIL BACKFILL CONDITIONS

SAN ONOFRE NUCLEAR GENERATING STATION

UNIT 1

JULY 12, 1983

ADDENDUM 1 TO REPORT ON SOIL BACKFILL CONDITIONS

This addendum provides additional information regarding the insitu backfill soil conditions which was not included in Chapters 1 to 3 and the appendices of the report on this matter. Specifically, this addendum provides (1) additional results of soil density tests and observations of footing conditions made at the site; 2) a discussion of the use of 85 percent relative compaction as a minimum average at the site.

Additional Test Data and Observations

The results of additional tests made in the backfill at the site are given in Table 1. The additional data are in the south extension of the Turbine Building and outside area pipe trench excavations. In addition, the following observations have been made:

- a) In reviewing the results of the tests given in Table 1, it was noted that soil backfill exposed in the Footing F excavation in the south extension of the Turbine Building shows several tests in the range of 81 to 87 percent relative compaction. The excavations also revealed the remnant of an old dewatering well (loose soil and gravel pack), the location of which is in general agreement with the construction photographs of the site. Some of the tests are low due to their proximity to the dewatering well backfill. Based on these test results and an inspection of the footing excavation, the soil characterization in this area has been modified locally from Category B to Category D soil fill. This change is reflected in the attached revised Figure 2-22.
- b) Review of additional observations made in December 1980 for the foundation for the dog house structure north of the Ventilation Equipment Building showed that the backfill beneath the west wall of the Ventilation Equipment Building is less than what was previously indicated in Section 2 of the report.

It should be noted that the above data are not reflected in the figures in sections 2 and 3 and the appendices of the Soil Backfill Conditions report. However, they are considered in section 4 and 5 of the report and in this addendum.

Discussion of 85 Percent Relative Compaction Charactarization

A density of 85 percent average relative compaction was used to characterize Category D fills as well as deep/narrow portions of Category B and C fills as shown in Figure 2-22. The relative compaction of the fill is an important parameter which is used as basic input to the evaluation of seismically induced settlements. Case histories indicate that the amount of seismically induced settlement for a sandy soil deposit can be calculated using the average density of the deposit.

The selection of the average value in this case was based on inspection of density test results for fill soils. For such fills a mean value of relative compaction for all tests on fills is about 89 percent with a standard

deviation of 5 to 6 percent. These observations represent all categories of Perhaps the most representative area to evaluate the average density of deep narrow fills is the backfill which was tested adjacent to the east side of the Fuel Storage Building. In that area, 11 tests were made in backfill between elevation +5 feet and +13 feet. These tests showed a mean relative compaction of between 85 and 86 percent and a standard deviation of 4 percent. It was not possible to obtain test results below elevation +5 feet in this area due to the congested nature of the excavation below that To evaluate the effect of elevation on relative compaction, the 175 tests taken on backfill between elevation 0 and 20 were statistically analyzed at 2-foot intervals. These tests were selected from density tests documented in Table B-1 of the soil conditions report and Table 1 of this addendum. It is noted that only those tests representing existing backfill were utilized. The calculated mean and mean minus one standard deviation of the available data are plotted in Figure 1 along with all data points for each interval. Also shown for reference is the mean and mean minus one standard deviation for all tests in the depth range.

As shown by Figure 1, the overall mean and mean minus one standard deviation are about 89 and 83 to 84 percent relative compaction, respectively. The corresponding two-foot interval results and the distribution of data points show no specific trend with elevation. Further, as shown in Figure 1, 85 percent relative compaction corresponds to 50 percent relative density while 80 percent relative compaction corresponds to 30 percent relative density. It is considered unlikely that a soil deposit could remain at 30 percent relative density areally in a location such as the SONGS site where vibrations due to the operation of the power plant equipment or construction equipment have been almost continuous for over 15 years. Based on the aforementioned observation, the results of the 11 tests obtained at the east end of the Fuel Storage Building and on the lack in trend of density with elevation shown in Figure 1, it is concluded that 85 percent relative compaction is the appropriate value for use in settlement calculations.



Job Name: SONGS 1

Field Data Sheet

Sheet No.: 19

Job Number: 41009K

SEISMIC	MODIFICATIONS	SHORT	TERM	OUTAGE	PROJECT

	Test Number	Retest by	Retest of	Number	Location o		1	Field Dry Density (pcf)	Moist.	Method	Max. Lab. (pcf)	Comp	Spec Reg.	Drawing No., Spec.	Qual Clas	
Jan 24	711		-	S12+85	Fill	M-N-8							Ī	See Plot		
Jan 24	/11	ļ		W4+99	Turbine Bldg.		- +14.5	97	4	s/	C 120	81	95	Plan	2	*
Jan 24	712			S12+94 W5+01	Fill	N-9	L				••				1	
	712			S12+79	Turbine Bldg.		+16.5	100	6	<u> </u>		83	**	. "	"	*
Jan 26	713			W4+93	Fill	M-8			_		,,					
	- /13	 		S12+99	Turbine Bldg. Fill		+11	98	5	<u> </u>		82	"	"	"	*
Feb 3	714			W4+93		N-8		00								
	717	<u> </u>	·	S11+71	Turbine Bldg. Fill		+16.	98	3	!"		81	"	"	"	
Feb 3	715			W5+42	Turbine Bldg.	Trench		1 100	. 🗖		•	-	.,			
				S11+84		Trench	+17.5	103	4		· · · · · ·	86		,,	•	*
Feb 3	716			W5+42	Turbine Bldg.		+17.5	' 104	5		••	86	.,		**	*
				S11+96	Backfill, E.		717.3	104		1		86	<u> </u>			
Feb 7	717			W5+72	Piping Trench		+11.5	' 115	9		**	96	,,			*
				S11+72	Backfill, N.	gide	- '11.5	113		╁		90			·	
Feb 7	718			W5+72	Piping Trench		+12'	115	9		••	96	11	11	99	•
				S12+72	Native	OVCICA	112	117	7			- 50	<u> </u>			
reb 8	719]		W5+72	Waste Oil Lin	e S.G.	+11'	120	5		**	100	••	••	**	4
				S13+36	Native	9.00				Н		100				
Feb 8	720			W5+71	Waste Oil Lin	e S.G.	+12'	120	4		•	100	11	**	••	*
				S13+40	Fill					Н		100				
Feb 9	721	726		W5+67	Waste Oil Lin	e S.G.	+12'	100	5			83		"	••	*
				S12+96	Native										· · · · · · · · · · · · · · · · · · ·	
Feb 11	722	•		W5+06	Turbine Bldg.	Ftg. "	" +16'	120	4	"	••	100	**	••	**	*
				S12+99	Native											
Feb 11	723			W4+97	Turbine Bldg.	Ftq. "	" +14.5	' 119	3	"		99	**		•	*
					Fill	M-8										
eb 11	724			W4+94	Turbine Bldg.	Ftg. "	+8.5	' 99	9	_"	**	82	19	10	11	*
					Native	_										
eb 15	725			W5+38	Waste Oil Lin	e S.G.	+14'	121	4		11	101	**	••	••	*

Class	1	&	2	Reviewed	By:	
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Job Name:

SONGS 1

Field Data Sheet

SEISMIC MODIFICATIONS SHORT TERM OUTAGE PROJECT

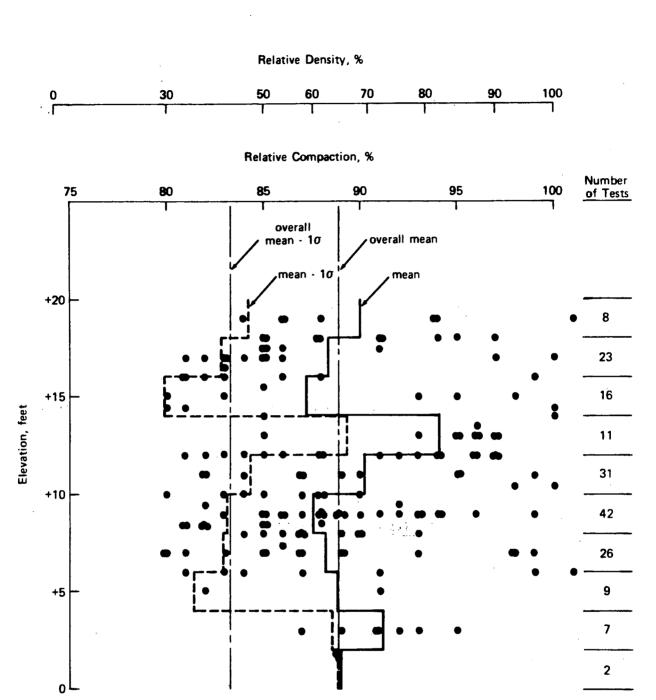
Sheet No.: 20

Job Number: 41009K

Dat		Test Number	Retest by	Retest of	Grid Number	Location of Test	Elev.	Field Dry Density (pcf)	Moist.	Method	Max. Lab. (pcf)	Comp	Spec Reg.	Drawing No., Spec.	Qual Clas	
		704			S13+39	Backfill								See Plot		
Feb 2	24	726	ļ		w5+68	Waste Oil Line S.G.	+12'	117	5	5/9	120	97	95	Plan	2	*2
		707]	I .	S12+77	Fill									ļ	
Feb 2	24	727			W5+03	Turbine Bldq. Ftg. "F	<u>" 8.5</u>	97	8	"	11	81	••		"	*2
		700		1	S12+98	Native									l	
Feb 2	26	728			W5+02	Turbine Bldg. Ftg. "F	<u>" +14.5</u>	120	4	"	11	100	**	11	-"-	*2
	_	700		I .	S12+61	Fill		i							i	
Mar	3	729				l" Eye Wash Line	+12'	109	7	"	**	91	01		-"-	*2
		700		B .	S12+52	Fill		ł								
Mar	3	730				l" Eye Wash Line	+12'	111	<u> 8 </u>	"	11	93	**	"	"	*2
		=				Fill, Drain Line						İ	j			
Mar	3	731			W4+90	Turbine Bldg. Ftg. "F	<u>" +17'</u>	100	6	"	11	83	"	"	-"-	*2
				I .	S12+90	Backfill										
Mar	7	732	733		W5+72	Oil Waste Line	+13'	110	6	"	**	92	**			*2
					512+93	Backfill				į '		1		I		
Mar	7	733				Oil Waste Line	+13'	114	8	"	11	95	10	"		*2
	_			1	513+42	Backfill		·				[İ	Į.		
Mar	8	734			w5+55_	Oil Waste Line	+15'	118	10	"	••	98	"	"	"	*2
				1	513+37	Backfill						İ		1	1	
Mar	8	735				Level Indicator Line	+19'	117	88	"	in .	98_	85	"		*2
			İ		513+13	Backfill			1			į	ľ			
Mar	9	736	}		w5+03	Level Indicator Line	+19'	113	7	"	11	94		"	- "	*2
_			1		512+87	Backfill				[]						
Mar 1	11	737	739		W3+18	Sewer Line Lateral	+18'	111	7	"	11	92	95	11	"	*2
			1		511+95	Backfill		ŀ				}			į	
Mar]	11	738	<u> </u>		W1+78	Sewer Line Lateral	+22'	116	9	"	**	97		"		*2
			i		512+87	Backfill			ļ					1		
Mar	11	739	ļ	737	W3+18	Sewer Line Lateral	+18'	115	9	-	**	_96_	. **	"	"	*2
Rema	ark	cs:*2 "	Cest requ	rested by	Pechtel		:··		4 .,				L	<u> </u>		

Remarks: *2 Test requested by Bechtel	
	•

Class	1	&	2	Reviewed	By:	
Class	3	&	4	Reviewed	Ву:	



Total Number of Tests = 175

LEGEND

Measured density

Project: SEISMIC RE-EVALUATION
Project No. 413521

SUMMARY OF PERCENT RELATIVE COMPACTION AS A FUNCTION OF ELEVATION

Fig.