

1985 RE-EVALUATION

OF

STEAM GENERATOR INSPECTION INTERVAL

SAN ONOFRE NUCLEAR GENERATING STATION

UNIT 1

MARCH 1985

SOUTHERN CALIFORNIA EDISON COMPANY

ANA, Inc.

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1. Introduction

On September 4, 1984, the San Onofre Unit 1 Provisional Operating License (POL) DPR-13 was amended to revise Condition 3.E which requires that a steam generator inspection be performed within 6 equivalent full power months (EFPM) of operation from startup following the 1982 to 1984 backfit outage. The objective of this required inspection is to monitor the condition of the non-sleeved steam generator tubes at San Onofre Unit 1. The time interval for this interim inspection was based upon assigning to the non-sleeved tubes the conservatively estimated intergranular attack (IGA) degradation rate of 15% per year of operation. This previously established 15% per year degradation rate was based on comparison of historical eddy current data from tubes that were within active regions of steam generator A and were also sleeved during the 1980 Sleeving Repair Project. The purpose of this report is to provide information upon which to establish a revised degradation rate applicable to non-sleeved tubes which more appropriately reflects the rate of progression of IGA among these tubes. The appropriate interval between inspections can then be established, based upon this revised degradation rate.

The revised degradation rate was determined based upon a review of historical eddy current examination data for non-sleeved tubes. Using this data, signals at the top of the tubesheet that are indicative of IGA were re-evaluated. The characteristics of eddy current signals in these non-sleeved tubes, over several inspection intervals, were then compared and contrasted with

signals over similar inspection intervals in sleeved tubes which are known to have undergone active degradation due to IGA. From such a comparison, an assessment of IGA progression rate was made for the relatively inactive regions and a revised value for non-sleeved tube degradation rate was established.

Such an assessment relies a) on the capability of eddy current techniques to detect IGA as found at San Onofre Unit 1, and b) on the ability to correlate the threshold of detectability with IGA depth of penetration. To this end, the in-situ eddy current responses of tubes, subsequently pulled from steam generators A and C during the 1980 Sleeving Repair Project, were re-evaluated and compared to the metallurgical results as reported in the 1981 Return to Power Report (Reference 1).

Verification of the assessment of IGA progression in non-sleeved tubes is obtained through the results of eddy current examinations conducted in 1982, following approximately 4.3 EFPM of operation (see Reference 2), and in 1984, following an extended shutdown to perform plant modifications.

Assurance of the continuing validity of the assigned value of degradation rate is supported by a review of the steam generator water chemistry history and controls subsequent to the 1980 Sleeving Repair Project. This review indicates that conditions which could accelerate IGA progression in non-sleeved tubes are unlikely to occur.

Section 2 of this report contains relevant background information on plant operating history, steam generator water chemistry,

eddy current examinations, and the 1980 Sleeving Repair Project. This Section also presents the methodology used to re-evaluate the steam generator inspection interval.

Section 3 contains information that confirms the detectability of IGA at San Onofre Unit 1.

Section 4 contains the assessment of IGA progression rate based on review and comparison of eddy current data over a number of inspection intervals for both non-sleeved and sleeved tubes.

Section 5 presents the conclusions in regard to the assessment of IGA progression rate in non-sleeved tubes, discusses the development of a revised degradation rate (10% per 15 EFPM) for the non-sleeved tubes, and presents the proposed interval for future inspections at San Onofre Unit 1.

Section 6 contains the list of references cited in this report.

2. Background and Re-evaluation Methodology

a. General

During the 1980-81 Sleeving Repair Project, it was established that IGA had occurred at the top of the tubesheet in the hot legs of San Onofre Unit 1 steam generators A, B, and C. The regions of aggressive attack were identified by eddy current testing and were corroborated by metallurgical examination of pulled tubes. Although the affected regions of all three steam generators were similar, steam generator A recorded the largest number of quantifiable eddy current indications, followed by C and then B which had the least number of affected tubes.

Figure 2-1 shows the distribution in steam generator A of quantifiable indications based on multi-frequency, differential bobbin coil data collected in 1980 prior to sleeving. The location of affected tubes is similar among the three steam generators. Figure 2-2 shows the locations of tubes which were removed from S/G's A and C for examination and the corresponding maximum depths of IGA penetration as determined by metallography.

Using eddy current test data and results of metallurgical examinations of pulled tubes to identify the active regions of IGA within each steam generator, boundaries were then formulated which encompassed these regions and all tubes within the boundary for each steam generator were sleeved. Figure 2-1 also shows the sleeving boundary for S/G A which is representative of the boundaries for all three S/G's. The regions outside the sleeving boundaries contain non-sleeved tubes. These tubes were

not sleeved because analysis of eddy current data collected during the sleeving project yielded no quantifiable indications of IGA at the top the tubesheet.

The conditions for return to power of San Onofre Unit 1 following the 1980 Sleeving Repair Project are set forth in Section 3 of the April, 1981 Return to Power Report (Reference 1). The limiting condition of a 6 EFPM operating interval was based on the 15% per year degradation rate which was conservatively applied to the non-sleeved tubes.

In summary, a rate of 15% per year was assumed to apply to these tubes with the added assumption that the depth of IGA penetration could be up to 40% before becoming detectable by eddy current techniques. Under these assumptions, an operating interval of 6 EFPM would limit non-sleeved tube degradation to less than 48% at the first inspection following post-sleeving return to power. This degradation level would, in turn, be less than the plugging limit of 50% for non-sleeved tubes.

The assumed degradation rate for non-sleeved tubes is characterized as being conservative in the 1981 Return to Power Report since (1) the rate was derived from tubes inside the sleeving boundary having quantifiable, unambiguous eddy current indications of IGA and (2) the time frame over which IGA was assumed to have progressed from threshold detection levels to quantifiable depth was conservatively limited to the period 1976 to 1980. Additional information on the basis for the currently assumed degradation rate is contained in Section 2.b below.

The assumption that non-sleeved peripheral tubes have IGA depths near the detectability level of 40% is also a conservatism in the formulation of the operating interval. Eddy current examination results from the 1982 and 1984 steam generator inspections indicate, further, that this assumption, when considered with an assumed degradation rate of 15% per year, is overly conservative. These inspections showed negligible progression of IGA in the non-sleeved tubes following approximately 4.3 EFPM of operation and 26 months in lay-up conditions. Were the 15% degradation rate applicable to non-sleeved tubes and were the depth of IGA at the 40% level at the time of the sleeving project, then evidence of progression of IGA in non-sleeved tubes would have been evident in the eddy current examination data. Additional information on the scope and findings of the 1982 and 1984 inspections is provided in Section 2.c below.

The apparent lack of significant progression of IGA in non-sleeved tubes is supported by the improvement in steam generator water chemistry specifications which have been in place since the sleeving repairs were implemented. An overview of steam generator chemistry prior to and subsequent to the sleeving repair project is given in Section 2.d below.

The above considerations provided the incentive to re-evaluate the degradation rate in non-sleeved tubes for the purpose of establishing a more appropriate operating interval between steam generator inspections. Accordingly, a re-evaluation

of the non-sleeved tube degradation rate and steam generator interval was performed as outlined in Section 2.e below.

b. Basis for 1981 Degradation Rate

The degradation rate applied to non-sleeved tubes prior to return to power in 1981 was developed based on the eddy current responses of 39 tubes in S/G A, located in active regions within the sleeving boundary. The locations of these tubes are shown on Figure 2-1. The reference data base was the 1980 multi-frequency, differential bobbin coil data. Section 3.1 of the 1981 Return to Power report describes the methodology used in deriving the 1981 degradation rate for these tubes. In connection with preparation of this 1985 report, the 1980 and prior eddy current data on these tubes were independently reviewed. Appendix A contains representative signatures from among the 39 tubes having the most complete examination histories. It is apparent from these signatures that the 39 tubes are within areas which have experienced active, significant degradation over time. No tube in the group exhibits a normal tube sheet entry signal throughout its inspection history which, in many cases, dates back to 1973. Many tubes in the active regions surrounding the 39 tubes exhibit the same characteristics.

In comparing the eddy current signatures of the 39 tubes from one inspection to the next, it does not appear that the rate of degradation during any one interval is significantly different than during another interval. In an attempt to

verify this qualitative judgement, phase angles and corresponding depths were assigned as appropriate to all available signatures at the top of the tube sheet from the 39 tubes. In those cases where it was inappropriate to assign phase angles, but the signal was distorted, a depth of 40% was assigned as being representative of the threshold of detectability of volumetric IGA. The results are presented in Table 2-1. The trends on a tube by tube basis are generally consistent with the view that a degradation process commenced prior to 1973 and that degradation progressed through 1980. At low depths of penetration, however, there is considerable scatter in the re-evaluated data which makes reliable estimation of degradation rates based on group statistics for early inspection intervals uncertain. Among the factors which contribute to this uncertainty are the following:

- (1) Denting in combination with thinning at the top of the tubesheet act to distort and oppose the formation of the flaw response of the differential coil at lower depths of IGA. The typical effect is to foreshorten and/or distort the upper lobe of the differential response, creating uncertainty in assignment of the proper phase angle.
- (2) The use of 400 kHz as the test frequency for .055" wall thickness Inconel 600 tubing results in low depth flaws being rotated more toward the horizontal plane and increases the masking effect of noise and dents on the coil response to IGA.

Notwithstanding the problem of reliable quantification at the lower depths of IGA, it is evident that for tubes in the active regions, IGA progresses at a significant rate, is detected in earlier inspections, and significantly alters the eddy current coil response in subsequent years.

c. 1982 and 84 Inspection Results

In 1982 following approximately 4.3 EFPM of operation after the 1981 Sleaving Repair Project, a comprehensive eddy current examination of sleeved and non-sleeved tubes was performed in all three steam generators. In the non-sleeved region, tubes were examined with both the 4x4 and bobbin coil probes. A total of 1212 tubes in all three steam generators were examined consistent with the pattern for steam generator A in Figure 2-3. The results were reported in the 1982 Return to Power Report and showed negligible change in progression of IGA in non-sleeved tubes. The seven tubes in S/G C and one tube in S/G A which showed evidence of minor change were located at the sleaving boundary near previously defined active regions. Moreover, the depth of IGA penetration was not such that the differential bobbin response was quantifiable.

In April of 1984, following approximately 26 months in lay-up conditions, the steam generators were again inspected in preparation for return to power scheduled for later 1984. Steam generator A was selected for inspection and both sleeved and non-sleeved tubes were eddy current examined. Approximately 226 non-sleeved tubes adjacent to the sleaving bondary were

examined using the 4x4 probe in accordance with the inspection pattern shown in Figure 2-4. Results showed no evidence of IGA progression.

d. Overview of Steam Generator Water Chemistry

(1) Pre-Sleeving History

San Onofre Unit 1 has operated on phosphate chemistry since initial operation in 1968 except for a period of approximately four months from December 1970 until April 1971 during which time volatile treatment was attempted. Due to hideout return and condenser leakage, excessive blowdown was required in order to maintain proper chemistry and, therefore, phosphate treatment was resumed. The chemistry history from that time up to the 1980 sleeving repair outage is discussed in Appendix A of the 1981 Return to Power Report (Reference 1).

(2) Post-Sleeving History

On June 17, 1981, the Unit 1 returned to service following the steam generator sleeving repair. A revised chemistry program was followed. This program included (a) a cold soak, (b) a hot soak, (c) new chemistry control parameters during heat-up, and (d) new chemistry control parameters during power escalation and steady state operation.

During the ensuing 4.3 EFPM of operation, there were three occasions in which the secondary water chloride limit of 0.5 ppm was exceeded. On one occasion, the chloride level

exceeded 5 ppm due to a condenser leak and the unit load was reduced to 30% to limit chloride hideout. The condenser was repaired and normal chloride levels restored within fourteen hours using blowdown. The other two occasions involved lesser chloride excursions of shorter duration without need for load reduction.

Phosphate concentrations during the 4.3 EFPM operating interval were out of specification on four occasions. At no time did this condition persist more than four hours. The proper phosphate concentrations were restored by blowdown and/or chemical feed.

On February 27, 1982, Unit 1 was shut down for a scheduled steam generator sleeving repair inspection. During the 4.3 EFPM of operation, it is considered that overall steam generator chemistry was significantly improved in comparison to pre-1981 operating history.

From February 27, 1982 through November 27, 1984, the steam generators were maintained in wet layup while in a Mode 5 extended cold shutdown. The secondary chemistry limits for this condition are specified as follows:

Phosphate	=<50 ppm
Chloride	=< 1 ppm
Na/PO4	1.0 - 3.0
pH	9.3 - 10.5
Hydrazine	50 - 150 ppm

Periodic drain and refill operations were necessary to

maintain these limits as sodium, phosphate and chloride leached from the sludge pile into solution. The need to drain and refill became less frequent as the outage progressed due to a decrease in the rate at which sodium, phosphate, and chloride entered into solution. Draindown was also required in order to perform steam generator secondary side inspections.

A nitrogen blanket was maintained on the steam generators during the outage to minimize oxygen ingress.

In November, 1984, Unit 1 was returned to service. Mode 1 steam generator chemistry limits are as follows:

Phosphate	15 - 30 ppm
Chloride	=< 500 ppb (typically < 100 ppb)
Na/PO4	2.3 - 2.6
pH	9.4 - 10.2

Also, continuous blowdown of approximately 1 % is being maintained to assist in steam generator chemistry control. Since the November, 1984 return to service, no primary to secondary leakage has been detected at Unit 1.

In early 1983, a new water chemistry procedure was implemented at Unit 1. The procedure, entitled "Unit 1 Steam Generator and Condensate/Feedwater Chemistry Control and Sampling Frequencies", defines normal and abnormal ranges of secondary water chemistry parameters and sampling frequencies for each of the plant operating modes, including lay-up periods. The administrative and management controls

of the procedure are consistent with the guidance of "PWR Secondary Water Chemistry Guidelines", EPRI Report NP-2704-SR dated October, 1982. The response to out of range parameters include mitigating actions, power reduction to 30% or less, and unit shutdown if site management determines that continued operation could adversely affect steam generator tube integrity. In all cases, site management is responsible for and has taken action to reduce power based upon the recommendations of the plant chemistry department.

e. Re-evaluation of Steam Generator Inspection Interval

The application to non-sleeved tubes of a degradation rate based on data from tubes in the active regions is judged to be overly conservative since (1) the non-sleeved tubes are in an "inactive" region, (2) the 1982 and 1984 inspection results confirm that there is no significant progression of IGA in non-sleeved tubes, and (3) current steam generator water chemistry controls provide assurance of continuing "inactivity". The practical consequence of applying this conservative rate is to require unscheduled unit shutdowns during the cycles of operation between refuelings. Approximately four weeks are needed to perform the evolution of cold shutdown, steam generator inspection, analysis of results, reporting of findings, and return to power. To the extent that such evolutions occur more frequently than necessary, otherwise avoidable plant operating costs and personnel radiation

exposure are incurred without benefit. Accordingly, a re-evaluation of the basis for the currently required steam generator inspection interval is warranted in order to justify an interval which more appropriately reflects the condition of the non-sleeved tubes and is adequately conservative, but is not overly restrictive.

The approach adopted in this re-evaluation relied on the existing eddy current data base to assess the rate of progression of IGA in non-sleeved tubes and to assign a degradation rate which reflects the actual rate of progression and at the same time is adequately conservative.

The reference inspection for assessing the progression of IGA is the 1980 inspection which lead to the sleeving repair effort. In that inspection, 100% of the tubes were inspected on the hot leg side below the fourth support in each steam generator using the multi-frequency bobbin coil. The test frequencies employed included 400 kHz, 340 kHz and 100 kHz differential and 100 kHz absolute.

In order to utilize the most extensive eddy current data base, steam generator A was selected for performing the assessment. The use of steam generator A in performing this assessment is justified on the basis that all three steam generators are performing in a like manner. Accordingly, the resultant, revised degradation rate can be applied to all three steam generators.

Inspections prior to 1980 were performed using single

frequency bobbin coil at 400 kHz differential. Therefore, for the purpose of comparative analysis of eddy current data, pre-1980 data is compared to the 400 kHz differential 1980 data. For comparison and evaluation of 1980 and subsequent inspection data, all channels of eddy current data are evaluated.

To confirm the capability of the bobbin coil to detect IGA as experienced at San Onofre Unit 1, the field eddy current data in 1980 for tubes pulled from S/G's A and C was compared to the metallurgical findings for these tubes. The detectability is measured by the depth of IGA above which there is reasonable assurance of obtaining a bobbin coil response.

A review of historical data for tubes in the active regions having discretely quantifiable, unambiguous eddy current signals in 1980 establishes the time frame over which conditions supporting IGA have been present. Tubes in the non-sleeved regions, which have at most a distorted signal indicative of IGA in 1980, can be assumed to have a depth of IGA penetration at or near the threshold of detectability. By assuming no IGA in these tubes at the start of the time frame established for tubes in the active regions, a conservative IGA degradation rate can be derived and assigned to the non-sleeved tubes.

The results of the 1982 and 1984 examinations provide confidence that the derived degradation rate is adequately

conservative. The improvements in steam generator chemistry procedures and controls implemented since sleeving provide assurance that conditions which could accelerate IGA progression in non-sleeved tubes have not occurred since 1981 and are unlikely to occur during future operation.

The sections which follow present the results of the re-evaluation effort based on the preceding approach and present the revised degradation rate established for non-sleeved tubes and the corresponding appropriate operating interval between steam generator inspections.

TABLE 2-1
RE-EVALUATION OF 1981 DEGRADATION RATE DATA

TUBE NO.		% DEPTH IN YEAR INSPECTED					
ROW	COL	80	79	77	76	75	73
28	23	74			61		
28	26	99		75	40		
30	28	98		92			
12	31	86					54
33	31	89		96			40
31	32	91		81		70	
32	32	96		66			
33	33	95					
33	34	93					40
33	35	91					81
13	40	96		89	65	40	
13	41	92	86	62		39	28
13	42	77	73	51		24	
12	43	77	67			46	
11	44	91	88			36	
38	44	77					
39	44	91					
10	45	87				90	
11	45	79	65			36	
39	45	80					
8	46	90					
9	46	79					
36	48	82					
37	55	83			70		
11	56						
36	56	86			29		
36	57	80	62		48		
11	58	94					
37	58	76			19		
28	70	98					55
24	71	95					
29	71	98		50			40
26	72	87		62			71
27	72	97		71			55
25	73	98		96			65
26	77	84					63
25	78	79					40
12	80	91		95			79
12	81	96		98			75
MEAN DEPTH OF TUBES RE-EVALUATED	=	88.2	73.5	77.4	47.4	47.6	56.1

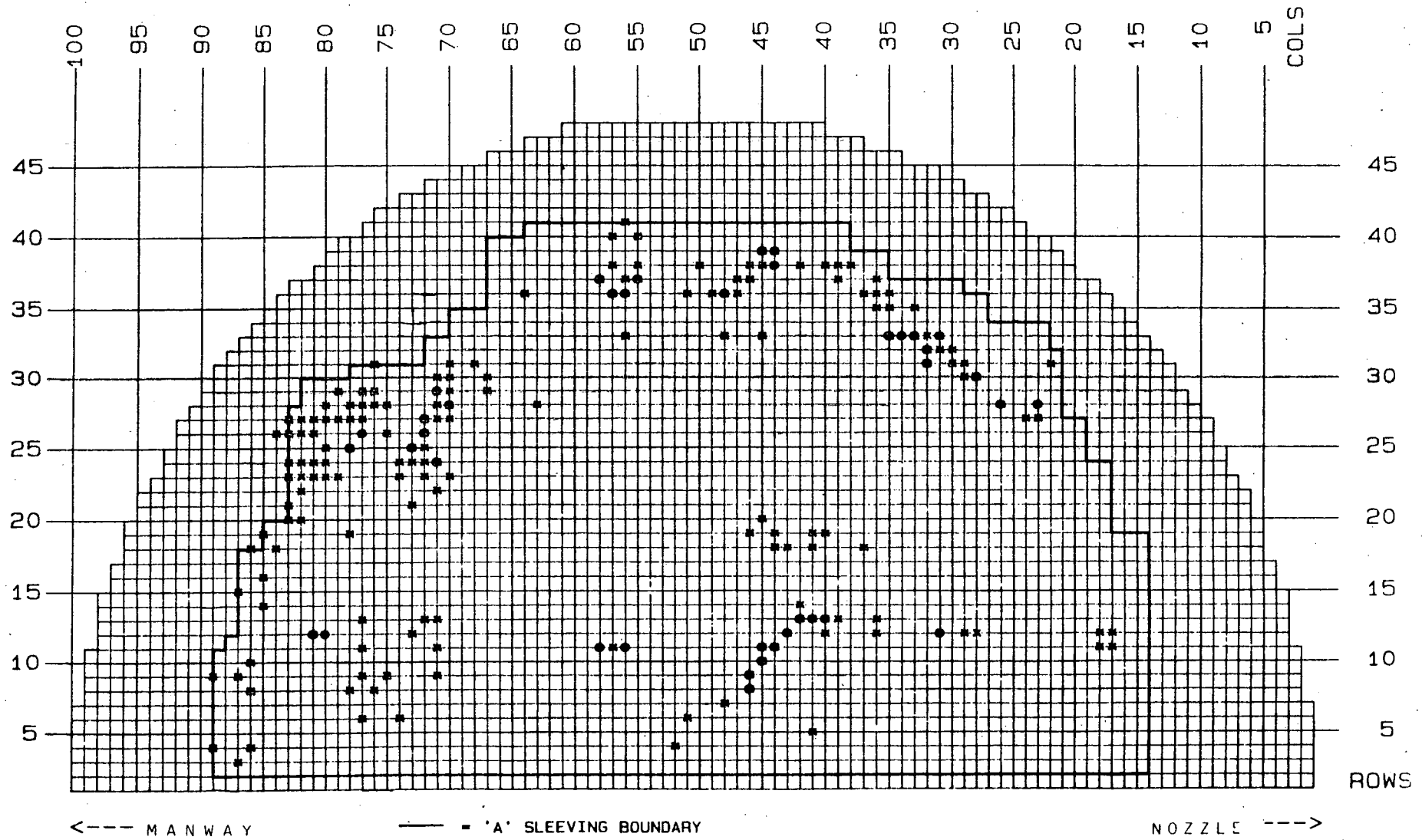
FIGURE 2-1

SAN ONOFRE UNIT 1 S/G 'A'

HOT LEG

ELEVATION: TUBESHEET

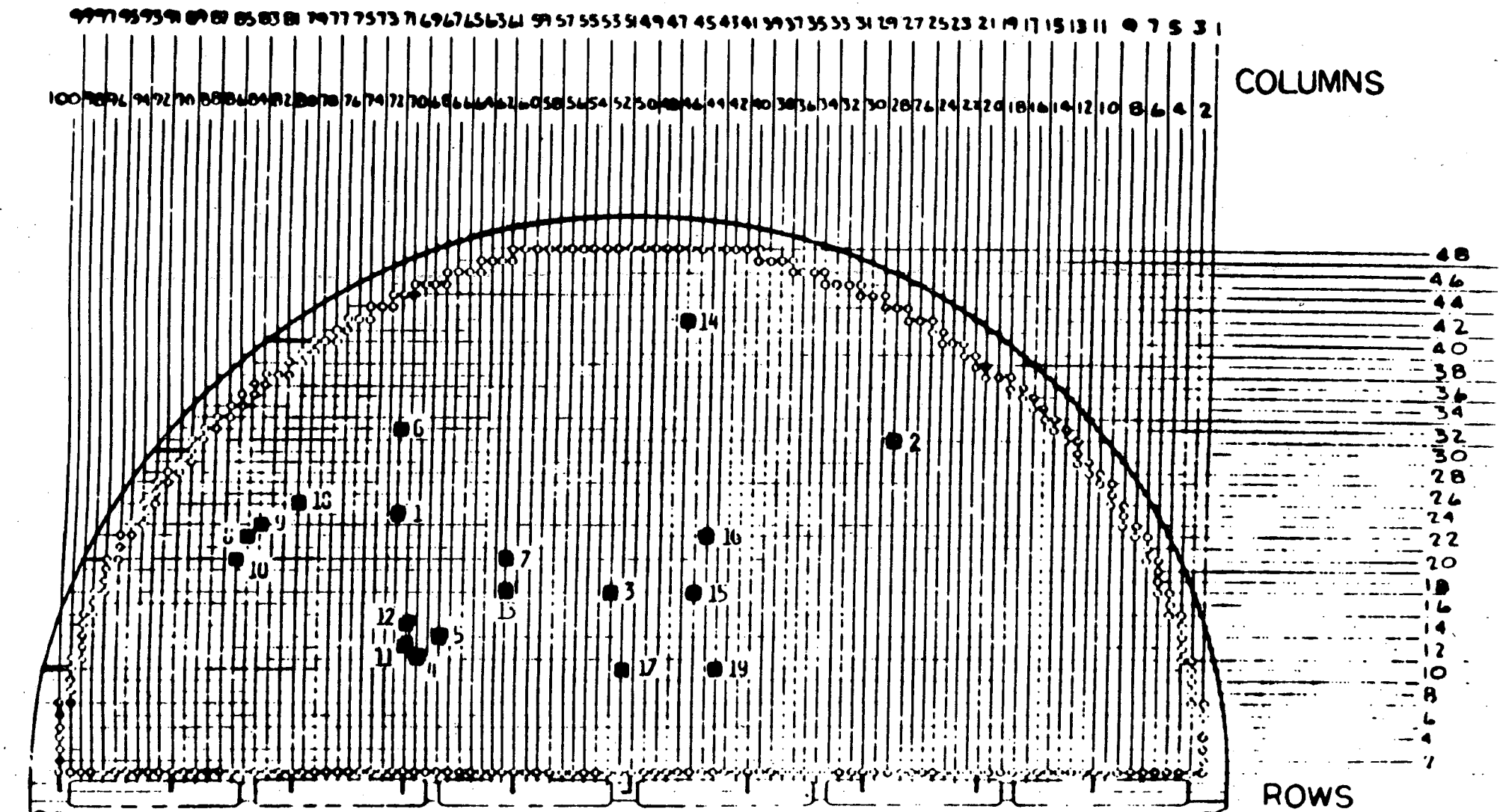
REPORT DATE: MARCH '85



x = '85 RE-EVALUATION: TUBES WITH IGA INDICATIONS

• = 39 TUBES USED TO ESTABLISH '81 IGA RATE

FIGURE 2-2



NOTE: SG(R-C)

- | | | | |
|------------------|------------------|------------------|----------------------------|
| 1. A(24-71) 95% | 6. C(32-71) 35% | 11. A(12-70) 50% | 16. C(22-44) 25% |
| 2. A(31-28) 90% | 7. A(20-60) 0 | 12. C(11-70) 30% | 17. C(10-51) NO METALLURGY |
| 3. A(17-52) 100% | 8. A(22-84) 20% | 13. A(17-61) 90% | 18. C(25-80) 40% |
| 4. C(11-69) 68% | 9. A(23-R3) 20% | 14. A(41-46) 17% | 19. C(10-43) NO METALLURGY |
| 5. C(13-67) 78% | 10. A(20-85) 80% | 15. C(17-45) 60% | |

Tubes Removed from San Onofre Steam Generators for Examination

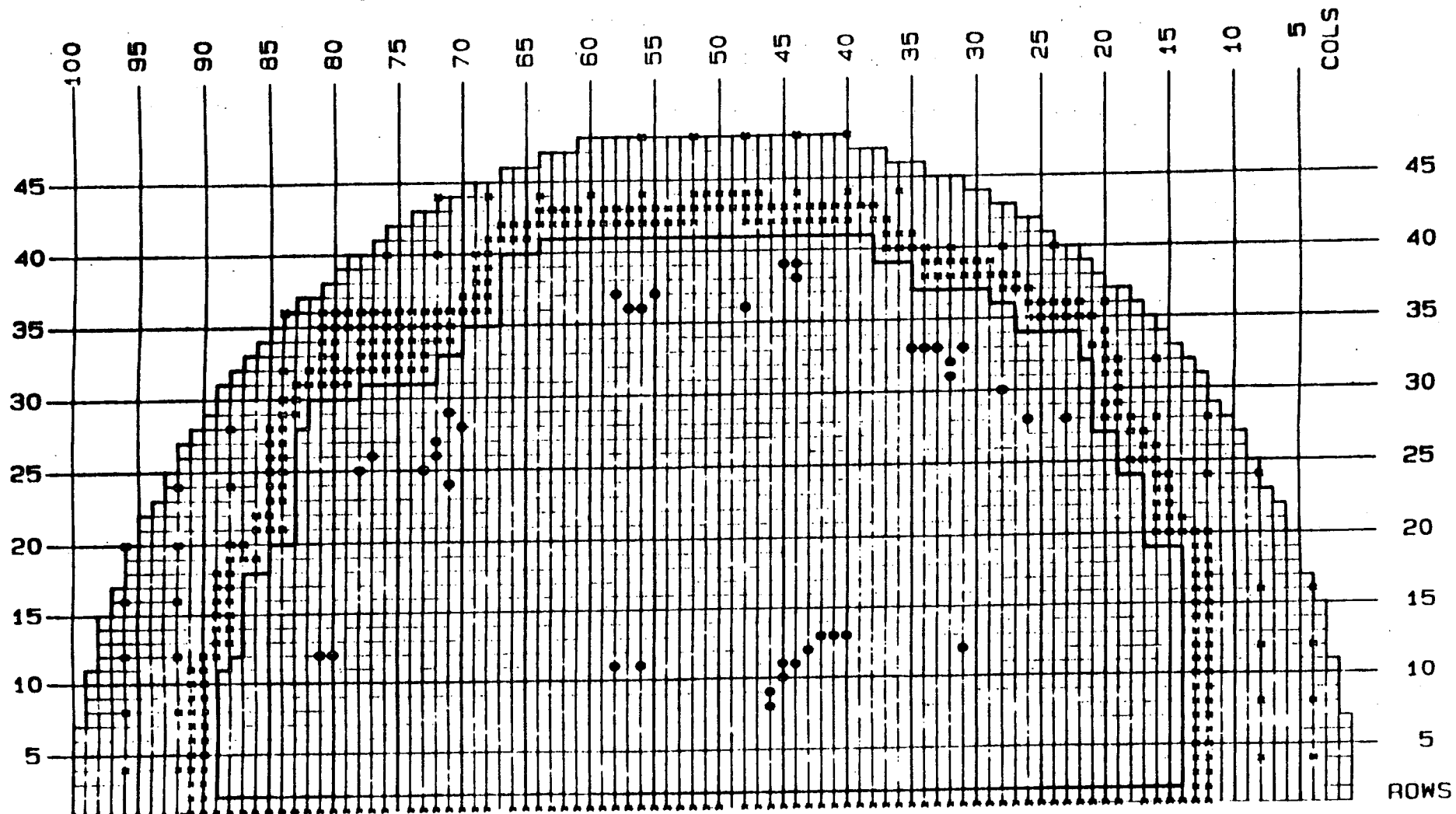
FIGURE 2-3

SAN ONOFRE UNIT 1 S/G A

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: FEB '85



<--- MANWAY

— = A SLEEVING BOUNDARY

NOZZLE --->

X = TUBES INSPECTED IN '82 AND RE-EVALUATED IN '85

● = TUBES USED TO ESTABLISH '81 IGA RATE

SCE-A HOT LEG 4X4 INSPECTION PROGRAM, APRIL 1984

20-APR-84 15:11:21

X = INSPECT THROUGH
TOP OF TUBESHEET
WITH 4X4 PROBE
TUBES TO INSPECT - 226

SERIES 27

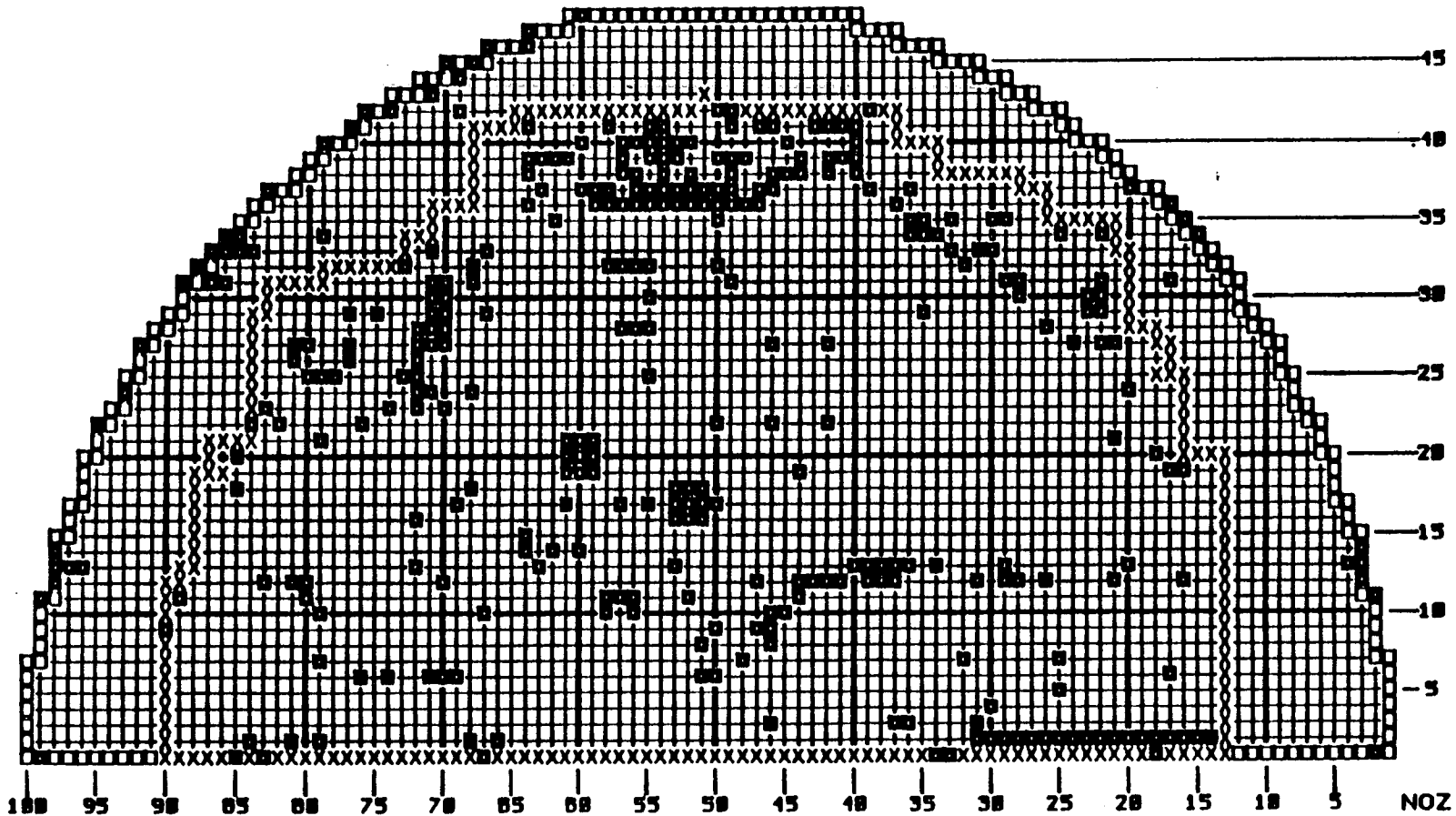


FIGURE 2-4

3. Correlation of Eddy Current and Pulled Tube Data

The purpose of this Section is to confirm the ability of the bobbin coil probe to detect the IGA which has occurred at San Onofre Unit 1. The methodology correlates the results of the 1980 pulled tube metallurgical examination with the re-evaluated field eddy current data.

Tube lengths were removed from hot leg sides of steam generators A and C during the Sleeving Repair Project. The field eddy current data collected from these tubes prior to removal have been re-evaluated and compared to the metallurgical examination results as reported in Table 2.2-7 of the 1981 Return to Power Report. Table 3-1 summarizes the results of this comparison. Appendix B contains computer printouts of the field eddy current responses for the pulled tubes.

The results show that in all cases the 100 kHz absolute bobbin coil detects the IGA condition reported by the metallurgical examination. The results further indicate that the 400 kHz differential bobbin exhibits a response to the IGA condition in the majority of cases where the metallurgical examination shows an IGA depth of >40%. An exception is Row 17 Col 45, for which there is essentially no response to the IGA which extends approximately 2 inches axially above the tube sheet. The lack of the differential coil response to this condition is explained by the similarity to a thinned condition. It is noted again that the 100 kHz absolute does respond to the IGA in Row 17 Col 45.

In summary, based on correlation of bobbin coil responses with pulled tube metallurgical examination results, it is concluded that the bobbin coil can detect IGA, as found at San Onofre Unit 1, at levels exceeding 20%. Specifically, the 400 kHz differential generally responds to IGA at levels in excess of 40% and the 100 kHz absolute detects IGA at levels exceeding 20%.

TABLE 3-1
RE-EVALUATION OF 1980 PULLED TUBE DATA

STEAM GEN'R	TUBE NO. ROW COL	PULLED CONDITION	1980 EVALUATION OF FIELD EDDY CURRENT	1985 RE-EVALUATION OF 1980 FIELD ECT DATA	1980 FRACTOGRAPHY AND METALLOGRAPHY
A	24 71	FRACTURED AT TTS	400 DIFF: 95% 100 ABS: ABNORMALITY NOTED	400 DIFF: 95% 100 ABS: 96%	95% CIRCUMFERENTIAL
A	31 28	FRACTURED AT TTS	400 DIFF: COMPLEX WITH DENT 100 ABS: ABNORMALITY NOTED	400 DIFF: 92% 100 ABS: 92%	90% CIRCUMFERENTIAL
A	17 52	INTACT	400 DIFF: 95% 4" BELOW TTS 100 ABS: 95% 4" BELOW TTS	400 DIFF: 95% 4" BELOW TTS 100 ABS: 48%	100% 3-4" BELOW TTS 50% 6" BELOW TTS
A	12 70	FRACTURED AT TTS	400 DIFF: DTS/DENT 100 ABS: ABNORMALITY NOTED RPC: <40%	400 DIFF: 31% 100 ABS: 34%	50% MAX
A	41 46 (COLD LEG)	INTACT	400 DIFF: DTS 100 ABS: ABNORMALITY NOTED RPC: INDICATION	400 DIFF: DTS 100 ABS: ABNORMAL INDICATION	THINNING MAX 17%
A	22 84	INTACT	400 DIFF: SMALL DENT DTS 100 ABS: OK RPC: OK	400 DIFF: DENT WITH DTS 100 ABS: 22%	20% MAX AT TTS
A	23 83	INTACT	400 DIFF: DENT/DTS 100 ABS: OK RPC: ABNORMALITY	400 DIFF: 21% 100 ABS: 20%	20% MAX IN 90 MIL BAND AT TTS
A	17 61	INTACT	400 DIFF: SMALL DENT DTS 100 ABS: ABNORMALITY NOTED RPC: SMALL INDICATION	400 DIFF: 91% 100 ABS: 91%	90% BASED ON VISUAL
A	20 85	FRACTURED AT TTS	400 DIFF: DENT 100 ABS: DENT RPC: 38%	400 DIFF: DIST'D DENT AND TUBESHEET 100 ABS: 52%	80% MAX

TABLE 3-1
RE-EVALUATION OF 1980 PULLED TUBE DATA

STEAM GEN'R	TUBE NO. ROW COL	PULLED CONDITION	1980 EVALUATION OF FIELD EDDY CURRENT	1985 RE-EVALUATION OF 1980 FIELD ECT DATA	1990 FRACTOGRAPHY AND METALLOGRAPHY
C	11 69	FRACTURED AT TTS	400 DIFF: LARGE DENT 100 ABS: DENT RPC: INDICATIONS	400 DIFF: DENT 100 ABS: 50%	>60% FOR 180 DEG 68% MAX
C	13 67	FRACTURED AT TTS	400 DIFF: DTS 100 ABS: ABNORMALITY NOTED RPC: INDICATIONS	400 DIFF: DIST'D DENT 100 ABS: 75%	>60% FOR 250 DEG 78% MAX
C	14 70	INTACT	400 DIFF: OK 100 ABS: OK RPC: INDICATIONS	400 DIFF: OK 100 ABS: <20%	30% MAX IN 40 MIL BAND
C	32 71	FRACTURED AT TTS	400 DIFF: DENT 100 ABS: SMALL DENT RPC: INDICATIONS	400 DIFF: DENT 100 ABS: 49%	35% AT AND BELOW FRACTURE
C	22 44	INTACT	400 DIFF: DTS 100 ABS: ABNORMALITY NOTED RPC: NO INDICATIONS	400 DIFF: DTS 100 ABS: 19%	25% MAX FOR 60 MILS
C	17 45	INTACT	400 DIFF: OK 100 ABS: OK RPC: NO INDICATIONS	400 DIFF: OK 100 ABS: 51%	GENERAL IGA FOR 2" ATS 60% MAX 1" ATS
C	25 80	INTACT (W/SLEEVE)	400 DIFF: NDD 100 ABS: NDD RPC: 48%	400 DIFF: DENT 100 ABS: 28%	40% MAX OVER 60 MIL BAND
C	10 43	FRACTURED AT TTS	400 DIFF: NDD 100 ABS: NDD RPC: 69%	400 DIFF: DENT 100 ABS: 60%	NOT PERFORMED

4. Assessment of IGA Progression

This Section describes the results of the 1985 re-evaluation of San Onofre Unit 1 eddy current data for sleeved and non-sleeved tubes. Eddy current data from 1973 to 1982 was reviewed and compared to determine the extent to which IGA and "IGA-like" indications have been present and have changed over the years.

Table 4-1 lists the inspections from which eddy current data was re-evaluated. Also included in this Table are the probe sizes and types as well as the test frequencies and modes and numbers of tubes from each inspection which were re-evaluated in 1985.

Figures 4-1 through 4-6 show the locations of tubes re-evaluated from each inspection. Table 4-2 lists the numbers of re-evaluated tubes which were common to two or more inspections.

From the inspections prior to 1980, composite eddy current signatures and horizontal and vertical channels of the 400 kHz differential bobbin were reproduced using the DDA-4 analysis system. From the 1980 and 1982 inspections, the 400 kHz (1980 only), 340 kHz and 340/100 kHz mix were reproduced as was the 100 kHz absolute. The documented signatures were then sorted into groups of tubes inside and outside the sleeving boundary. The signatures from various inspections of a given tube were compared to determine whether responses indicative of IGA were present and to what extent these have changed. Identification of IGA and "IGA-like" responses was based on pulled tube data (Section 3), data on tubes known to have leaked due to top of tube

sheet defects and data on tubes known to be within the active regions of IGA as identified in 1980.

Representative histories of tubes within active regions and having unambiguous indications of IGA at the top of the tubesheet in 1980 are contained in Appendix C. These histories are comparable to and supplement those in Appendix A. For all such tubes re-evaluated, there is evidence, dating back to the 1973 eddy current examination records, of IGA itself or signal distortions which can be attributed to IGA. For these tubes, there is also a consistent, detectable pattern of change toward greater degradation.

To illustrate the regionalization of activity within the tube bundle, eddy current signatures from columns of tubes which traverse active areas within the sleeving boundary were reviewed row by row to assess the similarity of responses. Representative data used in this review are presented in Appendix D. Data from columns 39 and 45 from the 1980 inspection and column 52 from the 1976 inspection are presented. Review of this type of data indicates that, associated with active and inactive regions, there are characteristic eddy current responses.

Representative histories of tubes in the non-sleeved regions, that are currently in service, are presented in Appendix E. In the review of non-sleeved tube inspection data, unlike data from tubes in active regions, no significant changes in eddy current signatures were observed from one inspection to the next. In addition, this review did not identify any discretely quantifiable, unambiguous IGA indications such as those found in the active regions. However, distorted tubesheet

indications (DTS) which may indicate the presence of IGA in the non-sleeved region were observed. The locations of these DTS indications are plotted in Figure 4-7. As noted above, comparison of historical data on these DTS indications show no significant change from inspection to inspection. From these results, it is concluded that there is not a significant IGA progression rate in the non-sleeved tubes.

In summary, it is concluded that IGA and "IGA-like" eddy current indications have been present since 1973, that there is regionalization of IGA activity within the tube bundle, and that the non-sleeved tubes are in a region of inactivity.

TABLE 4-1
 BOBBIN COIL EXAMINATIONS
 STEAM GENERATOR 'A'
SAN ONOFRE UNIT 1

<u>EXAMINATION DATE</u>	<u>PROBE SIZE</u>	<u>FREQUENCY</u>	<u>MODE</u>	<u>TUBES EVALUATED ('85)</u>
JUNE 1973	560 SPF*	400kHz	DIFF	355
APRIL 1975	560 SPF	400kHz	DIFF	519
OCT. 1976	560 SPF	400kHz	DIFF	541
SEPT. 1977	560 SF**	400kHz	DIFF	201
JUNE 1979	560 SF	400kHz	DIFF	111
APRIL 1980	580 SF	MULTI	DIFF/ ABS	3500
MARCH 1982	560 SF	MULTI	DIFF/ ABS	427

* special flex

** spring flex

TABLE 4-2
 NUMBER OF TUBES AND EDDY CURRENT SIGNALS
 COMPARED IN 1985 RE-EVALUATION
 STEAM GENERATOR 'A'
 SAN ONOFRE UNIT 1

<u>DATES OF INSPECTIONS COMPARED</u>	<u>NUMBER OF TUBES COMPARED</u>	<u>NUMBER OF TOP OF TUBESHEET SIGNALS</u>
73/80	255	510
73/80/82	63	189
73/76/80	9	27
73/76/80/82	4	16
73/77/80	4	12
73/77/79/80	1	4
73/77/80/82	1	4
75/80	78	156
75/76/80	25	75
75/76/77/80	3	12
75/77/80	46	138
75/79/80	16	48
76/80	243	486
76/80/82	37	111
76/77/80	130	390
76/77/80/82	16	64
76/77/79/80	8	32
76/77/79/80/82	1	5
76/79/80	7	21
77/80	176	352
77/79/80	3	9

TABLE 4-2 (CONTINUED)

<u>DATES OF INSPECTIONS COMPARED</u>	<u>NUMBER OF TUBES COMPARED</u>	<u>NUMBER OF TOP OF TUBESHEET SIGNALS</u>
77/80/82	55	165
79/80	74	148
79/80/82	2	6
80/82	257	514

TOTAL NUMBER OF
TUBES COMPARED = 1514

TOTAL NUMBER OF
SIGNALS COMPARED = 3494

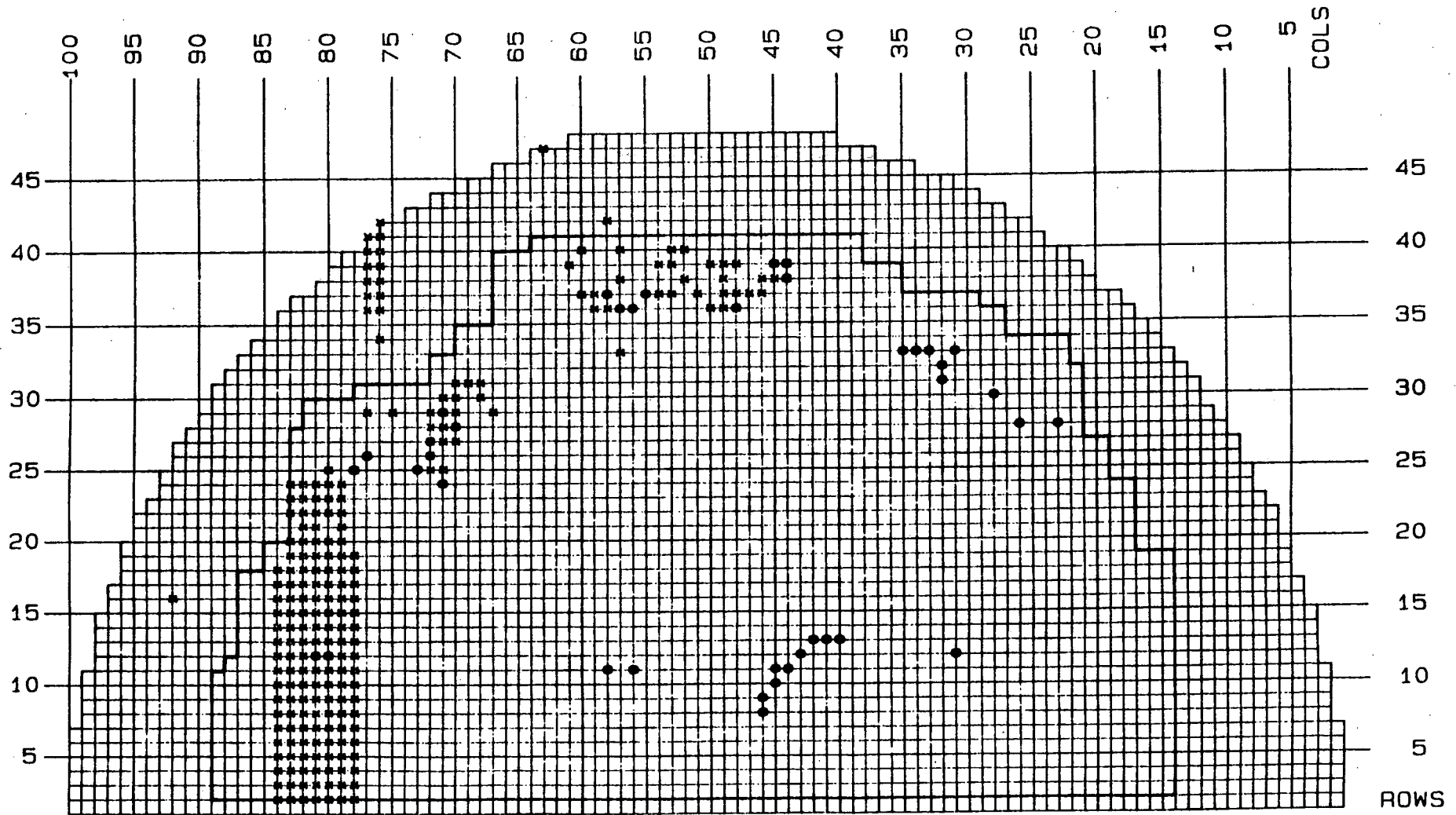
FIGURE 4-1

SAN ONOFRE UNIT 1 S/G 'A'

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: MARCH '85



<---MANWAY

— = 'A' SLEEVING BOUNDARY

NOZZLE--->

X - TUBES INSPECTED IN '73 AND RE-EVALUATED IN '85

● -39 TUBES USED TO ESTABLISH '81 IGA RATE

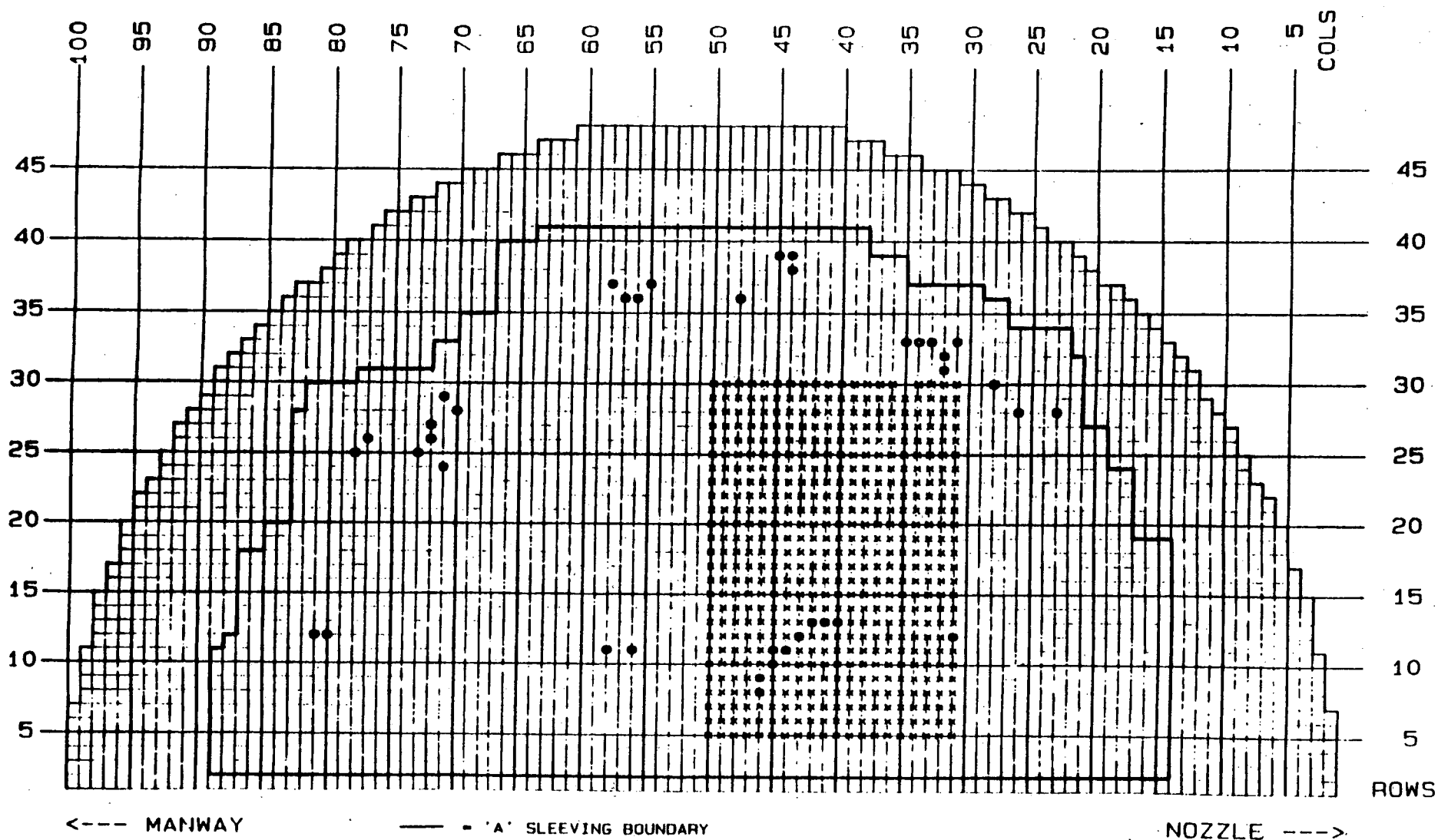
FIGURE 4-2

SAN ONOFRE UNIT 1 S/G A

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: FEB '85



X = TUBES INSPECTED IN '75 AND RE-EVALUATED IN '85

● = 39 TUBES USED TO ESTABLISH '81 IGA RATE

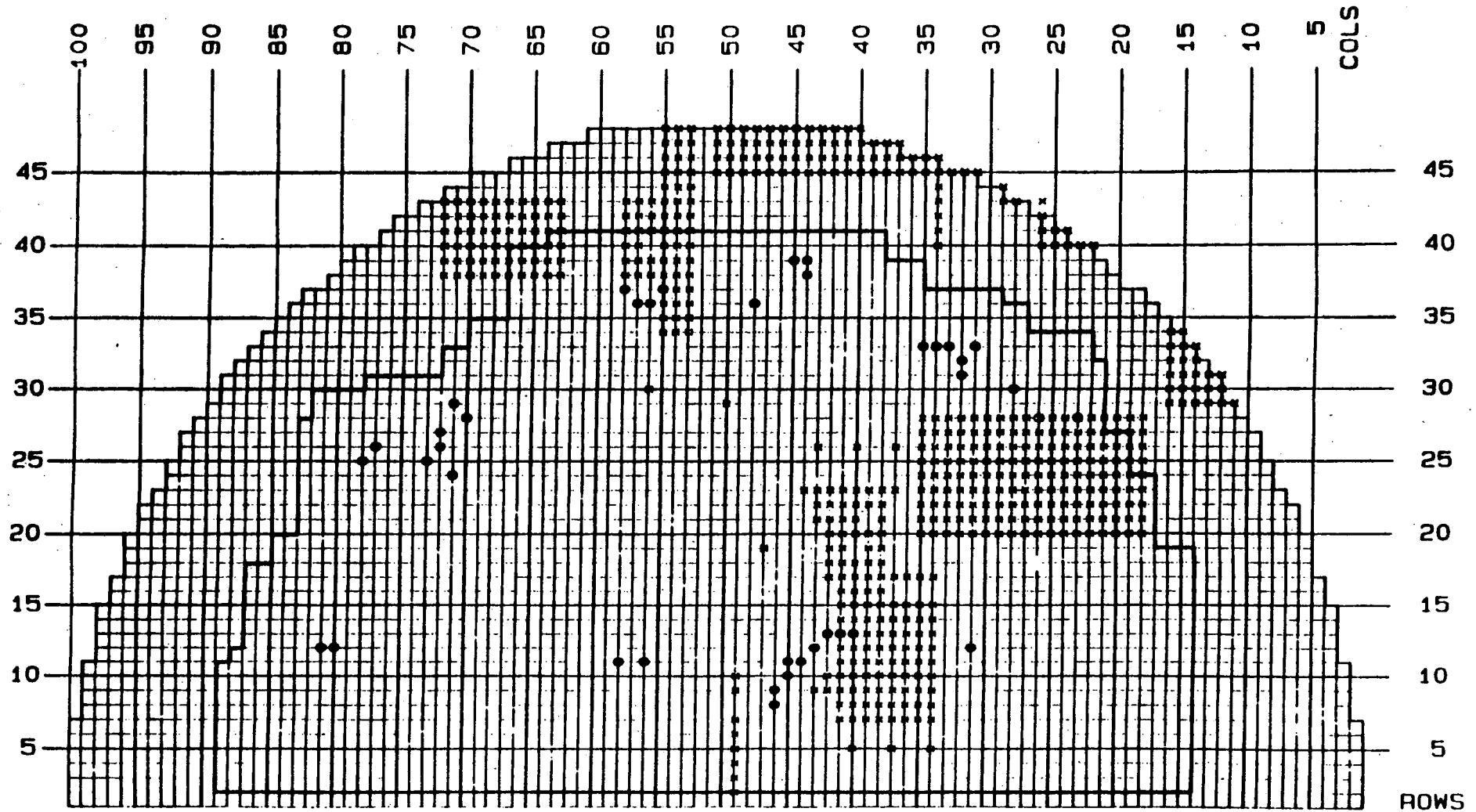
FIGURE 4-3

SAN ONOFRE UNIT 1 S/G A

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: FEB '85



<--- MANWAY

— A SLEEVING BOUNDARY

NOZZLE --->

X = TUBES INSPECTED IN '76 & RE-EVALUATED IN '85

● = 39 TUBES USED TO ESTABLISH '81 IGA RATE

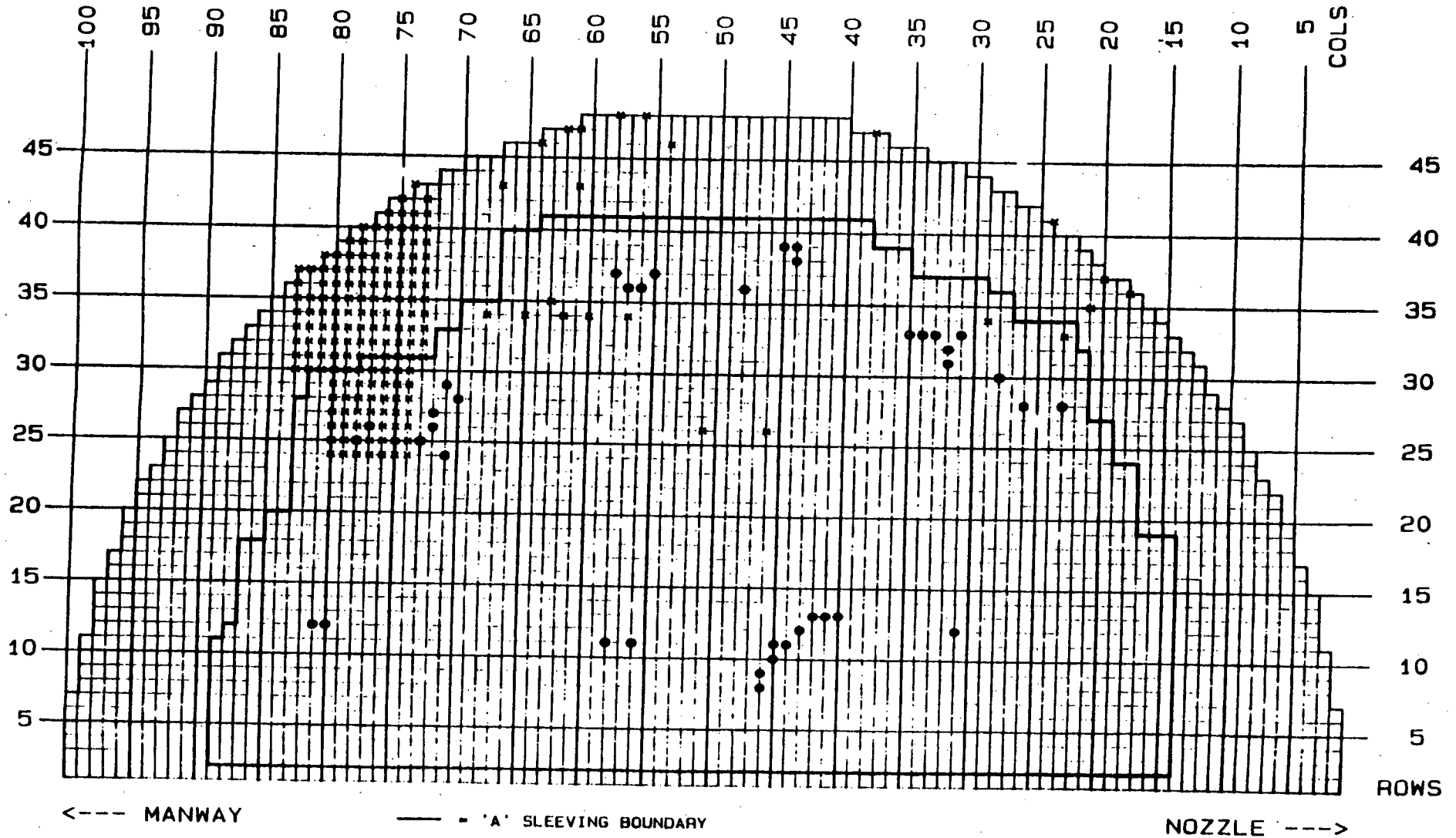
FIGURE 4-4

SAN ONOFRE UNIT 1 S/G 'A'

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: FEB '85



X = TUBES INSPECTED IN '77 AND RE-EVALUATED IN '85

● = 39 TUBES USED TO ESTABLISH '81 IGA RATE

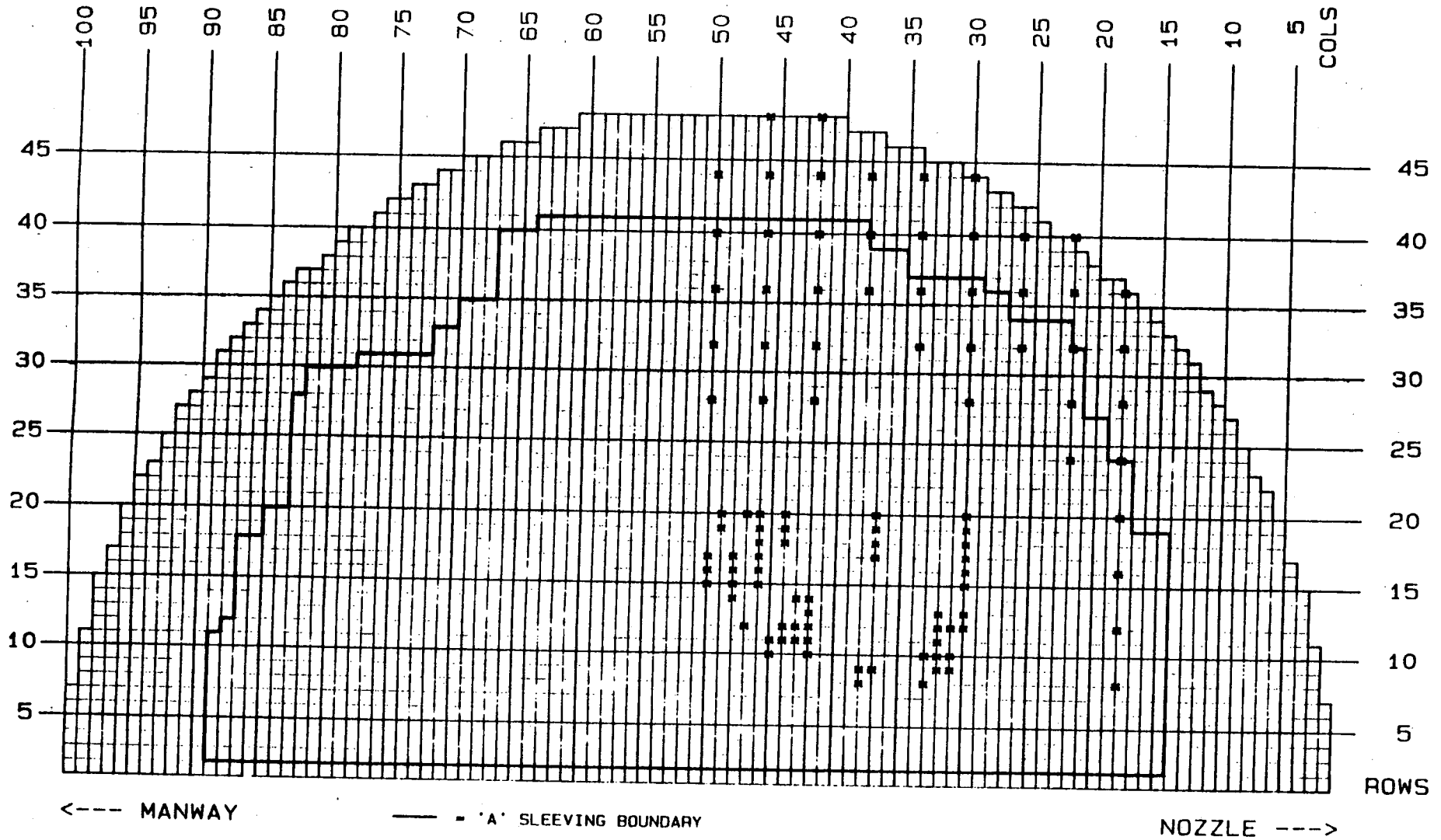
FIGURE 4-5

SAN ONOFRE UNIT 1 S/G 'A'

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: MARCH 1985



X = TUBES INSPECTED IN '79 AND RE-EVALUATED IN '85

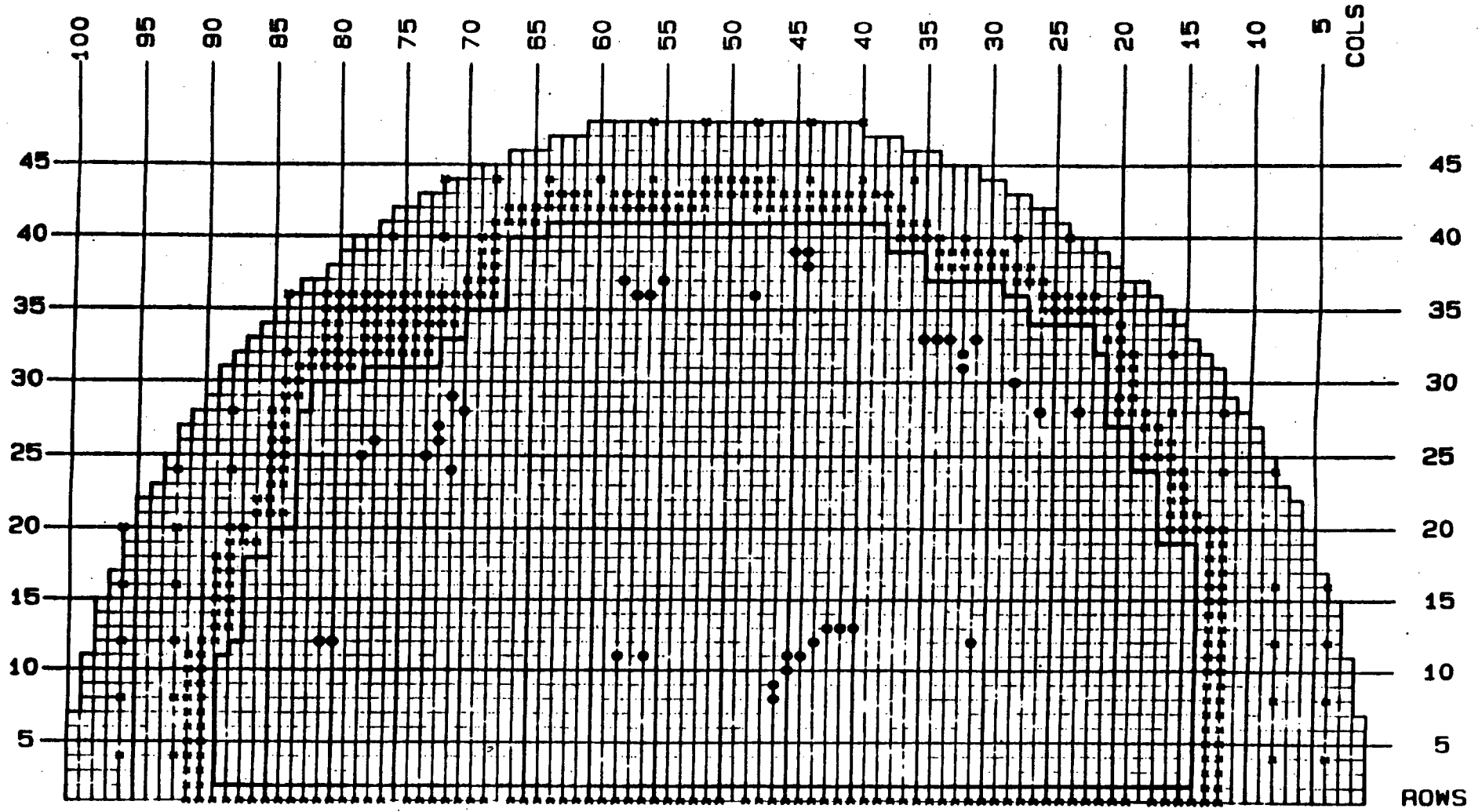
FIGURE 4-6

SAN ONOFRE UNIT 1 S/G A

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: FEB '85



<--- MANWAY

— A SLEEVING BOUNDARY

NOZZLE --->

X = TUBES INSPECTED IN '82 AND RE-EVALUATED IN '85

● = 39 TUBES USED TO ESTABLISH '81 IGA RATE

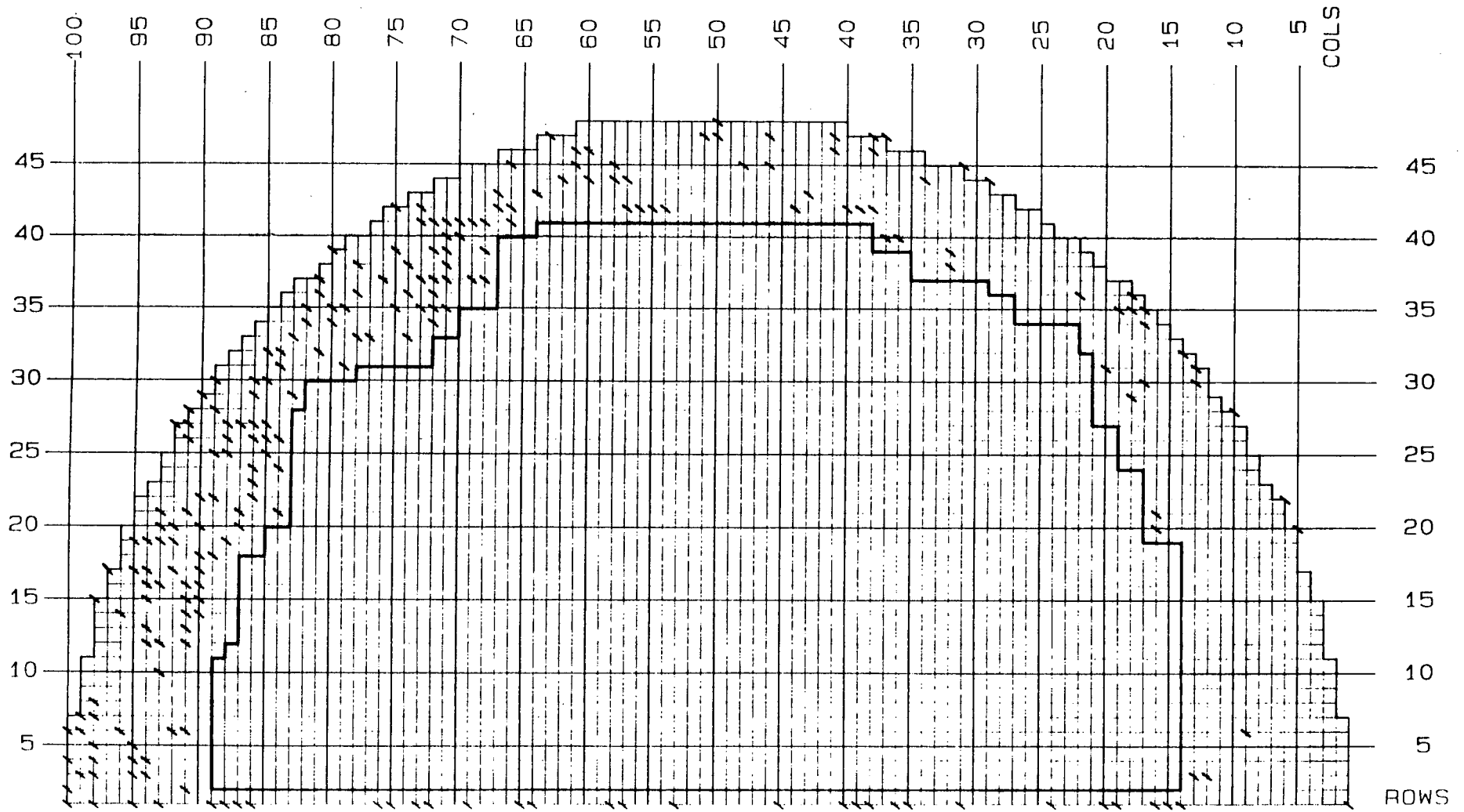
FIGURE 4-7

SAN ONOFRE UNIT 1 S/G 'A'

HOT LEG

ELEVATION: TUBESHEET

REPORT DATE: MARCH 1985



← --- MANWAY

— - 'A' SLEEVING BOUNDARY

NOZZLE --->

\ - DTS OR <5 V DENT

5. Conclusions

Based on the correlation of 1980 ECT data with the pulled tube metallurgical results, as discussed in Section 3, the bobbin coil can be used to detect IGA, as found at San Onofre Unit 1, at levels in excess of 20%. This value demonstrates the conservatism of the commonly accepted detectability threshold of 40%.

The results of the review presented in Section 4 of historical eddy current inspection data clearly identify the non-sleeved tubes as an "inactive" region of the tube bundle. However, the presence of non-quantifiable "IGA-like" indications in certain non-sleeved tubes indicates that IGA may be present, but based on the detectability threshold discussed above, it is concluded that IGA in the non-sleeved region is not likely to have progressed to levels greater than 40%.

Based on the comparison of historical data discussed in Section 4, evidence of IGA-like eddy current indications is present in the earliest available inspection data. This would indicate that IGA commenced sometime prior to 1973.

If it is conservatively assumed that the 1973 level of IGA in all non-sleeved tubes was 0% and it is acknowledged that IGA may have progressed to 1980 levels approaching 40%, then a conservative degradation rate for the non-sleeved region can be established. Since approximately 60 EFPM of operation occurred between 1973 and 1980, the assumed, worst case IGA progression rate is 40% per 60 EFPM, or 10% per 15 EFPM refueling cycle operating interval.

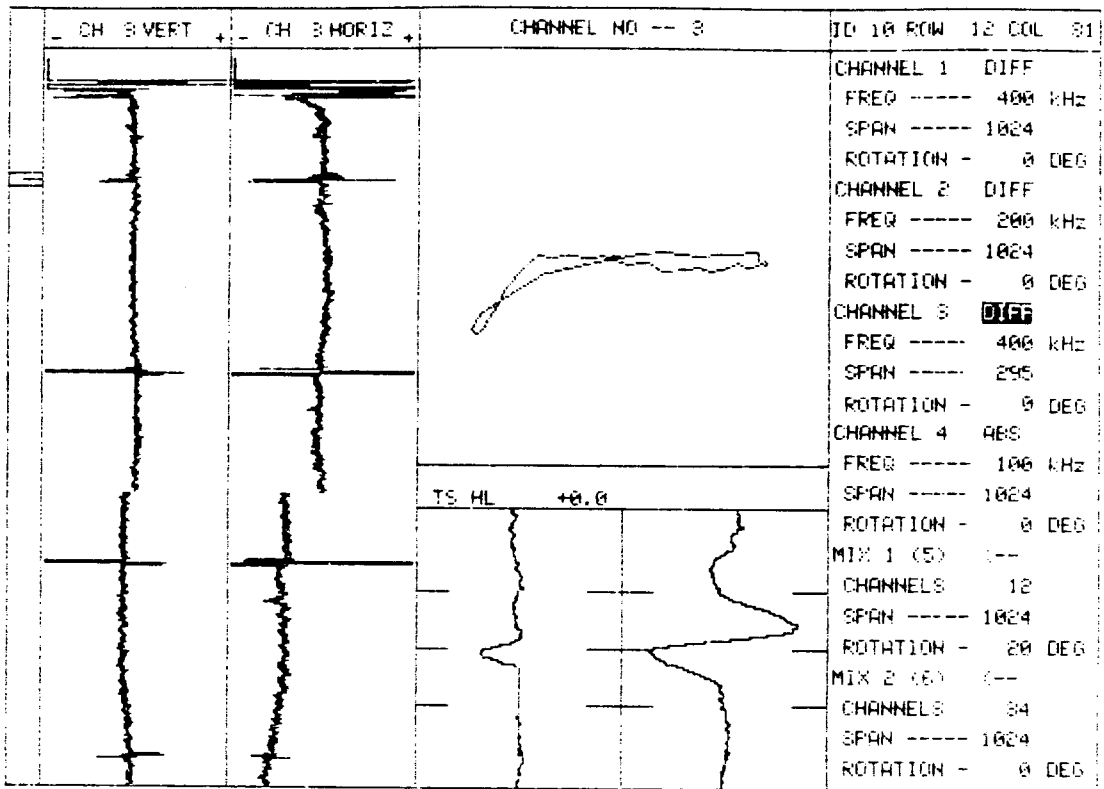
A review of Table 3-1 in Section 3 shows good detectability at IGA levels \geq 20%, which, when the DTS indications are considered, leads to the conclusion that the actual IGA level in non-sleeved tubes is not likely to have exceeded the 20% to 30% level. However, using the 10% per 15 EFPM IGA progression rate and conservatively assuming that IGA is near the 40% level in the non-sleeved tubes, eddy current inspections at refueling outage intervals will ensure that tube degradation due to IGA will be detected consistent with the 50% plugging limit for San Onofre Unit 1 non-sleeved tubes. Based on the results of the analysis presented in Appendix C.3.1 of Reference 2, non-sleeved tubes with up to 40% remaining wall and a potential loss of lateral support at the lower (one or two) support plates meet the applicable tube integrity design requirements. Therefore, it is concluded that, with a conservatively assumed IGA level of 40% and a 10% per 15 EFPM degradation rate, at the end of a 15 EFPM refueling cycle operating interval there is a 10% margin to the allowable minimum wall under postulated worst case accident conditions.

6. References

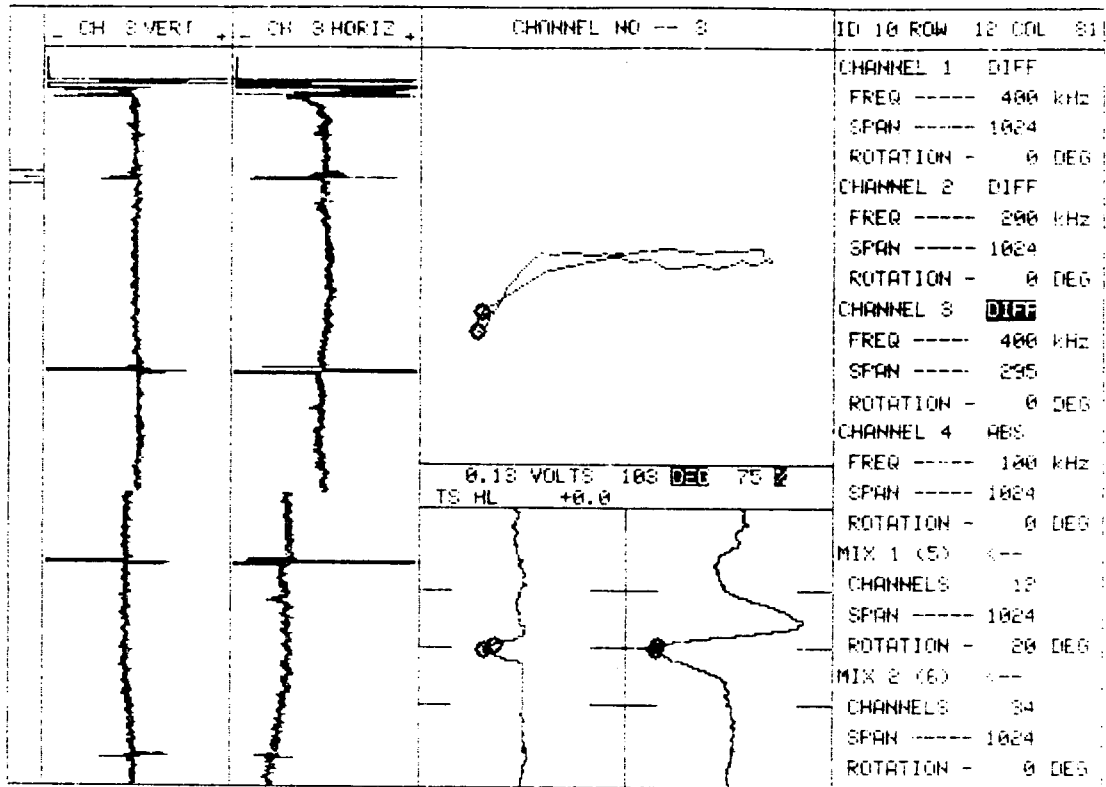
1. "STEAM GENERATOR REPAIR PROGRAM, RETURN TO POWER REPORT FOR SAN ONOFRE UNIT 1", April, 1981.
2. "STEAM GENERATOR INSPECTION PROGRAM, RETURN TO POWER REPORT, SAN ONOFRE NUCLEAR GENERATING STATION, UNIT 1", dated September, 1982, Volume I.

APPENDICIES

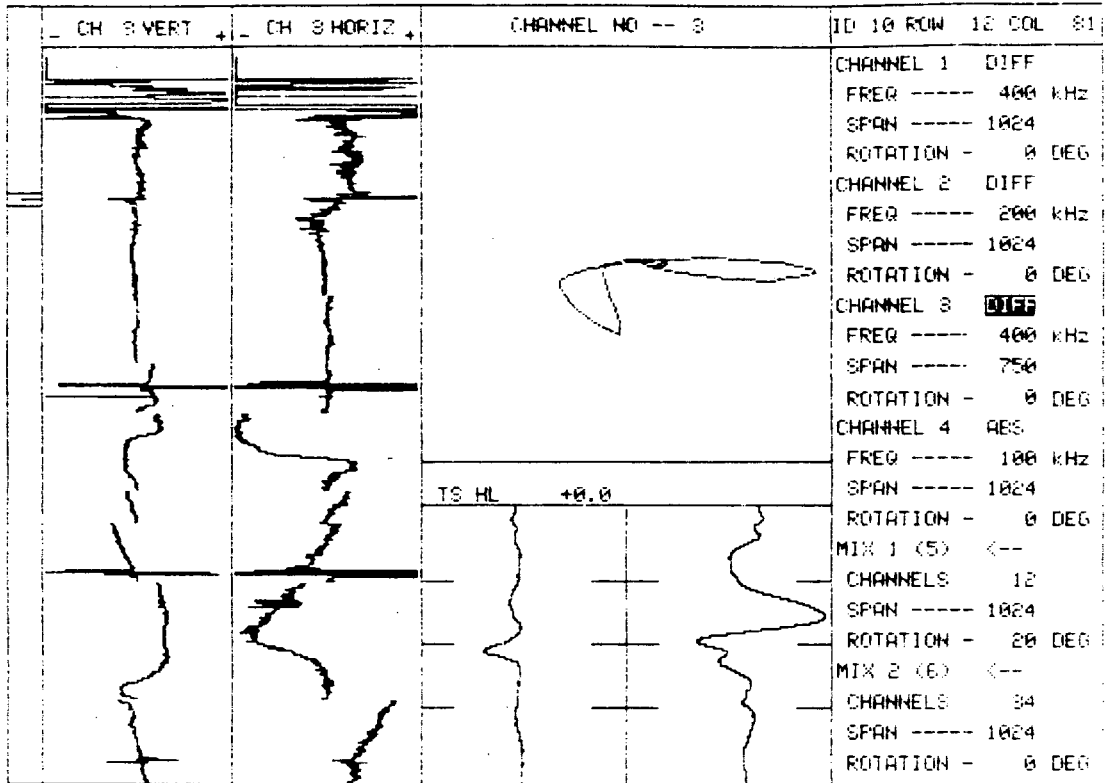
APPENDIX A



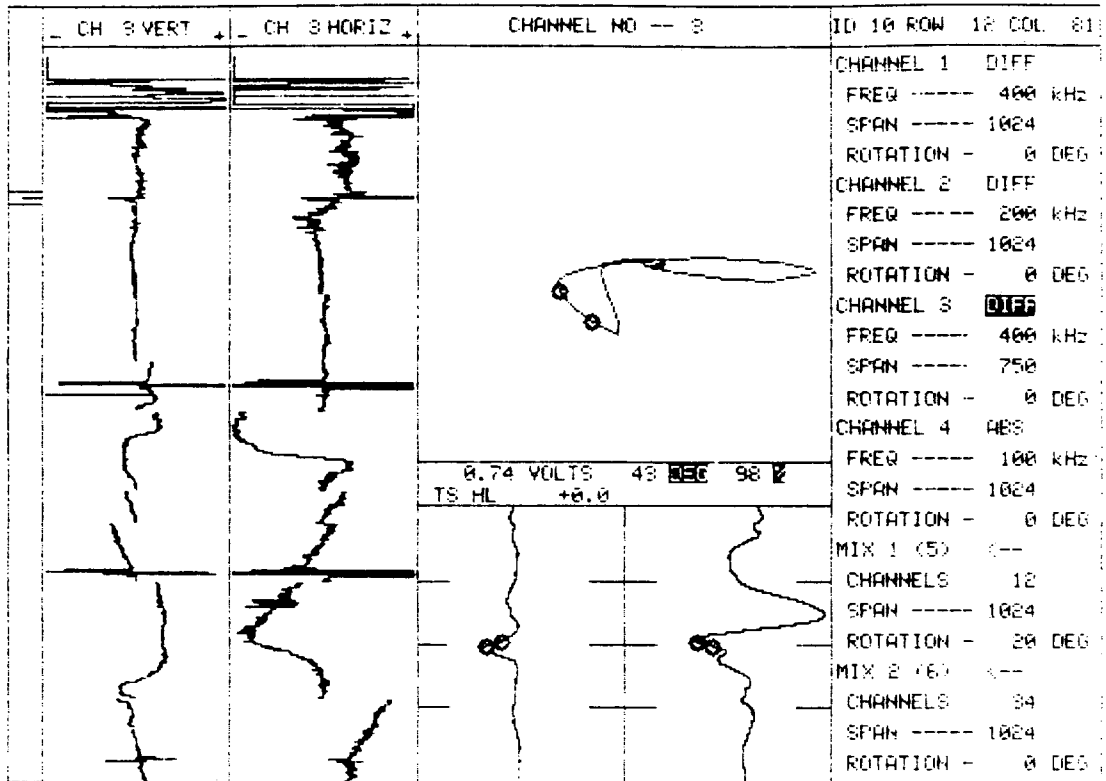
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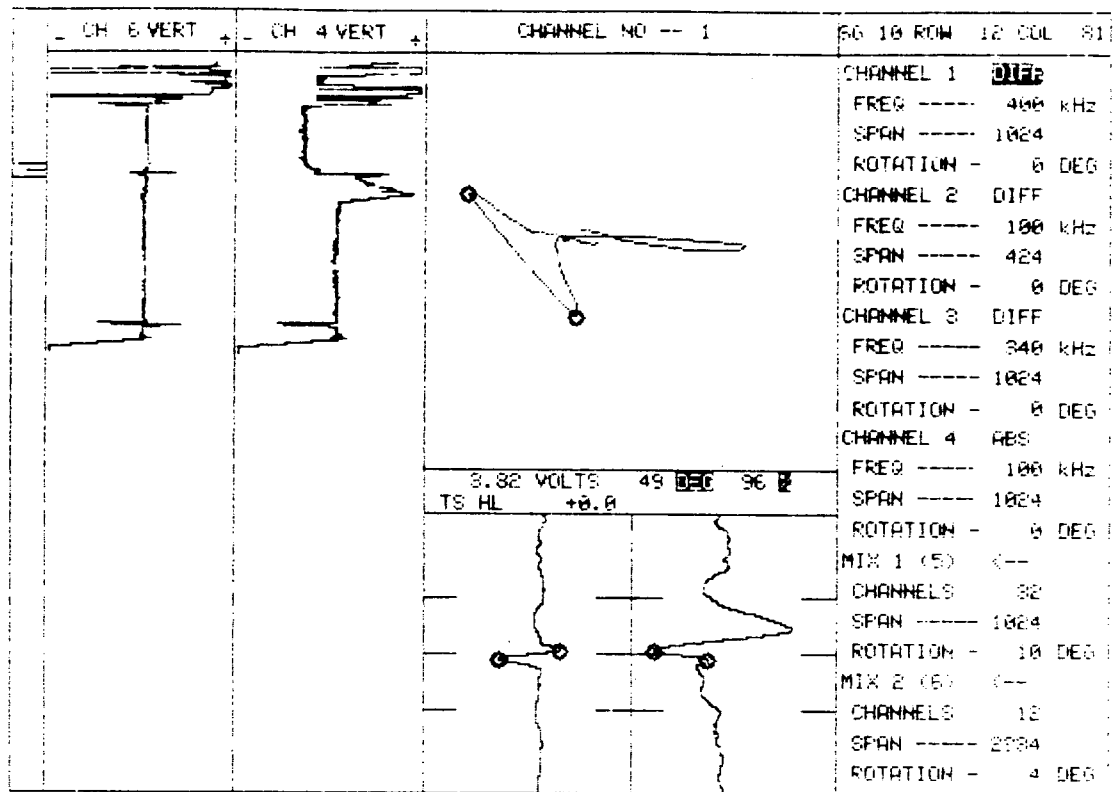
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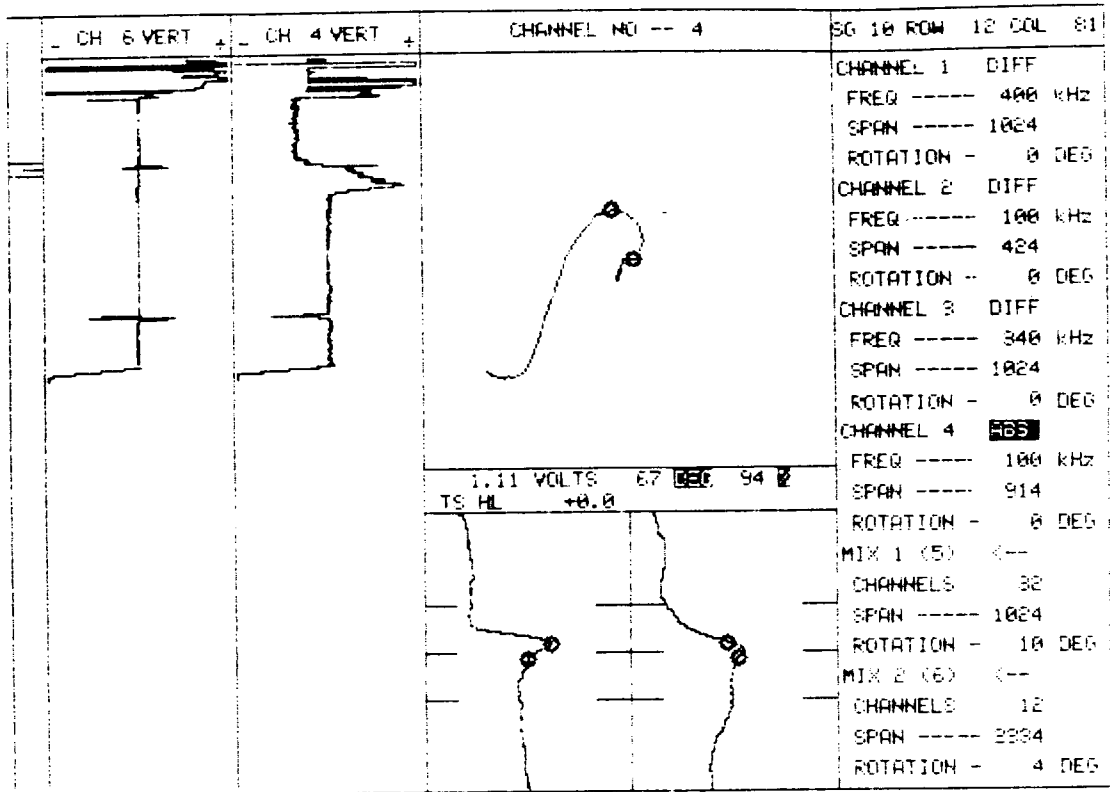
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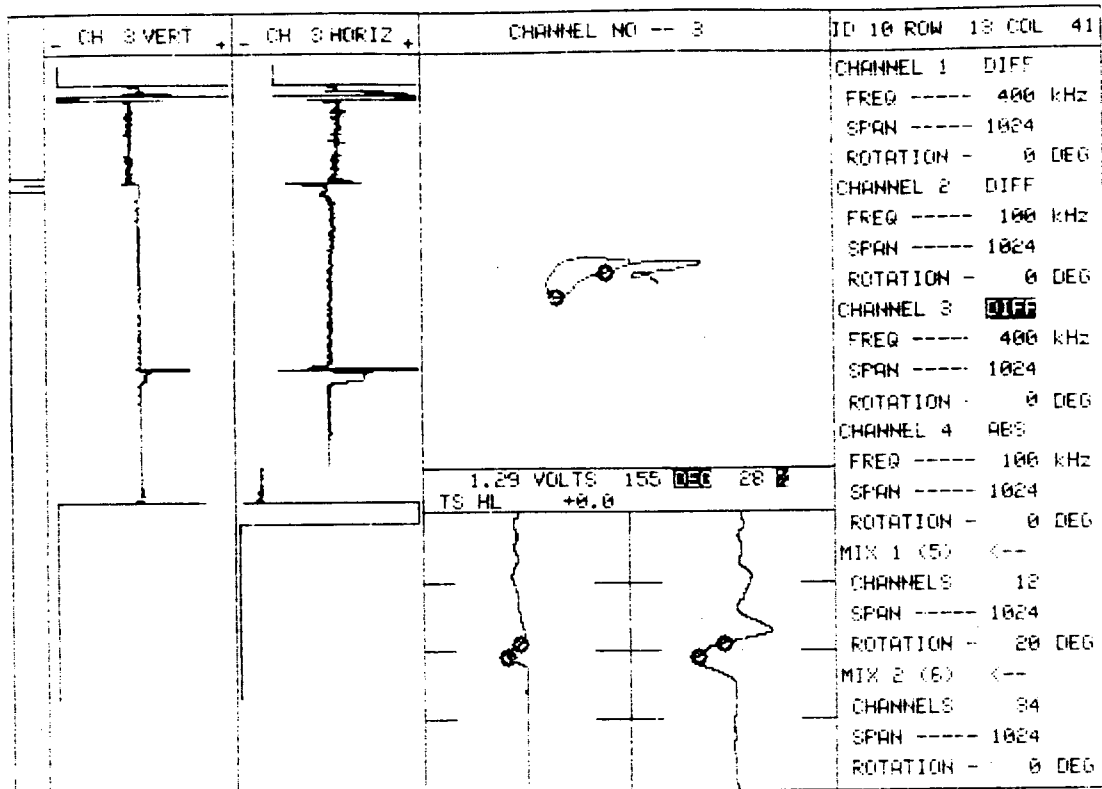
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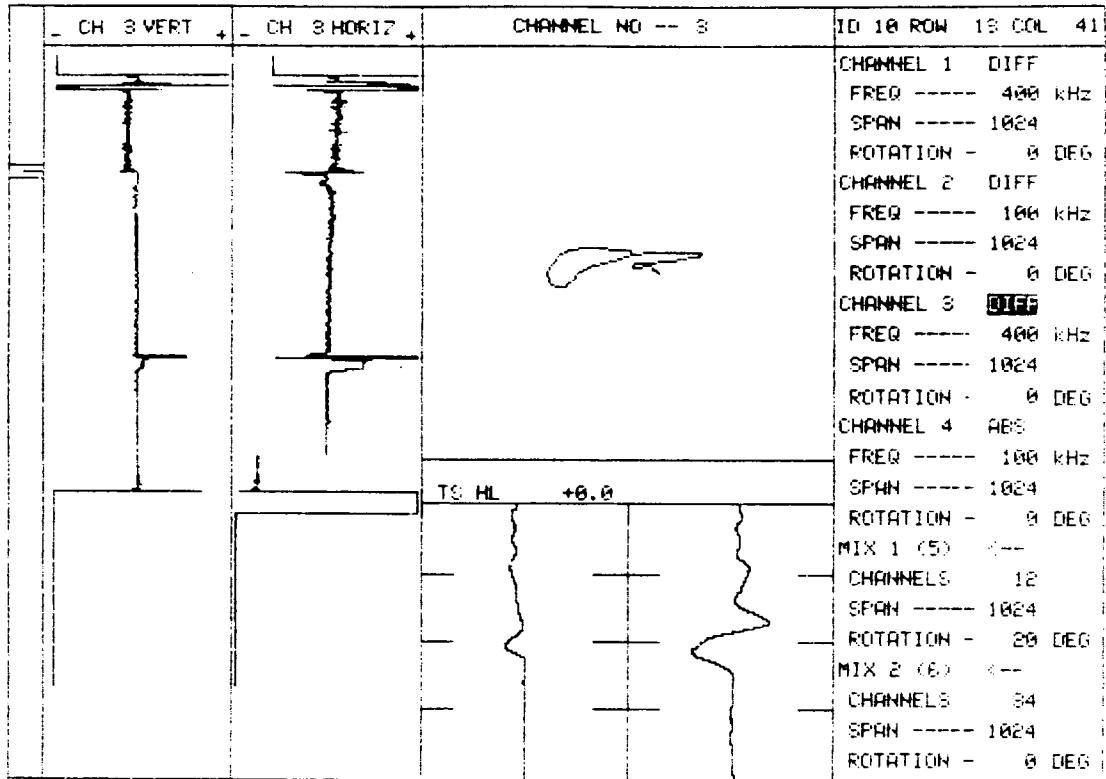
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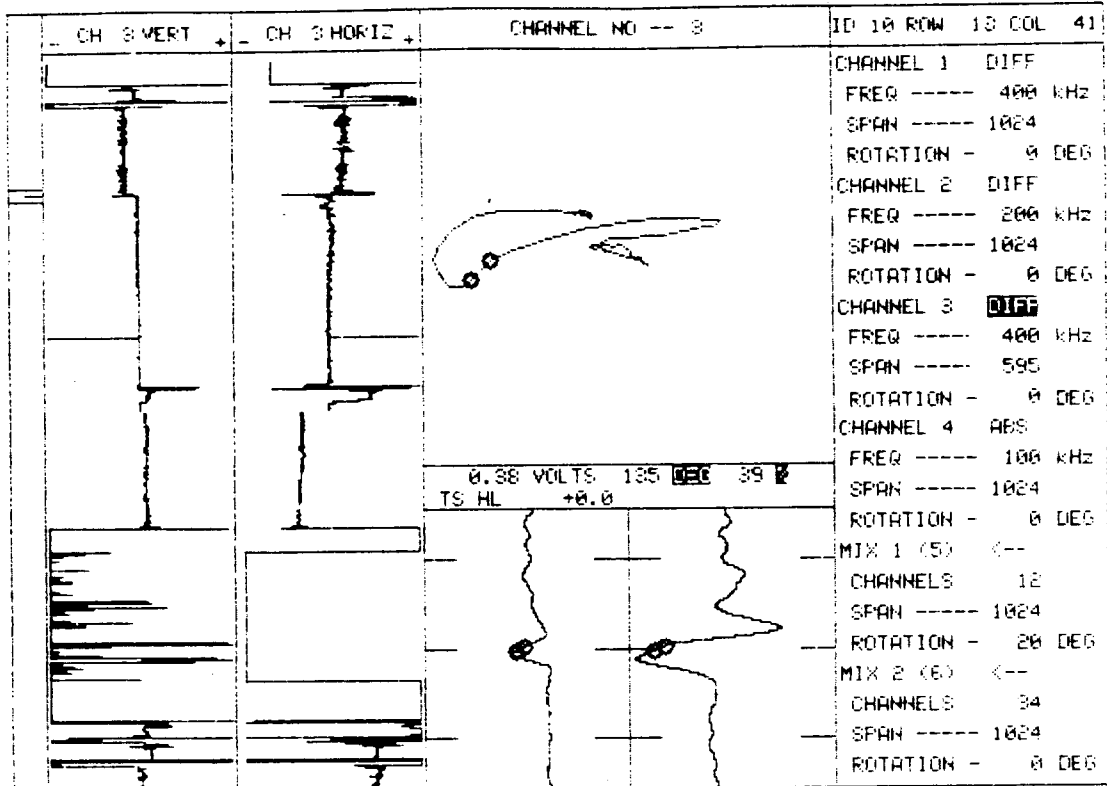
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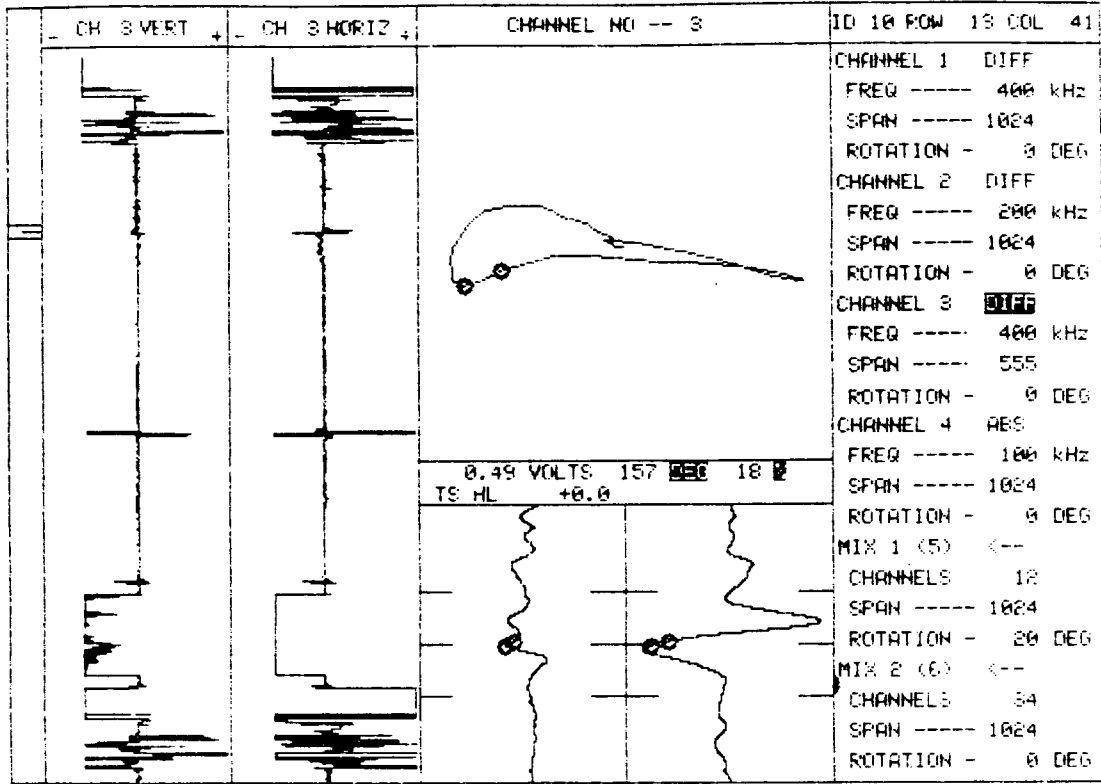
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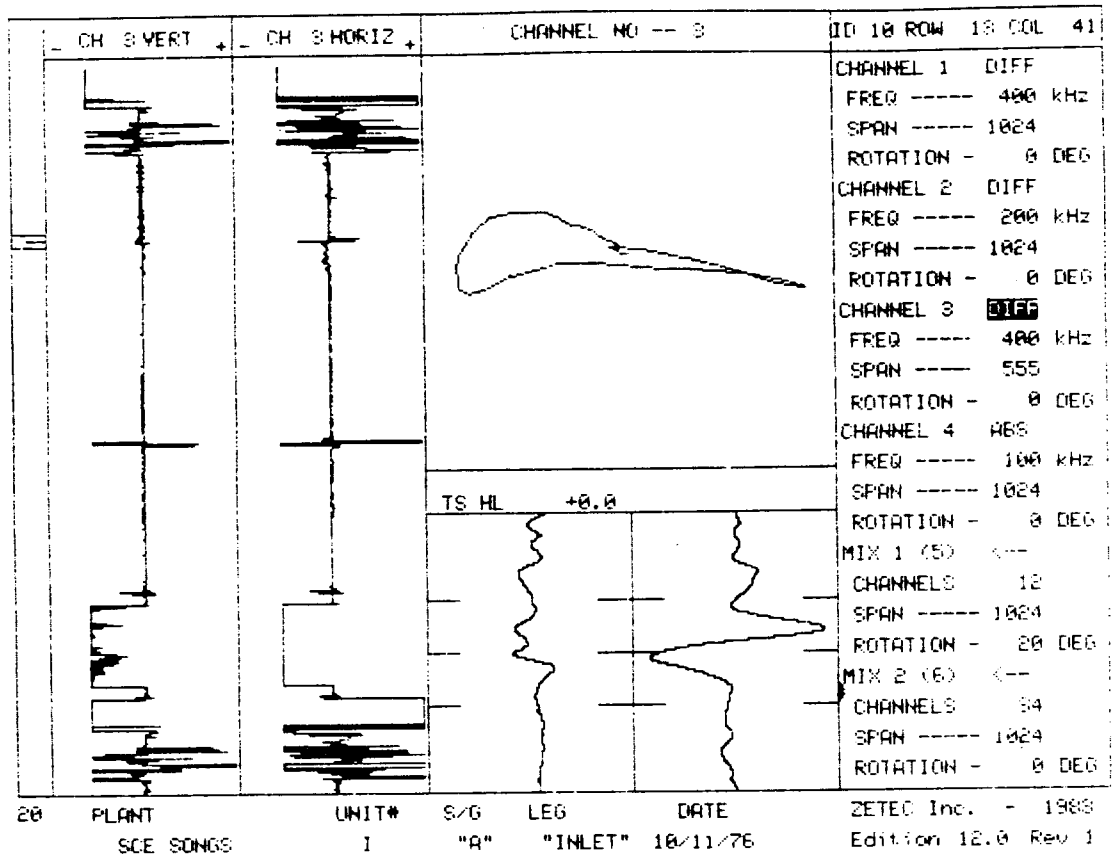


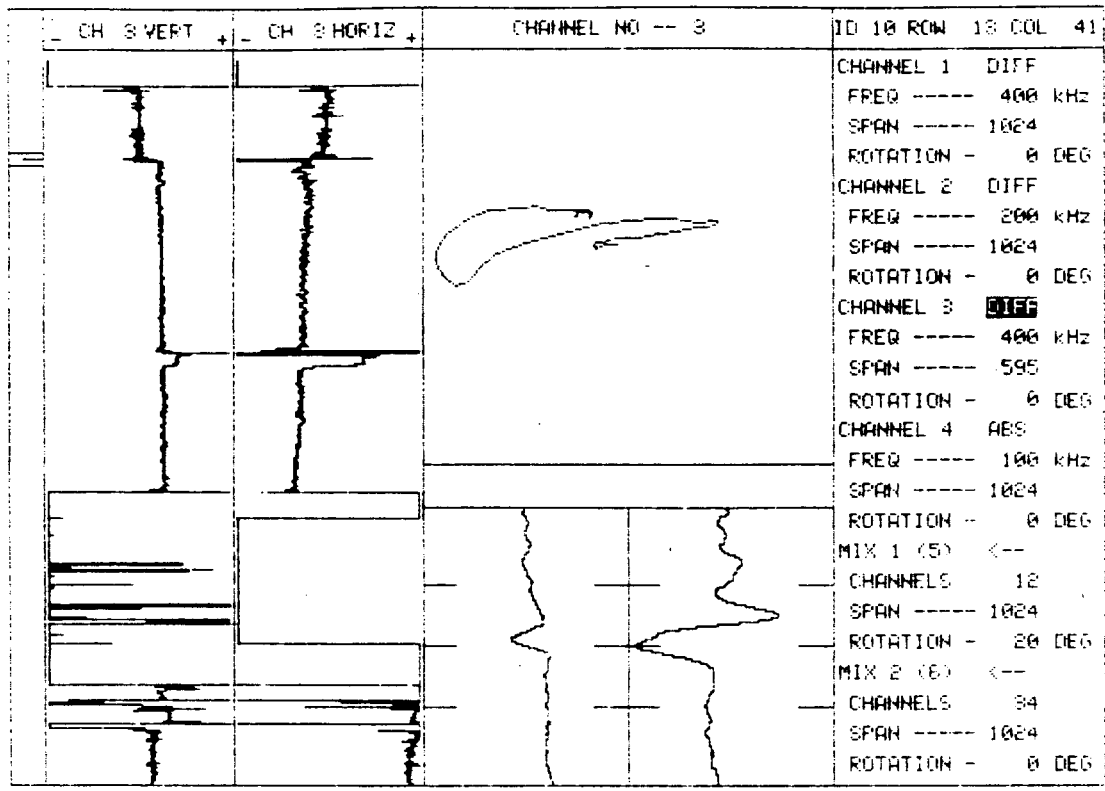
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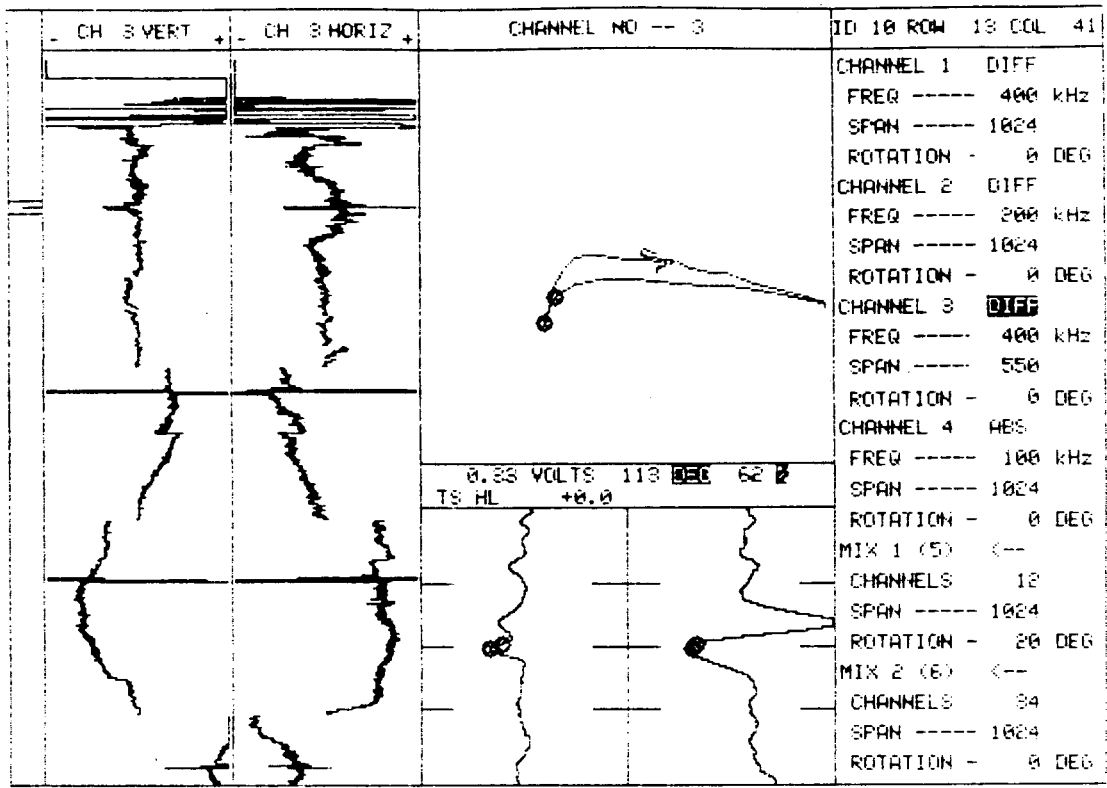
0.49 VOLTS 157 SEC 18 1/2
TS HL +0.0

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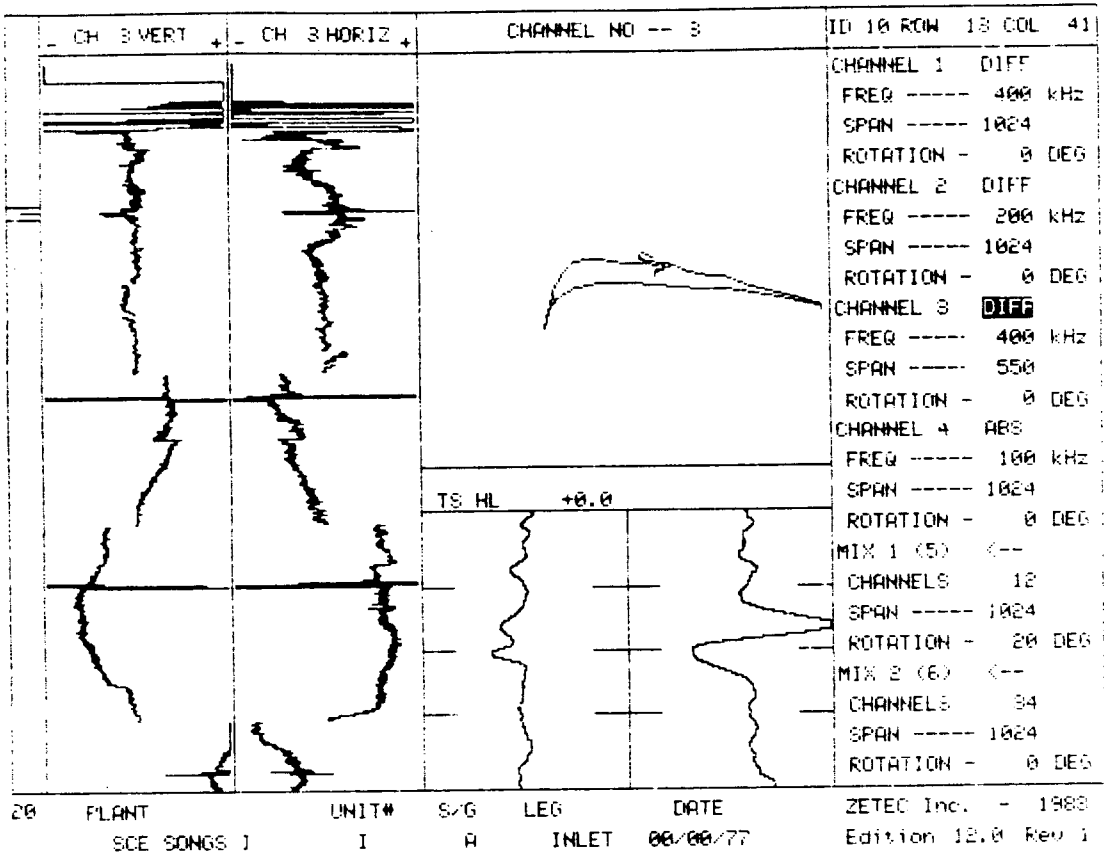




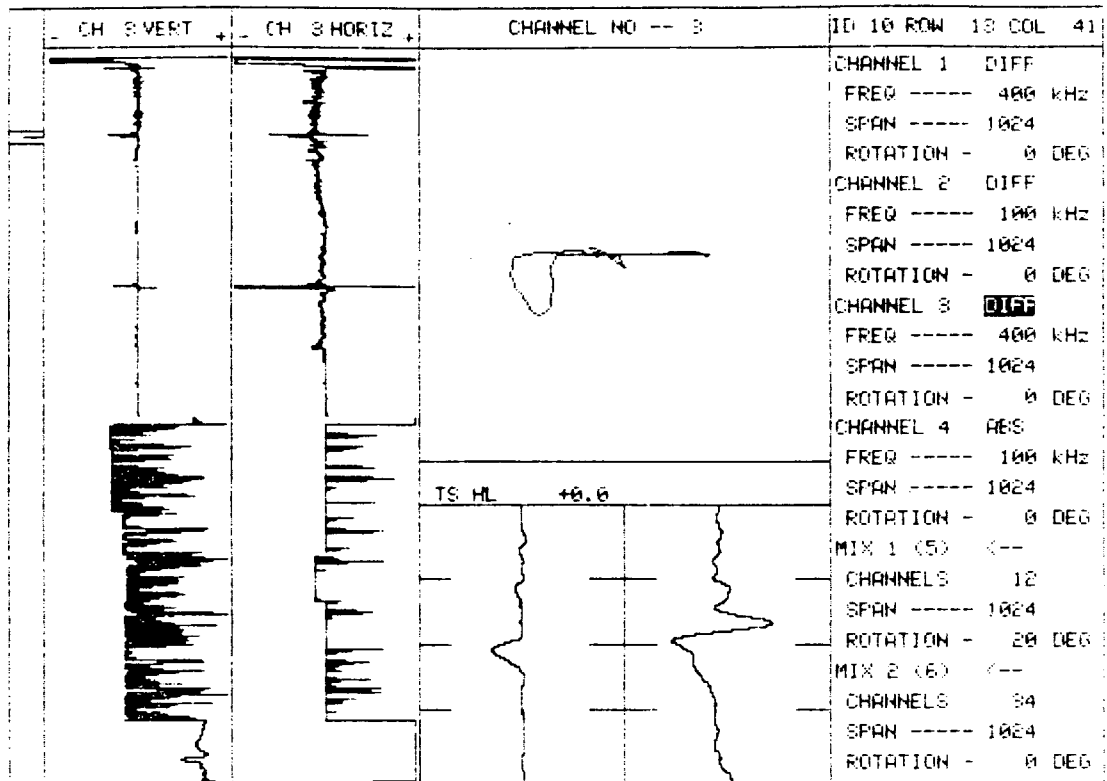
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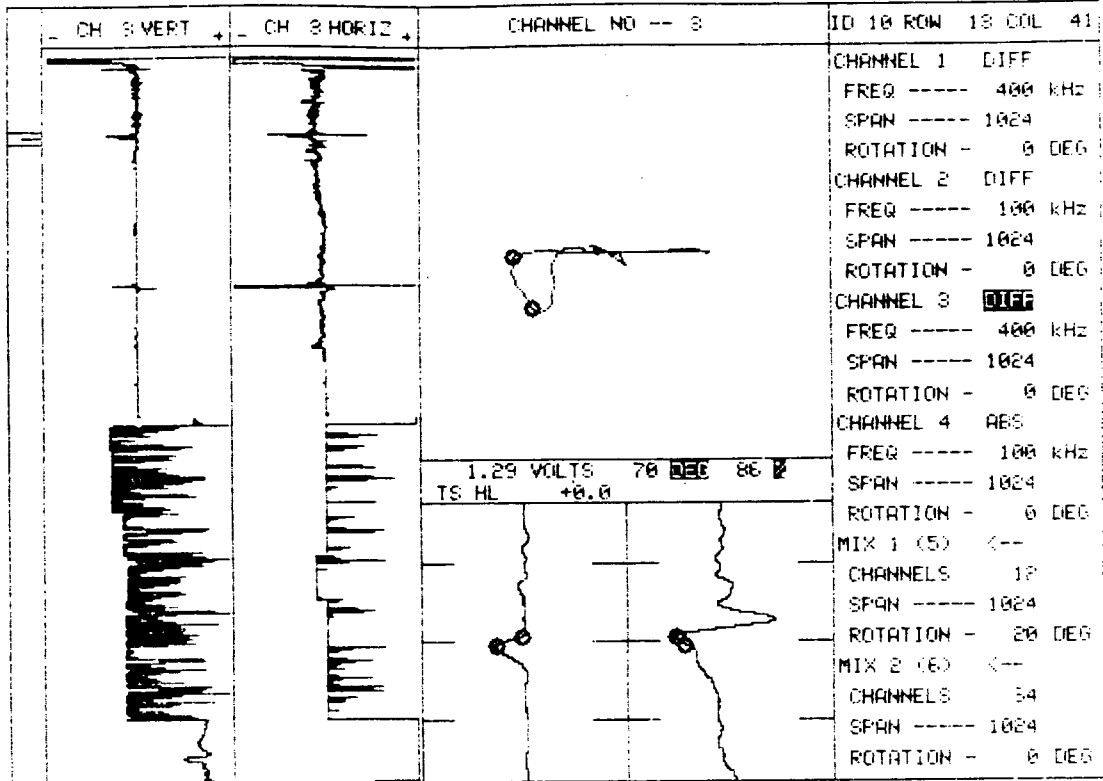
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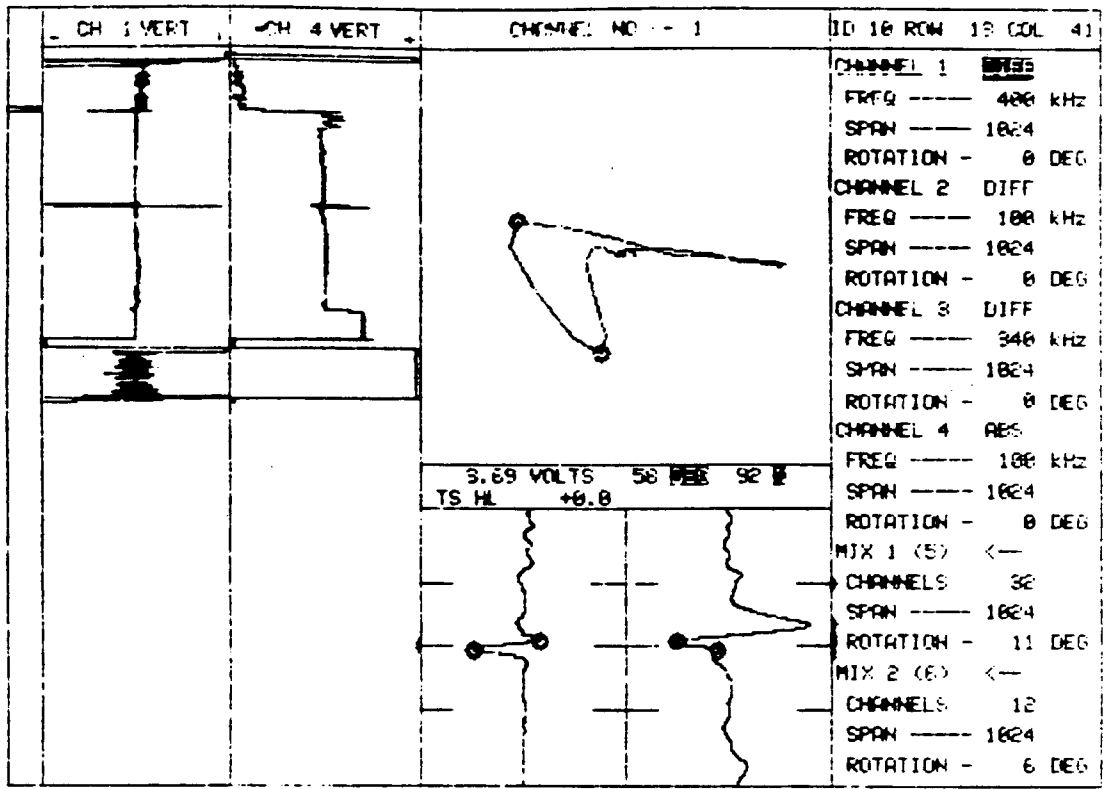
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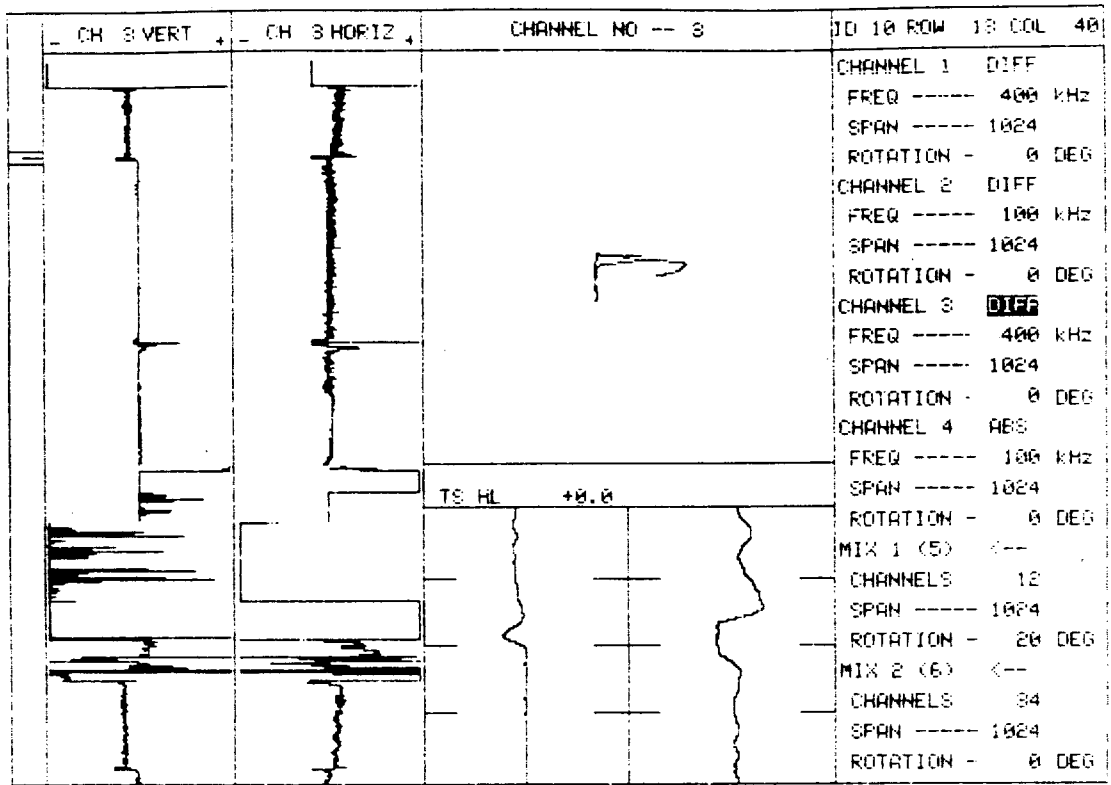
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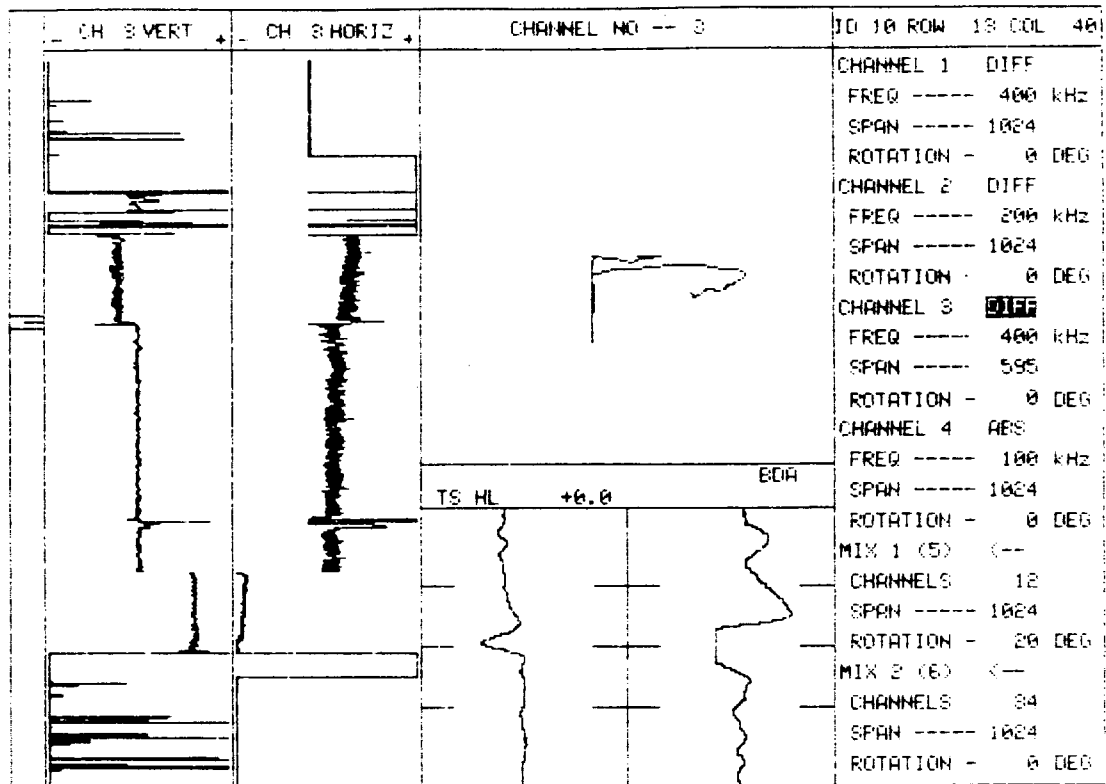
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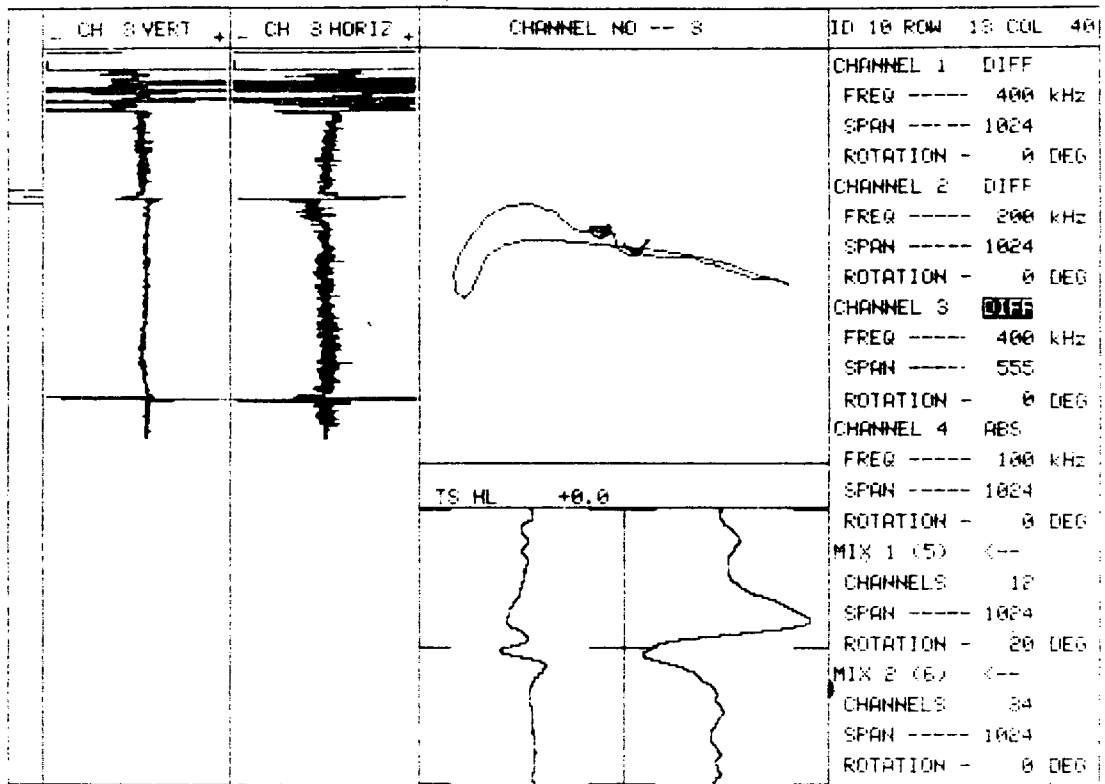
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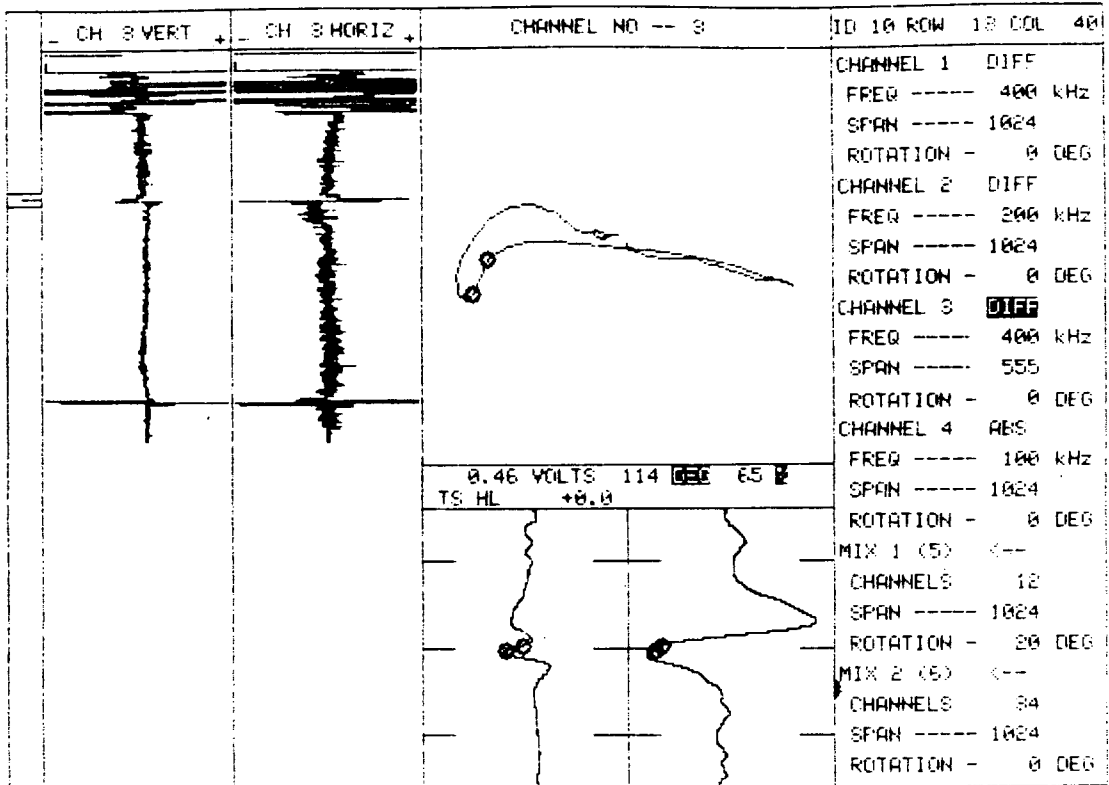
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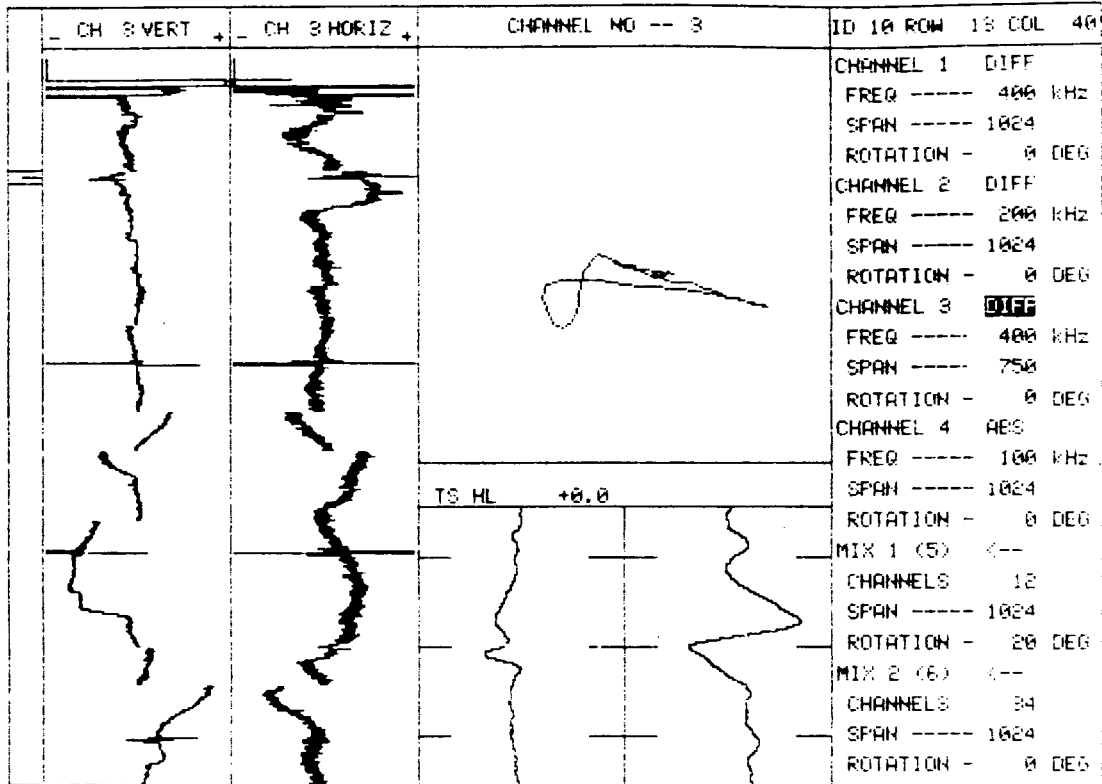


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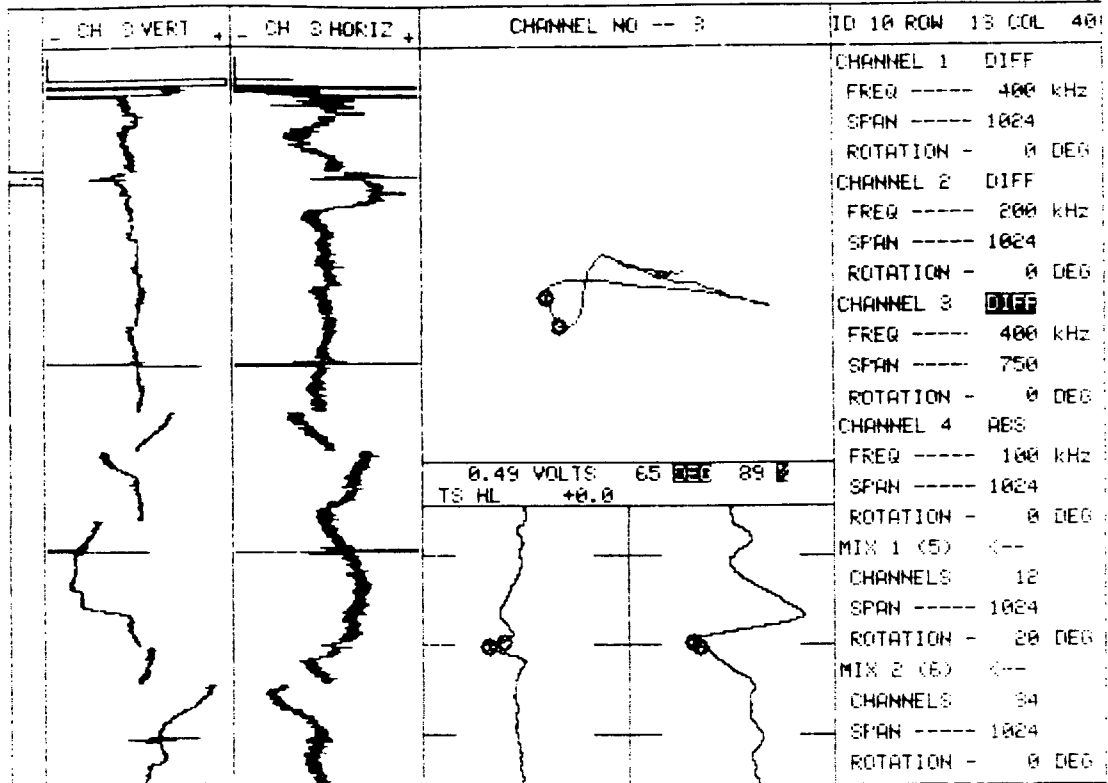


0.46 VOLTS 114 DEG 65 Hz
TS HL +0.0

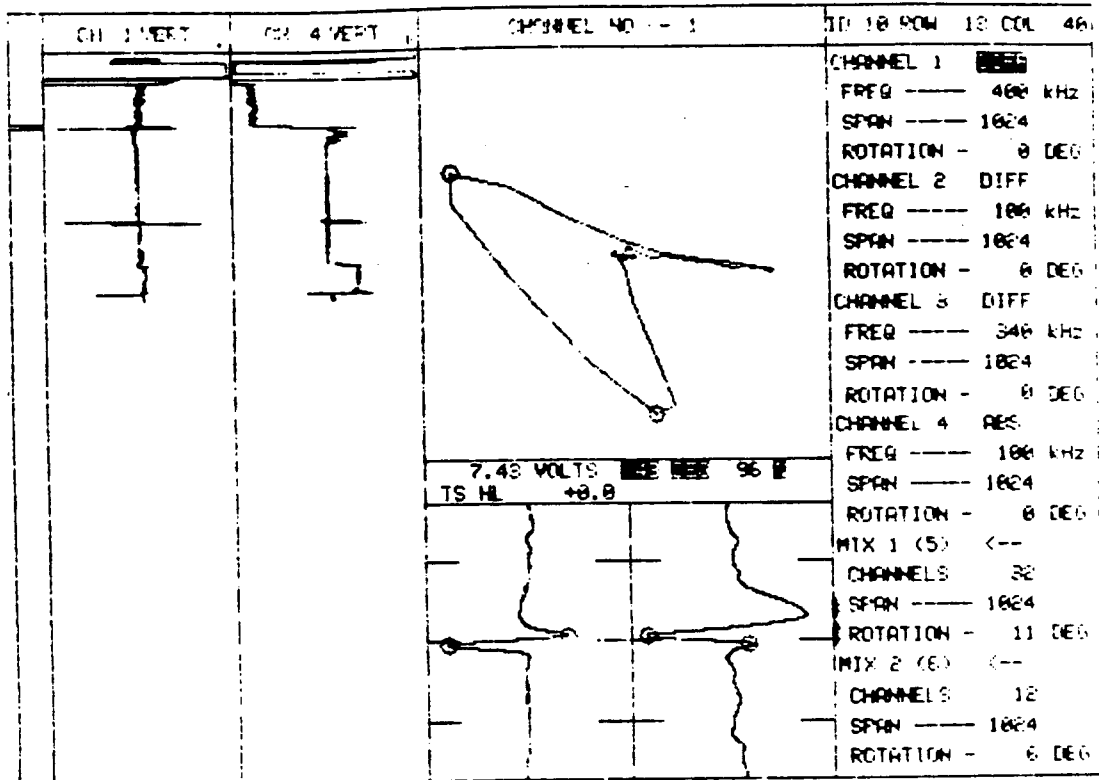
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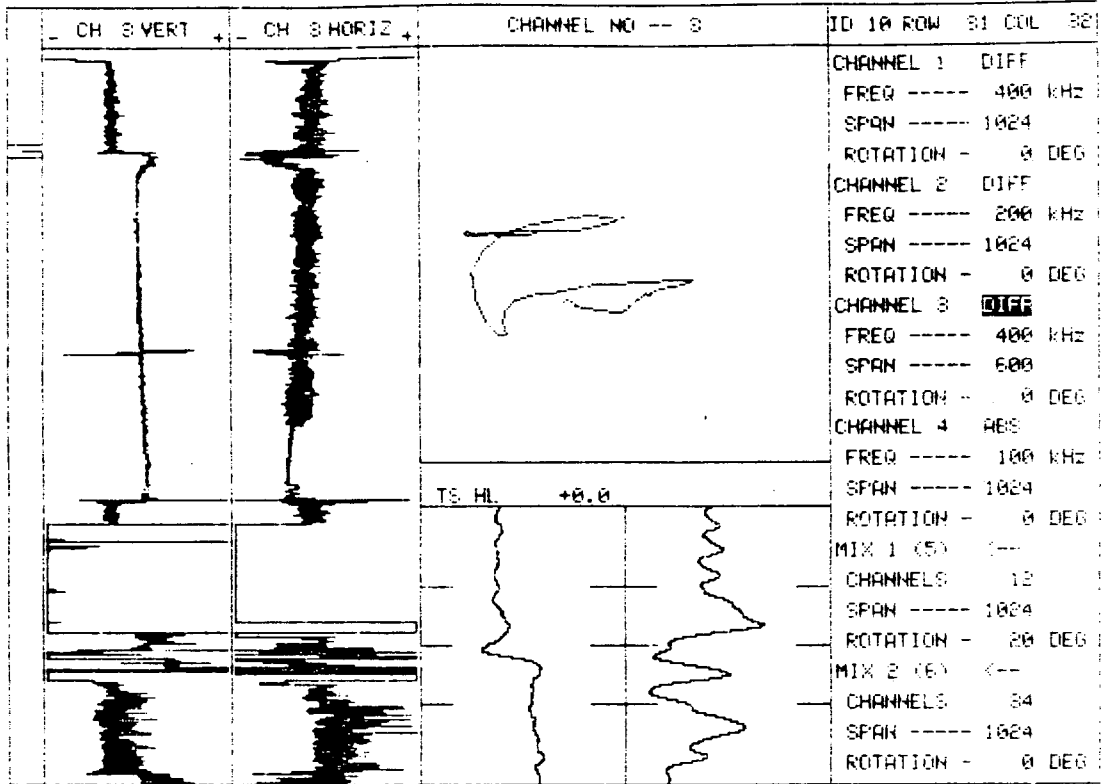


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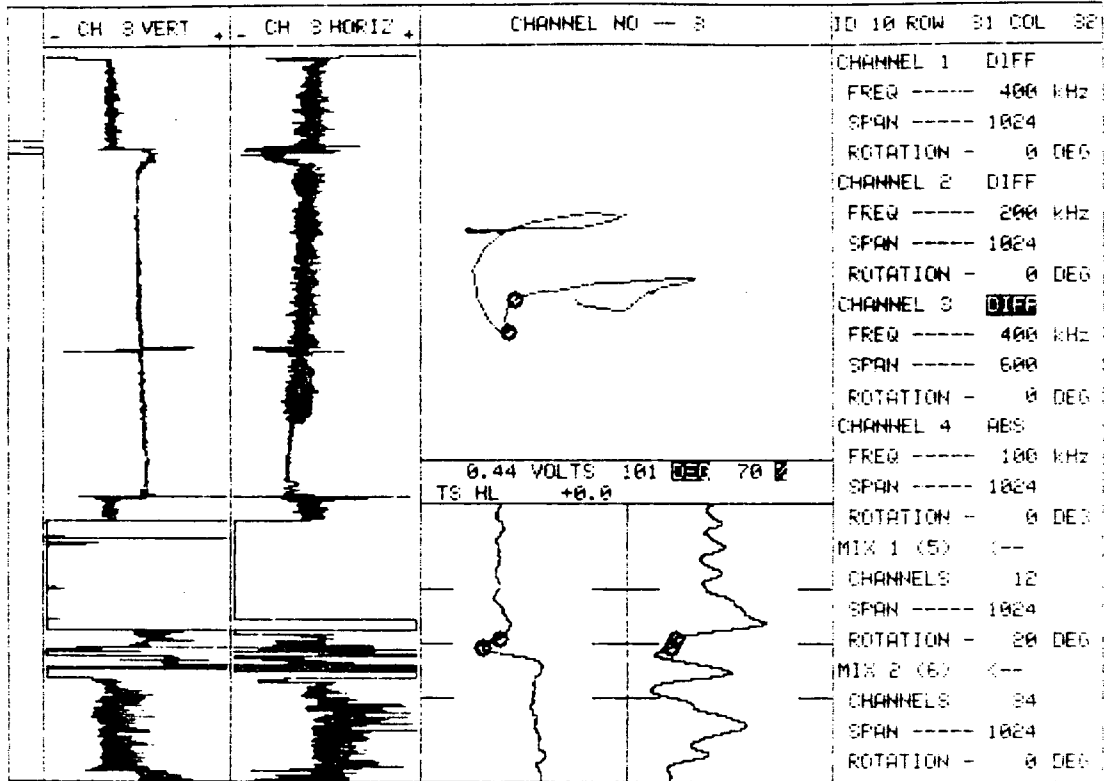


7.48 VOLTS **SEE SEE 96 E**
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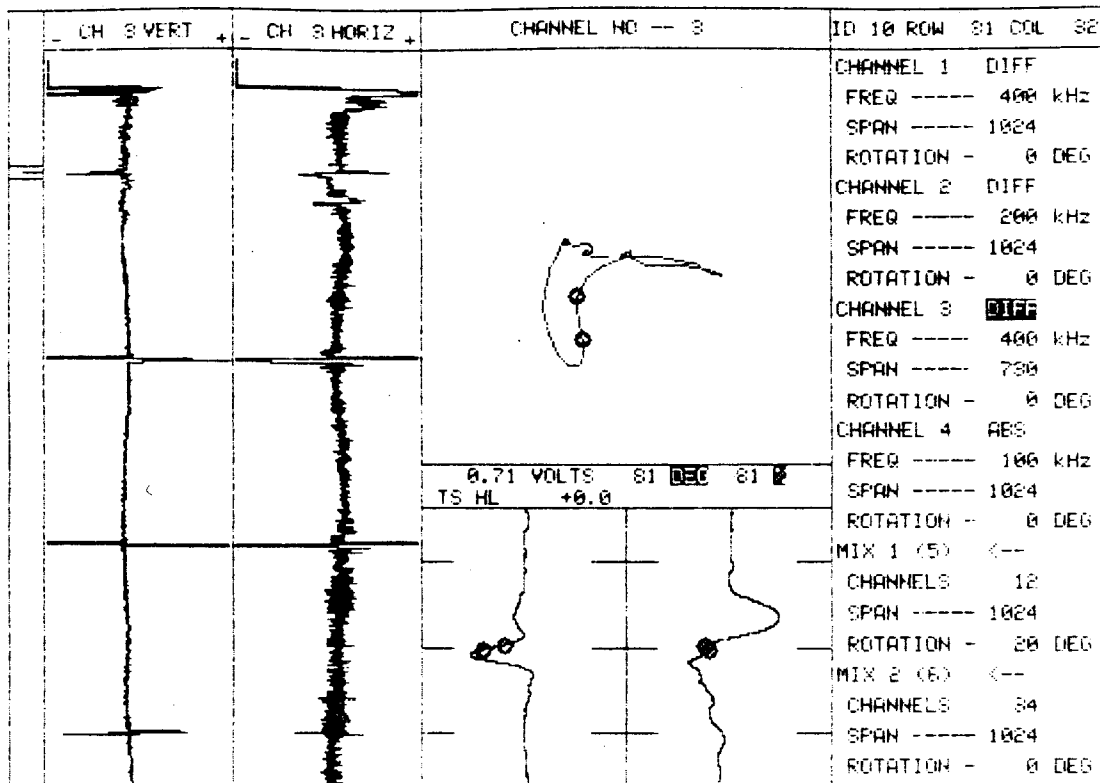
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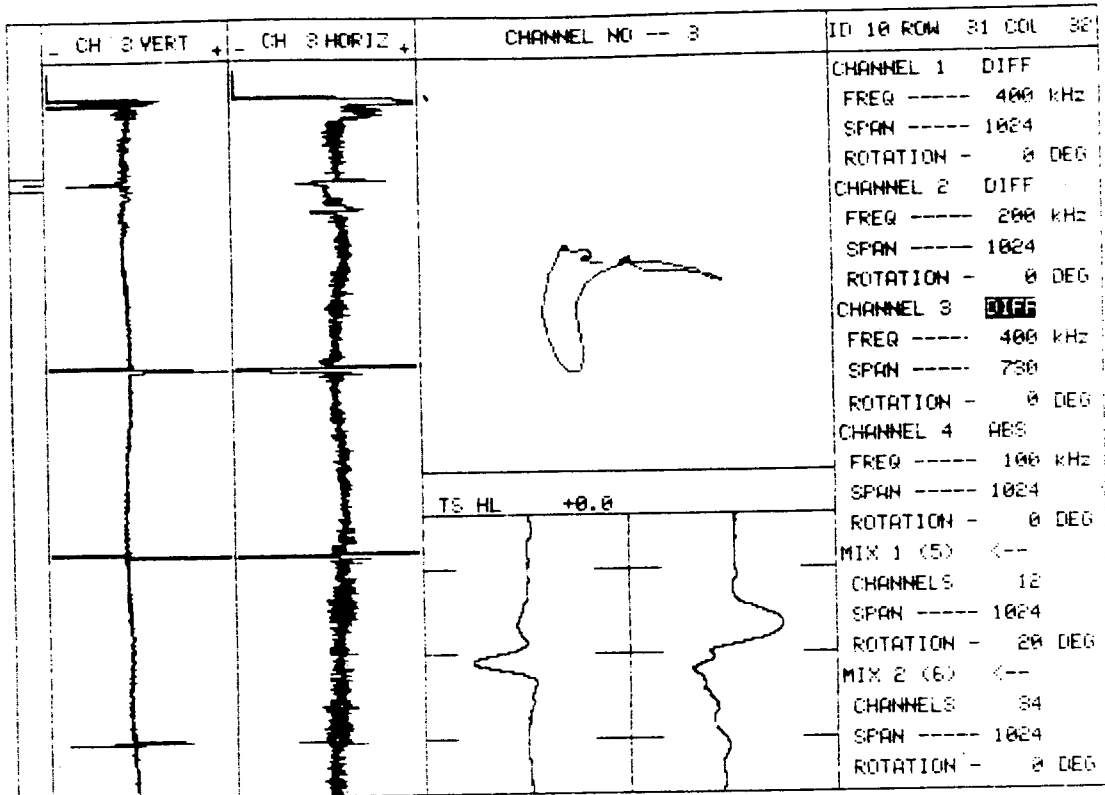
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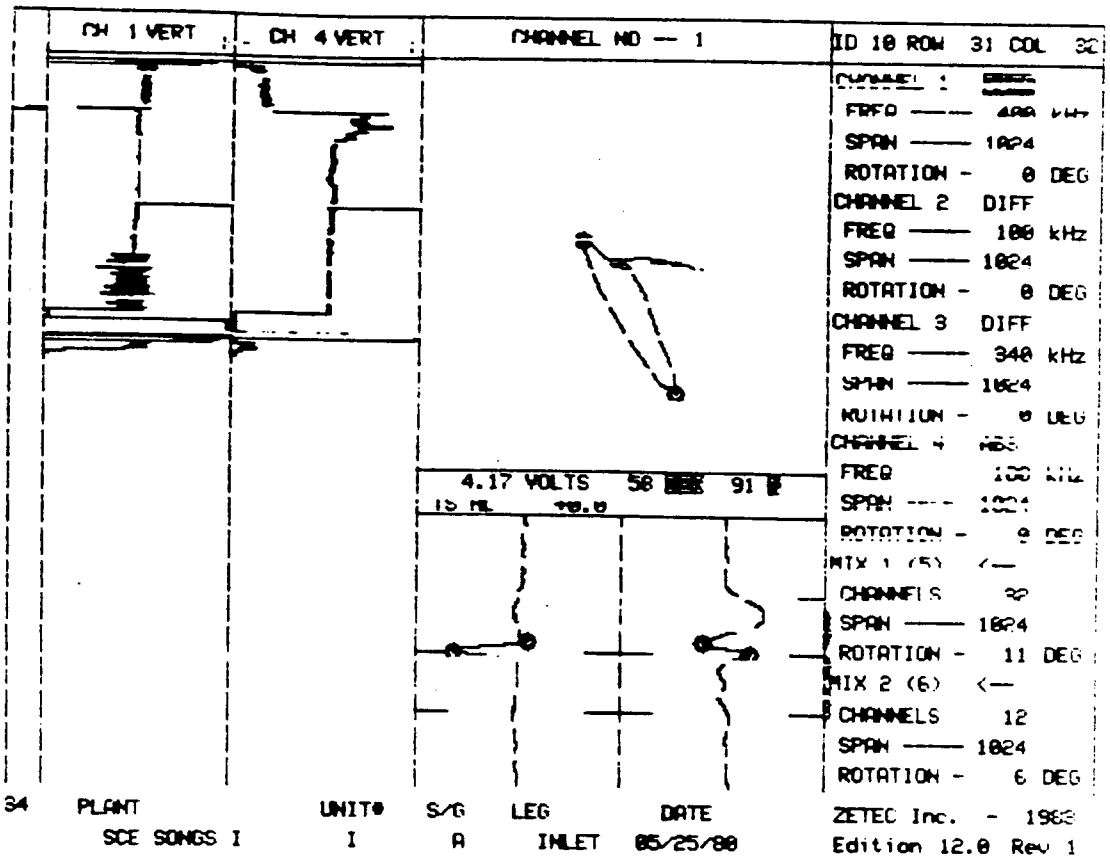
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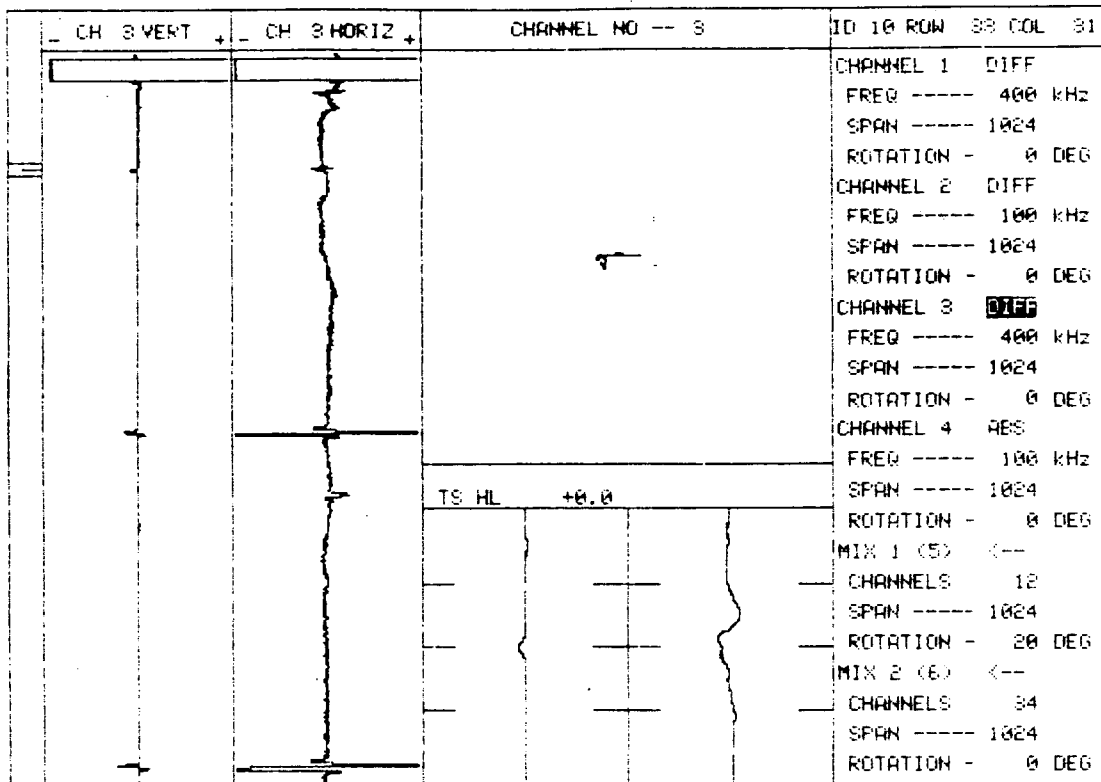
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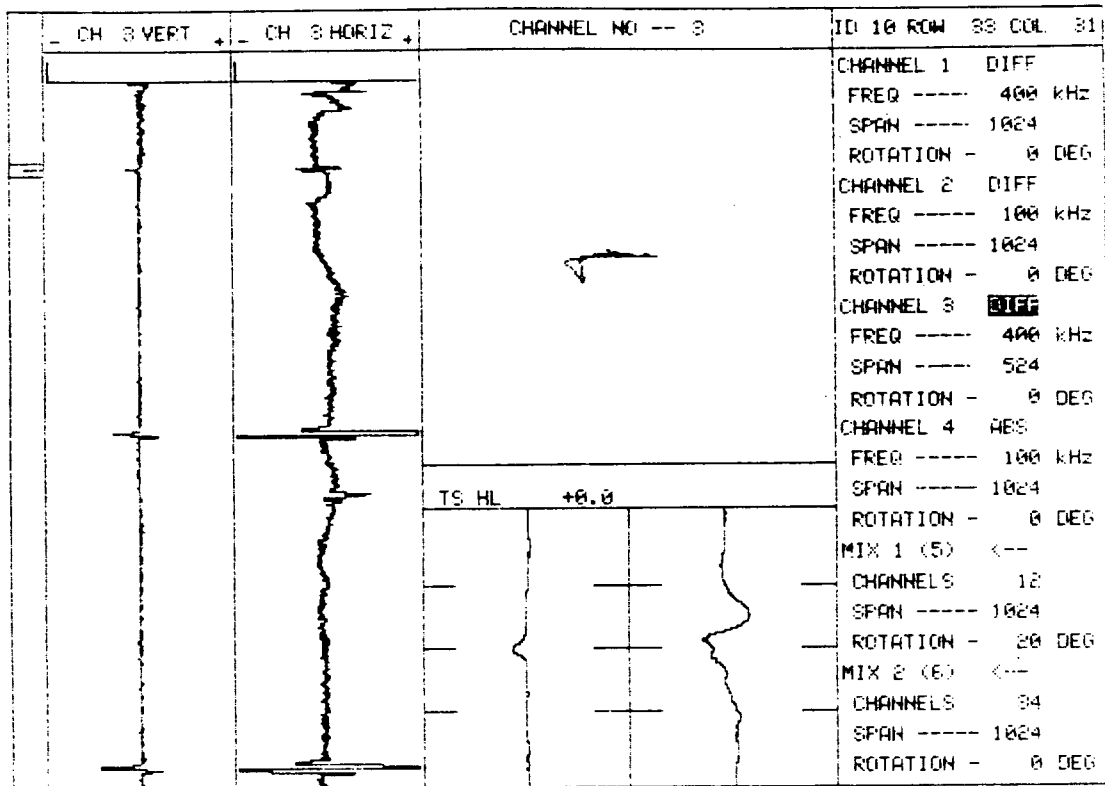
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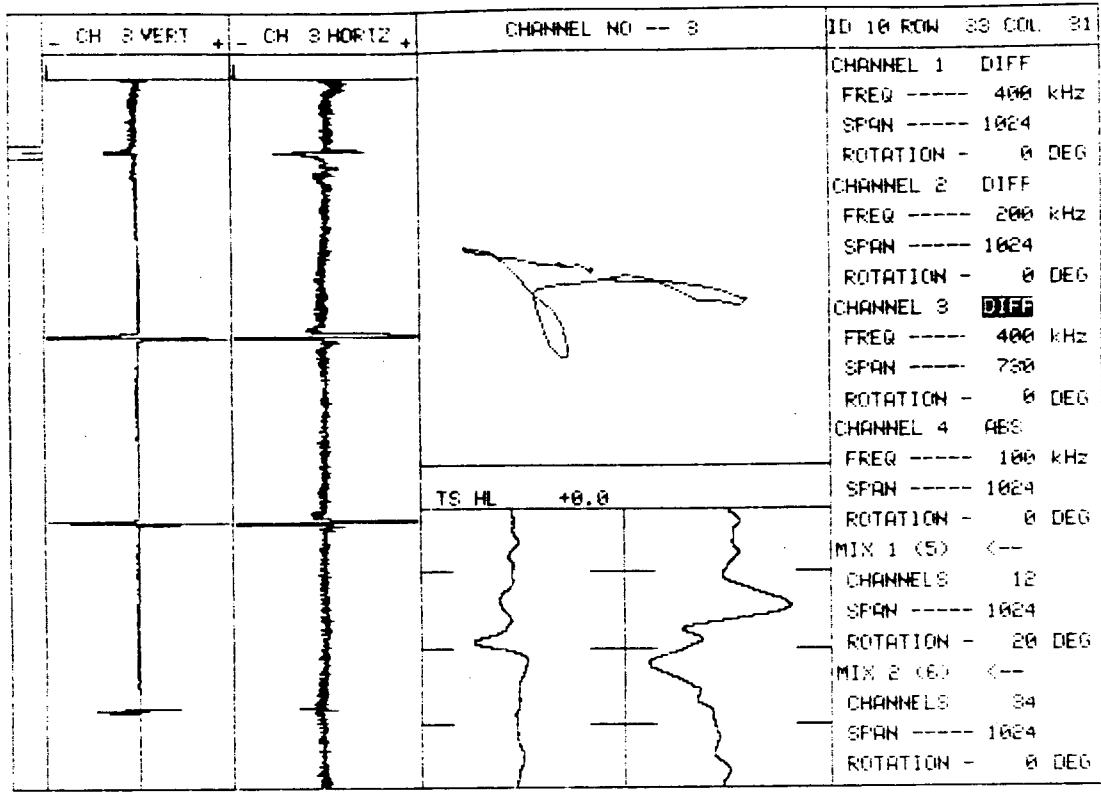
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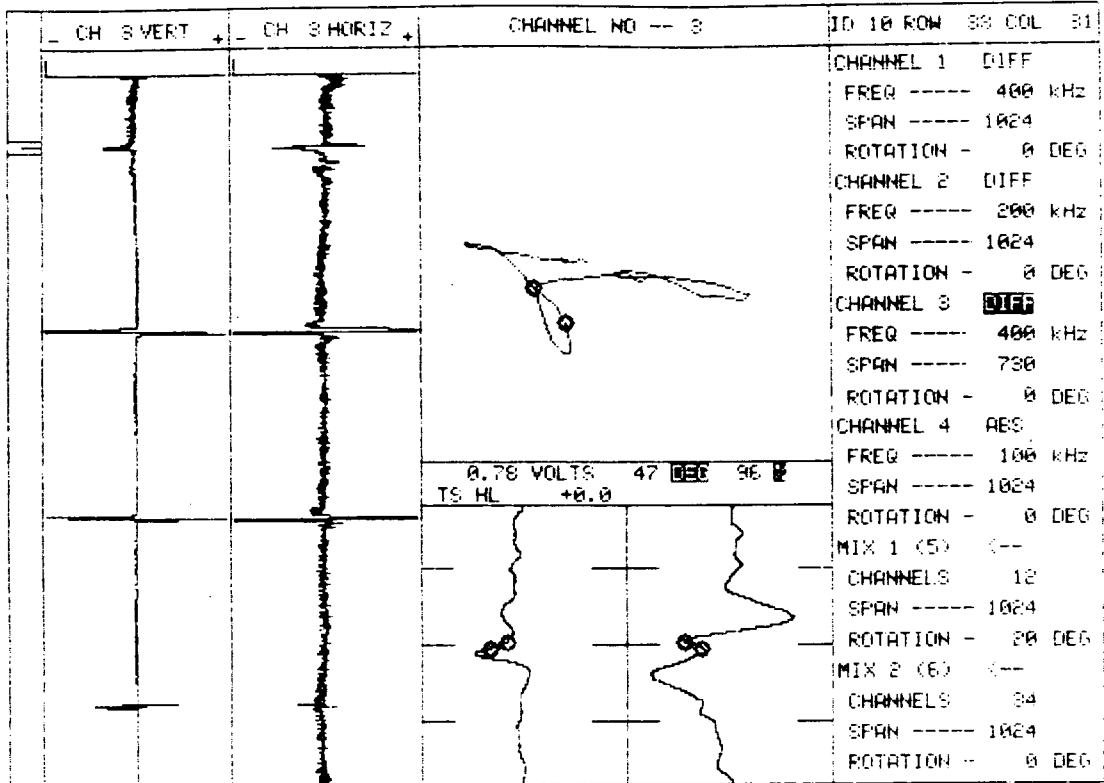
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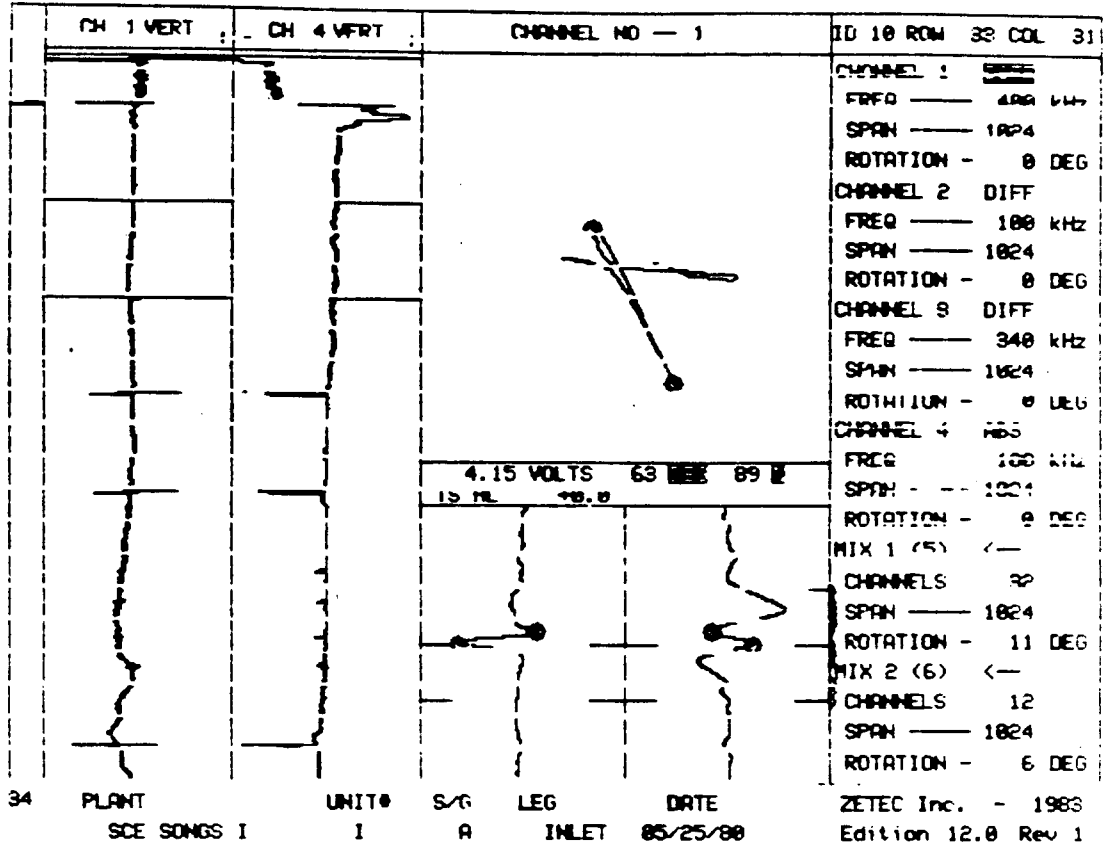
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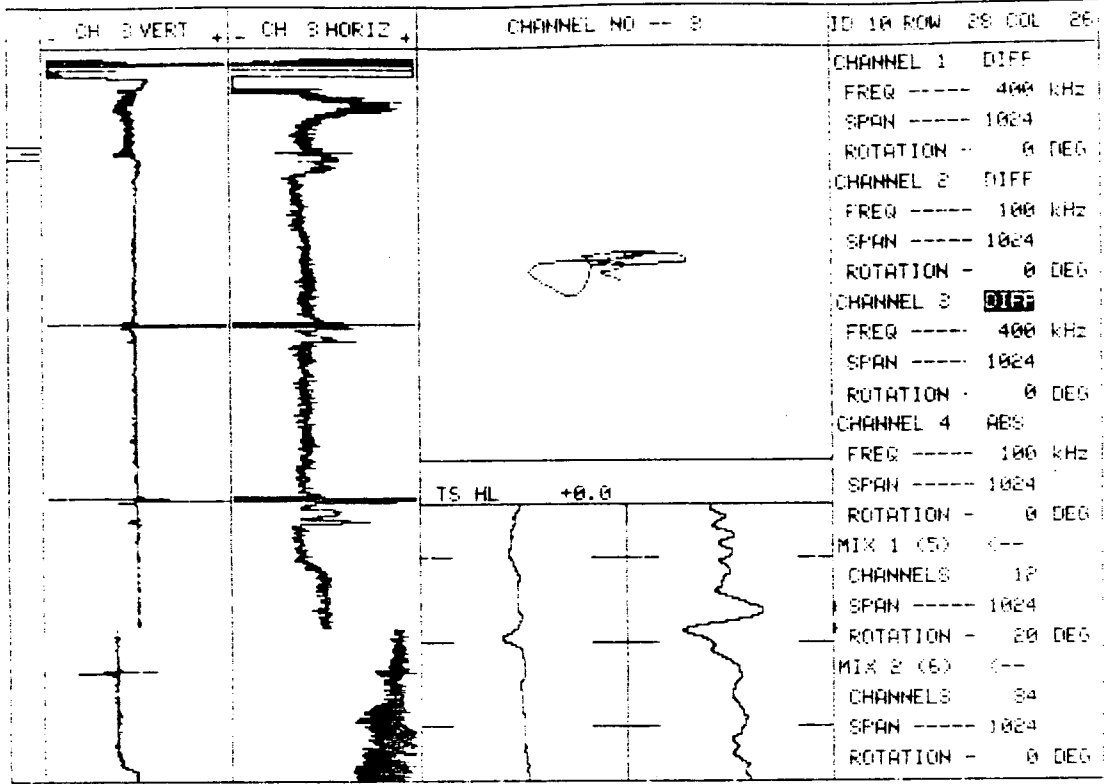


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	SCE SONGS I	I	A	INLET	00/00/77	Edition 12.0 Rev 1

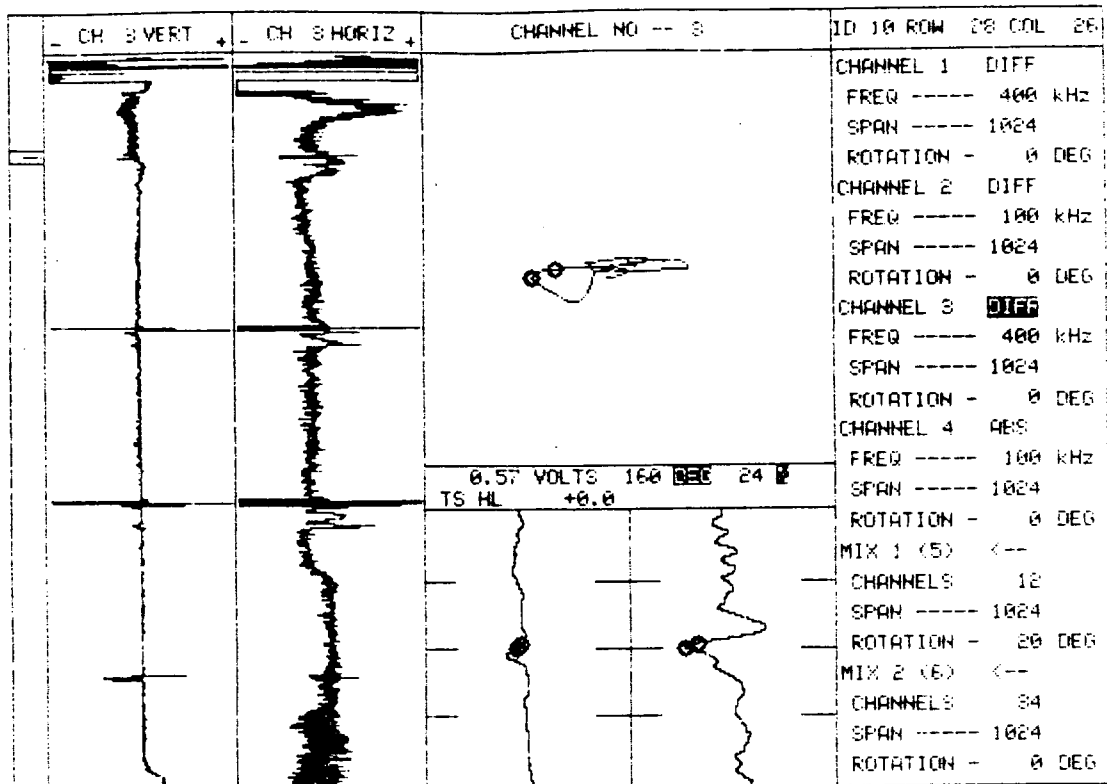


20	PLANT	UNIT#	S/O	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	R	INLET	00/00/77	Edition 12.0 Rev 1

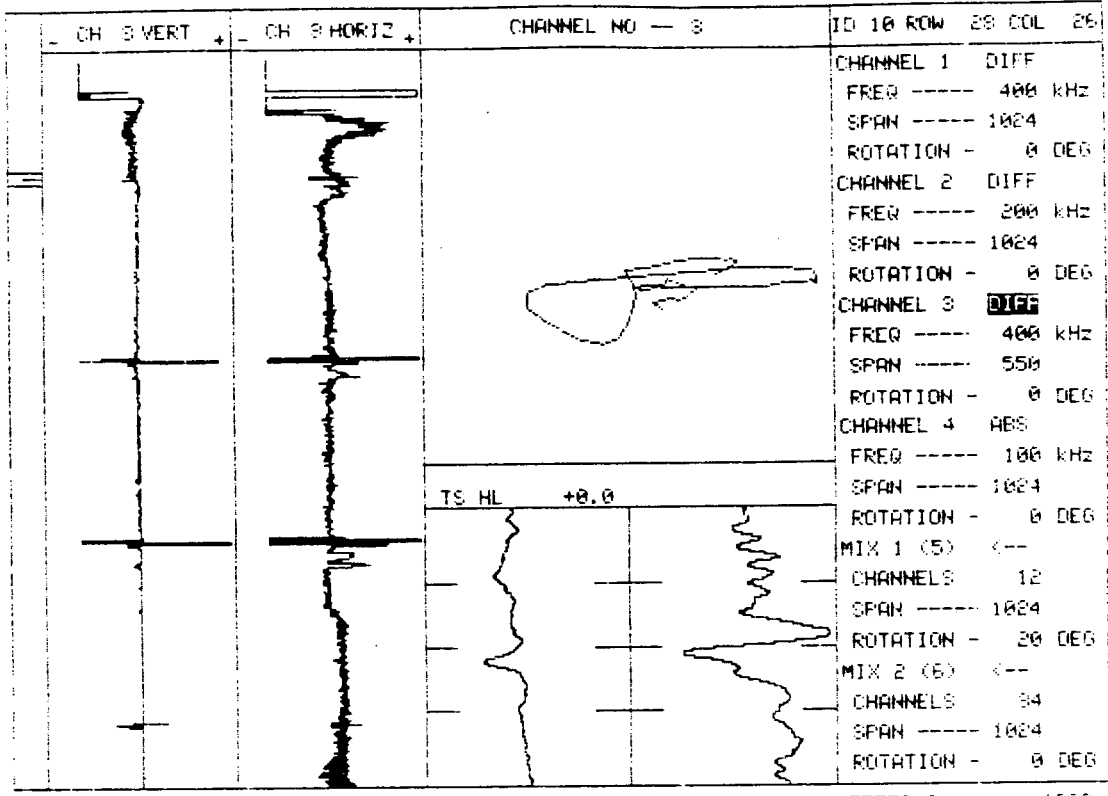




21 PLANT SCE SONGS UNIT# 1 S/O A LEG INLET DATE 05/06/76 ZETEC Inc. - 1988 Edition 12.0 Rev 1

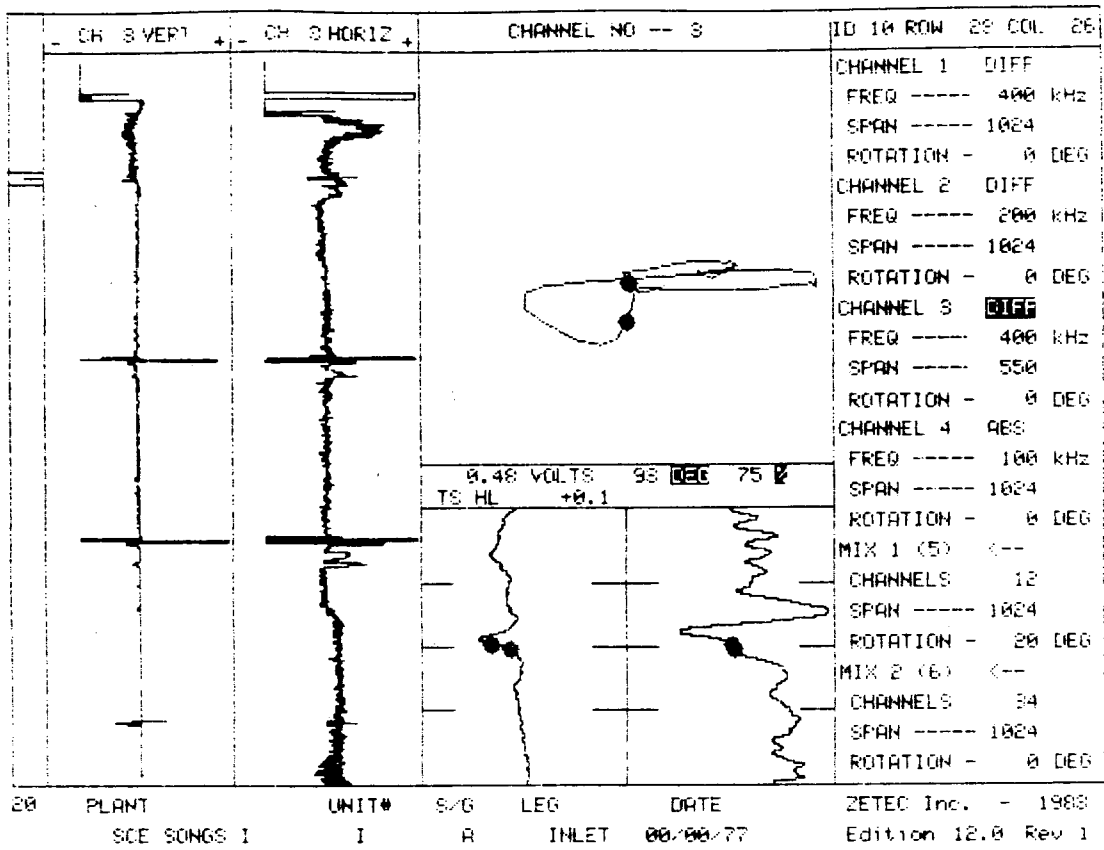


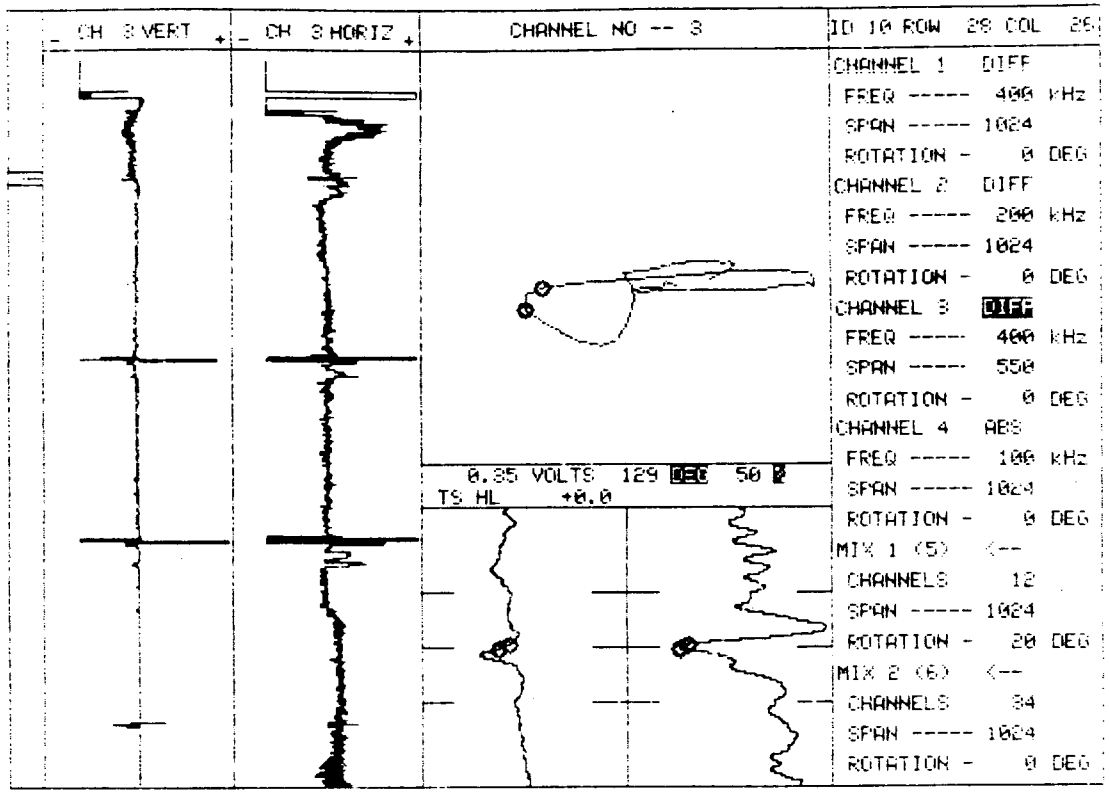
21	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS	1	A	INLET	05/06/76	Edition 12.0 Rev 1



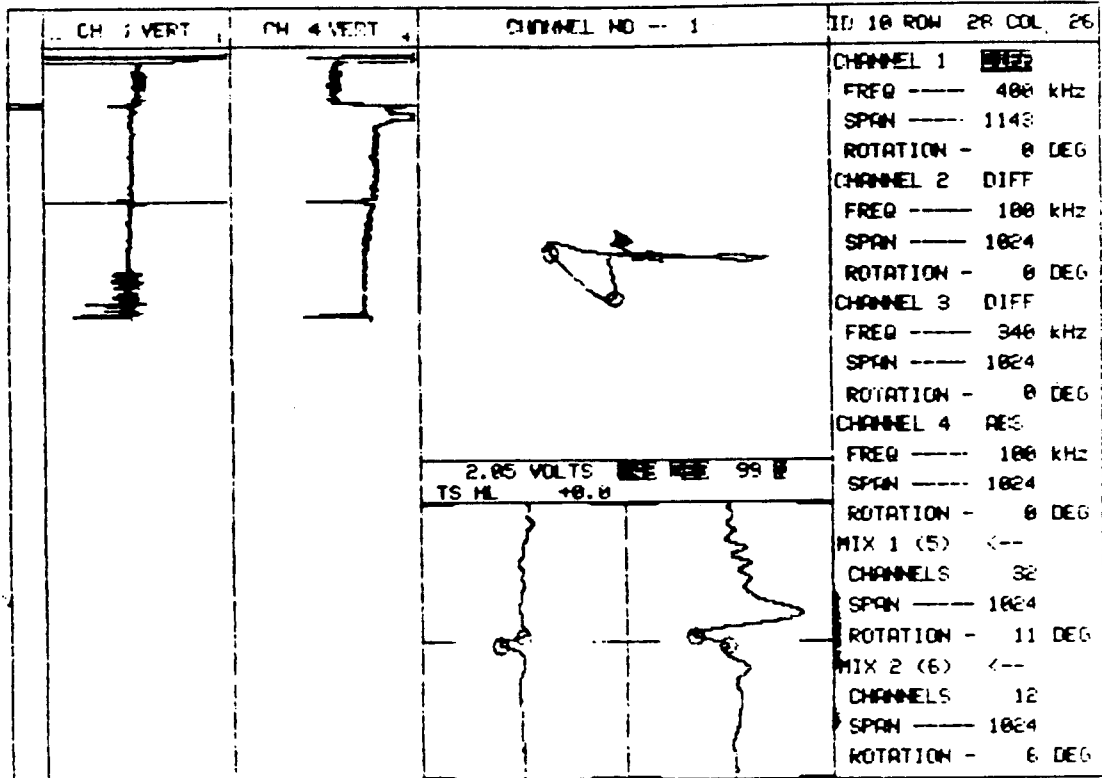
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CHANNEL 1	DIFF			
FREQ	----	400	KHZ	
SPAN	----	1024		
ROTATION	-	0	DEG	
CHANNEL 2	DIFF			
FREQ	----	200	KHZ	
SPAN	----	1024		
ROTATION	-	0	DEG	
CHANNEL 3	DIFF			
FREQ	----	400	KHZ	
SPAN	----	550		
ROTATION	-	0	DEG	
CHANNEL 4	ABS			
FREQ	----	100	KHZ	
SPAN	----	1024		
ROTATION	-	0	DEG	
MIX 1 (5)	<--			
CHANNELS		12		
SPAN	----	1024		
ROTATION	-	20	DEG	
MIX 2 (5)	<--			
CHANNELS		34		
SPAN	----	1024		
ROTATION	-	0	DEG	

20	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	A	INLET	00/00/77	Edition 12.0 Rev 1

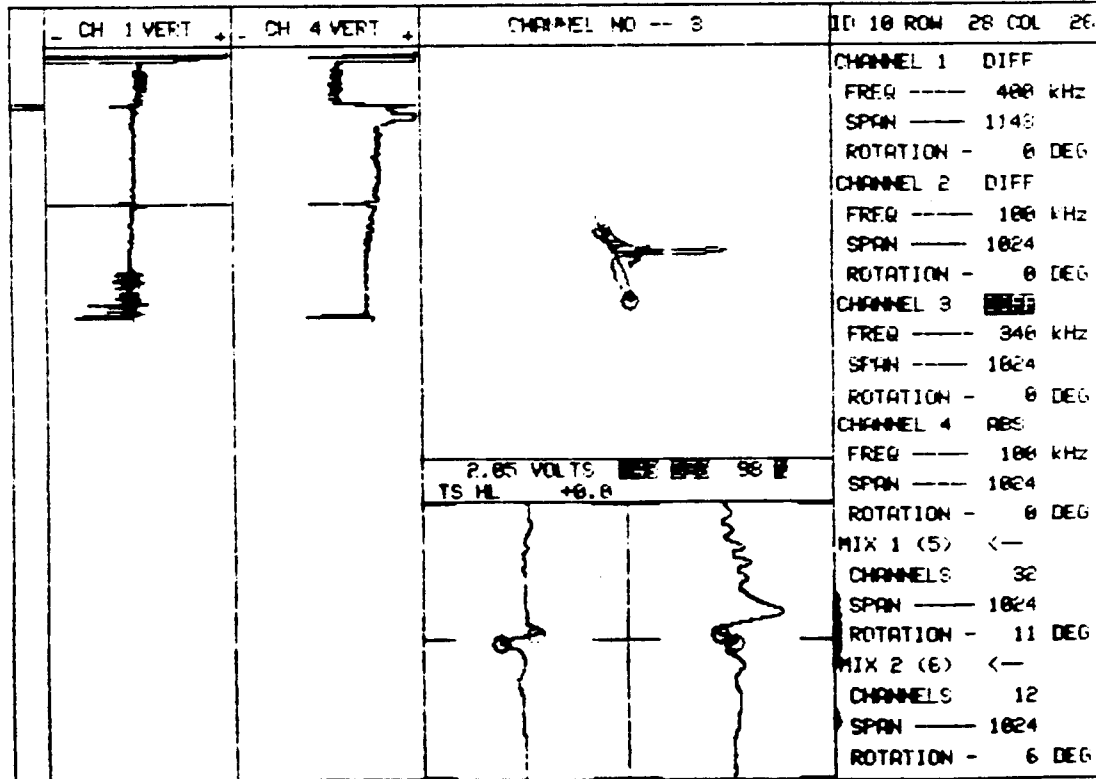




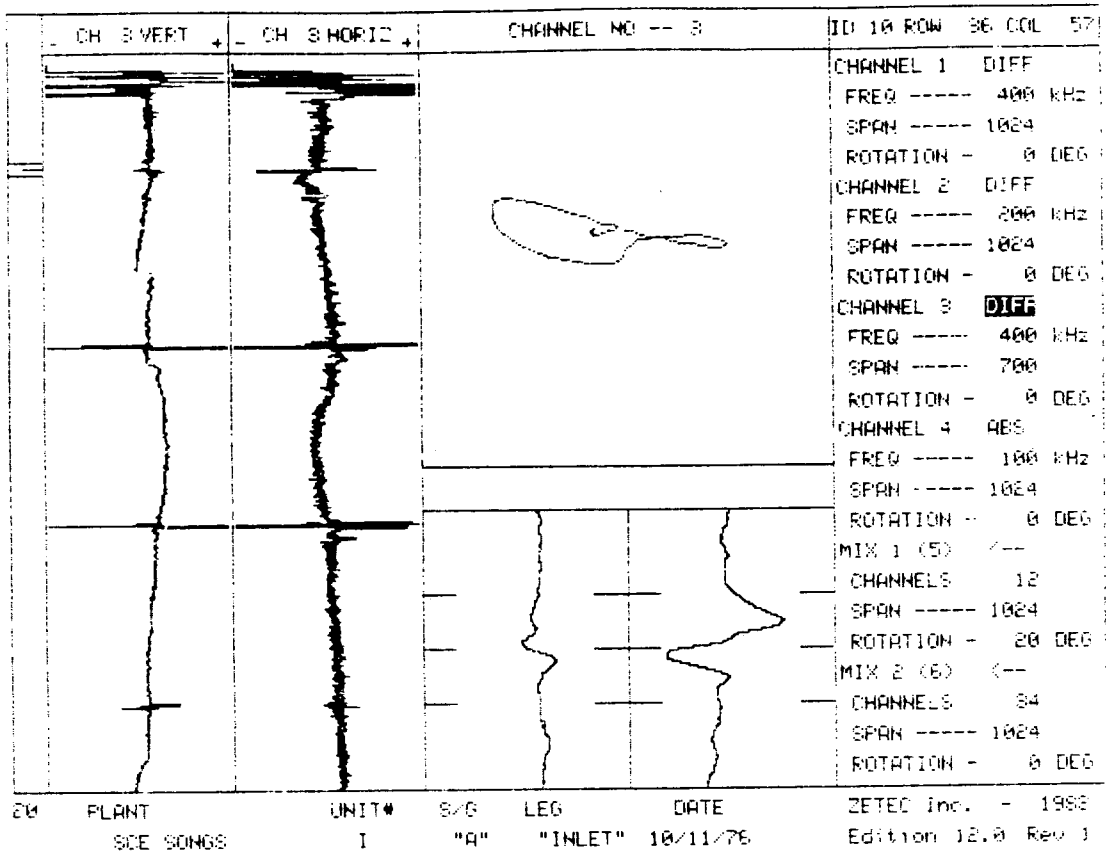
PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 00/00/77 ZETEC Inc. - 1988 Edition 12.0 Rev 1

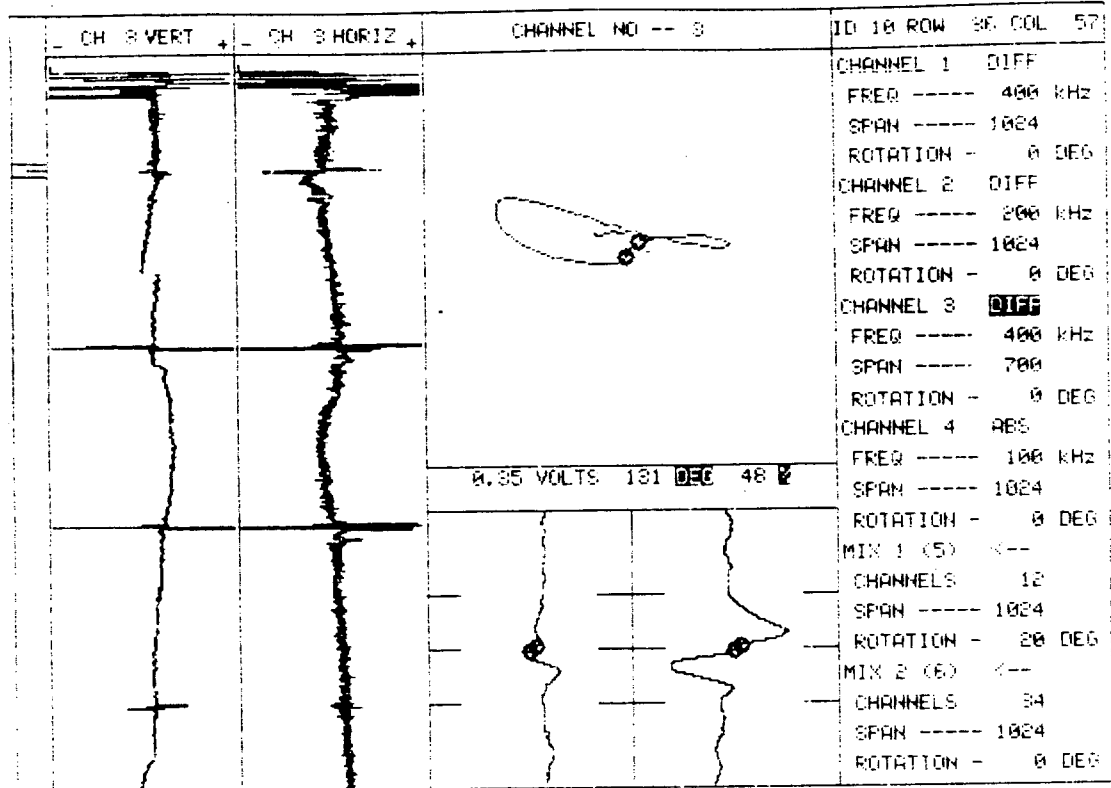


34 PLANT SCE SONGS I UNIT# I S/G "A" LEG INLET DATE 05/25/80 ZETEC Inc. - 1983 Edition 12.0 Rev 1

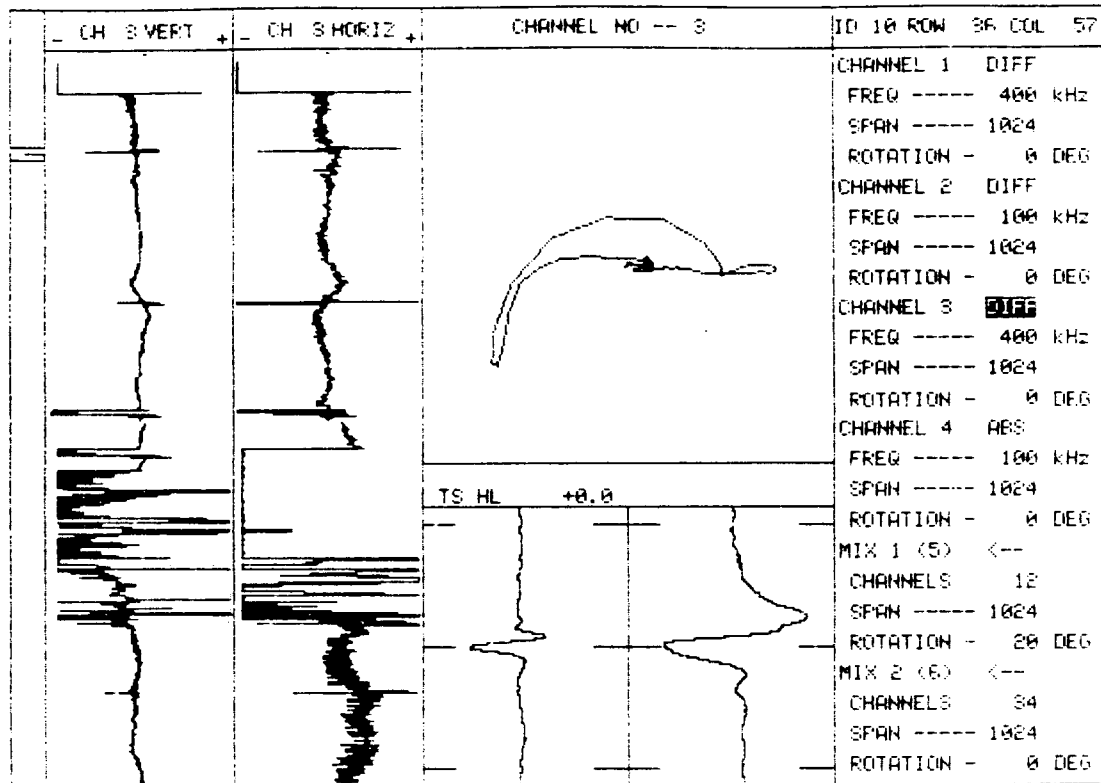


34 PLANT SCE SONGS I UNIT# I S/G "A" LEG INLET DATE 05/25/80 ZETEC Inc. - 1983 Edition 12.0 Rev 1

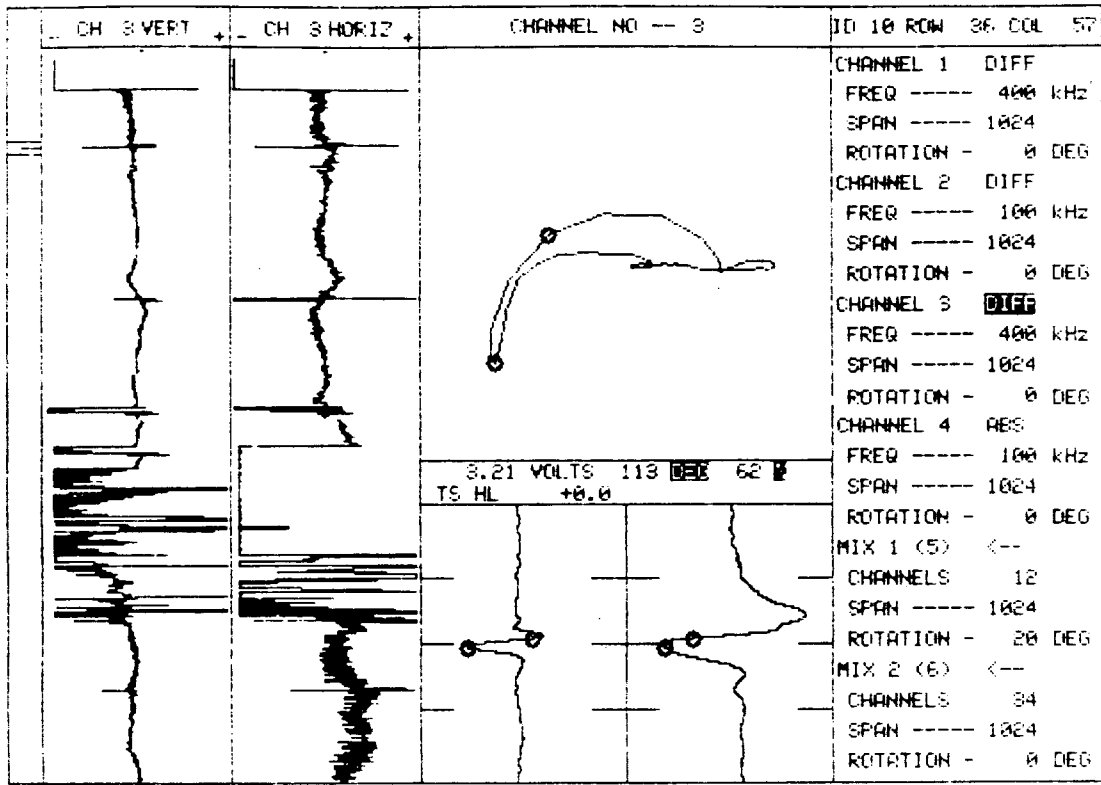




PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
SCE SONGS	1	"A"	"INLET"	10/11/76	Edition 12.0 Rev 1

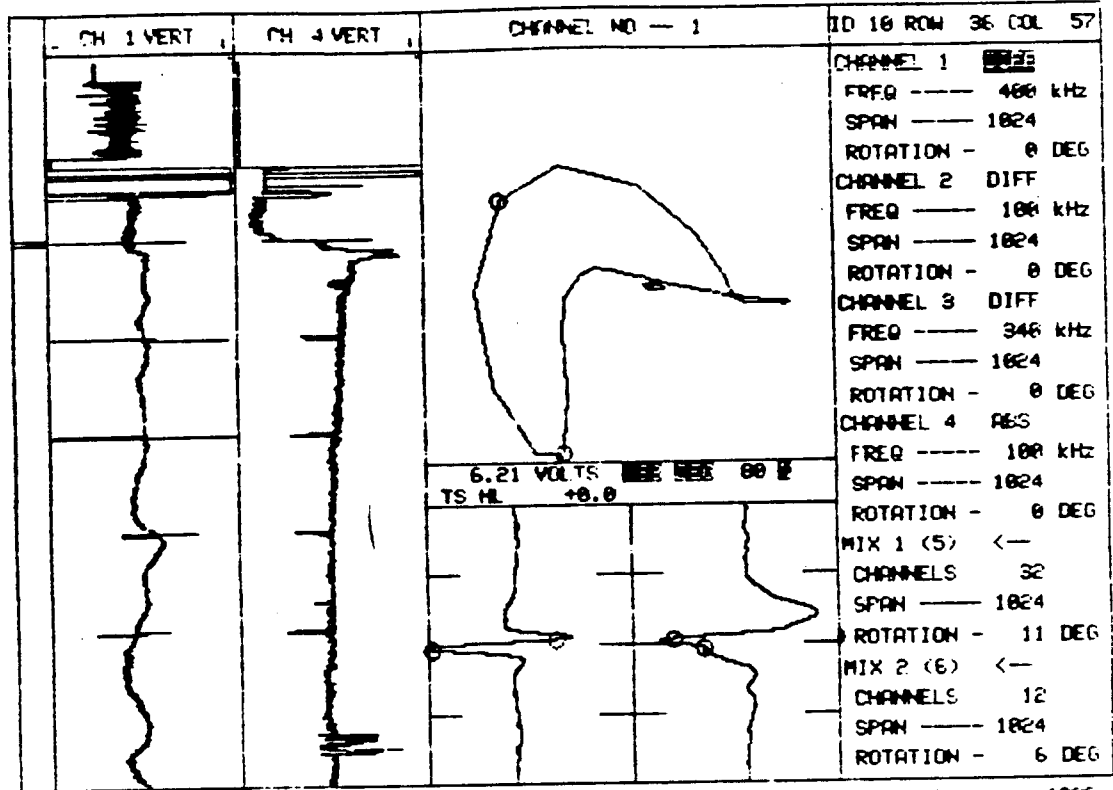


21	PLANT	UNIT#	S/O	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS	1	A	INLET	05/00/79	Edition 12.0 Rev 1



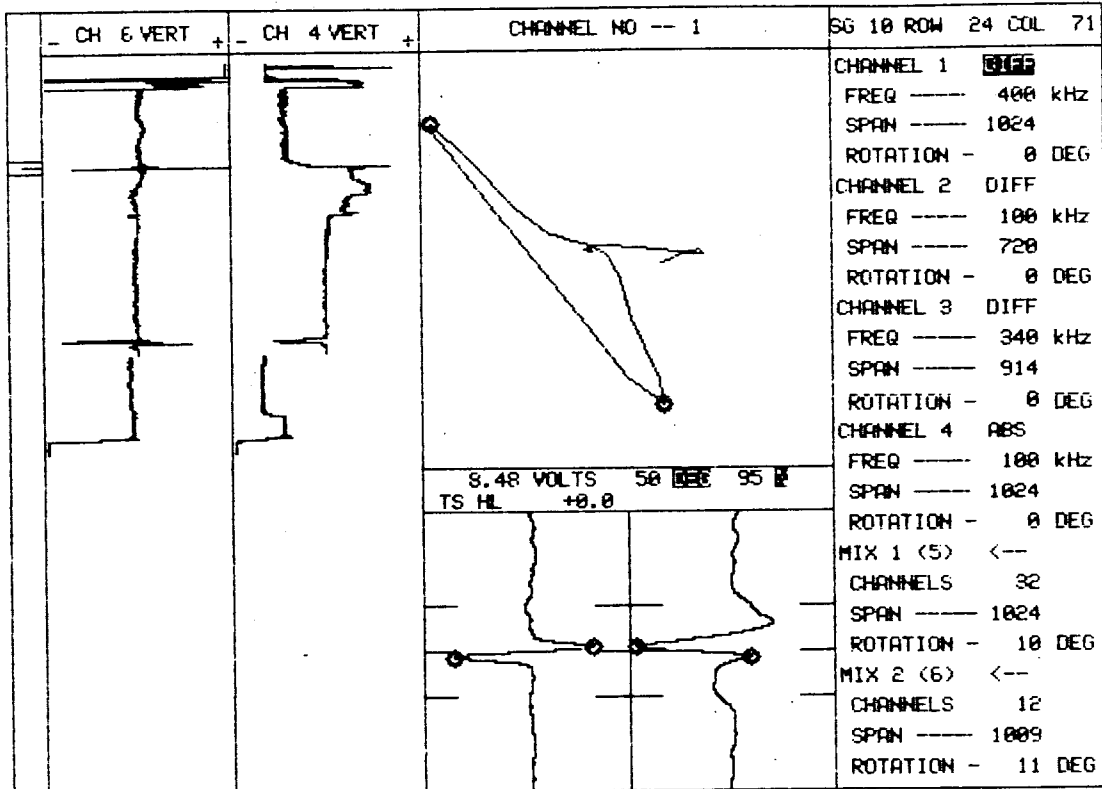
3.21 VOLTS 113 DEG 62
TS HL +0.0

21	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS	1	A	INLET	05/00/79	Edition 12.0 Rev 1

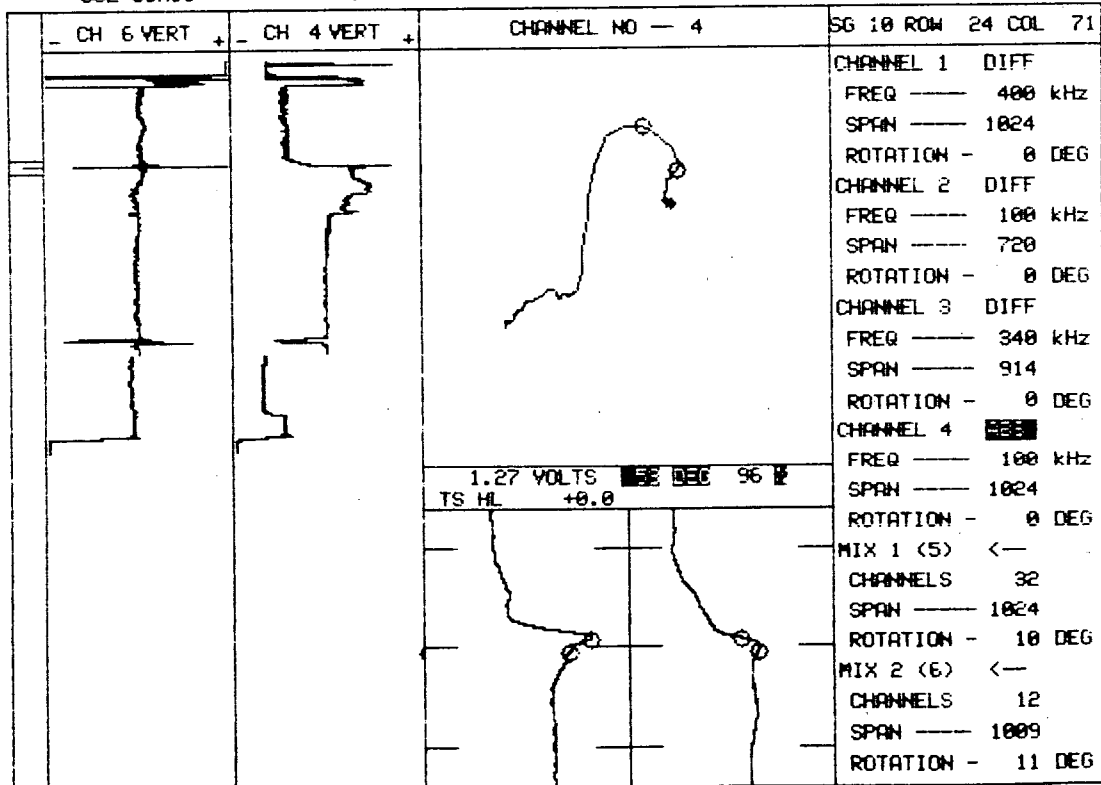


34	PLANT	UNIT#	S/G	LES	DATE	ZETEC Inc. - 1980
	SCE SONGS I	I	A	INLET	05/25/80	Edition 12.0 Rev 1

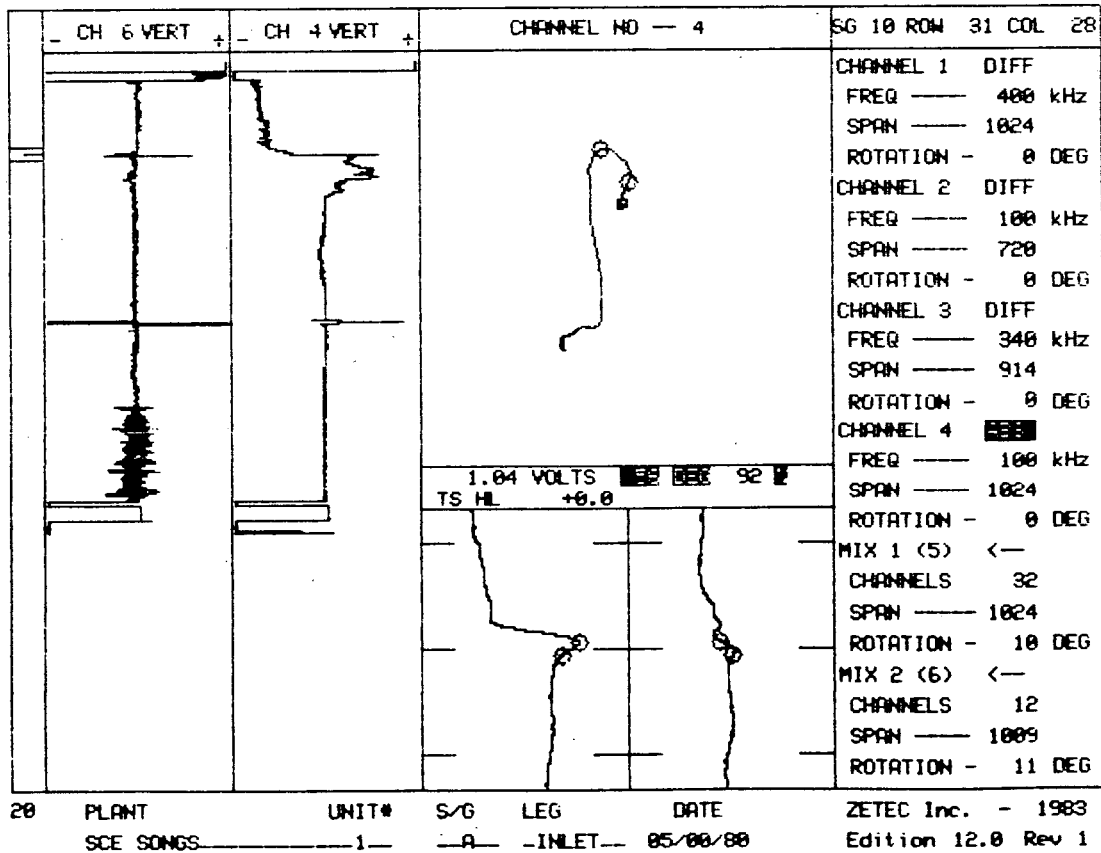
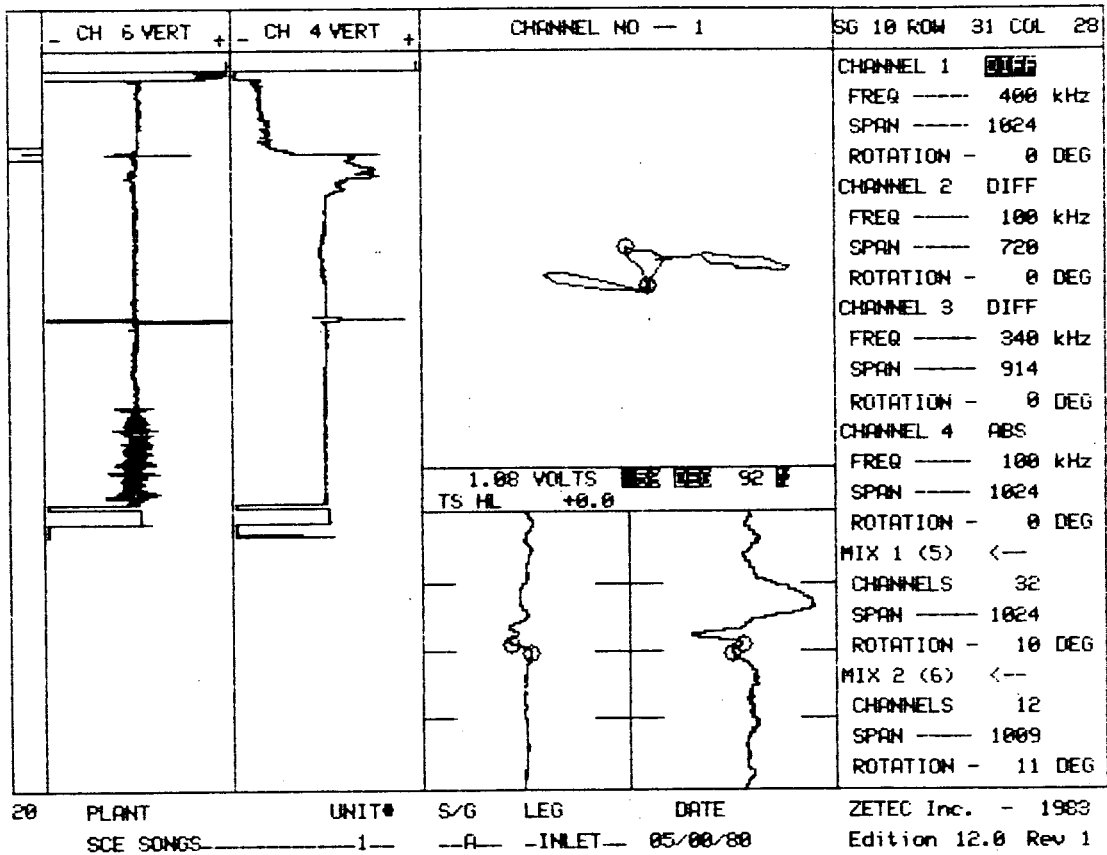
APPENDIX B

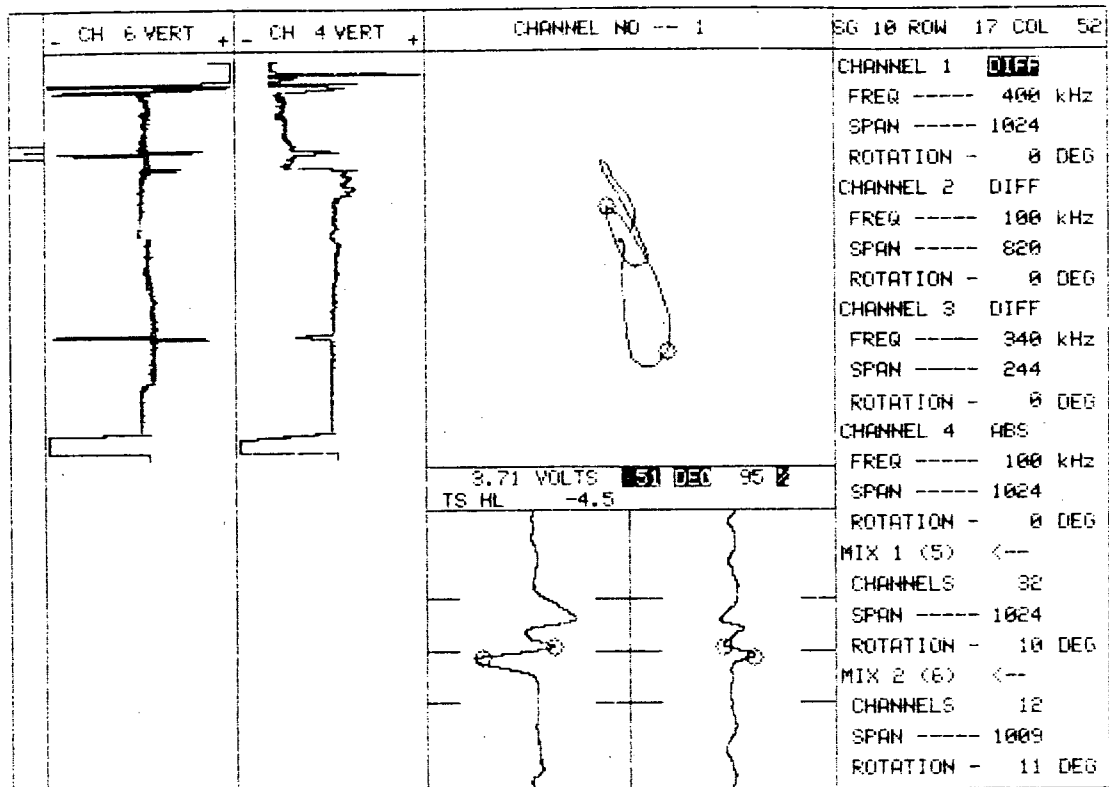


20 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1983
SCE SONGS 1 - A - INLET 05/00/80 Edition 12.0 Rev 1

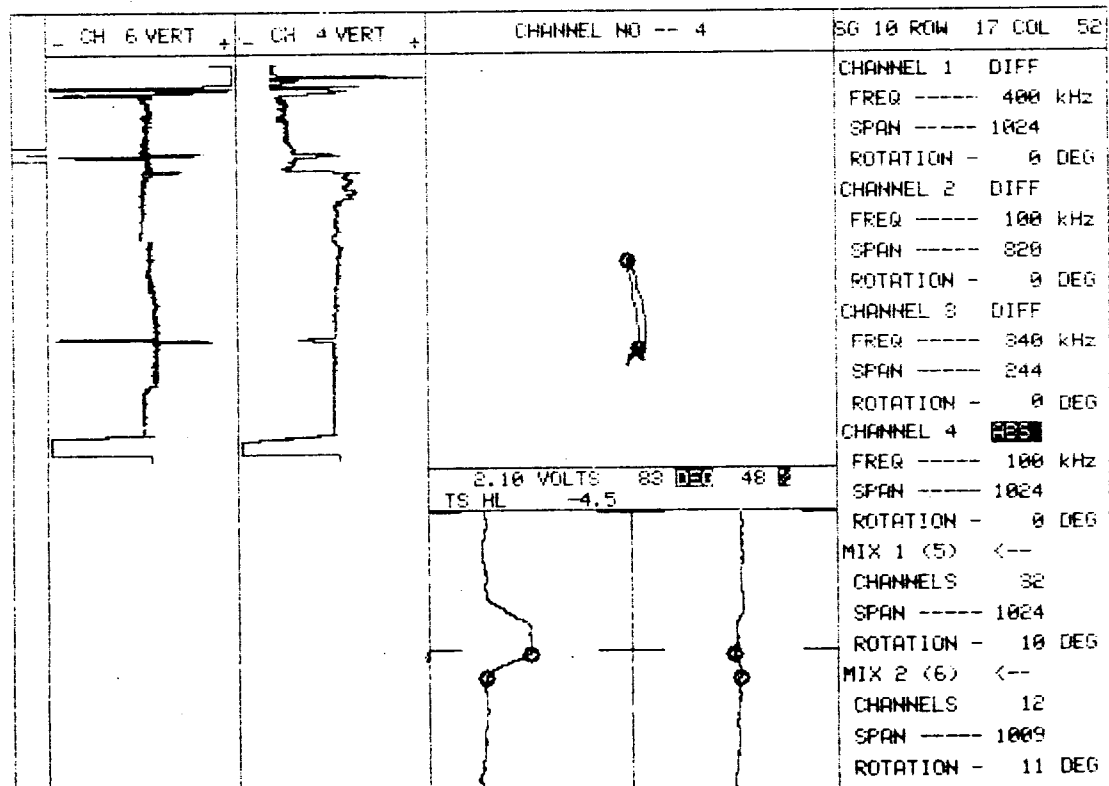


20 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1983
SCE SONGS 1 - A - INLET 05/00/80 Edition 12.0 Rev 1

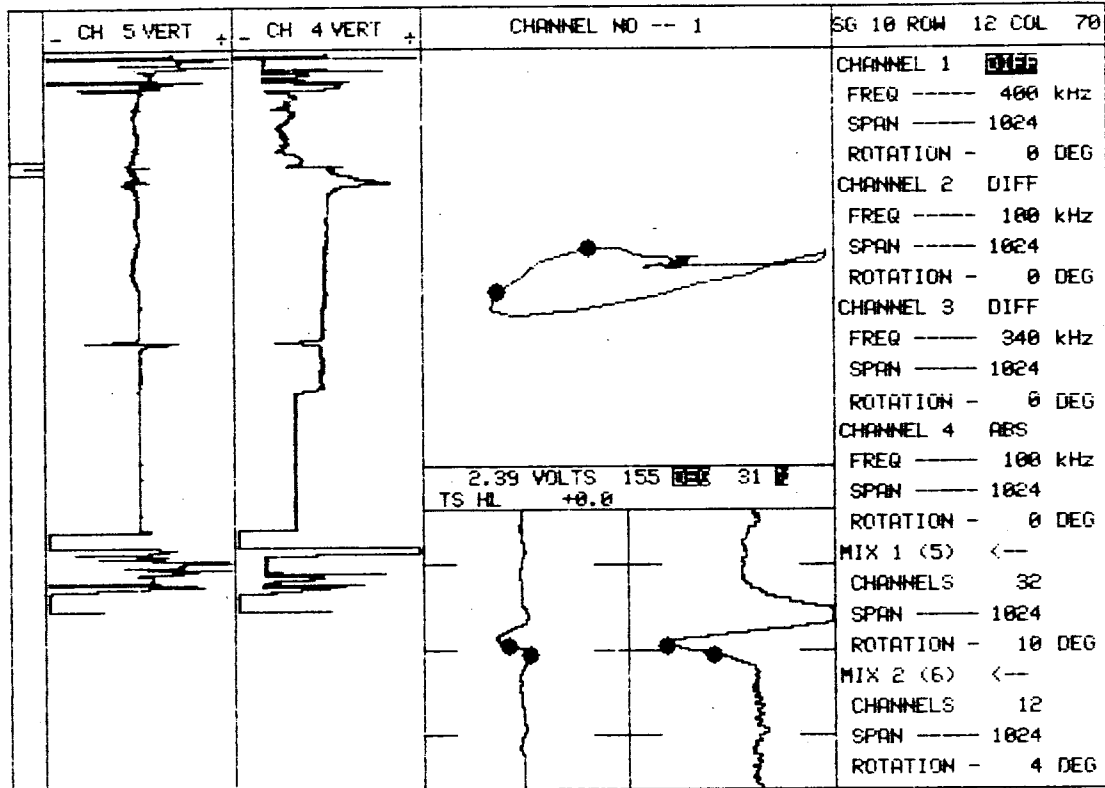




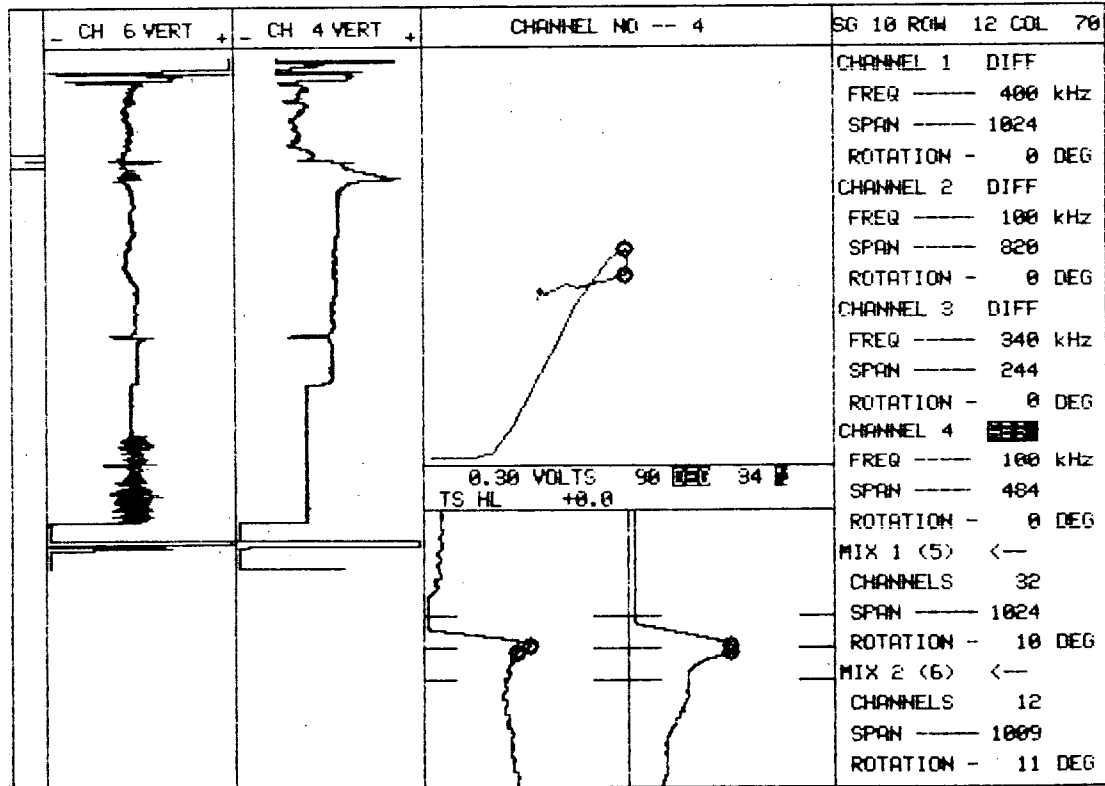
20 PLANT SCE SONGS-----1-- UNIT# 1 S/G --A-- LEG -INLET-- DATE 05/00/00 ZETEC Inc. - 1983 Edition 12.0 Rev 1



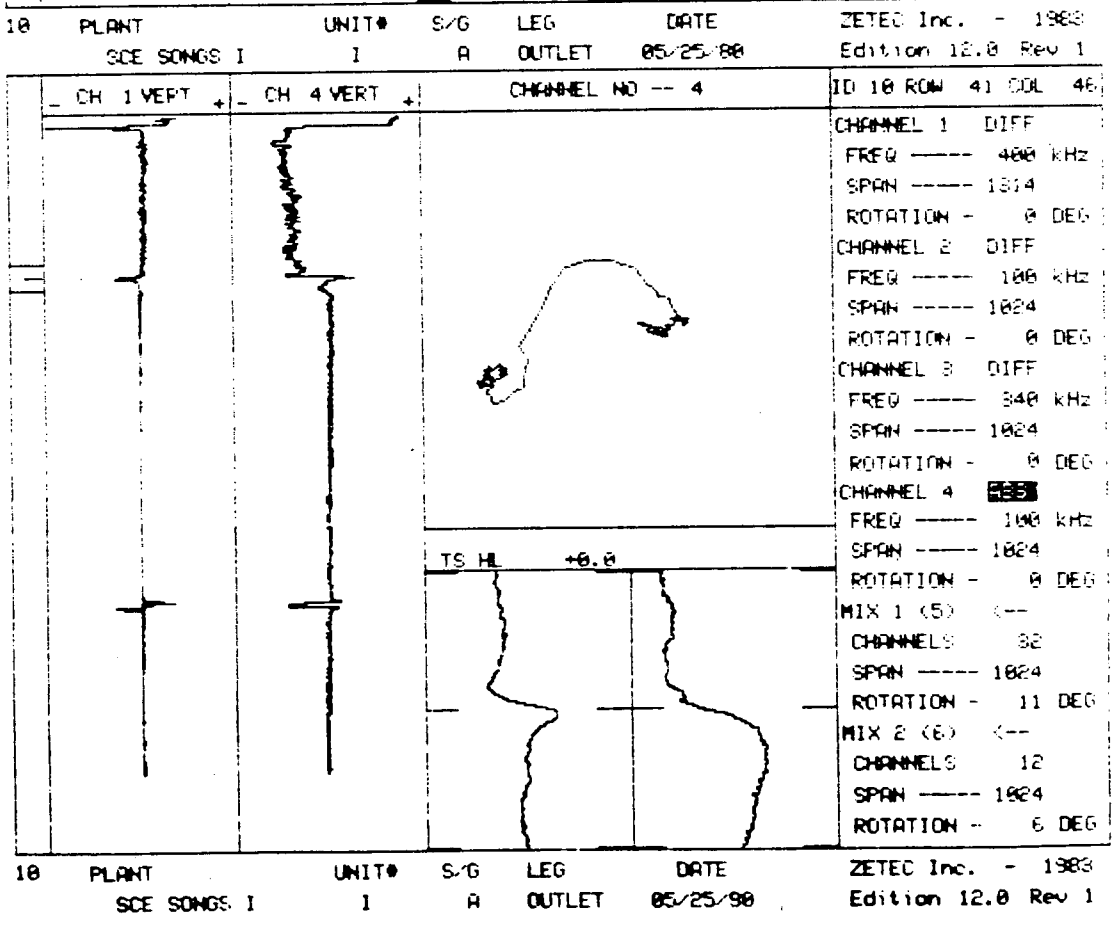
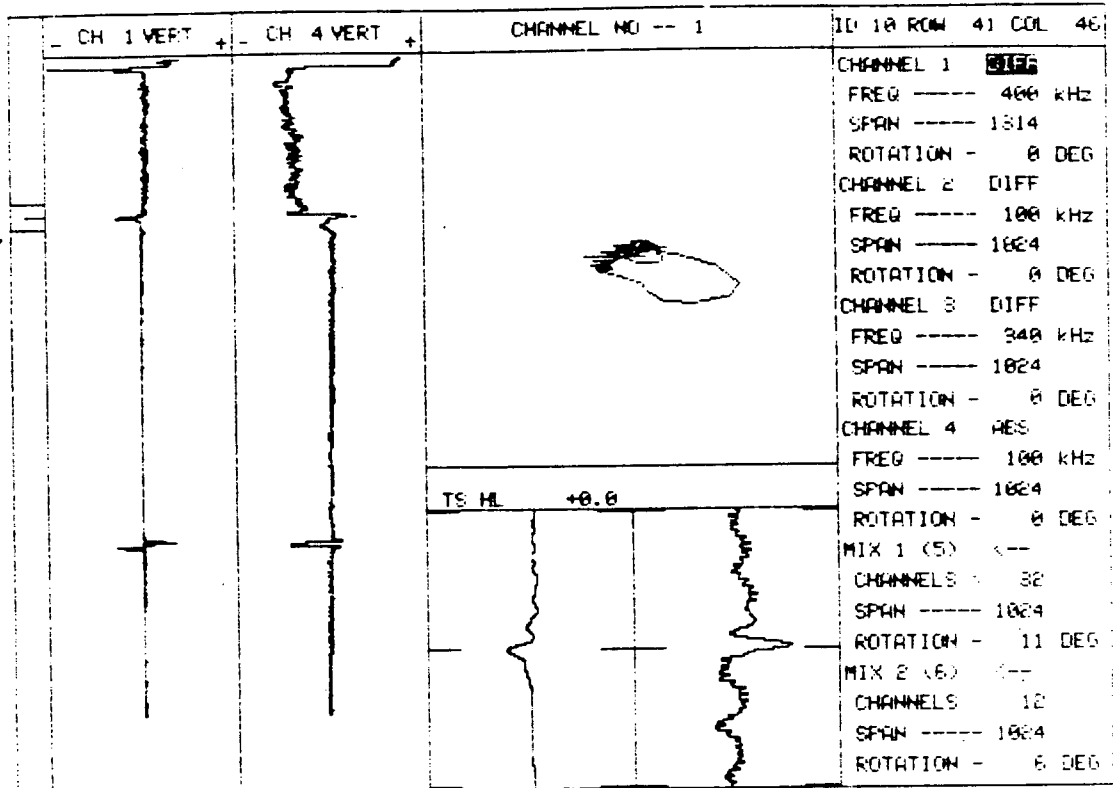
20 PLANT SCE SONGS-----1-- UNIT# 1 S/G --A-- LEG -INLET-- DATE 05/00/00 ZETEC Inc. - 1983 Edition 12.0 Rev 1

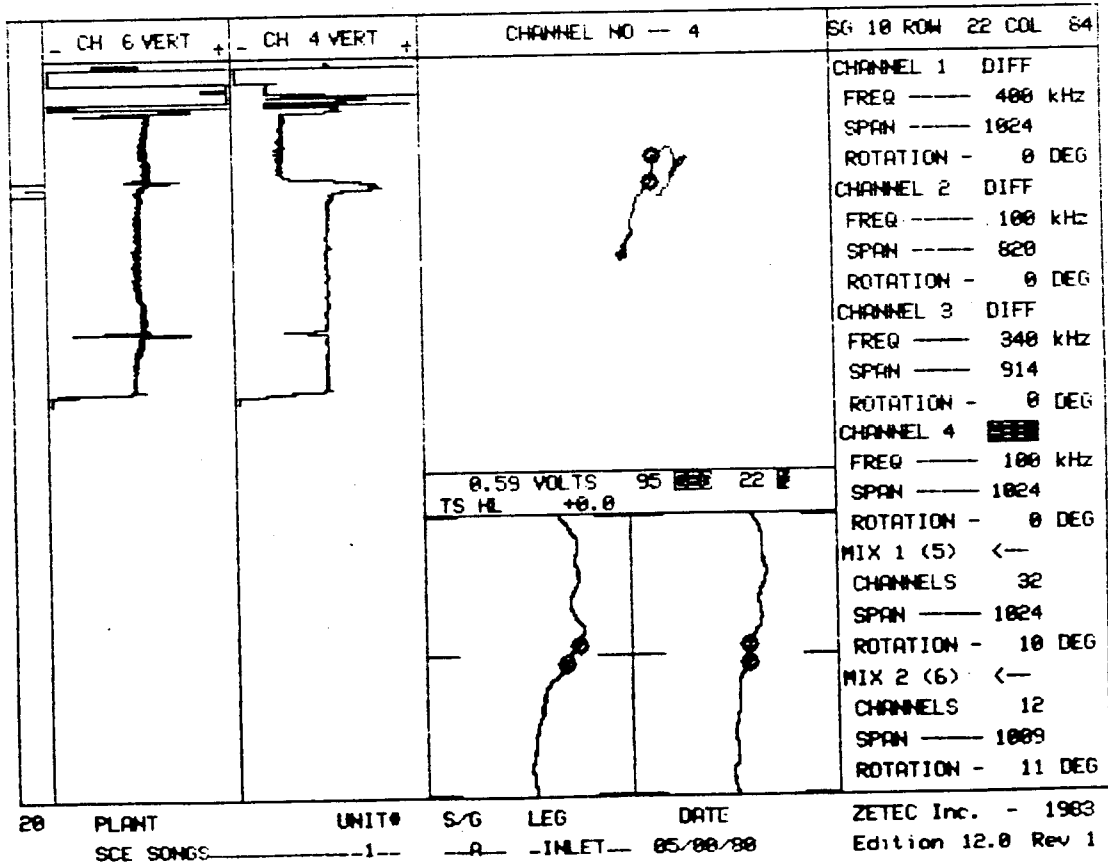
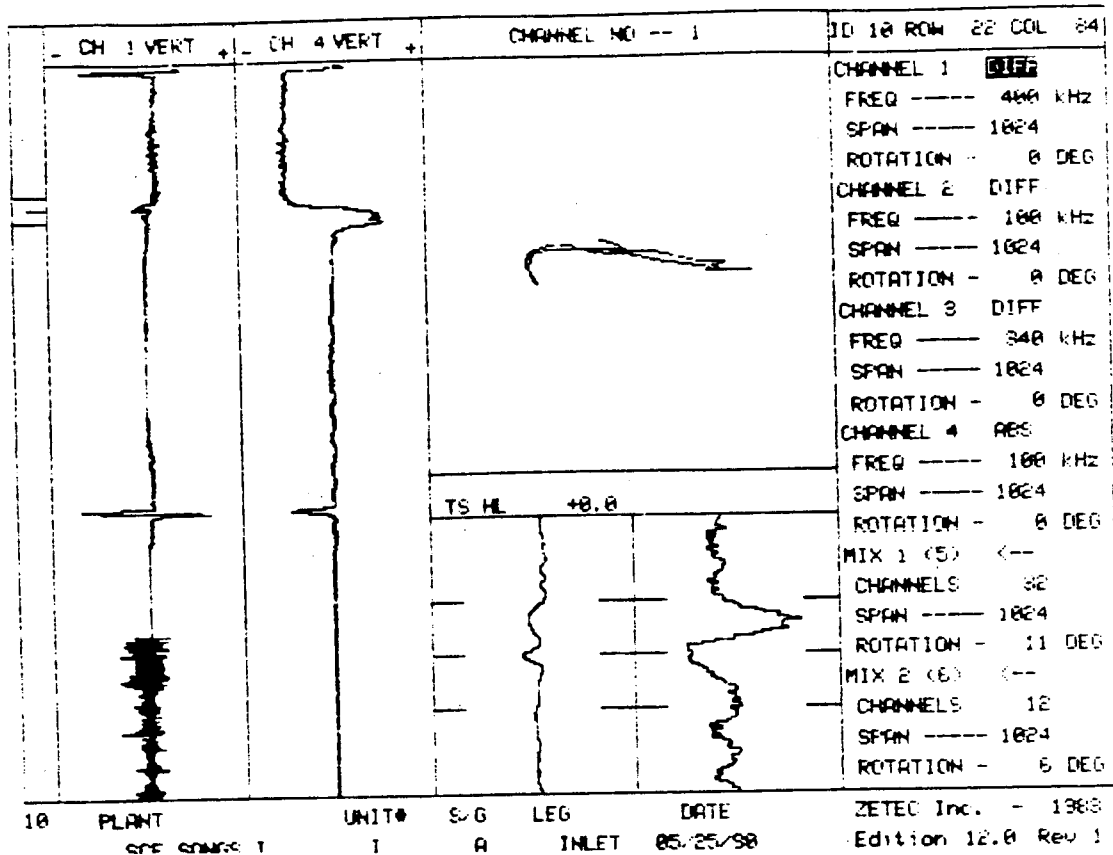


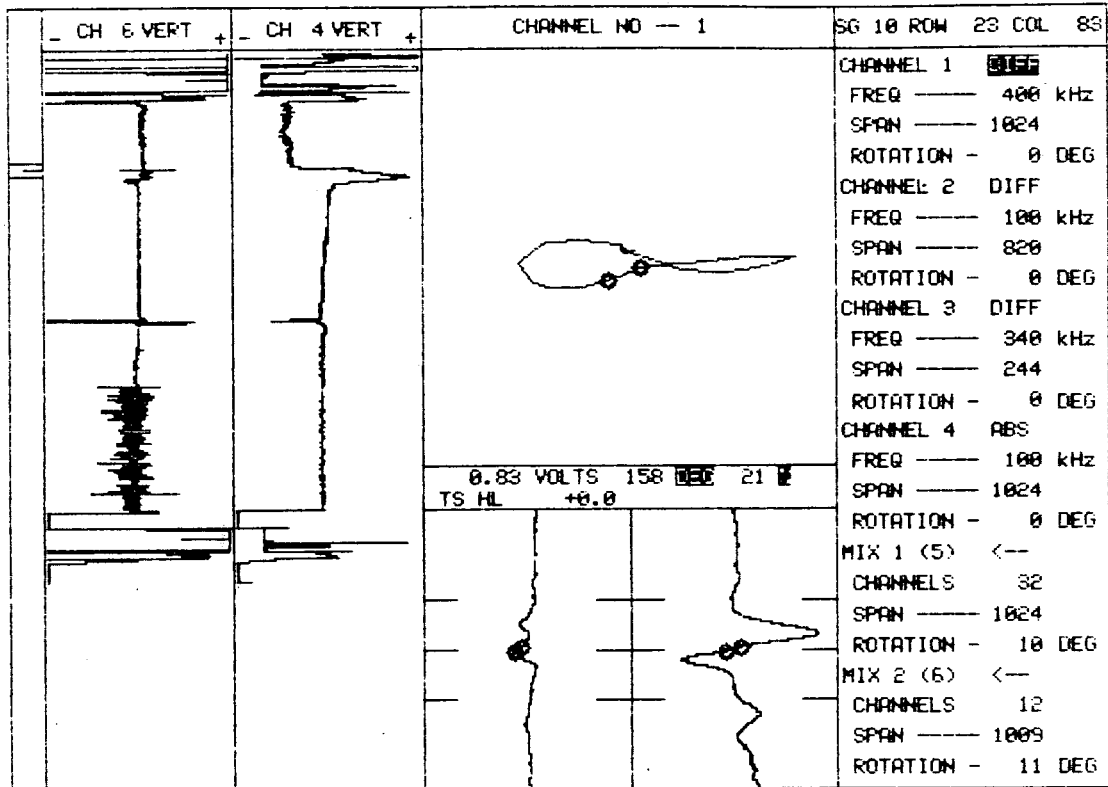
20 PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 05/25/80 ZETEC Inc. - 1983 Edition 12.0 Rev 1



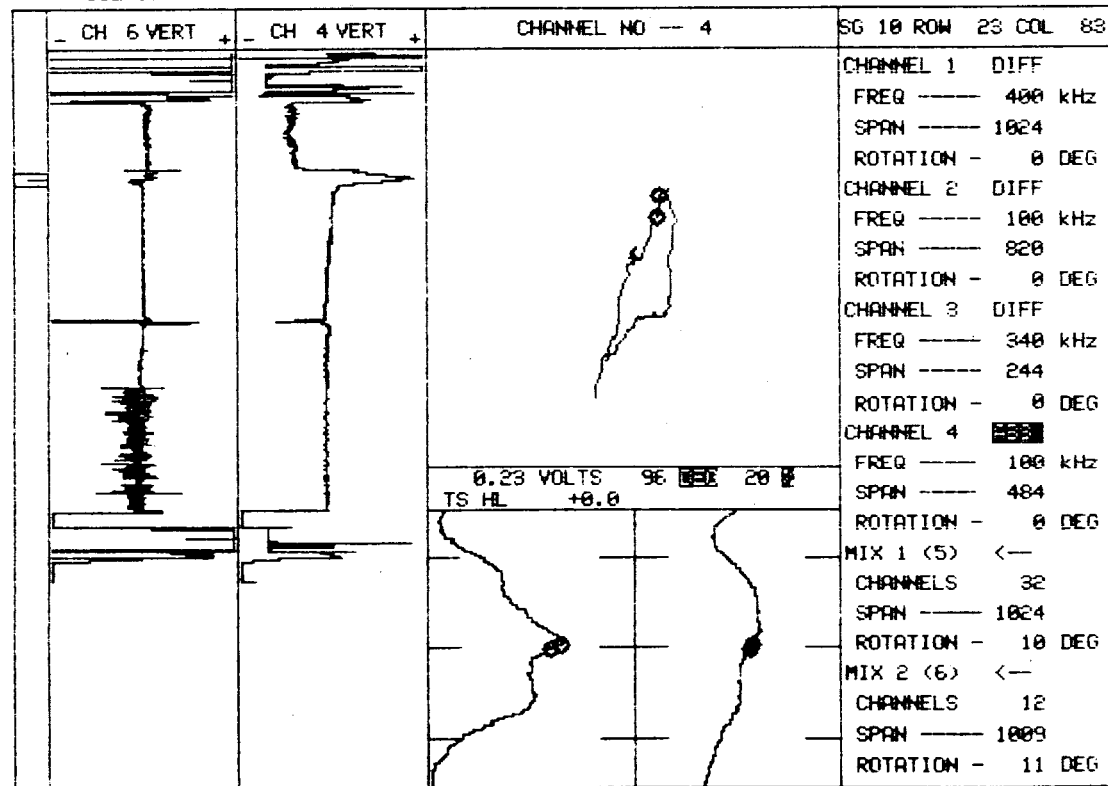
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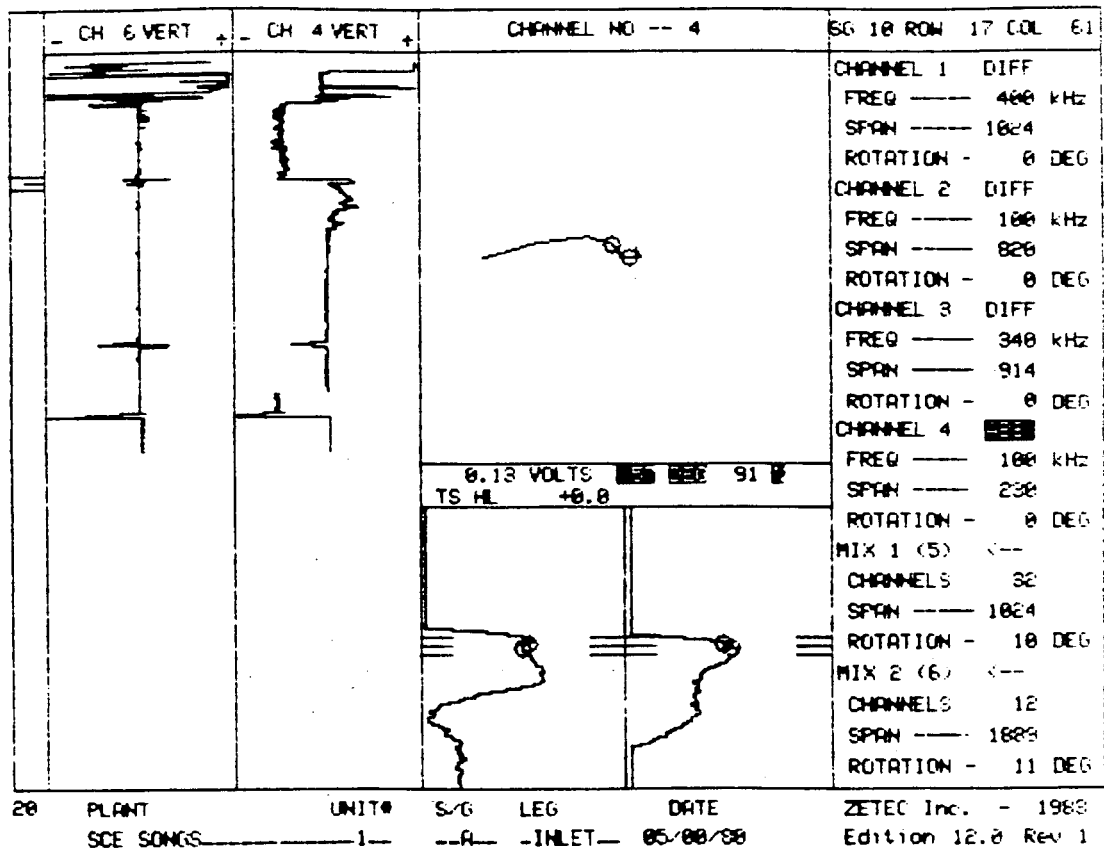
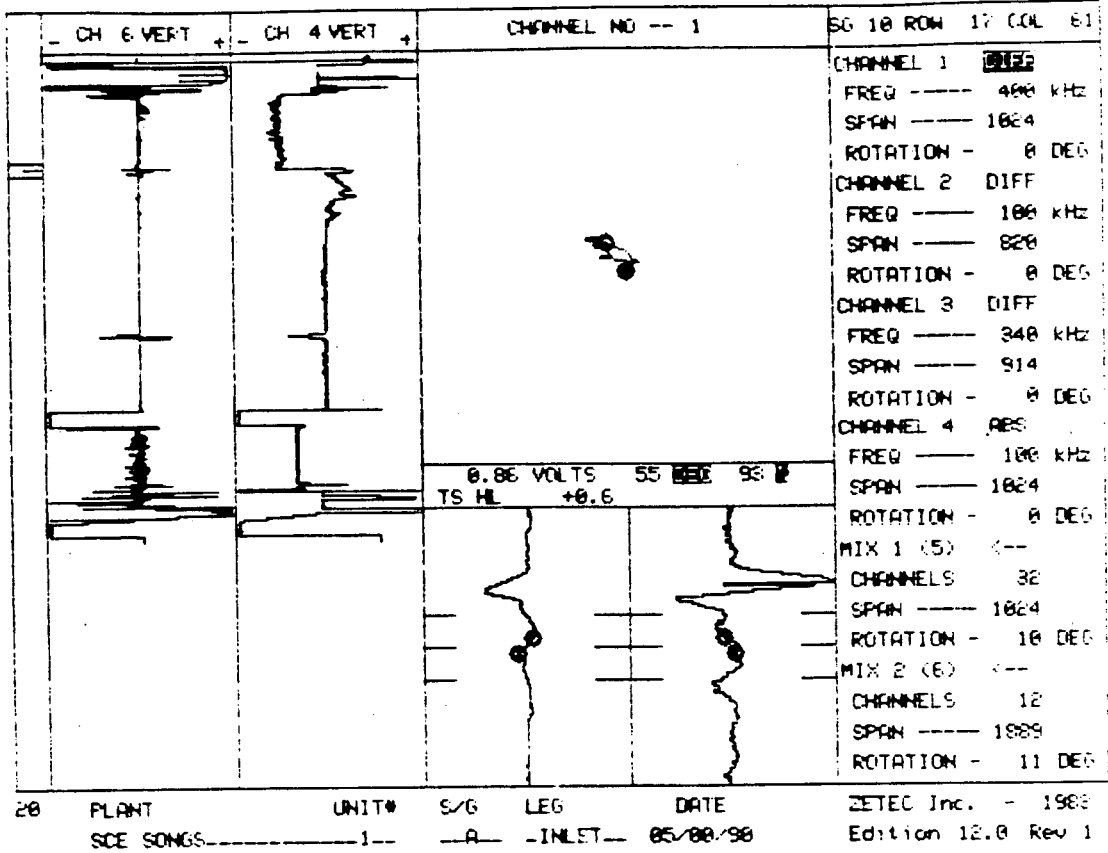


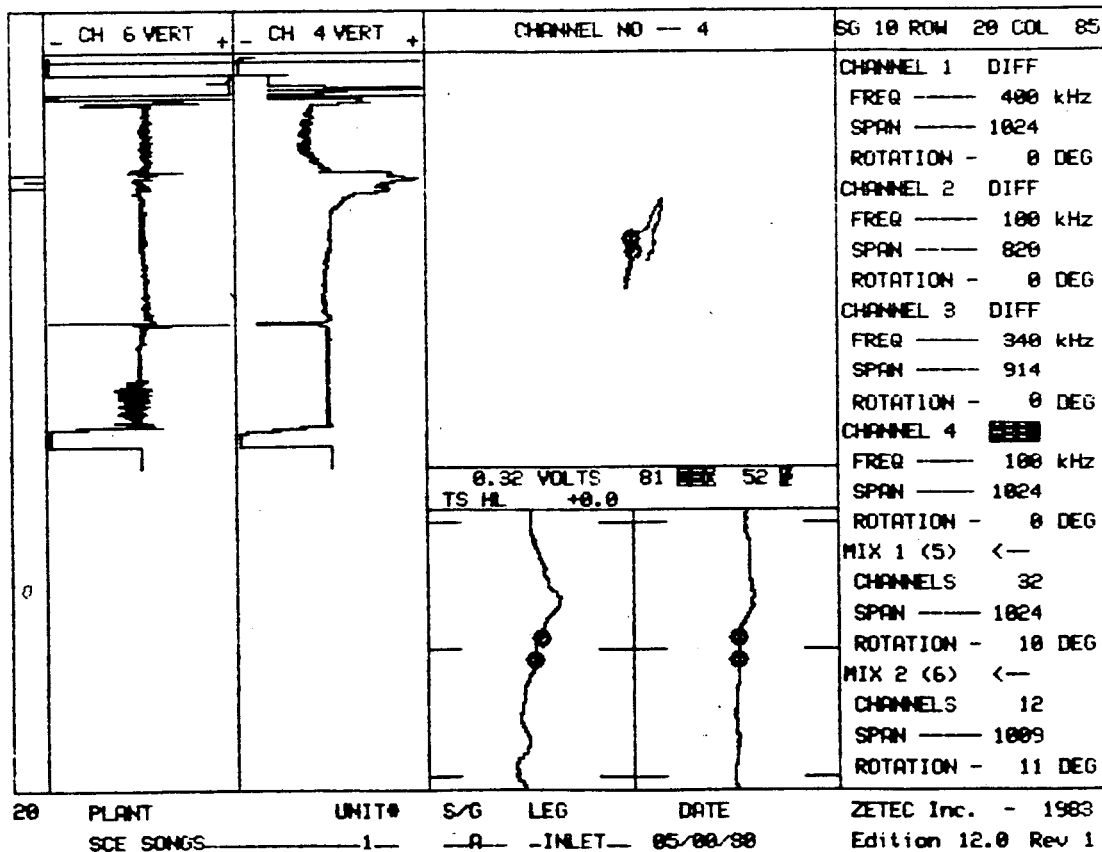
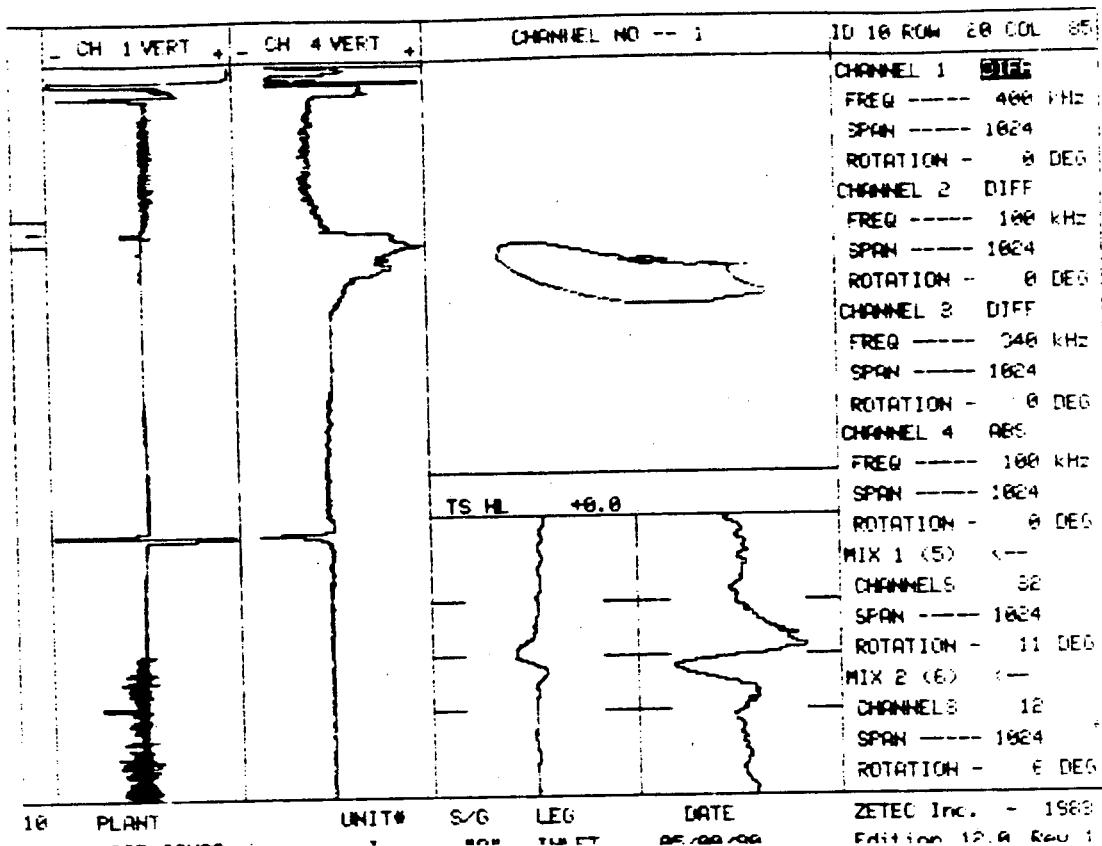


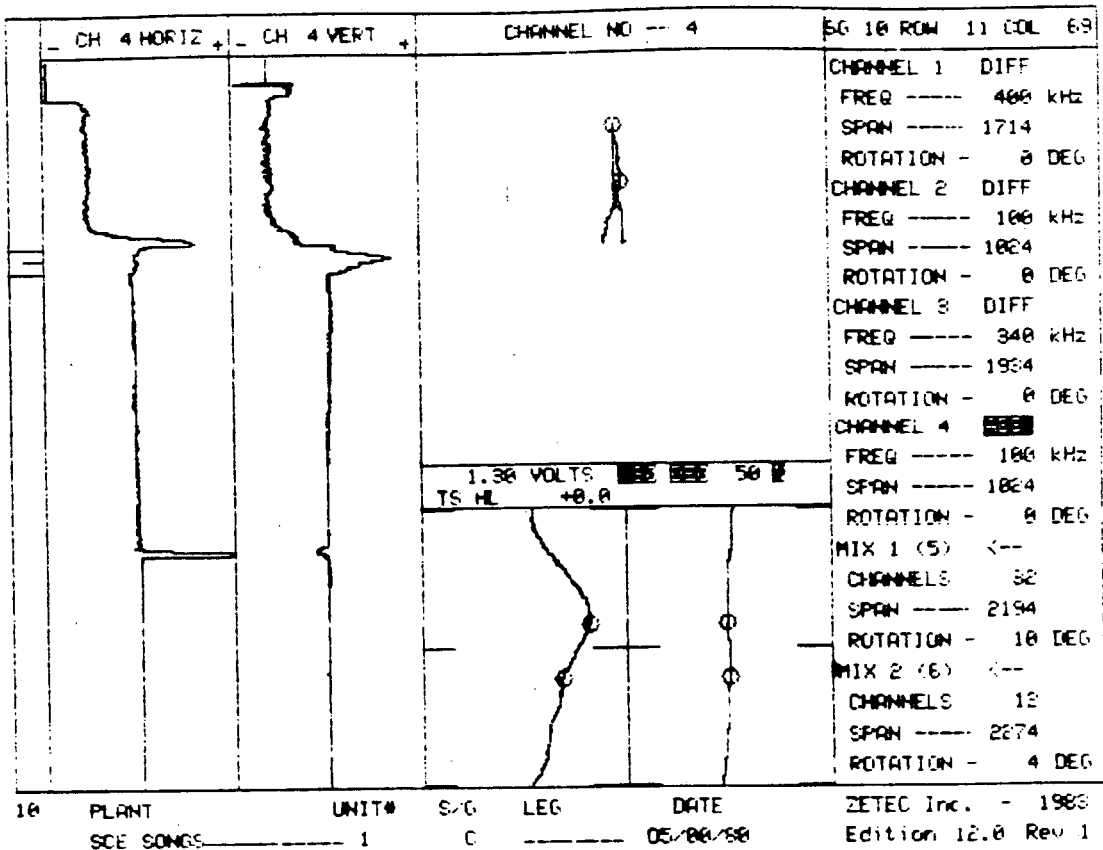
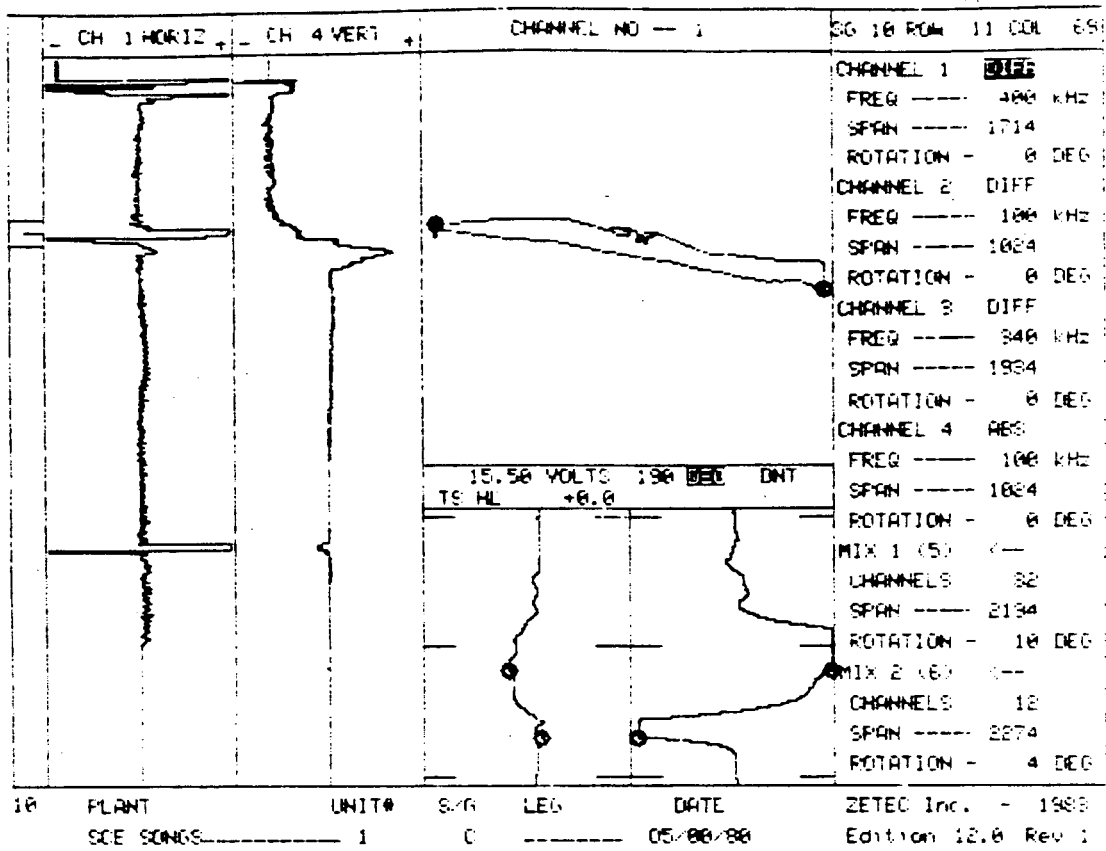
20 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1983
 SCE SONGS 1 -A- -INLET- 05/00/80 Edition 12.0 Rev 1

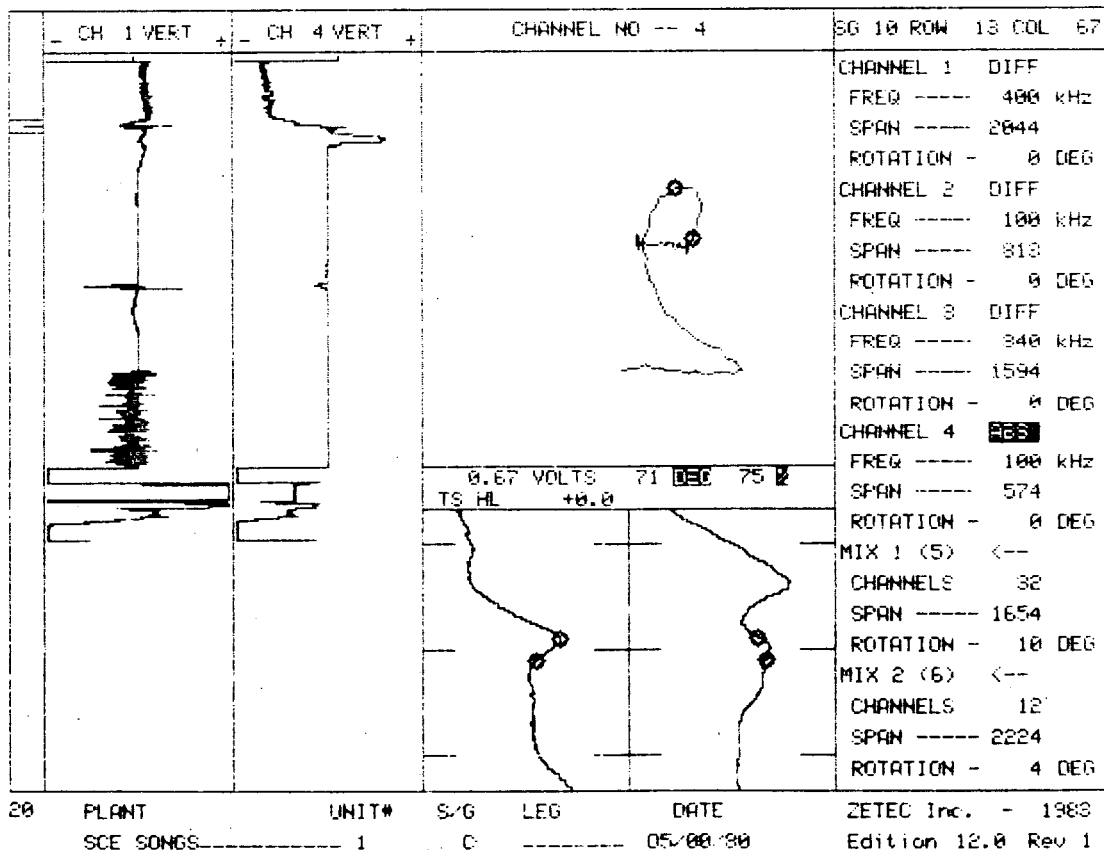
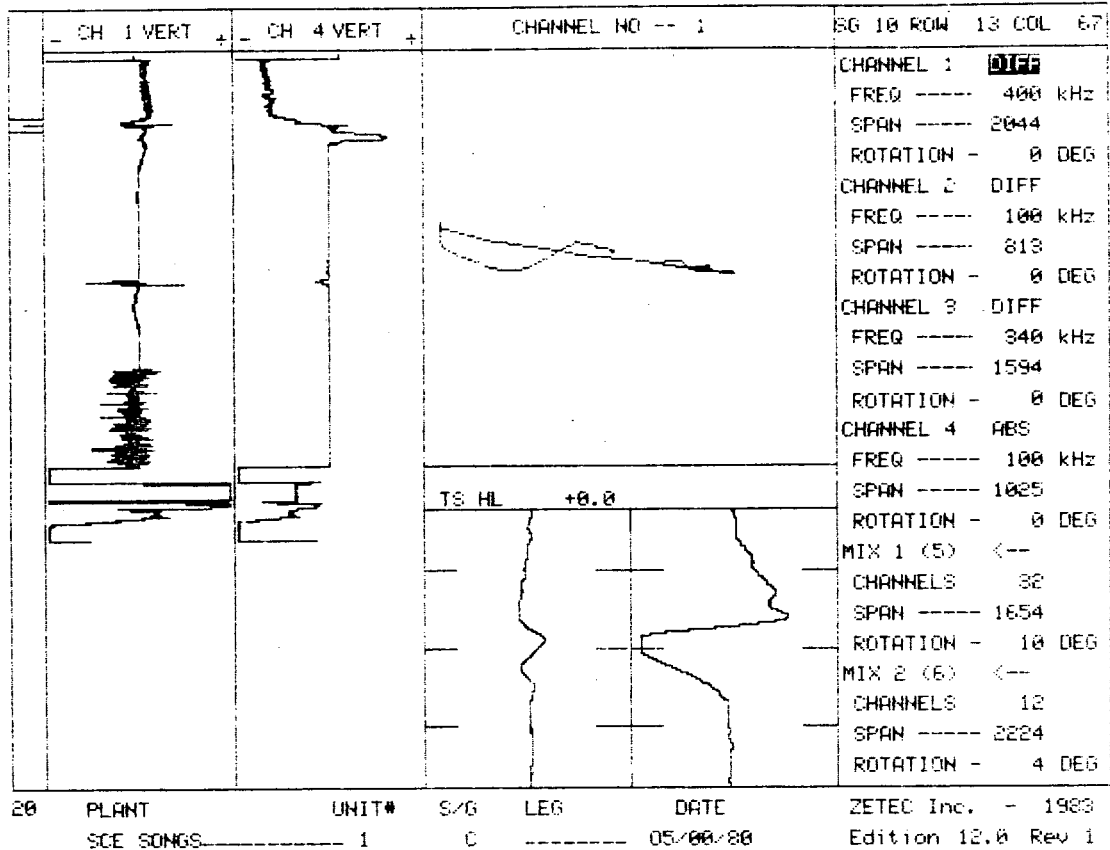


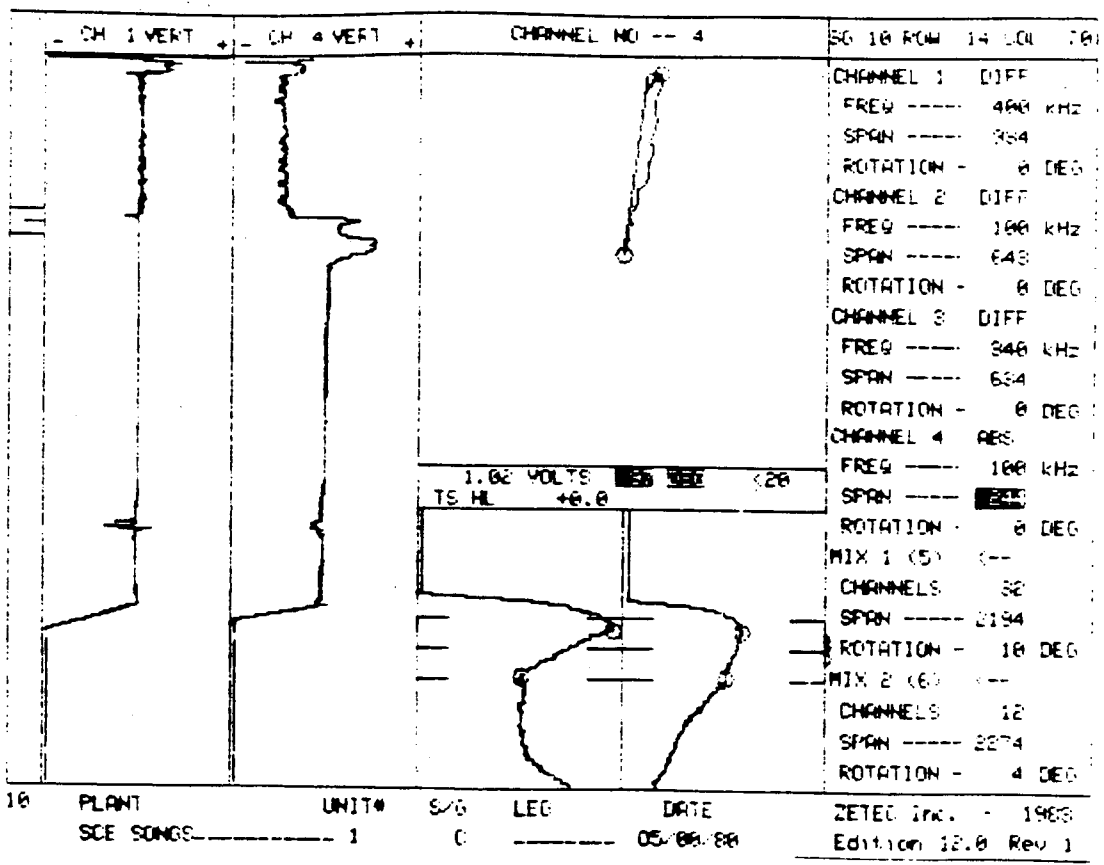
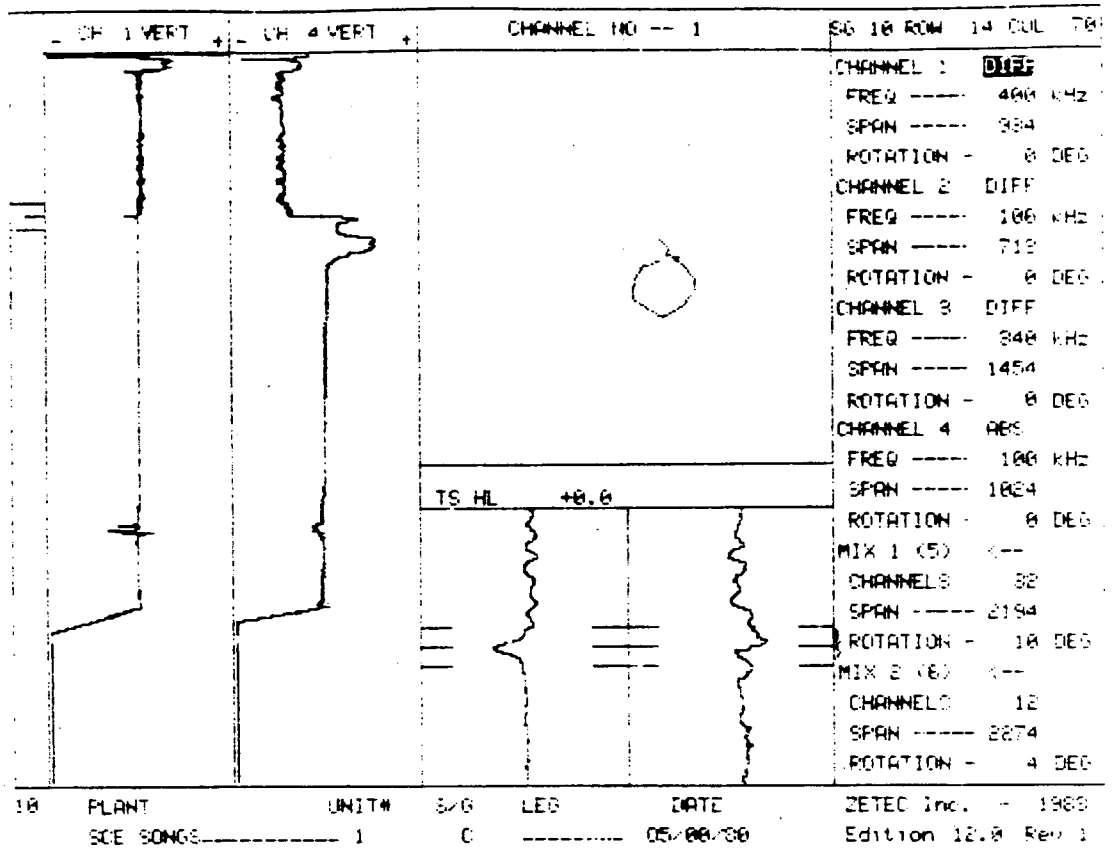
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 SCE SONGS 1 -A- -INLET- 05/00/80 Edition 12.0 Rev 1

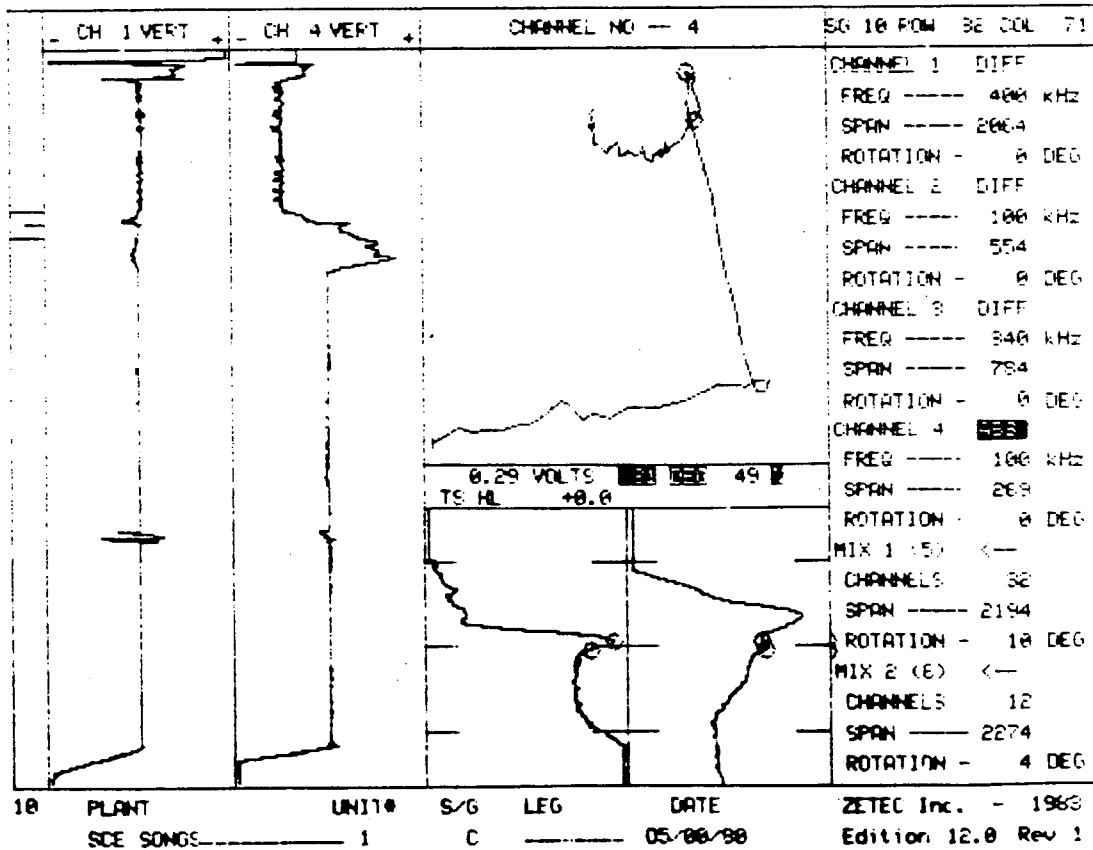
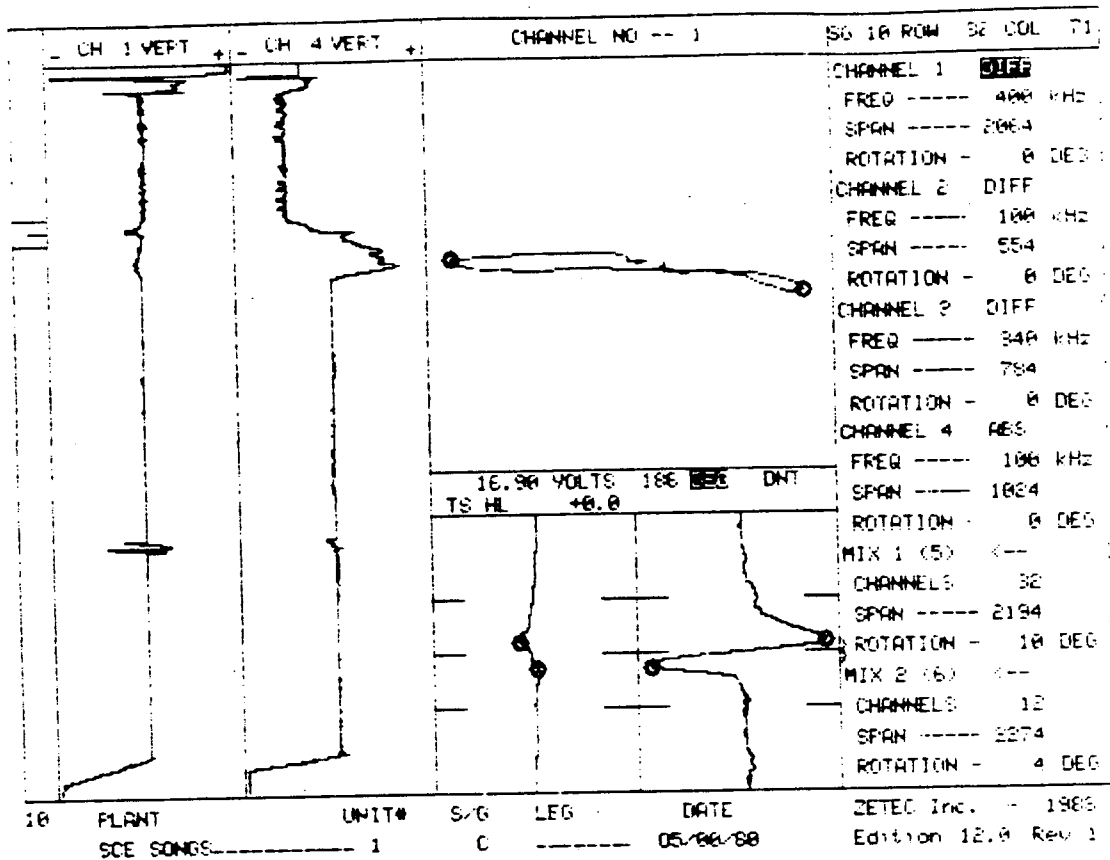


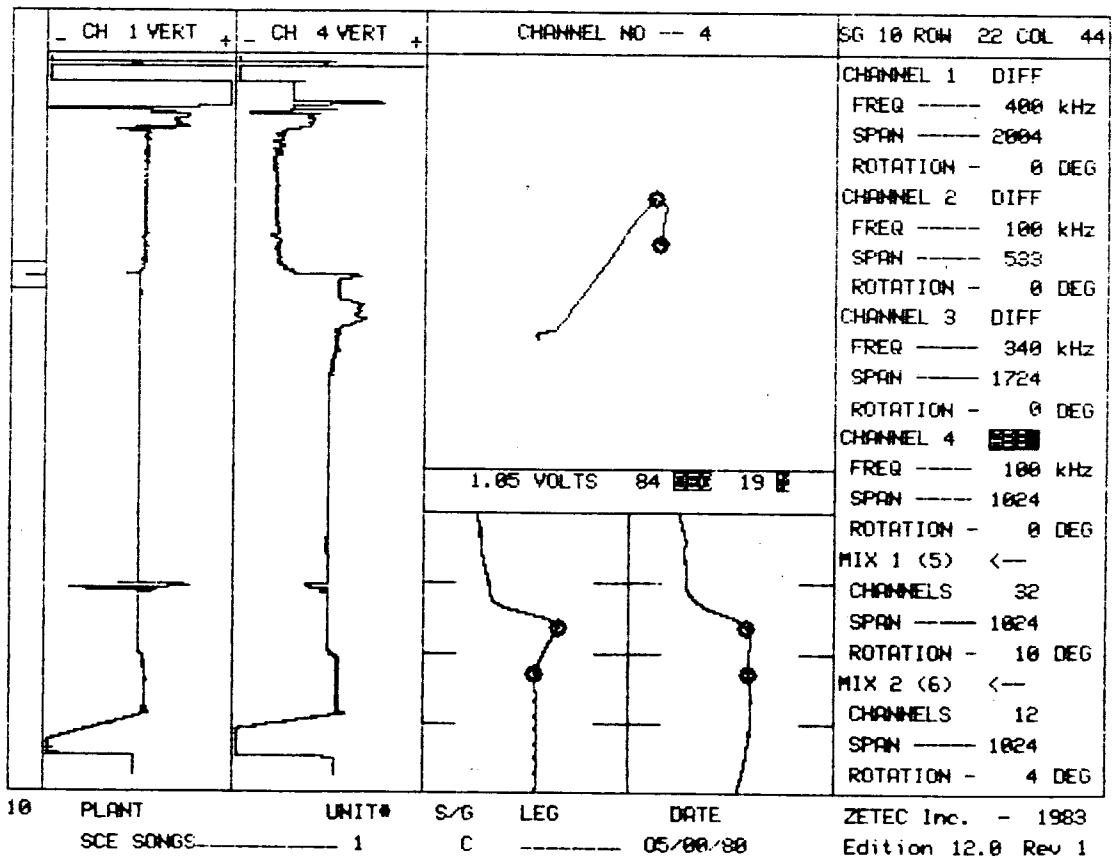
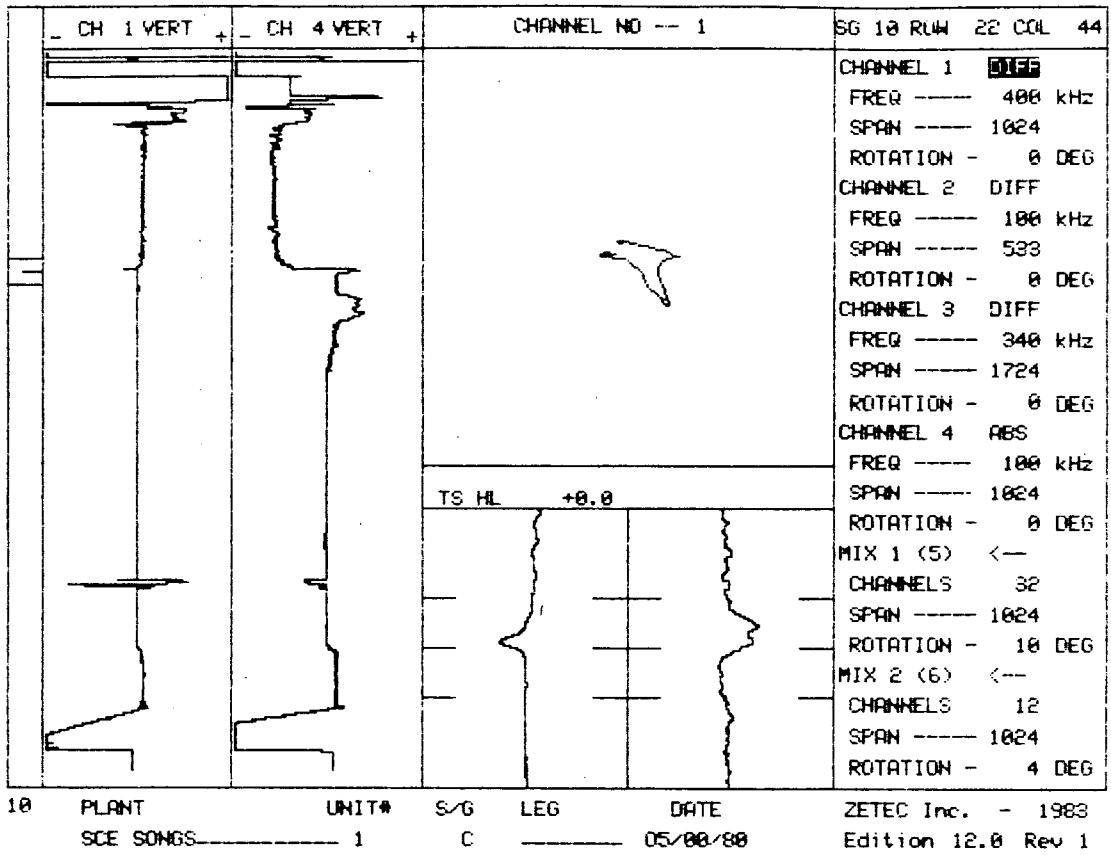


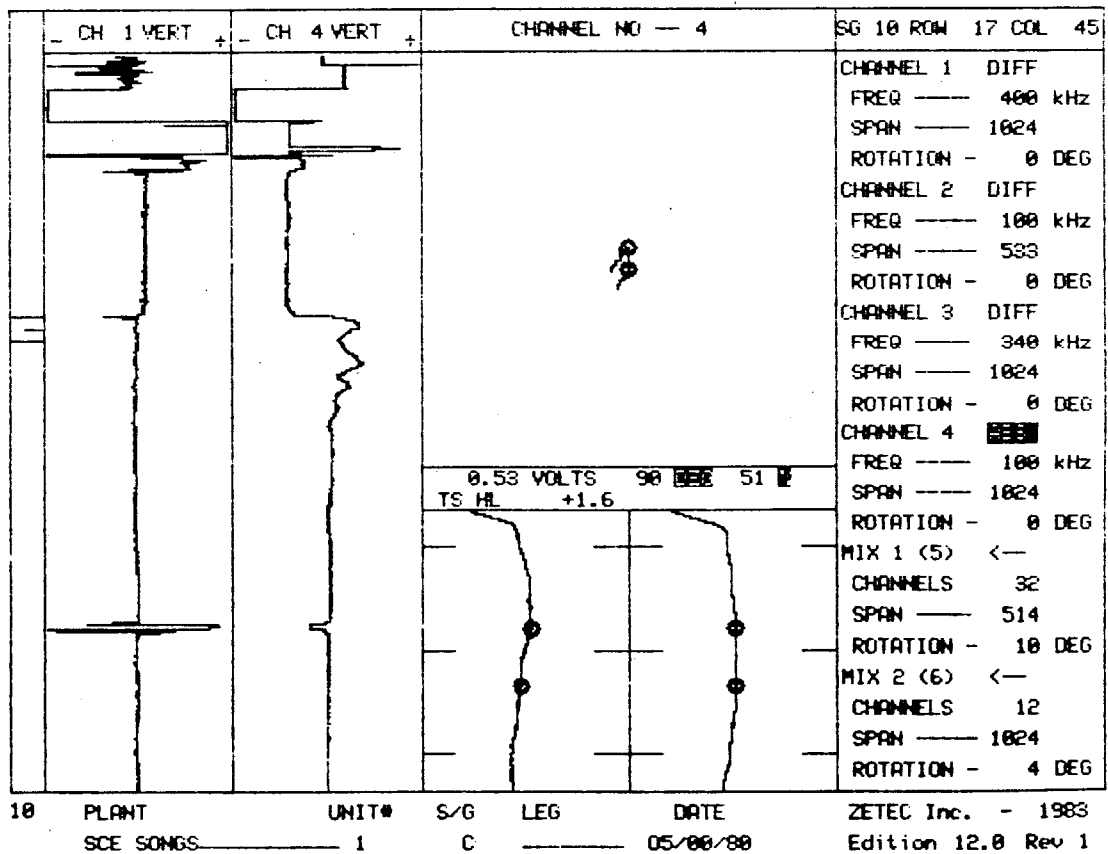
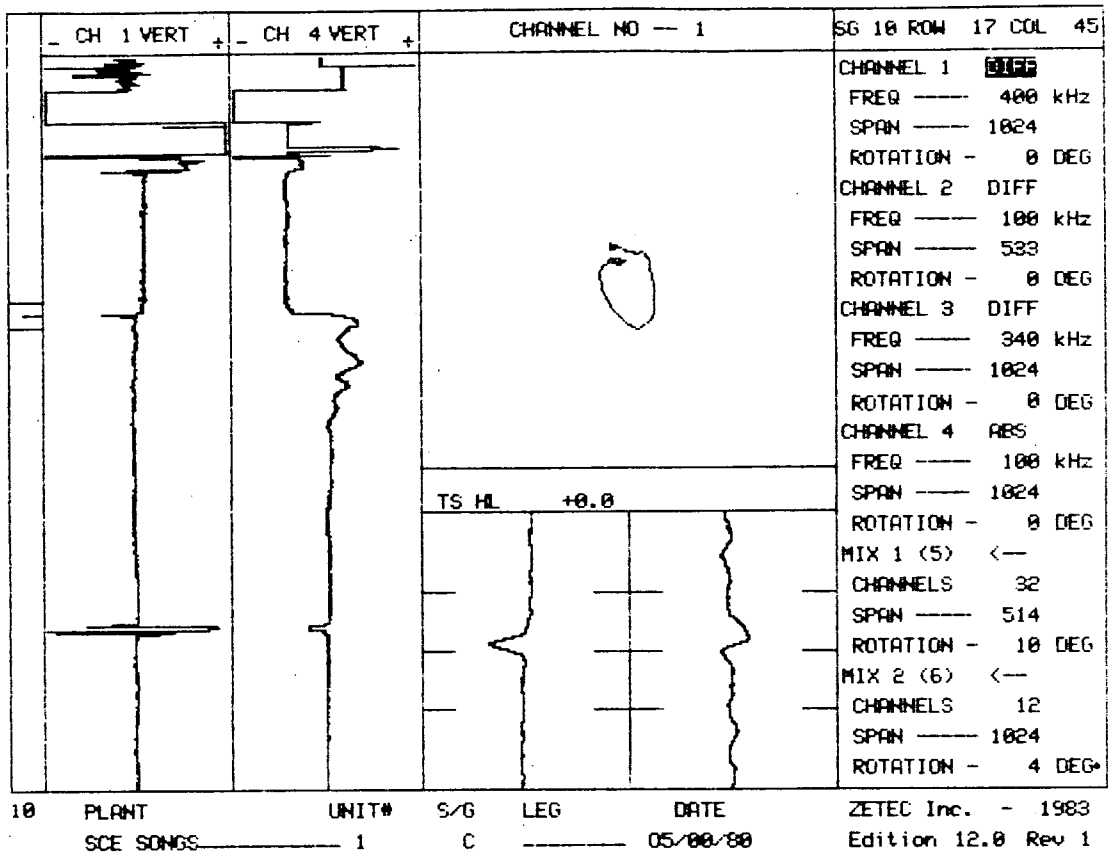


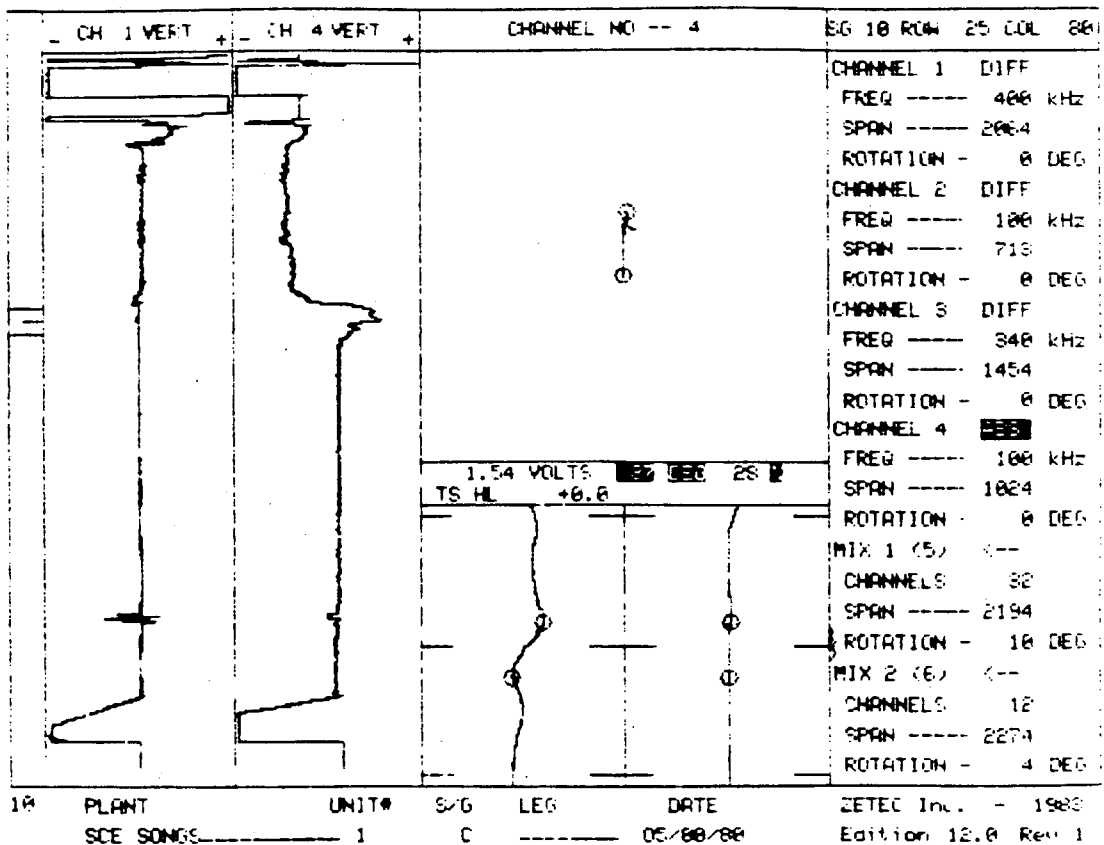
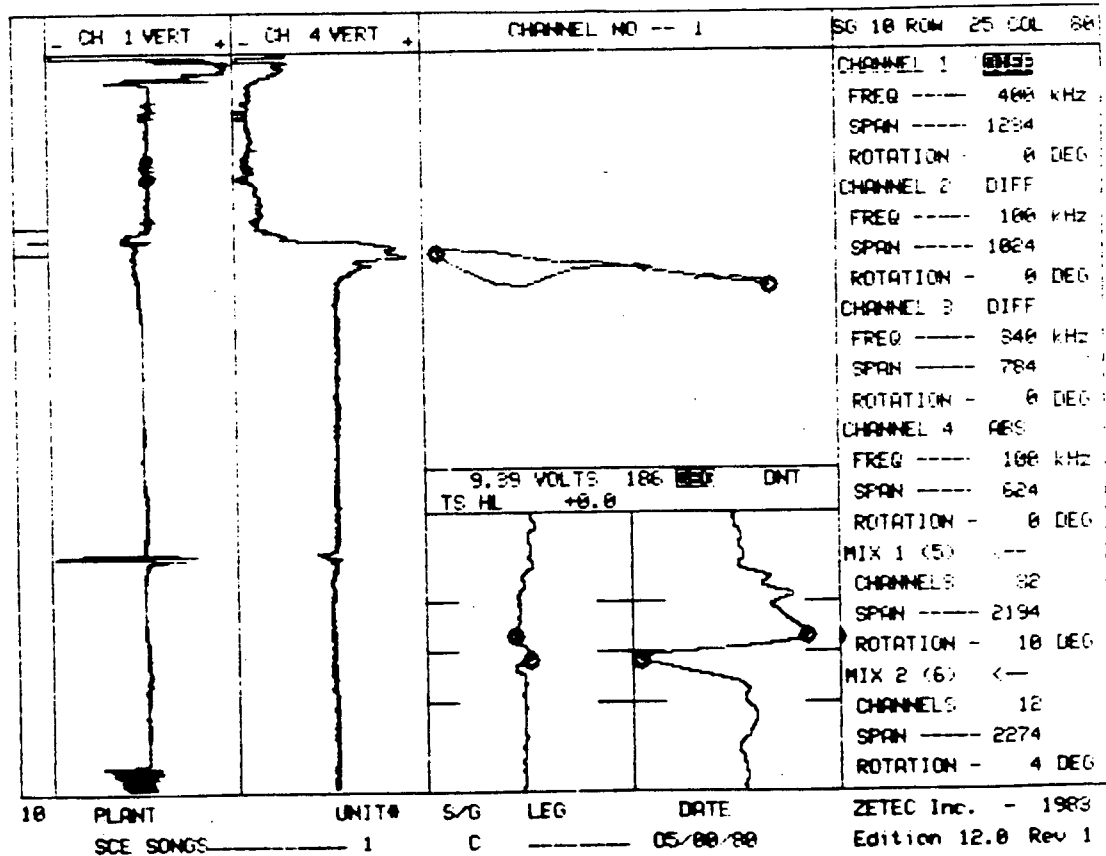


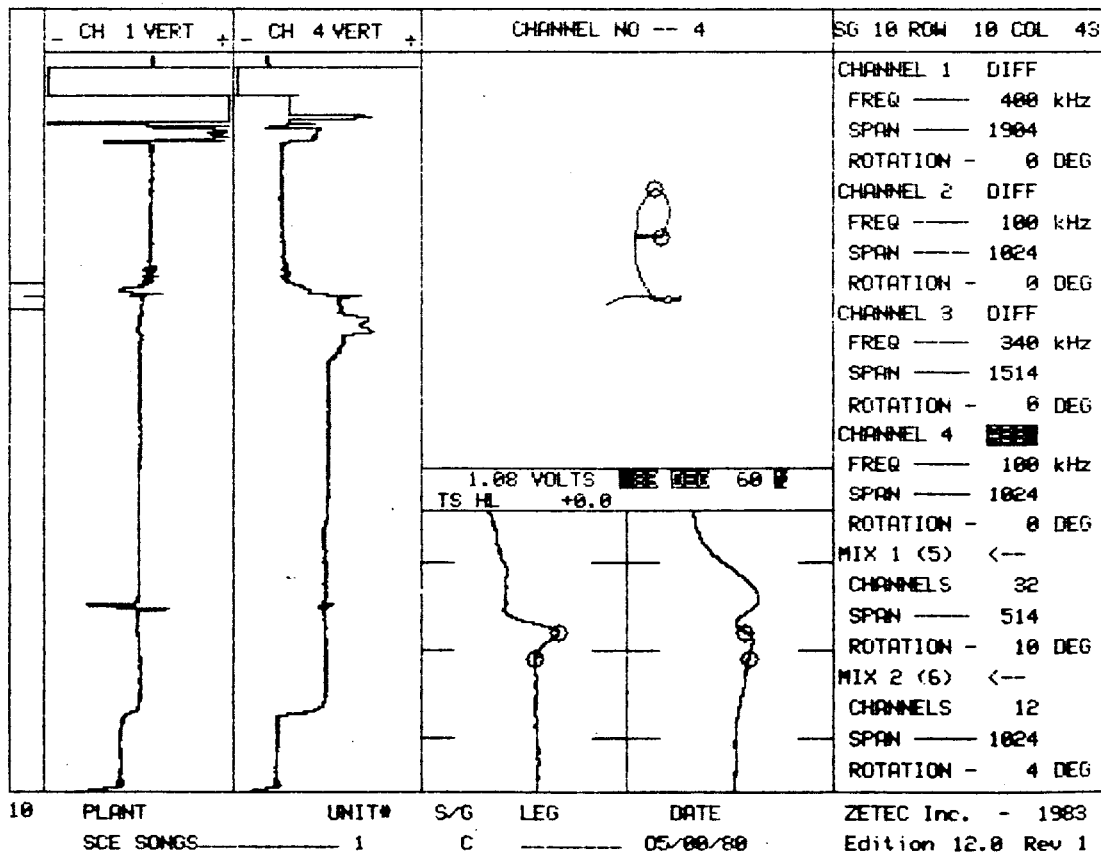
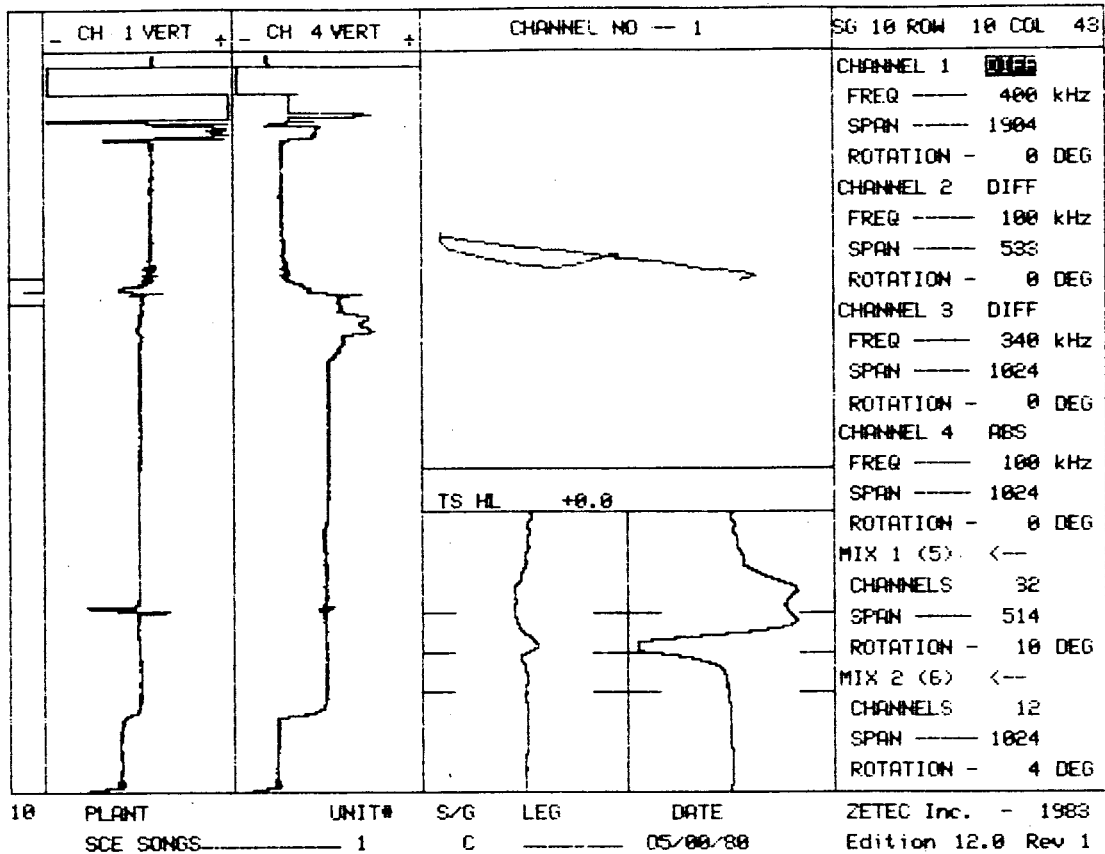




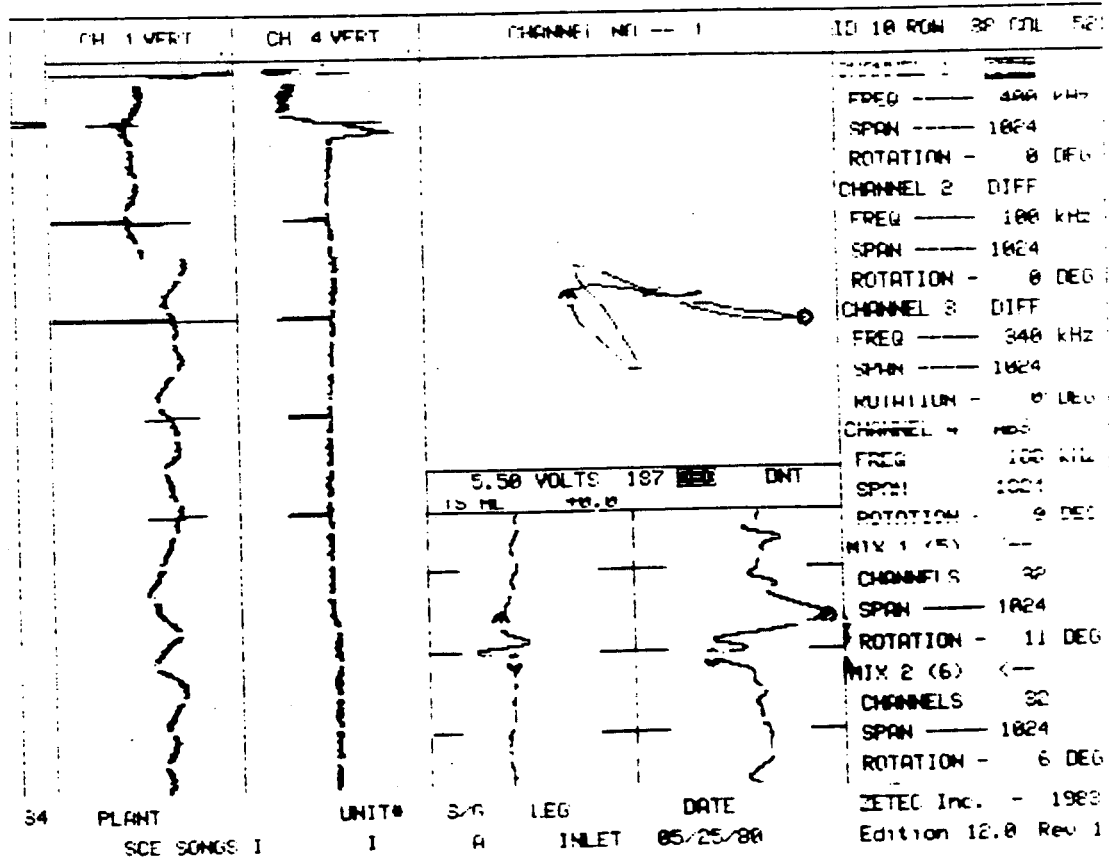
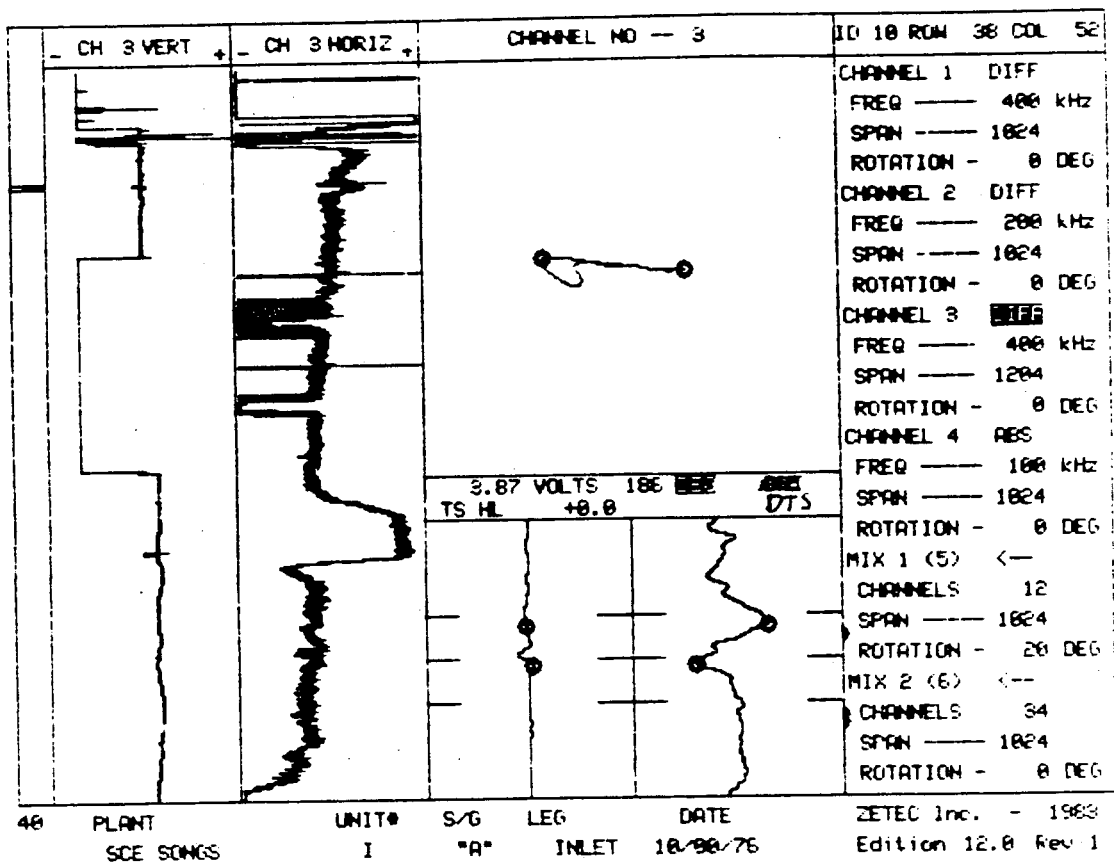


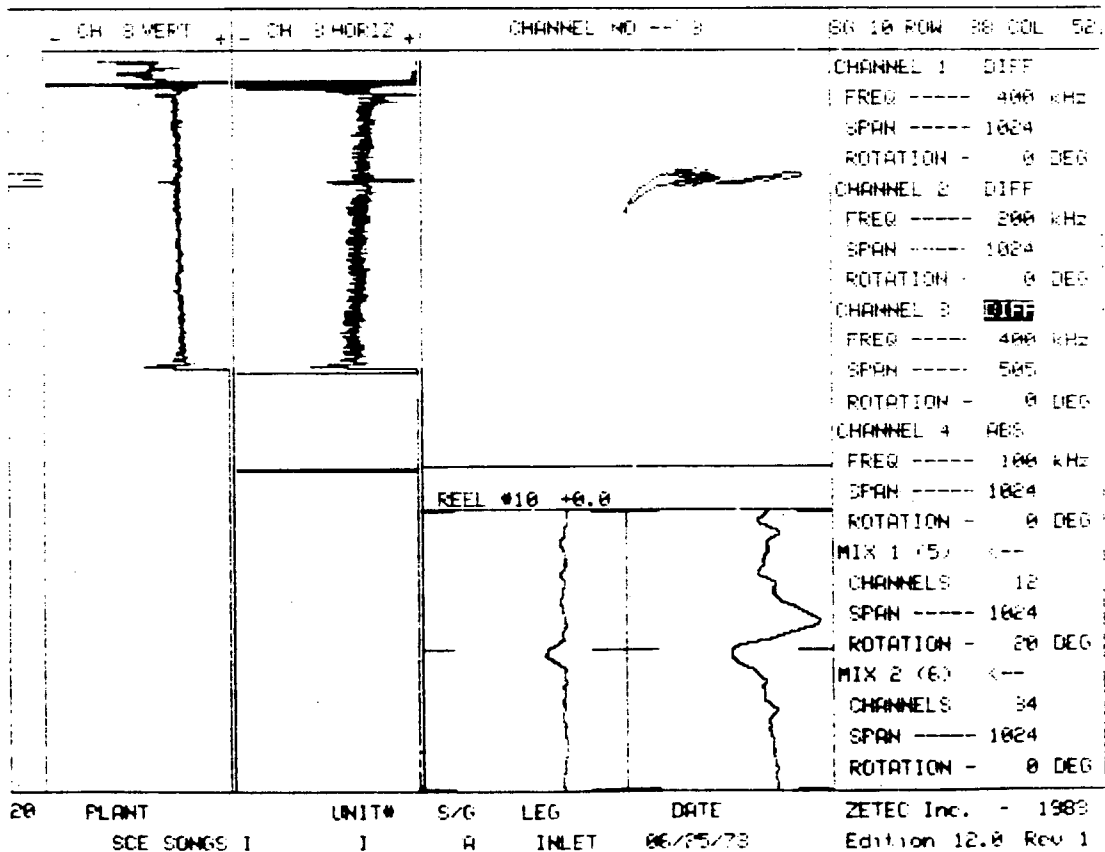
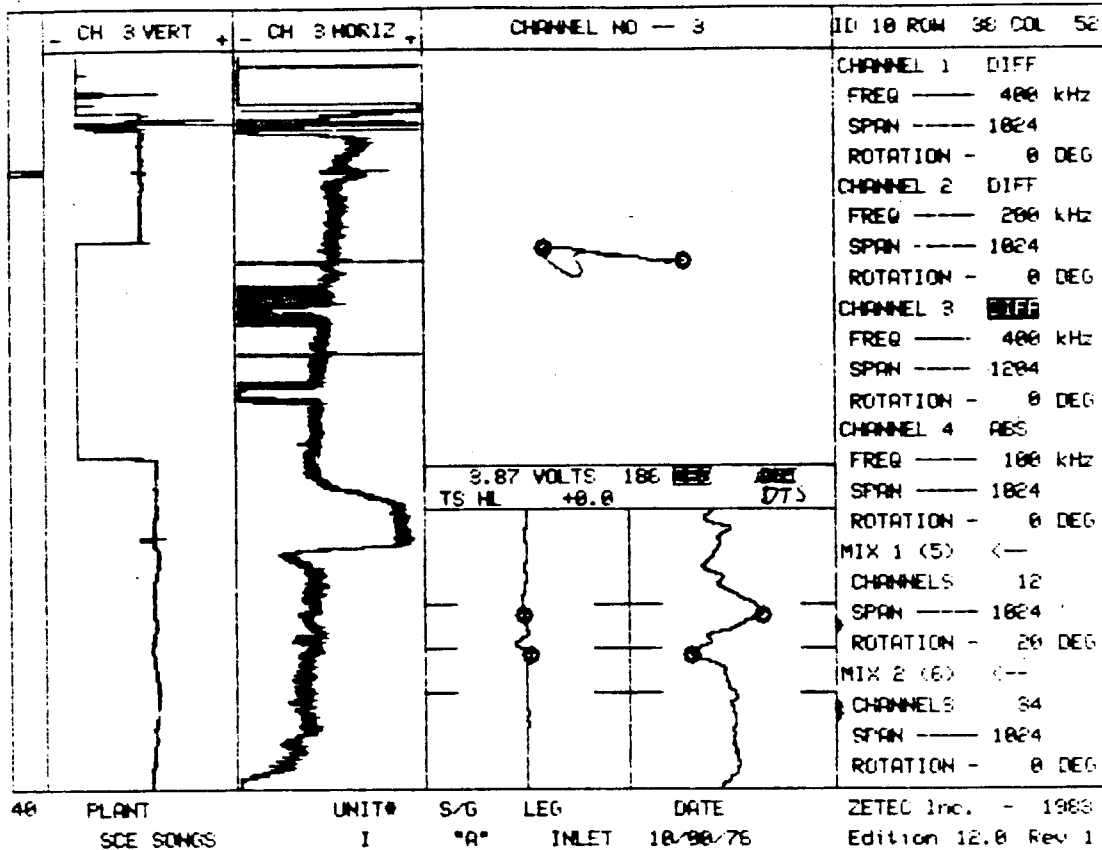


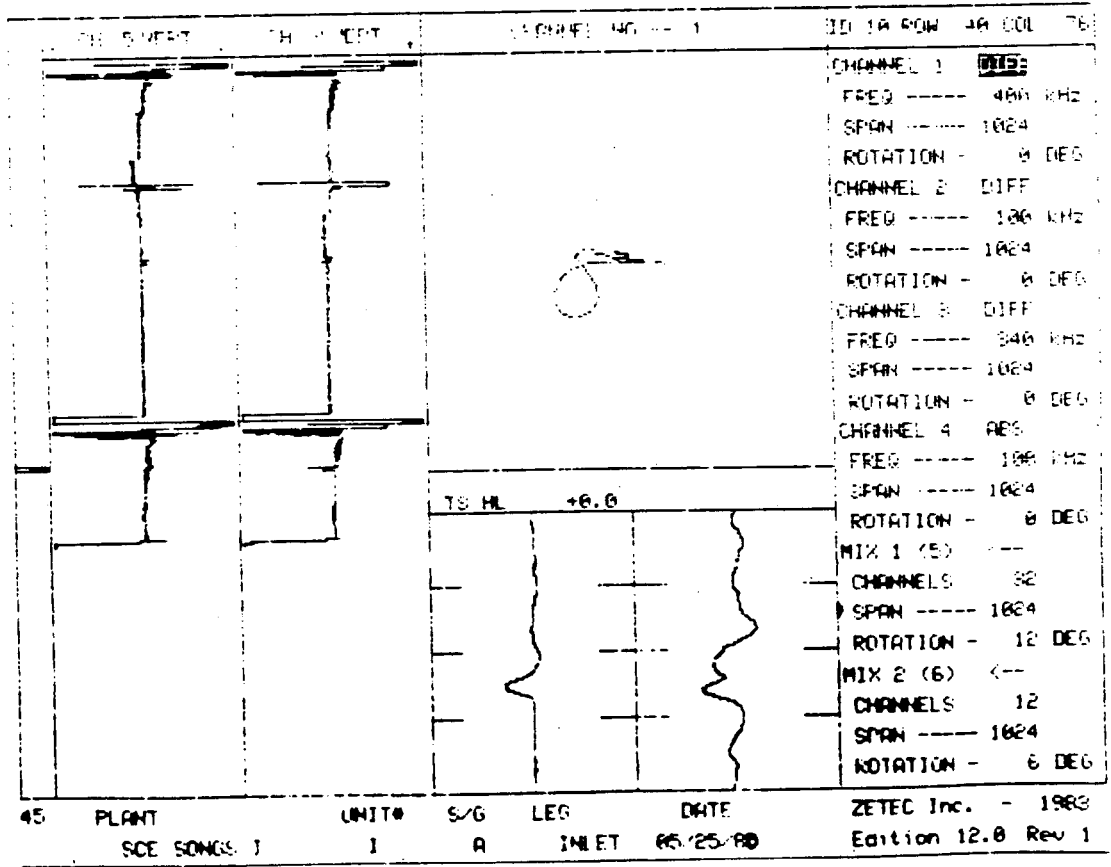
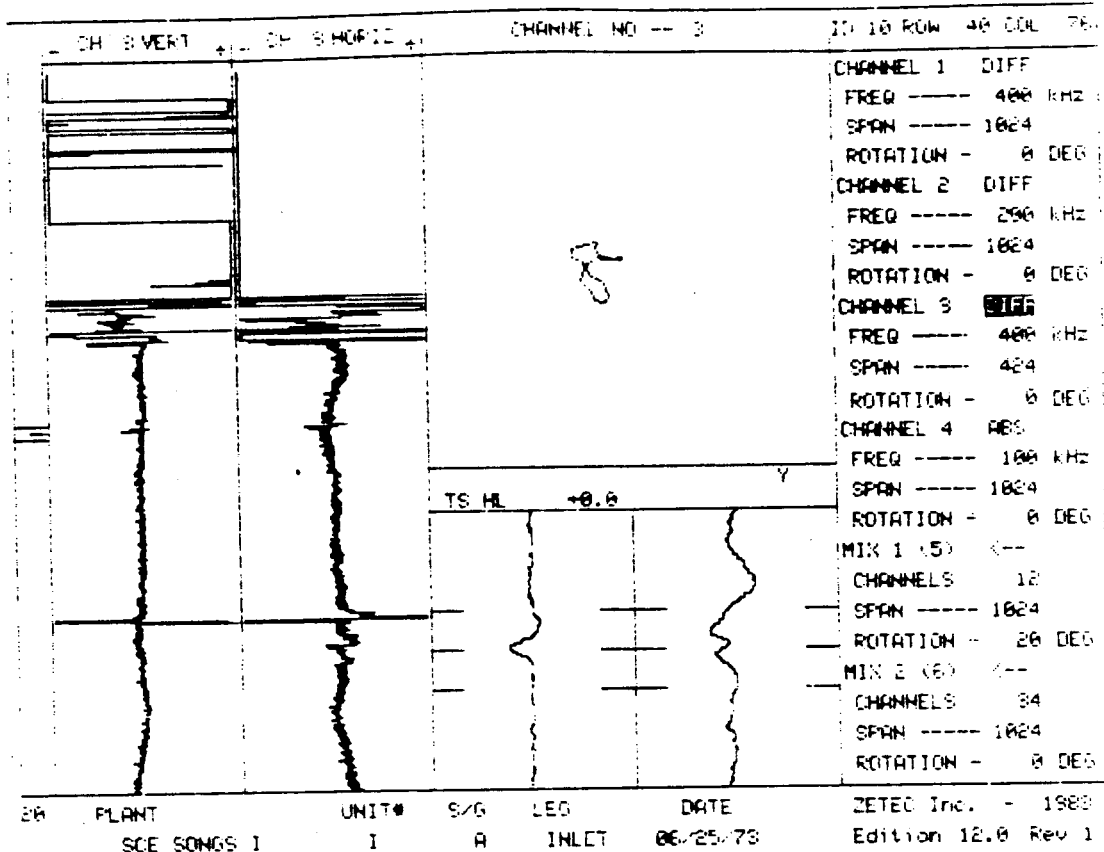


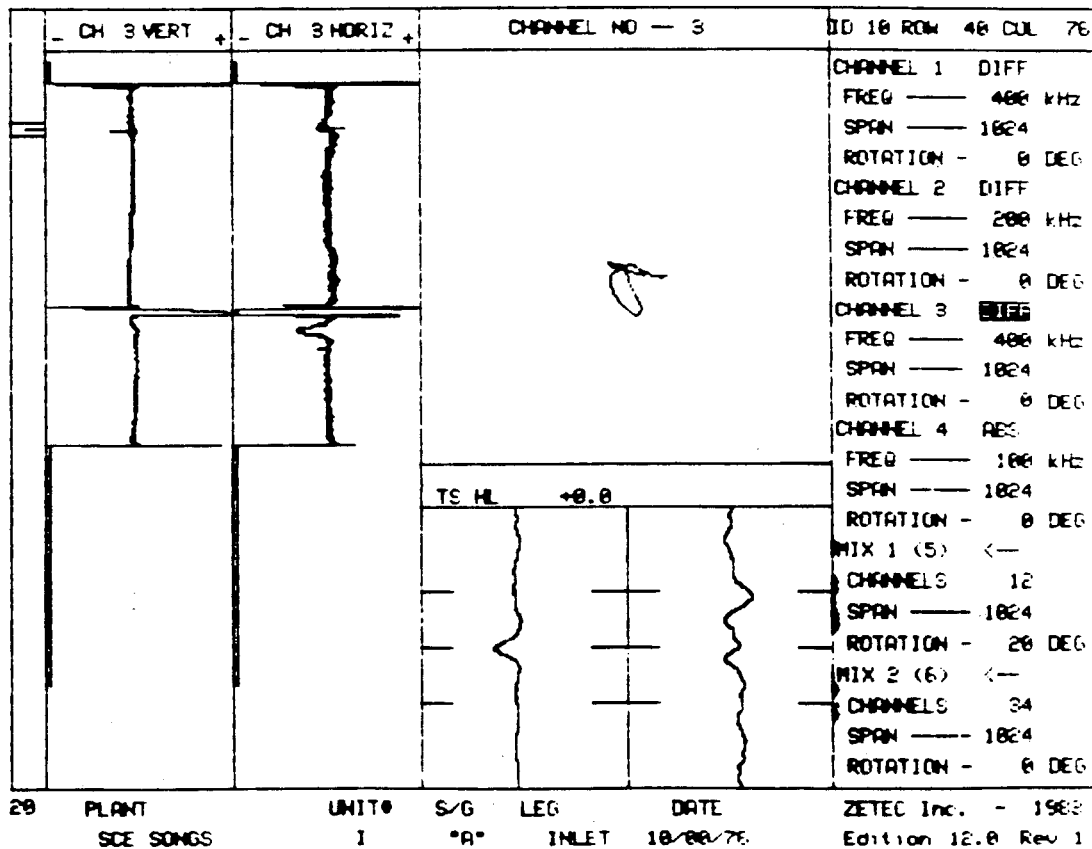
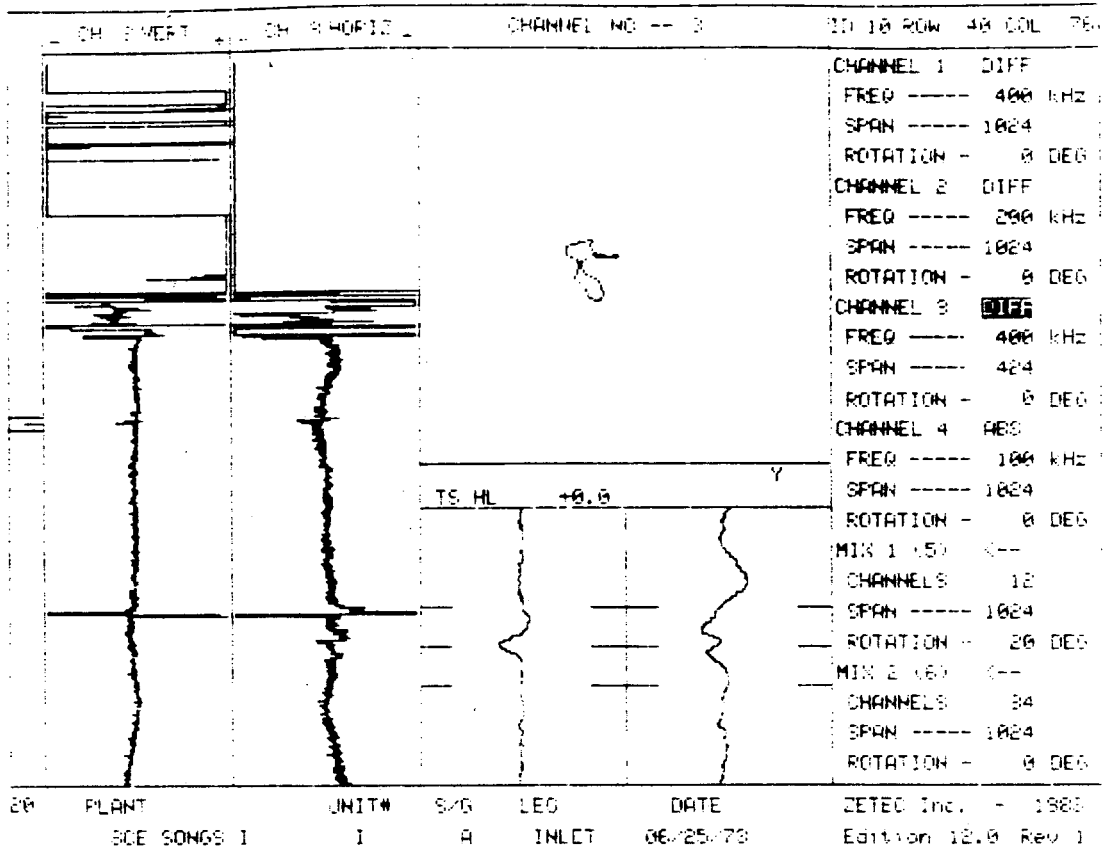


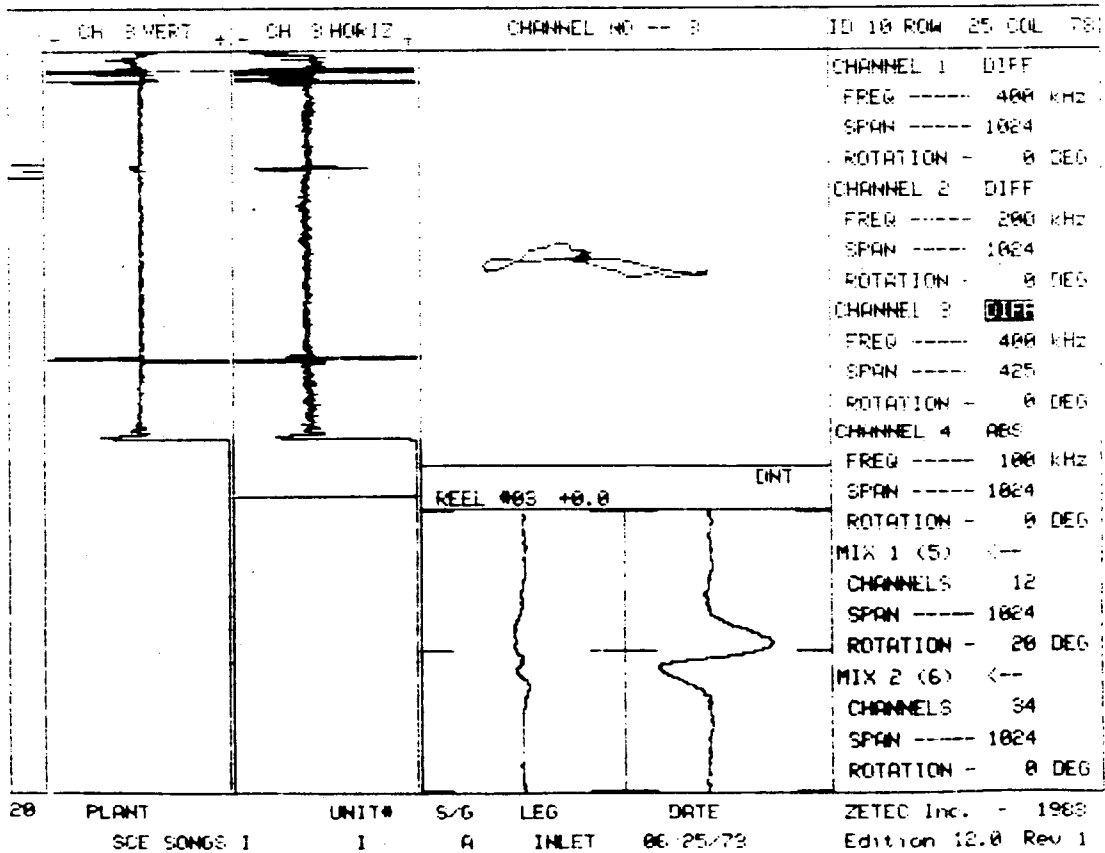
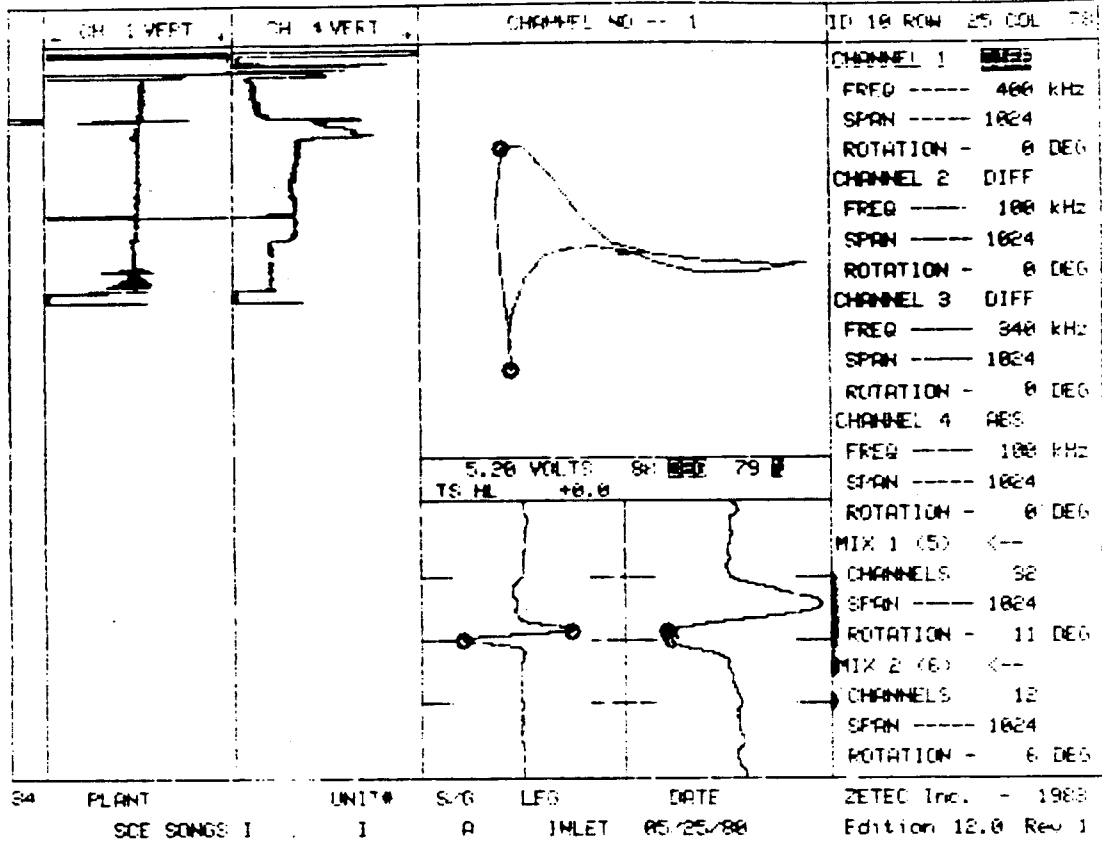
APPENDIX C

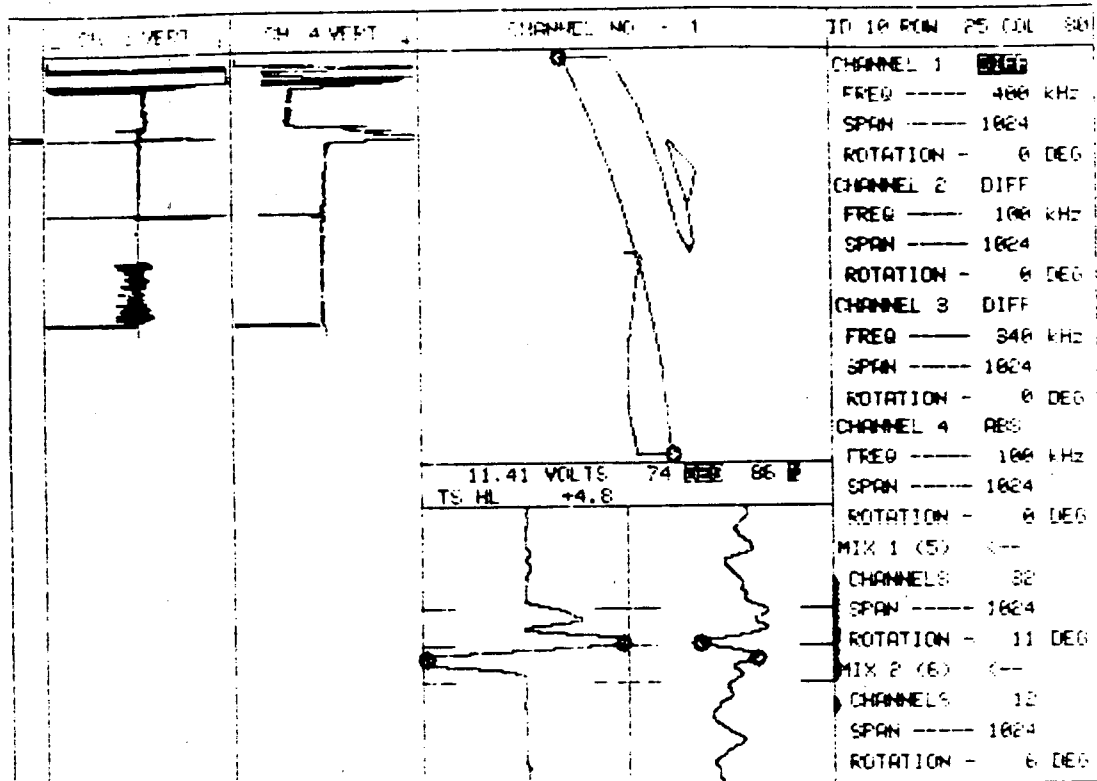




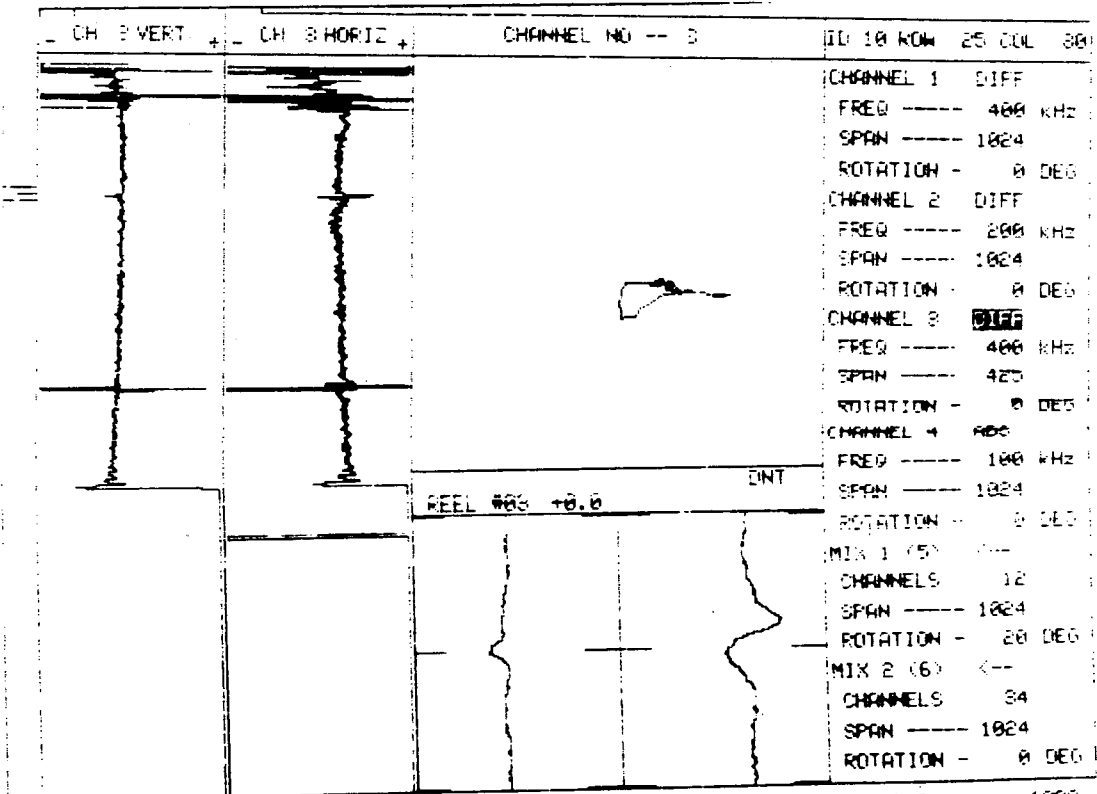








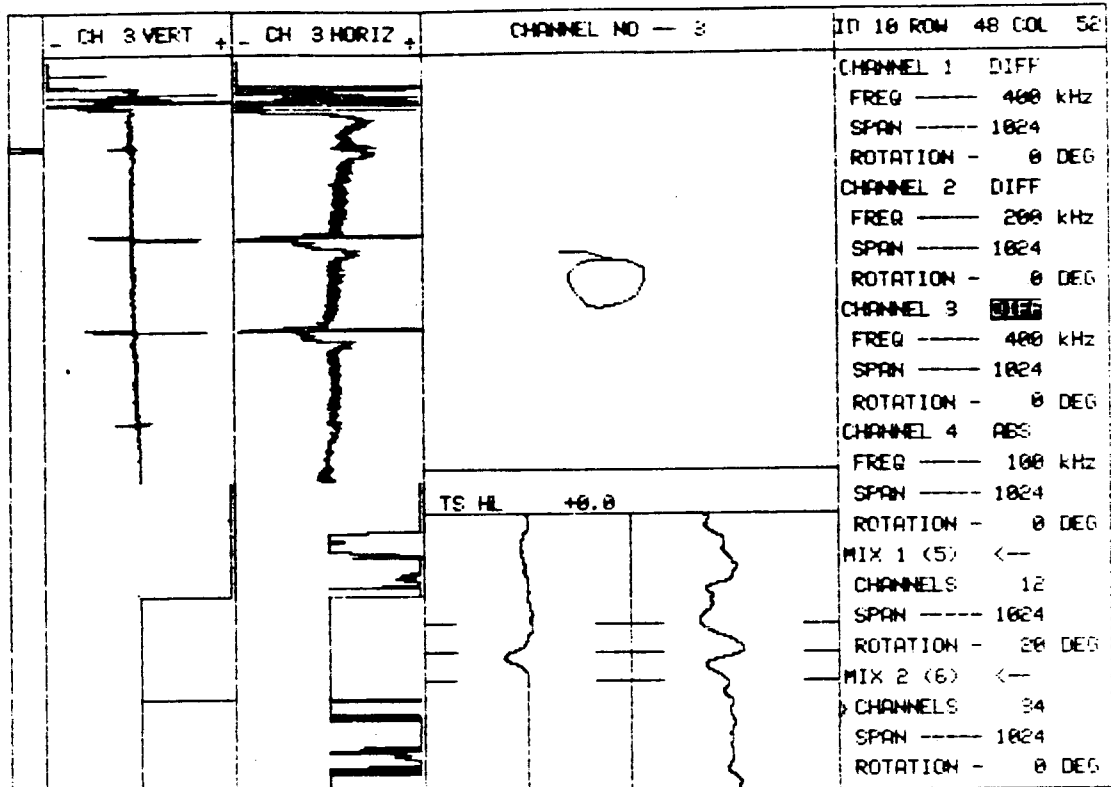
34 PLANT SCE SONGS I UNIT# 1 S/G A LEG INLET DATE 06/25/80 ZETEC Inc. - 1988 Edition 12.0 Rev 1



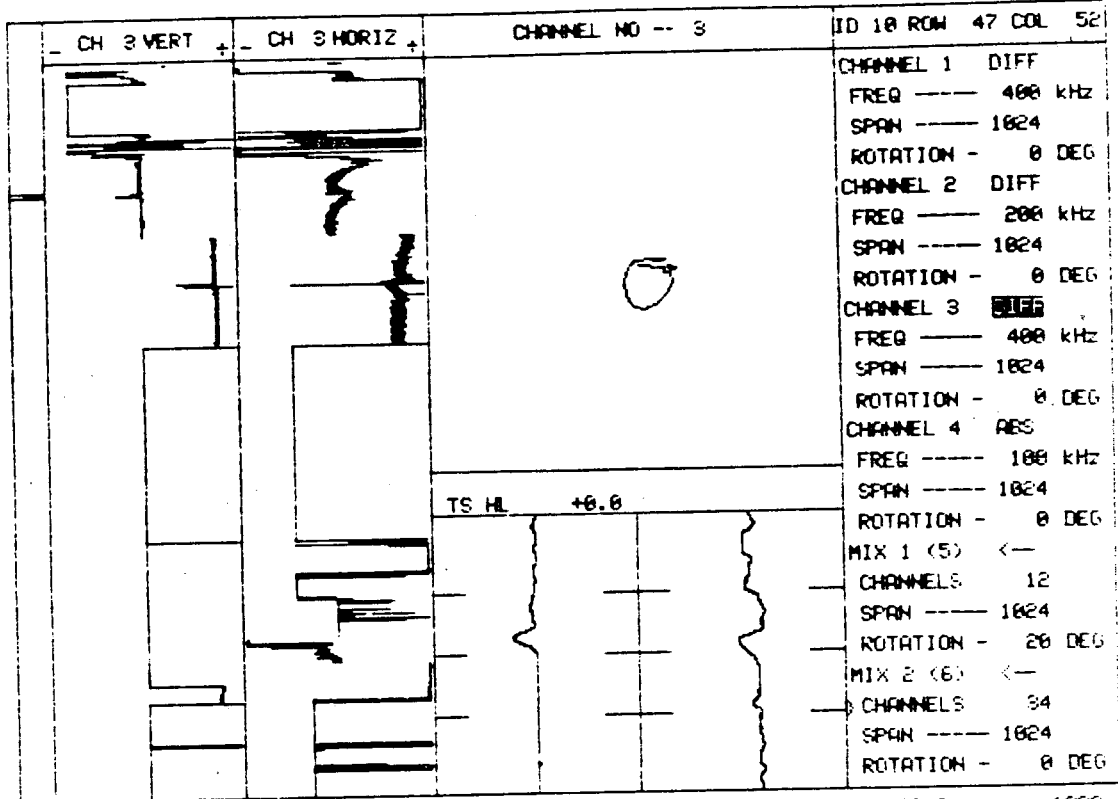
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APPENDIX D

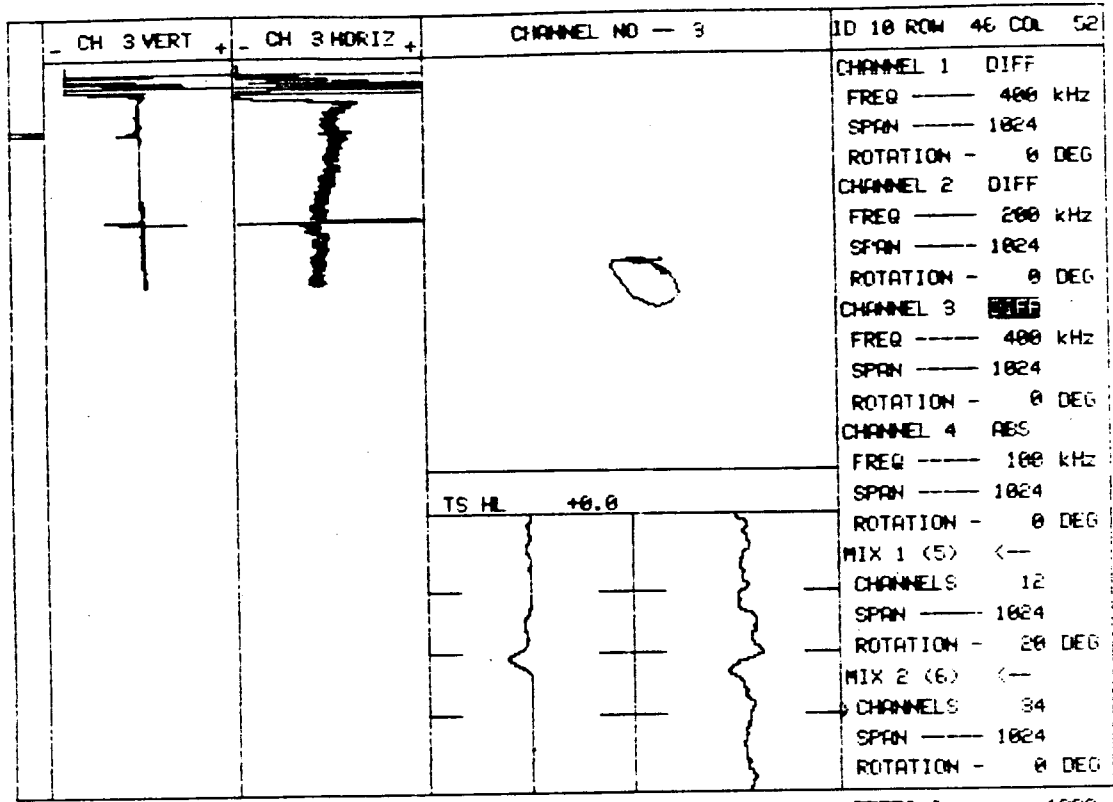
1976 COLUMN 52



40	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	I	"A"	INLET	10/06/76	Edition 12.0 Rev 1

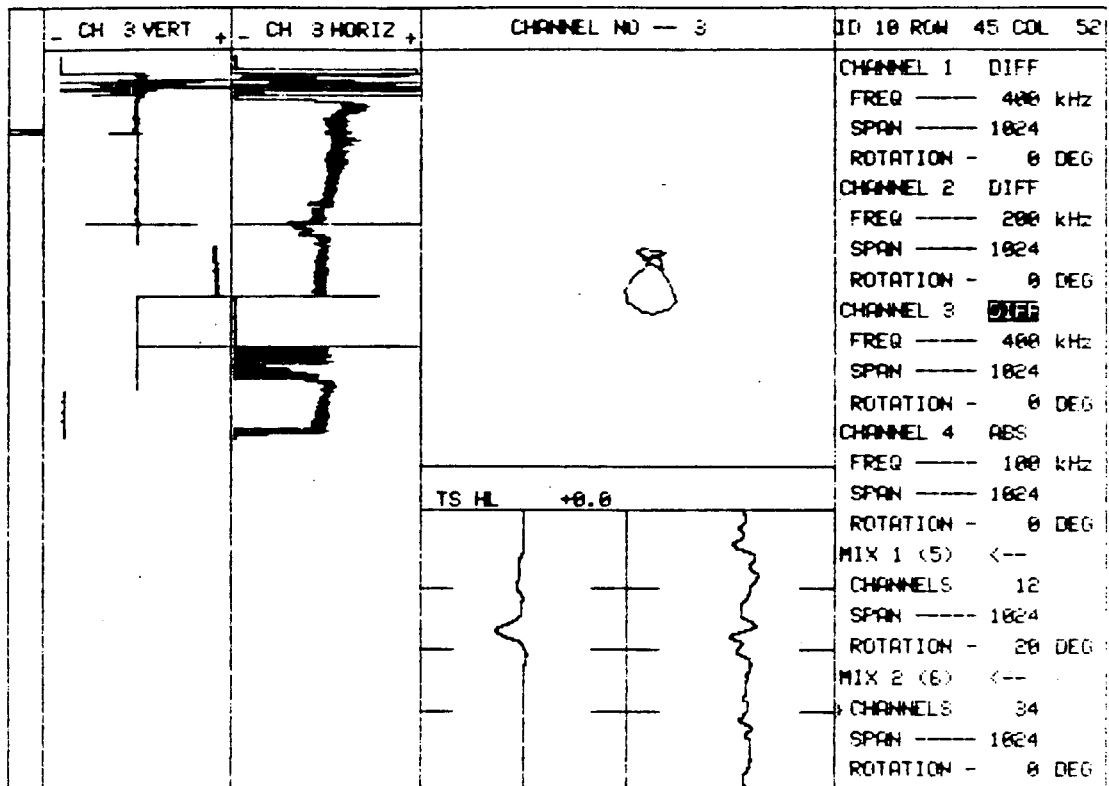


40 PLANT SCE SONGS UNIT# 1 S/G "A" LEG INLET DATE 10/00/75 ZETEC Inc. - 1983 Edition 12.0 Rev 1

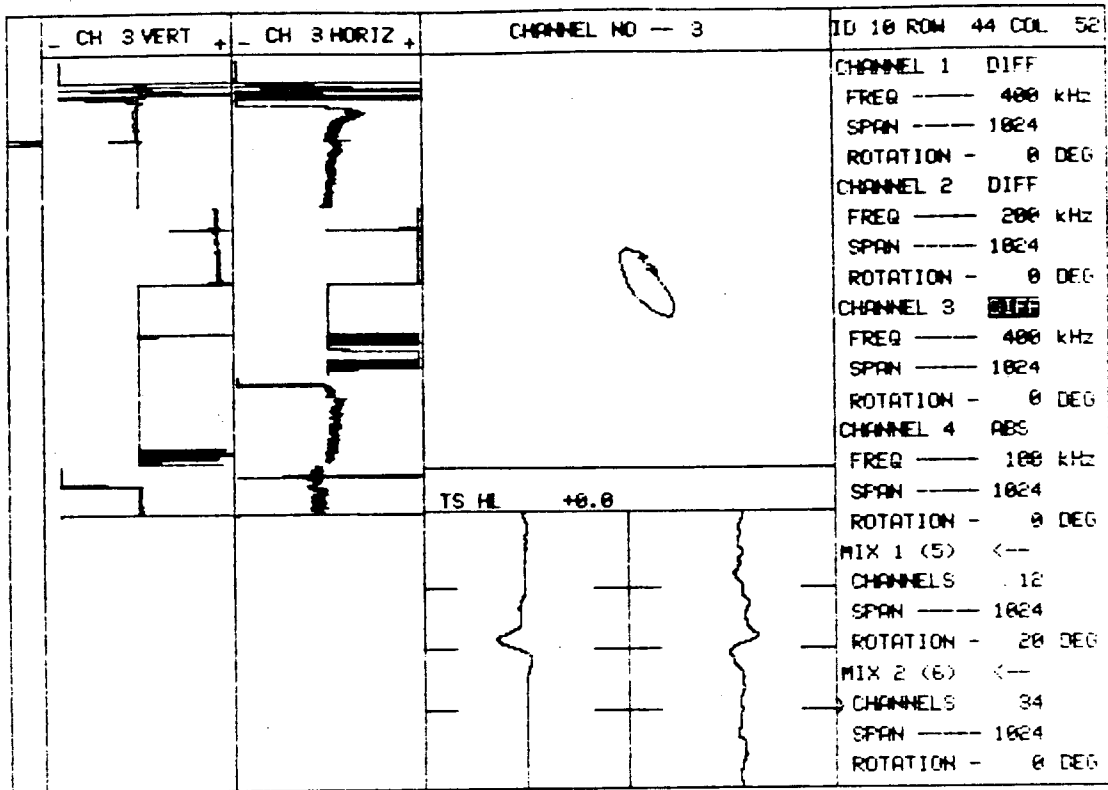


TS HL +0.0

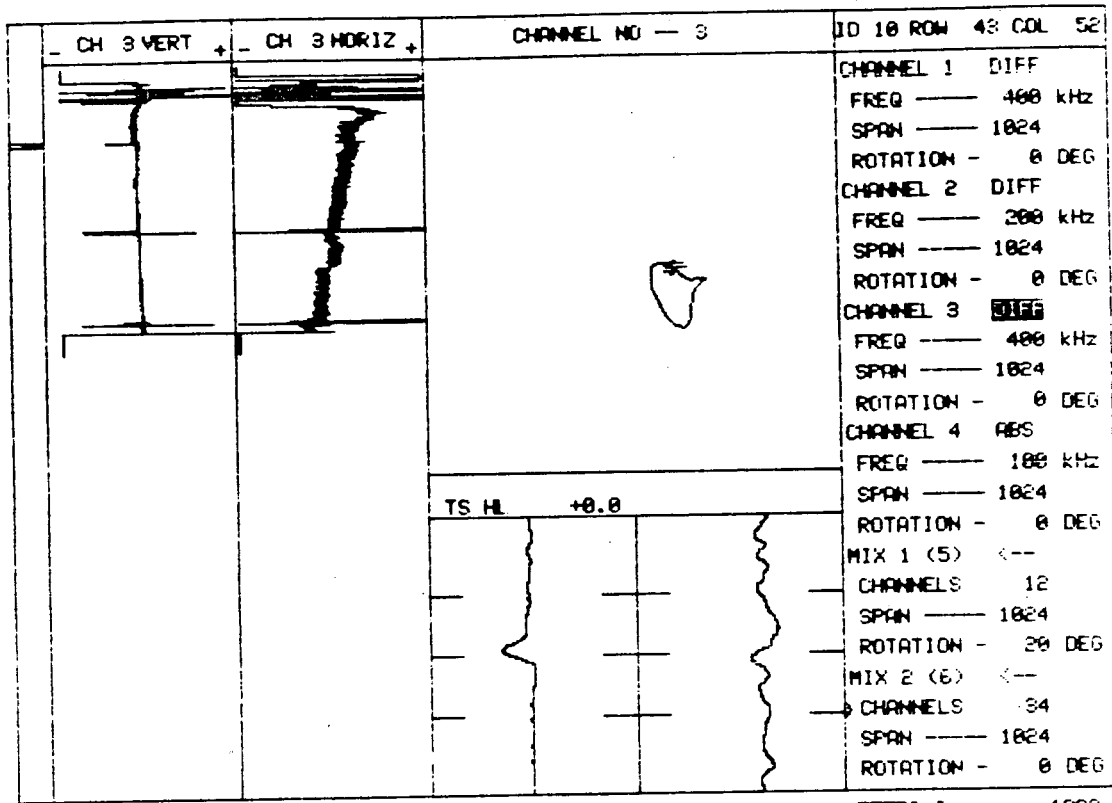
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	SCE SONGS	I	"A"	INLET	10/06/76	Edition 12.0 Rev 1



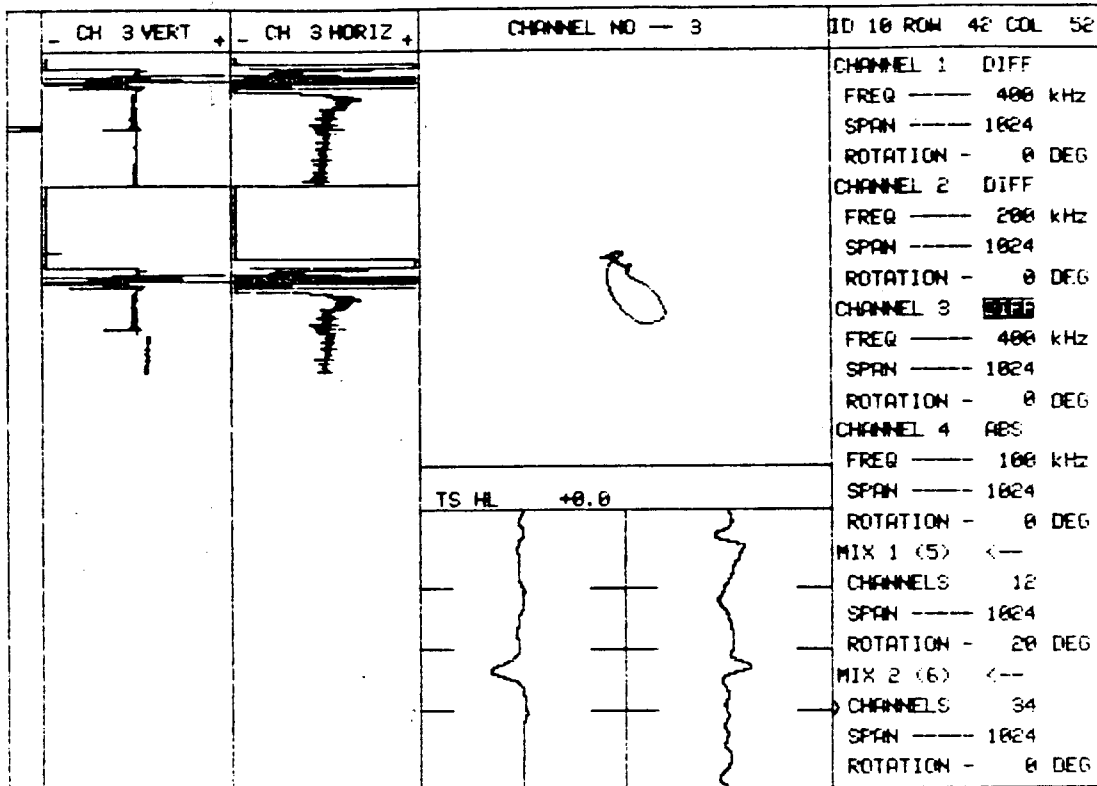
48	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1



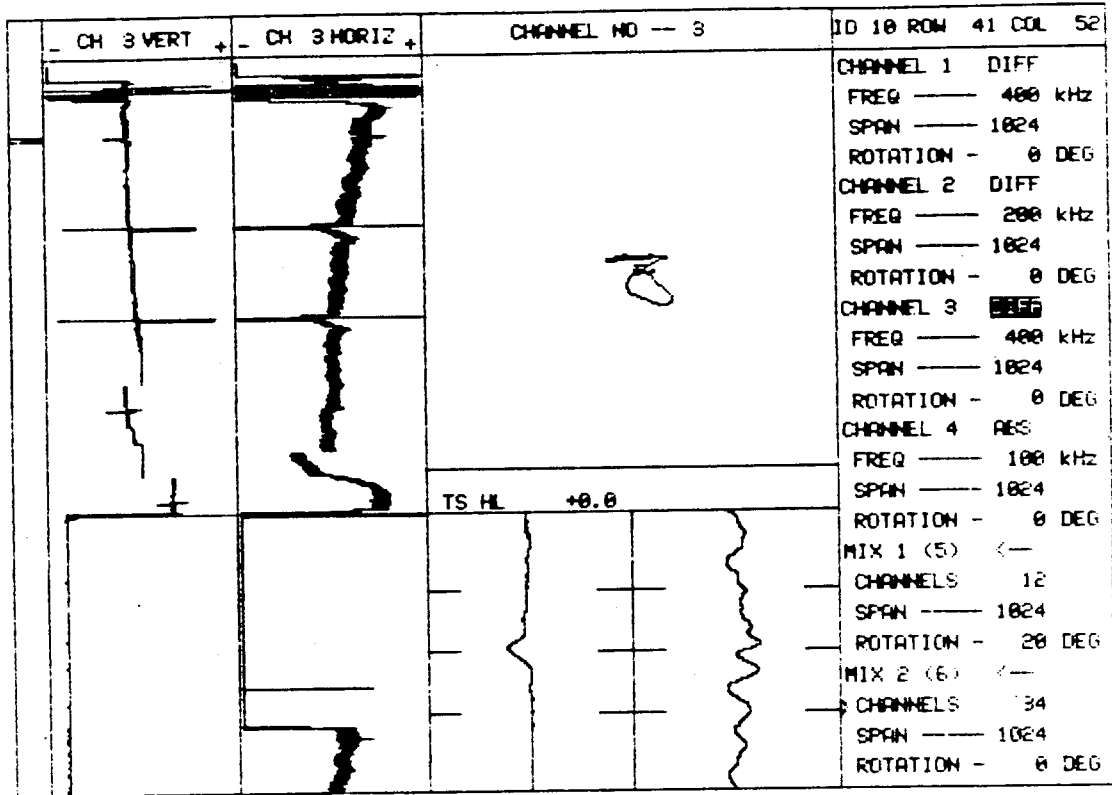
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	SCE SONGS	I	"A"	INLET	10/08/76	Edition 12.0 Rev 1



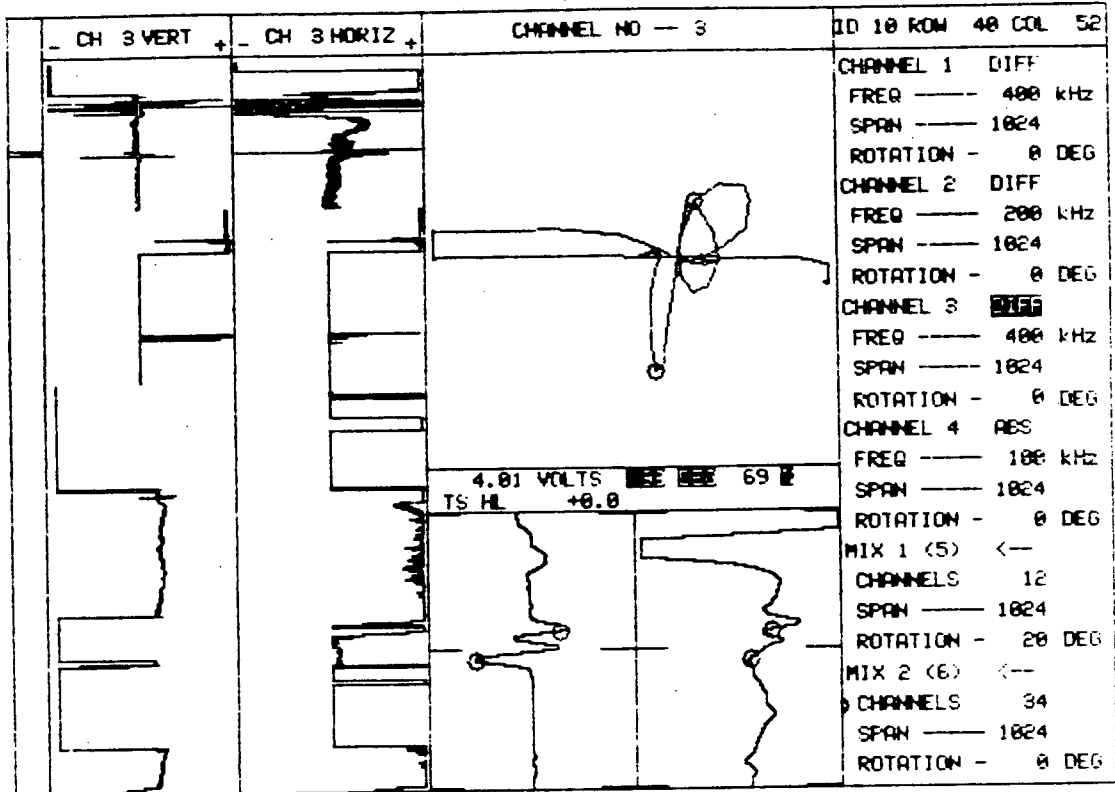
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	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1

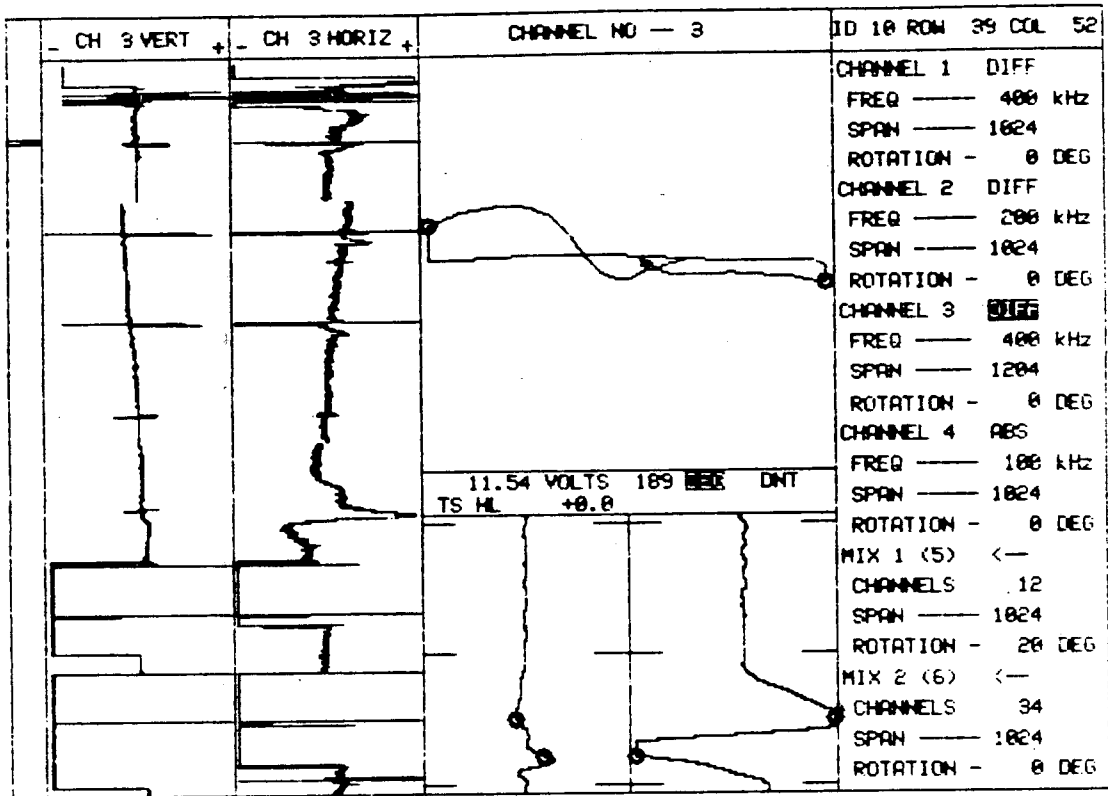


40	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1

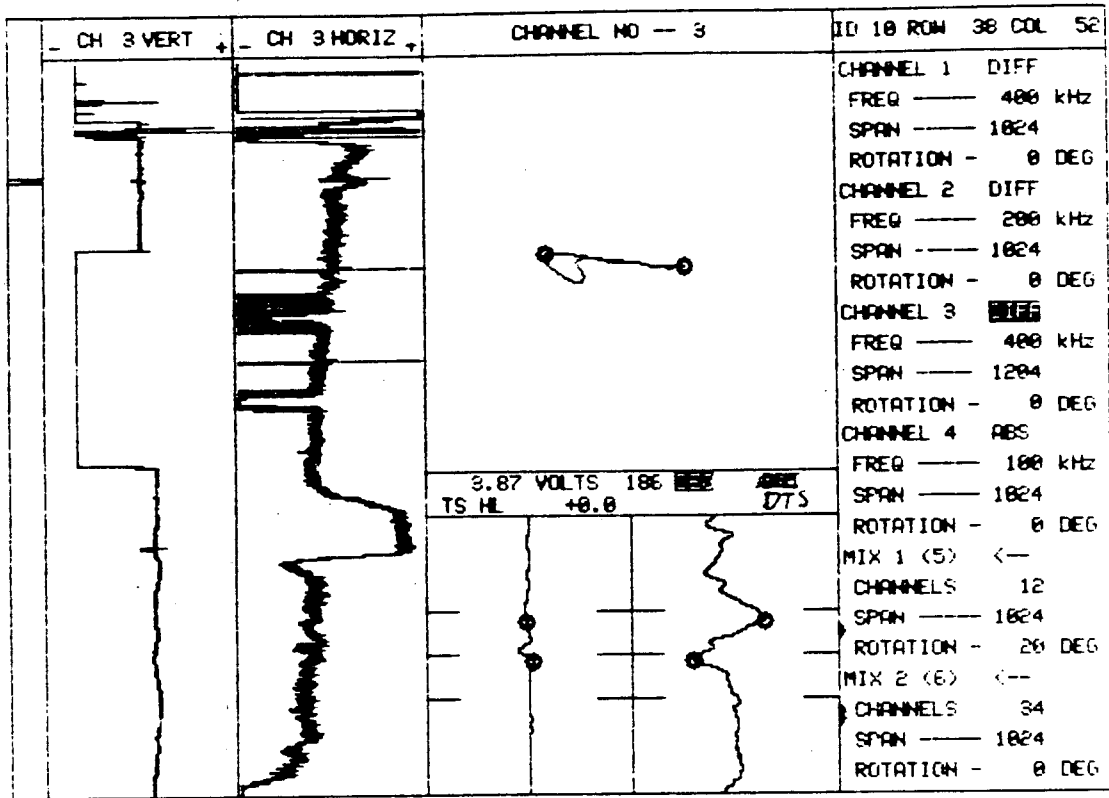


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	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1

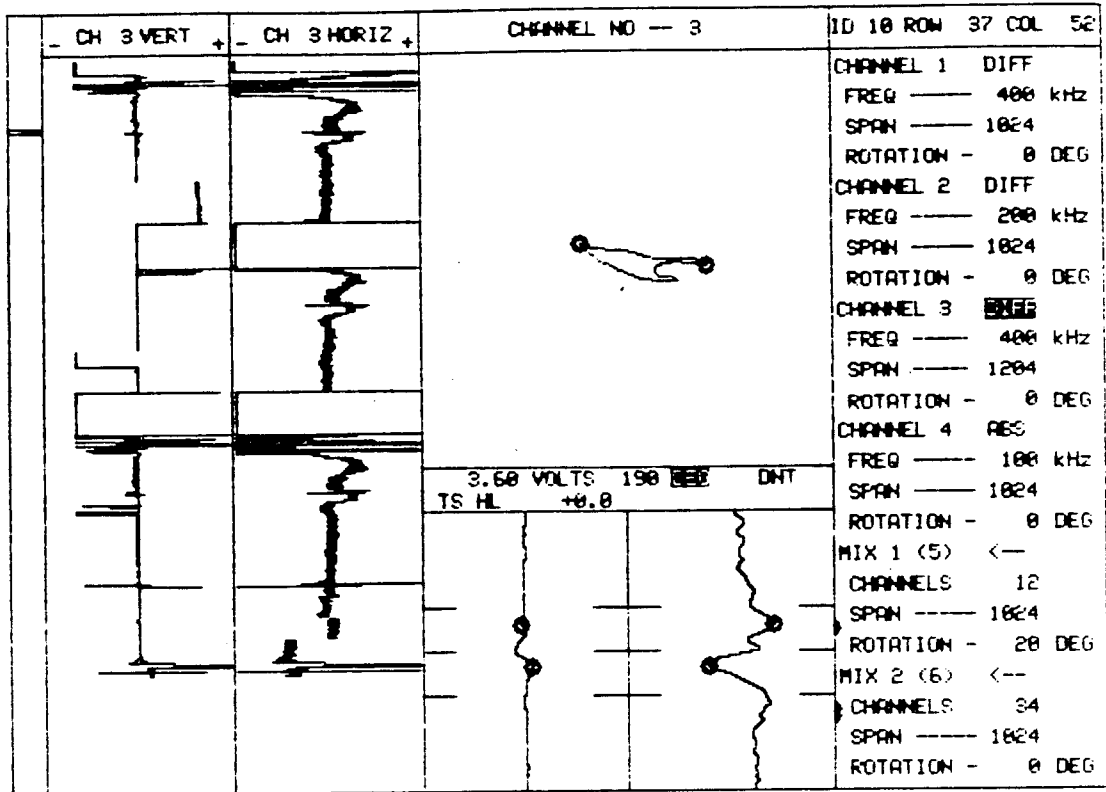




48 PLANT SCE SONGS UNIT# I S/G "A" LEG INLET DATE 10/00/76 ZETEC Inc. - 1983 Edition 12.0 Rev 1

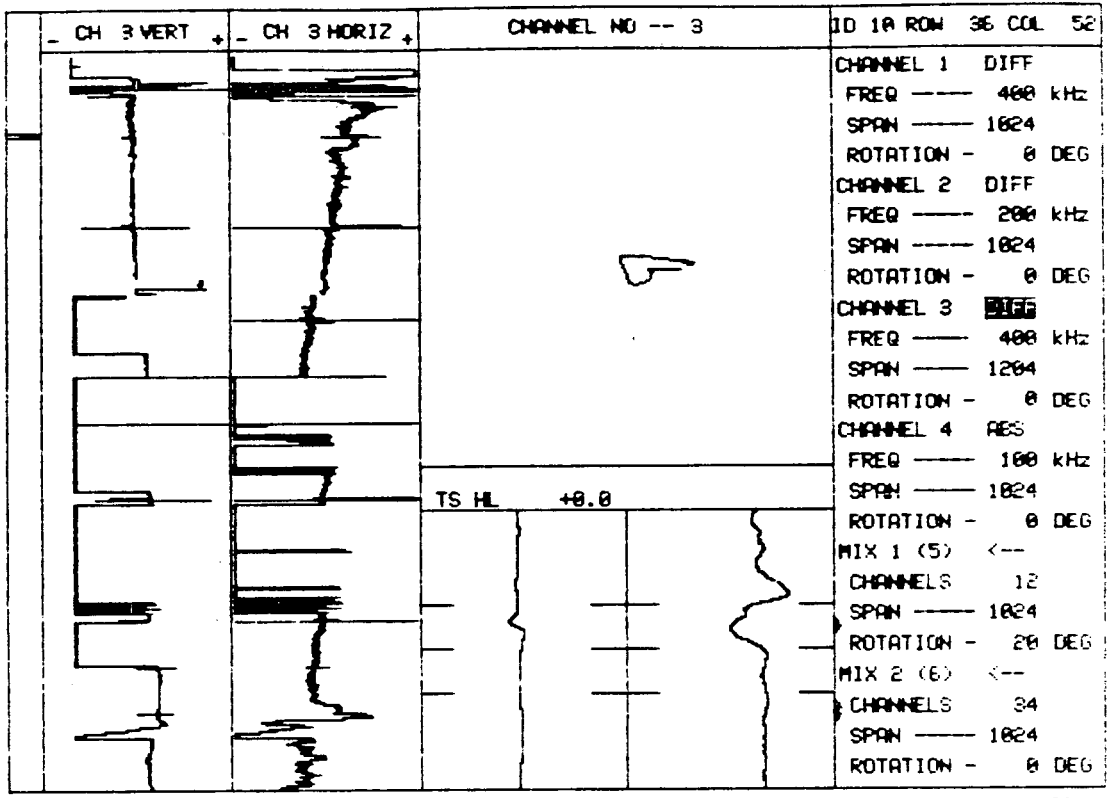


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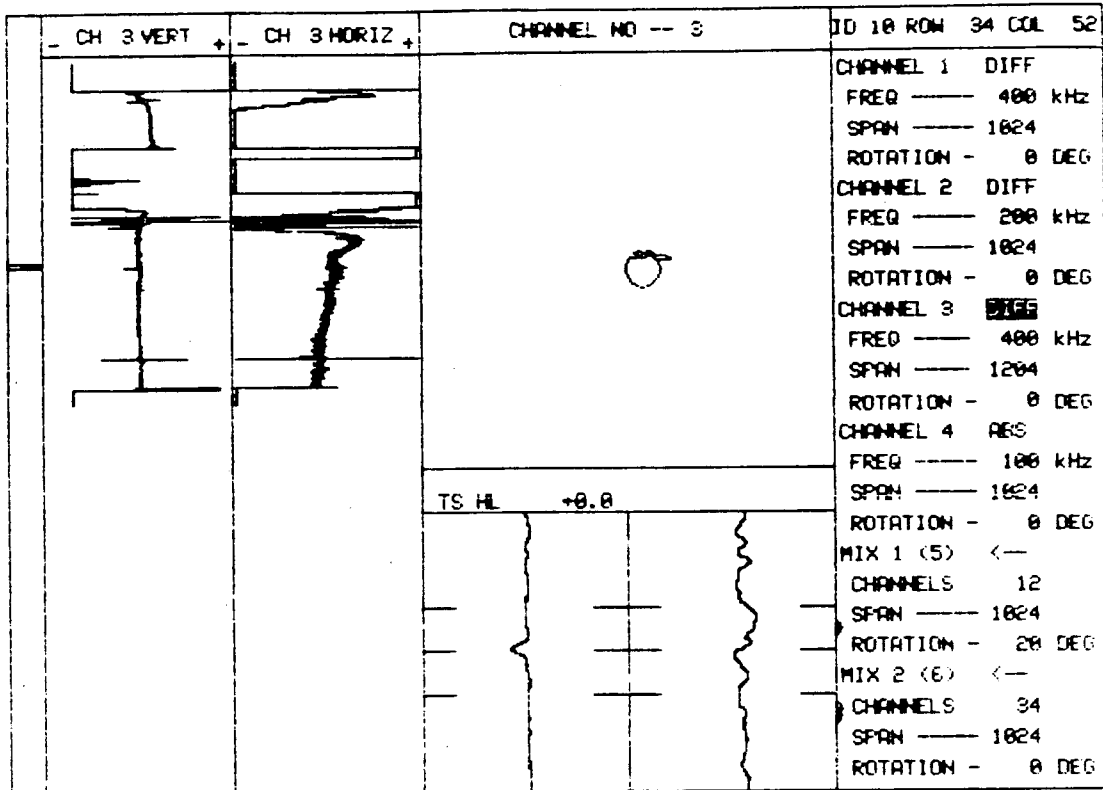


3.60 VOLTS 190 ~~000~~ DNT
TS HL +0.0

48 PLANT SCE SONGS UNIT# I S/G "A" LEG INLET DATE 10/00/76 ZETEC Inc. - 1983 Edition 12.0 Rev 1

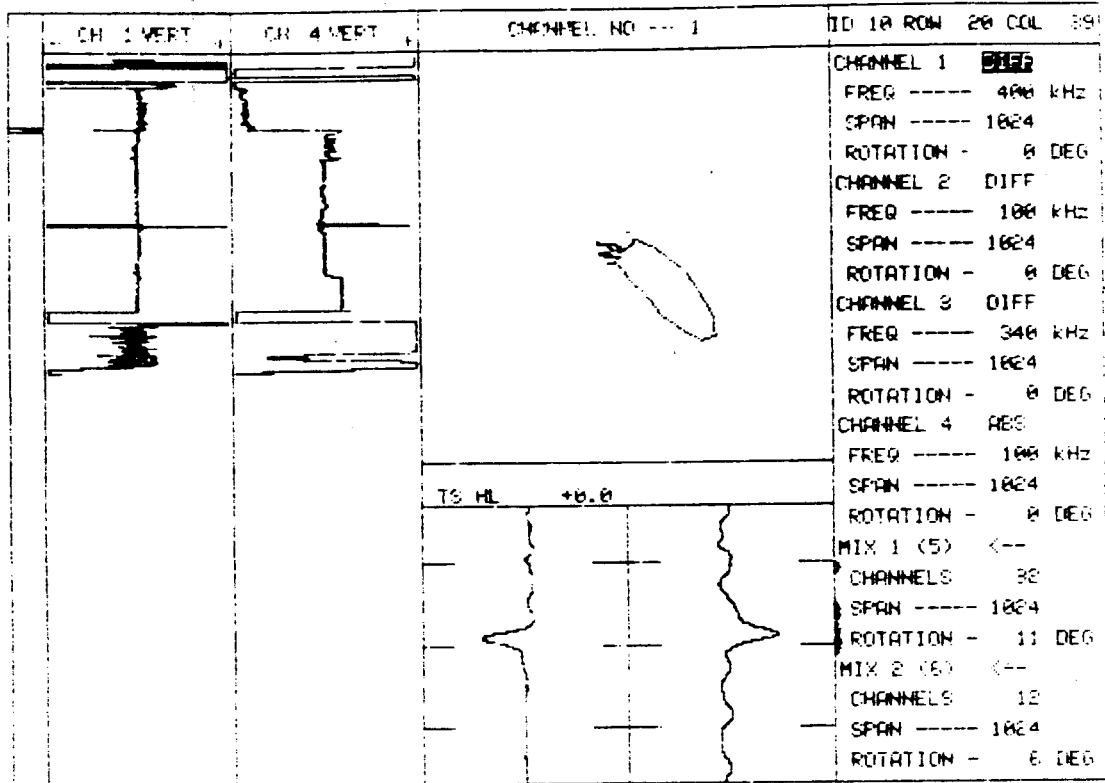


48 PLANT SCE SONGS UNIT# I S/G *A* LEG INLET DATE 10/08/76 ZETEC Inc. - 1983 Edition 12.0 Rev 1

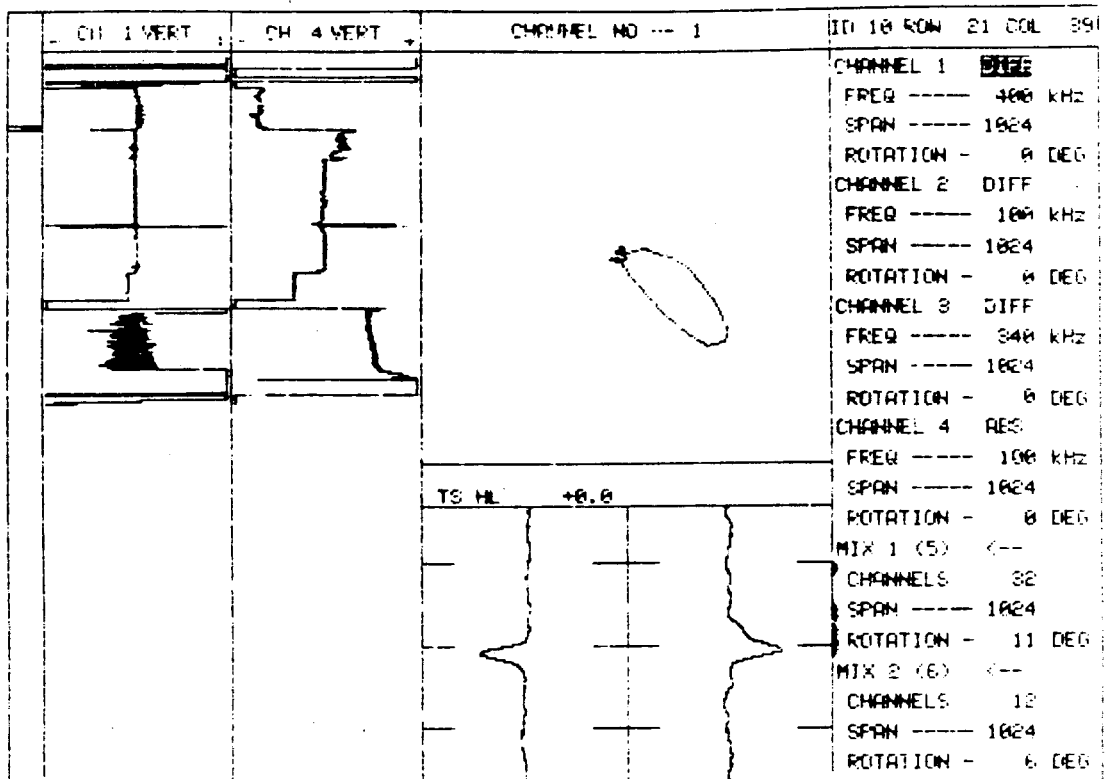


40	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1

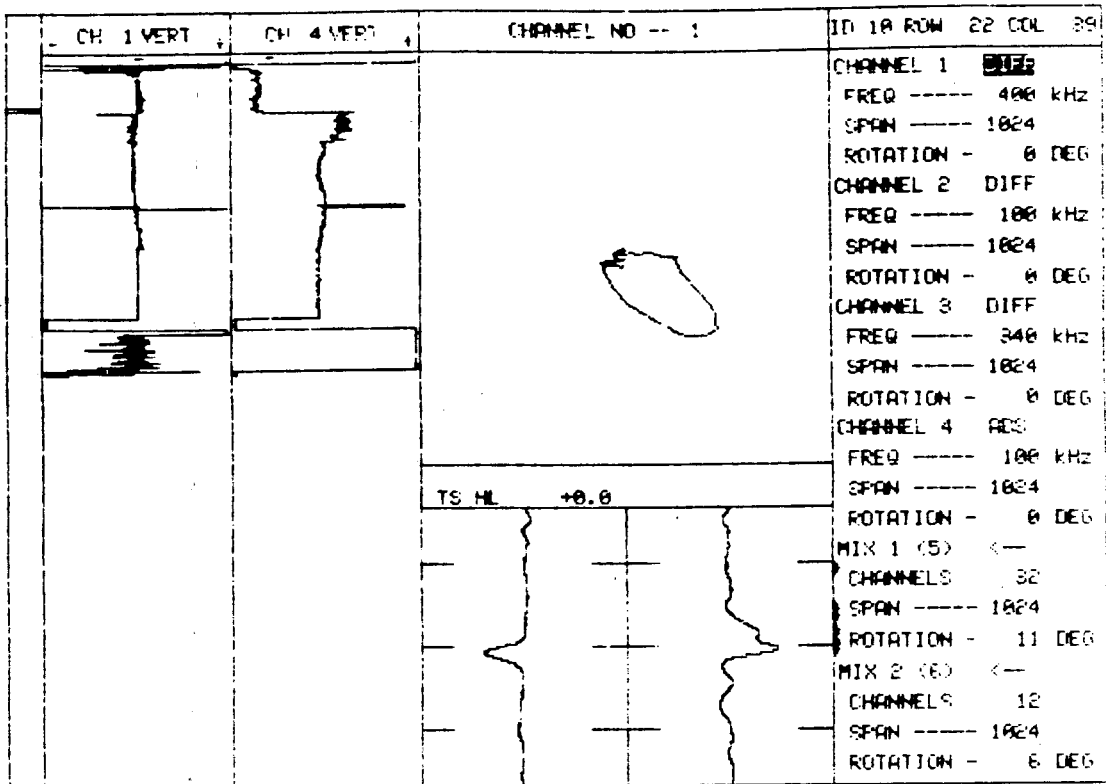
1980 COLUMN 39



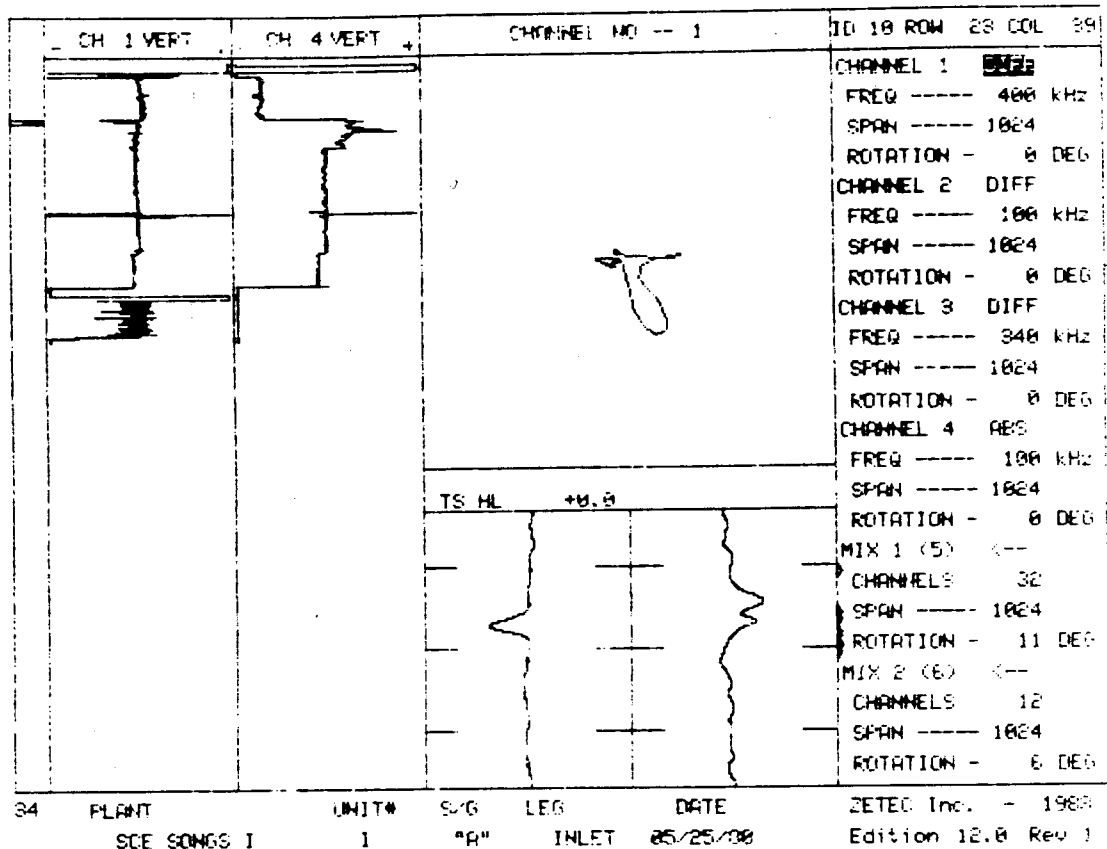
84	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS 1	1	"A"	INLET	05/25/88	Edition 12.0 Rev 1

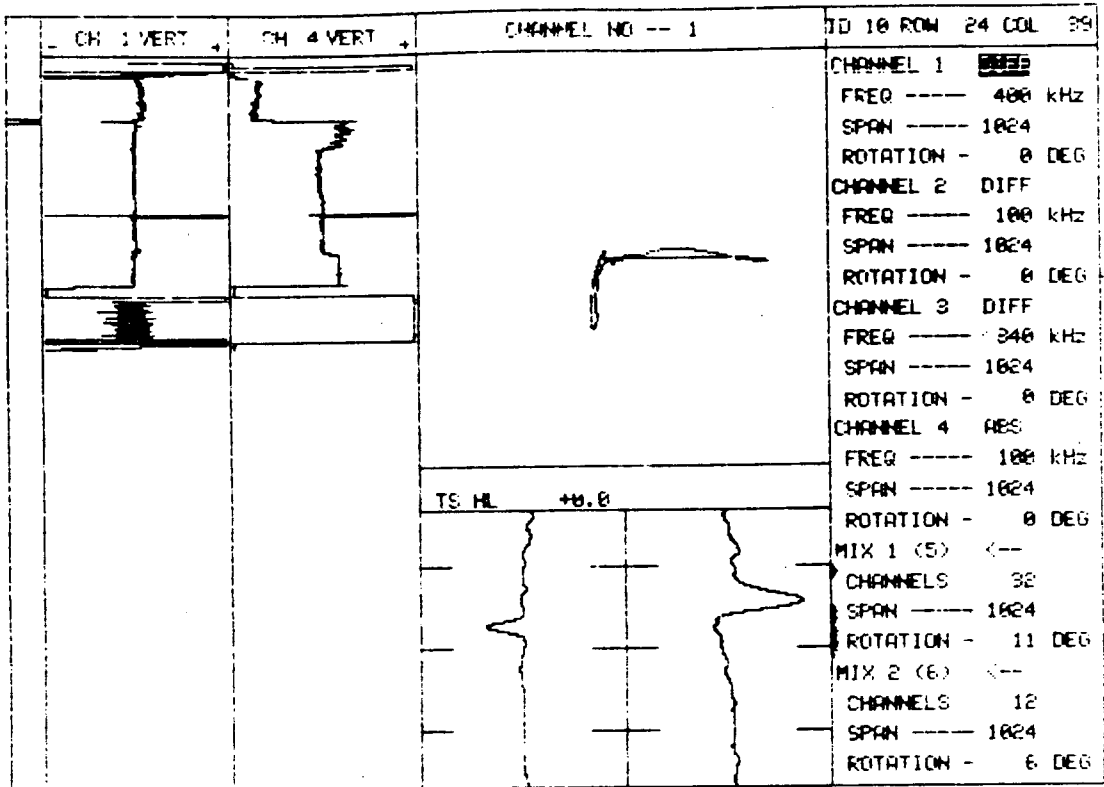


34	PLANT	UNIT#	S/G	LFG	DATE	ZETEC Inc. - 1983
	SCE SONGS 1	I	"A"	INLET	05/25/80	Edition 12.0 Rev 1

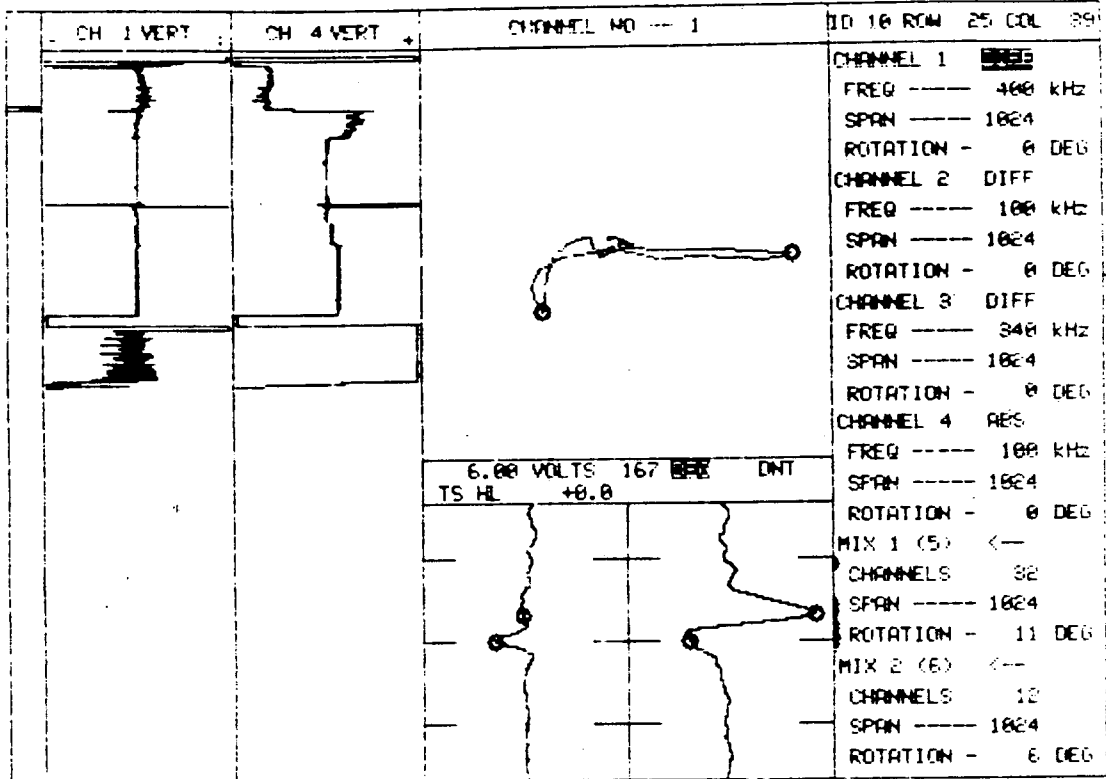


34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLET	05/25/80	Edition 12.0 Rev 1

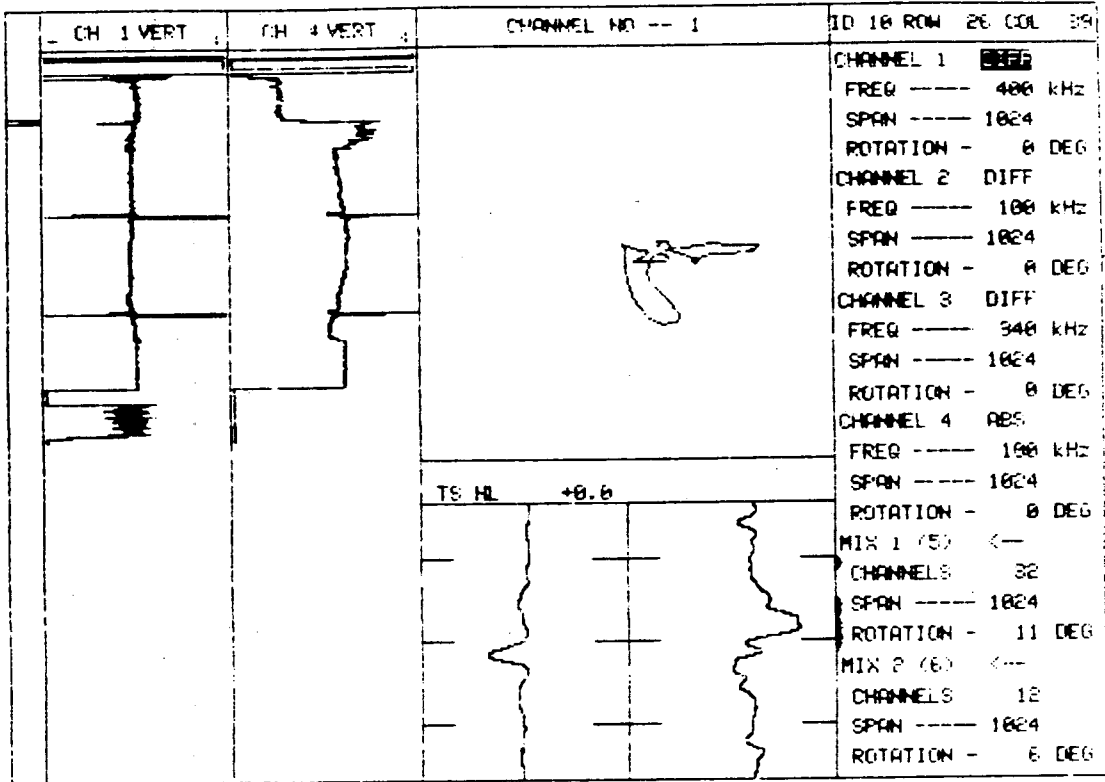




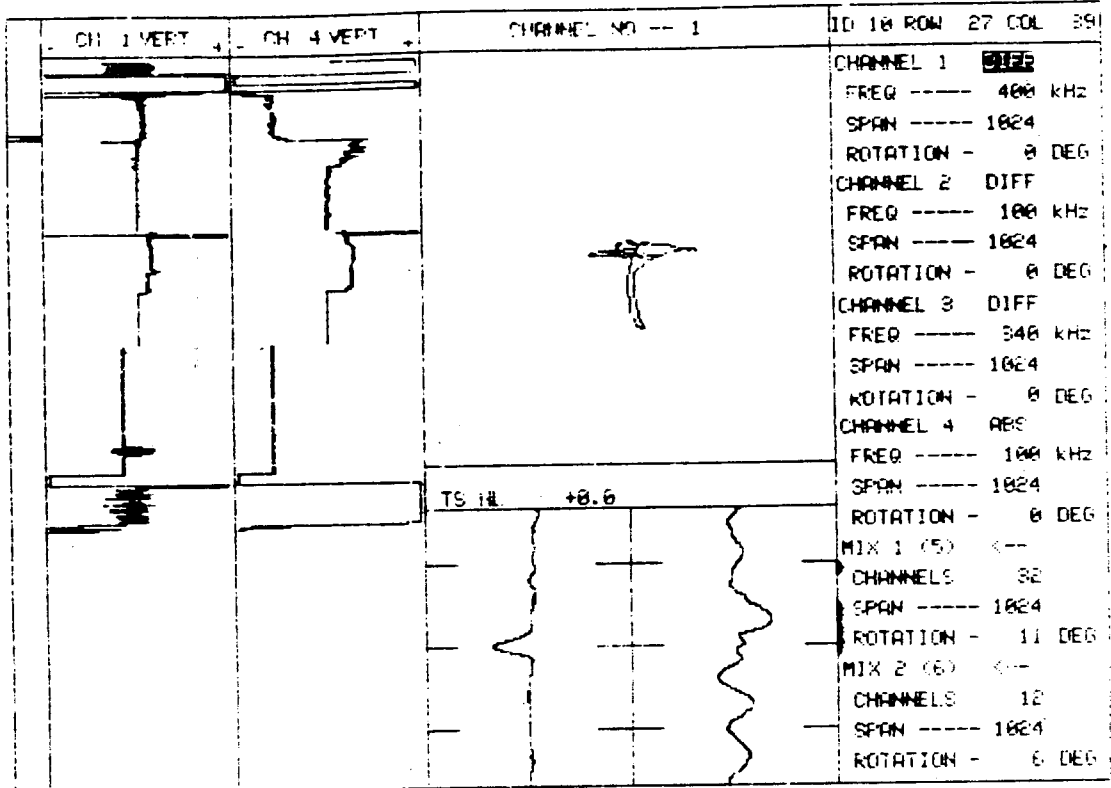
84	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLET	05/25/88	Edition 12.0 Rev 1



34 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1988
 SCE SONGS I I "A" INLET 05/25/80 Edition 12.0 Rev 1

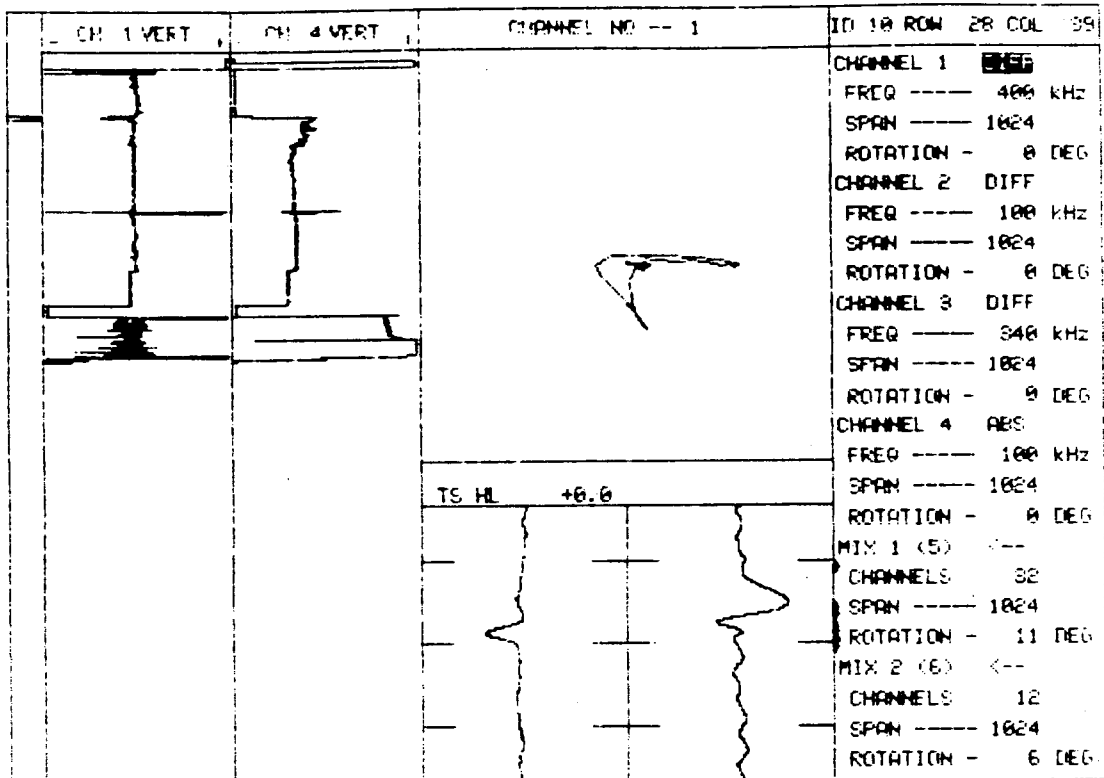


34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLET	05/25/88	Edition 12.0 Rev 1

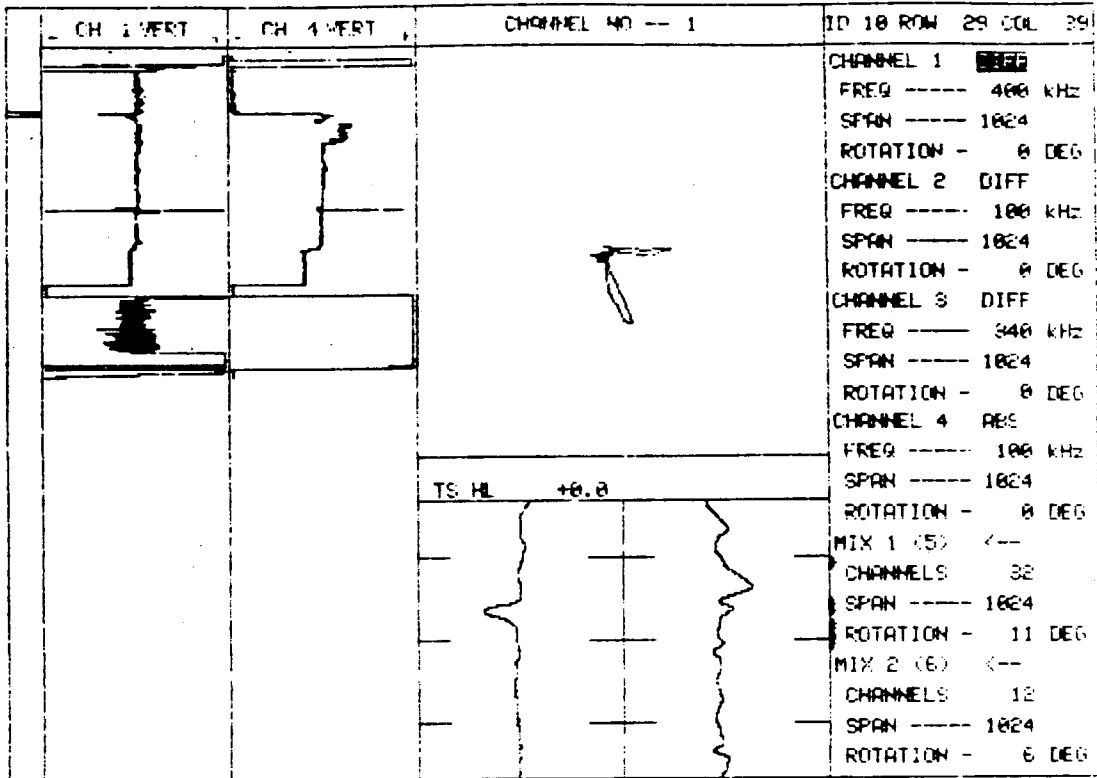


34 PLANT SCE SONGS I UNIT# I S/G "R" LEC INLET DATE 05/25/88

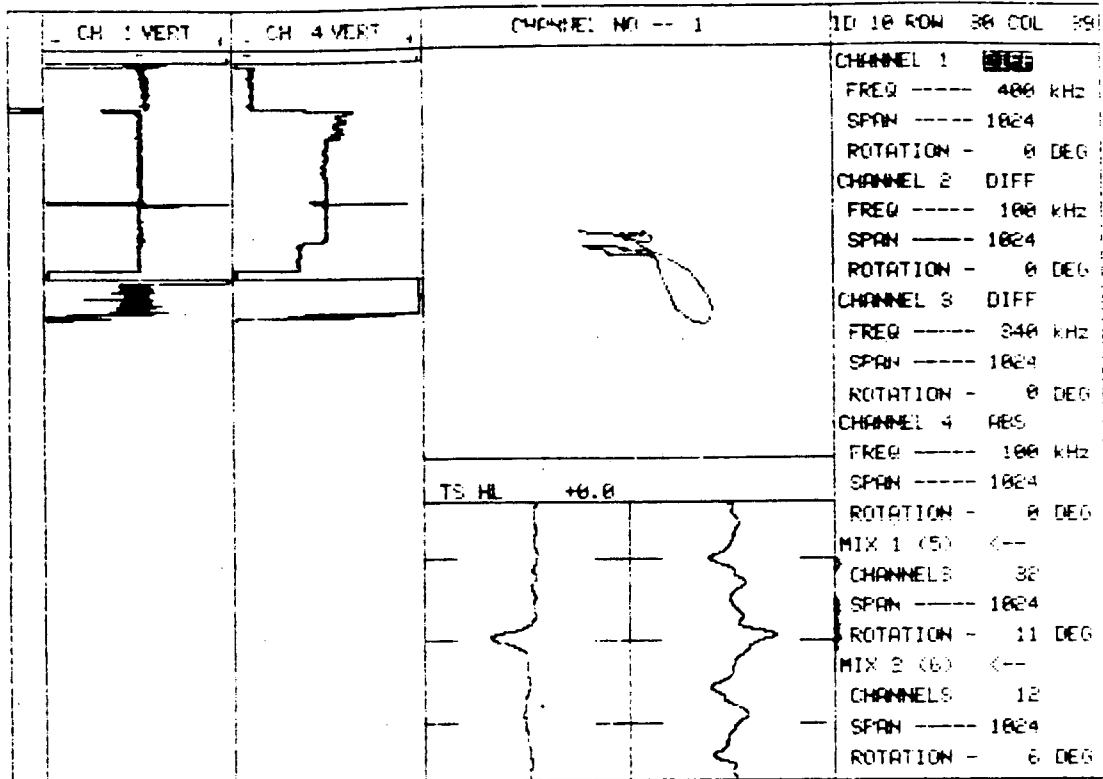
ZETEC Inc. - 1988
Edition 12.0 Rev 1



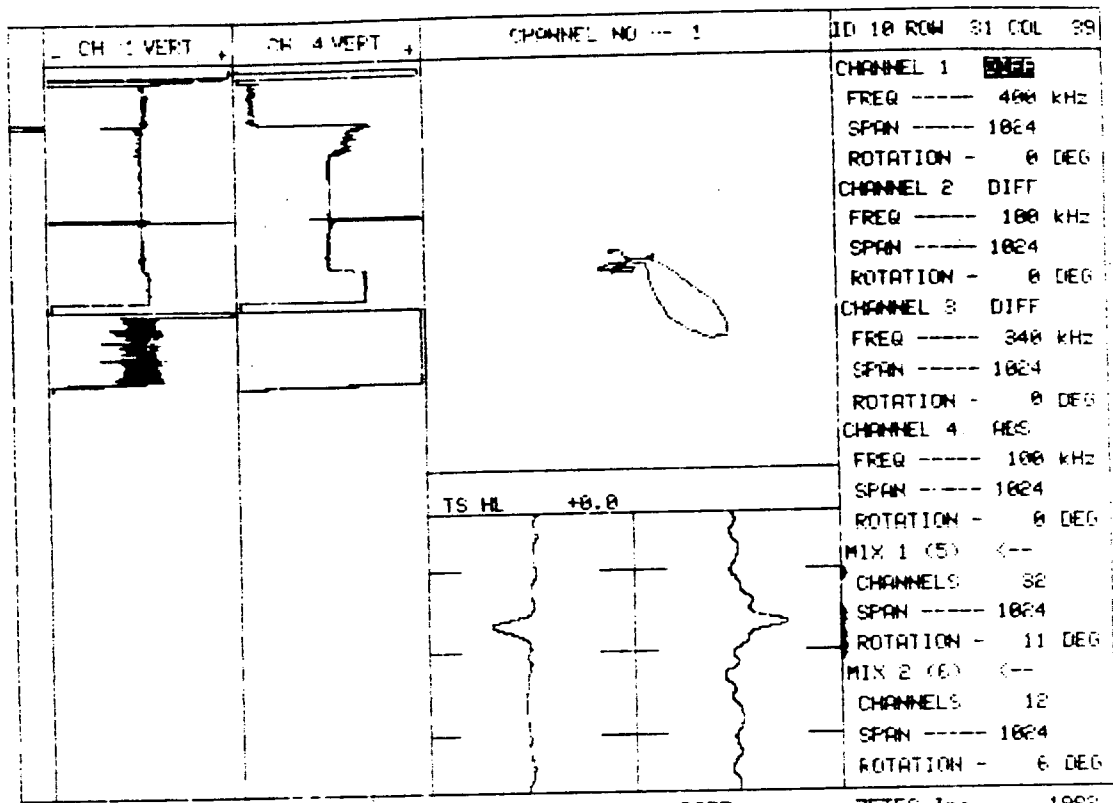
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	"A"	INLET	05/25/88	Edition 12.0 Rev 1



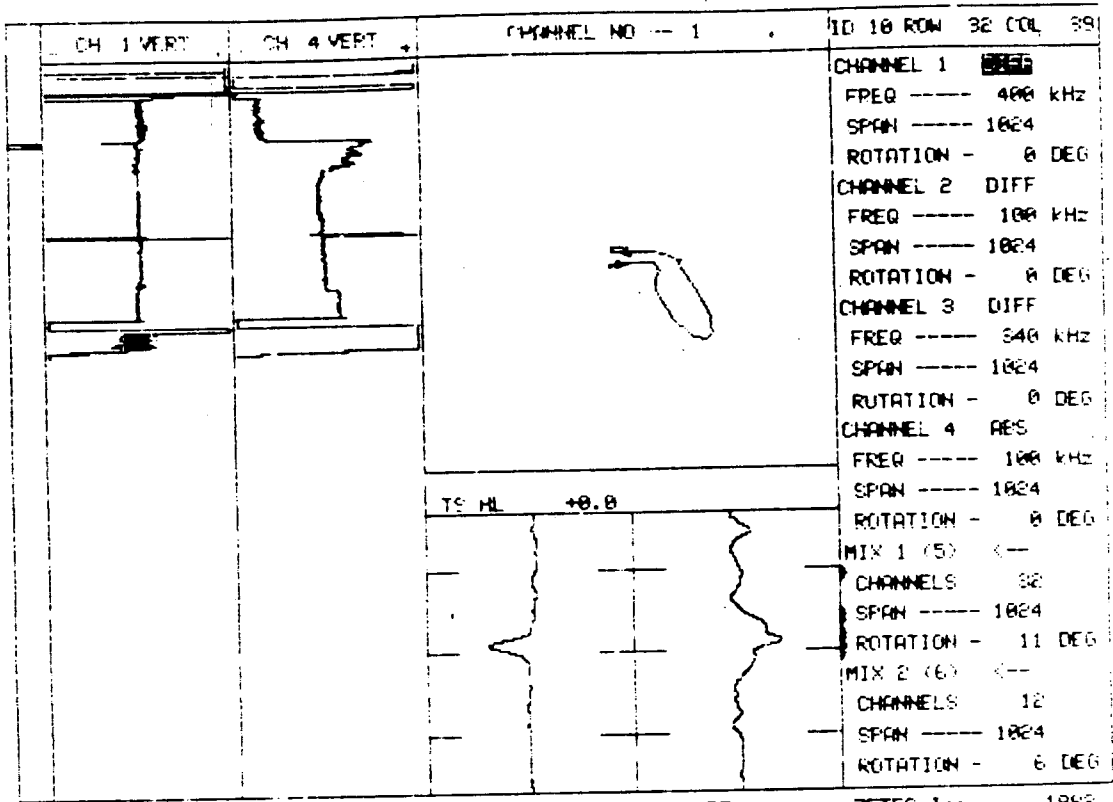
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLET	05/25/88	Edition 12.0 Rev 1



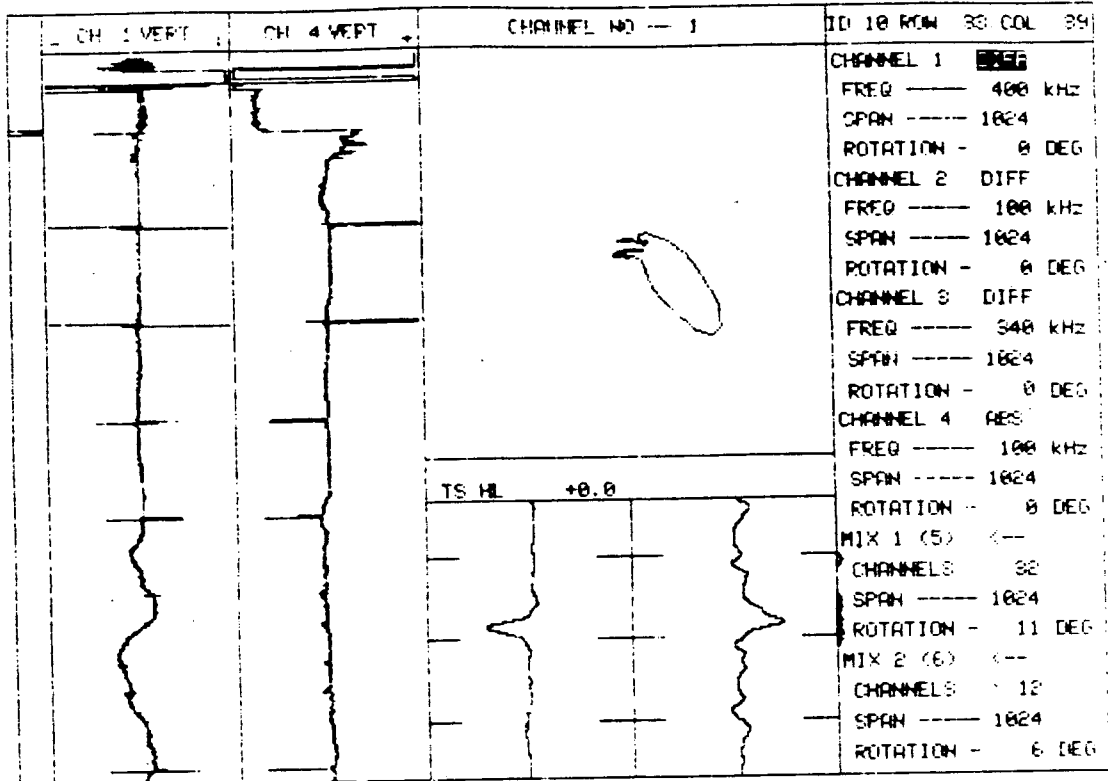
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLET	05/25/08	Edition 12.0 Rev 1



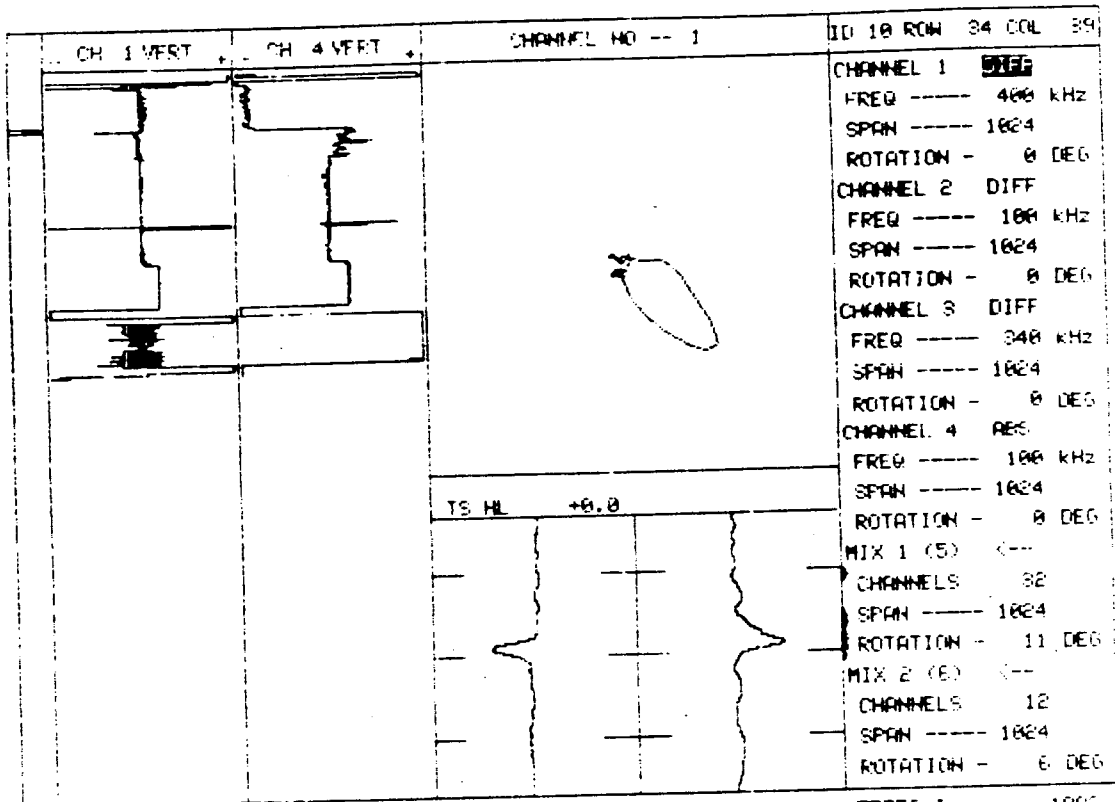
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	"A"	INLFT	05/25/88	Edition 12.0 Rev 1



84 PLANT SCE SONGS I UNIT# 1 S/G "P" LEG INLET DATE 05/25/88 ZETEC Inc. - 1988 Edition 12.0 Rev 1

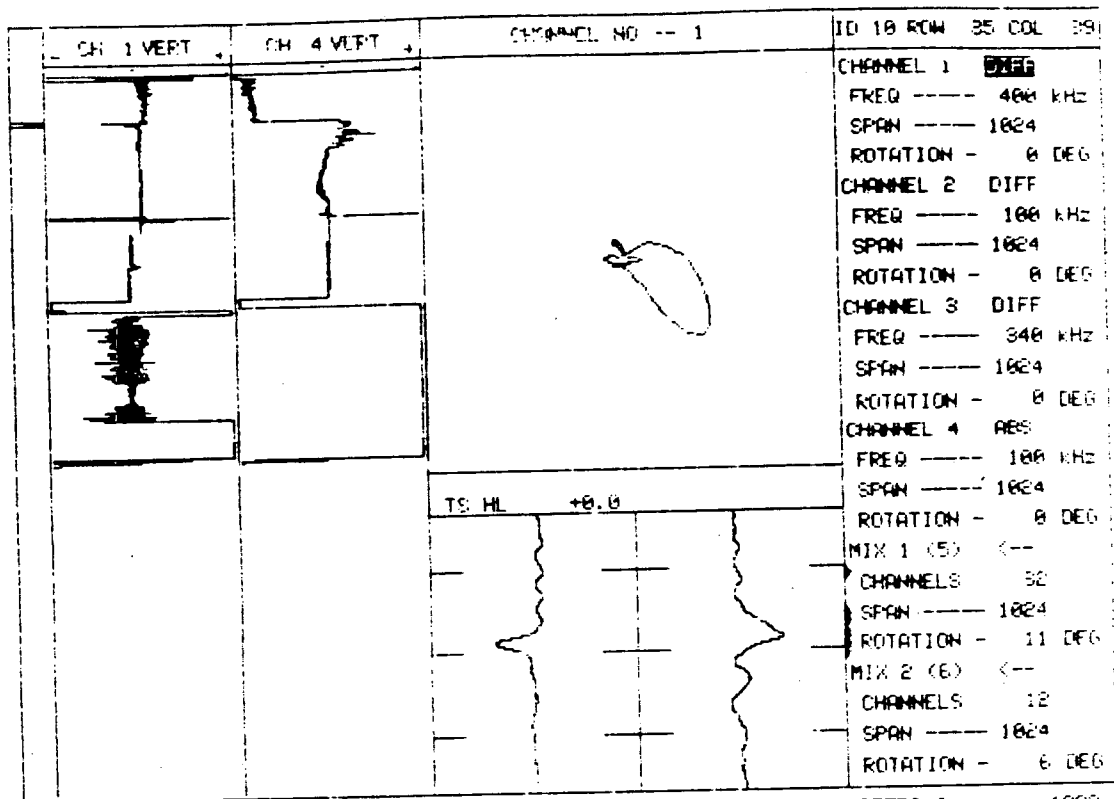


34 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1988
 SCE SONGS 1 I "A" INLET 05/25/90 Edition 12.0 Rev 1

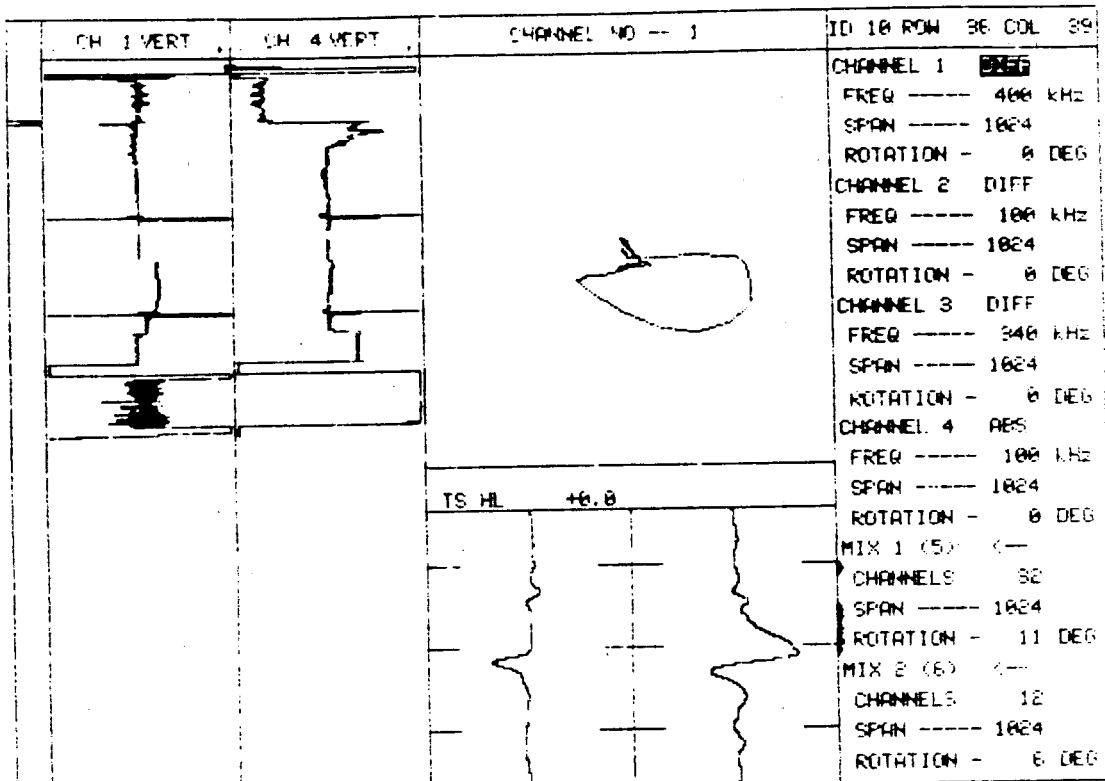


34 PLANT SCE SONGS I UNIT# I S/G "R" LEG INLET DATE 05/25/80

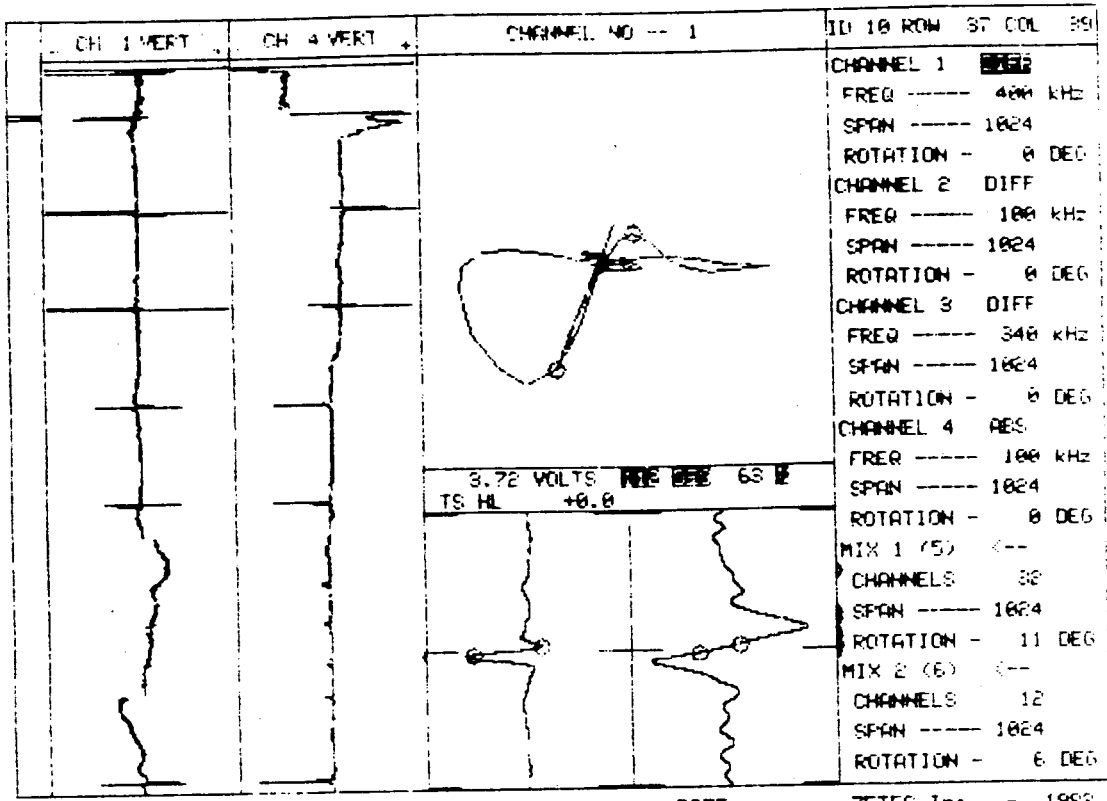
ZETEC Inc. - 1985
Edition 13.0 Rev 1



34 PLANT SCE SONGS I UNIT# I S/G "A" LEG INLET DATE 05/25/88 ZETEC Inc. - 1988 Edition 12.0 Rev 1



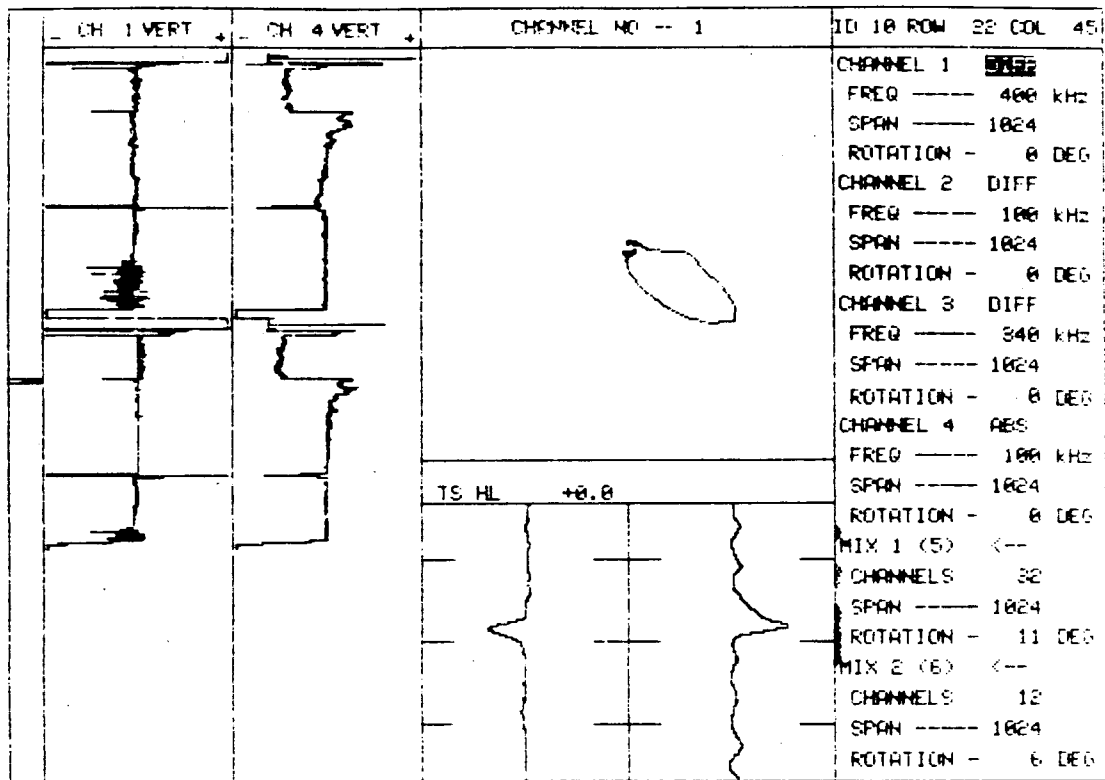
34 PLANT SCE SONGS I UNIT# I S/G "A" LEG INLET DATE 05/25/80
 ZETEC Inc. - 1983 Edition 12.0 Rev 1



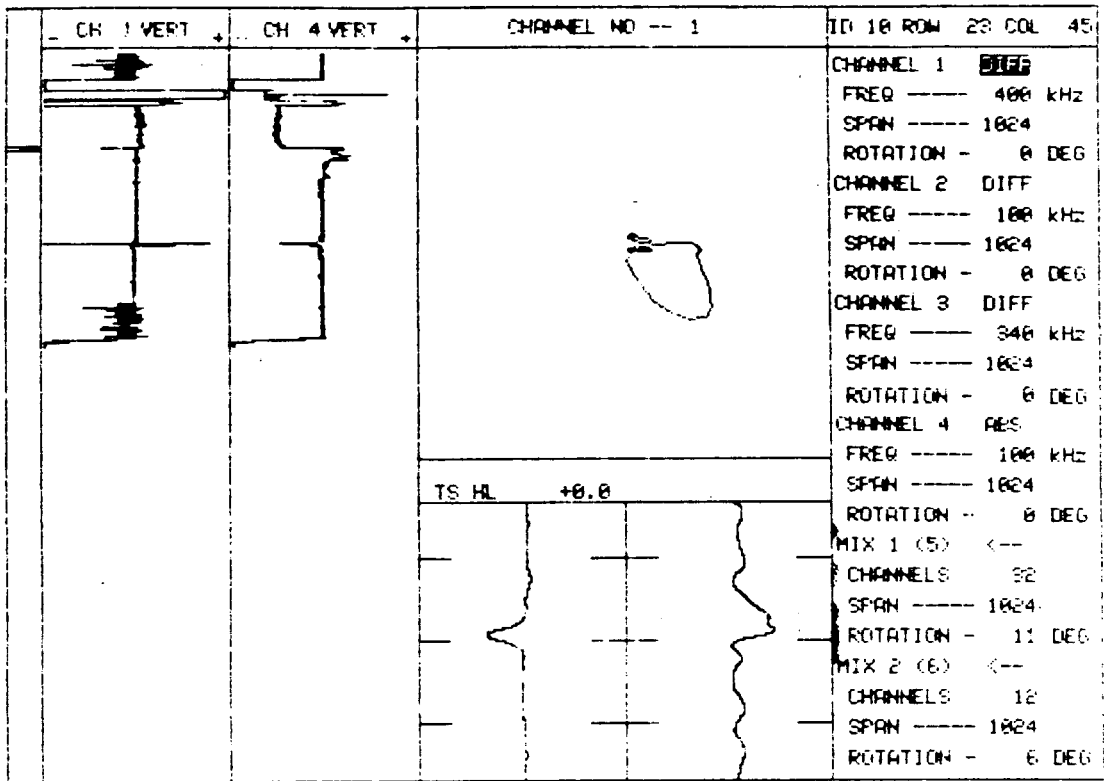
3.72 VOLTS **RES RES** 6S **RES**
 TS HL +0.0

34 PLANT SCE SONGS I UNIT# I S/G "A" LEG INLET DATE 05/25/88 ZETEC Inc. - 1983 Edition 12.0 Rev 1

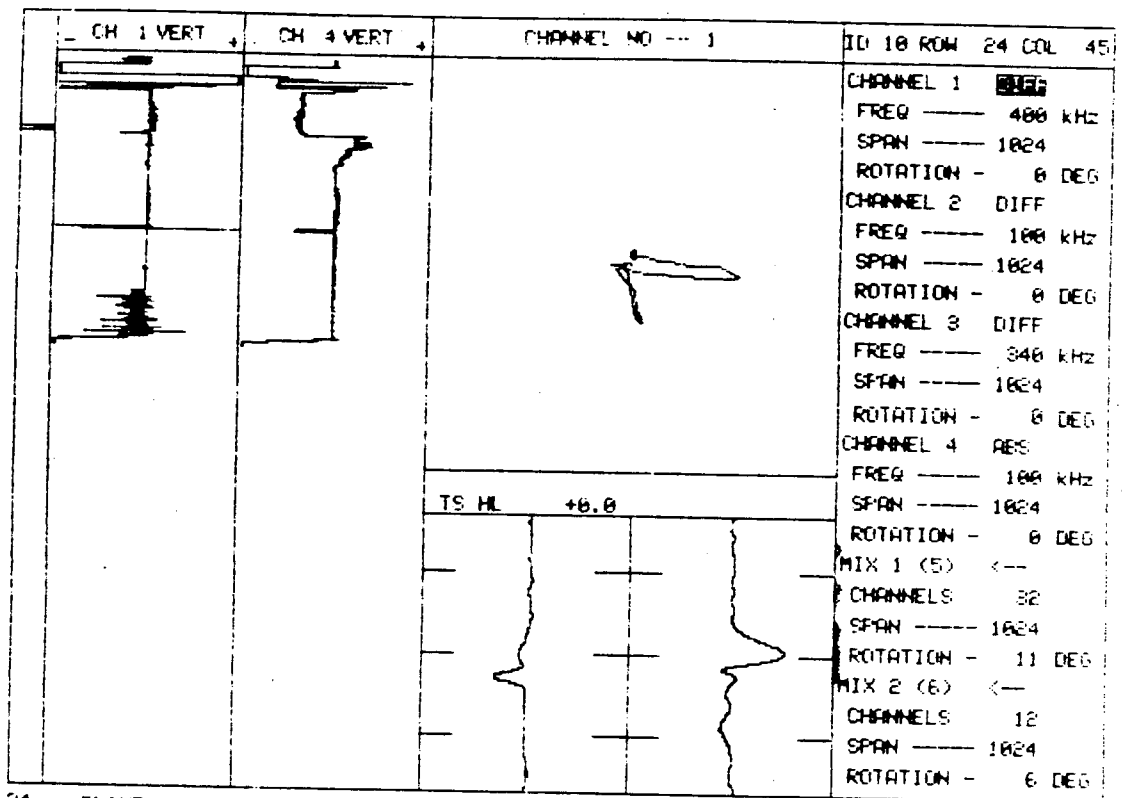
1980 COLUMN 45



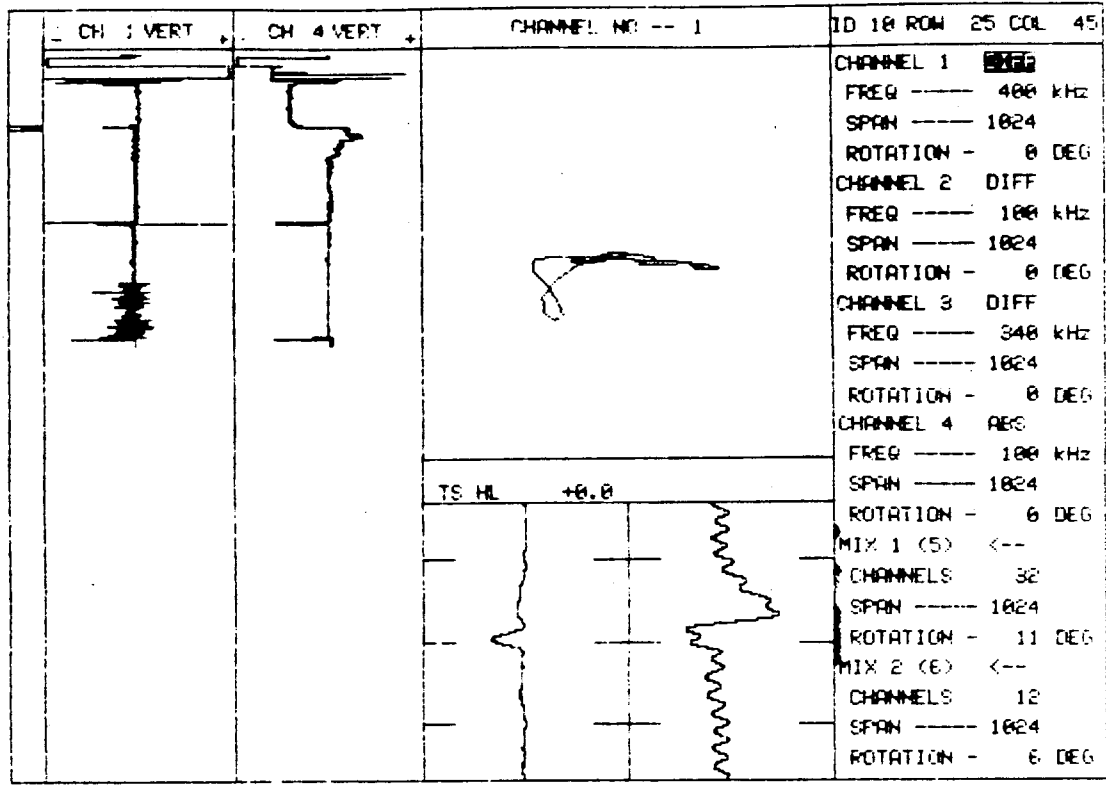
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	A	INLET	05/25/88	Edition 12.0 Rev 1



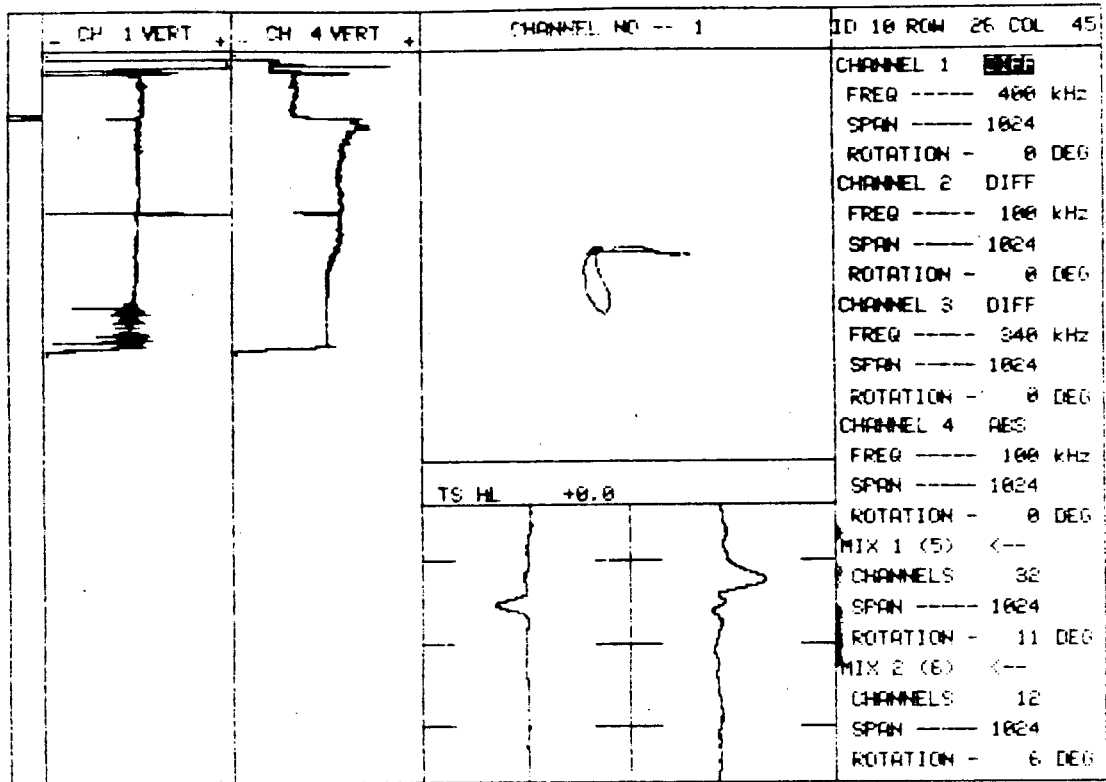
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	A	INLET	05/25/80	Edition 12.0 Rev 1



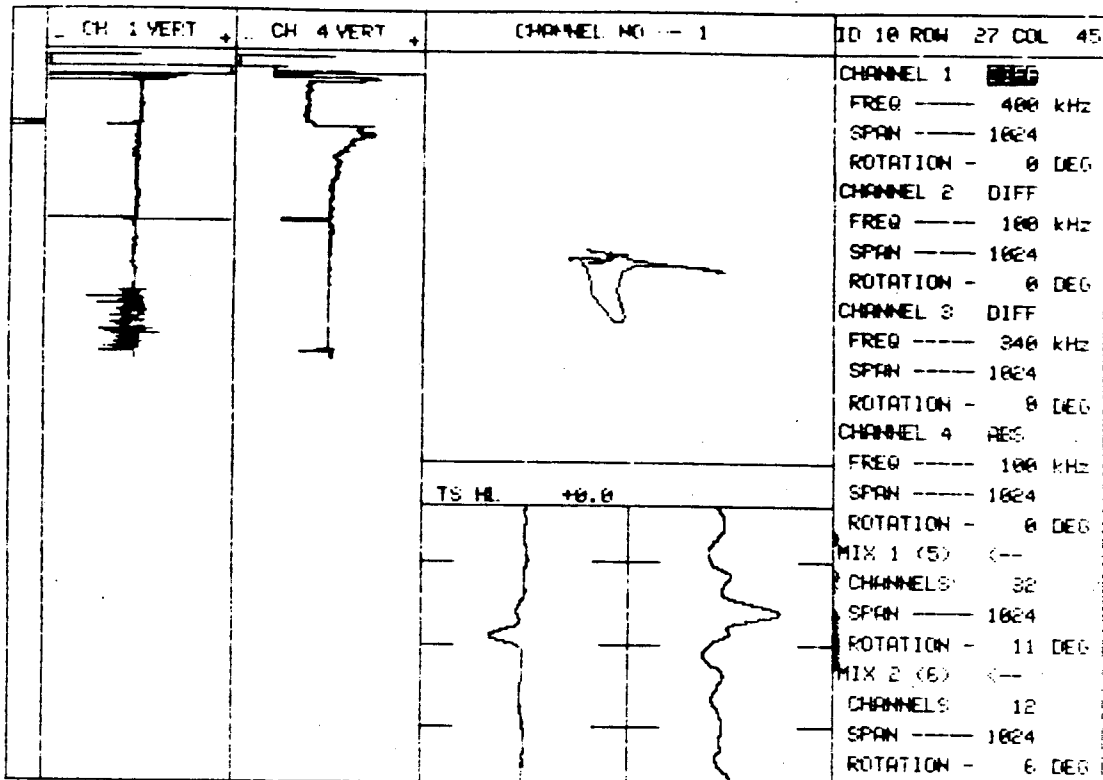
34 PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 05/25/88
 ZETEC Inc. - 1987 Edition 12.0 Rev 1



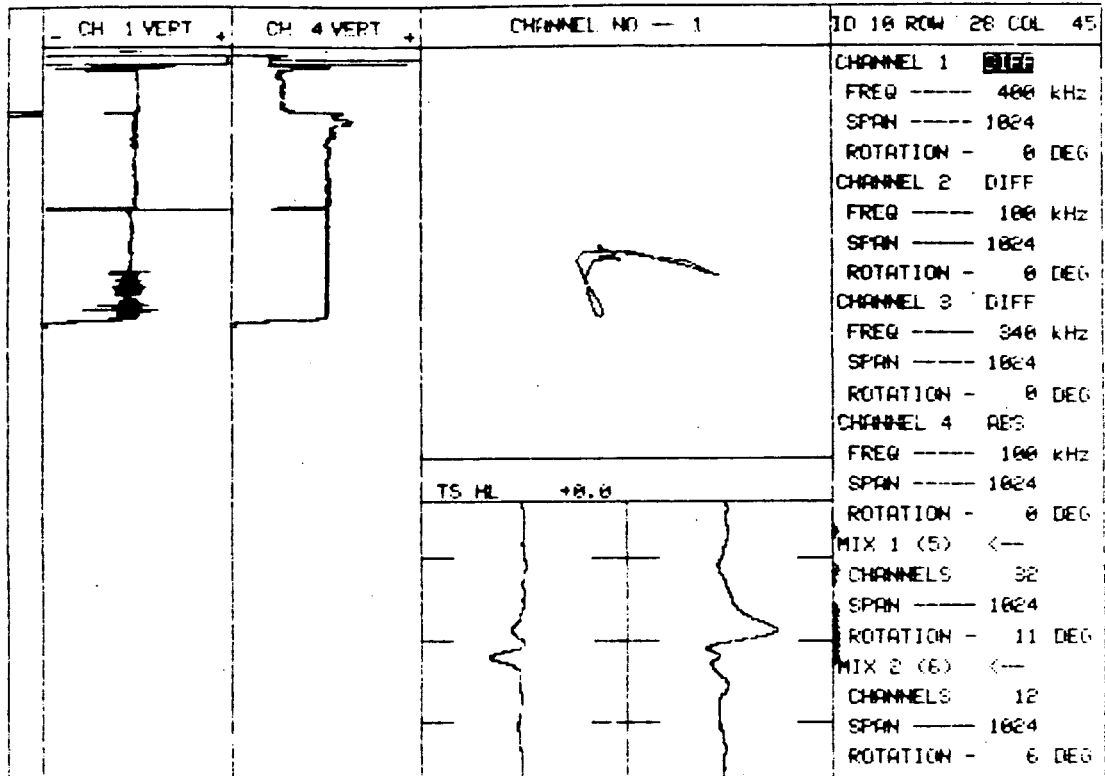
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	A	INLET	05/25/88	Edition 12.0 Rev 1



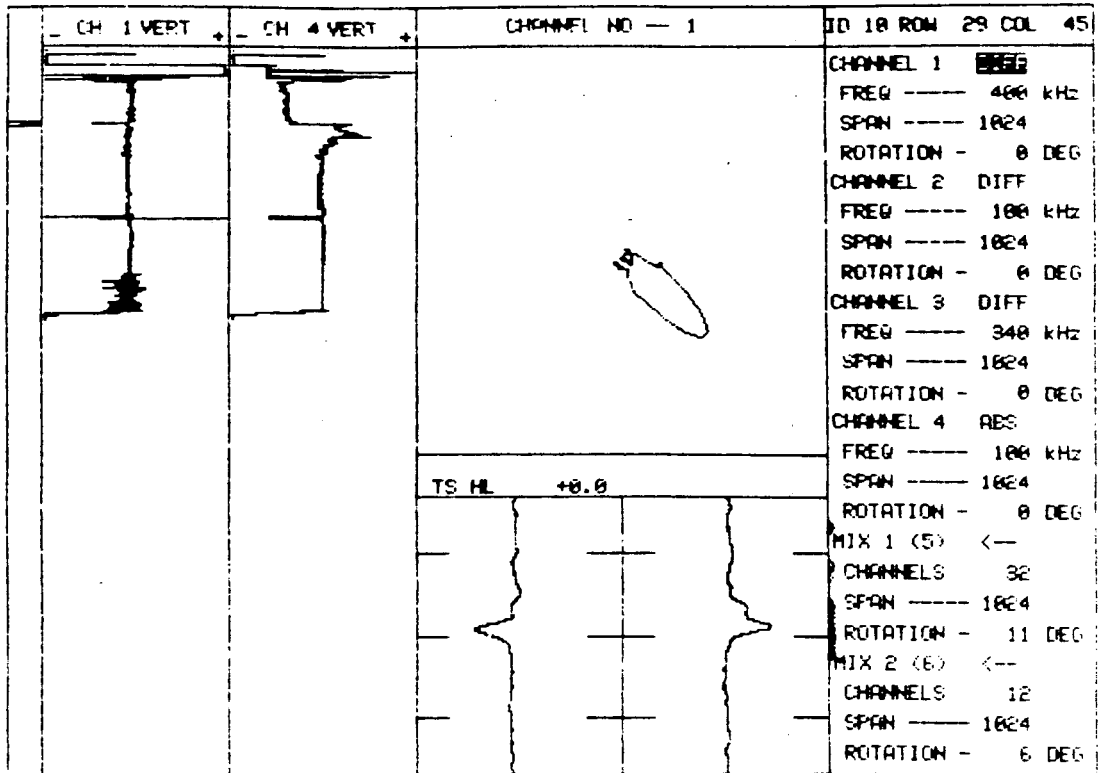
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	A	INLET	05/25/80	Edition 12.0 Rev 1



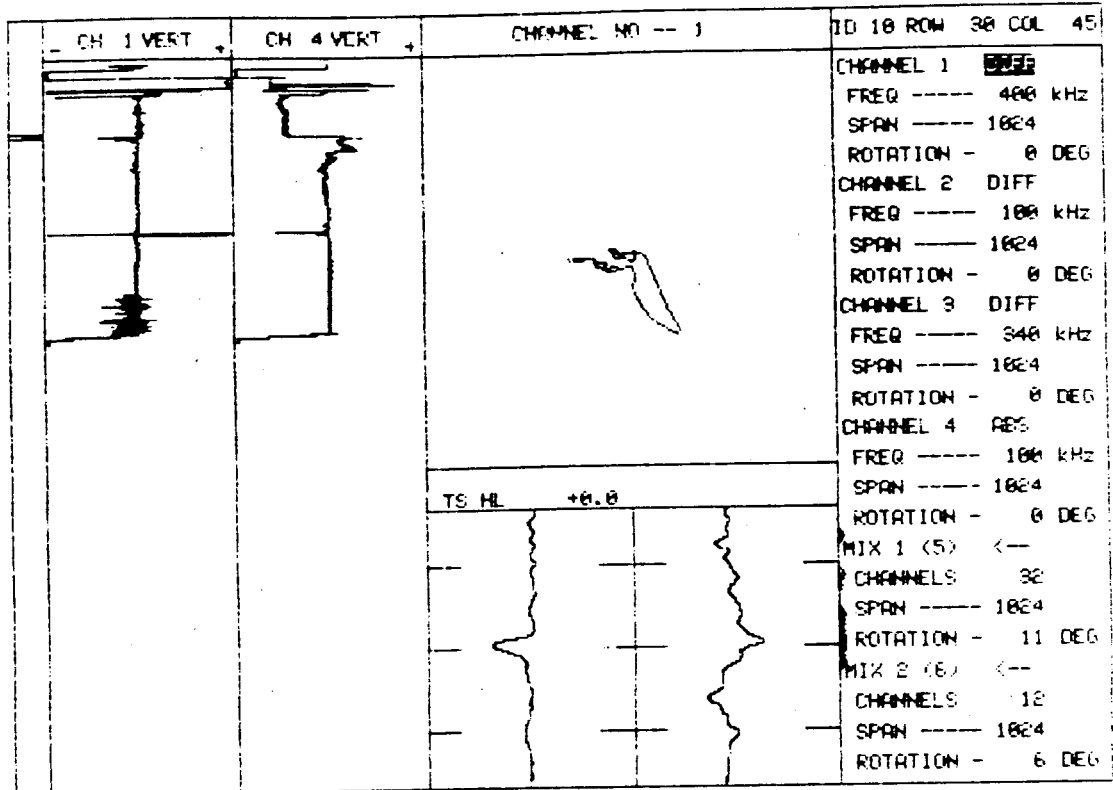
34 PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 05/25/88 ZETEC Inc. - 1988 Edition 12.0 Rev 1



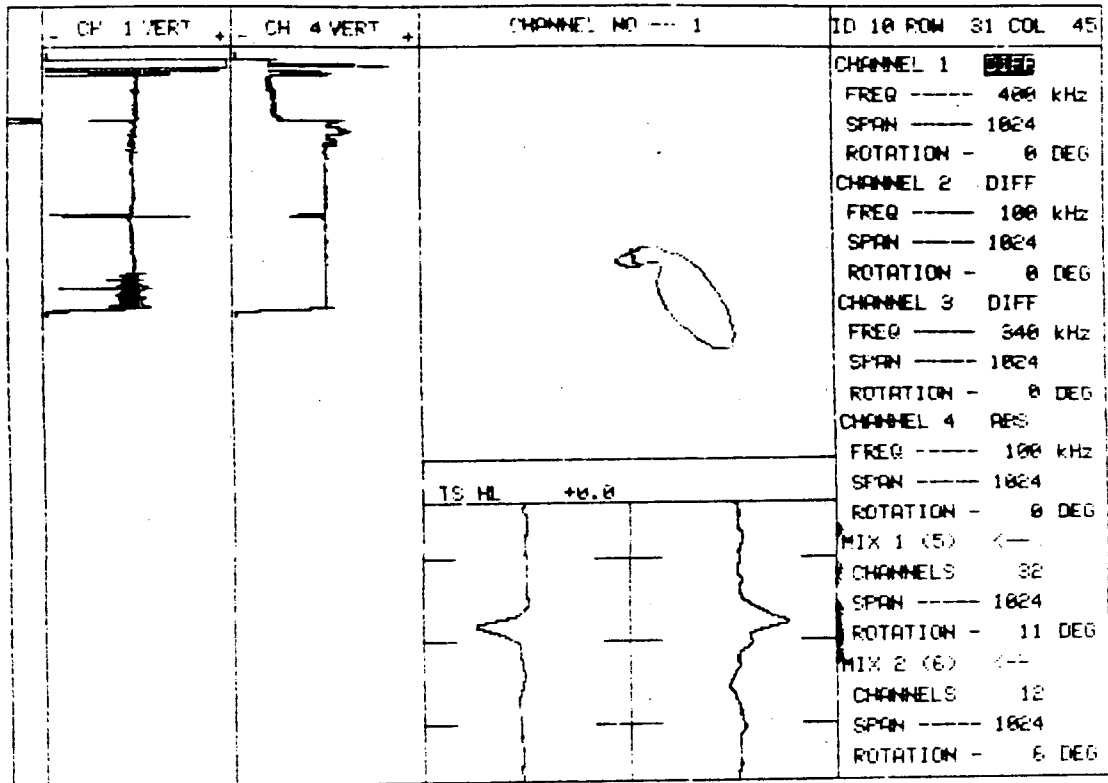
34 PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 05/25/89 ZETEC Inc. - 1988 Edition 12.0 Rev 1



34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	A	INLET	05/25/00	Edition 12.0 Rev 1

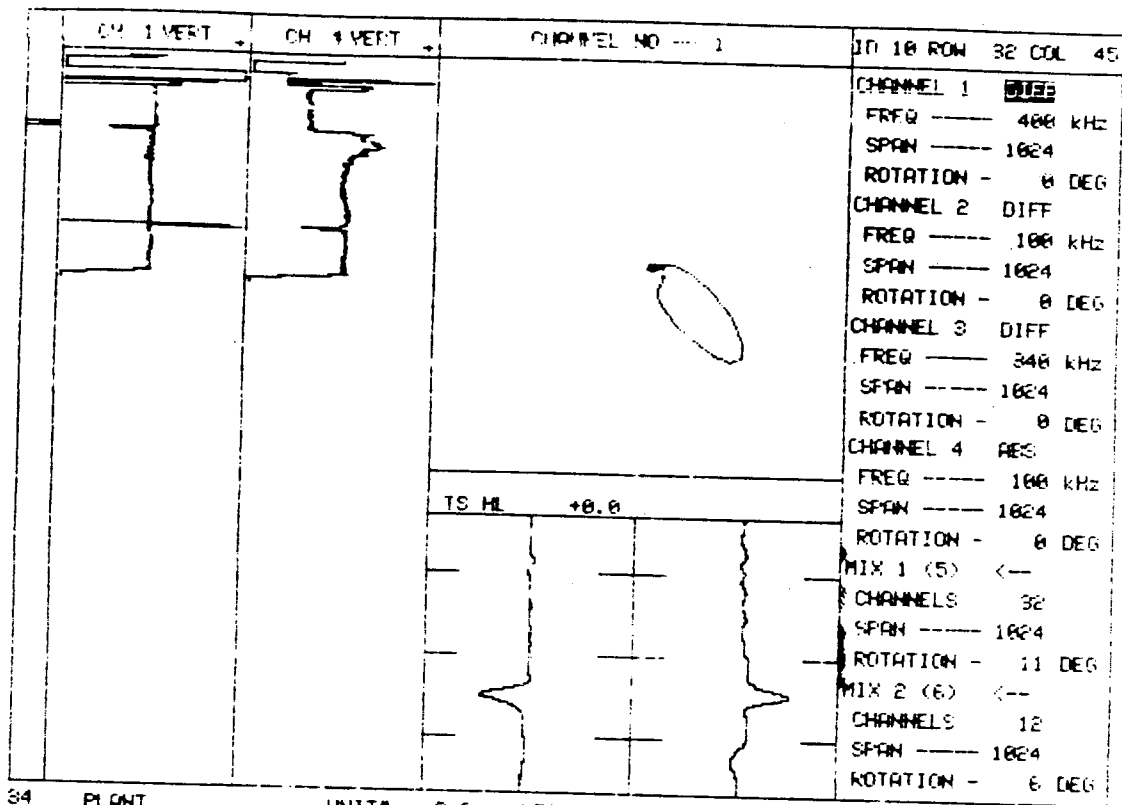


34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	A	INLET	05/25/88	Edition 12.0 Rev 1

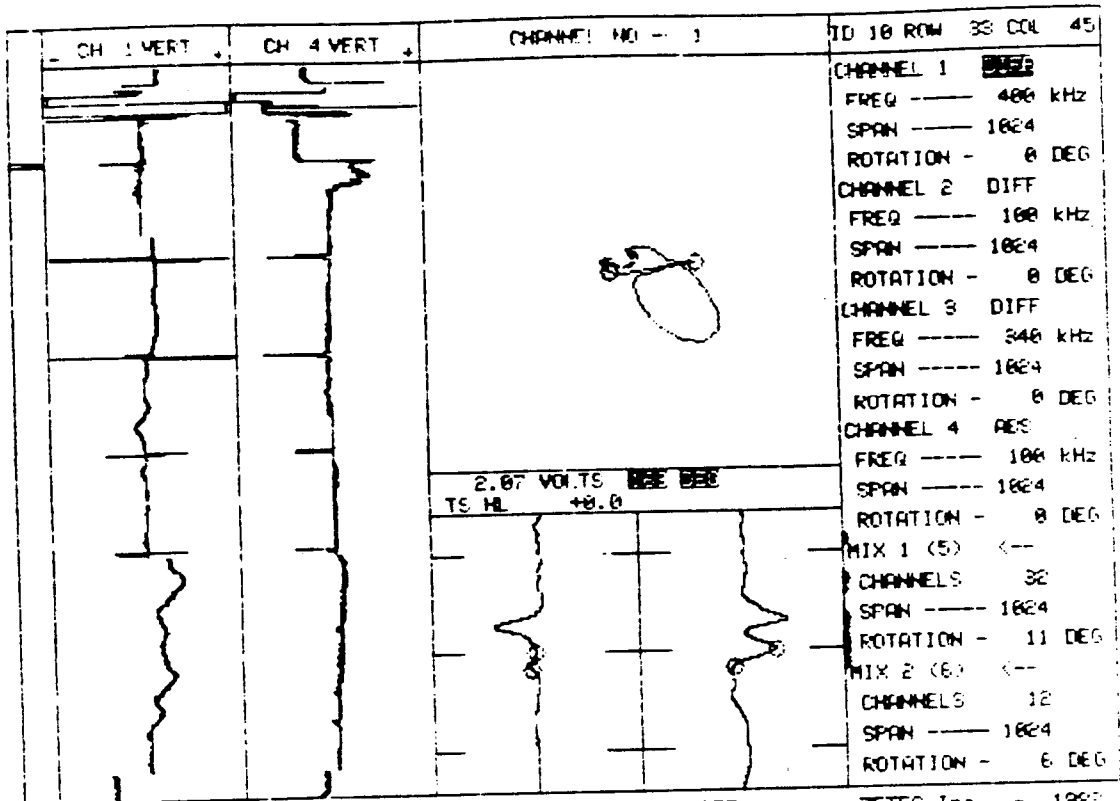


34 PLANT SCE SONGS I UNIT# I S/G A LEG INLET DATE 05/25/80

ZETEC Inc. - 1980
Edition 12.0 Rev 1

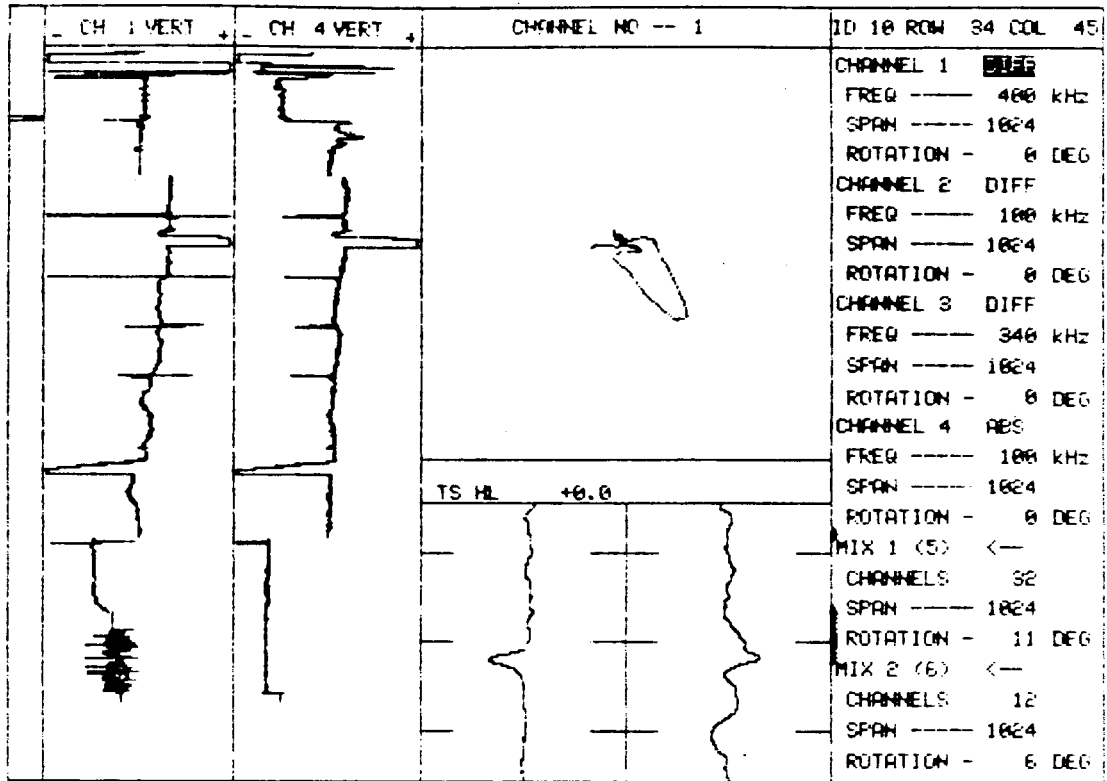


34 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1988
 SCE SONGS 1 1 A INLET 05/25/88 Edition 12.0 Rev 1



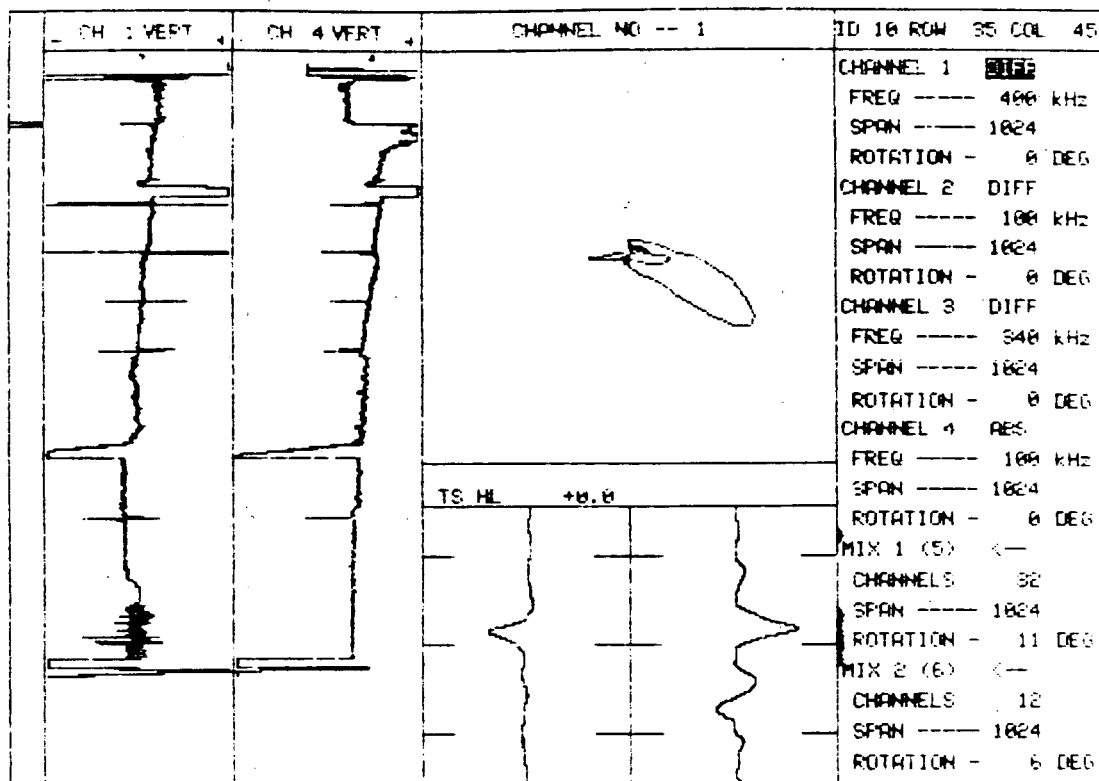
34 PLANT UNIT# S/G LEG DATE
 SCE SONGS 1 1 A INLET 05/25/88

ZETEC Inc. - 1988
 Edition 12.0 Rev 1

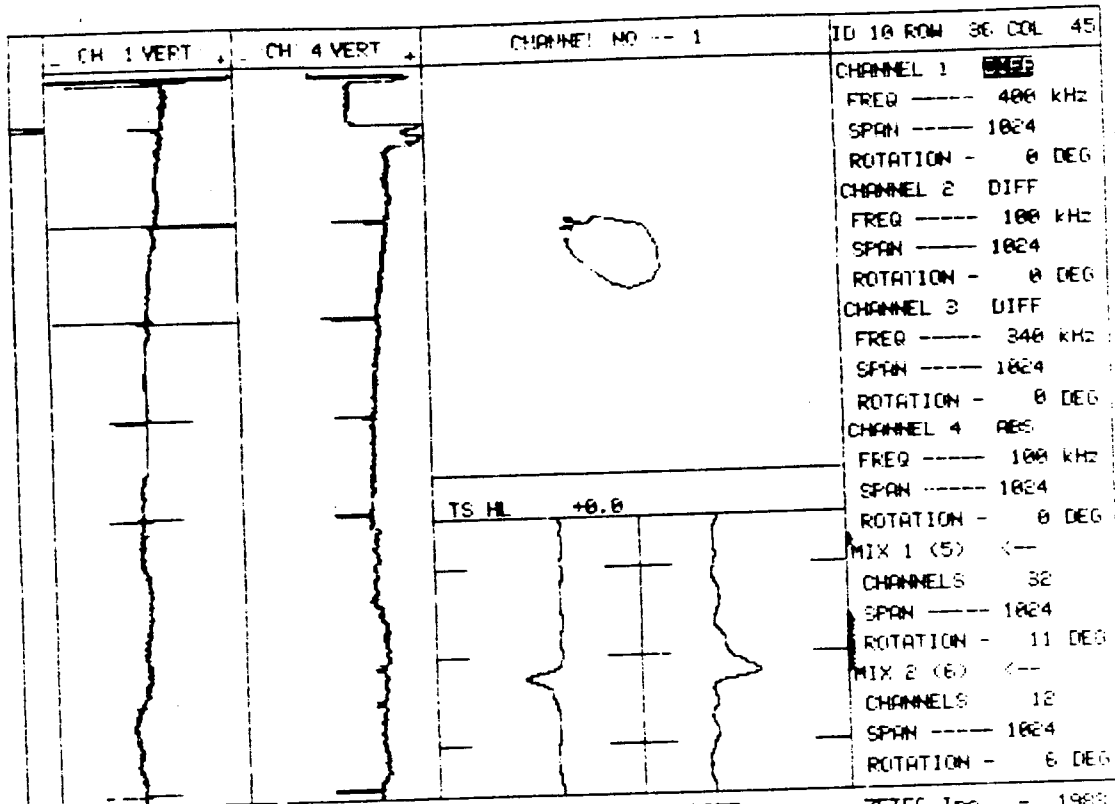


TS HL +0.0

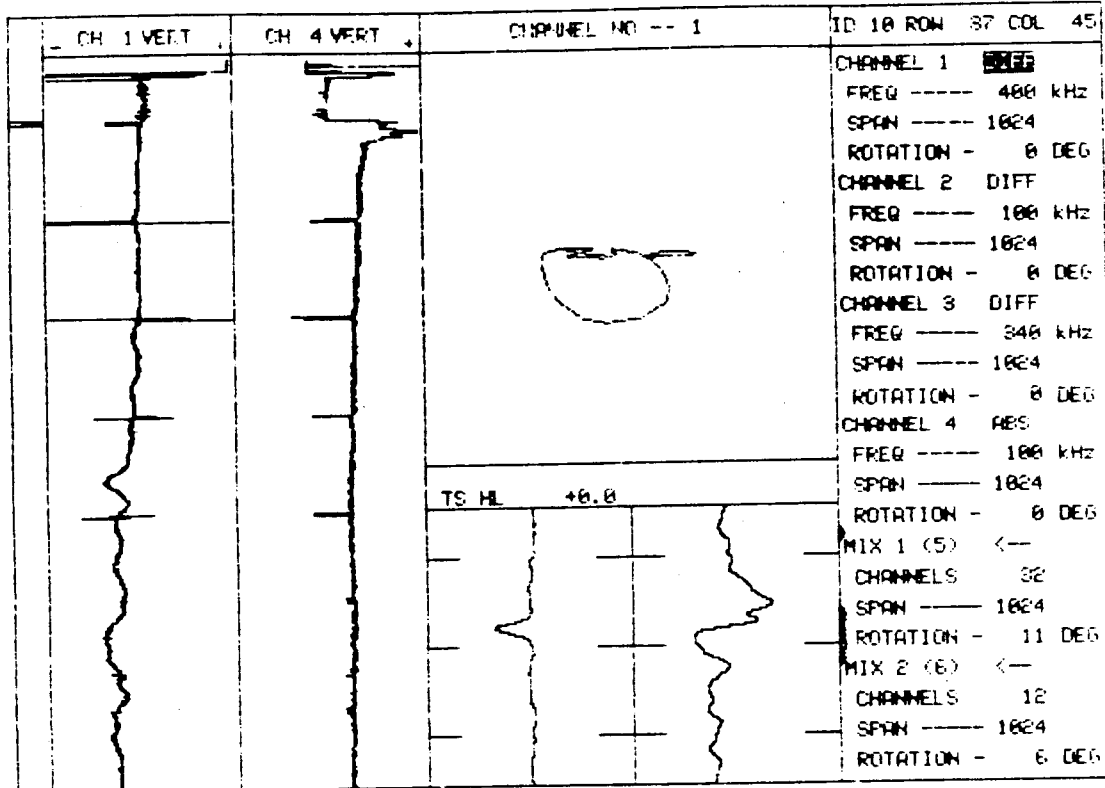
34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	P	INLET	05/25/88	Edition 12.0 Rev 1



84	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS I	I	A	INLET	05/25/80	Edition 12.0 Rev 1

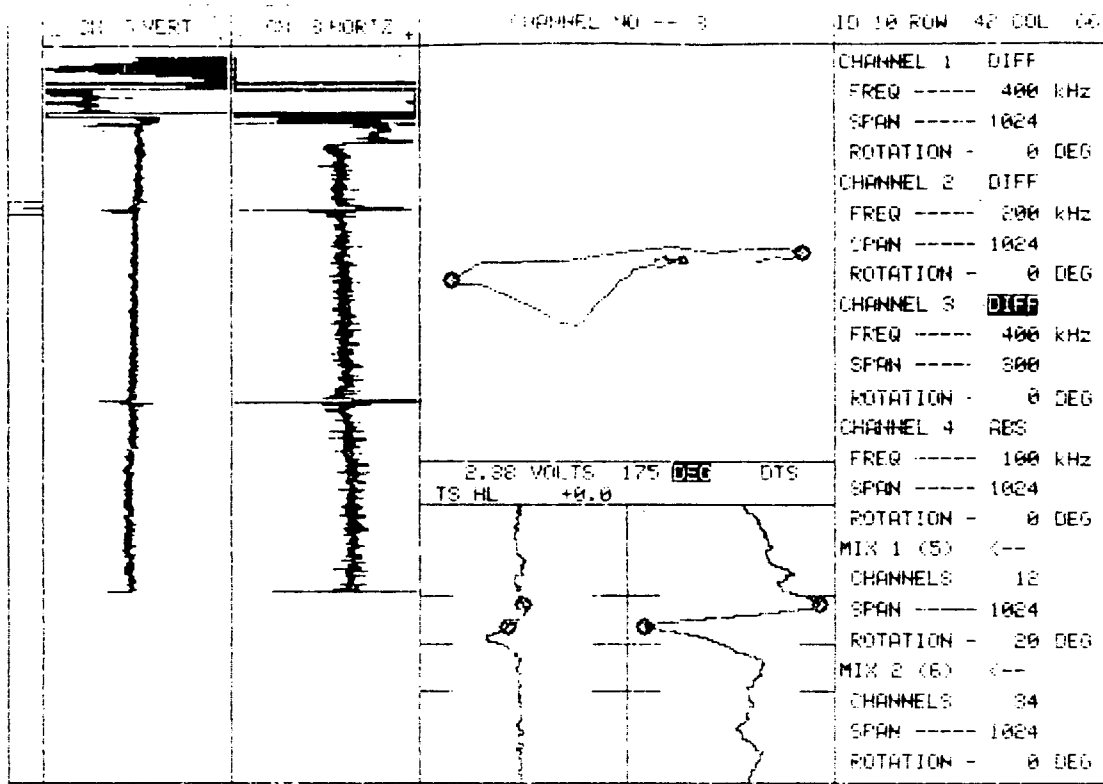


34 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1988
 SFE SONGS I I A INLET 05/25/88 Edition 12.0 Rev 1

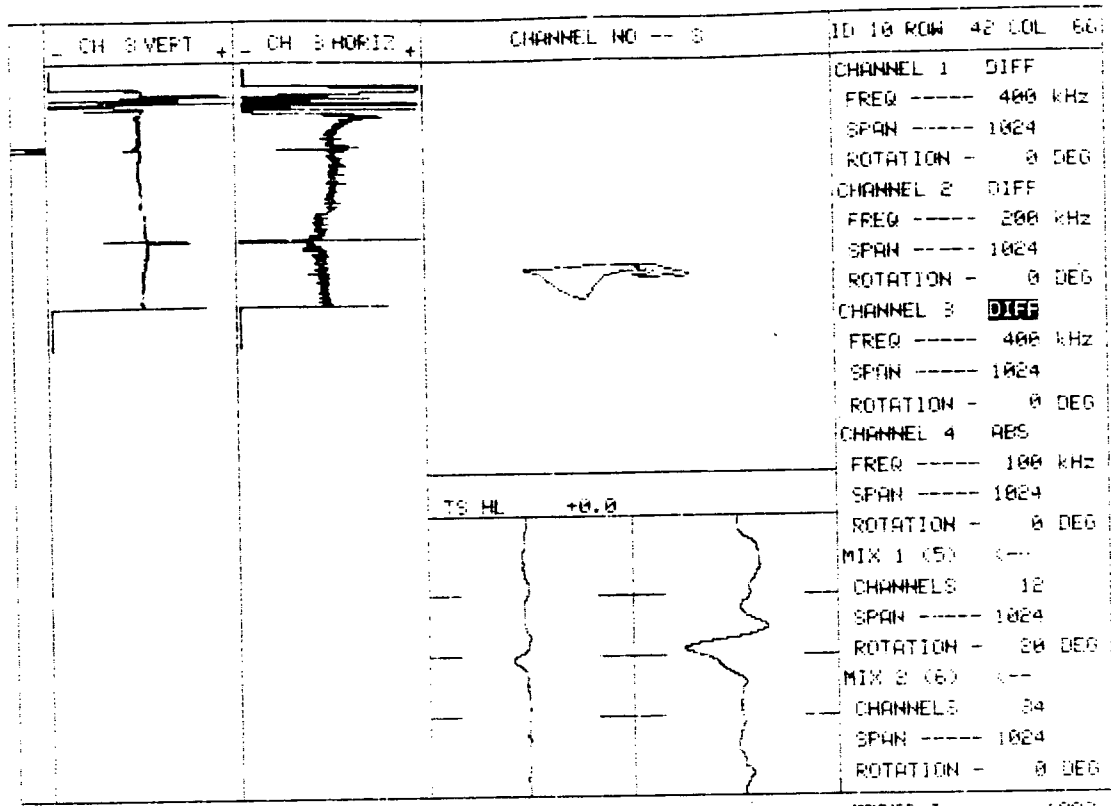


34	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1988
	SCE SONGS I	I	A	INLET	05/25/00	Edition 12.0 Rev 1

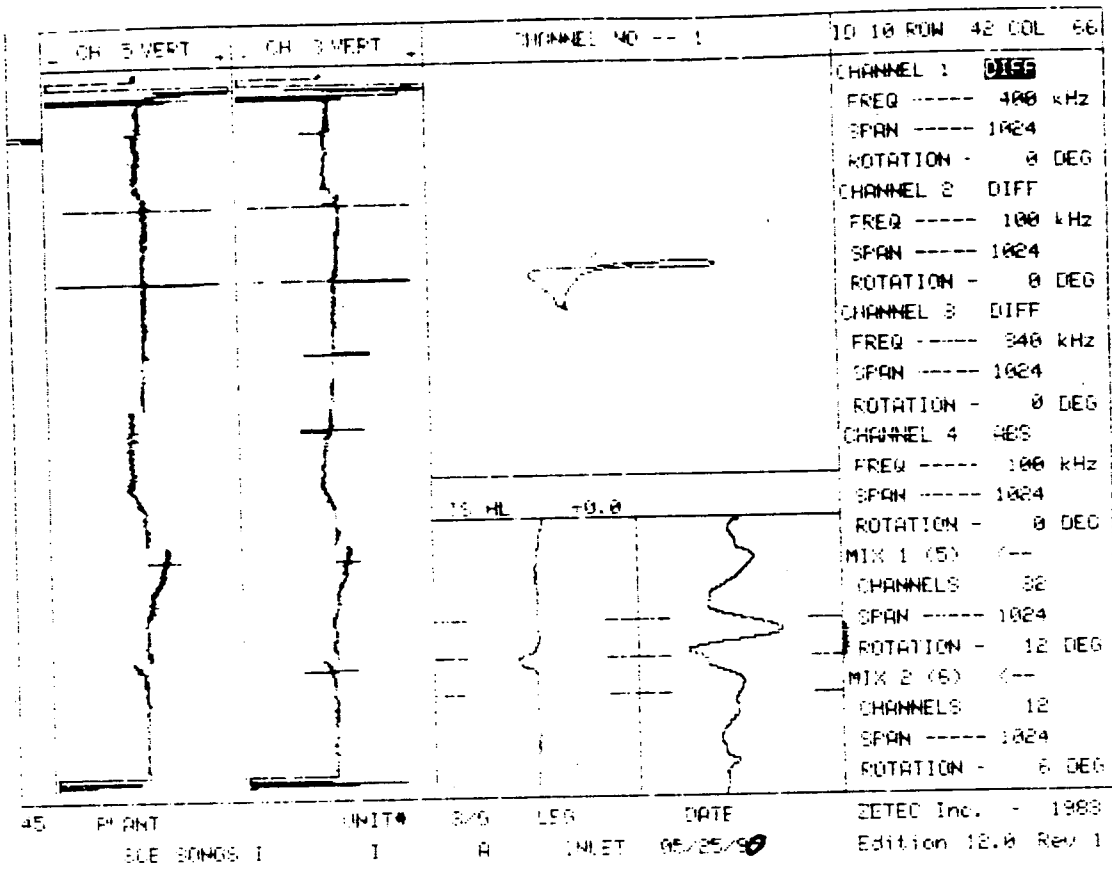
APPENDIX E

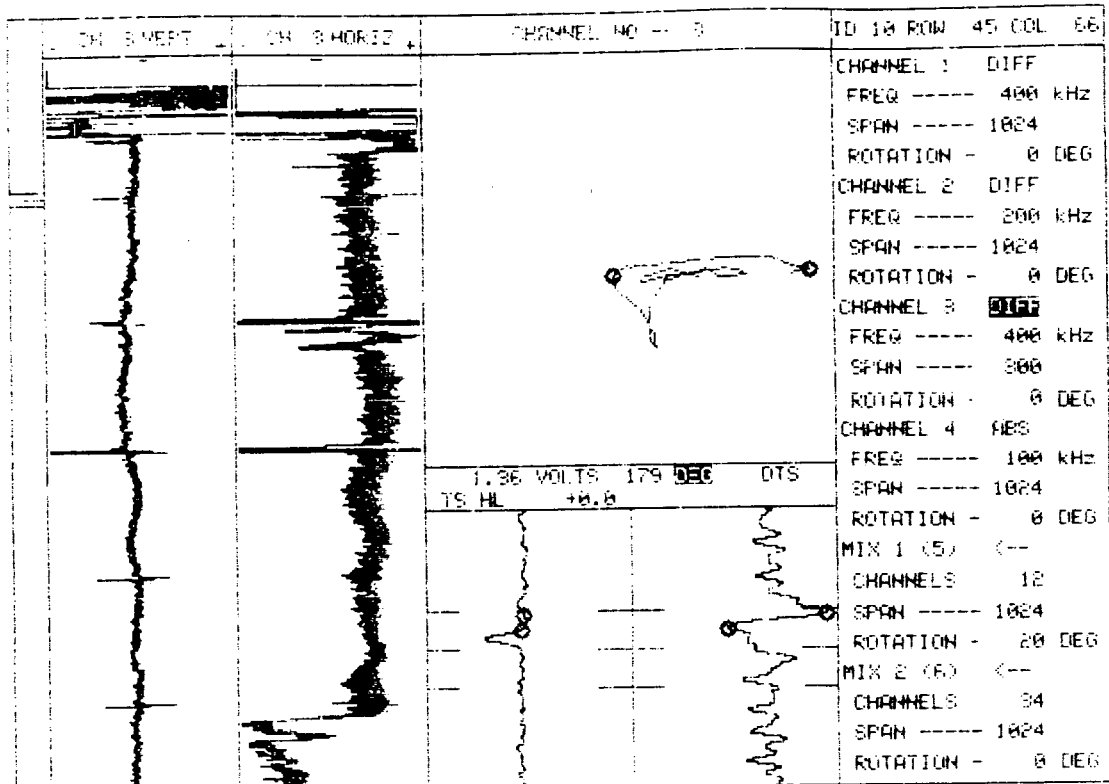


20	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCF SONGS I	I	A	INLET	06/ /73	Edition 12.0 Rev 1

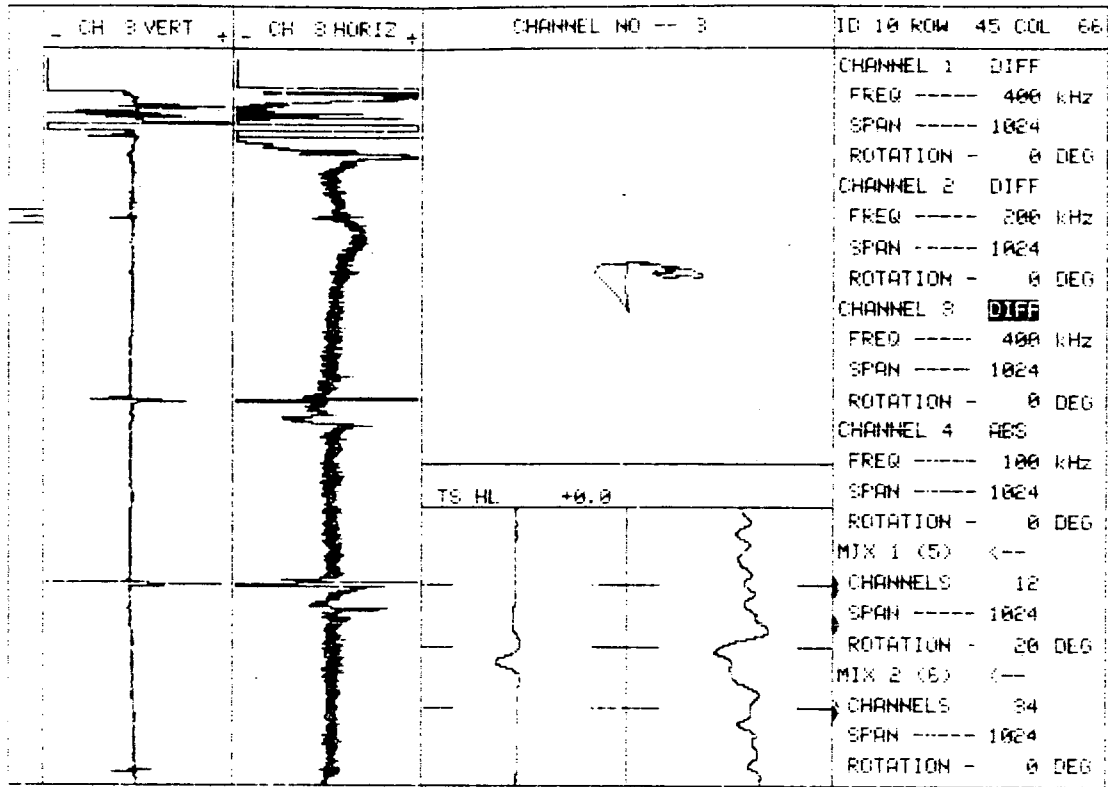


40 PLANT UNIT# S/G LEG DATE ZETEC Inc. - 1988
 SCE SONGS I "A" INLET 10/00/76 Edition 12.0 Rev 1

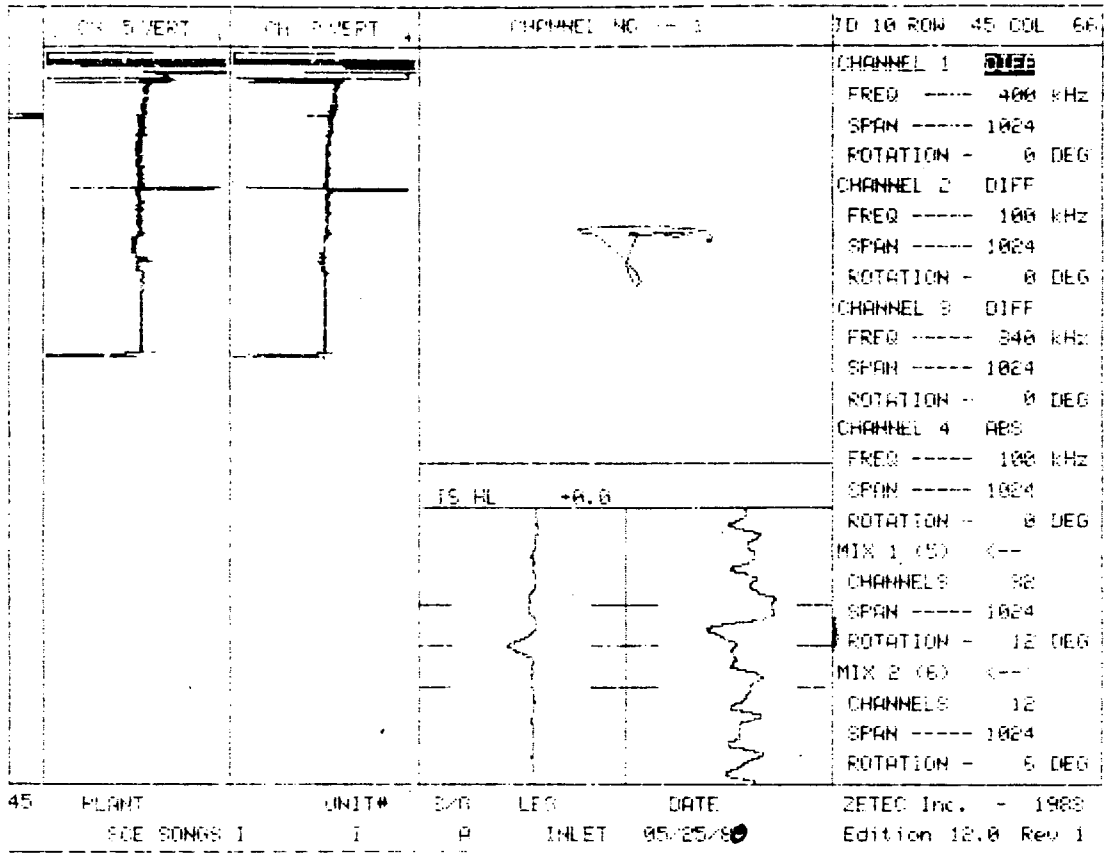


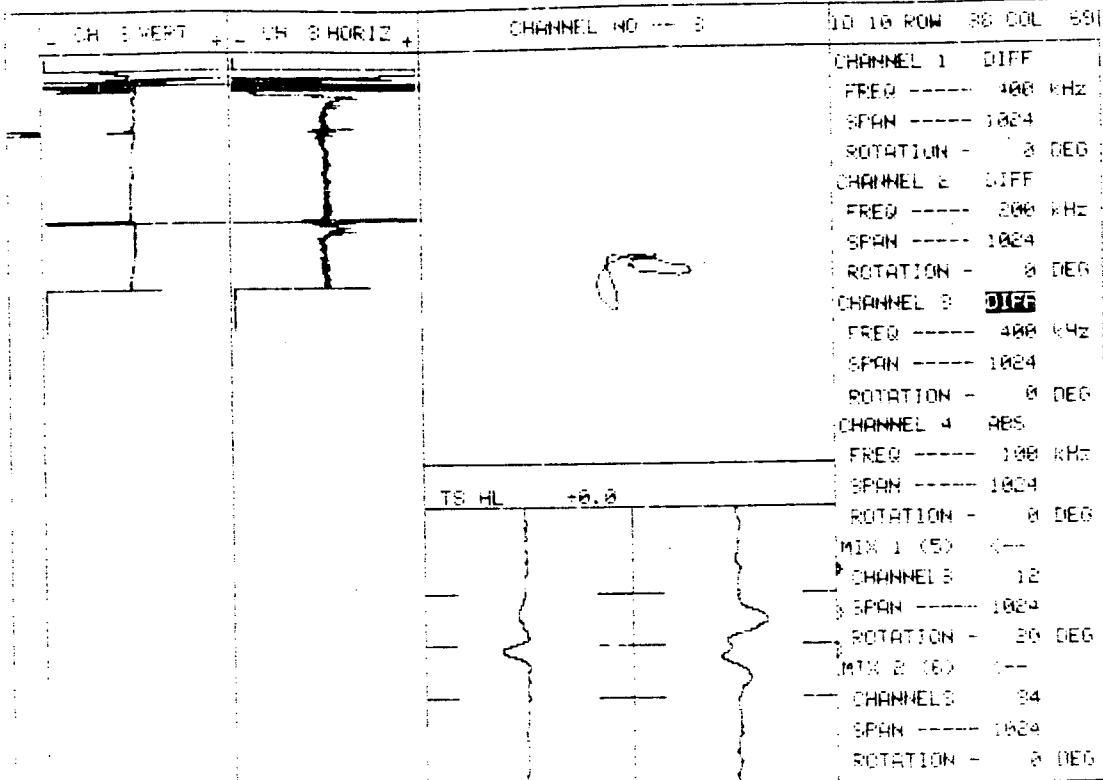


20 PLANT SDC SONGS I UNIT# I S-G R LFG - INLET DATE 06/1/78 ZETEC Inc. - 1983 Edition 12.0 Rev 1

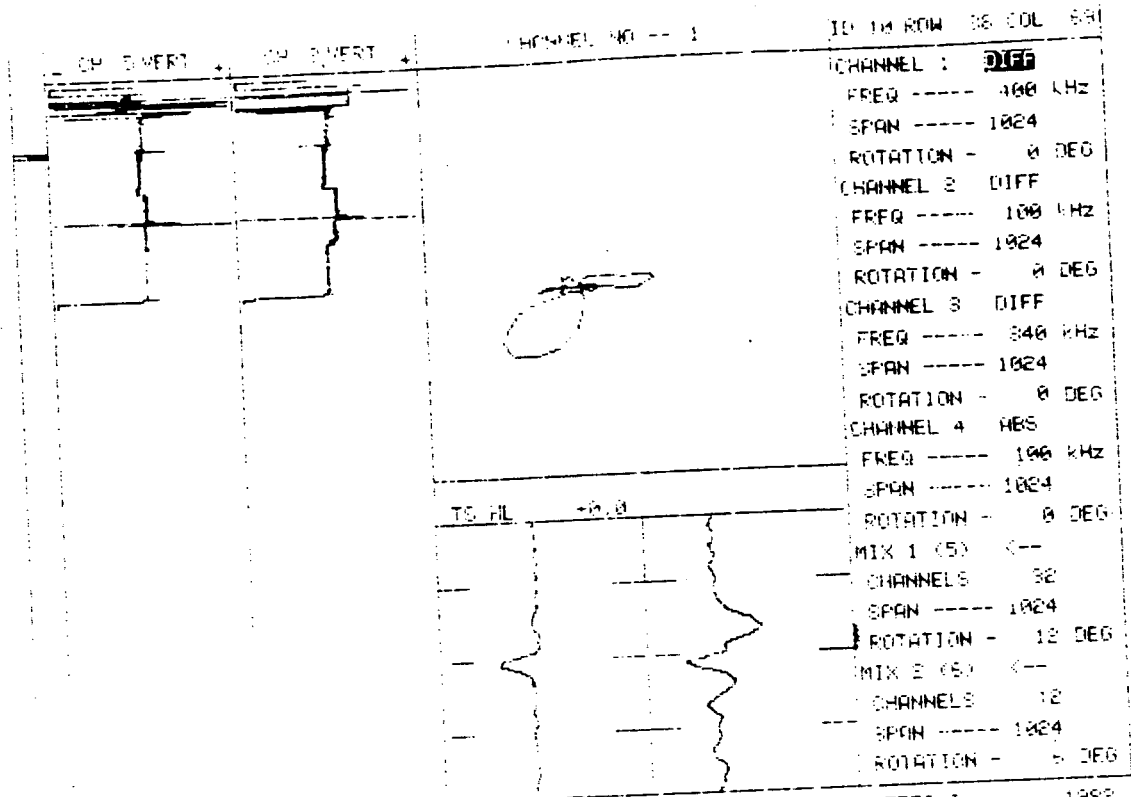


20	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	I	"A"	INLET	10/00/76	Edition 12.0 Rev 1



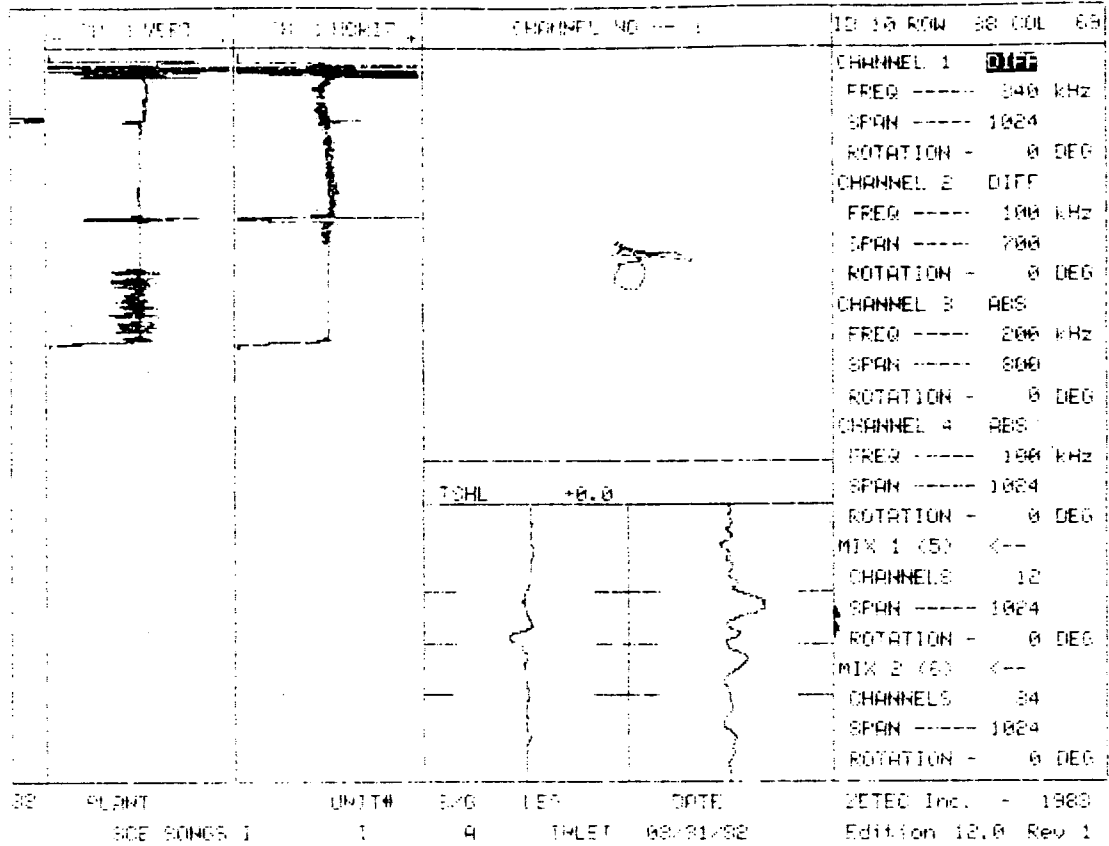


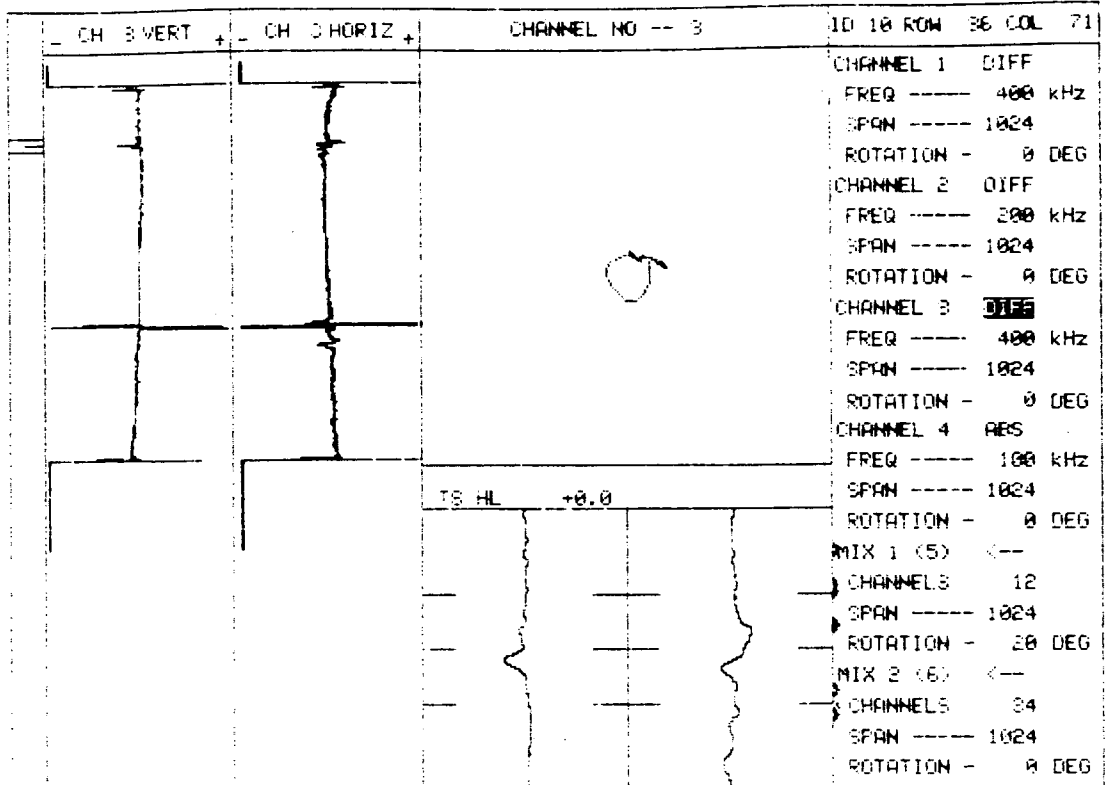
PLANT SCE SONGS UNIT# I S/G "R" LEG INLET DATE 10/00/76 ZETEC Inc. - 1983 Edition 12.0 Rev 1



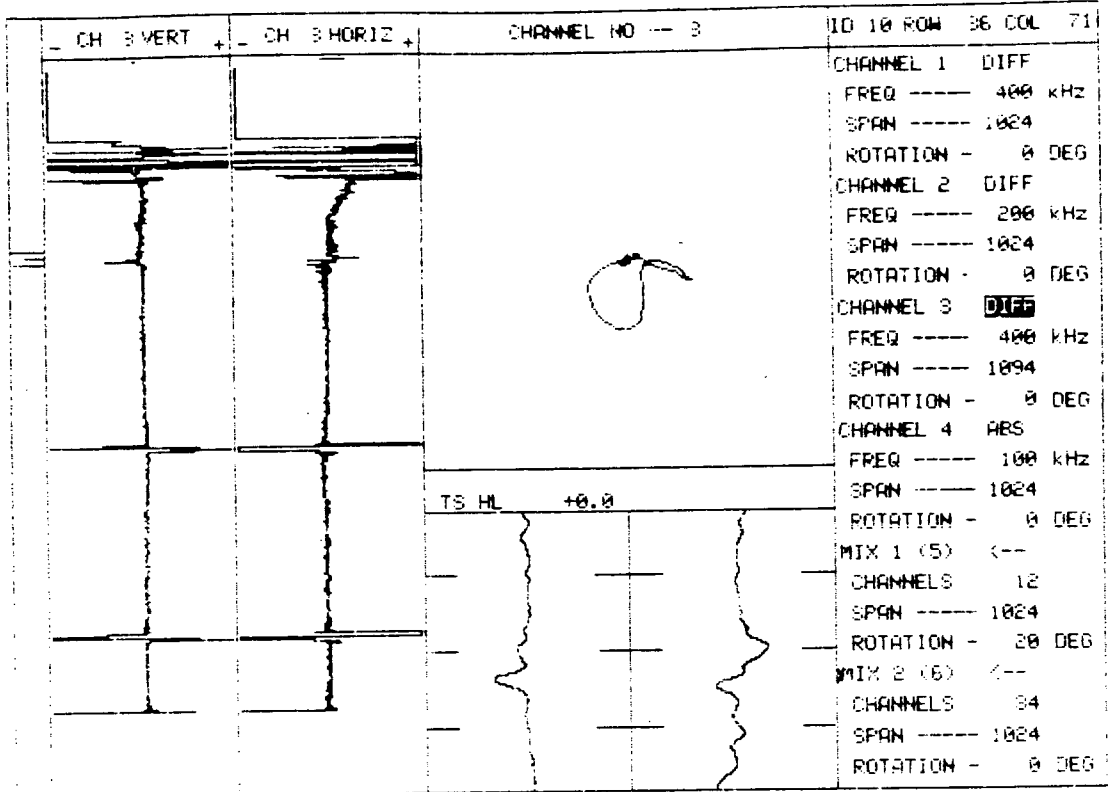
ID IN ROW 38 COL 591
 CHANNEL NO -- 1
 CHANNEL 1 DIFF
 FREQ ---- 100 KHZ
 SPAN ---- 1024
 ROTATION - 0 DEG
 CHANNEL 2 DIFF
 FREQ ---- 100 KHZ
 SPAN ---- 1024
 ROTATION - 0 DEG
 CHANNEL 3 DIFF
 FREQ ---- 340 KHZ
 SPAN ---- 1024
 ROTATION - 0 DEG
 CHANNEL 4 HES
 FREQ ---- 100 KHZ
 SPAN ---- 1024
 ROTATION - 0 DEG
 MIX 1 (5) ←
 CHANNELS 32
 SPAN ---- 1024
 ROTATION - 12 DEG
 MIX 2 (5) ←
 CHANNELS 12
 SPAN ---- 1024
 ROTATION - 5 DEG

45 PLANT UNIT# S/G L/SO DATE
 SEE SONGS 1 1 A INLET 05/25/80
 CETED Inc. - 1988
 Edition 12.0 Rev 1

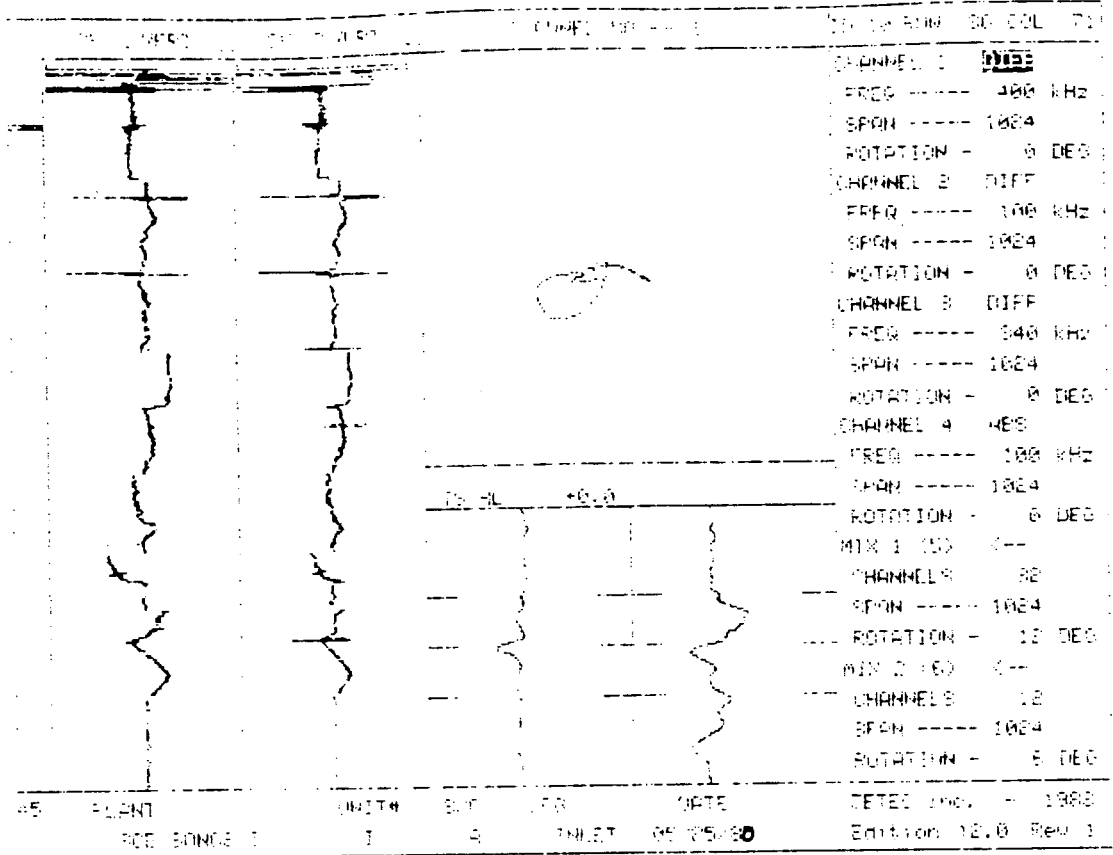




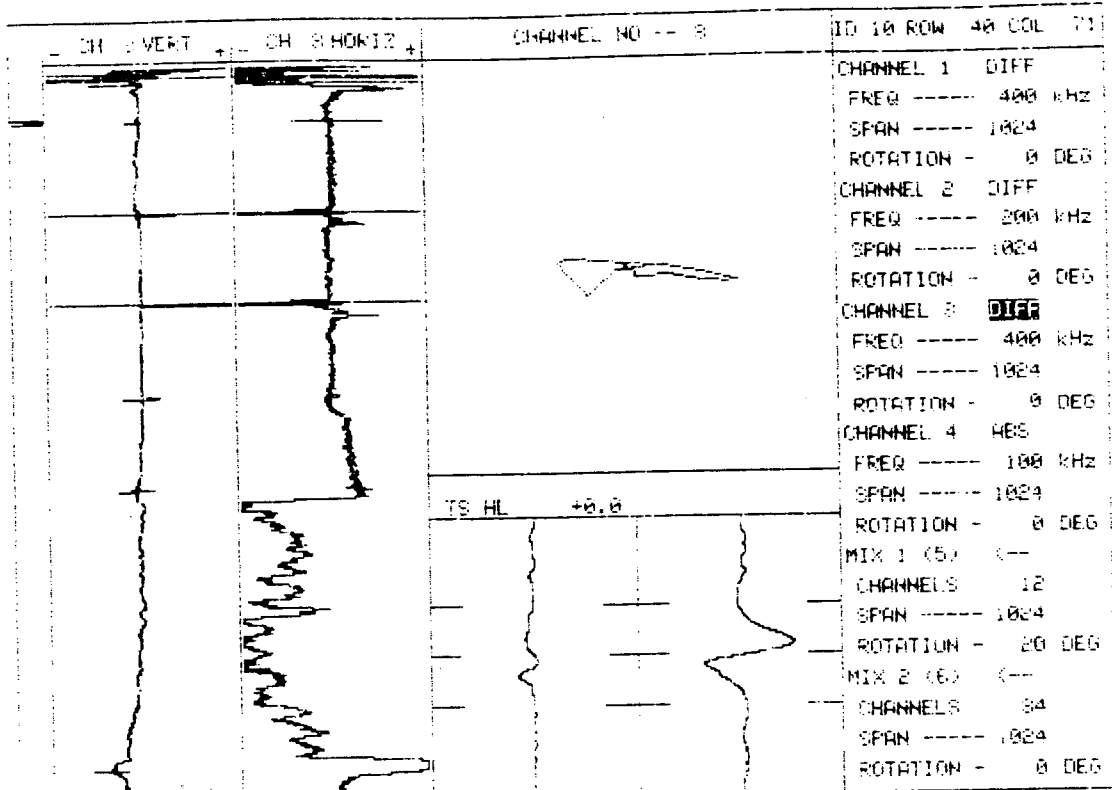
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	SCE SONGS	1	"A"	INLET	10/09/76	Edition 12.0 Rev 1



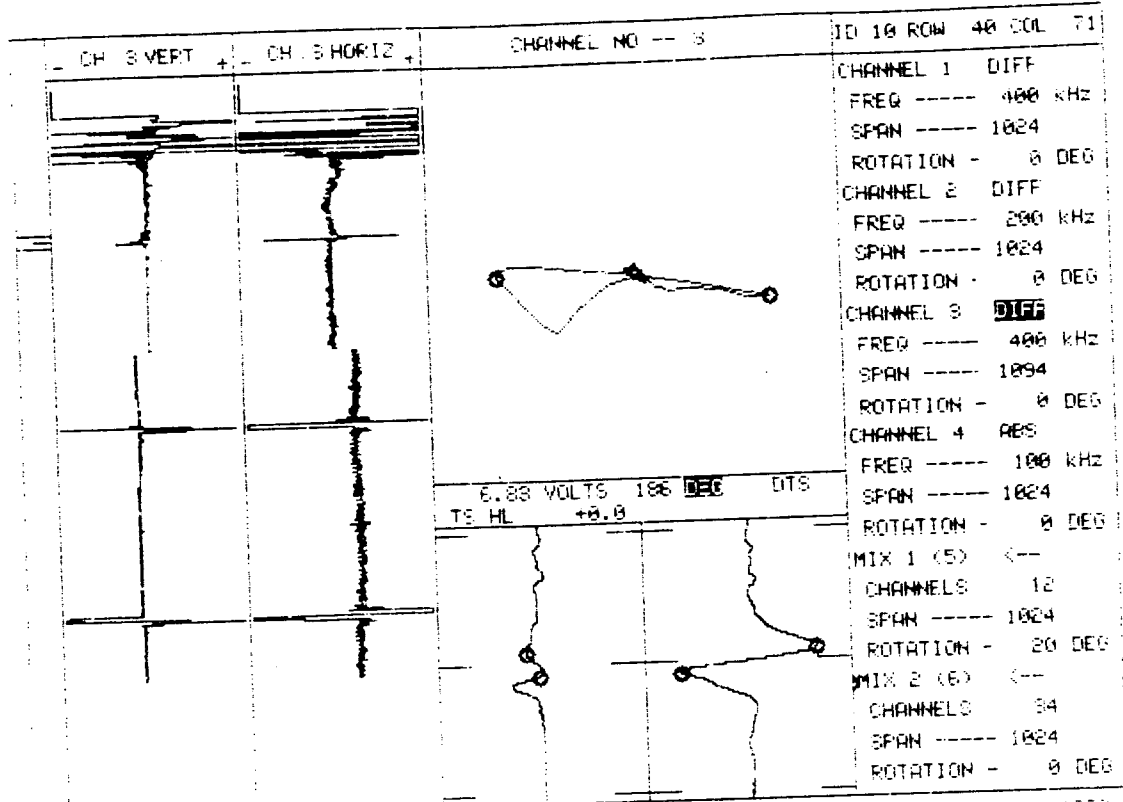
20	PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1983
	SCE SONGS	"I"	"R"	INLET	09/00/77	Edition 12.0 Rev 1



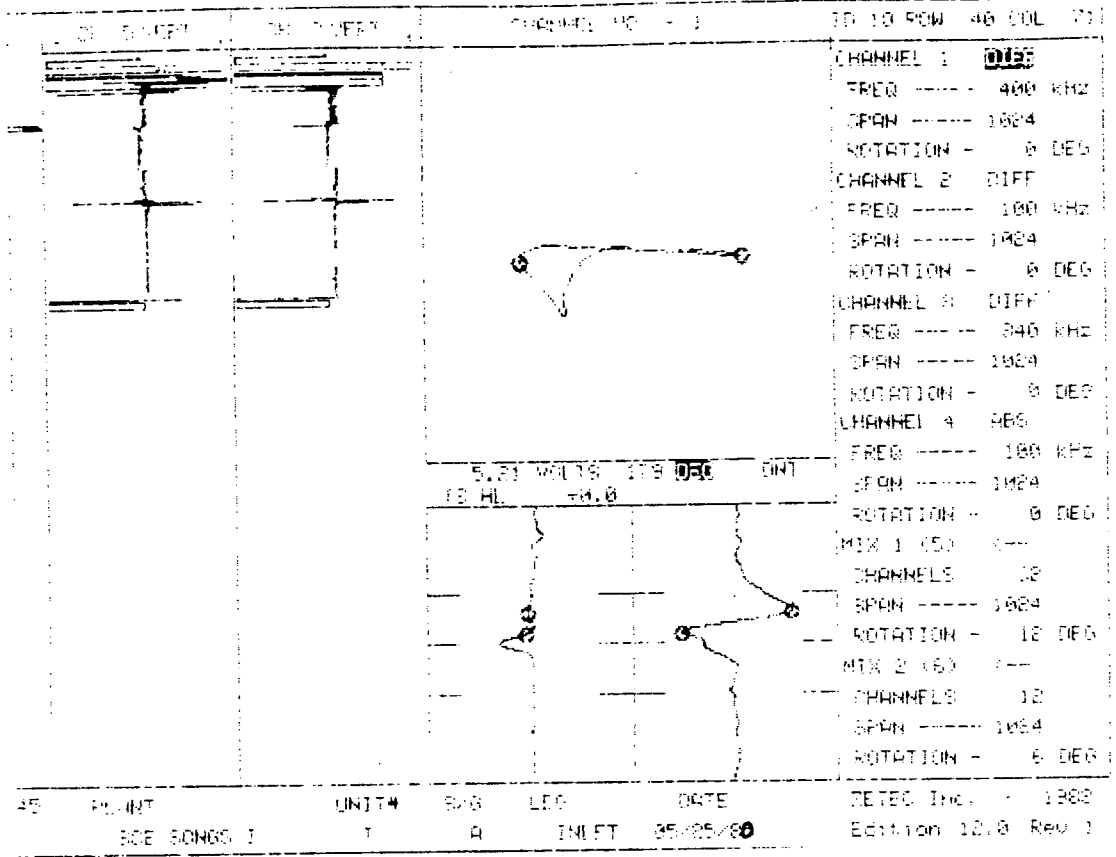
PLANT	UNIT#	BIT	LOG	DATE	DETEC (MHz)
ROE BONDG 1	1	4	INLET	05/25/80	1000



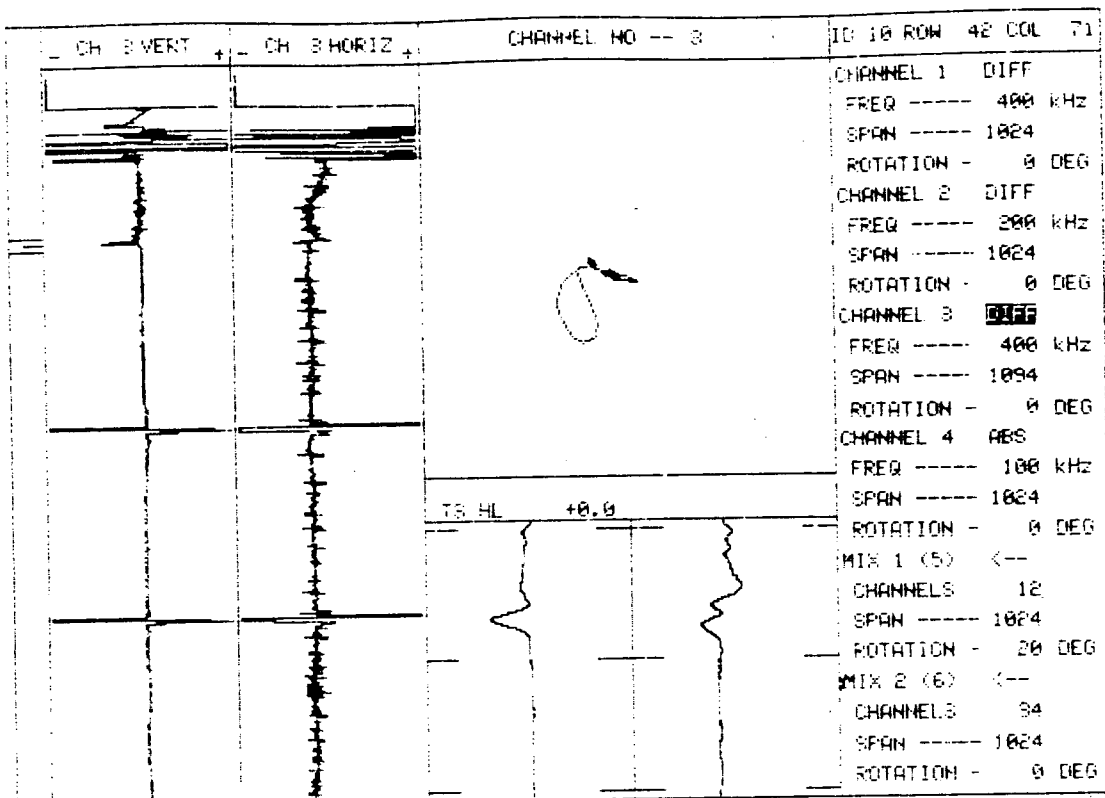
40 PLANT SCE SONGS UNIT# 1 S/G "R" LEG INLET DATE 10/06/75
 ZETEC Inc. - 1988 Edition 12.0 Rev 1



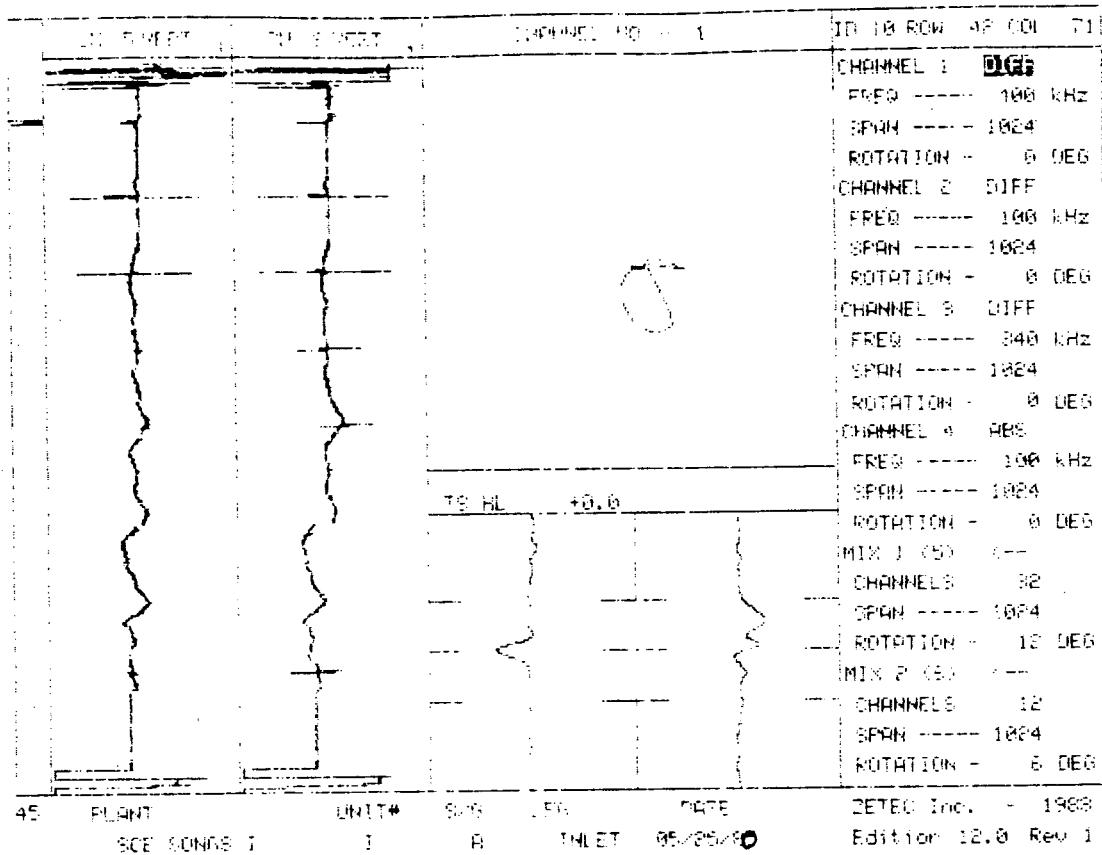
20 PLANT UNIT# S/W LEG DATE ZETEC Inc. - 1988
 SCE SONGS "1" "A" INLET 09/00/77 Edition 12.0 Rev 1

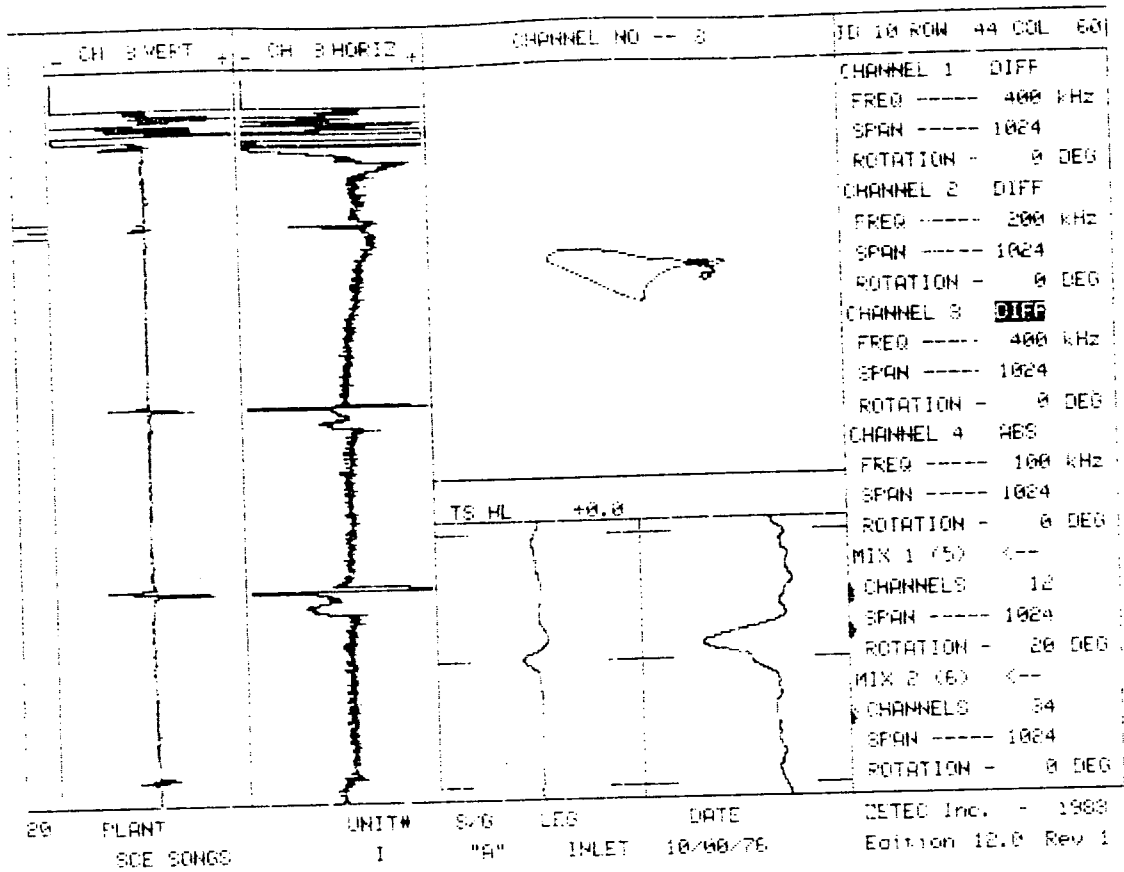


CH 3 VERT	CH 3 HORIZ	CHANNEL NO -- 3	10 18 ROW 42 COL 71		
		CHANNEL 1 DIFF			
		FREQ ----- 400 KHZ			
		SPAN ----- 1024			
		ROTATION - 0 DEG			
		CHANNEL 2 DIFF			
		FREQ ----- 200 KHZ			
		SPAN ----- 1024			
		ROTATION - 0 DEG			
		CHANNEL 3 DIFF			
		FREQ ----- 400 KHZ			
		SPAN ----- 1024			
		ROTATION - 0 DEG			
		CHANNEL 4 4BS			
		FREQ ----- 100 KHZ			
		SPAN ----- 1024			
		ROTATION - 0 DEG			
TS HL +0.0					
		MIX 1 (5) <--			
		CHANNELS 12			
		SPAN ----- 1024			
		ROTATION - 00 DEG			
		MIX 2 (6) <--			
		CHANNELS 34			
		SPAN ----- 1024			
		ROTATION - 0 DEG			
40 PLANT	UNIT#	S/G	LEG	DATE	ZETEC Inc. - 1980
SCE SONGS	I	"B"	INLET	10/00/75	Edition 12.0 Rev 1

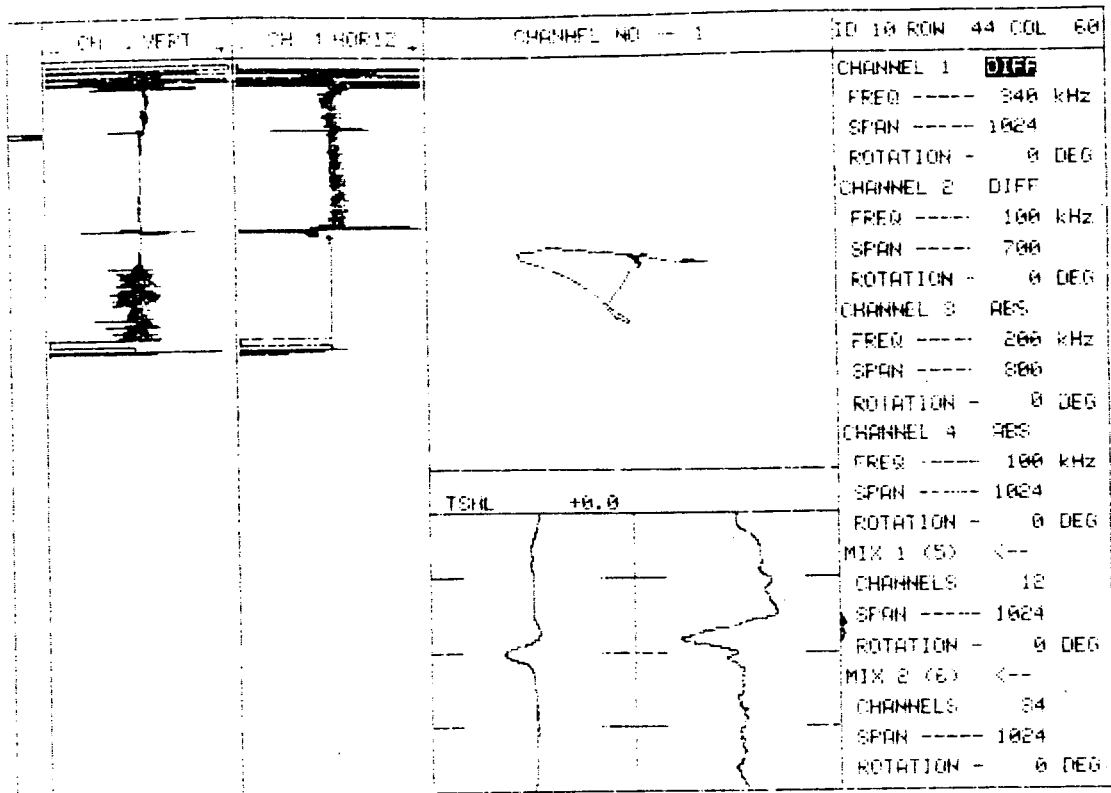


20 PLANT "I" S/G "A" LEG INLET DATE 09/00/77 DETED Inc. - 1983 Edition 12.0 Rev 1





DETEC Inc. - 1988
Edition 12.0 Rev 1



99	PLANT	UNIT#	S/S	LEG	DATE	ZETEC Inc. - 1983
	SCF SONGS I	I	A	INLET	08/31/82	Edition 12.0 Rev 1