

NRC Staff Perspective on MRP-227-A Action Item 7

November 19, 2013

Action Item 7 -Background

- CASS – Subject to loss of toughness due to thermal embrittlement (TE) and irradiation embrittlement (IE)
- For RVI, staff concerned about “synergistic” effect of IE +TE.
- Prior to MRP-227, guidance in GALL AMP XI.M13 for evaluating CASS RVI components (based on “Grimes Letter”)
- Industry intended MRP-227 to replace the former GALL program
- MRP-227 approach for CASS differs from existing NRC guidance

Staff Concerns Motivating

AI 7

- Implementation of GALL AMP requirements –
 - XI.M13 component-specific evaluation
- Uncertainty about threshold for IE, and existence of “synergistic effect” –
 - Existing data shows toughness decrease 0.3 dpa ($2E20$ n/cm²) - 1 dpa, ($6.7E20$ n/cm²)
 - lack of data 0.05 dpa ($1E17$ n/cm²) to 0.3 dpa ($2E20$ n/cm²)
 - MRP uses 1 dpa ($6.7E20$ n/cm²) as threshold for IE of CASS
- Fracture toughness can get very low at fluences > 5 dpa ($3.3E21$ n/cm²),
 - very small flaws could cause failure under normal operating loads
 - inspection resolution may be inadequate to detect such flaws
- Inspection accessibility limited for some components

Action Item 7

- For CASS components requiring aging management, perform plant-specific analysis or evaluation demonstrating the components will maintain functionality during PEO.
- MRP-227-A SE, Section 4.2.7: “The applicant/licensee shall include the plant-specific analysis as part of their submittal to apply the approved version of MRP-227.”
- Acceptable Evaluation Approaches
 - Screening, TE and IE or stress
 - Functionality analysis
 - Component specific flaw evaluation

Applicable To

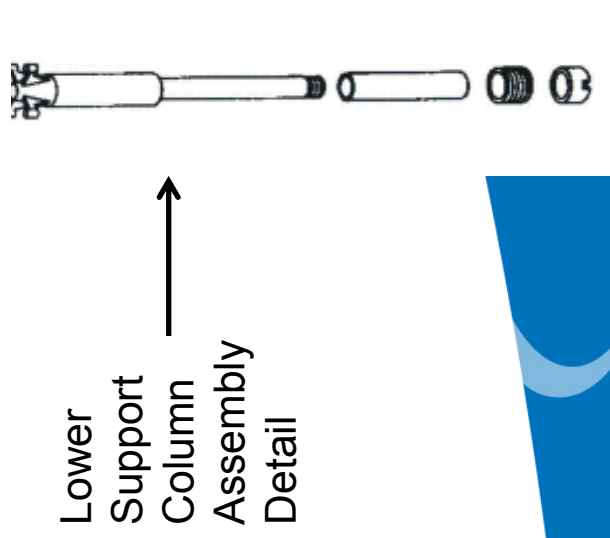
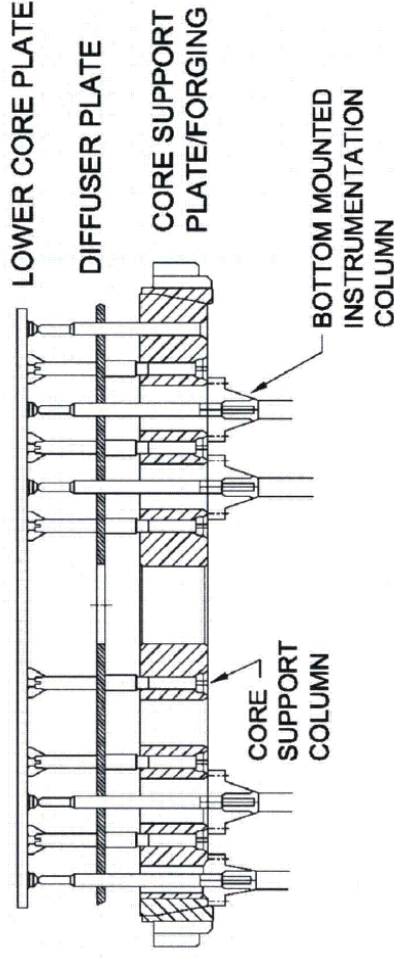
- B&W
 - IMI guide tube assembly spiders - Primary
 - CRGT spacer castings - Primary
- CE
 - Core support columns (welds are Primary)
- Westinghouse
 - lower core support column bodies - Expansion

Westinghouse Lower Support Column Body

- Only CASS expansion component
- High neutron fluence ($>1E21$ n/cm²) in top few inches of column.
- TE and IE screened in in MRP-227-A
- Inspection required if cracking found in CRGT lower flange weld
- Accessibility for inspection is limited, EVT-1 inspection may be difficult.

Westinghouse Lower Support Column Bodies

- Large population of redundant components
- Minimum pattern analysis should be feasible
- Mostly compressive loading
- Medium failure likelihood, low core damage likelihood



- FMECA Group 1

Plant-Specific Components Subject to TE

- Other CASS, martensitic and PH stainless components may be determined to require aging management, for example through AI 2
- The plant-specific evaluation under AI 2 may identify TE as an applicable aging mechanism.
- If so, these components are also subject to the requirements of AI 7.

Licensee Responses to AI 7 (to date)

- Level of detail provided in responses to AI 7 has generally not been sufficient to reach a safety conclusion
- Some licensees proposed commitments to provide the analysis at a later date

WCAP-17096-NP

- Provides evaluation methodologies for Primary and Expansion CASS components
- These methodologies would be acceptable for Action Item 7 analyses, with caveat that:
 - WCAP methodologies assume inspection has been done, thus inspection data available as input to functionality

Screening Approach

- Screen components for susceptibility to TE and IE
- May use May 19, 2000, "License Renewal Issue No. 98-0030, *Thermal Aging Embrittlement of Cast Stainless Steel Components*" (NRC ADAMS Accession No. ML003717179)
 - Allows screening based on chemistry and ferrite content if fluence < $1E17$ n/cm²
 - Allows screening based on low tensile/compressive stress if fluence $\geq 1E17$ n/cm²
 - MRP-227-A screening criteria for IE of CASS is fluence $\geq 6.7E20$ n/cm²

Functionality Approach

- Based on structural redundancy
- Determine maximum numbers and locations of failed structural components
- Does not rely on knowledge of fracture toughness properties
- May rely on conservative assumptions, such as component with a crack completely failed
- Similar approach successful for baffle-former bolts

Flaw Tolerance Approach

- Postulated or observed cracks (service-induced cracking not seen in CASS to date)
- Evaluate for a set time (EOL or next inspection)
- Crack growth prediction
- Crack stability evaluation at set time
- Requires fracture toughness properties
- No agreed-upon model for irradiated CASS toughness at present

Considerations for All CASS Plant-Specific Analyses

- Include with RVI Inspection Plan/AMP submittal
- Provide for Primary or Expansion category CASS component
- For Primary CASS components, ok to provide within one year of initial inspection
- If staff cannot accept the analysis for CASS Expansion components, licensees should consider inspecting these components as Primary

Considerations for Screening Approach

- Follow Grimes letter guidance, e.g., can't use TE criteria if fluence $\geq 1E17$ n/cm²;
- OR
- Provide a robust technical basis for applicability of TE screening criteria at higher fluences
- Can also screen based on low (<5 ksi) tensile stress, or compressive stress (mechanical loading assessment)
- Should have material-specific chemistry, ferrite, or justify assumptions.

Considerations for Functionality Approach

- Sufficient level of detail must be provided
 - Assumptions
 - Inputs – stresses, conditions and transients (must consider design basis events consistent with plant’s licensing basis)
- For Expansion components, need basis for assumed failures, since no inspection data
 - ASME Section XI Exam Results?
 - Operating Experience
- Without inspection, and possibility of very low toughness, is functionality approach feasible?

Functionality

Analysis – Low Toughness

- Existing data (NUREG/CR-7027) shows CASS toughness can be very low at fluences ≥ 5 dpa
- Some CASS RVI, e.g. lower core support columns, predicted to exceed this fluence in local areas
- For Expansion CASS components, no inspection data will be available to rule out small manufacturing flaws
- Considering low toughness, need demonstration that functionality would be maintained considering the presence of small flaws (even if service-induced cracking is unlikely)

Considerations for Flaw Tolerance Approach

- Use conservative model for fracture toughness
- Initial flaw size assumption must be justified
- Provide inputs and assumptions to analysis, e.g. stress, fluence
- Use plant-specific fluence and stress
- Address small flaws (if toughness very low)

Key Messages

- Address embrittlement of CASS in near term
- OR
- Plan to inspect “Expansion” CASS components as “Primary” components