

DESIGN SPECIFICATION REVISION RECORD
SAN ONOFRE NUCLEAR GENERATING STATION UNITS 2 & 3

REVISION NUMBER	REVISION DATE	P.E. APPROVAL/ DATE	PAGES AFFECTED
0	3-14-77		Issue complete design specification: Title Page, Pages i, ii, iii, and Pages 1 thru 4. Appendices A, B, C and D
1	11-17-77	<i>SCN DS-07 / 1-27-78</i>	Title Page, Page i, ii, iii, and Pages 1, 3, 4, and 5.
2	5-10-79		Title Page, Pages i, ii, iii, and Pages 1, 2, 3, 4 and 5.
3	1-31-80		Title Page, Pages i, ii, iii, and Pages 3, 4, and 5, Appendix D, and New Appendix E. Incorporate SCN DS-07 dated 12-5-79, and SCN DS-06 dated 6-20-79

ASME CODE, SECTION III
DESIGN SPECIFICATION DS-1201

SONGS UNITS 2 & 3

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ASME CODE, SECTION III
DESIGN SPECIFICATION DS-1201
SONGS UNITS 2 & 3

This Design Specification, including Appendices A, B, and C consists of design information as prescribed by Section III of the ASME B&PV Code, 1974 Edition through Summer '74 Addenda, Subsection NA-3252.

1. Functions of the components or appurtenances including any dimensions upon which the functional performance depends.

The major components of the Reactor Coolant System are a reactor vessel, two parallel heat transfer loops, each containing one steam generator and two reactor coolant pumps, and a pressurizer connected to one of the reactor vessel outlet pipes. A quench tank is provided to receive and condense discharges from the pressurizer safety valves. All components are located inside the containment building.

The specific functions of the Reactor Coolant System Piping are as follows:

- a. To transfer high pressure and high temperature water between the reactor vessel and the steam generators for the purpose of transferring fission energy.
- b. To transfer water under high pressure and high temperature between the reactor coolant loops and the pressurizer to accommodate expansion and contraction of the primary coolant, and for the purpose of controlling system pressure.
- c. To serve as a barrier to the release of fission products from the reactor core to the environment.

Listing of Project Class C and D instruments including applicable sensing line routing configurations are defined on Drawing No. 56288. | 2

2. Mechanical operational loadings including vibration and shock.

The design pressures and temperatures for the reactor coolant system piping components are defined in the Line Designation List included as part of this Design Specification for the various portions of the piping system.

Allowable material stress intensities and stress values to be used for the design of piping systems are given in the ASME Code, Subsection NA, Appendix I for acceptable materials at various temperatures. | 2

2 | The components of the reactor coolant system covered by this Design Specification are Seismic Category I. Combustion Engineering (CE) Response Spectra for the tributary piping nozzles are included in Appendix B. The Instructure Response Spectra for this piping are included as part of this specification in Appendix B.

The loading combinations for Code Class 1 and 2 and transients for the Code Class 1 portions of the Reactor Coolant System are included in Appendix C as part of this Design Specification.

Nozzle displacements due to thermal, dead weight, seismic and pipe rupture loadings are included in this specification as Appendix D.

2 | Code Case 1606-1 applies to this piping system.

3. Environmental conditions including radiation.

The reactor coolant system piping may be subject to an atmosphere with relative humidity varying from 0 percent to 100 percent and ambient temperatures of 34F to 300F depending on location. Specific temperatures for locations are defined as follows:

Area	Design Temperatures (FDB)	
	Summer	Winter (minimum)
Auxiliary Bldg. - Penetration	100	36
Containment	120 (300 FDB emergency)	50
Safety Equipment Bldg.	100 (104 FDB emergency)	NA

The reactor coolant system will be subject to a design integrated radiation dose over 40 years which is not to exceed 5×10^7 rads.

During the unlikely event of a LOCA condition, portions of piping and instrument sensing lines located inside the containment structure will be subjected to containment spray having the following composition:

- Boron \leq 2150 ppm as boric acid
- NaOH buffered to $8.0 \leq \text{pH} < 10.0$

4. Code classifications of the items covered.

The reactor coolant system contains Project Class A and C piping. Project Classification A requires design, fabrication, examination and testing in accordance with the requirements of the ASME B&PV Code, Section III, Subsection NB for Code Class 1 piping systems. Project Class C relates similarly to Subsection NC for Code Class 2 piping systems. Those portions of the piping system connecting the containment penetration assemblies to the isolation valves shall be Code Class 2. Instrument sensing lines connected to Code Class 1 piping systems are project Class C, and complies with the rules of Subsection NC between the root valve/restriction and the fitting connection at the instrument. Instrument sensing lines connected to Code Class 2 piping systems are Project Class C or D, and comply with the rules of Subsection NC and ND, respectively between the root valve/restriction and the fitting connection.

5. Definitions of the Piping System Component boundaries.

The boundaries and pertinent dimensions of the Reactor Coolant system piping are defined in the following P&ID's:

P&ID's

- 40111 Reactor Coolant System
- 40112 Safety Injection System
- 40113 Safety Injection System
- 40123 Coolant Chemical and Volume Control System
- 40124 Coolant Chemical and Volume Control System
- 40130 Reactor Coolant Pumps

The boundaries of individual components are also identified on the Line Designation List, Appendix A.

System Piping Components are comprised of individual, interconnected piping system subassemblies grouped together according to design pressure, design temperature and ASME Code Class. These groups are determined from data described in the Line Designation List, Appendix A.

The piping design shall include the following as a part of the system piping:

- Vent and drain lines through the first root valve.
- All connection welds at interfaces between piping and components.
- Expansion joints and instrument piping connections through the first root valve.

Instrument sensing lines for Quality Class I and II instrumentation shall be Project Class C or Project Class D between the piping root valve/restriction and through the instrument fitting connection. Instrument sensing lines connected to Code Class 1 equipment (pressurizer) are listed in Appendix E.

6. Material requirements, including impact tests where applicable.

Piping materials for the system are defined in the Piping Material Classification and the line class is shown on the P&IDs and the Line Designation List by line number.

Project Class C and D instrument sensing line material shall be ASME SA-213 Grade 316 stainless steel.

Material for Class 1 piping will be impact tested in accordance with the requirements of NB-2300 of the ASME Code Section III.

Material for piping attached to containment penetration assemblies extending to the valves required to provide a pressure boundary for the containment function (isolation valves) shall be impact tested in accordance with the requirements and limitations specified in NC-2300 at 40 F.

Impact testing is not required for other material.

The corrosion/erosion allowance used in the design of carbon steel piping is .0625 inch thickness. No corrosion/erosion allowance is used in stainless steel pipe design.

7. Code stamping requirements

The piping system will be stamped with the appropriate N-type symbol at the fabrication site after all Code requirements have been met. The N-5 data report, for the Code Class 2 instrument sensing lines listed in Appendix E, will cross reference the N-5 data report for process piping systems of the same pressure, temperature and hydrostatic testing requirements.

Design, fabrication, examination and testing will be in accordance with the ASME B&PV Code, 1974 Edition including addenda through Summer 1974, except Class 1 nominal pipe size 1 inch and smaller will be designed and analyzed to the requirements of the 1975 Summer Addenda, Section III, Subparagraph NB-3630(d).

Code Case 1745 (N-122) applies.

Permanent attachments, such as but not limited to pipe stanchions, shear lugs, and pipe sleeves, shall be attached to the piping pressure boundary by either a full penetration or partial penetration weld in accordance with Paragraph NC/ND-4433 of the ASME B&PV Code 1974 Edition, Winter 1974 Addendum for Code Class 2 and Code Class 3 piping. For Code Class 1 piping, welding of attachments will be in accordance with Paragraph NB-4430 of the above Code.

Permanent attachments meeting the requirements of NB-4433 and temporary or minor permanent attachments meeting the requirements of NB-4435 may be welded to the piping system in accordance with NB-4436 of the ASME B&PV Code 1974 Edition, Summer 1976 Addendum, after performance of the pressure test provided that:

- a. The welds do not require PWHT under NB-4622-7;
- b. The cross-sectional area of the material attached shall not exceed 6 square inches (3870 mm²) at the surface of the pressure boundary material;
- c. Welds shall be restricted to fillet welds not exceeding 3/8 inch (10 mm) throat thickness and to full penetration welds attaching materials not exceeding 1/2 inch (13 mm) in thickness;
- d. Welds shall be examined as required by NB-5000.

For Code Class 2 and Code Class 3 piping, Paragraph NC/ND-4436 shall be used for the installation of piping attachments after hydrostatic/pneumatic testing.

The connection between instrument tubing and the instrument will be verified for leak integrity during operational testing of the system to satisfy Code requirements for pressure boundary integrity.

APPENDIX A
LINE DESIGNATION LIST

The data presented in the Line Designation List is subject to periodic revision.

In using this specification, designers should verify that the information included herein corresponds with the latest controlled revision.

REPORT NO: HW121-50-R1
 SEQ: 1-10-04 DESC: TAG SYS/PROJ CLS LE 1
 MSTR VERSION: 22A LIST VERSION: 22A
 PGE=BRK=DESC: TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 SAN ONDRE NUCLEAR GENERATING STATION

REPORT DATE: 1
 PAGE: 1
 PGT: 1

LINE NUMBER	M	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLN CLS	PROJ CLS	INSULATION THICK	PP TYPE	DESIGN TEMP	OPERATION TEMP
(SHORT TAG)	D												
				DRAWING	P B TO	COORD	REV	CODE OF ACCOUNT	SYSTEM	M A T E R I A L	ACCROSS DATE		
821201ML001 000 82RC00100000		REACTOR VESSEL V001 SYS 110100	STEAM GENERATOR E0A9 SYS 13010	42.00 40111	N/A	N/A	0 C60	0 2X6A.6423	0 2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0611 00001A07R0000000		
831201ML001 83RC001		REACTOR VESSEL V001 SYS 1101	STEAM GENERATOR E0A9 SYS 1301	42.00 40111	N/A	N/A	C6	3X6A.6423		3.5 CMC BW N/A	X 2485 0650 2239 0611 01A07R		
821201ML002 82RC002		REACTOR VESSEL V001 SYS 1101	STEAM GENERATOR E0A9 SYS 1301	42.00 40111	N/A	N/A	C3	2X6A.6423	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0611 01A07R		
831201ML002 83RC002		REACTOR VESSEL V001 SYS 1101	STEAM GENERATOR E0A9 SYS 1301	42.00 40111	N/A	N/A	C3	3X6A.6423	3BRR	3.5 CMC RW N/A	X 2485 0650 2239 0611 27AP79		
821201ML003 82RC003		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P001 SYS 1201	30.00 40111	N/A	N/A	C8	2X6A.6323	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 01A07R		
831201ML003 83RC003		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P001 SYS 1201	30.00 40111	N/A	N/A	C8	3X6A.6323	3BRR	3.5 CMC BW N/A	X 2485 0650 2239 0553 27AP79		
821201ML004 82RC004		STEAM GENERATOR E0B8 SYS 1301	REACTOR COOLANT PUMP P004 SYS 1201	30.00 40111	N/A	N/A	C2	2X6A.6323	2BRR	3.5 CMC BW N/A	X 2485 0650 2239 0553 01A07R		
831201ML004 83RC004		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P004 SYS 1201	30.00 40111	N/A	N/A	C2	3X6A.6323	3BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 27AP79		
821201ML005 82RC005		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P003 SYS 1201	30.00 40111	N/A	N/A	D8	2X6A.6323	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 01A07R		
831201ML005 83RC005		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P003 SYS 1201	30.00 40111	N/A	N/A	D8	3X6A.6323	3BRR	3.5 CMC BW N/A	X 2485 0650 2239 0553 27AP79		
821201ML006 82RC006		STEAM GENERATOR E0B8 SYS 1301	REACTOR COOLANT PUMP P002 SYS 1201	30.00 40111	N/A	N/A	C2	2X6A.6323	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 01A07R		
831201ML006 83RC006		STEAM GENERATOR E0A9 SYS 1301	REACTOR COOLANT PUMP P002 SYS 1201	30.00 40111	N/A	N/A	C2	3X6A.6323	3BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 27AP79		
821201ML007 82RC007		REACTOR COOLANT PUMP P001 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A	B6	2X6A.6323	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 01A07R		
831201ML007 83RC007		REACTOR COOLANT PUMP P001 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A	B6	3X6A.6323	3BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 27AP79		
821201ML008 82RC008		REACTOR COOLANT PUMP P004 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A	D4	2X6A.6323	2BRR	3.5 CMC RW N/A	X 2485 0650 2239 0553 01A07R		

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLM CLS	PROJ CLS	INSULATION THICK	2" PP TYPE	DESIGN PHES	OPERATION TEMP	PPES TEMP
(SHORT TAG)				DRAWING	P & I COORD	REV	CODE OF ACCOUNT	SYSTEM ENG	M A T E R I A L	ACCESS DATE				
831201ML008 83RC008		REACTOR COOLANT PUMP P004 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A		R A	3.5 CMC RW	Y 2485 0650 2235 0553				
						04	3X6A,6323	3RRR	N/A	27AP79				
821201ML009 82RC009		REACTOR COOLANT PUMP P003 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A		R A	3.5 CMC RW	Y 2485 0650 2235 0553				
						05	2X6A,6323	2RRR	N/A	01A117A				
831201ML009 83RC009		REACTOR COOLANT PUMP P003 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A		R A	3.5 CMC RW	Y 2485 0650 2235 0553				
						05	3X6A,6323	3RRR	N/A	27AP79				
821201ML010 82RC010		REACTOR COOLANT PUMP P002 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A		R A	3.5 CMC RW	Y 2485 0650 2235 0553				
						06	2X6A,6323	2RRR	N/A	01A117A				
831201ML010 83RC010		REACTOR COOLANT PUMP P002 SYS 1201	REACTOR VESSEL V001 SYS 1101	30.00 40111	N/A	N/A		R A	3.5 CMC RW	Y 2485 0650 2235 0553				
						04	3X6A,6323	3RRR	N/A	27AP79				
821201ML011A 82RC011		LINE 007 RC COLD LOOP 1A SYS 1201	SPRAY CONTROL VALVE 2PV 0100A8YS 1201	3.00 40111	FE0	160		R A	4.0 CMC RW	2485 0650 2235 0553				
						C4		2RRR	ASME8A376GRT316	13PE7A				
831201ML011A 83RC011		LINE 007 RC COLD LOOP 1A SYS 1201	SPRAY CONTROL VALVE 3PV 0100A8YS 1201	3.00 40111	FE0	160		R A	4.0 CMC RW	2485 0650 2235 0553				
						C4		3RRR	ASME8A376GRT316	27AP79				
821201ML011B 82RC011		LINE 007 RC COLD LOOP 1A SYS 1201	SPRAY CONTROL VALVE 2PV 0100A8YS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	2485 0650 2235 0553				
						C4		2RRR	ASME8A376GRT316	20M479				
831201ML011B 83RC011		LINE 007 RC COLD LOOP 1A SYS 1201	SPRAY CONTROL VALVE 3PV 0100A8YS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	2485 0650 2235 0553				
						C4		3RRR	ASME8A376GRT316	27AP79				
821201ML012A 82RC012		SPRAY LOOP 1A VALVE 2PV 0100A8YS 1201	PRESSURIZER ASSEMBLY E0A7 SYS 1201	0.75 40111	FE0	160		R A	4.0 CMC RW	2485 0650 2235 0553				
						P4	2X6A,1A22	2RRR	ASME8A376GRT316	01A117A				
831201ML012A 83RC012		SPRAY LOOP 1A VALVE 3PV 0100A8YS 1201	PRESSURIZER ASSEMBLY E0A7 SYS 1201	0.75 40111	FE0	160		R A	4.0 CMC RW	2485 0650 2235 0553				
						P4	3X6A,1A22	3RRR	ASME8A376GRT316	27AP79				
821201ML012B 82RC012		SPRAY LOOP 1A VALVE 2PV 0100A8YS 1201	PRESSURIZER ASSEMBLY E0A7 SYS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	Y 2485 0650 2235 0553				
						P4	2X6A,1A22	2RRR	ASME8A376GRT316	01A117A				
831201ML012B 83RC012		SPRAY LOOP 1A VALVE 3PV 0100A8YS 1201	PRESSURIZER ASSEMBLY E0A7 SYS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	Y 2485 0650 2235 0553				
						P4	3X6A,1A22	3RRR	ASME8A376GRT316	27AP79				
821201ML013A 82RC013		LINE 009 RC COLD LOOP 1B SYS 1201	SPRAY VALVE 2PV 0100A 8YS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	Y 2485 0650 2235 0553				
						04	2X6A,1A22	2RRR	ASME8A376GRT316	20M479				
831201ML013A 83RC013		LINE 009 RC COLD LOOP 1B SYS 1201	SPRAY VALVE 3PV 0100A 8YS 1201	4.00 40111	FE0	120		R A	4.5 CMC RW	Y 2485 0650 2235 0553				
						04	3X6A,1A22	3RRR	ASME8A376GRT316	27AP79				

REPORT NO. 1-50-91
 SEQ# 1-10-04 DESC# TAG SYS/PROJ CLS LE 1
 MSTR VERSION# 228 LIST VERSION# 228
 PGE-ARK-DESCI TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 BAN CONDRE NUCLEAR GENERATING STATION

REPORT DATE 09/09
 PAGE# 006 3 RPT

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLM CLS	PROJ CLS	INSULATION THICK	2" PP 1 TYPE	DESIGN PRES	OPERATION TEMP	TEMP
(SHORT TAG)				P & ID DRAWING	COORD	REV	CODE OF ACCOUNT	SYSTEM ENG	M A T E R I A L	ACC#88 DATE				
821201ML0138		LINE 009 RC COLD LOOP 1A	SPRAY VALVE 2PV 0100R SYS 1201	3.00	FFO	DS	2X6A.1A22	B A	4.0 CMC RW	X 2885	0650	2234	0553	
831201ML0138		LINE 009 RC COLD LOOP 1A	SPRAY VALVE 3PV 0100R SYS 1201	3.00	FFO	DS	3X6A.1A22	B A	4.0 CMC RW	X 2885	0650	2234	0553	
821201ML018A		LINE 013 VALVE 043 LOOP 1B	LINE 012 PRESSURIZER E0A7 SYS 1201	0.75	FE0	E3	2X6M.2722	B A	4.0 CMC RW	2885	0650	2235	0553	
831201ML018A		LINE 013 VALVE 043 LOOP 1A	LINE 012 PRESSURIZER E0A7 SYS 1201	0.75	FE0	E3	3X6M.2722	B A	4.0 CMC RW	2885	0650	2234	0553	
821201ML018B		LINE 013 VALVE 043 LOOP 1A	LINE 012 PRESSURIZER E0A7 SYS 1201	4.00	FE0	E3	2X6A.1A22	B A	4.5 CMC RW	X 2885	0650	2234	0553	
831201ML018B		LINE 013 VALVE 043 LOOP 1B	LINE 012 PRESSURIZER E0A7 SYS 1201	4.00	FE0	E3	3X6A.1A22	B A	4.5 CMC RW	X 2885	0650	2234	0553	
821201ML015		LINE 001 RC HOT LOOP	PRESSURIZER ASSEMBLY E0A7 SYS 1201	12.00	FE0	E6	2X6A.3A22	B A	4.5 CMC RW	X 2885	0700	2234	0653	
831201ML015		LINE 001 RC HOT LOOP	PRESSURIZER ASSEMBLY E0A7 SYS 1201	12.00	FE0	E6	3X6A.3A22	B A	4.5 CMC RW	X 2885	0700	2235	0653	
821201ML016A		LINE 002 RC HOT LOOP	LINE 017 2HV 9337 SYS 1201	16.00	FE0	C4	2X6A.4A252	B A	3.5 CMC RW	X 2885	0650	2235	0611	
831201ML016A		LINE 002 RC HOT LOOP	LINE 017 3HV 9337 SYS 1201	16.00	FE0	C4	3X6A.4A252	B A	3.5 CMC RW	X 2885	0650	2235	0611	
821201ML016B		LINE 002 RC HOT LOOP	LINE 017 2HV 9337 SYS 1201	18.00	FFO	C4	2X6A.4A252	B A	3.5 CMC RW	X 2885	0650	2234	0611	
831201ML016B		LINE 002 RC HOT LOOP	LINE 017 3HV 9337 SYS 1201	18.00	FFO	C4	3X6A.4A252	B A	3.5 CMC RW	X 2885	0650	2234	0611	
821201ML017A		LINE 016 VALVE 2HV 9337 SYS 1201	SI PUMPS LN 032 SYS 1204 VA 015 SYS 1201	18.00	KE0	E5	2X6A.47252	B C	3.0 CPP RW	X 0835	0400	0361	0350	
831201ML017A		LINE 016 VALVE 3HV 9337 SYS 1201	SI PUMPS LN 032 SYS 1204 VA 015 SYS 1201	18.00	KE0	E5	3X6A.47252	B C	3.0 CPP RW	X 0835	0400	0361	0350	
821201ML017B		LINE 016 VALVE 2HV 9337 SYS 1201	SI PUMPS LN 032 SYS 1204 VA 015 SYS 1201	16.00	KE0	E6	2X6A.4A252	B C	3.0 CPP RW	X 0835	0400	0361	0350	

REPORT NO: NM121-50-R1
 SEQ: 1-10-04 DESC: TAG SYS/PROJ CLS LE I
 MSTR VERSION: 22A LIST VERSION: 22B
 PGE=BRK-DEBC: TAG SYSTEM NO.

LINE DESIGNATION LIST - MASTERFILE
 SAN ONOPRE NUCLEAR GENERATING STATION

REPORT DATE: 11/04/79
 PAGE: HPK 6 RPT 4

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE WALL THICK	CLN PROJ CLS	INSULATION TYPE	2" PP I	DESIGN TEMP	OPERATION TEMP	
(SHORT TAG)			P B ID	CODE OF ACCOUNT	SYSTEM ENG	M A T E R I A L	ACCESS DATE					
831201ML017B		LINE 016 # VALVE	BI PUMPS LN 032 SYS	16.00	KEO	20	R C	3.0 CPP RW	X 0435	0400	0361	0350
83RC017		3HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	E6		2X6A,46252	3RMA	8A358GRT304CL1	27AP79		
821201ML017C		LINE 016 # VALVE	BI PUMPS LN 032 SYS	16.00	KEO	20	B C	1.5 APP BW	X 0435	0400	0361	0350
82RC017		2HV 9337 SYS 1201	1204 VA 015 SYS 1201	40112	F6		2X6A,36252	2RMA	8A358GRT304CL1	058E79		
831201ML017C		LINE 016 # VALVE	BI PUMPS LN 032 SYS	16.00	KEO	20	R C	1.5 APP BW	X 0435	0400	0361	0350
83RC017		3HV 9337 SYS 1201	1204 VA 015 SYS 1201	40112	F6		2X6A,36252	3RMA	8A358GRT304CL1	27AP79		
821201ML017D		LINE 016 # VALVE	SI PUMPS LN 032 SYS	12.00	KEO	20	R C	1.5 APP BW	X 0435	0400	0361	0350
82RC017		2HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	DA		2X6A,36252	2RMA	8A358GRT304CL1	058E79		
831201ML017D		LINE 016 # VALVE	BI PUMPS LN 032 SYS	12.00	KEO	20	B C	1.5 APP RW	X 0435	0400	0361	0350
83RC017		3HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	DA		2X6A,36252	3RMA	8A358GRT304CL1	27AP79		
821201ML017E		LINE 016 # VALVE	BI PUMPS LN 032 SYS	8.00	KEO	20	B C	1.5 APP RW	X 0435	0400	0361	0350
82RC017		2HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	E7			2RMA	8A358GRT304CL1	058E79		
831201ML017E		LINE 016 # VALVE	BI PUMPS LN 032 SYS	8.00	KEO	20	B C	1.5 APP RW	X 0435	0400	0361	0350
83RC017		3HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	E7			3RMA	8A358GRT304CL1	27AP79		
821201ML017F		LINE 016 # VALVE	BI PUMPS LN 032 SYS	1.00	KEO	408	B C	1.0 DPP RW	0435	0400	0361	0350
82RC017		2HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	E7			2RMA	ASME8A376GRT304	058E79		
831201ML017F		LINE 016 # VALVE	BI PUMPS LN 032 SYS	1.00	KEO	409	B C	1.0 DPP BW	0435	0400	0361	0350
83RC017		3HV 9337 SYS 1201	1204 VA 015 SYS 1201	40113	E7			3RMA	ASME8A376GRT304	27AP79		
821201ML018		LINE 001 RC HOT	LINE 295 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC RW	X 2485	0650	2235	0611
82RC018		LOOP 1A SYS 1201	VALVE 001 SYS 1201	40111	C6		2264,27211	2RRA	ASME8A376GRT316	01A1U79		
831201ML018		LINE 001 RC HOT	LINE 295 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC BW	X 2485	0650	2235	0611
83RC018		LOOP 1A SYS 1201	VALVE 001 SYS 1201	40111	C6		3264,27211	3RRA	ASME8A376GRT316	27AP79		
821201ML019		LINE 003 RC COLD	LINE 001 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC RW	X 2485	0650	2235	0553
82RC019		LOOP 1A SYS 1201	VALVE 002 SYS 1201	40111	CA		2264,27211	2BRA	ASME8A376GRT316	01A1U79		
831201ML019		LINE 003 RC COLD	LINE 001 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC RW	X 2485	0650	2235	0553
83RC019		LOOP 1A SYS 1201	VALVE 002 SYS 1201	40111	CA		3264,27211	3BRA	ASME8A376GRT316	27AP79		
821201ML020		LINE 004 RC COLD	LINE 300 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC BW	X 2485	0650	2235	0553
82RC020		LOOP 2A SYS 1201	VALVE 003 SYS 1201	40111	DI		2264,27211	2RMA	ASME8A376GRT316	01A1U79		
831201ML020		LINE 004 RC COLD	LINE 300 SYS 1901 #	2.00	FEO	160	B A	3.0 CMC RW	X 2485	0650	2235	0553
83RC020		LOOP 2A SYS 1201	VALVE 003 SYS 1201	40111	DI		3264,27211	3BRA	ASME8A376GRT316	27AP79		

REPORT NO: NH121-50-R1
 SEQ: 1-10-00 DESCI TAG SYS/PROJ CLS LE I
 MSTR VERSION: 220 LIST VERSION: 220
 PGE=BRK=DESCI TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 SAN ONDRE NUCLEAR GENERATING STATION

REPORT DATE: 1
 PAGE: BRK= 5 PRT= 4

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLN CLS	PROJ CLS	INSULATION THICK	2 ND PP I	DESIGN PRES	OPERATION TEMP	TEMP
(SHORT TAG)														
				DRAWING	P & ID	COND REV	COND OF ACCOUNT	SYSTEM	M A T E R I A L	ACCPTS DATE				
821201ML021 82RC021		LINE 022 RC COLD LOOP 1B SYS 1201	LINE 293 SYS 1901 VALVE 004 SYS 1201	2.00 40111	FE0	160 DB	B A 226H,27211	3.0 CMC RW 288A	X 2885 ASME8A376GRT316	0650 2235 01A1U7R	0553			
831201ML021 83RC021		LINE 022 RC COLD LOOP 1B SYS 1201	LINE 293 SYS 1901 VALVE 004 SYS 1201	2.00 40111	FE0	160 DB	B A 326H,27211	3.0 CMC BW 388A	X 2885 ASME8A376GRT316	0650 2235 27AP79	0553			
821201ML022 82RC022		LINE 005 RC COLD LOOP 1B SYS 1201	REGENERATIVE HEAT EXCH E063 SYS 1208	2.00 40111	FE0	160 EB	B A 2X6H,27241	3.0 CMC RW 288A	X 2885 ASME8A376GRT316	0650 2235 01A1U7R	0553			
831201ML022 83RC022		LINE 005 RC COLD LOOP 1B SYS 1201	REGENERATIVE HEAT EXCH E063 SYS 120A	2.00 40111	FE0	160 EB	B A 3X6H,27241	3.0 CMC RW 388A	X 2885 ASME8A376GRT316	0650 2235 27AP79	0553			
821201ML023 82RC023		LINE 001 RC LOOP 1A SYS 1201	LINE 030 SYS 1212 VALVE 006 SYS 1201	0.75 40111	FE0	160 CS	B A 2X6L,616	3.0 CMC RW 288A	X 2885 ASME8A376GRT316	0650 2235 01A1U7R	0611			
831201ML023 83RC023		LINE 001 RC LOOP 1A SYS 1201	LINE 030 SYS 1212 VALVE 006 SYS 1201	0.75 40111	FE0	160 CS	B A 3X6L,616	3.0 CMC BW 388B	X 2885 ASME8A376GRT316	0650 2235 27AP79	0611			
821201ML025 82RC025		LINE 036 LP8I PUMP DISCH HDR SYS 1208	LINE 017 2HV 9359 & 2HV 9353 SYS 1201	8.00 40112	KE1	20 E1	B C 2X6A,26252	1.5 APP RW 288A	X 0619 ASME8A376GRT304	0400 0600 20MR79	0400			
831201ML025 83RC025		LINE 036 LP8I PUMP DISCH HDR SYS 1208	LINE 017 3HV 9359 & 3HV 9353 SYS 1201	8.00 40112	KE1	20 E1	B C 3X6A,26252	1.5 APP BW 388A	X 0619 ASME8A376GRT304	0400 0615 27AP79	0400			
821201ML027 82RC027		CVCS LN 098 SYS 1208 & VA 031 SYS 1201	SHUTDOWN COOLING LINE 017 SYS 1201	3.00 40112	KE0	408 FS	B C 2X6A,17241	1.5 DPP RW 288A	0435 ASME8A376GRT304	0400 0361 05SE7R	0350			
831201ML027 83RC027		CVCS LN 098 SYS 1208 & VA 031 SYS 1201	SHUTDOWN COOLING LINE 017 SYS 1201	3.00 40112	KE0	408 FS	B C 3X6A,17241	1.5 DPP RW 388A	0435 ASME8A376GRT304	0400 0361 27AP79	0350			
821201ML028 82RC028		LINE 018 RC HOT LOOP SYS 1201	REFUELING LEVEL INDICATOR SYS 1201	0.75 40111	FE0	160 CB	B A 2X6H,27293	3.0 CMC RW 288A	X 2885 ASME8A376GRT316	0650 2235 01A1U7R	0611			
831201ML028 83RC028		LINE 018 RC HOT LOOP SYS 1201	REFUELING LEVEL INDICATOR SYS 1201	0.75 40111	FE0	160 CB	B A 3X6H,27293	3.0 CMC RW 388A	X 2885 ASME8A376GRT316	0650 2235 27AP79	0611			
821201ML030 82RC030		REACTOR VESSEL V001 SYS 1101	LINE 09A SYS 1201	0.75 40111	N/A	N/A DS	B A 2X6H,27293	3.0 CMC RW 288A	X 2885 N/A	0650 2235 20MR79	0611			
831201ML030 83RC030		REACTOR VESSEL V001 SYS 1101	LINE 09A SYS 1201	0.75 40111	N/A	N/A DS	B A 3X6H,27293	3.0 CMC RW 388B	X 2885 N/A	0650 2235 27AP79	0611			
821201ML031 82RC031		LINE 006 RC COLD LOOP 2R SYS 1201	LINE 298 SYS 1901 VALVE 005 SYS 1201	2.00 40111	FE0	160 C2	B A 226H,27211	3.0 CMC BW 288A	X 2885 ASME8A376GRT316	0650 2235 01A1U7R	0553			

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLY CLS	PROJ CLS	INSULATION THICK	2 ND PP	DESIGN PHEB TEMP	OPERATION PHEB TEMP
(SHORT TAG)				DRAWING	Ø & ID	COORD	REV	CONF	OF	SYSTEM	M A T E R I A L	ACCESS DATE	
831201ML031		LINE 006 RC COLO LOOP 2B	LINE 20A SYS 1201 VALVE 005 SYS 1201	2.00	FE0	160		A	A	3.0	CNC BW	Y 2485	0650 2235 0553
821201ML032		PRESSURIZER ASSEMBLY E087 SYS 1201	VALVE 2P8V 0200 SYS 1201	6.00	EE0	160		B	A	4.5	CNC RW	Y 2485	0700 2235 0653
831201ML032		PRESSURIZER ASSEMBLY E087 SYS 1201	VALVE 3P8V 0200 SYS 1201	6.00	EE0	160		A	A	4.5	CNC RW	Y 2485	0700 2235 0653
821201ML033		PRESSURIZER ASSEMBLY E087 SYS 1201	VALVE 2P8V 0201 SYS 1201	6.00	EE0	160		B	A	4.5	CNC RW	Y 2485	0700 2235 0653
831201ML033		PRESSURIZER ASSEMBLY E087 SYS 1201	VALVE 3P8V 0201 SYS 1201	6.00	EE0	160		A	A	4.5	CNC RW	Y 2485	0700 2235 0653
821201ML034		LINE 032 & 033 CROSS TIE	LINE 036 SYS 1201 VALVE 010 SYS 1201	0.75	EE0	160		B	A	4.0	CNC RW	2485	0700 2235 0653
831201ML034		LINE 032 & 033 CROSS TIE	LINE 036 SYS 1201 VALVE 010 SYS 1201	0.75	EE0	160		B	A	4.0	CNC RW	2485	0700 2235 0653
821201ML040A		REACTOR COOLANT PUMP P001 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	1.50	FE0	160		A	C	N/A	BW	2485	0650 0150 0150
831201ML040A		REACTOR COOLANT PUMP P001 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	1.50	FE0	160		A	C	N/A	SW	2485	0650 0150 0150
821201ML040B		REACTOR COOLANT PUMP P001 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	0.75	FE0	160		A	C	1.5	CPP SW	2485	0650 0150 0150
831201ML040B		REACTOR COOLANT PUMP P001 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	0.75	FE0	160		B	C	1.5	CPP SW	2485	0650 0150 0150
821201ML041A		REACTOR COOLANT PUMP P002 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	1.50	FE0	160		B	C	1.5	CPP BW	2485	0650 0150 0150
831201ML041A		REACTOR COOLANT PUMP P002 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	1.50	FE0	160		B	C	1.5	CPP SW	2485	0650 0150 0150
821201ML041B		REACTOR COOLANT PUMP P002 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	0.75	FE0	160		B	C	1.5	CPP SW	2485	0650 0150 0150
831201ML041B		REACTOR COOLANT PUMP P002 SYS 1201	LINE 053 SYS 1201 T077 SYS 1208	0.75	FE0	160		A	C	1.5	CPP BW	2485	0650 0150 0150

REPORT NO. -90-R1
 SEQ: 1-10-04 DESC: TAG SYS/PROJ CLS LE I
 MSTR VERSION: 228 LIST VERSION: 228
 PGE-RRK-DEB: TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 SAN ONDRE NUCLEAR REACTOR STATION

REPORT DATE: 09/01/79
 PAGE: RRK 9 RPT

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLM CLS	PROJ CLS	INSULATION THICK	2 ND PP	DESIGN PRES	OPERATION TEMP
(SHORT TAG)													
821201ML059		LINE 022 VALVE 110	BLIND FLANGE	0.75	FE0	160		B	C	3.0 CPP RW	24RS	0650 2235	0553
82RC059		8YS 1201	8YS 1201	40123		07		2RGA		ASMEB3376GRT316		138E7A	
831201ML059		LINE 022 VALVE 110	BLIND FLANGE	0.75	FE0	160		B	C	3.0 CPP RW	24RS	0650 2235	0553
83RC059		8YS 1201	8YS 1201	40123		07		3RGA		ASMEB3376GRT316		27AP79	
821201ML060		LINE 011 VALVE	LINE 012 REACTOR	2.00	FE0	160		B	A	4.0 CMC RW	Y 24RS	0650 2235	0553
82RC060		2HV 9201 8YS 1208	COOLANT 8YS 1201	40123		C7	2X6H,27241	2RRR		ASMEB3376GRT316		058E7A	
831201ML060		LINE 011 VALVE	LINE 012 REACTOR	2.00	FE0	160		B	A	4.0 CMC RW	Y 24RS	0650 2235	0553
83RC060		3HV 9201 8YS 1208	COOLANT 8YS 1201	40123		C7	3X6H,27241	3RRR		ASMEB3376GRT316		27AP79	
821201ML061		LINE 010 8YS 120A	LINE 00A REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
82RC061		2HV 9202 8YS 1201	LOOP 2A 8YS 1201	40123		C7	2X6H,27241	2RRR		ASMEB3376GRT316		01A17A	
831201ML061		LINE 010 8YS 120A	LINE 00A REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
83RC061		3HV 9202 8YS 1201	LOOP 2A 8YS 1201	40123		C7	3X6H,27241	3RRR		ASMEB3376GRT316		27AP79	
821201ML062		LINE 009 8YS 1208	LINE 007 REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
82RC062		2HV 9203 8YS 1201	LOOP 1A 8YS 1201	40123		07	2X6H,27241	2RRR		ASMEB3376GRT316		01A17A	
831201ML062		LINE 009 8YS 1208	LINE 007 REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
83RC062		3HV 9203 8YS 1201	LOOP 1A 8YS 1201	40123		07	3X6H,27241	3RRR		ASMEB3376GRT316		27AP79	
821201ML063		LINE 056 VALVE 107	LINE 062 REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
82RC063		8YS 1201	LOOP 1A 8YS 1201	40123		07	2X6H,27241	2RRR		ASMEB3376GRT316		01A17A	
831201ML063		LINE 056 VALVE 107	LINE 062 REACT COOL	2.00	FE0	160		B	A	3.0 CMC RW	Y 24RS	0650 2235	0553
83RC063		8YS 1201	LOOP 1A 8YS 1201	40123		07	3X6H,27241	3RRR		ASMEB3376GRT316		27AP79	
821201ML064		REACTOR VESSEL	LINE 073 VALVE 044	0.75	FE0	160		B	C	3.0 CMC RW	24RS	0650 2235	0611
82RC064		V001 8YS 1201	8YS 1201	40111		05	226H,27211	2RRR		ASMEB3376GRT316		058E7A	
831201ML064		REACTOR VESSEL	LINE 073 VALVE 044	0.75	FE0	160		B	C	3.0 CMC RW	24RS	0650 2235	0611
83RC064		V001 8YS 1201	8YS 1201	40111		05	326H,27211	3RRR		ASMEB3376GRT316		27AP79	
821201ML065		LINE 002 RC HOT	LINE 167 8YS 1212	0.75	FE0	160		B	A	3.0 CMC RW	24RS	0650 2235	0611
82RC065		LOOP 8YS 1201	VALVE 034 8YS 1201	40111		C4	2X6L,412	2RRR		ASMEB3376GRT316		01A17A	
831201ML065		LINE 002 RC HOT	LINE 167 8YS 1212	0.75	FE0	160		B	A	3.0 CMC RW	24RS	0650 2235	0611
83RC065		LOOP 8YS 1201	VALVE 034 8YS 1201	40111		C4	3X6L,412	3RRR		ASMEB3376GRT316		27AP79	
821201ML071		LINE 072 RC HOT	LINE 017 LP91	10.00	FE0	20		B	C	2.5 CPP RW	X 0435	0400 0361	0350
82RC071		LOOP 2 8YS 1201	PUMP P015 8YS 1201	40113		04	226A,36262	2RHA		ASMEB339GRT304		058E7A	

REPORT NO: 1-50-01
 BEU: 1-10-04 DESC: TAG SYS/PROJ CLS LE I
 MSTR VERSION: 228 LIST VERSION: 278
 PGE-BRK-DESC: TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 SAN ONDOR NUCLEAR GENERATING STATION

REPORT DATE: 11 RPT

LINE NUMBER	M	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLN CLS	PROJ CLS	INSULATION THICK	2 ND TYPE	PP 1 CUMM	DESIGN PRES TEMP	OPERATION PRES TEMP
(SHORT TAG)	0													
				DRAWING	P & ID	COORD	REV	CODE	OF	SYSTEM	M A T E R I A L	ACCRS	DATE	
								ACCOUNT		ENG	8-U			
821201ML130 82RC13A		UPPER SEAL CAVITY PUMP P008 SYS 1201	VENT TO ATMOSPHERE & 2PT 0172 SYS 1201	0.75 40130	PEO CS	160 CS		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FF79	0650 0060	0110
831201ML13A 83RC13A		UPPER SEAL CAVITY PUMP P008 SYS 1201	VENT TO ATMOSPHERE & 3PT 0172 SYS 1201	0.75 40130	PEO CS	160 CS		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML130 82RC130		MIDDLE SEAL CAVITY PUMP P001 SYS 1201	VENT TO ATMOSPHERE & 2PT 0151 SYS 1201	0.75 40130	PEO CS	160 CS		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 30JN78	0650 0060	0110
831201ML130 83RC130		MIDDLE SEAL CAVITY PUMP P001 SYS 1201	VENT TO ATMOSPHERE & 3PT 0151 SYS 1201	0.75 40130	PEO CS	160 CS		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML140 82RC140		MIDDLE SEAL CAVITY PUMP P002 SYS 1201	VENT TO ATMOSPHERE & 2PT 0181 SYS 1201	0.75 40130	PEO CS	160 CS		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FE79	0650 0060	0110
831201ML140 83RC140		MIDDLE SEAL CAVITY PUMP P002 SYS 1201	VENT TO ATMOSPHERE & 3PT 0181 SYS 1201	0.75 40130	PEO CS	160 CS		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML141 82RC141		MIDDLE SEAL CAVITY PUMP P003 SYS 1201	VENT TO ATMOSPHERE & 2PT 0161 SYS 1201	0.75 40130	PEO CS	160 CS		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FE79	0650 0060	0110
831201ML141 83RC141		MIDDLE SEAL CAVITY PUMP P003 SYS 1201	VENT TO ATMOSPHERE & 3PT 0161 SYS 1201	0.75 40130	PEO CS	160 CS		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML142 82RC142		MIDDLE SEAL CAVITY PUMP P004 SYS 1201	VENT TO ATMOSPHERE & 2PT 0171 SYS 1201	0.75 40130	PEO CS	160 CS		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FE79	0650 0060	0110
831201ML142 83RC142		MIDDLE SEAL CAVITY PUMP P004 SYS 1201	VENT TO ATMOSPHERE & 3PT 0171 SYS 1201	0.75 40130	PEO CS	160 CS		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML143 82RC143		LINE 040 VAPOR SEAL CAVITY SYS 1201	VENT TO ATMOSPHERE & 2PT 0153 SYS 1201	0.75 40130	PEO BT	160 BT		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 30JN78	0650 0060	0110
831201ML143 83RC143		LINE 040 VAPOR SEAL CAVITY SYS 1201	VENT TO ATMOSPHERE & 3PT 0153 SYS 1201	0.75 40130	PEO BT	160 BT		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML144 82RC144		LINE 041 VAPOR SEAL CAVITY SYS 1201	VENT TO ATMOSPHERE & 2PT 0183 SYS 1201	0.75 40130	PEO BT	160 BT		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FE79	0650 0060	0110
831201ML144 83RC144		LINE 041 VAPOR SEAL CAVITY SYS 1201	VENT TO ATMOSPHERE & 3PT 0183 SYS 1201	0.75 40130	PEO BT	160 BT		R C 3X6M,27293		388A	N/A RW ASME SA376GRT316	2885 27AP79	0650 0060	0110
821201ML145 82RC145		LINE 043 VAPOR SEAL CAVITY SYS 1201	VENT TO ATMOSPHERE & 2PT 0163 SYS 1201	0.75 40130	PEO BT	160 BT		B C 2X6M,27293		288A	N/A RW ASME SA376GRT316	2885 02FE79	0650 0060	0110

REPORT NO: NM121-90-R1
 SEQ: 1-10-04 DESC: TAG SYS/PROJ CLS LE I
 MSTR VERSION: 228 LIST VERSION: 228
 PGE=ARK=DESC: TAG SYSTEM NO.

LINE DESIGNATION LIST - MASTERFILE
 SAN ONDRE NUCLEAR GENERATING STATION

REPORT DATE: 11/04/79
 PAGE: RPK= 12 RPT= 12

LINE NUMBER	M B D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLN CLS	PROJ CLS	INSULATION THICK	2" PP I	DESIGN PRES	OPERATION PRES	TEMP	TEMP
(SHORT TAG)															
				DRAWING	P & ID	REV	CODE OF ACCOUNT	SYSTEM ENG	M A T E R I A L	ACCESS DATE					
831201ML145		LINE 043 VAPOR SEAL CAVITY	VENT TO ATMOSPHERE & 3PT	0.75	FE0	160	B C								
83RC145		8YS 1201	0163 SYS 1201	40130		87	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML146		LINE 042 VAPOR SEAL CAVITY	VENT TO ATMOSPHERE & 2PT	0.75	FE0	160	B C								
82RC146		8YS 1201	0173 SYS 1201	40130		87	2X6M,27293	288A	N/A BW	2885	0650	0060	0110	02FF79	
831201ML146		LINE 042 VAPOR SEAL CAVITY	VENT TO ATMOSPHERE & 3PT	0.75	FE0	160	B C								
83RC146		8YS 1201	0173 SYS 1201	40130		87	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML147		LINE 065 VALVE 152	LINE 01A RC WDT LOOP	3.00	FF0	160	B A	3.0	CNC BW	X 2885	0650	2235	0611		
82RC147		8YS 1204	8YS 1201	40111		C5	2X6A,18262	288R	ASME8A376GRT316		053E78				
831201ML147		LINE 065 VALVE 152	LINE 01B RC WDT LOOP	3.00	FE0	160	B A	3.0	CNC BW	X 2885	0650	2235	0611		
83RC147		8YS 1204	8YS 1201	40111		C5	3X6A,18262	388R	ASME8A376GRT316		27AP79				
821201ML149		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
82RC149		P001 8YS 1201	8YS 1201	40130		C5	2X6M,27293	288A	N/A BW	2885	0650	0060	0110	30JN78	
831201ML149		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
83RC149		P001 8YS 1201	8YS 1201	40130		C5	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML150		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
82RC150		P002 8YS 1201	8YS 1201	40130		C5	2X6M,27293	288A	N/A BW	2885	0650	0060	0110	30JN78	
831201ML150		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
83RC150		P002 8YS 1201	8YS 1201	40130		C5	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML151		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
82RC151		P003 8YS 1201	8YS 1201	40130		C5	2X6M,27293	288A	N/A BW	2885	0650	0060	0110	30JN78	
831201ML151		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
83RC151		P003 8YS 1201	8YS 1201	40130		C5	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML152		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
82RC152		P004 8YS 1201	8YS 1201	40130		C5	2X6M,27293	288A	N/A BW	2885	0650	0060	0110	30JN78	
831201ML152		LOWER SEAL PUMP	VENT	0.75	FE0	160	B C								
83RC152		P004 8YS 1201	8YS 1201	40130		C5	3X6M,27293	388A	N/A BW	2885	0650	0060	0110	27AP79	
821201ML153		R C PUMP SUCTION	PRESS DIFF XMITTER	0.75	FE0	160	B C	3.0	CNC BW	2885	0650	2235	0553		
82RC153		P001 8YS 1201	2PDT 0110 SYS 1201	40130		86	2X6L,616	288A	ASME8A376GRT316		30JN78				
831201ML153		R C PUMP SUCTION	PRESS DIFF XMITTER	0.75	FE0	160	B C	3.0	CNC BW	2885	0650	2235	0553		
83RC153		P001 8YS 1201	3PDT 0110 SYS 1201	40130		86	3X6L,616	388A	ASME8A376GRT316		27AP79				

REPORT NO: 121-50-R1
 SEQ: 1-10-04 DESC: TAG SYS/PROJ CLS LE I
 MSTR VERSION: 220 LIST VERSION: 220
 PGE-RRK-DESC: TAG SYSTEM NO.

LINE DESIGNATION MASTERFILE
 SAN ONDRE NUCLEAR GENERATING STATION

REPORT DATE: 11/13/79
 PAGE: 446 13 RPT- 13

LINE NUMBER	M	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATERIAL CLS	PIPE SCHD	WALL THICK	CLM CLS	PROJ CLS	INSULATION THICK	2" PP I TYPE	DESIGN PRES	OPERATION TEMP	DESIGN TEMP	OPERATION TEMP	SYSTEM ENG	MATERIAL	ACCESS DATE
821201ML154 82RC154	R	PUMP SUCTION P002 SYS 1201	PRESS DIFF XMITTER 2PDT 0122 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
831201ML154 83RC154	R	PUMP SUCTION P002 SYS 1201	PRESS DIFF XMITTER 3PDT 0122 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
821201ML155 82RC155	R	PUMP SUCTION P003 SYS 1201	PRESS DIFF XMITTER 2PDT 0112 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
831201ML155 83RC155	R	PUMP SUCTION P003 SYS 1201	PRESS DIFF XMITTER 3PDT 0112 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
821201ML156 82RC156	R	PUMP SUCTION P004 SYS 1201	PRESS DIFF XMITTER 2PDT 0120 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
831201ML156 83RC156	R	PUMP SUCTION P004 SYS 1201	PRESS DIFF XMITTER 3PDT 0120 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2235 0553 03MY79
821201ML157 82RC157	R	PUMP DISCHARGE P001 SYS 1201	PRESS DIFF XMITTER 2PDT 0111 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2250 0553 01AU78
831201ML157 83RC157	R	PUMP DISCHARGE P001 SYS 1201	PRESS DIFF XMITTER 3PDT 0111 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2250 0553 27AD79
821201ML158 82RC158	R	PUMP DISCHARGE P002 SYS 1201	PRESS DIFF XMITTER 2PDT 0123 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
831201ML158 83RC158	R	PUMP DISCHARGE P002 SYS 1201	PRESS DIFF XMITTER 3PDT 0123 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
821201ML159 82RC159	R	PUMP DISCHARGE P003 SYS 1201	PRESS DIFF XMITTER 2PDT 0113 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
831201ML159 83RC159	R	PUMP DISCHARGE P003 SYS 1201	PRESS DIFF XMITTER 3PDT 0113 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
821201ML160 82RC160	R	PUMP DISCHARGE P004 SYS 1201	PRESS DIFF XMITTER 2PDT 0121 SYS 1201	0.75	FEO	160											3.0 CMC BW 28AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
831201ML160 83RC160	R	PUMP DISCHARGE P004 SYS 1201	PRESS DIFF XMITTER 3PDT 0121 SYS 1201	0.75	FEO	160											3.0 CMC BW 38AA ASME8A376GRT316	2885 0650 2250 0553 03MY79
821201ML161 82RC161		LINE 017 RC HOT LOOP SYS 1201	PSV (FUTURE) SYS 1201	6.00	KEO	109											N/A RW 28AA	0835 0400 0435 0400 058E78

REPORT NO: NM121-50-R1
 SEQ: 1-10-04 DESC: TAG BYB/PROJ CLS LE I
 MSTR VERSION: 228 LIST VERSION: 228
 PGE-BRK-DESC: TAG SYSTEM NO.

LINE DESIGNATION LIST - MASTERFILE
 SAN ONDRE NUCLEAR GENERATING STATION

REPORT DATE: 11/14/79
 PAGE: BRK= 14 RPT= 14

LINE NUMBER	M S D	DESCRIPTION FROM	DESCRIPTION TO	PIPE SIZE	MATL CLS	PIPE SCHED	WALL THICK	CLN CLS	PROJ CLS	INSULATION THICK	2" PP I	DESIGN PREB TEMP	OPERATION PRES TEMP
(SHORT TAG)													
				P & ID DRAWING	COORD	REV	ENGR	OF	SYSTEM ENG	MATERIAL	ACCESS DATE		
831201ML161 83RC161		LINK 017 RC HOT LOOP	PBV (FUTURE) BYB 1201	6.00 40113	HE0	109 E5			R C	3RMA	N/A BW	0835.0400	0434 0400 27AP79

RECORDS PRINTED THIS PAGE-BREAK: 196

March 14, 1977

APPENDIX B

1. Seismic Category I Instructure Response Spectra (as listed on Page 2).
2. CE Reactor Coolant System Tributary Nozzle Response Spectra, Seismic Category I.

(Contained in enclosure to CE to BPC letter, S-CE-3122, dated July 30, 1976).....S023-900-B-45-0

thru 47-0,

52-0

thru 59-0,

62-0

thru 66-0

(Contained in enclosure to CE to BPC letter, S-CE-3165, dated August 13, 1976).....S023-900B-71-0

and-72-0

(Contained in enclosure to CE to BPC letter, S-CE-3364, dated October 22, 1976).....S023-900B-73

and-74

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d = DISPLACEMENT RESPONSE (INCHES)
 T = PERIOD (SEC.)
 S_a = ACCELERATION RESPONSE (g 's)

DAMPING VALUES
 AS PERCENT OF CRITICAL

BECHTEL
 BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

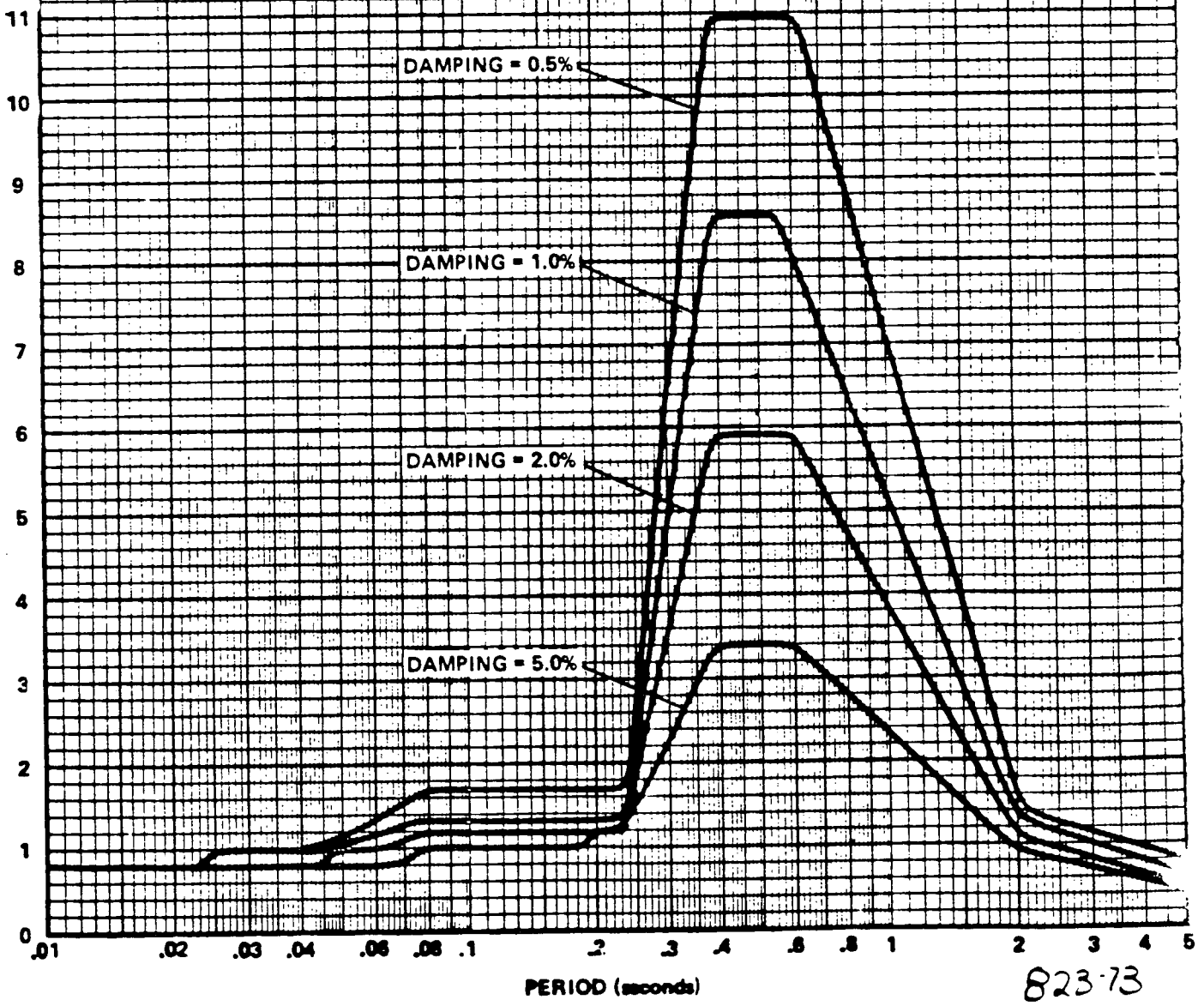
SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE BASEMAT

Prepared By <i>JWW KMS</i>	Reviewed By <i>LGH</i>	Approved By <i>WAB</i>
-------------------------------	---------------------------	---------------------------

JOB NO 1304-803	SKETCH NO S023-SK-S-627	REV Δ
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ACCELERATION (g 's)



823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE BASEMAT

Prepared By

JWW KMS

Reviewed By

IGH QB

Approved By

WAB JRE

JOB NO.

1304-803

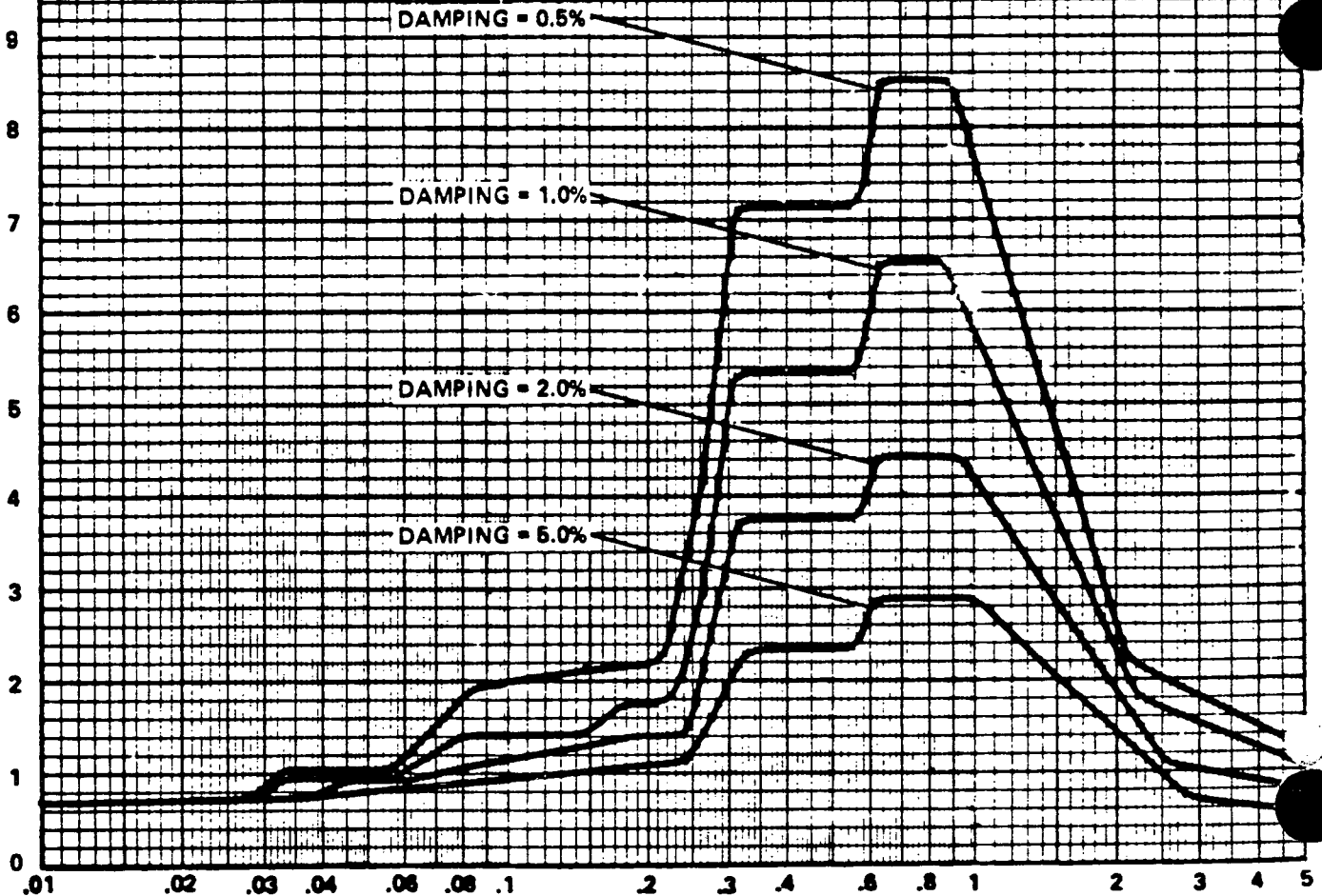
SKETCH NO.

8023-SK-S-828

REV

A

ACCELERATION (g's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 30'-0"

Prepared By

Reviewed By

Approved By

JWW KMS

LGH *[Signature]*

WAB *[Signature]*

JOB NO
1304-803

SKETCH NO.
S023-SK-S-629

REV.
A

ACCELERATION (g 's)

11

10

9

8

7

6

5

4

3

2

1

0

DAMPING = 0.5%

DAMPING = 1.0%

DAMPING = 2.0%

DAMPING = 5.0%

PERIOD (seconds)

.01

.02

.03

.04

.06

.08

.1

.2

.3

.4

.5

.8

1

2

3

4

5

823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)

**DAMPING VALUES
 AS PERCENT OF CRITICAL**



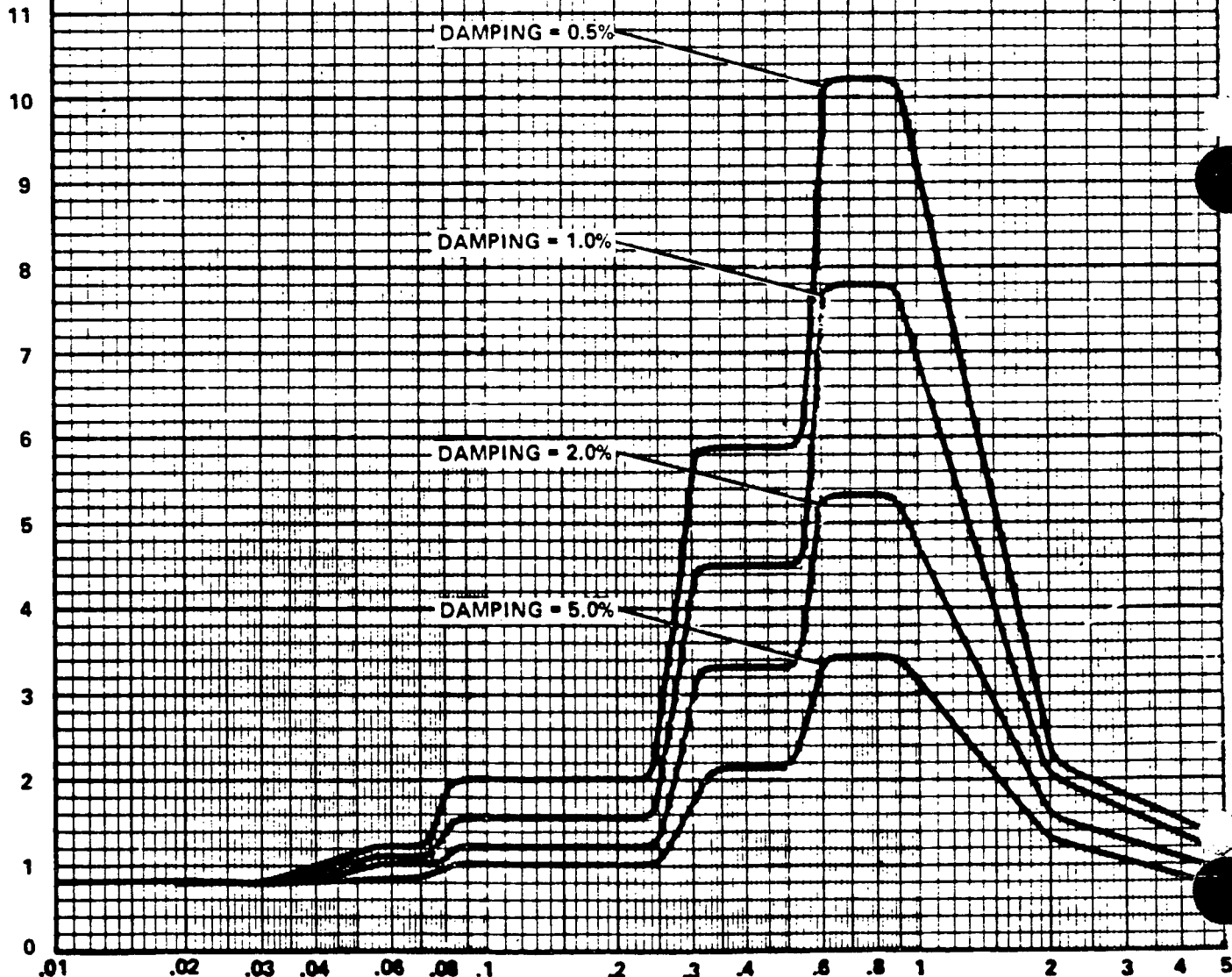
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 30'-0"

Prepared By <i>JWW</i> KMS	Reviewed By <i>IGH</i> <i>DB</i>	Approved By <i>WAB</i> <i>WFE</i>
JOB NO 1304-803	SKETCH NO. S023-SK-S-630	REV <i>A</i>

ACCELERATION (g 's)



PERIOD (seconds)

823-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC.)

S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

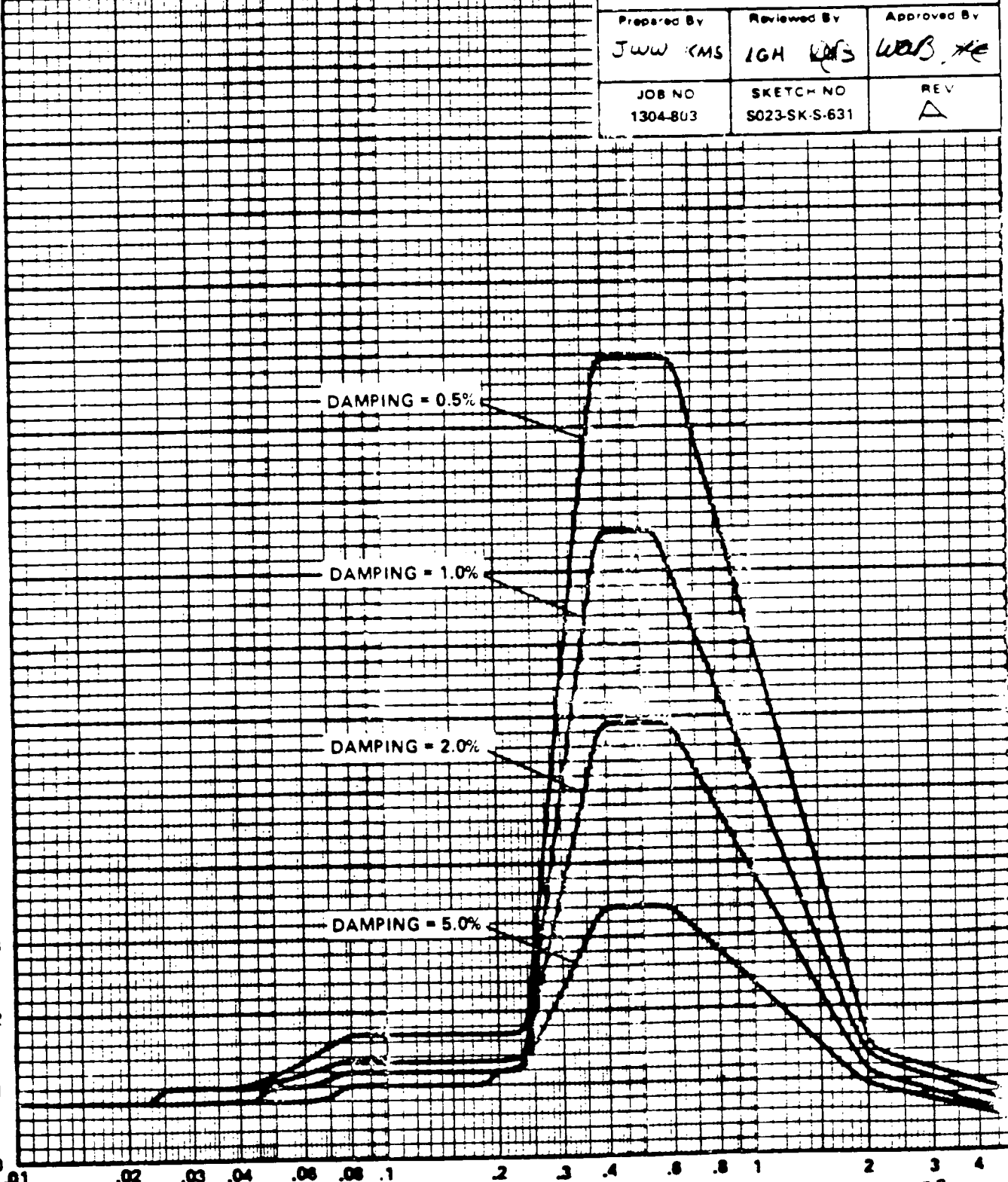
SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 45'-0"

Prepared By JWW (MS)	Reviewed By IGH (MS)	Approved By WAB, HE
JOB NO 1304-803	SKETCH NO S023-SK-S-631	REV A

ACCELERATION (g's)

11
10
9
8
7
6
5
4
3
2
1
0



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$$S_d = 10 T^2 S_a$$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC.)

S_a = ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION,
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 45'-0"

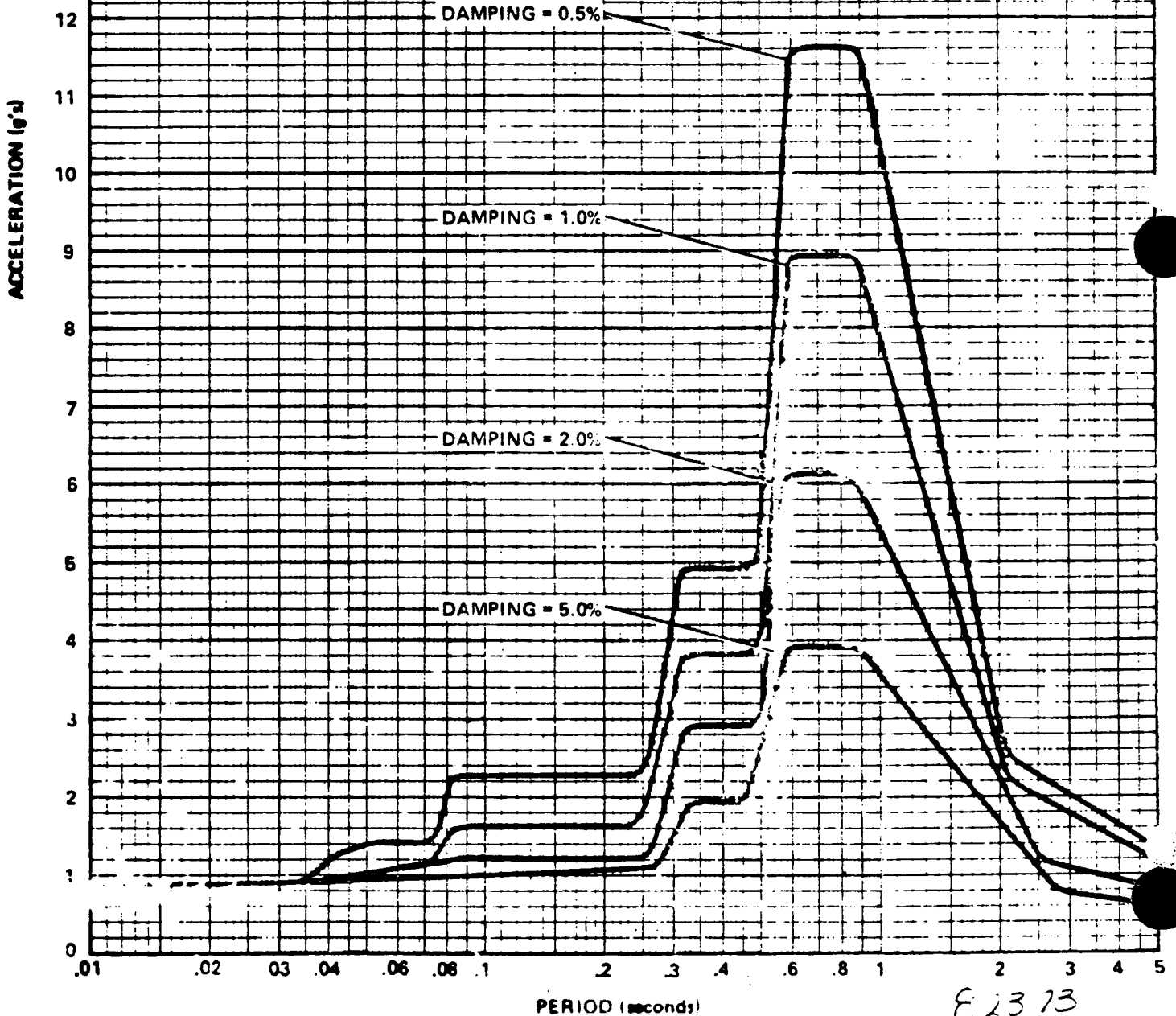
Prepared By Reviewed By Approved By

KMS *LGH* *WOB*

JOB NO
1304-803

SKETCH NO
S023-SK-S-632

REV
A



E 23 73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 63'-6"

Prepared By

JWW KMS

Reviewed By

IGH *[Signature]*

Approved By

WLB *[Signature]*

JOB NO

1304-803

SKETCH NO

S023-SK-S-633

REV

△

ACCELERATION (g's)

11

10

9

8

7

6

5

4

3

2

1

0

DAMPING = 0.5%

DAMPING = 1.0%

DAMPING = 2.0%

DAMPING = 5.0%

PERIOD (seconds)

.01

.02

.03

.04

.06

.1

.2

.3

.4

.6

.8

1

2

3

4

5

8-23-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 63'-6"

Prepared By

Reviewed By

Approved By

JWW KMS

LGH JG

WUB JRE

JOB NO

SKETCH NO.

REV

1304-803

S023-SK-S-634

A

ACCELERATION (g's)

14

13

12

11

10

9

8

7

6

5

4

3

2

1

0

DAMPING = 0.5%

DAMPING = 1.0%

DAMPING = 2.0%

DAMPING = 5.0%

.01

.02

.03

.04

.06

.08

.1

.2

.3

.4

.6

.8

1

2

3

4

5

PERIOD (seconds)

823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



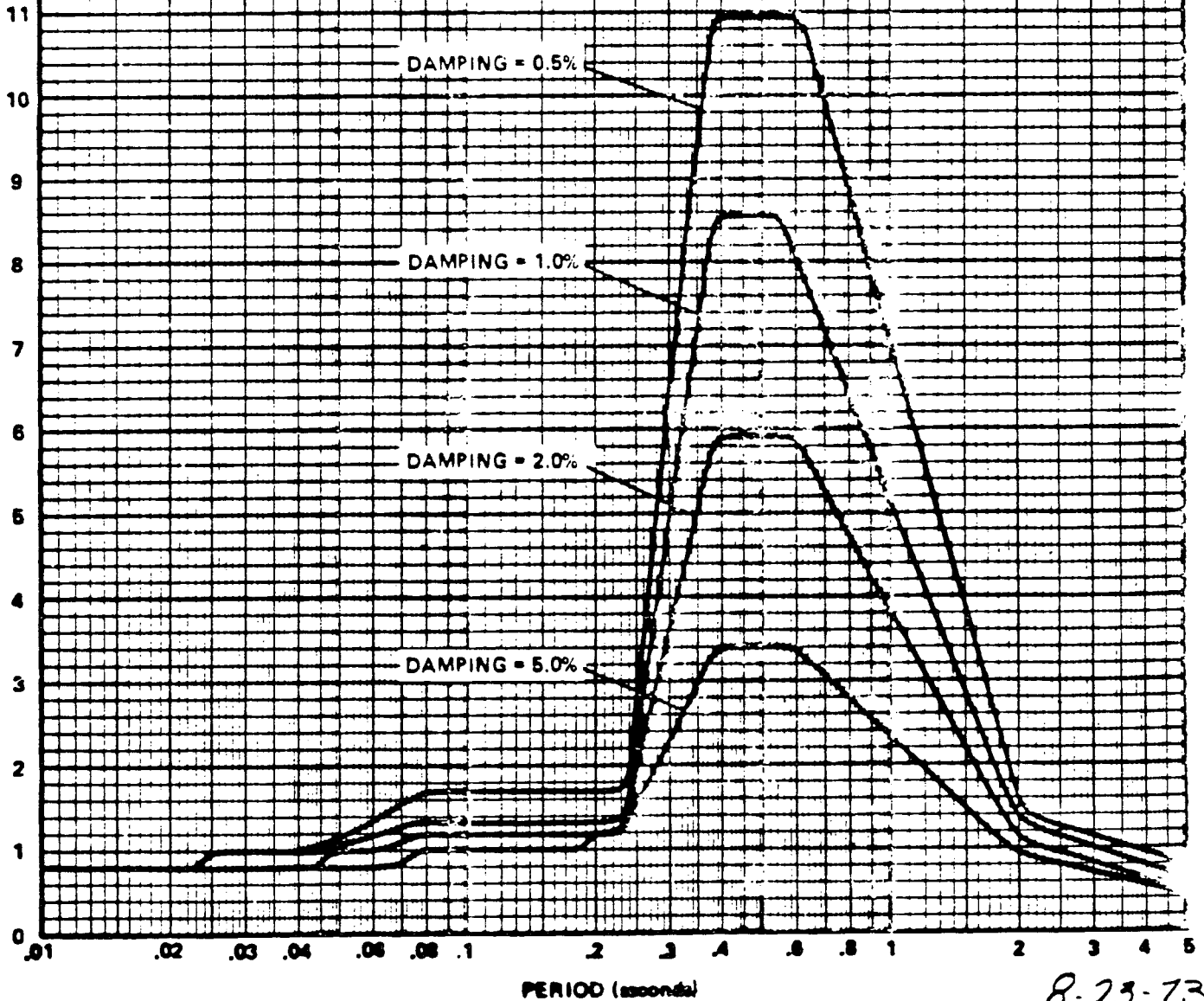
BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE ELEVATION 80'-6"

Prepared By: JWW/KMS	Reviewed By: LGH/CRB	Approved By: WAB/JHE
JOB NO. 1304-803	SKETCH NO. S023-SK-S-635	REV A

ACCELERATION (g 's)



8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL

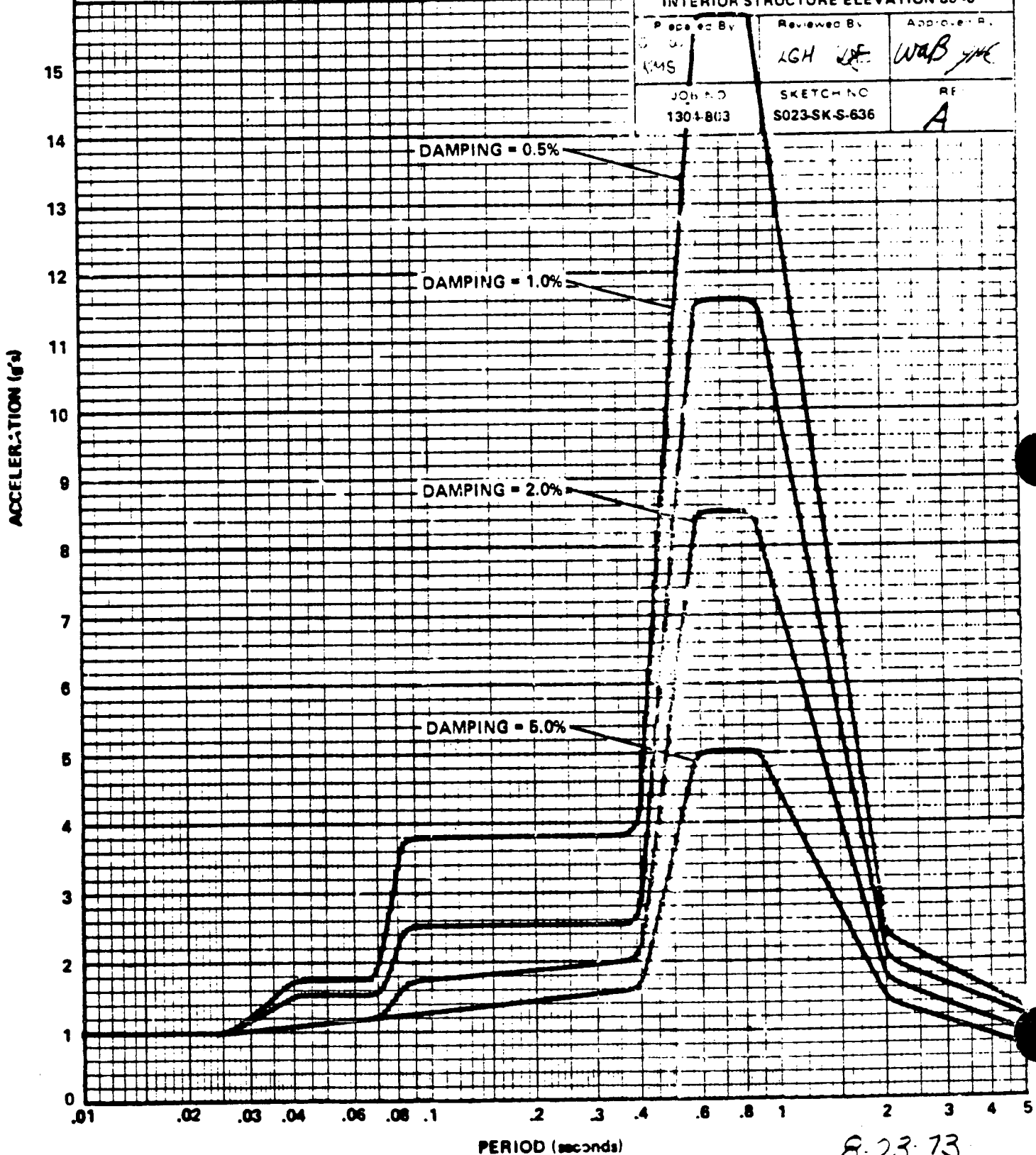


BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN Geronimo NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 80'-6"

Prepared By KMS	Reviewed By LGH JDE	Approved By WAB JHE
Job No 1304-803	Sketch No S023-SK-S-636	RF A



8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

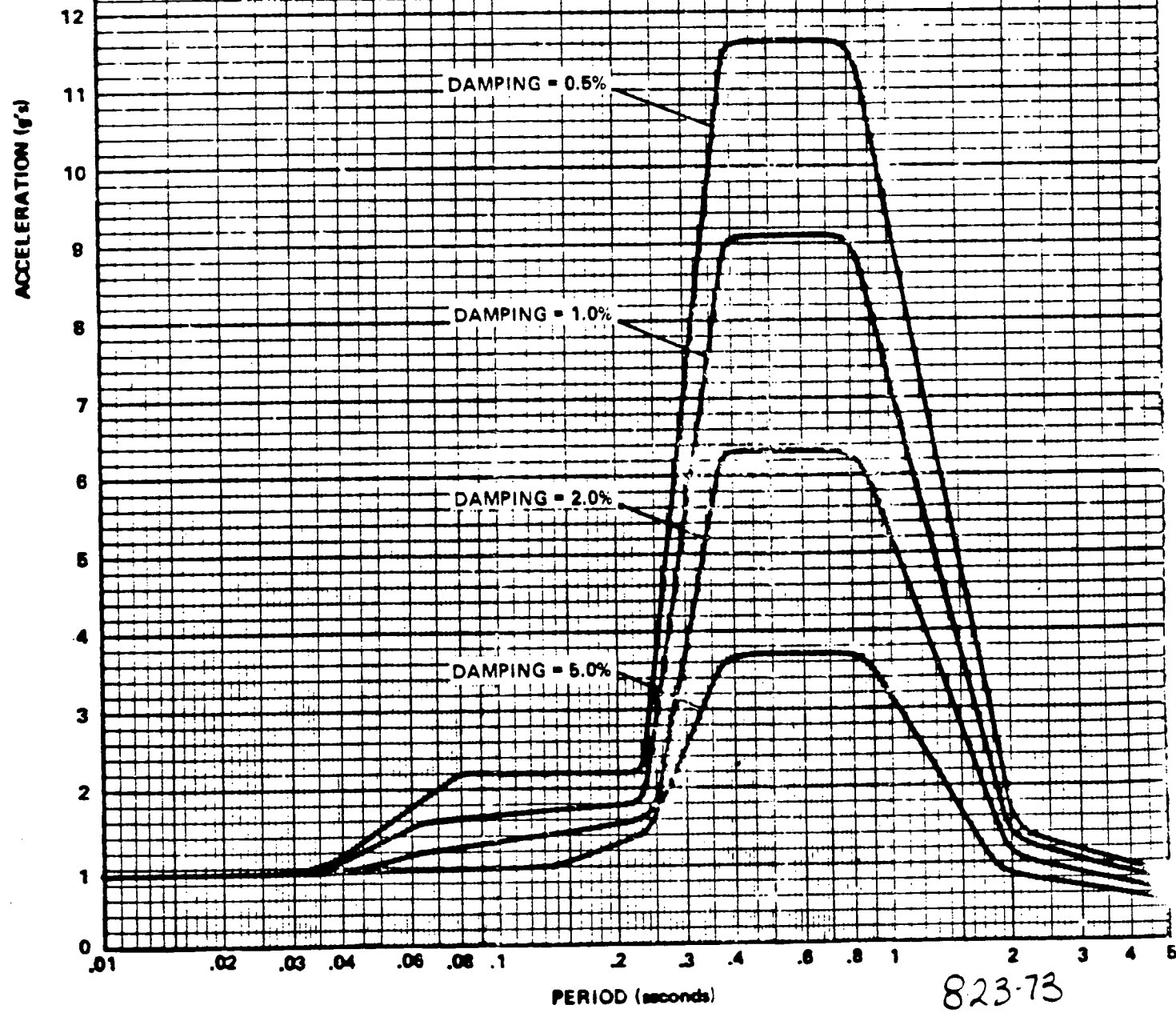
BECHTEL BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION
 SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DAMPING VALUES
 AS PERCENT OF CRITICAL

DESIGN BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 EXTERIOR SHELL BASEMAT

Prepared By <i>JWW</i> KMS	Reviewed By LGH <i>LGH</i>	Approved By WAB <i>WAB</i>
-------------------------------	-------------------------------	-------------------------------

JOB NO 1304-803	SKETCH NO S023-SK-S-637	REV A
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823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC.)

S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL BASEMAT

Prepared By

Jaw
KMS

Reviewed By

AGH
LGB

Approved By

WAB

JOB NO

1304-803

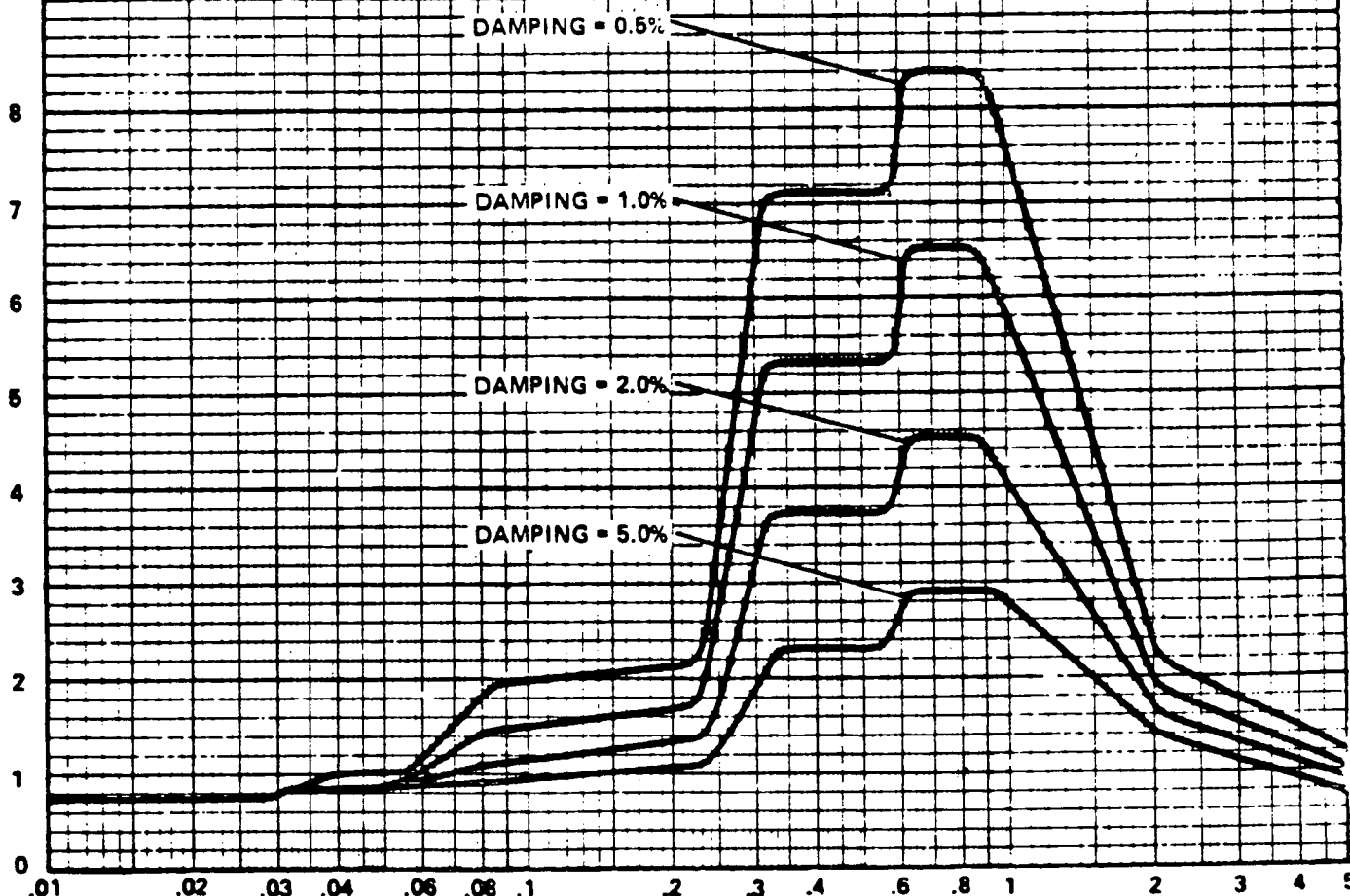
SKETCH NO.

S023-SK-S-638

REV

A

ACCELERATION (g's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



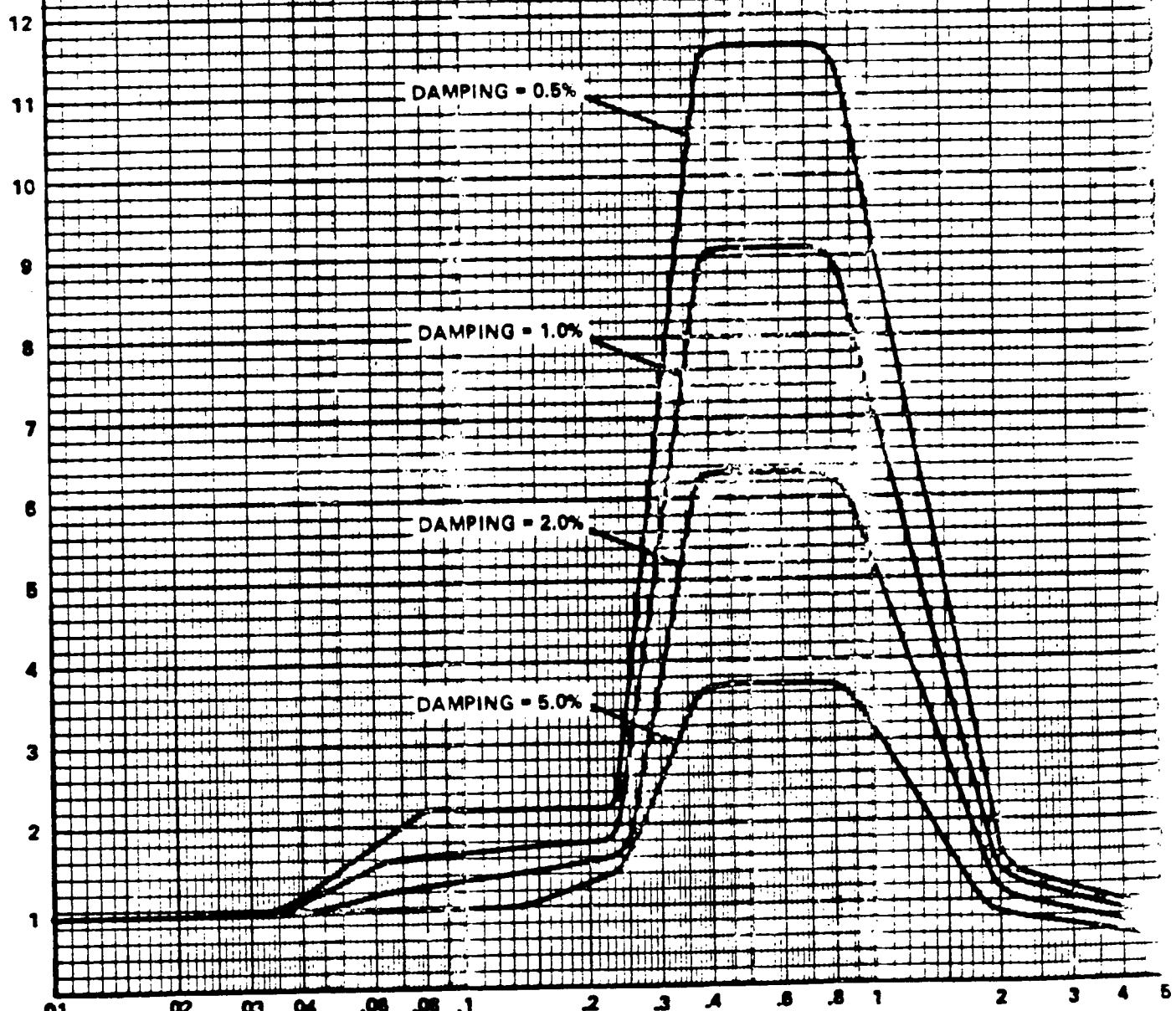
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL ELEVATION 36'-0"

Prepared By JWW KMS	Reviewed By LGM QB	Approved By WAB g/c
JOB NO 1304-803	SKETCH NO. S023-SK-S-639	REV A

ACCELERATION (g's)



8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC.)

S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BCHTEL POWER CORPORATION,
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL ELEVATION 36'-0"

Prepared By

Reviewed By

Approved By

JWW KMS

LGH

WDB

JOB NO

SKETCH NO.

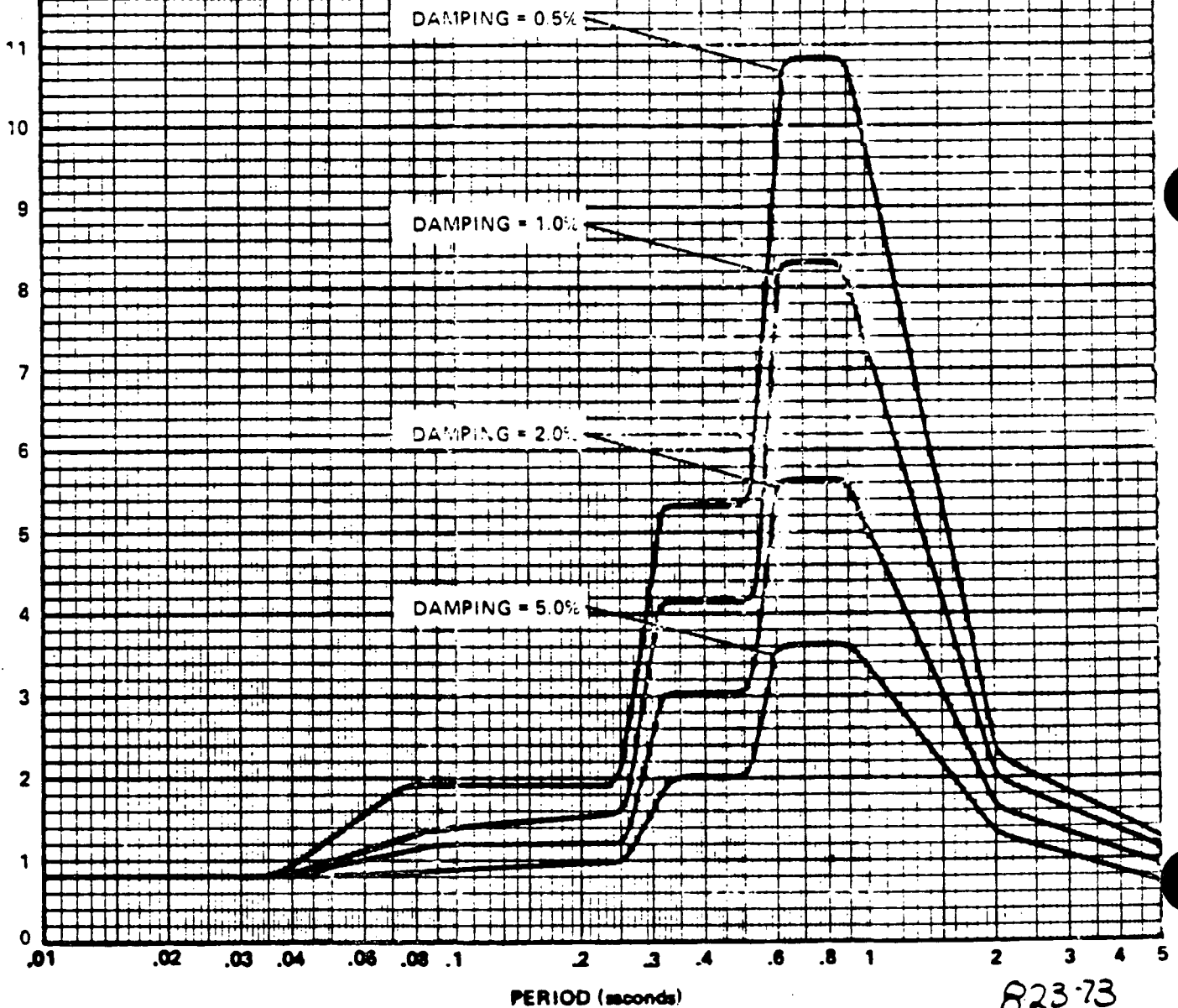
REV

1304 800

S023 SK S-640

A

AC. IP. (g)



823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10^{-12} S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC)

S_a = ACCELERATION RESPONSE (g)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE BASEMAT

Prepared By

Jaw KMS

Reviewed By

LGH *[signature]*

Approved By

[signature]

JOB NO

1304-803

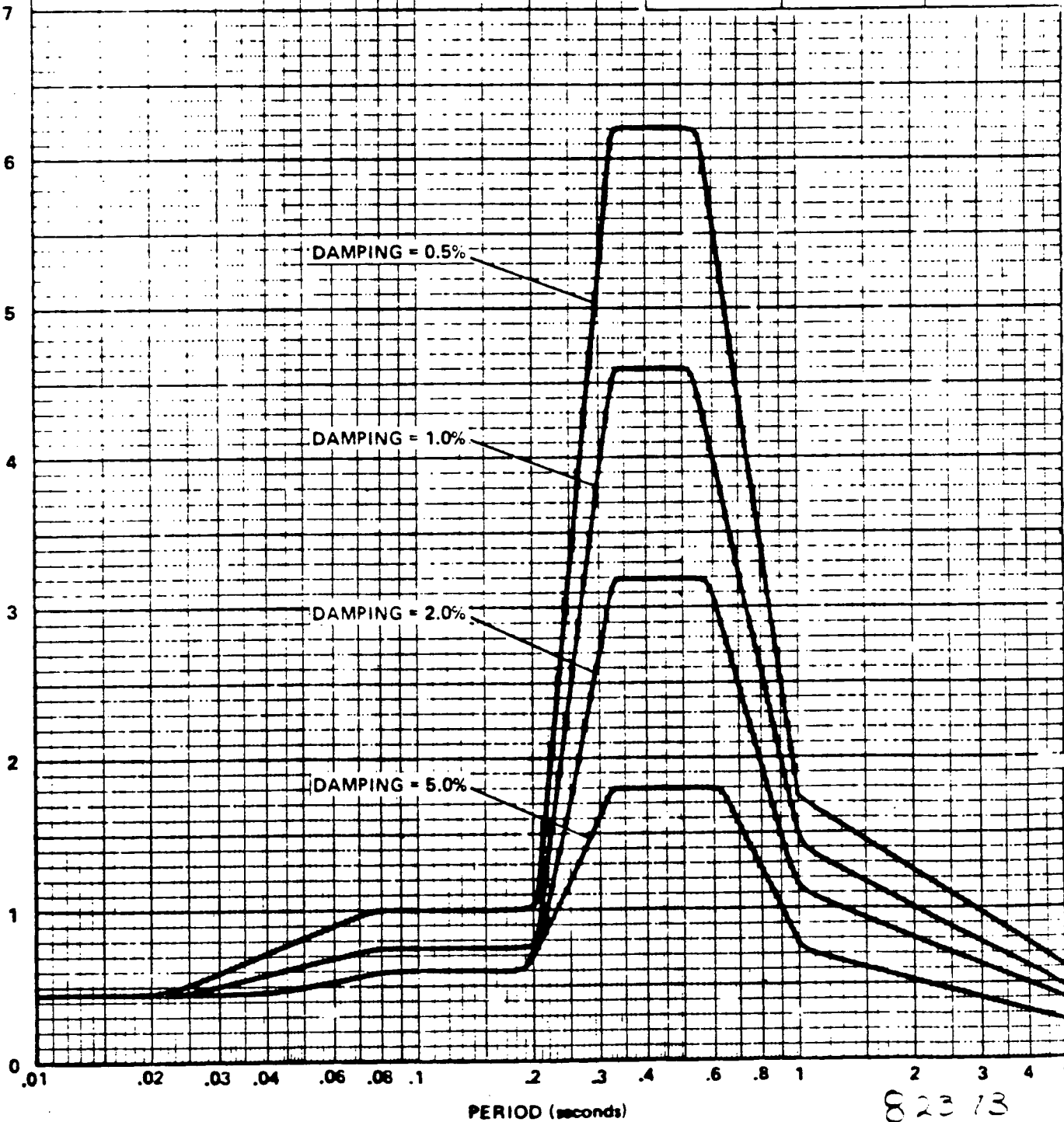
SKETCH NO

S023-SK-S-649

RE

△

ACCELERATION (g's)



823 13

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d = DISPLACEMENT RESPONSE (INCHES)
 T = PERIOD (SEC.)
 S_a = ACCELERATION RESPONSE (g 's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



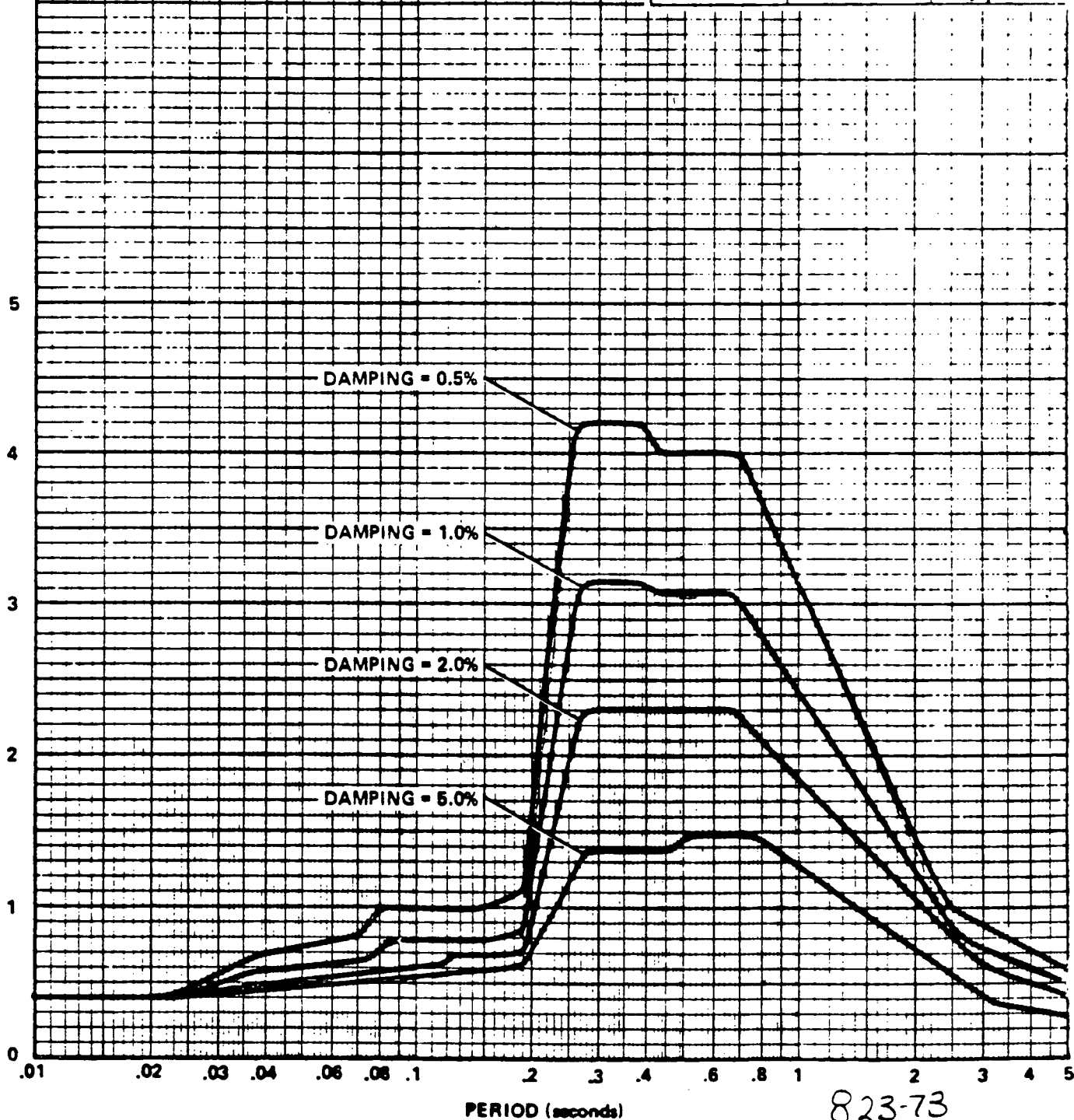
BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 HORIZONTAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE BASEMAT

Prepared by: J.W. KMS	Reviewed by: LGH WAF	Checked by: WAF
Job No. 1304-803	Sketch No. S023-SK-S-650	PI A

ACCELERATION (g 's)




823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

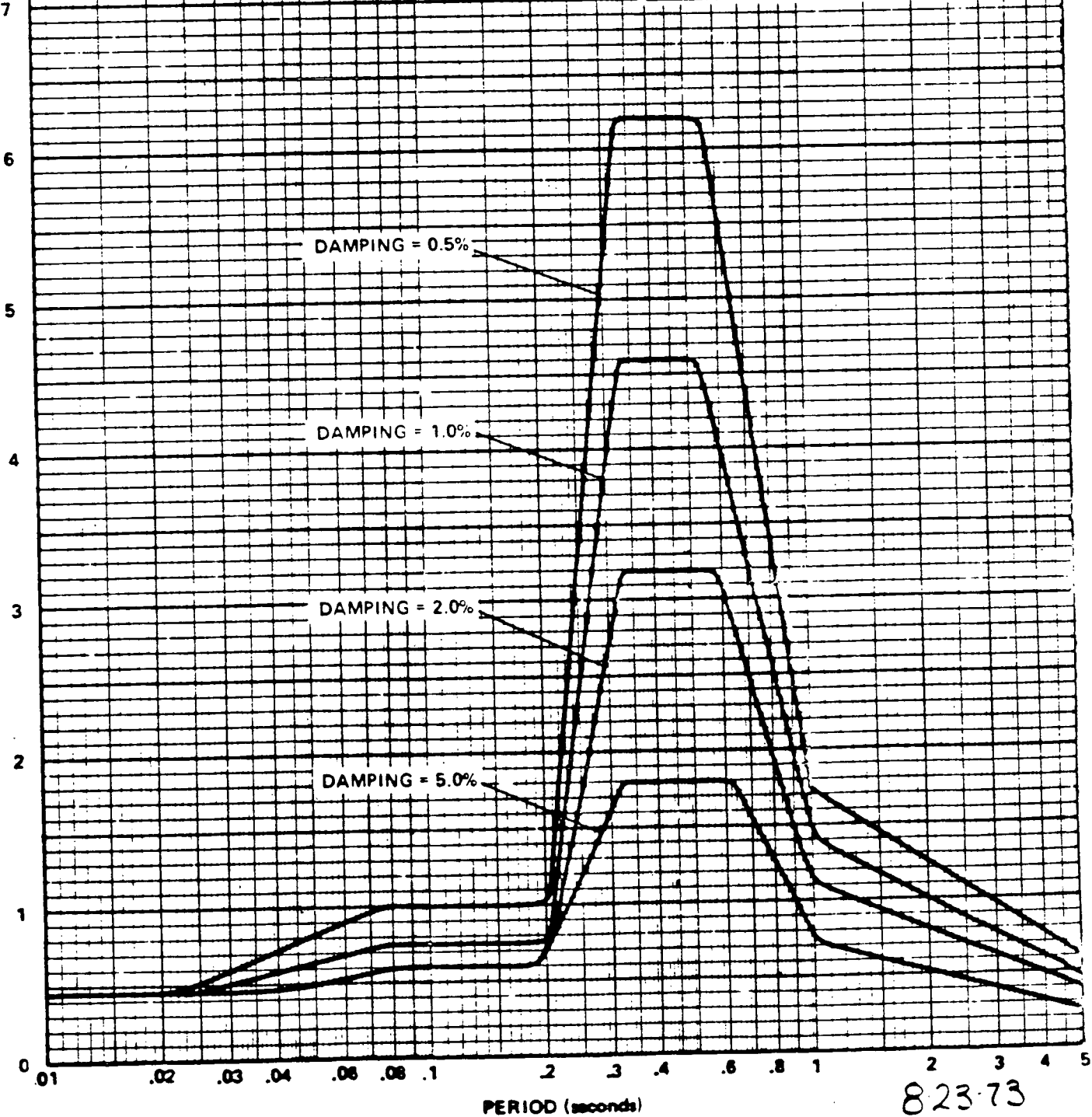
DAMPING VALUES
AS PERCENT OF CRITICAL


 BECHTEL POWER CORPORATION,
 LOS ANGELES DIVISION
 SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE ELEVATION 30'-0"

Prepared By JWW KMS	Reviewed By LGH <i>(signature)</i>	Approved By WAB <i>(signature)</i>
JOB NO 1304-803	SKETCH NO. S023-SK-S-651	REV A

ACCELERATION (g's)



PERIOD (seconds)

823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



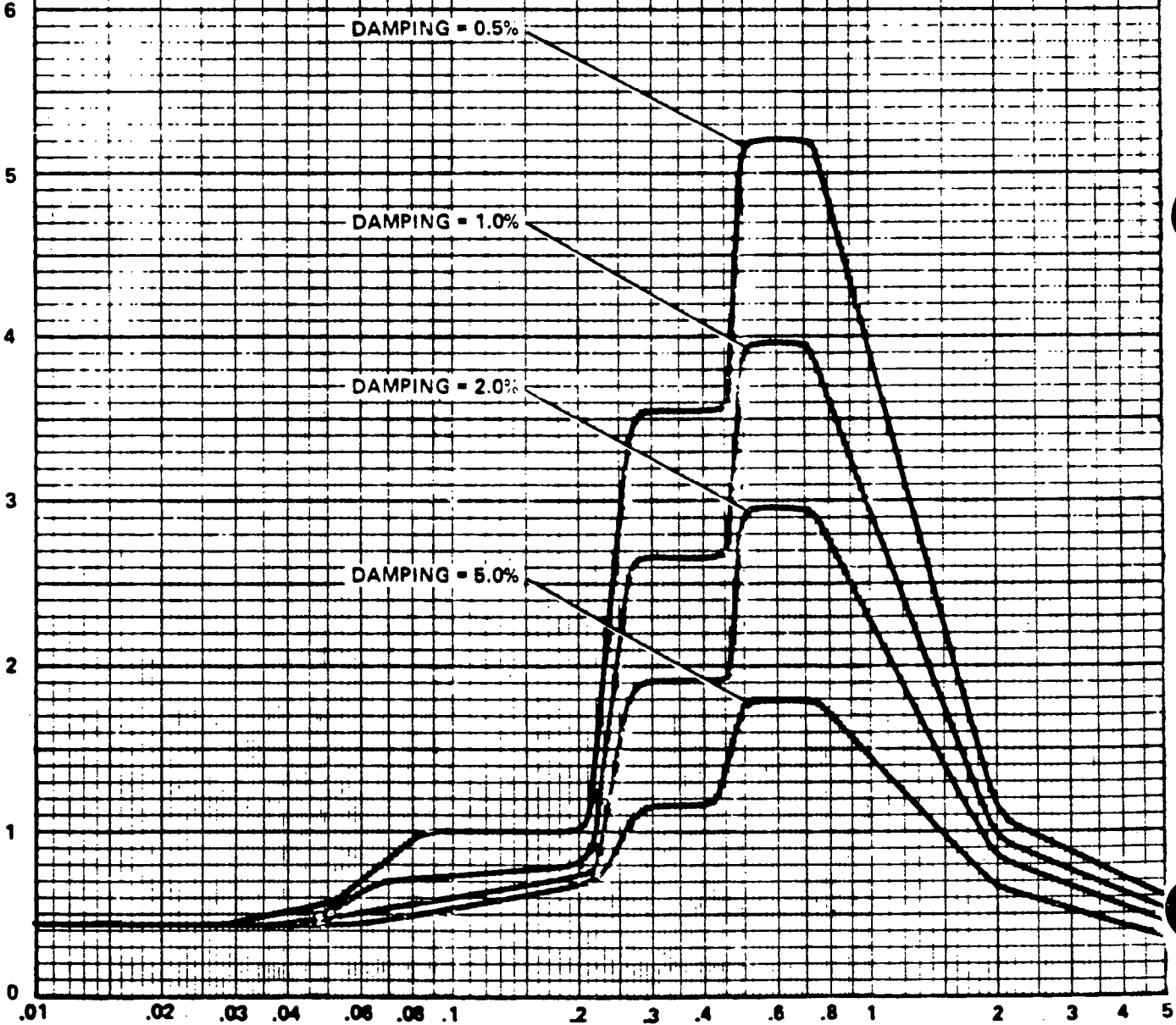
BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 HORIZONTAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE ELEVATION 30'-0"

Prepared By <i>JWA KMS</i>	Reviewed By <i>LGH JRE</i>	Approved By <i>WAB JRE</i>
JOB NO 1304-803	SKETCH NO S023-SK-S-652	RE <i>A</i>

ACCELERATION (g's)



PERIOD (seconds)

823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



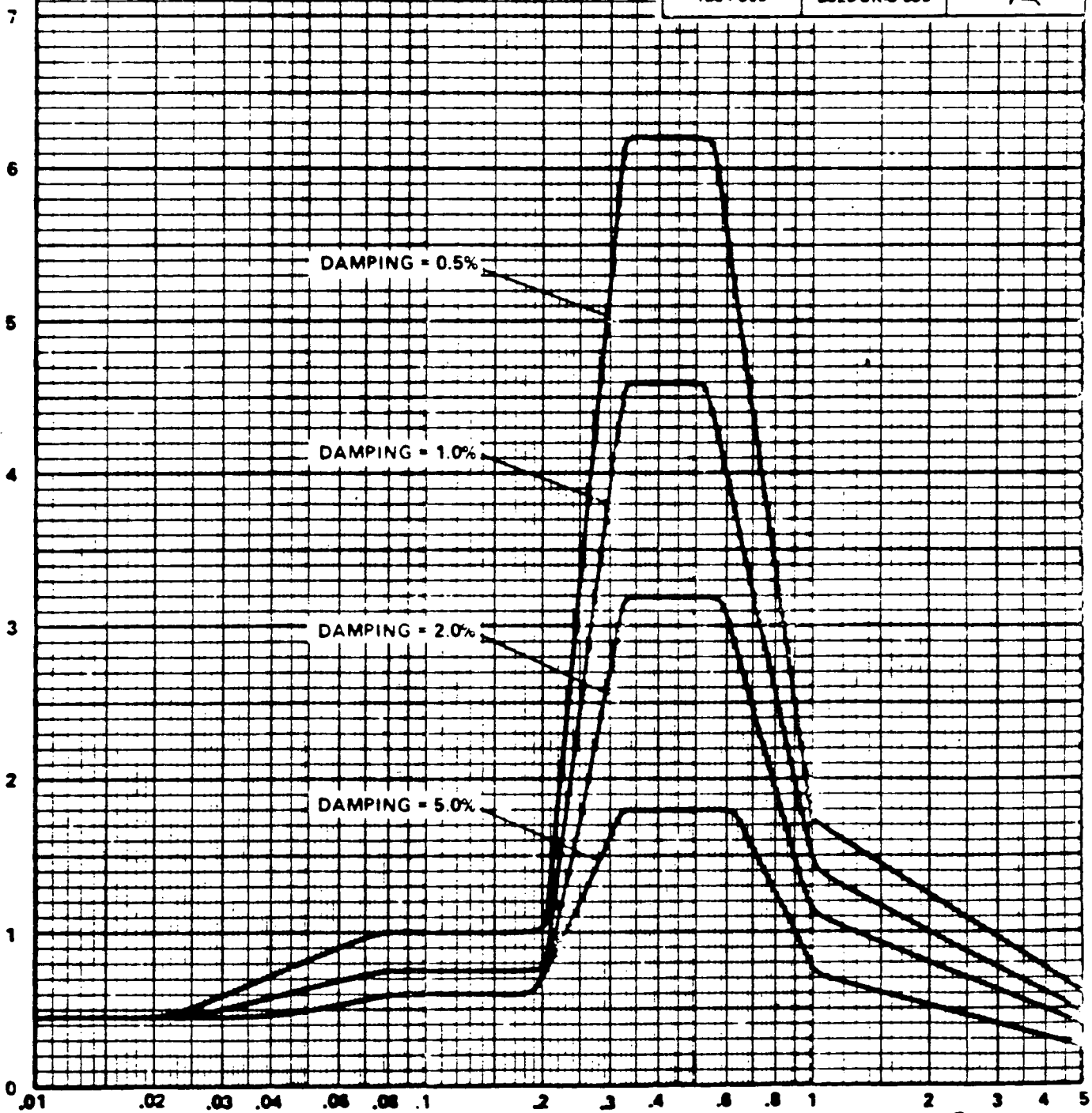
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 45'-0"

Prepared By JWW KMS	Reviewed By LGH QBS	Approved By WAB JF
JOB NO 1304-803	SKETCH NO. S023-SK-S-653	REV A

ACCELERATION (g 's)



8-23-73

PERIOD (seconds)

FREQUENCY (cycles per second):

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

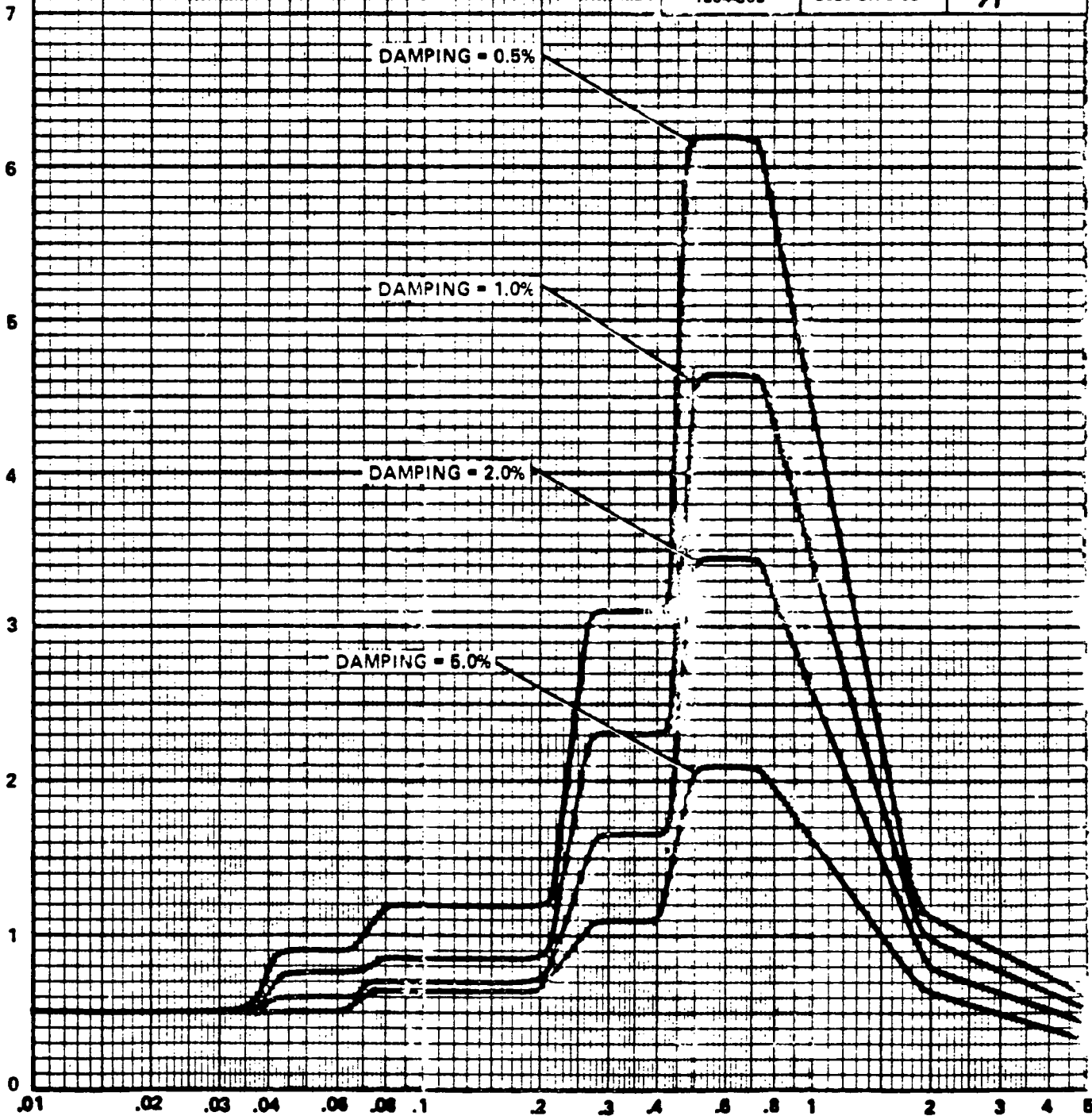
SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 45'-0"

Prepared By: JWW KMS	Reviewed By: LGN [Signature]	Approved By: WAB [Signature]
JOB NO 1304-803	SKETCH NO. S023-SK-S-654	REV. A

DAMPING VALUES
AS PERCENT OF CRITICAL

ACCELERATION (g's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 63'-6"

Prepared By

JWW KMS

Reviewed By

LGH *[Signature]*

Approved By

WAB *[Signature]*

JOB NO

1304-803

SKETCH NO.

S023-SK-S-655

REV

A

ACCELERATION (g's)

7

6

5

4

3

2

1

0

DAMPING = 0.5%

DAMPING = 1.0%

DAMPING = 2.0%

DAMPING = 5.0%

.01 .02 .03 .04 .05 .1 2 3 4 5

PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



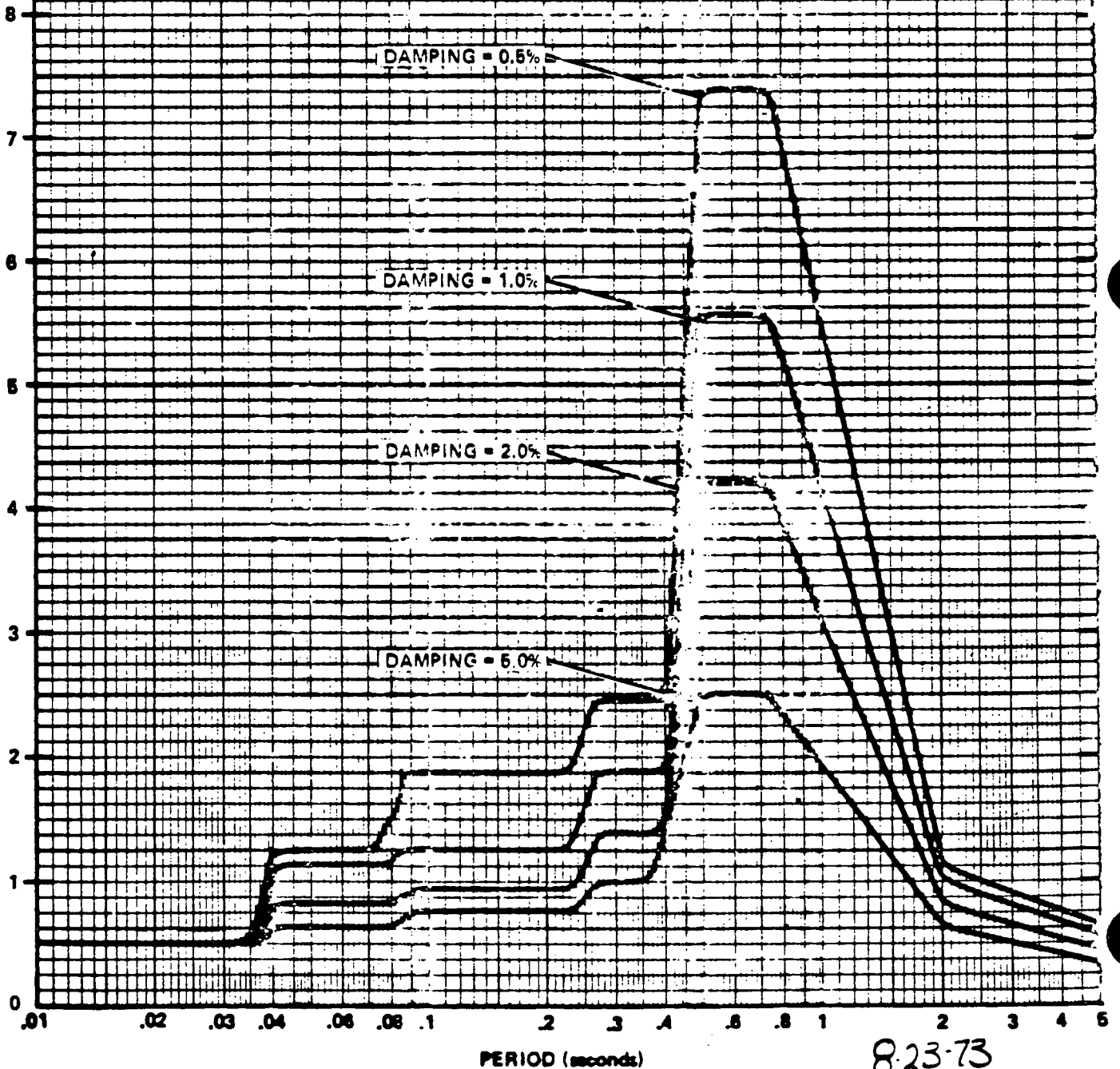
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 63'-6"

Prepared By JWW KMS	Reviewed By LGH QBS	Approved By WAB
JOB NO 1304-803	SKETCH NO. S023-SK-S-856	REV. A

ACCELERATION (g 's)




8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL

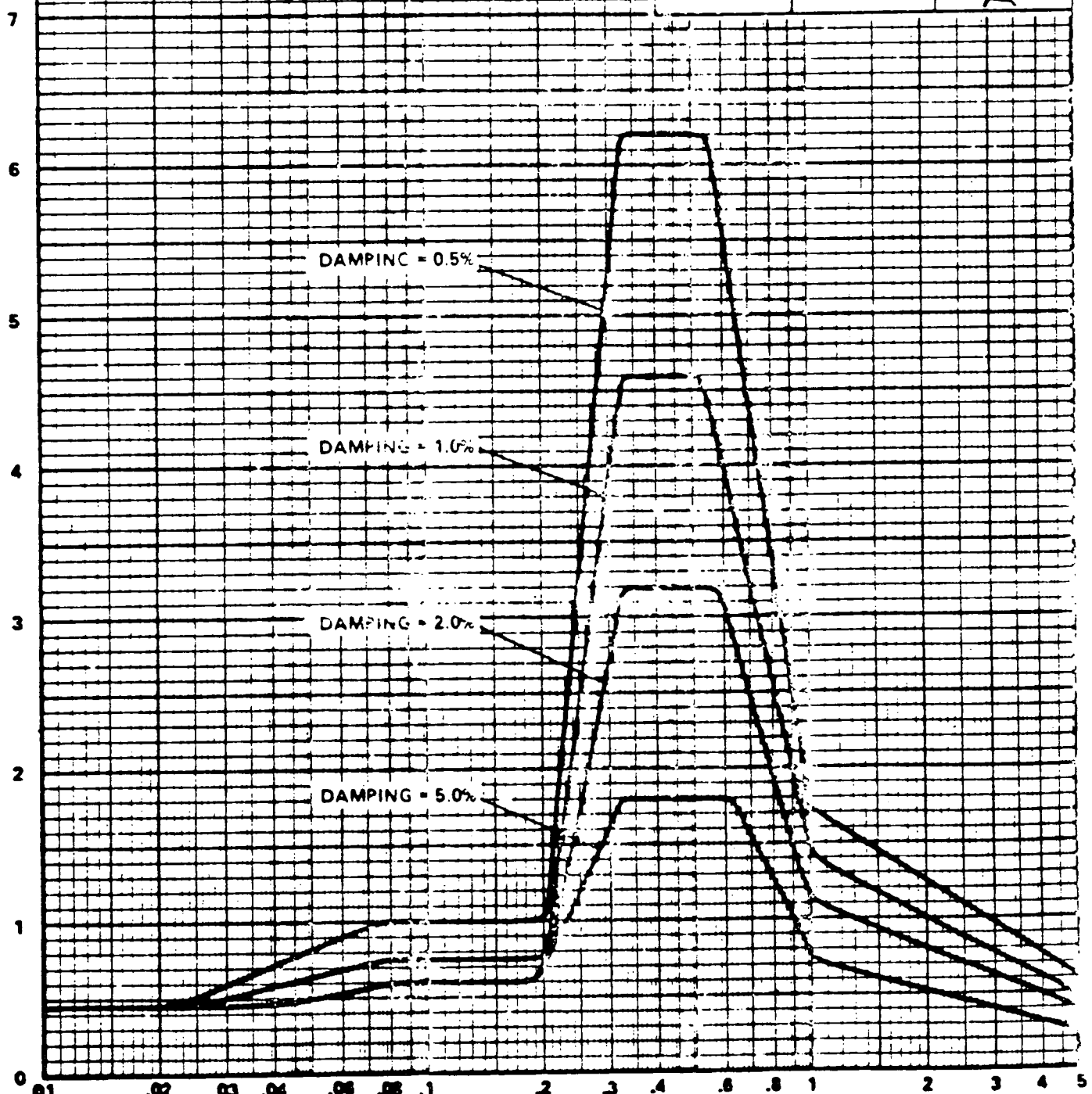

 BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 INTERIOR STRUCTURE ELEVATION 80'-6"

Prepared By <i>JWKMS</i>	Reviewed By <i>LGH QB</i>	Approved By <i>Ward</i>
JOB NO 134-803	SKETCH NO. S023-SK-S-657	REV A

ACCELERATION (g 's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



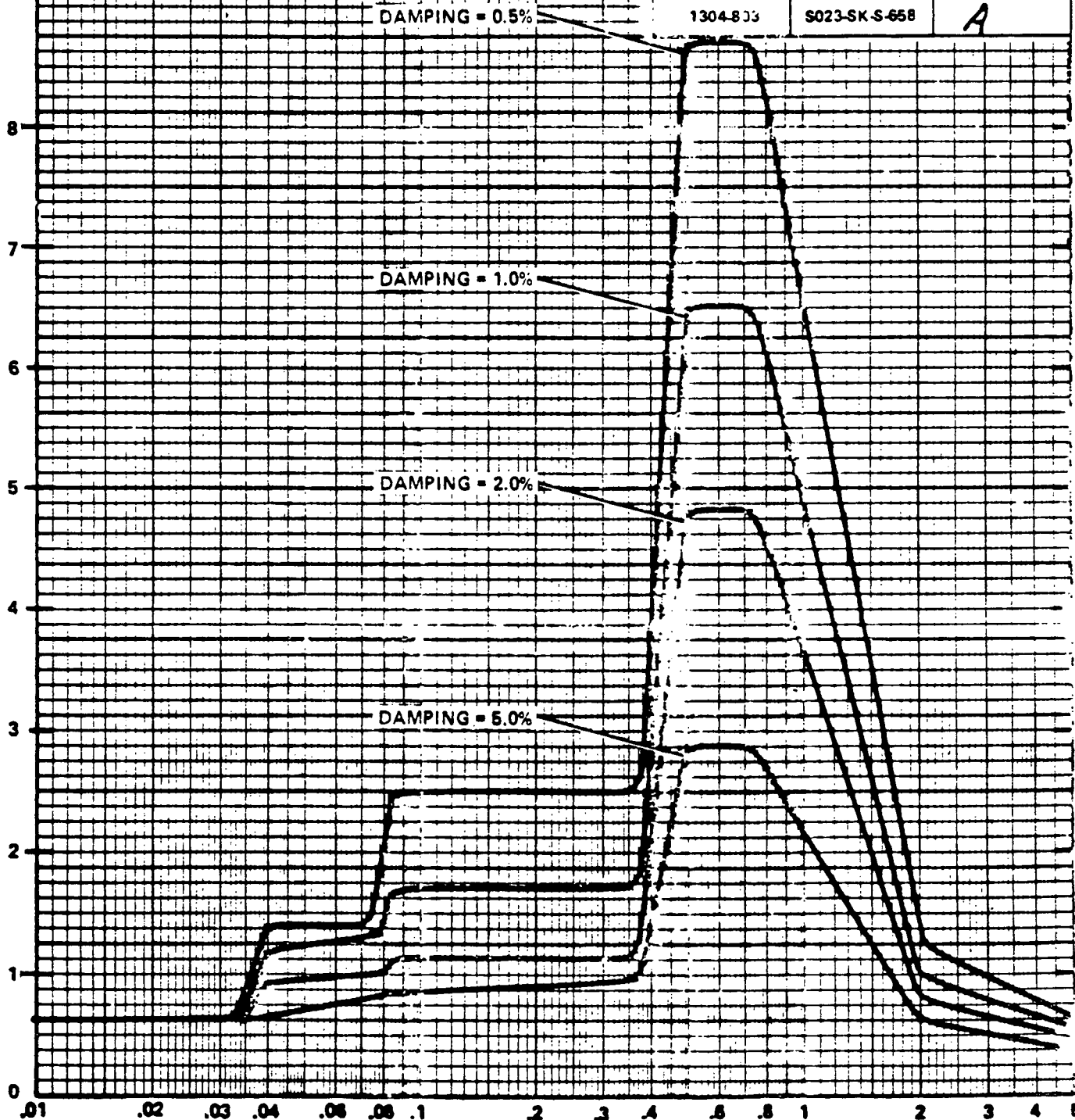
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
INTERIOR STRUCTURE ELEVATION 80'-6"

Prepared By JWS KMS	Reviewed By LGH UP	Approved By WAS WC
JOB NO 1304-833	SKETCH NO. S023-SK-S-658	REV A

ACCELERATION (g's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

.2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL BASEMAT

Prepared By

Reviewed By

Approved By

JWA KMS

LGH VLB

WAB SK

JOB NO

SKETCH NO.

REV

1304-803

8023-SK-S-659

A

ACCELERATION (g's)

7

6

5

4

3

2

1

0

DAMPING = 0.5%

DAMPING = 1.0%

DAMPING = 2.0%

DAMPING = 5.0%

.01

.02

.03

.04

.06

.1

2

3

4

.8

.8

1

2

3

4

5

PERIOD (seconds)

823-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



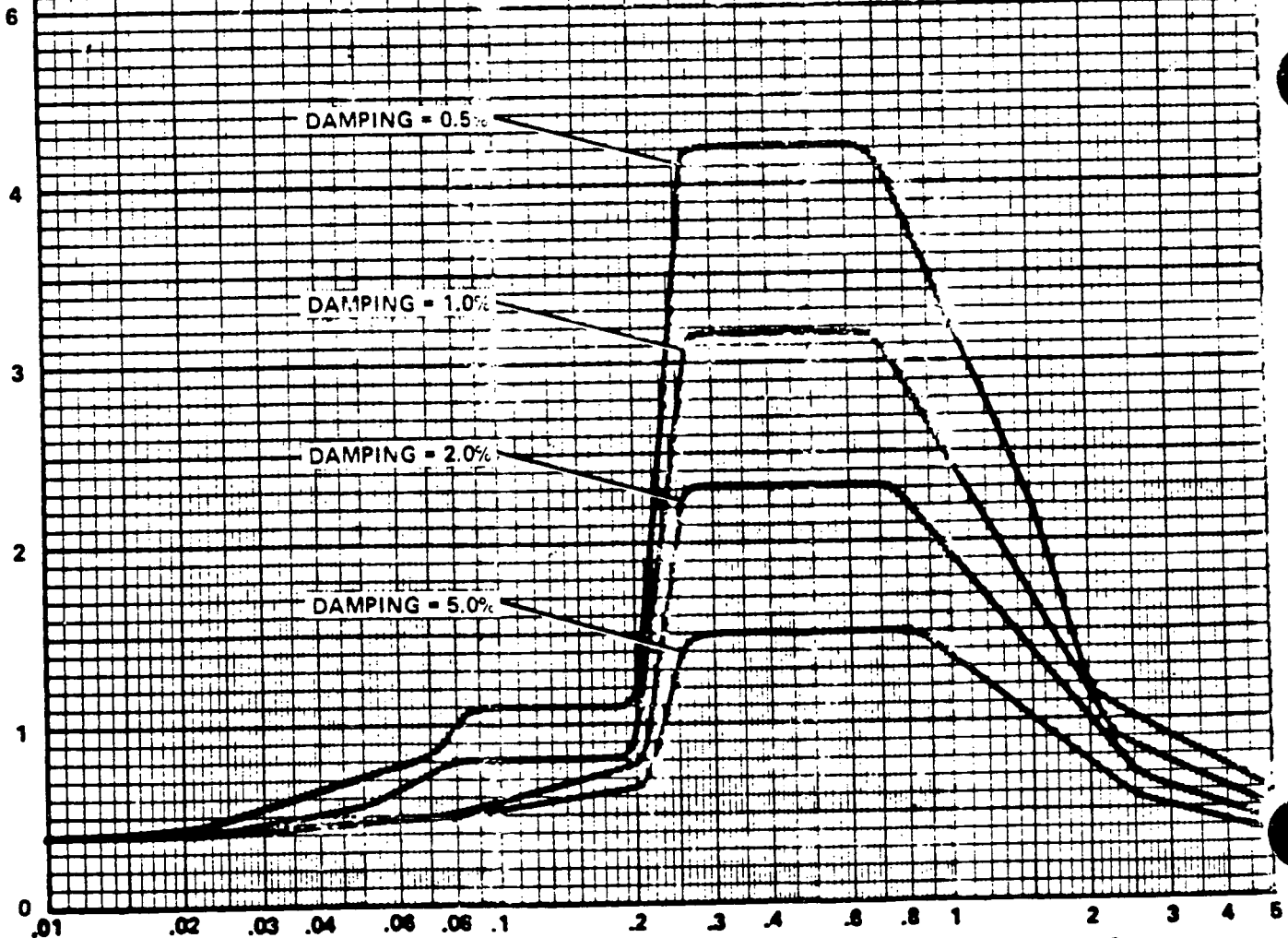
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL BASEMAT

Prepared By J.W. KMS	Reviewed By IGH QJB	Approved By WAB SKC
JOB NO 1304-803	SKETCH NO. S023-SK-S-660	REV A

ACCELERATION (g 's)



PERIOD (seconds)

8-23-73

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

2

$S_d = 10 T^2 S_a$
 S_d = DISPLACEMENT RESPONSE (INCHES)
 T = PERIOD (SEC.)
 S_a = ACCELERATION RESPONSE (g 's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

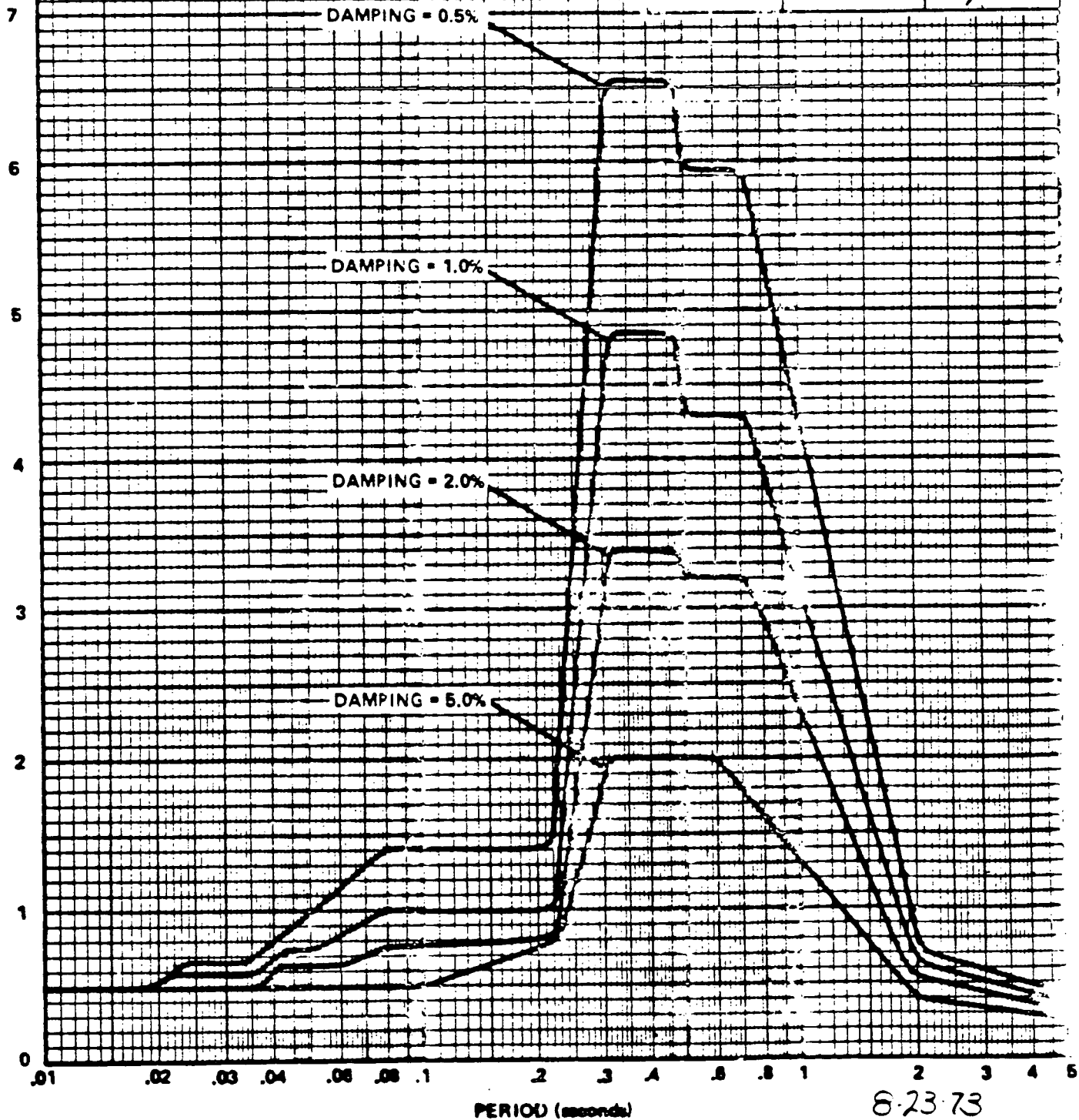
SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA FOR CONTAINMENT
 EXTERIOR SHELL ELEVATION 36'-0"

Prepared By <i>J.W. KMS</i>	Reviewed By <i>LGH JDB</i>	Approved By <i>WAB SRE</i>
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JOB NO 1304-803	SKETCH NO S023-SK-S-661	REV <i>L</i>
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ACCELERATION (g 's)



8-23-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC.)

S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

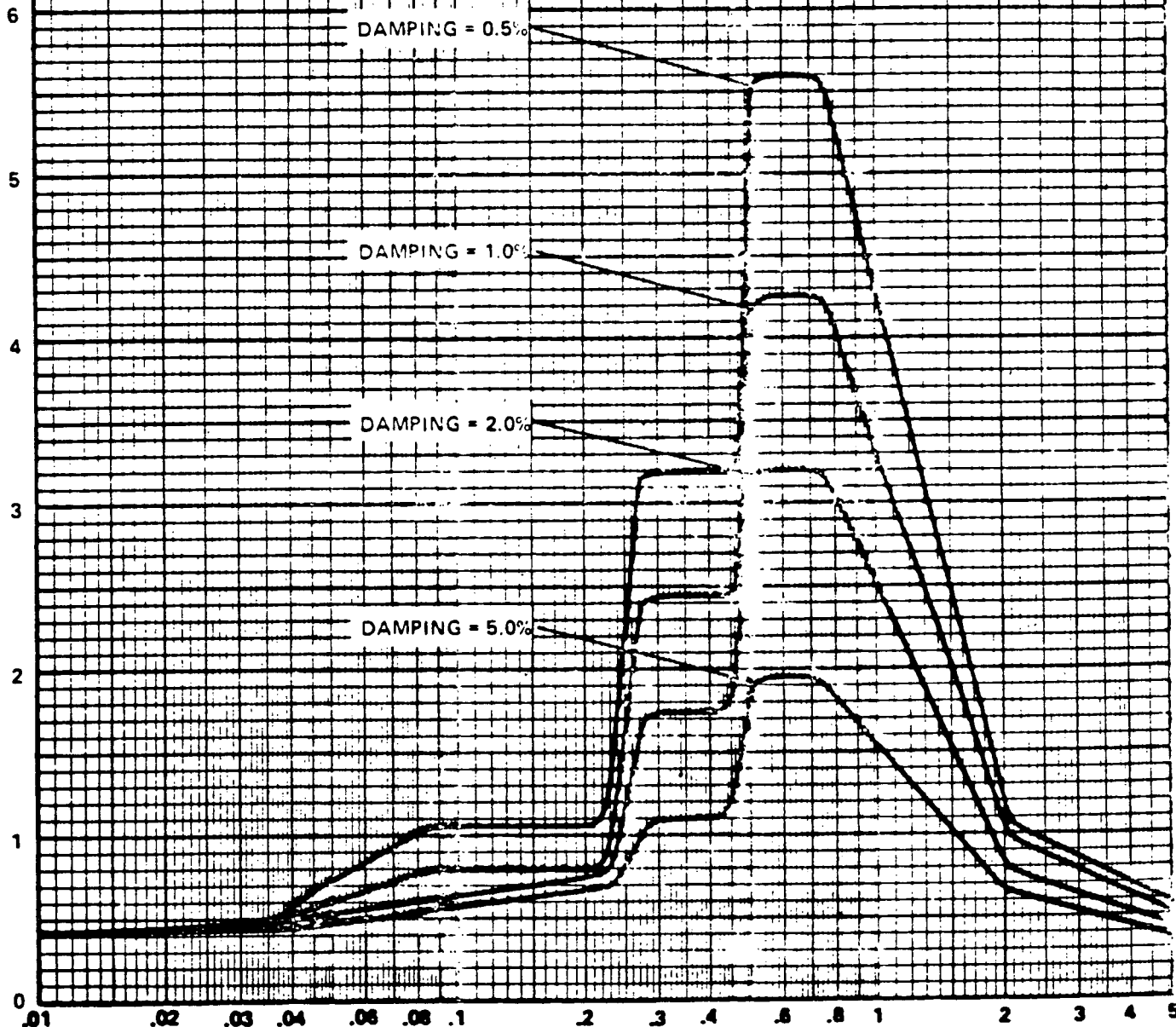
OPERATING BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA FOR CONTAINMENT
EXTERIOR SHELL ELEVATION 36'-0"

Prepared By Reviewed By Approved By

JWW KMS IGH DB WAB GRE

JOB NO SKETCH NO REV
1304-803 S023-SK-S-662 A

ACCELERATION (g's)



823-73

PERIOD (seconds)

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)

 DAMPING VALUES
 AS PERCENT OF CRITICAL

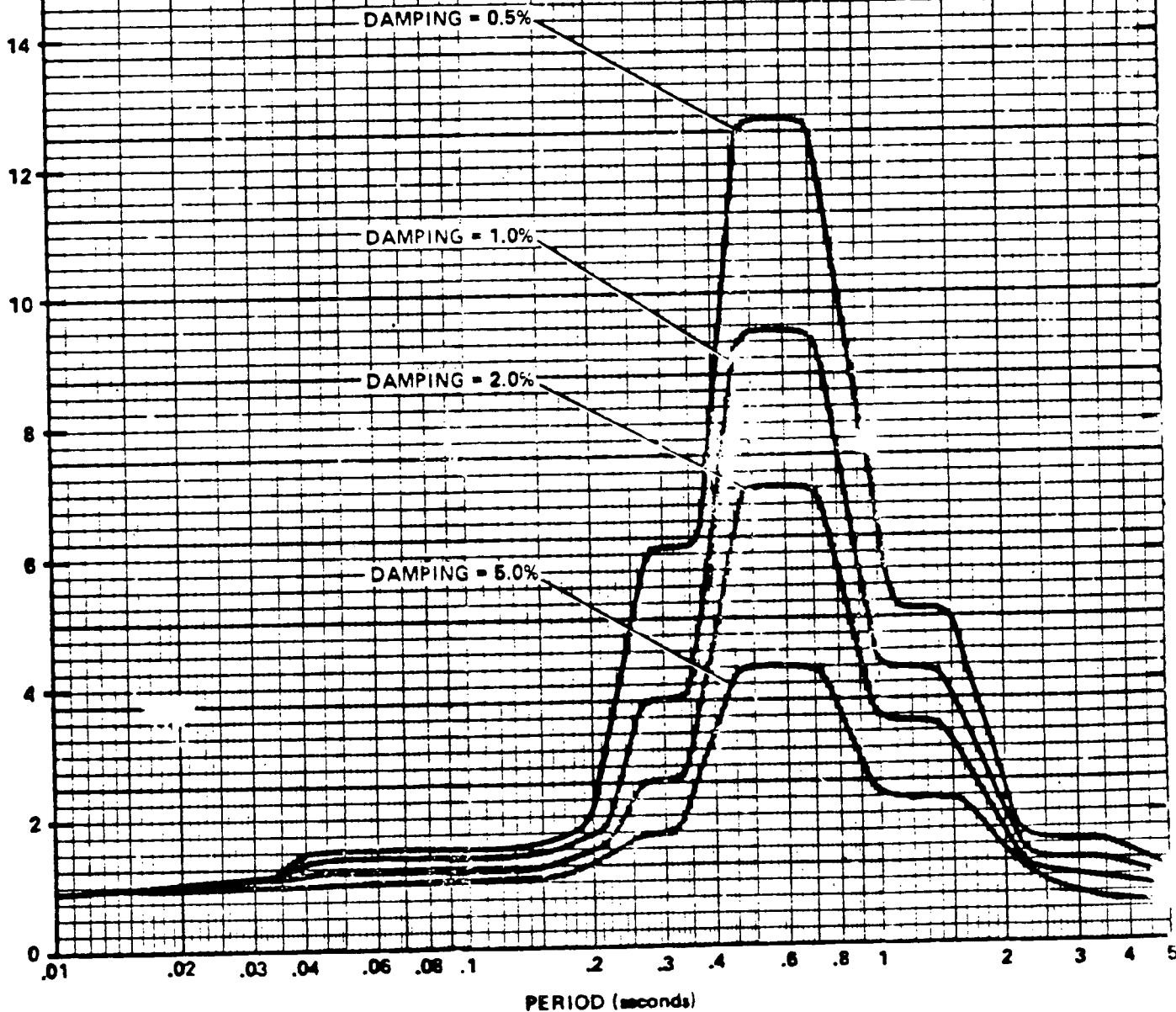

 BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 HORIZONTAL ACCELERATION RESPONSE
 SPECTRA AT NODE 1, ELEVATION 9'-0"
 OF AUXILIARY BUILDING

Prepared By AL	Reviewed By FLG <i>LGH</i>	Approved By WAB
JOB NO 1304-803	SKETCH NO S023-SK-S-689	REV A

ACCELERATION (g 's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d = DISPLACEMENT RESPONSE (INCHES)
 T = PERIOD (SEC.)
 S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



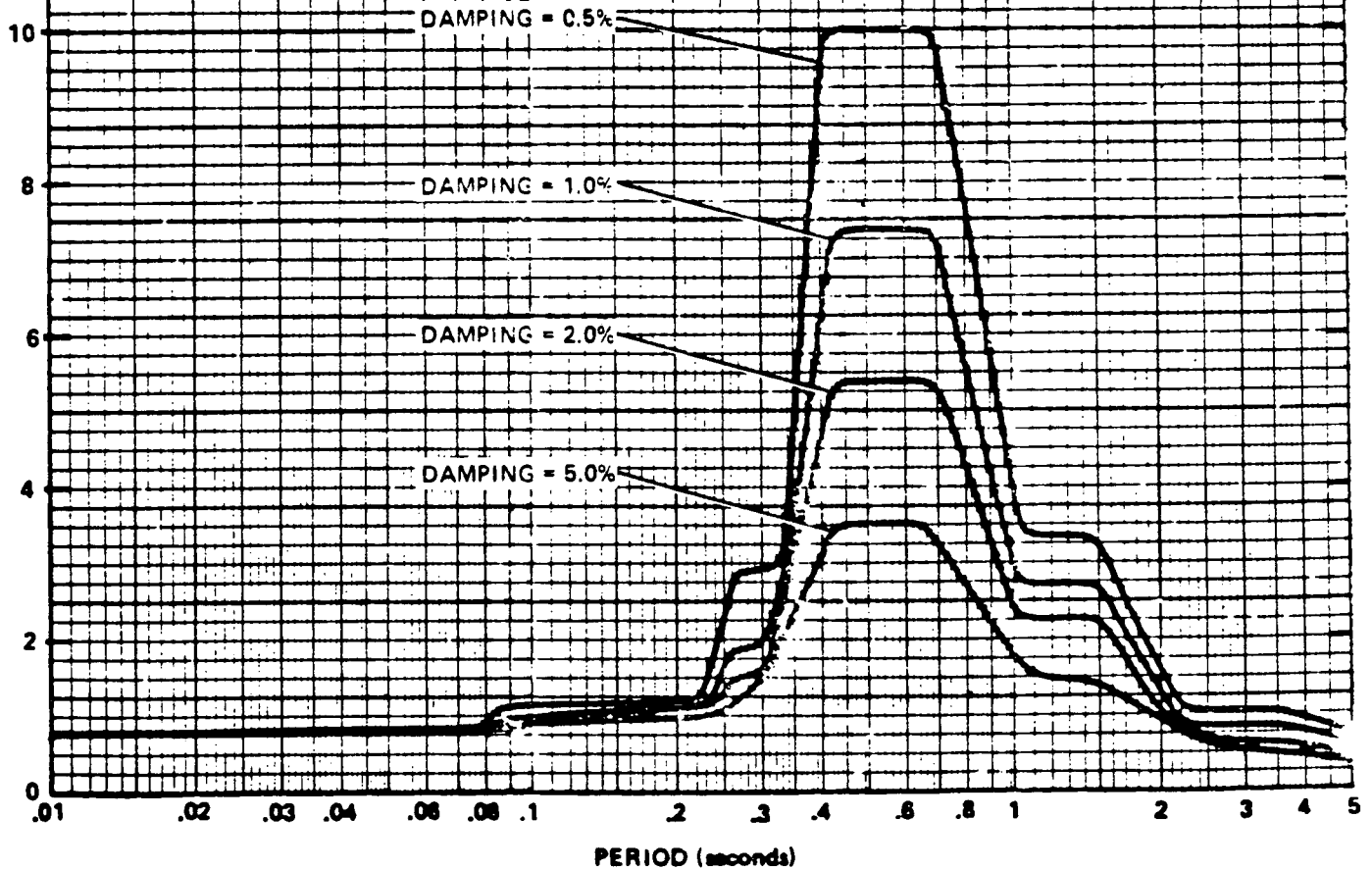
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA AT NODE 1, ELEVATION 9'-0"
OF AUXILIARY BUILDING

Prepared By AL	Reviewed By FLG LGH	Approved By WAB
JOB NO 1304-803	SKETCH NO. S023-SK-S-690	REV. A

ACCELERATION (g's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$

S_d = DISPLACEMENT RESPONSE (INCHES)

T = PERIOD (SEC)

S_a = ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



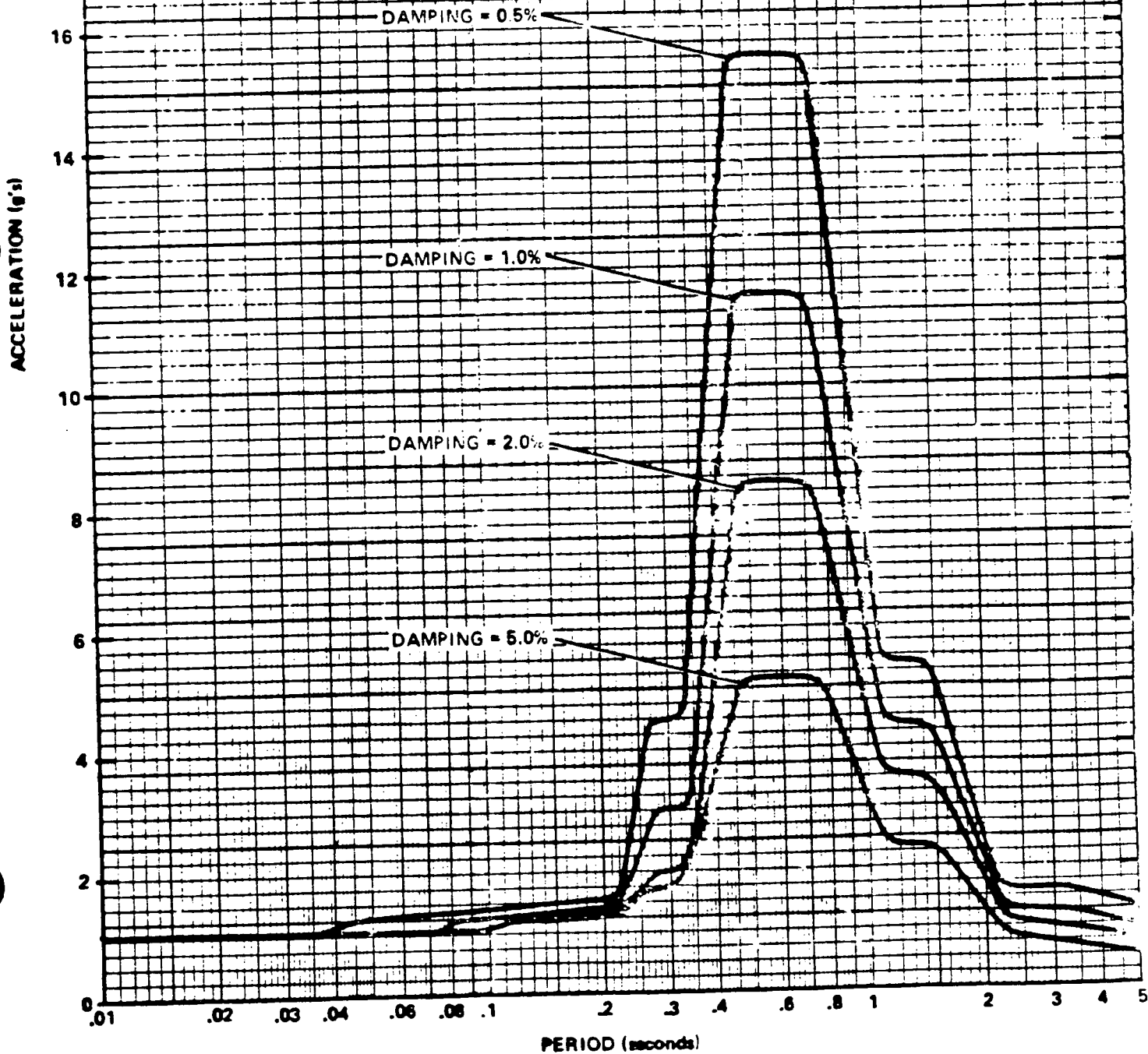
BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
HORIZONTAL ACCELERATION RESPONSE
SPECTRA AT NODE 3 OR 4, ELEVATION 30'-0"
OF AUXILIARY BUILDING

Prepared By AL	Reviewed By FLG LGH SDB	Approved By WJW
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JOE NO 1304-803	SKETCH NO S023-SK-S-693	REV. A 7/24/63
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FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d = DISPLACEMENT RESPONSE (INCHES)
 T = PERIOD (SEC.)
 S_a = ACCELERATION RESPONSE (g's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



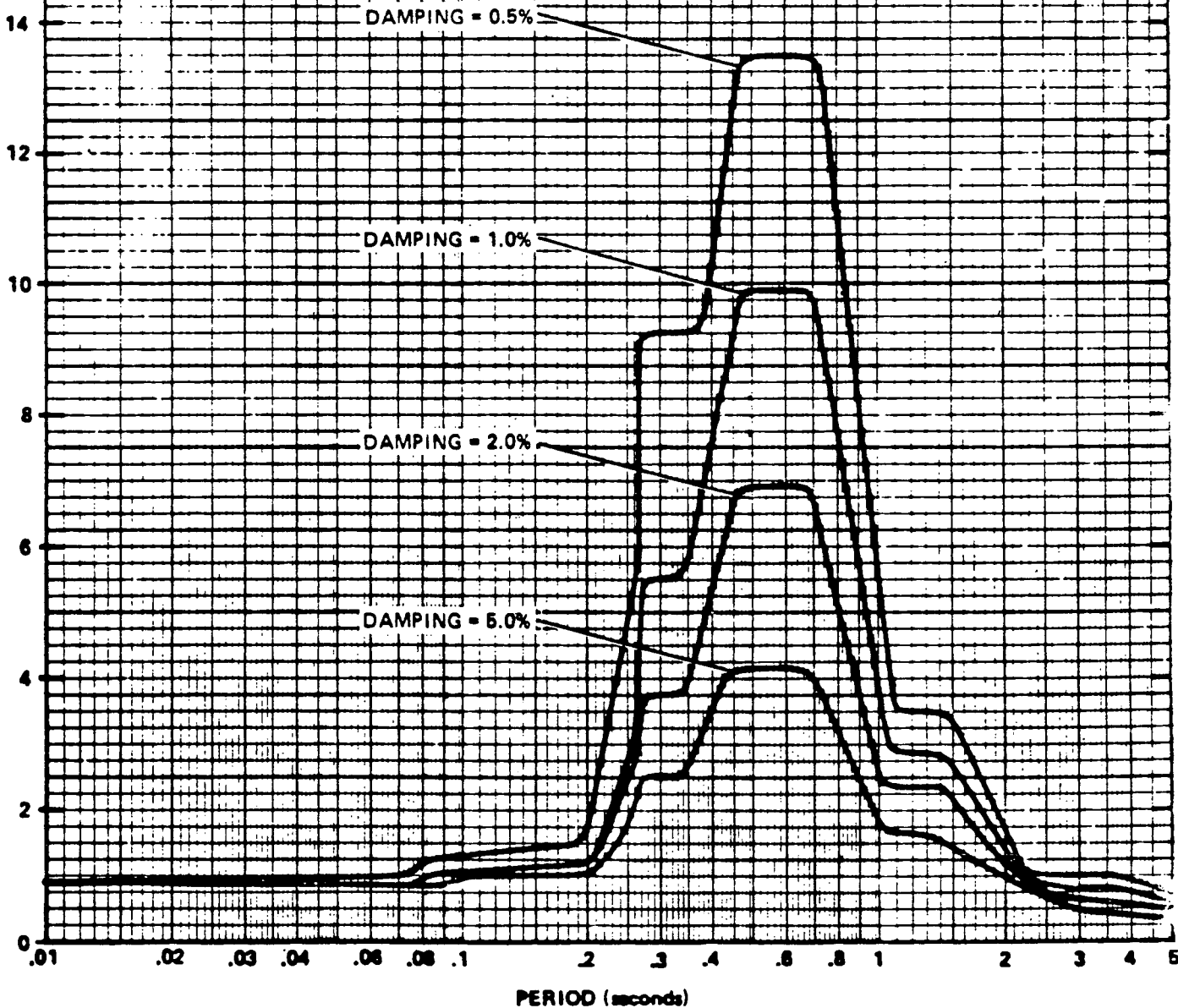
BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA AT NODE 3 OR 4, ELEVATION 30'-0"
 OF AUXILIARY BUILDING

Prepared By AL	Reviewed By FLG LCH JAB	Approved By WAB
JOB NO 1304-803	SKETCH NO S023-SK-S-694	REL. A 7/23/73

ACCELERATION (g's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
 AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

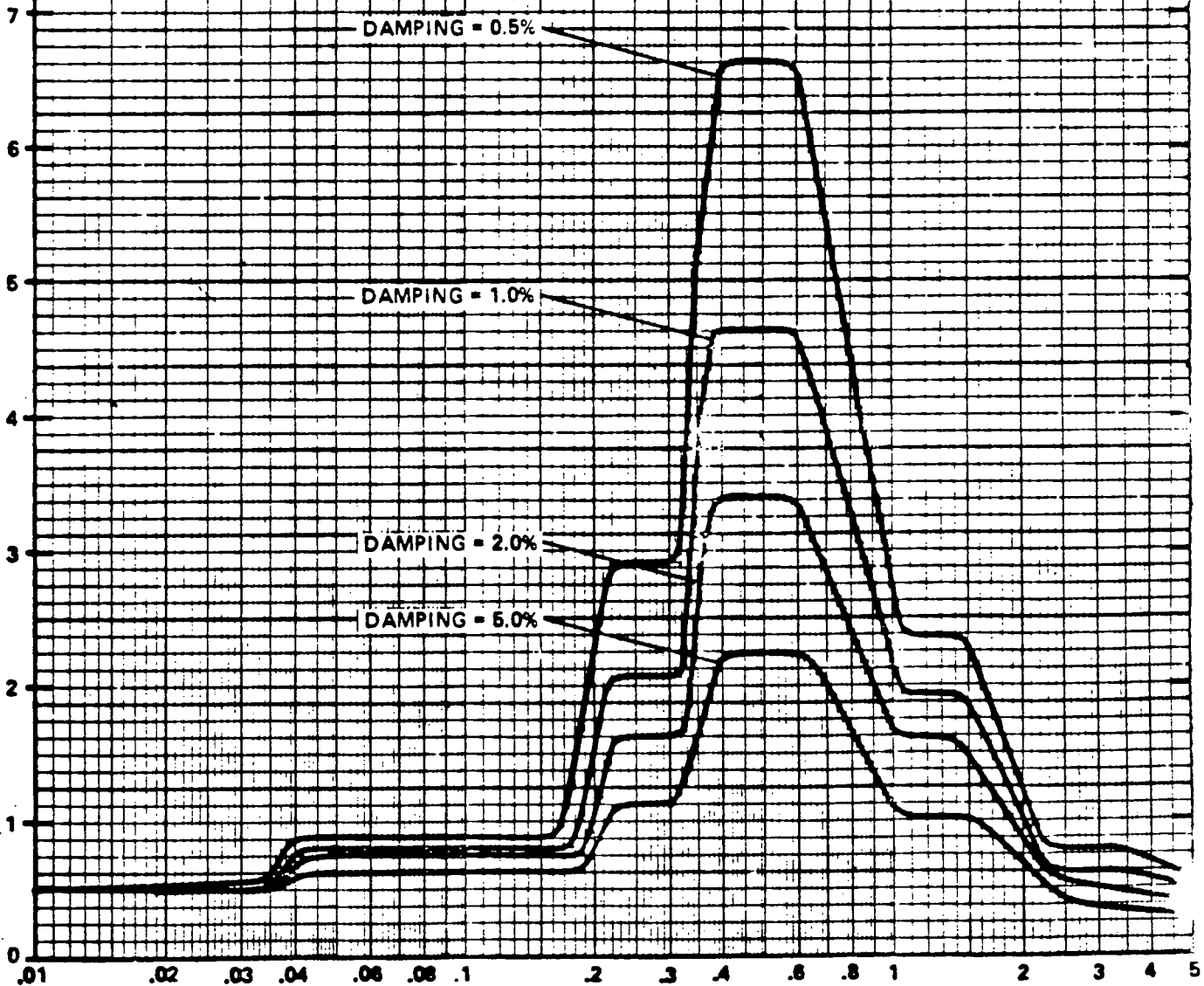
SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
 HORIZONTAL ACCELERATION RESPONSE
 SPECTRA AT NODE 1, ELEVATION 9' 0"
 OF AUXILIARY BUILDING

Prepared By AL	Reviewed By FLG LGH	Approved By WAB
-------------------	------------------------	--------------------

JOB NO 1304-803	SKETCH NO. 8023-SK-S-713	REV A
--------------------	-----------------------------	----------

ACCELERATION (g 's)



PERIOD (seconds)

7-24-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g 's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

OPERATING BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA AT NODE 1, ELEVATION 9'-0"
OF AUXILIARY BUILDING

Prepared By

AL

Reviewed By

FLG LGH QB

Approved By

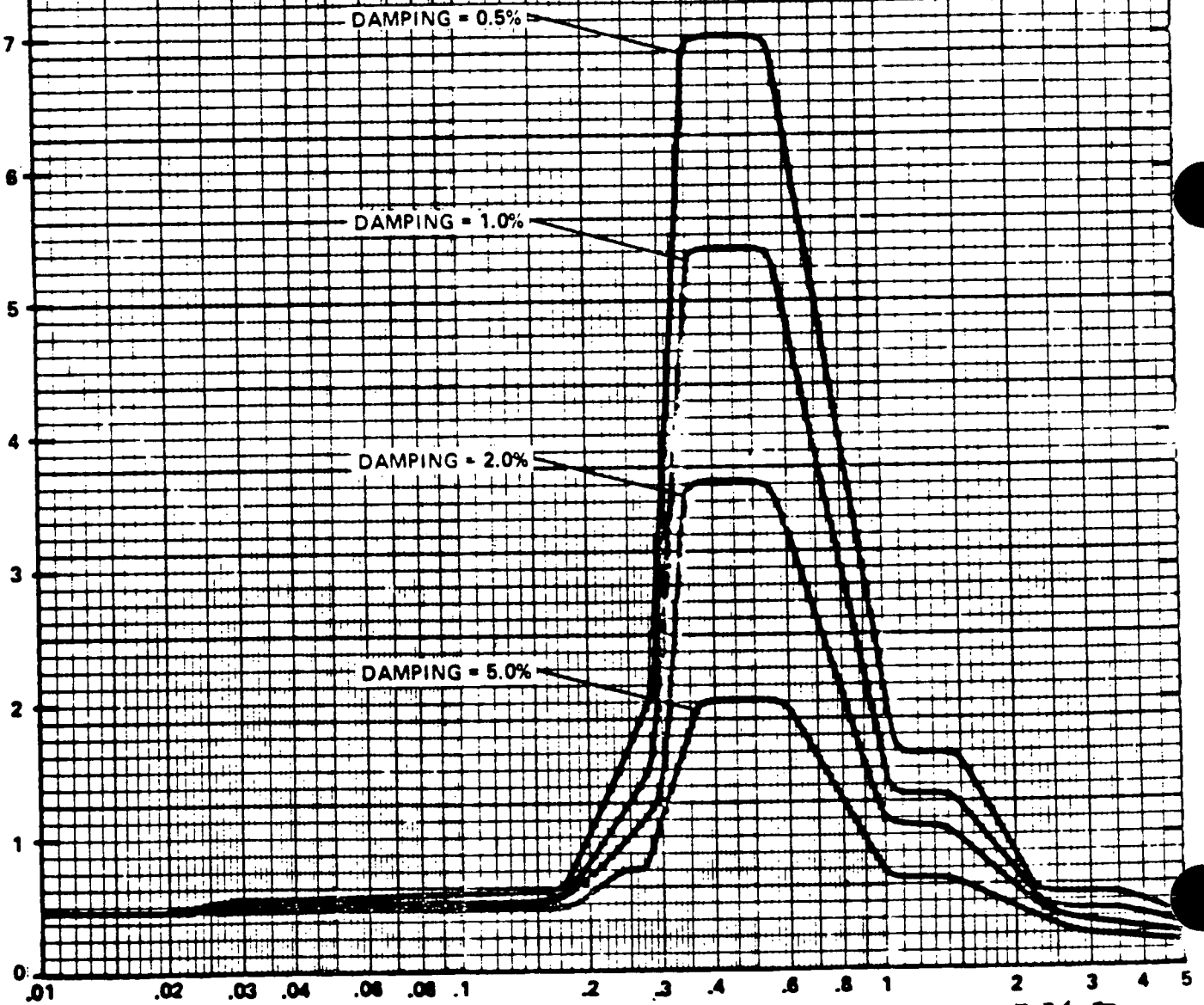
WAB

JOB NO
1304-803

SKETCH NO.
S023-SK-S-714

REV
A

ACCELERATION (g 's)



PERIOD (seconds)

7-24-73

FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g 's)
DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION,
LOS ANGELES DIVISION

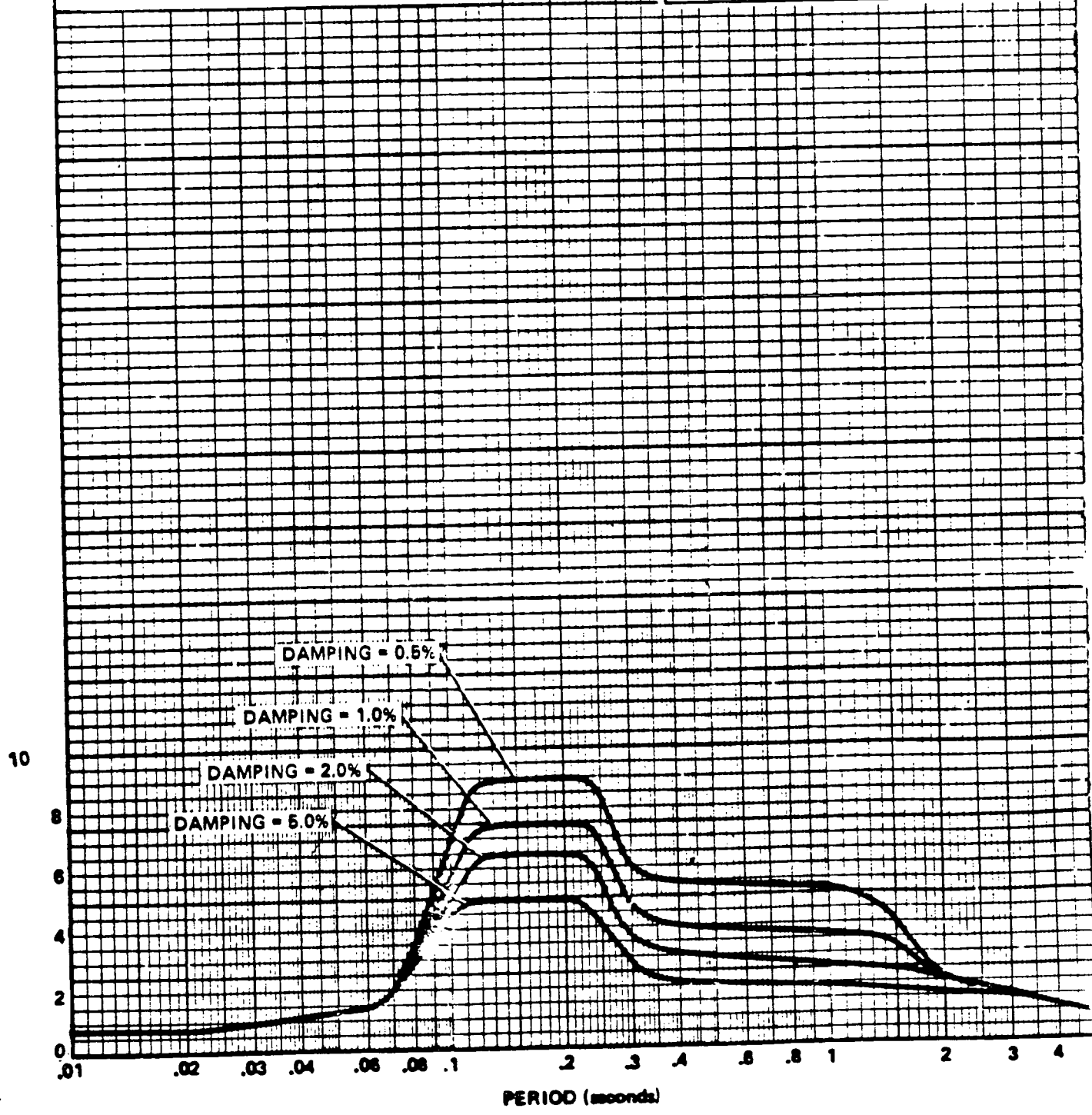
SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
E-W HORIZONTAL ACCELERATION RESPONSE
SPECTRA AT ELEV (-) 15'-6" OF
SAFETY EQUIPMENT BUILDING
(SAFETY INJECTION AREA)

TO OBTAIN OPERATING BASIS
EARTHQUAKE RESPONSE ACCELERATION,
MULTIPLY BY 0.55

Prepared By <i>JDC</i>	Reviewed By <i>W.H. KH</i>	Approved By <i>NE</i>
JOB NO 10079-003	SKETCH NO. S023-SK-S-927	REV B 12/31/75

ACCELERATION (g 's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
 AS PERCENT OF CRITICAL

TO OBTAIN OPERATING BASIS
 EARTHQUAKE RESPONSE ACCELERATION,
 MULTIPLY BY 0.55



BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 E-W HORIZONTAL ACCELERATION RESPONSE
 SPECTRA AT ELEV (-) 5'-3" OF
 SAFETY EQUIPMENT BUILDING
 (COMPONENT COOLING AREA)

Prepared By

JOK

Reviewed By

KHJ LGH

Approved By

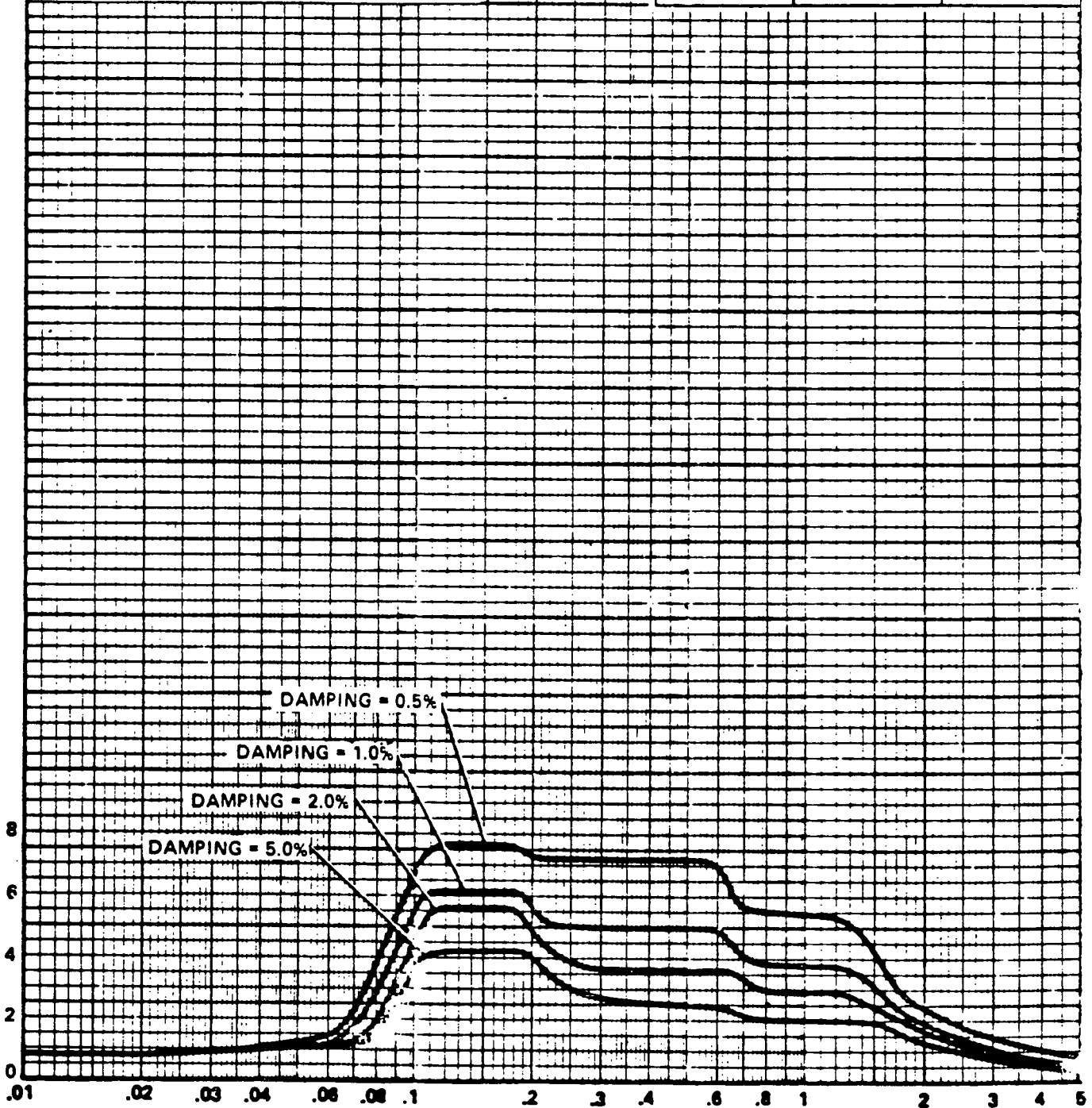
WJG

JOB NO
 10079-003

SKETCH NO.
 S023-SK-S-928

REV
 B 4-3-75

ACCELERATION (g's)



PERIOD (seconds)

FREQUENCY (cycles per second)

100

50

25

10

5

2

1

.5

2

$S_d = 10 T^2 S_a$

S_d - DISPLACEMENT RESPONSE (INCHES)

T - PERIOD (SEC.)

S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
N-S HORIZONTAL ACCELERATION RESPONSE
SPECTRA AT ELEV (-) 15'-6" OF
SAFETY EQUIPMENT BUILDING
(SAFETY INJECTION AREA)

Prepared By

BPIC

Reviewed By

RMD IGH

Approved By

WGO

JOB NO

10079-003

SKETCH NO.

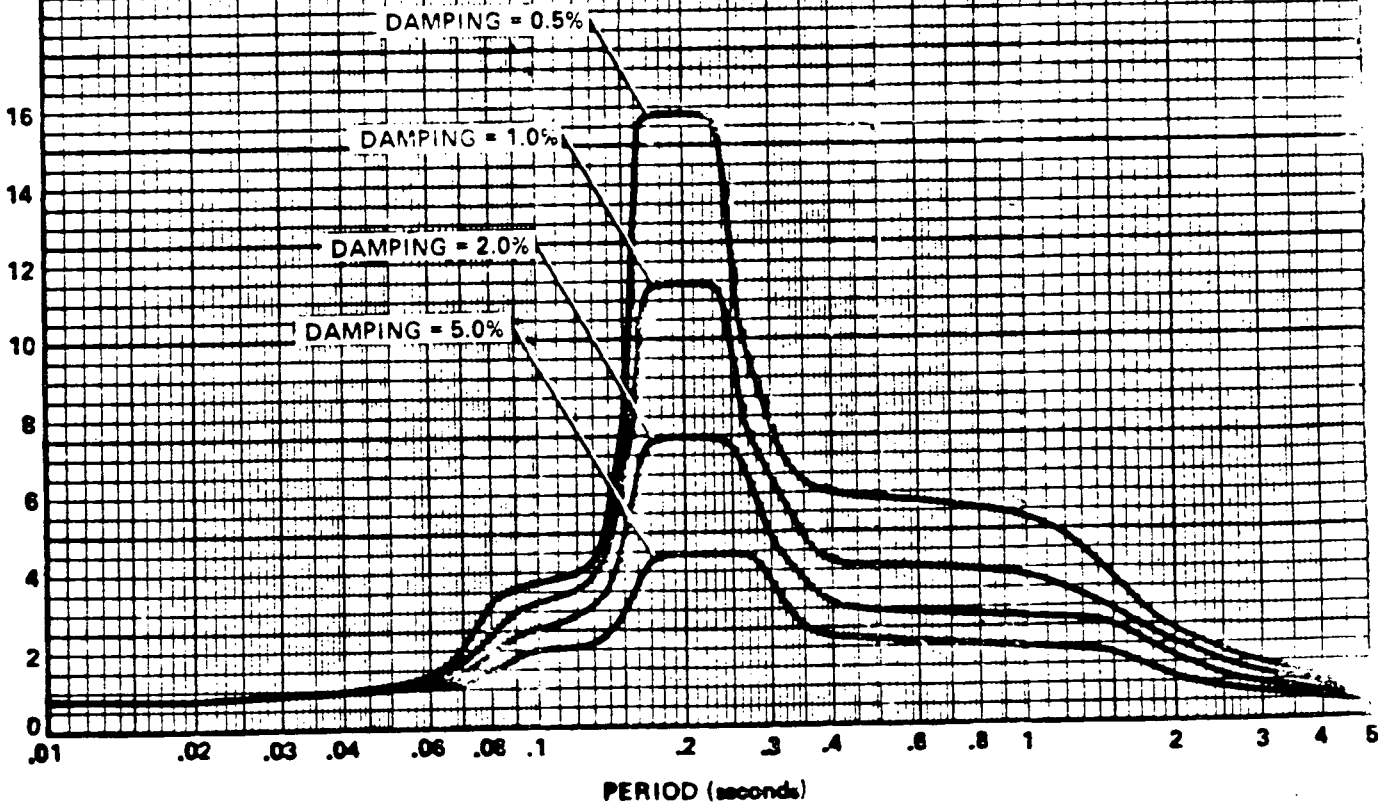
S023-SK-S-932

REV

B 6/3/75

TO OBTAIN OPERATING BASIS
EARTHQUAKE RESPONSE ACCELERATION,
MULTIPLY BY 0.55

ACCELERATION (g)



FREQUENCY (cycles per second):

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)
**DAMPING VALUES
 AS PERCENT OF CRITICAL**


BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

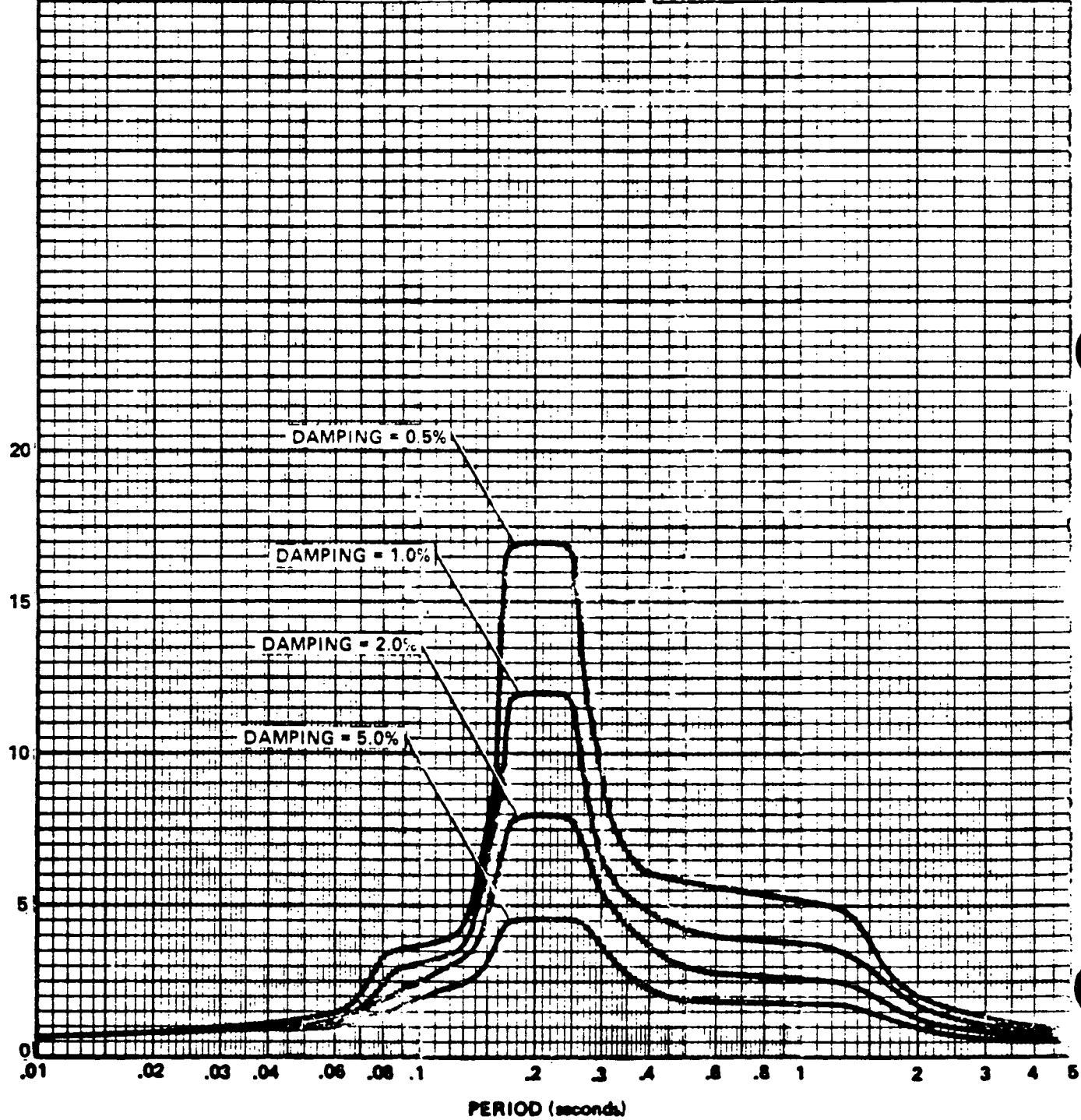
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 SAN ONOFRE NUCLEAR GENERATING STATION
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DESIGN BASIS EARTHQUAKE
 N-S HORIZONTAL ACCELERATION RESPONSE
 SPECTRA AT ELEV (-) 5'-3" OF
 SAFETY EQUIPMENT BUILDING
 (COMPONENT COOLING AREA)

TO OBTAIN OPERATING BASIS
 EARTHQUAKE RESPONSE ACCELERATION,
 MULTIPLY BY 0.55

Prepared By	Reviewed By	Approved By
<i>JPC</i>	<i>RAd LSH</i>	<i>WJG</i>
JOB NO 10079-003	SKETCH NO. S023-SK-S-933	REV B 12-31-75

ACCELERATION (g's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)



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SOUTHERN CALIFORNIA EDISON COMPANY
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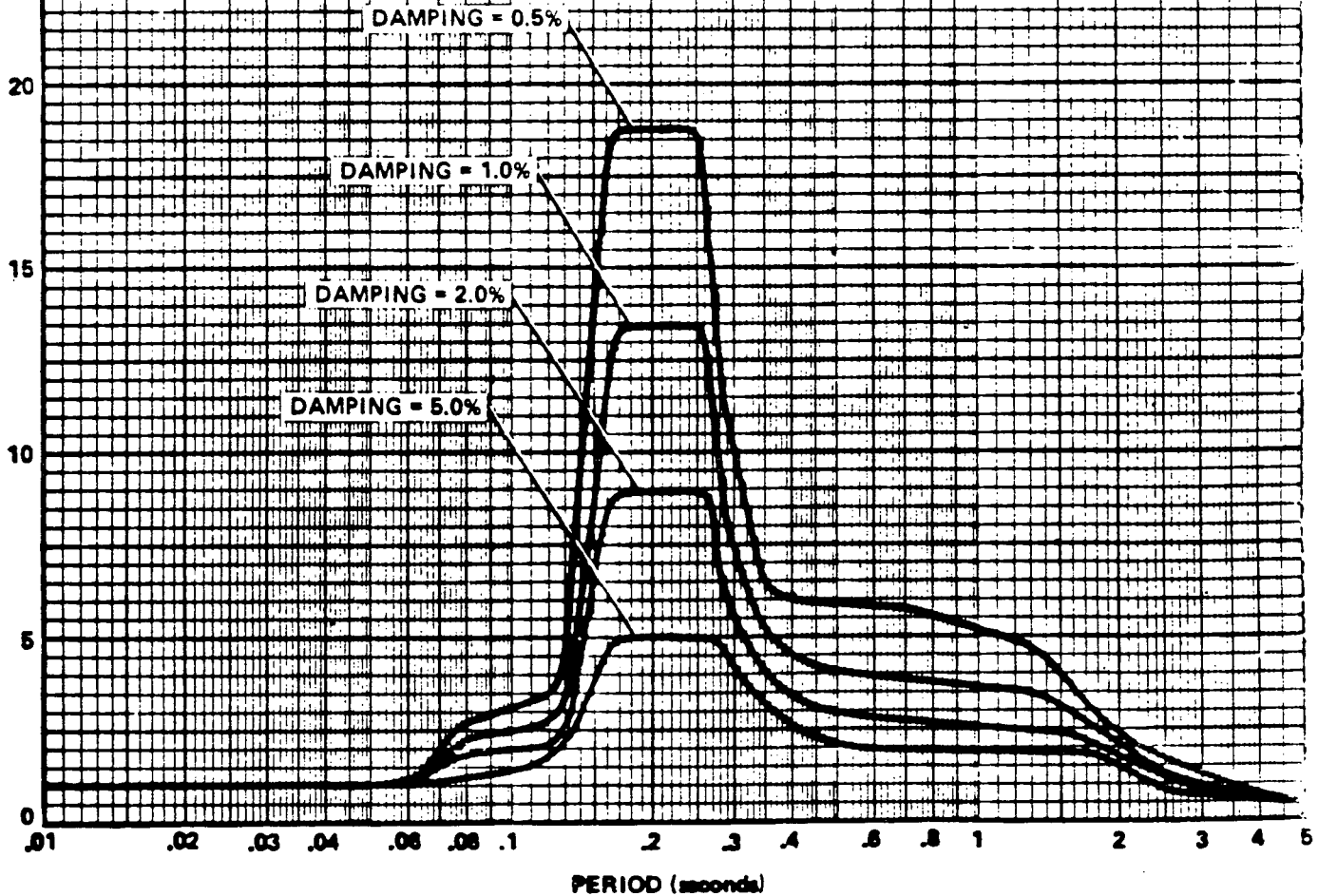
DAMPING VALUES
 AS PERCENT OF CRITICAL

DESIGN BASIS EARTHQUAKE
 N-S HORIZONTAL ACCELERATION RESPONSE
 SPECTRA AT ELEV (+) 8'-0" OF
 SAFETY EQUIPMENT BUILDING

TO OBTAIN OPERATING BASIS
 EARTHQUAKE RESPONSE ACCELERATION,
 MULTIPLY BY 0.55

Prepared By: <i>JMC</i>	Reviewed By: <i>KMD AGH</i>	Approved By: <i>AG</i>
JOB NO 10079-003	SKETCH NO. S023-SK-S-934	REV B 4-23-75

ACCELERATION (g)



$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL

TO OBTAIN OPERATING BASIS
EARTHQUAKE RESPONSE ACCELERATION,
MULTIPLY BY 0.60



BECHTEL POWER CORPORATION
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION RESPONSE
SPECTRA AT ELEV (-) 15'-6" OF
SAFETY EQUIPMENT BUILDING
(SAFETY INJECTION AREA)

Prepared By

EDIC

Reviewed By

Rhd KGH

Approved By

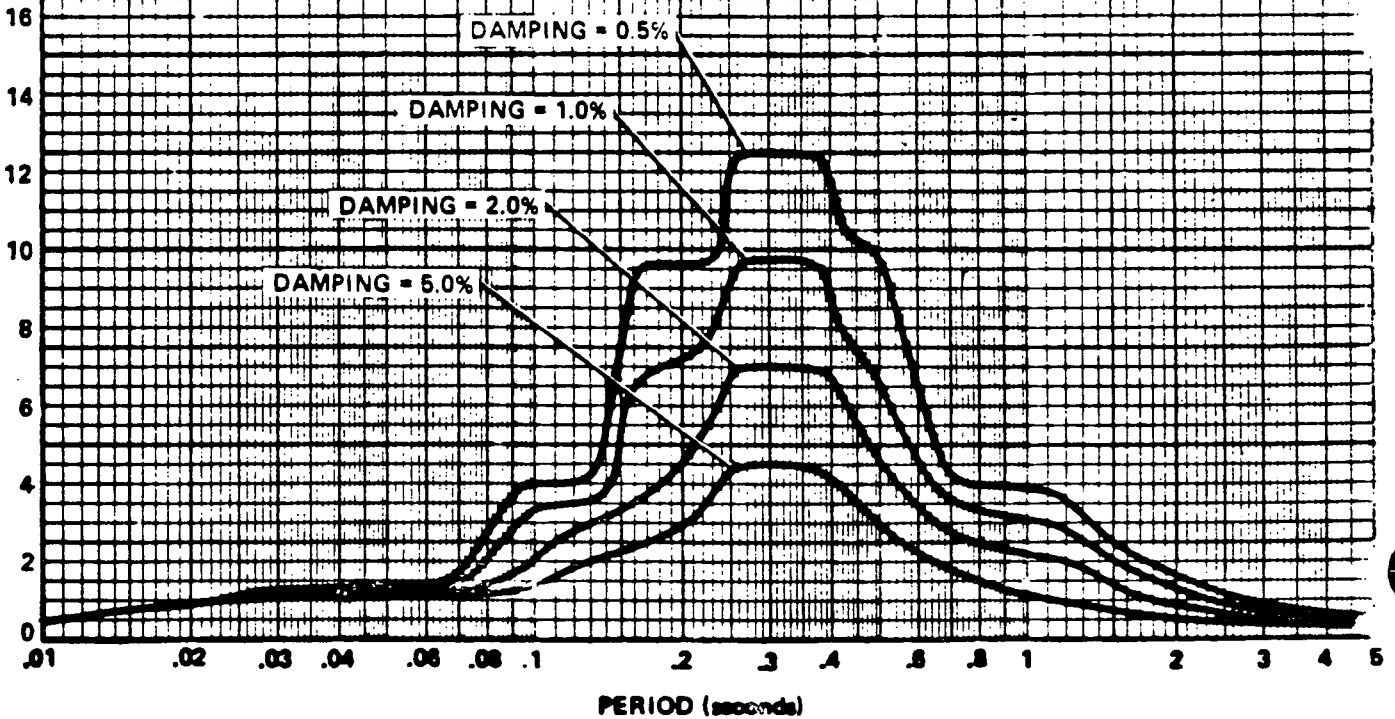
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JOB NO
10079-003

SKETCH NO.
S023-SK-S-937

REV
B 12-31-75


ACCELERATION (g's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 .2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
 T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)
 DAMPING VALUES
 AS PERCENT OF CRITICAL

 BECHTEL POWER CORPORATION
 LOS ANGELES DIVISION

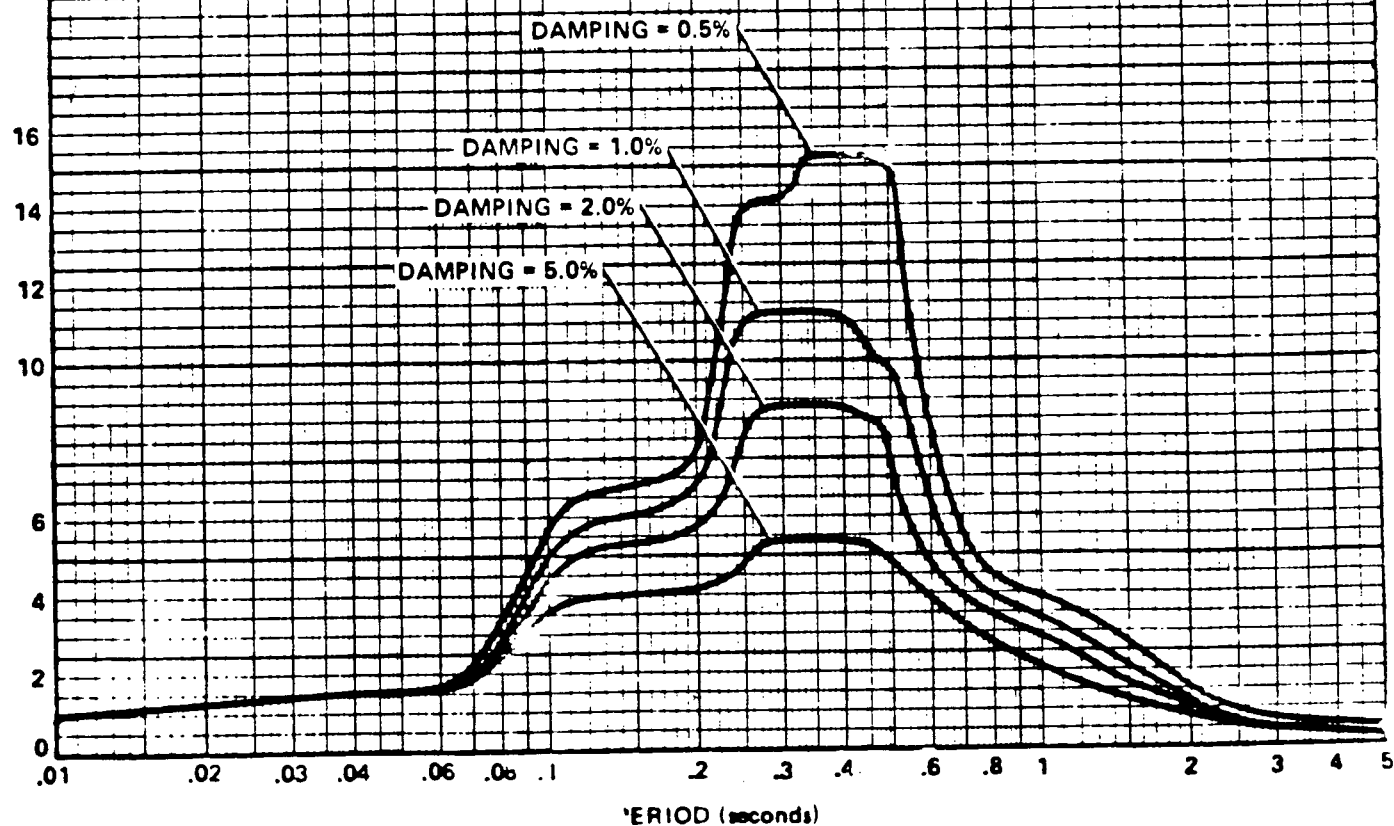
SOUTHERN CALIFORNIA EDISON COMPANY
 SAN ONOFRE NUCLEAR GENERATING STATION
 UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
 VERTICAL ACCELERATION RESPONSE
 SPECTRA AT ELEV (-) 5'-3" OF
 SAFETY EQUIPMENT BUILDING
 (COMPONENT COOLING AREA)

TO OBTAIN OPERATING BASIS
 EARTHQUAKE RESPONSE ACCELERATION,
 MULTIPLY BY 0.60

Prepared By <i>APIC</i>	Reviewed By <i>2/2nd LGH</i>	Approved By <i>[Signature]</i>
JOB NO 10079-003	SKETCH NO. S023-SK-S-938	REV B/12.3.75

ACCELERATION (g's)



FREQUENCY (cycles per second)

100 50 25 10 5 2 1 .5 2

$S_d = 10 T^2 S_a$
 S_d - DISPLACEMENT RESPONSE (INCHES)
T - PERIOD (SEC.)
 S_a - ACCELERATION RESPONSE (g's)

DAMPING VALUES
AS PERCENT OF CRITICAL

TO OBTAIN OPERATING BASIS
EARTHQUAKE RESPONSE ACCELERATION,
MULTIPLY BY 0.60



BECHTEL POWER CORPORATION,
LOS ANGELES DIVISION

SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

DESIGN BASIS EARTHQUAKE
VERTICAL ACCELERATION-RESPONSE
SPECTRA AT ELEV (+) 8'-0" OF
SAFETY EQUIPMENT BUILDING
(SAFETY INJECTION AREA)

Prepared By

Reviewed By

Approved By

JDC

KAL KCH

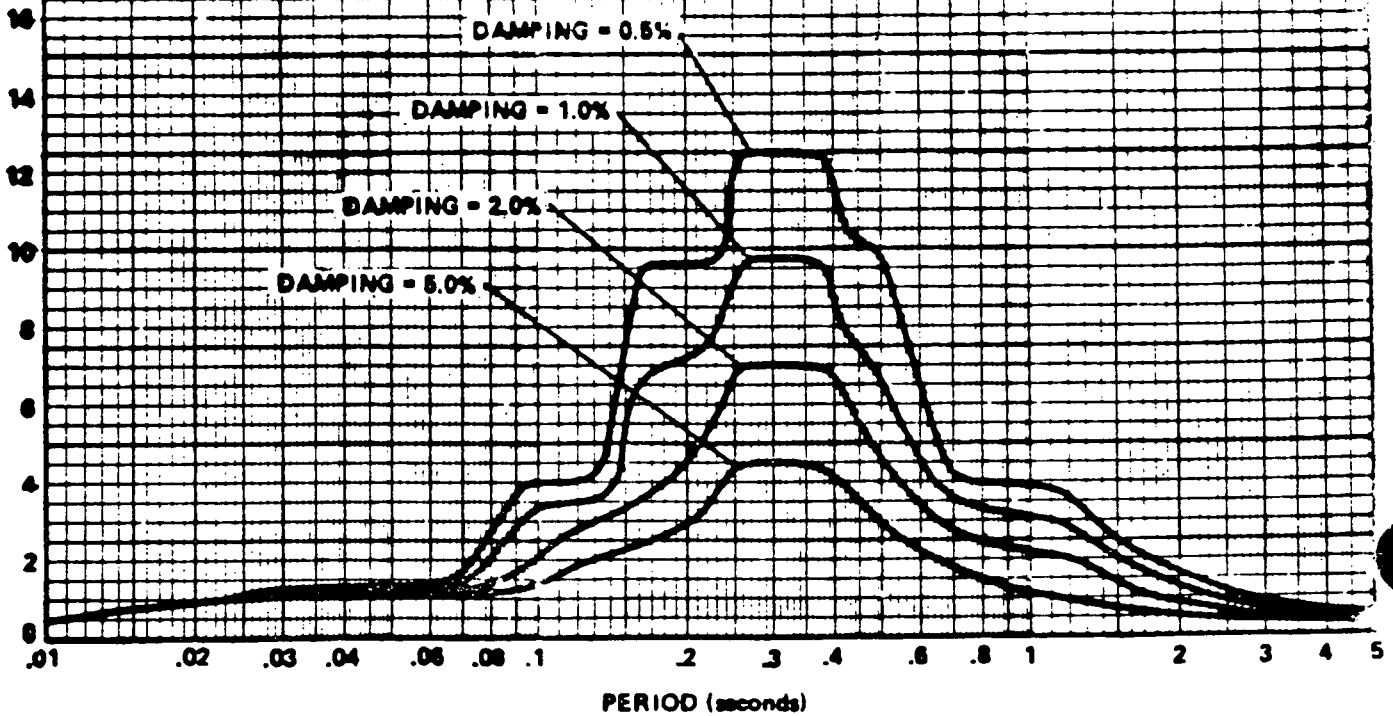
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SKETCH NO.
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REV
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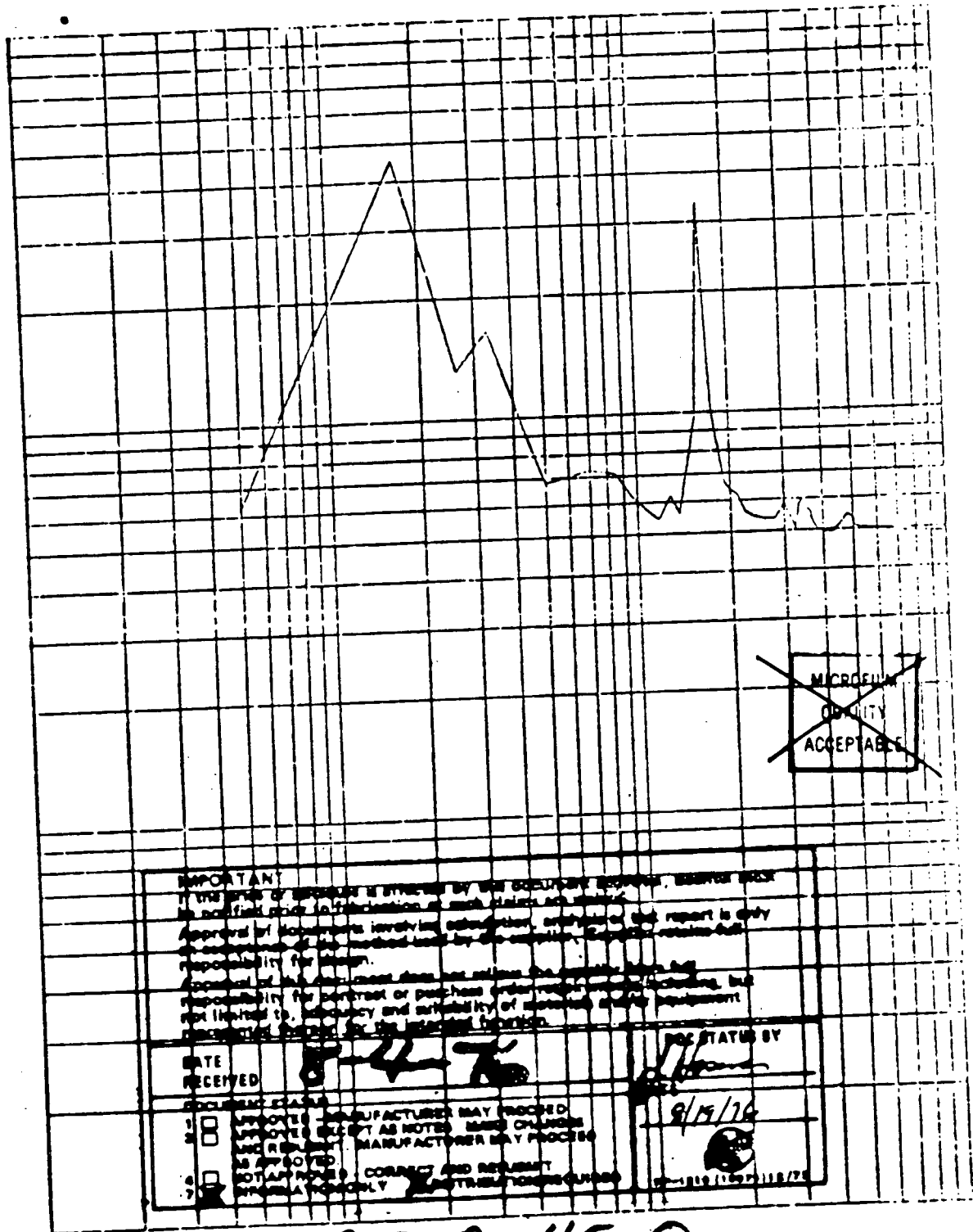
ACCELERATION (g's)



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(SUPERSEDES 900-B-14-0)

FREQUENCY (CPS)

Total 187

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58(Y)
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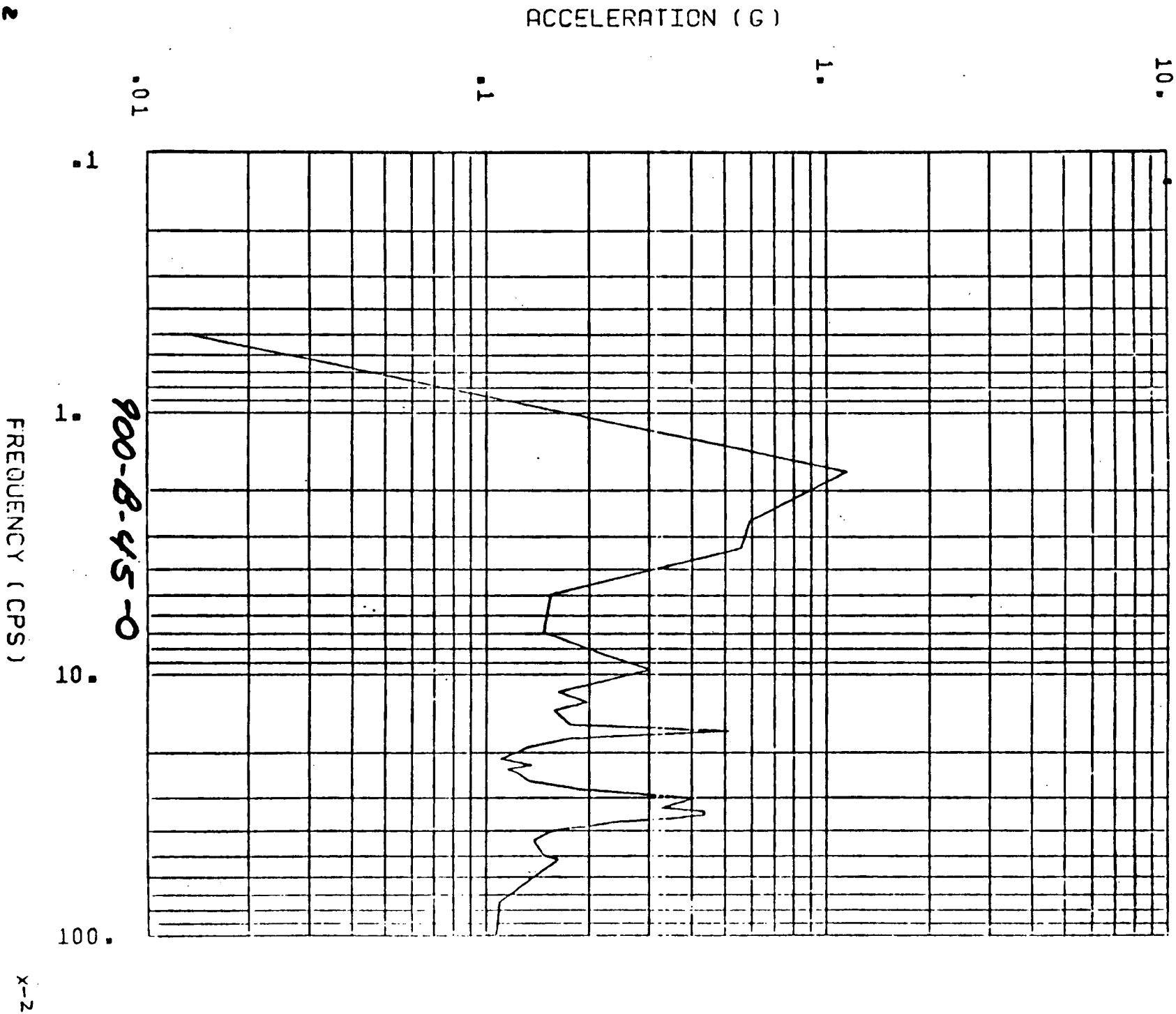
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X-1

SCC SURGE LINE NOZ, Y-RESPONSE DUE TO X-OBE .01 DRIPPING

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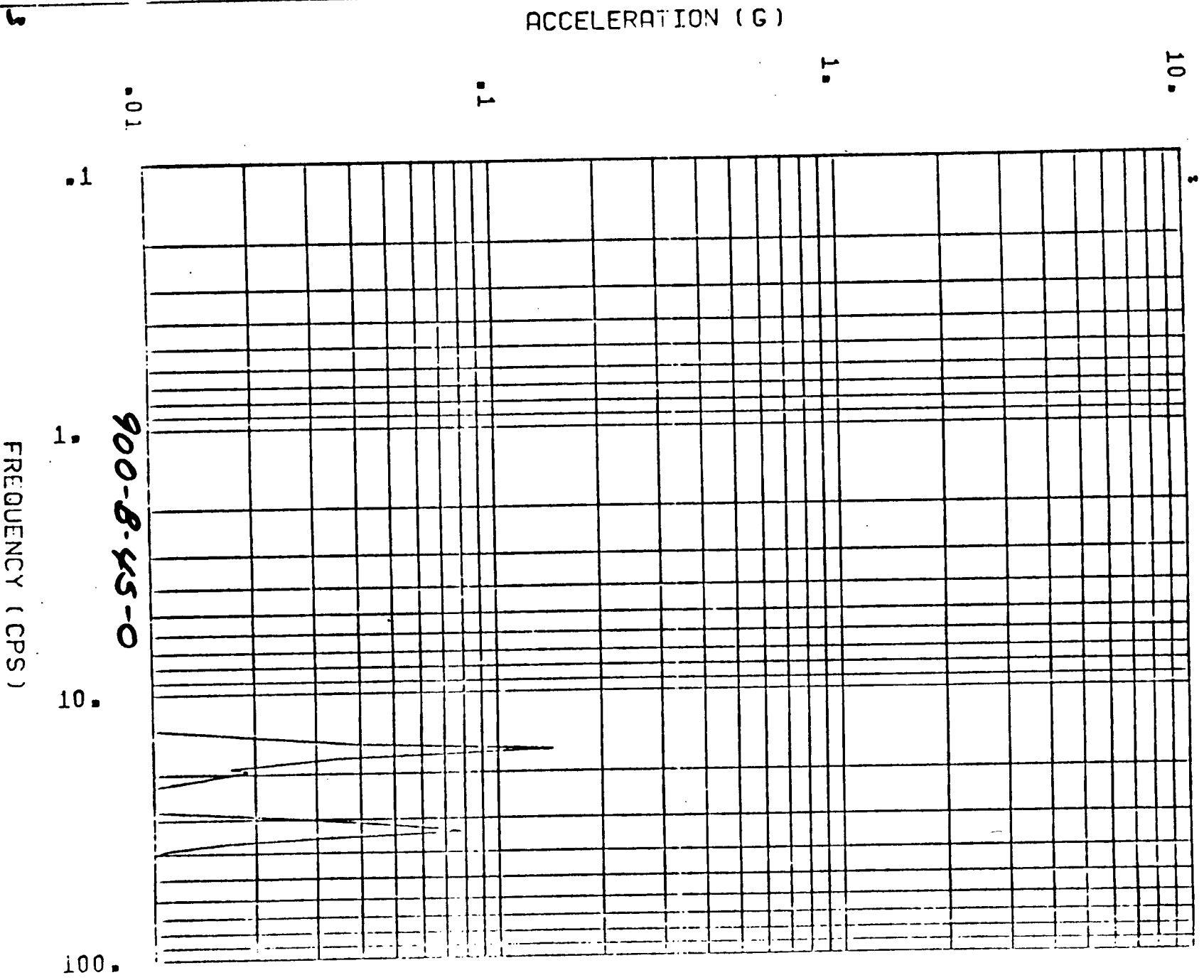
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SEE SOURCE LINE NOZ. Z-RESPONSE DUE TO X-09E .01 DAMPING

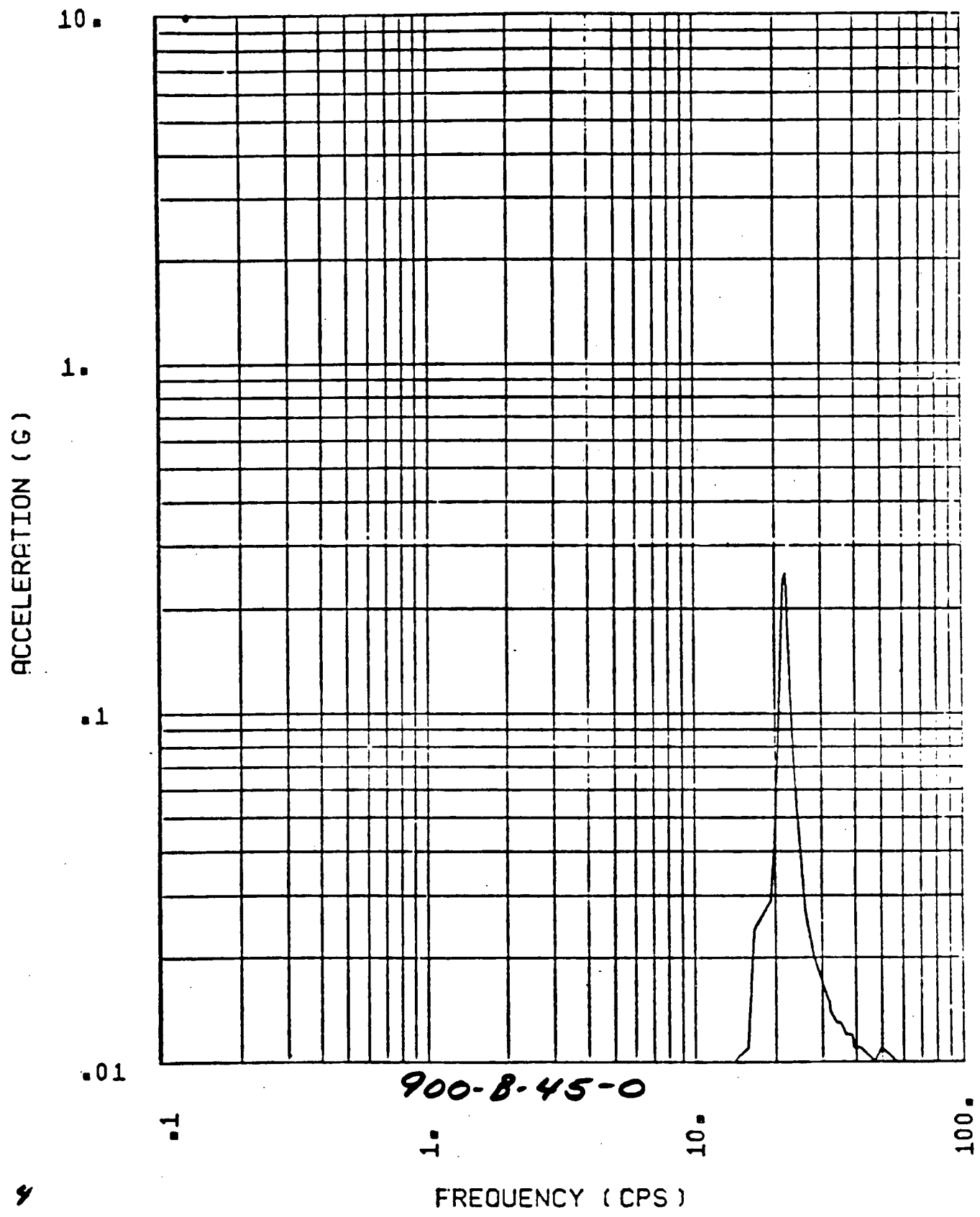
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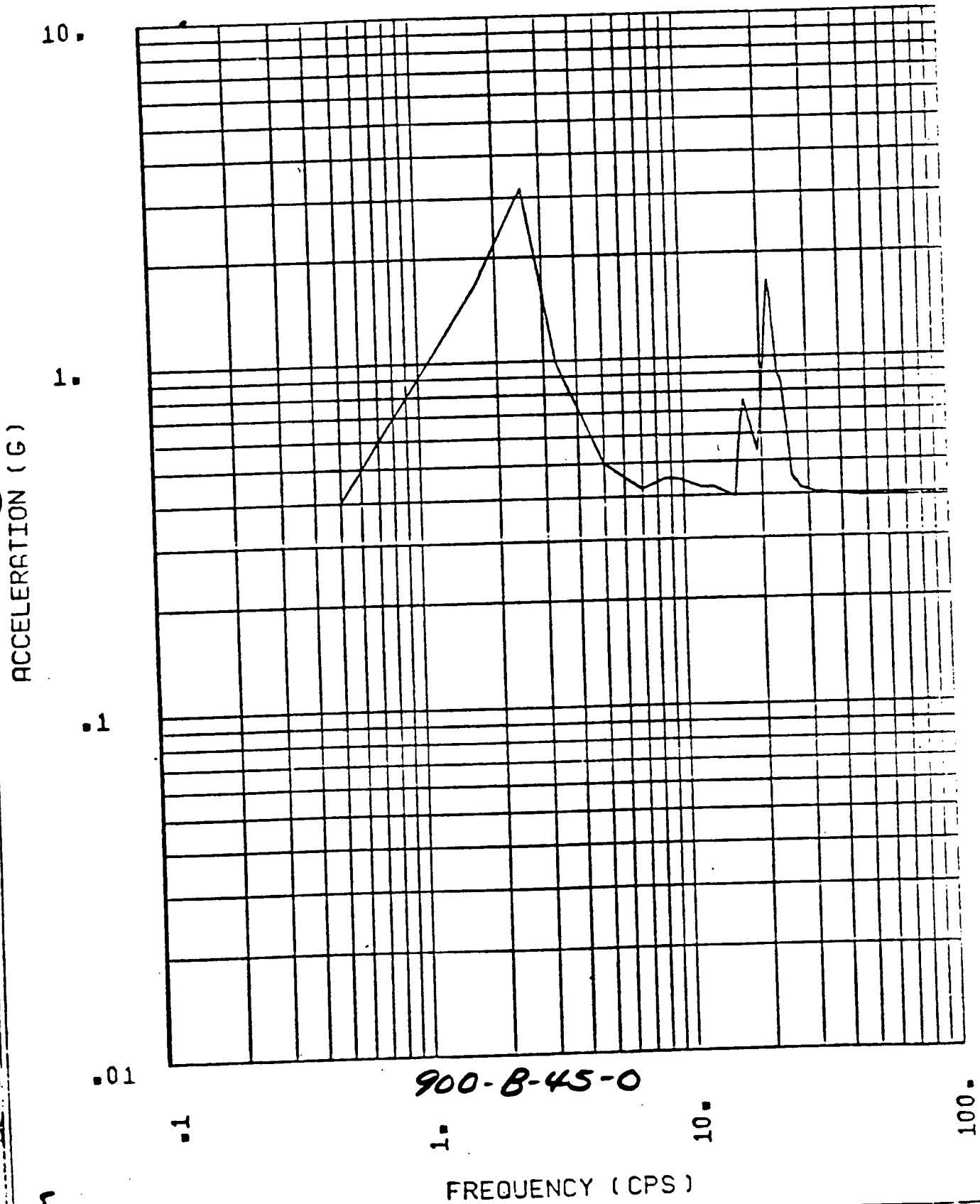


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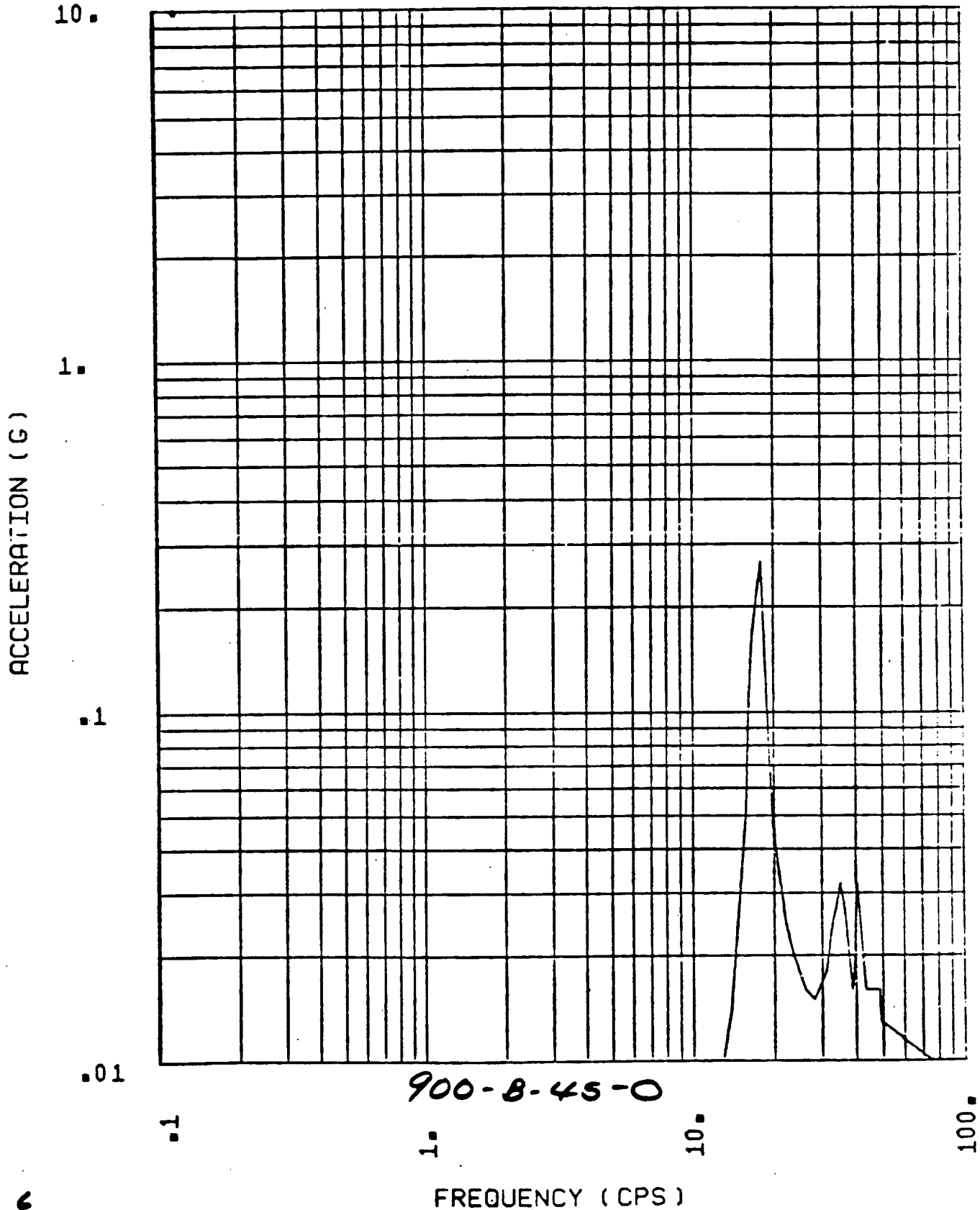


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Coupled Motion

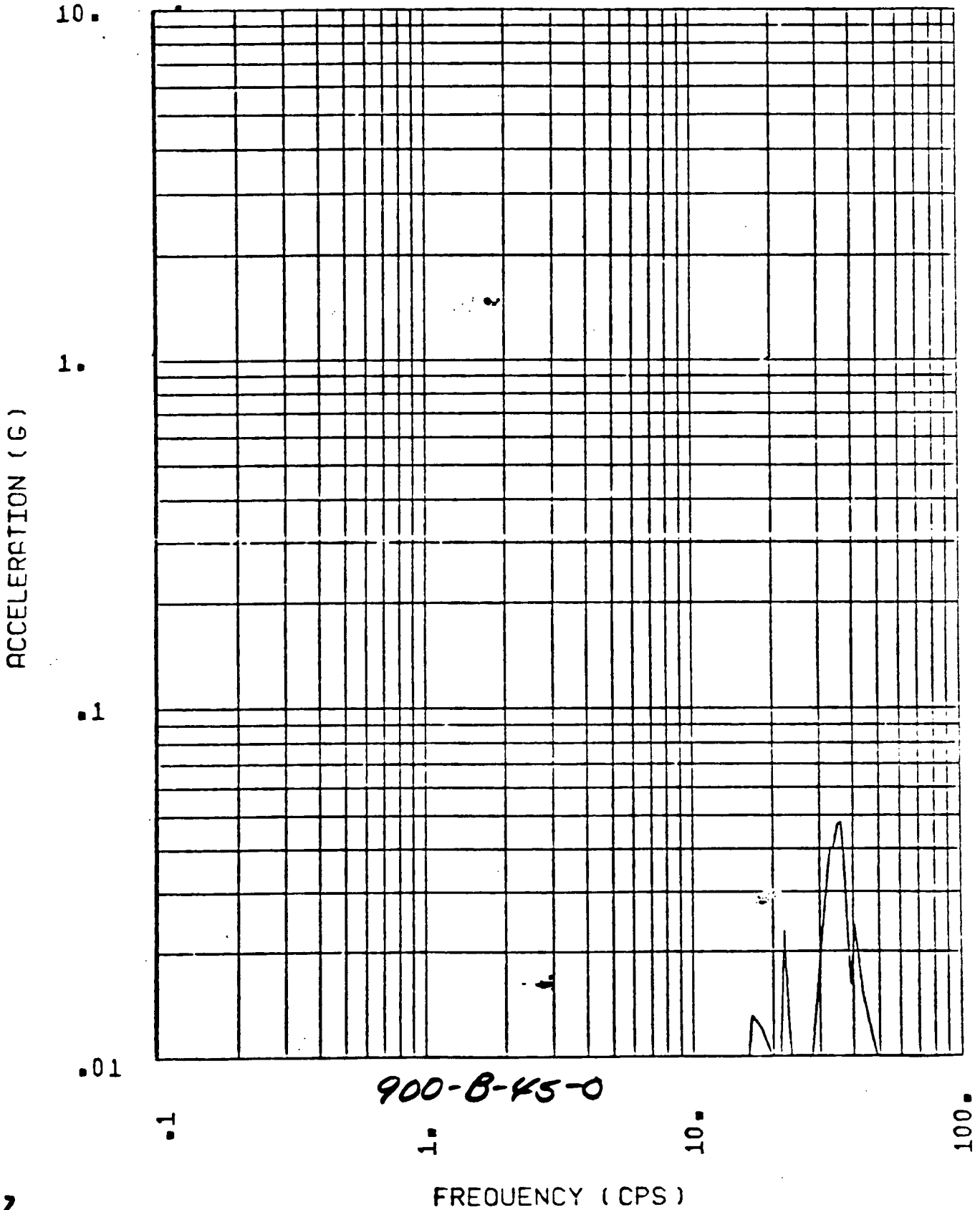
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SCE SURGE LINE NOZ. Y-RESPONSE FOR Z-OBE, .01 DAMPING

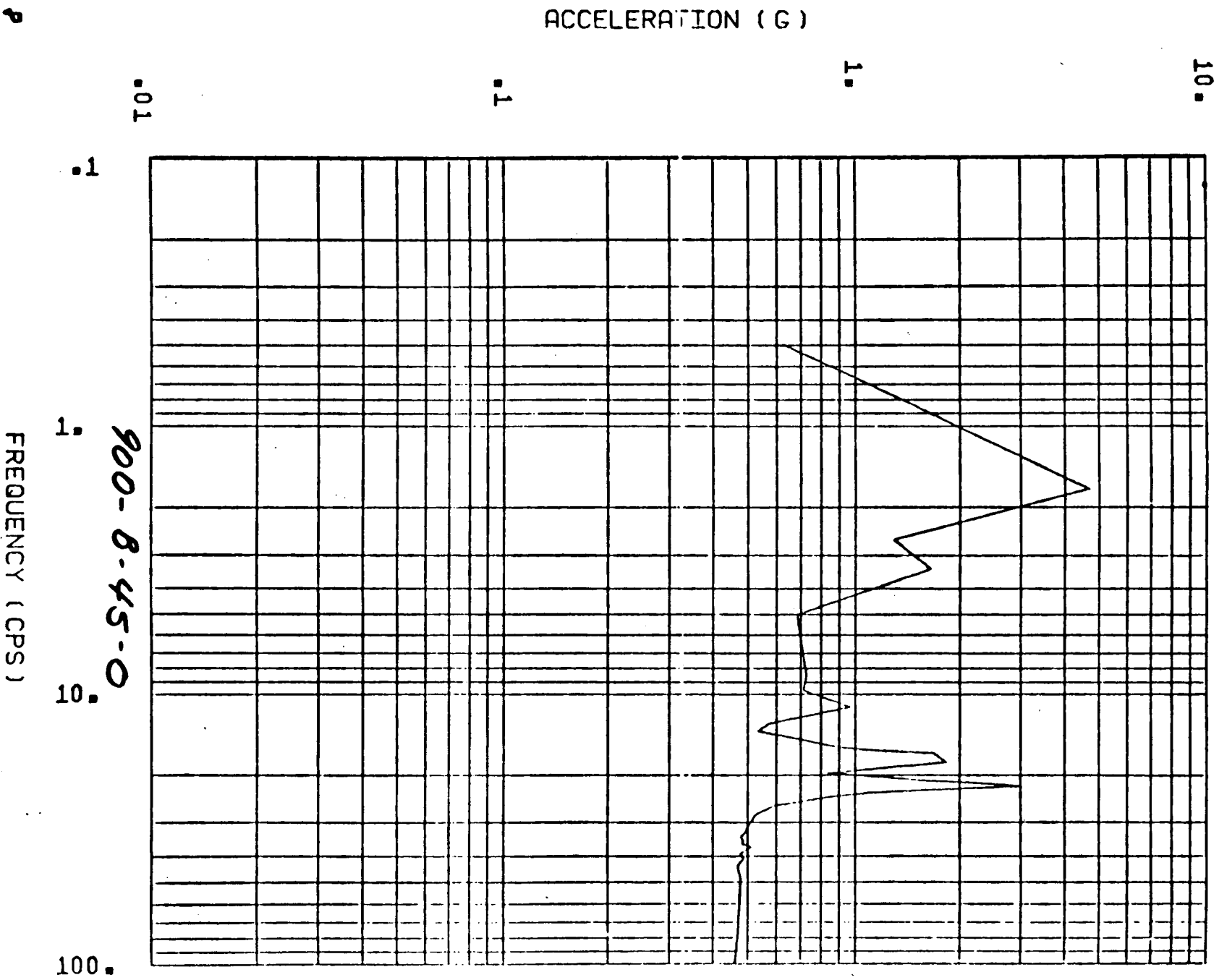
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Coupled Model

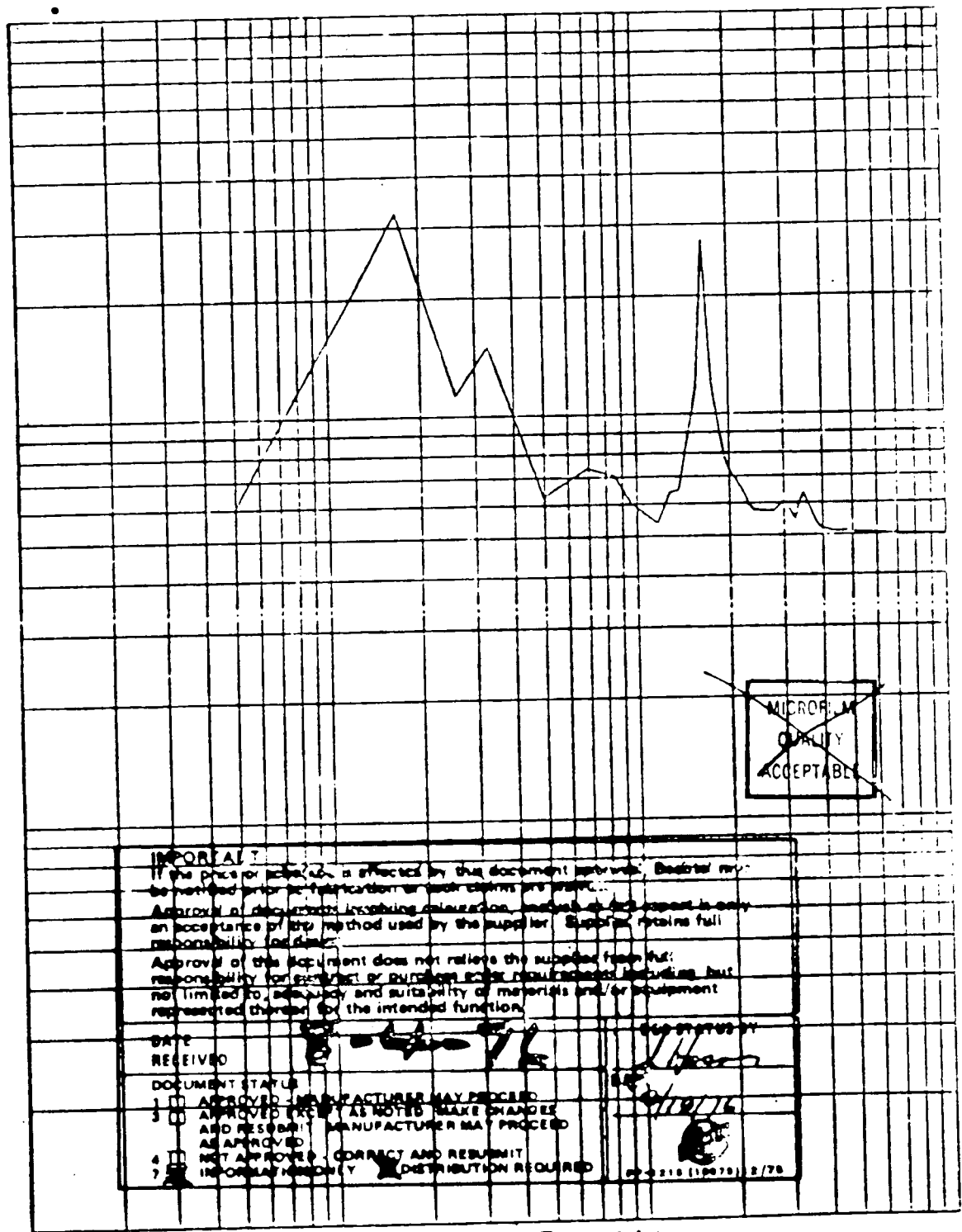
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ACCELERATION (G)

10.
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62-210 (1079) 2/78

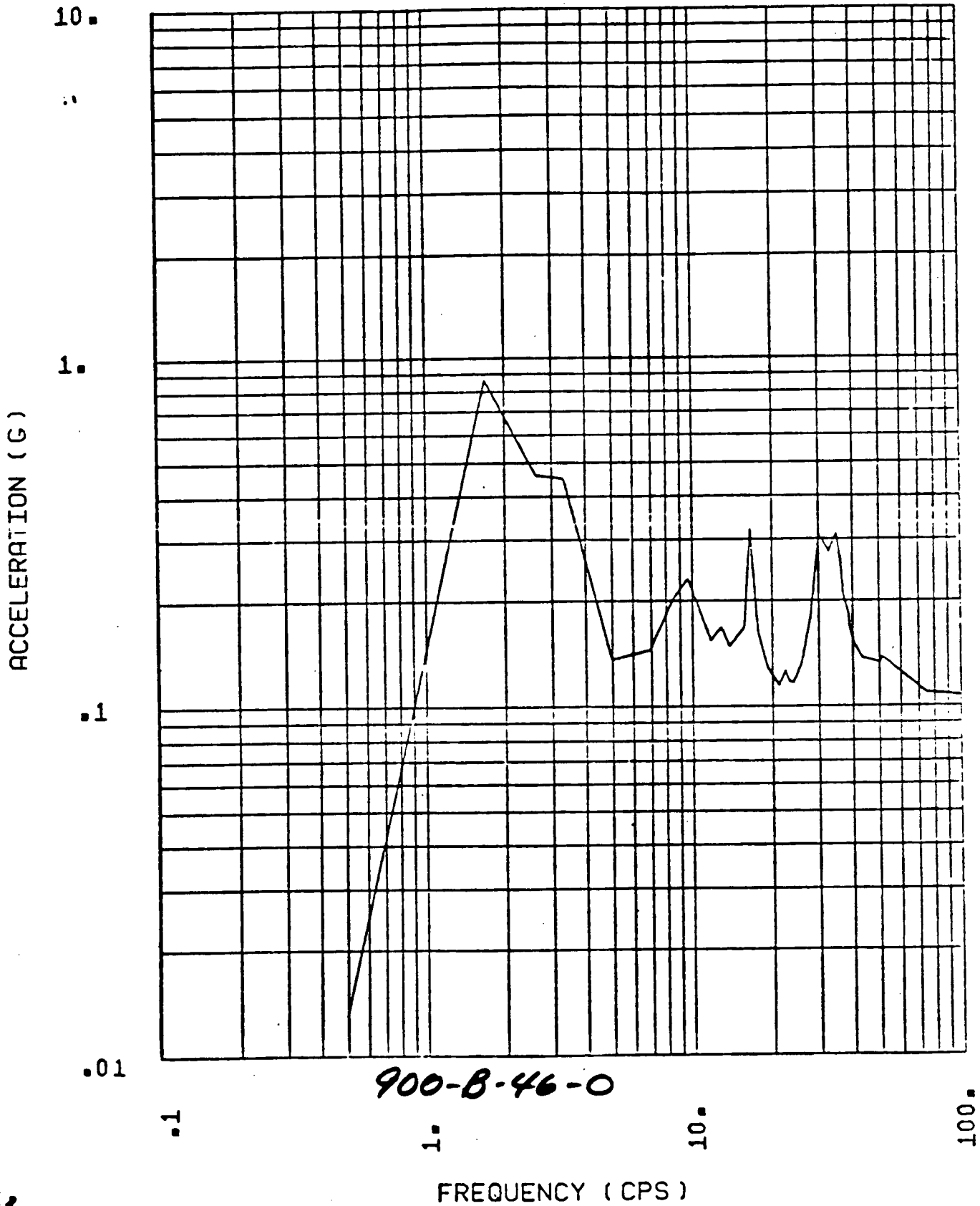
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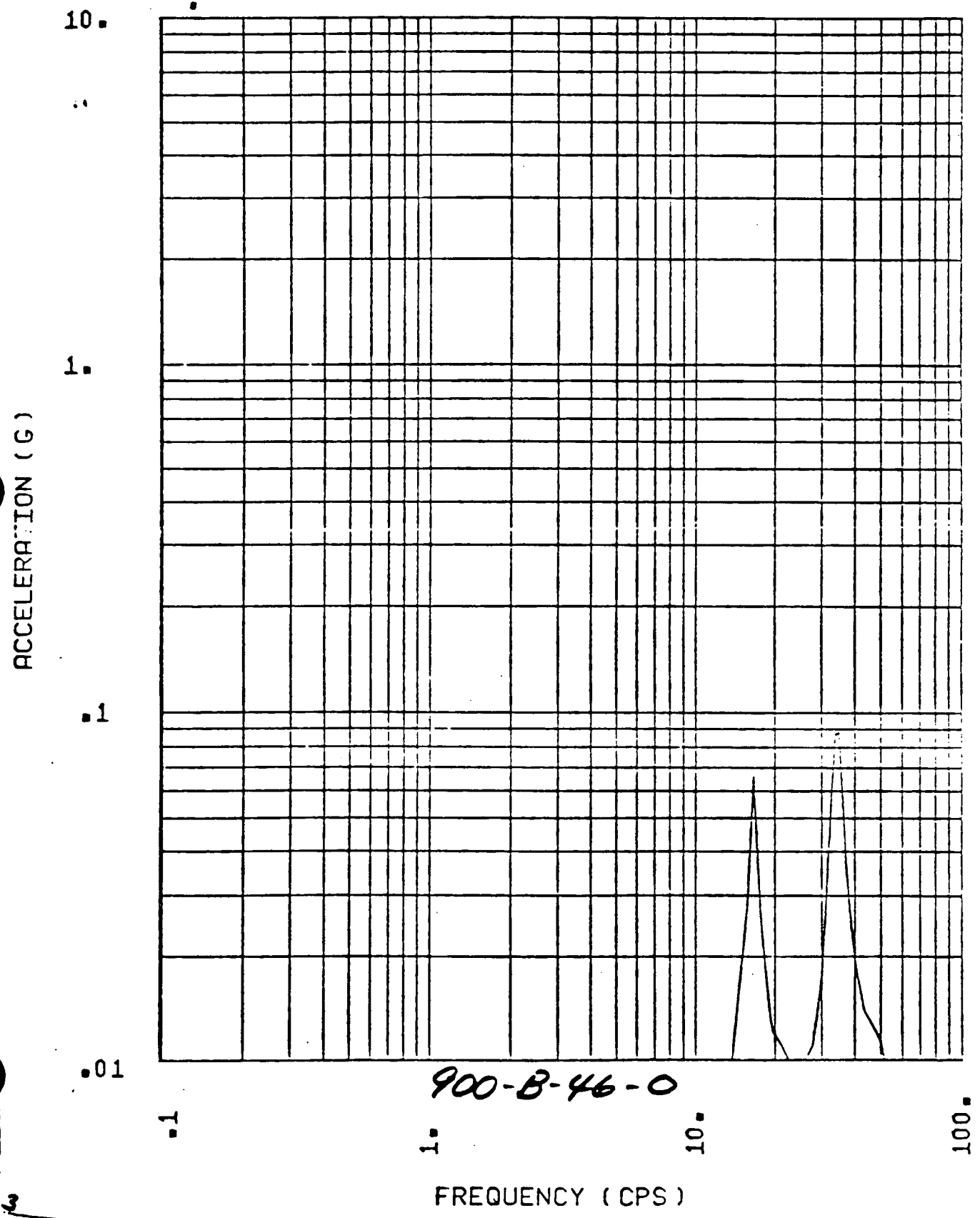
FREQUENCY (CPS)

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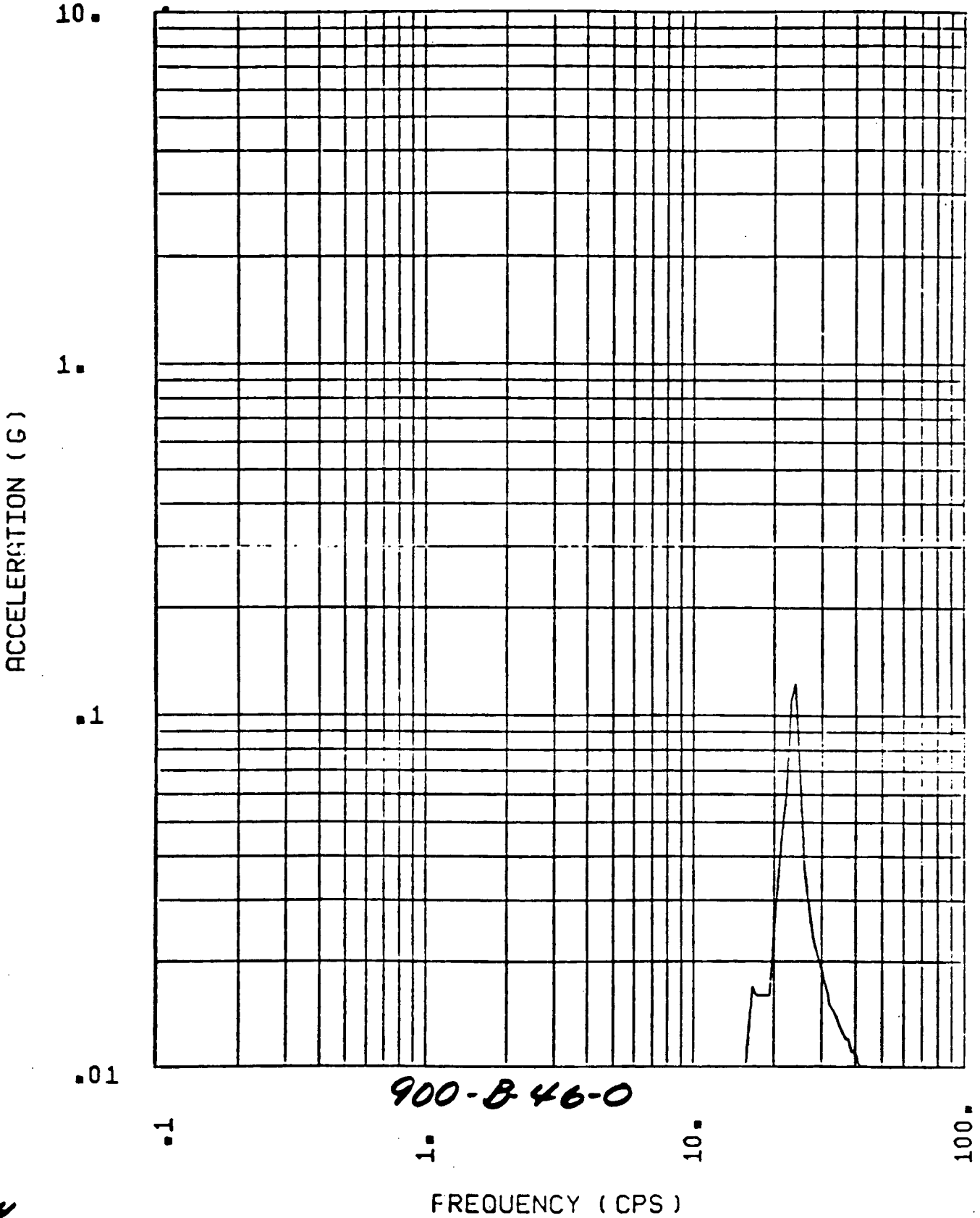


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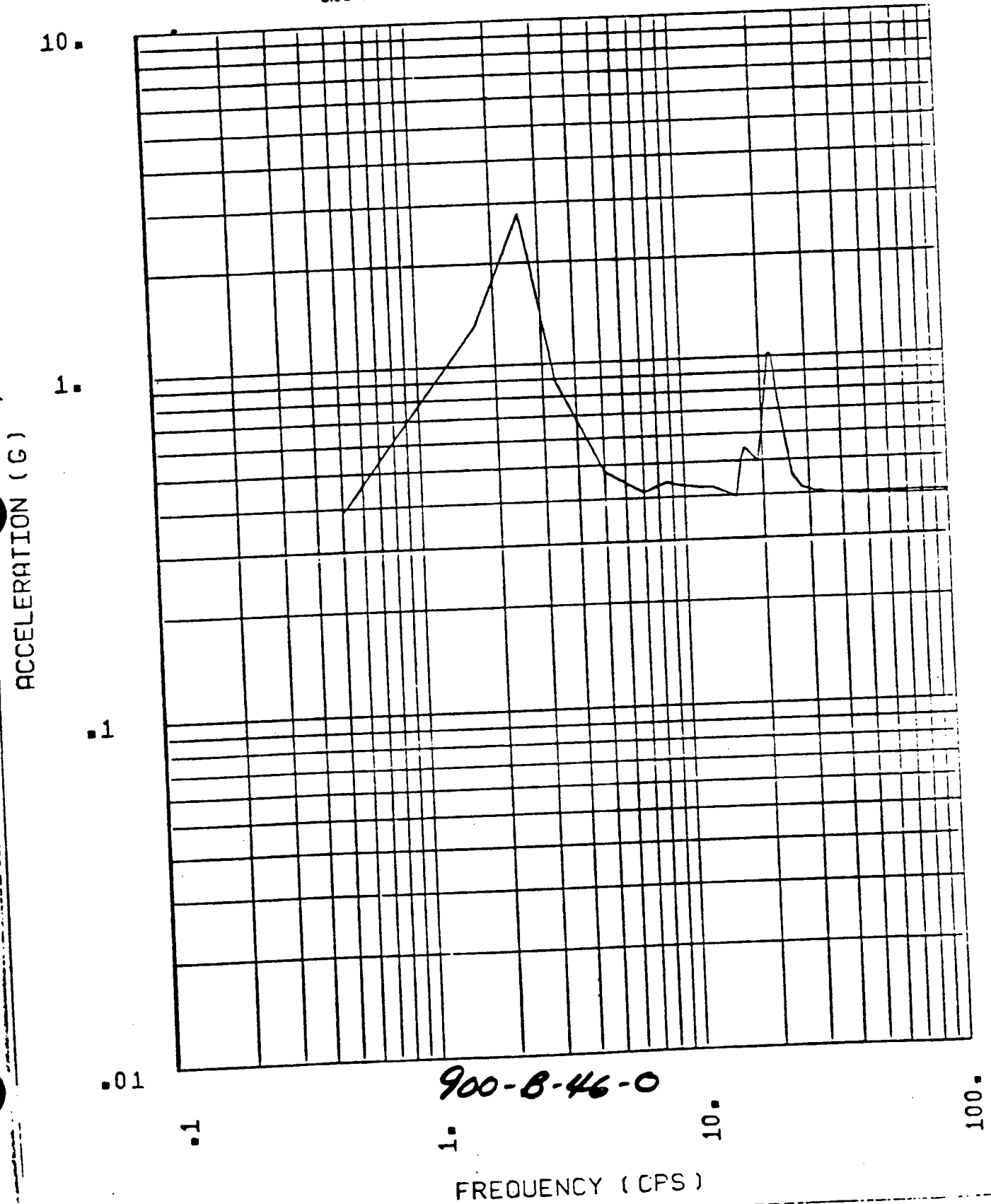


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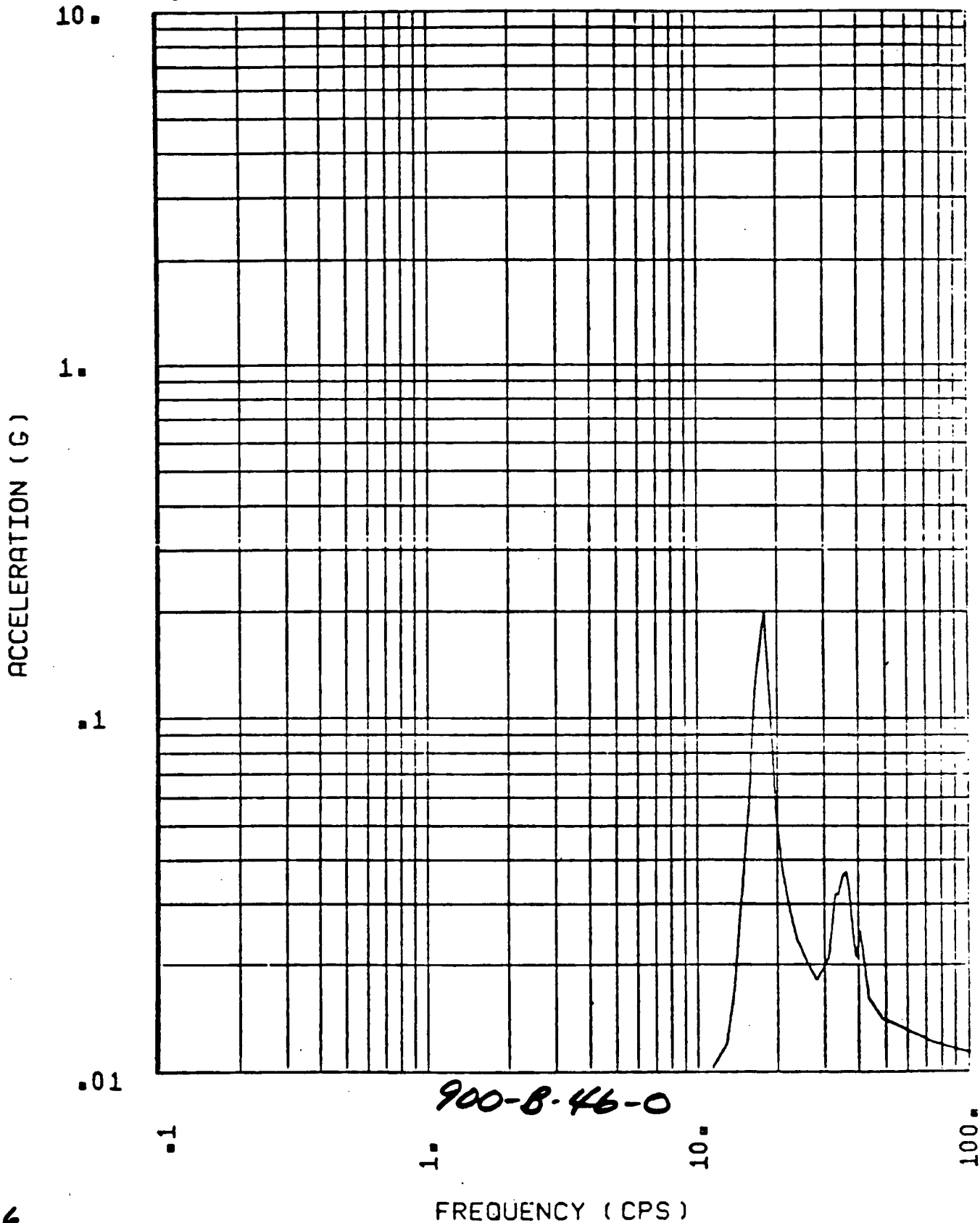
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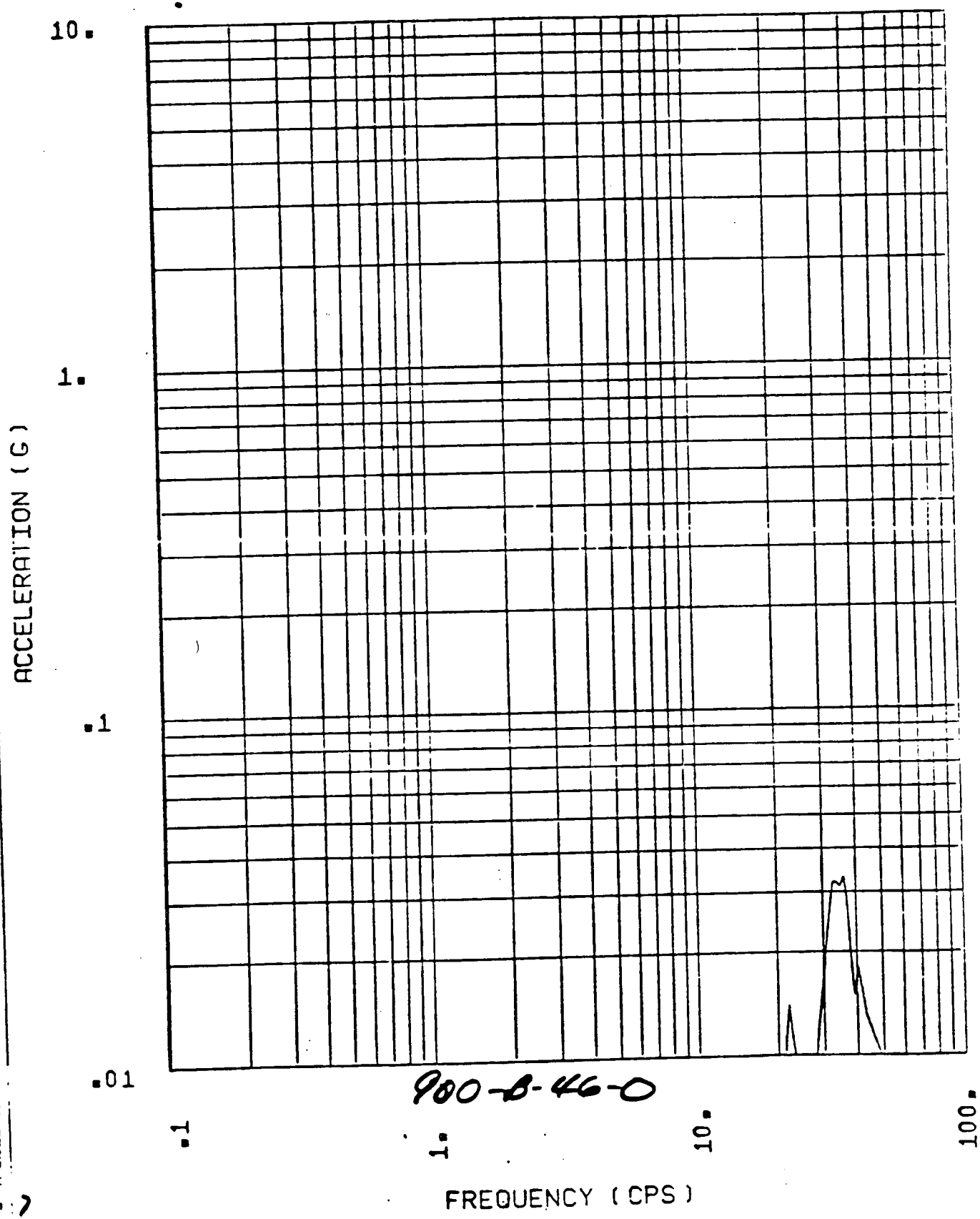
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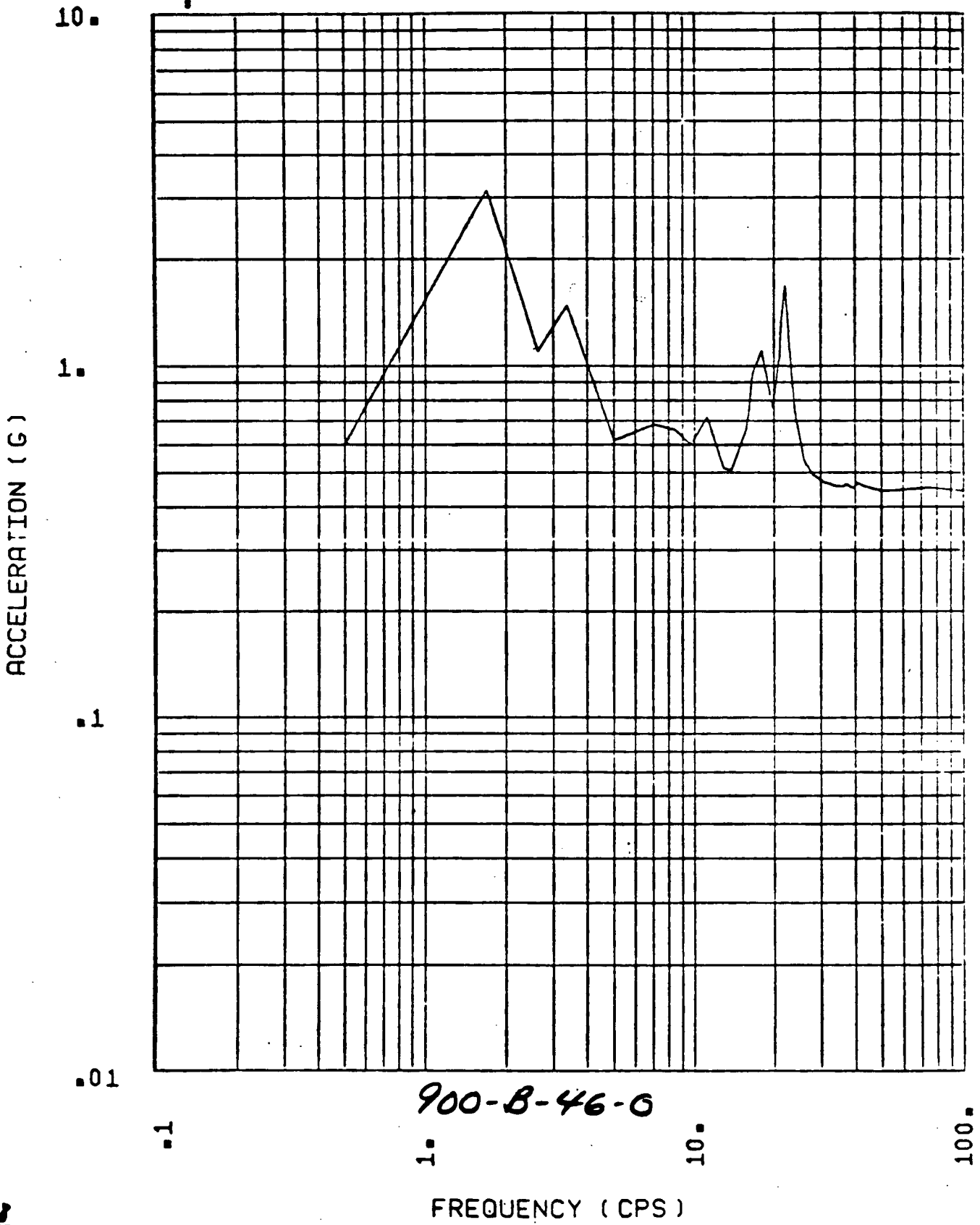
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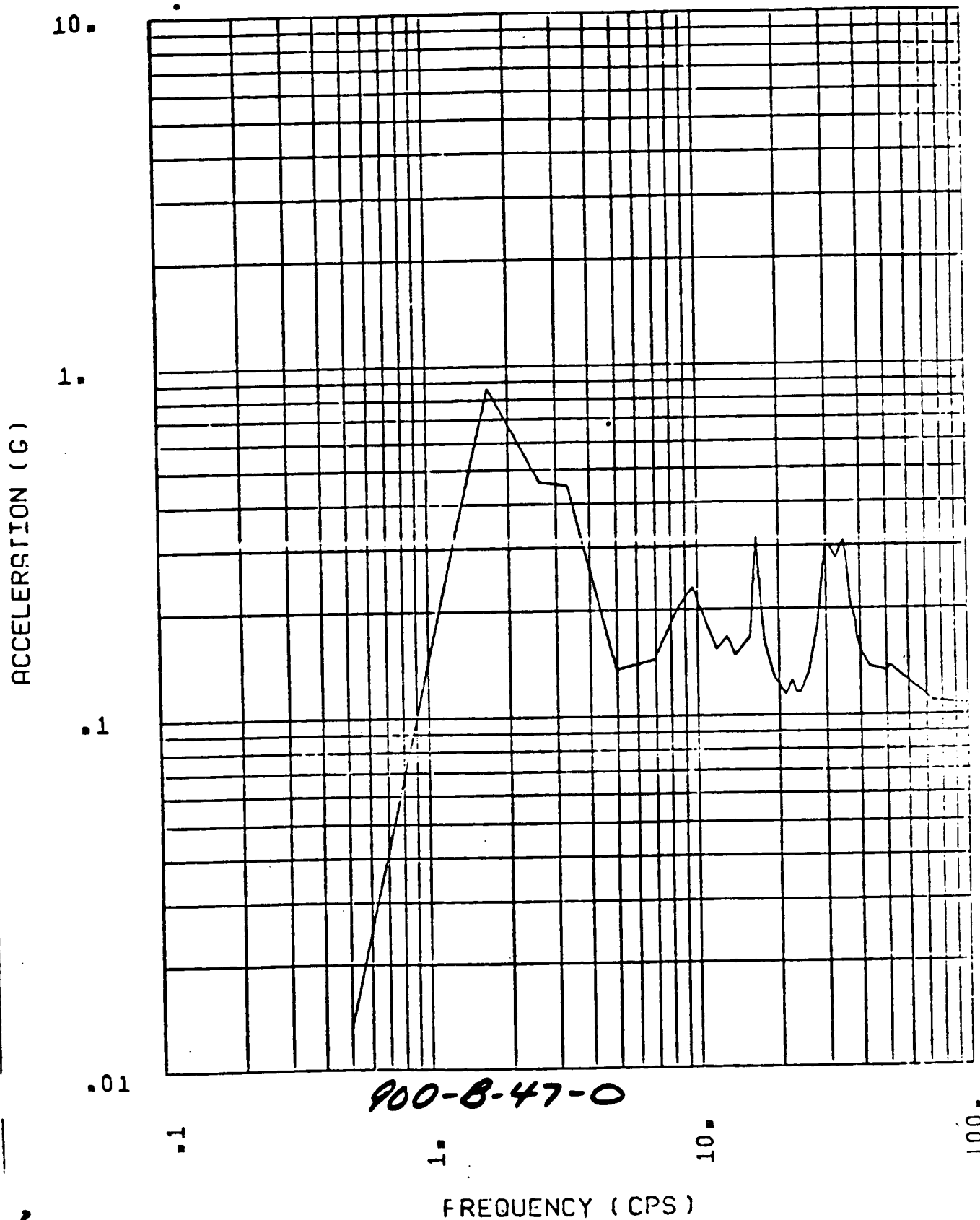
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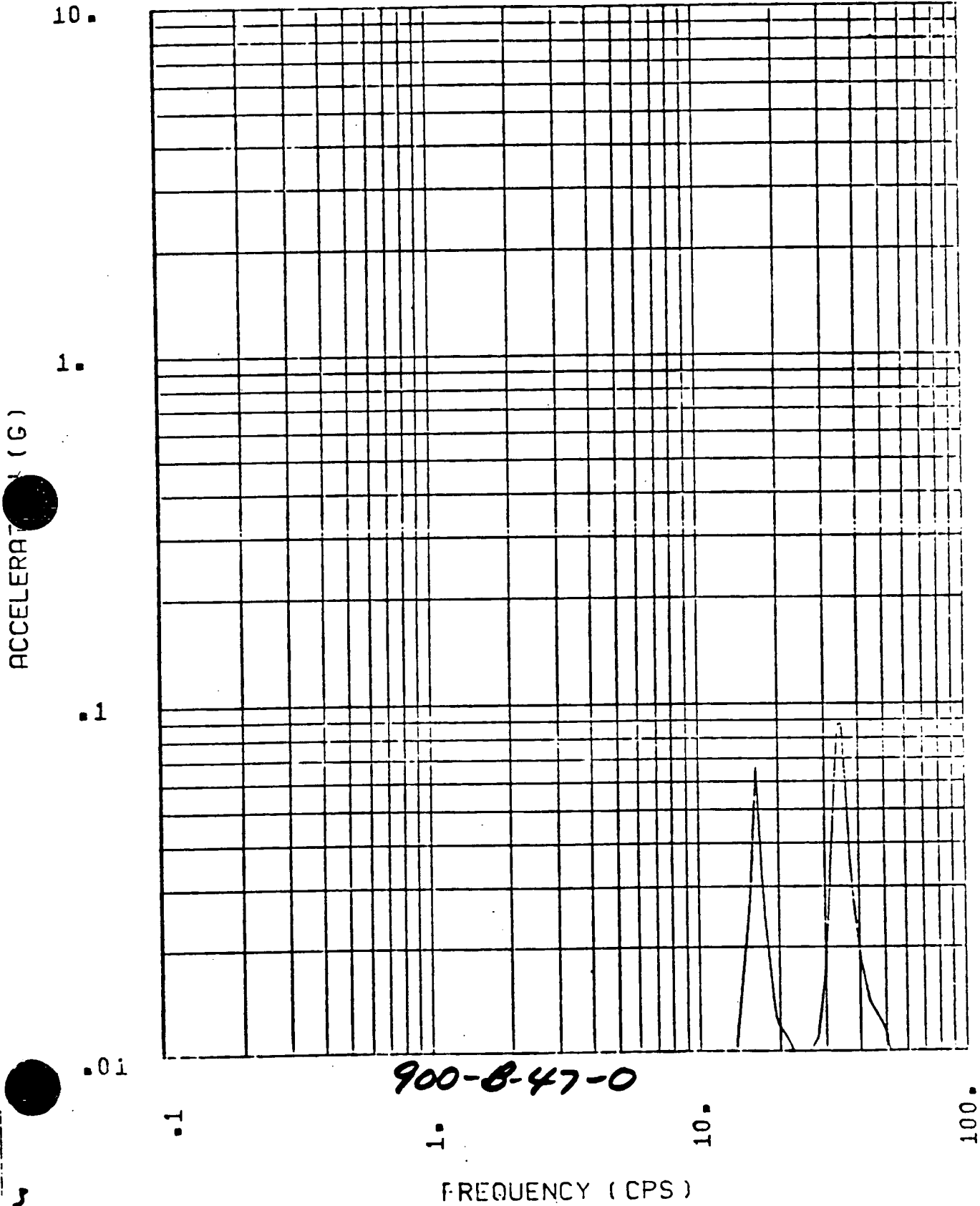


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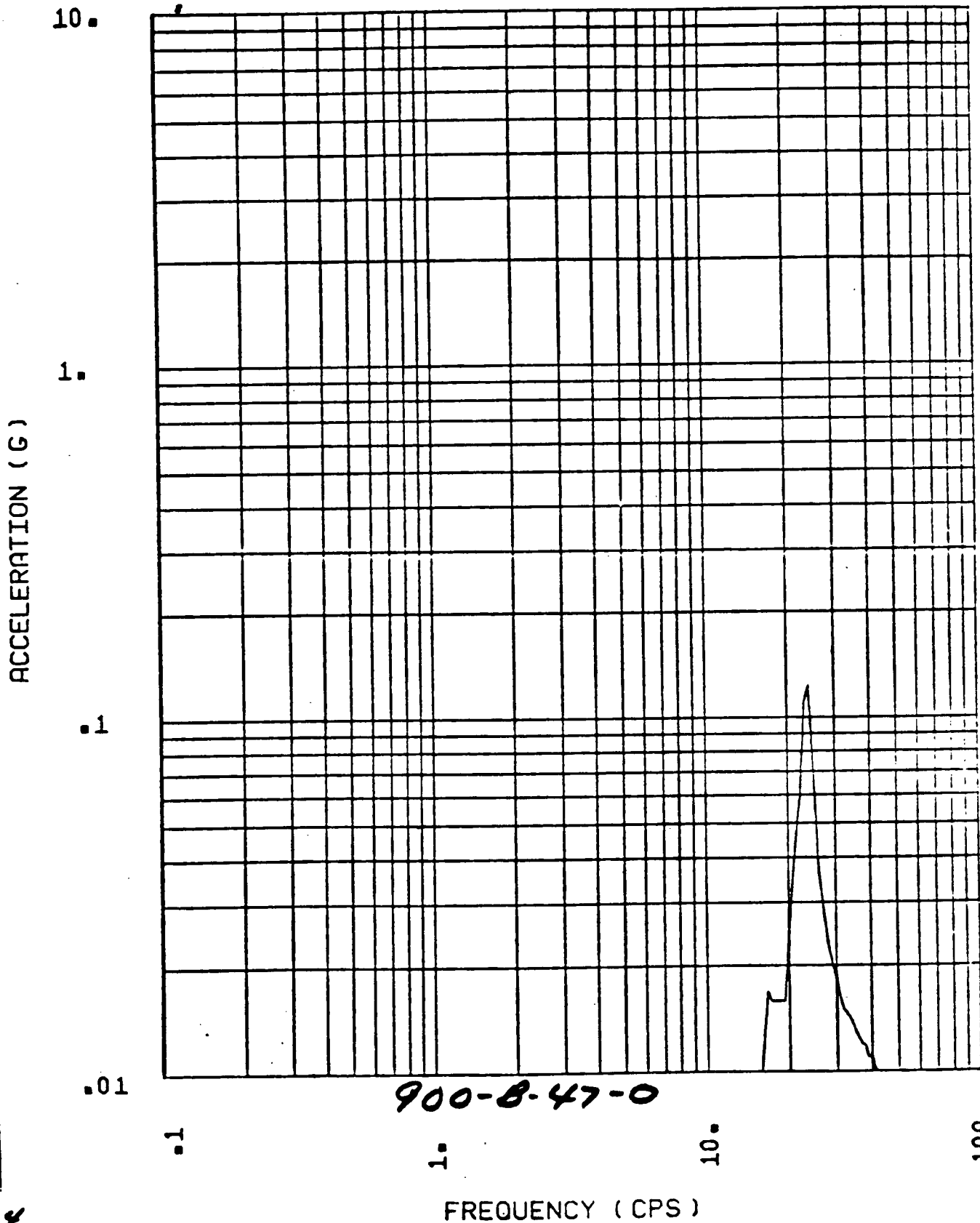


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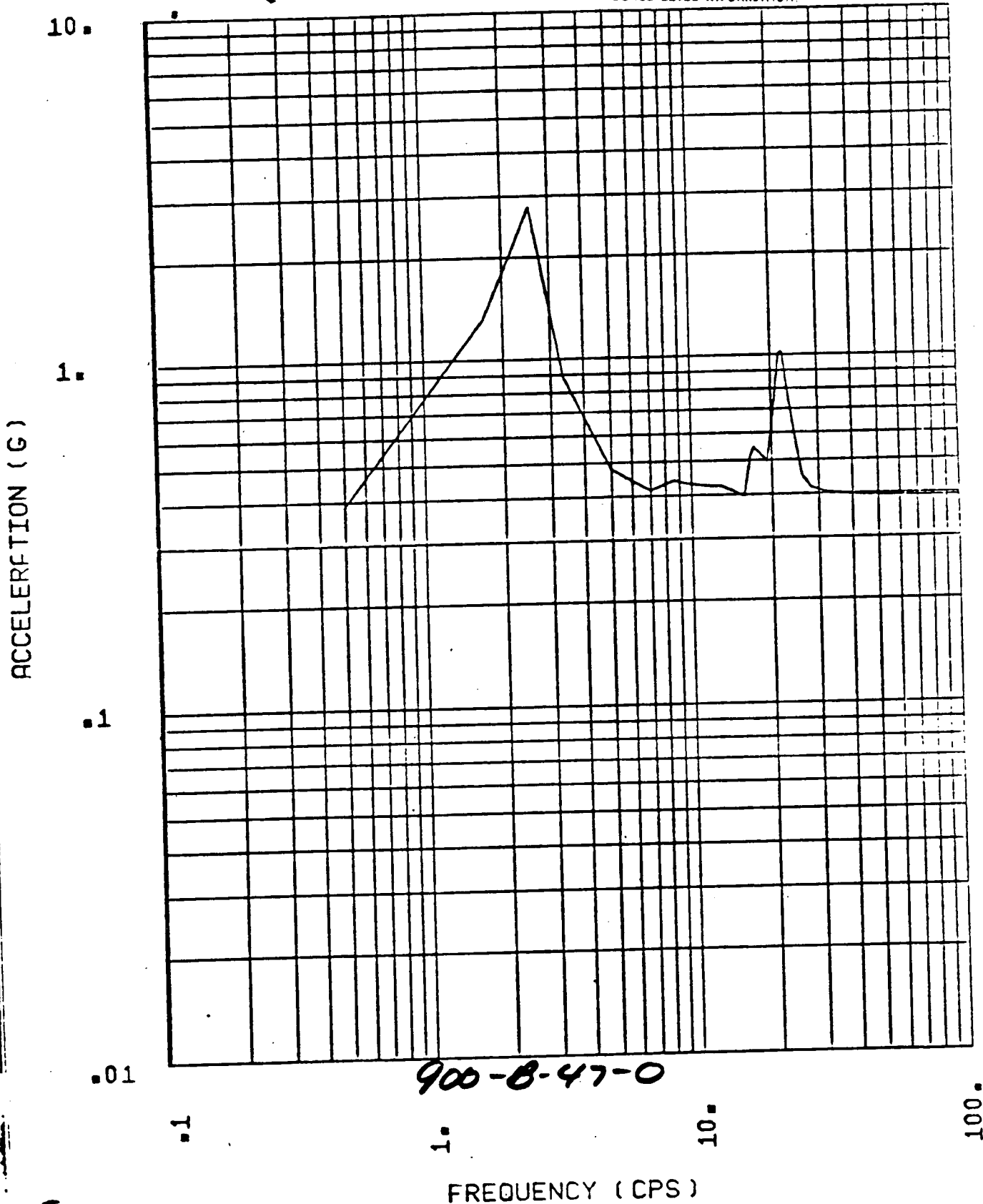


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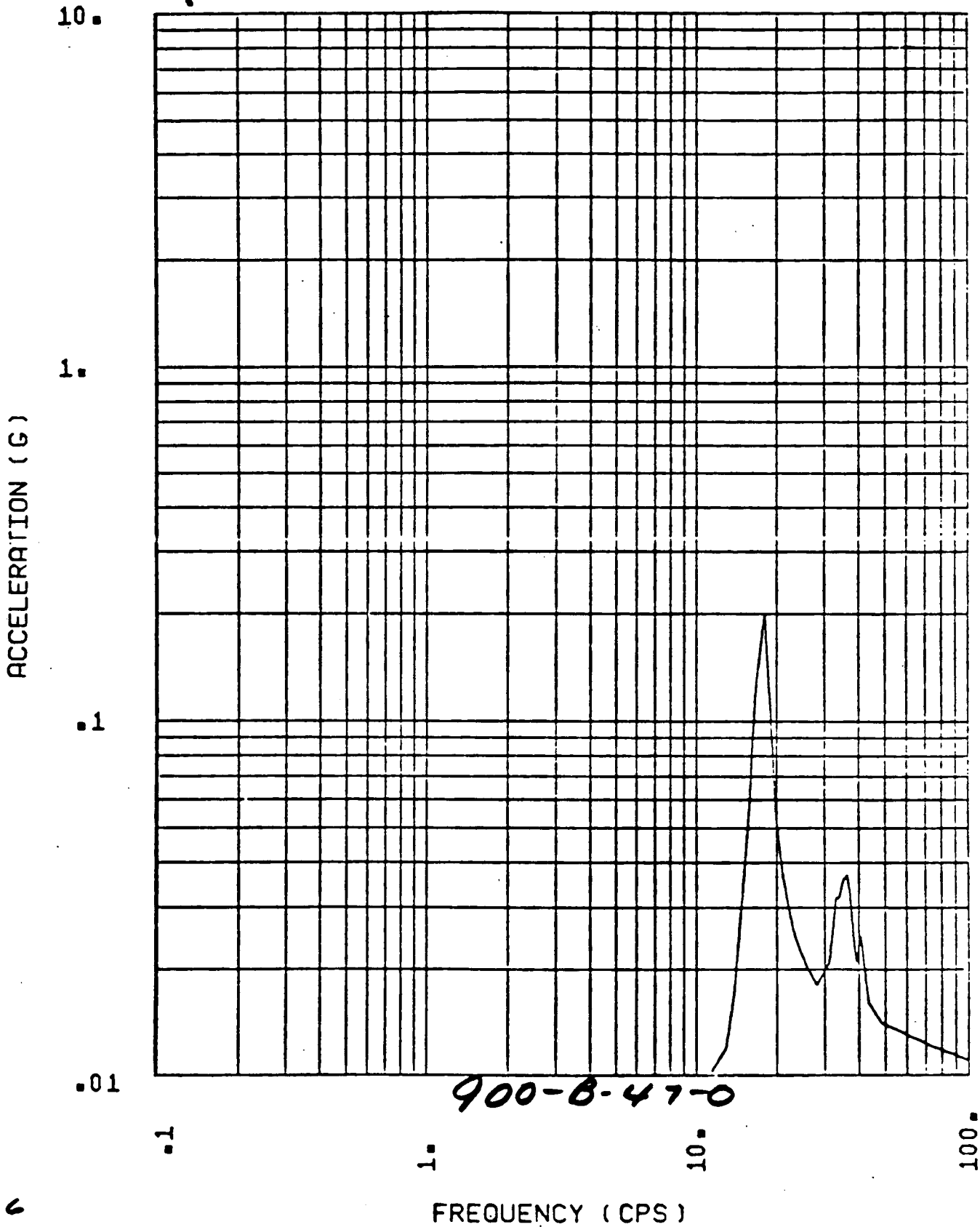


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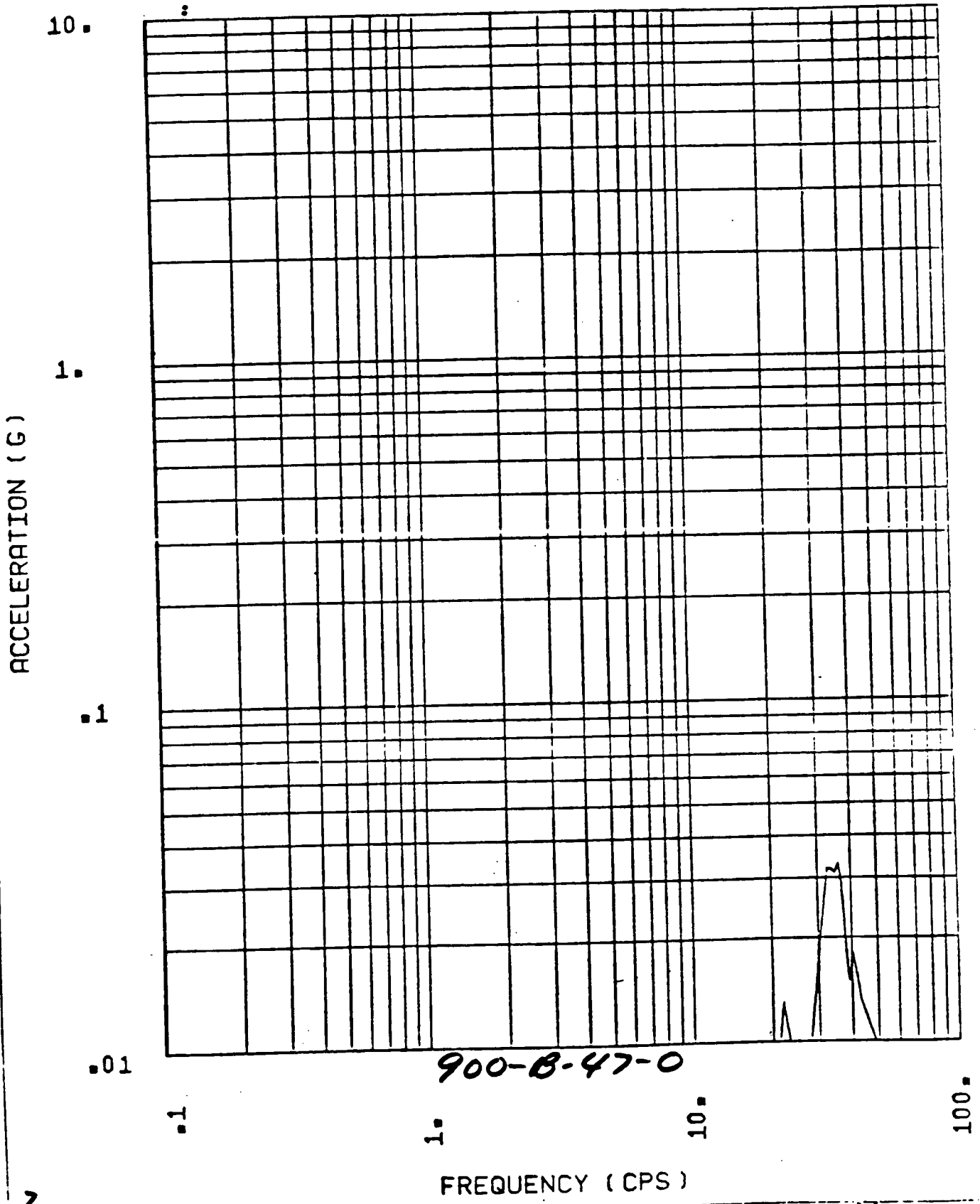
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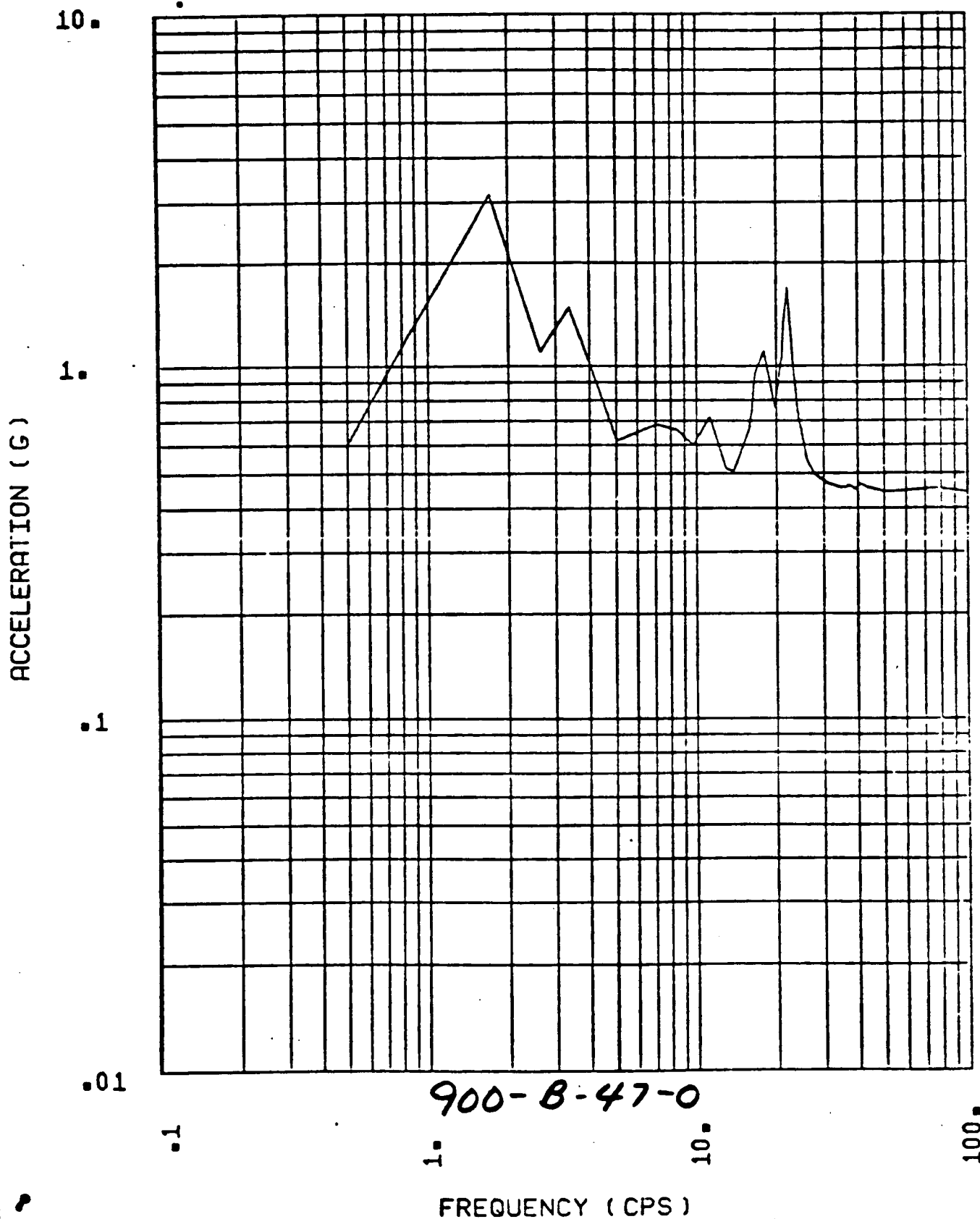
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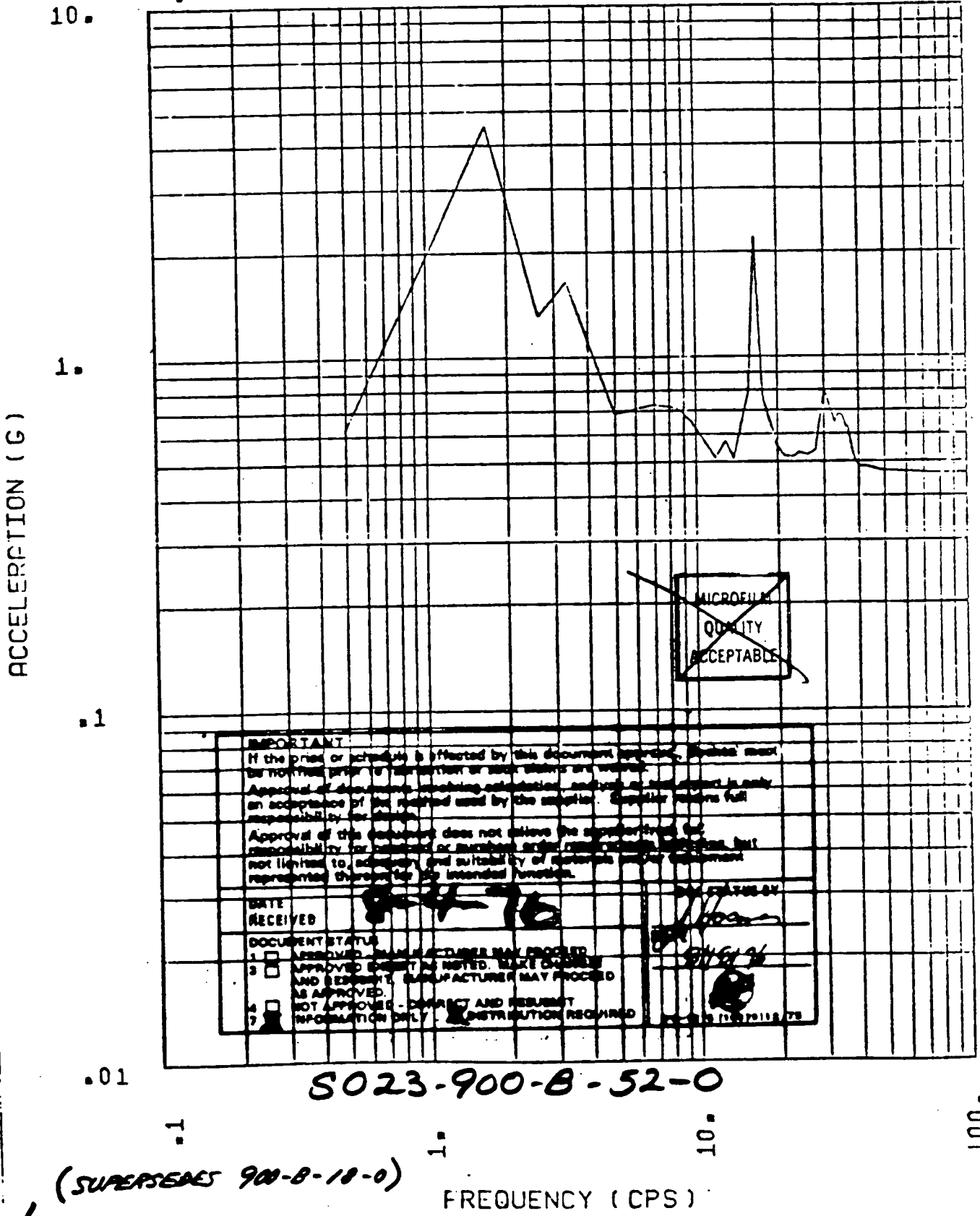


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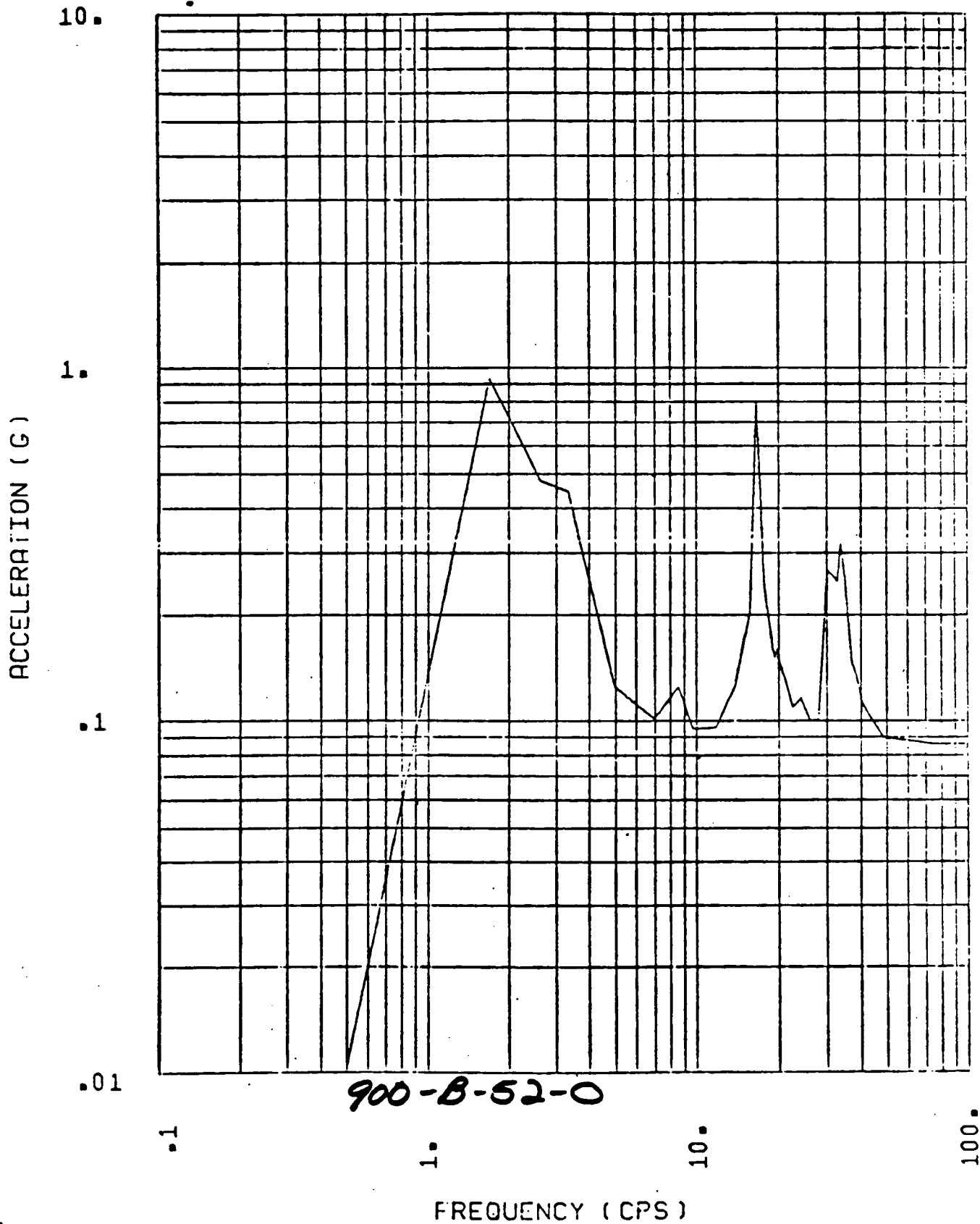
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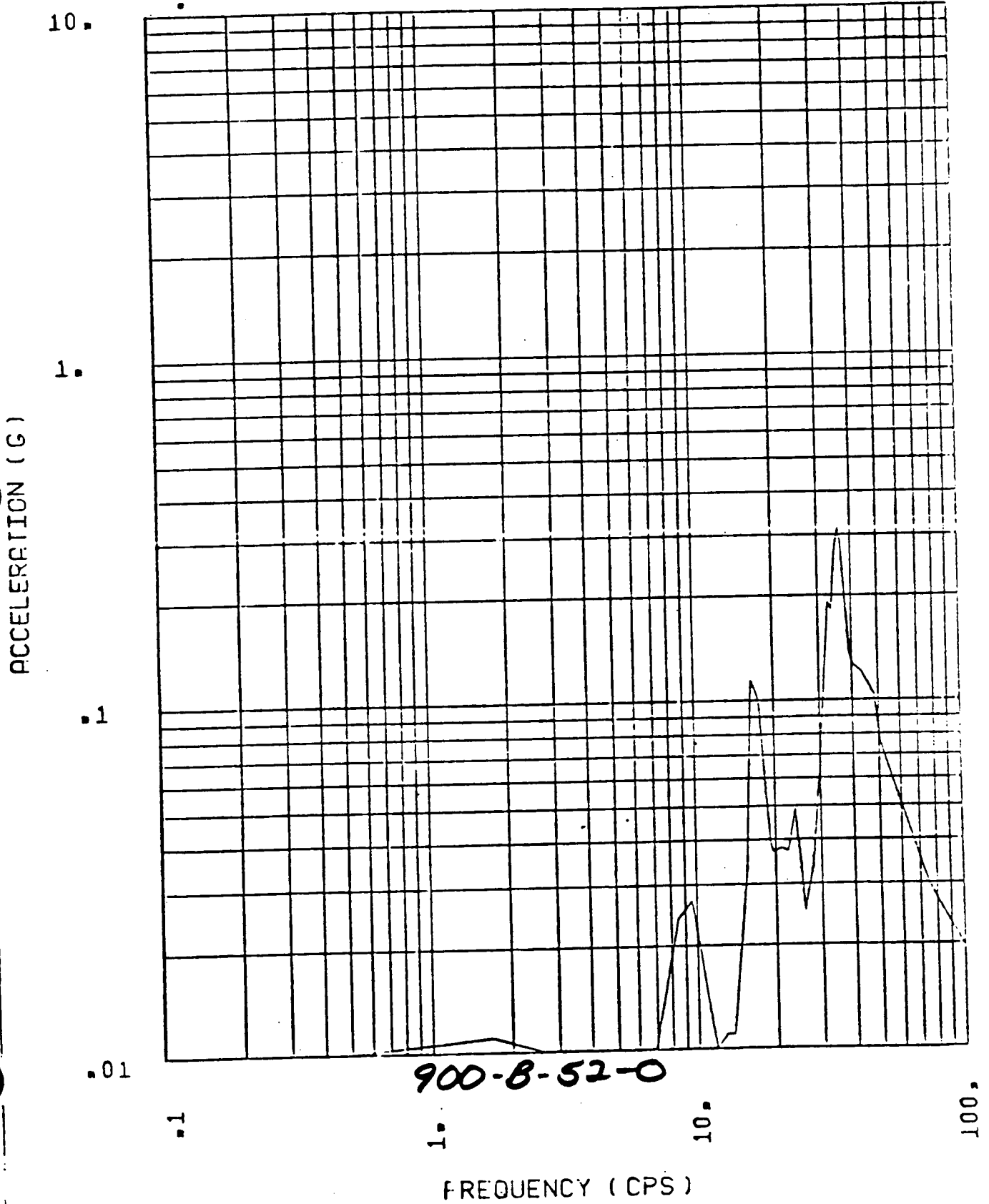
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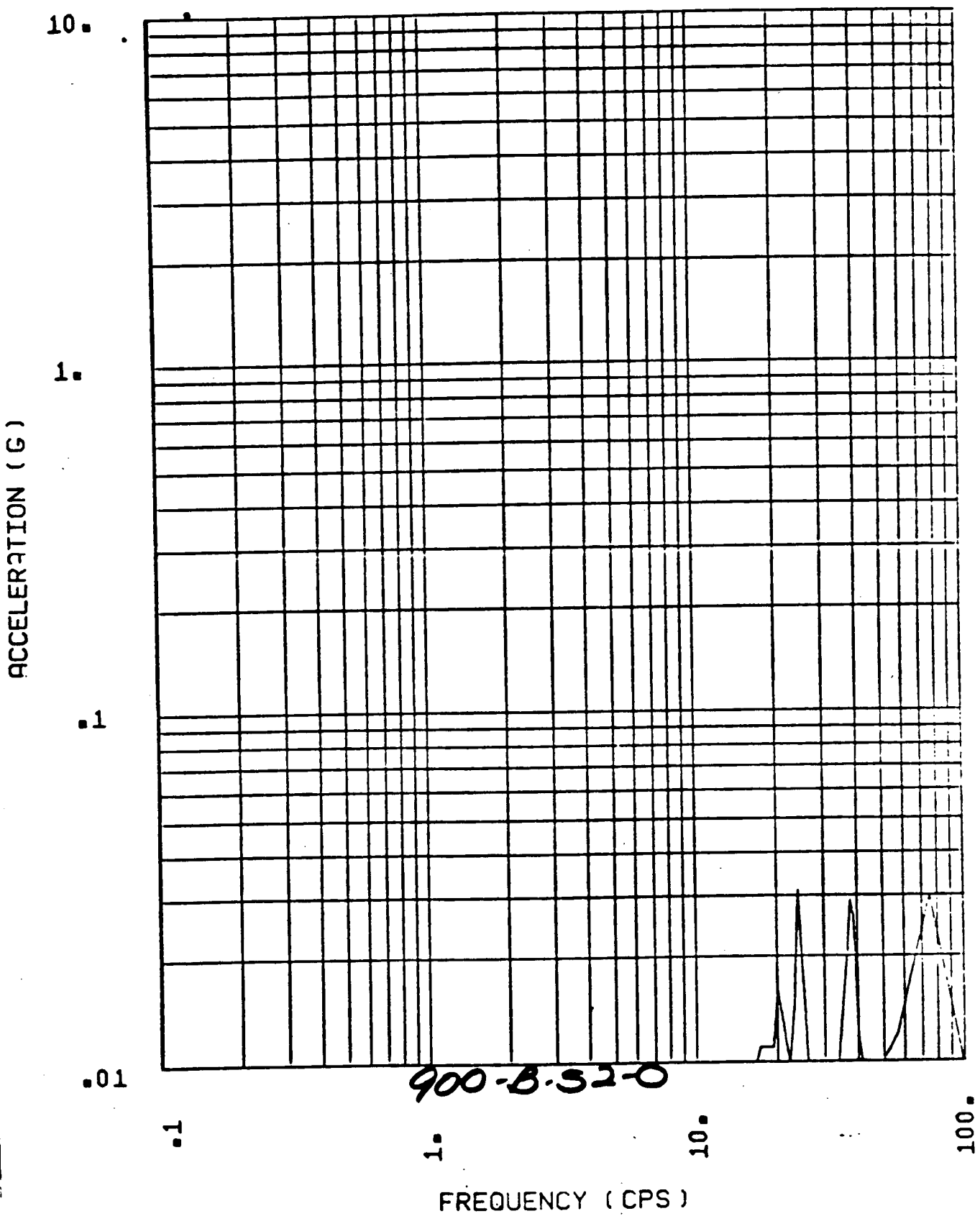


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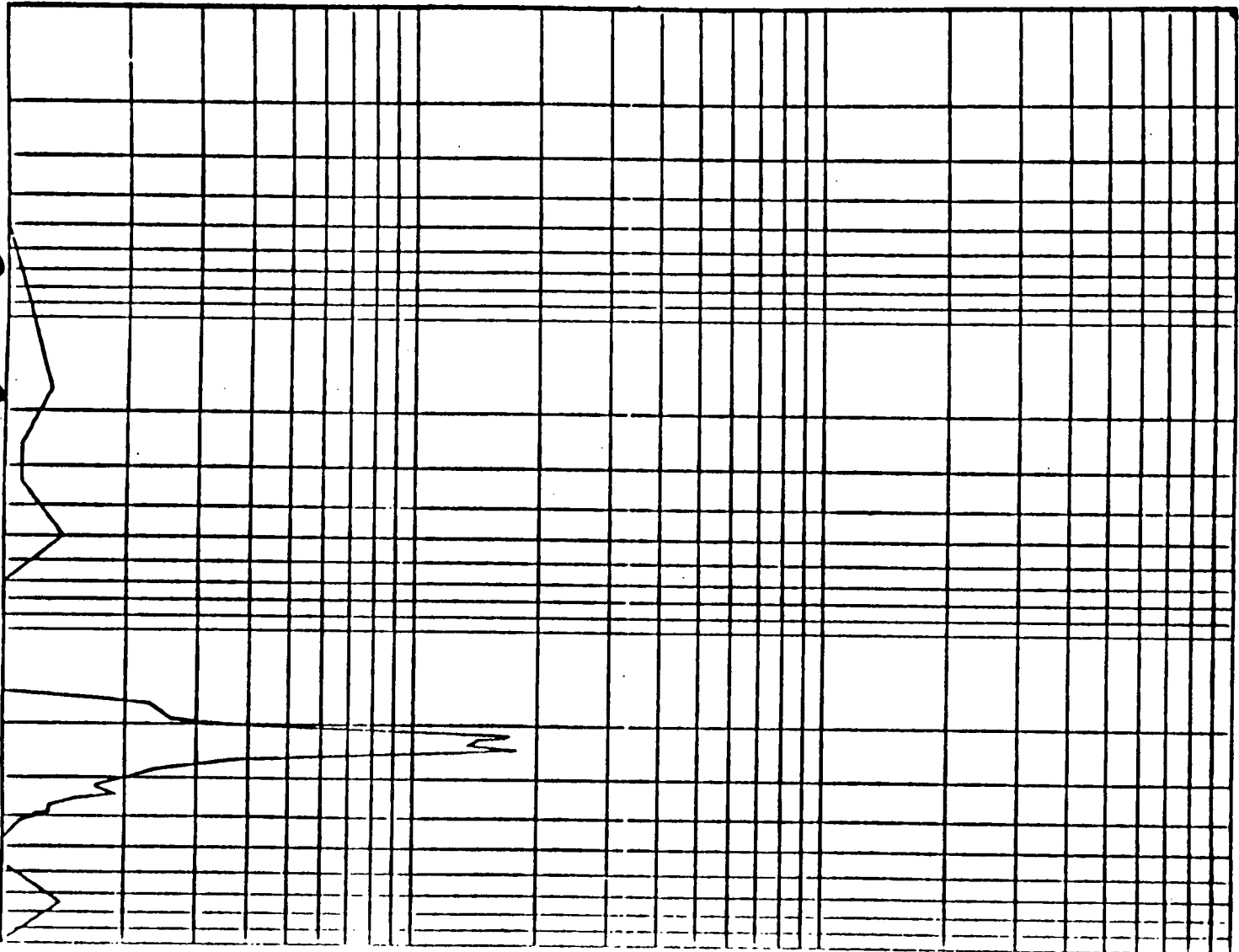
ACCELERATION (G)

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1.

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1
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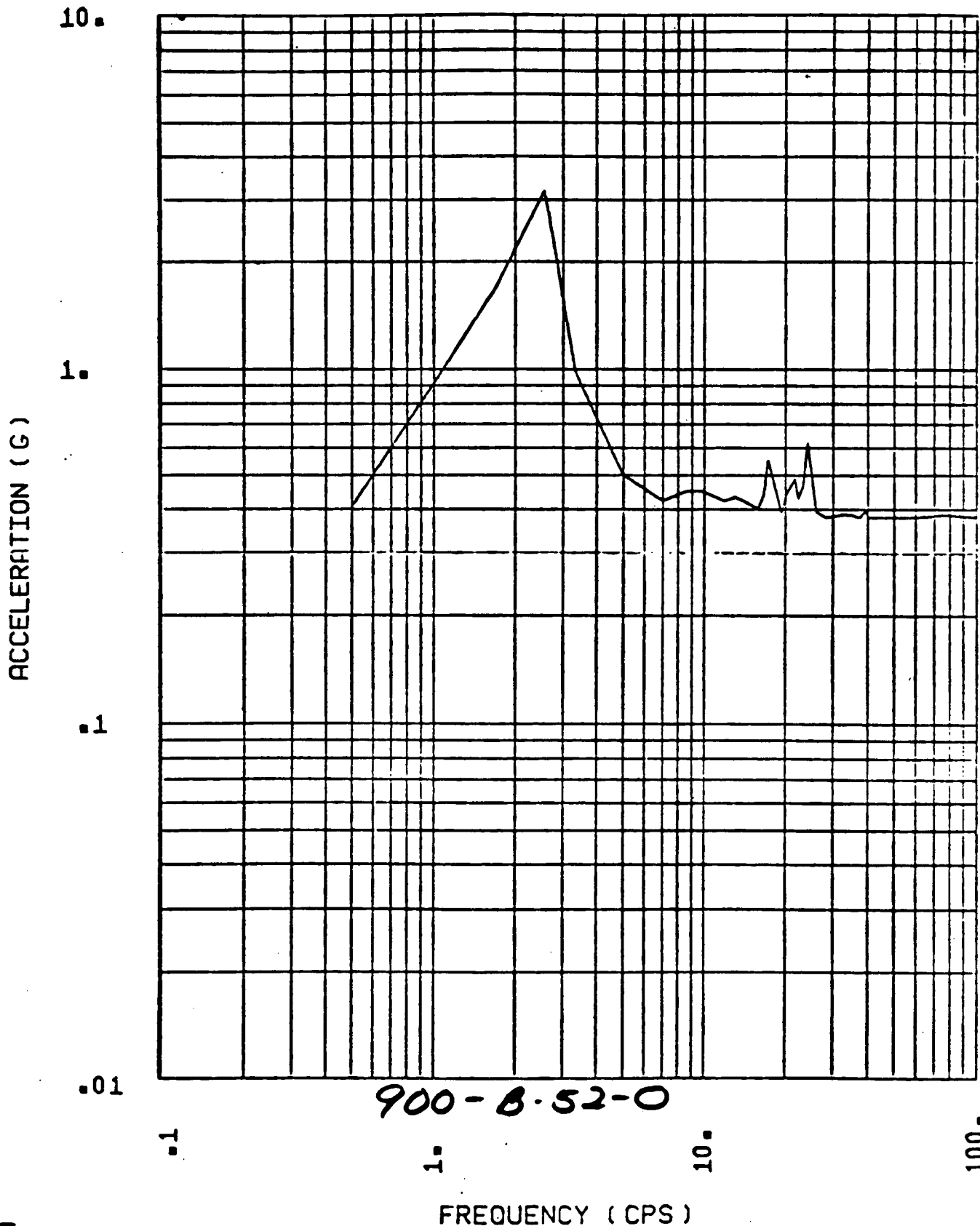
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Y-09E

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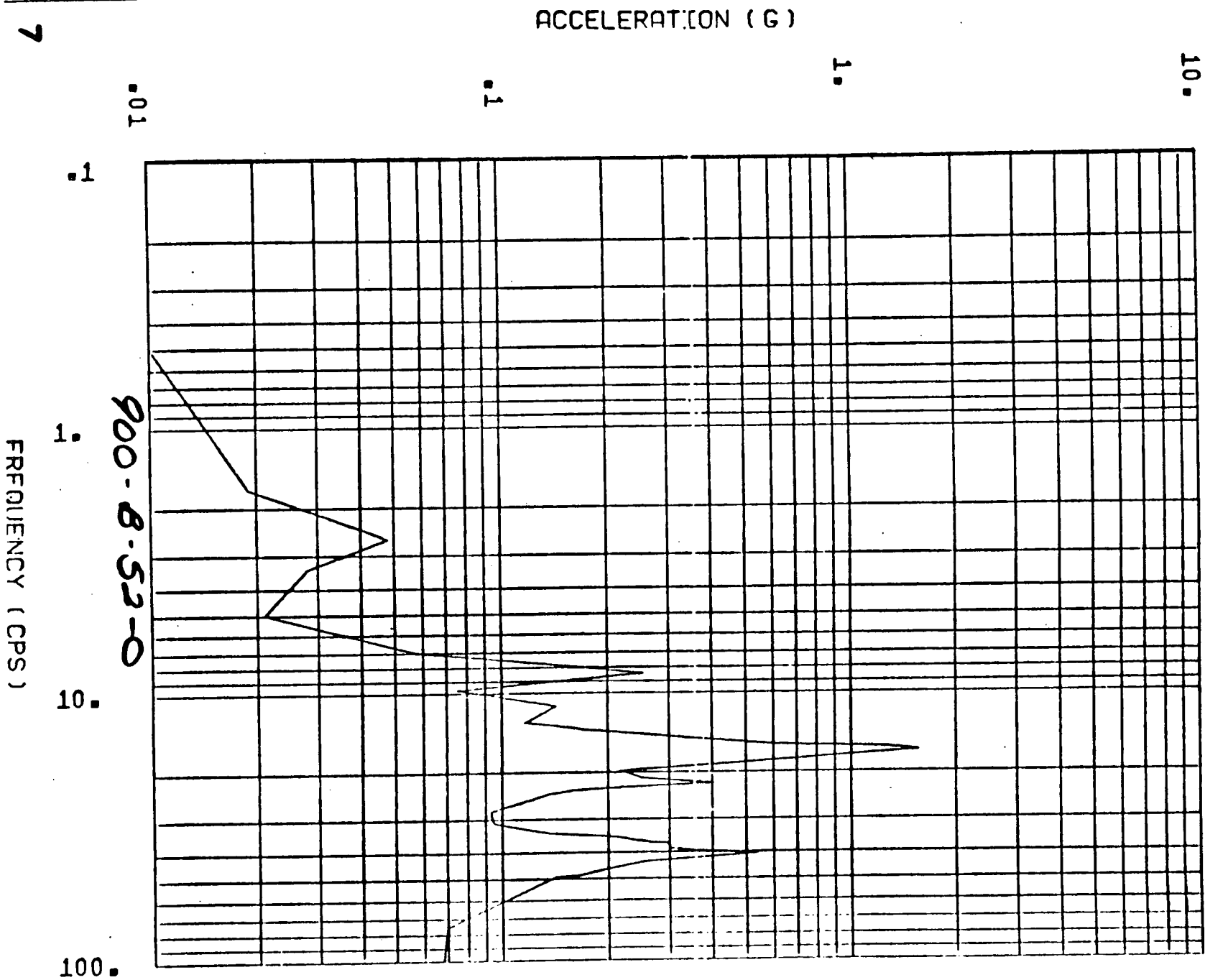
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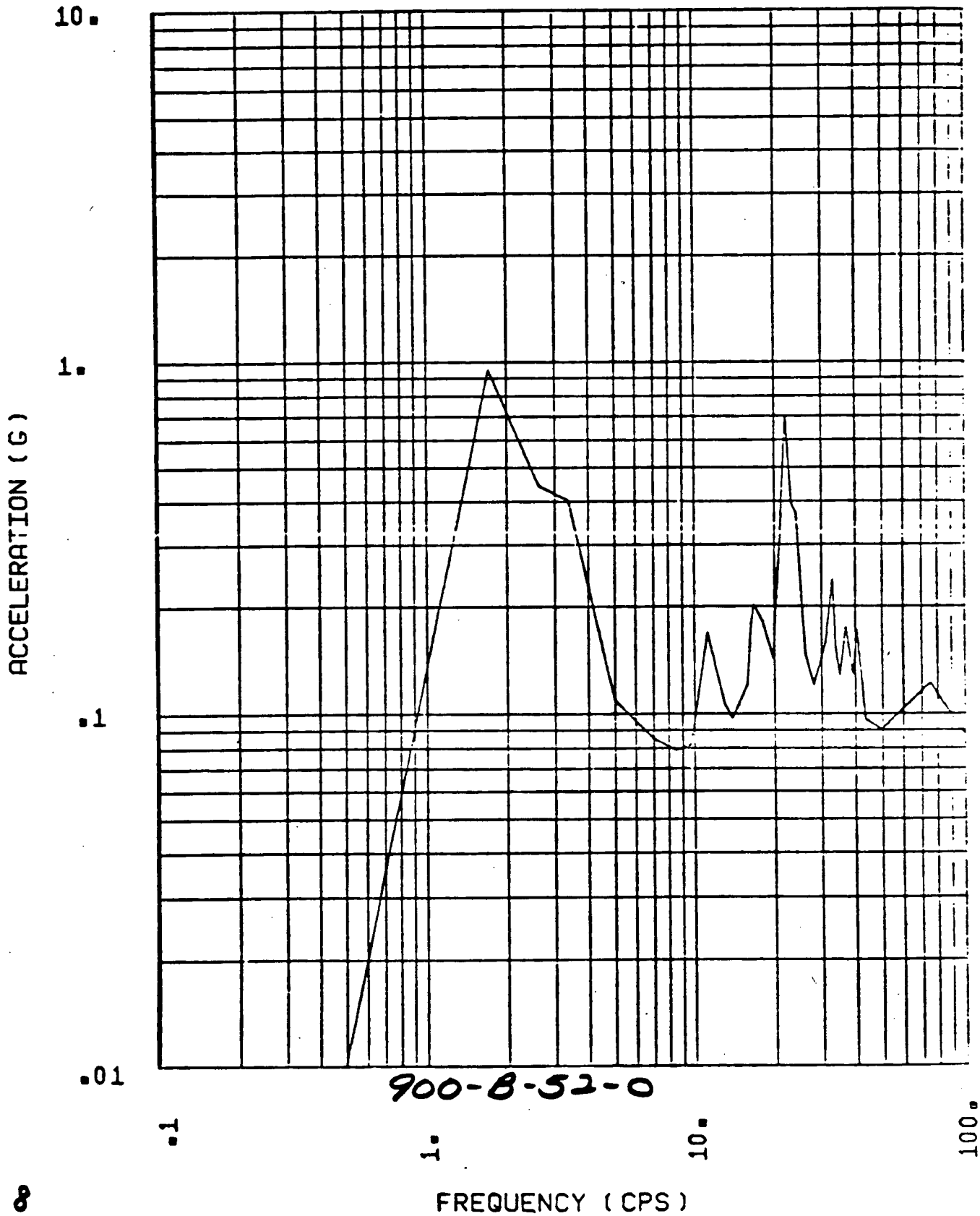
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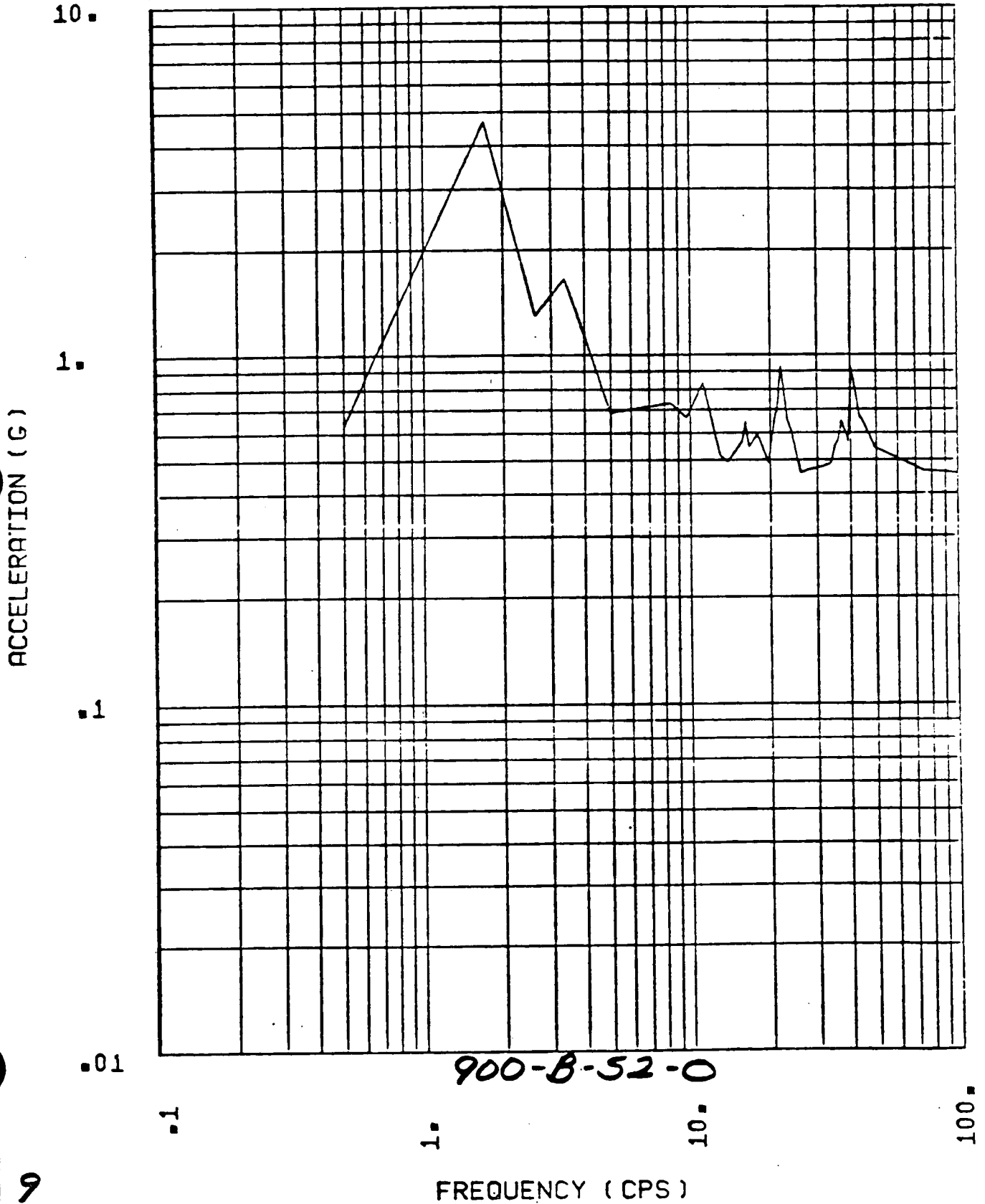
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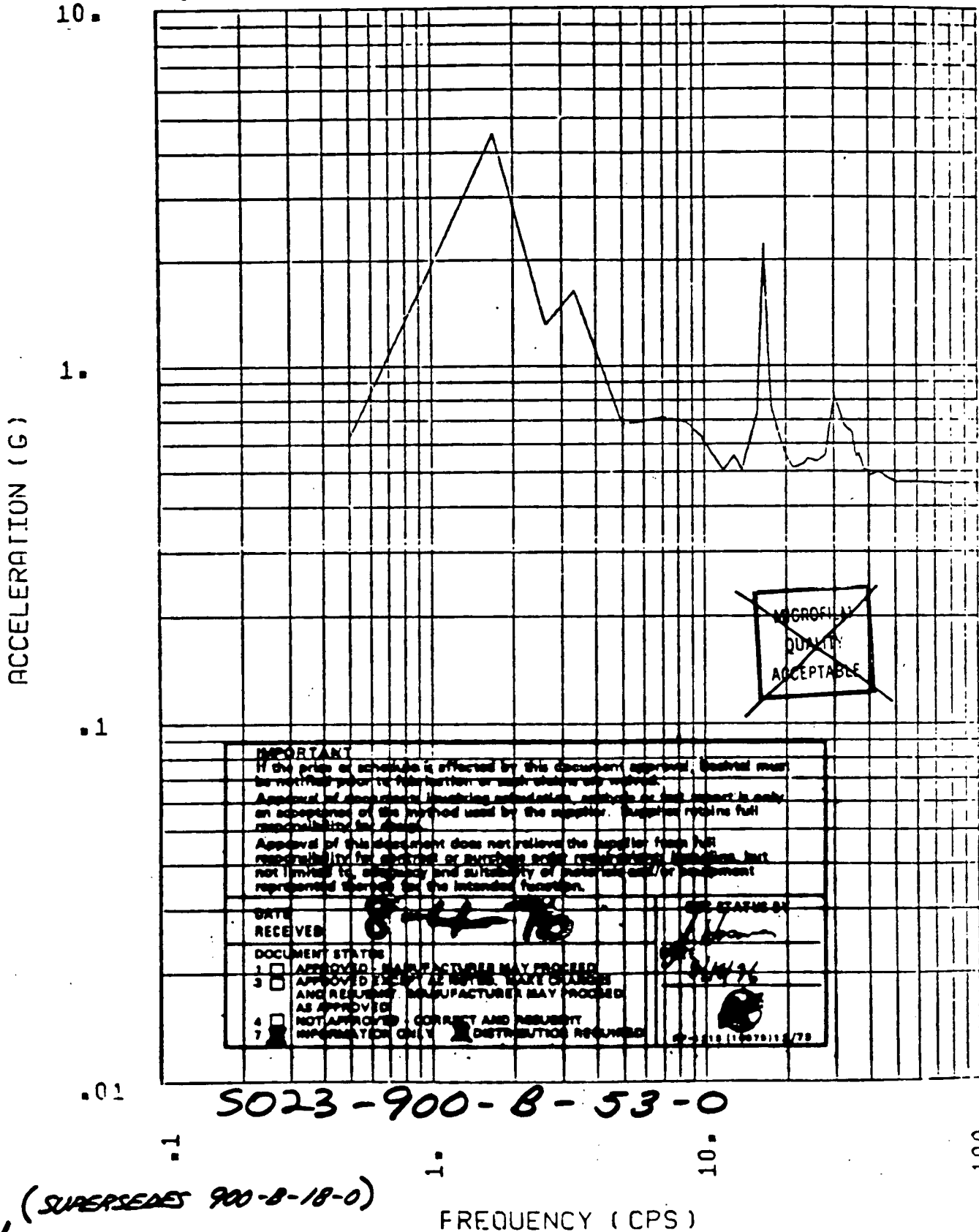
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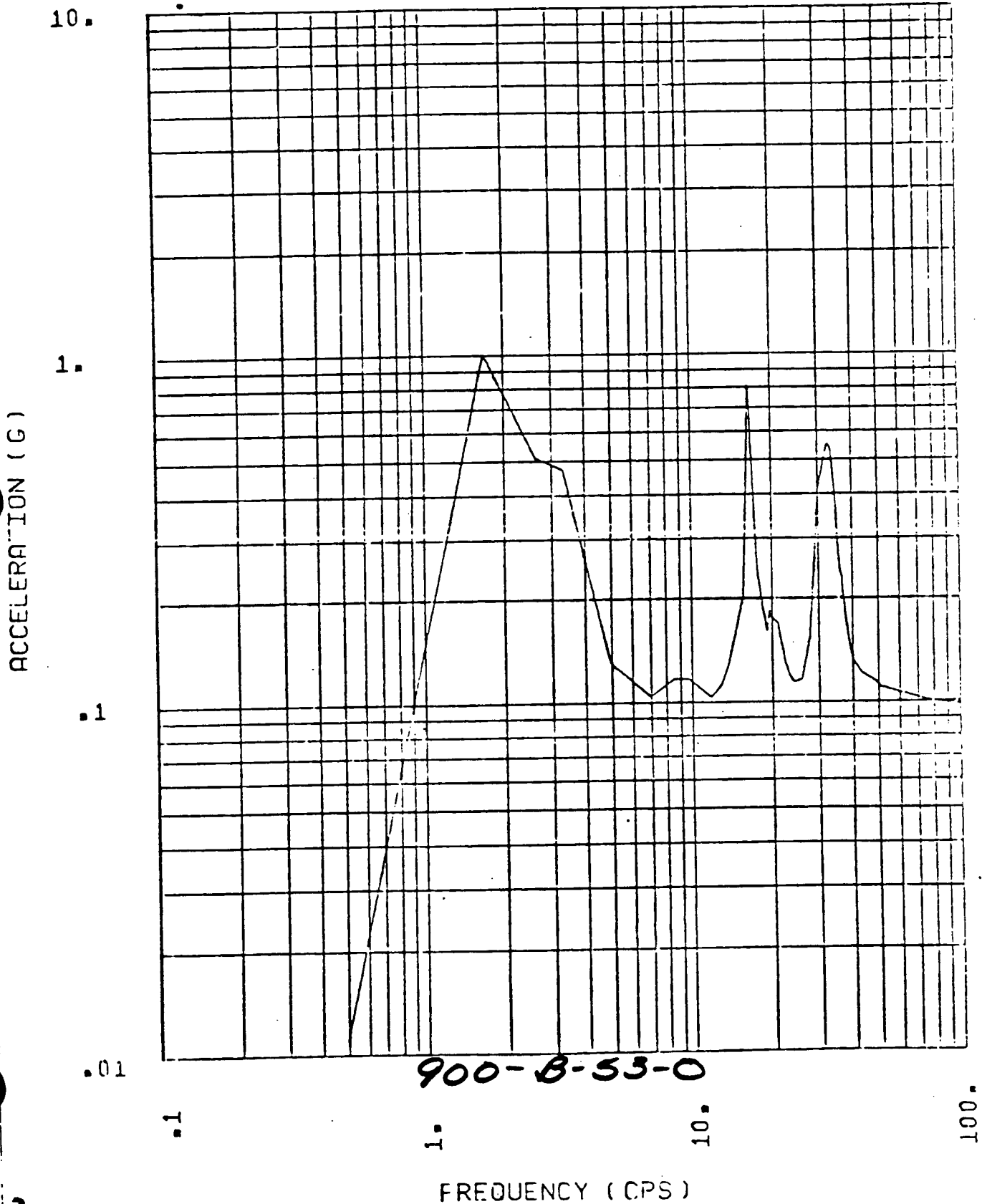
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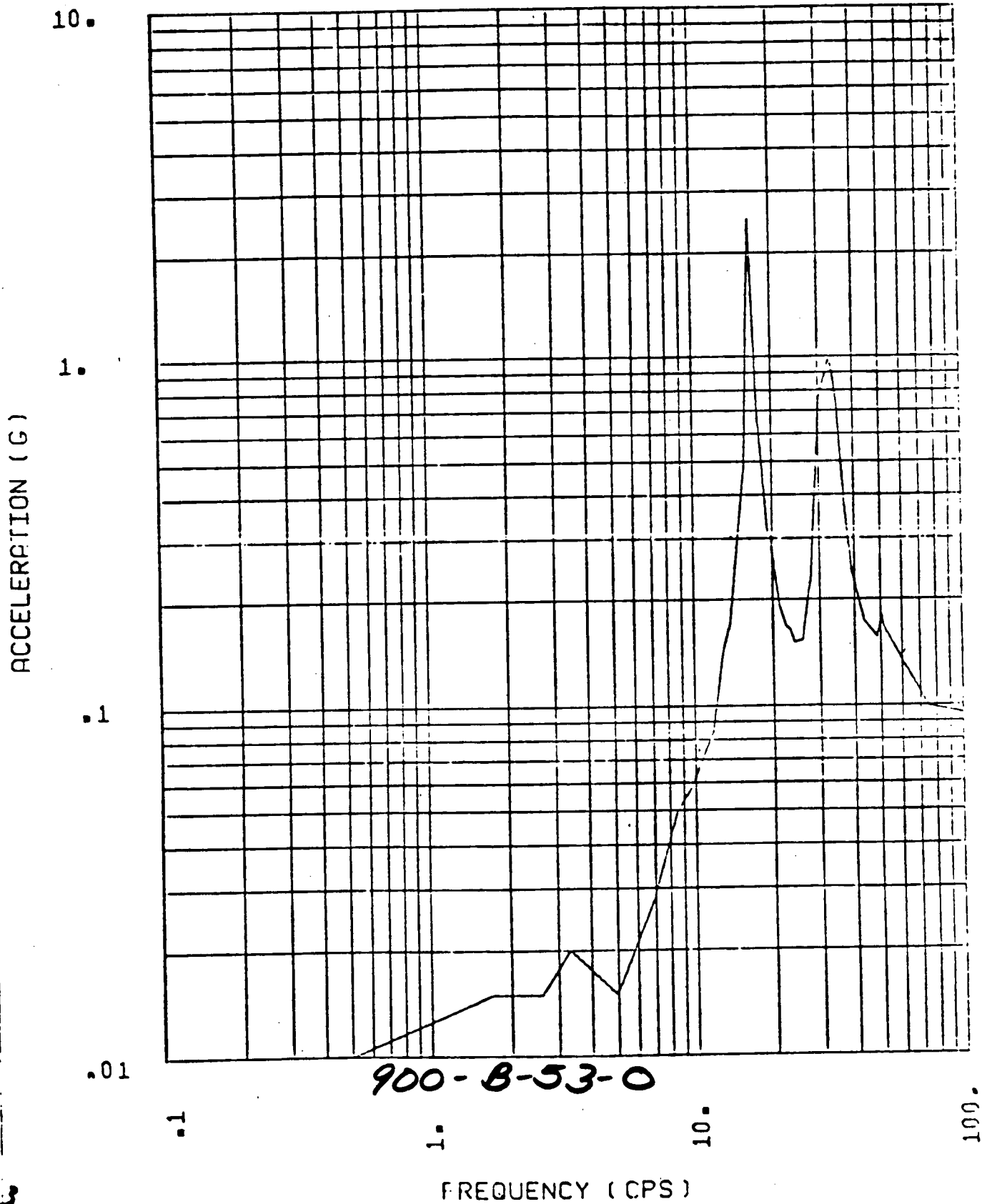
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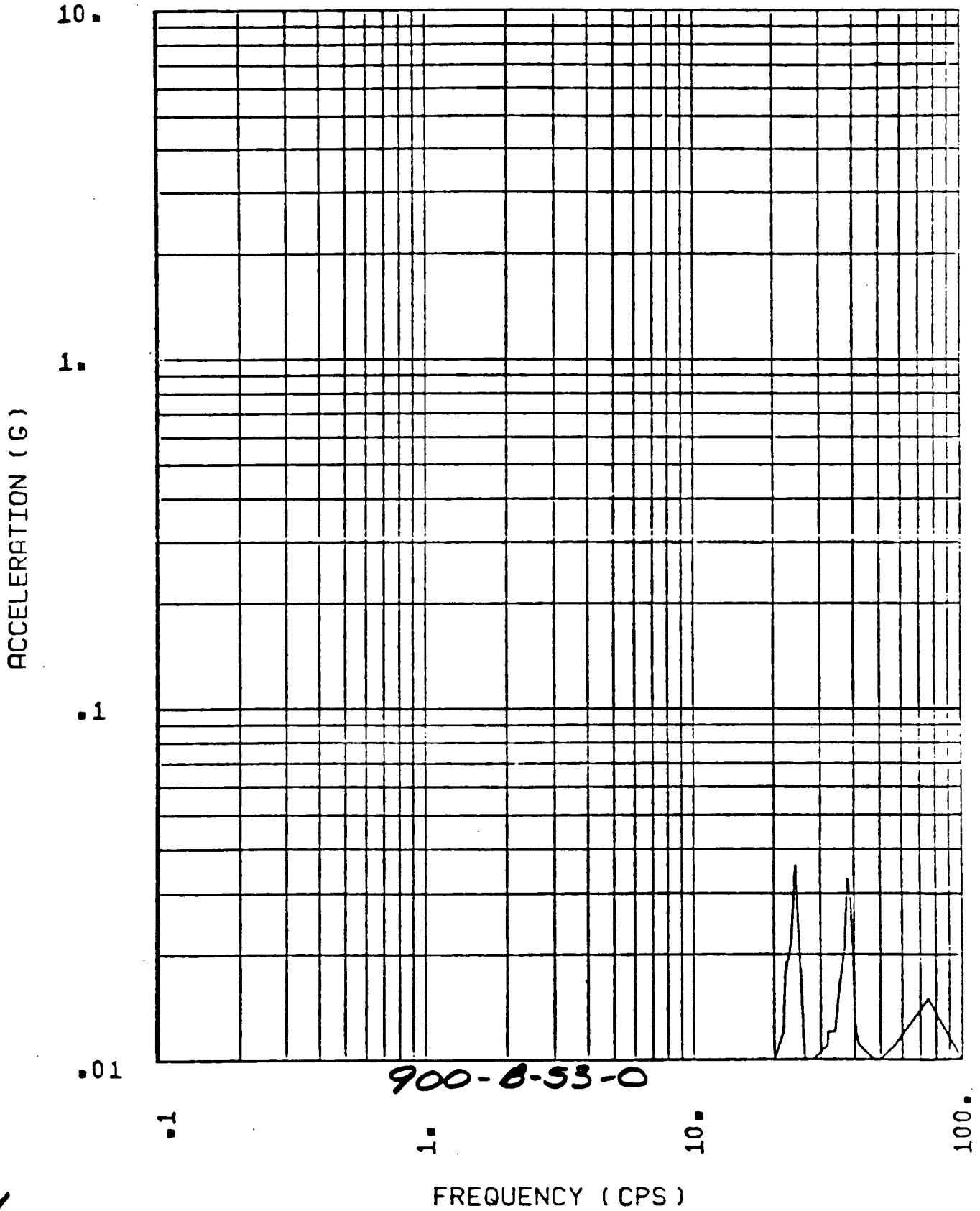


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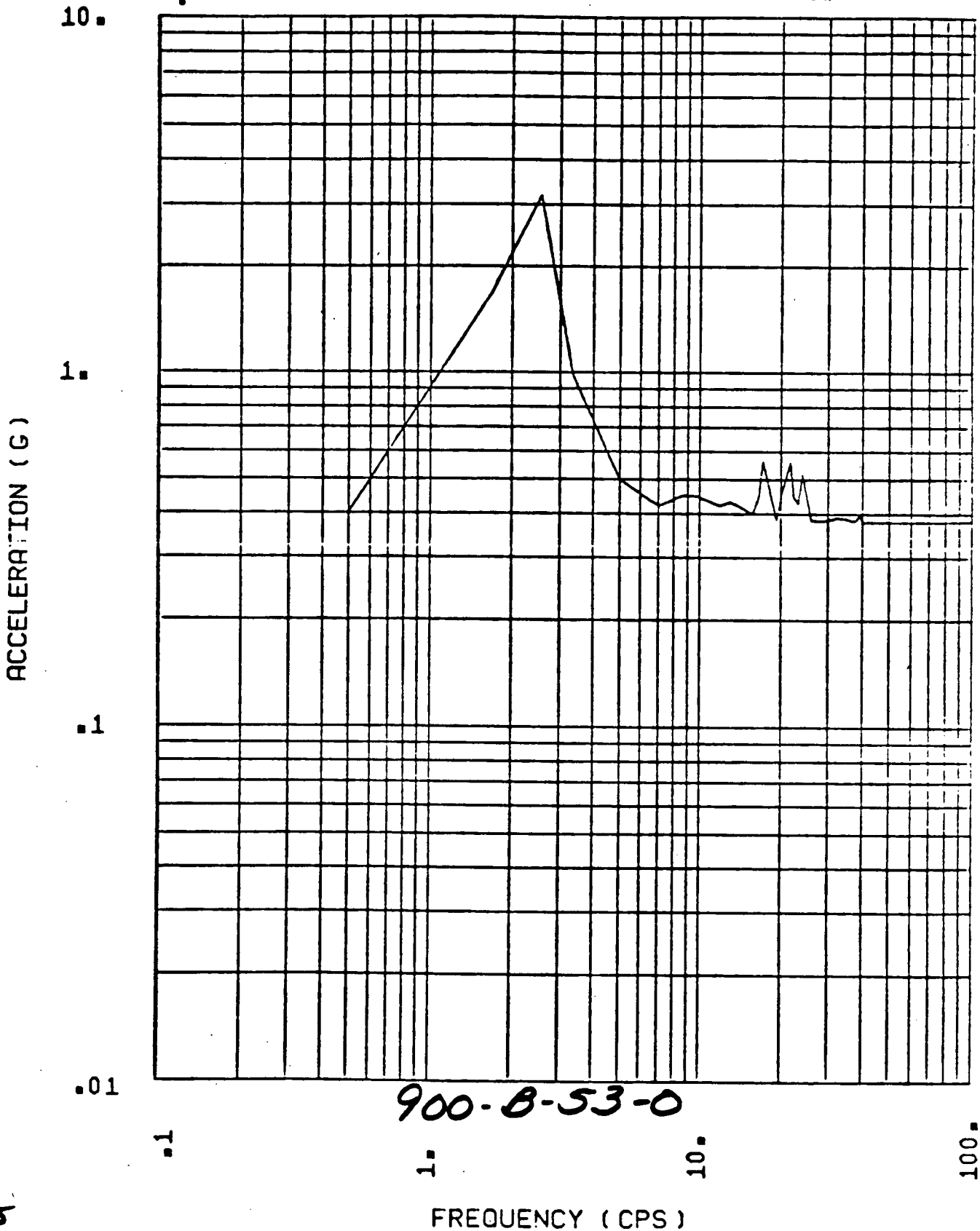
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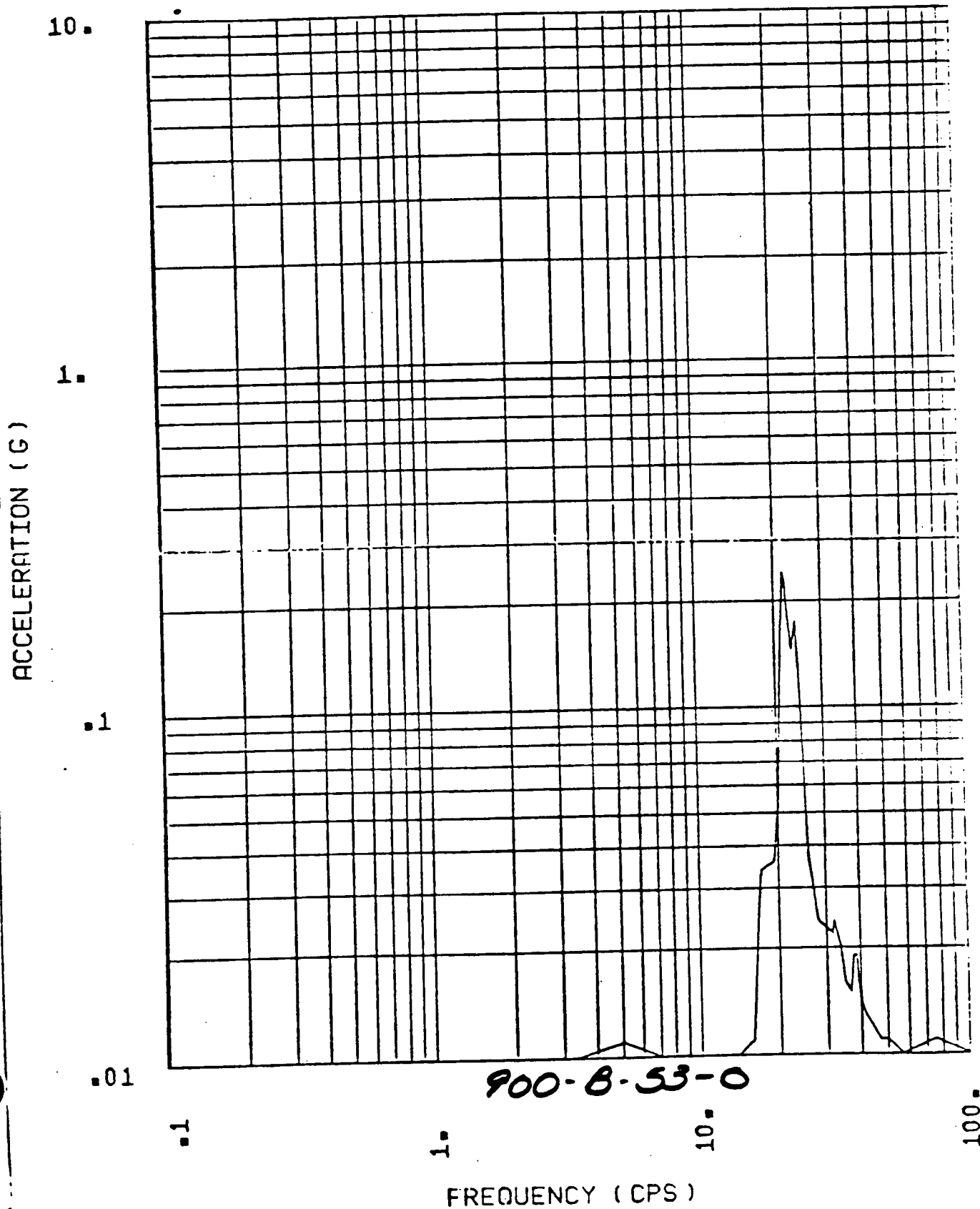
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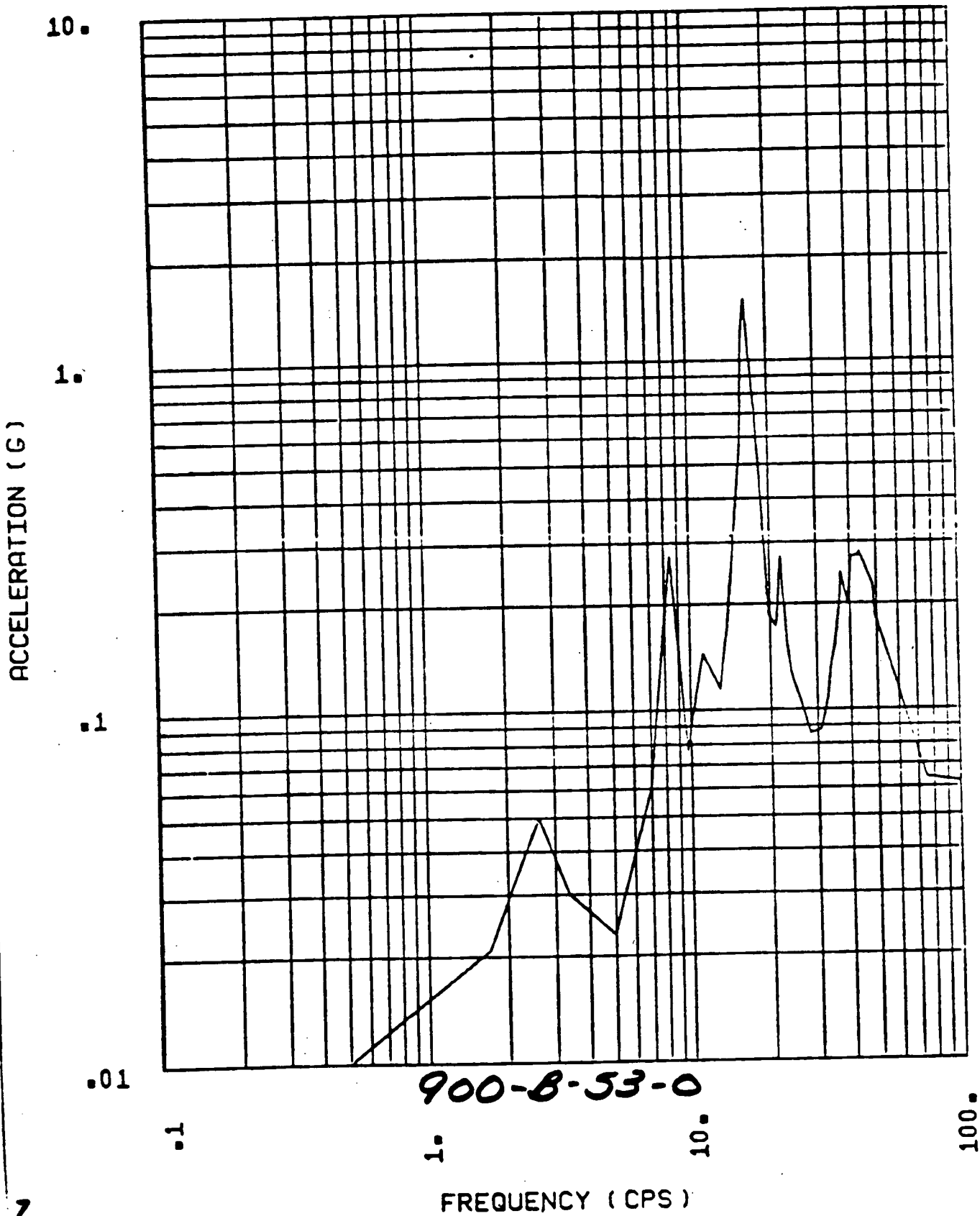
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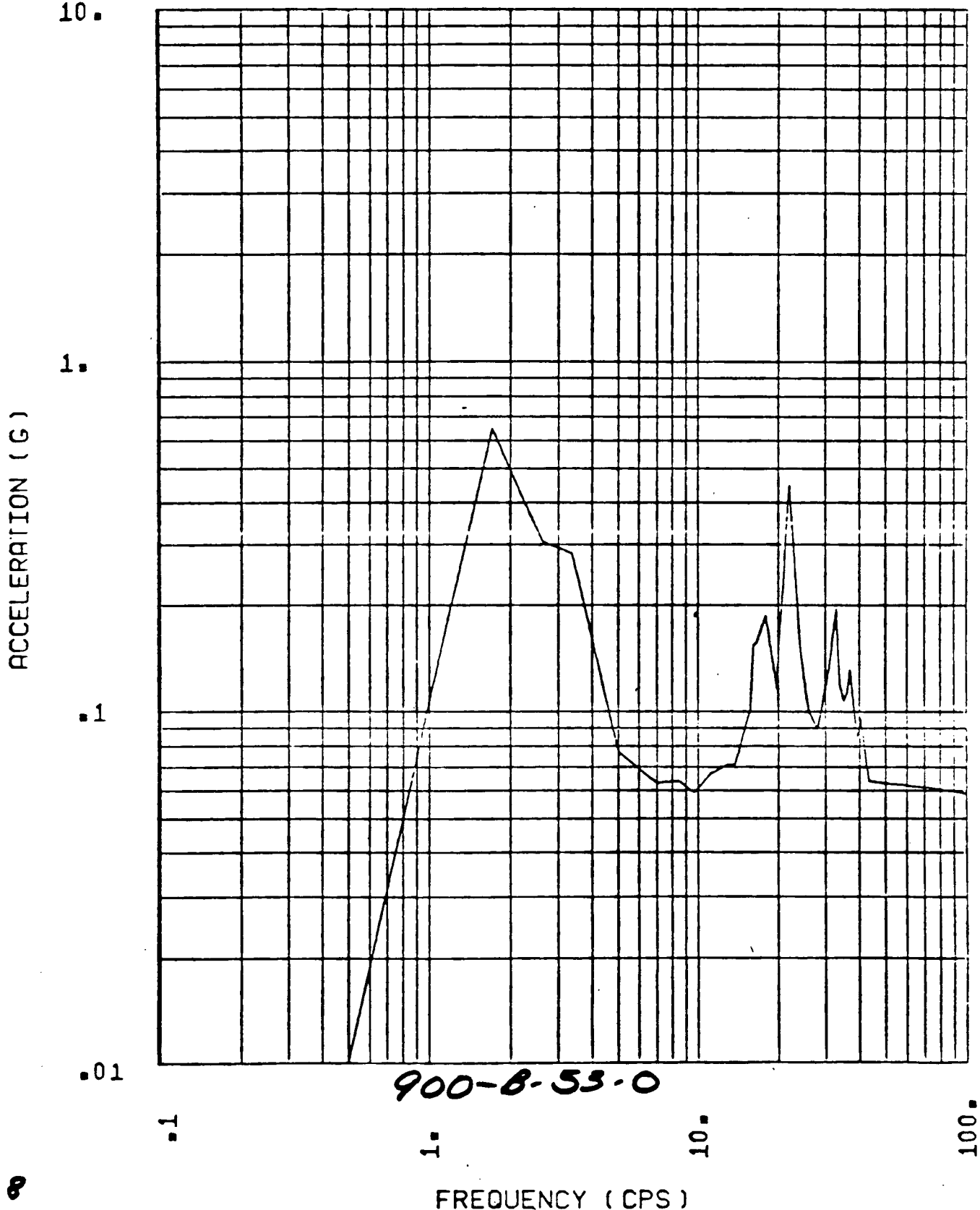
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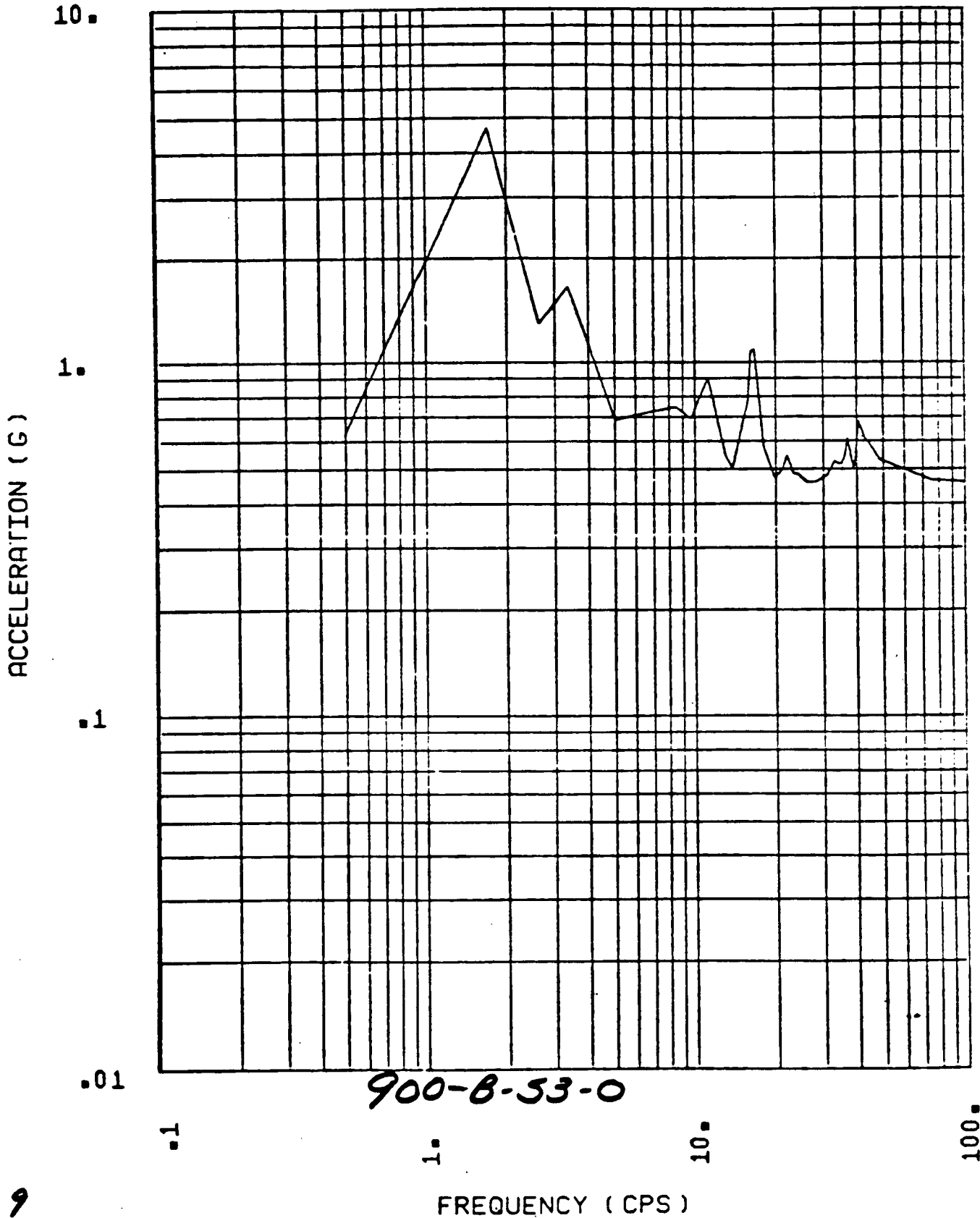
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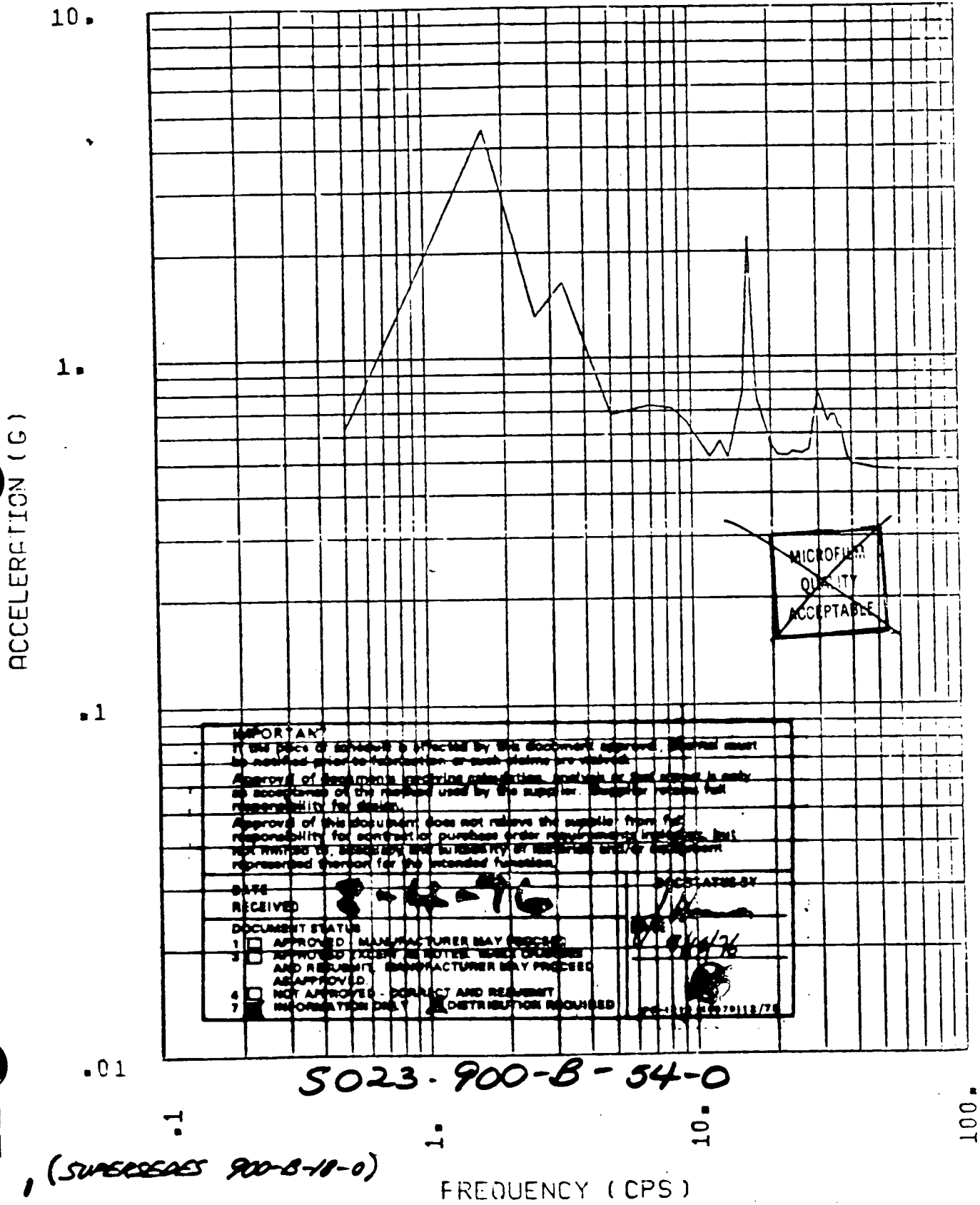


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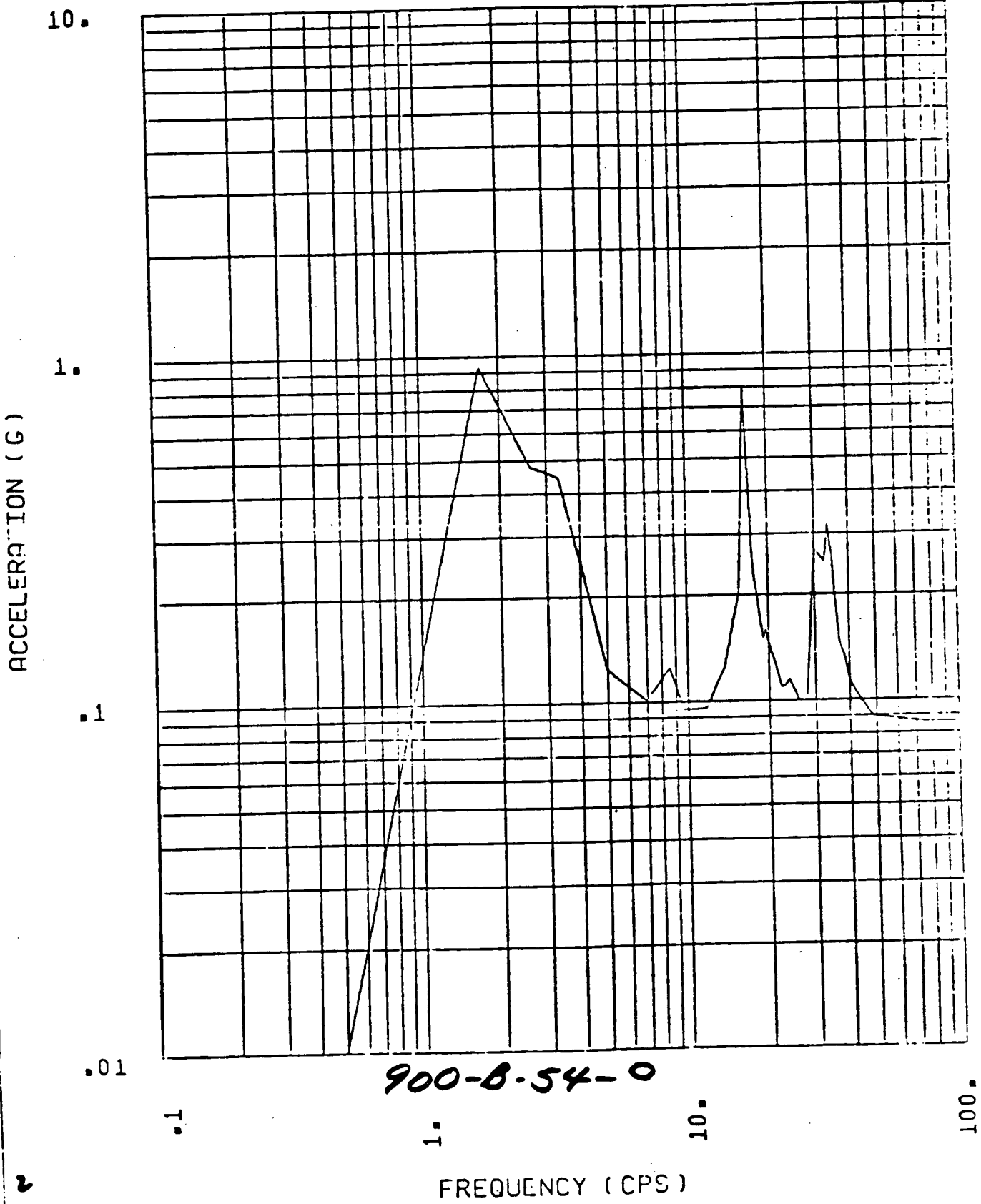
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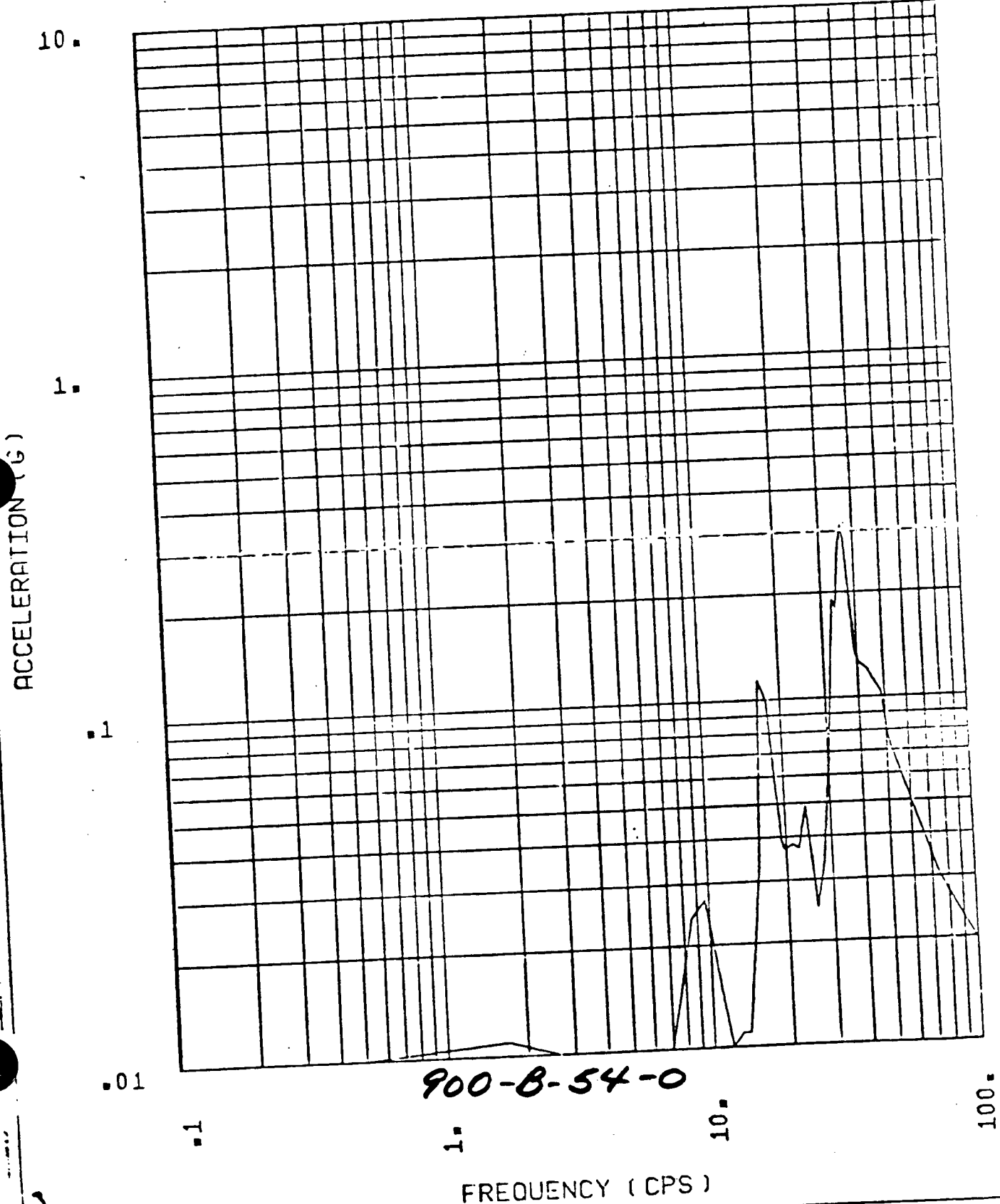
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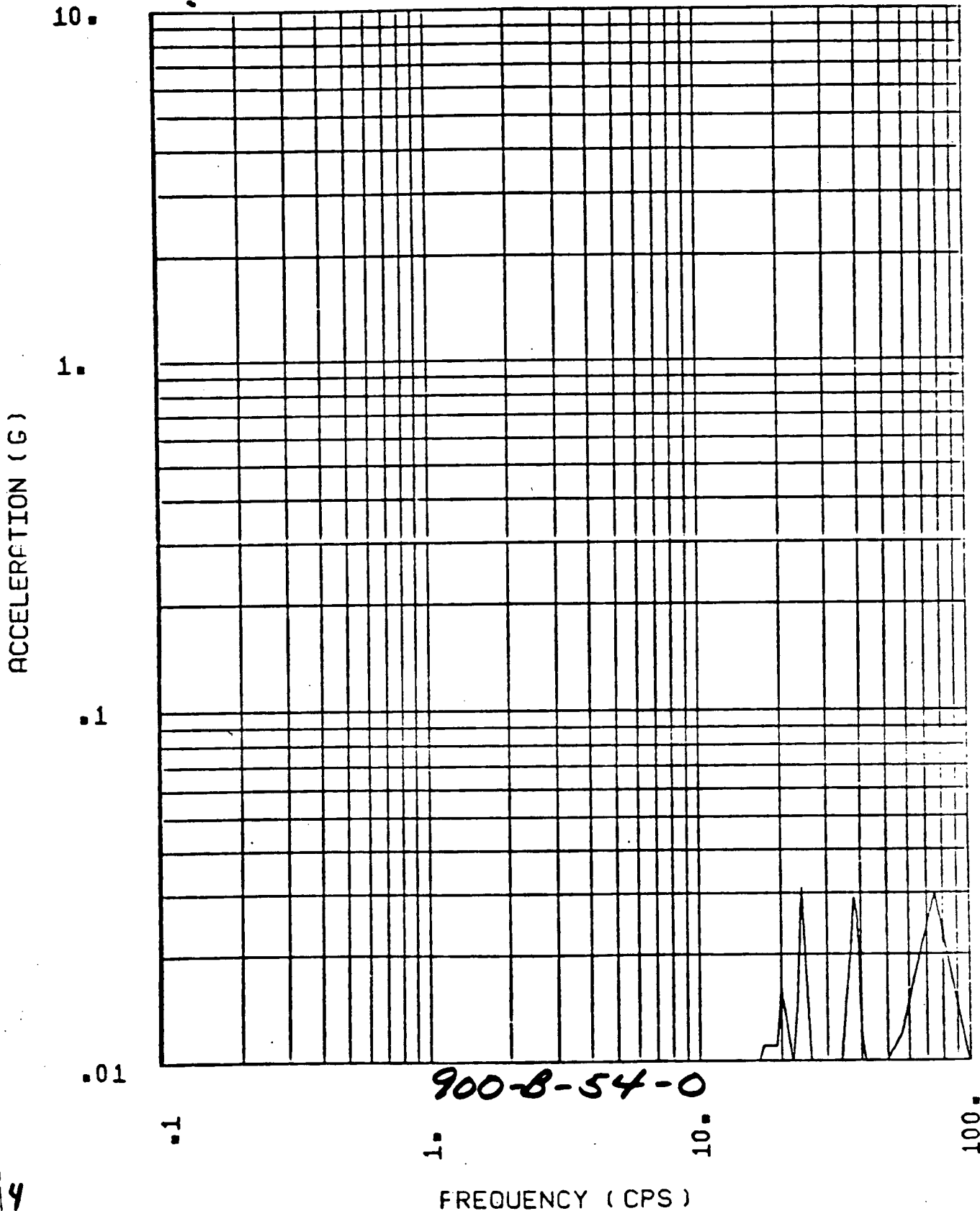


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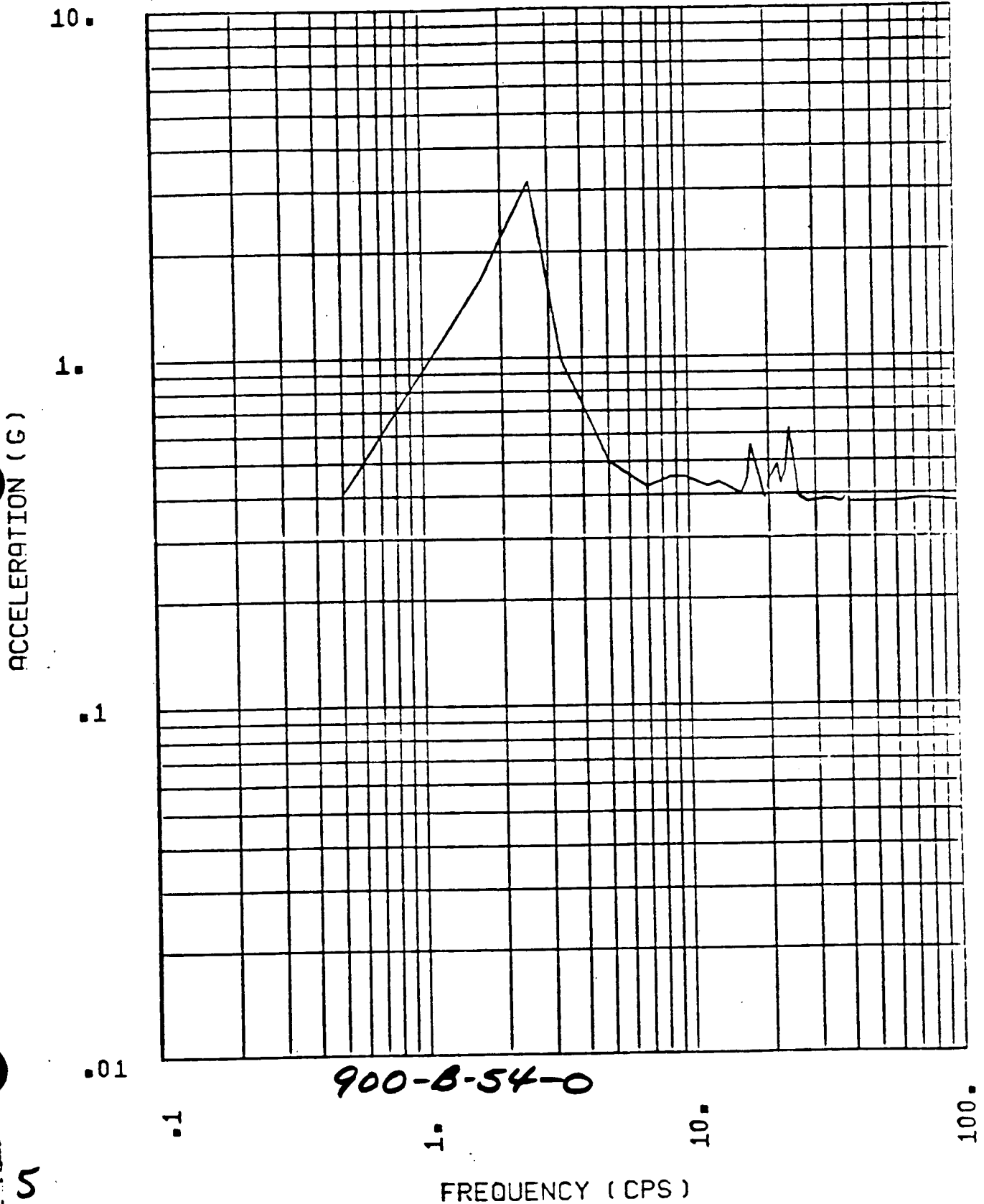
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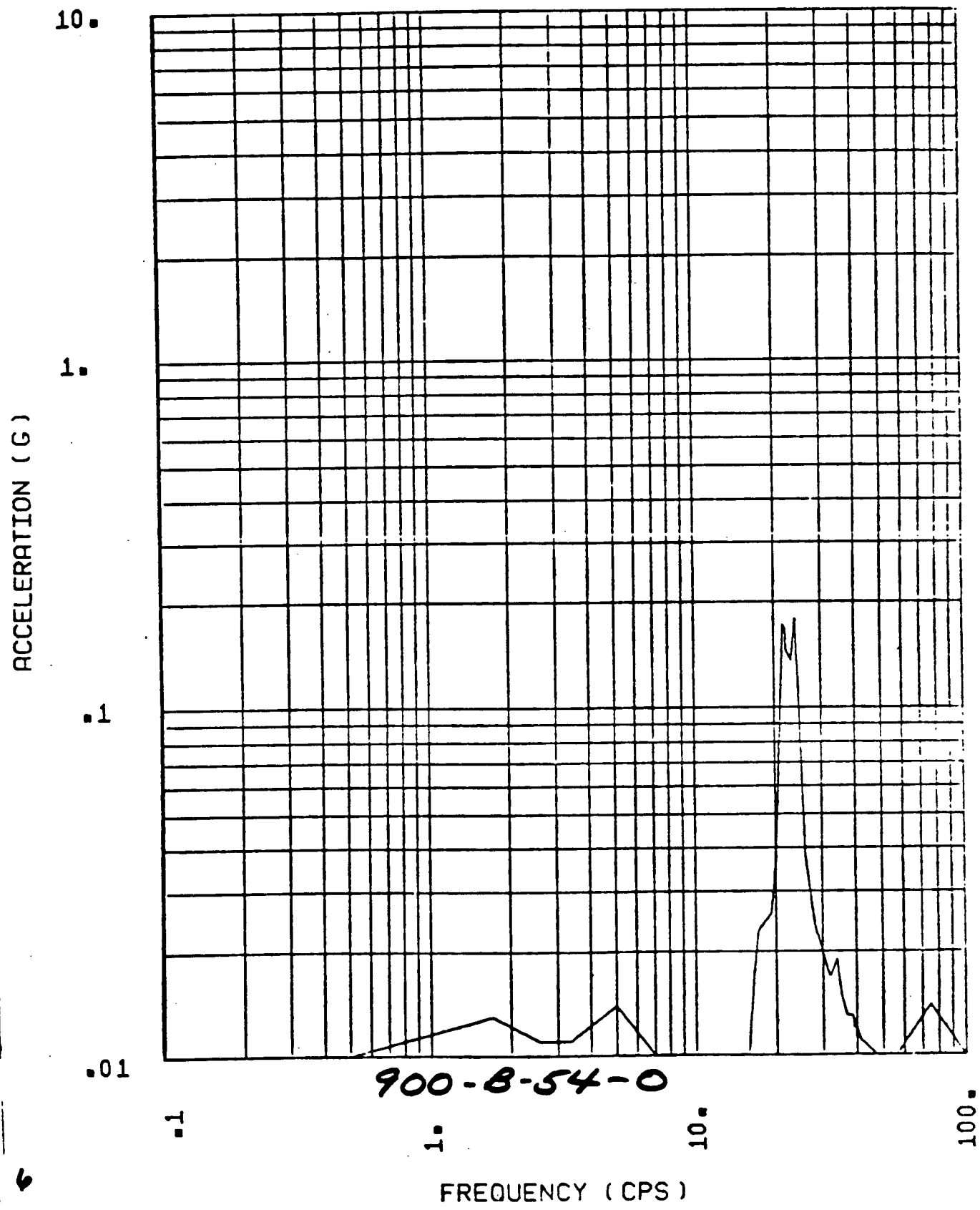
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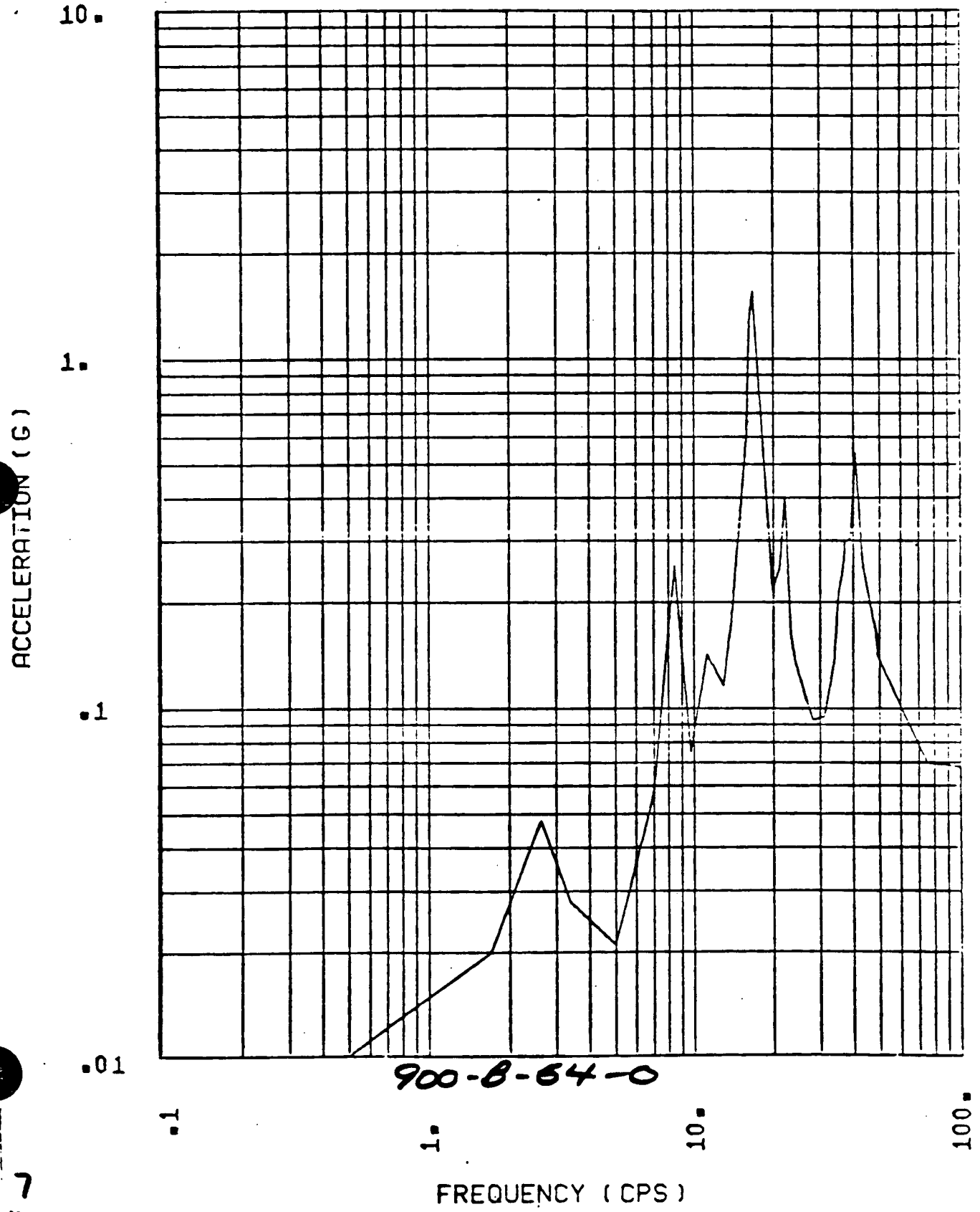
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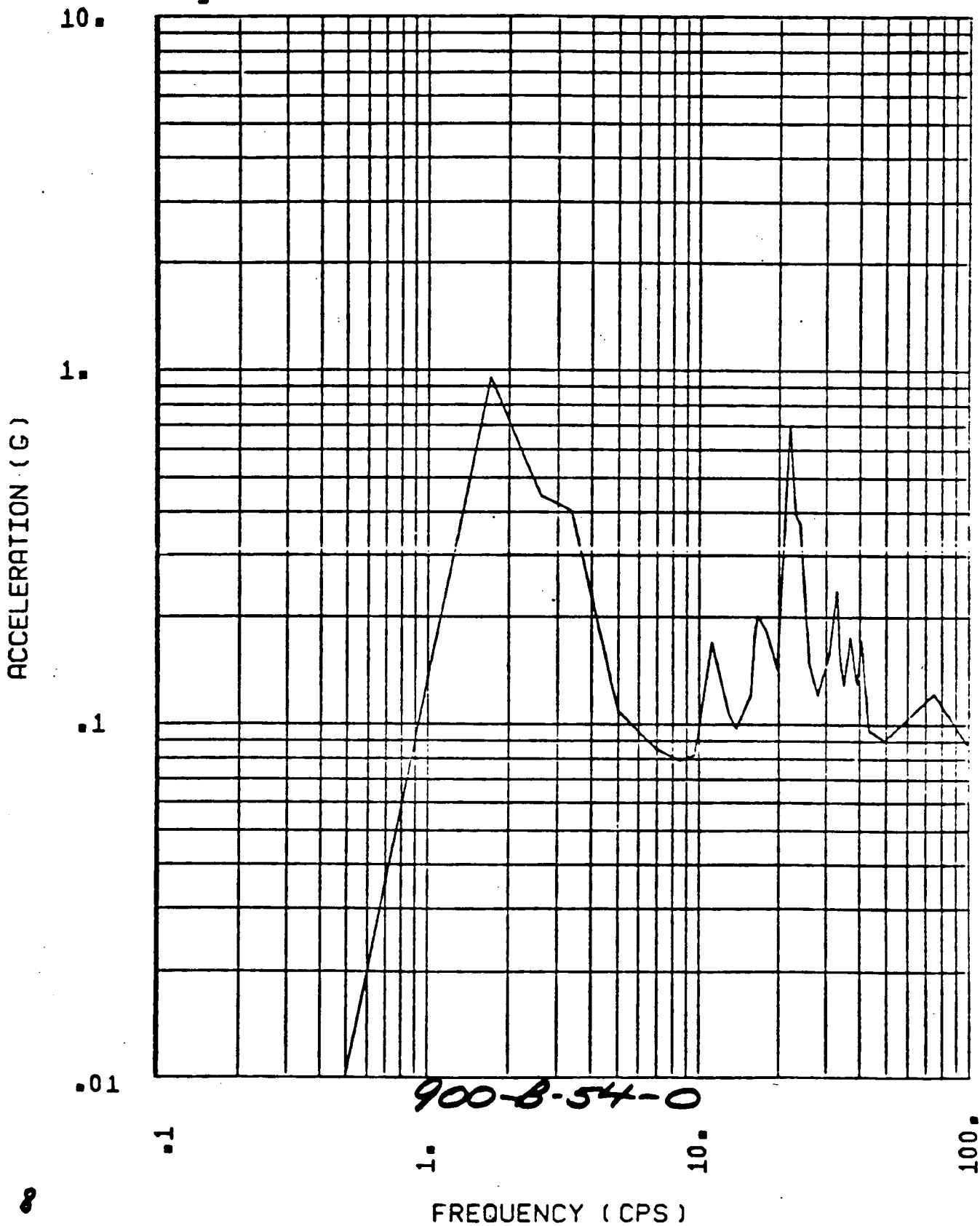
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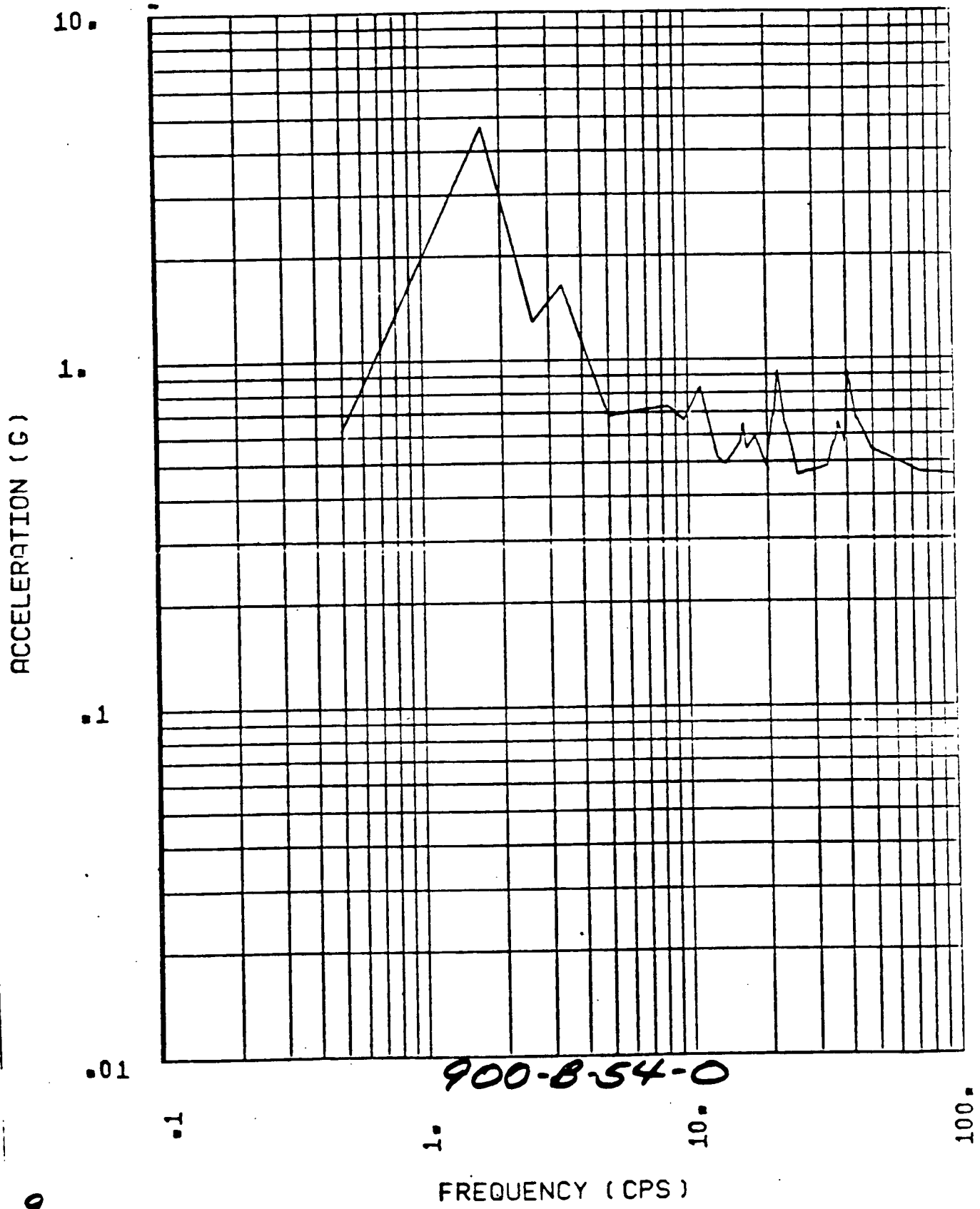
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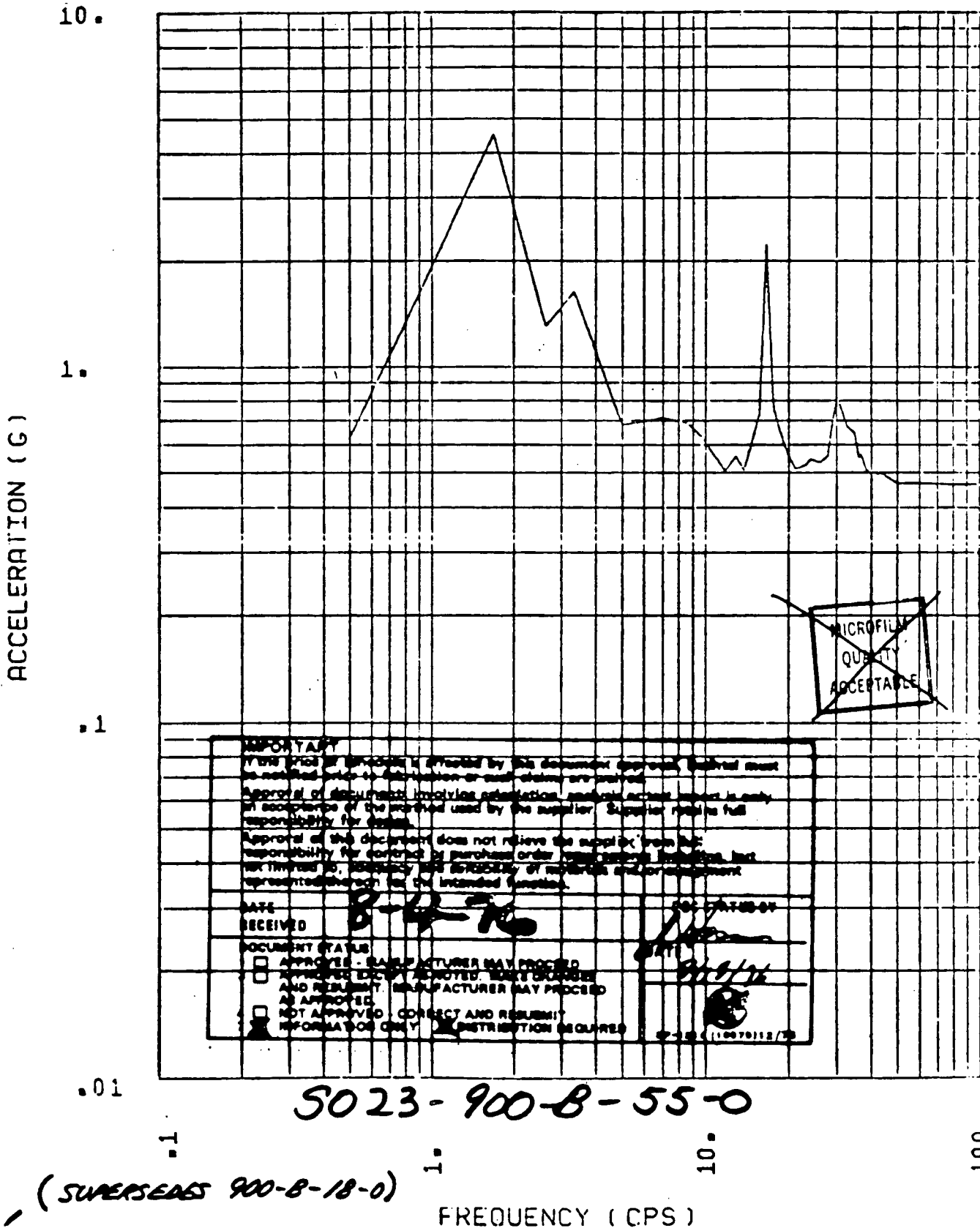
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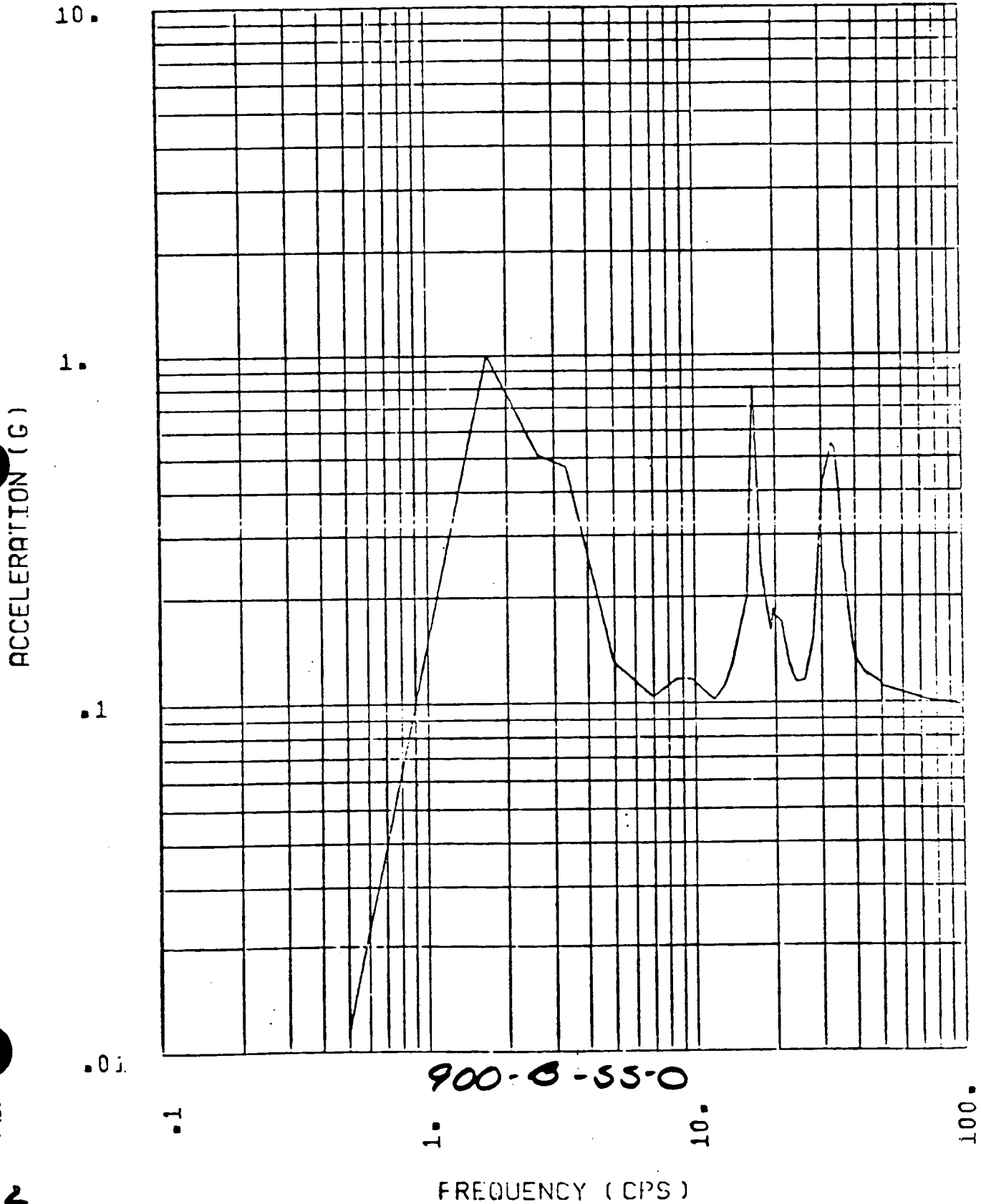
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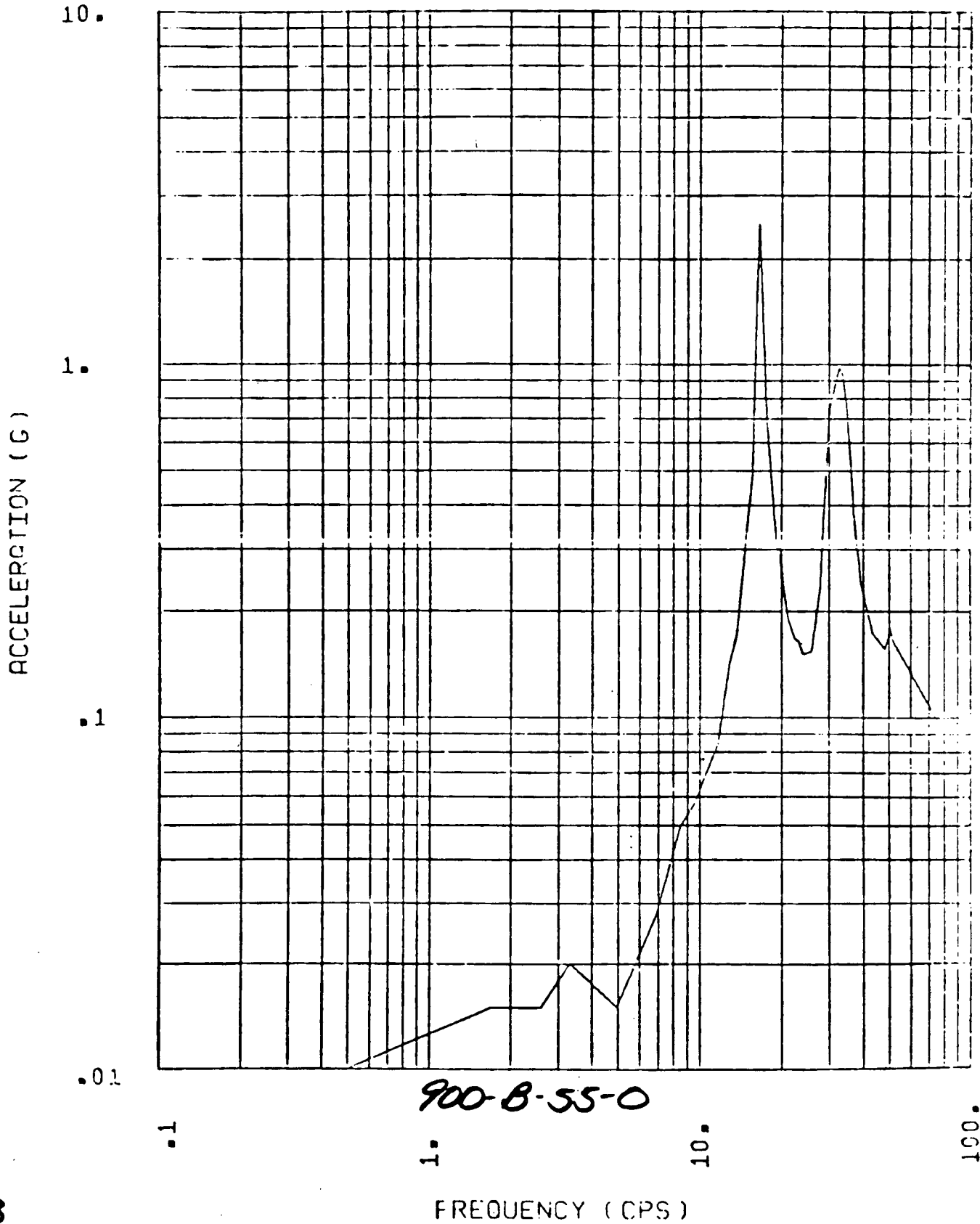
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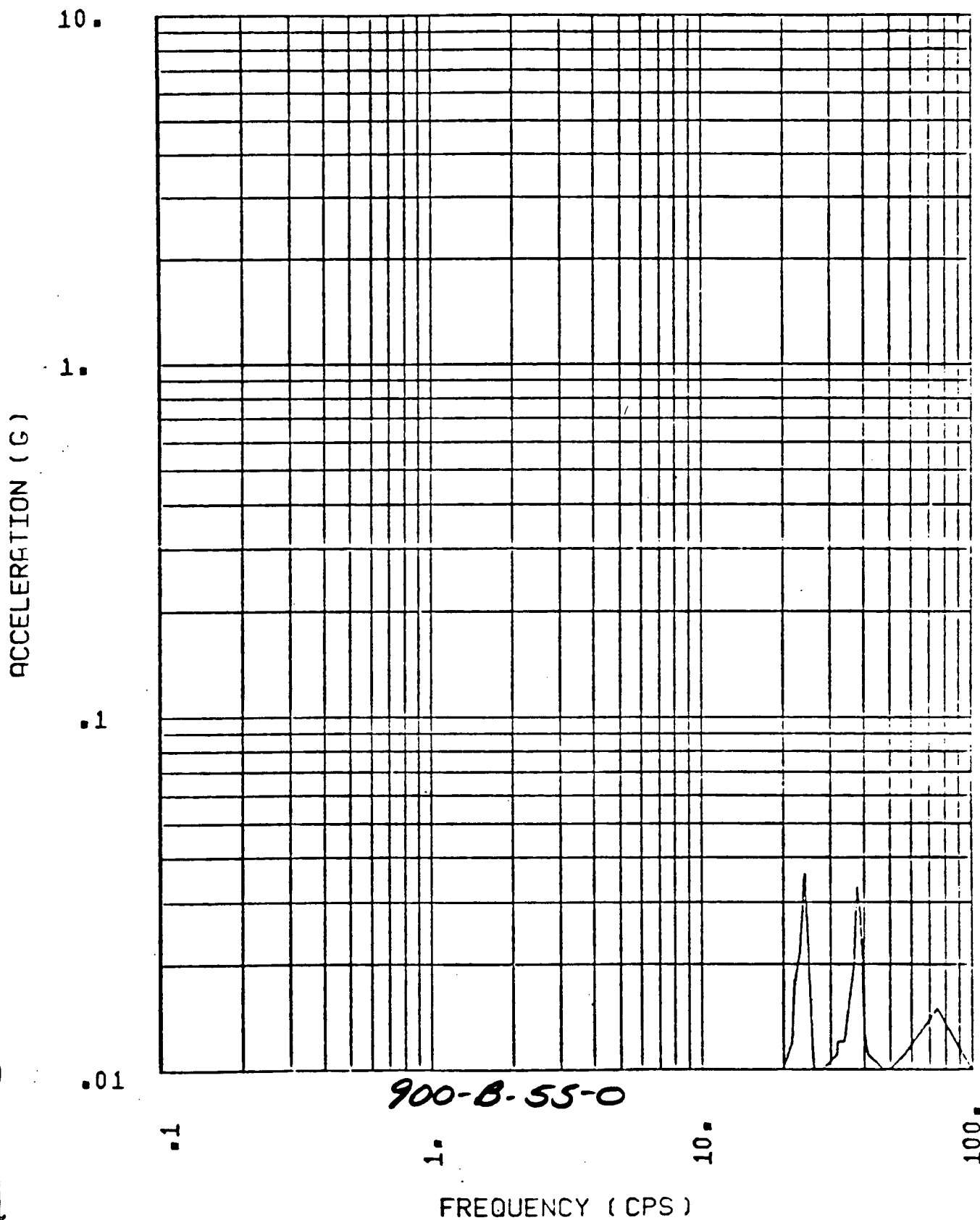
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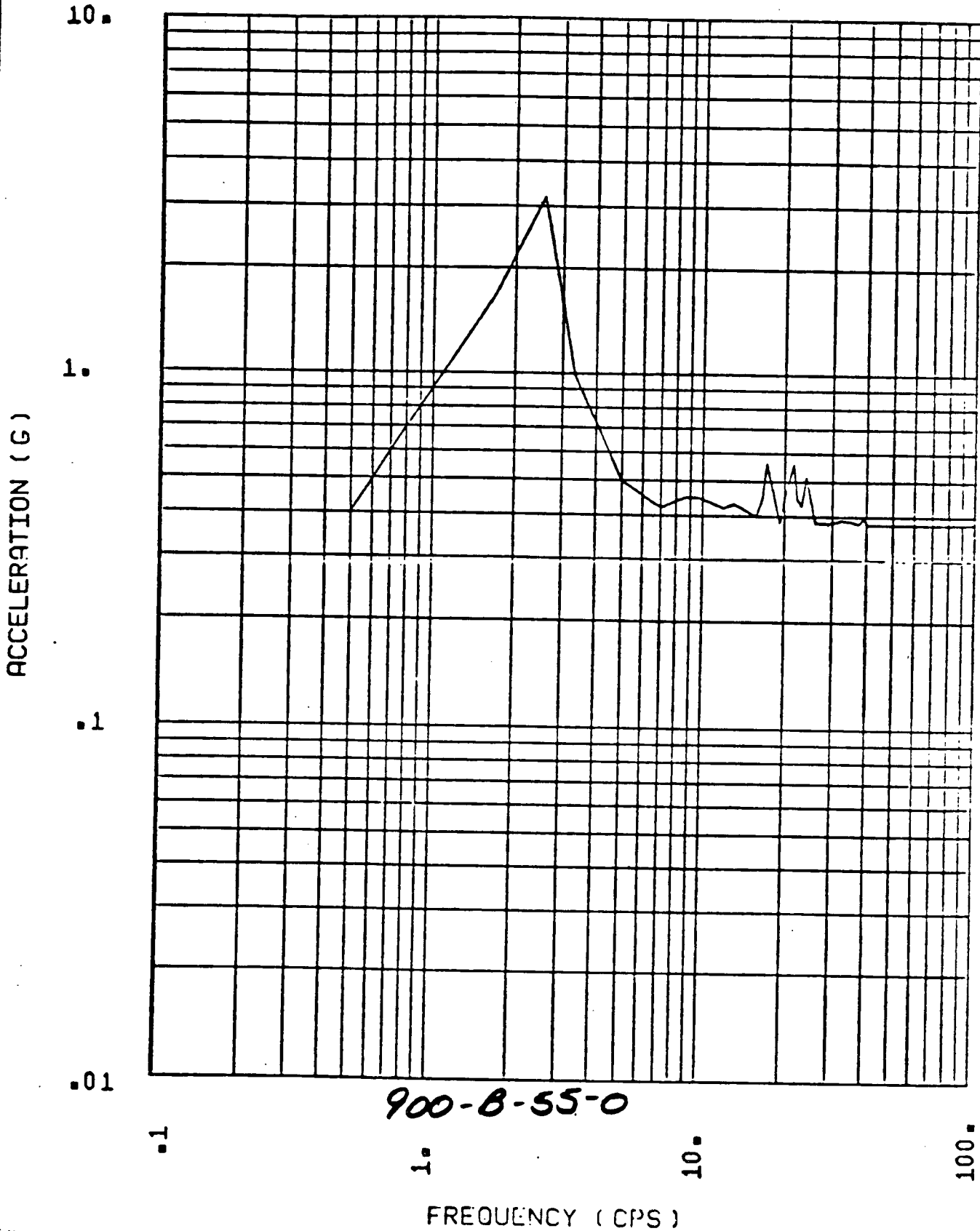
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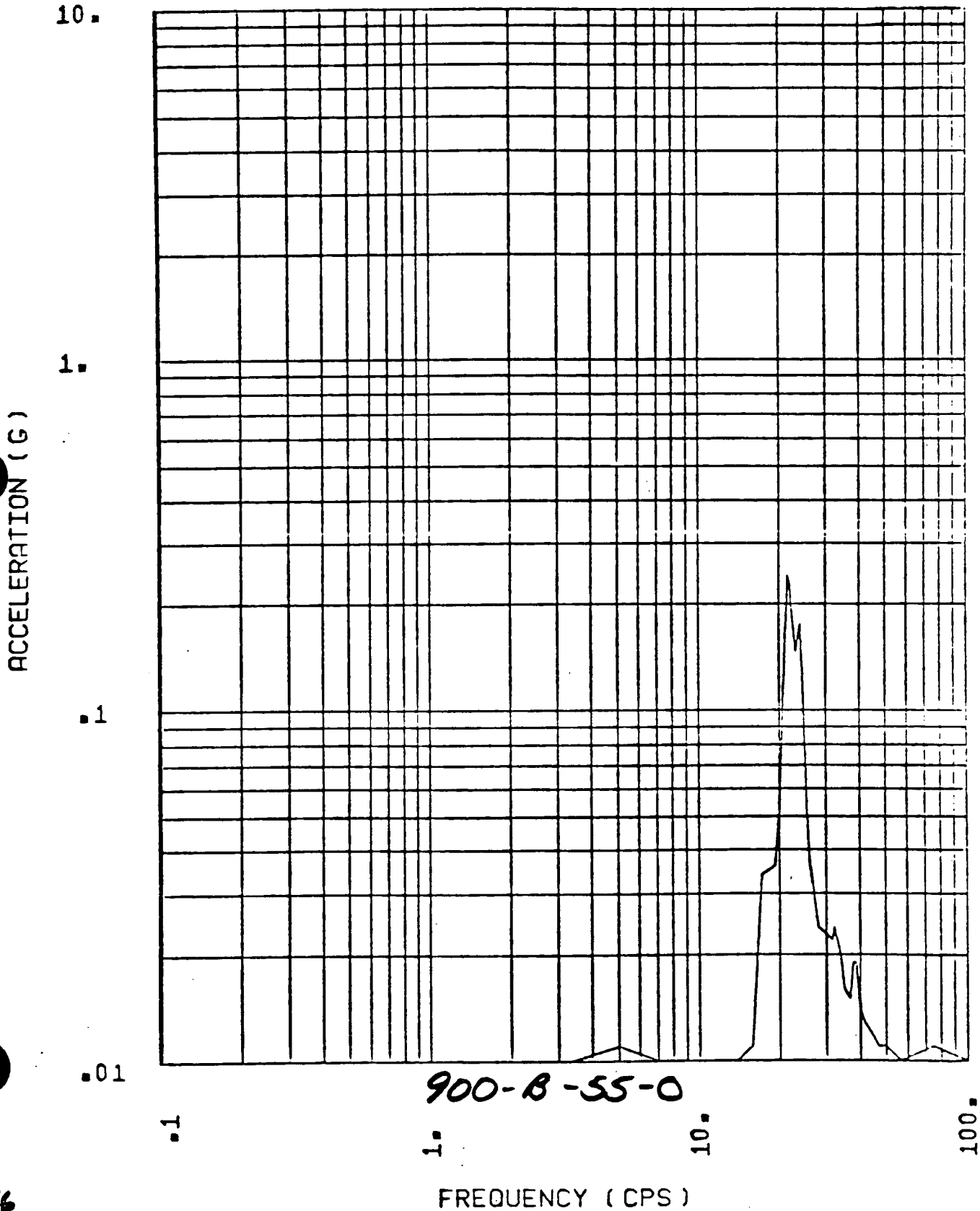
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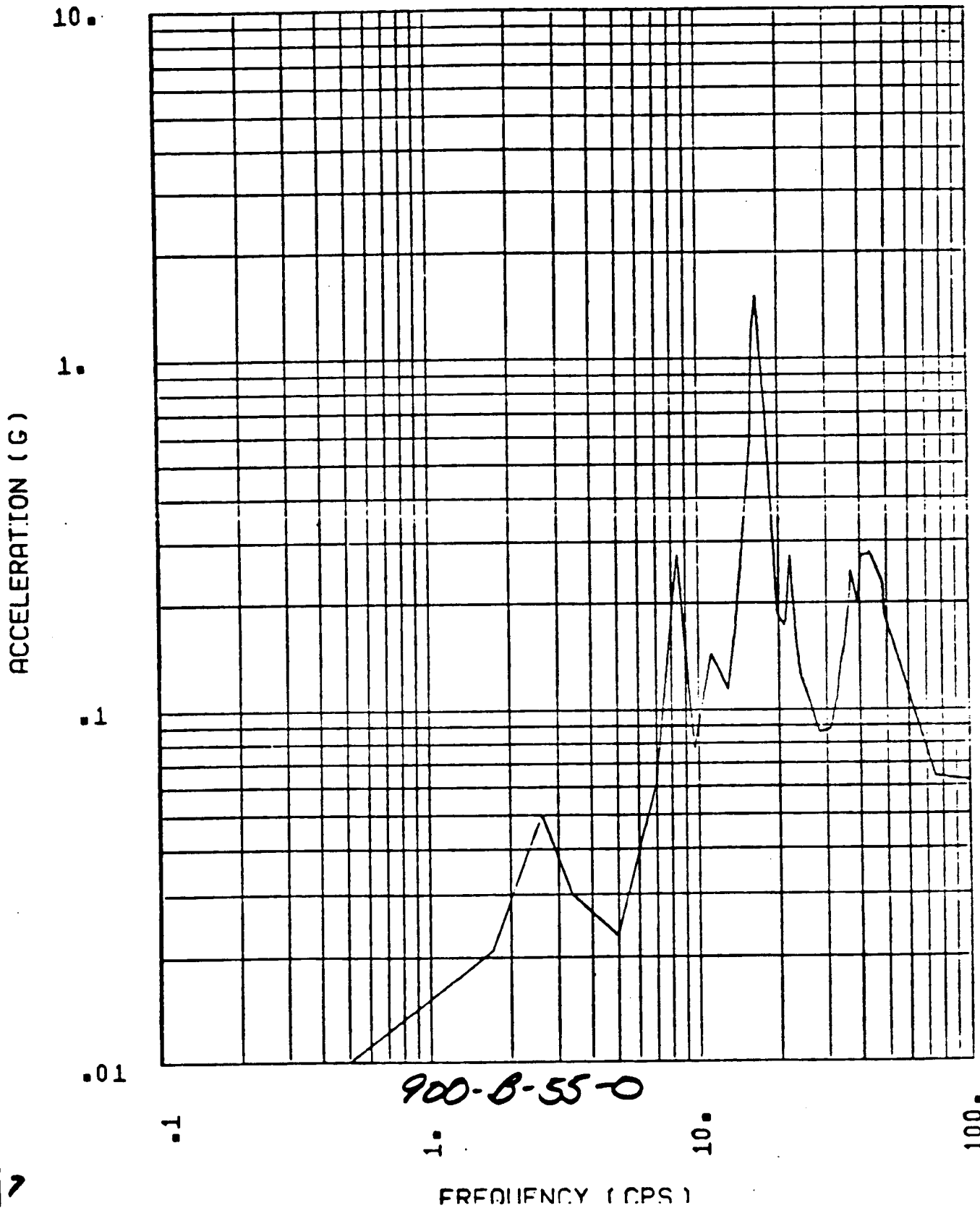
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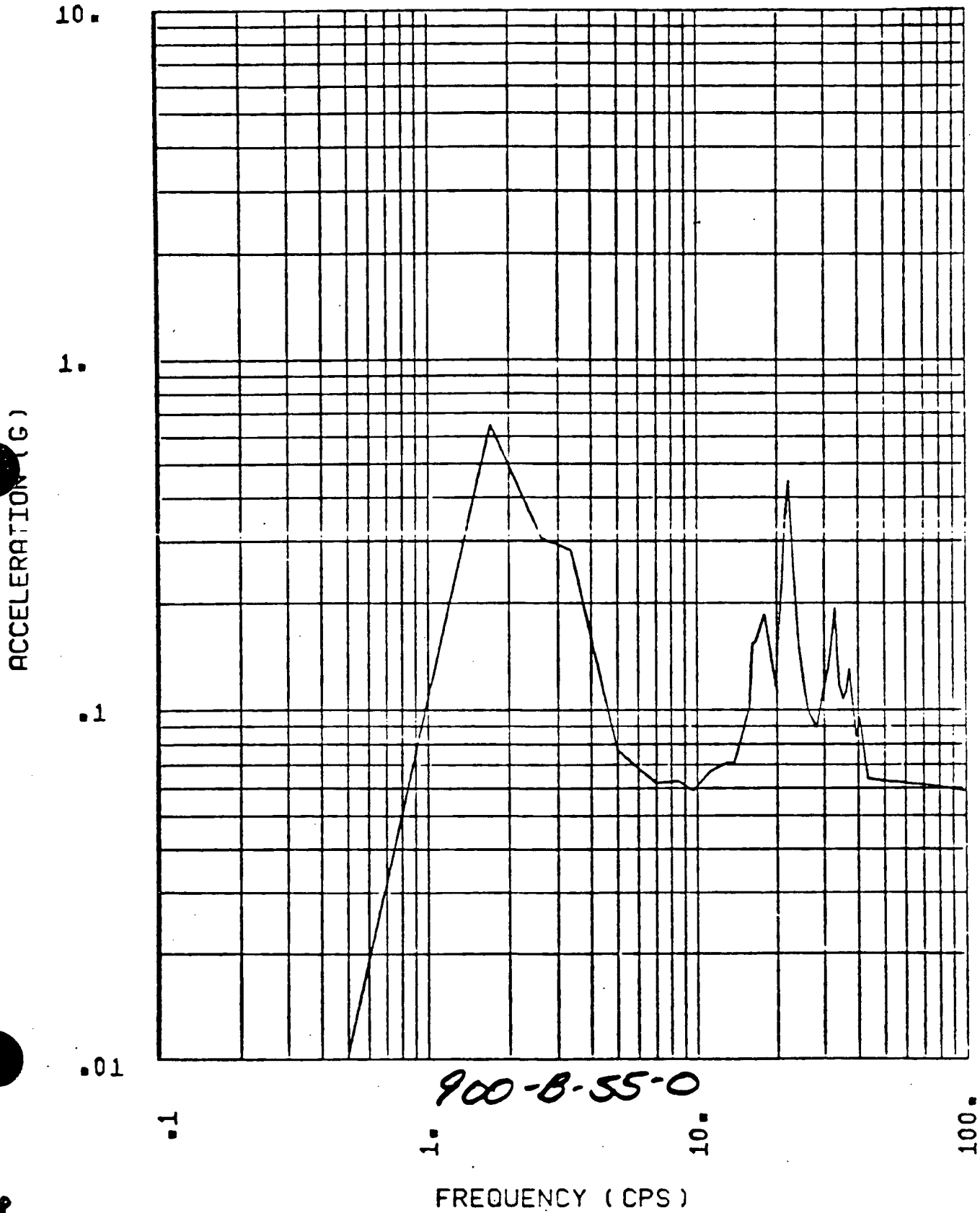
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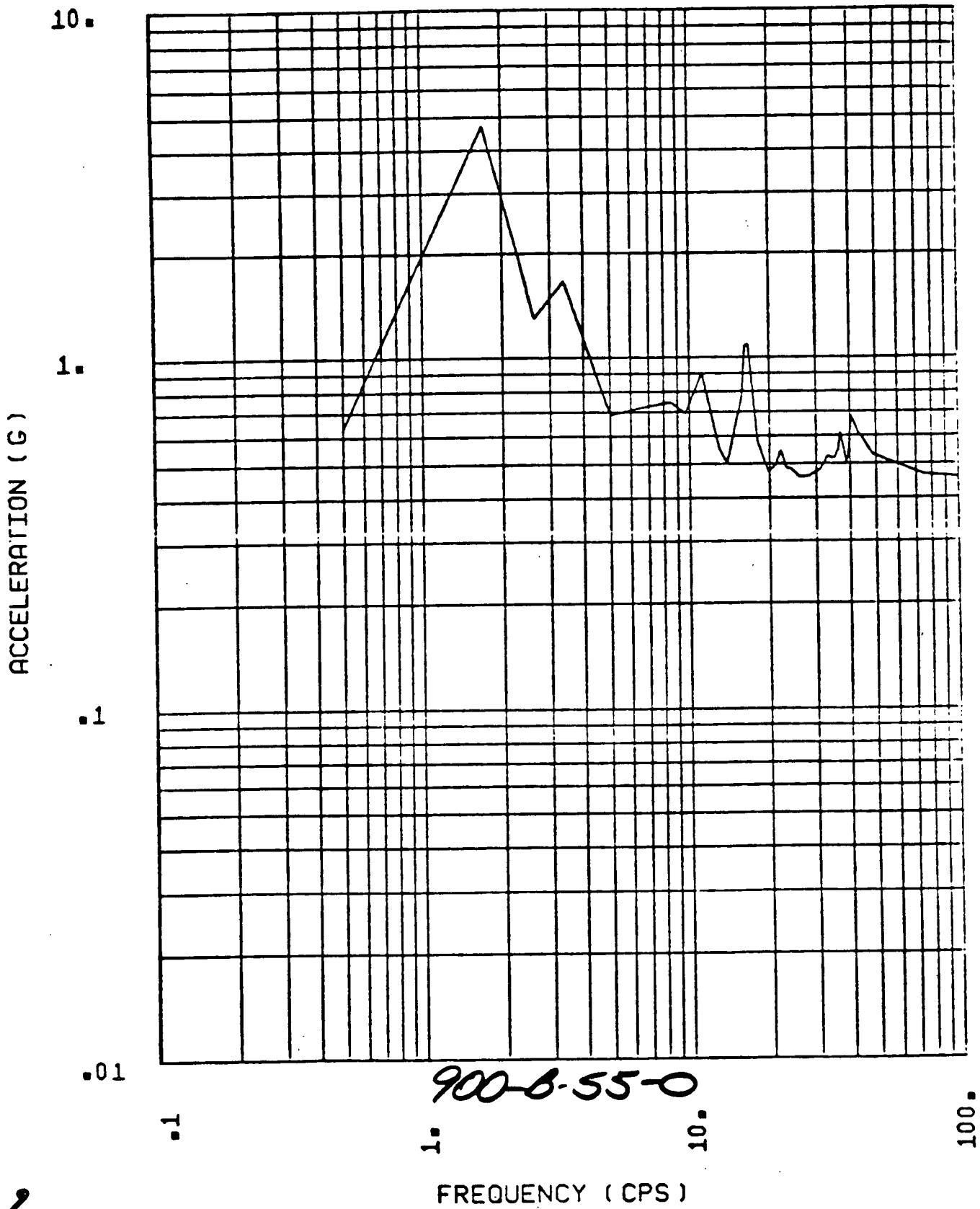
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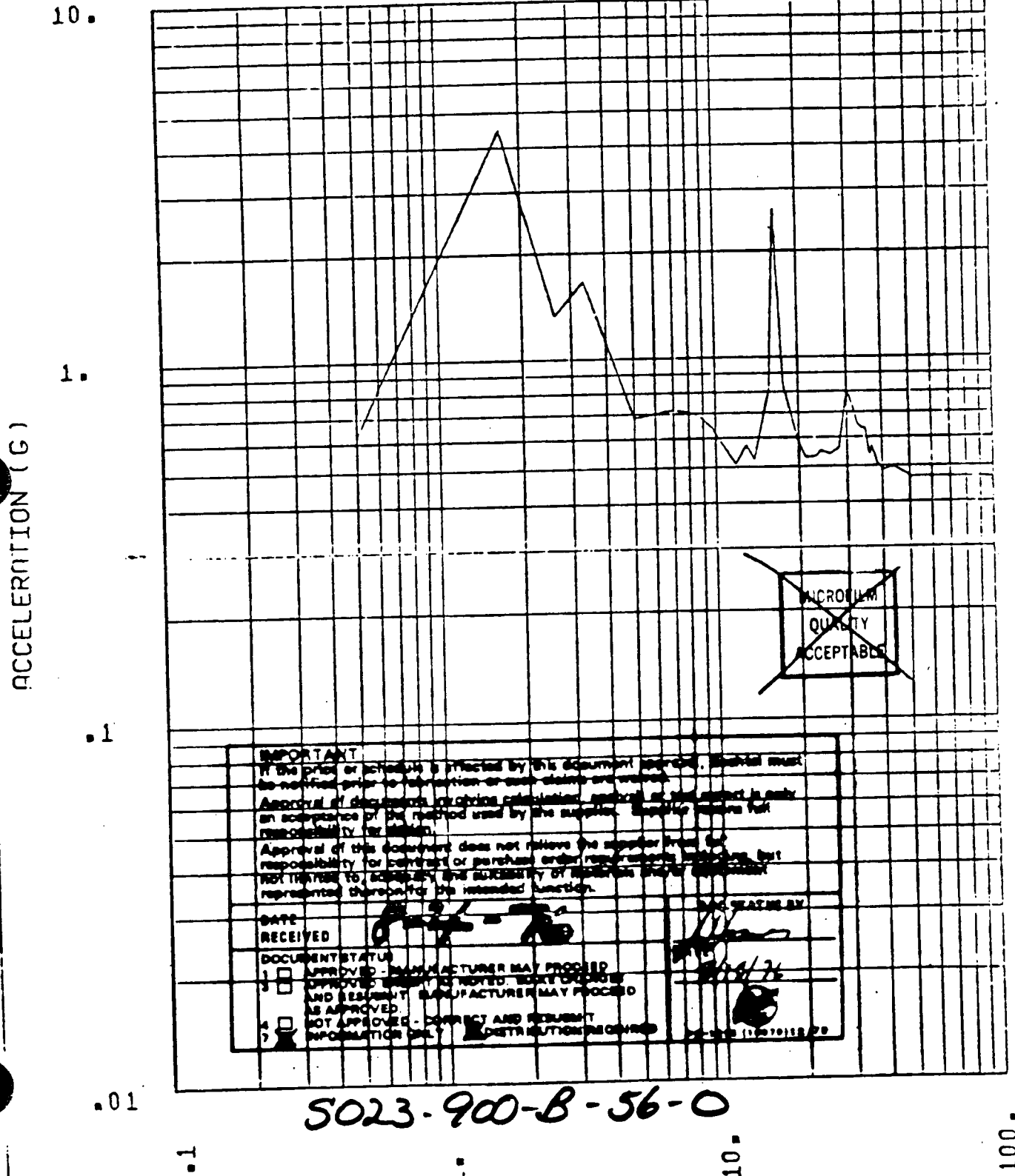
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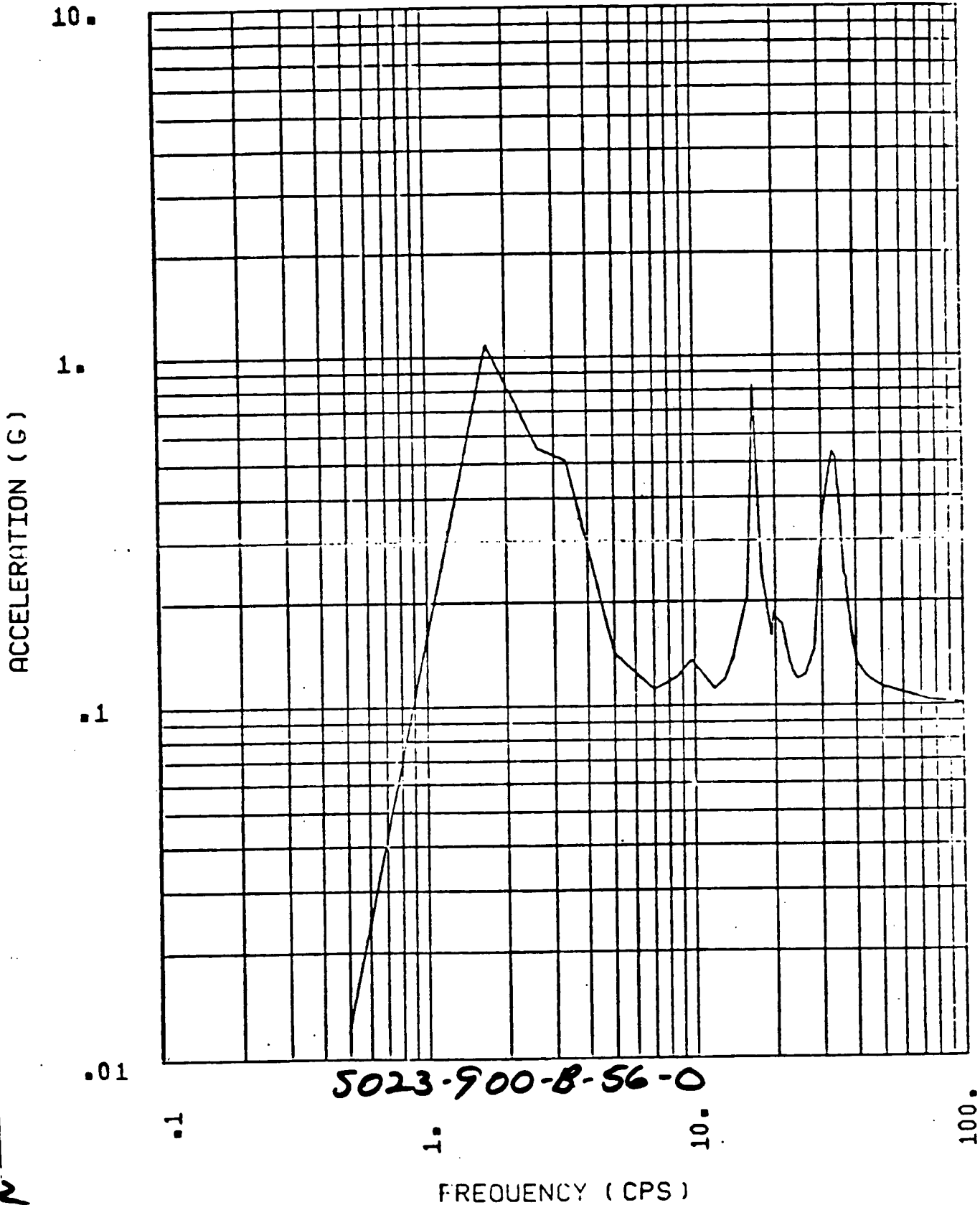
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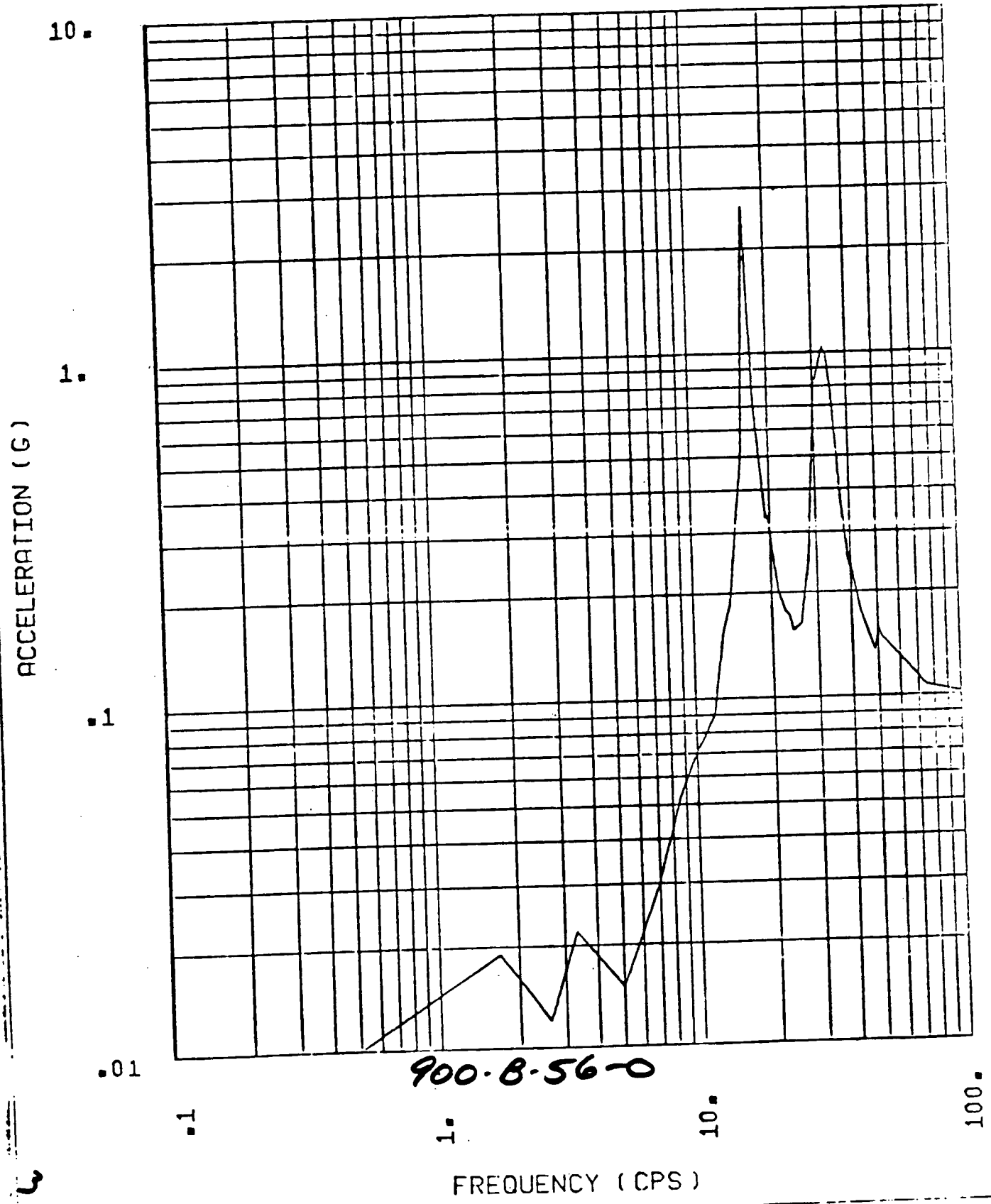
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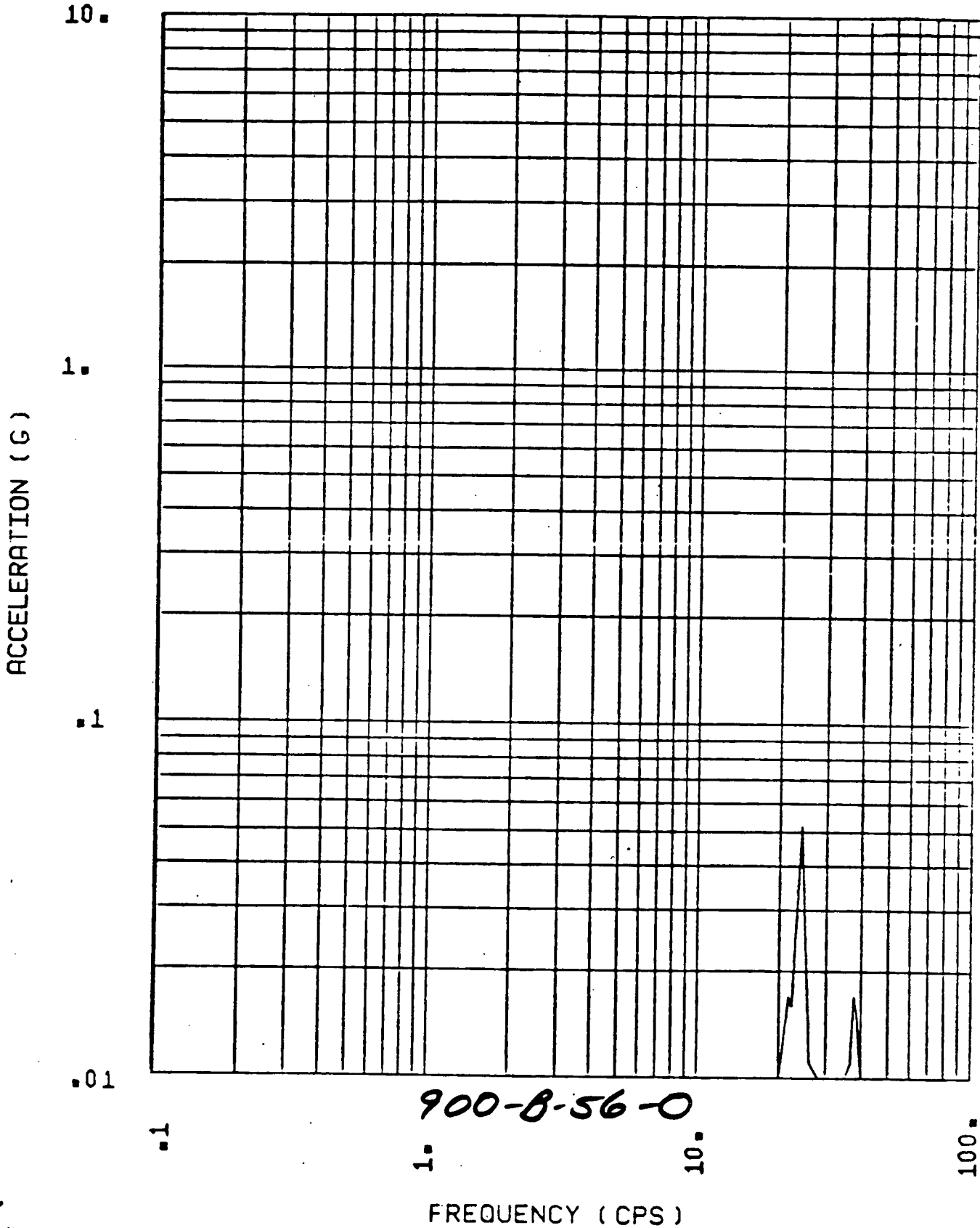
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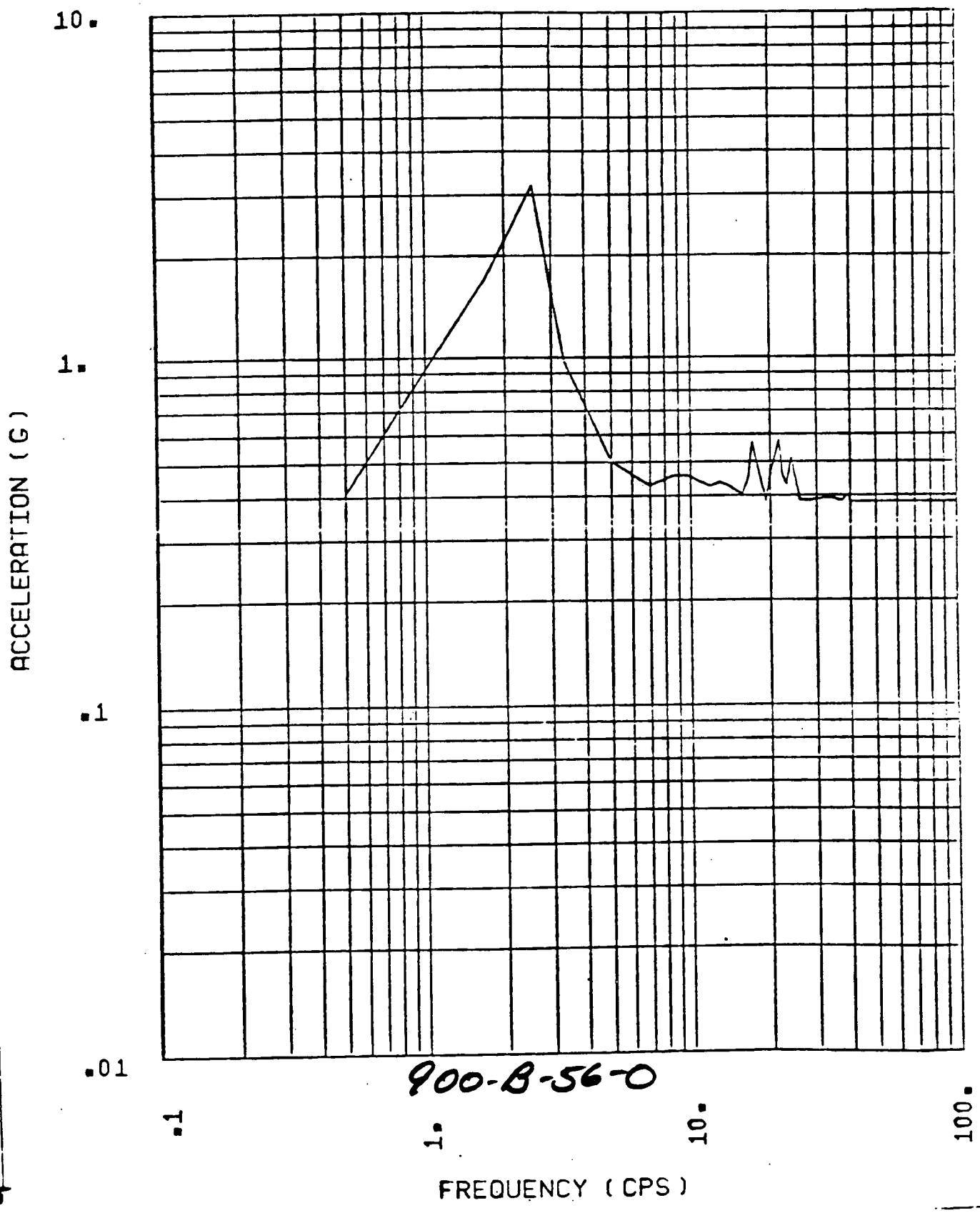
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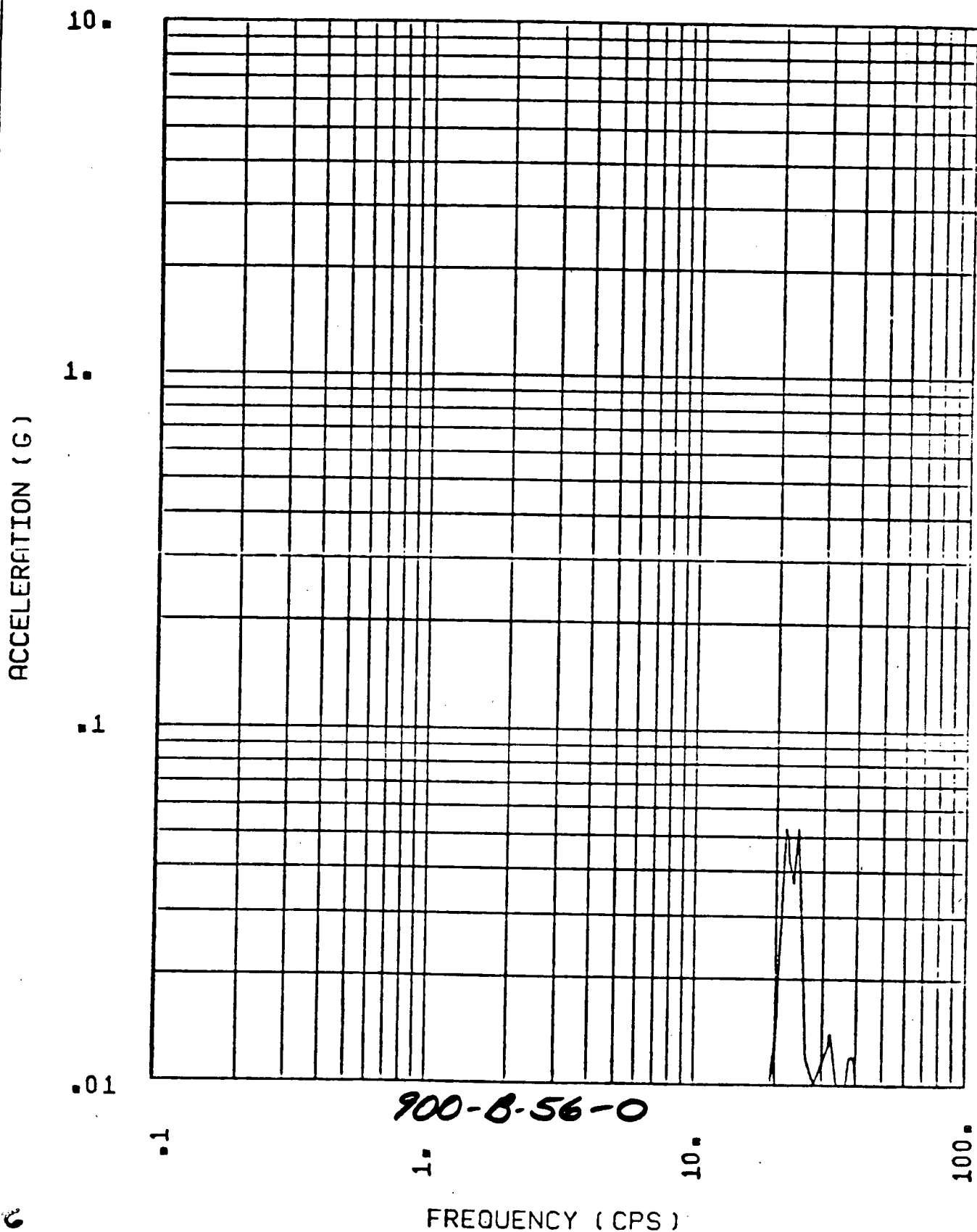


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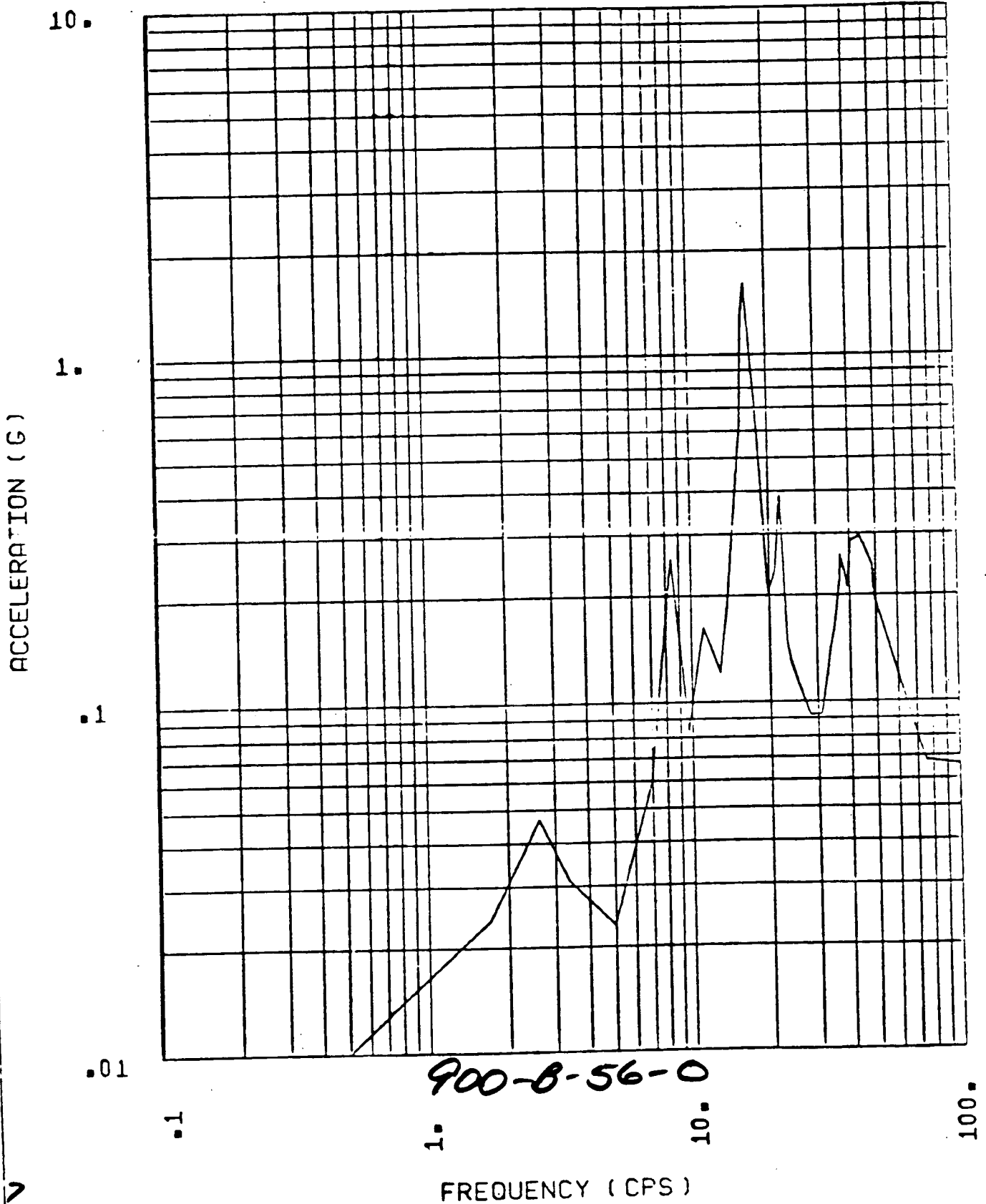
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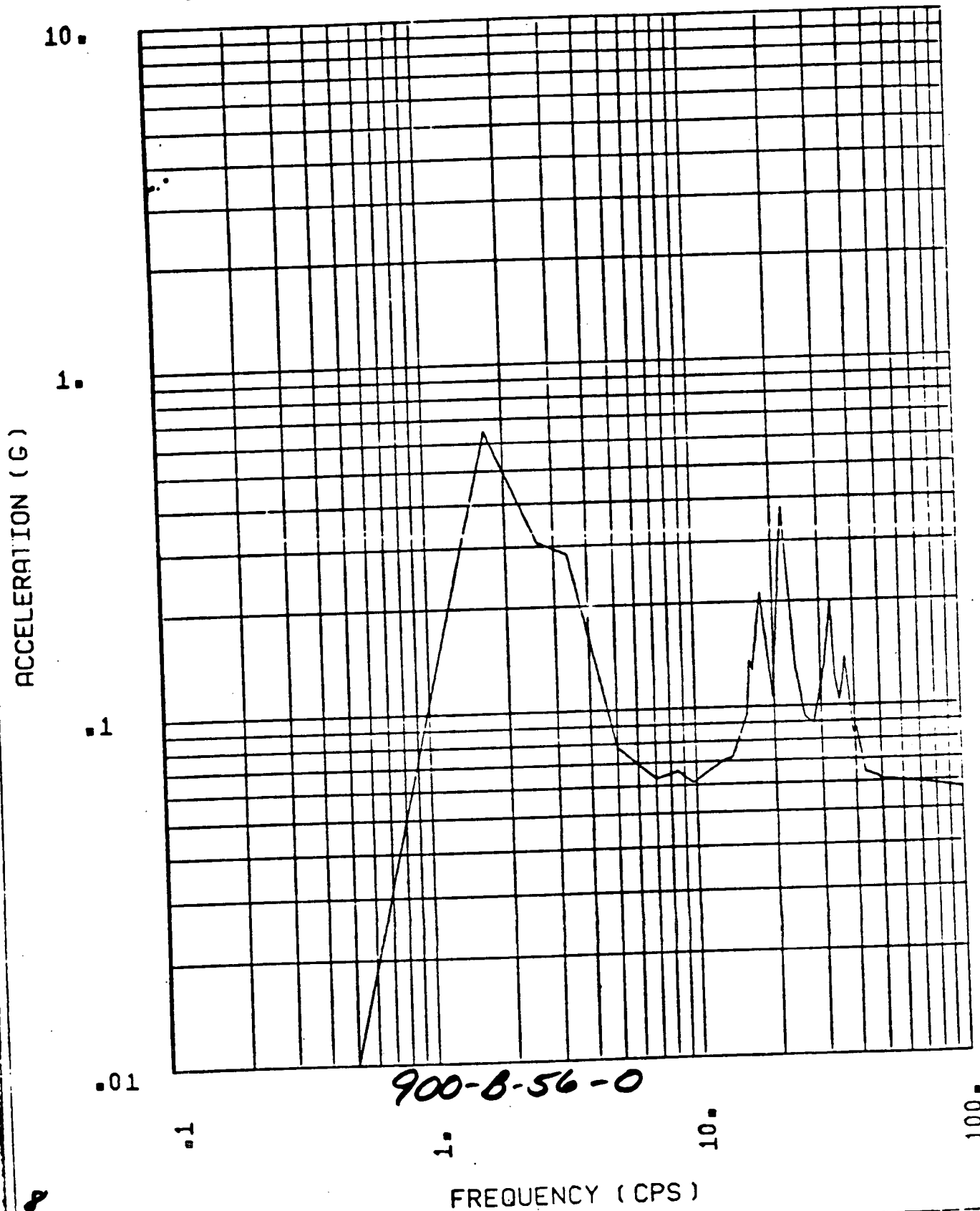
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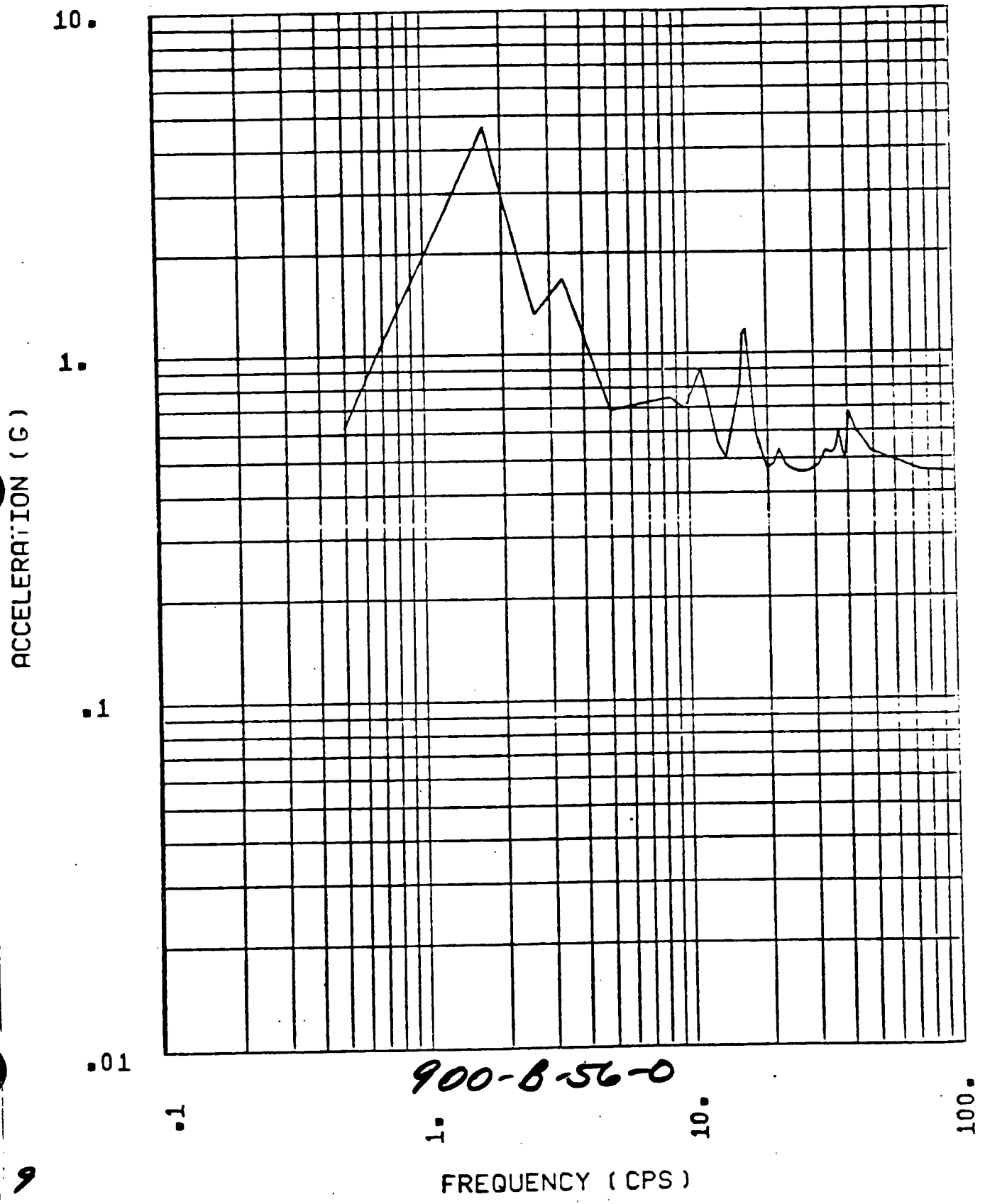
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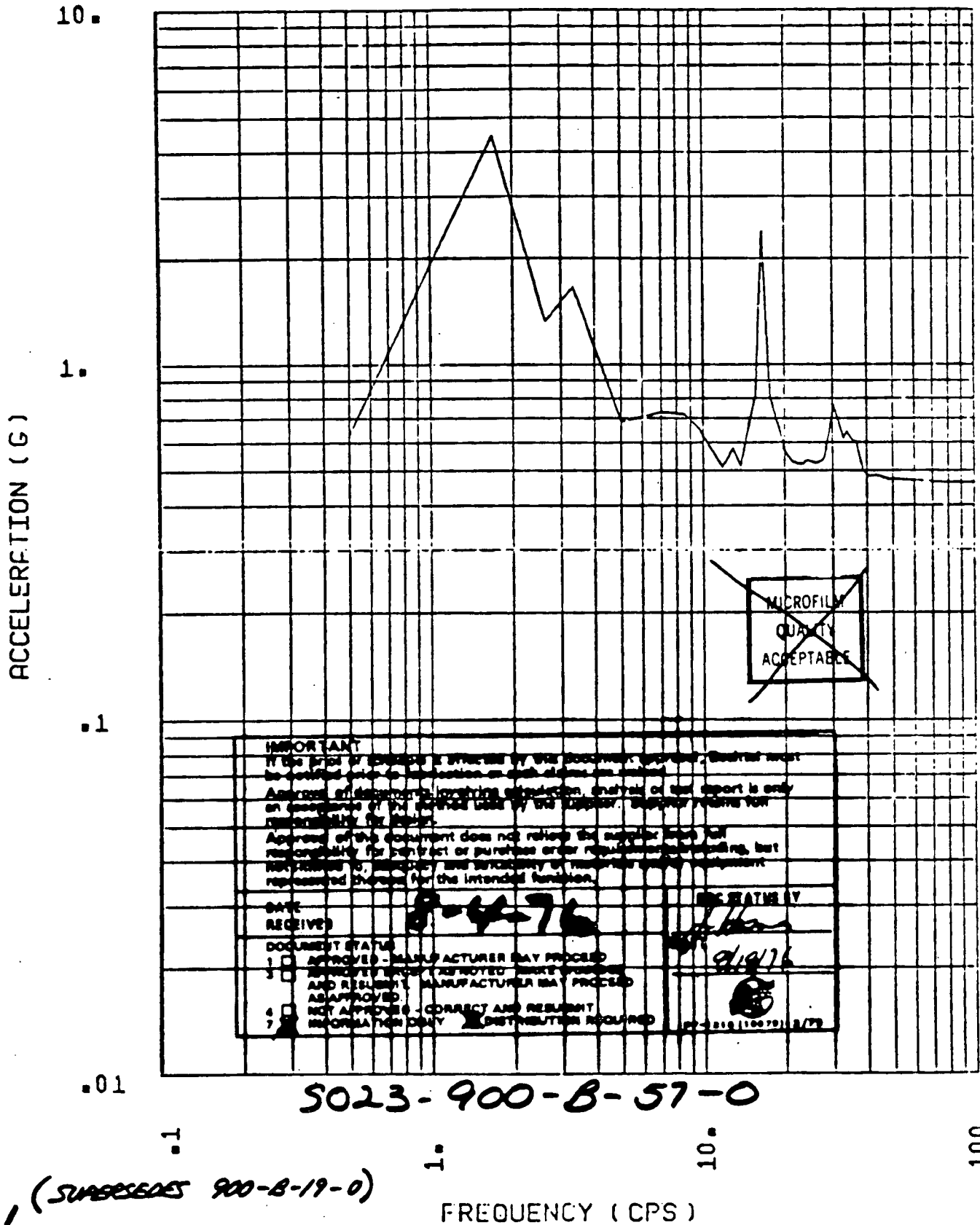
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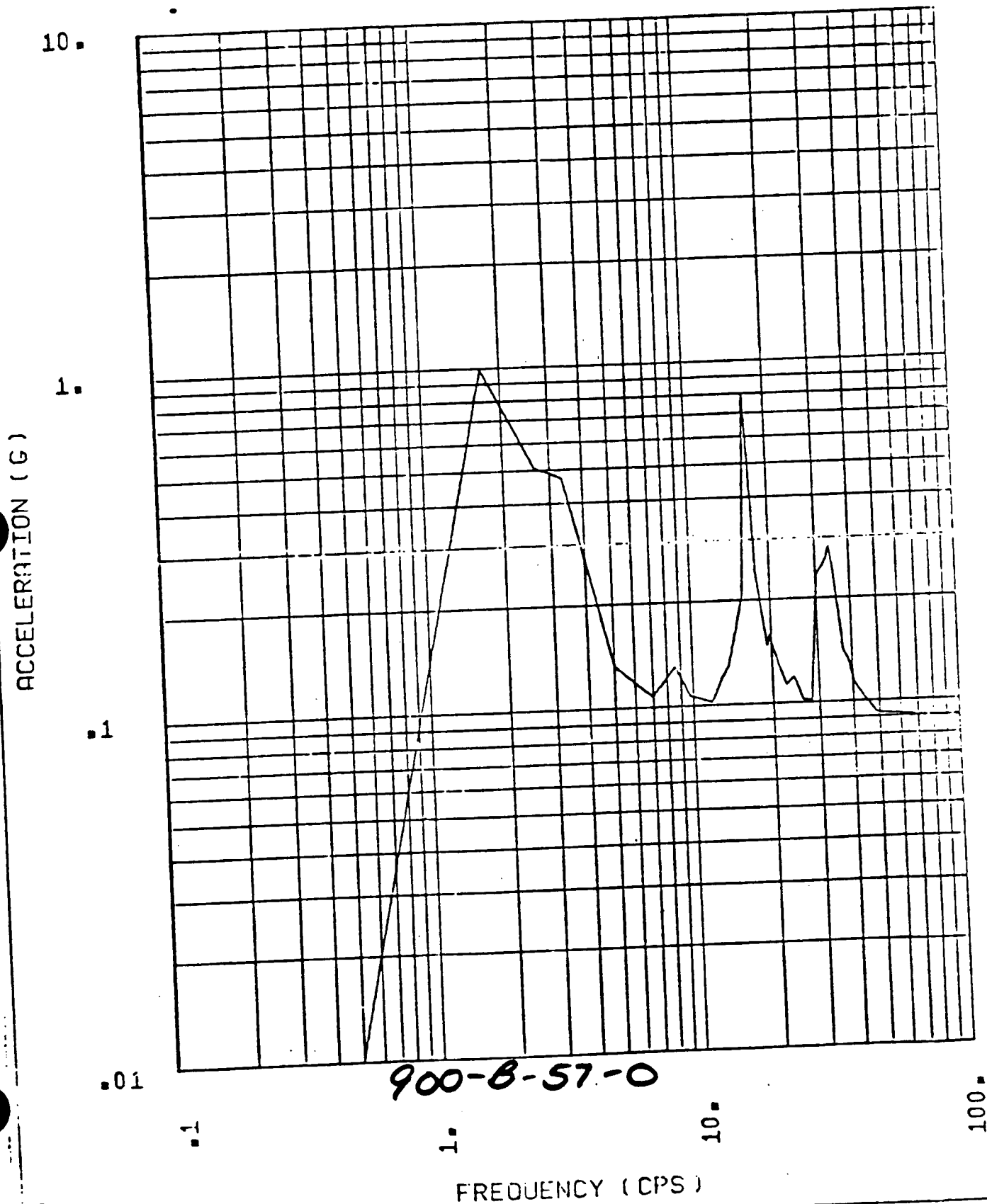


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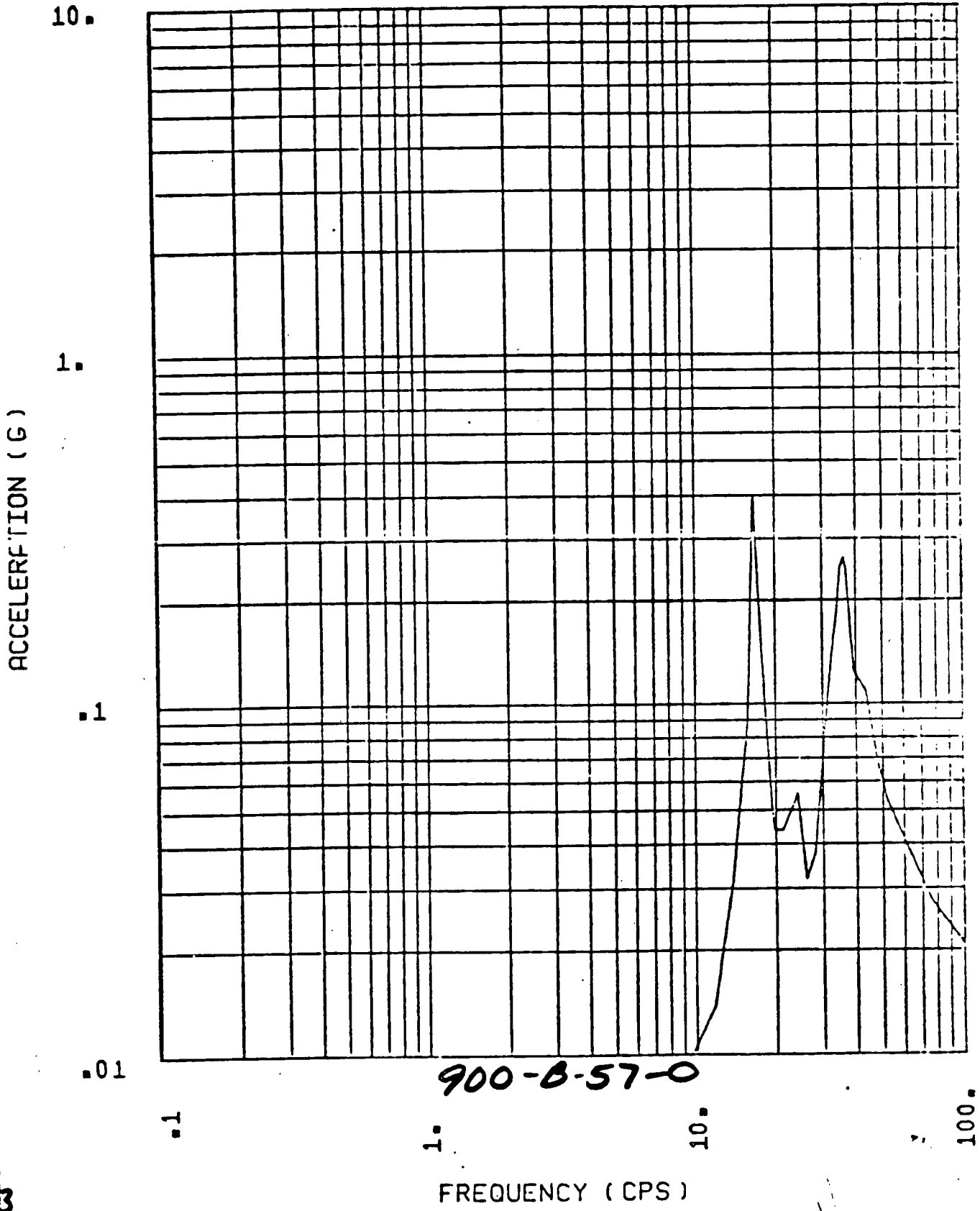
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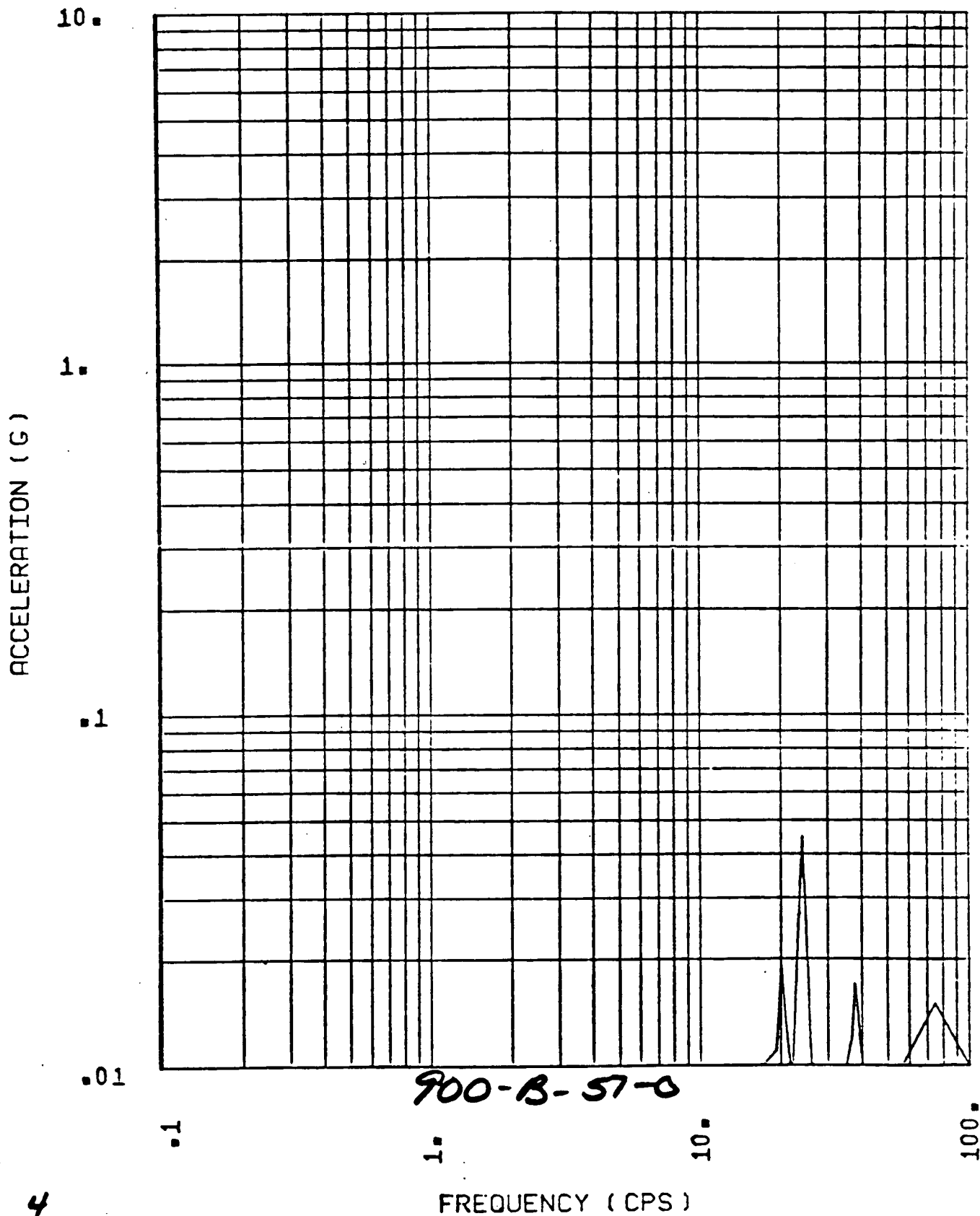
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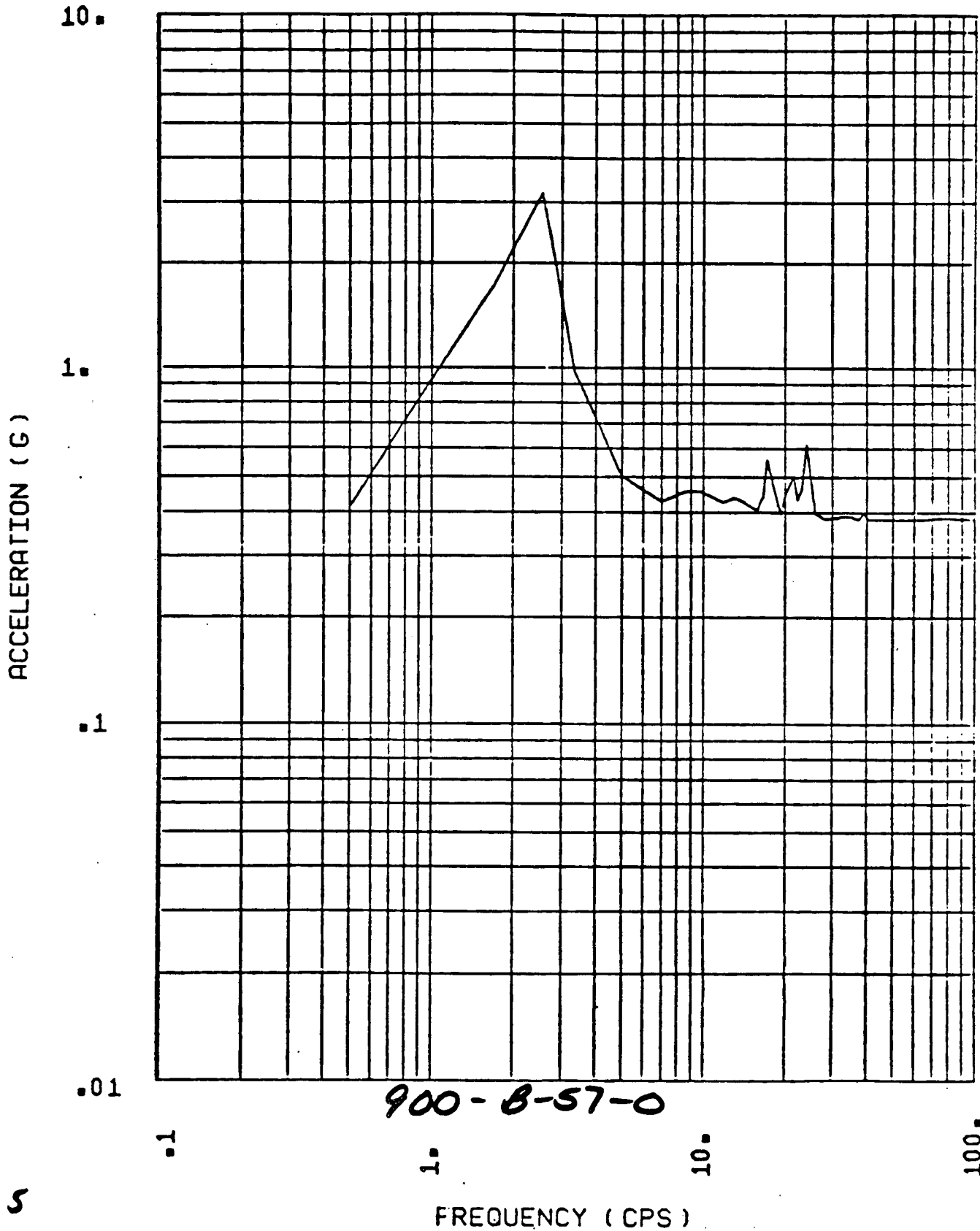
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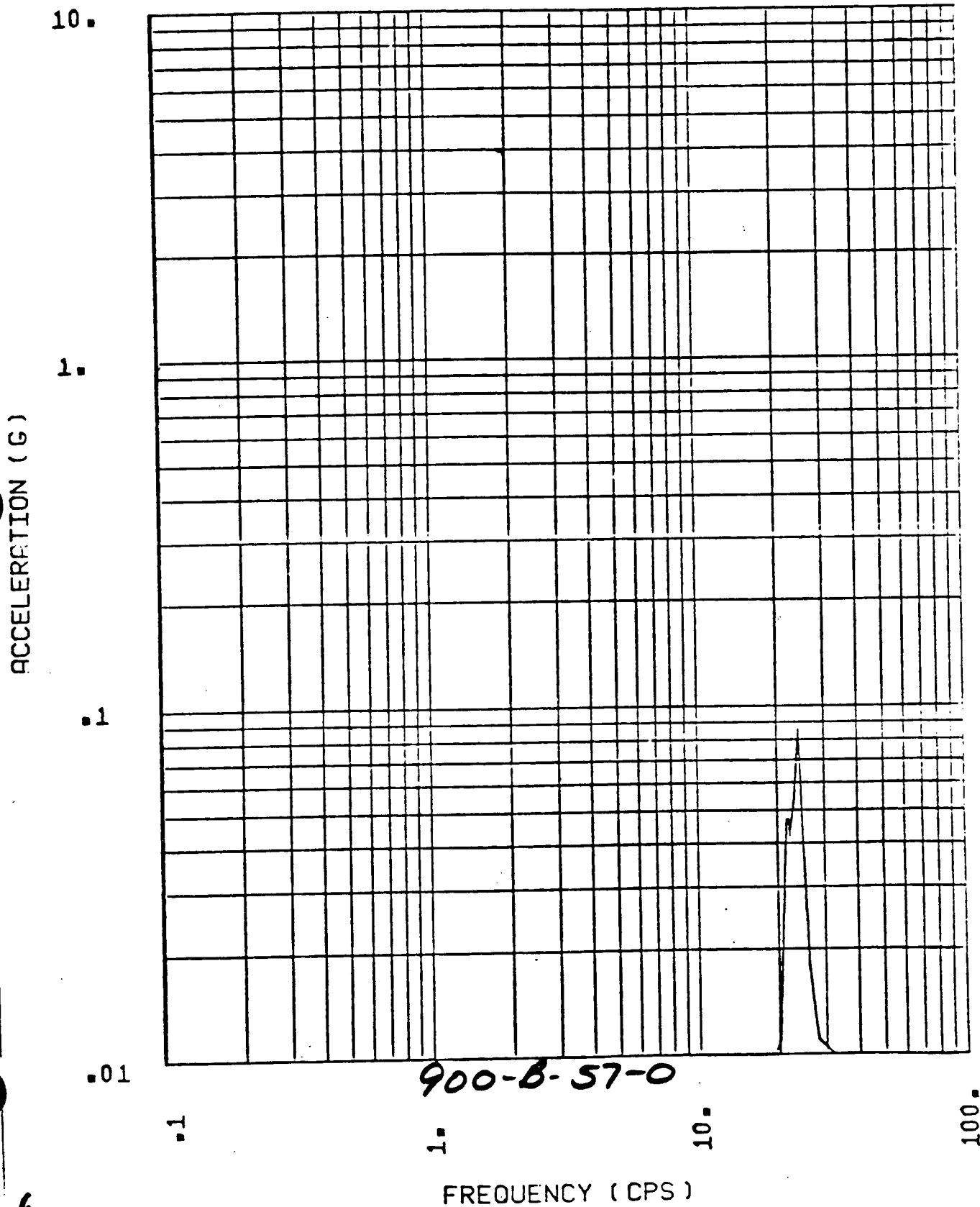


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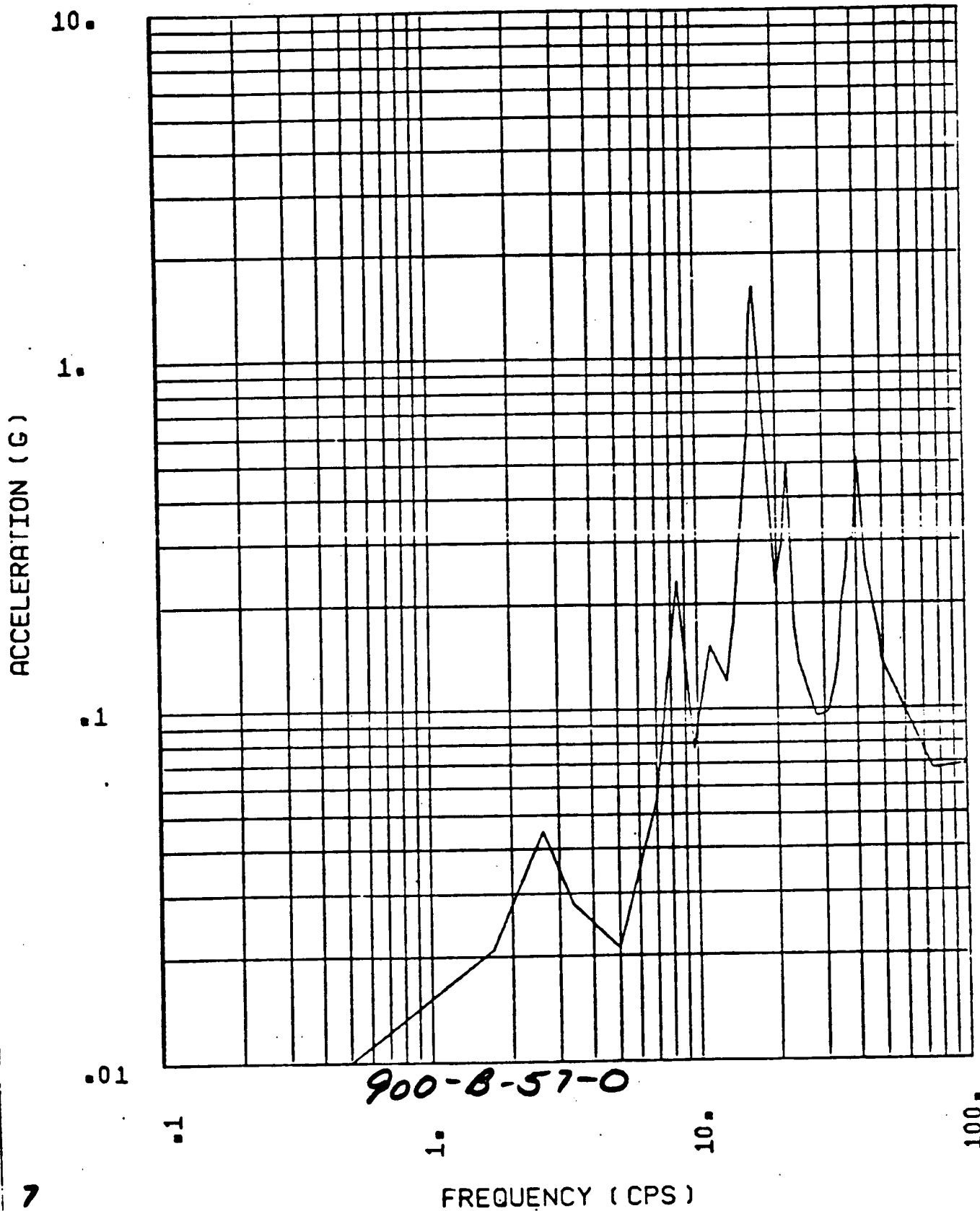
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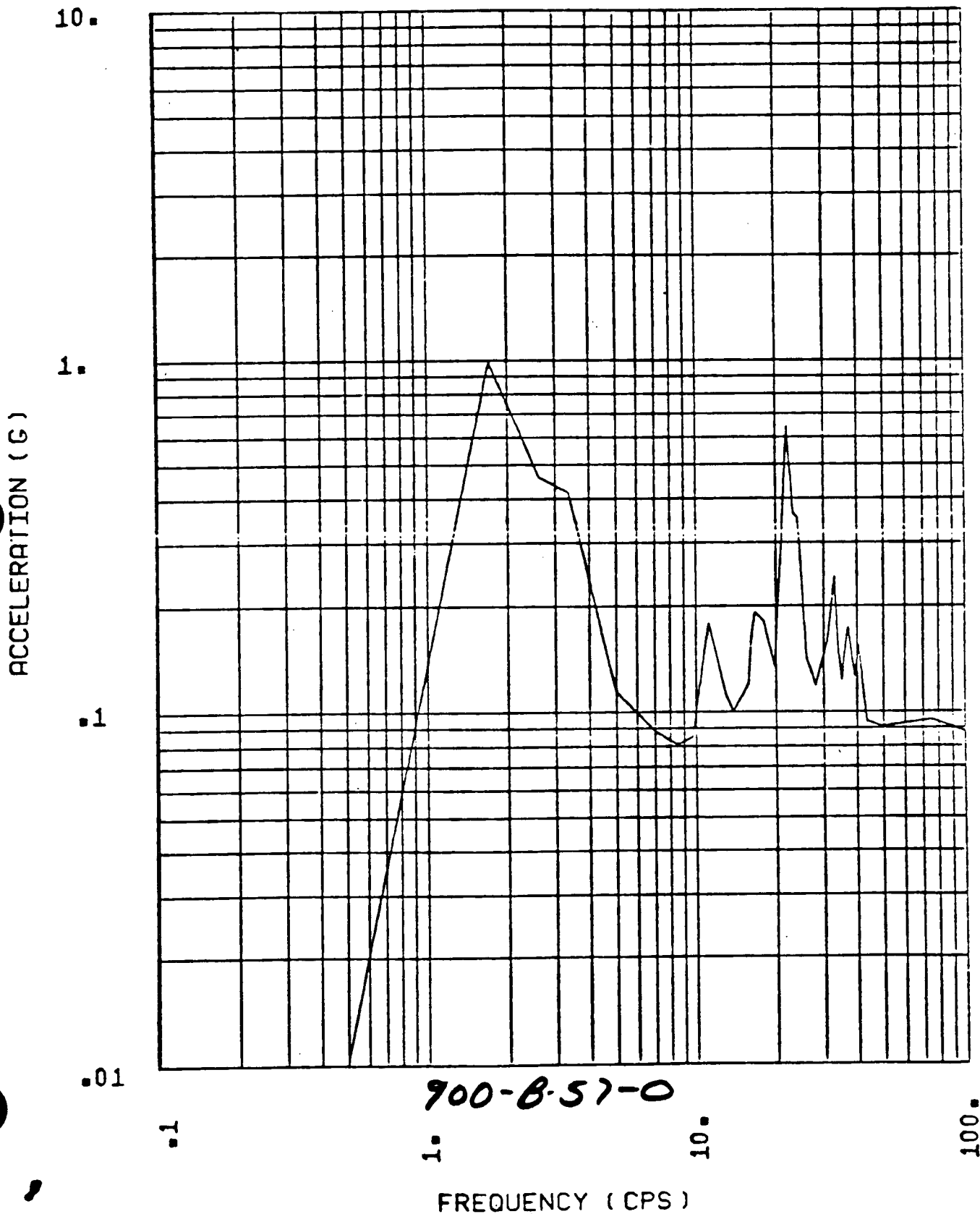
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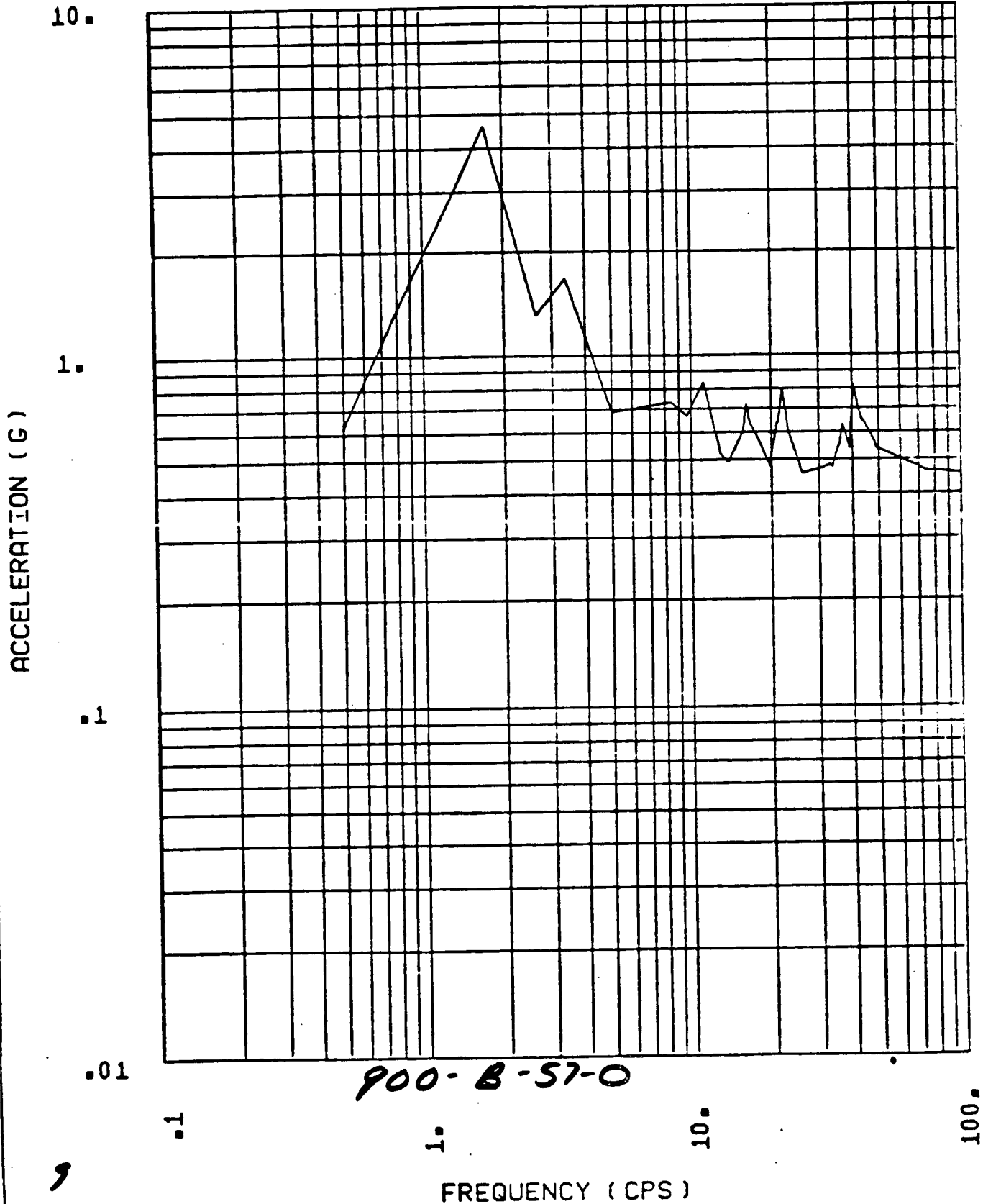
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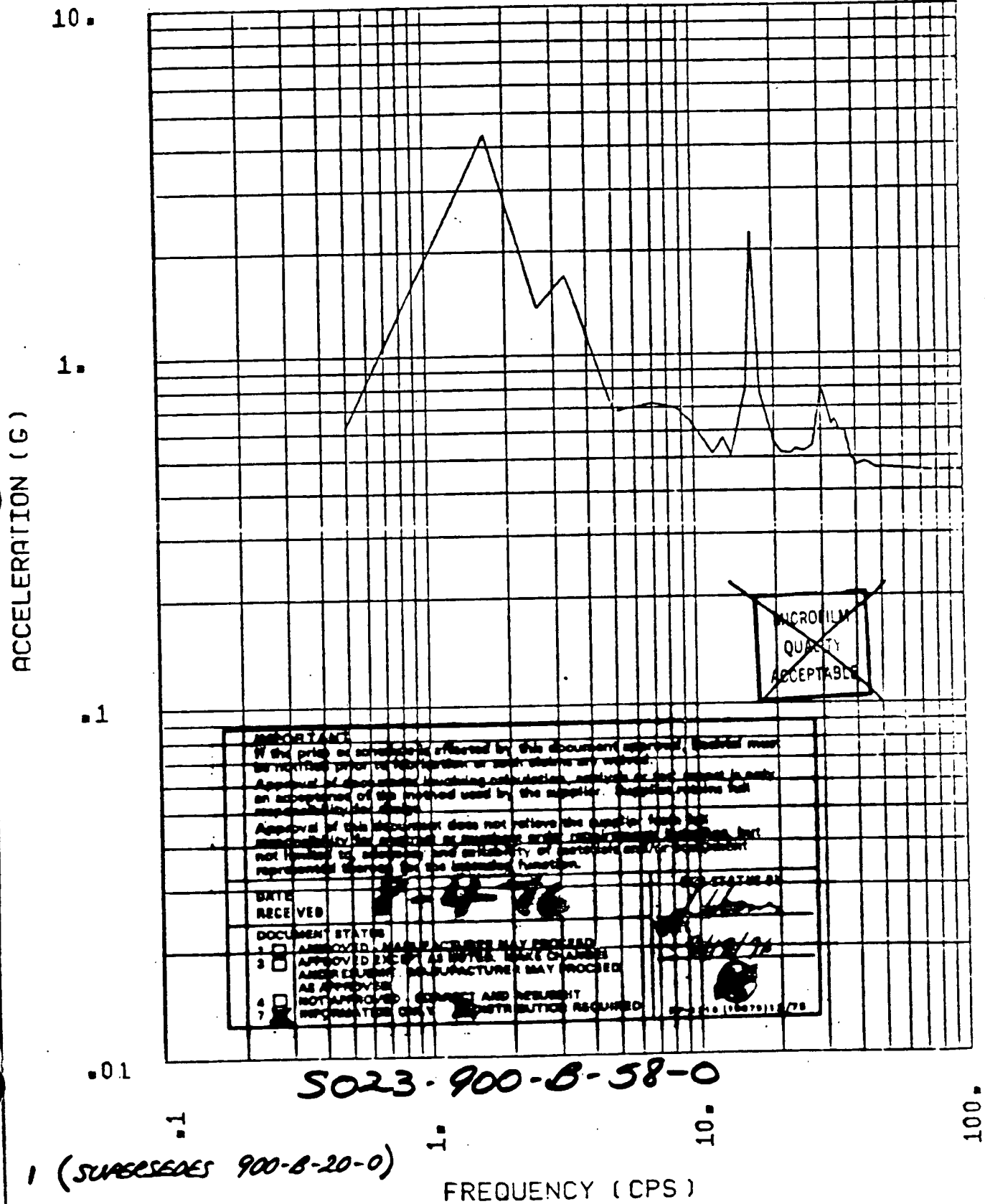
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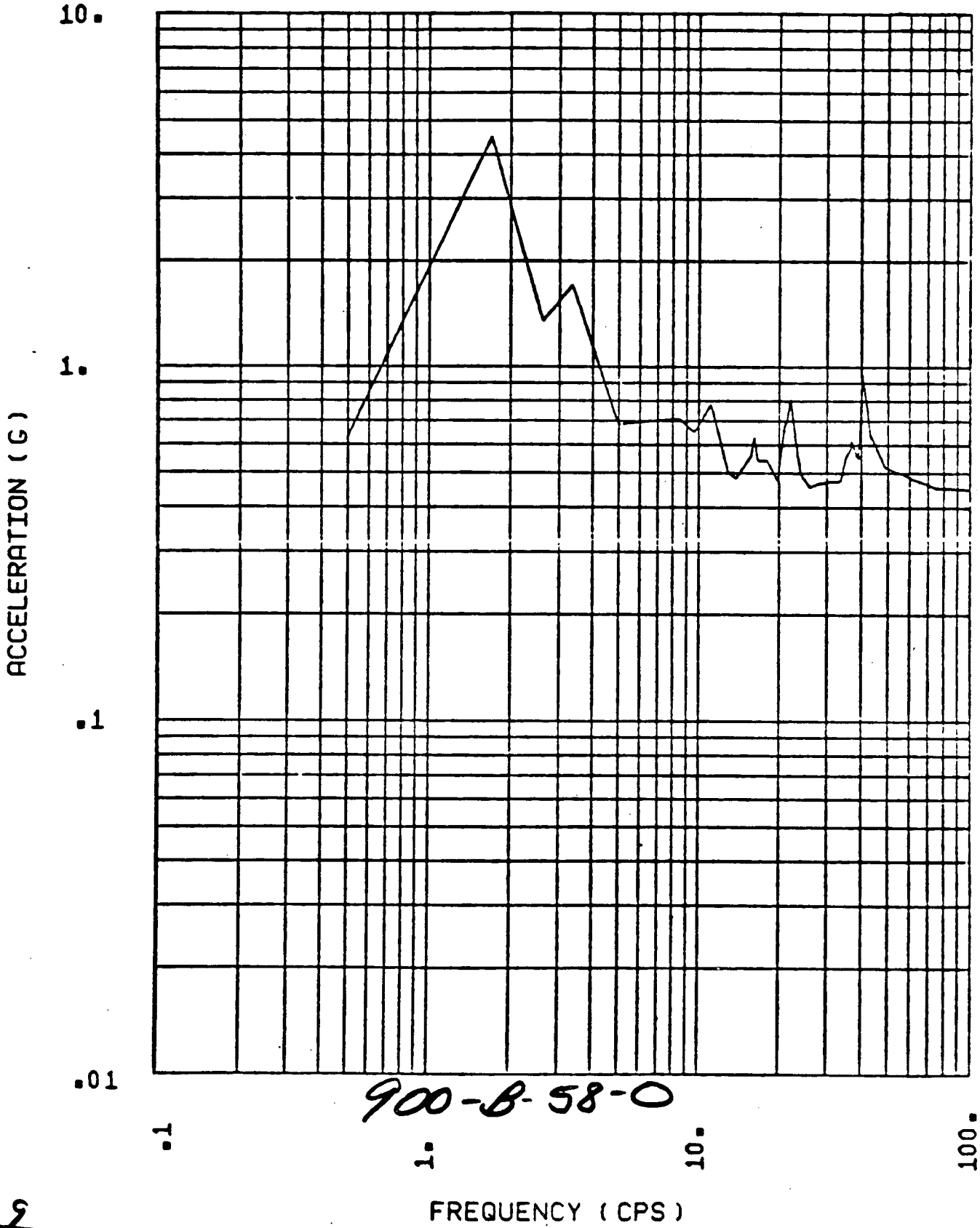


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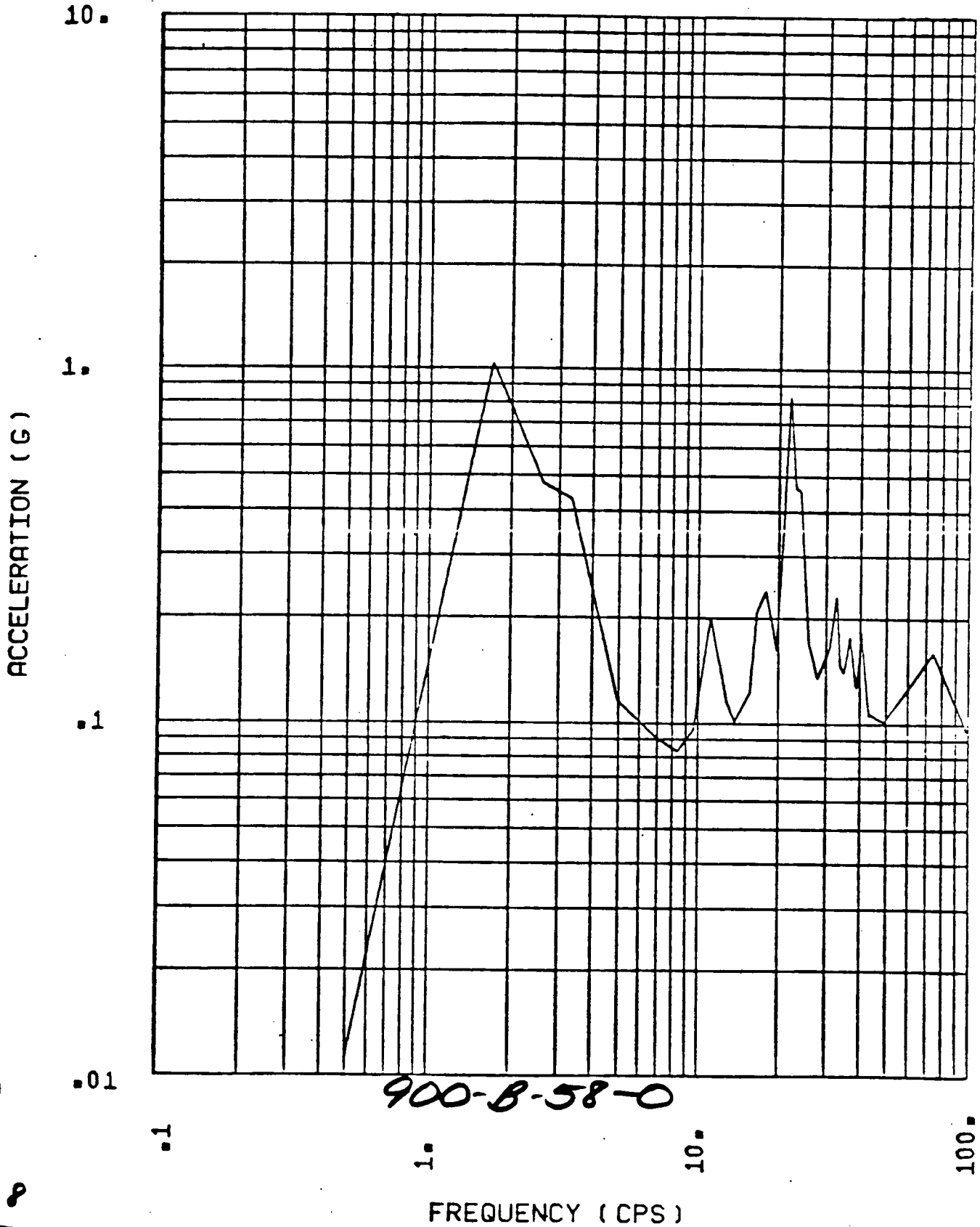
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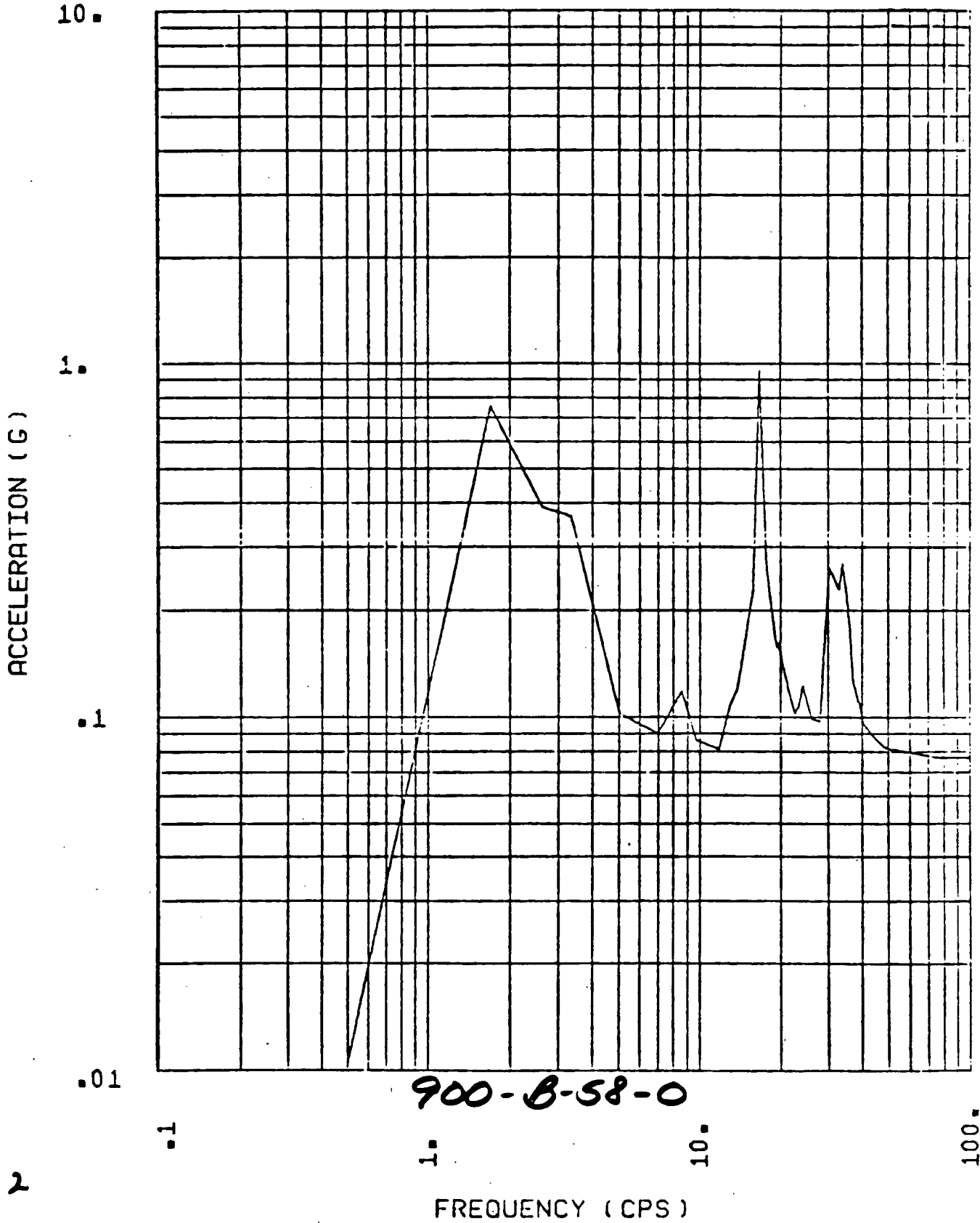
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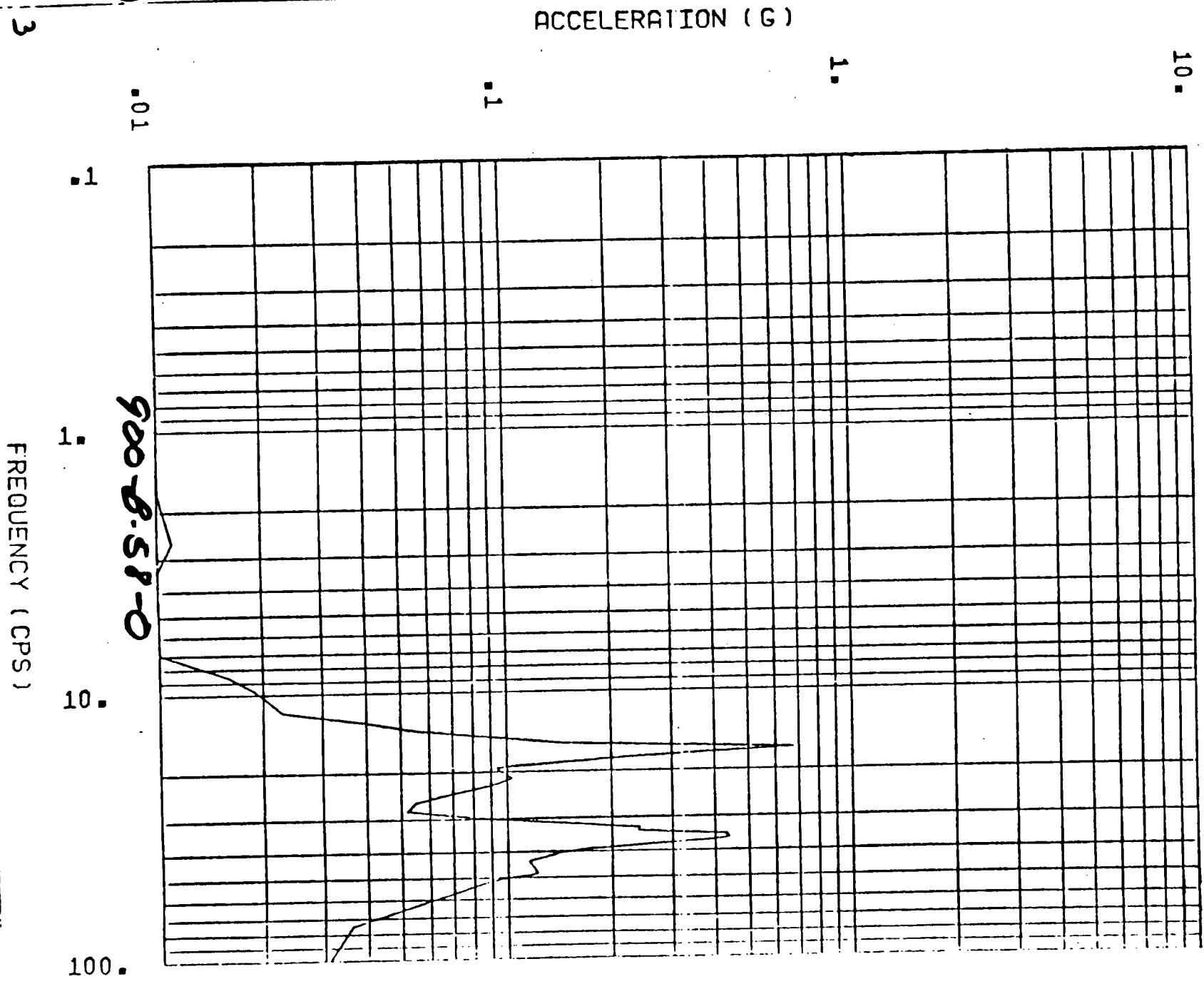
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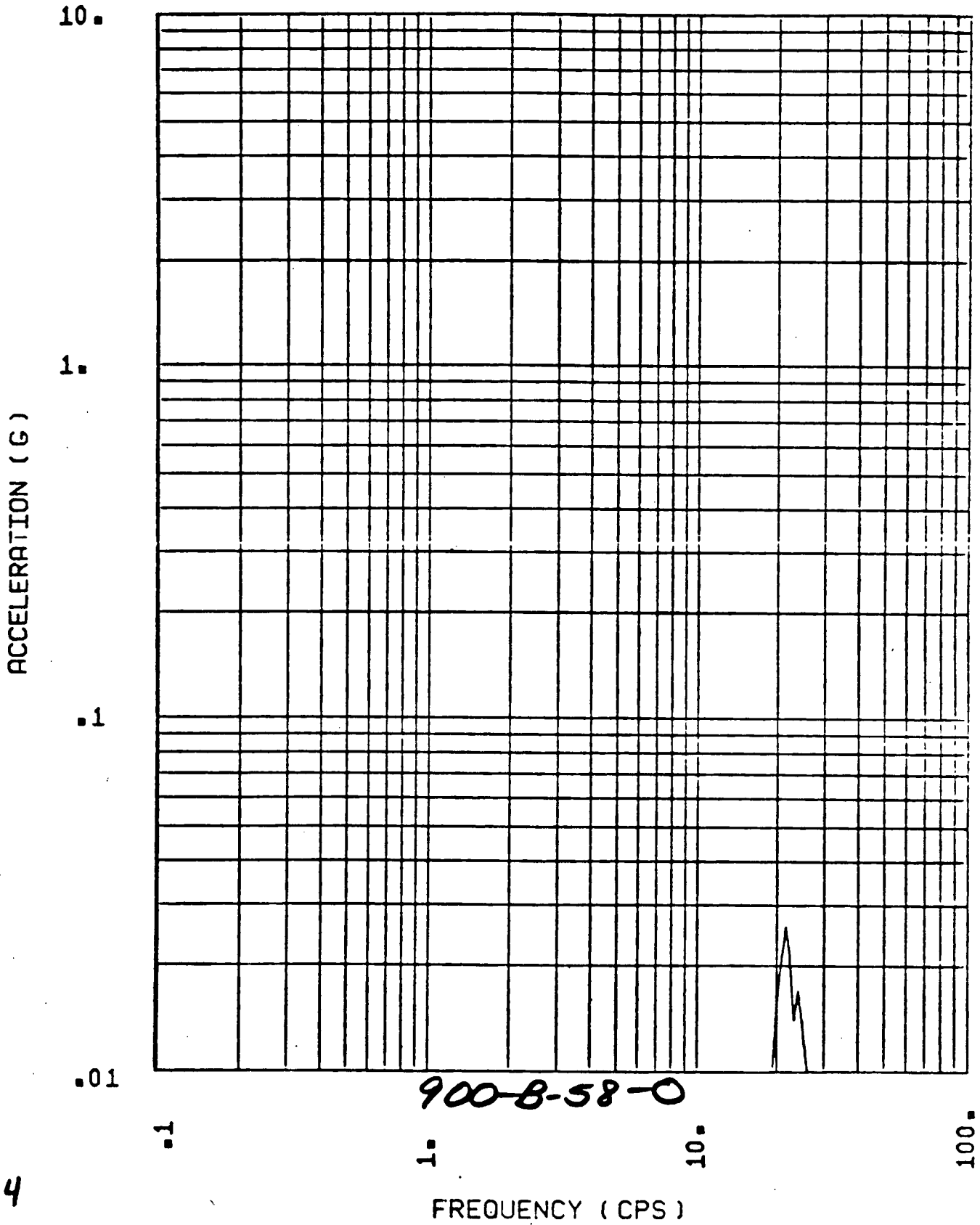
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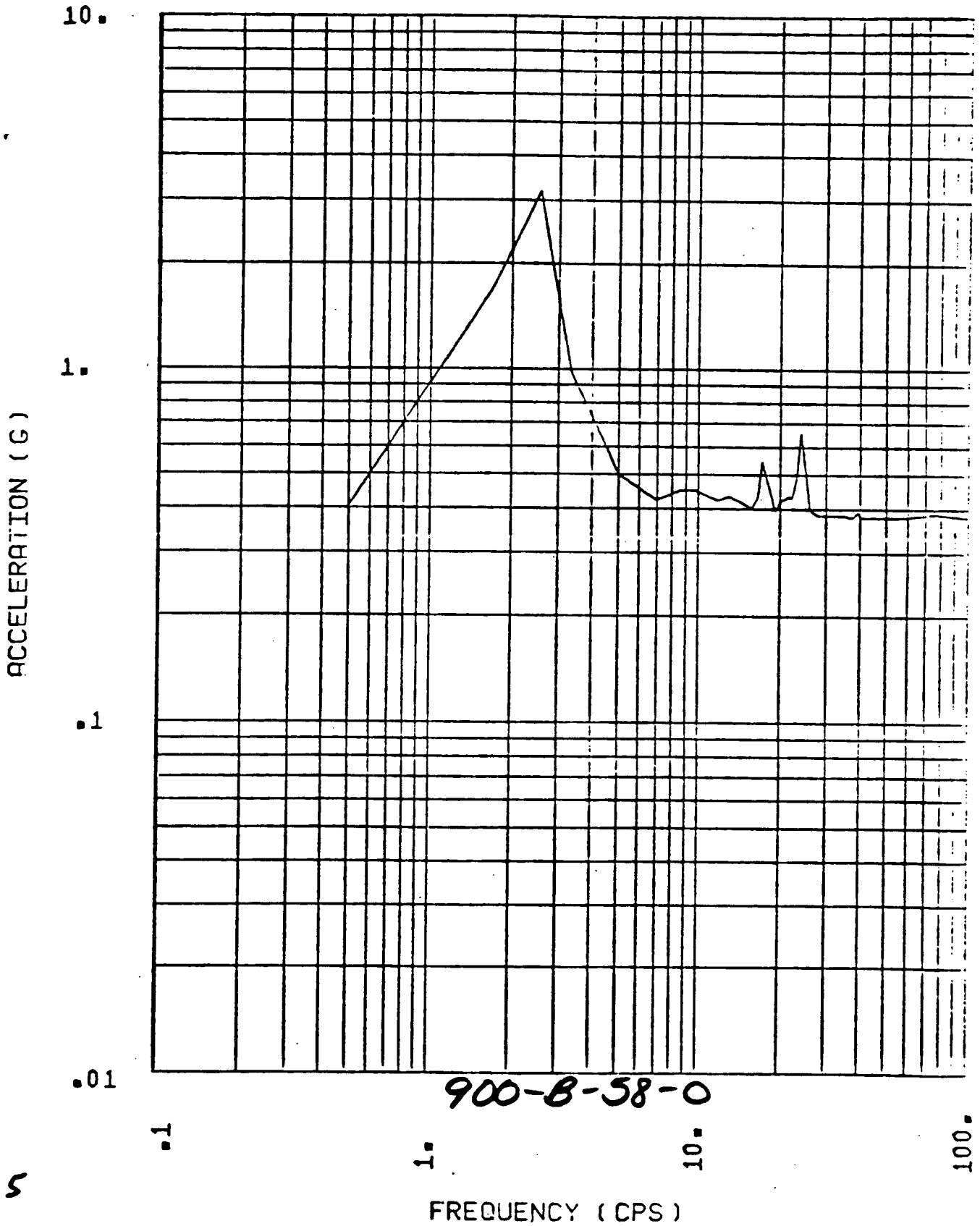
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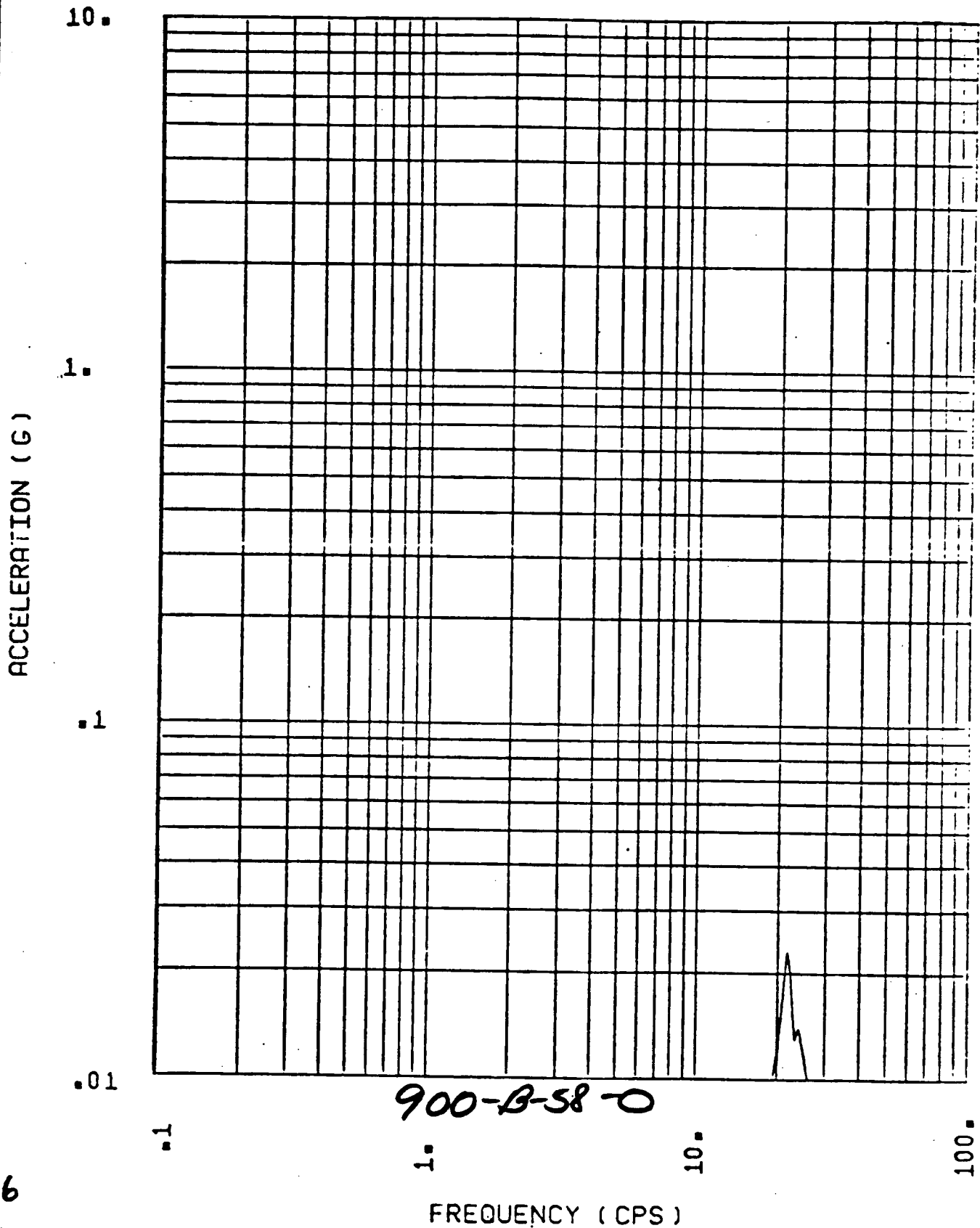
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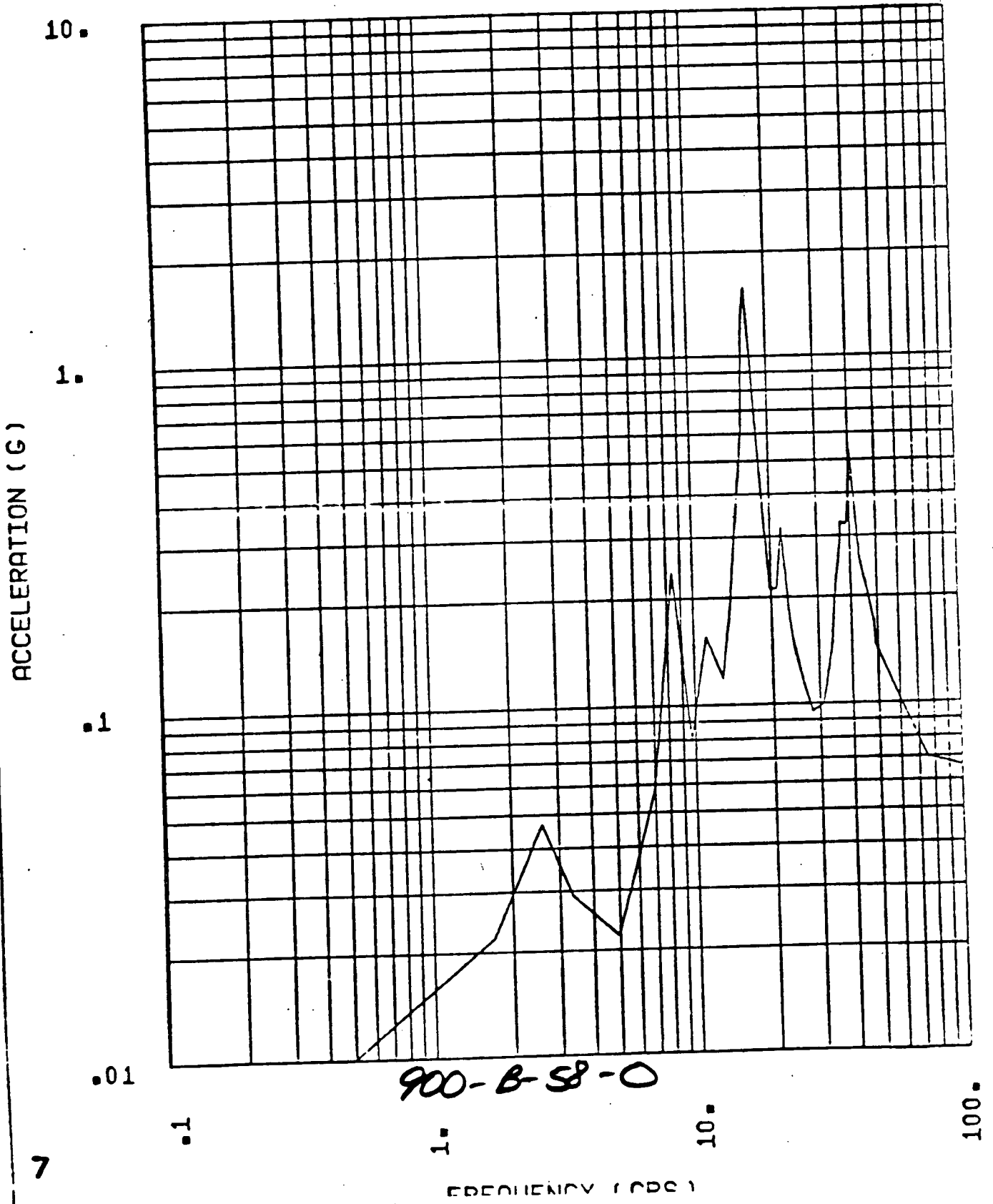
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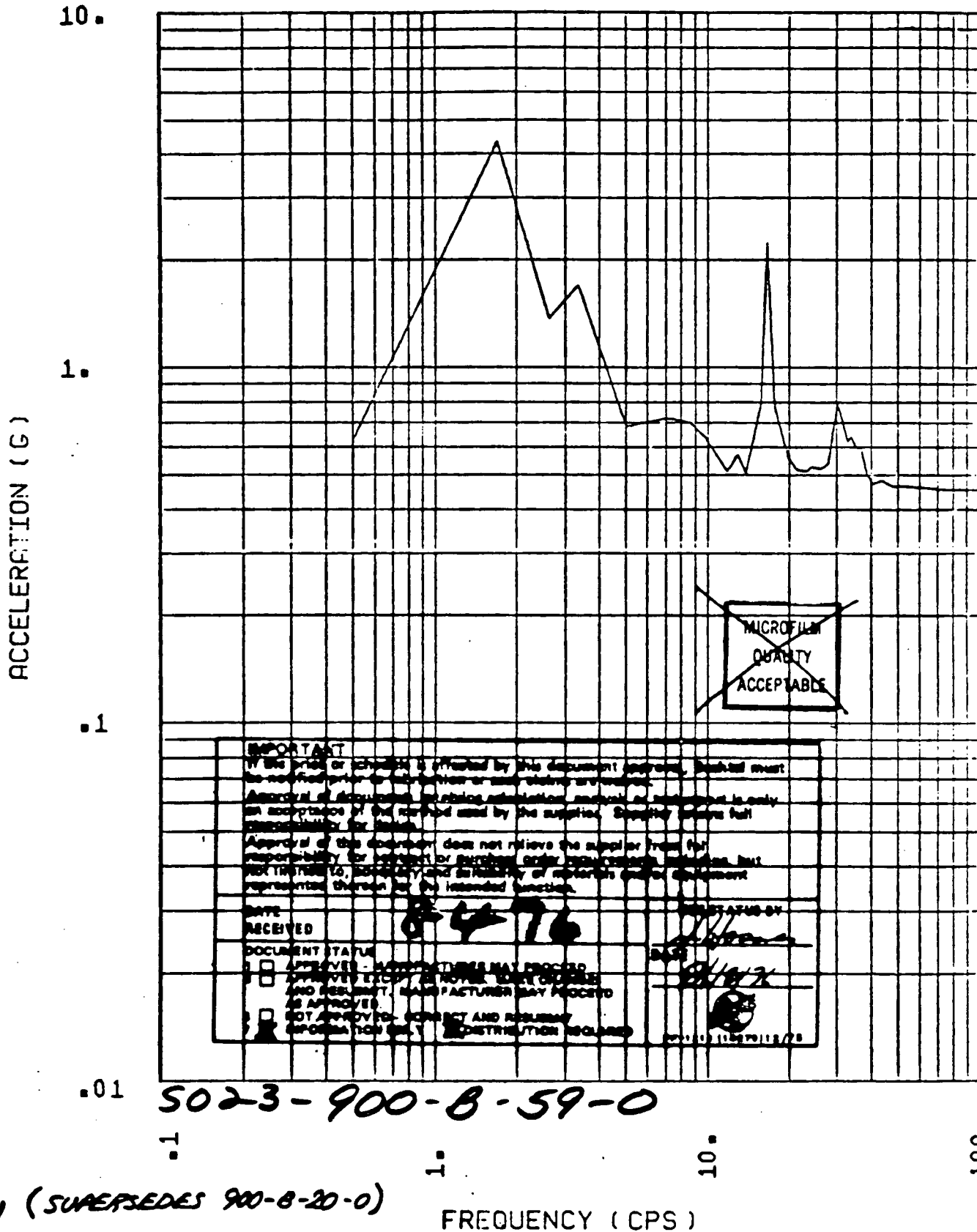
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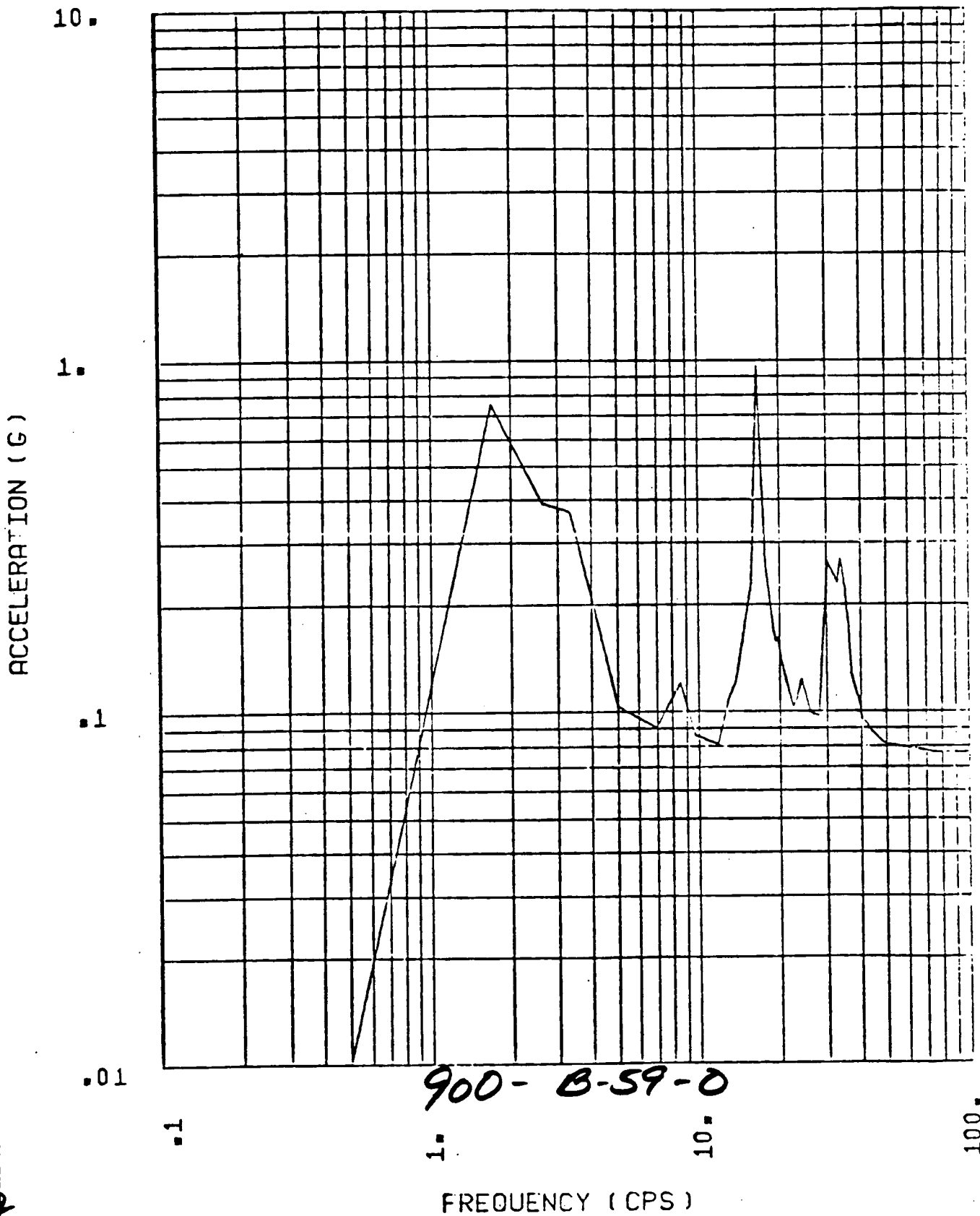
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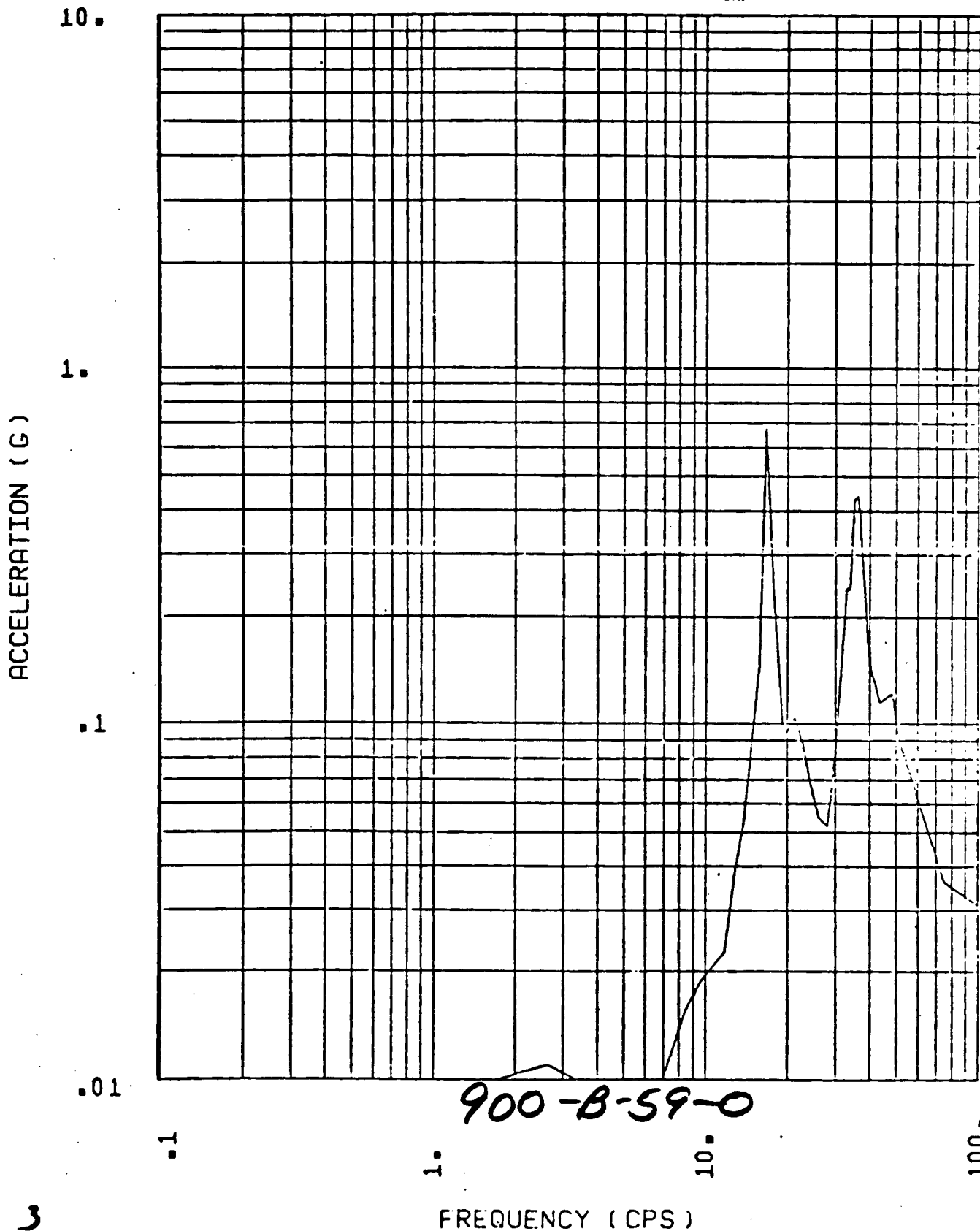
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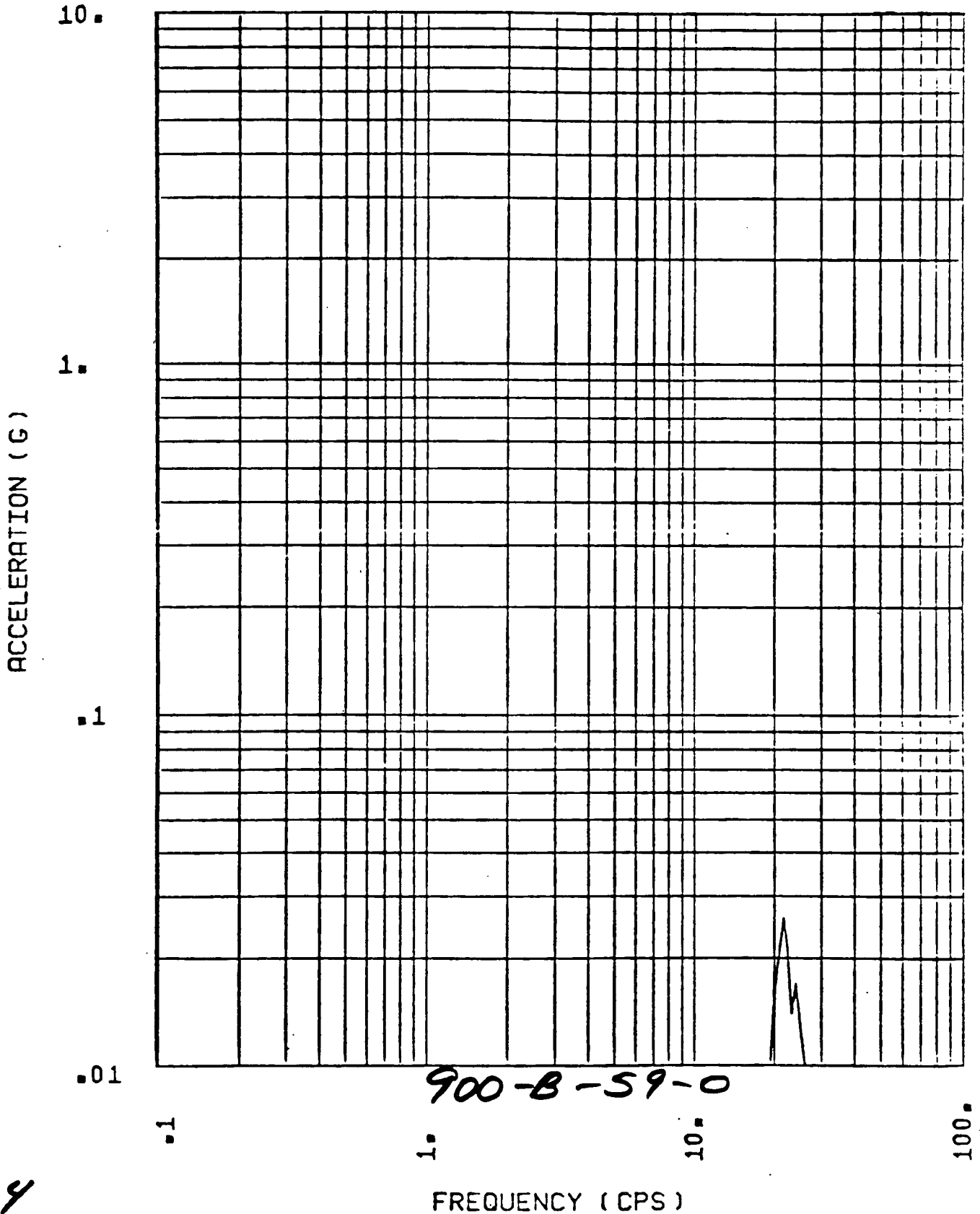
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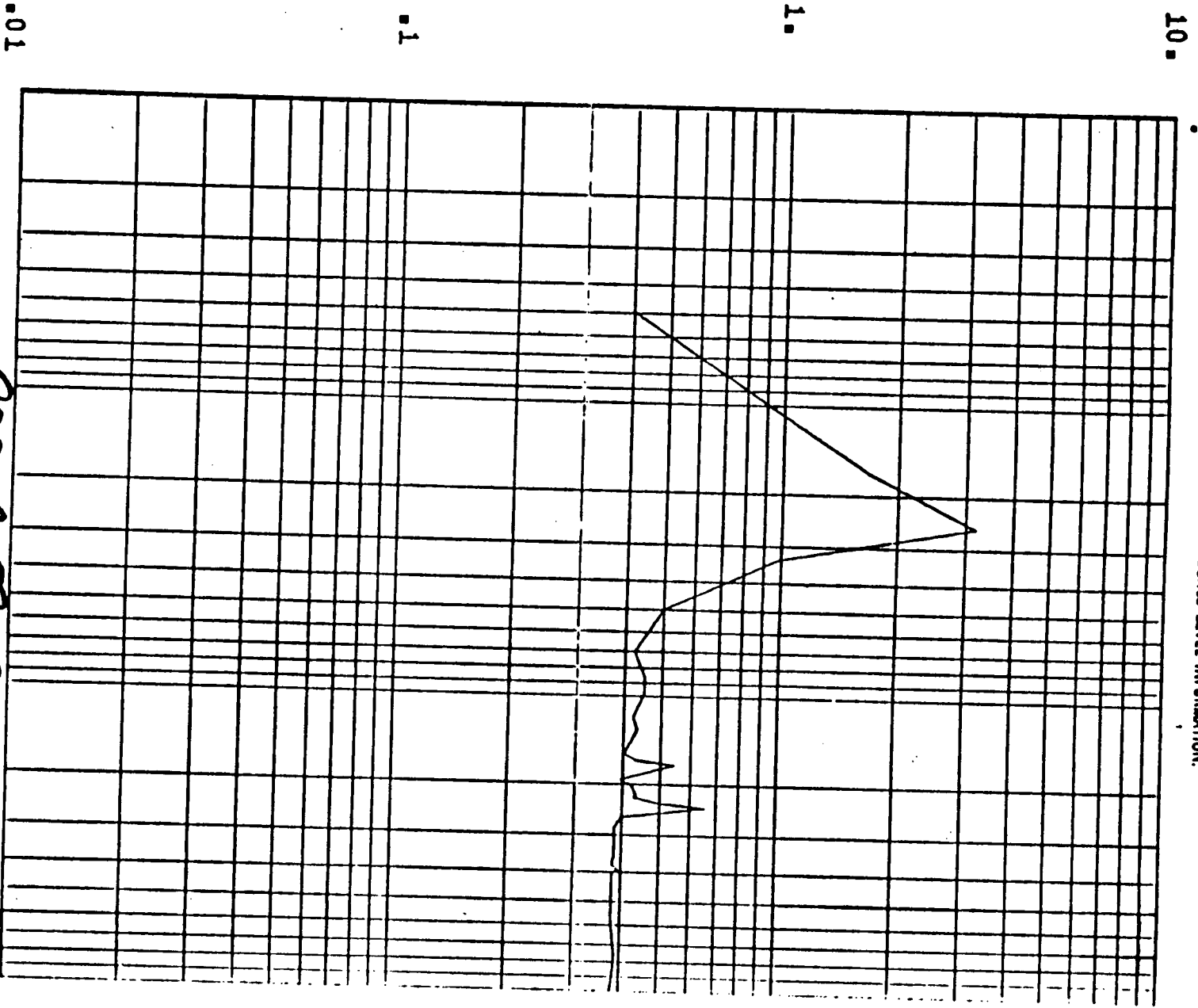


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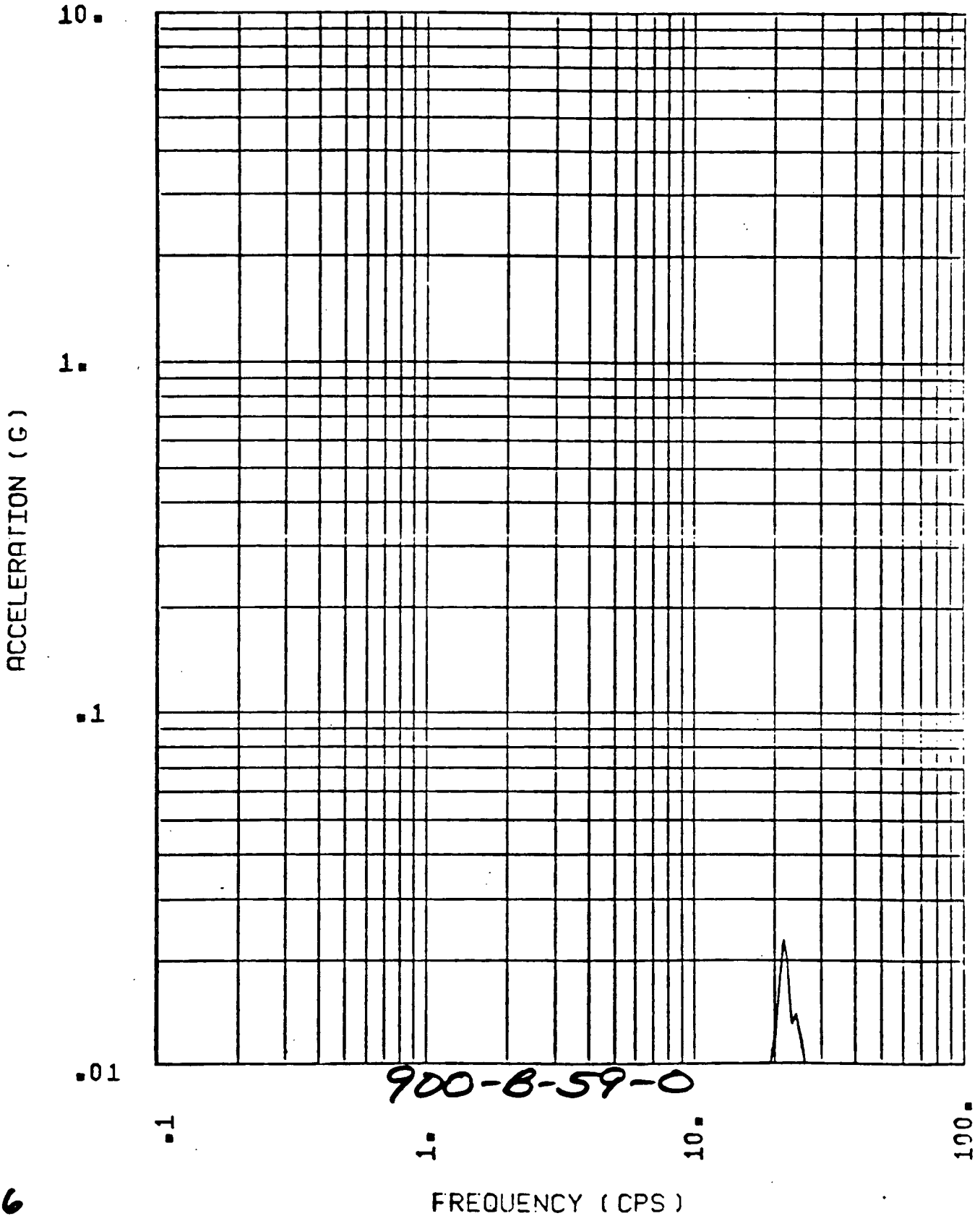
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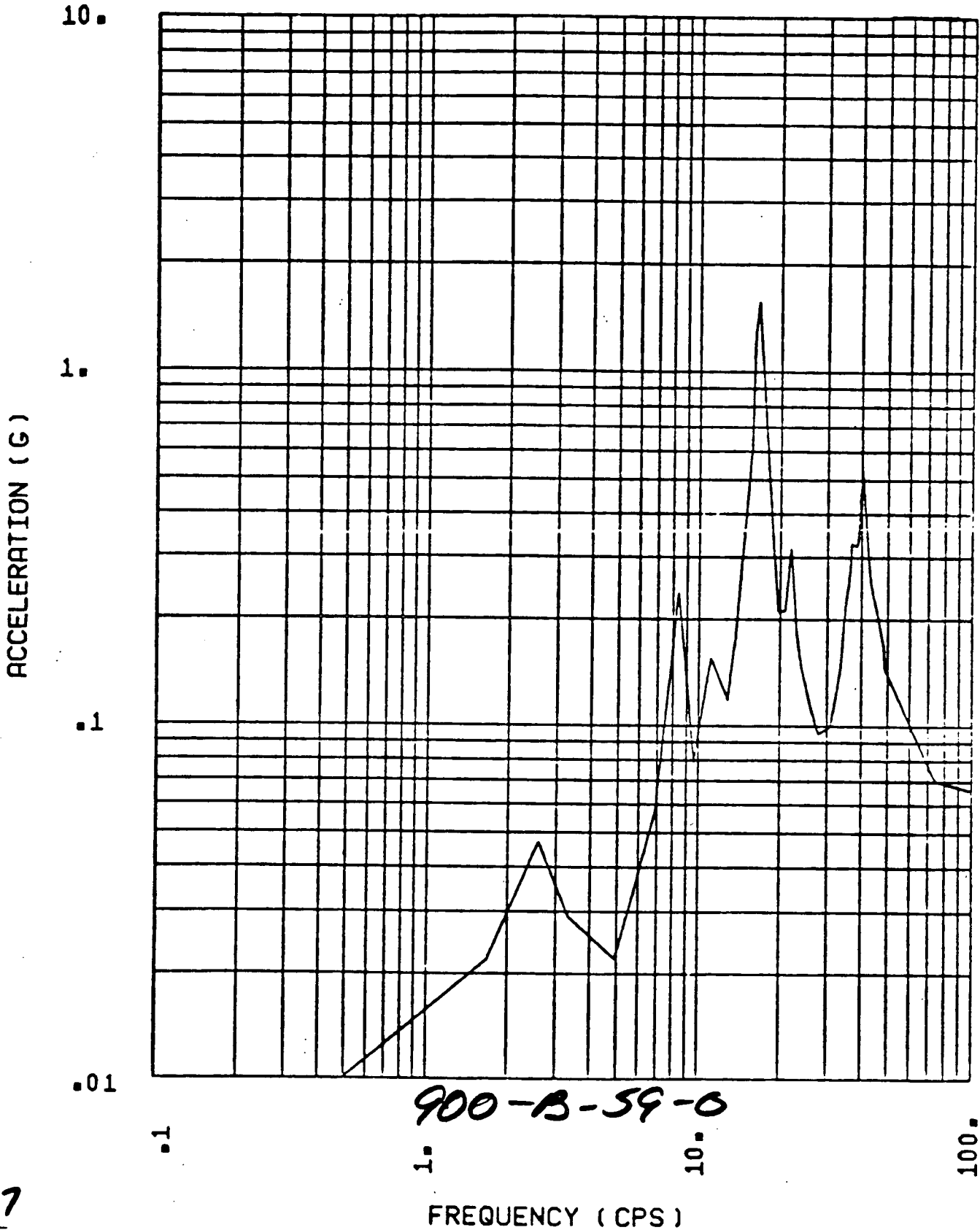
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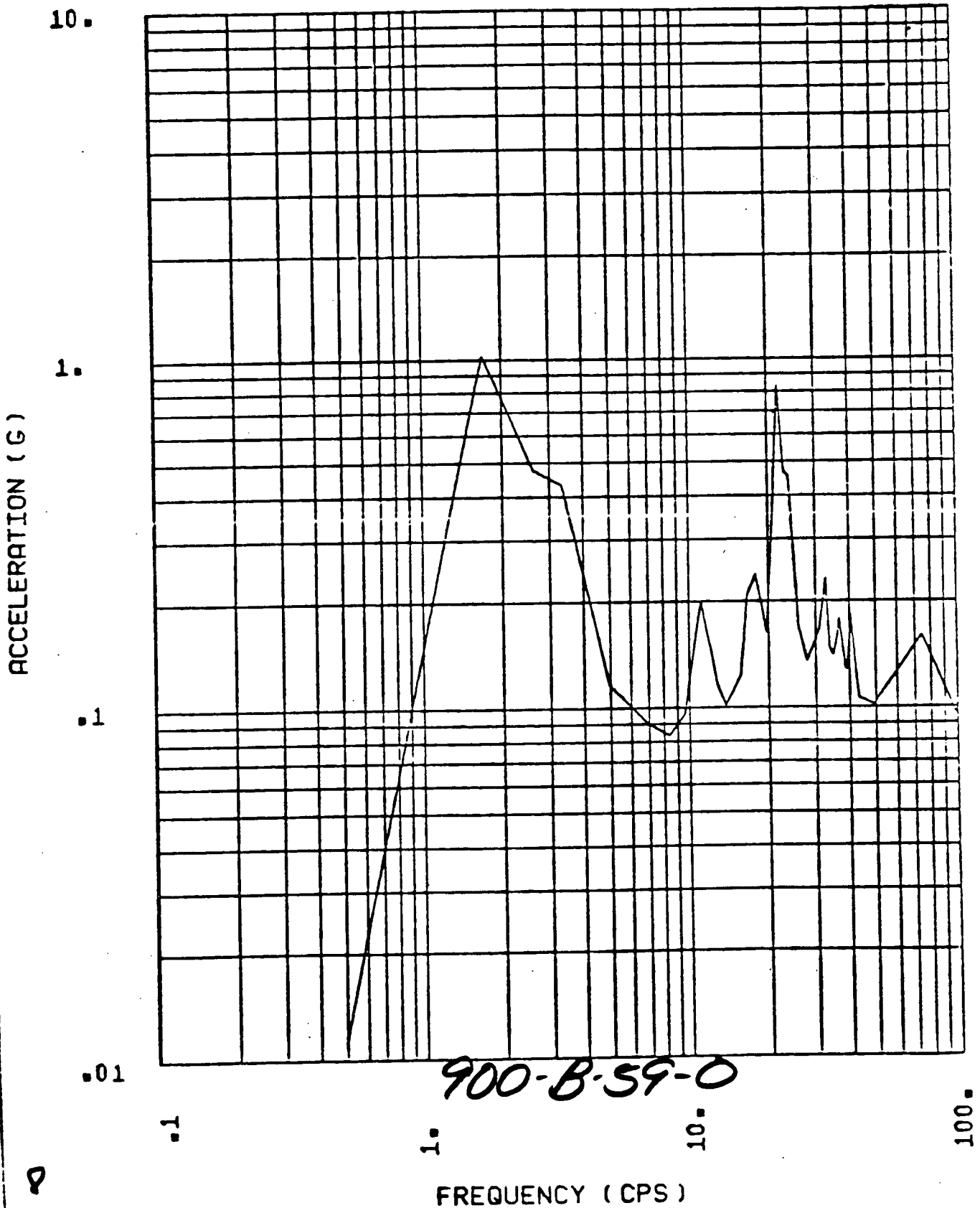
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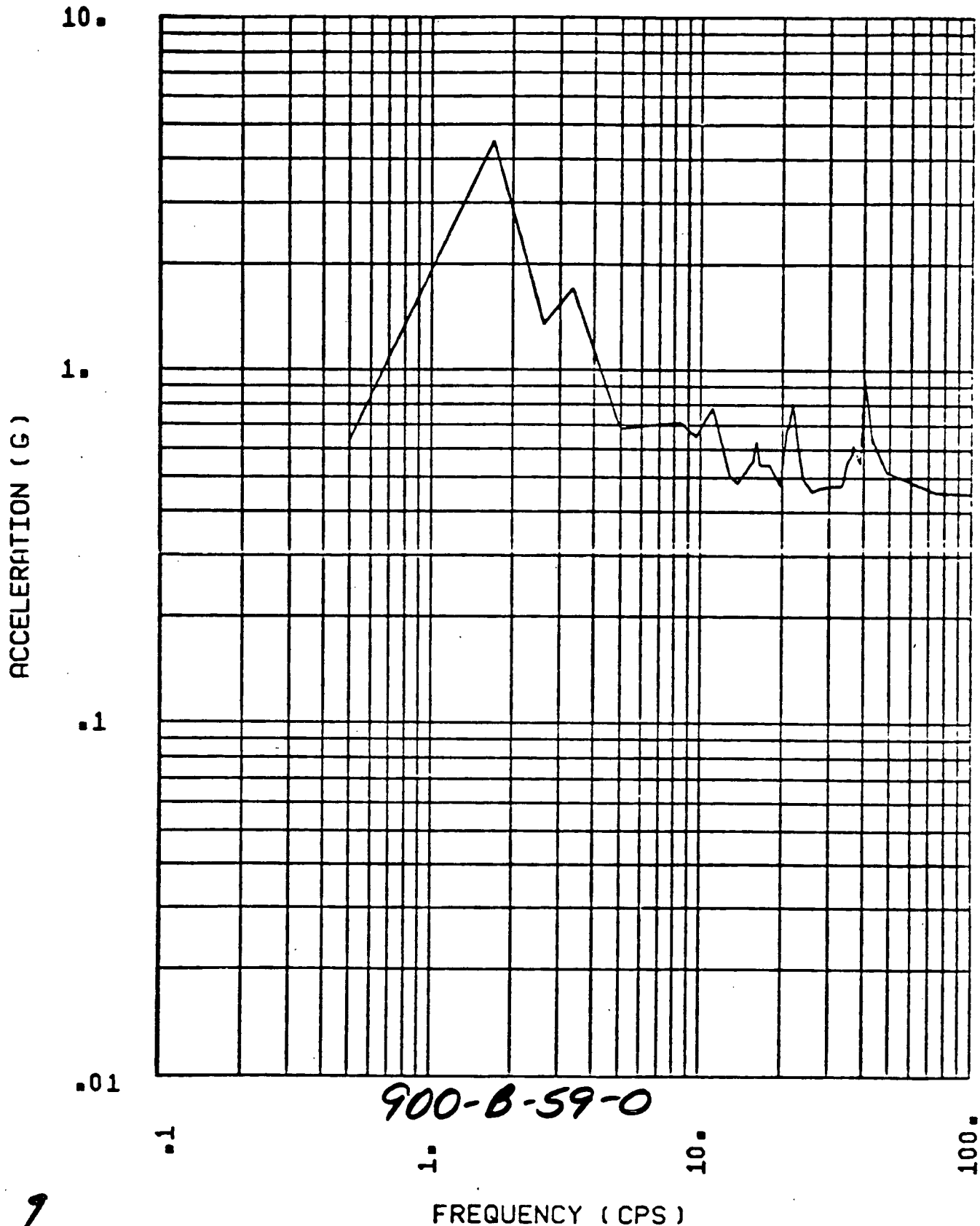
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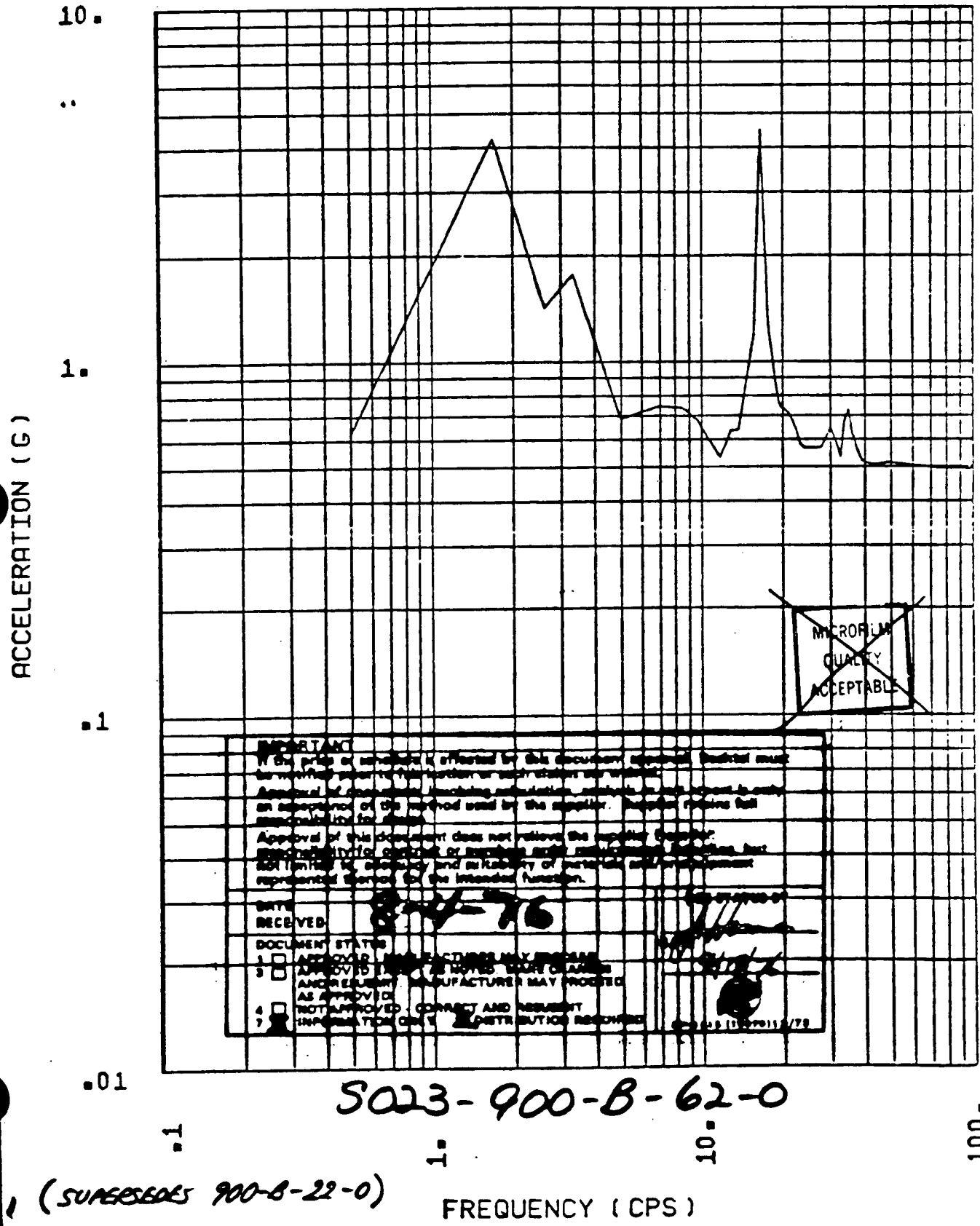
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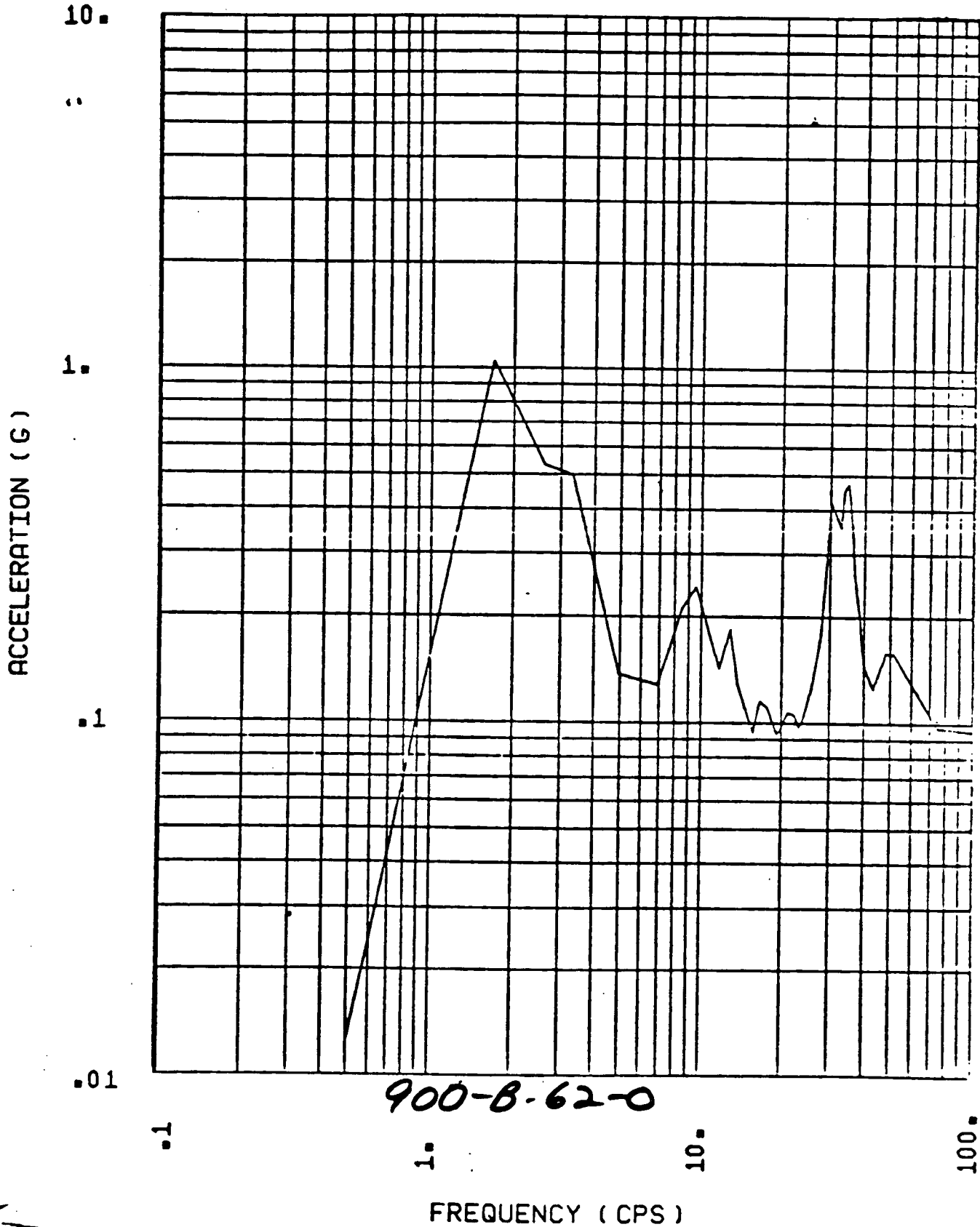
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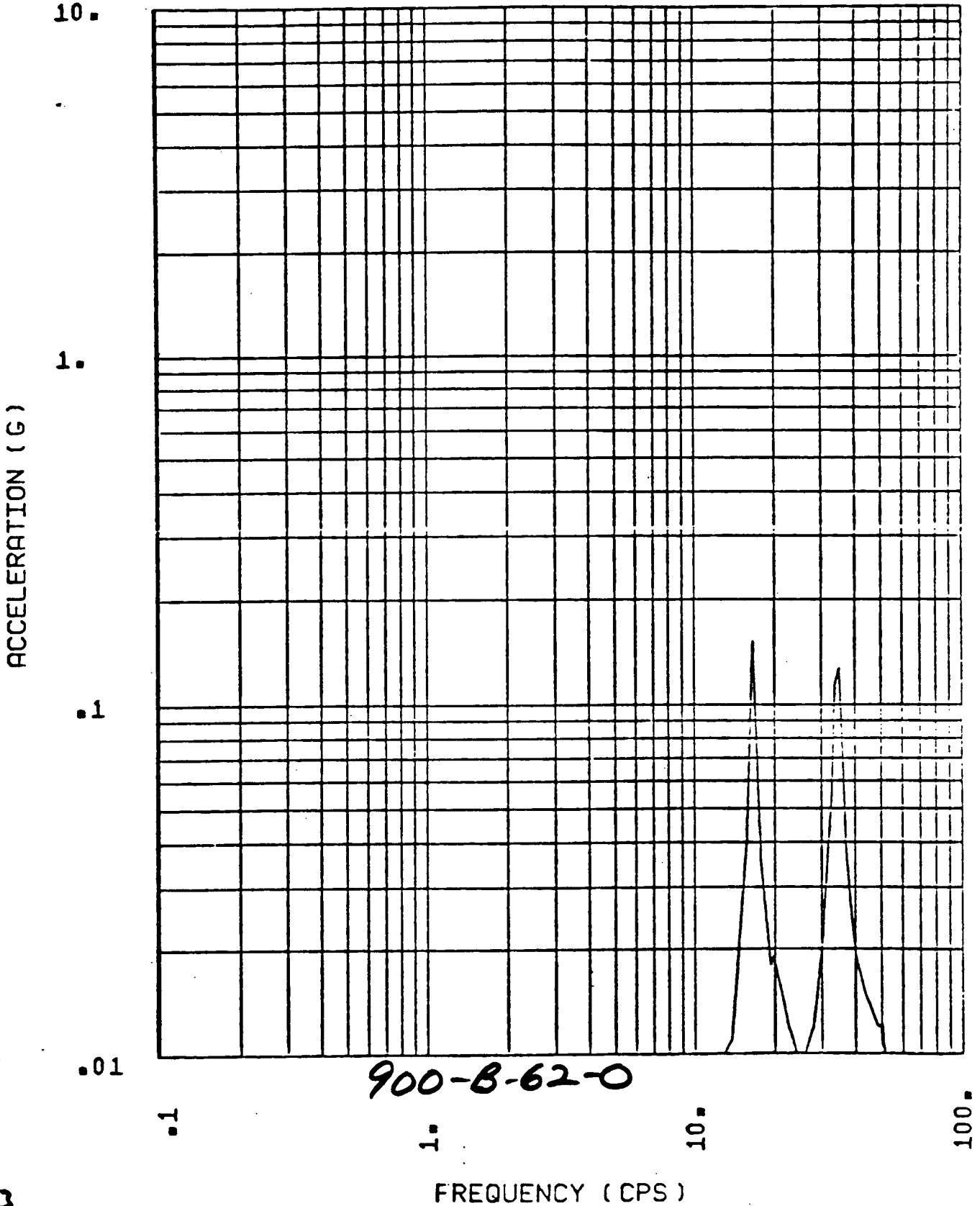
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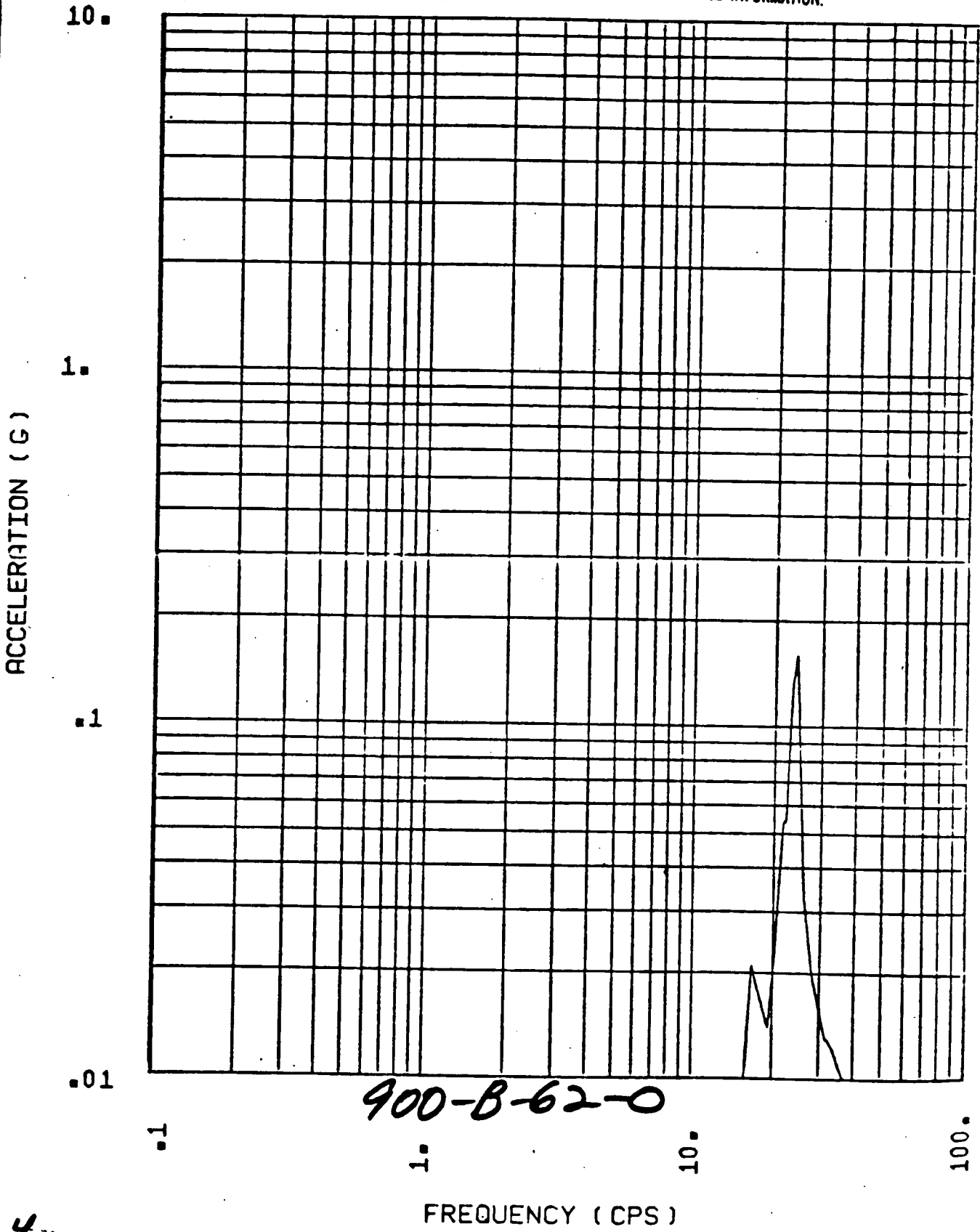
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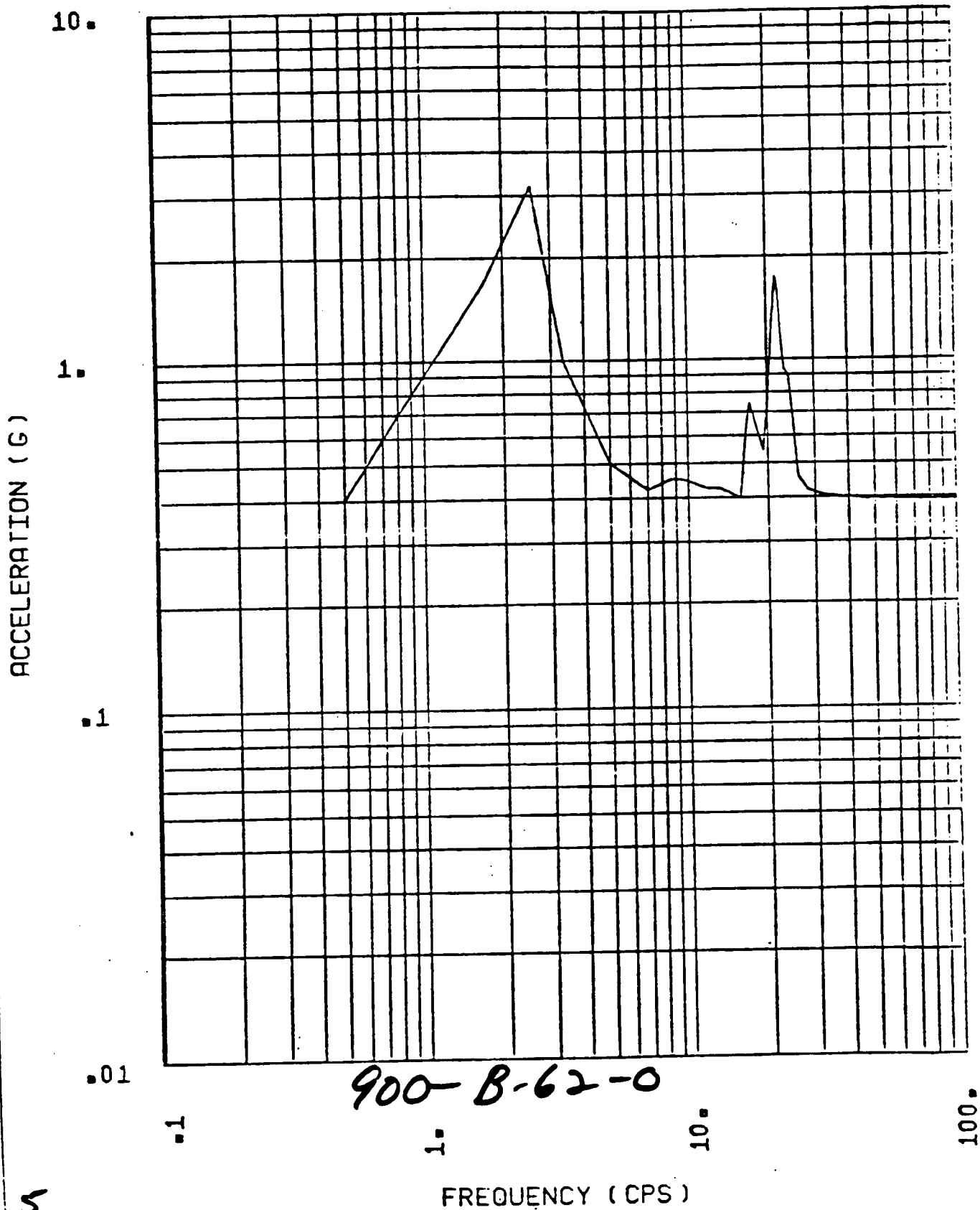
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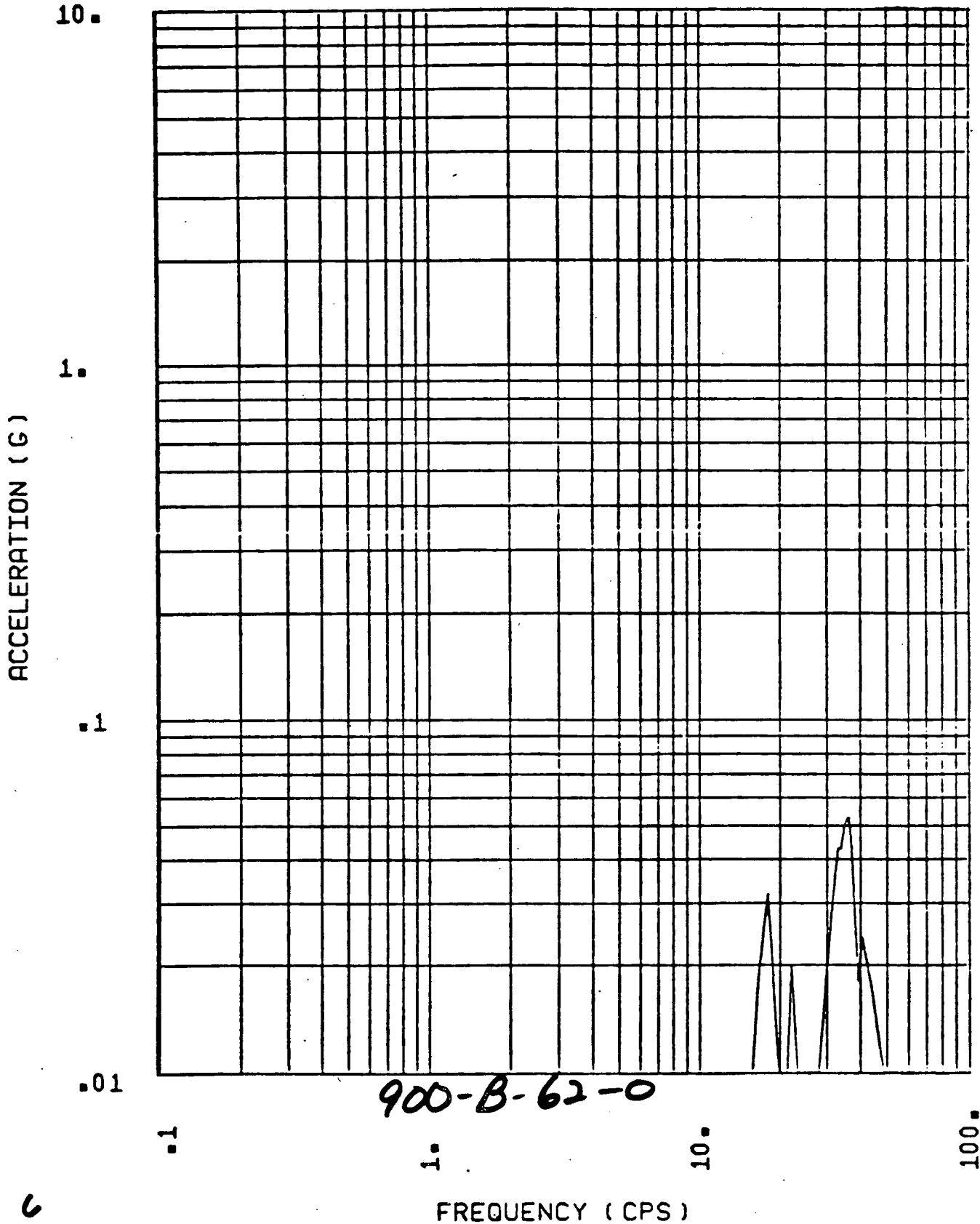
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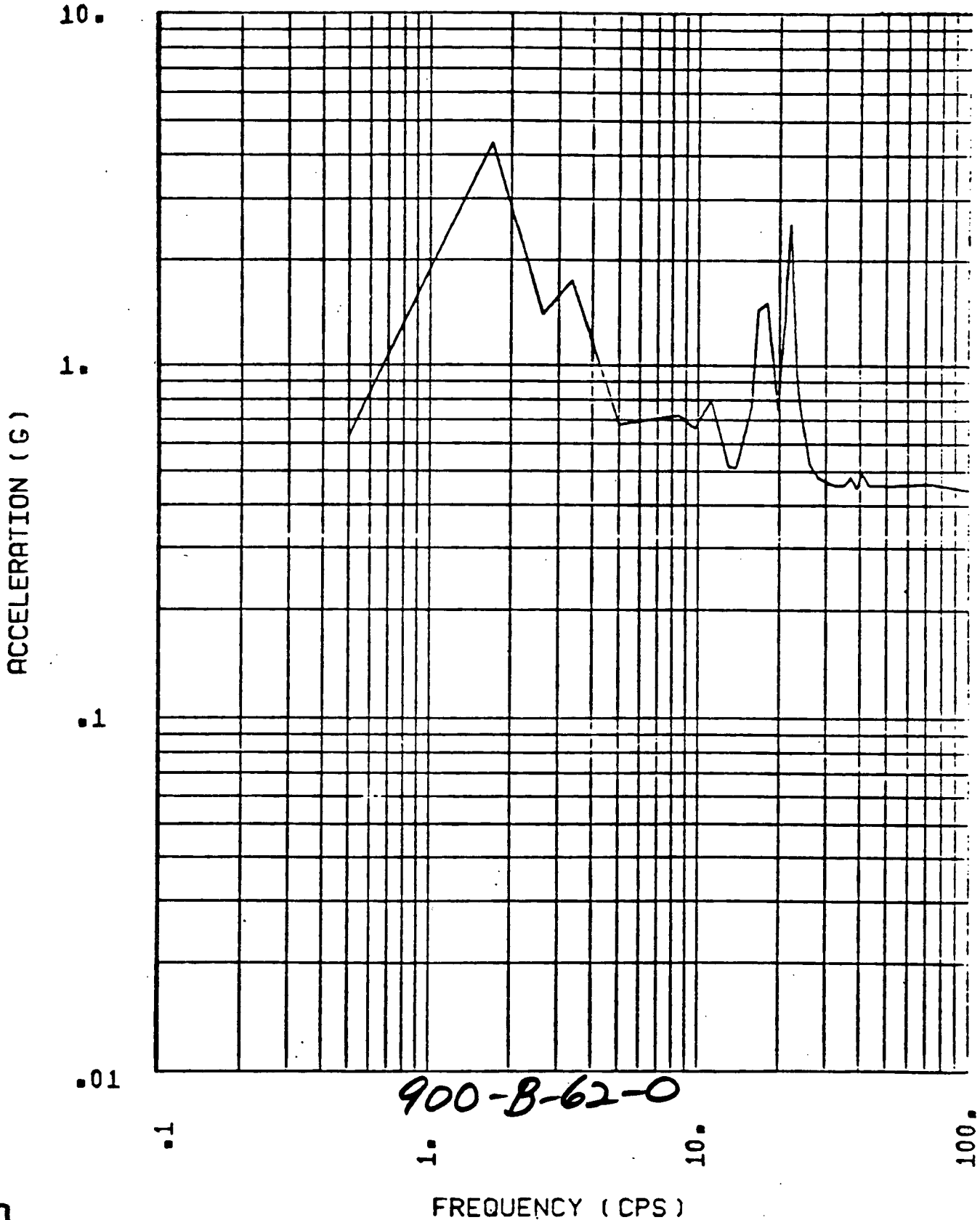
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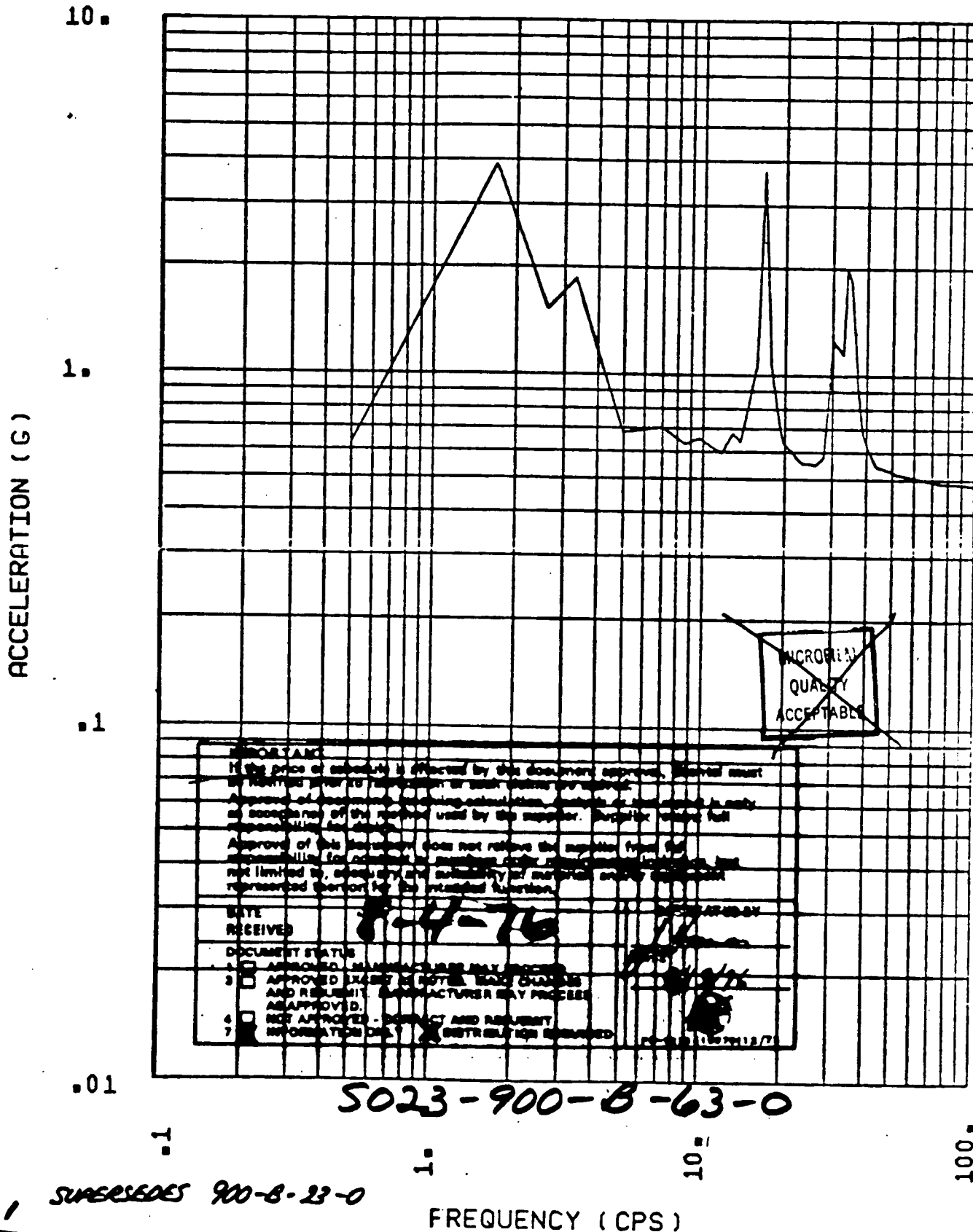
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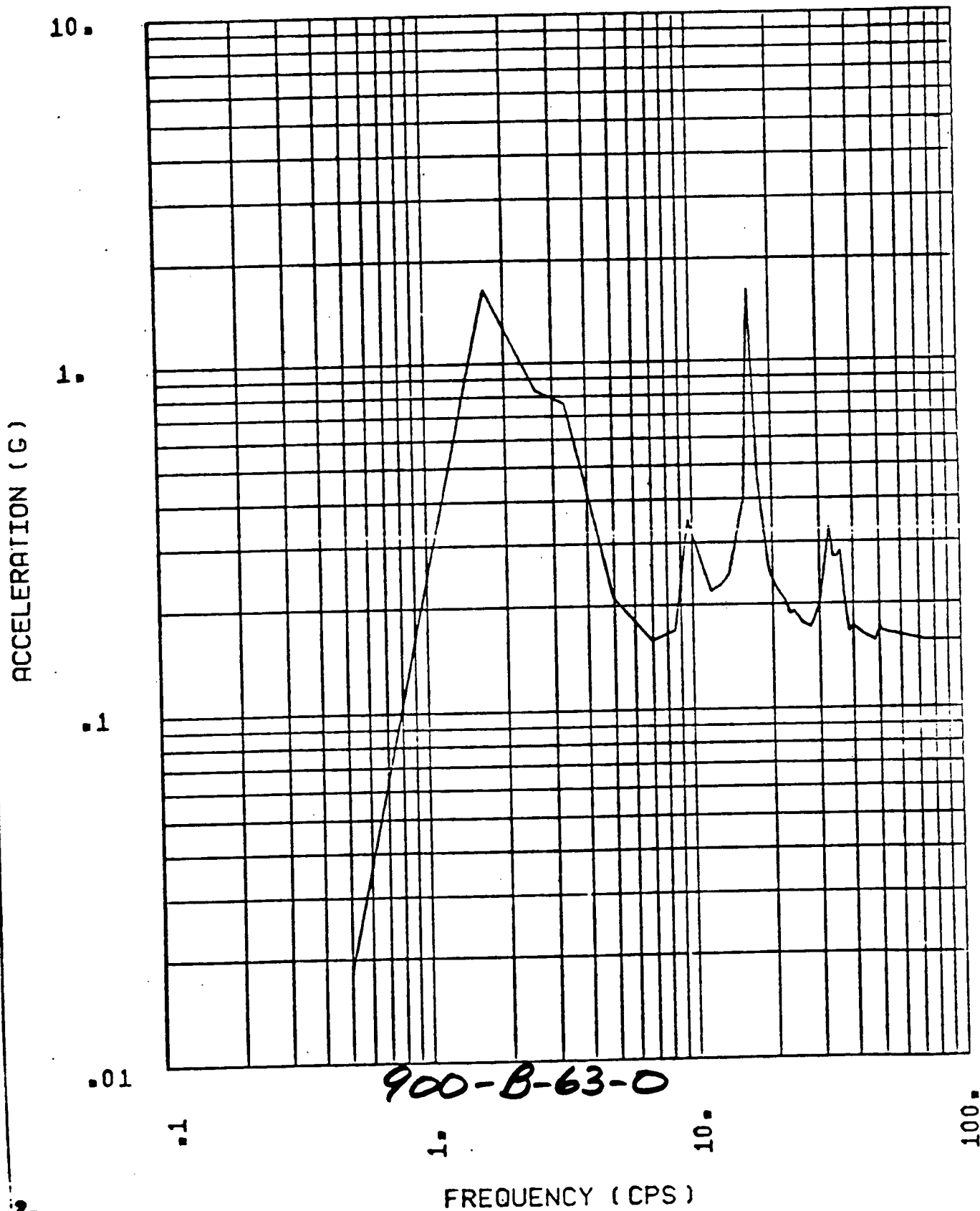
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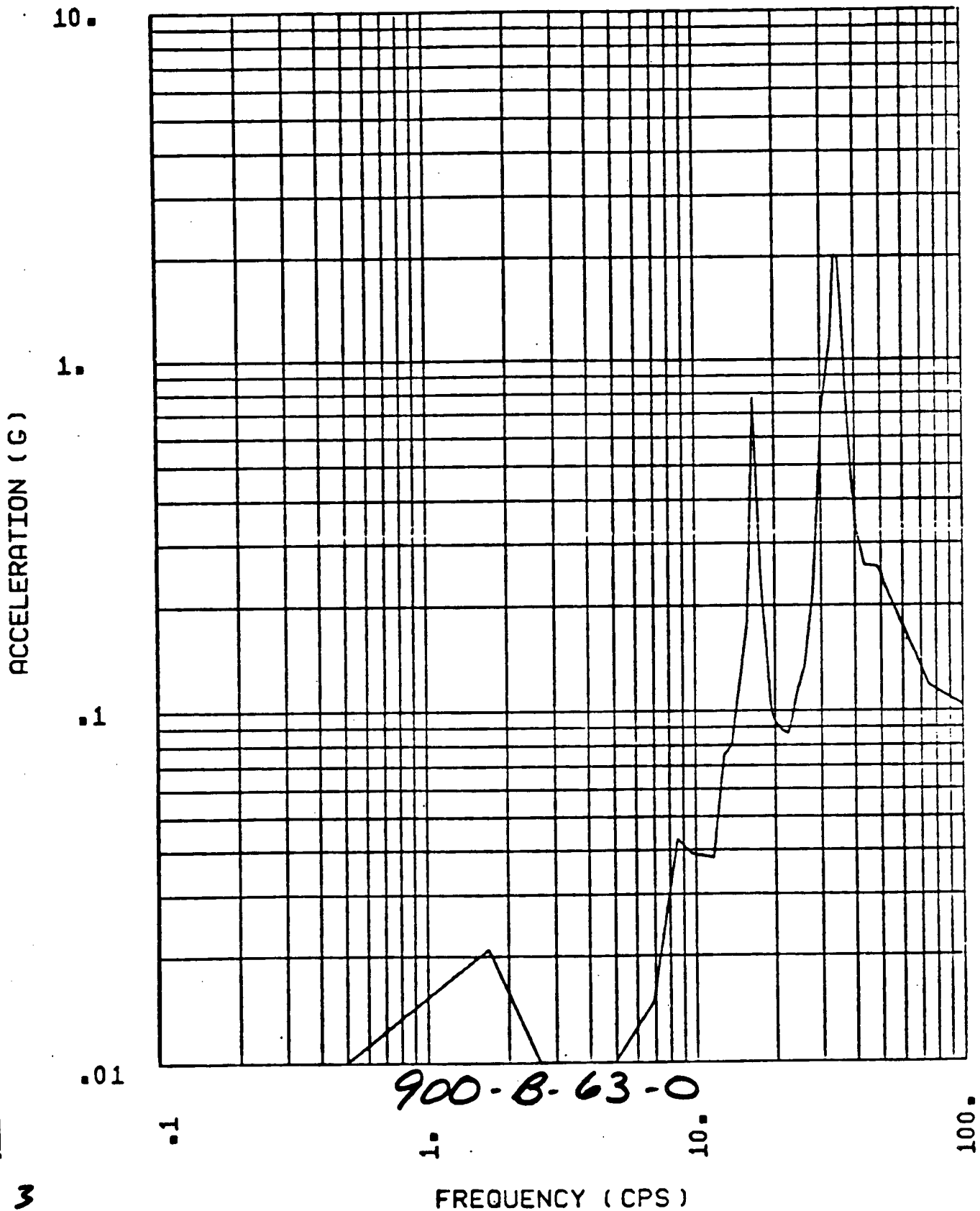
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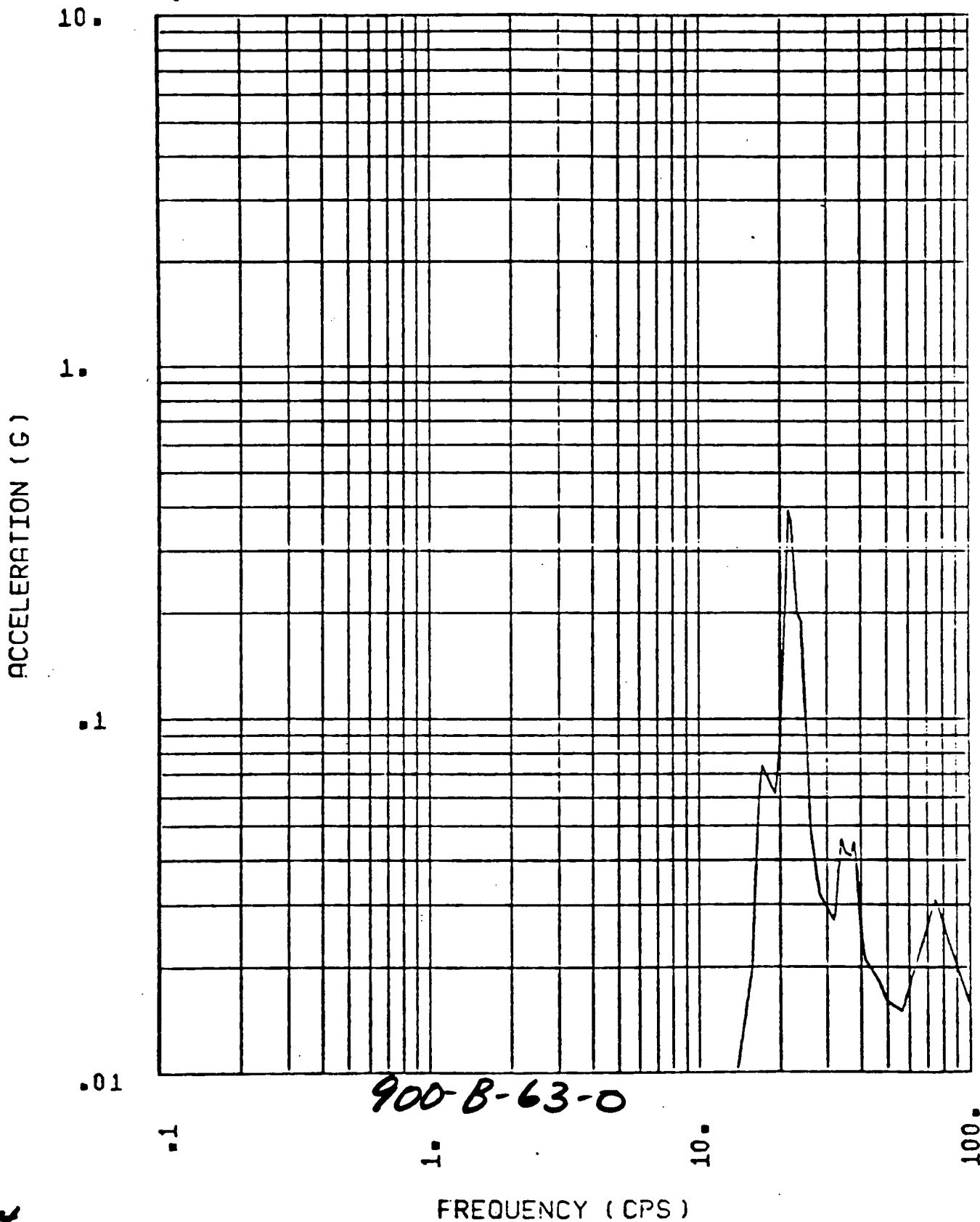
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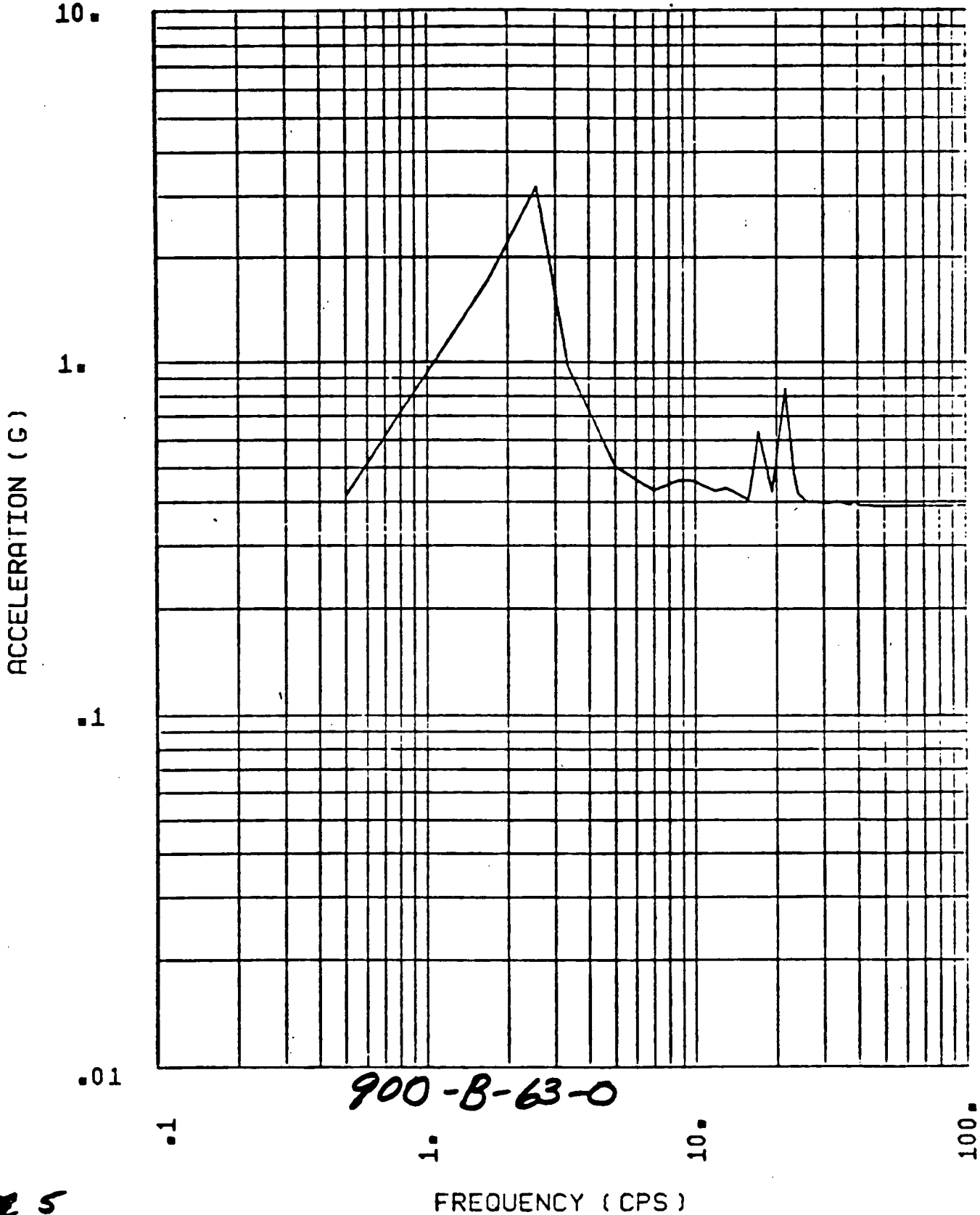
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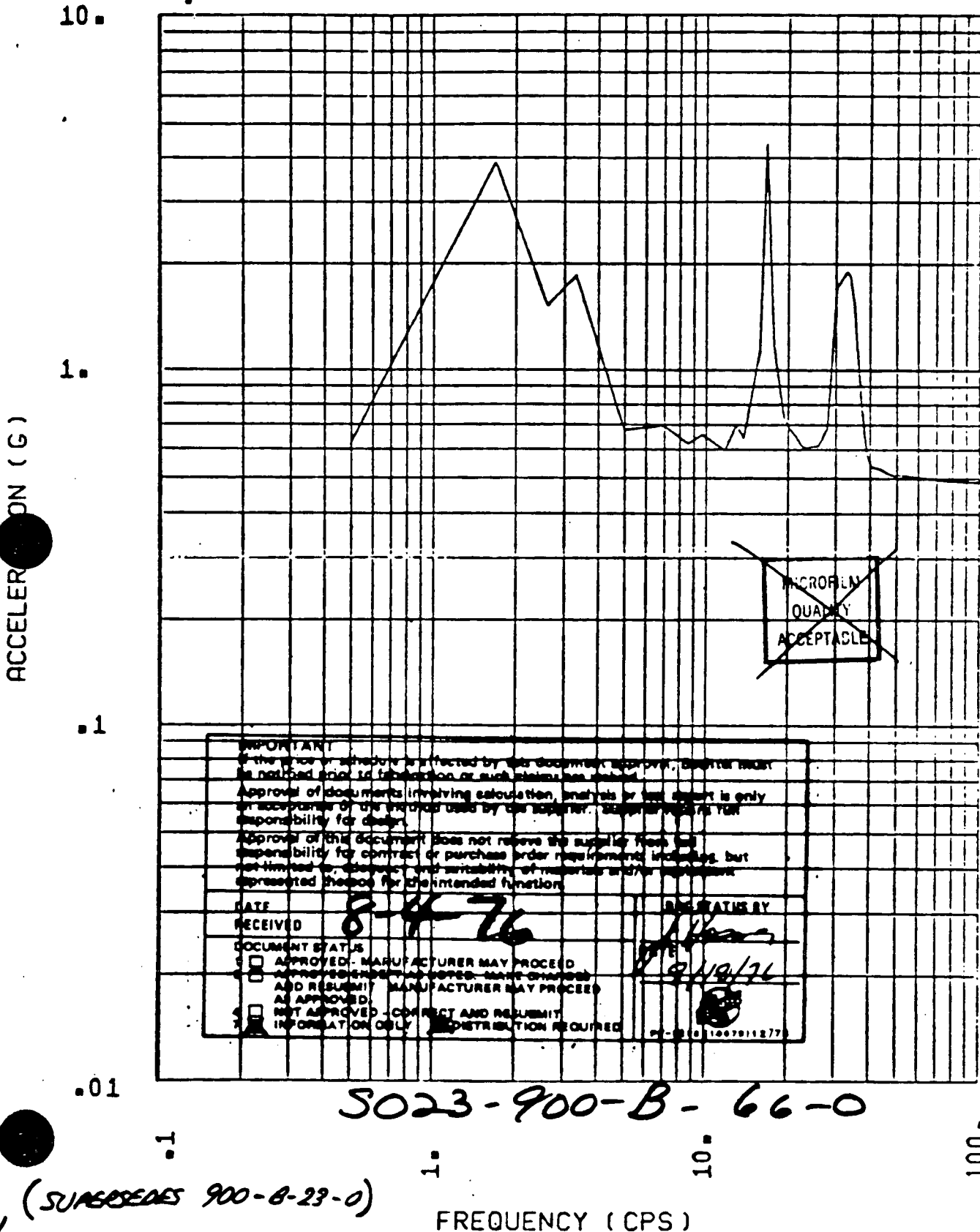
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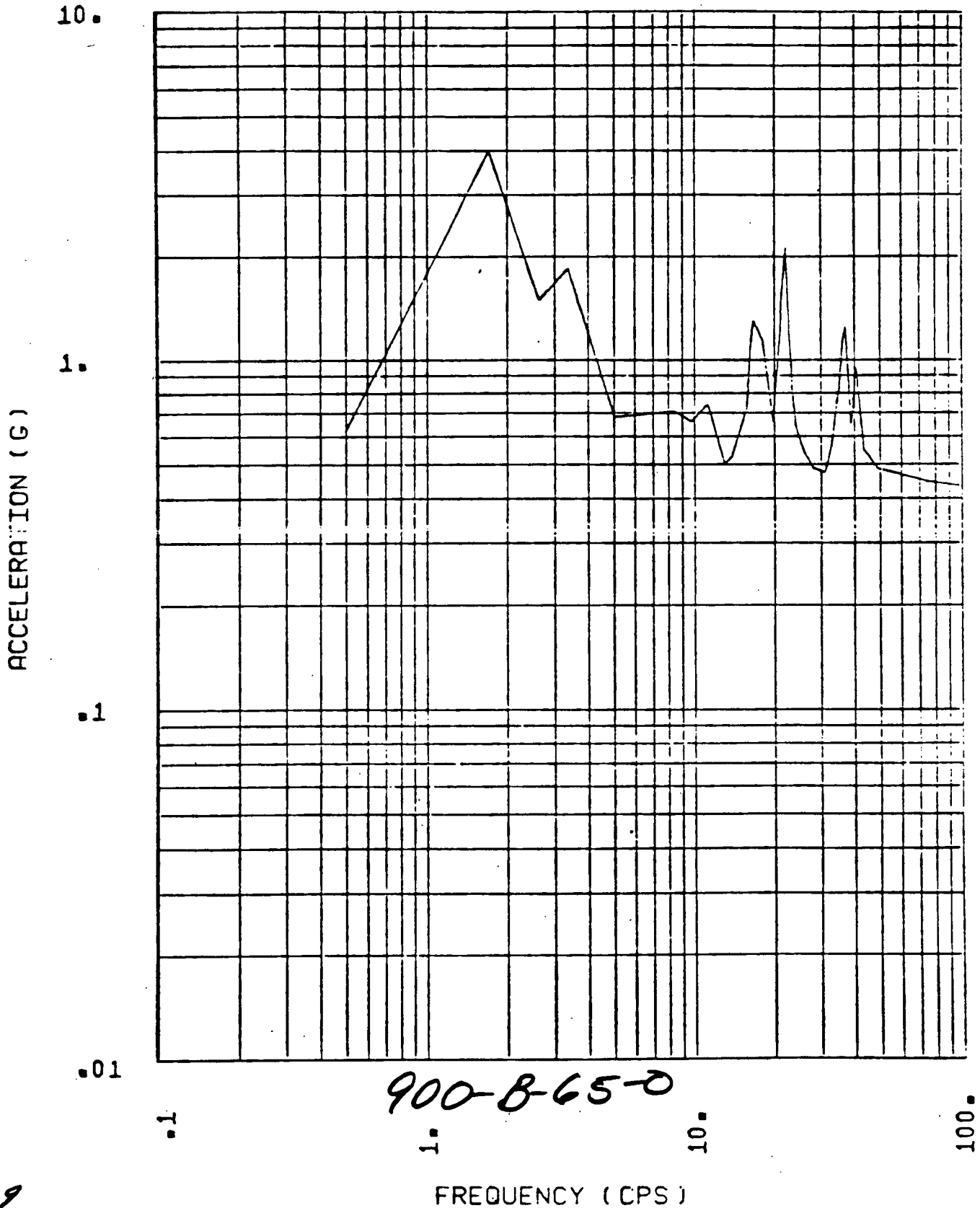
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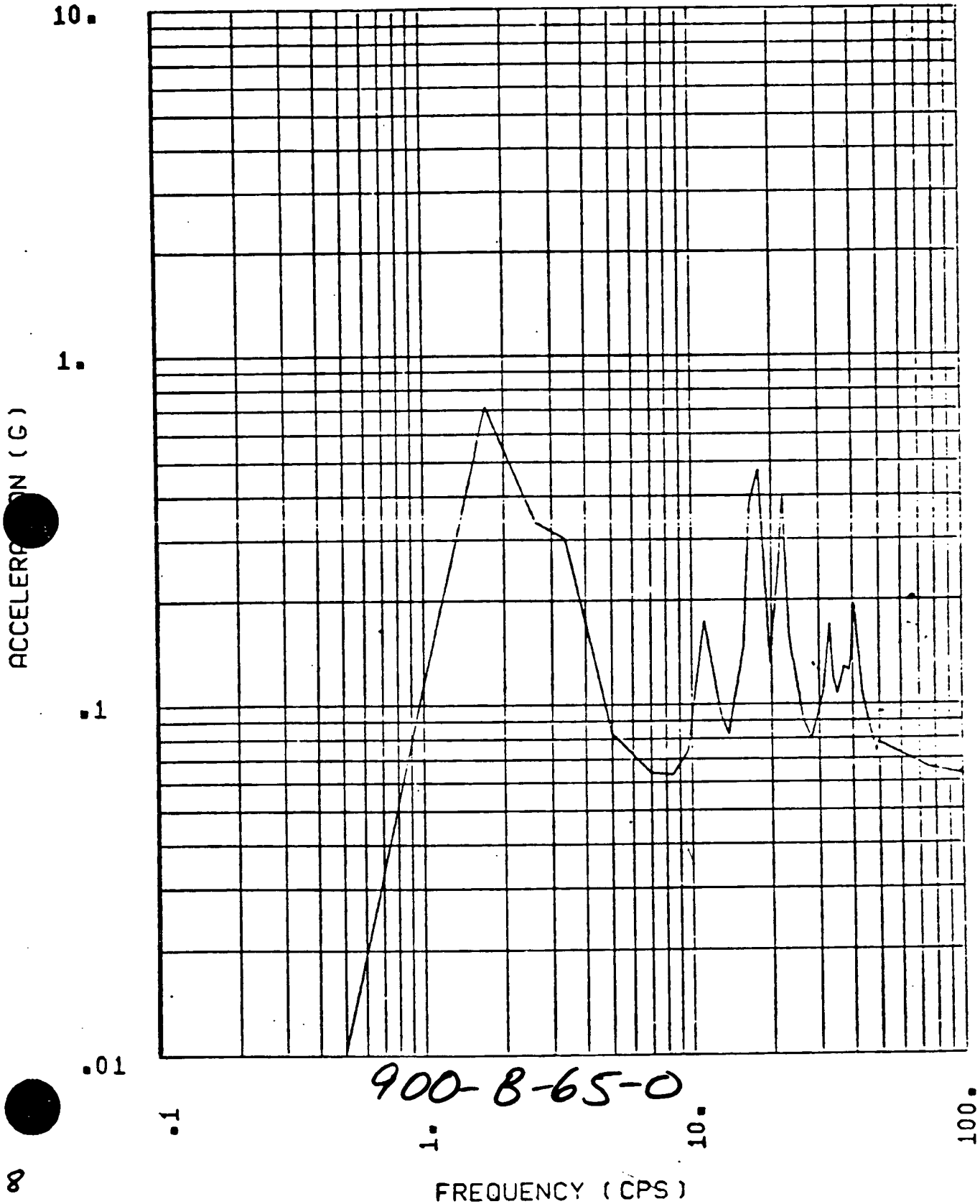
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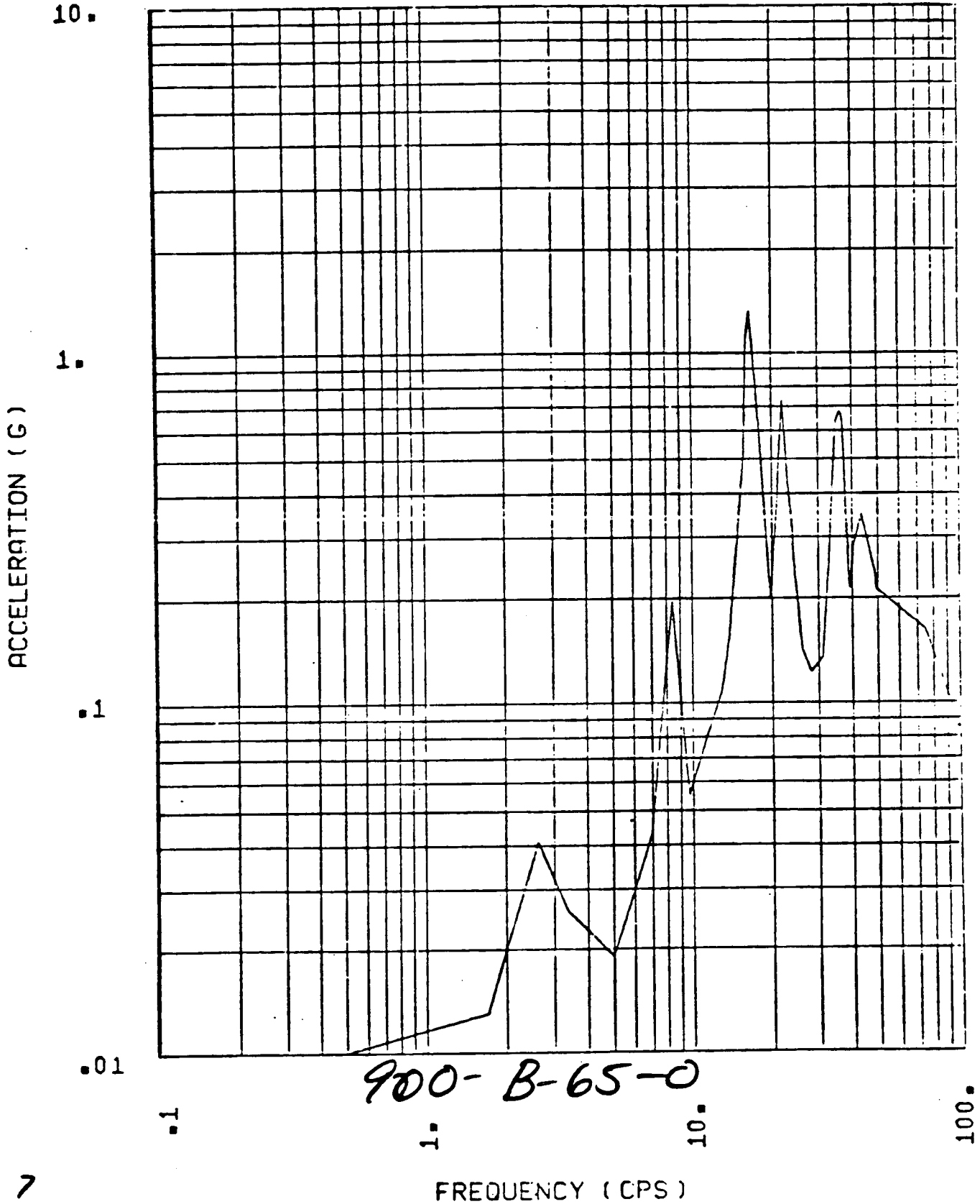
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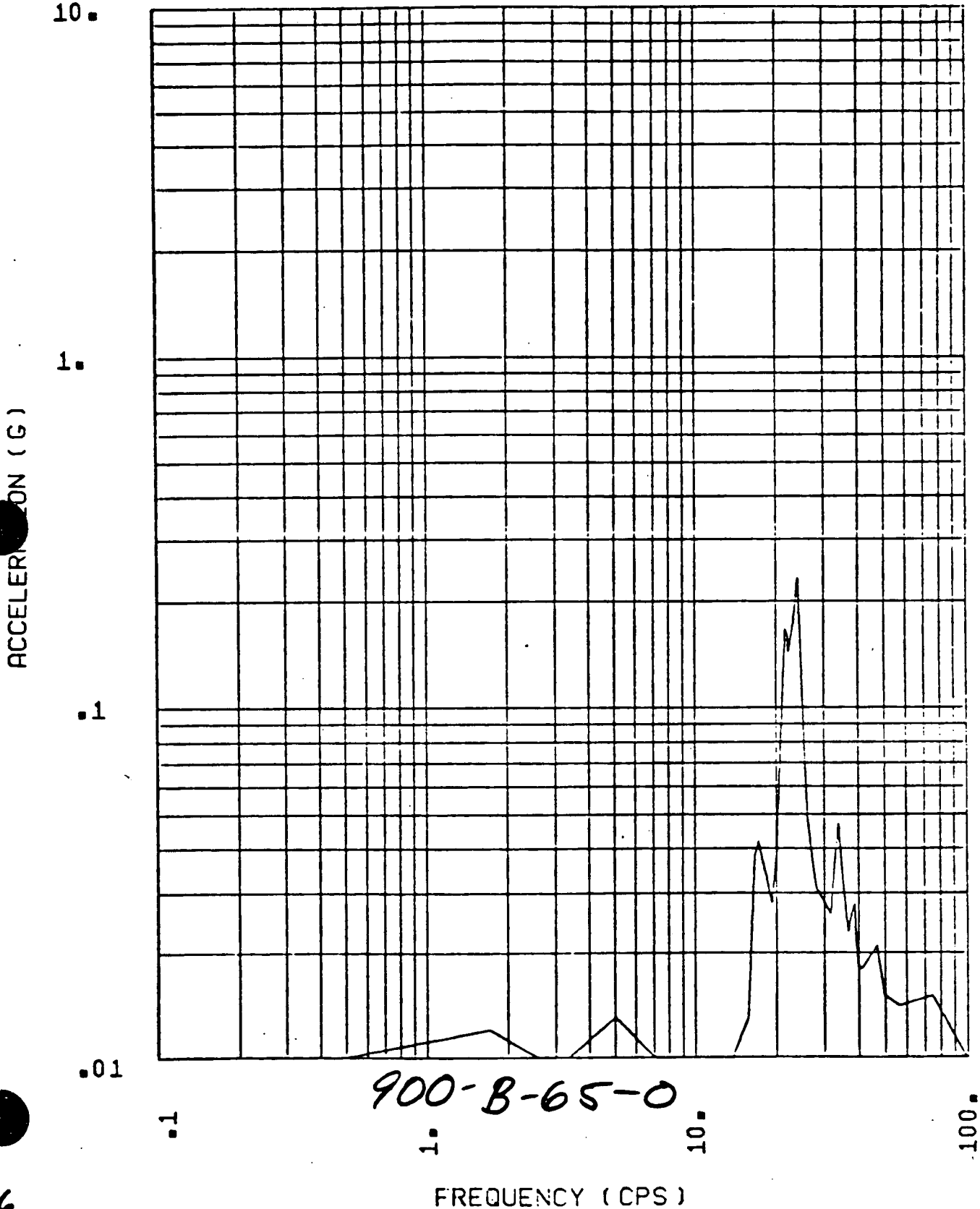
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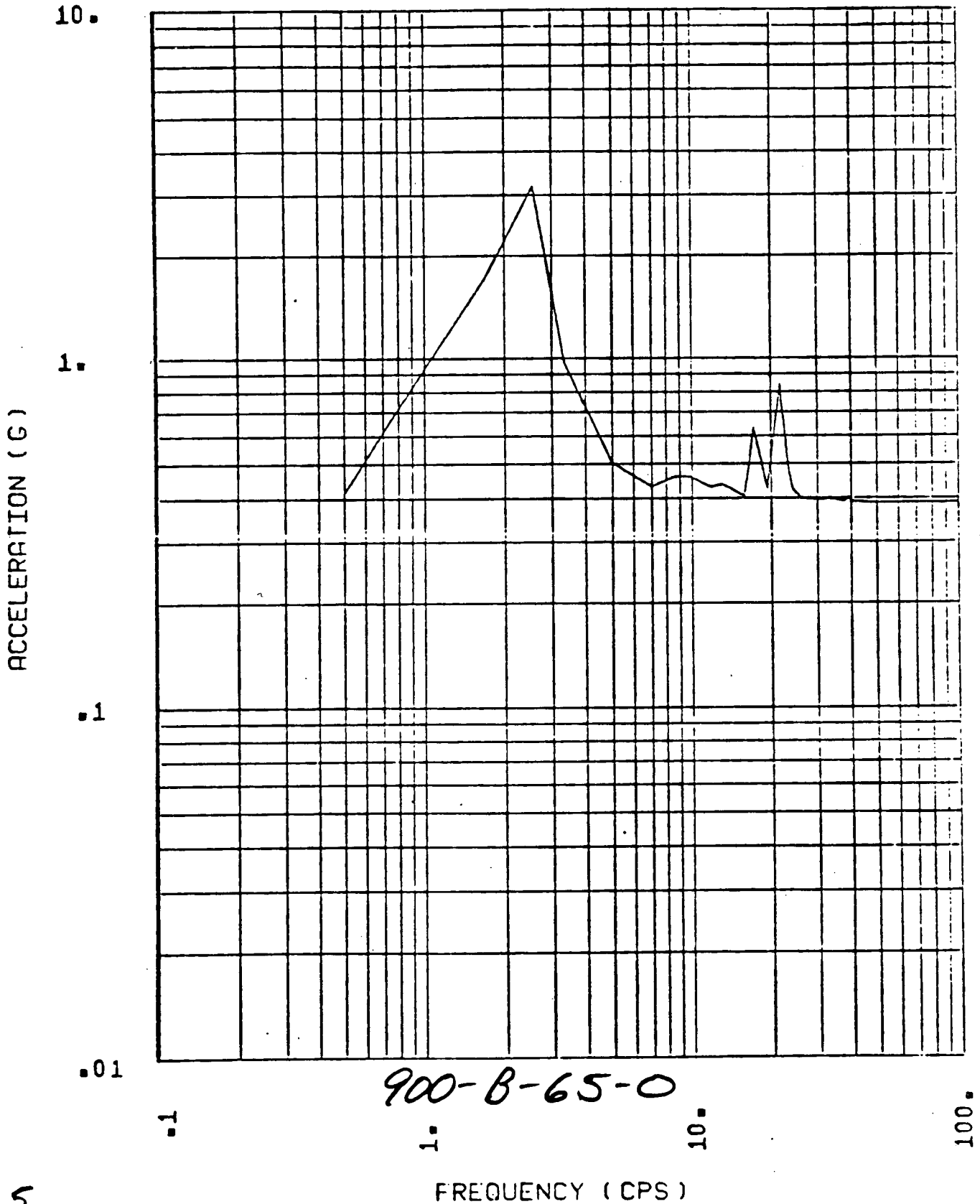
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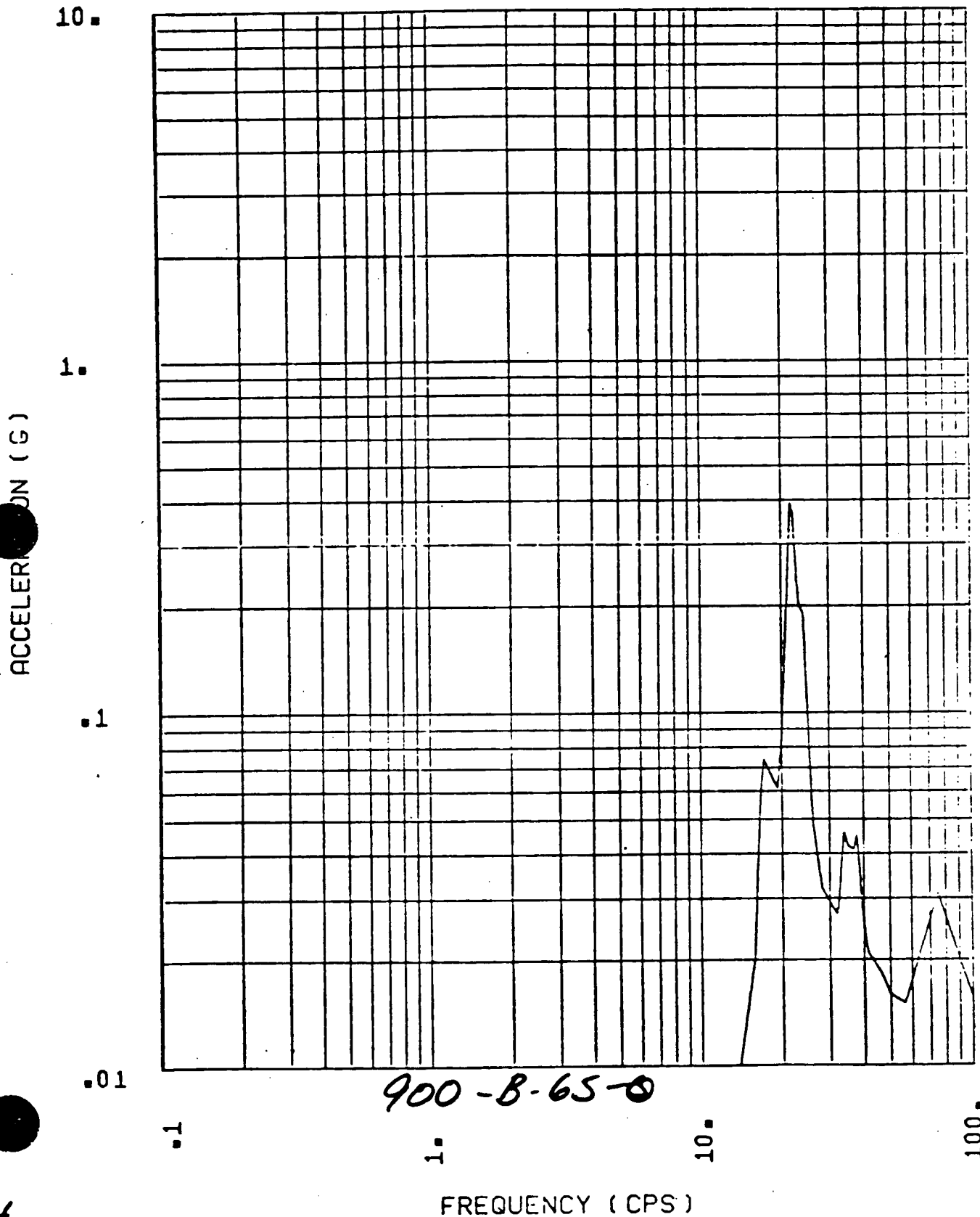
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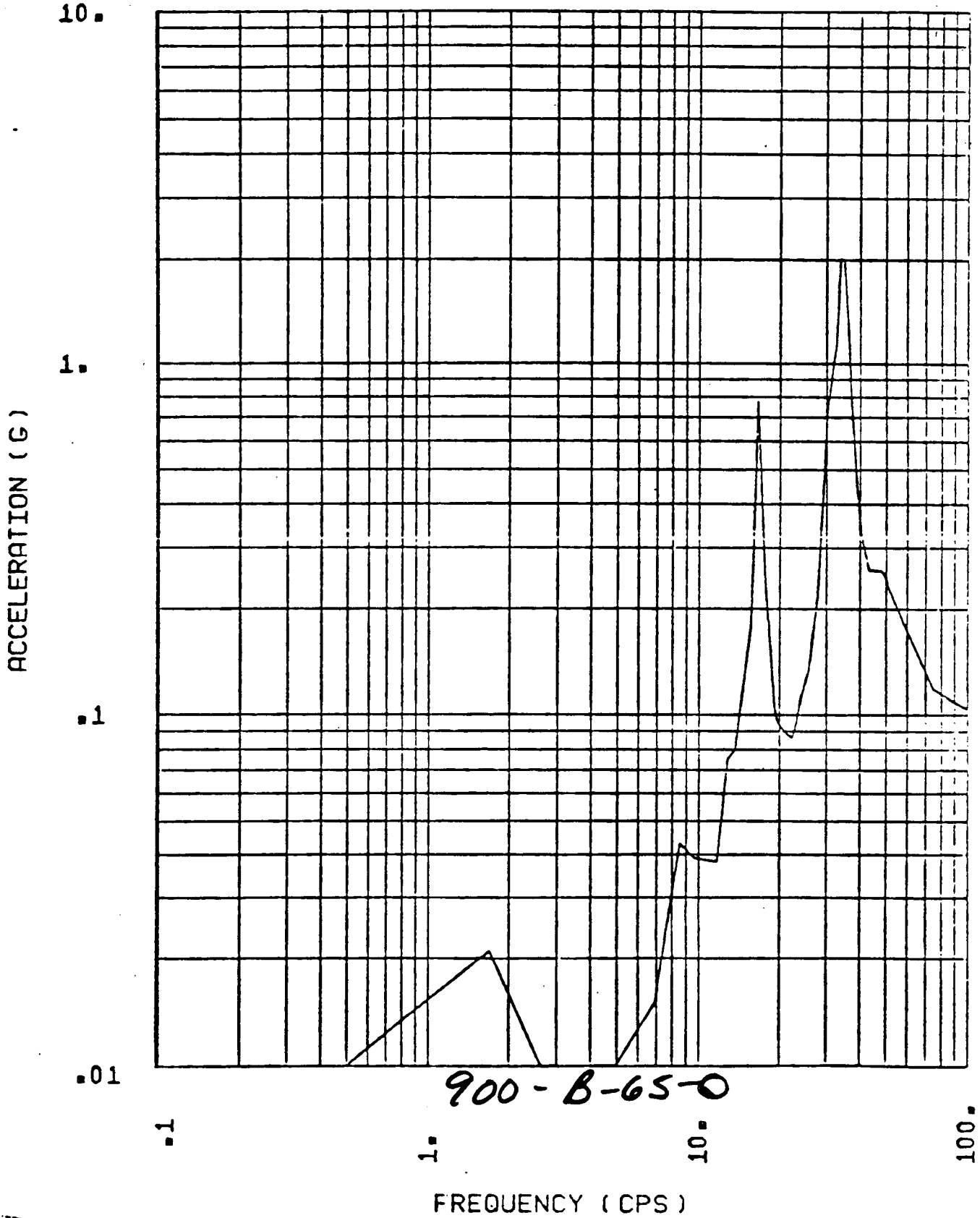
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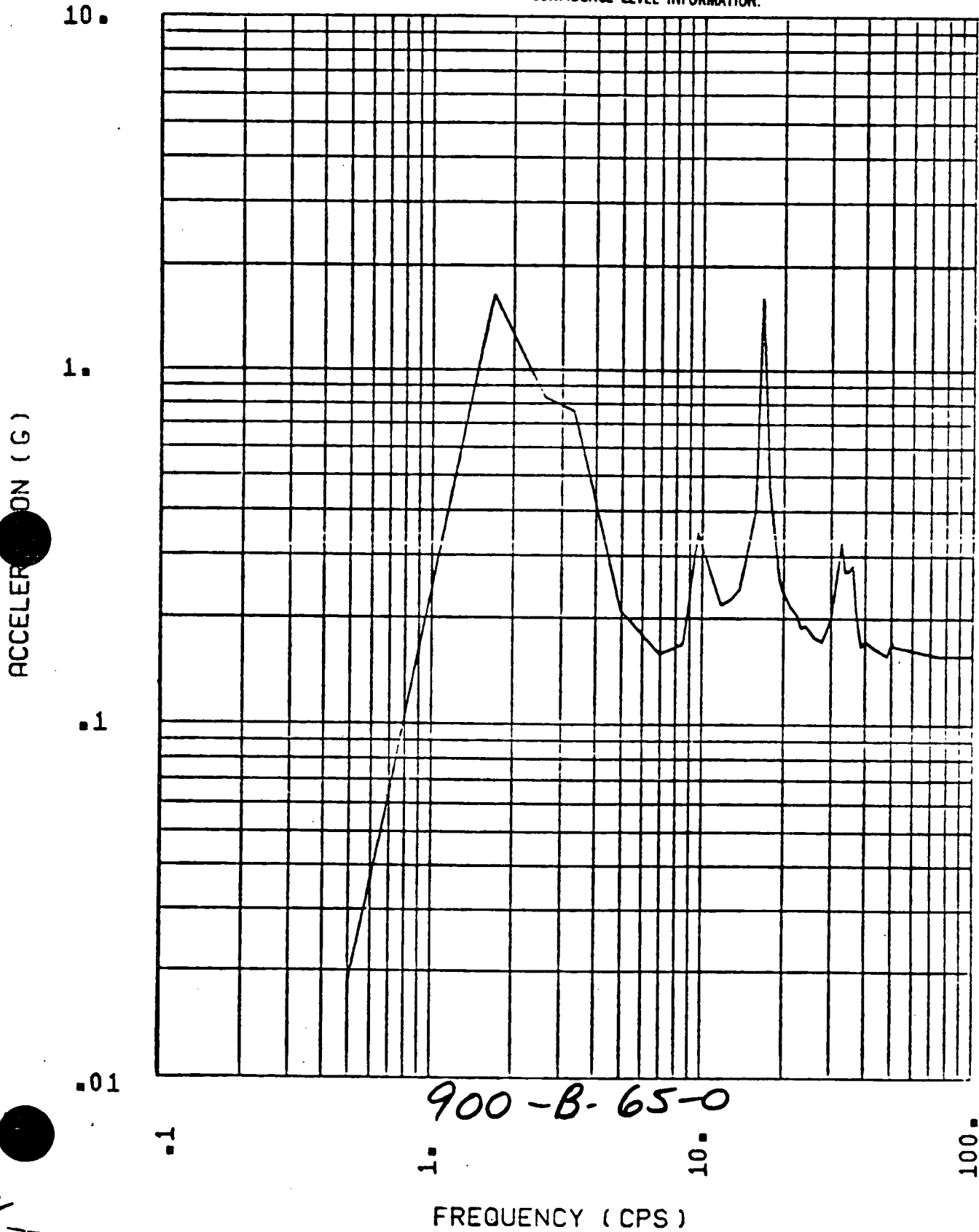
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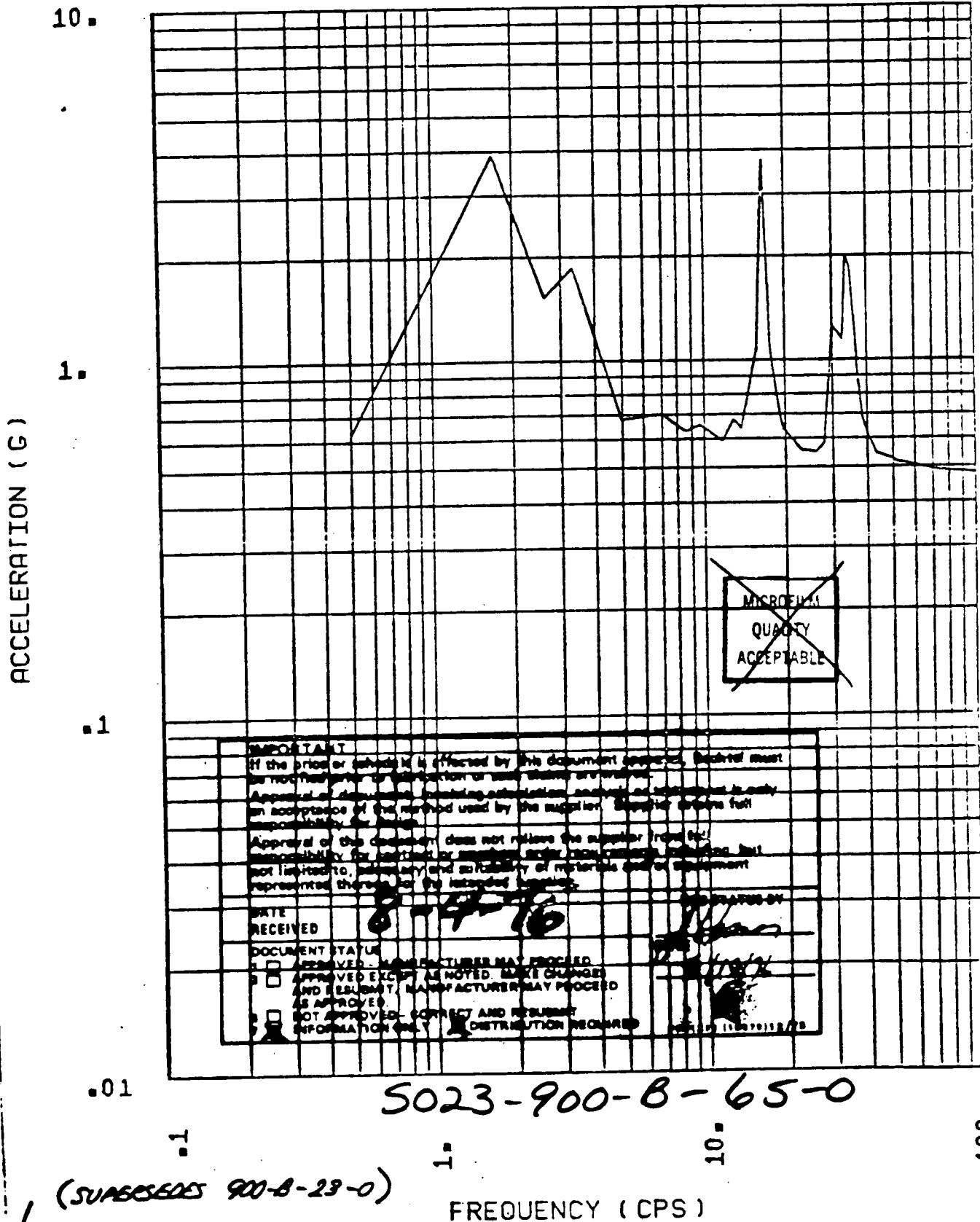
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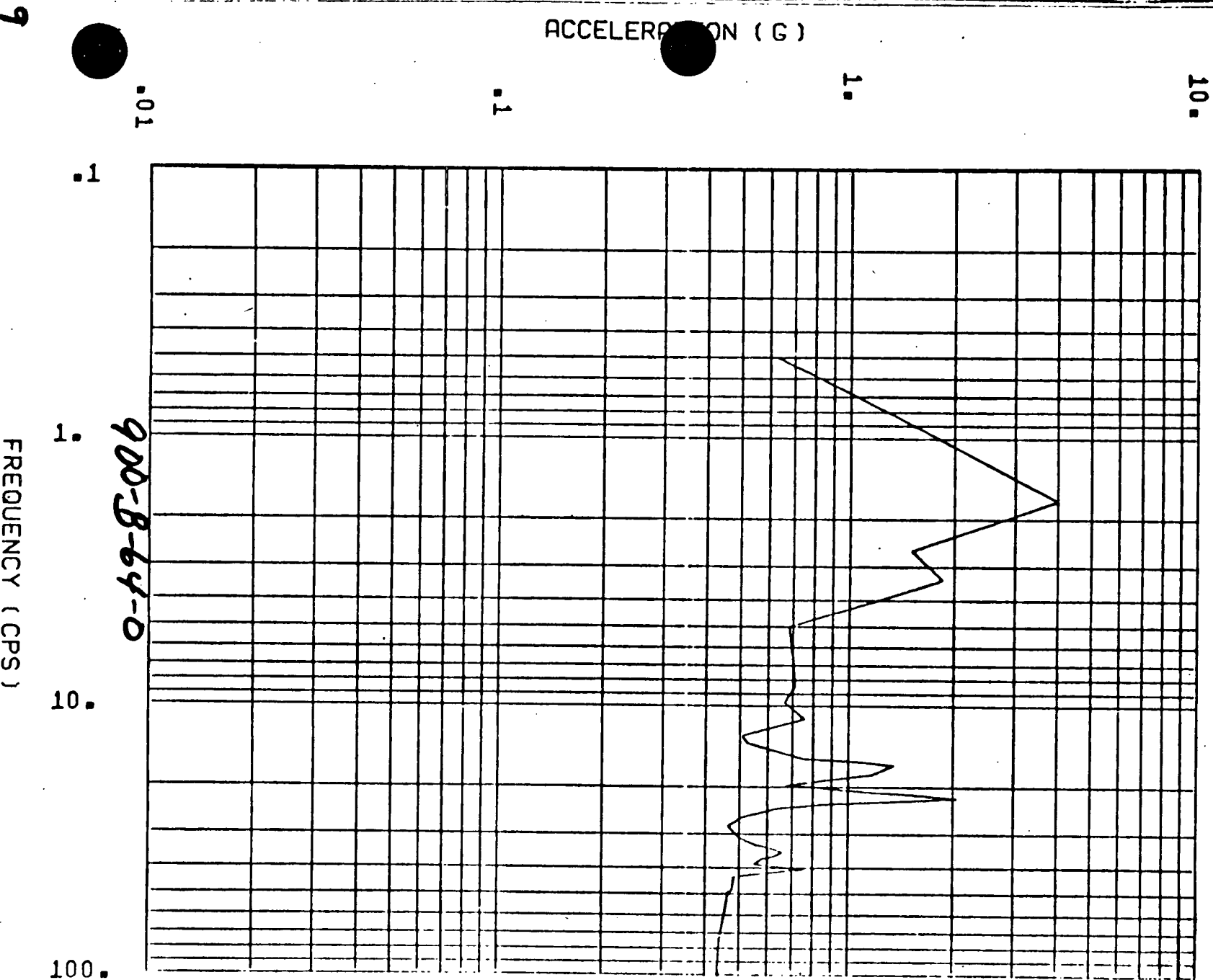
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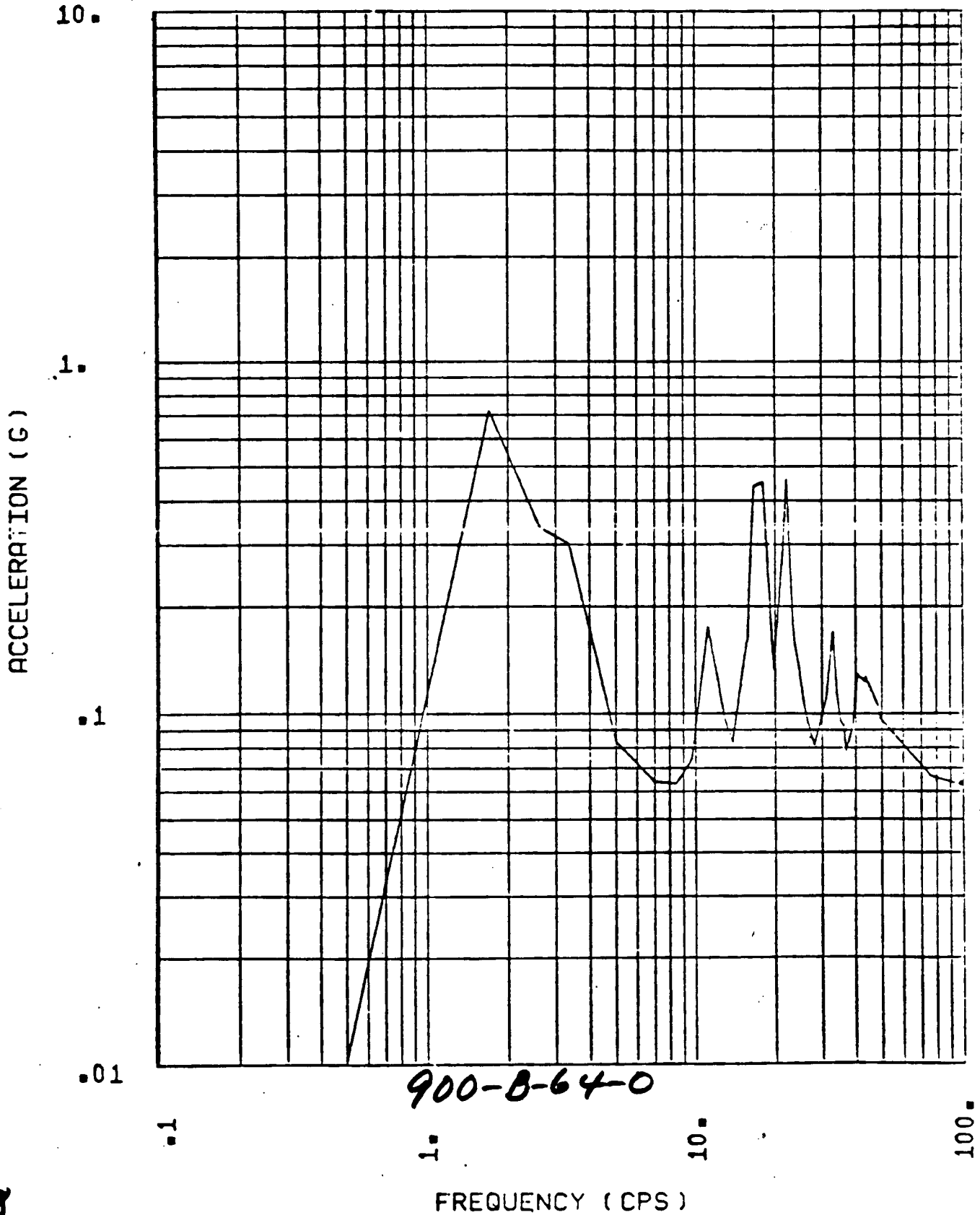
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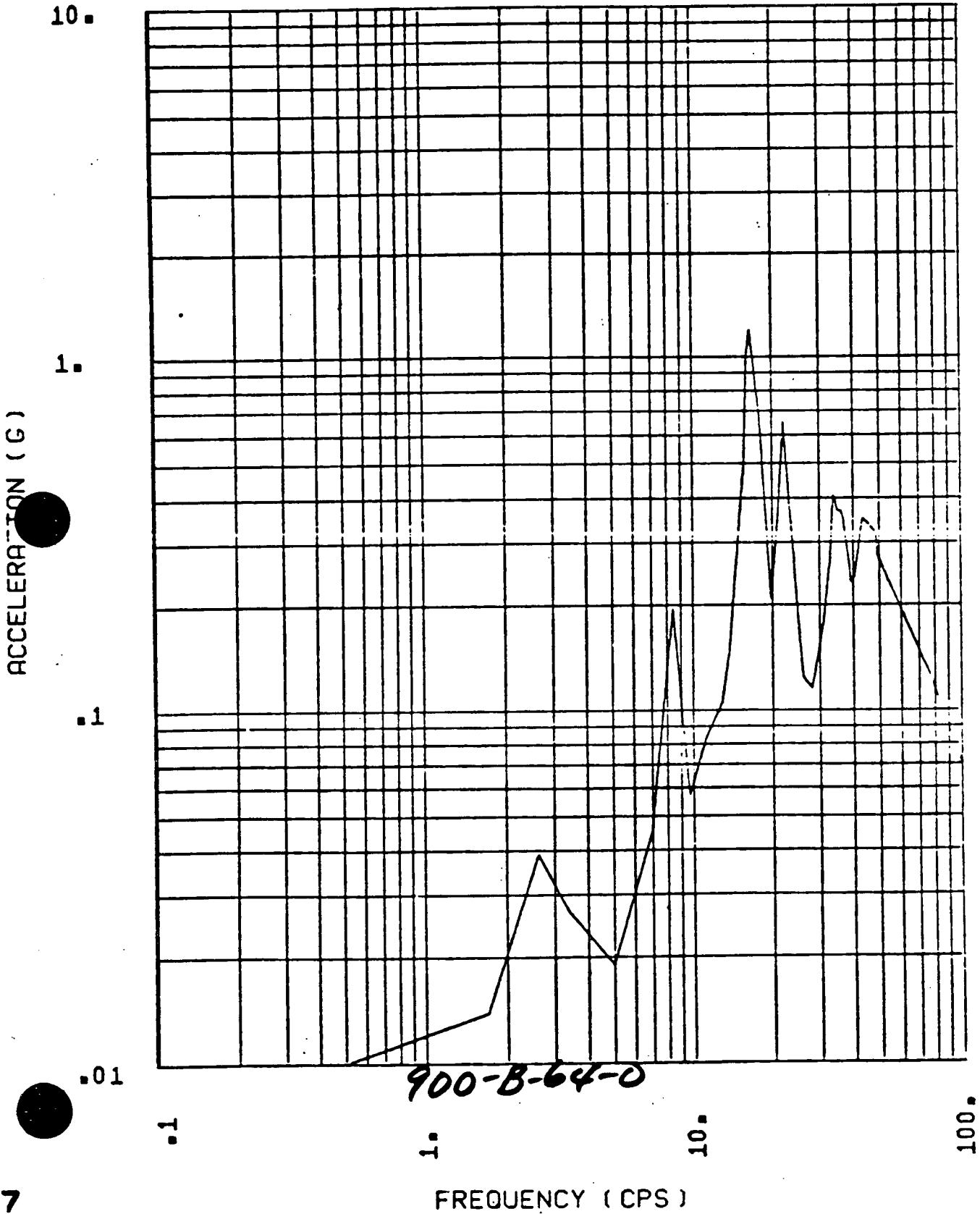
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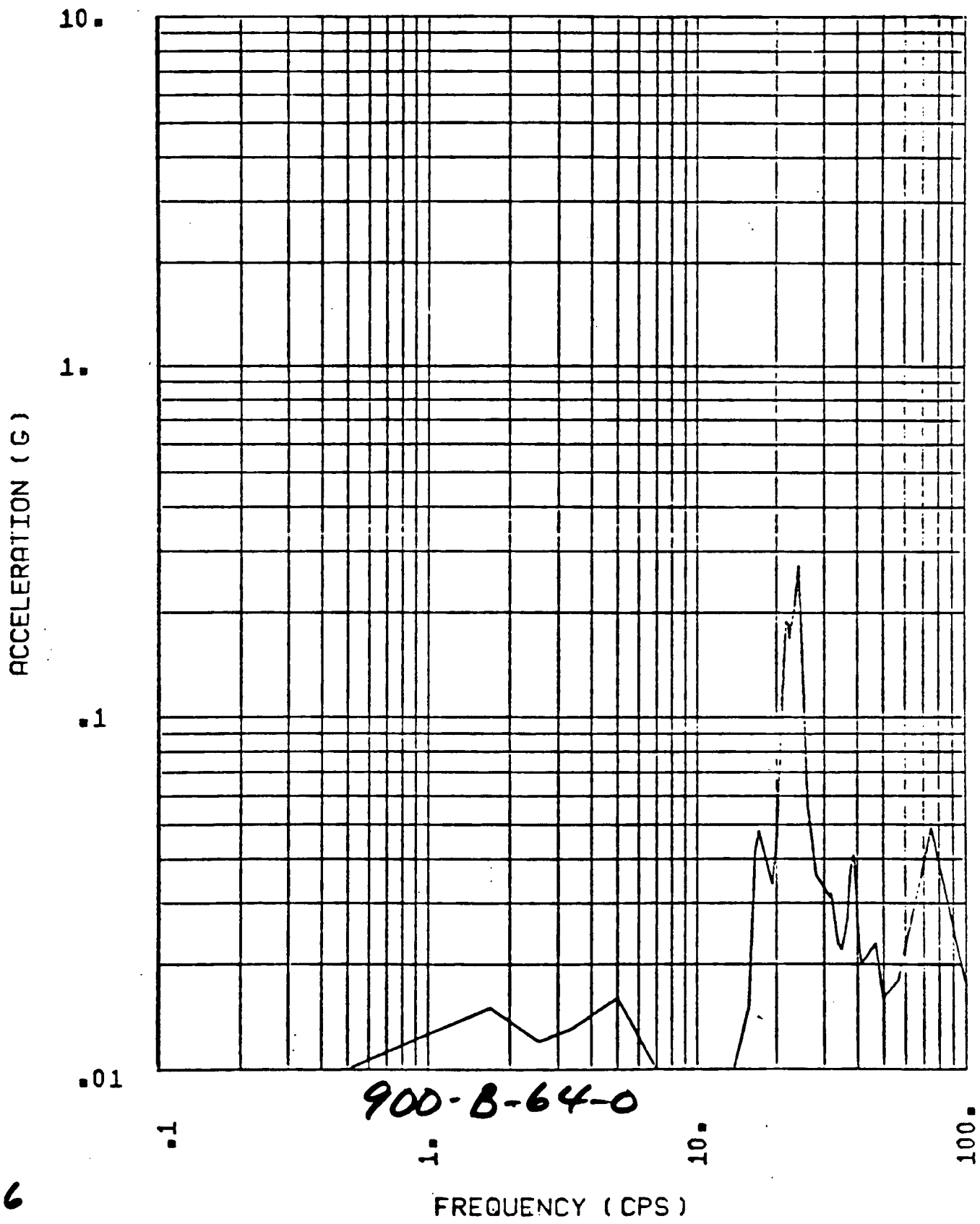
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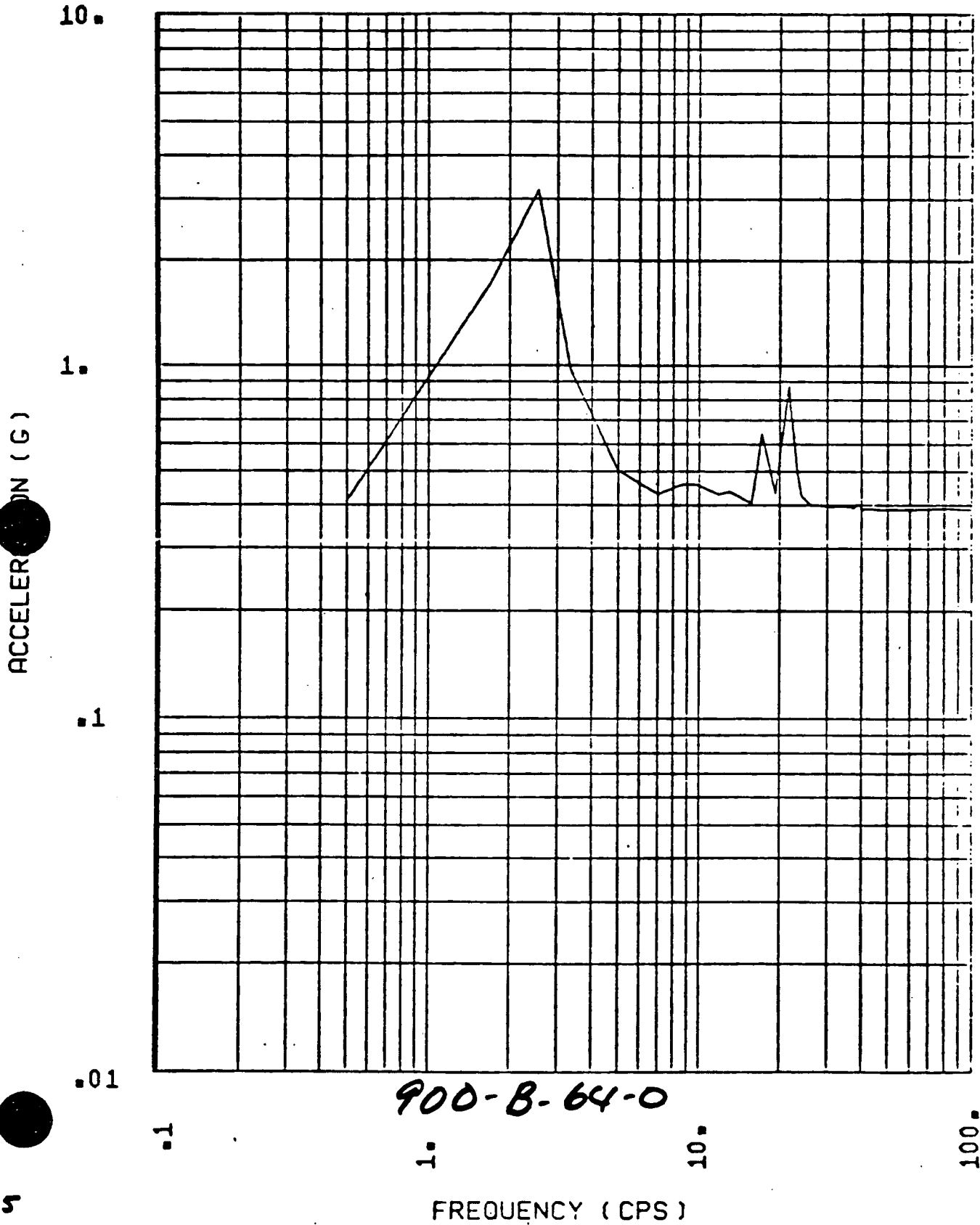
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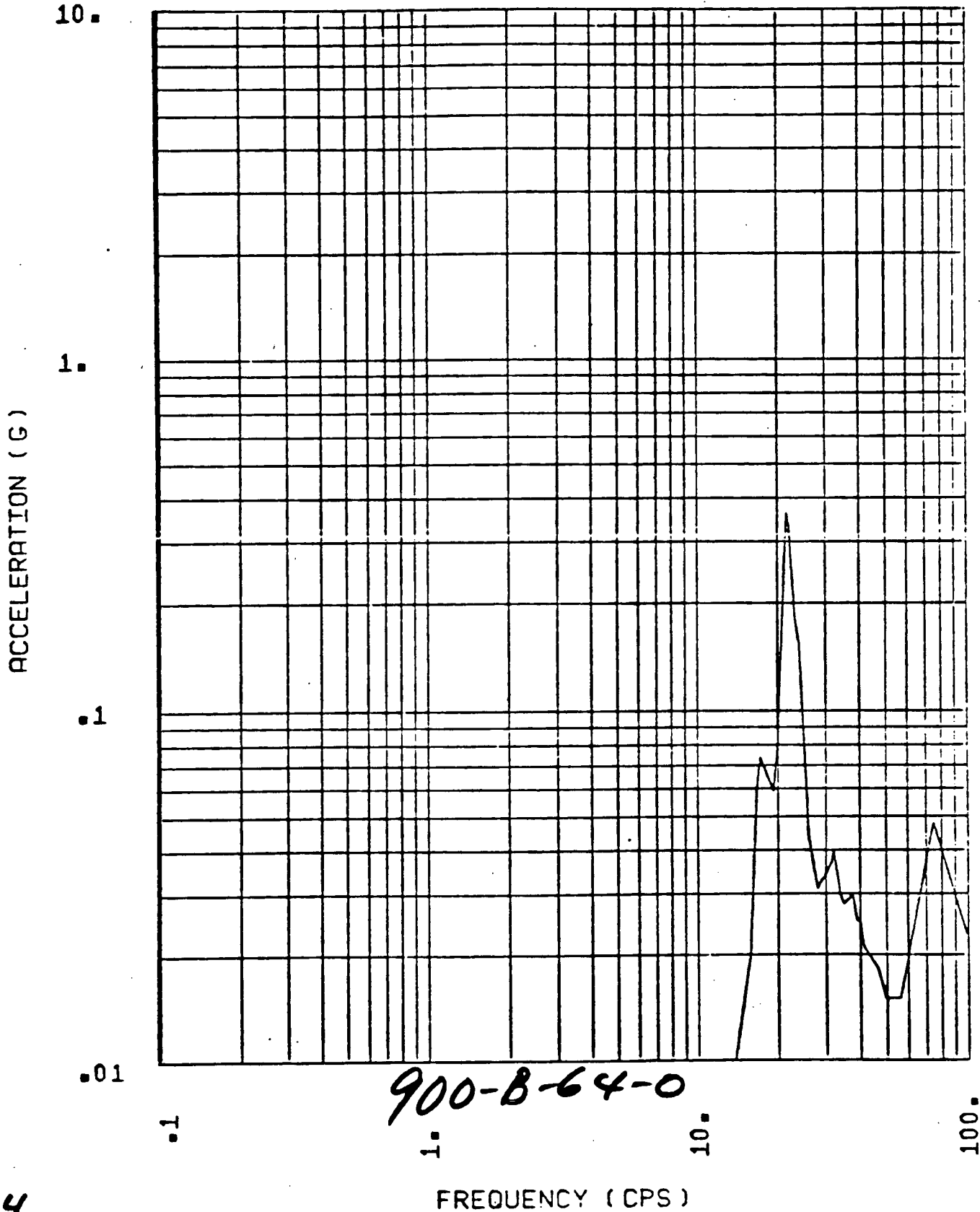
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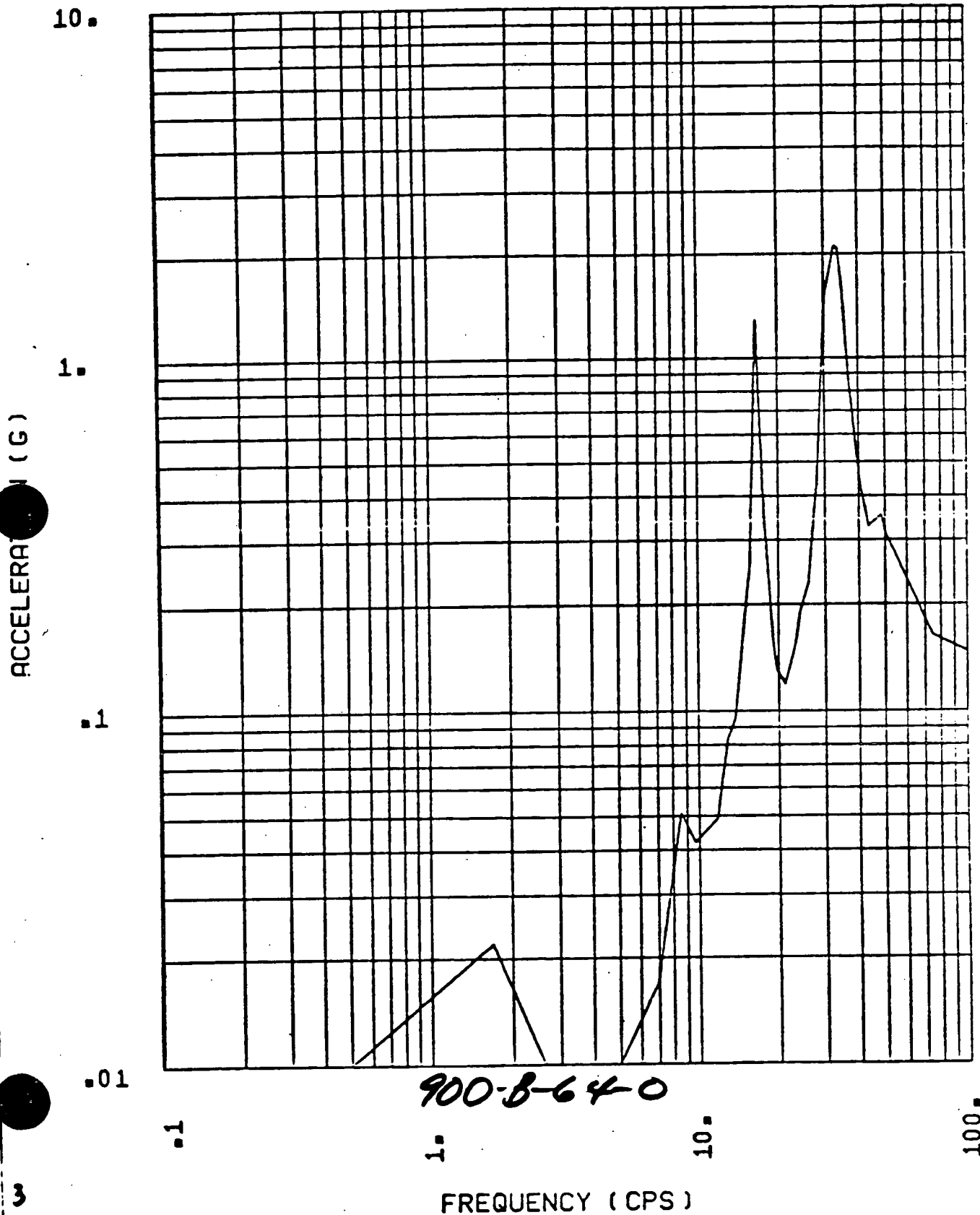


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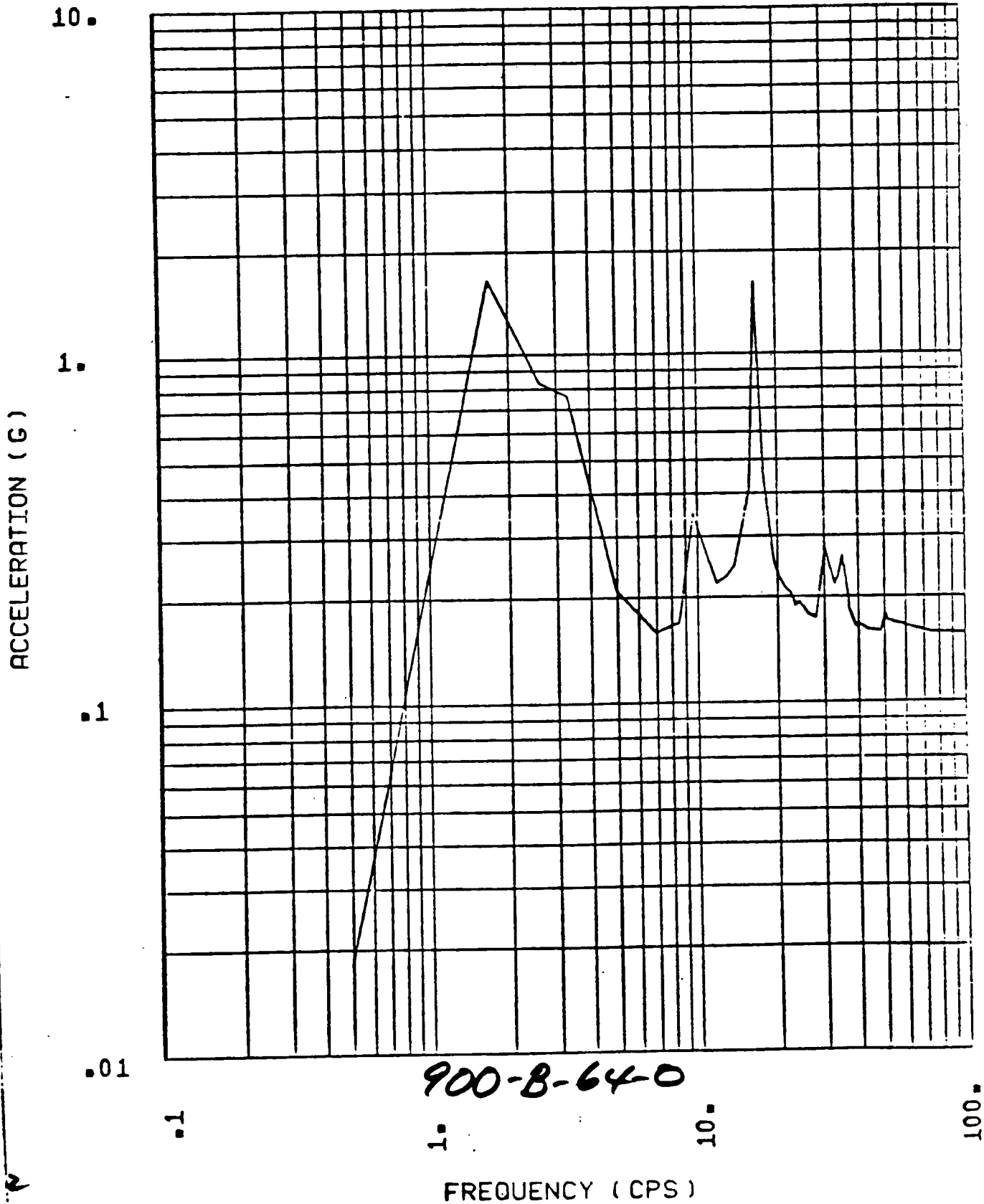


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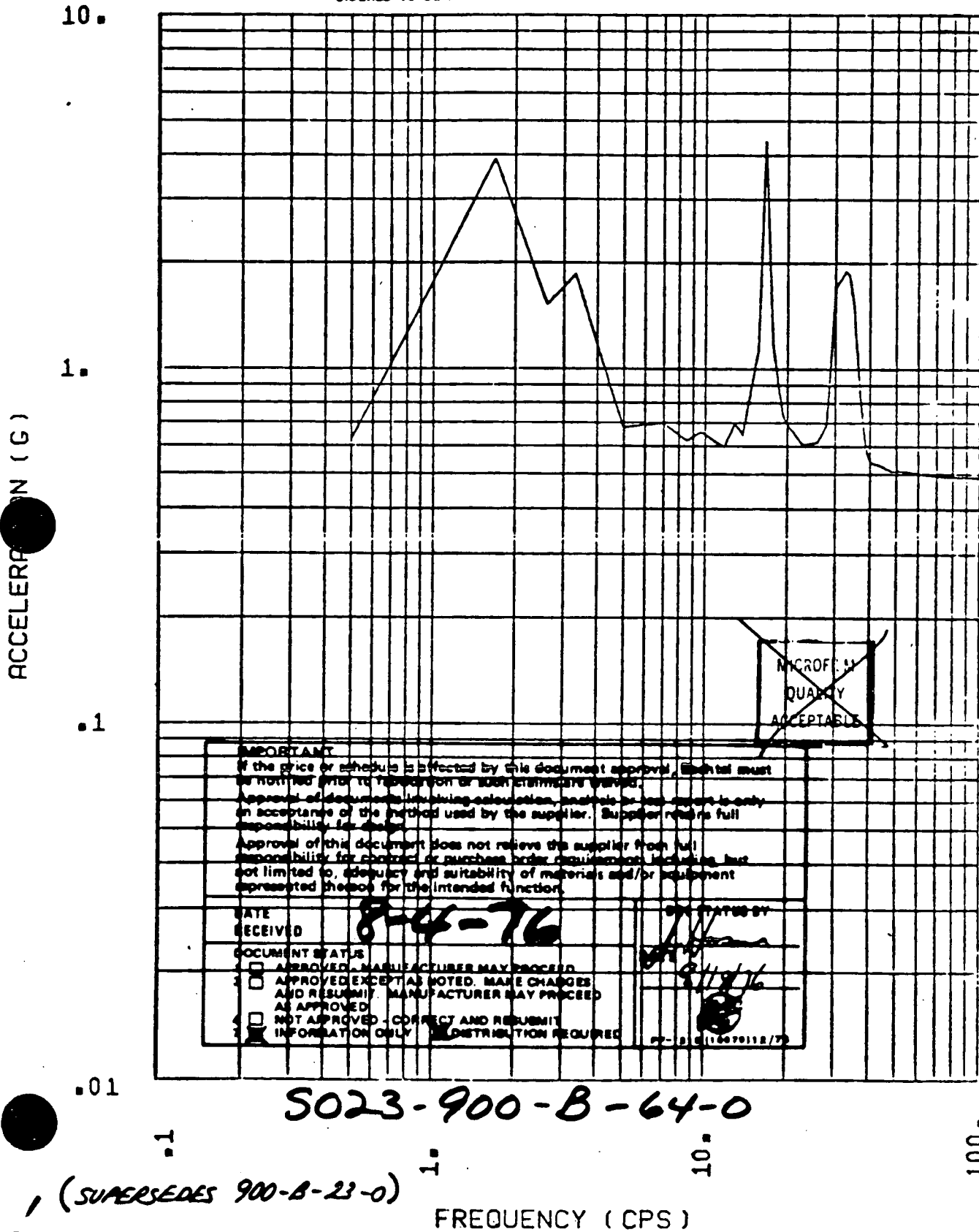


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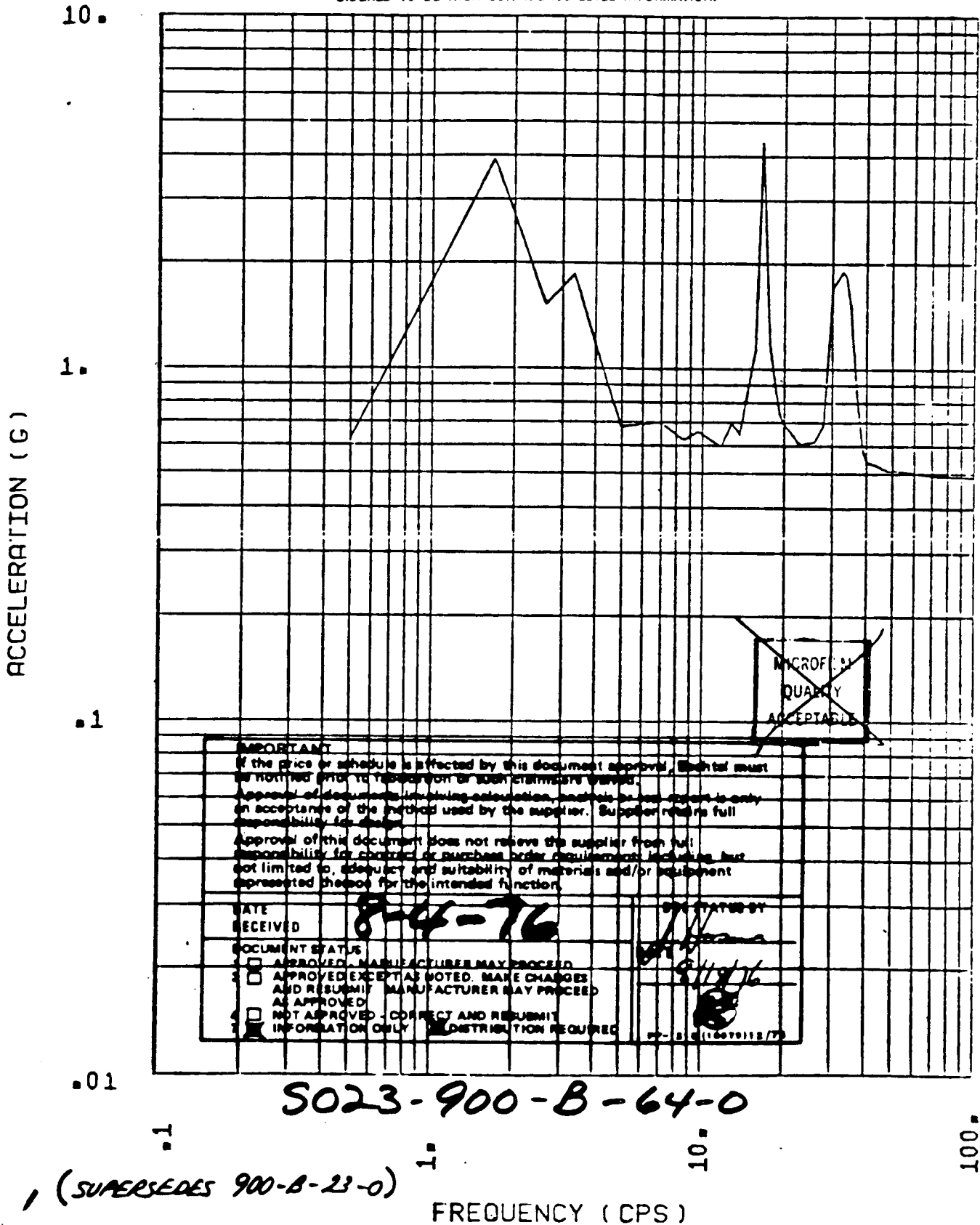
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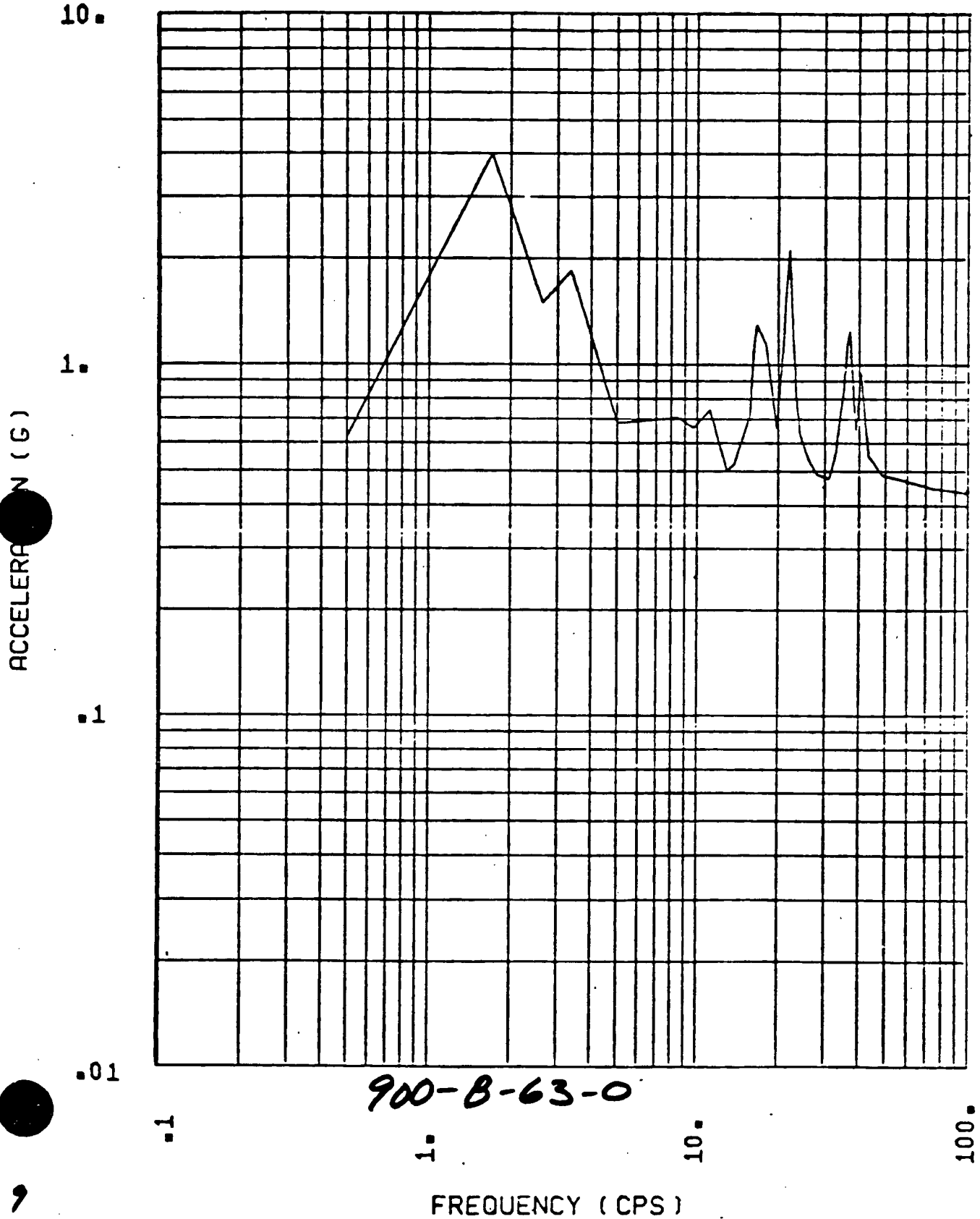
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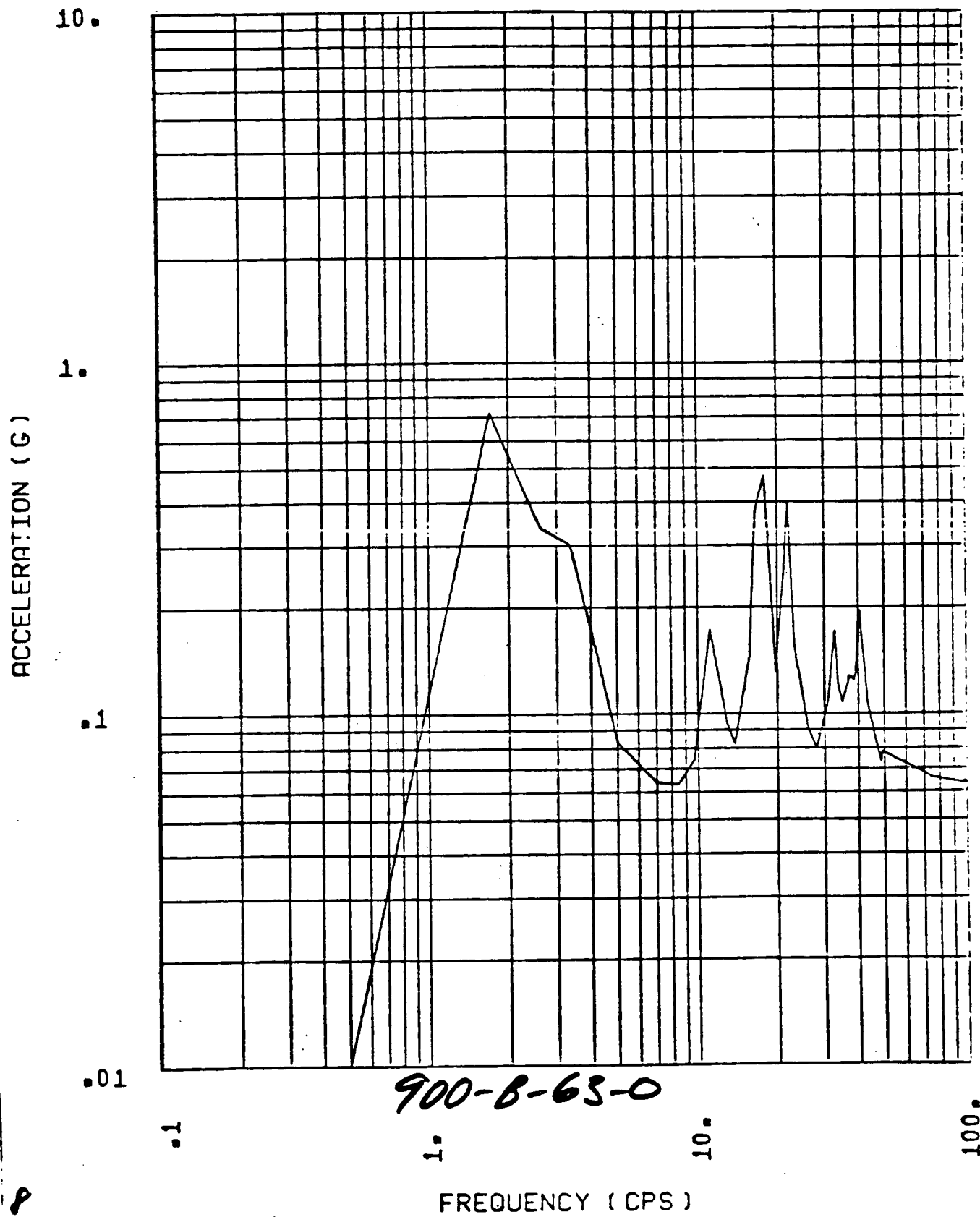


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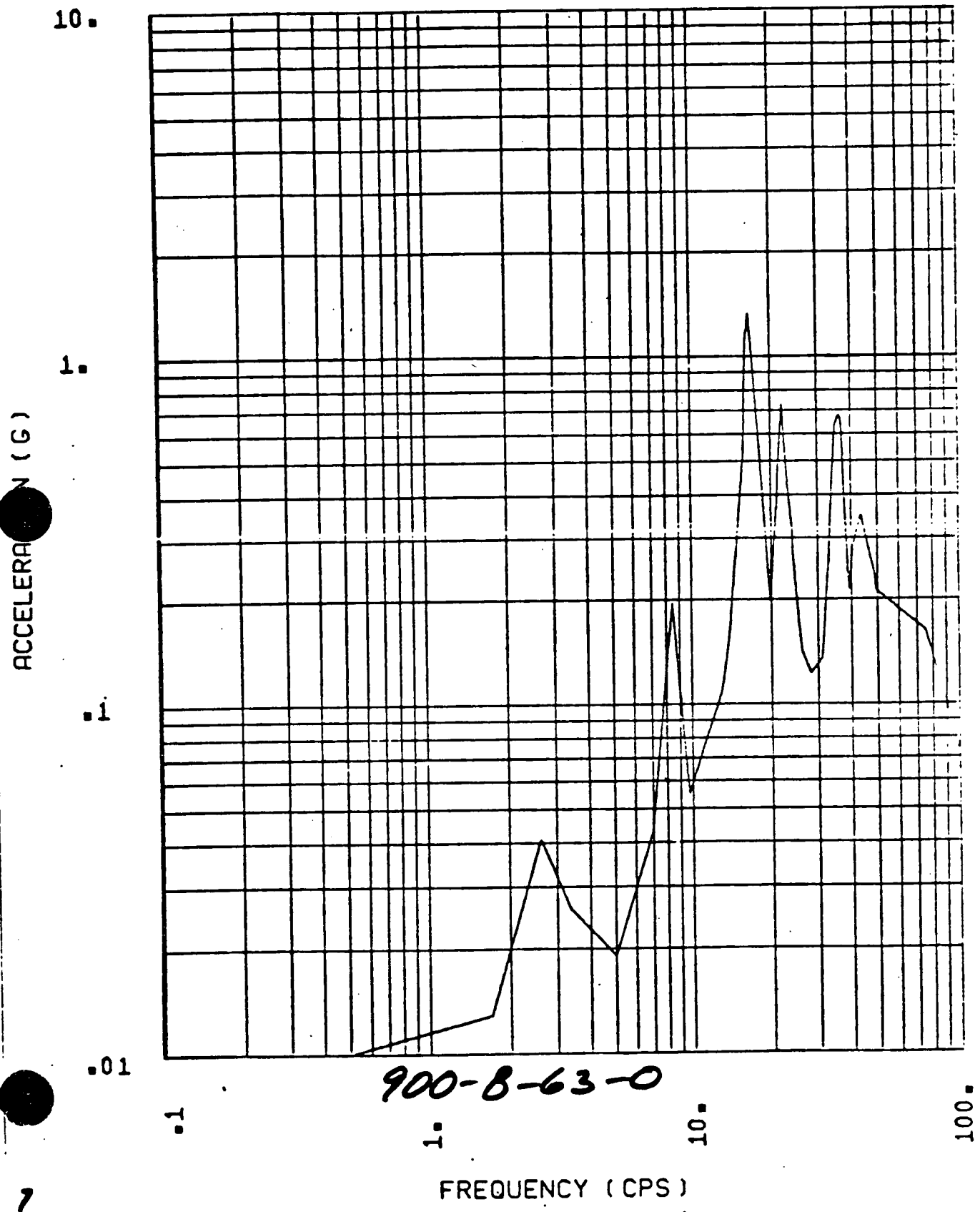
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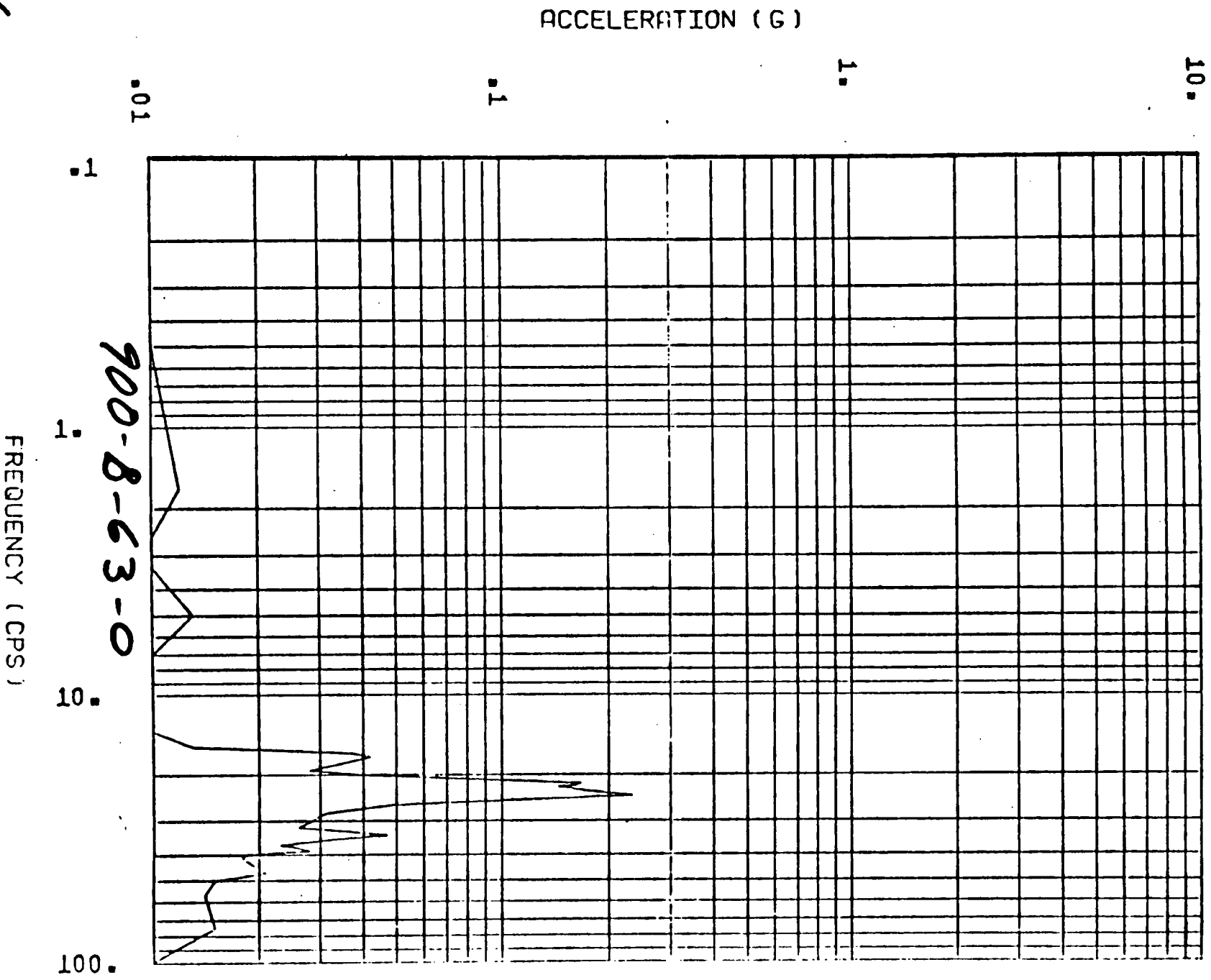
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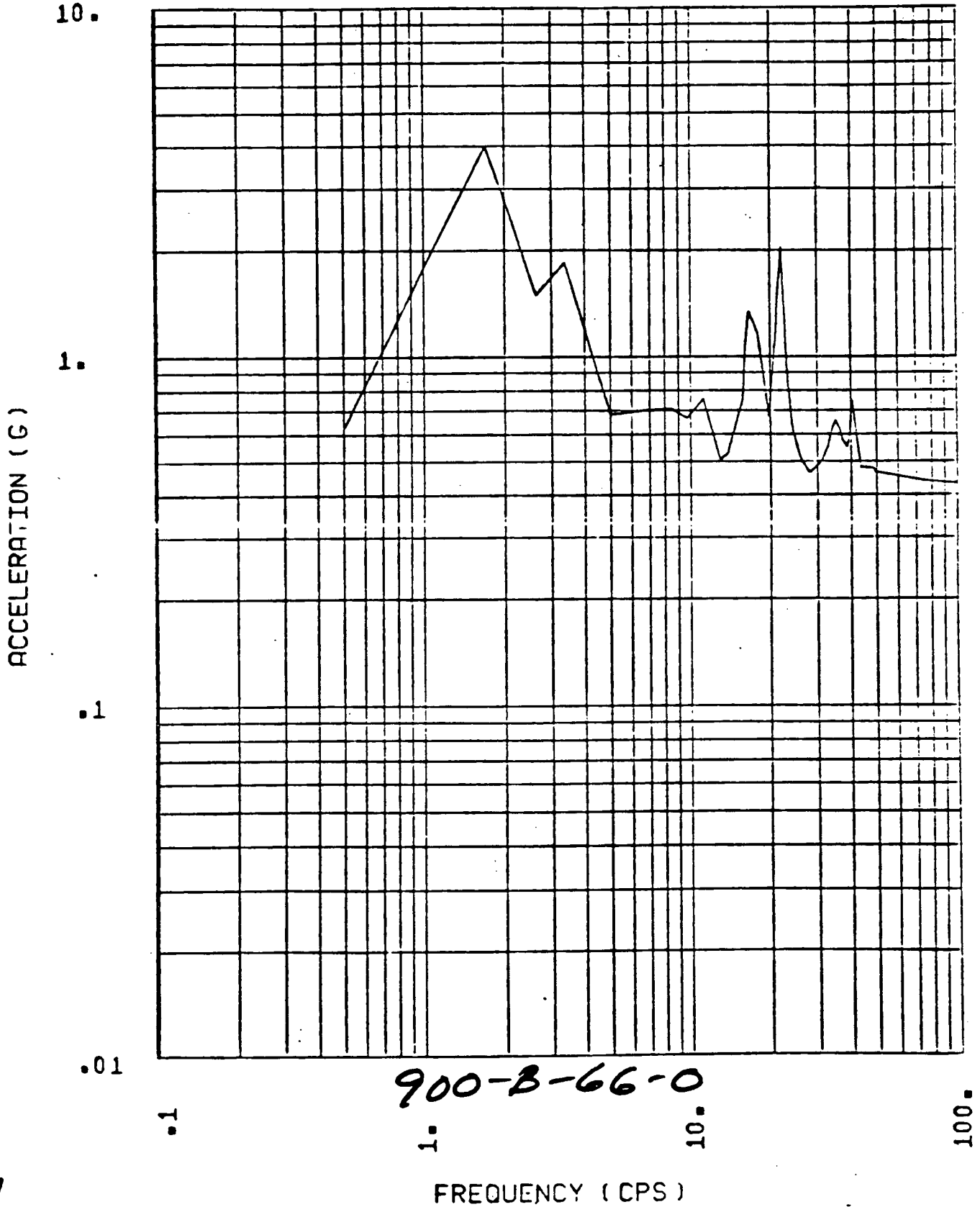
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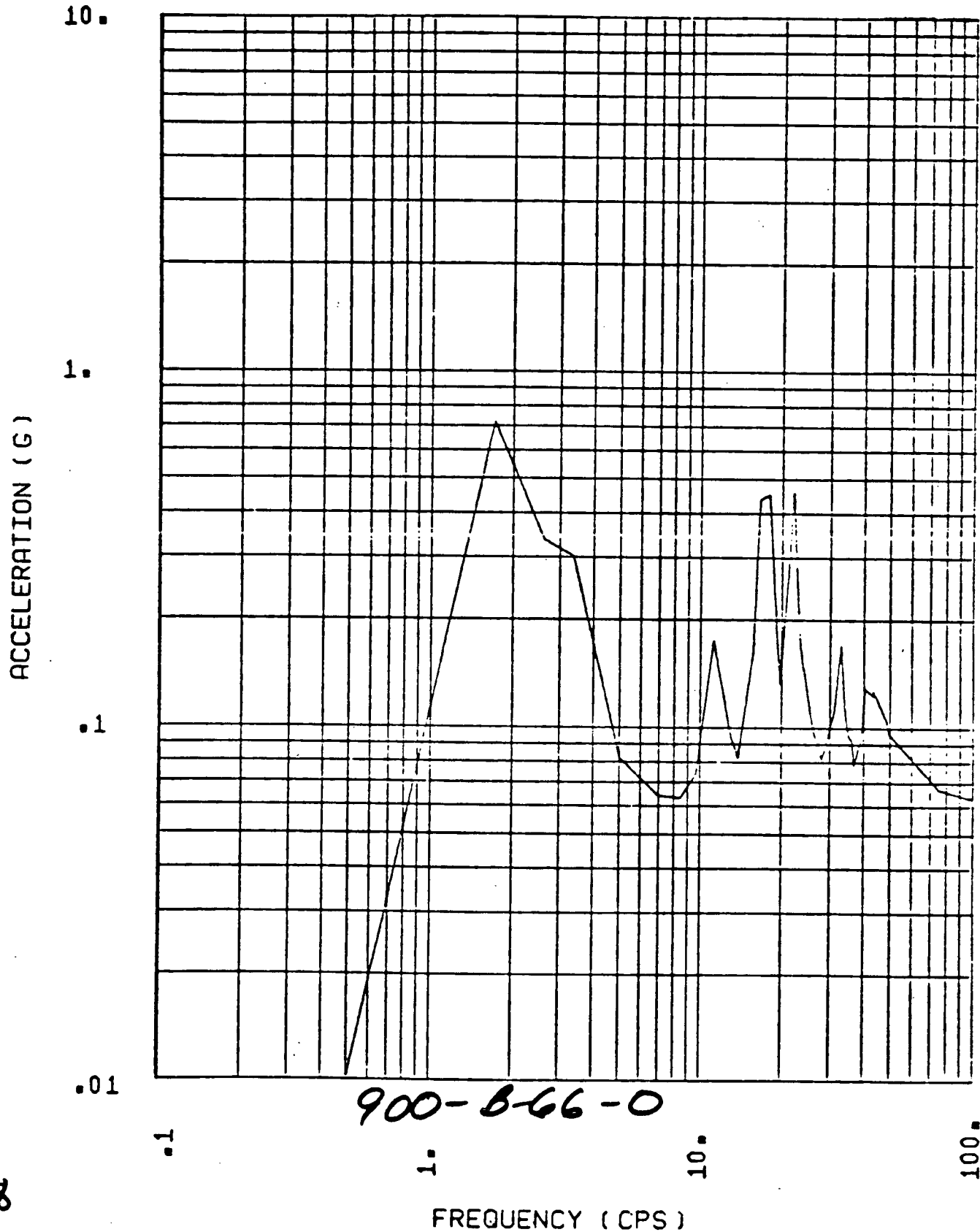
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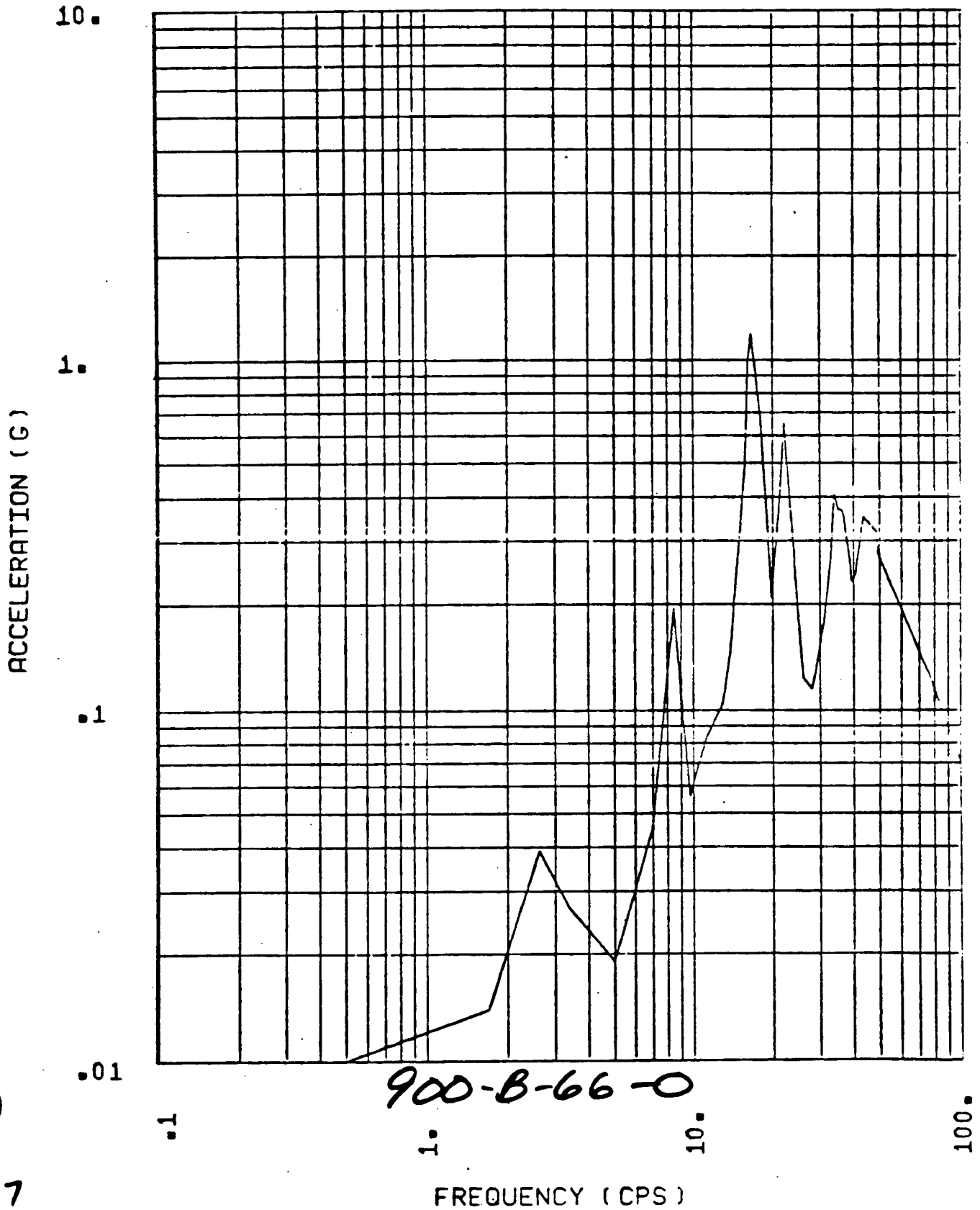
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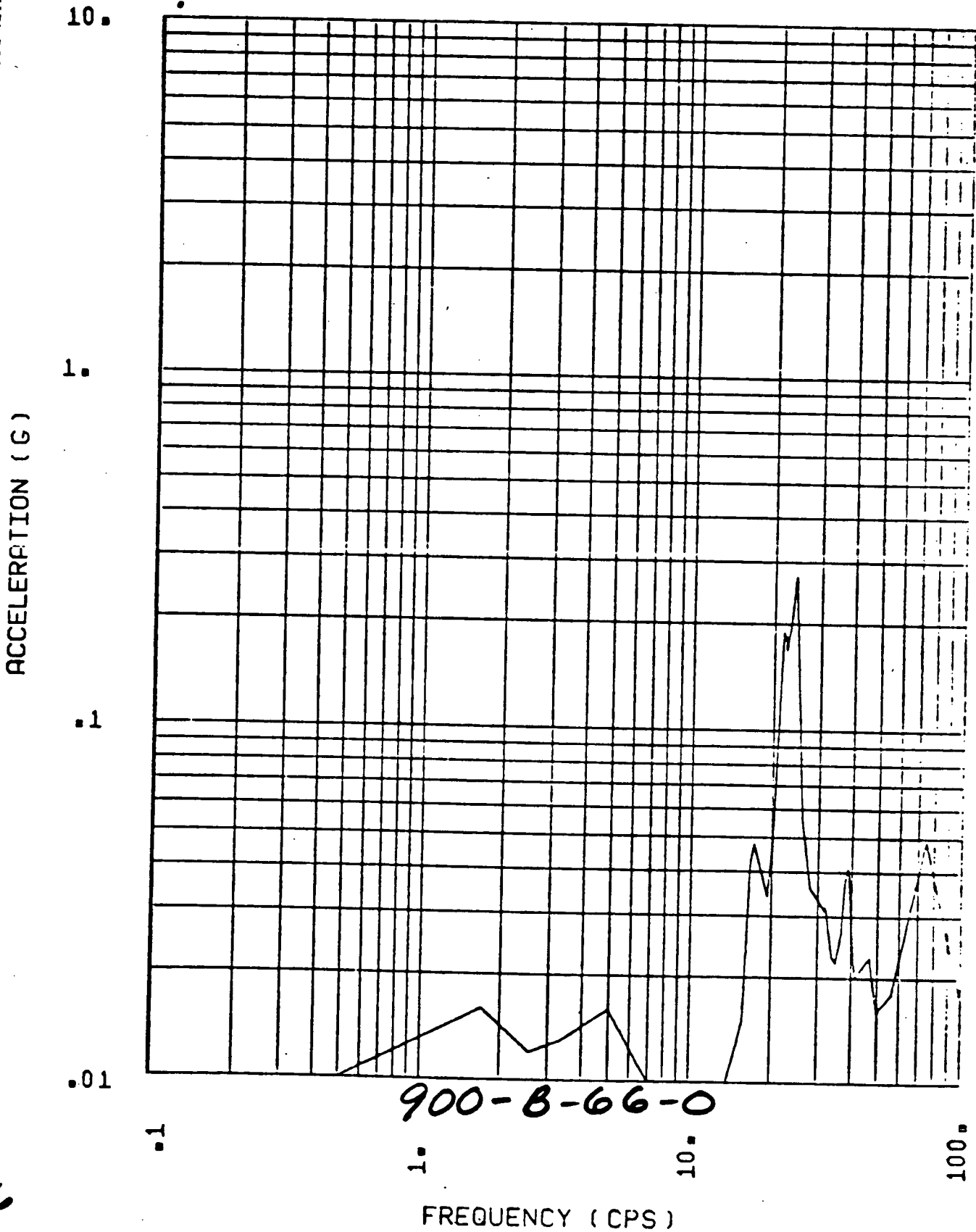
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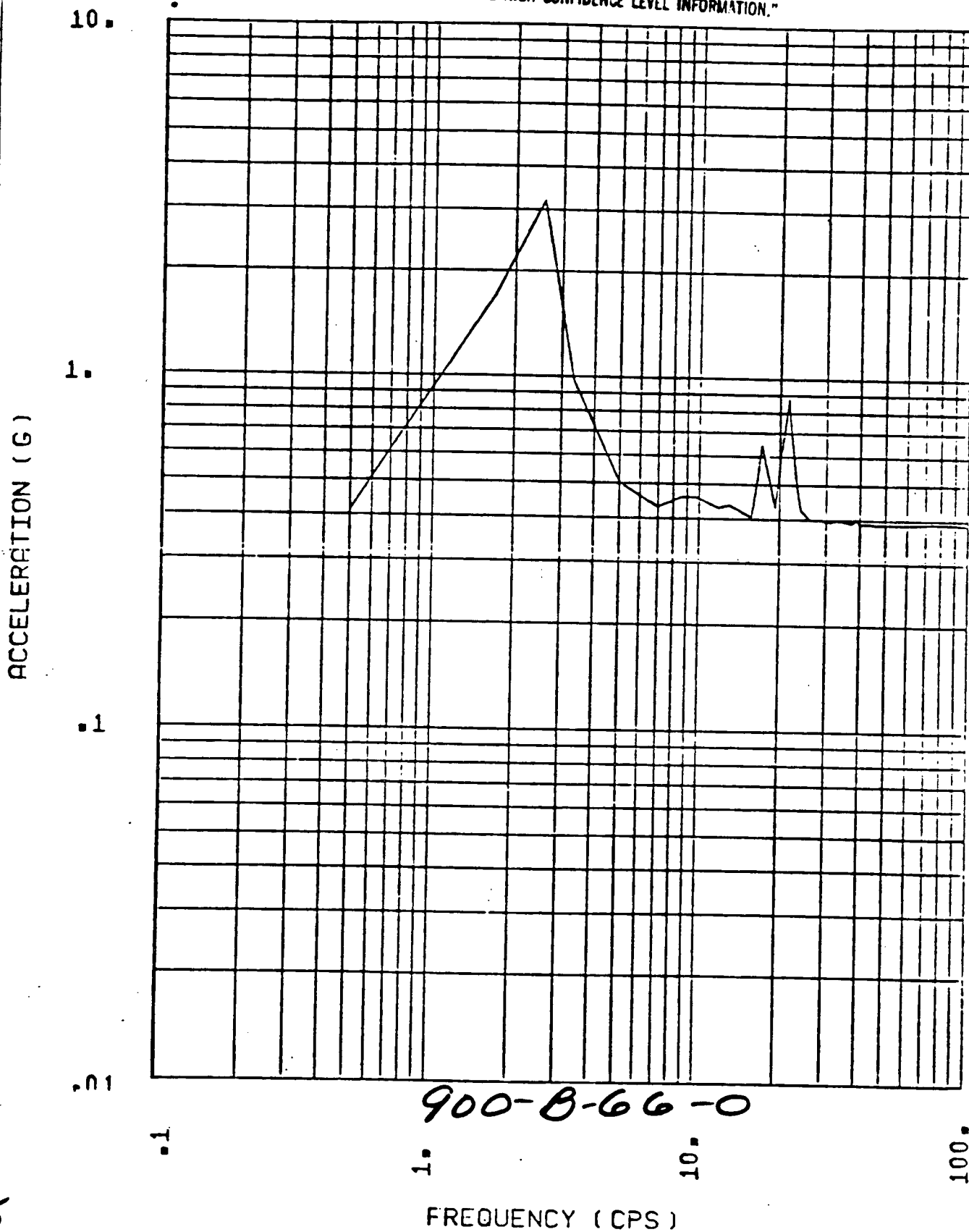
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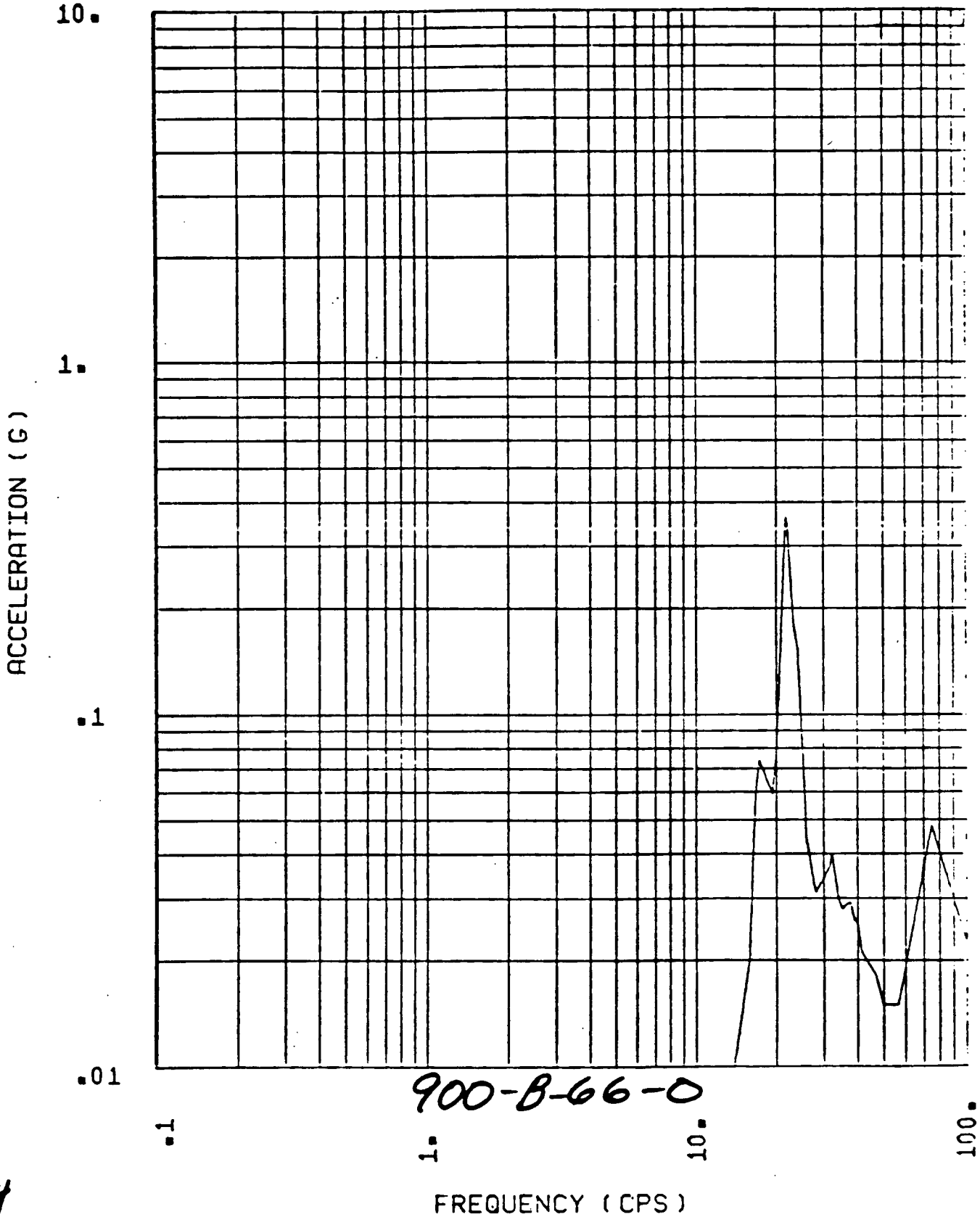
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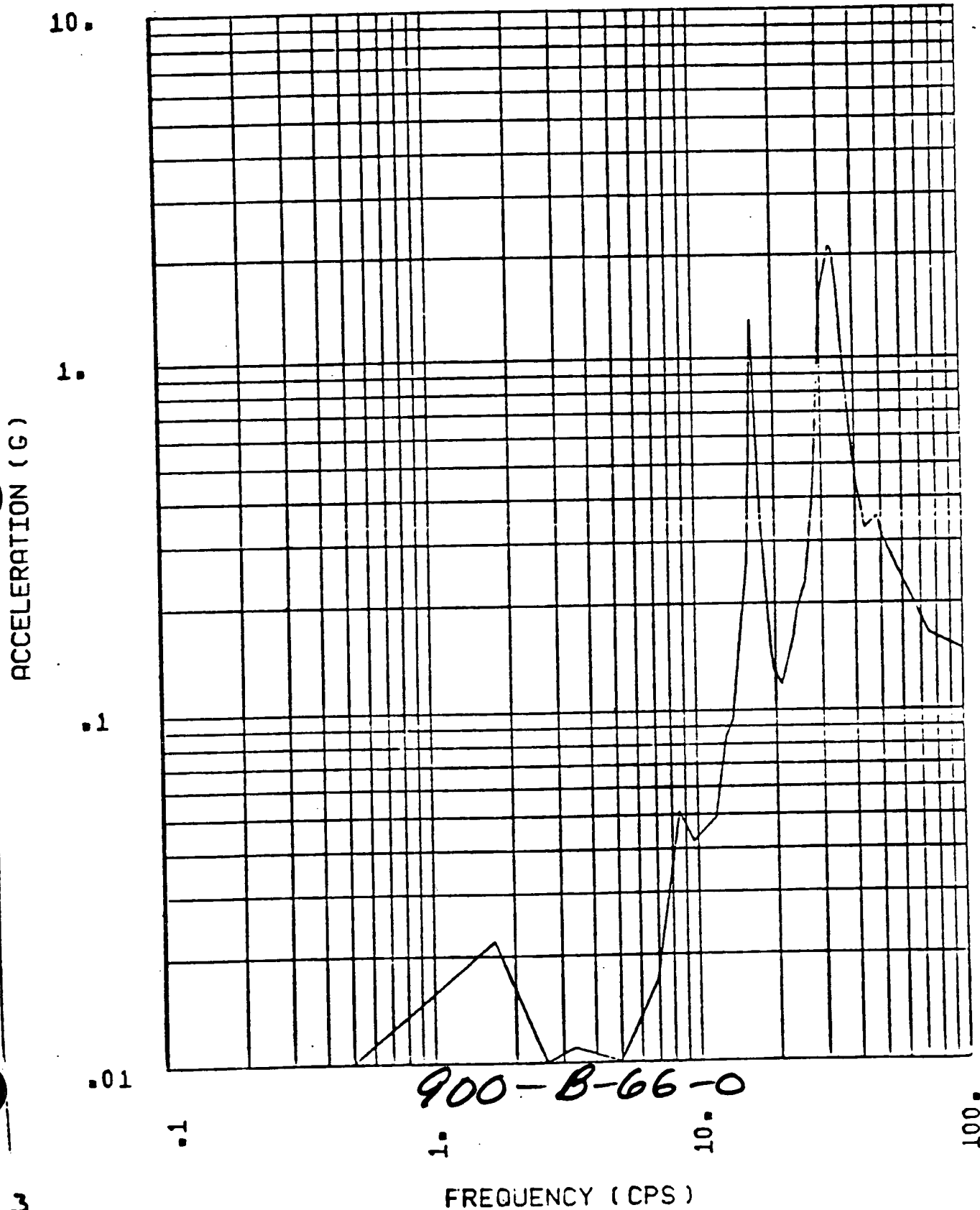


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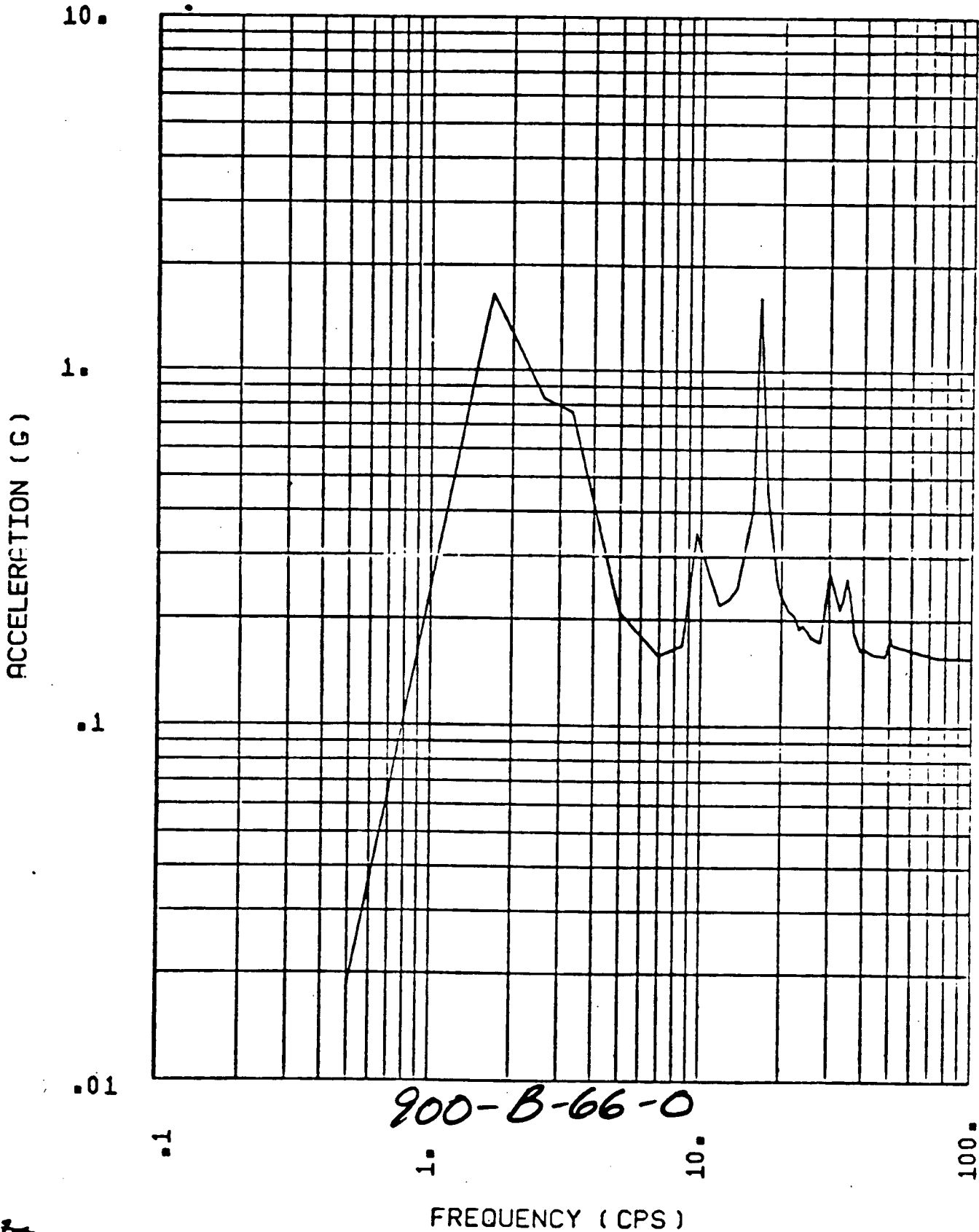


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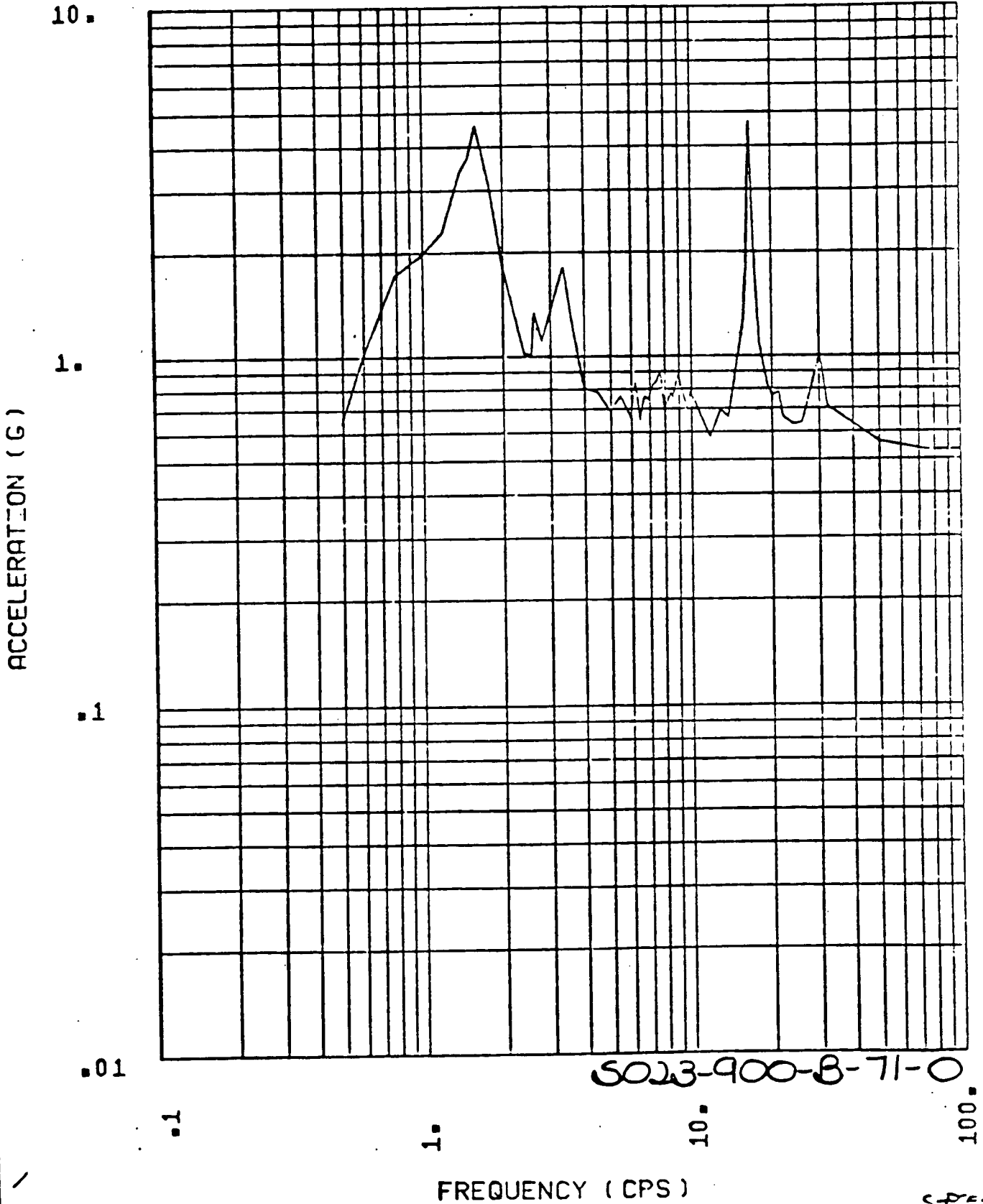
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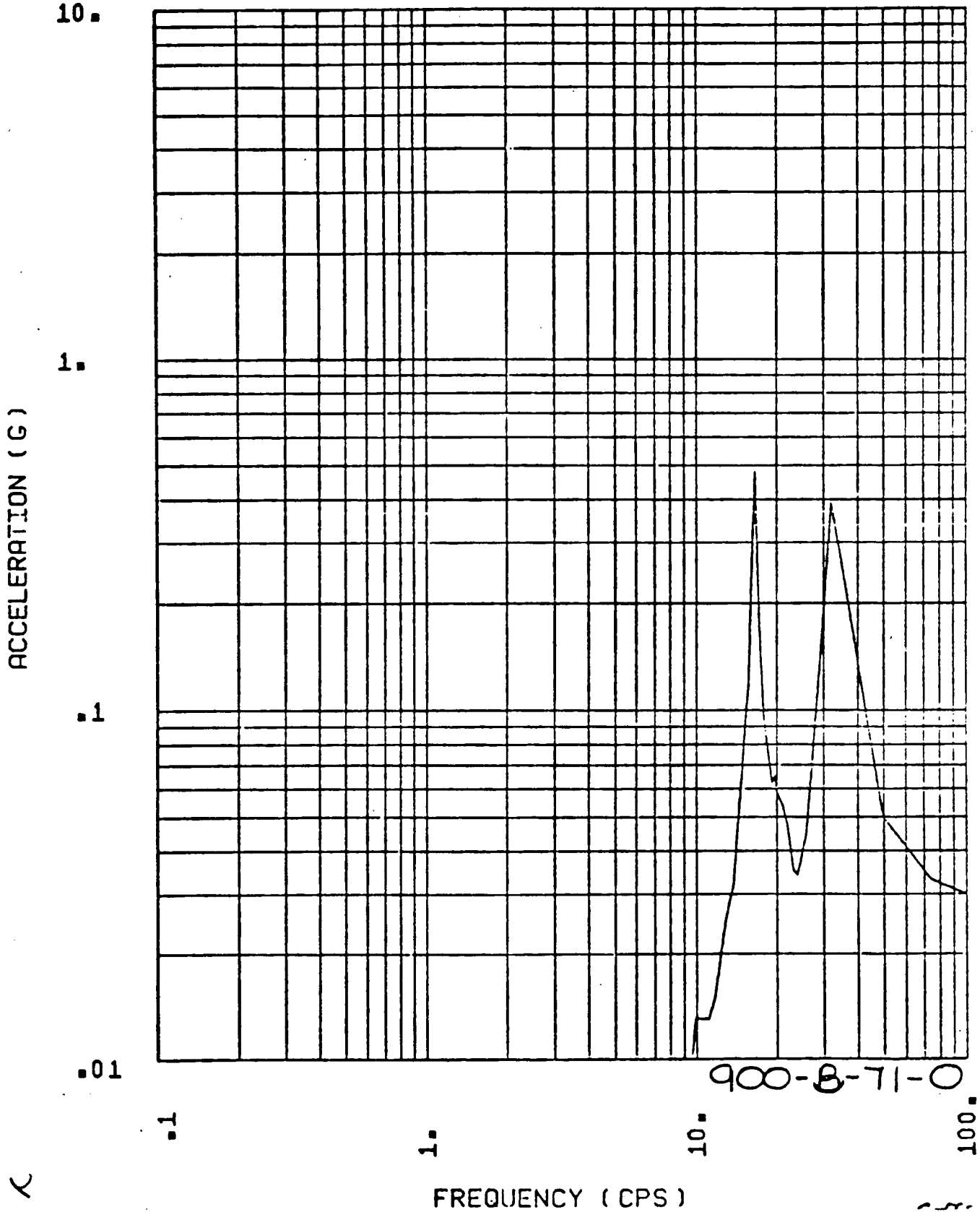
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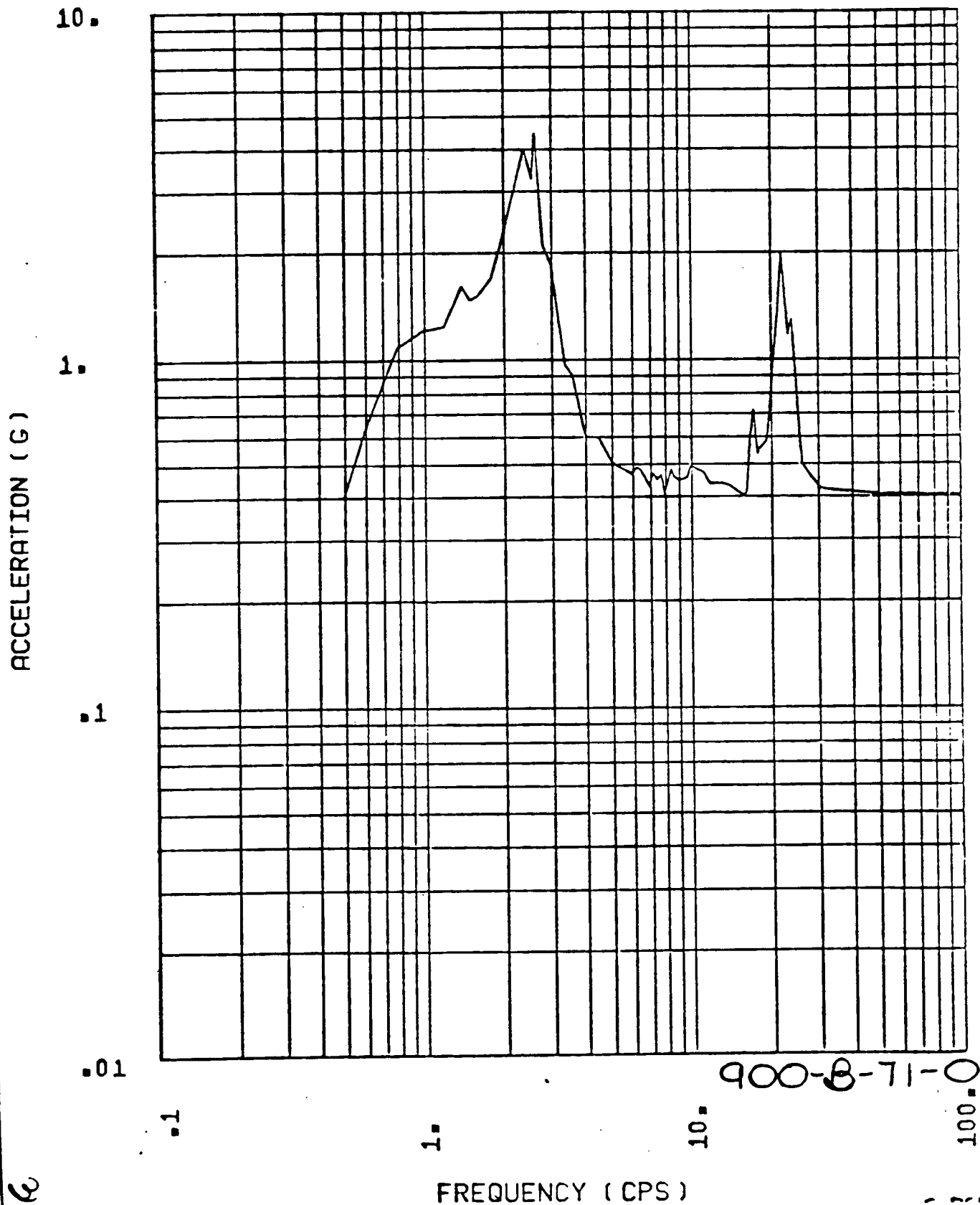


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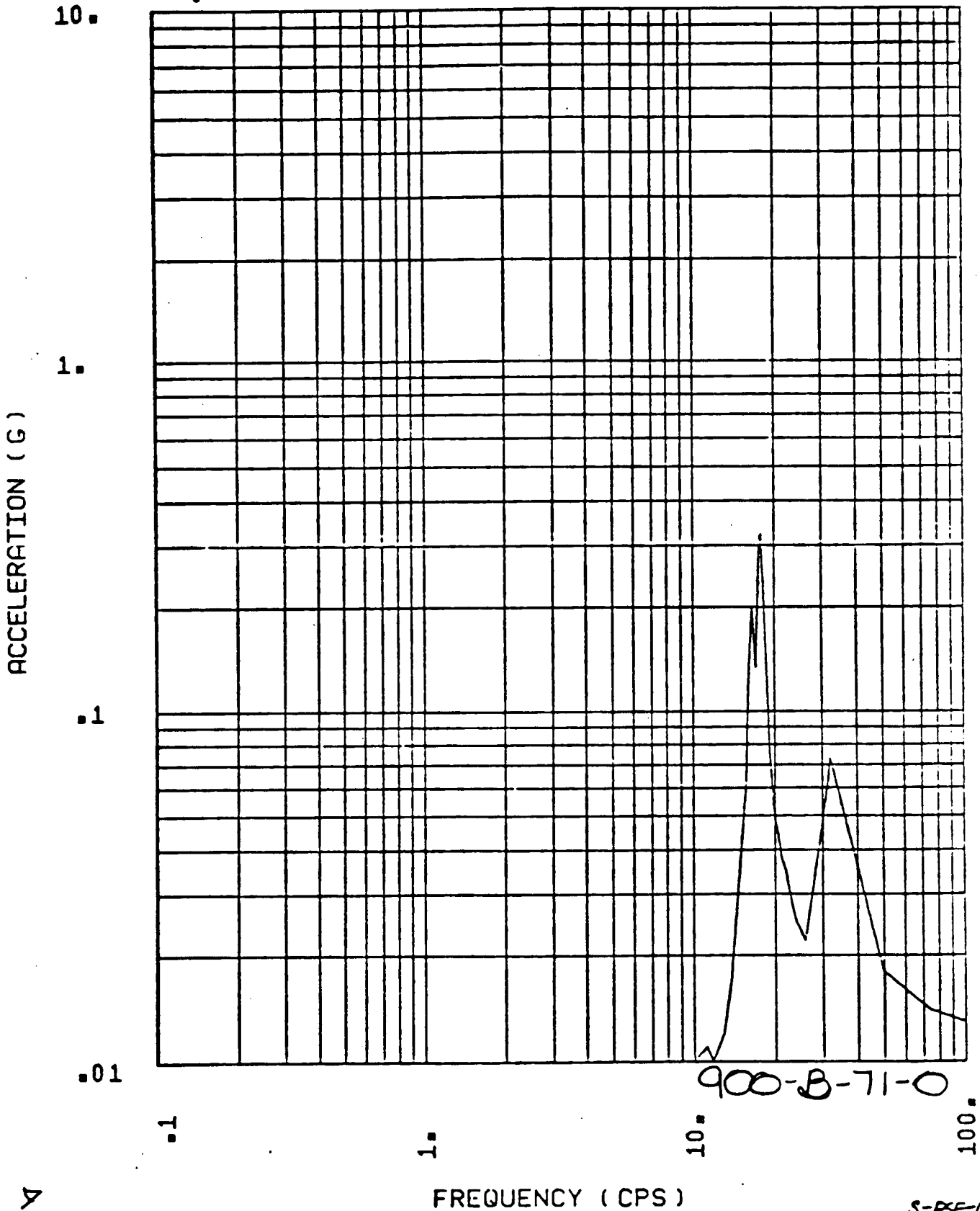
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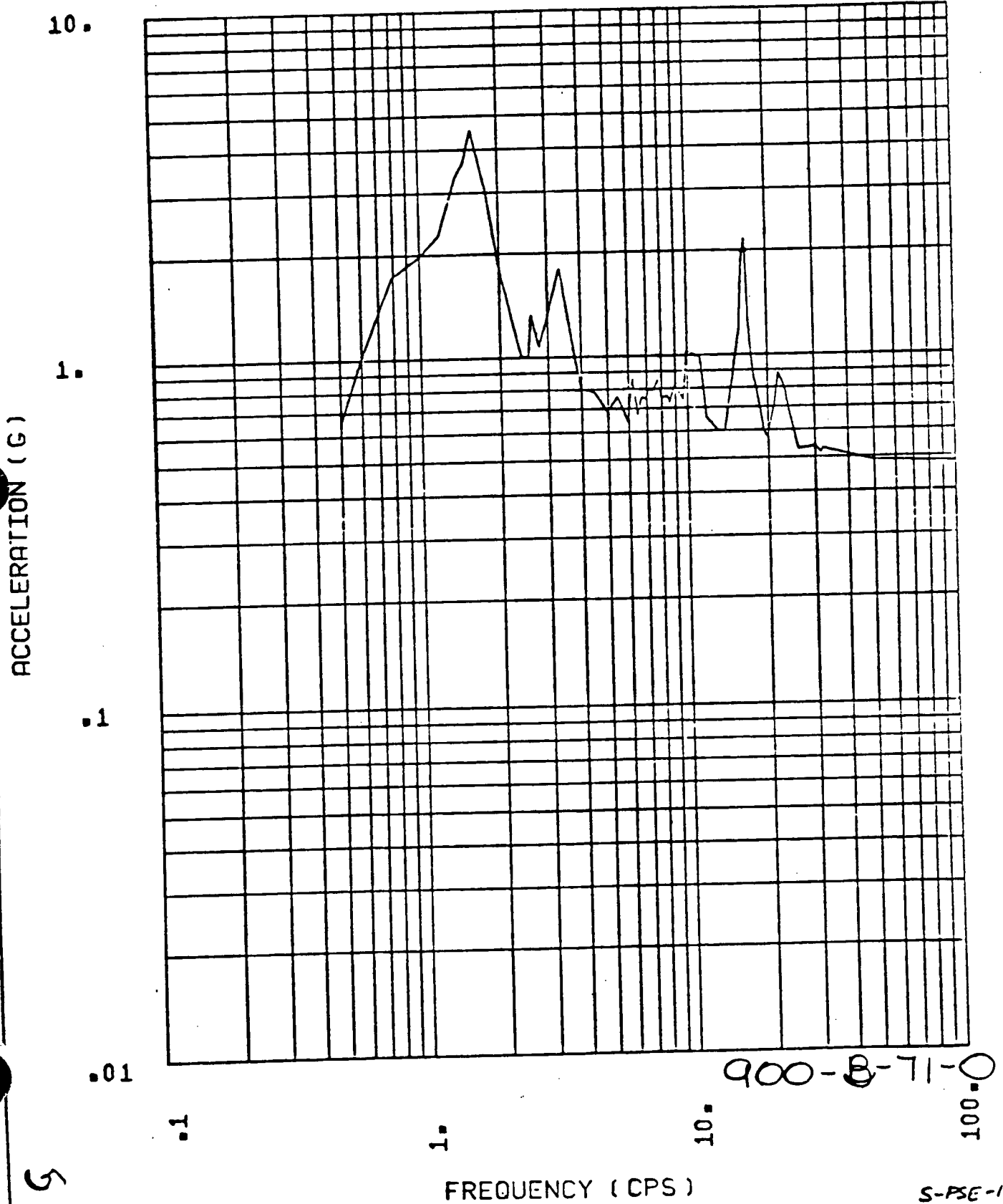


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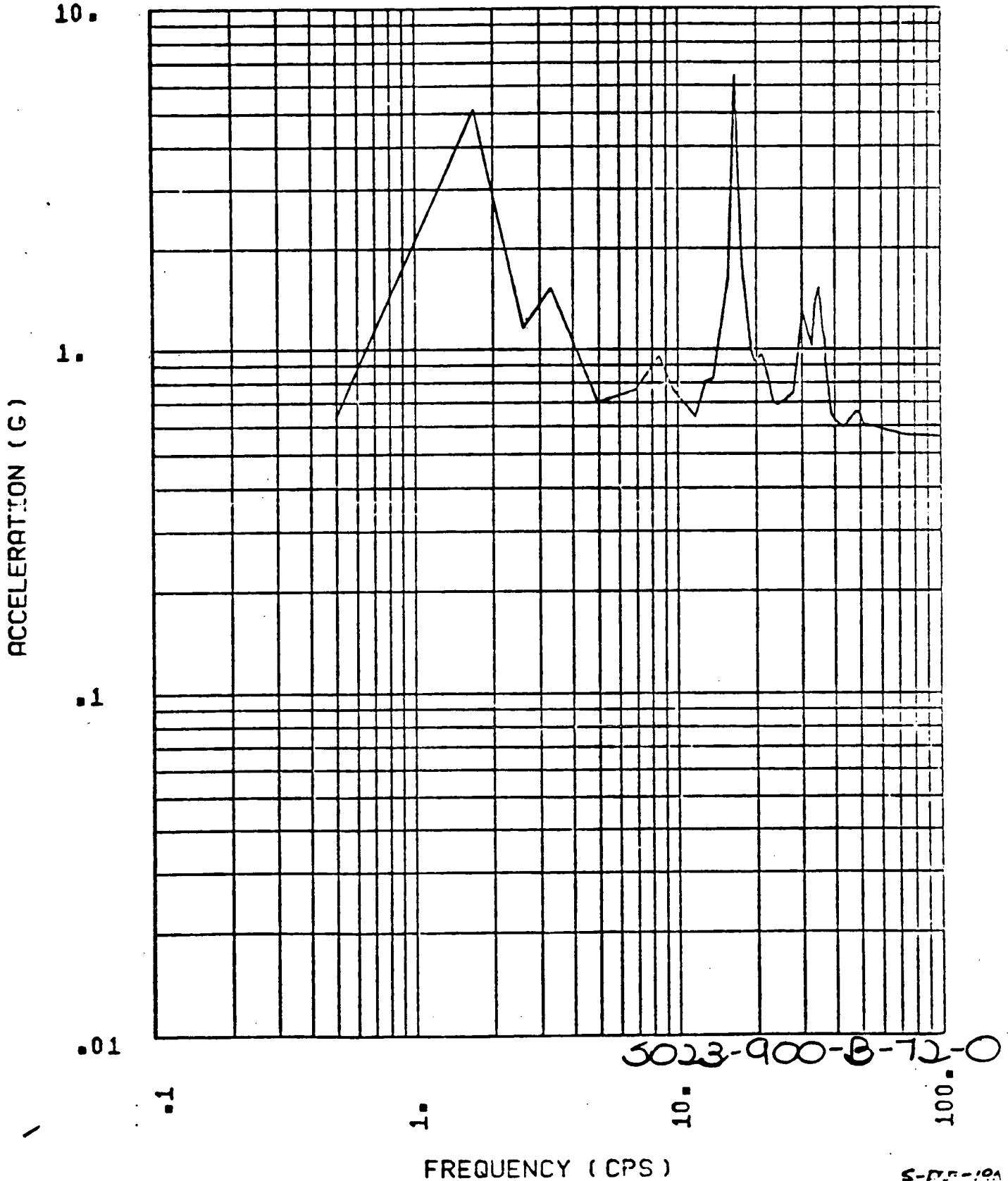
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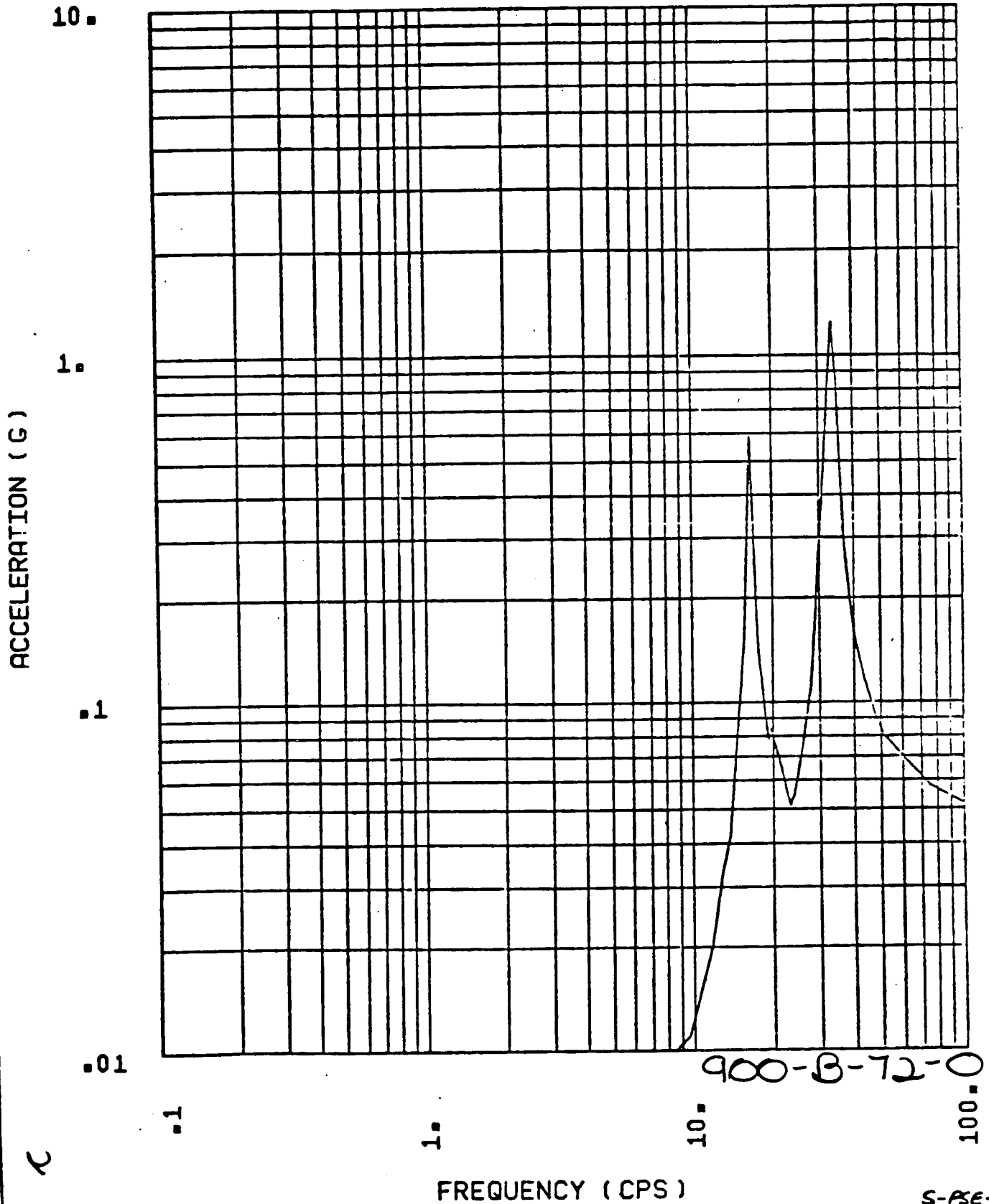
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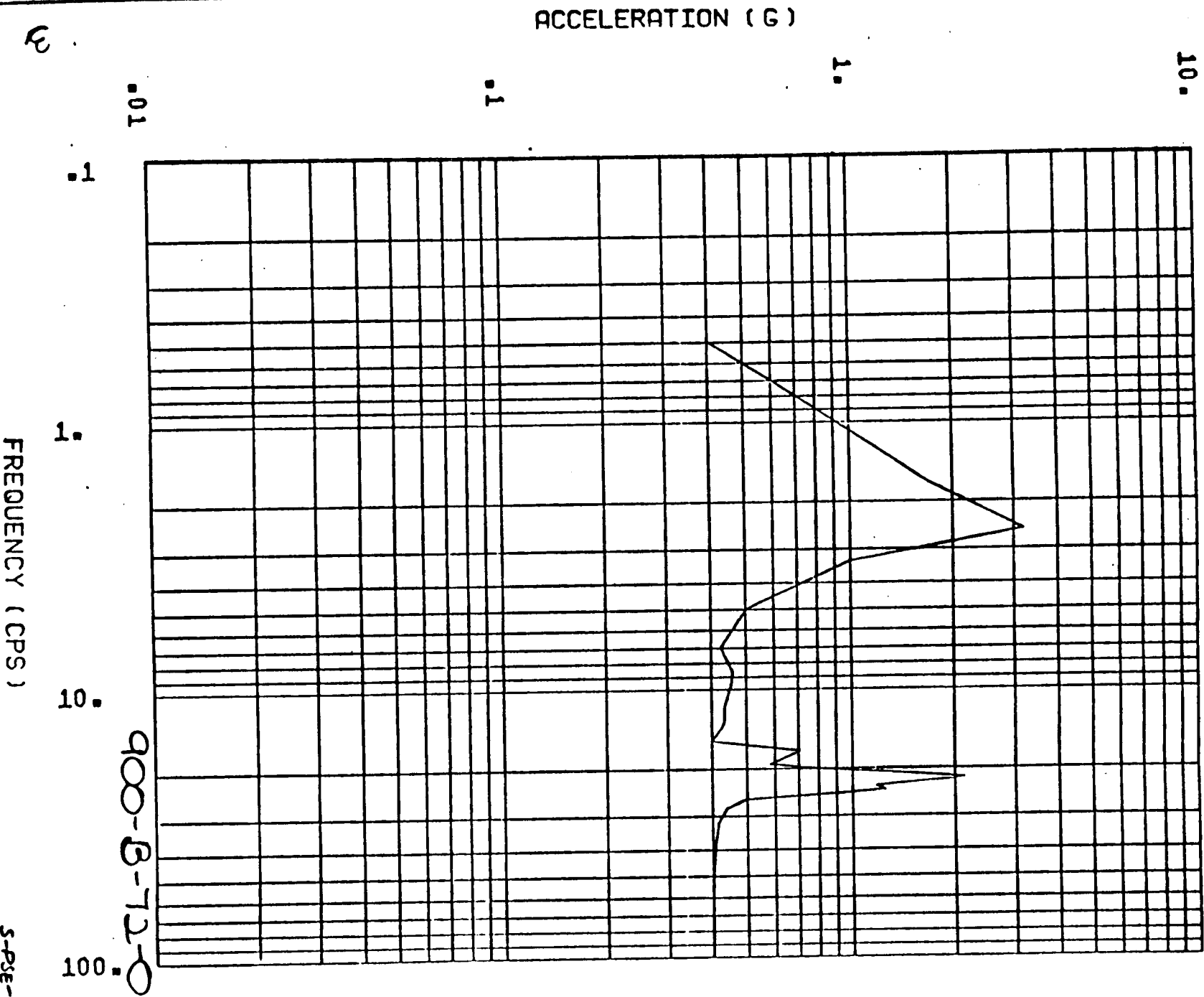
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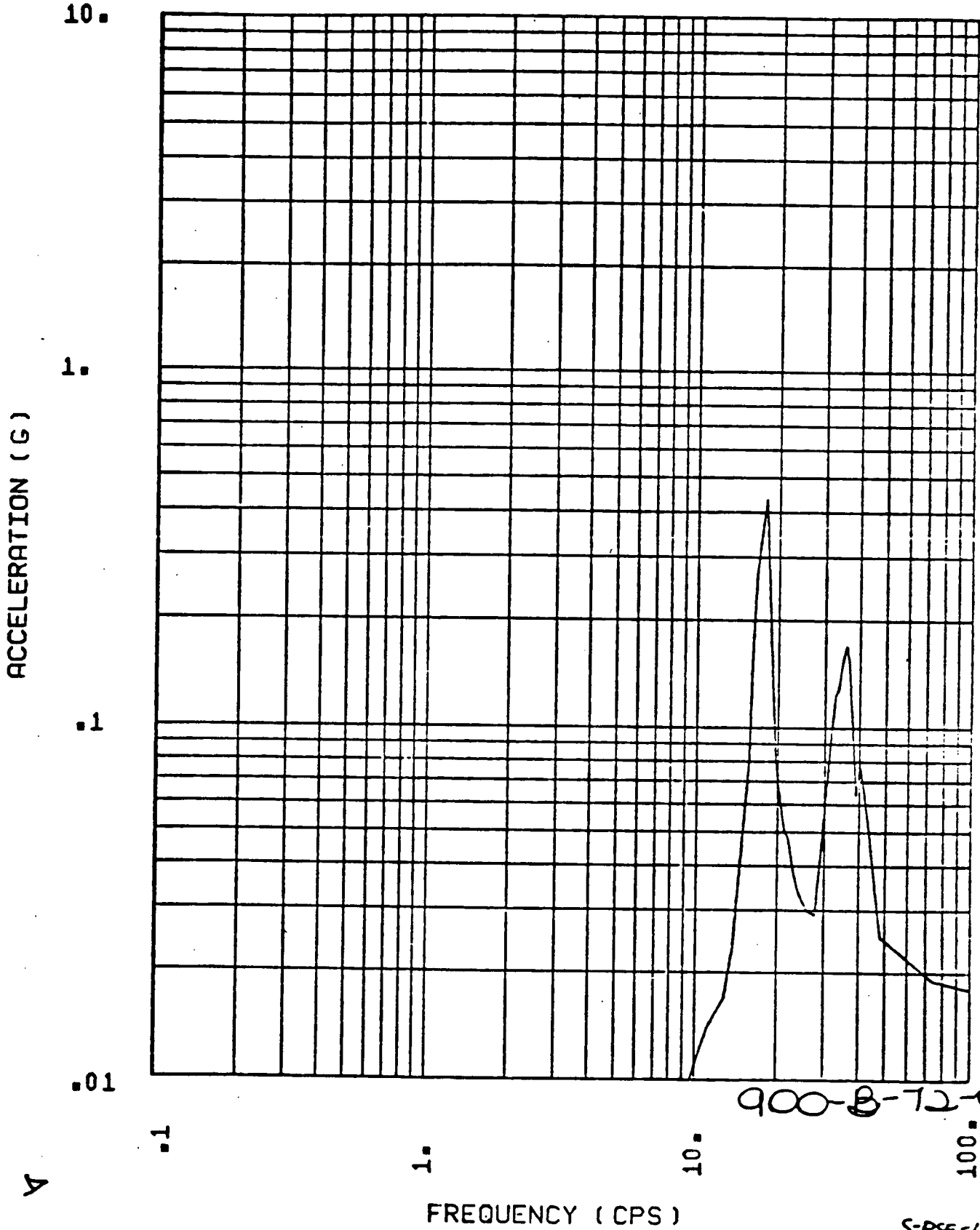


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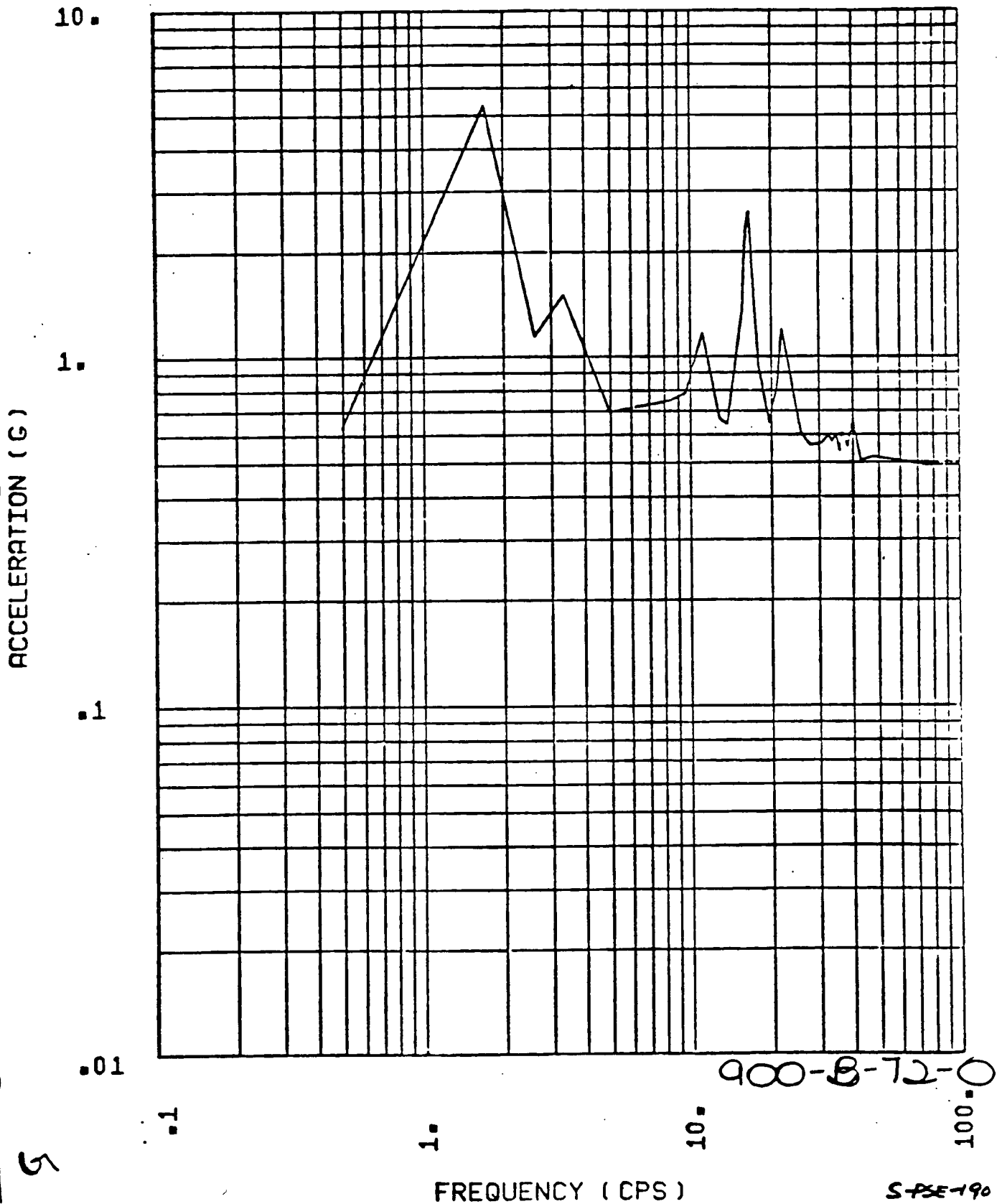
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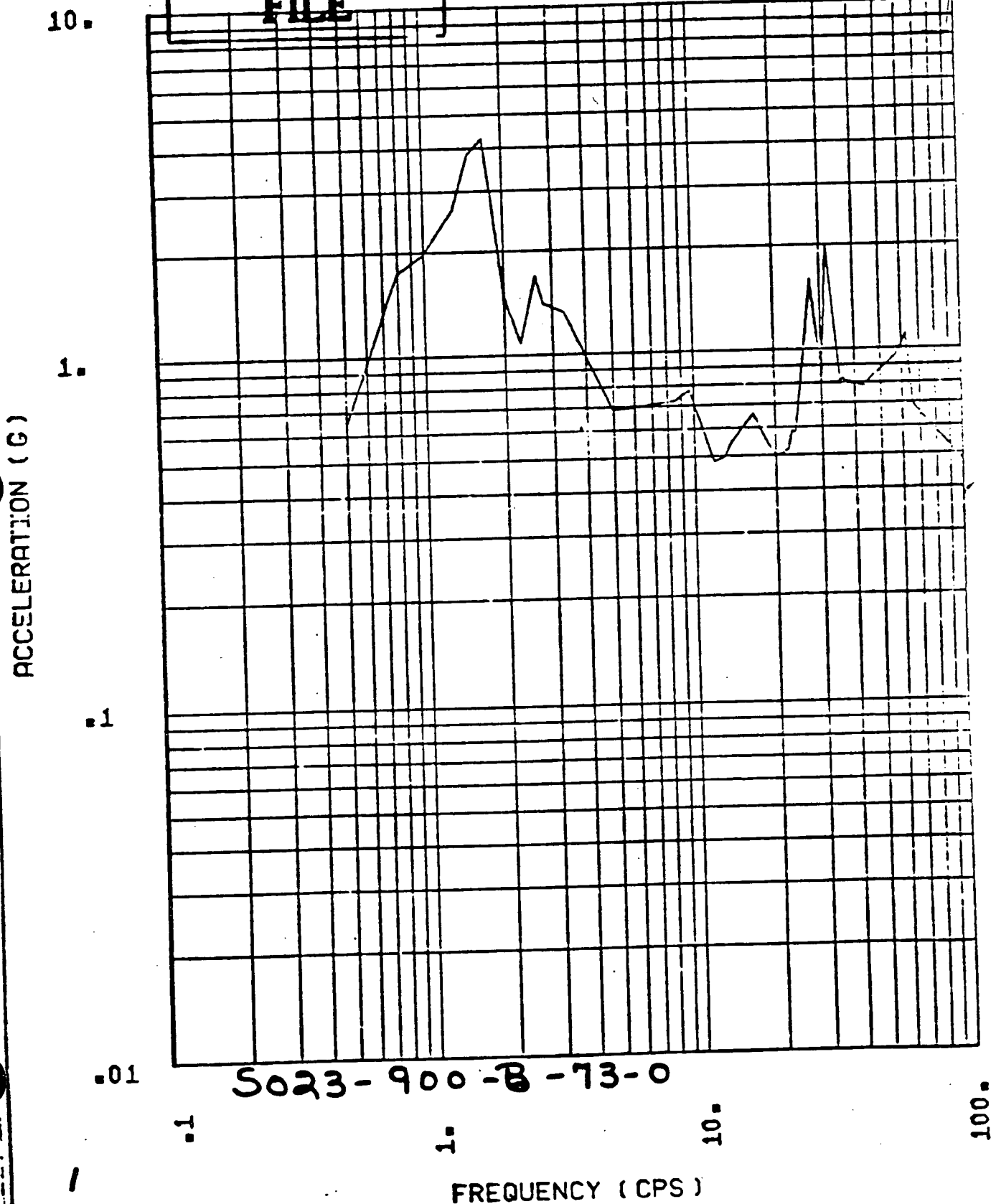


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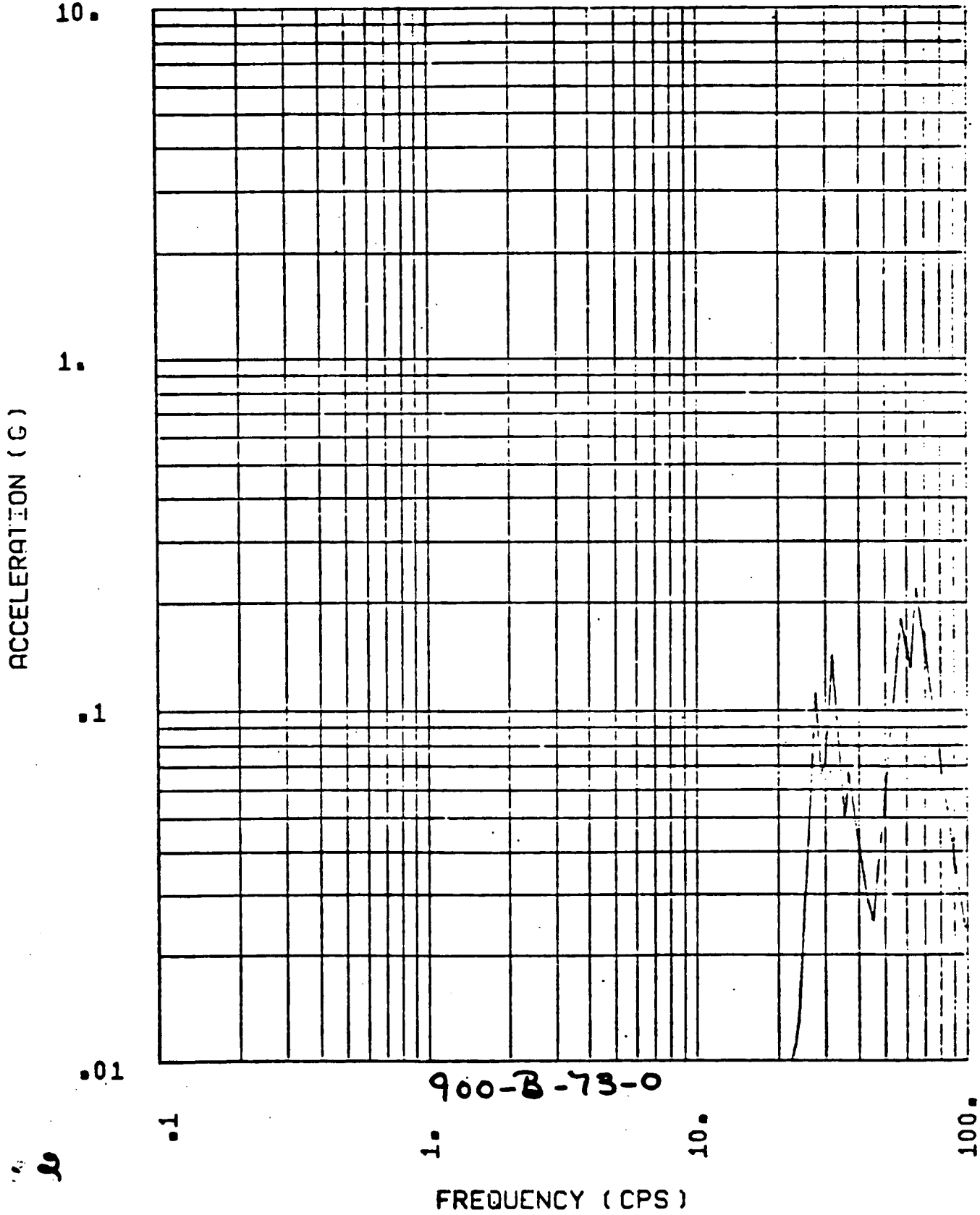
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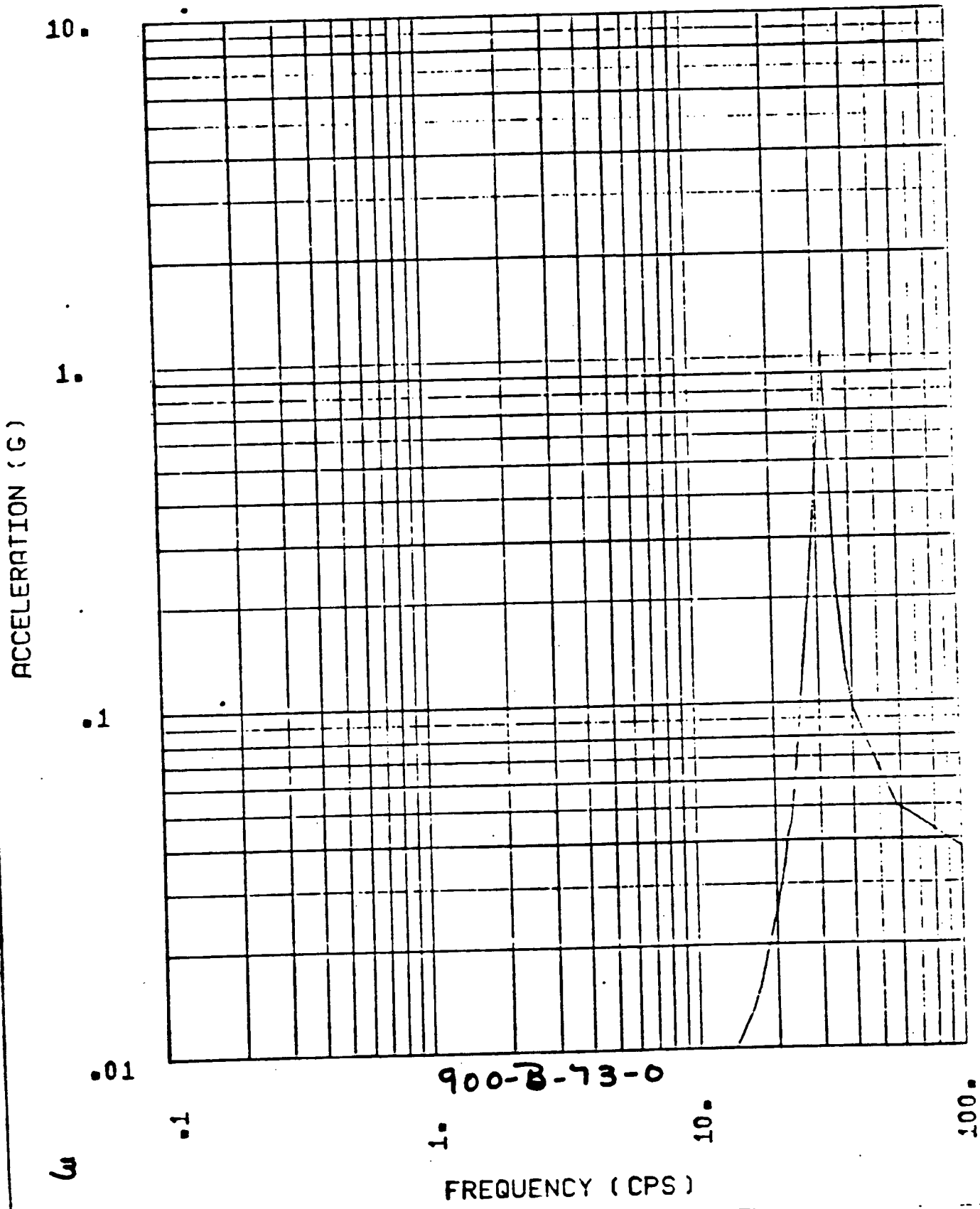


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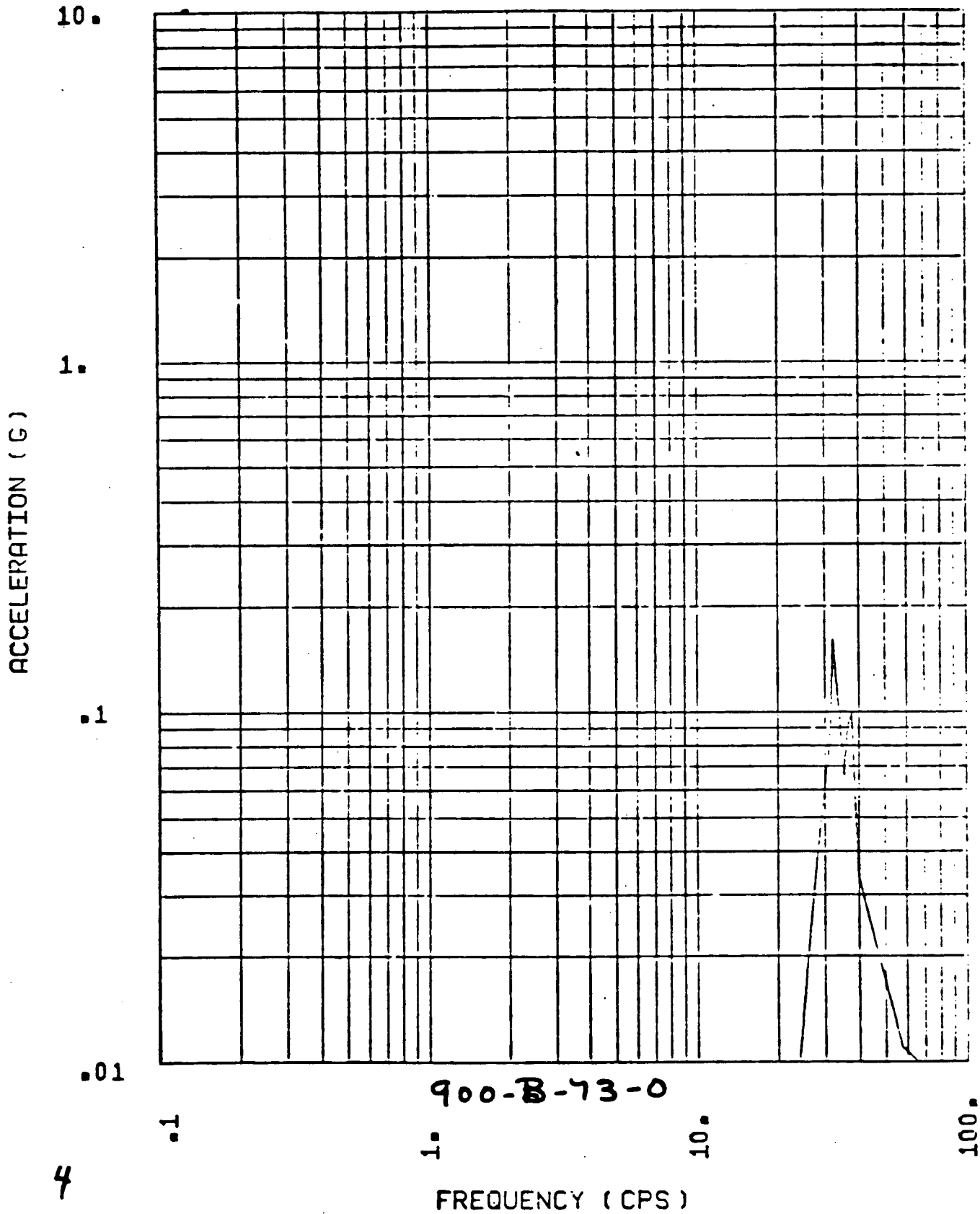


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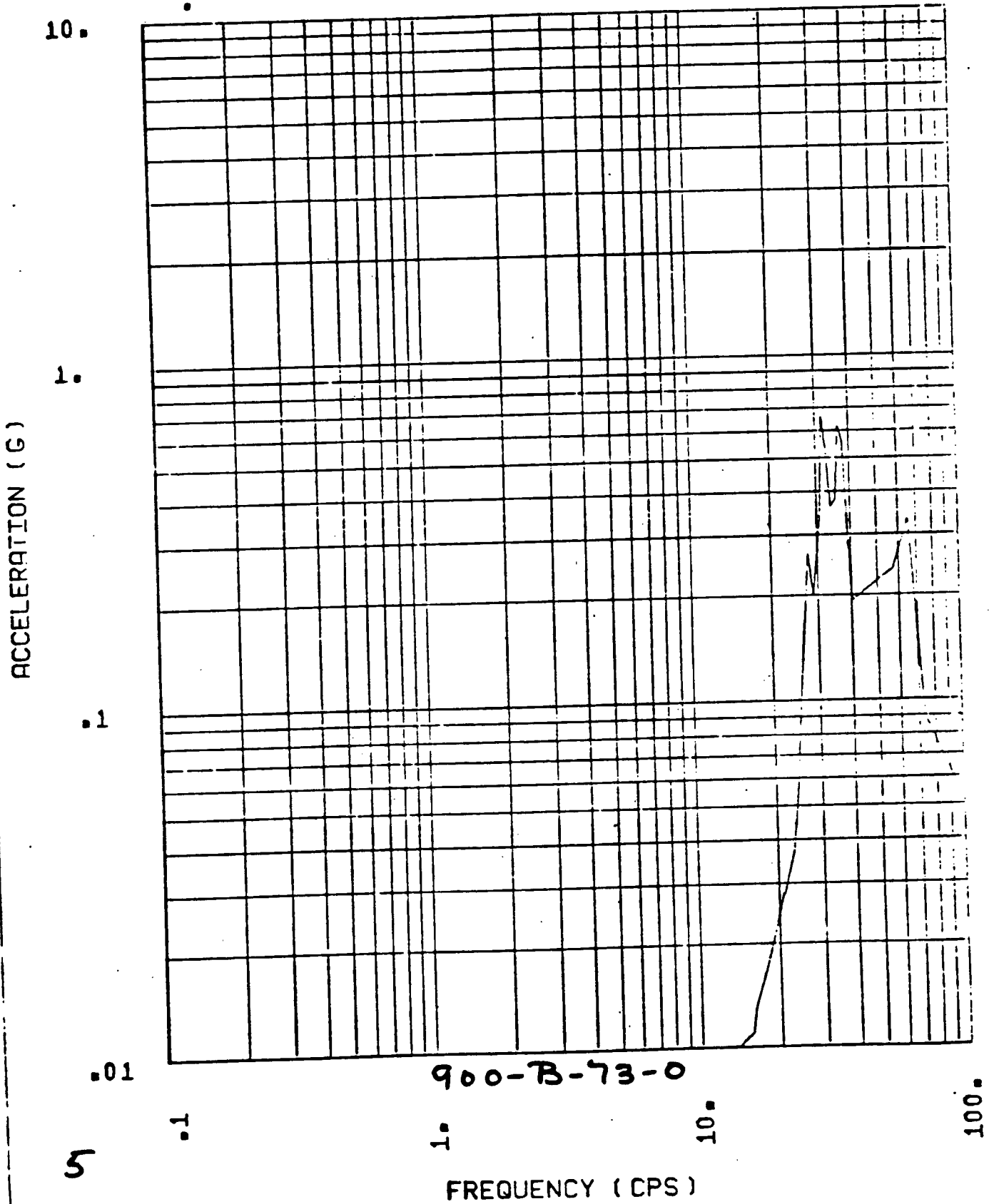
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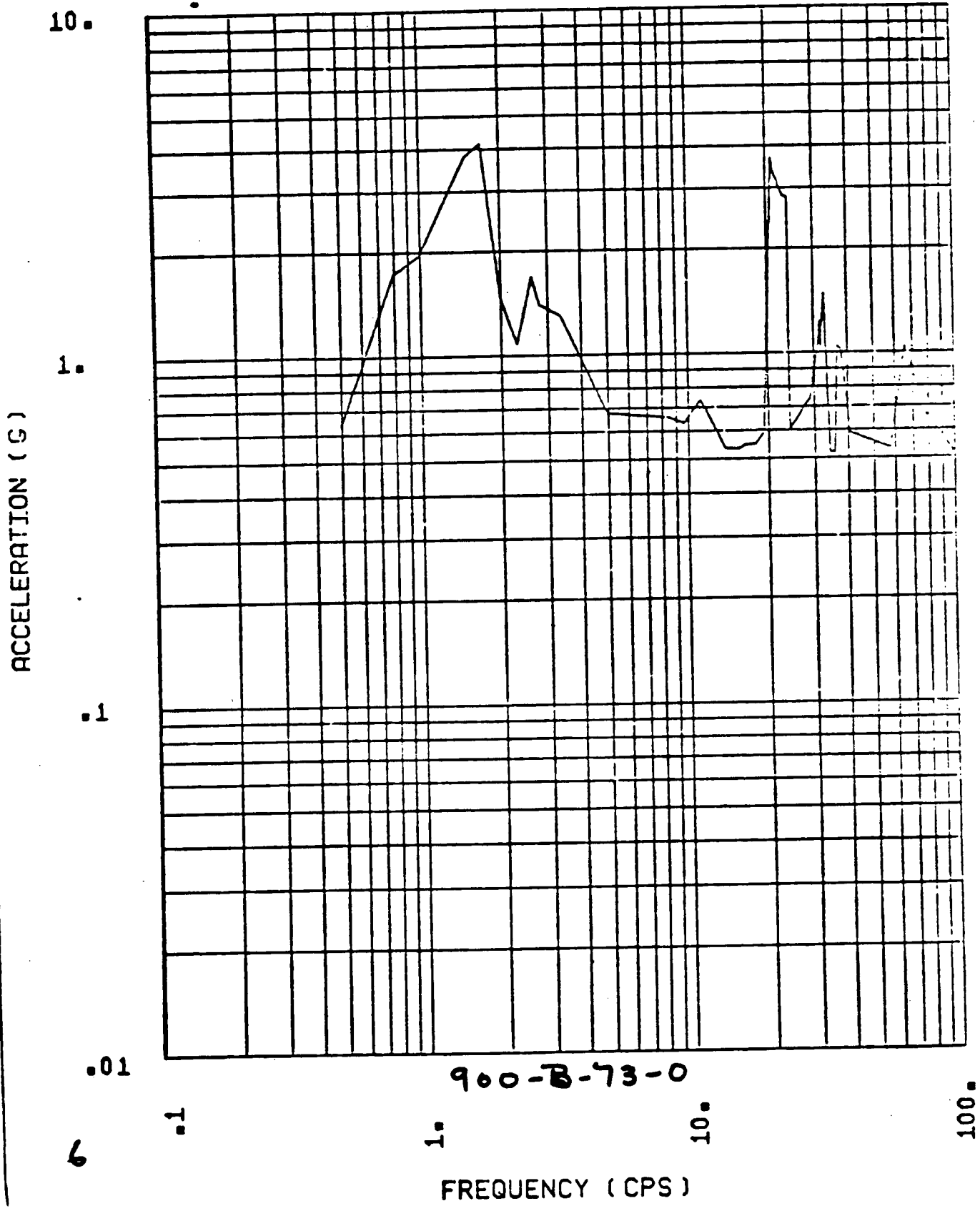
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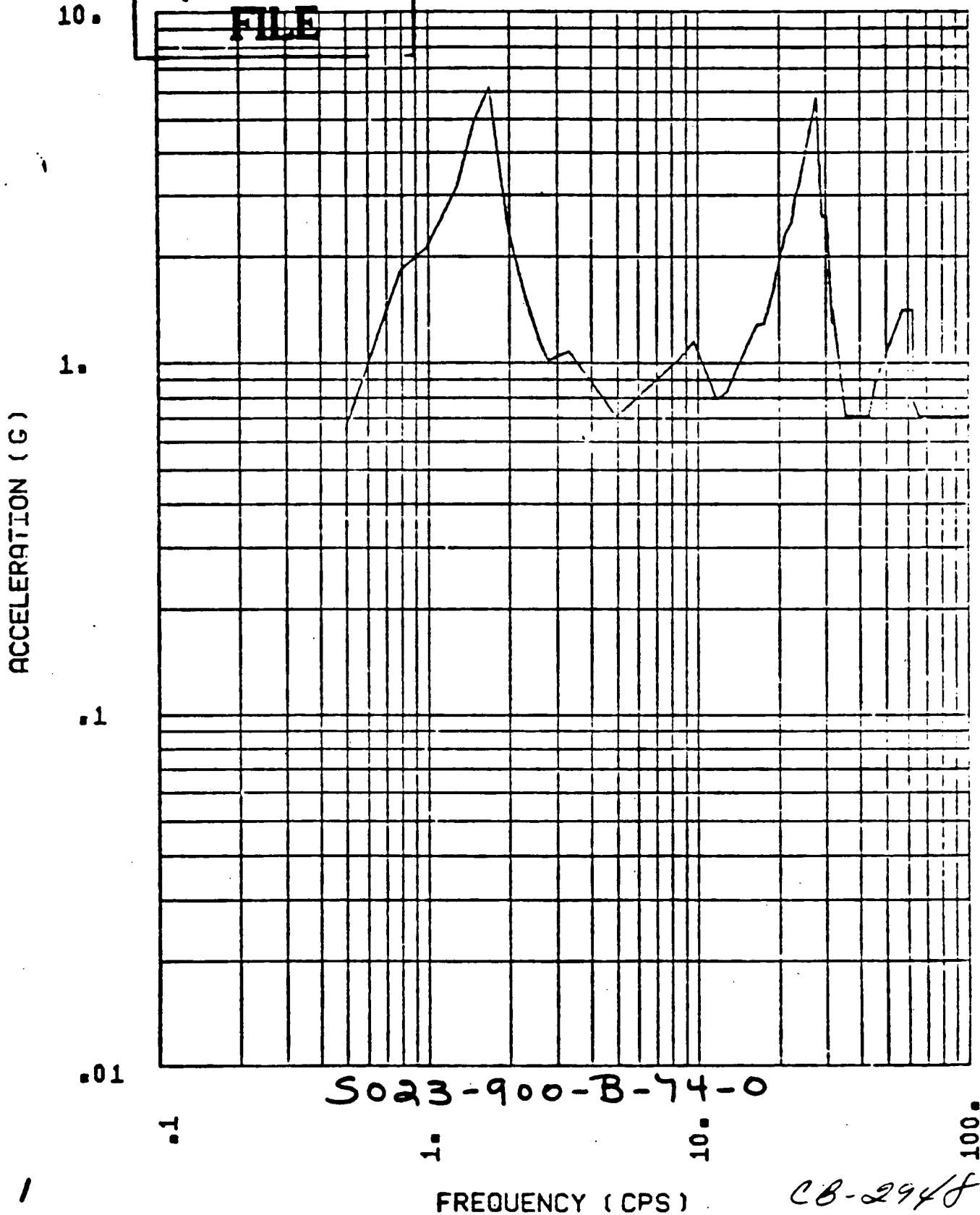
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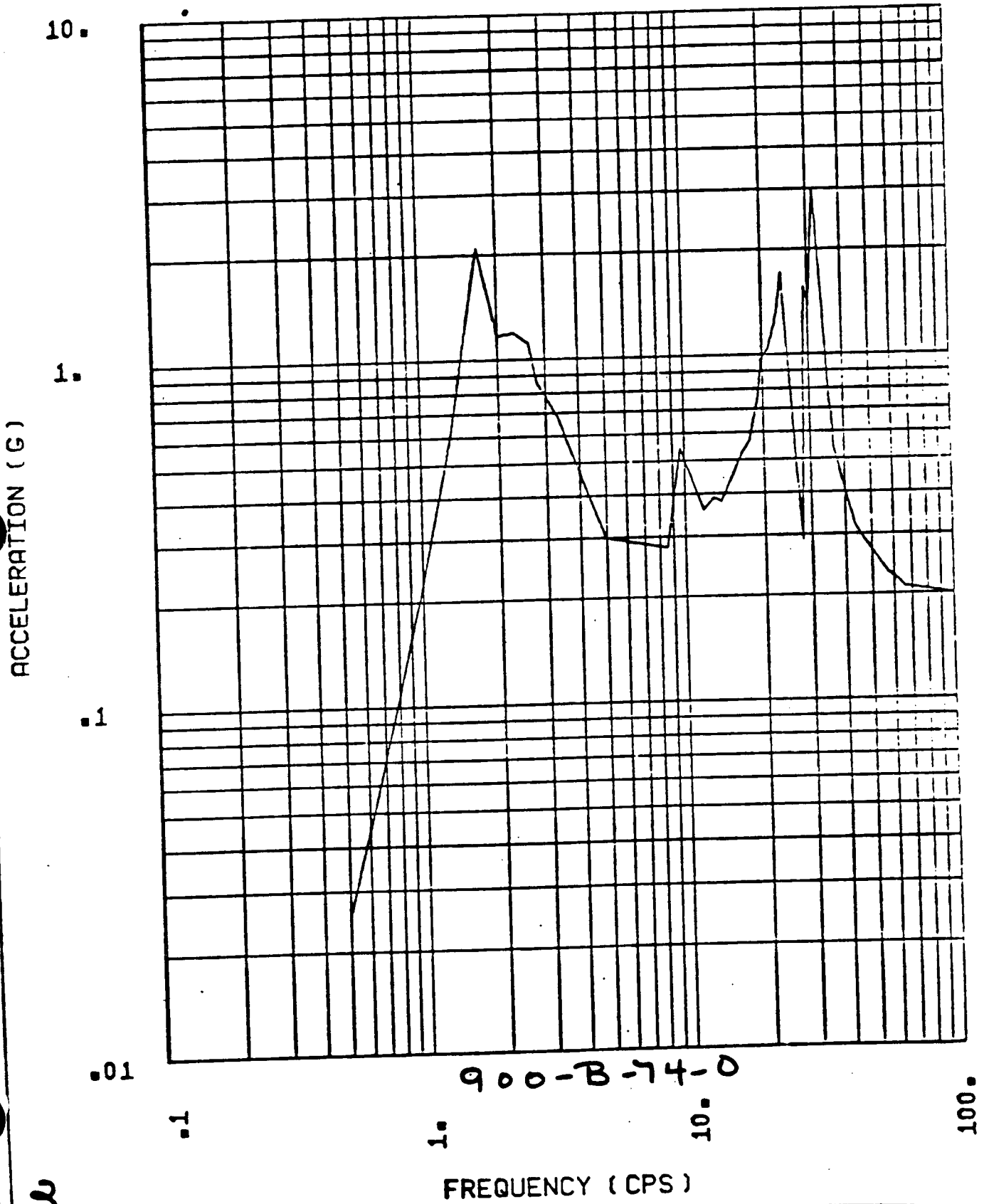
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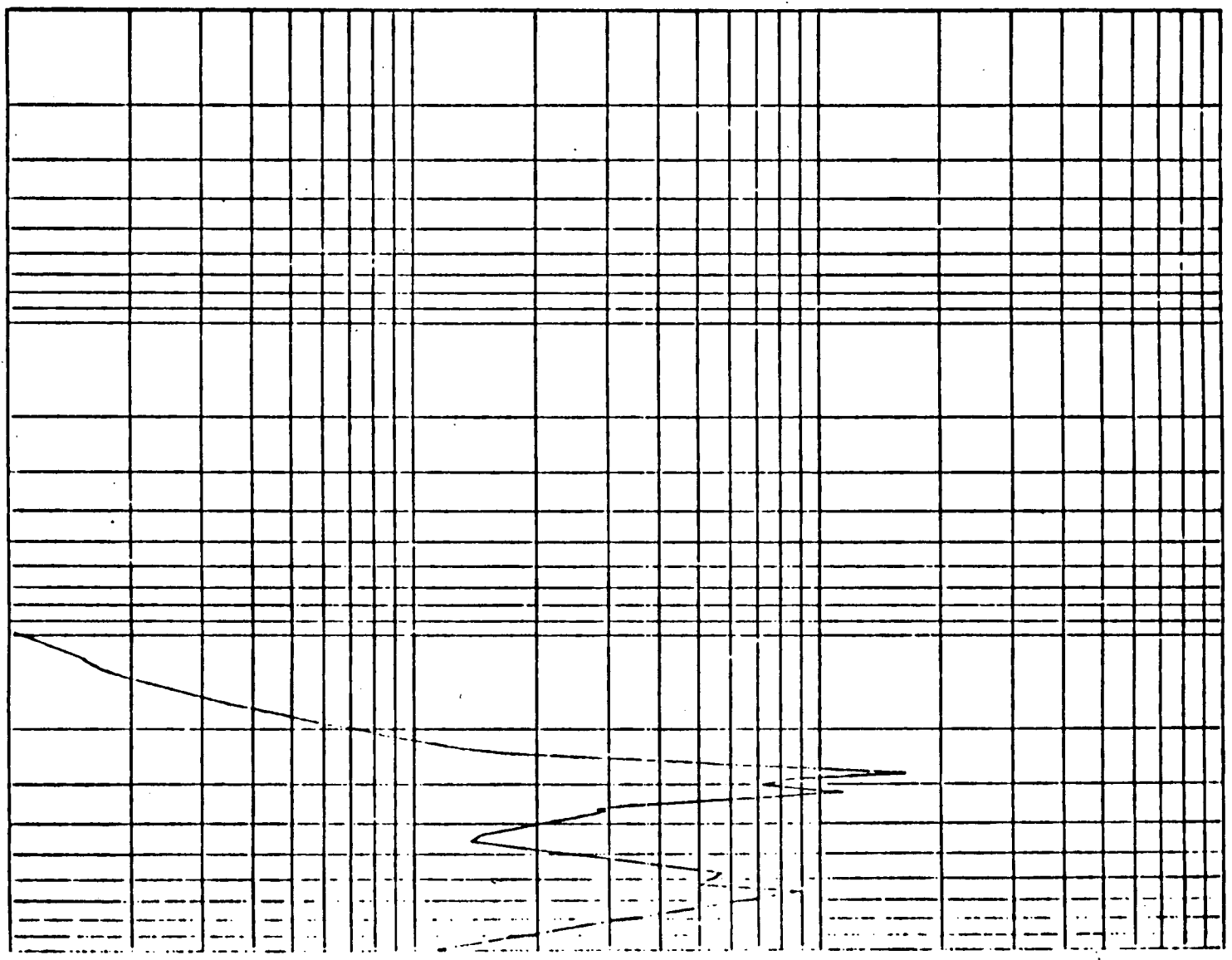
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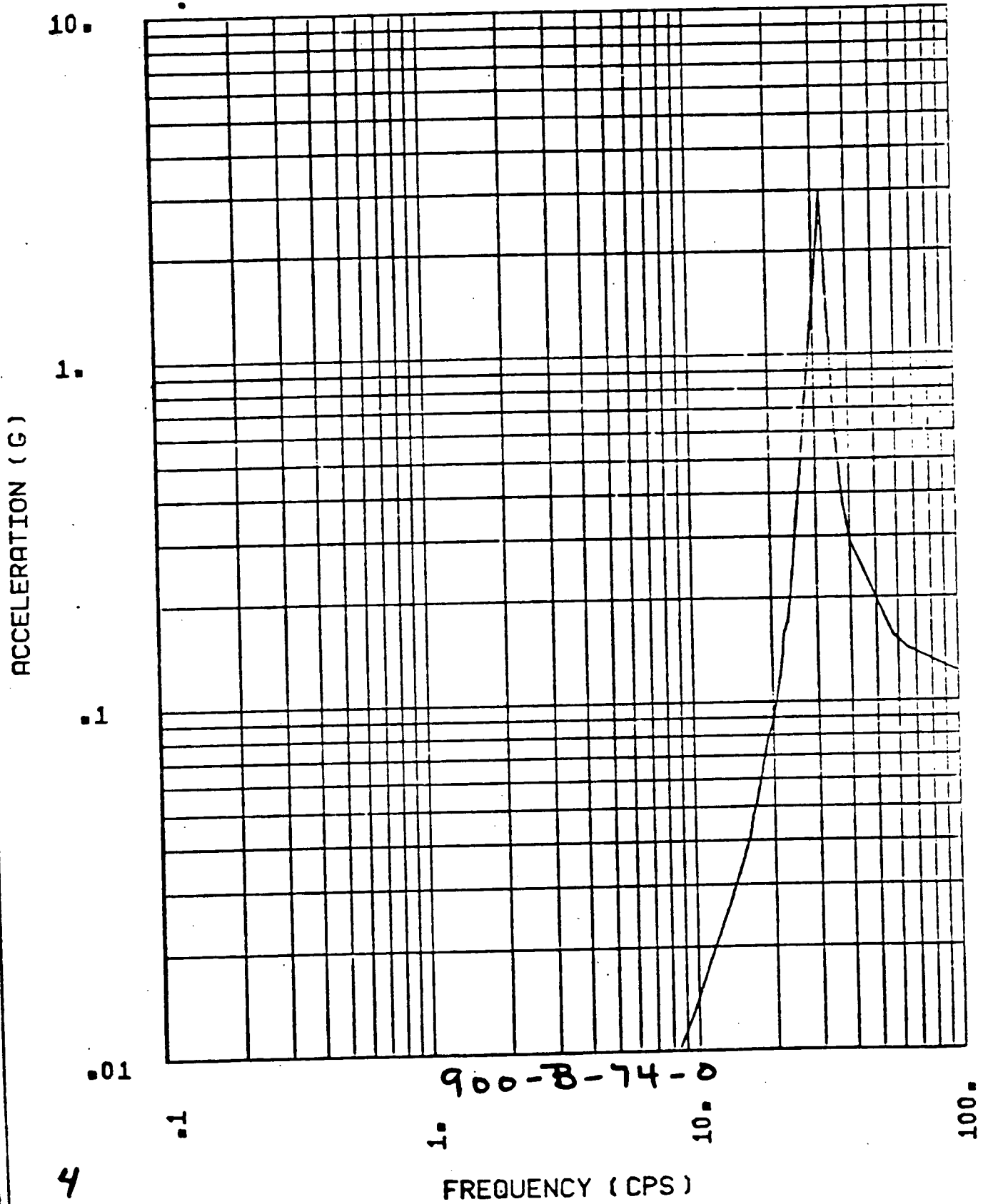
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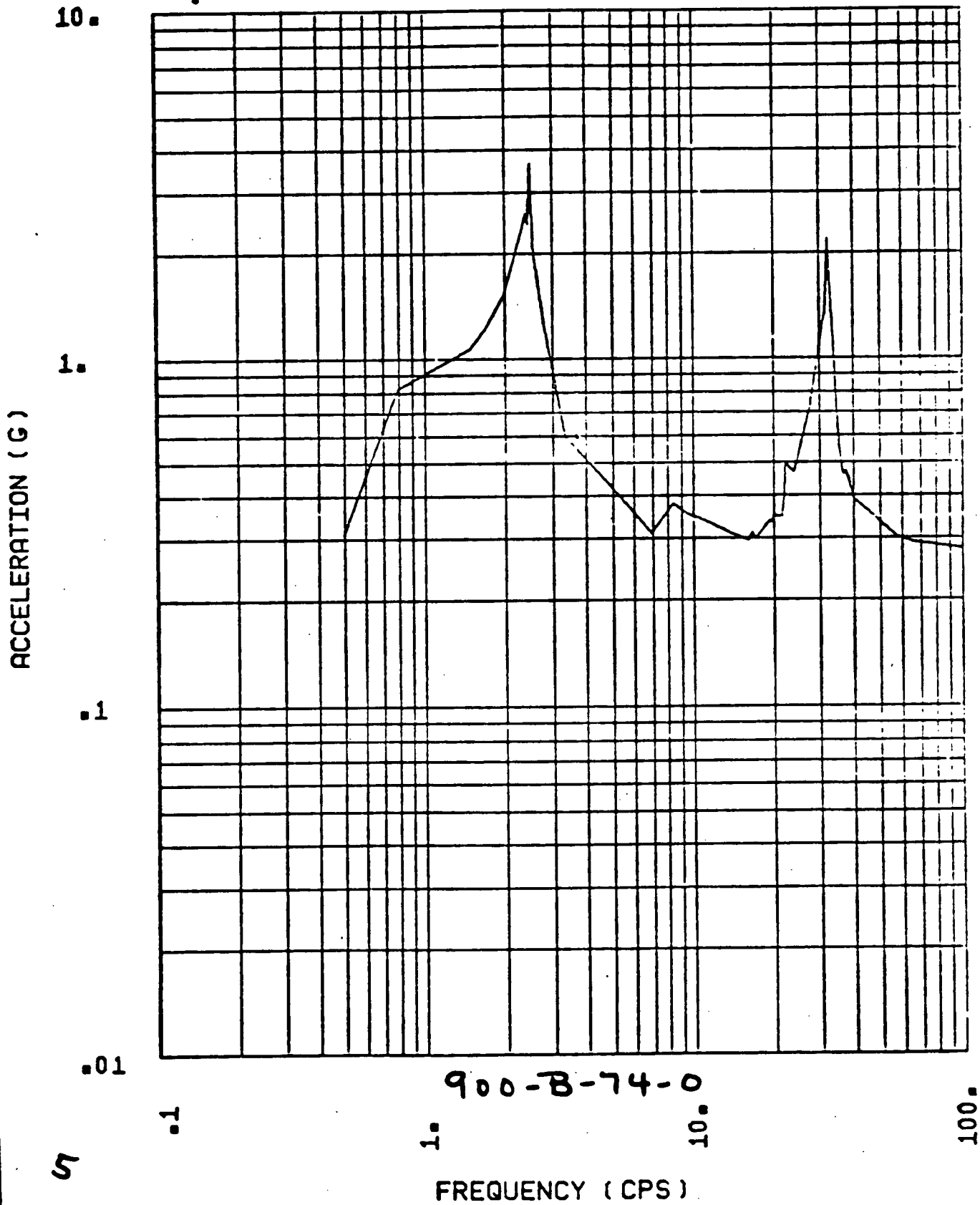
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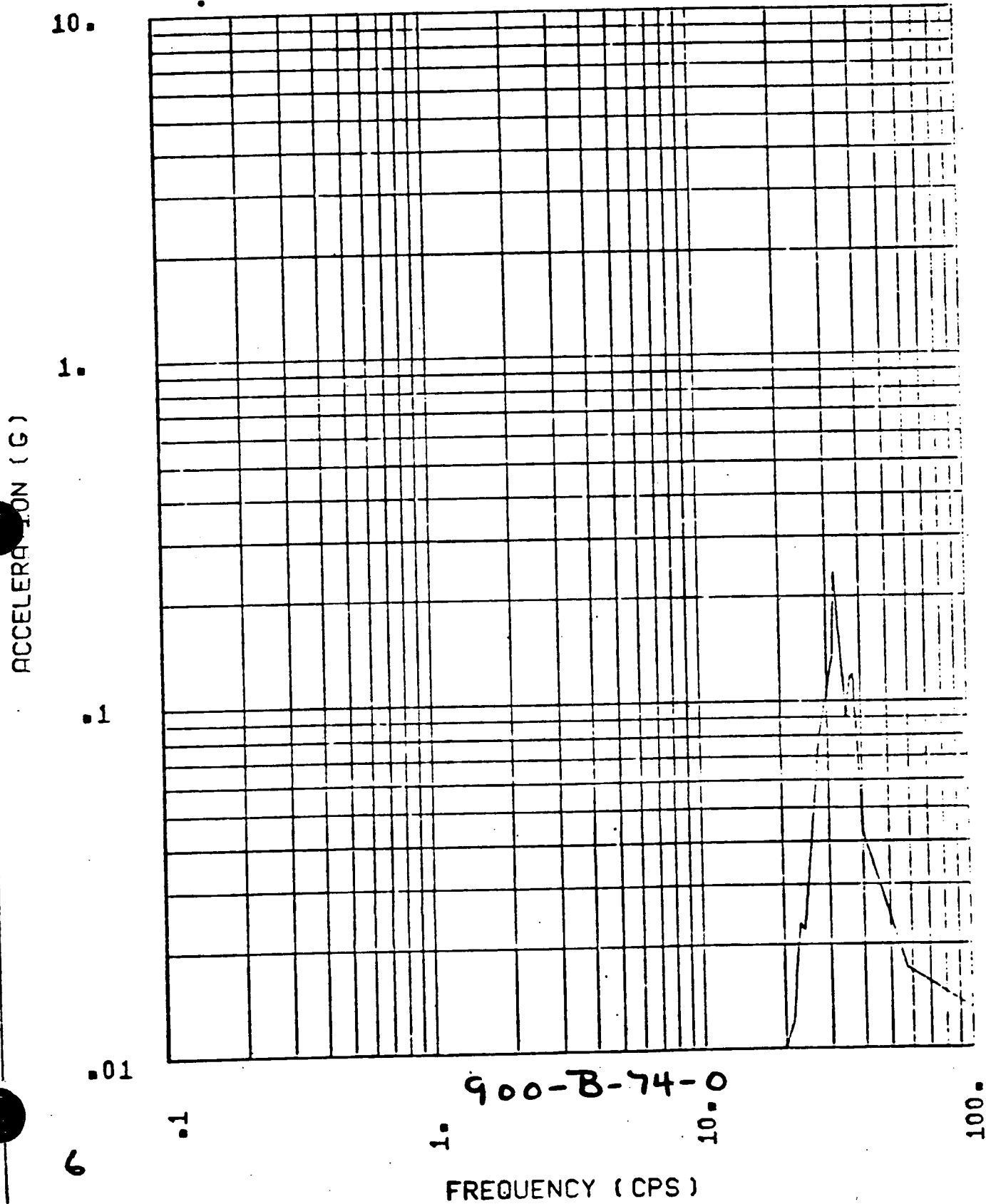


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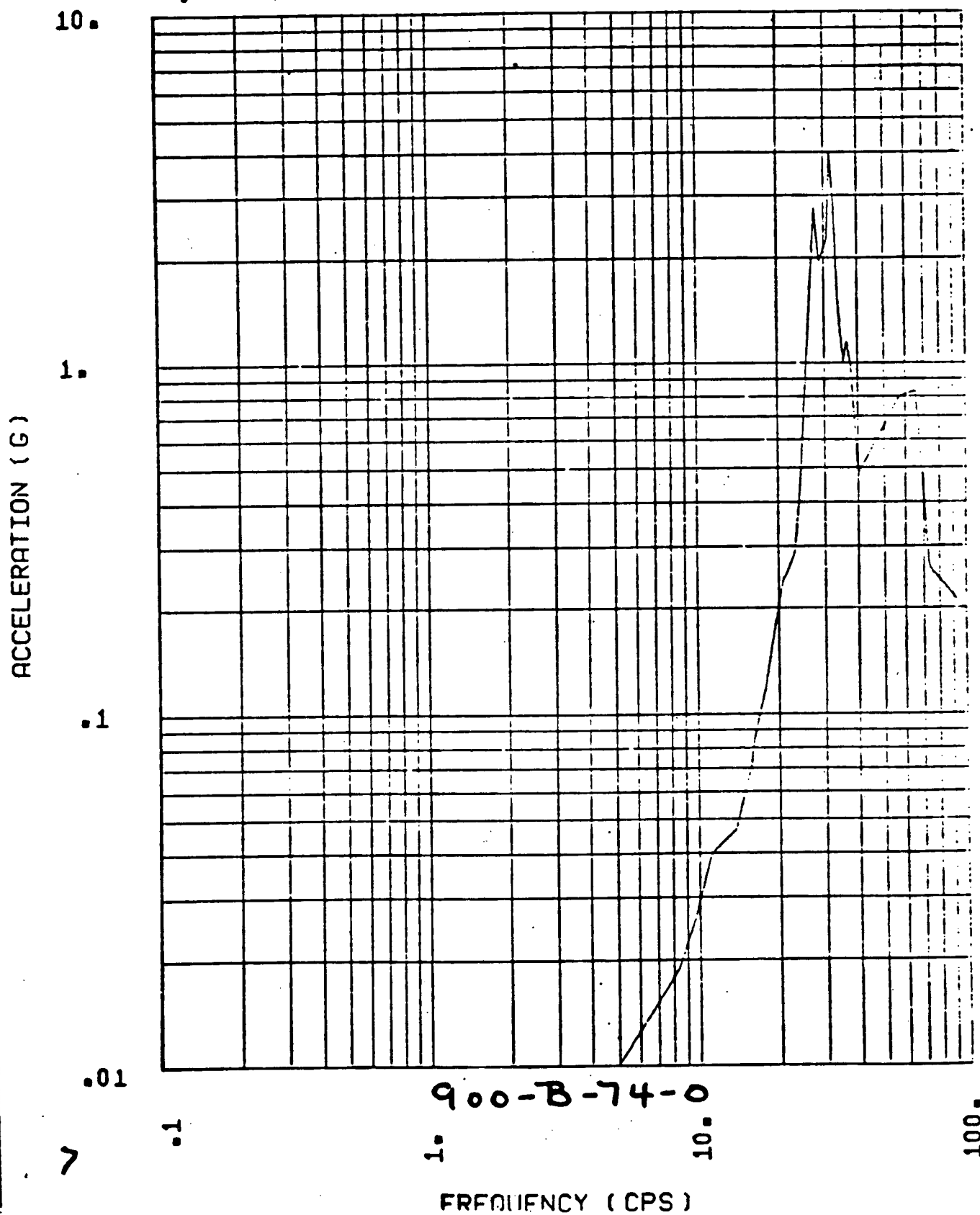


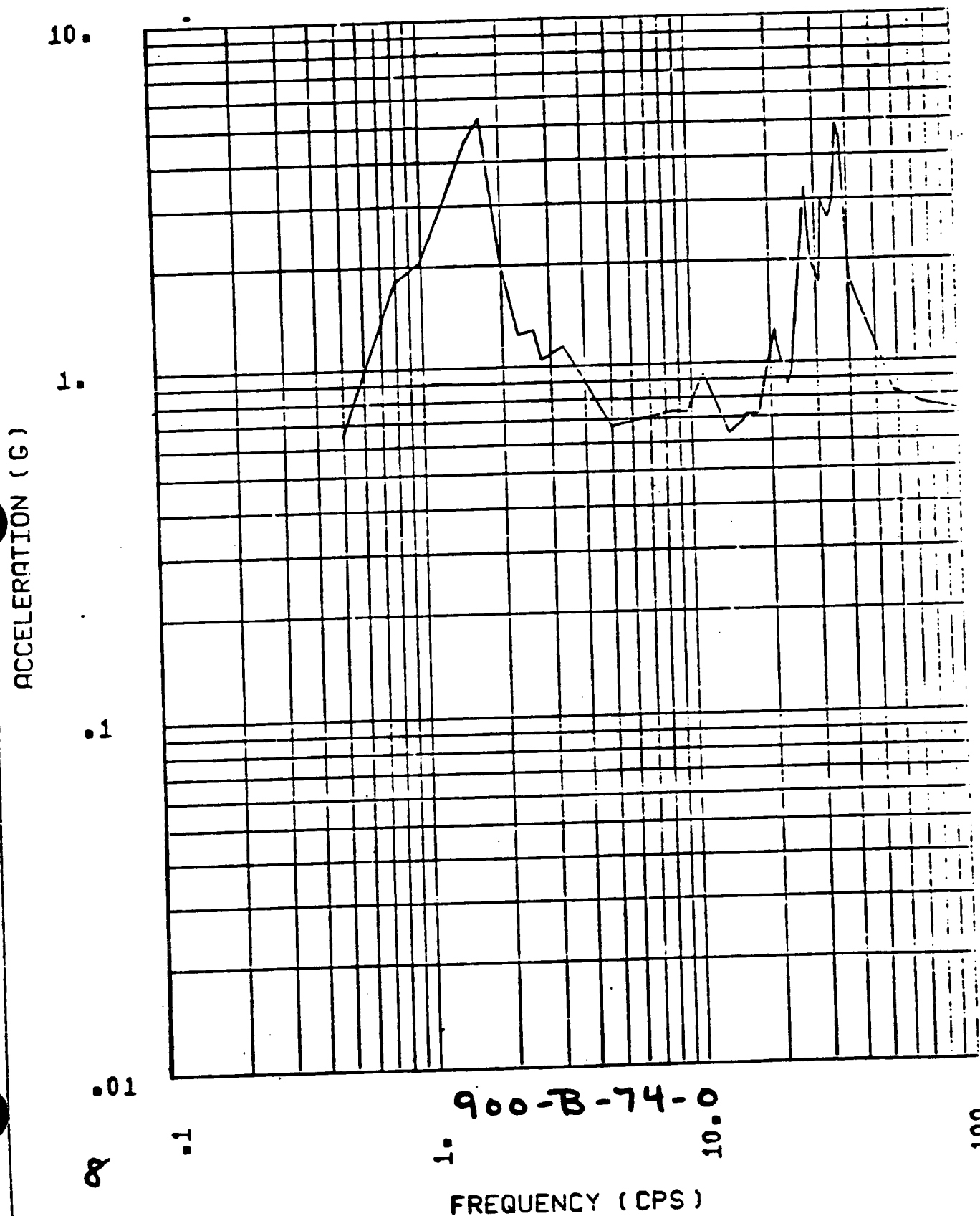
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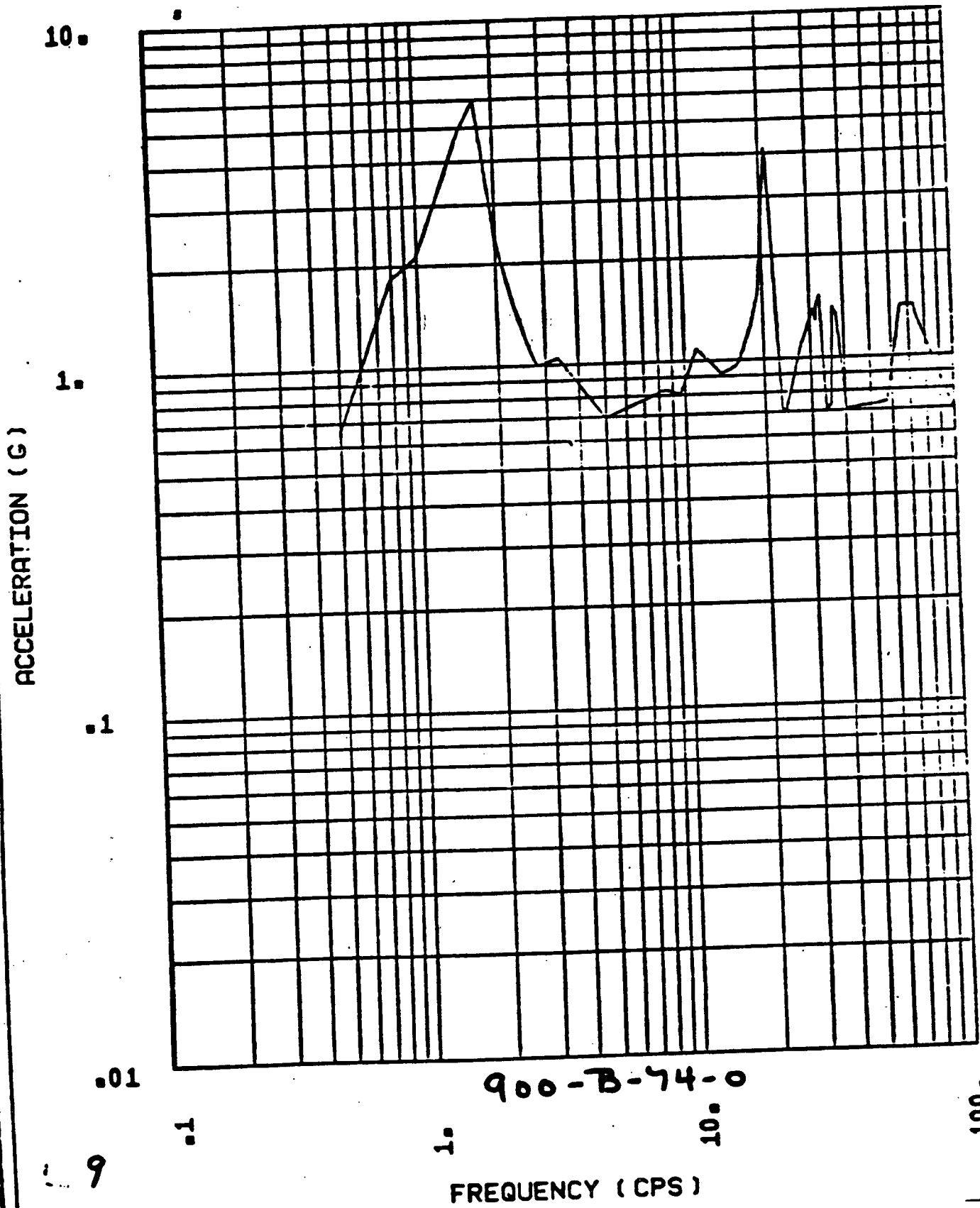




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APPENDIX C

DESIGN TRANSIENTS
AND LOADING COMBINATIONS

:

1. Code Class 1 and 2 Loading Combinations.
2. Preliminary Design Transients for Code Class 1 Reactor Coolant Piping System.

(Contains information taken from Enclosures (1) and (2) of Combustion Engineering (CE) to BPC letter, S-CE-2452, dated January 6, 1976 and designated as S023-900-B-41-0 and S023-900-B-42-0.)

DESIGN LOADING COMBINATIONS FOR ASME CODE
 CLASS 1 AND 2 REACTOR COOLANT SYSTEM PIPING COMPONENTS

Condition	Design Loading Combinations
Design	PD
Normal	PO + DW
Upset ^(a)	PO + DW + OBE
	PO + DW + RVC
	PO + DW + FV
	PO + DW + OBE + RVO
	PO + DW + DU
Emergency	PO + DW + DE
Faulted	PO + DW + DBE + RVO
	PO + DW + DBE + DF ^(b)
	PO + DW + DF

LEGEND: PD - Design pressure
 PO - Operating pressure
 DW - Dead weight
 OBE - Operating basis earthquake (inertia portion)
 DBE - Design basis earthquake (inertia portion)
 FV - Fast valve closure
 RVC - Relief valve - closed system (transient)
 RVO - Relief valve - open system (sustained)
 DU - Other transient dynamic events associated with the upset plant condition
 DE - Dynamic events defined as emergency condition
 DF - Dynamic events associated with a LOCA during which or following which the piping system being evaluated must remain intact

- a. As required by the ASME Code, Section III, Division I, other loads, such as thermal transient, thermal gradients, and anchor point displacement portion of the OBE, may require additional consideration in addition to those primary stress-producing loads listed.
- b. This loading combination (PO + DW + DBE + DF) applies only to components of the reactor coolant pressure boundary.

I. Reactor Vessel Specification

1. Heatup/Cooldown

The most significant transients from the standpoint of meeting the 3 Sm stress intensity range and fatigue limits in the vessel are the Plant Heatup, Plant Cooldown and Leak Test operations. The Plant Heatup (and Plant Cooldown) rate of 100F/hr is retained since nuclear heatup is a probable future requirement. The number of occurrences (500 each) is unchanged.

The previous specification formulation imposed a restriction that the loop fluid temperature be no more than 200F cooler than the pressurizer fluid temperature. This has proved to be an impediment to certain phases of the low power physics test program and to plant operations, particularly plant cooldown. To remove this artificial restriction, the heatup (cooldown) of the loop is divorced from that of the pressurizer by allowing the system pressure to be at any point between the loop saturation pressure and the normal operating pressure of 2250 psia. The revised pressure/temperature curves for Plant Heatup/Plant Cooldown are attached as Figure 1.

2. Loading/Unloading

NCD noted (Reference G) that subsequent to the Consumers Power vessel the plant loading and unloading (+5%/min) transients are analyzed as thermal steps. However, it is decided to retain the ramp characteristics of the transient since they exhibit a fairly large temperature change. The revised pressure/temperature curves for Plant Loading/Plant Unloading are attached as Figure 2. The number of occurrences (15,000 each) is unchanged.

It is noted that the change in temperature (pressure) is plotted, with the initial condition to be determined from the reactor coolant temperature versus load program. This technique (used for all power range transients) then requires only a change to the specification temperature control program (as appropriate) from one contract to the next. In addition, the temperature change occurring during any transient is somewhat increased to cover future minor changes in plant design. By exhibiting the loading and unloading transients separately, confusion concerning end-point consistency is avoided.

The transient curves are slightly idealized (from those in Reference A) to aid the stress analyst. In addition as noted, the temperature/pressure envelope is increased to cover future minor changes in plant response. For example, the hot leg temperature change (expected) of 57F is increased to 60F while the cold leg temperature change is increased from 8F (expected) to 10F. The very mild pressure transient during plant unloading is idealized

by drawing a mean curve through the oscillatory curve of Reference A.

Plant maneuvering between 0 - 15 percent power is performed manually and quite slowly (<1%/min). The pressure/temperature changes are part of the 10^6 occurrences of Normal Plant Variations.

3. Step Power Changes/Normal Plant Variations

NCD noted (Reference G) that the ± 10 percent power steps in past specifications exhibit temperature and pressure fluctuation within the range of the specified normal plant variations. It is decided to increase the Normal Plant Variations from $\pm 6F$, ± 50 psi to $\pm 10F$, ± 100 psi to encompass the revised power step transients (Reference A) and to envelope future plant responses. The ± 10 percent power step transient curves are replaced by a statement that these maneuvers (2000 occurrences) are within the 10^6 cycles of normal plant temperature and pressure fluctuations.

4. Plant Trips

Past specifications contained three separate transients, Reactor Trip (400 occurrences), Loss of Primary Flow (40 occurrences), and Loss of Load (40 occurrences), which exhibit quite similar characteristics. It is decided to produce a composite transient with a total of 480 cycles. The pressure and hot leg temperature transients are those of the Loss of Load transient. The cold leg temperature transient is a composite of the Loss of Load and Loss of Primary Flow transients to produce the most conservative temperature change. The composite transient curves are slightly idealized (from those in Reference A) to aid the stress analyst and the temperature/pressure envelope is increased to cover future minor changes in plant response. For example, the hot leg temperature change (expected) of 64F is increased to 70F while the cold leg temperature change is more rapid and a composite of the largest temperature swings. The revised pressure/temperature curves for this composite transient are attached as Figure 3.

5. Loss of Secondary Pressure

Since the number of occurrences established for this transient is only five, the condition is included in the Emergency Condition category. Therefore, it is recommended that the condition be excluded from the fatigue evaluation of the component. However, the designer should consider the effects which may be produced by the relative thermal movement of component parts due to the large, rapid change in loop temperature.

This transient is considered to represent all the rare (<25 occurrences) plant conditions which might produce a significant temperature change. Any accidental steam release from the steam generator by inadvertent valve actuation is thus represented. A second example involves the start of a third reactor coolant pump in a two-loop (four pump) plant when operating at reduced power (~50%) with two pumps in the same loop. The start of the third pump will produce a flow reversal and subsequent change in fluid temperature through one reactor vessel hot leg nozzle of approximately 70F. This type of transient is enveloped by the far more severe pressure/temperature curves for Loss of Secondary Pressure which are attached as Figure 4.

6. Hydrostatic Test

The graphical presentation of the hydrostatic test is replaced by a statement that the reactor vessel is to be hydrostatically tested in accordance with the ASME Boiler and Pressure Vessel Code, Section III, Nuclear Vessels. The primary side temperature is held essentially constant (between 100F-400F) for any one test. The number of occurrences (10) is unchanged.

7. Plant Leak Test

The plant leak test is conducted at the normal operating pressure of 2250 psia in accordance with Figure 5. The steam generator secondary side is at atmospheric pressure. The number of occurrences (200) is unchanged.

8. Bolting of the Closure Head

NCD noted (Reference G) that in past vessel specifications the number of stud elongations is specified and that this has been assumed (by NCD) to correspond instead to the number of bolt ups of the closure head. This is more conservative since there are several stud pulls per closure head bolt-up cycle. For clarification the revised specification wording requires that the reactor vessel assembly be designed for a minimum of fifty head bolt-up cycles.

II. Steam Generator Specification

Items 1-7 of Section I (Reactor Vessel Specification) are applied to the revision of the steam generator specification. In addition, the following modifications are made:

1. Normal Plant Variations

An allowance is made for secondary pressure fluctuations of ± 80 psi (10^6 lifetime occurrences) in addition to the primary temperature and pressure fluctuations.

2. Cold Feedwater at Hot Standby/Loss of Feedwater Flow

During both of these conditions, the source of the auxiliary feedwater flow in many plants is the condensate storage tank exterior to the turbine building. Typically, this tank is heated only to prevent freezing. In specifications to date, the auxiliary feedwater flow temperature is specified to be 70F. This is changed to the standard value for nonheated tanks of 40F to eliminate an increase in the balance-of-plant requirements (for heating of the fluid stream).

In past specifications for the loss of feedwater flow conditions, cold feedwater is introduced with the secondary side dry. A conservative computer simulation of the condition (Reference F) shows that after 5 minutes following the loss of normal feedwater from a full load condition, the secondary side contains 28 percent of full load inventory. At this time, auxiliary feedwater at 700 gpm is initiated. To prevent the imposition of an unduly restrictive NDTT condition upon the tubesheet, the specification is revised from a dry condition to the calculated minimum secondary inventory.

3. Secondary Leak Test

The first sentence of Paragraph 4.3.5 in the specification is as follows:

"Secondary side leak test will be conducted with the secondary side pressurized from 820 to 1100 psia". To be more general, this will be changed to " . . . from 820 to design pressure". The 820 psia is permitted with the 0.048 inch wall tubing. The test pressure will be appropriately changed if the tube wall thickness is changed.

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III. Reactor Coolant Pump Specification

Items 1-7 of Section I (Reactor Vessel Specification) are applied to the revision of the Pump Specification.

IV. Pressurizer Specification

1. Heatup/Cooldown

As noted in Item 1 of Section I (Reactor Vessel Specification), the previous specification requirement that the loop fluid temperature be no more than 200F cooler than the pressurizer fluid temperature impeded plant operations. Accordingly, the heatup (cooldown) of the pressurizer is divorced from that of the loop. At any pressurizer temperature, the pressurizer pressure may be at any point between the saturation condition and the normal operating pressure of 2250 psia. Hence, the point at which the bubble is pulled is not defined thereby permitting operations personnel the widest possible latitude.

Past specifications defined a pressurizer heatup rate of 100F/hr and a cooldown rate of 200F/hr. The former was based on the pressurizer heater output with a solid pressurizer. However, with the hot standby water level established after a bubble pull, the possible heatup rate is substantially increased. Accordingly, the heatup rate of the pressurizer is increased to 200F/hr. The heatup/cooldown rates of the specification limit plant operations since with the actual quantity of spray available for cooldown and the actual heater power available (after bubble pull) for heatup, the process rates could actually be exceeded in the plant. The revised fluid pressure/temperature curves for pressurizer heatup/cooldown are attached as Figure 6. The number of occurrences (500 each) is unchanged.

During the pressurizer cooldown process, the bubble is collapsed by introducing cold auxiliary spray until the pressurizer is filled with subcooled water. This generally takes place just after reactor coolant pump operation is discontinued prior to the initiation of shutdown cooling. The transient is defined as the filling of the pressurizer with 40F auxiliary spray water at 133 gpm starting with an initial water volume equal to that required to cover the heaters. The initial fluid temperature is 400F. This is a conservative description of the process. The Vendor is required to integrate the pressurizer fill analysis with the previously described cooldown process (Figure 6).

2. Loading-Unloading/Step Power Changes/Normal Plant Variations

Inspection of the transient curves of Reference A reveals minor pressurizer pressure and fluid temperature variations during the plant loading and unloading operations. During the loading maneuver, pressure exhibits a maximum variation of 35 psi. The steam temperature exhibits a maximum variation of 2F and the water temperature exhibits a maximum variation of -11F from the equilibrium set point. During the unloading maneuver, pressure exhibits a

maximum swing of +20 psi to -60 psi from the set point. The steam/water spaces are essentially in thermal equilibrium throughout the transient with a maximum decrease in temperature of 4F from the set point.

Similar minor pressurizer pressure and fluid temperature variations are noted during the step power changes. The pressurizer pressure varies +50, -50 psi and +50, -100 psi from the set point during the power step increase and decrease, respectively. The maximum fluid temperature swings are +3, -4F and +3, -8F from the set point during the power step increase and decrease, respectively.

It is concluded that the Loading/Unloading and Step Power changes may be considered within the 10^6 cycles of normal plant temperature and pressure fluctuations. The Normal Pressurizer Variations in past specifications of +50 psi, +7F are increased to +100 psi, +20F to include these transients.

3. Plant Trips

In Section I (Reactor Vessel Specification) a composite transient (480 occurrences) is developed to include Reactor Trip (400 occurrences), Loss of Primary Flow (40 occurrences) and Loss of Load (40 occurrences). The most severe pressure transient (that of the Loss of Load) is used to represent the composite transient. The accompanying pressurizer steam/water temperature transient is slightly idealized (from those in Reference A) to aid the stress analyst and to cover future minor changes in plant response. The revised pressure/temperature curves for this composite transient are attached as Figure 7.

4. Loss of Secondary Pressure

The pressurizer fluid temperature transient accompanying the pressurizer pressure transient (Figure 4) during this incident (discussed in Item 5 of Section I) is attached as Figure 8.

5. Hydrostatic Test

The graphical presentation of the hydrostatic test is replaced by a statement that the pressurizer is to be hydrostatically tested in accordance with the ASME Boiler and Pressure Vessel Code, Section III, Nuclear Vessels. The fluid temperature is held essentially constant (between 100F-400F) for any one test.

6. Plant Leak Test

The pressurizer leak test is an integral part of the Plant Leak Test (Figure 5) as discussed in Item 7 of Section I (Reactor Vessel Specification).

7. Spray Nozzle/Surge Nozzle

During the transients discussed above, the pressurizer surge and spray nozzle flow rates (and fluid temperature) vary. In past specifications these conditions were depicted graphically. After much discussion, it was decided that the following conservatively represents the additional transient conditions to be imposed upon the surge and spray nozzles.

a. Loading

During plant loading, the surge flow temperature transient is as follows (Reference A). At time zero, the small continuous spray (1.5 gpm) produces a flow out of the pressurizer at the equilibrium temperature of 653F. As the power ramp is initiated, the surge flow reverses and a step decrease in temperature (to that of the hot leg) of about 100F occurs. As power is increased, the surge flow temperature rises with the hot leg temperature until at the end of the power ramp the temperature is only about 40F below the pressurizer equilibrium fluid temperature. At this point, the surge flow reverses to accommodate the continuous spray and a step increase in surge flow temperature of 40F occurs.

A statement to the effect that the surge flow temperature undergoes a step decrease of 110F and, after the establishment of equilibrium conditions, a step increase of 110F will conservatively represent this transient. The representation of the transient as a complete stress reversal is more conservative than the time dependent curves supplied previously. The assumption of a constant heat transfer coefficient will eliminate the necessity to define the surge flow rates. This assumption is made for all the surge nozzle transients. The maximum surge flow during plant loading is about 30 lbm/sec (Reference A).

The spray flow during plant loading (Reference B) increases from the continuous spray rate of 1.5 gpm to about 100 gpm and then returns to 1.5 gpm when equilibrium conditions are reached. At the continuous spray flow rate, it is estimated that a 55F fluid temperature drop exists between the loop cold leg and the pressurizer spray nozzle. Upon initiating

proportional spray, it is conservatively assumed that this temperature drop is eliminated. The spray flow temperature transient then consists of a 55F step increase followed by the change in the loop cold leg temperature during the transient. The latter is generally of the order of 10F or less. Upon termination of proportional spray, a 55F step decrease in spray fluid temperature is assumed.

It is decided that a statement to the effect that the spray flow temperature undergoes a step increase of 110F and after the establishment of equilibrium conditions a step decrease of 110F will conservatively represent this transient. The temperature range is expanded to 110F to eliminate any differences from plant-to-plant since the Architect-Engineer typically supplies the spray piping and its associated insulation. Accompanying the temperature step, the spray flow is assumed to step from the initial value of 1.5 gpm (continuous spray) to the maximum proportional spray flow of (375 gpm). This maximizes the film heat transfer coefficient.

b. Unloading

During plant unloading, the surge flow temperature transient is similar except that in addition to the 100F step there is an additional 42F step (Reference A). The proportional spray is not activated during plant unloading. The same logic outlined above is used to specify for the unloading transient an additional 15,000 cycles of 110F step change (complete reversal) and 15,000 cycles of 60F step change (complete reversal) in surge flow temperature. There is no spray flow transient for plant unloading.

c. Step Power Changes

A similar approach is taken for the power step transients. During a step load increase there are two surge flow temperature reversals of about 45F. During the step load decrease there is one surge flow temperature reversal of about 42F and two of about 50F. The maximum sustained surge flow during the step power changes is about 50-60 lbm/sec. To the unloading transient an additional 10,000 cycles of 60F step change (complete reversal) in surge flow temperature are added.

The proportional sprays are turned on twice during both the step load increase and the step load decrease transients. To the loading transient an additional 8000 cycles of 110F step change (complete reversal) in spray flow temperature are added. Similarly, maximum spray flow (375 gpm) is assumed to occur during the transients to maximize the film heat transfer coefficient.

d. Plant Trips

During the Reactor Trip, Loss of Primary Flow and Loss of Load transients, there is a brief surge flow reversal toward the pressurizer at time zero which lasts for about 10 seconds. Since the surge line is typically 50 feet in length and the associated pipe velocities are in the 5-10 ft/sec range, the pressurizer surge nozzle will not "feel" this initial flow reversal. For the next 100 seconds, the flow is out of the pressurizer at a temperature which decreases somewhat ($\sim 30F$) due to the decreasing pressurizer saturation temperature. At 100 seconds, there is a surge flow reversal toward the pressurizer as hot leg water enters to restore the equilibrium pressurizer water level. This is accompanied by a characteristic (for the trip cases) 75F step decrease in surge flow temperature. The maximum sustained surge flow during the trip cases is in the range of 400-600 lbm/sec. To the loading transient an additional 500 cycles of 110F step change (complete reversal) in surge flow temperature are added.

The proportional sprays are turned on once during both the Loss of Load and Loss of Primary Flow transients. This represents only 80 occurrences but for conservatism an additional total of 500 cycles of 110F step change (complete reversal) in spray flow temperature are added to the loading transient. Maximum spray flow (375 gpm) occurs during these incidents.

e. Loss of Secondary Pressure

During this incident there is a very rapid draining of the pressurizer in 6 seconds during which the surge flow reaches a maximum of a few thousand pounds per second. Thereafter the pressurizer contains steam until the refill transient is initiated at 1550 seconds. Based on Figure 8, a statement to the effect that the surge flow temperature undergoes a step decrease of 250F and, after the establishment of equilibrium conditions, a step increase of 250F will conservatively represent this transient. There is no accompanying spray flow transient.

f. Summary

- It is concluded that a conservative representation for the structural design of the spray nozzle and pressurizer surge nozzle (in addition to vessel heatup/cooldown, normal plant variations, hydrostatic test and leak test) is the following:

<u>Condition</u>	<u>Cycles</u>	<u>Complete Fluid Temperature Reversal</u>	
		Surge Nozzle	Spray Nozzle
(Initial Nozzle Fluid Temperature		653F	450F)
Plant Loading	15,000	110F	110F
Plant Unloading	15,000	110F	-
	15,000	60F	-
Step Power Increase	4,000	60F	110F
Step Power Decrease	6,000	60F	-
	4,000	-	110F
Plant Trips	500	110F	110F
Loss of Secondary Pressure	5	250F	-

To determine film heat transfer coefficients associated with the surge nozzle fluid temperature transients, the accompanying flow transients are required. As shown in Reference A, these are highly non linear and vary considerably in magnitude from case to case. From inspection of these curves in conjunction with the expertise developed from reviewing NCD component analytical stress reports, the following values of constant film coefficients are selected.

The maximum surge flow associated with the 30,500 cycles of the 110F surge nozzle fluid complete temperature reversals occurs during the 500 cycles of plant trips. Based on these flows, a conservative constant film coefficient of 1800 Btu/hr-ft²-°F is selected for the total 30,500 cycles.

The maximum surge flow associated with the 25,000 cycles of the 60F surge nozzle fluid complete temperature reversals occurs during the power steps. Based on these flows, a conservative constant film coefficient of $95 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected for the total 25,000 cycles.

Based on the surge flows during a loss of secondary pressure, a conservative constant film coefficient of $3600 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected for the 5 cycles of the 250F surge nozzle fluid complete temperature reversal.

For the spray nozzle fluid transients, the specification statement includes (in addition to the fluid temperature step change) the step change in spray flow rate. The Vendor is responsible for determining the film coefficient for the 23,500 cycles of 110F spray nozzle fluid complete temperature reversals.

V. Reactor Coolant Pipe & Fittings Specification

This specification is applied to the primary piping (hot leg, cold leg, (including discharge and suction leg) and surge line and nozzle attachments (surge, shutdown cooling, safety injection, charging, letdown, spray, instruments, drains, and sampling).

1. Piping.

Items 1-7 of Section I (Reactor Vessel Specification) are applied to the revision of that portion of the specification concerned with the hot leg and cold leg (including discharge and suction leg). In addition, the following revisions are made to that portion of the specification concerned with the surge line.

For the heatup (cooldown) of the surge line a composite curve is developed from the heatup (cooldown) of the reactor vessel (loop piping end of the surge line) and from the heatup (cooldown) of the pressurizer (pressurizer end of the surge line). The revised pressure/temperature curves for surge line heatup cooldown are attached as Figure 9. During both the heatup and cooldown operations there is a net flow out of the pressurizer. The maximum flow rate is about 12 lbm/sec.

For Plant Loading (unloading), Step Power Increase (decrease), and Plant Trips, the pressurizer specification section concerning the pressurizer surge nozzle (Item 7.f of Section IV) is applied directly to the surge line.

The Normal Pressurizer Variations of ± 100 psi, ± 20 F (Item 2 of Section IV) are applied to the surge line.

For the Loss of Secondary Pressure, the pressurizer specification curve (Item 4 of Section IV) is applied directly to the surge line.

For the Hydrostatic Test and Leak Test, the reactor vessel specification paragraphs (Items 6, 7 of Section I) are applied directly to the surge line.

The NRC is requiring annual testing of the safety injection system. Since the low pressure system is used during plant cooldown, operation of this system is normally annual and is defined in the specification. The high pressure system is not used during normal plant operation and an annual test is now defined. With the pressurizer pressure at 1000 psia (545F) and the loop fluid temperature at 295F, high pressure safety injection flow is initiated. Since this flow exceeds the letdown system capability, flow from the loop to the pressurizer occurs. High pressure safety injection flow is also initiated at two lower pressurizer pressures with the loop fluid temperature held constant at 295F. Based on a maximum flow of 500 gpm, a conservative constant film coefficient of 250 Btu/hr-ft²-°F is selected for the surge line.

For conservatism, the specification considers the entire 120 occurrences as taking place at the maximum loop-to-pressurizer differential temperature of 250F.

2. Nozzles

For the nozzles which only permit flow from the primary loop piping (shutdown cooling, letdown, spray, instruments, drains, sampling), Items 1-7 of Section I (Reactor Vessel Specification) are applied consistent with the nozzle location on the primary piping. No additional special transients are developed. For the nozzles which permit flow to the primary loop piping (surge, safety injection, charging), the following is considered.

3. Surge Nozzle

The surge nozzle attached to the primary loop piping is assigned the same transient description as the surge line in the specification.

4. Safety Injection Nozzles

Items 1-7 of Section I (Reactor Vessel Specification) are applied to the safety injection nozzles consistent with the nozzle location on the primary loop piping. The following modifications to these transients are added.

a. Plant Cooldown

During plant cooldown when the primary loop temperature is at a maximum of 350F (300 psia), flow through the safety injection nozzles into the primary loop, and flow through the shutdown cooling nozzles out of the primary loop is initiated. This flow is recycled to heat the shutdown cooling heat exchangers from the containment temperature (maximum 120F) to 350F in a minimum 15 minute period. Once the heat exchangers are warmed up, the cooldown of the primary loop is continued. The fluid temperature passing through the safety injection nozzles decreases in an exponential manner from 350F to 70F in a 24 hour period.

This transient is conservatively described in the specification as follows. The fluid in the safety injection nozzles undergoes a step decrease in temperature from 350F to 40F for a period of 15 minutes, followed by a step increase to 350F followed by a ramp decrease at 100F/hr to 70F.

For conservatism, the temperature of the source (refueling water tank) of the shutdown cooling flow is selected (40F) rather than the containment temperature for the safety injection nozzle fluid temperature.

Based on a maximum flow of 10,000 gpm, a conservative constant film coefficient of $2770 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected for the safety injection nozzles.

b. Emergency Conditions

A total of seven occurrences are provided to accommodate the Design Basis Accident (1 occurrence), Loss of Secondary Pressure (5 occurrences) and the testing of the safety injection system at full temperature (1 occurrence). The transient is defined as a step change in the nozzle fluid temperature from 565F to 40F (1240 psia). The nozzle fluid temperature remains at 40F. Based on a maximum flow of 10,000 gpm a conservative constant film coefficient of $2770 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected for the safety injection nozzles.

c. Testing of Safety Injection System

As noted under the surge line section, an annual testing of the high pressure safety injection system is defined. For the safety injection nozzles, this test is conservatively defined as 120 occurrences of a step change in the nozzle fluid temperature from 565F to 40F. Based on a maximum flow of 500 gpm, a conservative constant film coefficient of $250 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected.

5. Charging Nozzles

There is continuous injection of 400F water at 32 gpm per nozzle into the primary cold leg which is operating at a T cold equivalent to 100 percent power and 2250 psia.

a. Heatup/Cooldown

During plant heatup, the charging water fluid temperature increases linearly from 70F to 400F over a 4.8 hour period. This time period is consistent with the 100F/hr heatup of the primary loop. The maximum charging flow is 44 gpm.

During plant cooldown, the charging water fluid temperature experiences a step decrease from 400F to 200F followed by a linear ramp to 70F over a 4.8 hour period. This time period is consistent with the 100F/hr cooldown of the primary loop. The maximum charging flow is 132 gpm. Based upon this flow rate, a conservative constant film coefficient of $2400 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$ is selected for both the heatup and cooldown operations.

b. Loading/Unloading

Inspection of the transient curves of Reference C shows that during plant loading the charging water fluid temperature increases about 80F in a gradual manner over 1000 seconds prior to a gradual return to the equilibrium set point. The transient is defined as a 100F step increase from 400F in the charging fluid temperature and, after the establishment of equilibrium conditions, a 100F step decrease to 400F. The maximum charging flow is 44 gpm. A conservative constant film coefficient of 900 Btu/hr-ft²-°F is selected.

Inspection of the transient curves of Reference C shows that during plant unloading the charging water fluid temperature decreases (in two steps) about 190F in 500 seconds followed (after 500 seconds) by a similar return to the equilibrium set point. The transient is defined as a 200F step decrease from 400F in the charging fluid temperature and, after the establishment of equilibrium conditions, a 200F step increase to 400F. The maximum charging flow is 132 gpm. A conservative constant film coefficient of 2400 Btu/hr-ft²-°F is selected.

c. Step Power Changes

Inspection of the transient curves of Reference C shows that during a step load increase the charging fluid temperature increases about 100F over 100 seconds followed by a gradual return to the equilibrium set point. The transient is defined as a 100F step increase from 400F in the charging fluid temperature and, after the establishment of equilibrium conditions, a 100F step decrease to 400F. The maximum charging flow is 44 gpm. The definition is identical to the loading transient.

Inspection of the transient curves of Reference C shows that during a step load decrease the charging fluid temperature decreases about 200F over 100 seconds followed after 200 seconds by a 100F step increase in fluid temperature and then a gradual return to the equilibrium set point. The transient is defined as a 200F step decrease from 400F in the charging fluid temperature and after the establishment of equilibrium conditions a 200F step increase to 400F. Although the maximum charging flow of 88 gpm is less than that during plant unloading, the step load decrease is defined identically to the unloading transient.

d. Normal Plant Variations

- The normal plant temperature and pressure fluctuations are the same as those appearing in the reactor vessel specification (Item 3 of Section I).

e. Plant Trips

The Reactor Trip, Loss of Load and Loss of Primary Flow transients are considered as a group since the charging flow temperature transients are quite similar. Inspection of the transient curves for the Loss of Load case (the worst of the three cases) of Reference C shows a rapid drop of charging fluid temperature of 258F followed after 800 seconds by a 150F step increase in fluid temperature and then a gradual return to the equilibrium set point. The transient is defined as a 260F step decrease from 400F in the charging fluid temperature and after the establishment of equilibrium conditions a 260F step increase to 400F. The maximum charging flow is 132 gpm. A conservative constant film coefficient of 2400 Btu/hr-ft²-°F is selected.

f. Loss of Secondary Pressure

After an inspection of the transient curves of Reference C, the transient is defined as a 280F step decrease from 400F in the charging fluid temperature and after the establishment of equilibrium conditions a 280F step increase to 400F. The maximum charging flow is 132 gpm. A conservative constant film coefficient of 2400 Btu/hr-ft²-°F is selected.

g. Hydrostatic Test/Plant Leak Test

For the Hydrostatic Test and Plant Leak Test, the reactor vessel specification paragraphs (Items 6, 7 of Section I) are applied to the charging nozzles.

h. CVCS Transients

(1) Purification

Inspection of the transient curves of Reference C shows a rapid drop of charging fluid temperature of 85F followed after a long period of time by a similar return to the equilibrium set point. The transient is defined as a 100F step decrease from 400F in the charging fluid temperature and after the establishment of equilibrium conditions a 100F step increase to 400F. The maximum charging flow is 132 gpm. A conservative constant film coefficient of 2400 Btu/hr-ft²-°F is selected.

(2) Low Volume Control Tank

Inspection of the transient curves of Reference C shows a 35F change in charging fluid temperature. Since this is very mild, this transient is eliminated from the specification.

(3) Boric Acid Dilution

Inspection of the transient curves of Reference C shows this transient to be very similar to the purification transient and hence receives the same description. A total of 15,000 occurrences is assigned which assumes daily operation for primary loop chemistry/crud control and/or load following maneuvers.

(4) Loss of Charging/RHX Isolation Long Term & Short Term

Inspection of the transient curves of Reference C shows that the transient for the RHX isolation-short term is less severe than that for the RHX isolation-long term. The former transient loses its separate identity and is included in the latter transient. Moreover it is seen that the Loss of Charging Flow and RHX Isolation - Long Term are identical with regards to the thermal transient imposed on the charging nozzle. Hence, the three transients are represented by a single transient. The total number of cycles for these three transients in the old specification is 1400. This is excessive since the transient covers equipment failures in the charging system and is not part of normal plant operations. The number of occurrences is revised to 100.

Previously, NCD could not comply with the stress intensity limits in the charging nozzle for the Loss of Charging transient as represented in past specifications. Based on Reference E, this transient is defined as follows. From an initial temperature of 400F and a flow rate of 44 gpm, the charging flow stops. The water temperature in the nozzle, as a function of time, is determined from the heat input from the loop water and nozzle metal by the designer. After equilibrium temperatures are reached, the charging flow is re-established at 44 gpm and 120F for a period of 60 seconds followed by a 30 second ramp increase in temperature to 400F. The designer determines the film heat transfer coefficient. The nozzle design must accommodate this transient since this definition is final.

(5) Loss of Letdown

Previously, NCD could not comply with the stress intensity limits in the charging nozzle for the Loss of Letdown transient as represented in past specifications. Based on Reference E, this transient is defined as follows. From an initial temperature of 400F and a flow rate of 400 gpm, the charging fluid temperature decreases linearly to 120F in 60 seconds. After thermal equilibrium in the nozzle is established, the charging flow stops. After equilibrium temperatures are reached, the charging flow is re-established at 44 gpm and 120F for a period of 60 seconds followed by a 30 second ramp increase in temperature to 400F. The designer determines the film heat transfer coefficient. The nozzle design must accommodate this transient since this definition is final. The number of occurrences is 100.

(6) Summary

It is concluded that a conservative representation for the structural design of the charging nozzles (in addition to loop heatup/cooldown, normal plant variations, hydrostatic test, leak test, loss of charging and loss of letdown) is the following:

<u>Condition</u>	<u>Cycles</u>	<u>Complete Fluid Temp. Reversal</u>	<u>Direction of Initial Temp. Change</u>	<u>Film HTC (Btu/hr-ft²-°F)</u>
(initial charging nozzle fluid temperature 400F)				
Plant Loading	15,000	100F	Increase	900
Plant Unloading	15,000	200F	Decrease	2400
Step Power Increase	2,000	100F	Increase	900
Step Power Decrease	2,000	200F	Decrease	2400
Plant Trips	500	260F	Decrease	2400
Loss of Secondary Pressure	5	280F	Decrease	2400
Purification/Boric Acid Dilution	15,000	100F	Decrease	2400

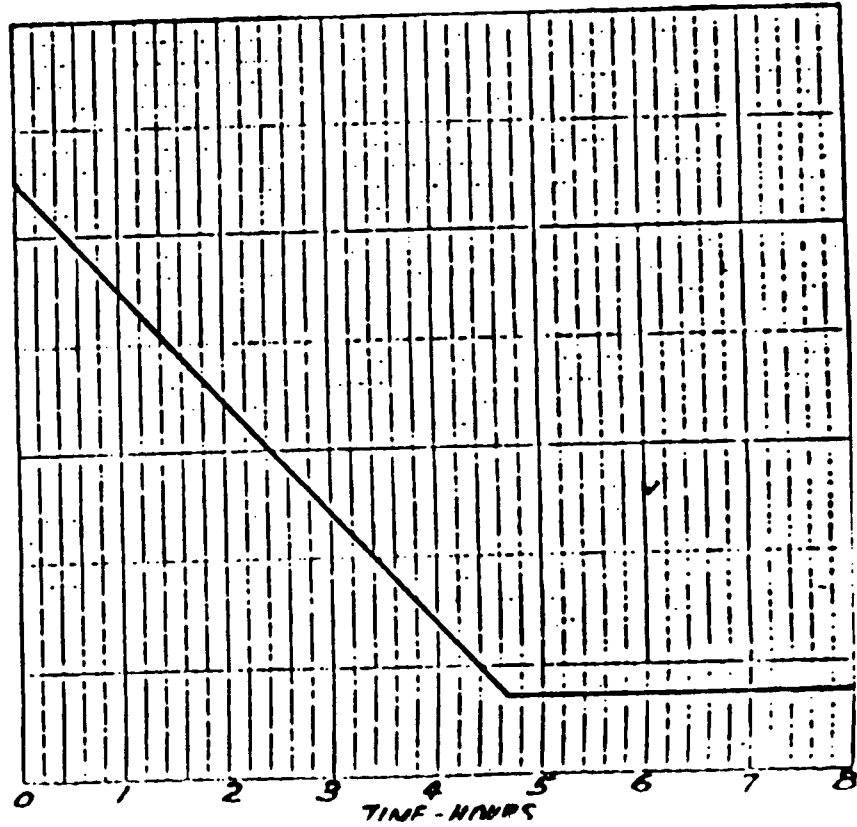
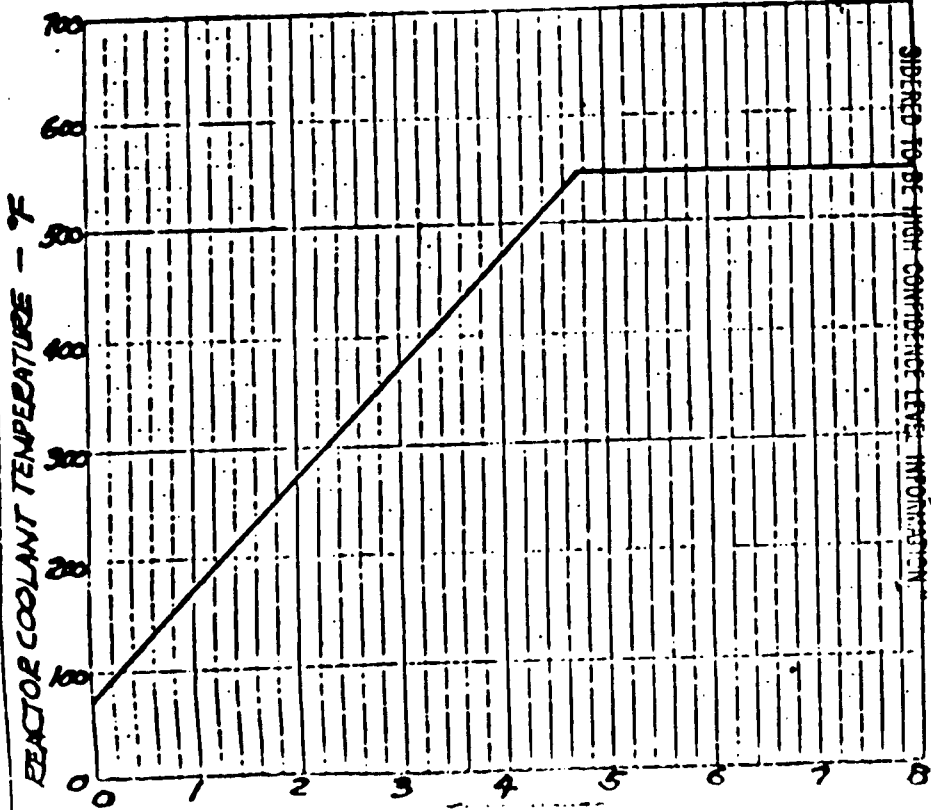
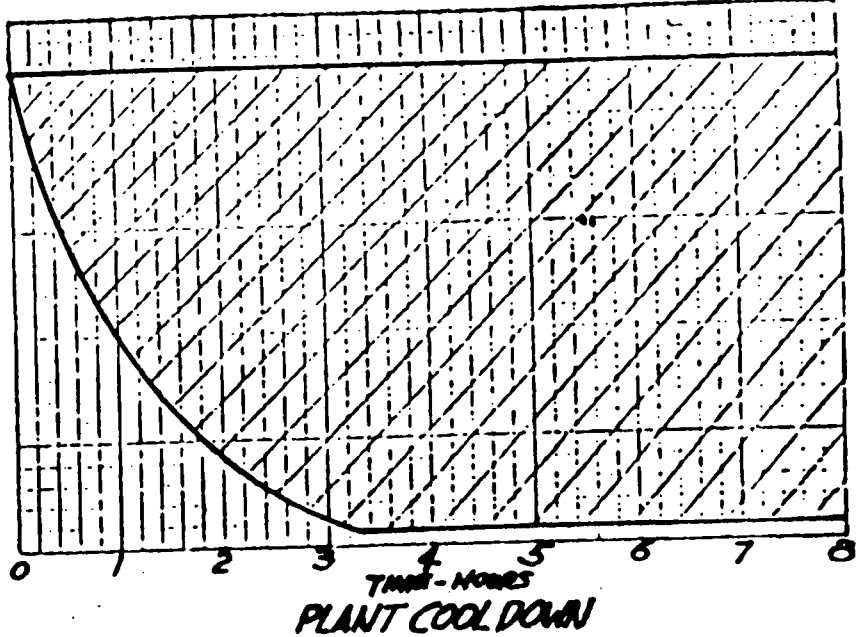
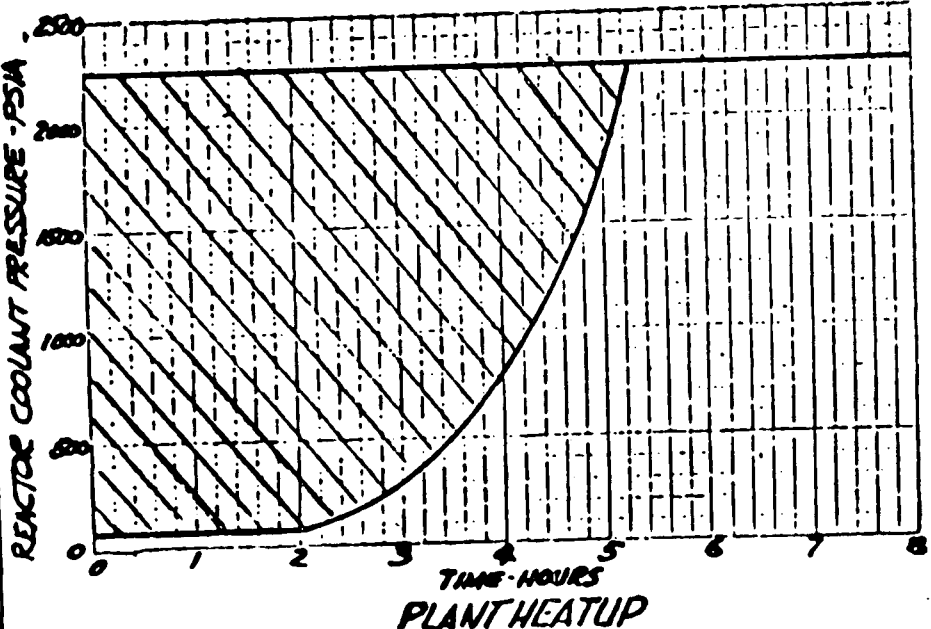
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FIGURE - 5000

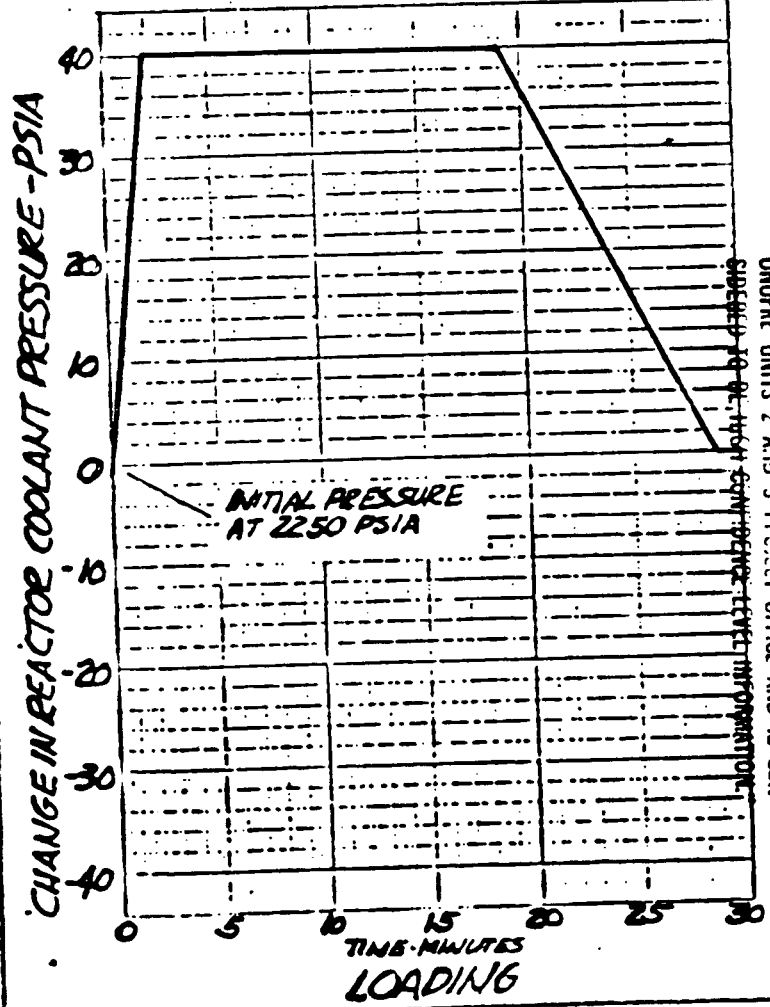
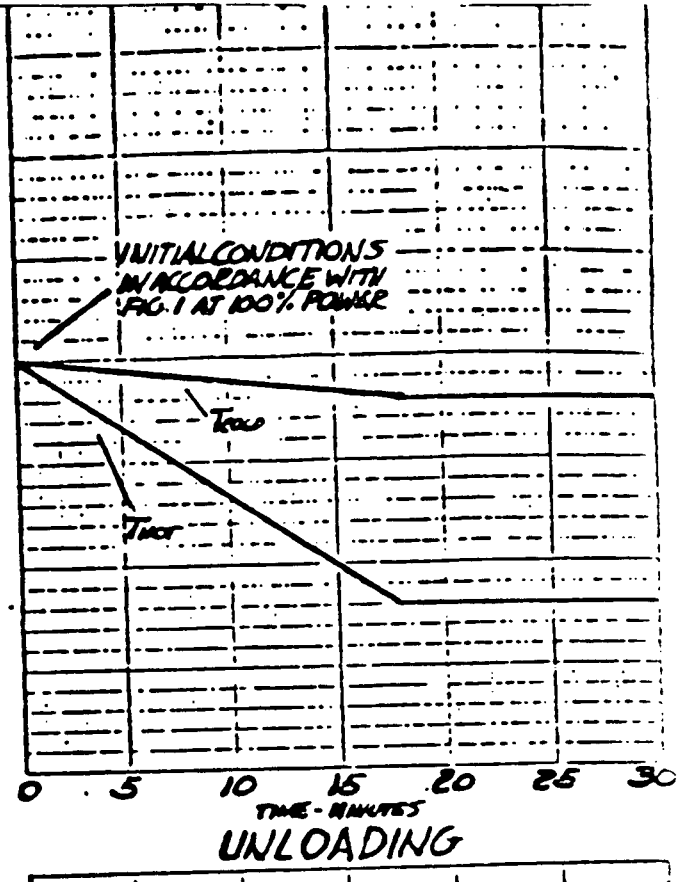
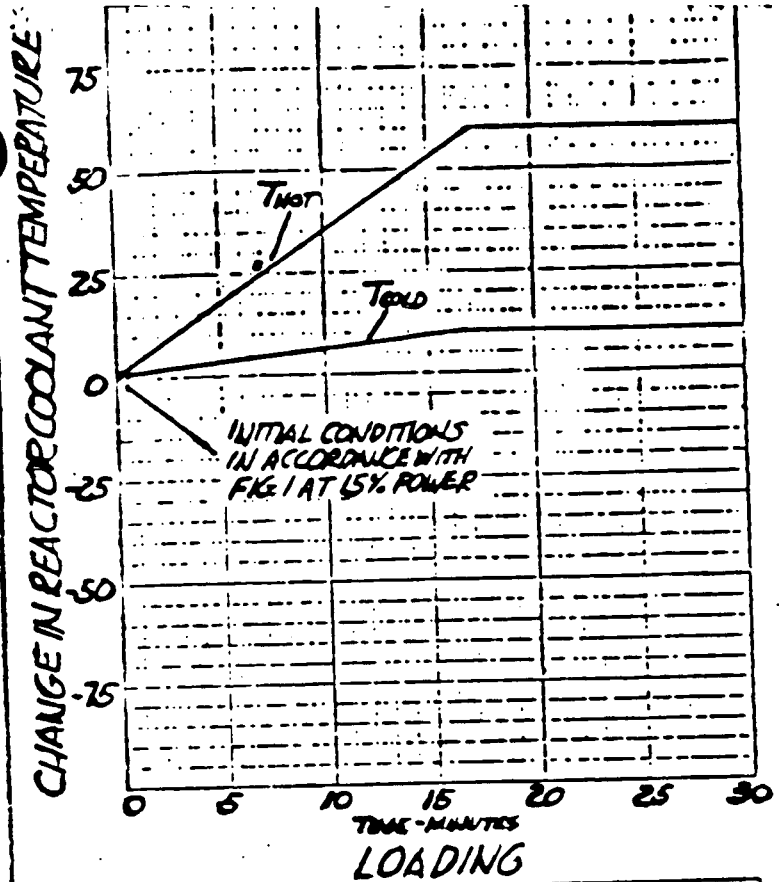
PLANT HEATUP & COOLDOWN

TITLE:



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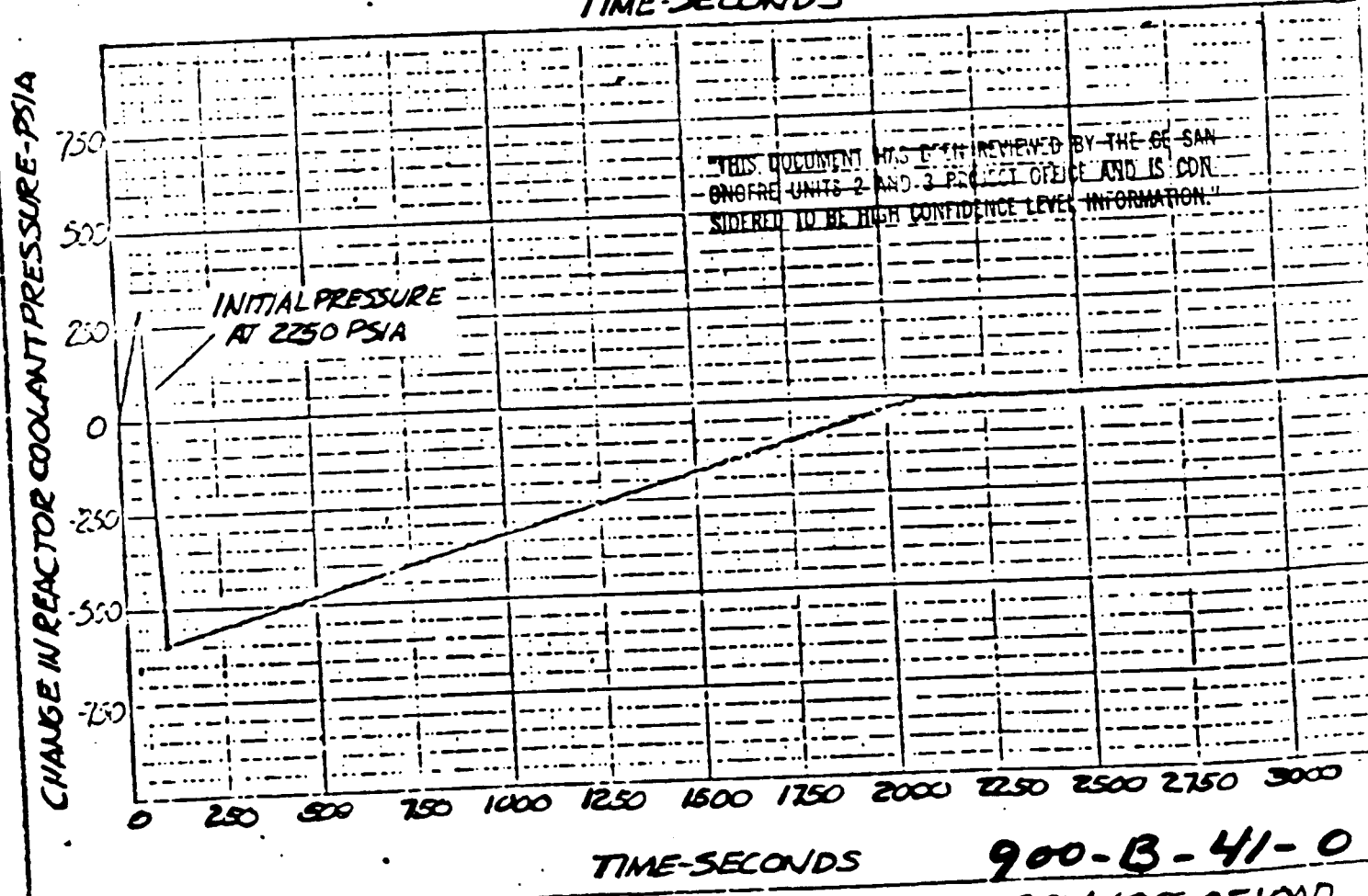
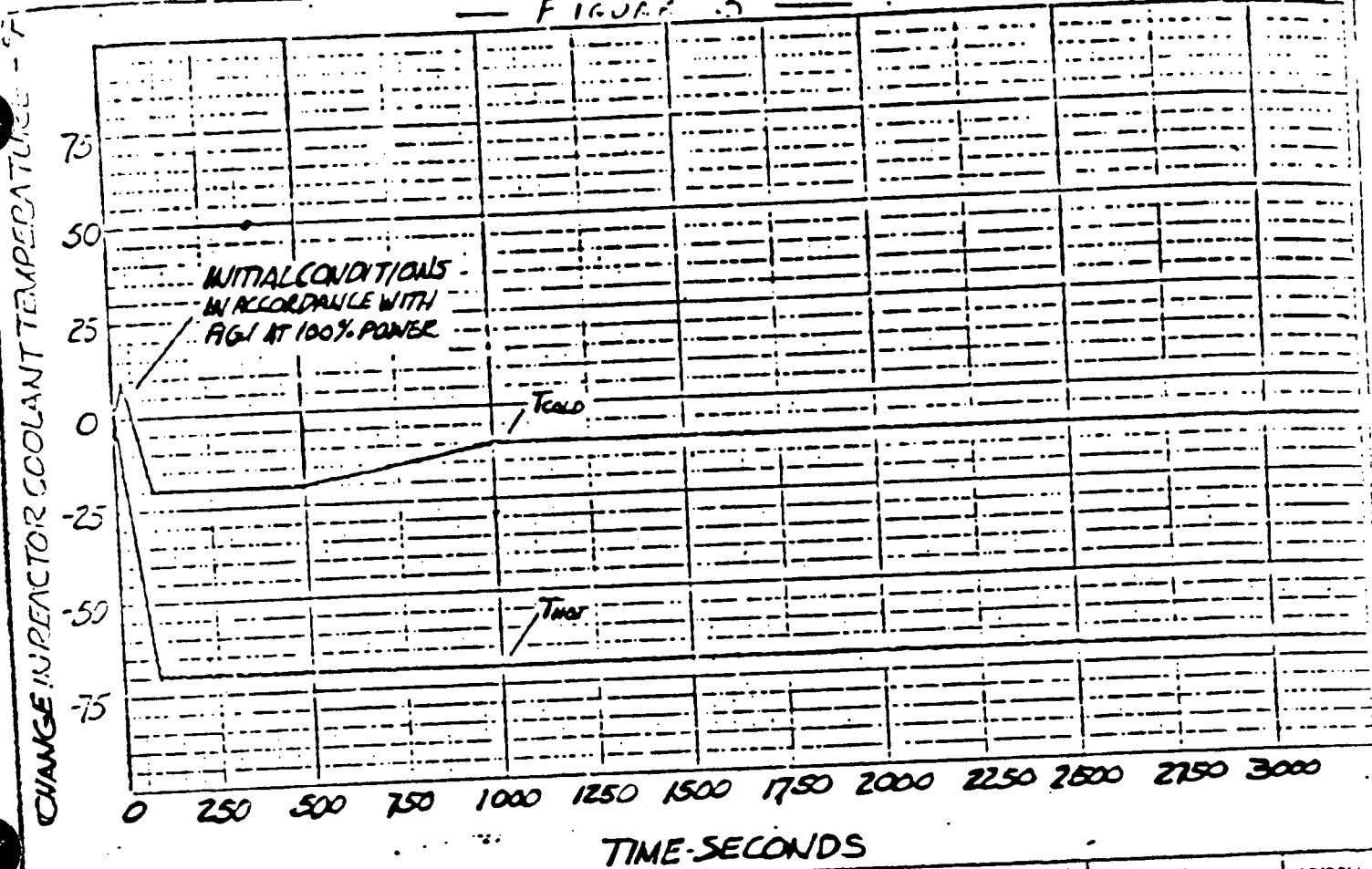
900-130-41-0



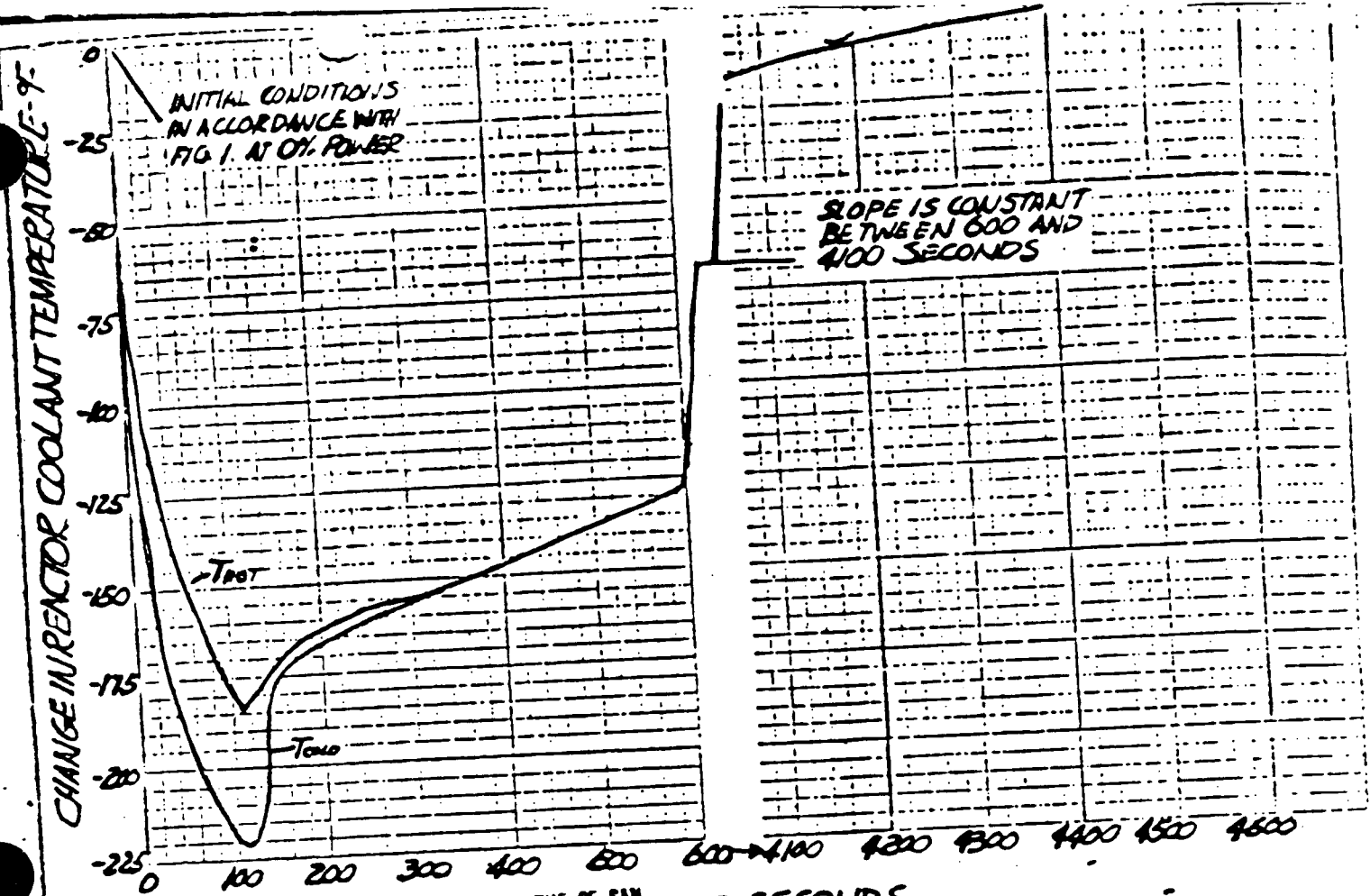
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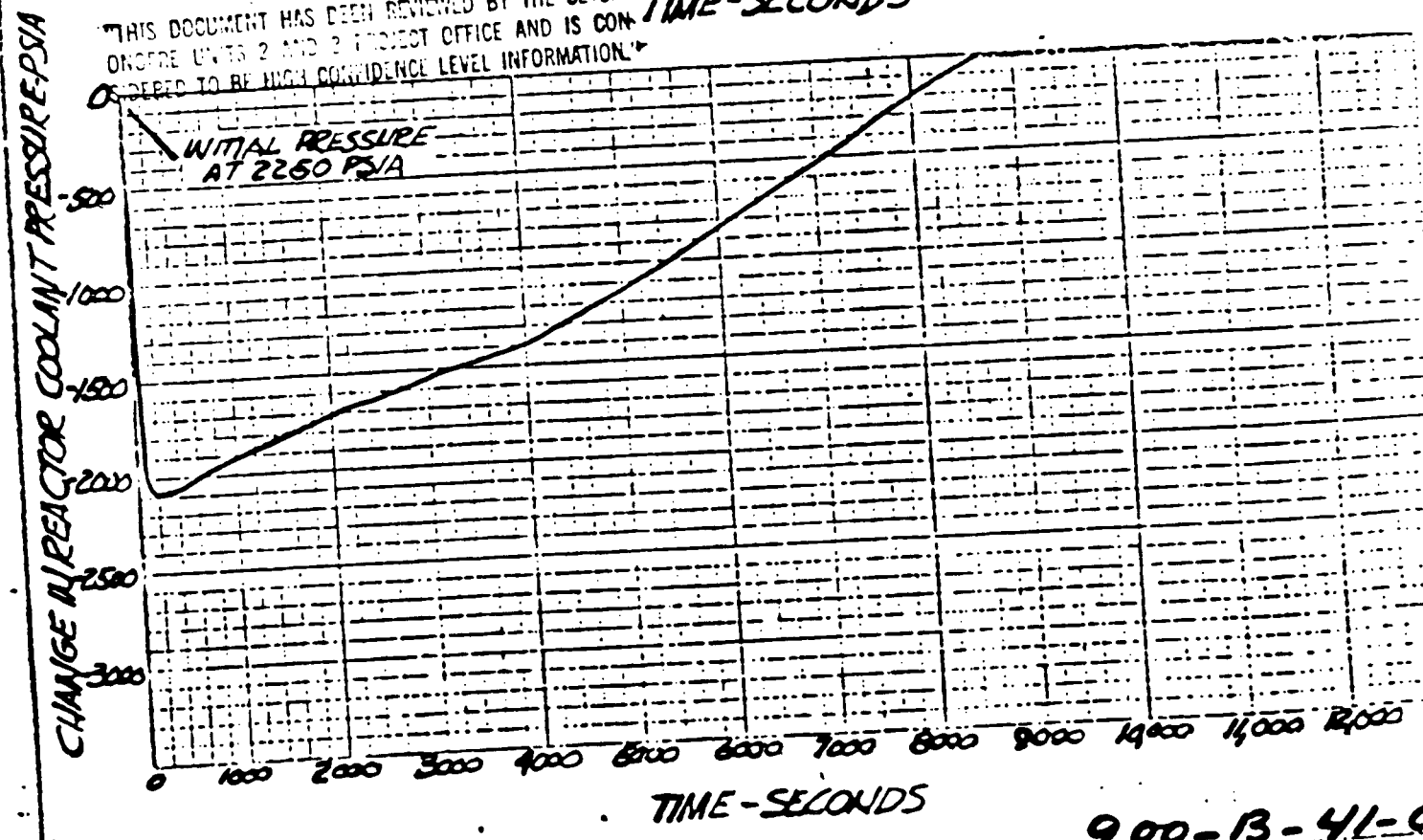
FIGURE 3



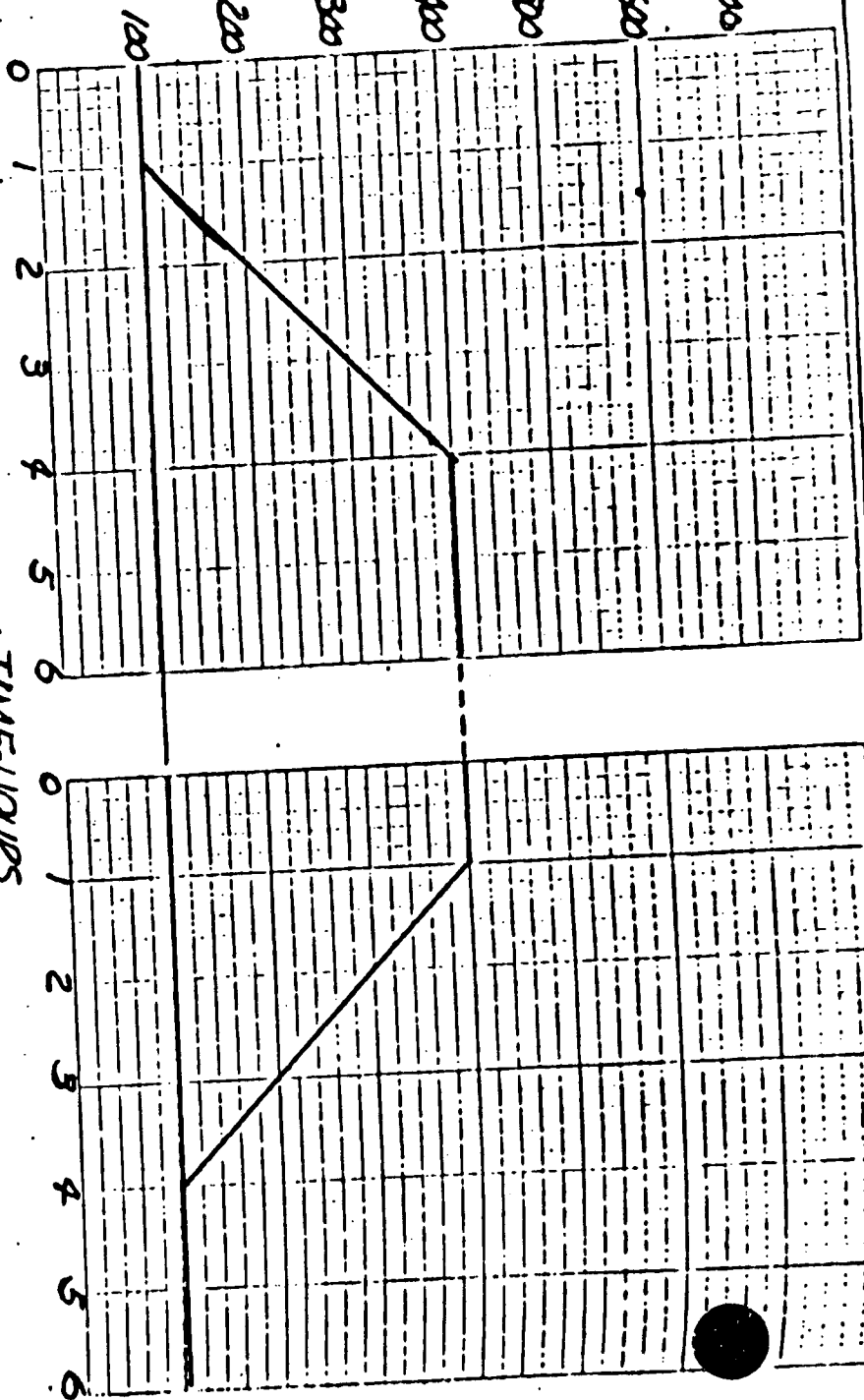
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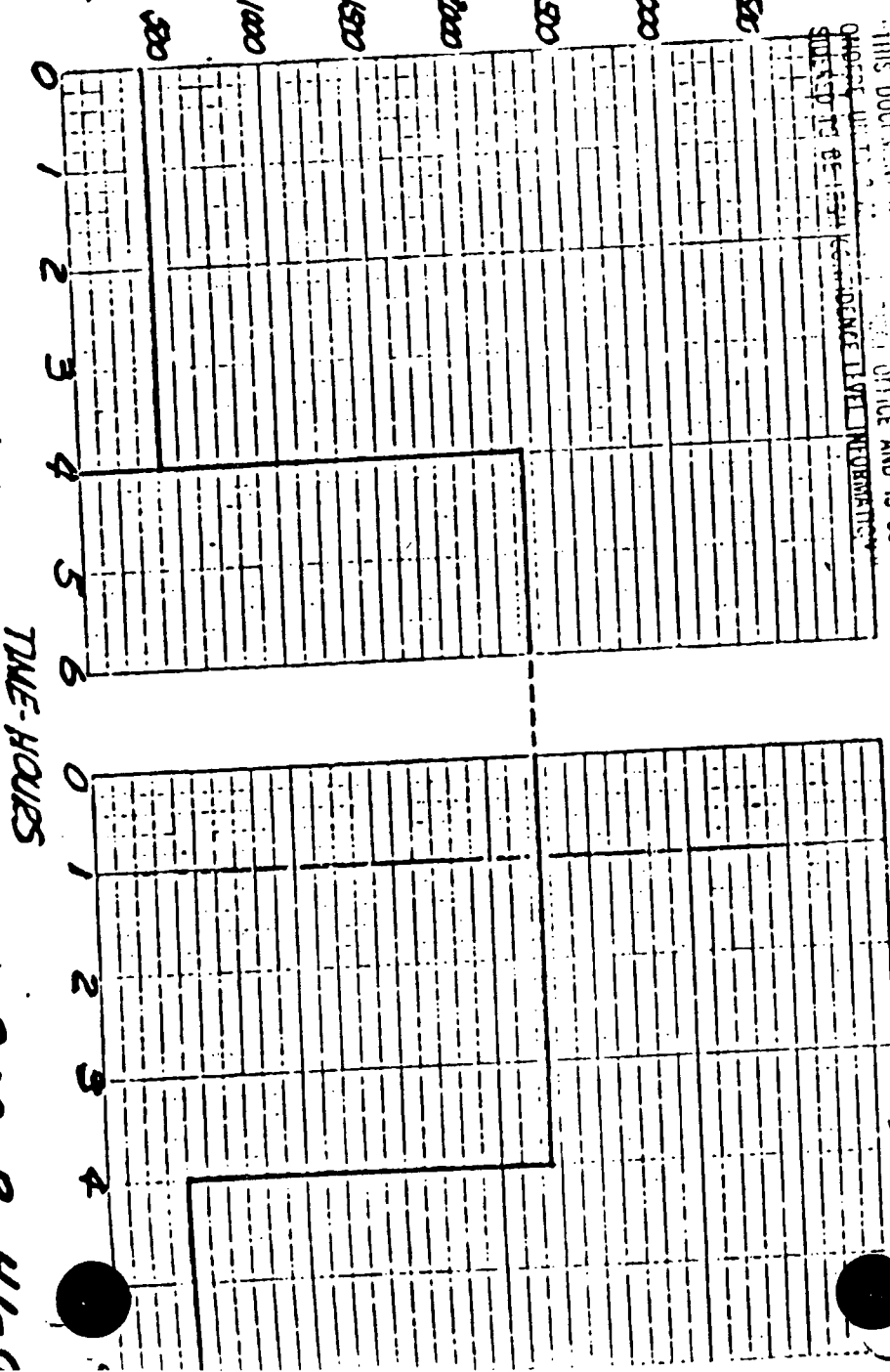
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REACTOR COOLANT TEMPERATURE °F



REACTOR COOLANT PRESSURE - PSIA



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TIME-HOURS

TIME-HOURS

PLANT LEAK TEST

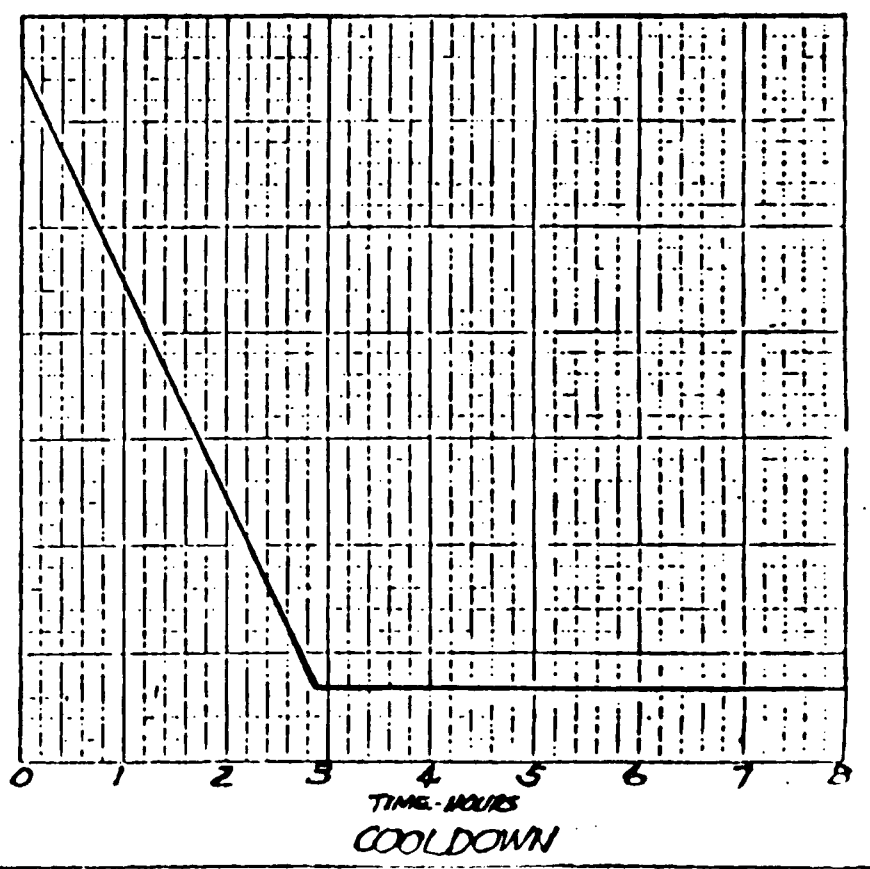
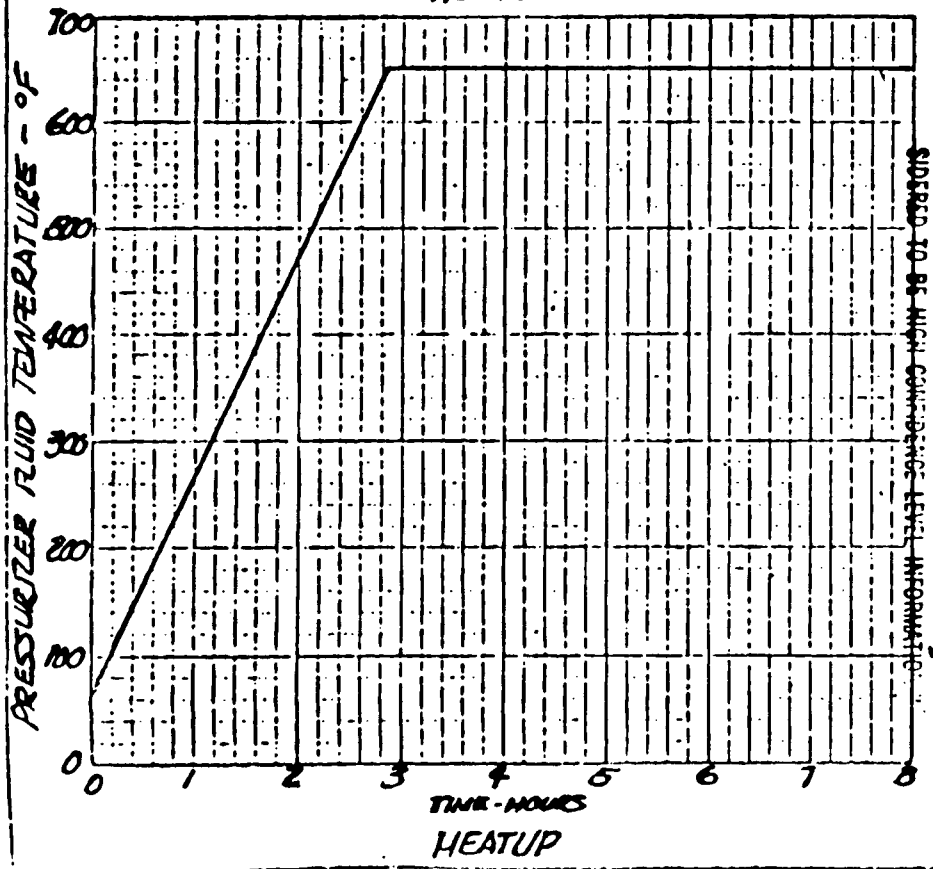
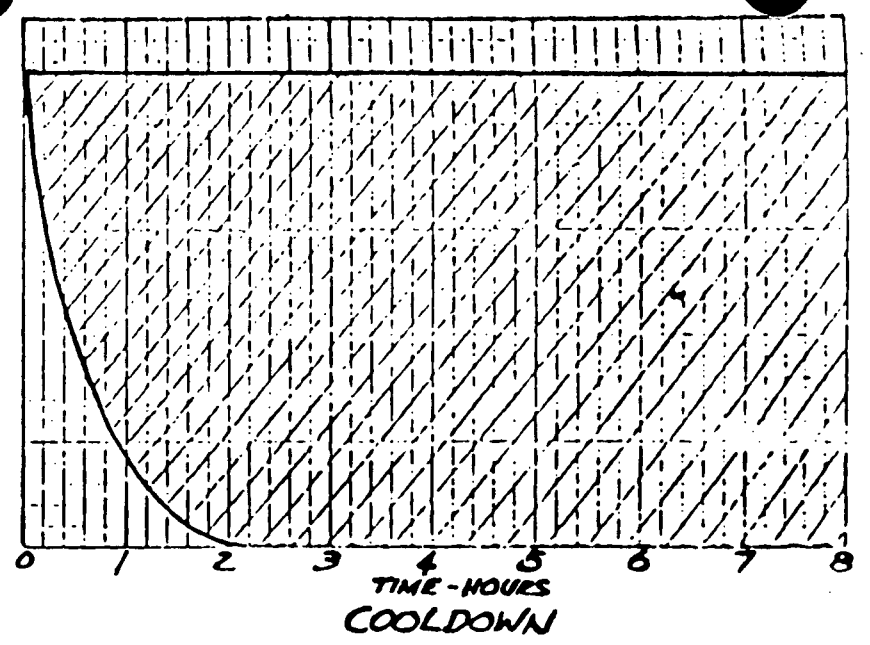
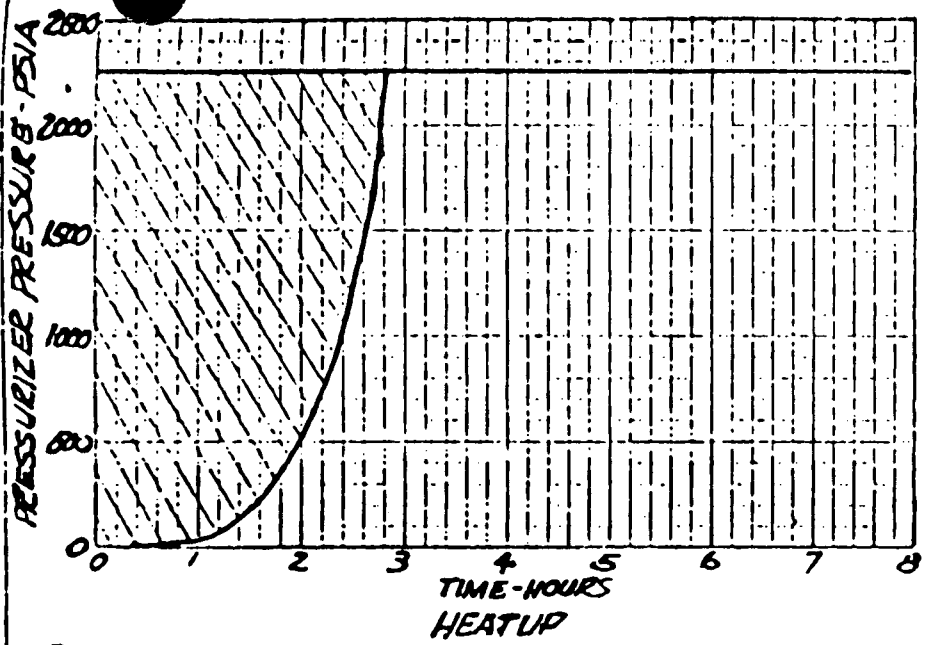
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PLANT LEAK TEST

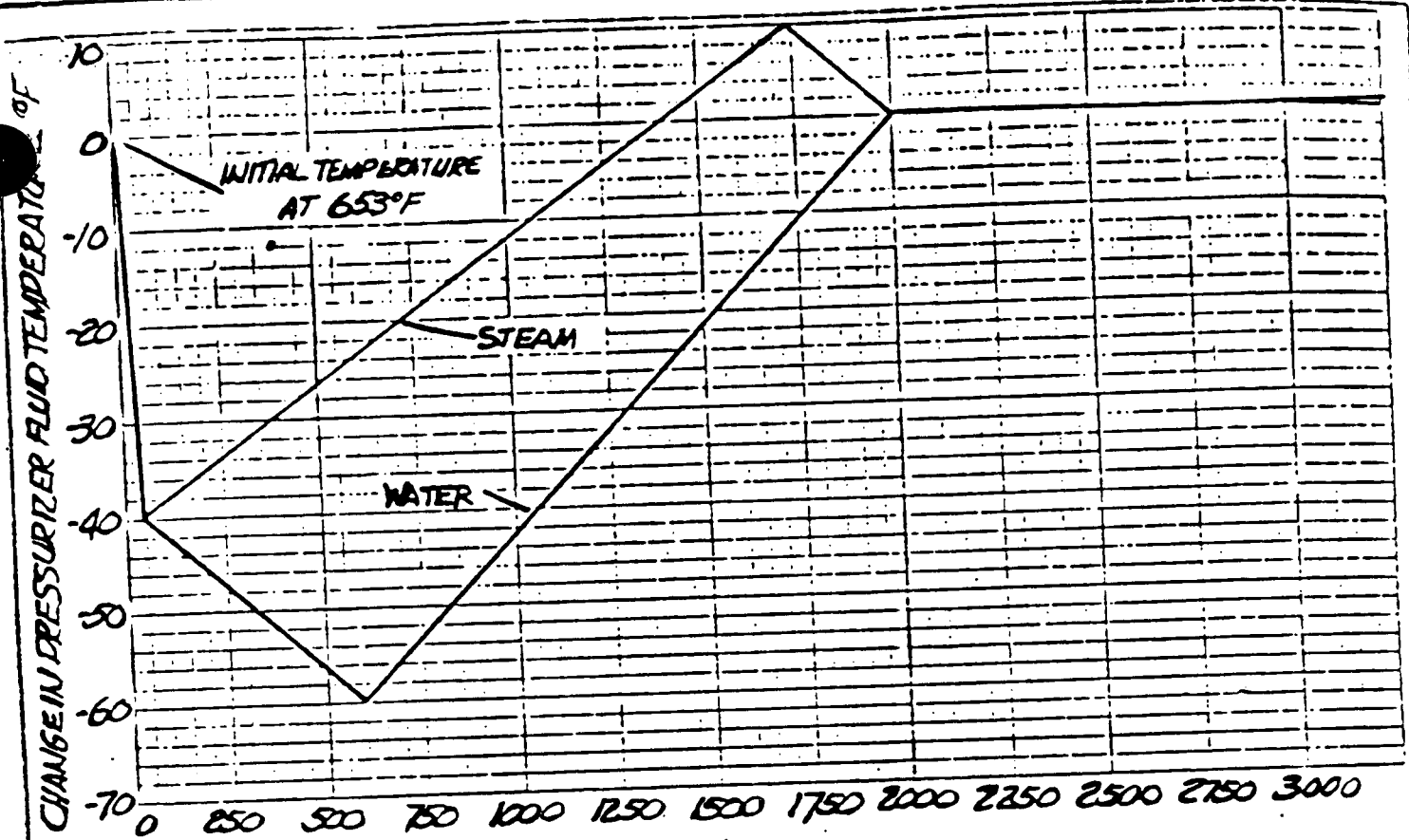
Figure

PRESSURIZER HEATUP & COOLDOWN 900-B-41-0

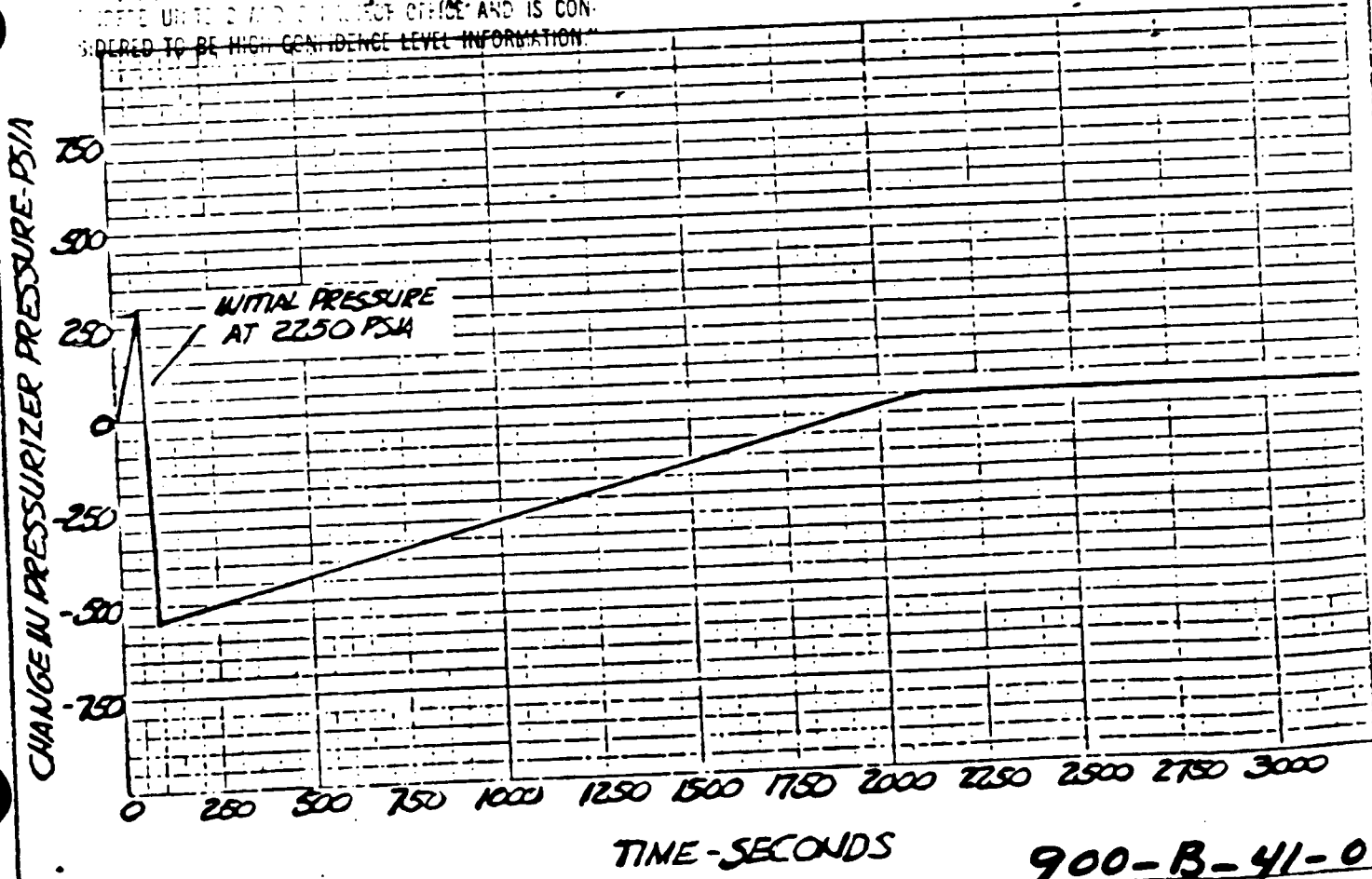


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Figure 6

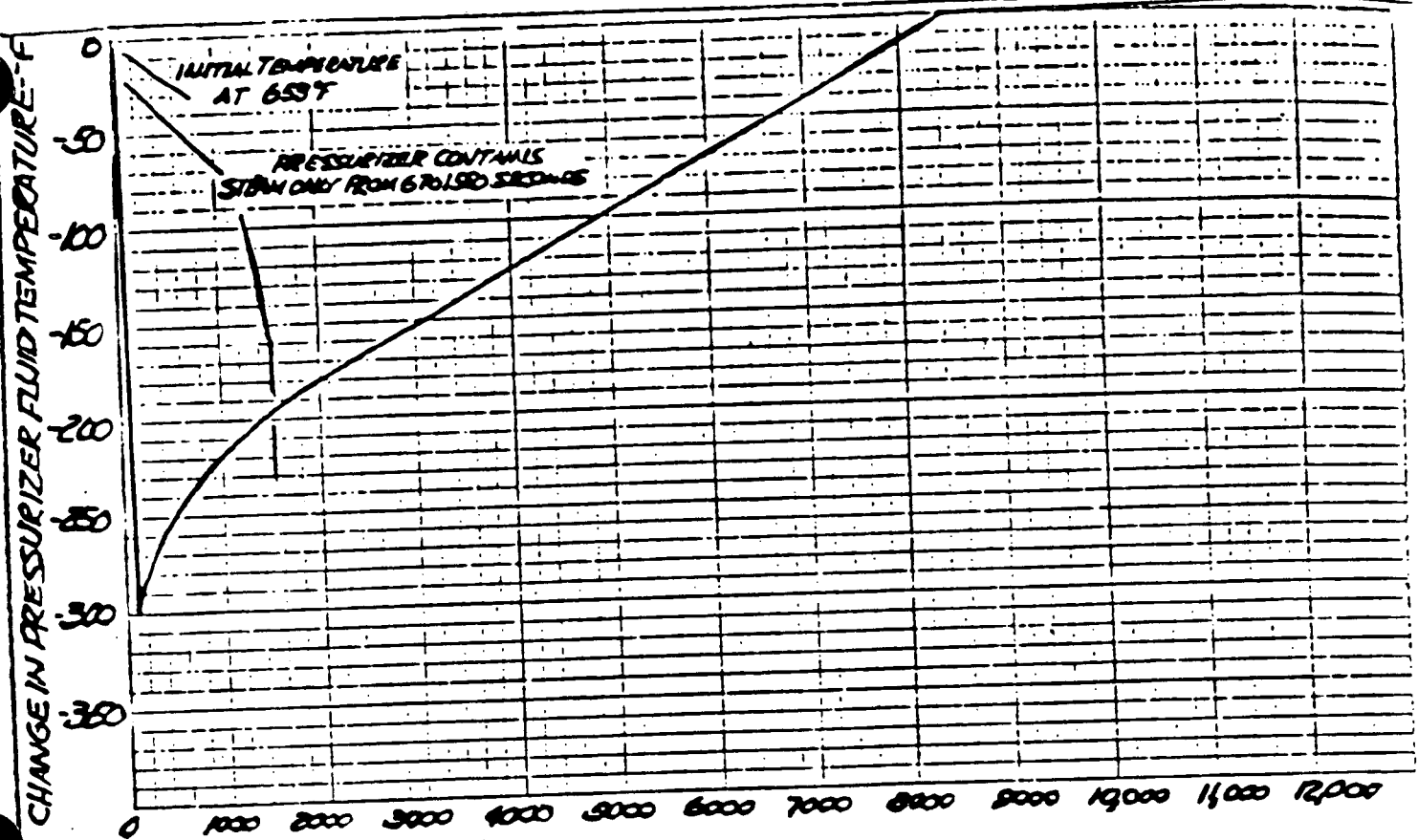


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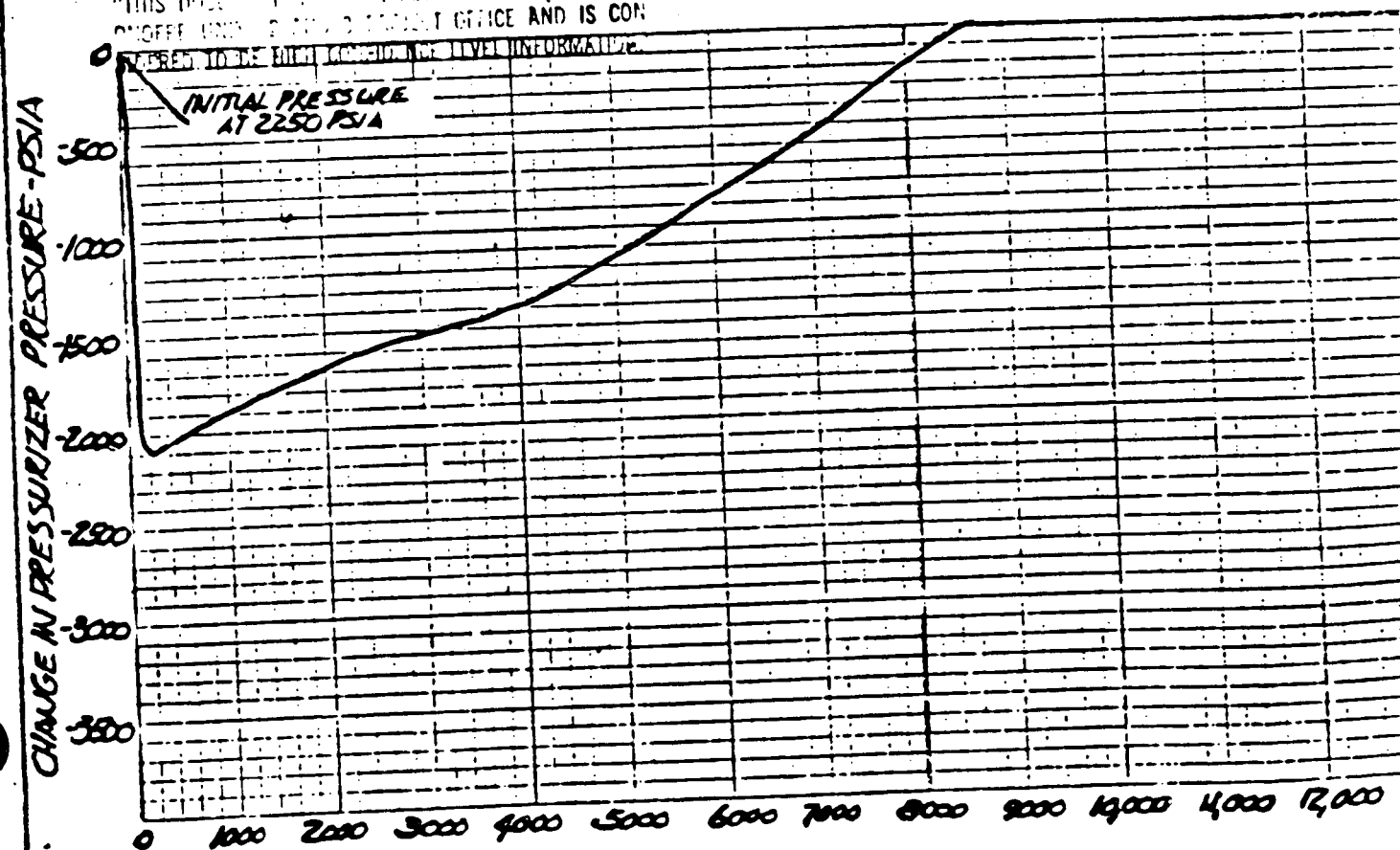


900-B-41-0

— Figure 8 —



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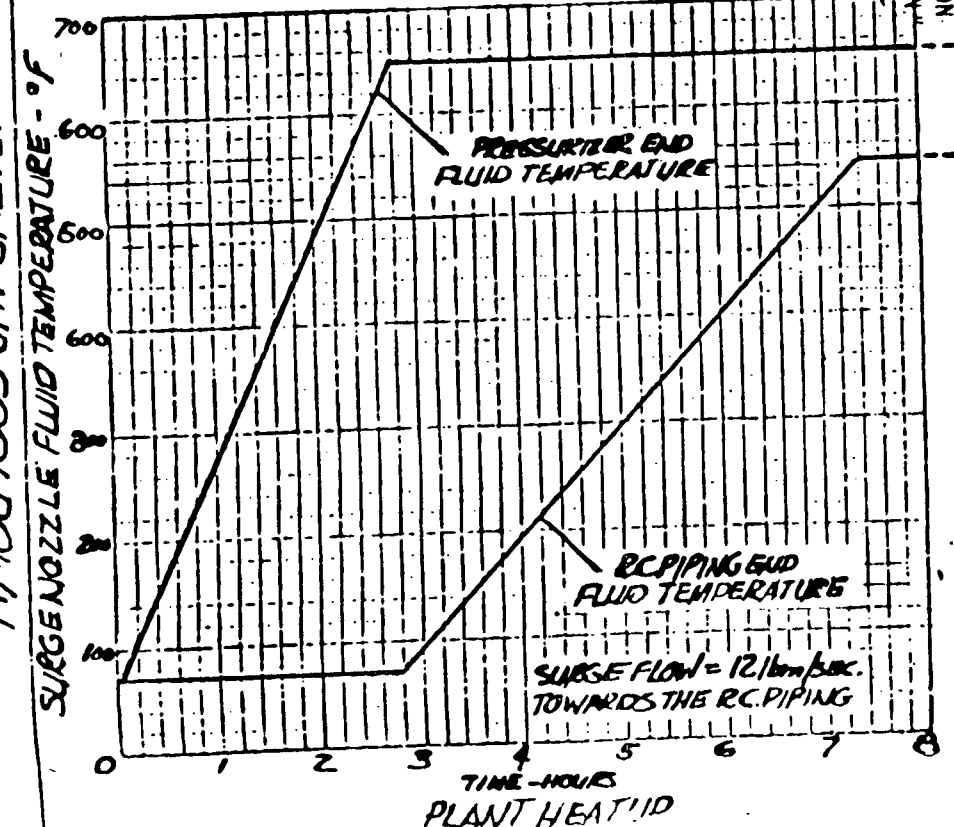
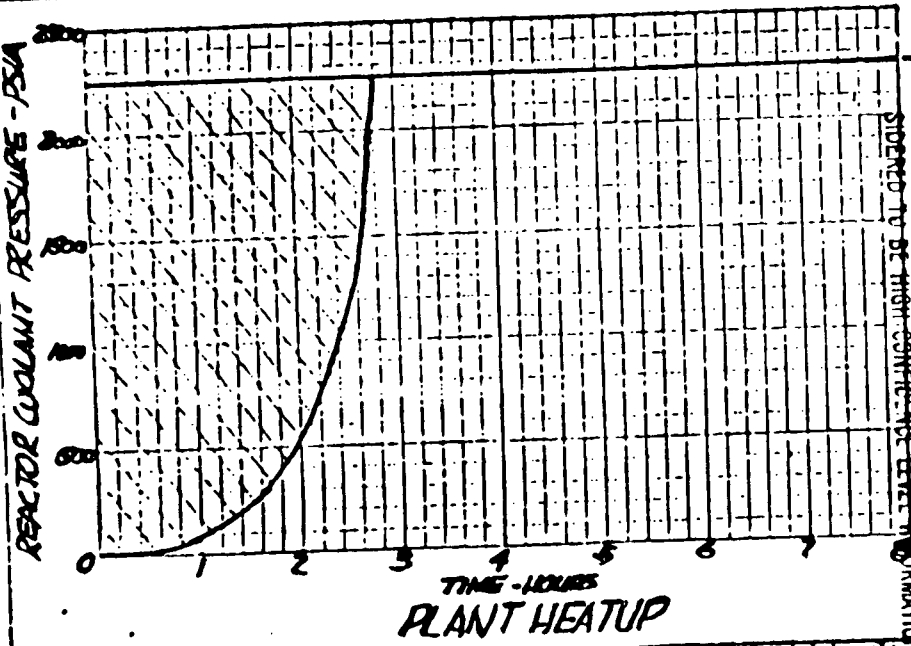


TIME - SECONDS

900-B-41-0

TRANSIENTS - LOSS OF SECONDARY PRESSURE

PROJECT: SURGE LINE TRANSIENT - HEATUP AND COOLDOWN



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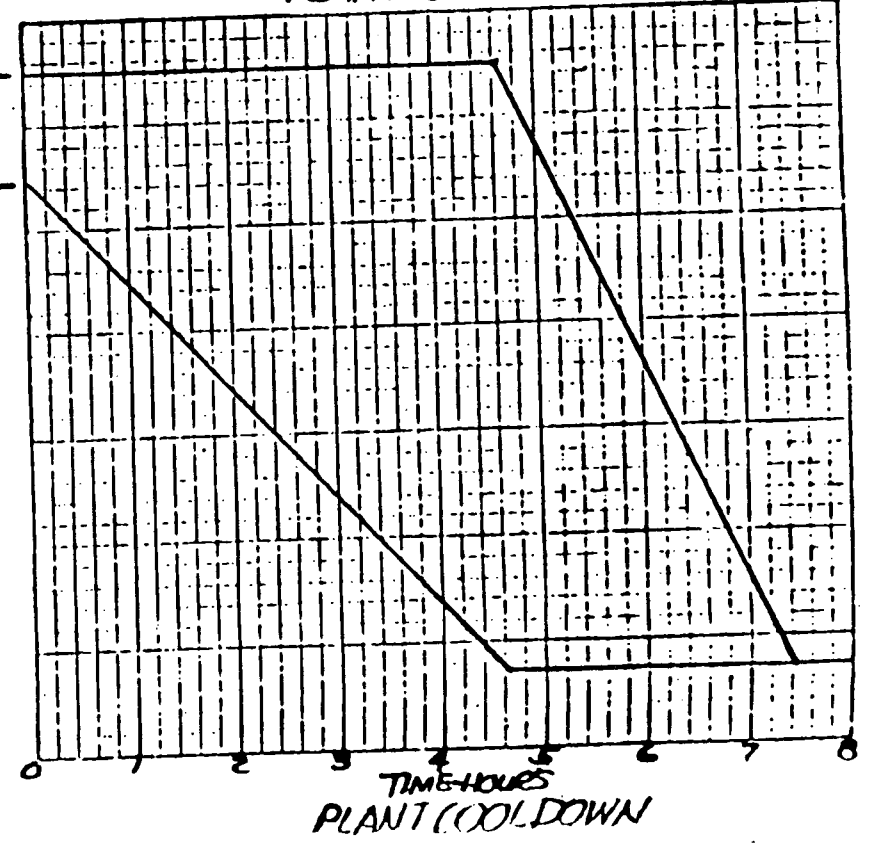
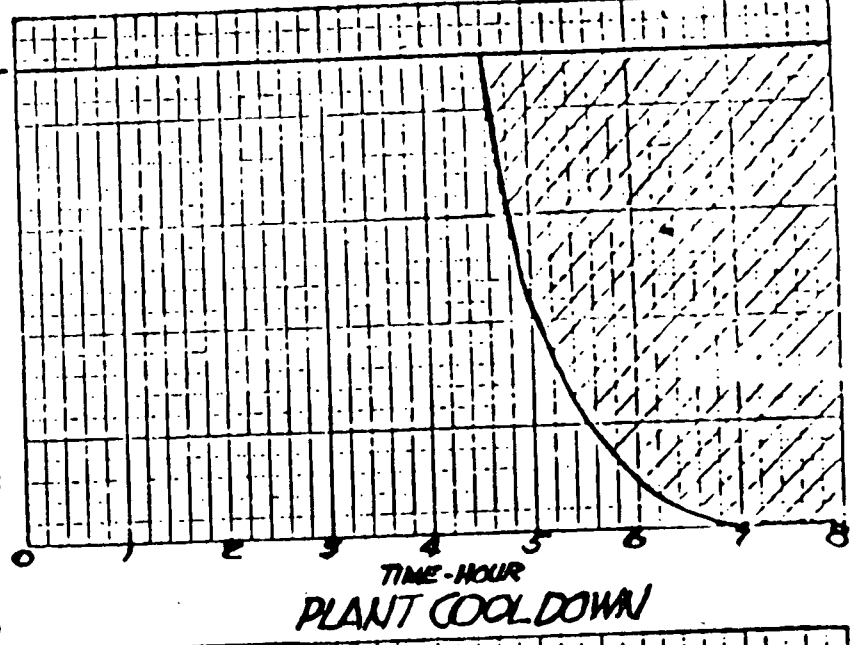



Figure 9 +

Introduction to Transient Curves

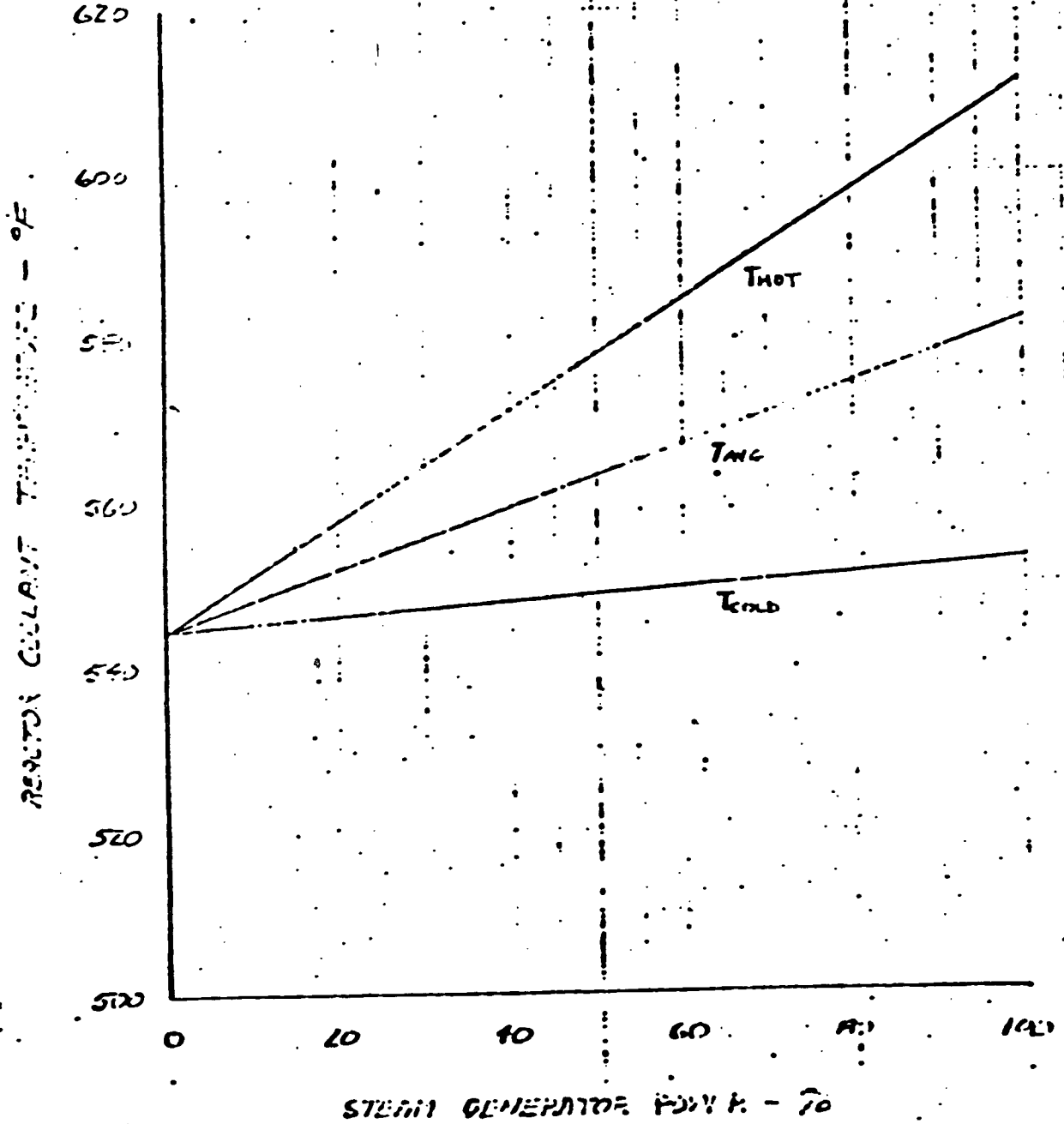
1. All Temperature curves report the change in temperature as a function of time after initiation of transient. The basis for the temperature change is the steady state temperature preceding the initiation of the transient. In all cases the pressurizer steam and water temperatures and the surge line water temperature are 652.8F at time zero. The reactor coolant hot and cold leg temperatures at time zero can be determined from Figure 1 (Reactor Coolant Temperature Versus Power).
2. At time zero the primary system pressure is 2250 psia for all transients. The curves show change in primary pressure as a function of time after the transient has begun.
3. The net surge flow rate has been designated as positive when flow is into the pressurizer.
4. In the Loss of Load Transient the reactor is tripped when primary pressure reaches 2400 psia following the turbine trip. Preceding the transient, the plant is operating at 100 percent power.
5. In the Loss of Flow Transient the reactor is tripped when the vessel coolant flow rate has decreased to 93 percent that of full flow. Preceding the transient, the plant is operating at 100 percent power.
6. The Turbine and Reactor Trip Transient occurs at 100 percent full load plant operation.
7. The Loss of Secondary Pressure Transient is initiated at no load conditions.
8. The secondary pressure at 100 percent power is 900 psia and 1000 psia at no load conditions.

<u>Figures</u>	<u>Transients</u>	<u>Number of Occurrences</u>
2-1 thru 2-5	90%-100% Power Step	2,000
3-1 thru 3-5	100%-90% Power Step	2,000
4-1 thru 4-5	15%-25% Power Step	--
5-1 thru 5-5	25%-15% Power Step	--
6-1 thru 6-5	15%-100% Power Ramp at 5%/minute	15,000
7-1 thru 7-5	100%-15% Power Ramp at -5%/minute	15,000
8-1 thru 8-5	Turbine-Reactor Trip	Plant Trip { 400 } 480 { 40 } { 40 } { 5 }
9-1 thru 9-5	Loss of Load	
10-1 thru 10-5	Loss of Flow	
11-1 thru 11-5	Loss of Secondary Pressure	

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STEAM GENERATOR POWER - MW

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10% = 540 MW

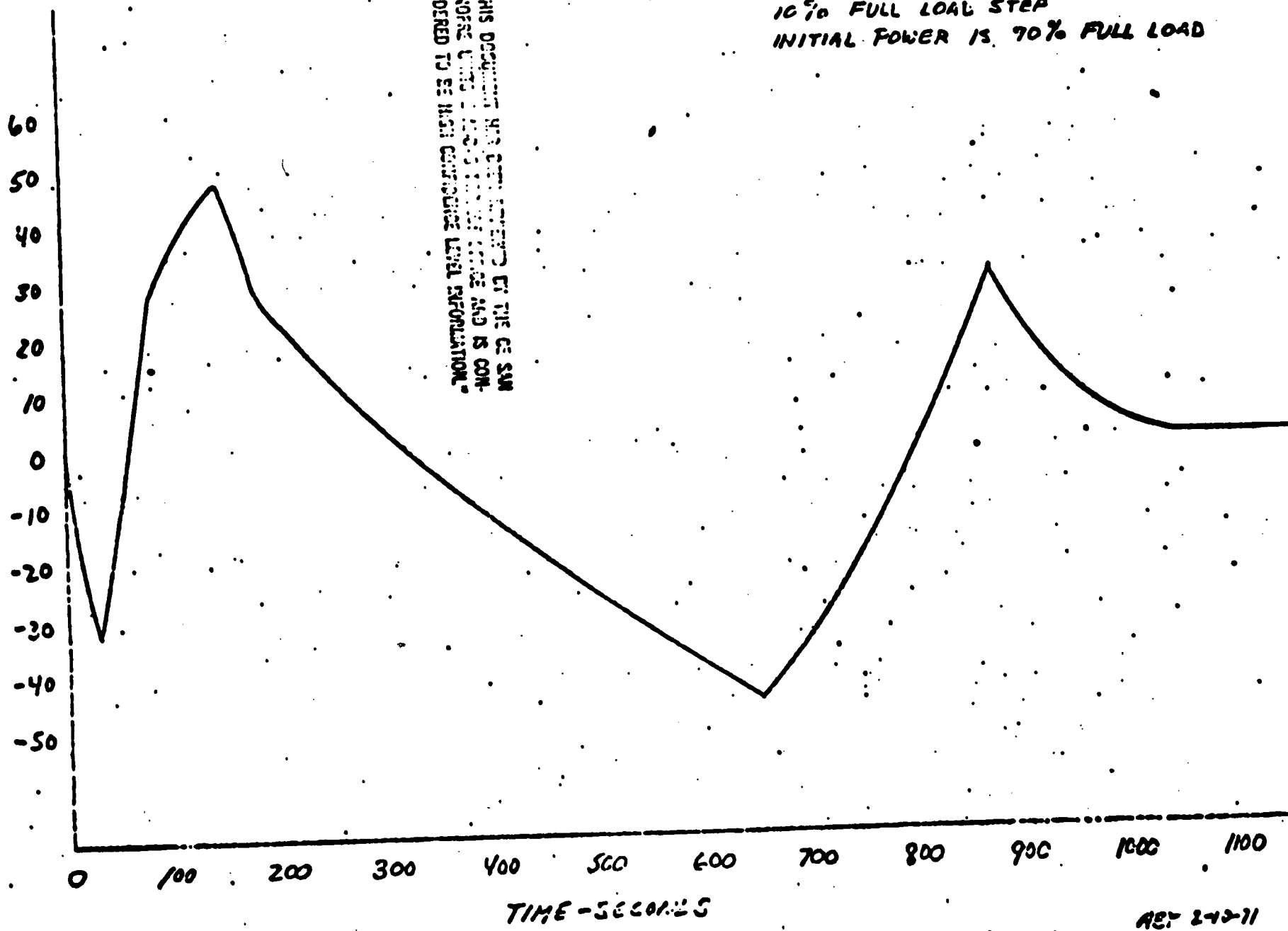
FIG 1

900-B-42-0

900-B-42-0

CHANGE IN THIRTY PRESSURE - TSI/H

1-2 5/1



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STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 70% FULL LOAD

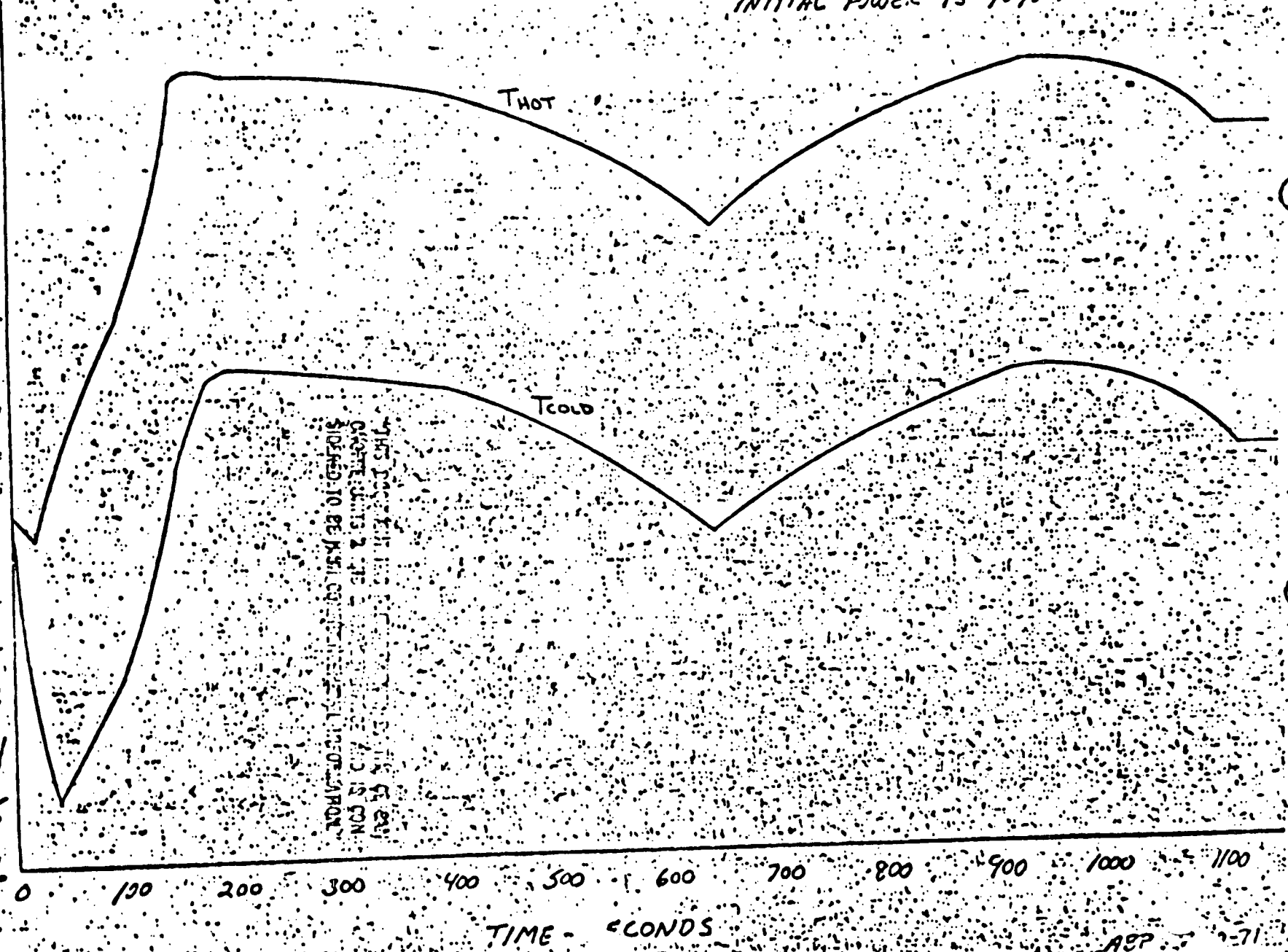
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4

STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 90% FULL LOAD

CHANGE IN REACTOR COOLANT TEMPERATURE

900.B-42-0



THIS POINT IS THE POINT WHERE THE REACTOR COOLANT TEMPERATURE IS 2.45 IN CONSIDERED TO BE A SIGNIFICANT POINT

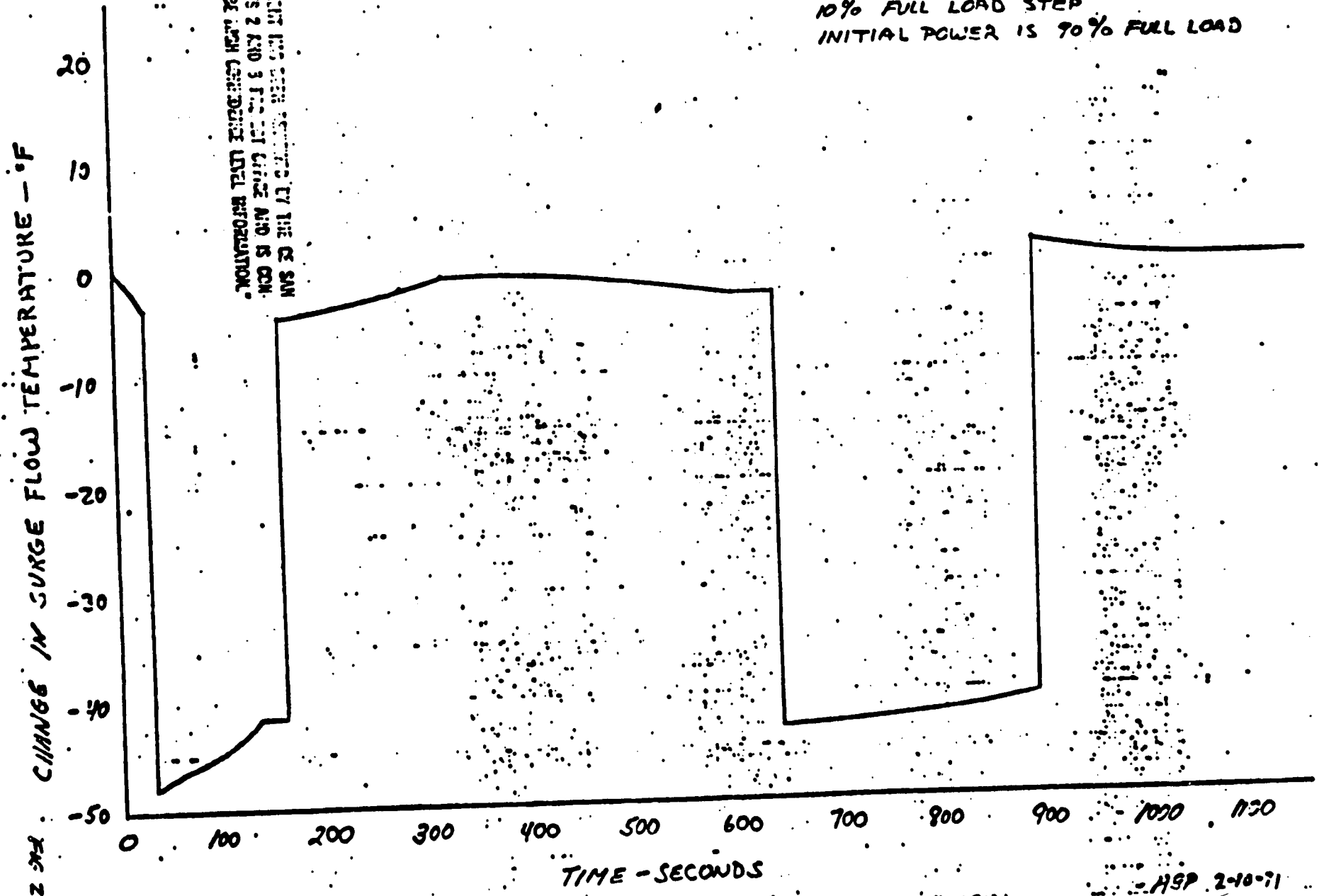
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ASP

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STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 90% FULL LOAD

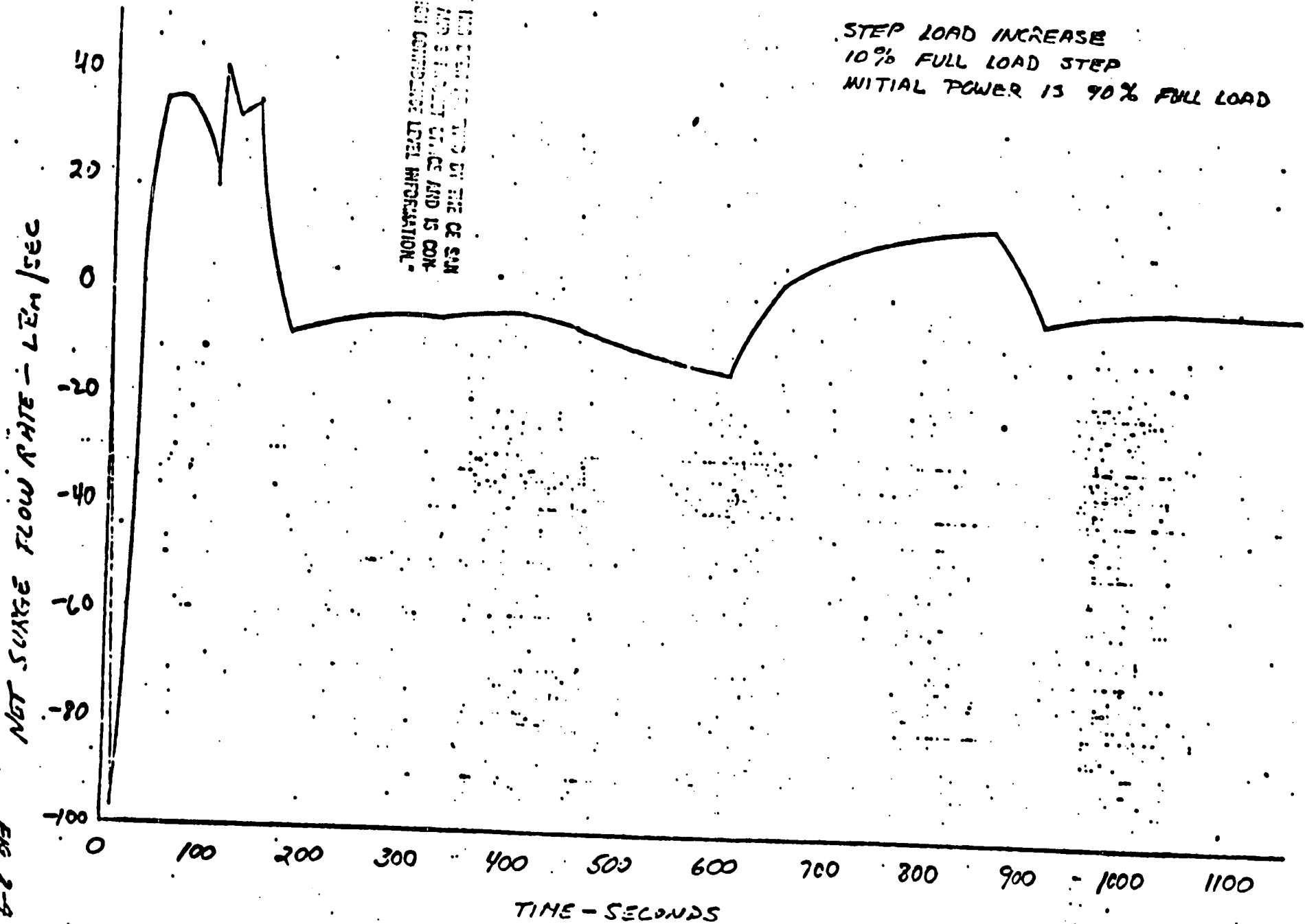


E-2-3

MSP 2-10-71

THIS EXPERIMENT WAS CONDUCTED IN THE CE SW
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STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 90% FULL LOAD

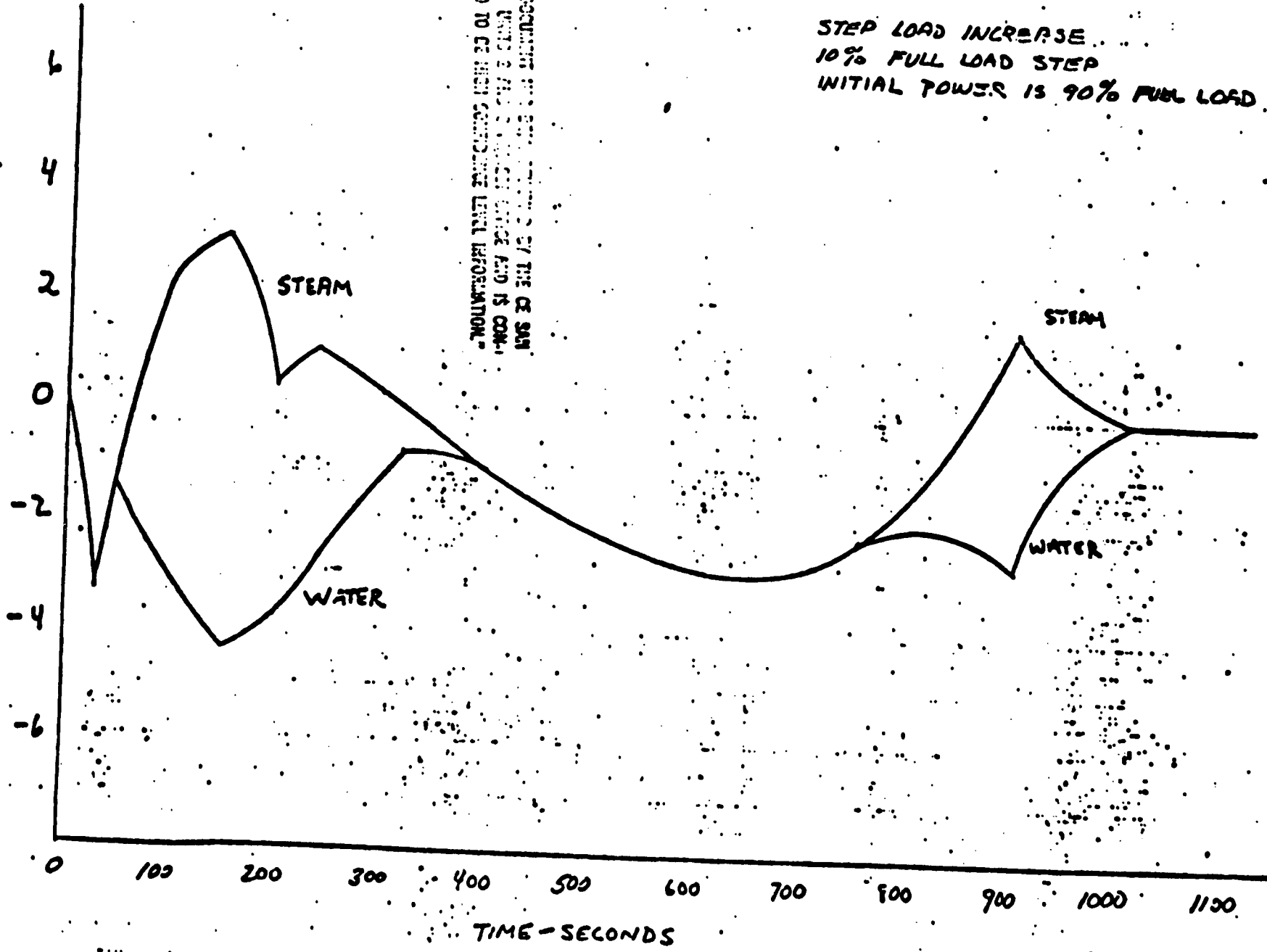


900-13-42-0
NET SURGE FLOW RATE - CC/MIN
FIG 2-9

900-B-42-0

CHANGE IN PRESSURIZER TEMPERATURE - °F

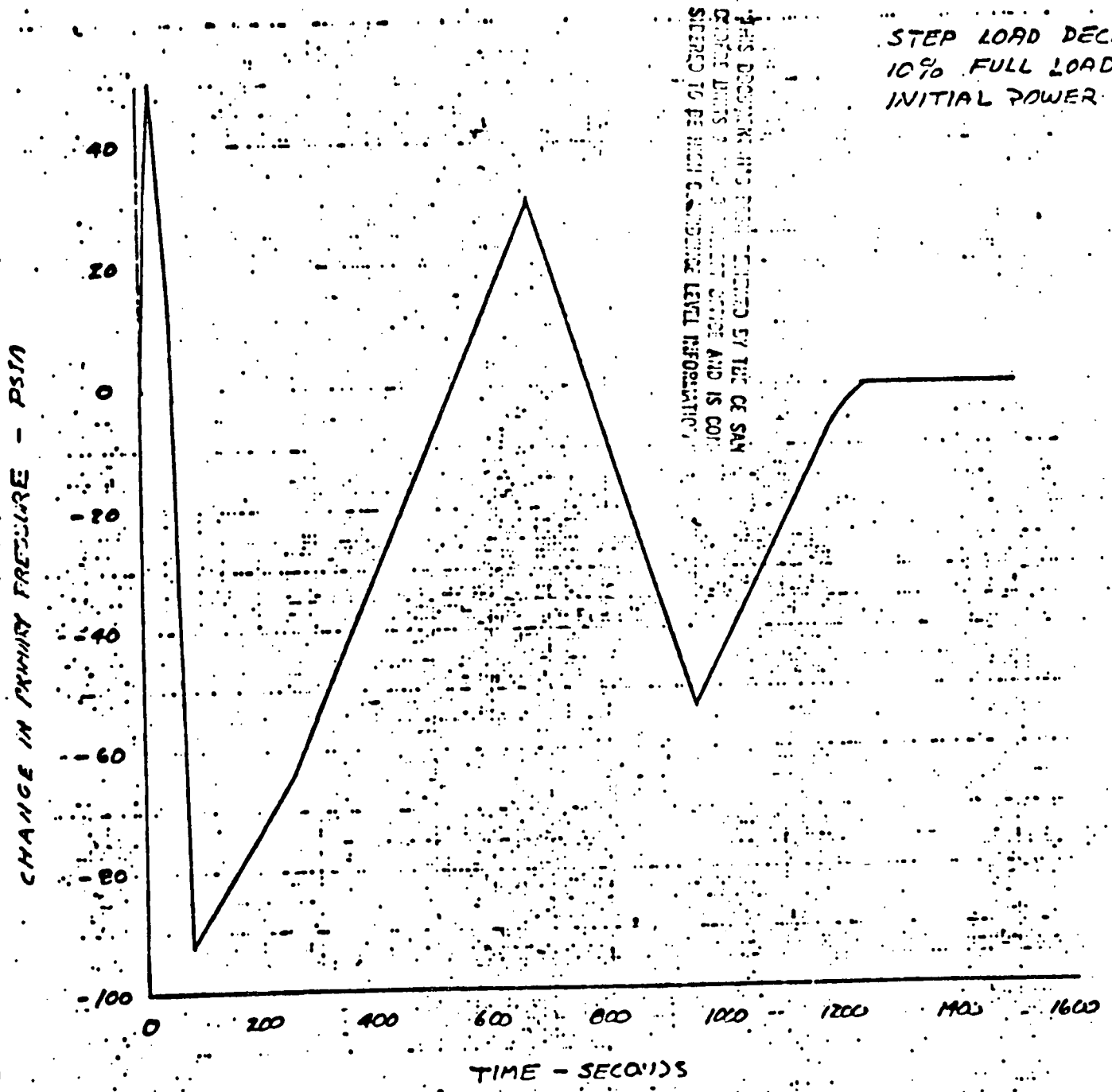
FIG 2-5



STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 90% FULL LOAD

900-B-42-0

FIG 3-1

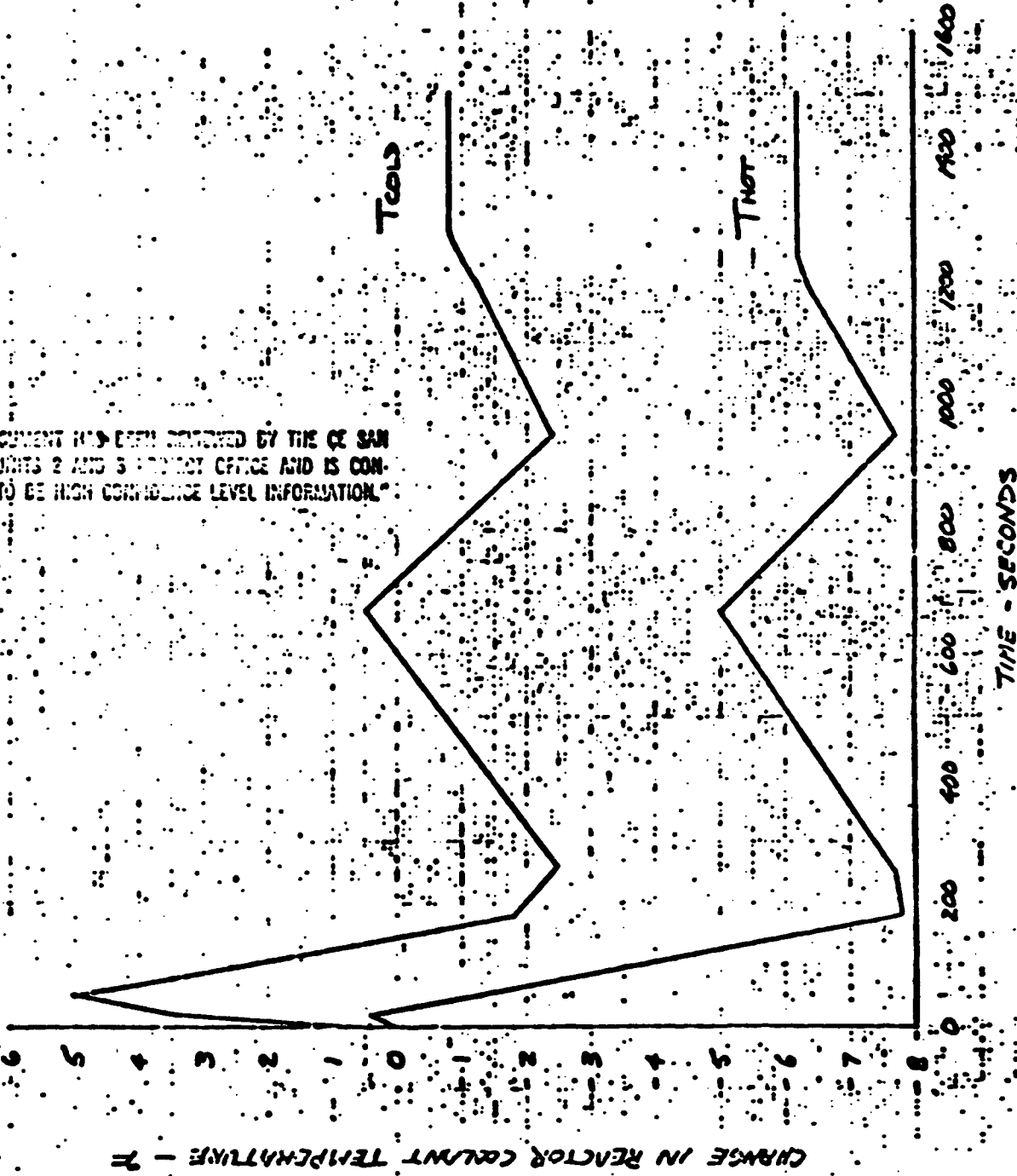


THIS DECREASE IN PRESSURE IS CAUSED BY THE CE SAM
CHANGE LIMITS AND IS CONSIDERED TO BE HIGH CONDENSATE LEVEL REGULATION.

STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 100% FULL LOAD

STEP LOAD DECREASE
 10% FULL LOAD STEP
 INITIAL POWER IS 100% FULL LOAD

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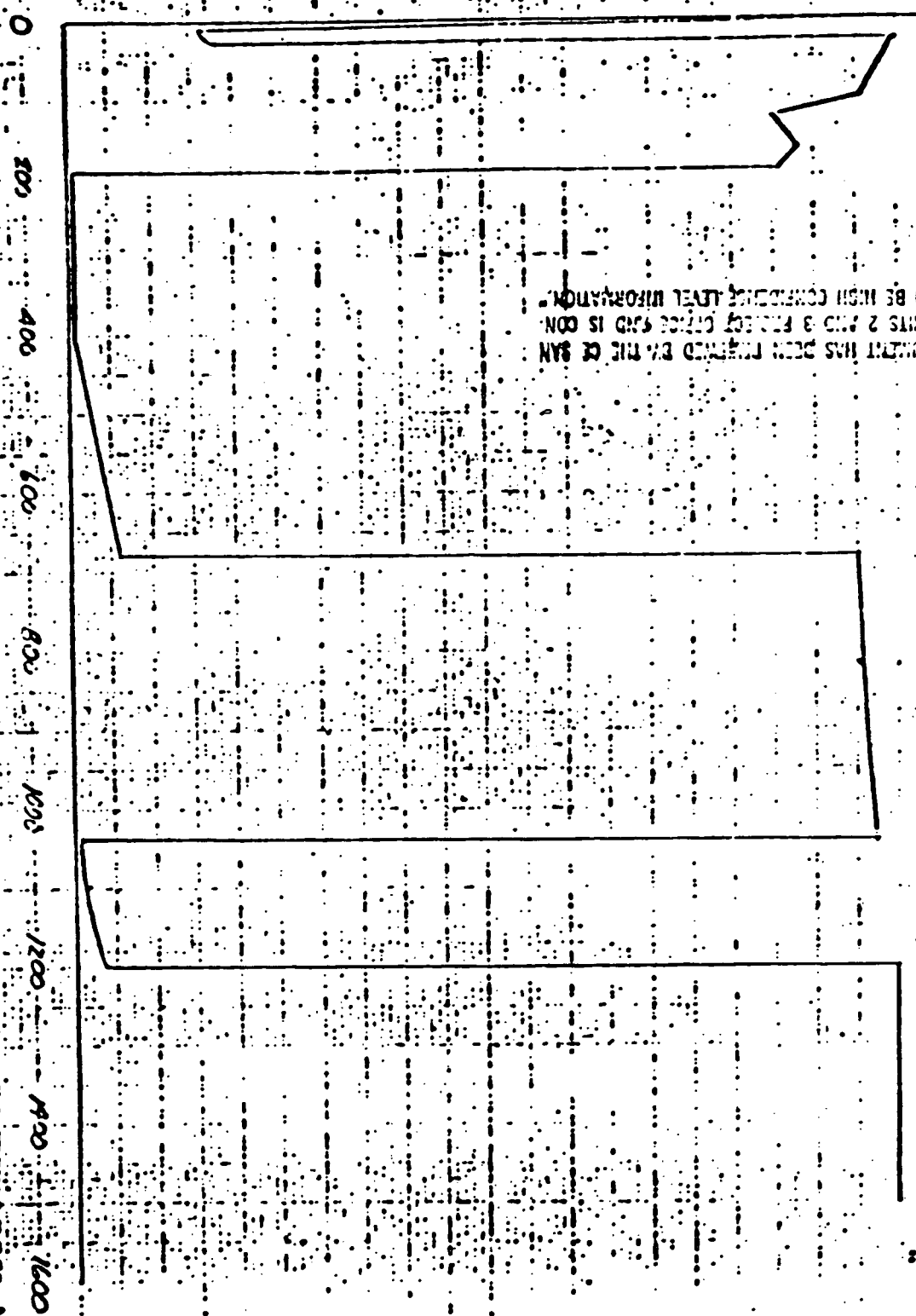


2-E 91F

CHANGE IN SURGE FLOW TEMPERATURE - 7-

E-E FIG 3-3

0
-10
-20
-30
-40
-50



STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 100% FULL LOAD

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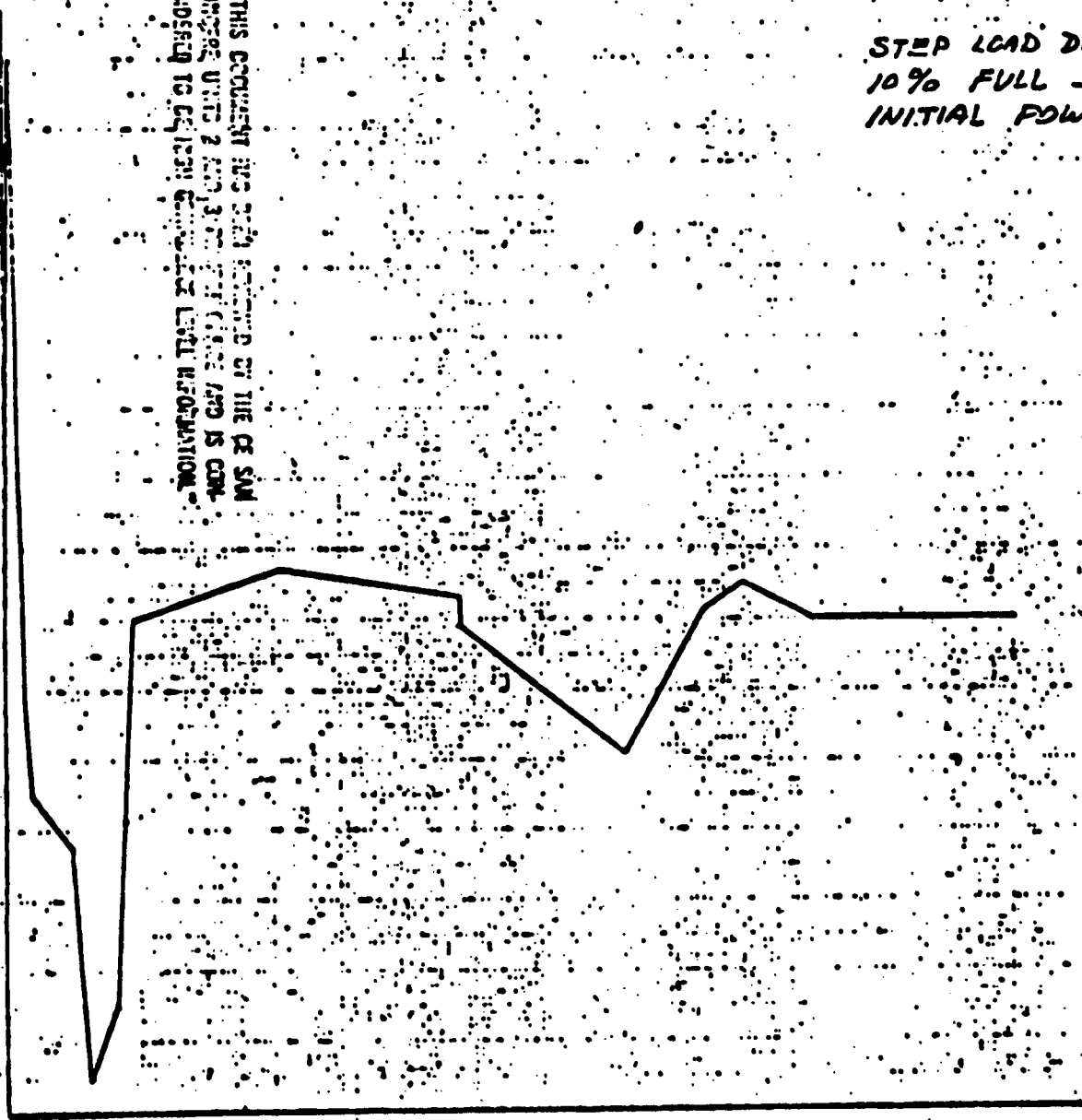
FIG 3-3

STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 100% FULL LOAD

THIS COMMENT AND DATA REPORTED BY THE CE SWL
DRIVER UNIT 2 AND 3. THE DATA IS FOR THE
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NET SURGE FLOW RATE - IR/SEC

80
70
60
50
40
30
20
10
0
-10
-20
-30
-40
-50
-60
-70



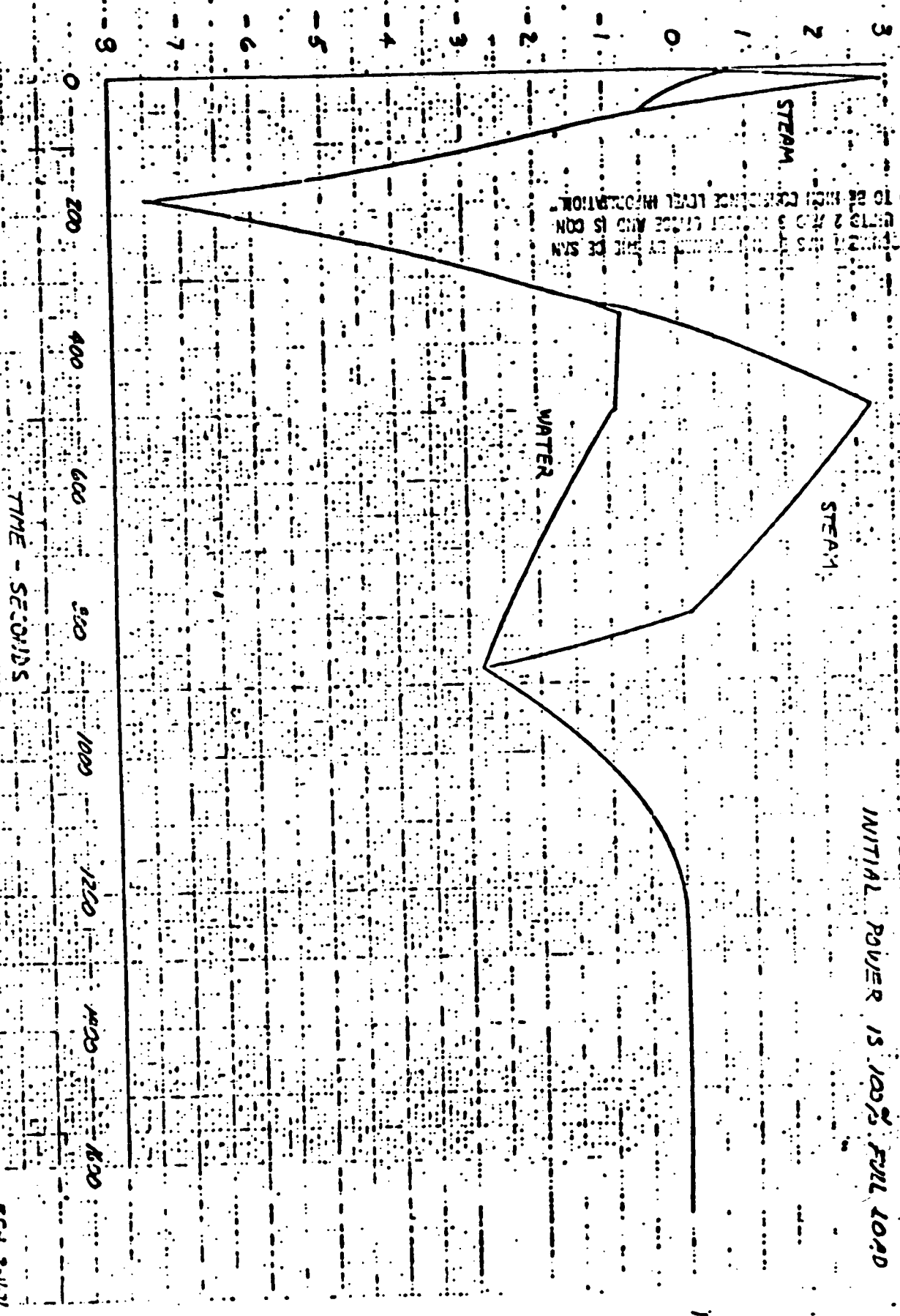
TIME - SECONDS

900-B-42-0

FK 3-7

ERA 2-11-71

CHANGE IN PRESSURIZED TEMPERATURE - °F



STEP LOAD DECREASE
 10% FULL LOAD STEP
 INITIAL POWER IS 100% FULL LOAD

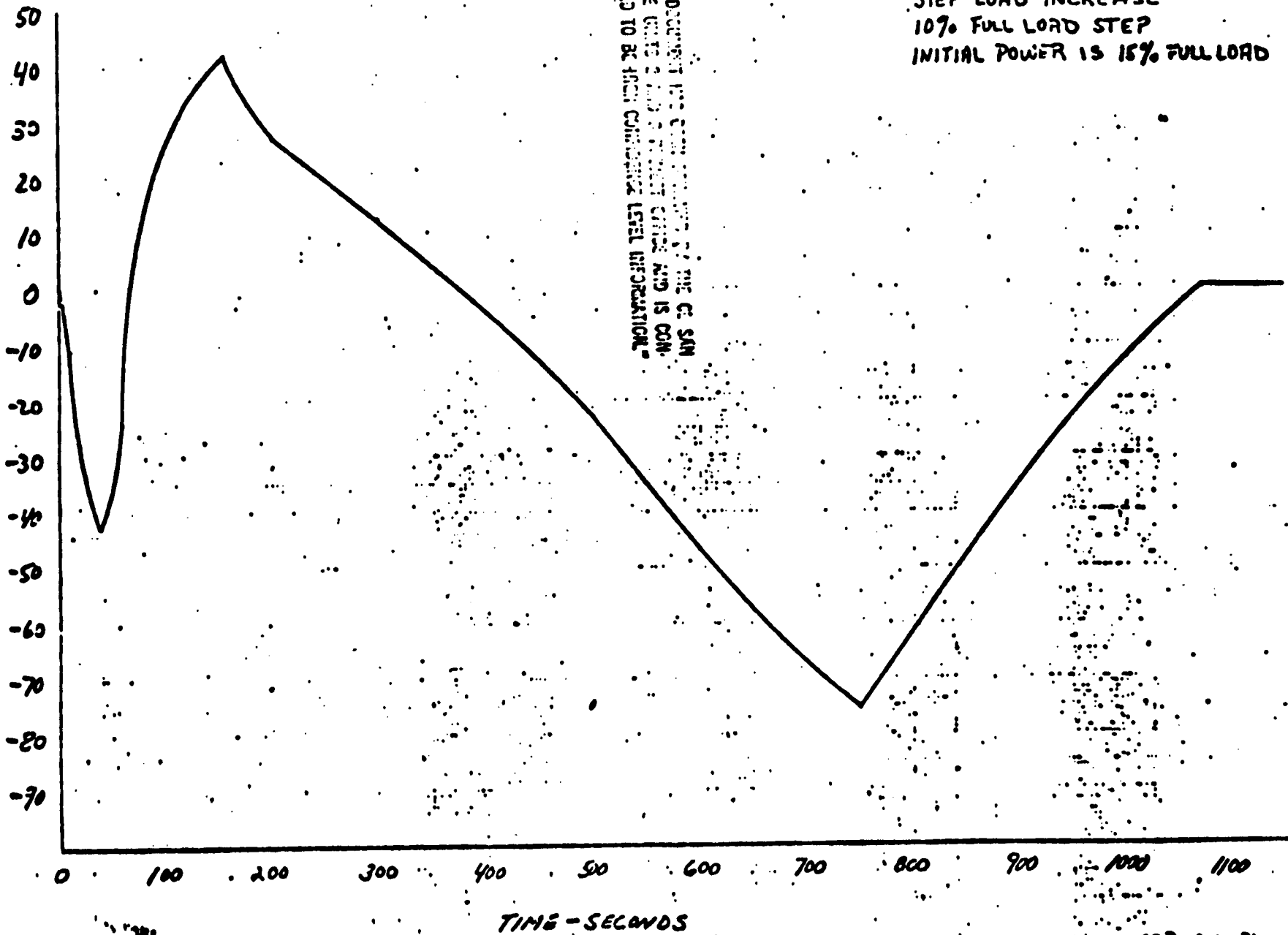
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TIME - SECONDS

900-B-42-0

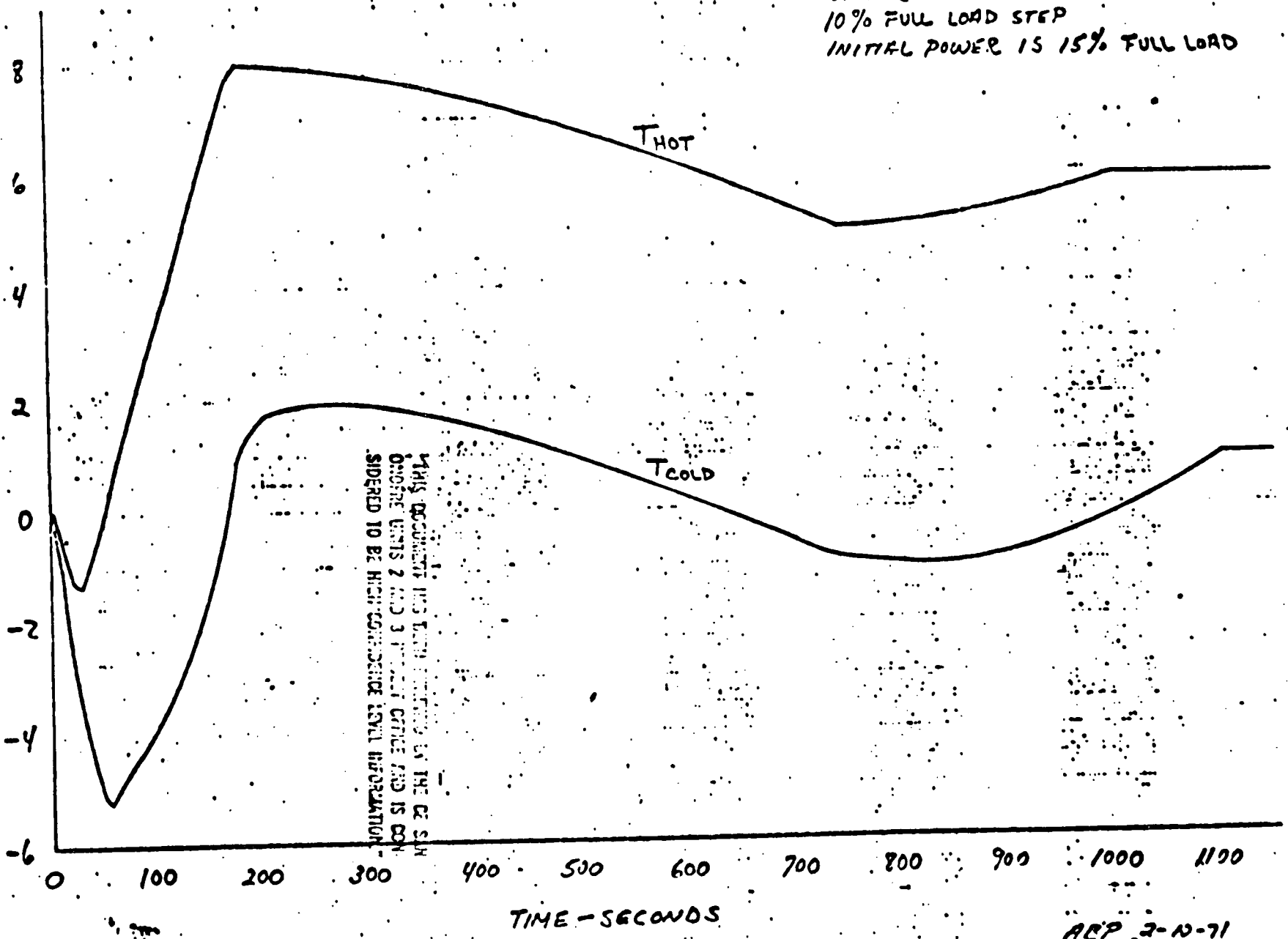
CHANGE IN PRIMARY PRESSURE - PSI

FIG 1-1



A&P 2-10-71

STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 15% FULL LOAD



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CHANGE IN TEMPERATURE - F

TIME - SECONDS

SEP 2-10-71

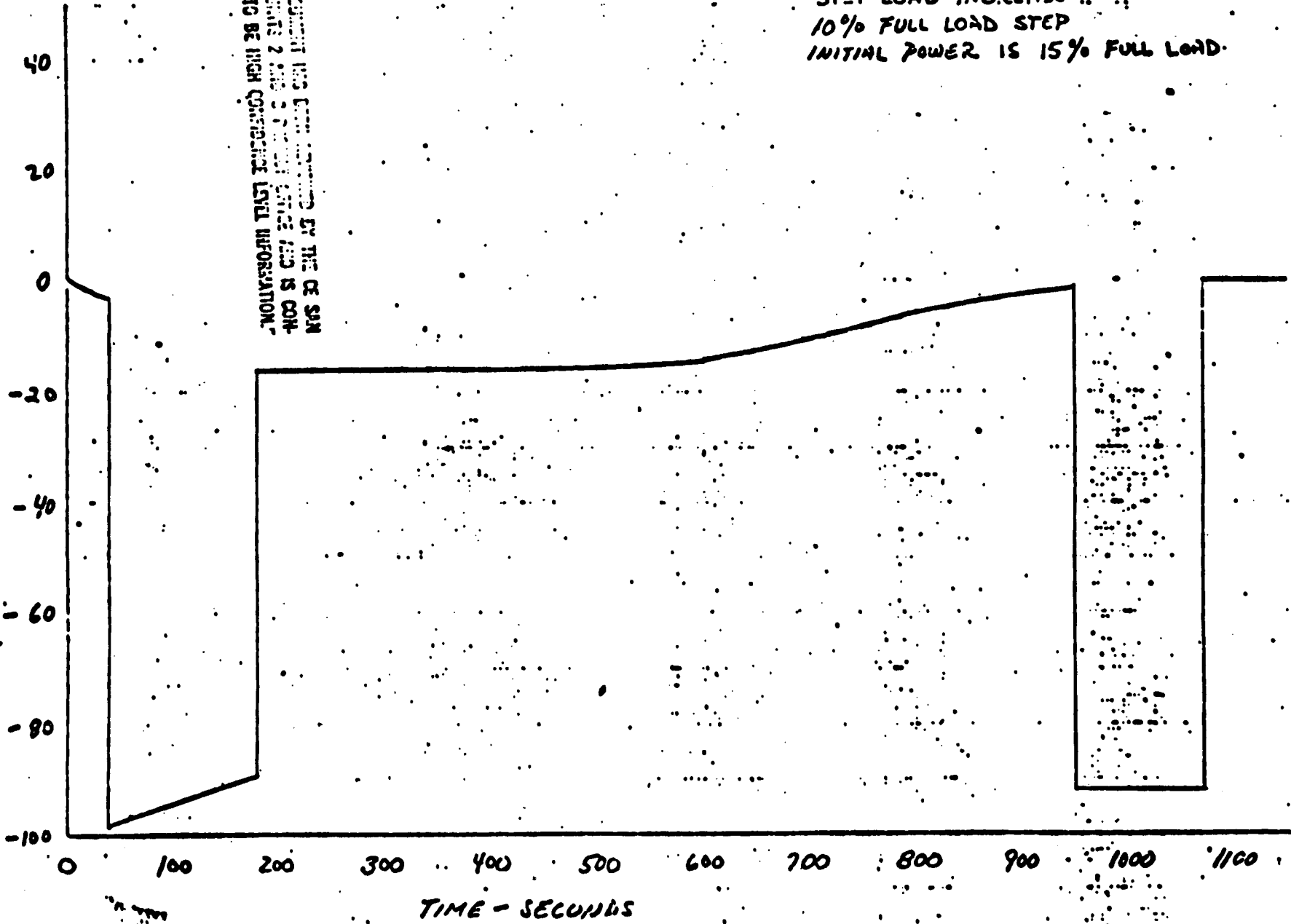
900-B-42-0

FIG 4-2

900-B-42-0

CHANGE IN SURGE FLOW TEMPERATURE - °F

FIG 4-3

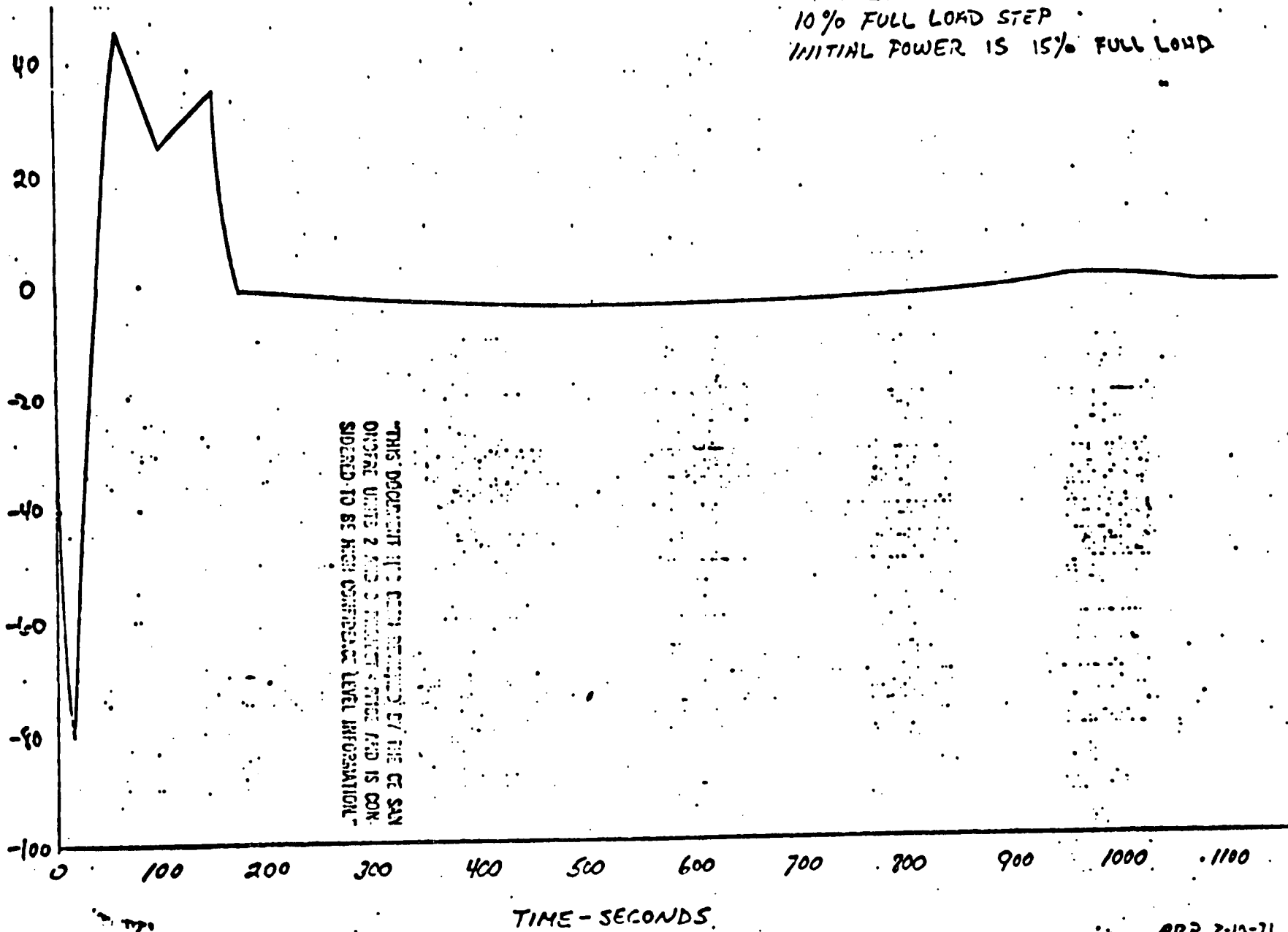


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STEP LOAD INCREASE
10% FULL LOAD STEP
INITIAL POWER IS 15% FULL LOAD.

ASP 2-10-71

STEP LOAD INCREASE ...
10% FULL LOAD STEP
INITIAL POWER IS 15% FULL LOAD



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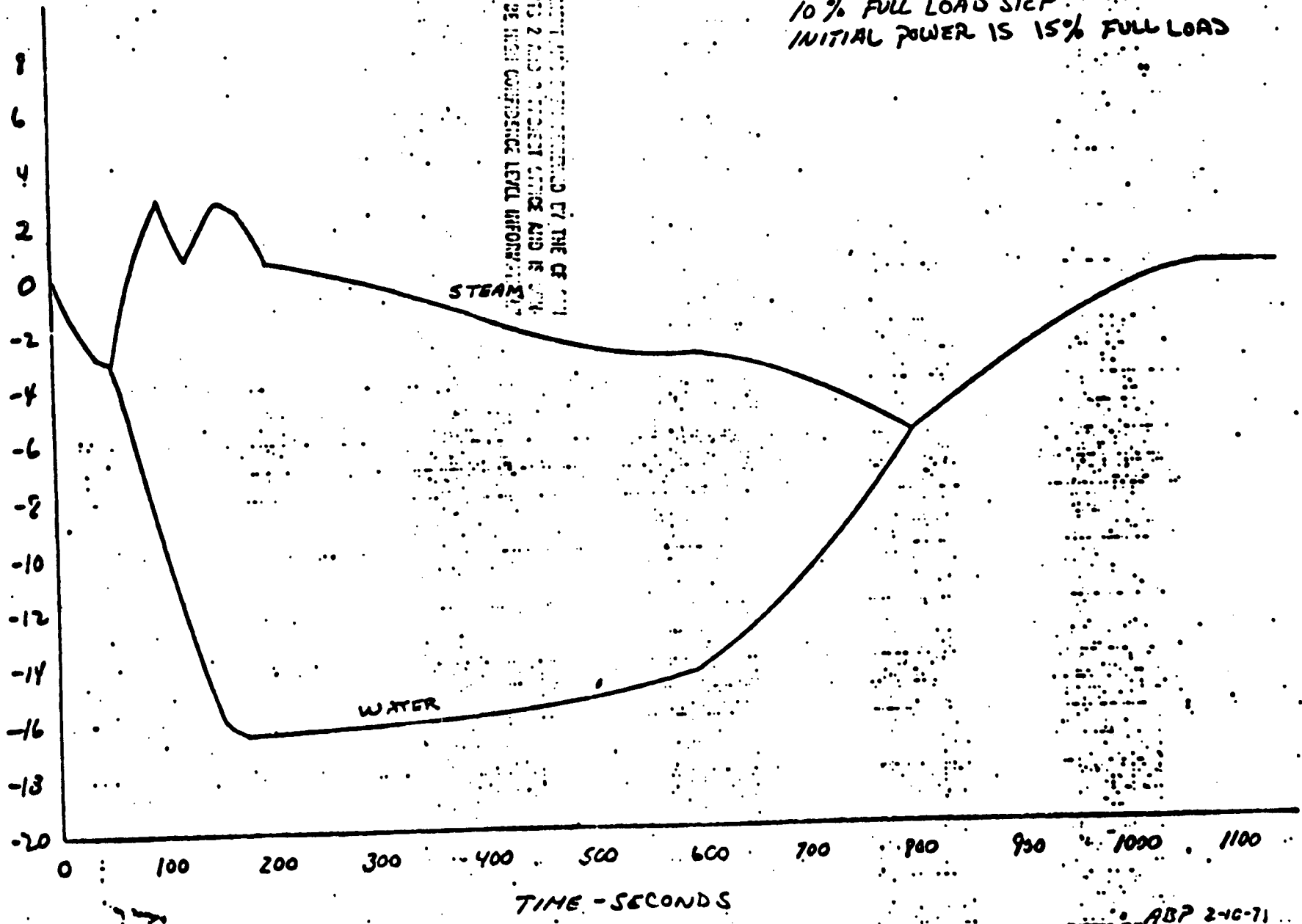
FIG 4-4

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ABP 2-15-71

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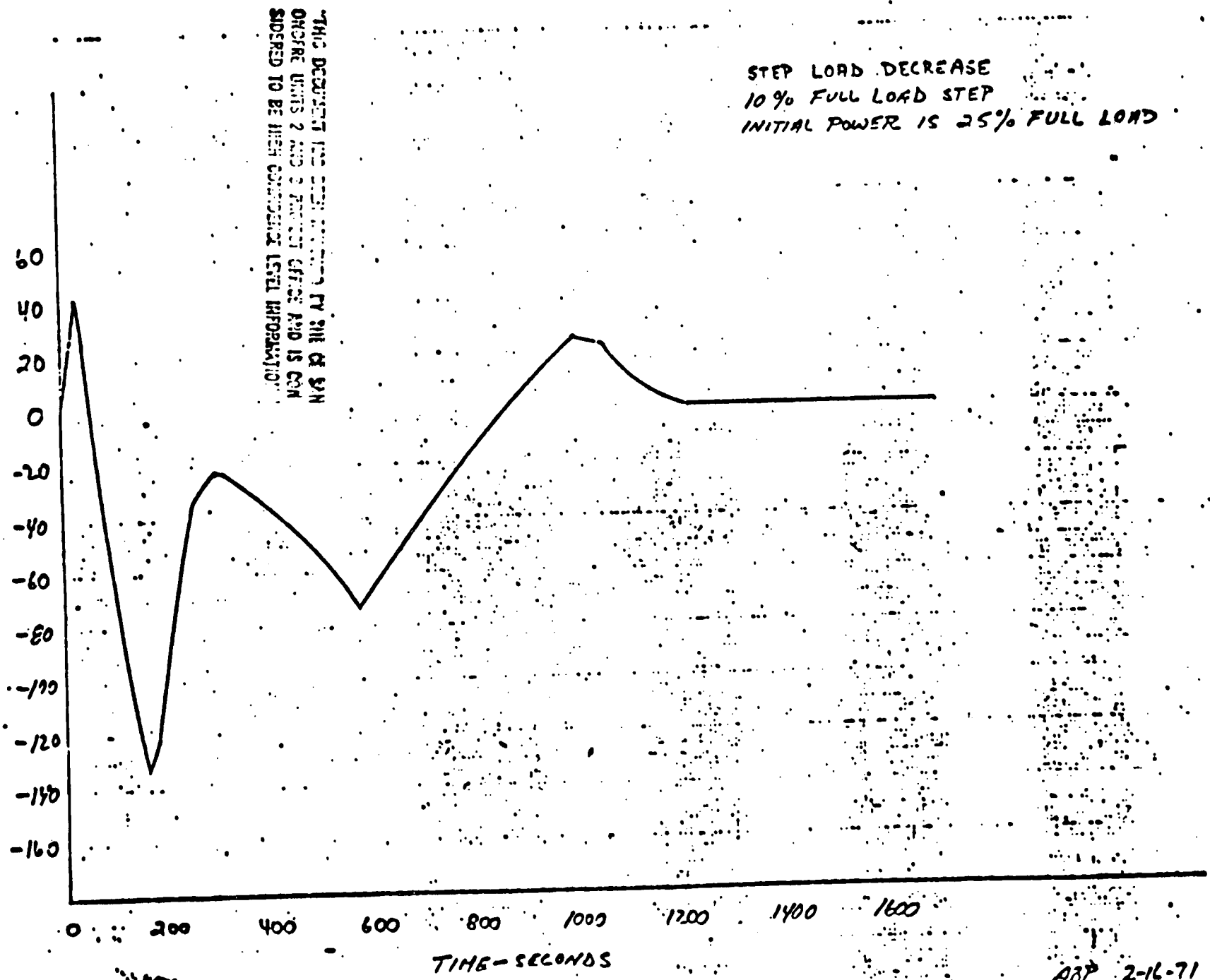
PERCENT CHANGE IN PRESSURIZER TEMPERATURE - °F



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10% FULL LOAD STEP
INITIAL POWER IS 15% FULL LOAD

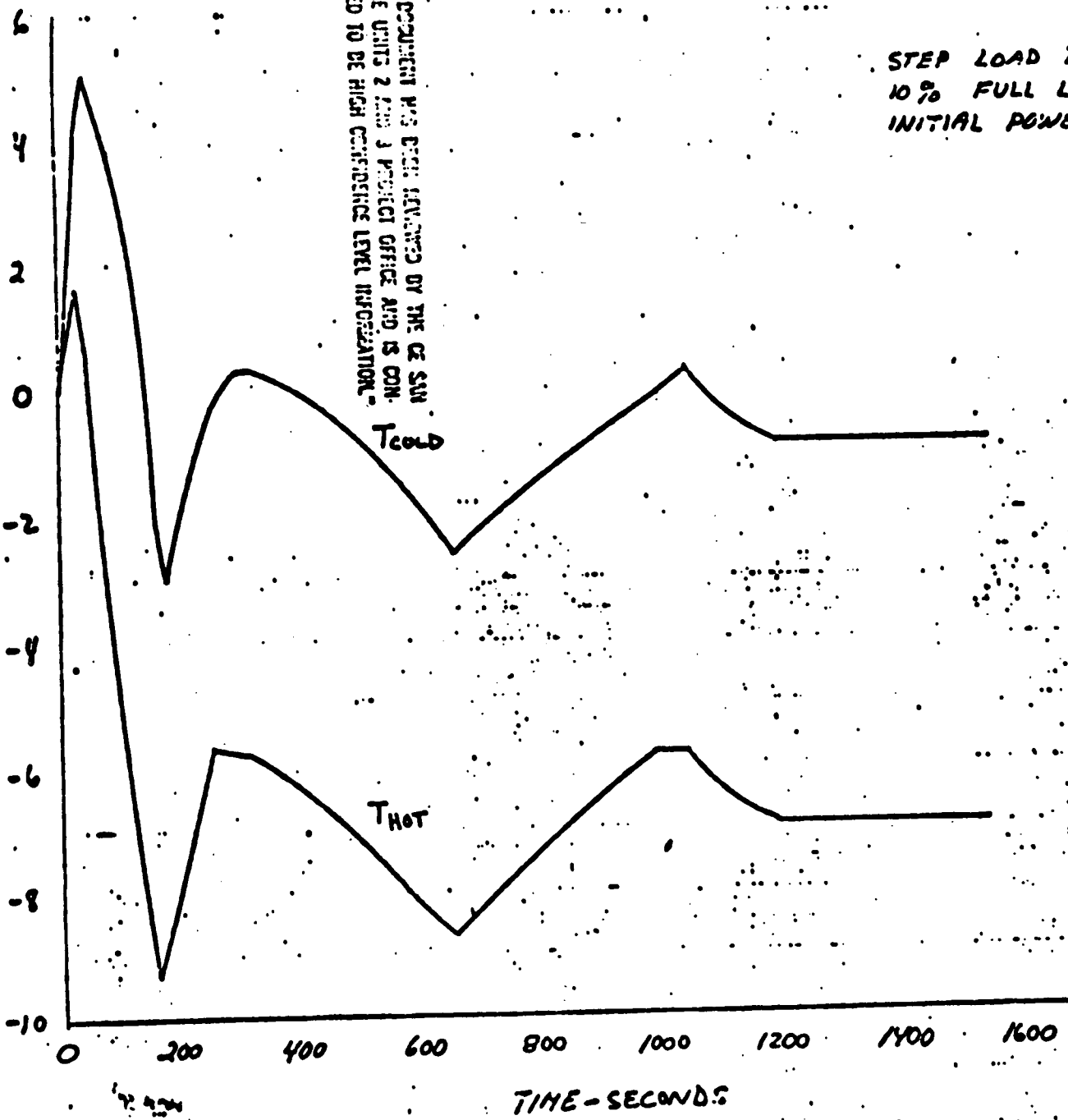
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FIG 5-1
CHANGE IN PRIMARY PRESSURE -- PSI



ADP 2-16-71

900-B-42-0

CHANGE IN REACTOR COOLANT TEMPERATURE - F



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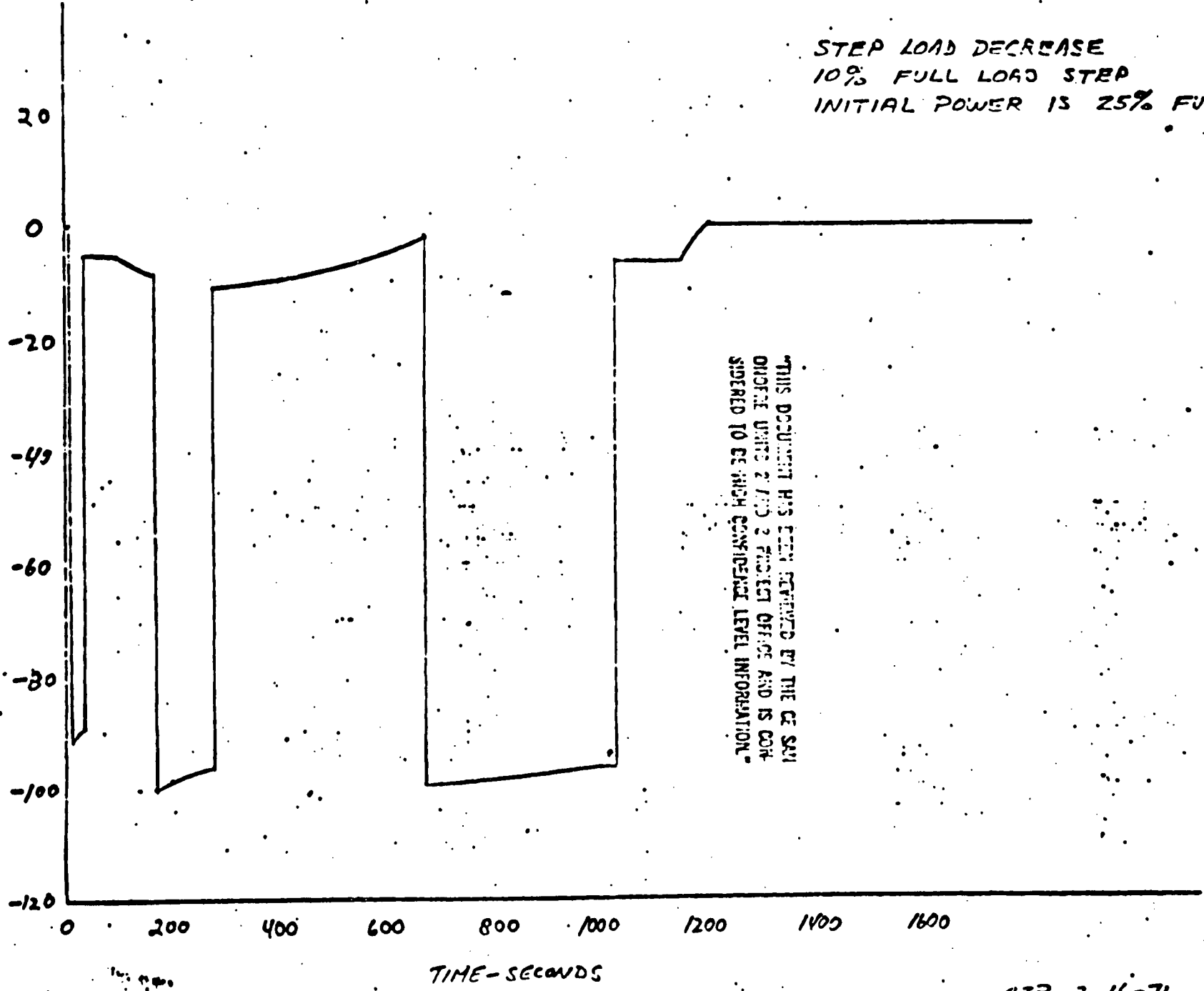
STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 25% FULL LOAD

TIME-SECONDS

ABP 2-16-71

900-B-42-0

FIG 5-3 CHANGE IN SURGE FLOW TEMPERATURE - OF

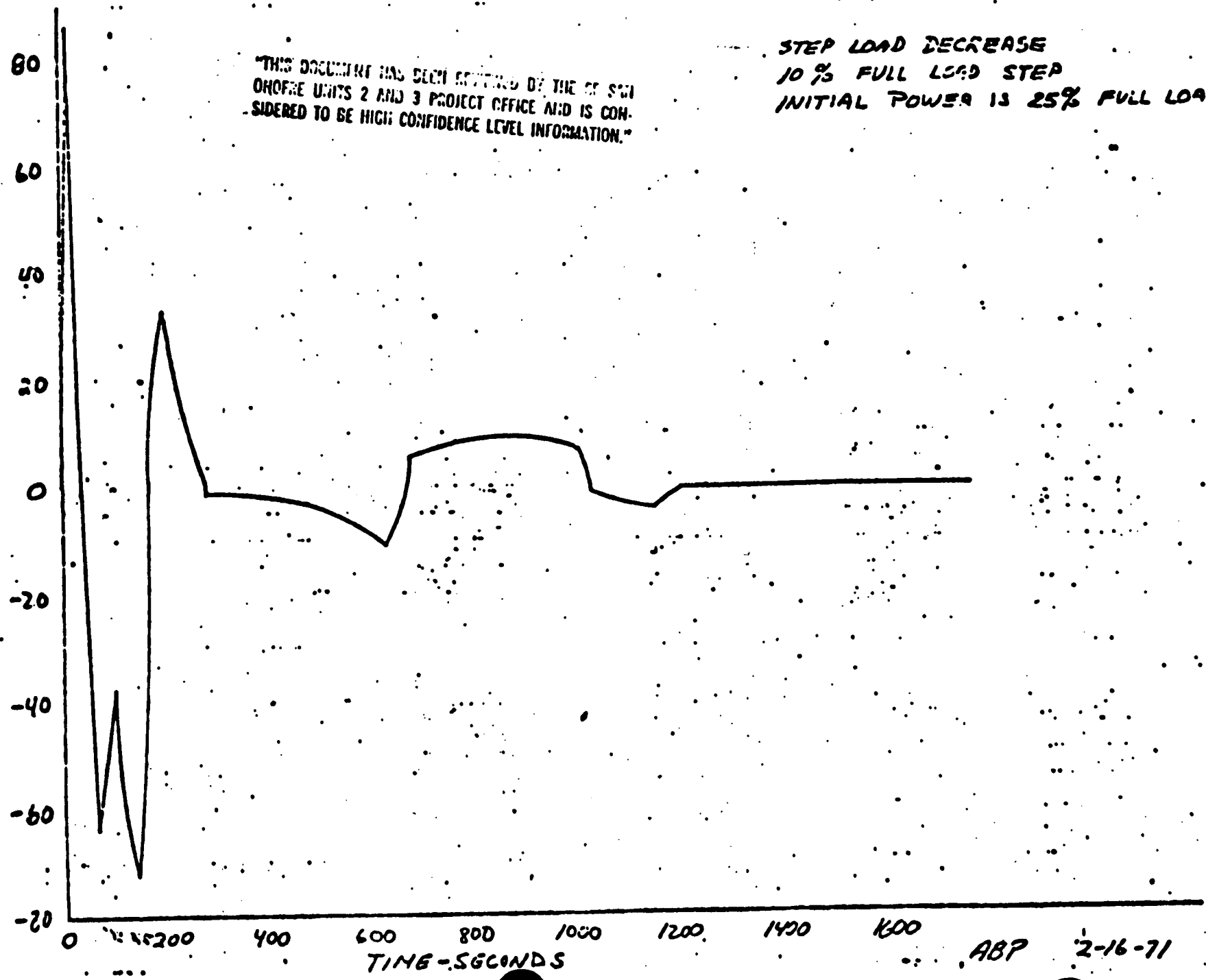


STEP LOAD DECREASE
 10% FULL LOAD STEP
 INITIAL POWER IS 25% FULL LOAD

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NET SURGE FLOW RATE - LBS/SEC



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STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 25% FULL LOAD

FIG 5-9

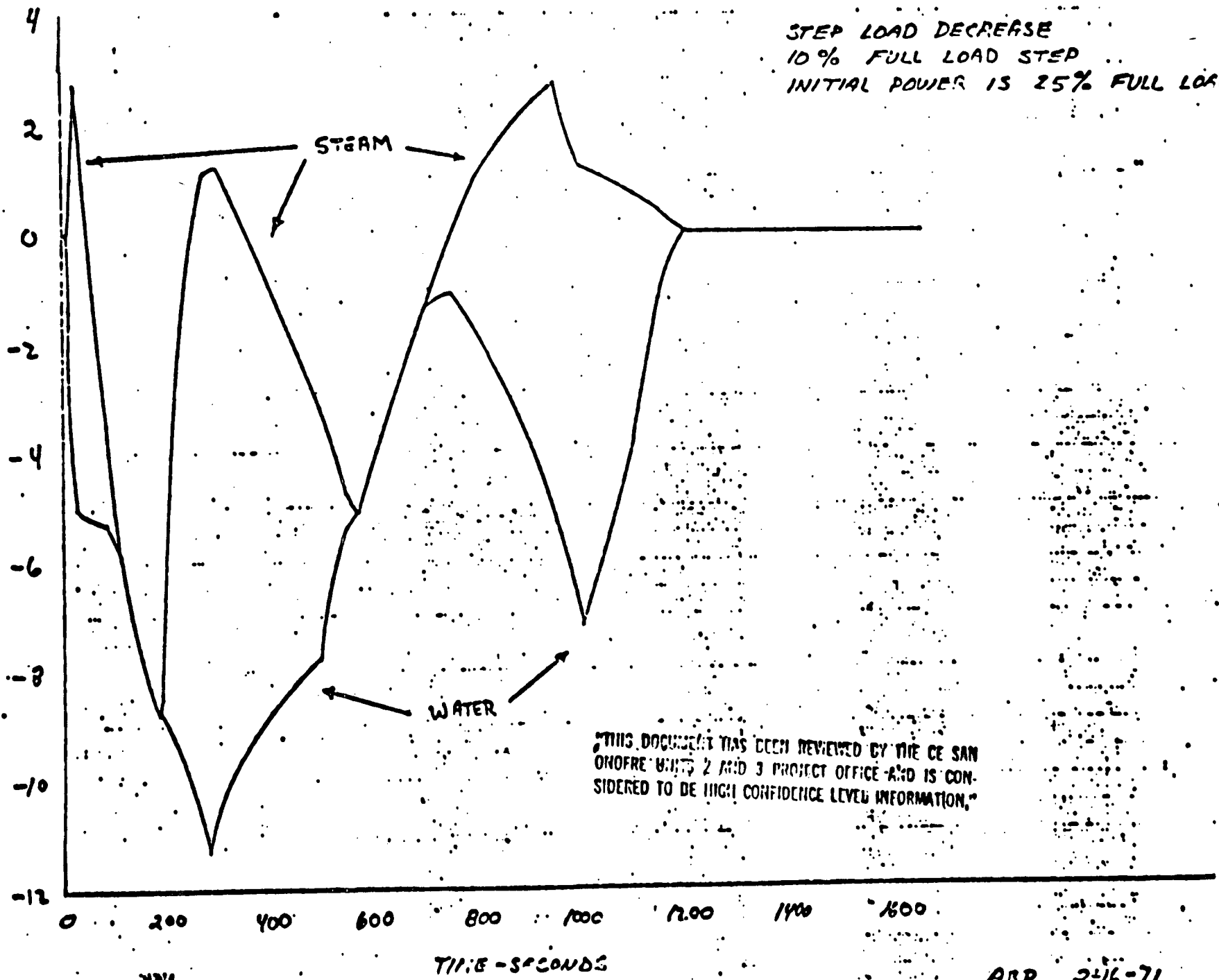
TIME-SECONDS

ABP 2-16-71

900-B-42-0

CHANGE IN PRESSURE TEMPERATURE -- °F

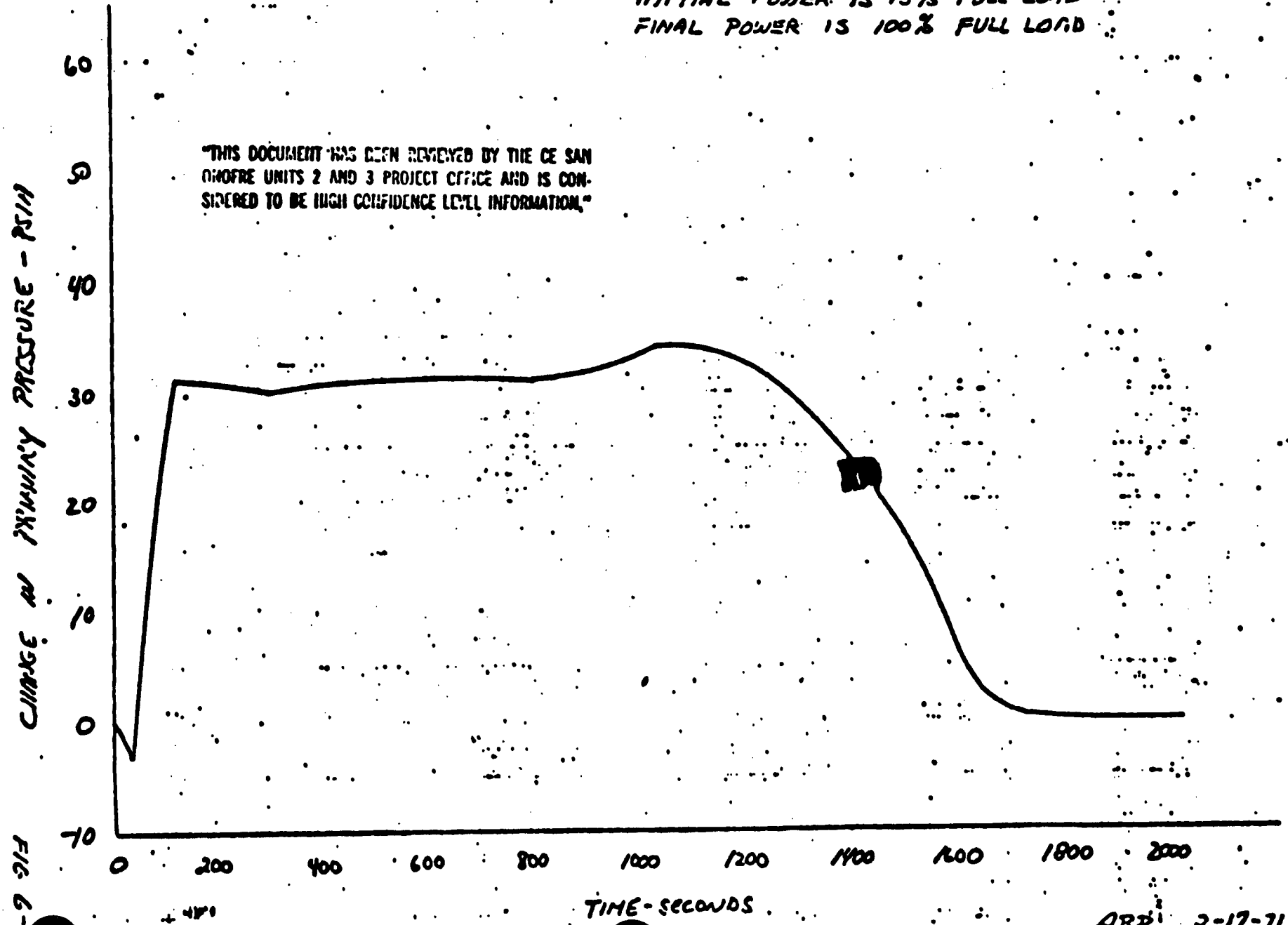
FIG 5-5



ABP 2-16-71

PLANT LOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 15% FULL LOAD
FINAL POWER IS 100% FULL LOAD

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CHANGE IN PRIMARY PRESSURE - PSIA
FIG 6-1

TIME - SECONDS

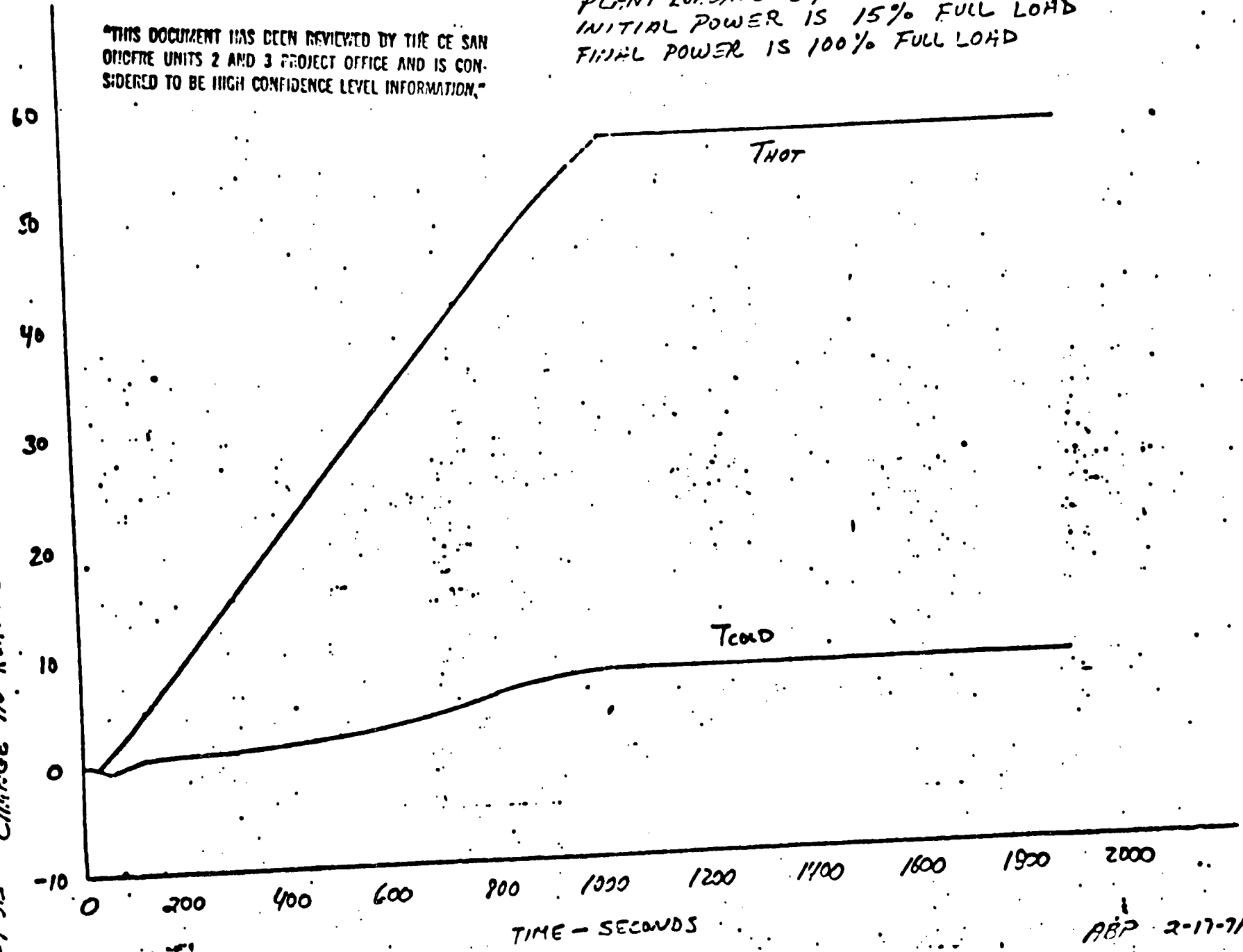
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FIG 6-2 CHANGE IN REACTOR COOLANT TEMPERATURE - °F

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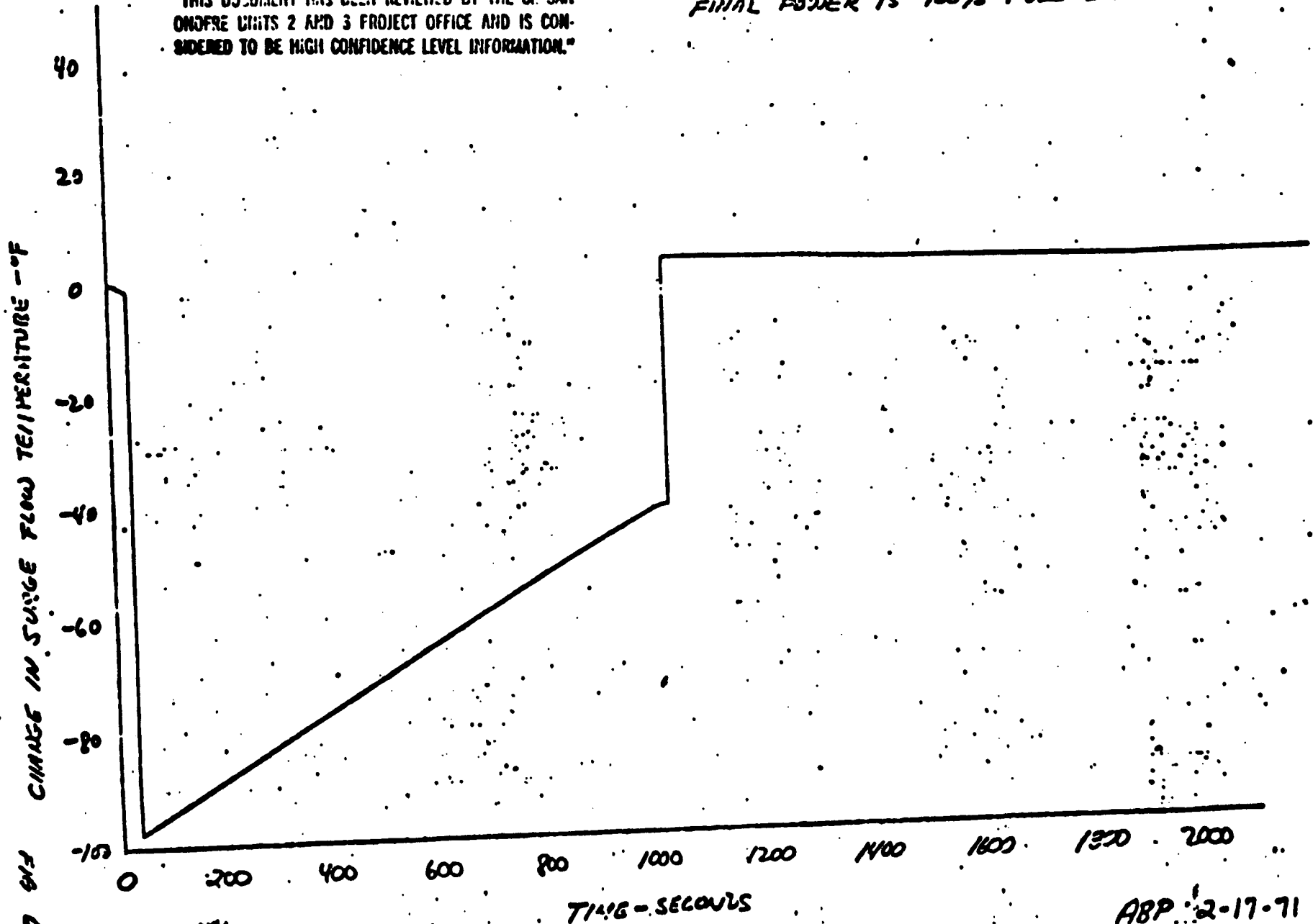
PLANT LOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 15% FULL LOAD
FINAL POWER IS 100% FULL LOAD



ABP 2-17-71

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PLANT LOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 15% FULL LOAD
FINAL POWER IS 100% FULL LOAD.

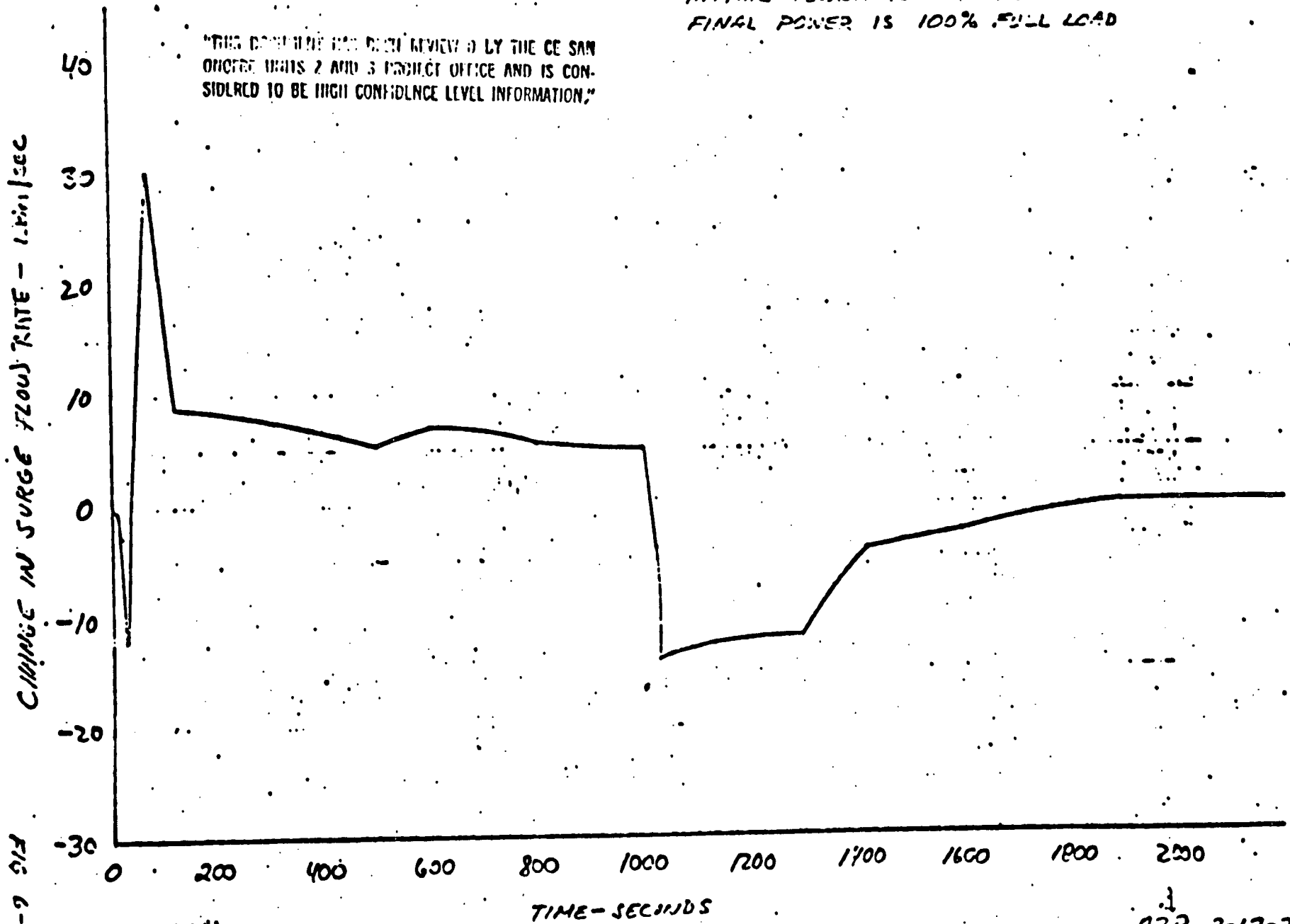


900-13-42-0

ABP 2-17-71

PLANT LOADINGS - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 15% FULL LOAD
FINAL POWER IS 100% FULL LOAD

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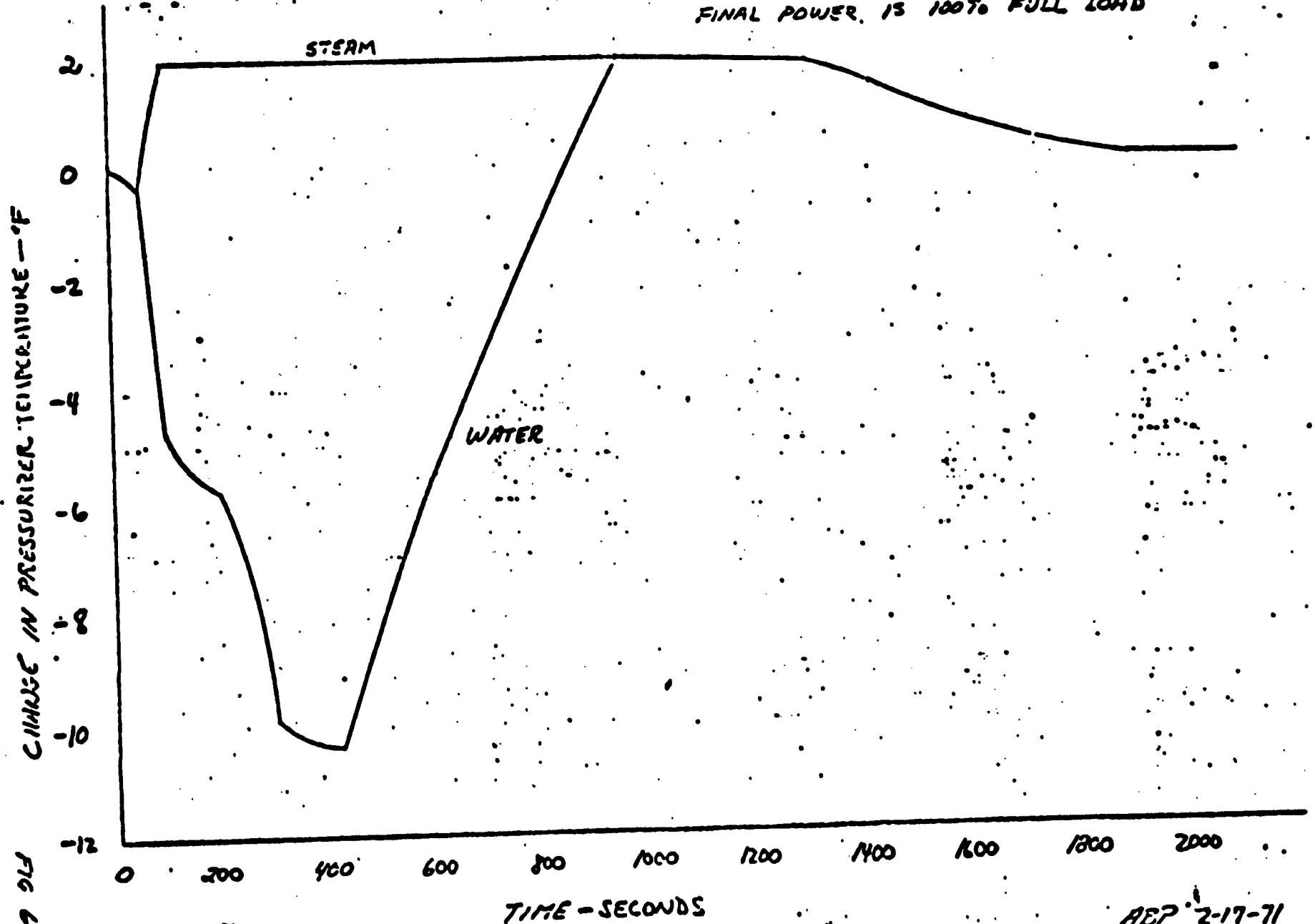
FIG 6-4

11-24-71

ARP 2-17-71

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PLANT LOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 15% FULL LOAD
FINAL POWER IS 100% FULL LOAD



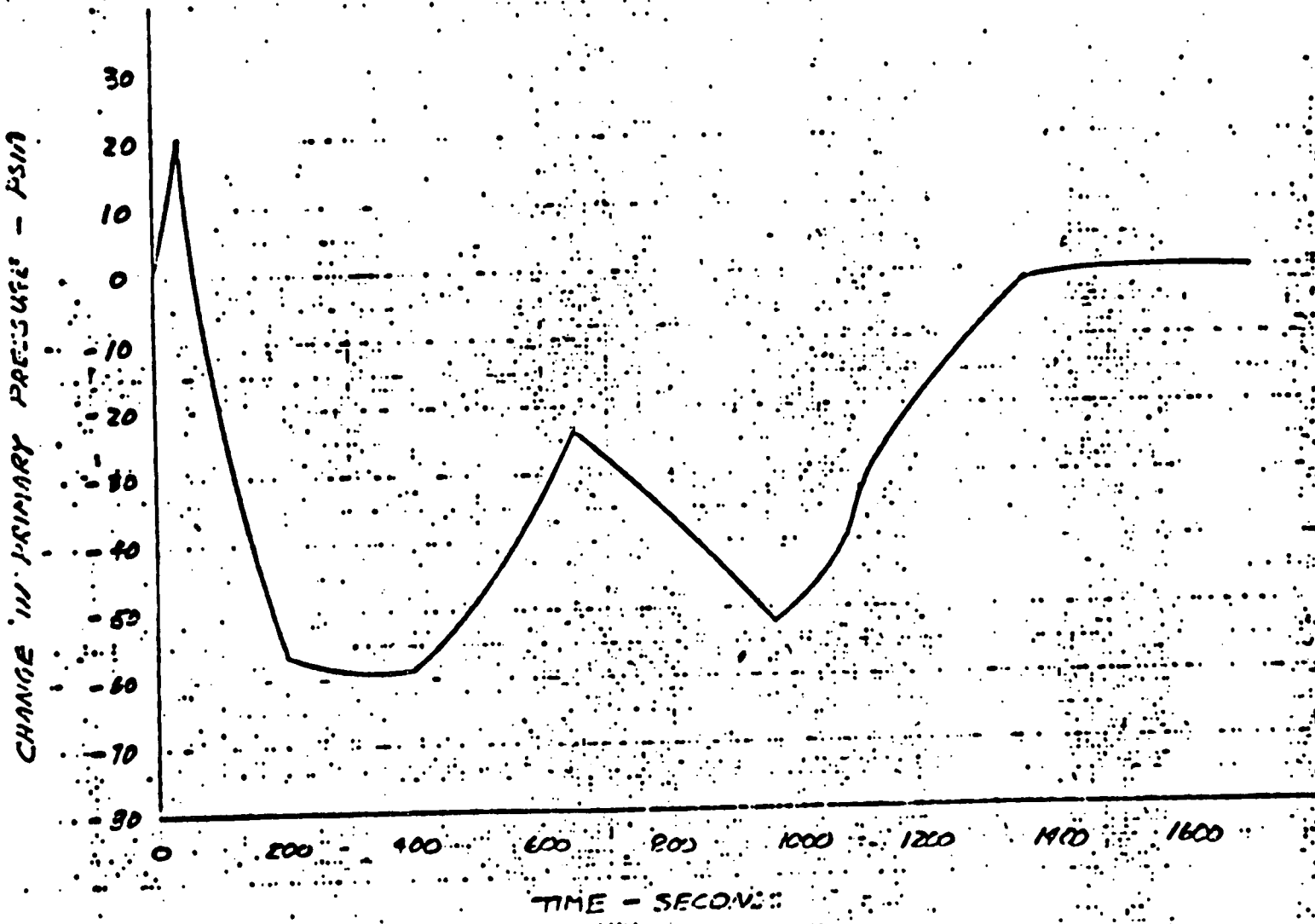
900-B-42-0

FIG 6-5

REP 2-17-71

PLANT UNLOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 100% FULL LOAD
FINAL POWER IS 15% FULL LOAD

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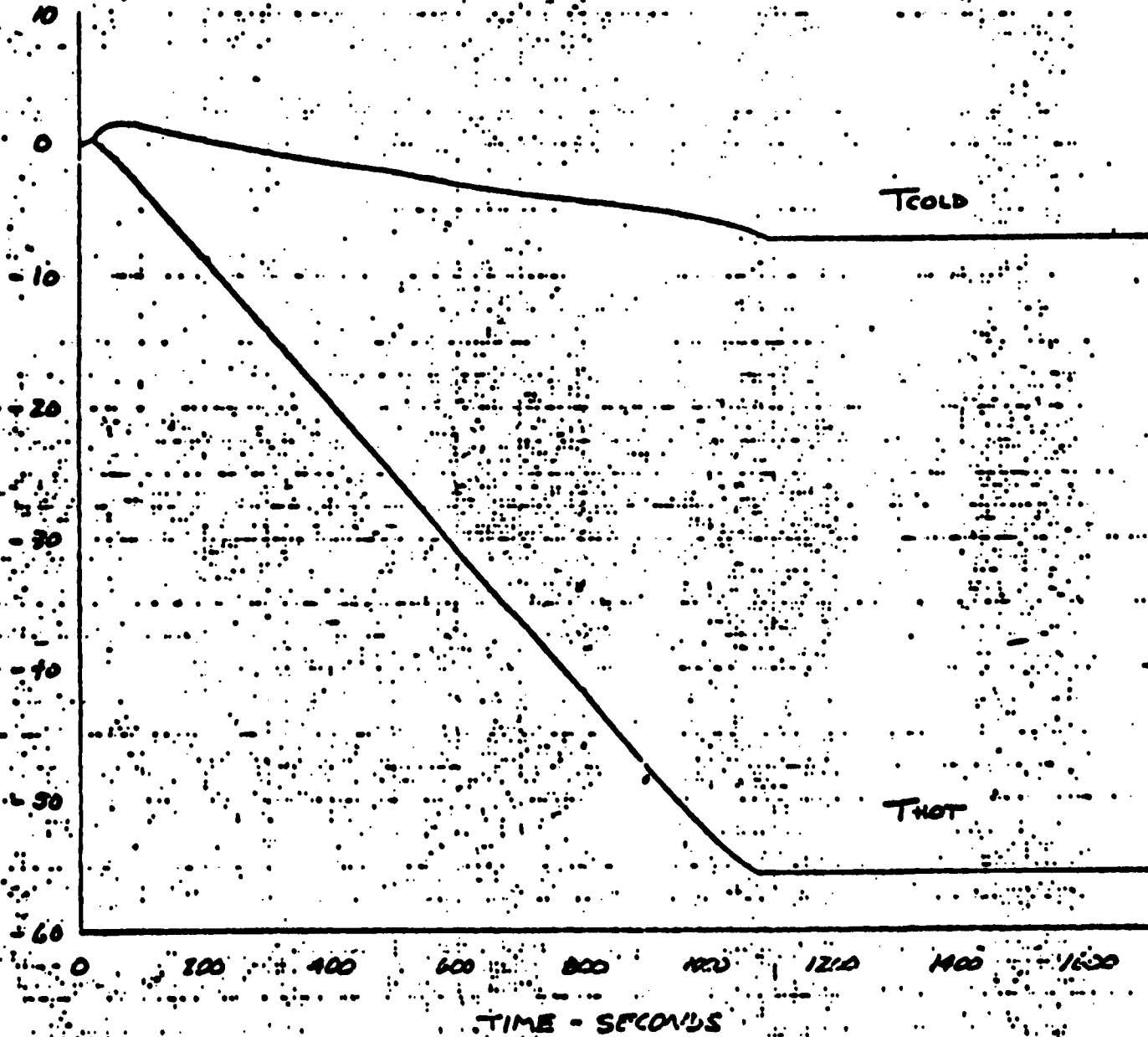
900-B-42-0

FIG. 7-1

900-B-42-0

FIG. 7-2

CHANGE IN REACTOR COOLANT TEMPERATURE - °F



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PLANT UNLOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 100% FULL LOAD
FINAL POWER IS 15% FULL LOAD

ERN 247-71

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PLANT UNLOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 100% FULL LOAD
FINAL POWER IS 15% FULL LOAD

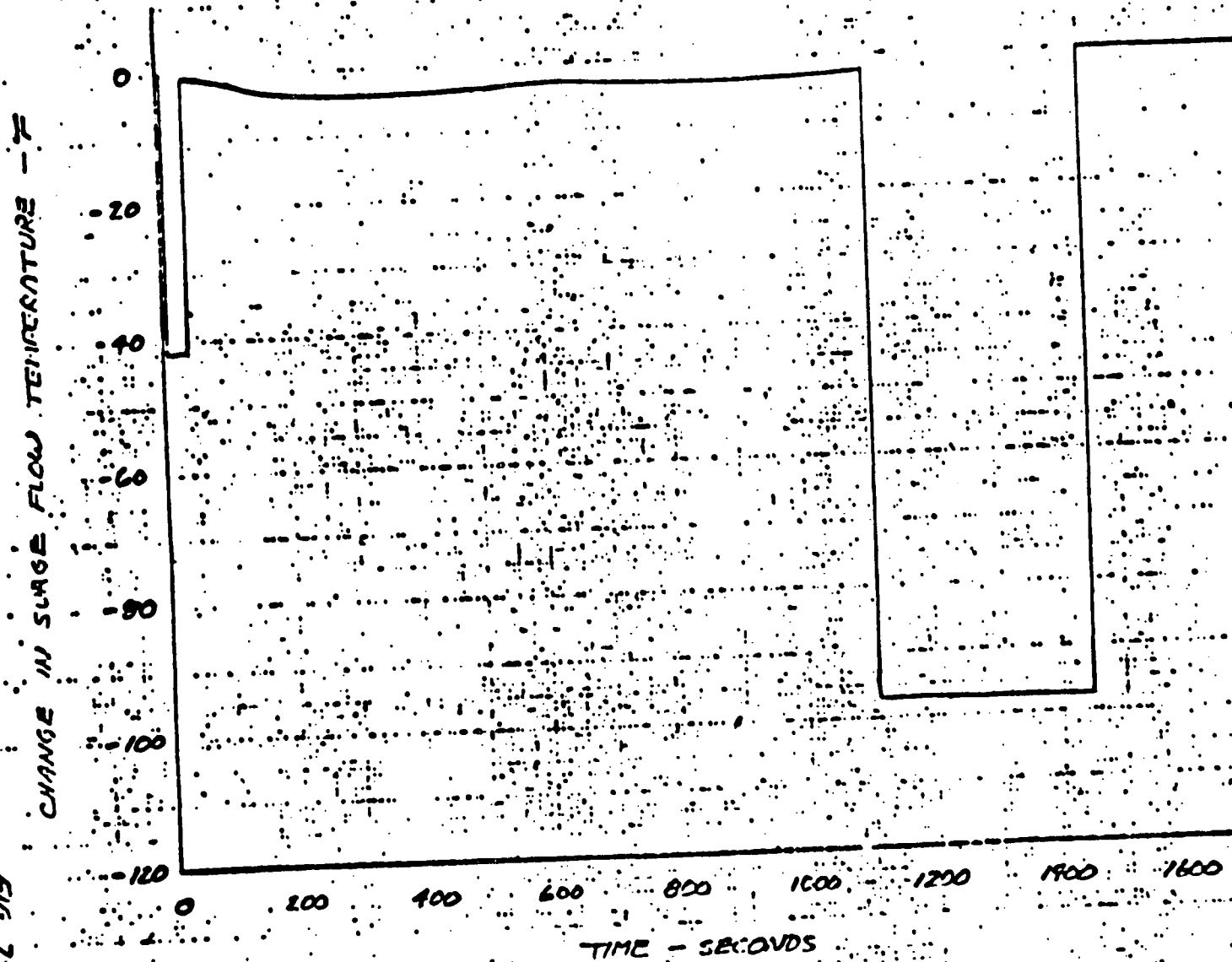


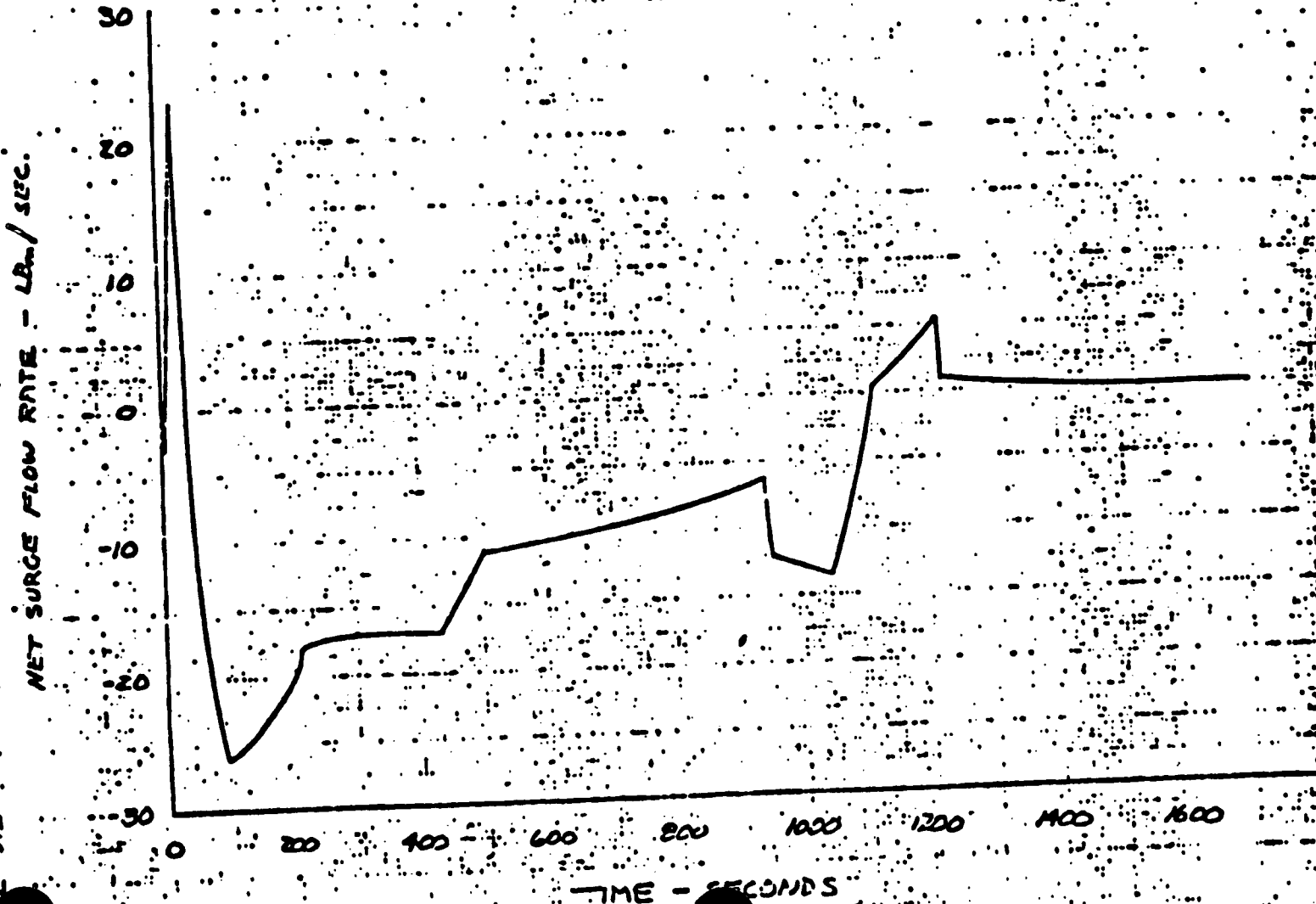
FIG 7-3

900-B-42-0

END 2-17-71

PLANT UNLOADING - 5% FULL LOAD PER MINUTE
INITIAL POWER IS 100% FULL LOAD
FINAL POWER IS 15% FULL LOAD

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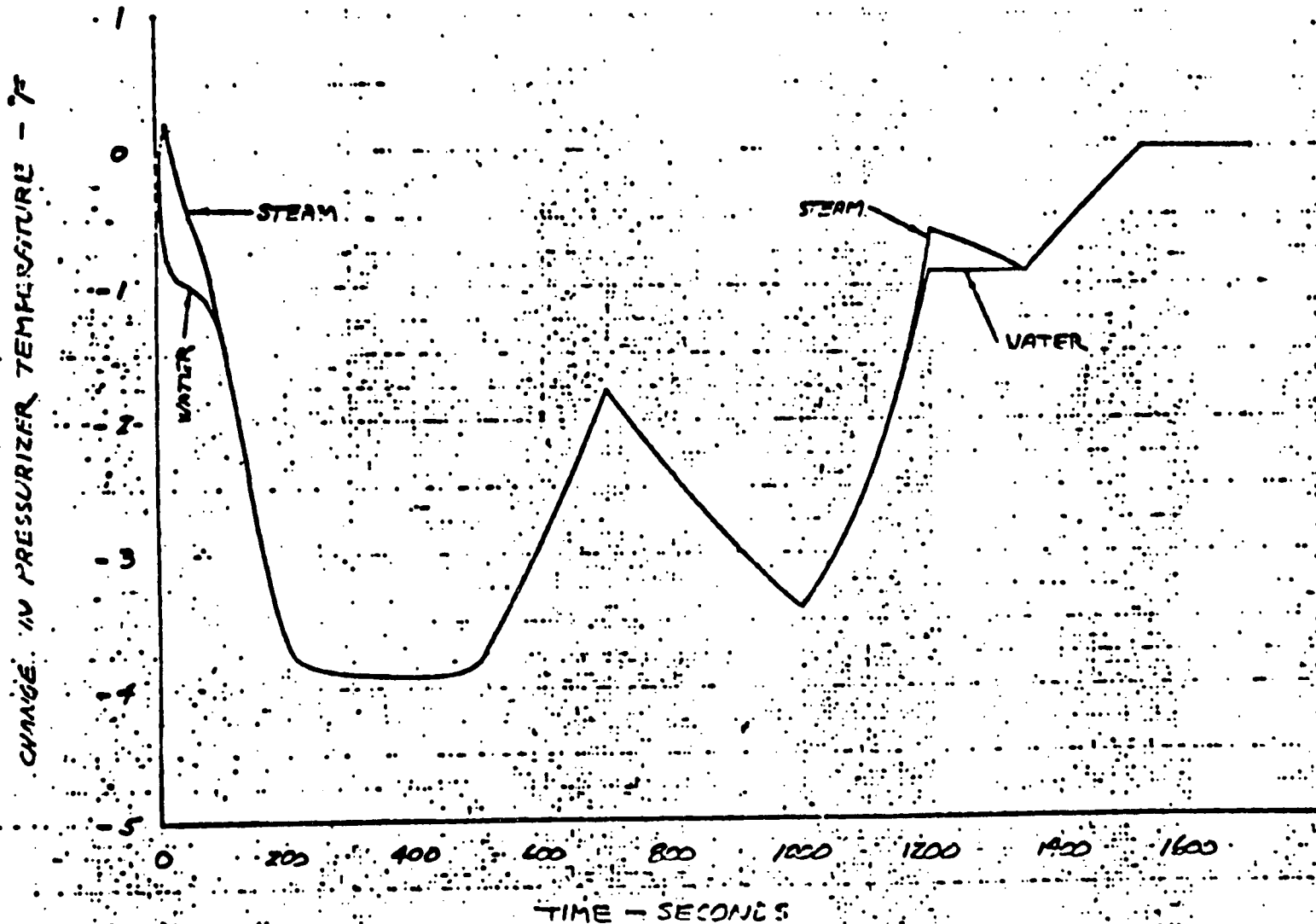


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FHS 7

ANT UNLOADING - 5% FULL LOAD PER MIN
INITIAL POWER IS 100% FULL LOAD
FINAL POWER IS 15% FULL LOAD

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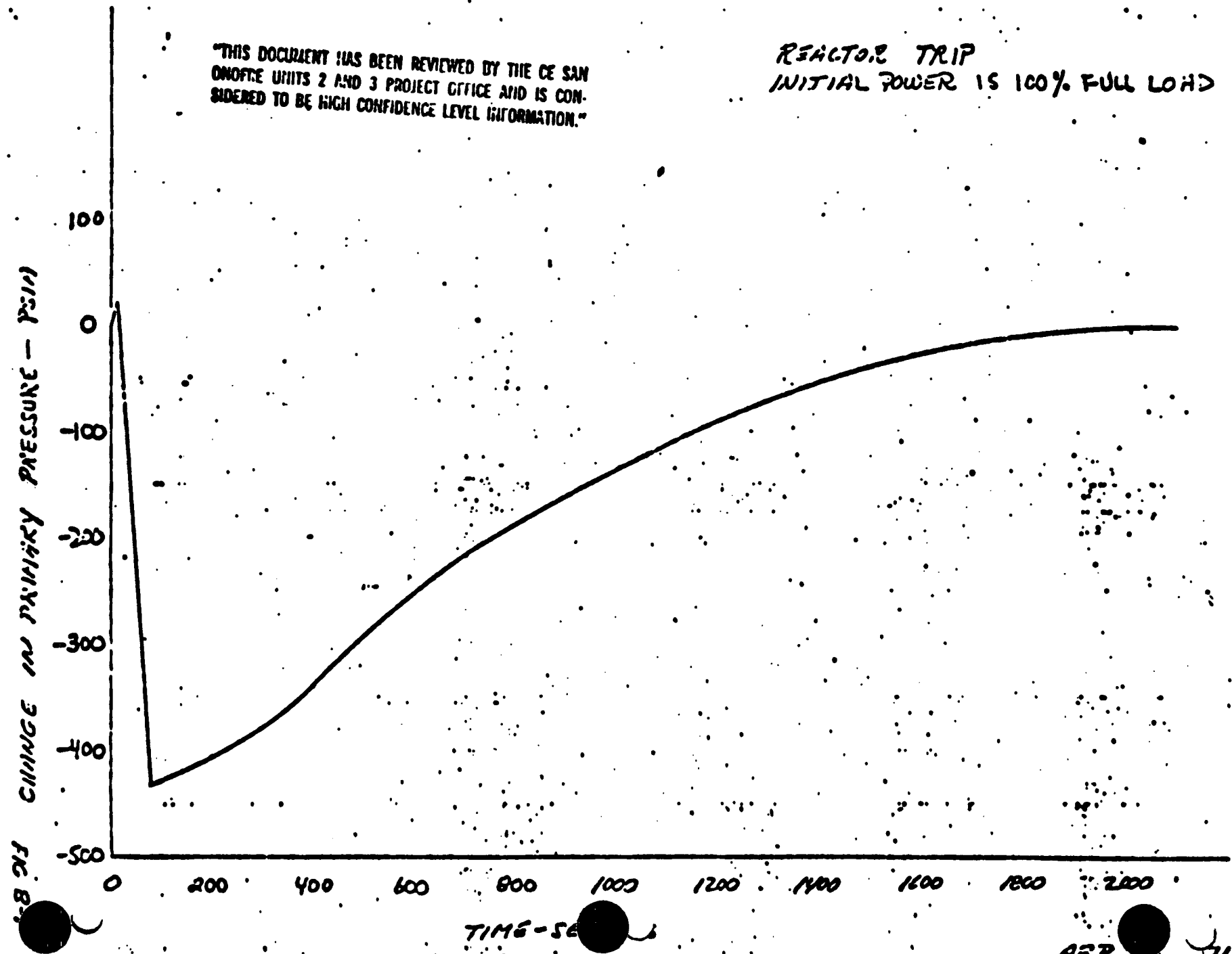
FIG 7-5

BN 2-12-71

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REACTOR TRIP
INITIAL POWER IS 100% FULL LOAD

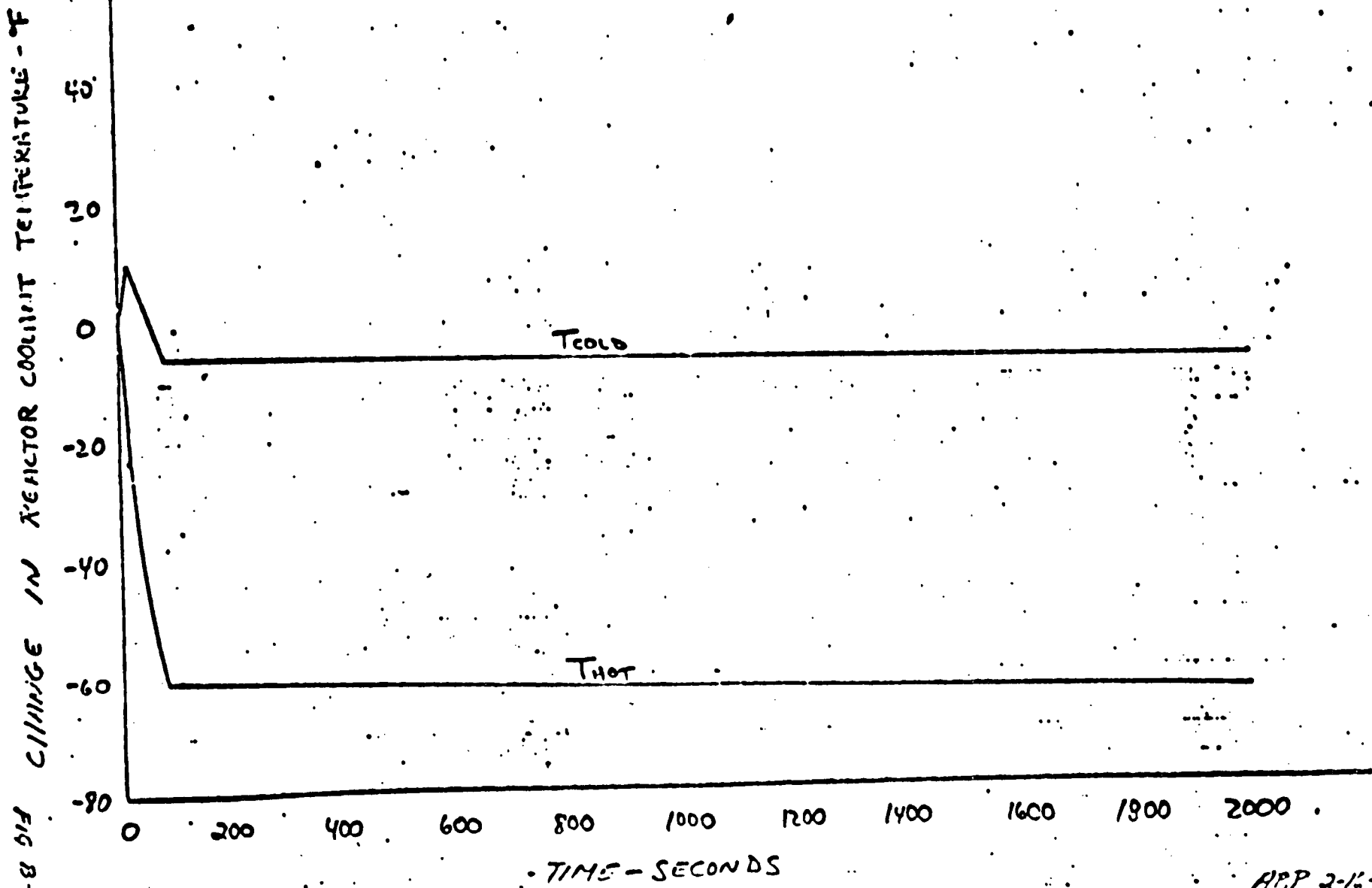
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REACTOR TRIP
INITIAL POWER IS 100% FULL LOAD

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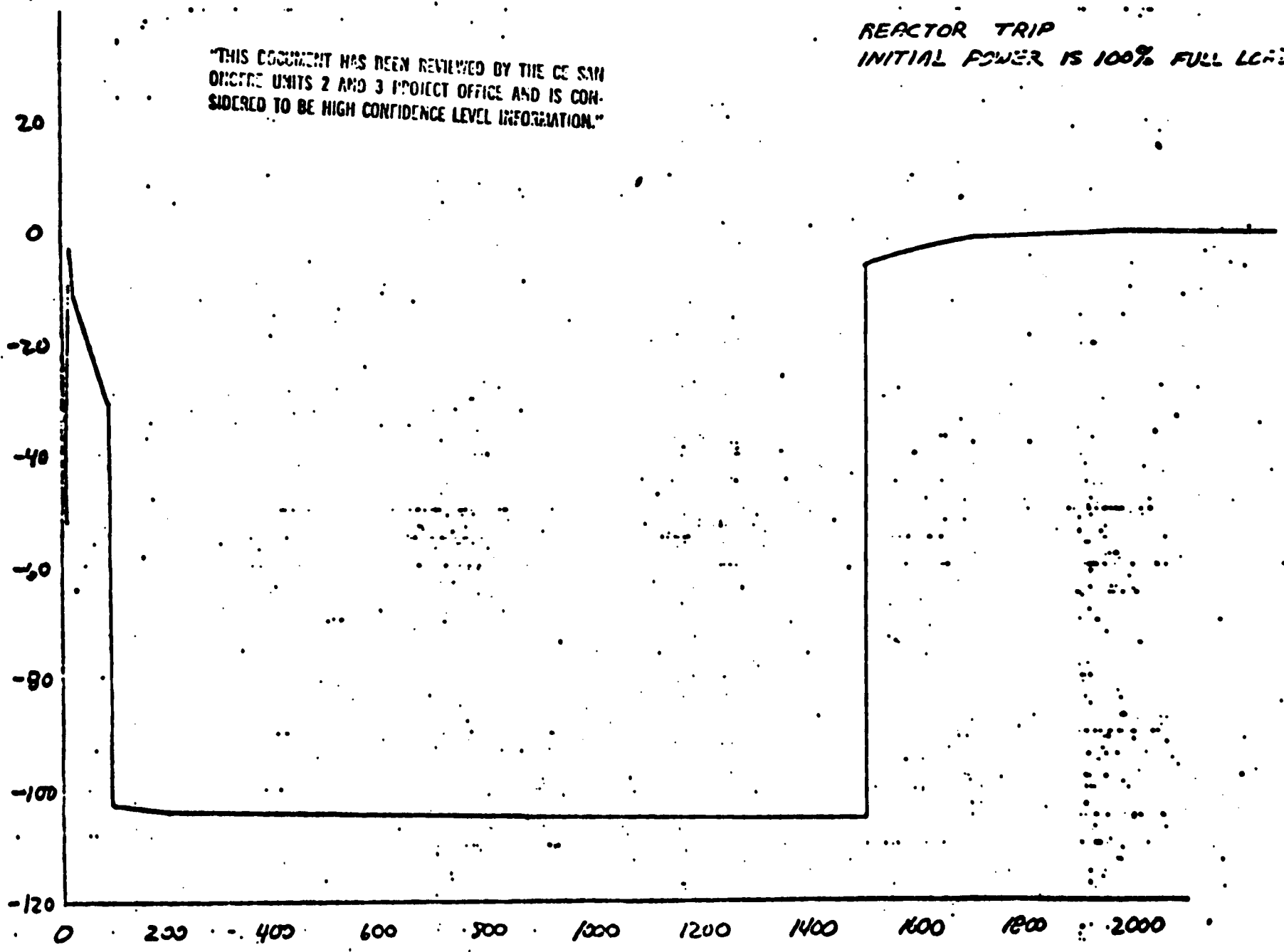
FIG B-2

ABP 2-12-71

REACTOR TRIP
INITIAL POWER IS 100% FULL LOAD

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CHANGE IN SURFACE TEMPERATURE - F



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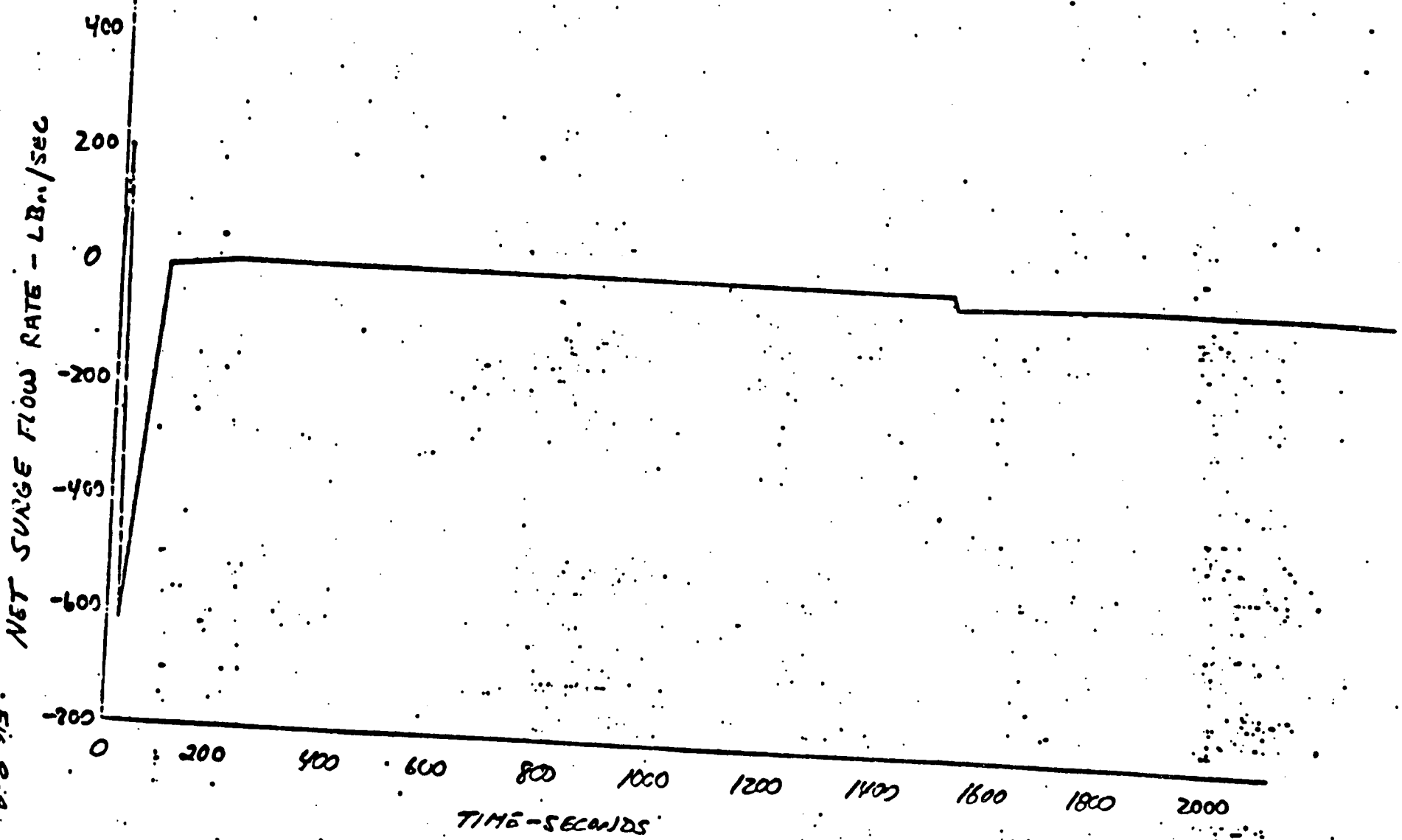
FIG 5-3

TIME - SECONDS

AB 11 71

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REACTOR TRIP
INITIAL POWER IS 100% (FULL LOAD)



900-B-42-0

FIG 9-4

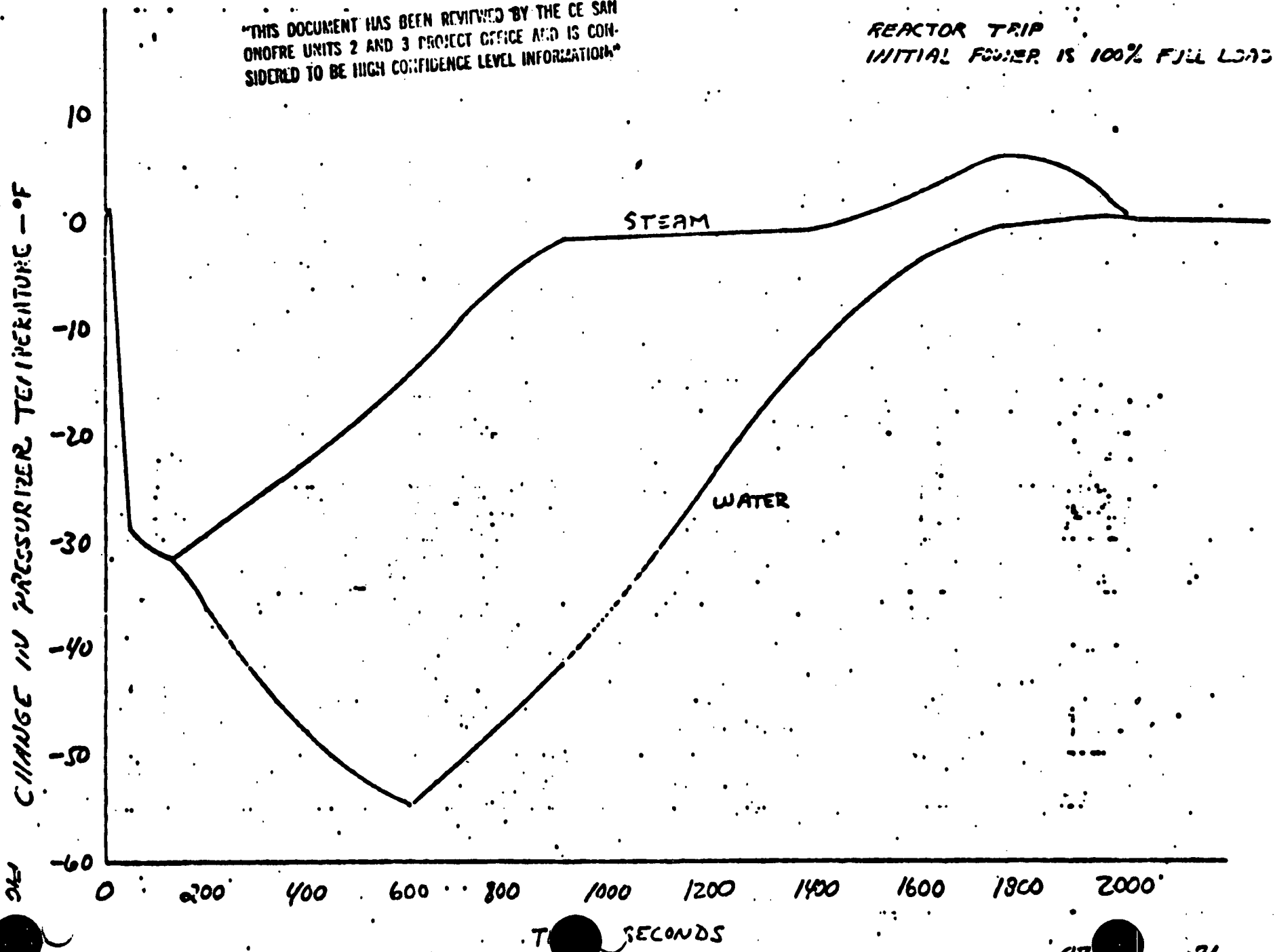
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37

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REACTOR TRIP
INITIAL POWER IS 100% FULL LOAD



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43 71

LOSS OF LOAD
INITIAL POWER IS 100% FULL LOAD

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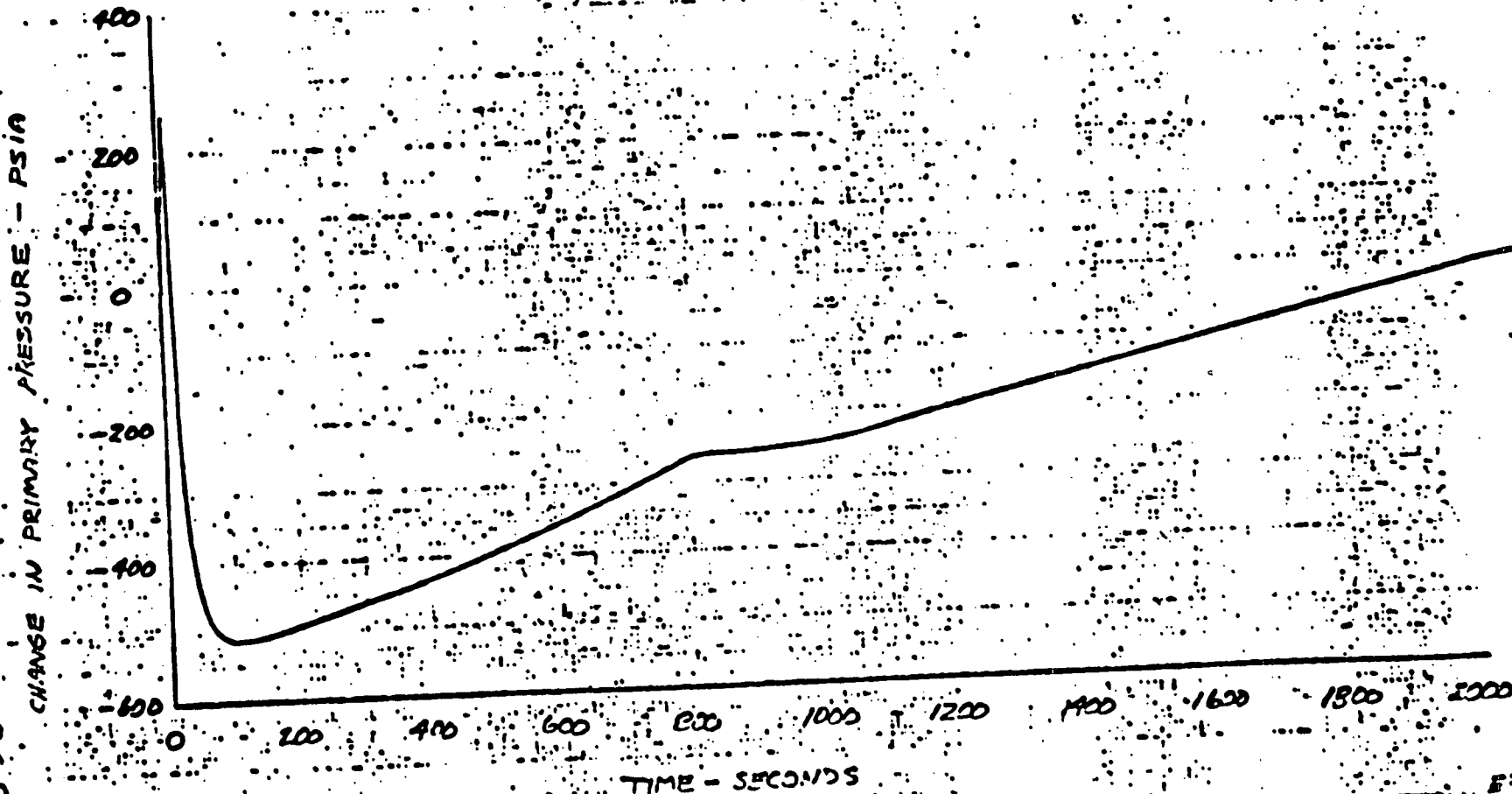


FIG 5-1

EPH 2-12

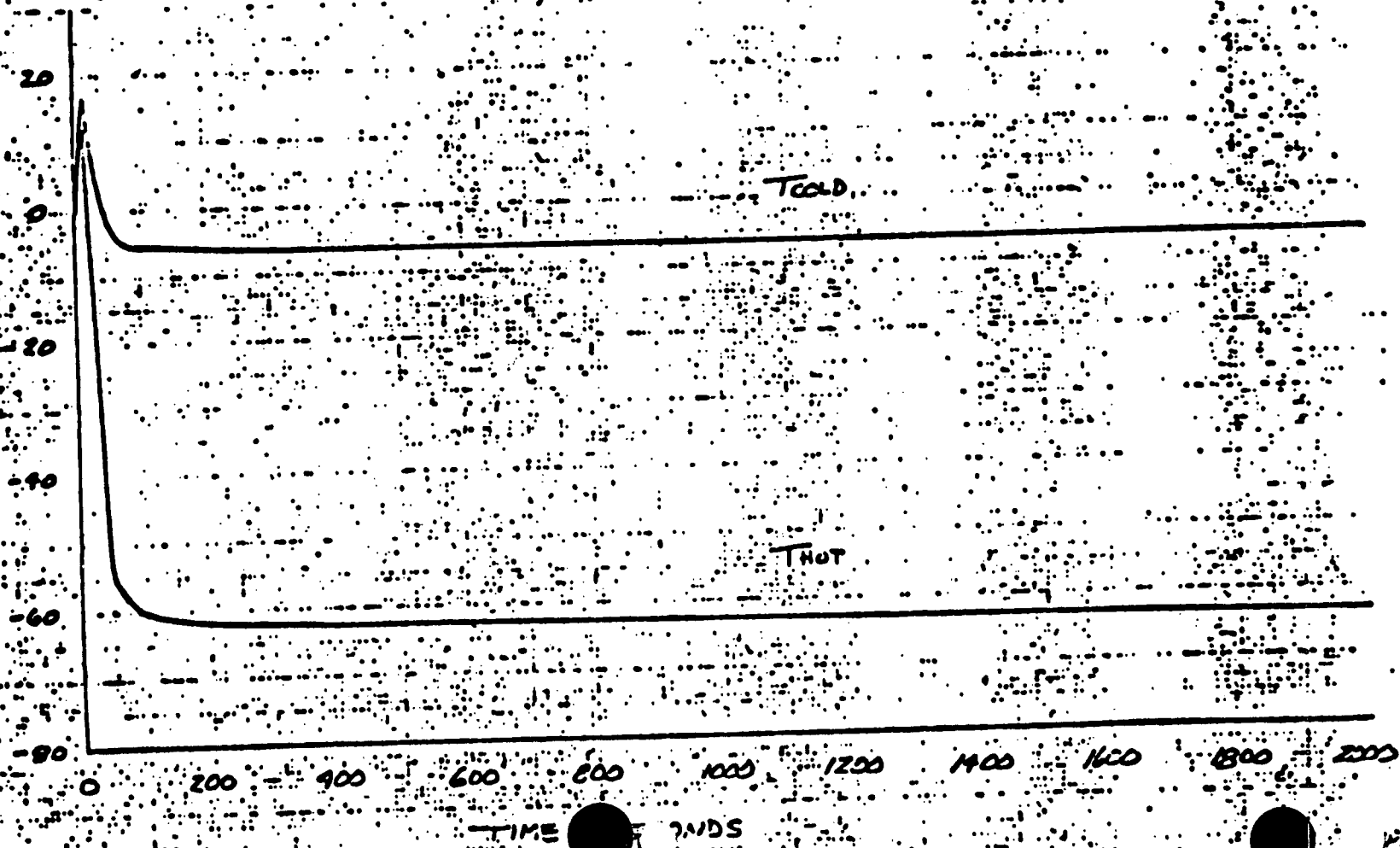
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LOSS OF LOAD
INITIAL POWER IS 100% FULL LOAD

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CHANGE IN REACTOR COOLANT TEMPERATURE - °F



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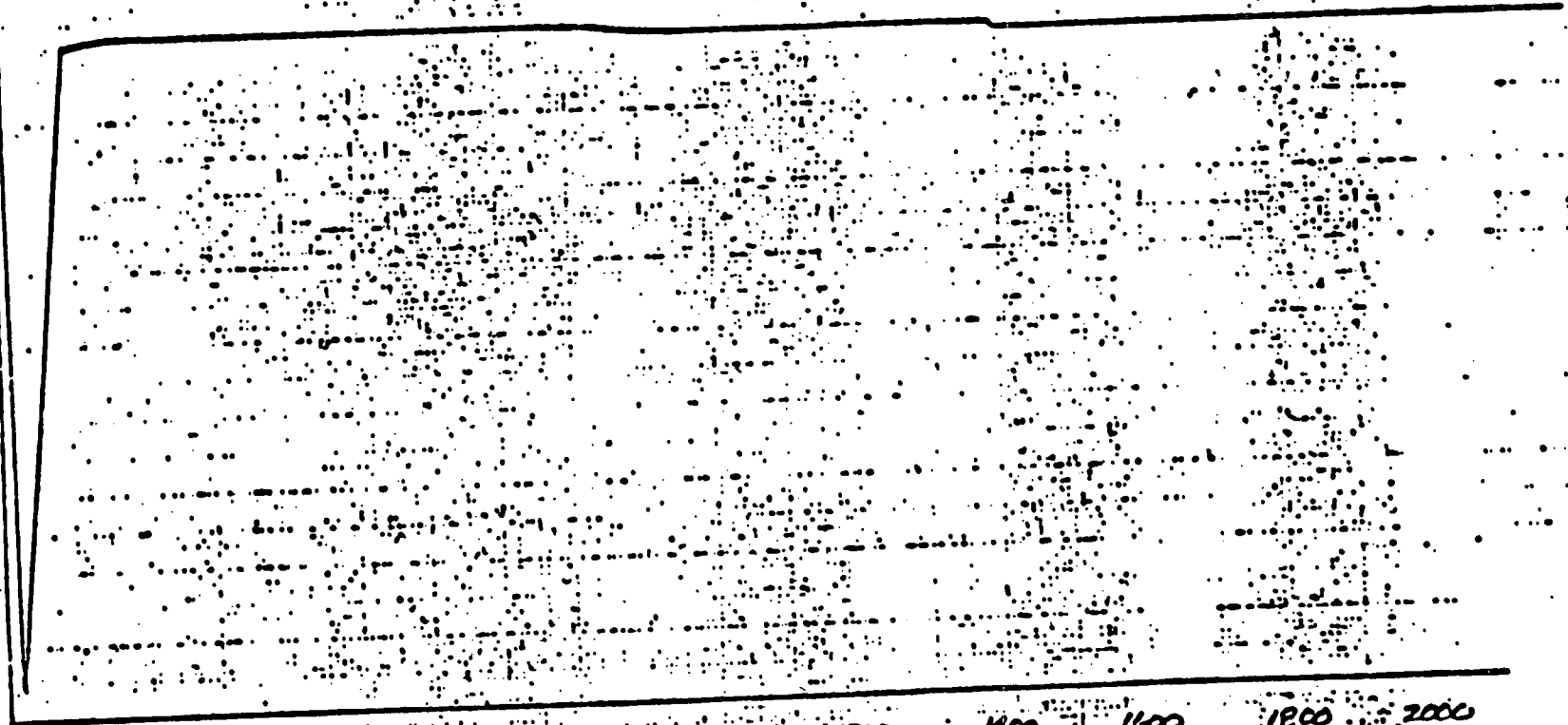
FIG. 2

LOSS OF LOAD
INITIAL POWER IS 100% FULL LOAD

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NET SURGE FLOW RATE - LTR / SEC.

700
600
500
400
300
200
100
0
-100
-200
-300
-400
-500
-600
-700
-800
-900



0 200 400 600 800 1000 1200 1400 1600 1800 2000
TIME - SECONDS

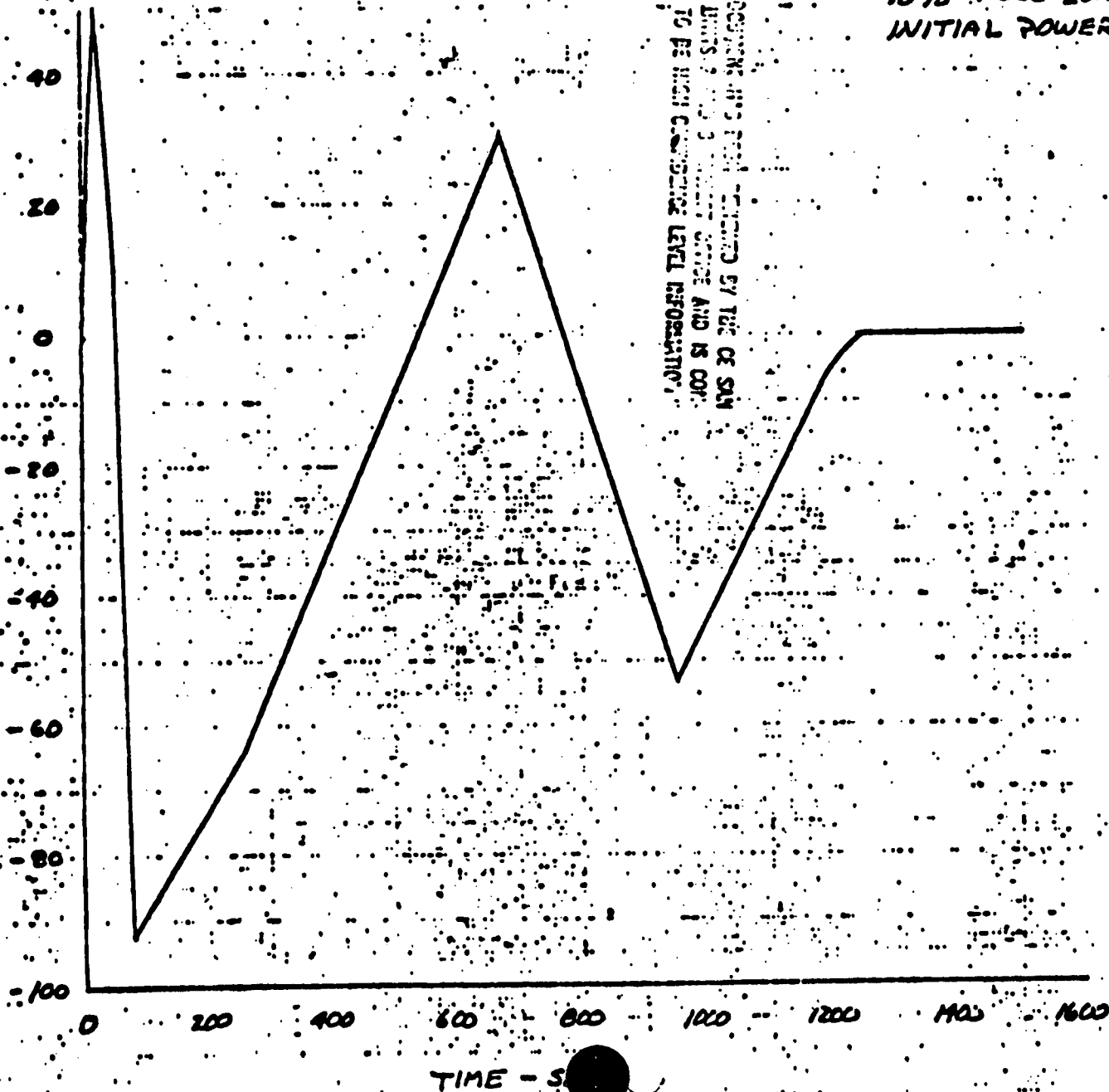
ERR 2-2

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FIG 9-1

900-B-42-0

CHANGE IN PRIMARY PRESSURE - PSIA



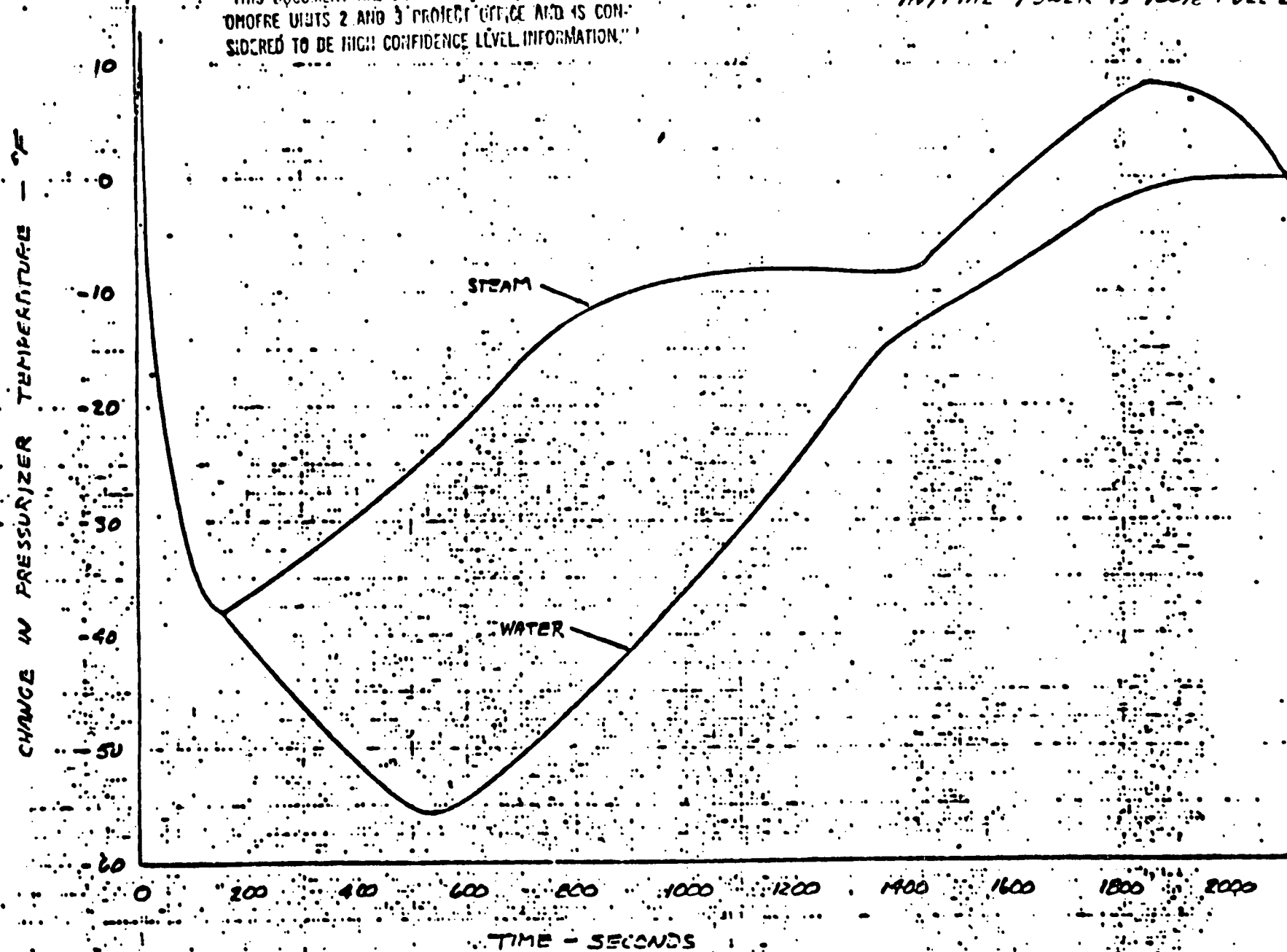
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STEP LOAD DECREASE
10% FULL LOAD STEP
INITIAL POWER IS 100% FULL LOAD

FIG

900-B-42-0

FIG 9-5



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LOSS OF LOAD
INITIAL POWER IS 100% FULL LOAD

ETM 2-571

10

10

LOSS OF FLOW
INITIAL POWER IS 100% FULL LOAD

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CHANGE IN PRIMARY PRESSURE - PSII

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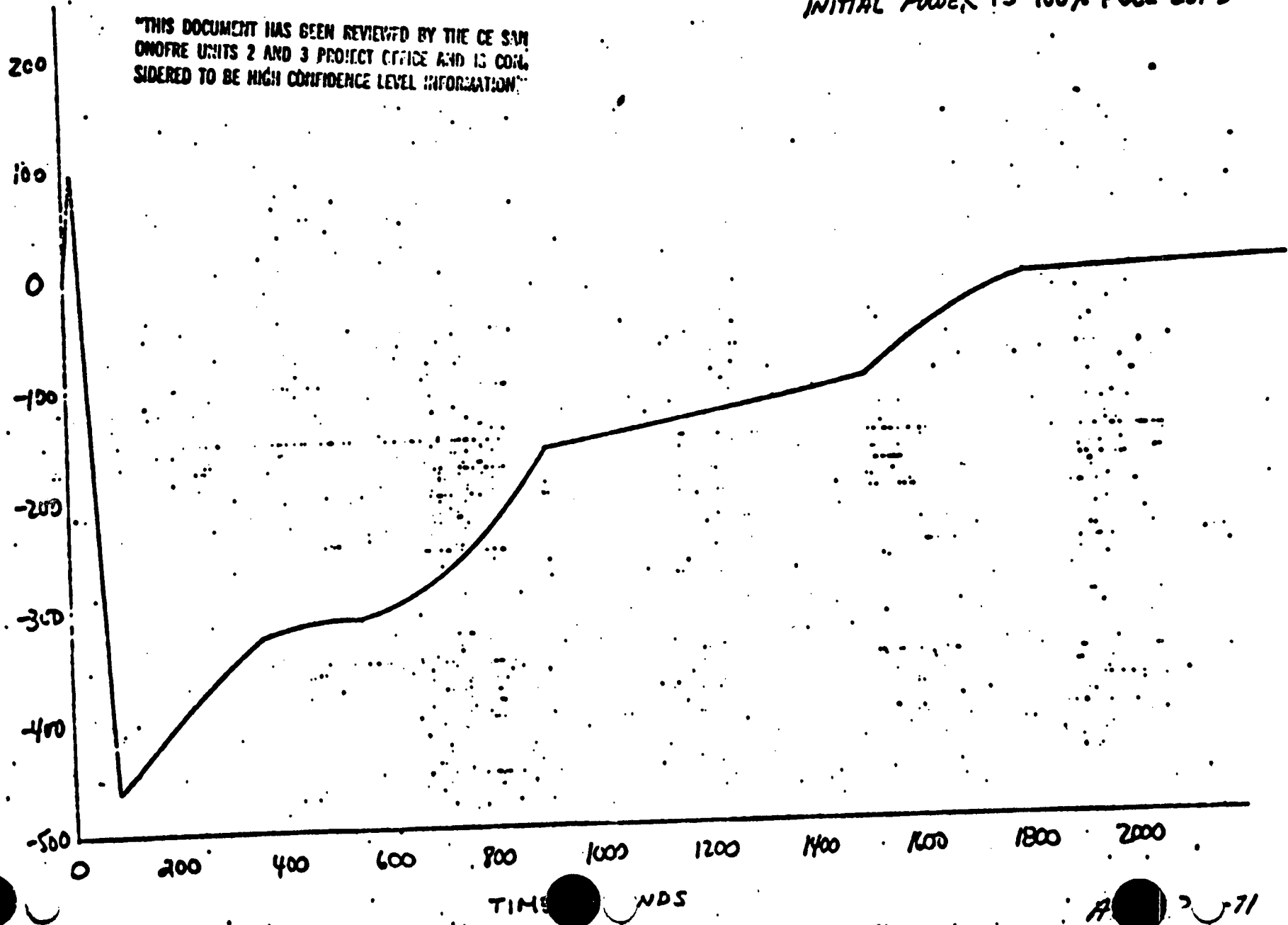


FIG.

TIME MDS

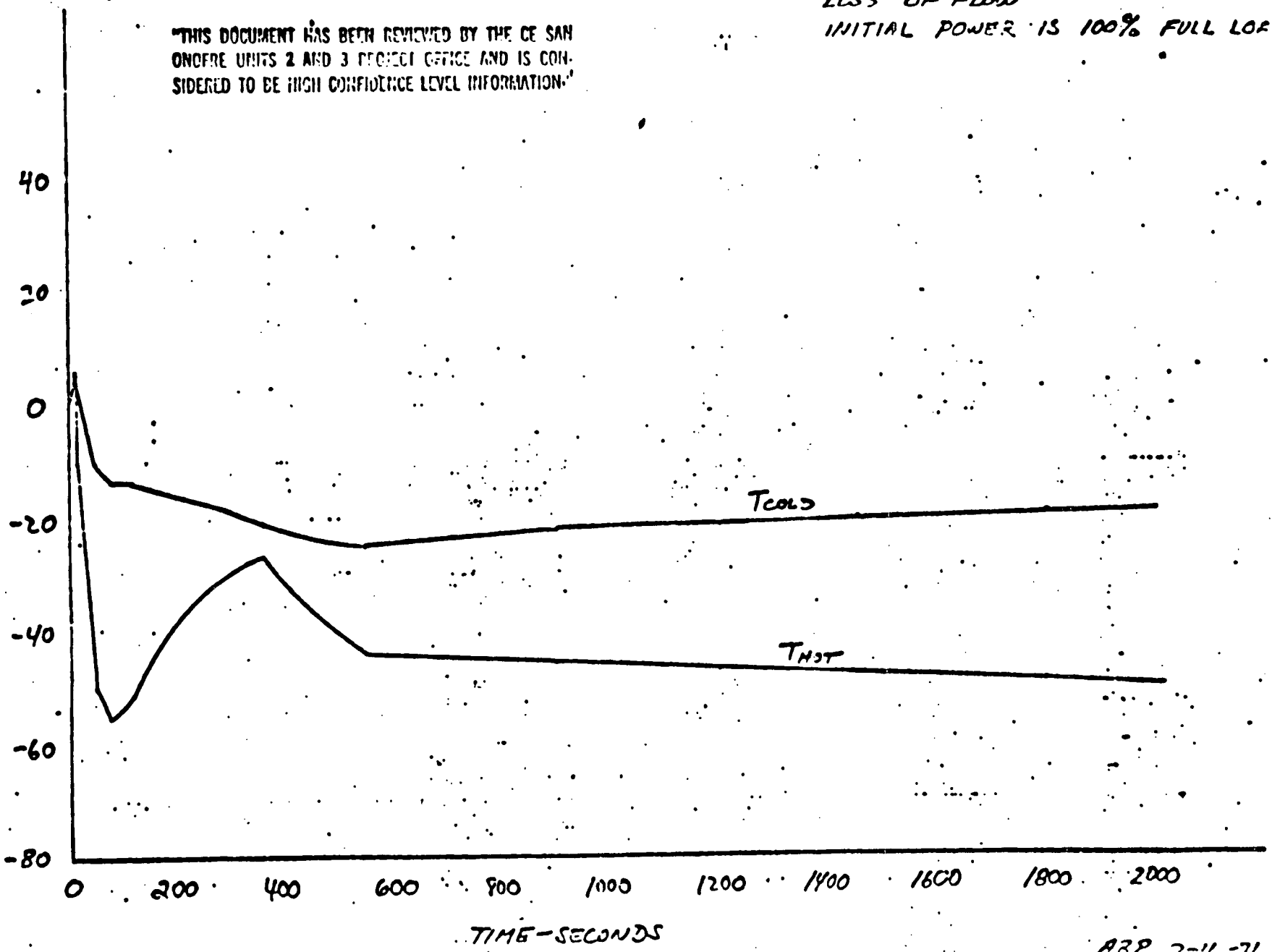
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CHANGE IN RECTOR COOLANT TEMPERATURE - °F

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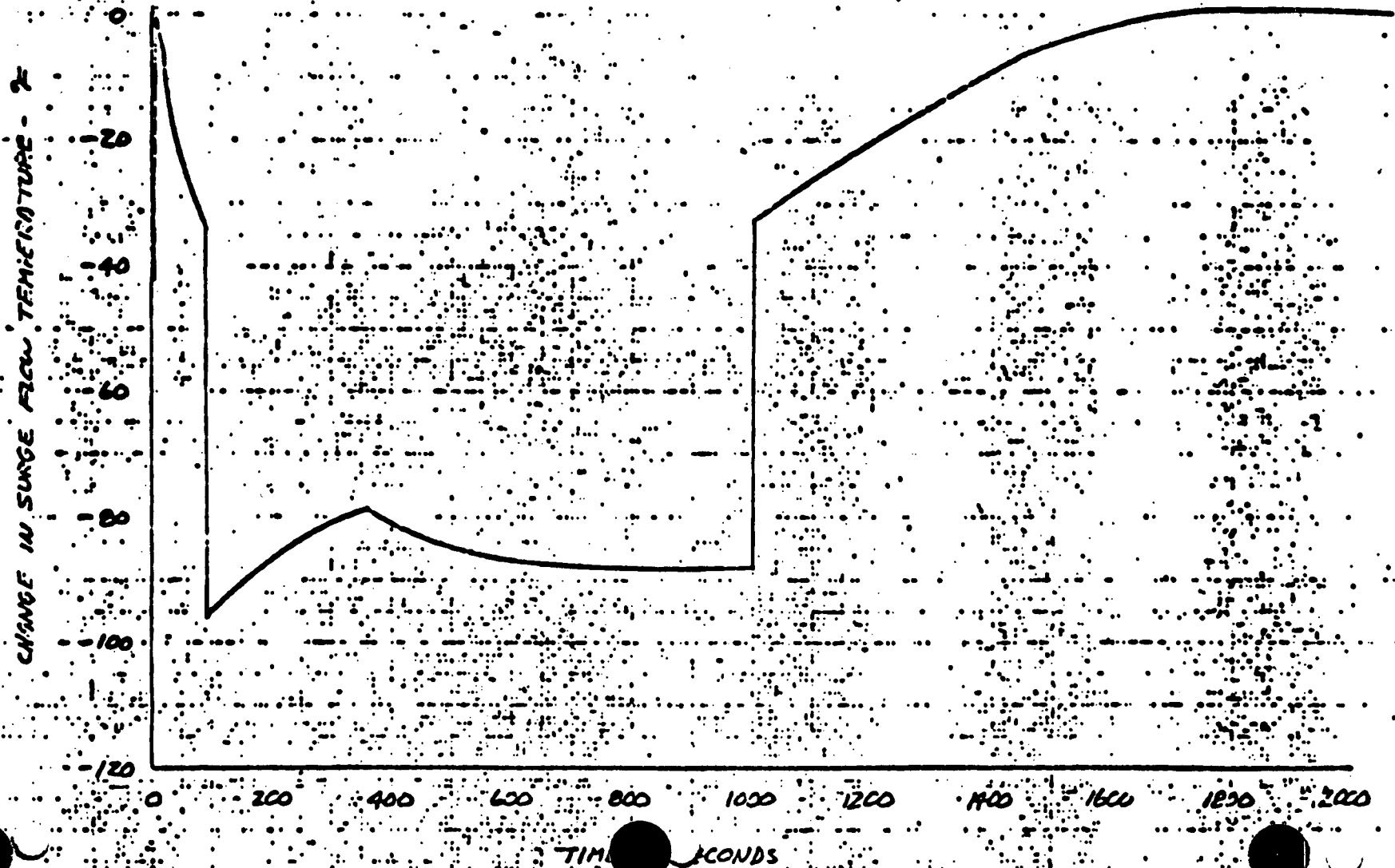
LOSS OF FLOW
INITIAL POWER IS 100% FULL LOAD



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LOSS OF FLOW
INITIAL POWER IS 100% FULL LOAD



900-B-42-0

FIG.

96
900-B-42-0

LOSS OF FLOW
INITIAL POWER IS 100% FULL LOAD

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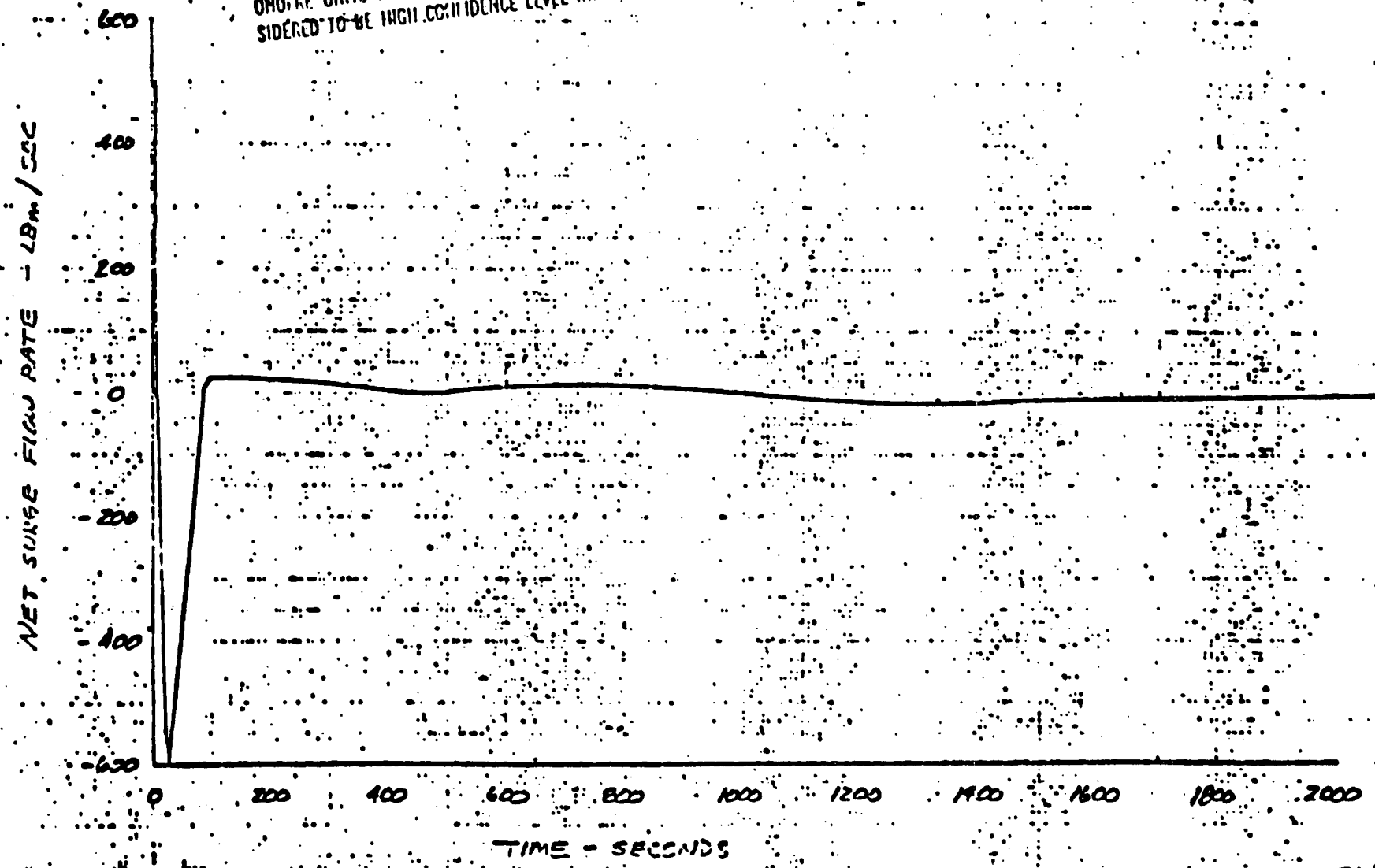


FIG 10-4

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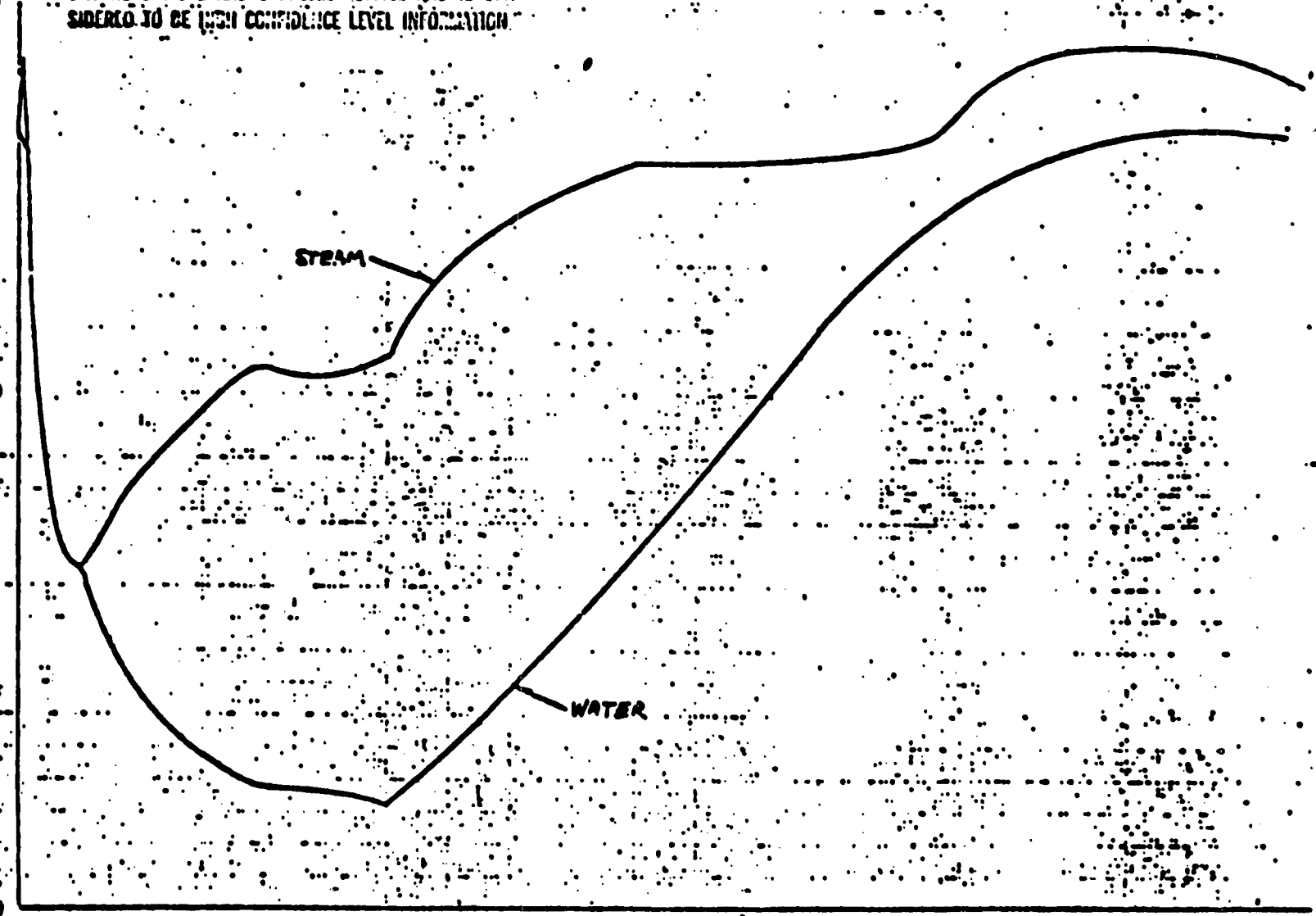
LOSS OF FLOW
INITIAL POWER IS 100% FULL LOAD

CHANGE IN PRESSURIZER TEMPERATURE - °F

10
0
-10
-20
-30
-40
-50
-60
-70

STEAM

WATER



0 200 400 600 800 1000 1200 1400 1600 1800 2000

TIME - SEC

900-B-42-0

FIG 1

LOSS OF SECONDARY PRESSURE

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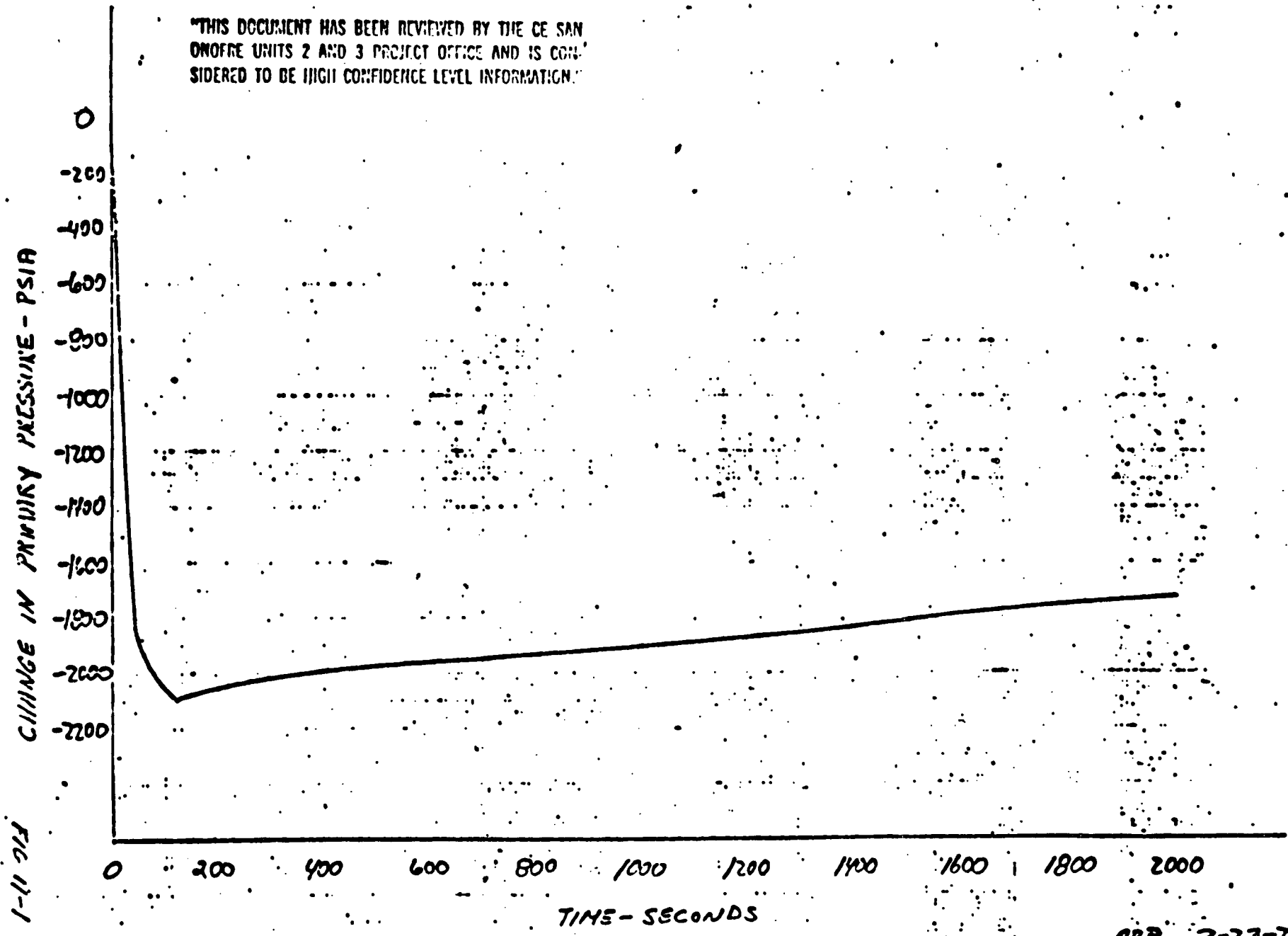


FIG 11-1

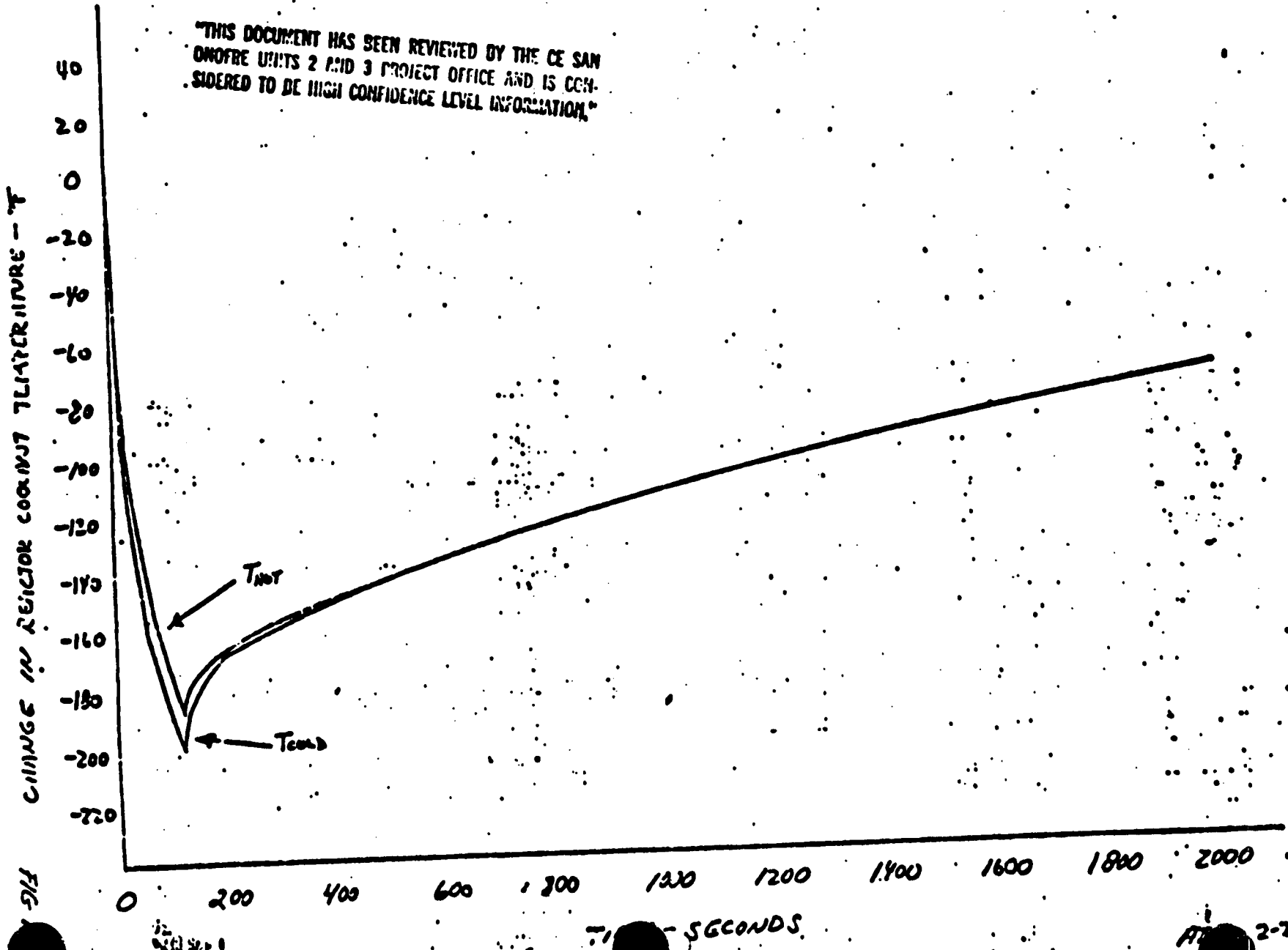
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D

LOSS OF SECONDARY PRESSURE

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FIG

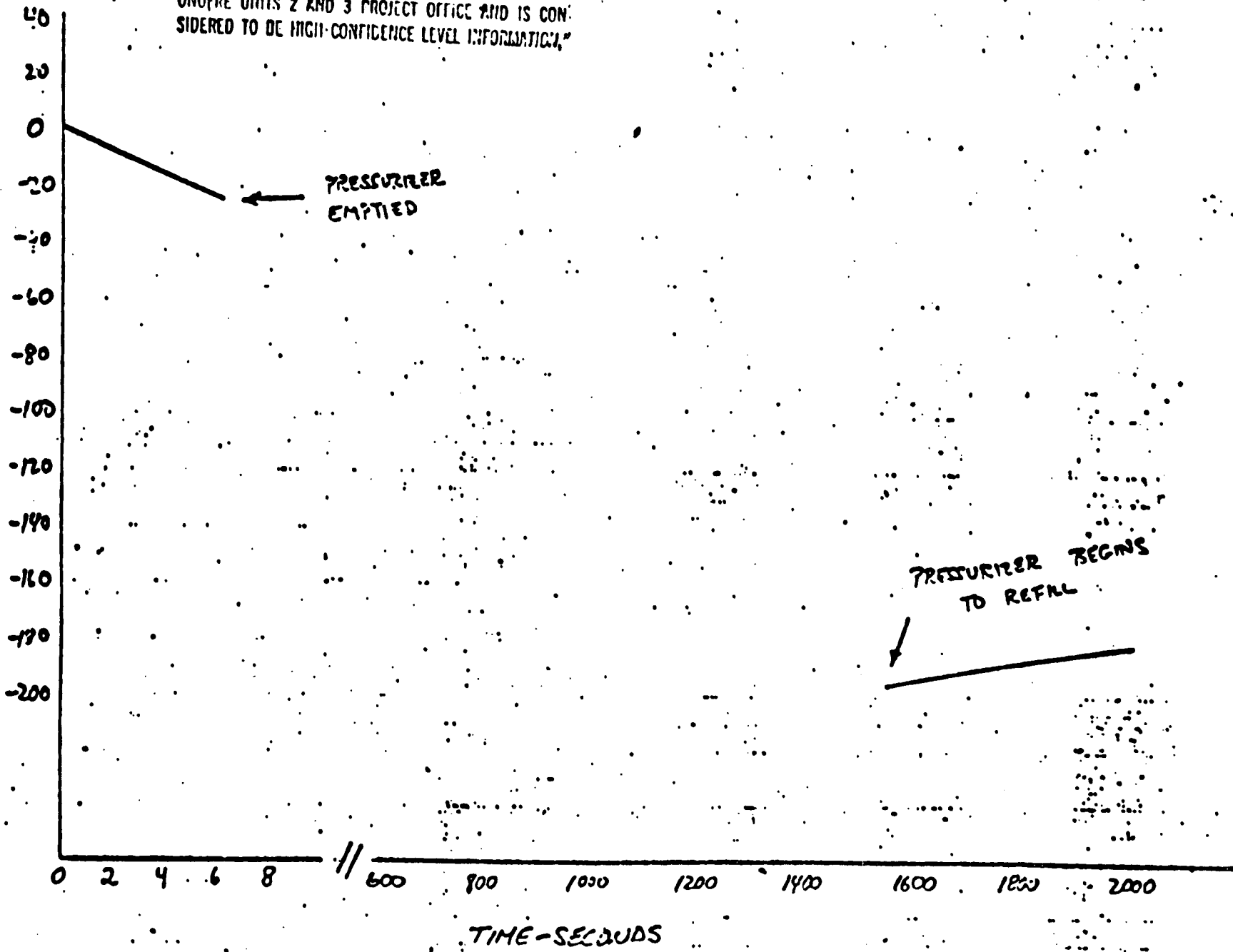
TIME - SECONDS

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LOSS OF SECONDARY PRESSURE

CHANGE IN SURGE FLOW TEMPERATURE - °F



900-B-42-0

FIG 11-3

57

10

LOSS OF SECONDARY PRESSURE

PRESSURIZER BEGINS TO REFILL

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PRESSURIZER EMPTIED

900-B-42-0

NET SURGE FLOW RATE - LPM/SEC

0
-200
-400
-600
-800
-1000
-1200
-1400
-1600
-1800
-2000
-2200
-2400
-2600
-2800
-3000

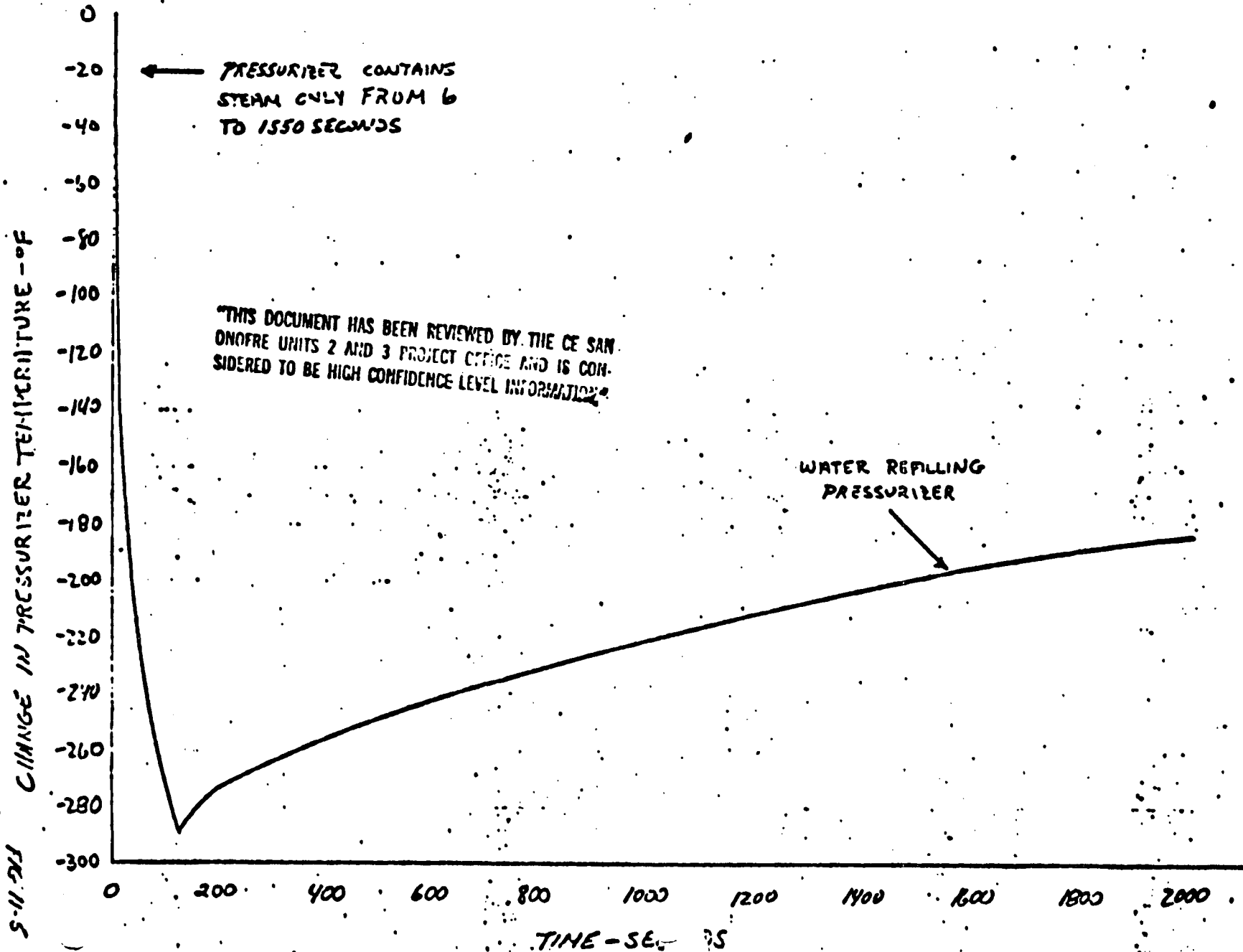
0 2 4 6 8 // 600 800 1200 1400 1600 1800 2000

TIME - SECONDS

ARP 7-13-71



LOSS OF SECONDARY PRESSURE



900-B-42-0

FIG. 11.5 CHANGE IN PRESSURIZER TEMPERATURE - °F

APPENDIX D

NOZZLE DISPLACEMENTS

1. Seismic N-D Pages 1-22
(Enclosure to Combustion Engineering to Bechtel
Letter, S-CE-1137, dated May 27, 1974.)
2. Thermal and Dead Weight N-D Pages 23-32
(Enclosure (1) of Combustion Engineering to Bechtel
Letter, S-CE-3228, dated Sept. 8, 1976)
3. Pipe Rupture N-D Pages 33-36
(Enclosure (3) of Combustion Engineering to Bechtel
Letter, S-CE-3228, dated September 8, 1976.)
4. Unit 3 RCS Nozzle Movement (Thermal and Weight). . . Pages 37-47
(Enclosure (1,2) of Combustion Engineering to Bechtel)
(Letter-SCE-4113, dated August 9, 1977)

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, X-RESPONSE DUE TO X-OBE

MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS
 LOCATION DIRECTION MAX. REL. DISPL (IN) TIME (SEC)
 GLOBAL

Table 1

SURGE LINE NOZZLE,	JOINT 750	DISP X	-.53994E-01	45.0650
		Y	-.28249E-01	45.0600
		Z	-.77341E-03	45.0500
		ROTN X	-.17478E-05	6.9150
		Y	.94421E-05	45.0525
		Z	-.12354E-03	45.0275
SHUTDOWN COOLING NOZ.,	JOINT 3750	DISP X	-.76245E-01	45.0650
		Y	.26259E-01	45.0600
		Z	-.67250E-03	45.0500
		ROTN X	-.17635E-05	6.9150
		Y	-.34358E-05	45.0525
		Z	-.12376E-03	45.0275
S.G. FEED WATER NOZ.,	JOINT 301	DISP X	-.60961E-01	9.0450
		Y	.29022E-01	45.0575
		Z	.56929E-03	45.0450
		ROTN X	.46155E-05	19.9550
		Y	.36103E-05	45.0550
		Z	-.18691E-03	45.0575
S.G. FEED WATER NOZ.,	JOINT 3301	DISP X	-.60981E-01	9.0450
		Y	-.29022E-01	45.0575
		Z	.56938E-03	45.0450
		ROTN X	.48196E-06	19.5550
		Y	-.36113E-05	45.0650
		Z	-.15681E-03	45.0575
S.G. BOT BLOWDOWN NOZ.	JOINT 418	DISP X	-.53297E-01	45.0175
		Y	-.62111E-03	45.0200
		Z	-.13268E-03	53.7325
		ROTN X	-.10975E-05	19.5275
		Y	.63025E-05	45.0550
		Z	-.16722E-03	45.0600
S.G. BOT BLOWDOWN NOZ.	JOINT 3413	DISP X	-.53297E-01	45.0175
		Y	.61111E-03	45.0200
		Z	-.13252E-03	53.7325
		ROTN X	-.10973E-05	19.5275
		Y	-.67037E-05	45.0550
		Z	-.16721E-03	45.0500
SAFETY INJECTION NOZ.,	JOINT 1765	DISP X	-.61178E-01	45.0300
		Y	.80387E-02	10.3325
		Z	-.16283E-01	45.0475
		ROTN X	.04105E-04	9.1825
		Y	-.91859E-04	9.4700
		Z	-.48795E-04	45.0500
SAFETY INJECTION NOZ.,	JOINT 2765	DISP X	-.47747E-01	45.0650
		Y	.11047E-01	10.3350
		Z	.29914E-01	9.1825
		ROTN X	.63769E-07	45.0450
		Y	-.34249E-04	23.8350
		Z	-.76628E-04	45.0175
SAFETY INJECTION NOZ.,	JOINT 4765	DISP X	-.47745E-01	45.0550
		Y	-.11046E-01	10.3350
		Z	.24914E-01	9.1325

LOCATION	DIRECTION GLOBAL	MAX. REL. DISPL. (IN)	TIME (SEC)	
Table 1				
SAFETY INJECTION NOZ.,	JOINT 5765	ROTN X	.63769E-04	45.0650
		Y	.34247E-04	23.8850
		Z	-.75530E-04	45.0175
		DISP X	-.61177E-01	45.0300
		Y	-.80878E-02	10.3325
		Z	-.18282E-01	45.0475
		ROTN X	.84101E-04	9.1825
		Y	.91859E-04	9.4400
		Z	-.45793E-04	45.0500
PRESURIZER SPRAY NOZ.,	JOINT 1757	DISP X	-.64055E-01	45.0300
		Y	.56009E-02	45.3325
		Z	-.18094E-01	45.0475
		ROTN X	.53810E-04	23.9400
		Y	.17471E-03	45.0300
		Z	.82254E-04	10.3325
		DISP X	-.53858E-01	45.0300
		Y	.76801E-02	10.3350
		Z	.25769E-01	9.1825
PRESURIZER SPRAY NOZ.,	JOINT 2757	DISP X	-.60032E-04	10.3375
		Y	.26815E-03	45.0650
		Z	.93054E-04	10.3325
		DISP X	-.63577E-01	45.0300
		Y	.39757E-02	10.3325
		Z	-.13956E-01	45.0475
		ROTN X	.84103E-04	9.1825
		Y	-.91859E-04	9.4400
		Z	-.46795E-04	45.0500
CHARGING INLET NOZZLE,	JOINT 1780	DISP X	-.63579E-01	45.0300
		Y	-.89755E-02	10.3325
		Z	-.13955E-01	45.0475
		ROTN X	.84101E-04	9.1825
		Y	.91859E-04	9.4400
		Z	-.46793E-04	45.0500
		DISP X	-.10702E+00	9.0475
		Y	.54728E-03	35.3900
		Z	.23812E-03	63.6150
CHARGING INLET NOZZLE,	JOINT 5780	DISP X	.52313E-06	19.5550
		Y	.34478E-05	45.0550
		Z	-.16936E-03	45.0575
		DISP X	-.10702E+00	9.0475
		Y	-.56717E-03	35.3900
		Z	.23507E-03	63.6150
		ROTN X	.52314E-06	19.5550
		Y	-.34491E-05	45.0650
		Z	-.16965E-03	45.0575
S.G. OUTLET NOZZLE,	JOINT 102	DISP X	-.12440E+00	45.0650
		Y	-.11452E-05	36.4750
		Z	-.17823E-02	6.9100
		ROTN X	.43296E-05	9.4050
		Y	.10338E-03	45.0575
		Z	.29480E-03	45.0300
		DISP X	-.78229E-01	45.0650
		Y	-.28249E-01	45.0500
		Z	-.67145E-03	45.0500
S.G. OUTLET NOZZLE,	JOINT 3102	DISP X	-.17479E-05	6.9130
		Y	.94421E-05	45.0525
		Z	-.12354E-03	45.0275
		DISP X	-.12440E+00	45.0650
		Y	-.11452E-05	36.4750
		Z	-.17823E-02	6.9100
		ROTN X	.43296E-05	9.4050
		Y	.10338E-03	45.0575
		Z	.29480E-03	45.0300
REACTOR VESSEL HEAD,	JOINT 9991	DISP X	-.78229E-01	45.0650
		Y	-.28249E-01	45.0500
		Z	-.67145E-03	45.0500
		ROTN X	-.17479E-05	6.9130
		Y	.94421E-05	45.0525
		Z	-.12354E-03	45.0275
		DISP X	-.78229E-01	45.0650
		Y	-.28249E-01	45.0500
		Z	-.67145E-03	45.0500
SHUTDN COLNG OUT NOZ.,	JOINT 753	DISP X	-.17479E-05	6.9130
		Y	.94421E-05	45.0525
		Z	-.12354E-03	45.0275

LOCATION	DIRECTION GLOBAL	MAX. REL. DISPL (IN)	TIME (SEC)
----------	---------------------	----------------------	------------

Table 1

DRAIN NOZZLE, HL,	JOINT 754 DISP X	-.74851E-01	45.0650
	Y	-.30385E-01	45.0500
	Z	-.82710E-03	45.0500
	ROTN X	-.19826E-05	6.9150
	Y	.10818E-04	45.0525
	Z	-.10212E-03	45.0175
DRAIN NOZZLE, 1A CL,	JOINT 1586 DISP X	-.82219E-01	45.0625
	Y	-.39354E-02	9.2375
	Z	.10178E-01	45.0525
	ROTN X	-.53353E-04	19.5075
	Y	.58145E-04	23.0875
	Z	.75512E-04	45.4000
DRAIN NOZZLE, 1B CL,	JOINT 2586 DISP X	-.91445E-01	45.0650
	Y	.54858E-02	45.0650
	Z	-.11762E-01	45.0650
	ROTN X	.14062E-03	45.0350
	Y	-.44821E-04	38.3250
	Z	-.14069E-03	45.0650
DRAIN NOZZLE, 2B CL,	JOINT 4586 DISP X	-.91443E-01	45.0650
	Y	-.54856E-02	45.0650
	Z	-.11761E-01	45.0650
	ROTN X	.15061E-03	45.0350
	Y	.44814E-04	38.3250
	Z	-.16088E-03	45.0650
DRAIN NOZZLE, 2A CL,	JOINT 5586 DISP X	-.82226E-01	45.0625
	Y	.39370E-02	9.2375
	Z	.10175E-01	45.0525
	ROTN X	-.53340E-04	19.5075
	Y	-.56159E-04	23.0875
	Z	.73398E-04	45.4000

Table 2

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, Y-RESPONSE DUE TO X-OBE
 MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
SURGE LINE NOZZLE, JOINT 750 DISP	X	.45206E-02	45.0425
	Y	.13568E-01	45.0175
	Z	-.36130E-03	45.0600
ROTN	X	-.81914E-06	45.0550
	Y	-.19914E-05	45.0400
	Z	-.11338E-03	45.0225
SHUTDOWN COOLING NOZ., JOINT 3750 DISP	X	-.57034E-02	45.0175
	Y	-.12388E-01	7.5950
	Z	.27996E-03	45.3400
ROTN	X	-.72432E-06	9.4225
	Y	.16849E-05	45.0400
	Z	-.11915E-03	45.0175
S.G. FEEDWATER NOZ., JOINT 301 DISP	X	-.54097E-03	55.7475
	Y	.23714E-01	45.0200
	Z	.37637E-03	45.0600
ROTN	X	-.41273E-06	35.8500
	Y	.24296E-05	45.0600
	Z	-.49030E-05	31.2675
S.G. FEEDWATER NOZ., JOINT 3301 DISP	X	-.53035E-03	55.7475
	Y	-.24358E-01	7.5950
	Z	.30307E-03	45.0300
ROTN	X	-.48417E-06	35.8500
	Y	-.19522E-05	45.0300
	Z	-.47058E-05	9.0925
S.G. BOT BLOWDOWN NOZ. JOINT 418 DISP	X	.13636E-02	31.2425
	Y	.20260E-01	45.0200
	Z	.35225E-04	30.2050
ROTN	X	.50918E-06	17.6950
	Y	.42409E-05	45.0600
	Z	.28702E-05	7.9025
S.G. BOT BLOWDOWN NOZ. JOINT 3418 DISP	X	-.13690E-02	9.0925
	Y	-.18100E-01	45.0175
	Z	.47163E-04	30.2025
ROTN	X	.56437E-06	17.6125
	Y	-.34079E-05	45.0300
	Z	.27402E-05	23.3175
SAFETY INJECTION NOZ. JOINT 1765 DISP	X	-.28402E-02	9.1550
	Y	-.16830E-01	30.1800
	Z	-.17044E-02	45.0350
ROTN	X	.39239E-04	45.3450
	Y	-.66736E-05	35.7950
	Z	-.63122E-04	45.0300

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
SAFETY INJECTION NOZ. JOINT 2765 DISP	X	-.37290E-02	30.1800
	Y	-.16398E-01	30.1800
	Z	.15055E-02	27.5425
ROTN	X	-.20227E-04	45.3450
	Y	-.12979E-04	35.7300
	Z	-.81221E-04	45.0300
SAFETY INJECTION NOZ. JOINT 4765 DISP	X	-.41242E-02	30.1800
	Y	.17322E-01	30.1800
	Z	.19067E-02	43.3325
ROTN	X	-.23213E-04	7.3150
	Y	.14935E-04	35.7050
	Z	.81364E-04	45.3450
SAFETY INJECTION NOZ. JOINT 5765 DISP	X	-.30809E-02	30.1775
	Y	.17480E-01	45.3450
	Z	.16857E-02	45.3775
ROTN	X	.43395E-04	30.1800
	Y	.74584E-05	35.7950
	Z	-.64671E-04	45.0300
PRESURIZER SPAY NOZ. JOINT 1757 DISP	X	.12849E-02	38.3100
	Y	.17797E-01	44.4125
	Z	-.73527E-03	6.3650
ROTN	X	.16129E-04	9.1575
	Y	.11084E-04	35.7825
	Z	-.30929E-04	45.0600

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
PRESURIZER*SPAY NOZ. JOINT 2757 DISP	X	-.15686E-02	55.7950
	Y	-.17539E-01	30.1800
	Z	.13963E-02	63.5600
ROTN	X	.11826E-04	45.0400
	Y	-.47129E-05	23.3150
	Z	-.36715E-04	45.0600
CHARGING INLET NOZZLE, JOINT 1780 DISP	X	.81737E-03	38.3100
	Y	-.15386E-01	30.1800
	Z	-.11700E-02	63.0250
ROTN	X	.39239E-04	45.3450
	Y	-.66736E-05	35.7950
	Z	-.63122E-04	45.0300
CHARGING INLET NOZZLE, JOINT 5780 DISP	X	.92540E-03	37.5550
	Y	.15941E-01	45.3450
	Z	-.13023E-02	35.7575
ROTN	X	.43395E-04	30.1800
	Y	.74584E-05	35.7950
	Z	-.64671E-04	45.0300
S.G. OUTLET NOZZLE, JOINT 102 DISP	X	.18294E-02	22.7625
	Y	.24091E-01	45.0200
	Z	-.18498E-03	35.8500
ROTN	X	-.44394E-06	35.8500
	Y	.23201E-05	45.0600
	Z	-.50401E-05	31.2675
S.G. OUTLET NOZZLE, JOINT 3102 DISP	X	-.17578E-02	9.1150
	Y	-.25583E-01	7.5950
	Z	-.21740E-03	35.8500
ROTN	X	-.52055E-06	35.8500
	Y	-.18645E-05	45.0300
	Z	-.47940E-05	9.0925
REACTOR VESSEL HEAD, JOINT 9991 DISP	X	.27208E-02	43.3975
	Y	-.28692E-02	10.3500
	Z	-.35614E-03	35.7475
ROTN	X	-.11825E-05	35.7475
	Y	.35562E-07	30.8475
	Z	-.79230E-05	9.4250
SHUTDN COLNG OUT NOZ, JOINT 753 DISP	X	-.56466E-02	45.0200
	Y	.13568E-01	45.0175
	Z	-.30323E-03	45.0600
ROTN	X	-.81914E-06	45.0550
	Y	-.19914E-05	45.0400
	Z	-.11338E-03	45.0225
DRAIN NOZZLE, HL, JOINT 754 DISP	X	-.46705E-02	45.0200
	Y	.11129E-01	45.0175
	Z	-.27694E-03	45.0600
ROTN	X	.80434E-06	30.2075
	Y	-.22493E-05	45.0400
	Z	-.109005-03	45.0200

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
DRAIN NOZZLE, 1A CL, JOINT 1586 DISP	X	.62682E-02	35.7700
	Y	.16521E-01	44.4125
	Z	-.46322E-02	45.4075
ROTN	X	.63515E-04	9.1875
	Y	-.34613E-04	35.8225
	Z	.81960E-04	35.7700
DRAIN NOZZLE, 1B CL, JOINT 2586 DISP	X	.61680E-02	35.7725
	Y	.18941E-01	44.4125
	Z	-.39247E-02	17.5775
ROTN	X	.42706E-04	7.6175
	Y	-.22049E-04	14.9700
	Z	.76053E-04	35.7725
DRAIN NOZZLE, 2B CL, JOINT 4586 DISP	X	.77973E-02	35.7725
	Y	-.17777E-01	44.4125
	Z	-.44124E-02	17.5775
ROTN	X	.53275E-04	7.6175
	Y	-.23816E-04	37.9275
	Z	.97291E-04	35.7725
DRAIN NOZZLE, 2A CL, JOINT 5586 DISP	X	.81568E-02	35.7700
	Y	-.15658E-01	44.4125
	Z	.51210E-02	17.5725
ROTN	X	.69973E-04	30.1825
	Y	.39399E-04	35.7675
	Z	.10660E-03	35.7700

Table 3

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, Y-RESPONSE DUE TO Y-OBE, XY MODEL
 MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)	
SURGE LINE NOZZLE, JOINT 750 DISP	X	-.56662E-03	6.2200	
	Y	.33485E-02	6.2175	
	Z	-.14091E-04	44.2250	
	ROTN	X	-.32748E-07	44.2350
		Y	-.35680E-07	44.2250
		Z	.12620E-04	6.2175
SHUTDOWN COOLING NOZ., JOINT 3750 DISP	X	-.47315E-03	6.2150	
	Y	.33484E-02	6.2150	
	Z	.12581E-04	44.2250	
	ROTN	X	.32763E-07	44.2350
		Y	-.35535E-07	44.2250
		Z	-.12621E-04	6.2175
S.G. FEEDWATER NOZ., JOINT 301 DISP	X	-.24816E-04	16.9775	
	Y	.42836E-02	6.2125	
	Z	.13439E-04	6.2225	
	ROTN	X	-.25038E-07	44.2500
		Y	.93767E-07	6.2300
		Z	-.10147E-05	45.2975
S.G. FEEDWATER NOZ., JOINT 3301 DISP	X	.24306E-04	16.9775	
	Y	.42838E-02	6.2125	
	Z	-.13442E-04	6.2225	
	ROTN	X	.25071E-07	44.2500
		Y	.93750E-07	6.2300
		Z	.10145E-05	45.2975
S.G. BOT BLOWDOWN NOZ. JOINT 418 DISP	X	-.27734E-03	8.2275	
	Y	.28018E-02	6.2100	
	Z	.45547E-05	13.4275	
	ROTN	X	-.34974E-07	44.2375
		Y	.16364E-06	6.2300
		Z	.27179E-06	45.2975
S.G. BOT BLOWDOWN NOZ. JOINT 3418 DISP	X	.27729E-03	8.2275	
	Y	.28020E-02	6.2100	
	Z	-.45568E-05	13.4275	
	ROTN	X	.34967E-07	44.2375
		Y	.16366E-06	6.2300
		Z	-.27174E-06	45.2975
SAFETY INJECTION NOZ. JOINT 1765 DISP	X	.18603E-03	44.2250	
	Y	.14691E-02	44.2250	
	Z	.33912E-03	6.2150	
	ROTN	X	.81139E-05	6.2175
		Y	-.20977E-06	44.2250
		Z	.32040E-05	9.5075

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
SAFETY INJECTION NOZ. JOINT 2765 DISP	X	.21519E-03	44.2275
	Y	.15893E-02	44.2275
	Z	-.54697E-03	6.2175
ROTN	X	-.13473E-04	6.2175
	Y	.56848E-06	44.2275
	Z	-.36077E-05	44.2000
SAFETY INJECTION NOZ. JOINT 4765 DISP	X	-.21518E-03	44.2275
	Y	.15893E-02	44.2275
	Z	.54098E-03	6.2175
ROTN	X	.13473E-04	6.2175
	Y	.56872E-06	44.2275
	Z	.36077E-05	44.2000
SAFETY INJECTION NOZ. JOINT 5765 DISP	X	-.18601E-03	44.2250
	Y	.14690E-02	44.2250
	Z	-.33911E-03	6.2150
ROTN	X	-.81141E-05	6.2175
	Y	-.21004E-06	44.2250
	Z	-.32040E-05	9.5075
PRESURIZER SPAY NOZ. JOINT 1757 DISP	X	.79439E-04	44.2250
	Y	-.14980E-02	9.5075
	Z	.52168E-04	6.2100
ROTN	X	.19561E-05	6.2175
	Y	-.51760E-06	44.2250
	Z	-.11876E-05	6.2250

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
PRESURIZER SPAY NOZ. JOINT 2757 DISP	X	.10250E-03	44.2275
	Y	.16363E-02	44.2275
	Z	-.12273E-03	44.2400
	ROTN X	-.35175E-05	6.2150
	Y	-.16688E-06	44.2275
	Z	-.94936E-06	6.2300
CHARGING INLET NOZZLE, JOINT 1730 DISP	X	.56400E-04	44.2250
	Y	.13163E-02	44.2250
	Z	.50169E-04	44.2250
	ROTN X	.81139E-05	6.2175
	Y	-.20977E-06	44.2250
	Z	.32040E-05	9.5075
CHARGING INLET NOZZLE, JOINT 5780 DISP	X	-.56377E-04	44.2250
	Y	.13163E-02	44.2250
	Z	-.50221E-04	44.2250
	ROTN X	-.81141E-05	6.2175
	Y	-.21004E-06	44.2250
	Z	-.32048E-05	9.5075
S.G. OUTLET NOZZLE, JOINT 102 DISP	X	.34826E-03	45.2975
	Y	.45733E-02	6.2100
	Z	-.11557E-04	44.2500
	ROTN X	-.26229E-07	44.2500
	Y	.89515E-07	6.2300
	Z	-.10418E-05	45.2975
S.G. OUTLET NOZZLE, JOINT 3102 DISP	X	-.34821E-03	45.2975
	Y	.45737E-02	6.2100
	Z	.11568E-04	44.2500
	ROTN X	.26262E-07	44.2500
	Y	.89548E-07	6.2300
	Z	.10417E-05	45.2975
REACTOR VESSEL HEAD, JOINT 9991 DISP	X	-.18561E-06	45.2975
	Y	.51938E-02	6.2175
	Z	.98491E-08	10.8150
	ROTN X	.22116E-10	10.7650
	Y	.18691E-07	44.2375
	Z	-.48560E-09	45.2750
SHUTDN COLNG OUT NOZ, JOINT 753 DISP	X	.47317E-03	6.2150
	Y	.33485E-02	6.2175
	Z	-.12570E-04	44.2250
	ROTN X	-.32748E-07	44.2350
	Y	-.35680E-07	44.2250
	Z	.12620E-04	6.2175
DRAIN NOZZLE, HL, JOINT 754 DISP	X	.38381E-03	6.2125
	Y	.36191E-02	6.2175
	Z	-.11927E-04	44.2250
	ROTN X	-.27960E-07	44.2350
	Y	-.52799E-07	44.2275
	Z	.12640E-04	6.2175

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
DRAIN NOZZLE, 1A CL, JOINT 1586 DISP	X	-.63646E-03	44.2400
	Y	.19363E-02	6.2300
	Z	.16328E-03	9.4700
ROTN	X	-.50331E-05	9.4700
	Y	.26954E-05	44.2375
	Z	-.10609E-04	44.2400
DRAIN NOZZLE, 1B CL, JOINT 2586 DISP	X	-.65848E-03	44.2400
	Y	.21982E-02	6.2300
	Z	-.26561E-03	23.2275
ROTN	X	-.64292E-05	6.2150
	Y	-.18914E-05	44.2400
	Z	-.10686E-04	44.2400
DRAIN NOZZLE, 2B CL, JOINT 4586 DISP	X	.65860E-03	44.2400
	Y	.21982E-02	6.2300
	Z	.26555E-03	23.2275
ROTN	X	.64294E-05	6.2150
	Y	-.18917E-05	44.2400
	Z	.10689E-04	44.2400
DRAIN NOZZLE, 2A CL, JOINT 5586 DISP	X	.63660E-03	44.2400
	Y	.19363E-02	6.2300
	Z	-.16328E-03	9.4700
ROTN	X	.50332E-05	9.4700
	Y	.26959E-05	44.2375
	Z	.10612E-04	44.2400

Table 4

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, Y-RESPONSE DUE TO Z-OBE
 MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
SURGE LINE NOZZLE, JOINT 750 DISP	X	-.99253E-03	50.5300
	Y	.12385E-02	50.5300
	Z	.68923E-03	21.9925
ROTN	X	.29865E-05	27.6000
	Y	-.75129E-05	37.4950
	Z	.18569E-04	50.5300
SHUTDOWN COOLING NOZ., JOINT 3750 DISP	X	-.59900E-03	37.2900
	Y	.12470E-02	50.3875
	Z	.58938E-03	21.9925
ROTN	X	.30546E-05	27.6000
	Y	.75966E-05	37.4950
	Z	-.18364E-04	50.3875
S.G. FEEDWATER NOZ., JOINT 301 DISP	X	-.12105E-03	63.7000
	Y	.59630E-03	50.7625
	Z	.27194E-03	45.0400
ROTN	X	.88287E-06	37.3175
	Y	-.15253E-05	21.9925
	Z	-.29900E-05	20.8725
S.G. FEEDWATER NOZ., JOINT 3301 DISP	X	-.12625E-03	63.7300
	Y	-.59350E-03	20.8500
	Z	.24760E-03	45.0400
ROTN	X	.90199E-06	37.3175
	Y	.13334E-05	21.9925
	Z	-.31054E-05	50.7875
S.G. BOT BLOWDOWN NOZ. JOINT 418 DISP	X	.78342E-03	20.8950
	Y	.15375E-03	50.7575
	Z	.17937E-03	10.0300
ROTN	X	-.10791E-05	16.1325
	Y	-.28626E-05	21.9925
	Z	.14099E-05	4.8900
S.G. BOT BLOWDOWN NOZ. JOINT 3418 DISP	X	-.75979E-03	20.8525
	Y	-.15311E-03	62.0550
	Z	.17274E-03	10.0300
ROTN	X	-.12363E-05	18.1325
	Y	.23276E-05	21.9925
	Z	.13372E-05	4.8625
SAFETY INJECTION NOZ. JOINT 1765 DISP	X	.25395E-02	9.1925
	Y	-.14822E-01	45.0400
	Z	-.15585E-02	9.1925
ROTN	X	.40403E-04	45.0400
	Y	.28142E-05	33.3375
	Z	.53835E-04	45.0400

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)	
SAFETY INJECTION NOZ. JOINT 2765 DISP	X	-.42951E-02	16.1225	
	Y	.18640E-01	45.0400	
	Z	-.22327E-02	16.1225	
	ROTN	X	.26051E-04	45.0150
	Y	.14655E-04	16.1625	
	Z	-.84789E-04	45.0400	
SAFETY INJECTION NOZ. JOINT 4765 DISP	X	-.33022E-02	9.1925	
	Y	-.14065E-01	45.0675	
	Z	-.16436E-02	21.9625	
	ROTN	X	.23208E-04	45.0400
	Y	-.11580E-04	16.1600	
	Z	-.69020E-04	45.0400	
SAFETY INJECTION NOZ. JOINT 5765 DISP	X	-.30853E-02	45.0150	
	Y	.19886E-01	45.0400	
	Z	.17222E-02	45.0150	
	ROTN	X	.46483E-04	45.0675
	Y	-.37505E-05	62.0975	
	Z	.63381E-04	45.0400	
PRESURIZER SPAY NOZ. JOINT 1757 DISP	X	-.14935E-02	37.7625	
	Y	-.15739E-01	45.0400	
	Z	-.79584E-03	9.2550	
	ROTN	X	.15020E-04	45.0400
	Y	-.68523E-05	63.5475	
	Z	.21203E-04	45.0375	

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)	
PRESURIZER SPAY NOZ. JOINT 2757 DISP	X	-.19939E-02	16.1225	
	Y	.19957E-01	45.0400	
	Z	.18278E-02	16.1625	
	ROTN	X	.11553E-04	45.0150
		Y	.23562E-05	16.4150
		Z	-.30633E-04	45.0400
CHARGING INLET NOZZLE, JOINT 1780 DISP	X	-.14304E-02	37.7625	
	Y	-.13550E-01	45.0400	
	Z	.88713E-03	27.5975	
	ROTN	X	.40403E-04	45.0400
		Y	.28142E-05	33.3375
		Z	.53835E-04	45.0400
CHARGING INLET NOZZLE, JOINT 5780 DISP	X	-.15055E-02	37.5025	
	Y	.18369E-01	45.0400	
	Z	-.11350E-02	34.3100	
	ROTN	X	.48483E-04	45.0675
		Y	-.37505E-05	62.0975
		Z	.63381E-04	45.0400
S.G. OUTLET NOZZLE, JOINT 102 DISP	X	-.11092E-02	50.4125	
	Y	.17236E-03	60.2300	
	Z	.37307E-03	16.1650	
	ROTN	X	.92303E-06	37.3175
		Y	-.14567E-05	21.9925
		Z	-.30764E-05	20.8725
S.G. OUTLET NOZZLE, JOINT 3102 DISP	X	.11357E-02	20.8500	
	Y	-.16105E-03	5.8125	
	Z	.38754E-03	16.1650	
	ROTN	X	.96688E-06	37.3175
		Y	.12734E-05	21.9925
		Z	-.32109E-05	50.7875
REACTOR VESSEL HEAD, JOINT 9991 DISP	X	.64182E-03	39.6725	
	Y	.37423E-02	50.5300	
	Z	.31864E-02	37.4975	
	ROTN	X	.86934E-05	27.6000
		Y	-.63605E-07	13.6600
		Z	-.17435E-05	39.6725
SHUTDN COLNG OUT NOZ. JOINT 753 DISP	X	.57682E-03	37.6675	
	Y	.12385E-02	50.5300	
	Z	.63121E-03	21.9925	
	ROTN	X	.29865E-05	27.6000
		Y	-.75129E-05	37.4950
		Z	.18569E-04	50.5300
DRAIN NOZZLE, HL, JOINT 754 DISP	X	.48554E-03	37.6675	
	Y	.16089E-02	50.5300	
	Z	.76420E-03	21.9925	
	ROTN	X	.37872E-05	27.6000
		Y	.78308E-05	41.0675
		Z	.18522E-04	50.5300

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
DRAIN NOZZLE, 1A CL, JOINT 1586 DISP	X	.40853E-02	16.1200
	Y	-.11166E-01	45.0400
	Z	.32534E-02	9.1675
ROTN	X	.52245E-04	45.0700
	Y	-.21308E-04	62.0550
	Z	-.77599E-04	45.0400
DRAIN NOZZLE, 1B CL, JOINT 2586 DISP	X	-.71376E-02	16.1225
	Y	.15202E-01	45.0400
	Z	-.46203E-02	39.6725
ROTN	X	.59085E-04	16.4025
	Y	-.26784E-04	37.3000
	Z	.93119E-04	45.0400
DRAIN NOZZLE, 2B CL, JOINT 4586 DISP	X	-.50342E-02	16.1200
	Y	-.11458E-01	45.0400
	Z	.42419E-02	16.1025
ROTN	X	-.48881E-04	16.1025
	Y	.23034E-04	37.3000
	Z	.74892E-04	45.0400
DRAIN NOZZLE, 2A CL, JOINT 5585 DISP	X	.65185E-02	16.1200
	Y	.14646E-01	45.0400
	Z	-.41837E-02	15.7975
ROTN	X	-.62625E-04	9.1950
	Y	.29671E-04	16.1725
	Z	-.10173E-03	45.0400

Table 5

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, Z-RESPONSE DUE TO Z-OBE
 MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)	
SURGE LINE NOZZLE, JOINT 750 DISP	X	-.62984E-03	7.3250	
	Y	.36276E-03	9.4500	
	Z	-.78228E-01	45.0350	
	ROTN	X	-.79364E-04	38.2850
		Y	-.45772E-03	45.0325
		Z	-.33488E-05	45.0300
SHUTDOWN COOLING NOZ., JOINT 3750 DISP	X	.67394E-03	37.0575	
	Y	-.36279E-03	49.4500	
	Z	-.72785E-01	45.0350	
	ROTN	X	-.79285E-04	38.2850
		Y	.45797E-03	45.0325
		Z	-.33493E-05	45.0300
S.G. FEEDWATER NOZ., JOINT 301 DISP	X	-.81604E-04	45.0050	
	Y	-.36013E-03	63.7450	
	Z	-.53388E-01	38.2825	
	ROTN	X	.16918E-03	45.0700
		Y	-.4777E-04	45.0450
		Z	.23656E-05	63.7450
S.G. FEEDWATER NOZ., JOINT 3301 DISP	X	-.81519E-04	45.0050	
	Y	.36034E-03	63.7450	
	Z	-.53382E-01	38.2825	
	ROTN	X	.16918E-03	45.0700
		Y	.47701E-04	45.0450
		Z	.23663E-05	63.7450
S.G. BOT BLOWDOWN NOZ, JOINT 418 DISP	X	.78528E-02	45.0450	
	Y	.18334E-01	45.0625	
	Z	-.10194E+00	45.0350	
	ROTN	X	.19527E-03	45.0625
		Y	-.83397E-04	45.0450
		Z	.32702E-05	45.0750
S.G. BOT BLOWDOWN NOZ. JOINT 3418 DISP	X	.78403E-02	45.0450	
	Y	-.18337E-01	45.0625	
	Z	-.10195E+00	45.0350	
	ROTN	X	.19530E-03	45.0625
		Y	.83264E-04	45.0450
		Z	.32687E-05	45.0750
SAFETY INJECTION NOZ. JOINT 1765 DISP	X	-.15976E-01	8.2600	
	Y	-.38516E-02	35.3700	
	Z	-.71483E-01	45.0625	
	ROTN	X	.52602E-04	9.8000
		Y	.33066E-04	53.6500
		Z	.17994E-04	26.7000

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
SAFETY INJECTION NOZ. JOINT 2765			
DISP	X	.12340E-01	8.1675
	Y	-.46673E-02	44.4225
	Z	-.50315E-01	45.0625
ROTN	X	.62792E-04	45.0850
	Y	-.42934E-04	45.3950
	Z	-.30710E-04	45.0650
SAFETY INJECTION NOZ. JOINT 4765			
DISP	X	.12340E-01	8.1675
	Y	.46675E-02	44.4225
	Z	-.50315E-01	45.0625
ROTN	X	.62786E-04	45.0850
	Y	.42931E-04	45.3950
	Z	-.30710E-04	45.0650
SAFETY INJECTION NOZ. JOINT 5765			
DISP	X	-.15976E-01	8.2600
	Y	.38517E-02	35.3700
	Z	-.71483E-01	45.0625
ROTN	X	.52601E-04	9.8900
	Y	-.33066E-04	53.6500
	Z	.17993E-04	26.7000
PRESURIZER SPAY NOZ. JOINT 1757 DISP	X	-.17391E-01	45.0250
	Y	-.39512E-02	35.3706
	Z	-.70731E-01	45.0475
ROTN	X	.68644E-04	9.8925
	Y	.10017E-03	45.0200
	Z	-.44213E-04	45.4000

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)	
PRESSURIZER SPAY NOZ, JOINT 2757 DISP	X	.13396E-01	8.1675	
	Y	-.44066E-02	8.2450	
	Z	-.52015E-01	45.0625	
	ROTN	X	.66769E-04	9.8900
		Y	-.14294E-03	45.0450
		Z	.58601E-04	45.4000
CHARGING INLET NOZZLE, JOINT 1780 DISP	X	-.16520E-01	8.2600	
	Y	-.46261E-02	35.3700	
	Z	-.72142E-01	45.0450	
	ROTN	X	.52602E-04	9.8900
		Y	.33066E-04	53.6500
		Z	.17994E-04	26.7000
CHARGING INLET NOZZLE, JOINT 5780 DISP	X	-.16520E-01	8.2600	
	Y	.46260E-02	35.3700	
	Z	-.72142E-01	45.0450	
	ROTN	X	.52601E-04	9.8900
		Y	-.33066E-04	53.6500
		Z	.17993E-04	26.7000
S.G. OUTLET NOZZLE, JOINT 102 DISP	X	-.81430E-03	63.7450	
	Y	.29770E-04	4.8400	
	Z	-.48261E-01	23.2150	
	ROTN	X	.17065E-03	45.0675
		Y	-.45626E-04	45.0460
		Z	.24154E-05	63.7450
S.G. OUTLET NOZZLE, JOINT 3102 DISP	X	-.81454E-03	63.7450	
	Y	-.29734E-04	4.8400	
	Z	-.48261E-01	23.2150	
	ROTN	X	.17065E-03	45.0675
		Y	.45554E-04	45.0450
		Z	.24163E-05	63.7450
REACTOR VESSEL HEAD, JOINT 9991 DISP	X	-.17364E-02	45.0300	
	Y	-.92929E-07	10.2650	
	Z	-.93944E-01	45.0625	
	ROTN	X	-.21363E-03	45.0525
		Y	.28921E-07	45.0500
		Z	.62412E-05	45.0300
SHUTDN COLNG OUT NOZ, JOINT 753 DISP	X	.67377E-03	37.0575	
	Y	.36276E-03	9.4500	
	Z	-.72737E-01	45.0350	
	ROTN	X	-.79364E-04	38.2850
		Y	-.45772E-03	45.0325
		Z	-.33488E-05	45.0300
DRAIN NOZZLE, HL, JOINT 754 DISP	X	.65670E-03	37.0575	
	Y	.37589E-03	28.7375	
	Z	-.62061E-01	45.0350	
	ROTN	X	-.87178E-04	45.0325
		Y	-.39556E-03	45.0325
		Z	-.36015E-05	45.0300

Location	Direction Global	Max. Rel. Displ (in)	Time (sec)
DRAIN NOZZLE, 1A CL, JOINT 1586 DISP	X	-.10311E-01	38.1625
	Y	.33059E-02	33.8850
	Z	-.77749E-01	45.0450
ROTN	X	.74860E-04	15.8400
	Y	-.34080E-03	45.0375
	Z	.79813E-04	8.2400
DRAIN NOZZLE, 1B CL, JOINT 2586 DISP	X	.11190E-01	44.9700
	Y	-.44285E-02	9.4475
	Z	-.78008E-01	45.0450
ROTN	X	.55316E-04	37.2325
	Y	-.32258E-03	45.0325
	Z	.65308E-04	34.0675
DRAIN NOZZLE, 2B CL, JOINT 4586 DISP	X	.11190E-01	44.9700
	Y	.44279E-02	9.4475
	Z	-.78006E-01	45.9450
ROTN	X	.55225E-04	37.2325
	Y	.32258E-03	45.0325
	Z	.65306E-04	34.0675
DRAIN NOZZLE, 2A CL, JOINT 5586 DISP	X	-.10411E-01	38.1625
	Y	-.33458E-02	33.8850
	Z	-.77749E-01	45.0450
ROTN	X	.74159E-04	15.8400
	Y	.34041E-03	45.0375
	Z	.79102E-04	8.2400

THE MAX REL. DISPLACEMENTS OF SCE NOZZLES, Y-RESPONSE DUE TO Y-OBE, YZ, MEDCL
 MAXIMUM RELATIVE DISPLACEMENTS OF BRANCH LINE CONNECTION POINTS
 LOCATION DIRECTION MAX. REL. DISPL (IN) TIME (SEC)
 GLOBAL

Table 6

LOCATION	DIRECTION	MAX. REL. DISPL (IN)	TIME (SEC)
SURGE LINE NOZZLE,	JOINT 750 DISP X	-.78826E-03	6.2250
	Y	.47483E-02	6.2250
	Z	-.18065E-04	6.2250
	ROTN X	-.45023E-07	6.2275
	Y	-.39777E-07	44.2775
	Z	.17510E-01	6.2225
SHUTDOWN COOLING NOZ.,	JOINT 3750 DISP X	-.65829E-03	6.2175
	Y	.47481E-02	6.2250
	Z	.15647E-04	44.2225
	ROTN X	.45837E-07	6.2275
	Y	-.39557E-07	44.2775
	Z	-.17511E-04	6.2275
S.G. FEED WATER NOZ.,	JOINT 301 DISP X	-.30703E-04	16.9500
	Y	.60885E-02	6.2275
	Z	.18852E-04	6.2250
	ROTN X	.23352E-07	17.5675
	Y	.13339E-06	6.2325
	Z	-.88019E-06	38.9475
S.G. FEED WATER NOZ.,	JOINT 3301 DISP X	.30692E-04	16.9805
	Y	.60882E-02	6.2275
	Z	-.18957E-04	6.2250
	ROTN X	-.23354E-07	17.5675
	Y	.13337E-06	6.2526
	Z	.88010E-06	38.9475
S.G. BOT BLOWDOWN NOZ.,	JOINT 418 DISP X	-.29038E-03	38.9475
	Y	.39492E-02	6.2225
	Z	.44868E-06	13.4275
	ROTN X	-.42118E-07	14.2350
	Y	.23279E-06	6.2325
	Z	-.25969E-06	38.9700
S.G. BOT BLOWDOWN NOZ,	JOINT 3418 DISP X	.29036E-03	38.9475
	Y	.39492E-02	6.2225
	Z	-.44909E-05	13.4875
	ROTN X	.42112E-07	44.2550
	Y	.23281E-06	6.2325
	Z	.25976E-06	38.9700
SAFETY INJECTION NOZ.	JOINT 1765 DISP X	.22026E-03	44.2225
	Y	.19872E-02	6.2306
	Z	.47262E-03	6.2200
	ROTN X	.11311E-04	6.2200
	Y	-.20795E-06	44.2225
	Z	.41676E-05	9.5075
SAFETY INJECTION NOZ.	JOINT 2765 DISP X	.24388E-03	44.2250
	Y	.21229E-02	6.2300
	Z	-.75968E-03	6.2200
	ROTN X	-.18877E-04	6.2225
	Y	-.54258E-06	44.4775
	Z	-.43137E-05	44.2500
SAFETY INJECTION NOZ.	JOINT 4765 DISP X	-.24367E-03	44.2250
	Y	.21229E-02	6.2300
	Z	.75911E-03	6.2200
	ROTN X	.18878E-04	6.2225
	Y	-.54854E-06	44.4775
	Z	.43137E-05	44.2500

LOCATION	DIRECTION GLOBAL	MAX. REL. DISPL. (IN)	TIME (SEC)
Table 6			
SAFETY INJECTION NOZ.	JOINT 5765 DISP X	-.22023E-03	44.2225
	Y	.19872E-02	6.2500
	Z	-.47261E-03	6.2200
	ROTN X	-.11311E-04	6.2200
	Y	-.20816E-04	54.2225
	Z	-.41677E-05	9.5075
PRESURIZER SPRAY NOZ,	JOINT 1757 DISP X	.90436E-04	44.2225
	Y	.20315E-02	6.2250
	Z	.85085E-04	6.2260
	ROTN X	.27245E-05	6.2200
	Y	-.48687E-06	44.2225
	Z	-.16929E-05	6.2275
PRESURIZER SPRAY NOZ.	JOINT 2757 DISP X	.10868E-03	44.2250
	Y	.21962E-02	6.2300
	Z	.13771E-03	9.5200
	ROTN X	-.49222E-05	6.2225
	Y	-.18958E-06	44.2250
	Z	-.13349E-05	6.2325
CHARGING INLET NOZZLE,	JOINT 1780 DISP X	.59068E-04	44.2225
	Y	.17306E-03	6.2300
	Z	.52746E-04	44.2225
	ROTN X	.11311E-04	6.2200
	Y	-.20796E-06	44.2225
	Z	.41676E-05	9.5075
CHARGING INLET NOZZLE,	JOINT 5780 DISP X	-.59054E-04	44.2225
	Y	.17306E-02	6.2300
	Z	-.52786E-04	44.2225
	ROTN X	-.11311E-04	6.2200
	Y	-.20816E-06	44.2225
	Z	-.41677E-05	9.5075
S.G. OUTLET NOZZLE,	JOINT 102 DISP X	.26036E-03	44.2425
	Y	.64416E-02	6.2225
	Z	-.10700E-04	47.3725
	ROTN X	.24238E-07	17.5675
	Y	.12734E-06	6.2325
	Z	-.89536E-06	38.9475
S.G. OUTLET NOZZLE,	JOINT 3102 DISP X	-.28034E-03	44.2425
	Y	.64415E-02	6.2225
	Z	.10705E-04	17.3725
	ROTN X	-.24240E-07	17.5675
	Y	.12739E-06	6.2325
	Z	.89529E-06	38.2475
REACTOR VESSEL HEAD,	JOINT 9991 DISP X	-.14942E-06	17.4050
	Y	.73007E-02	6.2225
	Z	.10661E-07	44.2650
	ROTN X	.21353E-10	44.2625
	Y	.24353E-07	44.2375
	Z	.41230E-02	17.4450
SHUTDN COLNG OUT NOZ.,	JOINT 753 DISP X	.65034E-03	6.2175
	Y	.47483E-02	6.2850
	Z	-.15634E-04	44.2225
	ROTN X	-.45023E-07	6.2275
	Y	-.39777E-07	44.2175
	Z	.17510E-04	6.2225

LOCATION	DIRECTION GLOBAL	MAX. REL. DISPL. (IN)	TIME (SEC)
Table 6			
DRAIN NOZZLE, HL.	JOINT 754 DISP X	.58339E-03	6.2175
	Y	.51106E-02	6.2250
	Z	-.14977E-04	44.2225
	ROTN X	-.38449E-07	6.2275
	Y	-.62371E-07	44.2775
	Z	.17520E-04	6.2225
DRAIN NOZZLE, 14 CL.	JOINT 1586 DISP X	-.71440E-03	44.2375
	Y	.27559E-02	6.2300
	Z	.18280E-03	9.4975
	ROTN X	.67892E-05	6.2175
	Y	.28318E-05	44.2375
	Z	-.13555E-04	6.2175
DRAIN NOZZLE, 1B CL.	JOINT 2586 DISP X	.72815E-03	9.5200
	Y	.31312E-02	6.2500
	Z	.36610E-03	6.2225
	ROTN X	-.90617E-05	6.2200
	Y	-.25373E-05	6.2500
	Z	-.14691E-04	6.2175
DRAIN NOZZLE, 2B CL.	JOINT 2636 DISP X	-.72012E-03	8.5204
	Y	.31311E-02	6.2300
	Z	-.36609E-03	6.2225
	ROTN X	.90620E-05	6.2200
	Y	-.25373E-05	6.2300
	Z	.14692E-04	6.2175
DRAIN NOZZLE, 2A CL.	JOINT 5586 DISP X	.71455E-03	44.2575
	Y	.27558E-02	6.2500
	Z	-.18276E-03	9.4975
	ROTN X	-.67893E-05	6.2175
	Y	.28324E-05	44.2375
	Z	.13556E-04	6.2175

Figure 1 Sheet 1

"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN
ONCFRE UNITS 2 AND 3 PROJECT OFFICE, AND IS CON-
SIDERED TO BE HIGH CONFIDENCE LEVEL INFORMATION."

Piping Assembly See Fig. 1 Sheet 3		Reference Point	Reference Point Location With Respect to Co-ordinate System Shown on Fig. 1 Sheet 3		
			X(feet)	Y(feet)	Z(feet)
P - 1 See Fig. 1 Sheet 4		760	-21.222	0	0
		770	-20.389	0	0
		780	-19.556	0	0
See Fig. 1 Sheet 5	P-3	1600	-30.744	-6.635	10.281
	P-7	2600	-30.744	-6.635	-10.281
	P-12	5600	30.744	-6.635	-10.281
	P-16	4600	30.744	-6.635	10.281
See Fig. 1 Sheet 6	P-5	1757	-18.860	0	16.348
		1760	-18.484	0	16.168
		1765	-16.179	0	15.062
	P-14	5757	18.860	0	-16.354
		5760	18.484	0	-16.168
		5765	16.179	0	-15.062
See Fig. 1 Sheet 7	P-9	2757	-20.084	0	-10.969
		2760	-19.667	0	-10.969
		2765	-17.110	0	-10.969
	P-18	4757	20.084	0	10.969
		4760	19.667	0	10.969
		4765	17.110	0	10.969
P-10 See Fig. 1 Sheet 8		3760	21.222	0	0
		3770	20.389	0	0
		3780	19.556	0	0

SCE-3-903-17-1

TITLE: Reactor Coolant Piping Nozzle Locations

CB 2824 (2)

Figure 1 Sheet 2

Piping Assembly See Fig. 1 Sheet 3		Reference Point	Reference Point Movement with Respect to Co-ordinate System Shown on Fig. 1 Sheet 3					
			Displacement (inches)			Rotation (radians)		
			ΔX	ΔY	ΔZ	CX	CY	CZ
P - 1 See Fig. 1 Sheet 4		760	-.999	.272	.001	0	-.00001	.00133
		770	-.960	.297	.001	0	0	.00132
		780	-.921	.302	.001	0	0	.00130
See Fig. 1 Sheet 5	P-3	1600	-1.340	-.162	.410	.00065	.00030	.00040
	P-7	2600	-1.344	-.163	-.411	-.00065	-.00024	.00039
	P-12	5600	1.340	-.162	-.410	-.00065	.00030	-.00040
	P-16	4600	1.344	-.163	.411	.00065	-.00024	-.00039
See Fig. 1 Sheet 6	P-5	1757	-.798	.180	.732	.00058	-.00007	.00020
		1760	-.782	.185	.725	.00060	-.00005	.00024
		1765	-.686	.224	.679	.00070	.00003	.00106
	P-14	5757	.798	.180	-.734	-.00058	-.00007	-.00020
		5760	.782	.185	-.725	-.00060	-.00005	-.00024
		5765	.686	.224	-.679	-.00070	.00003	-.00106
See Fig. 1 Sheet 7	P-9	2757	-.864	.204	-.440	-.00055	.00025	.00032
		2760	-.846	.209	-.441	-.00053	.00025	.00038
		2765	-.740	.243	-.450	-.00052	.00023	.00112
	P-18	4757	.864	.204	.440	.00054	.00025	-.00032
		4760	.846	.209	.441	.00053	.00025	-.00038
		4765	.740	.243	.450	.00052	.00023	-.00112
P - 10 See Fig. 1 Sheet 8		3760	.999	.272	-.001	0	-.00001	-.00133
		3770	.960	.287	-.001	0	-.00001	-.00132
		3780	.921	.302	-.001	0	-.00001	-.00130

Normal Operation - Dead Weight +100% Power Operation
Computer Ref. - (1009-1109)

923-17-1

TITLE: Reactor Coolant Piping Nozzle Movements - Normal OP.

Figure 1 Sheet 2-1

"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN ONOPRE UNITS 2 AND 3 PROJECT OFFICE AND IS CONSIDERED TO BE HIGH CONFIDENCE LEVEL INFORMATION."

Piping Assembly See Fig. 1 Sheet 3	Reference Point	Reference Point Movement with Respect to Co-ordinate System Shown on Fig. 1 Sheet 3						
		Displacement (inches)			Rotation (radians)			
		ΔX	ΔY	ΔZ	ΘX	ΘY	ΘZ	
P - 1 See Fig. 1 Sheet 4	760							
	770	.256	1.181	.170	.00013	.00116	.01208	
	780							
See Fig. 1 Sheet 5	P-3 1600							
	P-7 2500							
	P-12 5600							
	P-16 4600							
See Fig. 1 Sheet 6	P-5	1757						
		1760						
		1765	.432	.186	.644	.00138	.00606	.00195
	P-14	5757						
		5760						
		5765	.432	.186	.644	.00138	.00606	.00195
See Fig. 1 Sheet 7	P-9	2757						
		2760						
		2765	.436	.229	.533	.00105	.00718	.00213
	P-18	4757						
		4760						
		4765	.436	.229	.533	.00105	.00718	.00213
P - 10 See Fig. 1 Sheet 8	3760							
	3770	.256	1.181	.170	.00013	.00116	.01208	
	3780							

NOTE: 1. Tabulated displacements and rotations can be either positive or negative.
 2. Displacements and rotations due to pipe rupture and subcompartment pressurization only.

923-17-1

TITLE: Reactor Coolant Piping Nozzle Movements - Ruptured Line

Figure 1 Sheet 2.2

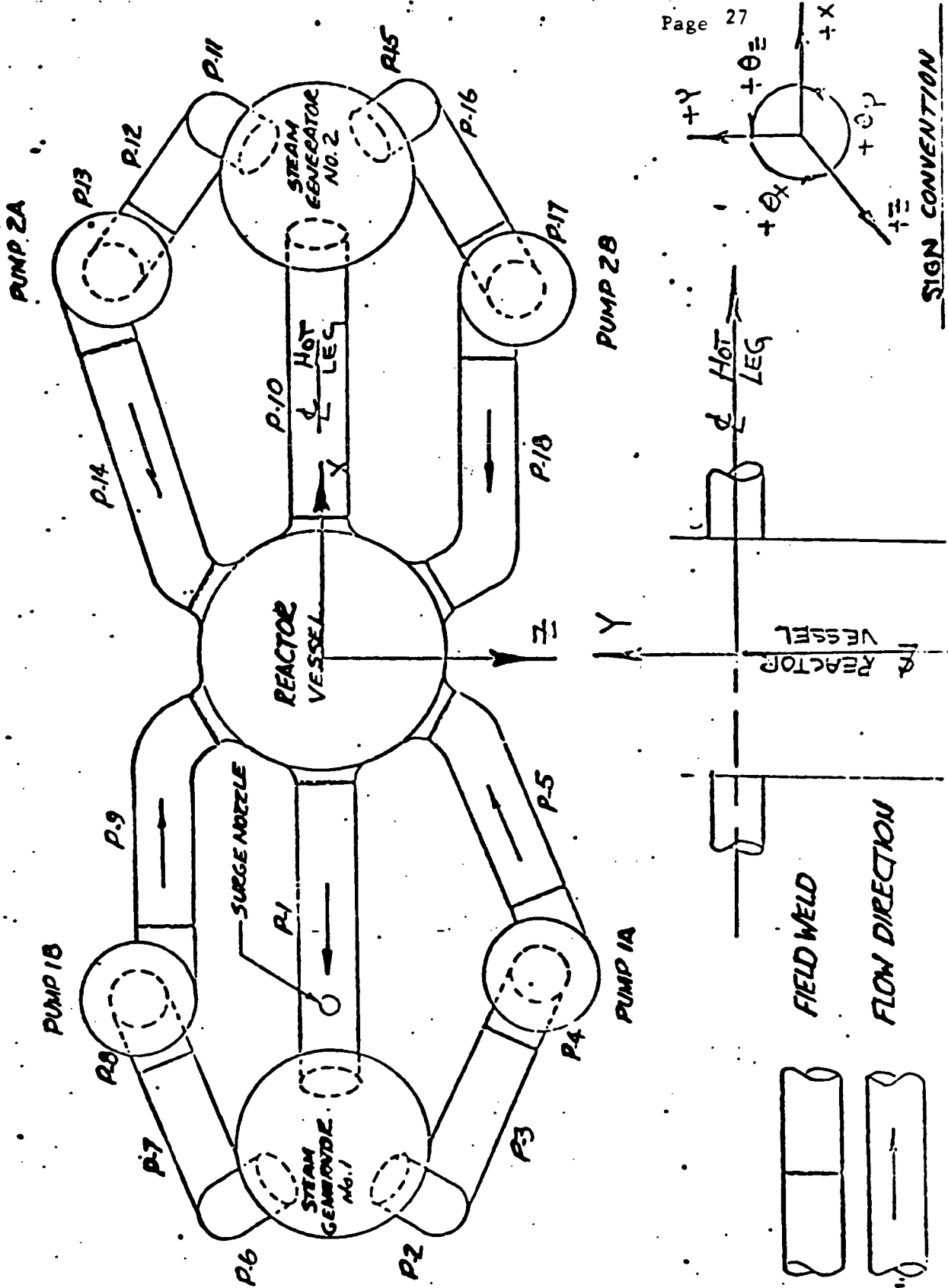
"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN ONOFRE UNITS 2 AND 3 PROJECT OFFICE AND IS CONSIDERED TO BE HIGH CONFIDENCE LEVEL INFORMATION."

Piping Assembly See Fig. 1 Sheet 3	Reference Point	Reference Point Movement with Respect to Co-ordinate System Shown on Fig. 1 Sheet 3						
		Displacement (inches)			Rotation (radians)			
		ΔX	ΔY	ΔZ	ΘX	ΘY	ΘZ	
P - 1 See Fig. 1 Sheet 4	760	.074	.102	.064	.00015	.00079	.00074	
	770	.074	.093	.073	.00014	.00080	.00075	
	780	.075	.085	.083	.00013	.00081	.00074	
See Fig. 1 Sheet 5	P-3	1600	.112	.132	.036	.00083	.00100	.00093
	P-7	2600	.113	.131	.030	.00078	.00106	.00097
	P-12	5600	.112	.132	.036	.00083	.00100	.00093
	P-16	4600	.113	.131	.030	.00078	.00106	.00097
See Fig. 1 Sheet 6	P-5	1757	.087	.022	.064	.00021	.00028	.00028
		1760	.086	.024	.066	.00022	.00033	.00033
		1765	.081	.043	.078	.00038	.00057	.00053
	P-14	5757	.087	.022	.064	.00021	.00028	.00028
		5760	.086	.024	.066	.00022	.00033	.00033
		5765	.081	.043	.078	.00038	.00057	.00053
See Fig. 1 Sheet 7	P-9	2757	.070	.028	.044	.00020	.00029	.00033
		2760	.070	.030	.046	.00019	.00034	.00038
		2765	.070	.049	.059	.00023	.00062	.00064
	P-18	4757	.070	.028	.044	.00020	.00029	.00033
		4760	.070	.030	.046	.00019	.00034	.00038
		4765	.070	.049	.059	.00023	.00062	.00064
P - 10 See Fig. 1 Sheet 8	3760	.074	.102	.064	.00015	.00079	.00074	
	3770	.074	.093	.073	.00014	.00080	.00075	
	3780	.075	.085	.083	.00013	.00081	.00074	

- NOTES: 1. Tabulated displacements and rotations can be positive or negative.
2. Displacements and rotations due to pipe rupture and subcompartment pressurization only.

923-17-1

TITLE: Reactor Coolant Piping Nozzle Movements Unruptured Line



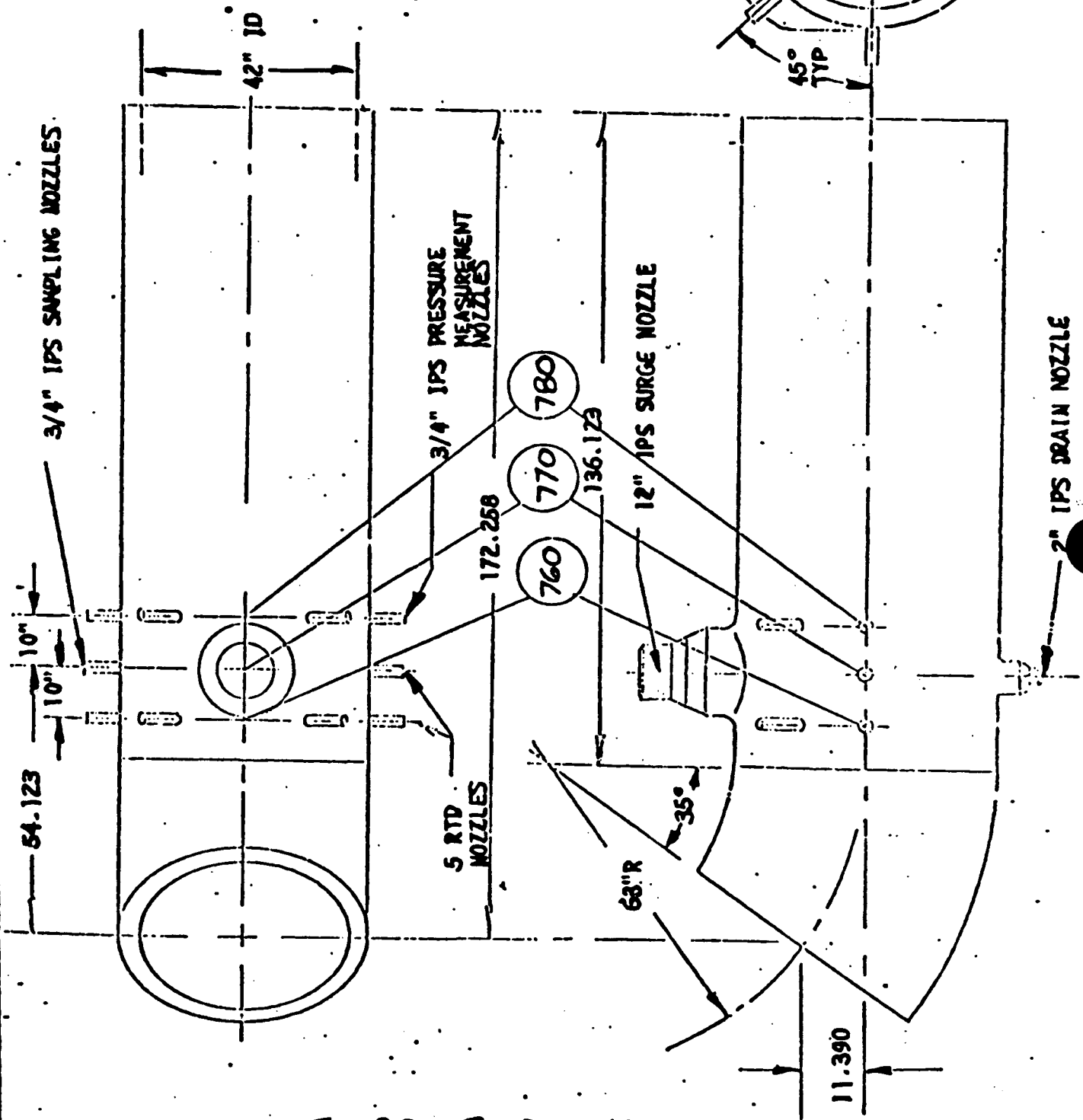
SIGN CONVENTION

TITLE: REACTOR COOLANT PIPING ARRANGEMENT - PLAN VIEW

Fig. 1 Sheet 3

923-17-1

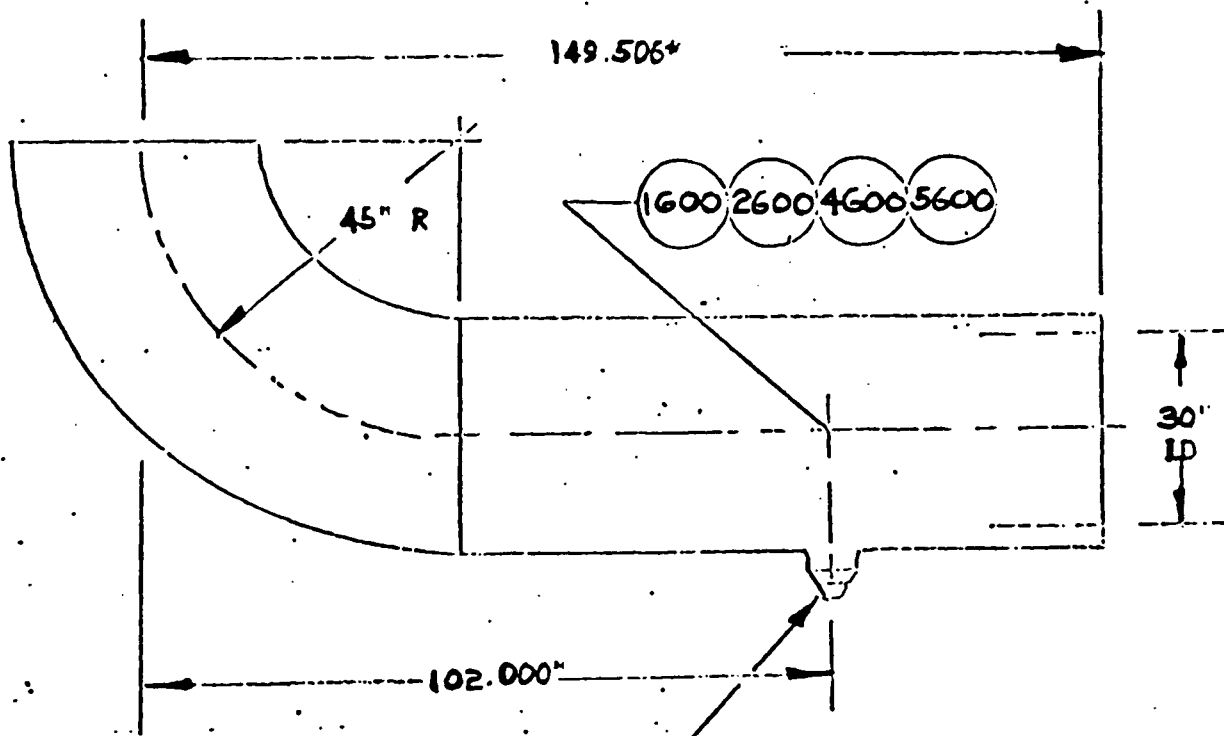
"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN ONOFRE UNITS 2 AND 3 PROJECT OFFICE AND IS CONSIDERED TO BE HIGH CONFIDENCE LEVEL INFORMATION."



5023-923-17-0

REACTOR COOLANT PIPING DETAILS - Assembly P-1

Fig. 1 Sheet 4



2" IPS Drain Nozzle (P-3, P-12, P-16)
 2" IPS Letdown & Drain Nozzle (P-7)

INFORMATION ONLY
 APPROVAL NOT REQUIRED
 JUL 31 1975
 BECHTEL
 LOS ANGELES

*This is a calculated dimension.
 Add 2" extra length per Paragraph 4.9.2
 of Specification 00000-PE-140.

5023-923-17-0

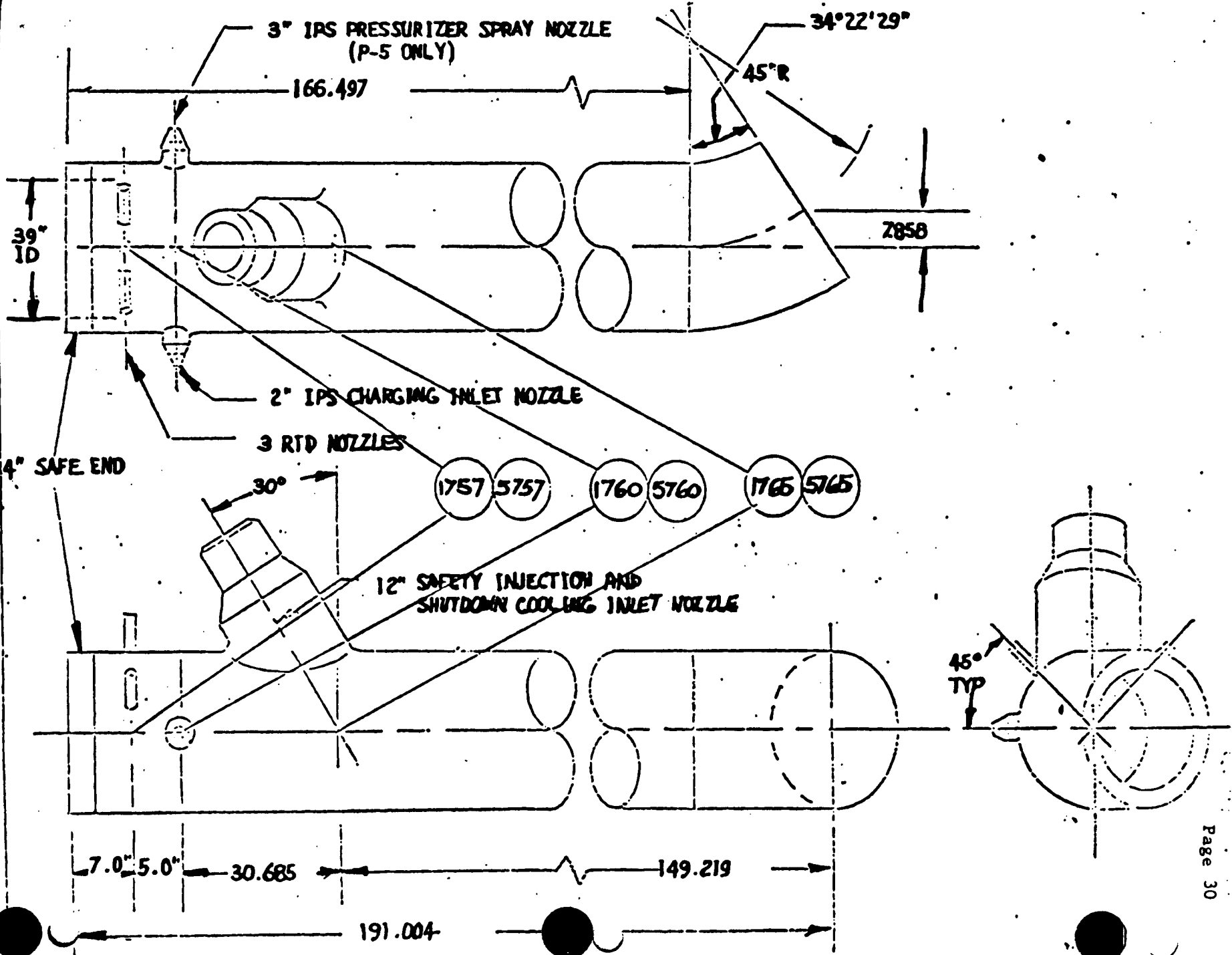
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REACTOR COOLANT PIPING DETAILS - Assemblies P-5, 14

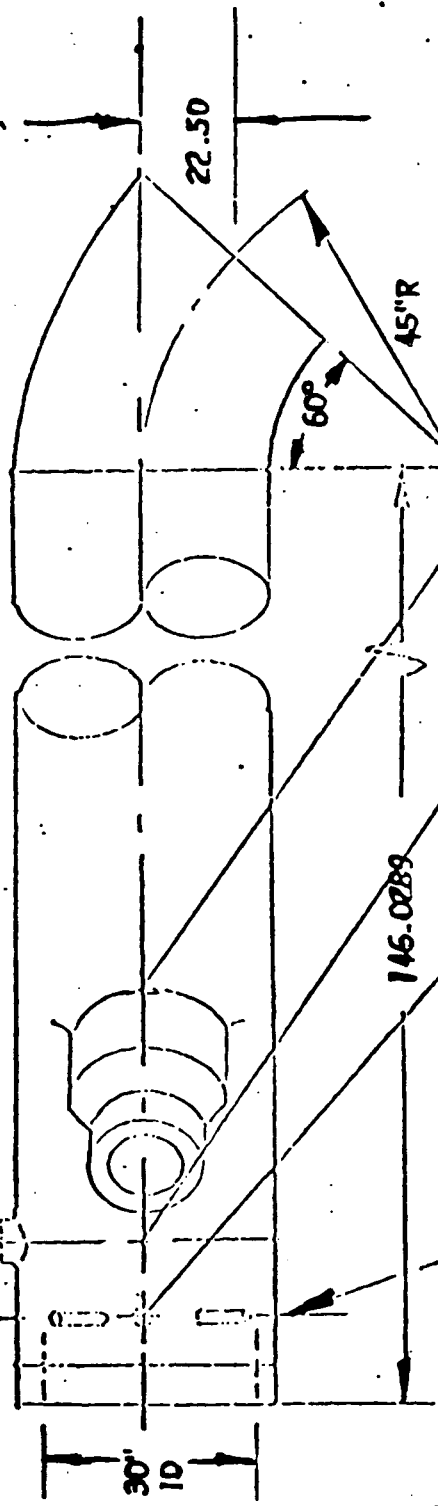
SO 23-923-17-0

PAGE R.5.117

Fig. 1 Sheet 6



3" IPS PRESSURIZER SPRAY NOZZLE
(P-9 ONLY)



146.0289

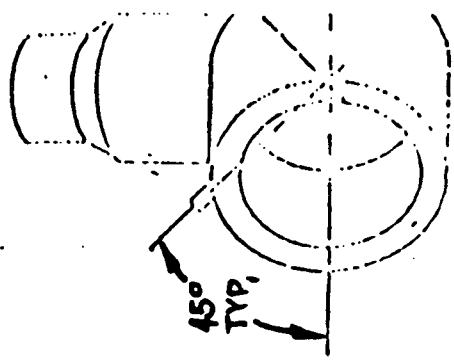
3 RTD NOZZLES

4" SAFE END

30"

2757 4757
2760 4760
2765 4765

12" IPS SAFETY INJECTION AND
SHUTDOWN COOLING INLET NOZZLE



142.313

30.687

185.000

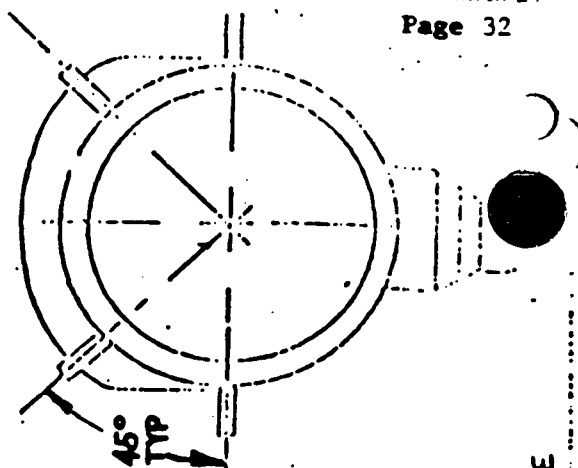
7.0" 5.0"

REACTOR COOLANT PIPING DETAILS - Assemblies P-9, 18 Fig. 1 Sheet 7

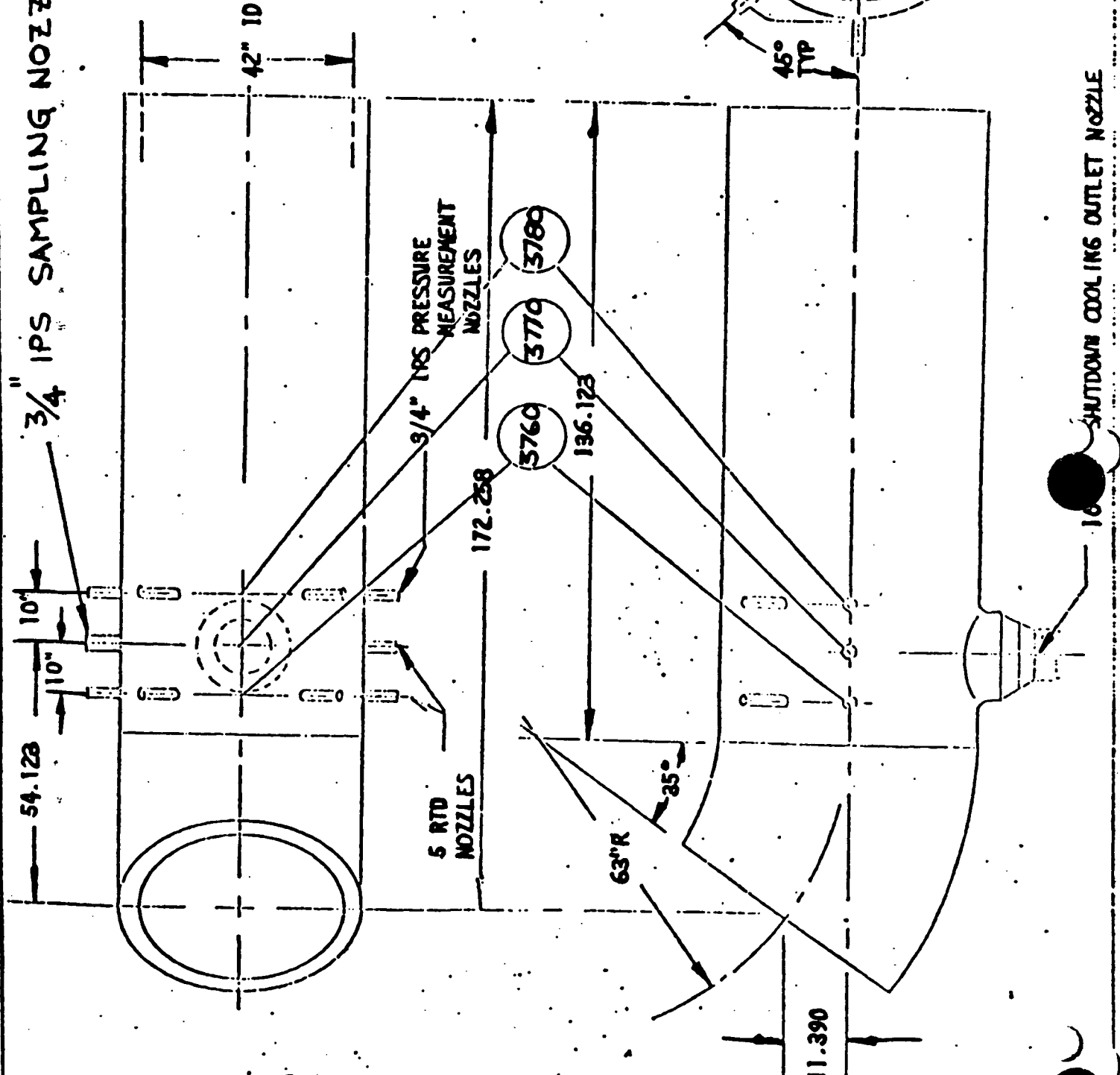
5023-923-17-0

PAGE R, S, T, U

1. <input type="checkbox"/> MFG. MAY PROCEED 2. <input type="checkbox"/> SUBMIT FINAL DWG. - MFG. MAY PROCEED 3. <input type="checkbox"/> EXCEPT AS NOTED - MAKE CHANGES & RESUBMIT 4. <input type="checkbox"/> MFG. MAY PROCEED AS APPROVED 5. <input type="checkbox"/> APPROVAL NOT REQUIRED MFG. MAY PROCEED	
DATE RECEIVED	JUL 31 1954
DWG. STATUS	SIGNED
DATE	
IMPORTANT: Vendor's drawings will be reviewed and approved only as to design and performance to the specifications. The purchaser relieves the Vendor of any liability for the suitability of materials and workmanship thereon for the intended purpose.	
BECHTEL LOS ANGELES	



3/4" IPS SAMPLING NOZZLE

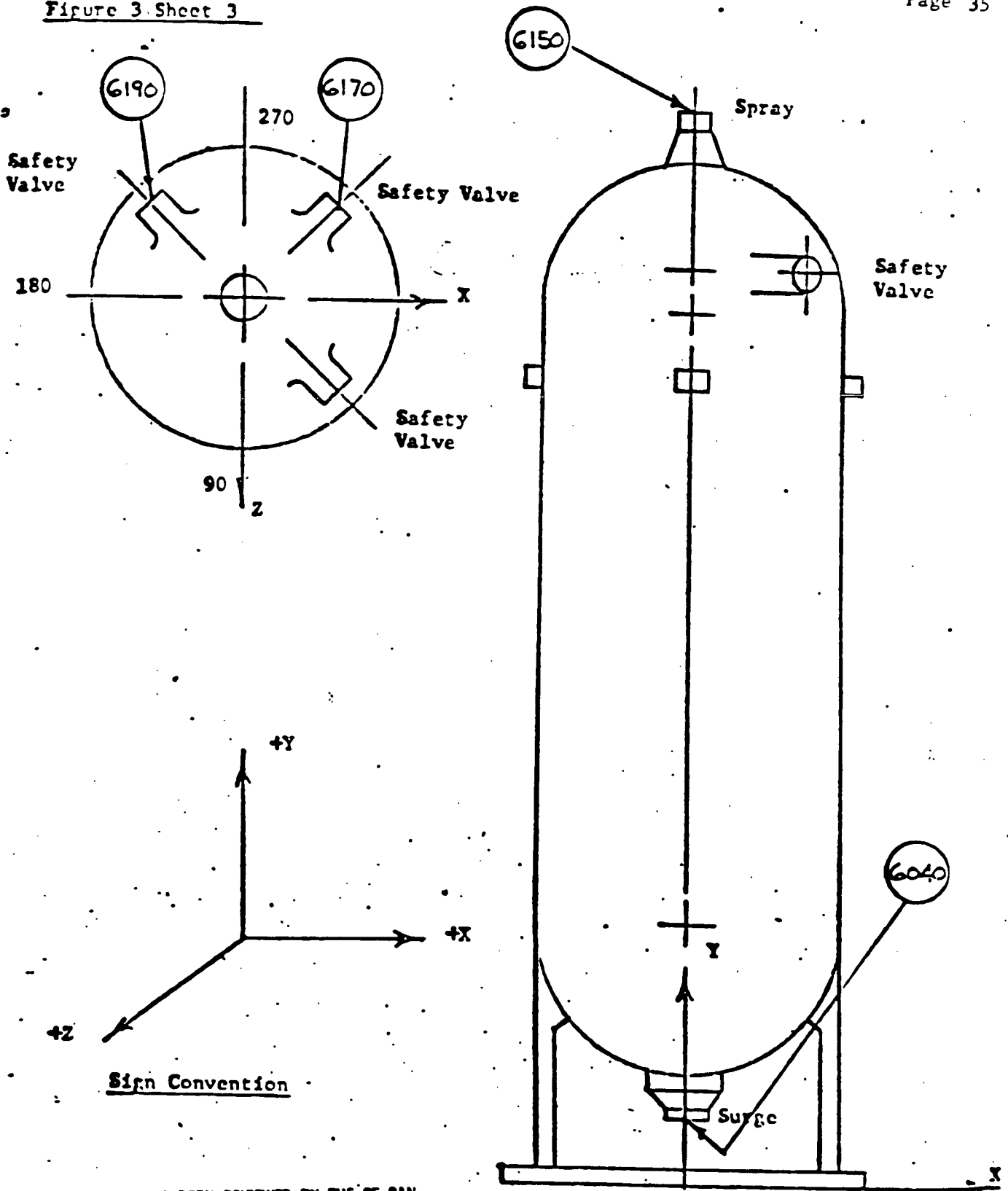


5023-923-17-0

Title: REACTOR COOLANT PIPING DETAILS - Assembly P-10

Fig. 1 Sheet 8

8



"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN ONOFRE UNITS 2 AND 3 PROJECT OFFICE AND IS CONSIDERED TO BE HIGH CONFIDENCE LEVEL INFORMATION."

TITLE: Pressurizer Nozzles

919-24-2

IMPORTANT
 If the price or schedule is affected by this document approval, Details must be notified or in
 fabrication or such claims are waived.
 Approval of document involving calculation, analysis or test report is only on completion of
 the method used by the supplier. Supplier retains full responsibility for design.
 Approval of this document does not relieve the supplier from full responsibility for contract or
 purchase order requirements including, but not limited to, adequacy and establishability of
 materials and/or equipment represented thereon for the intended function.

DATE RECEIVED	SEP 16 1976	DOC STATUS BY	J. H. [Signature]
DOCUMENT STATUS		DATE	12-9-76
1 <input checked="" type="checkbox"/> APPROVED — MANUFACTURER MAY PROCEED			
2 <input type="checkbox"/> APPROVED EXCEPT AS NOTED. MAKE CHANGES AND RESUBMIT. MANUFACTURER MAY PROCEED AS APPROVED.			
3 <input type="checkbox"/> NOT APPROVED — CORRECT AND RESUBMIT			
4 <input type="checkbox"/> INFORMATION ONLY <input type="checkbox"/> DISTRIBUTION REQUIRED			

PP-1218 (10076) 12/75

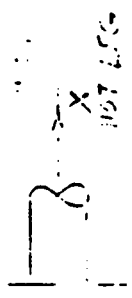
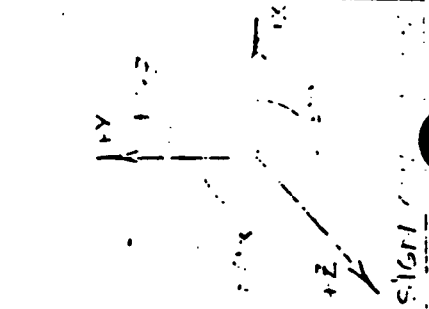
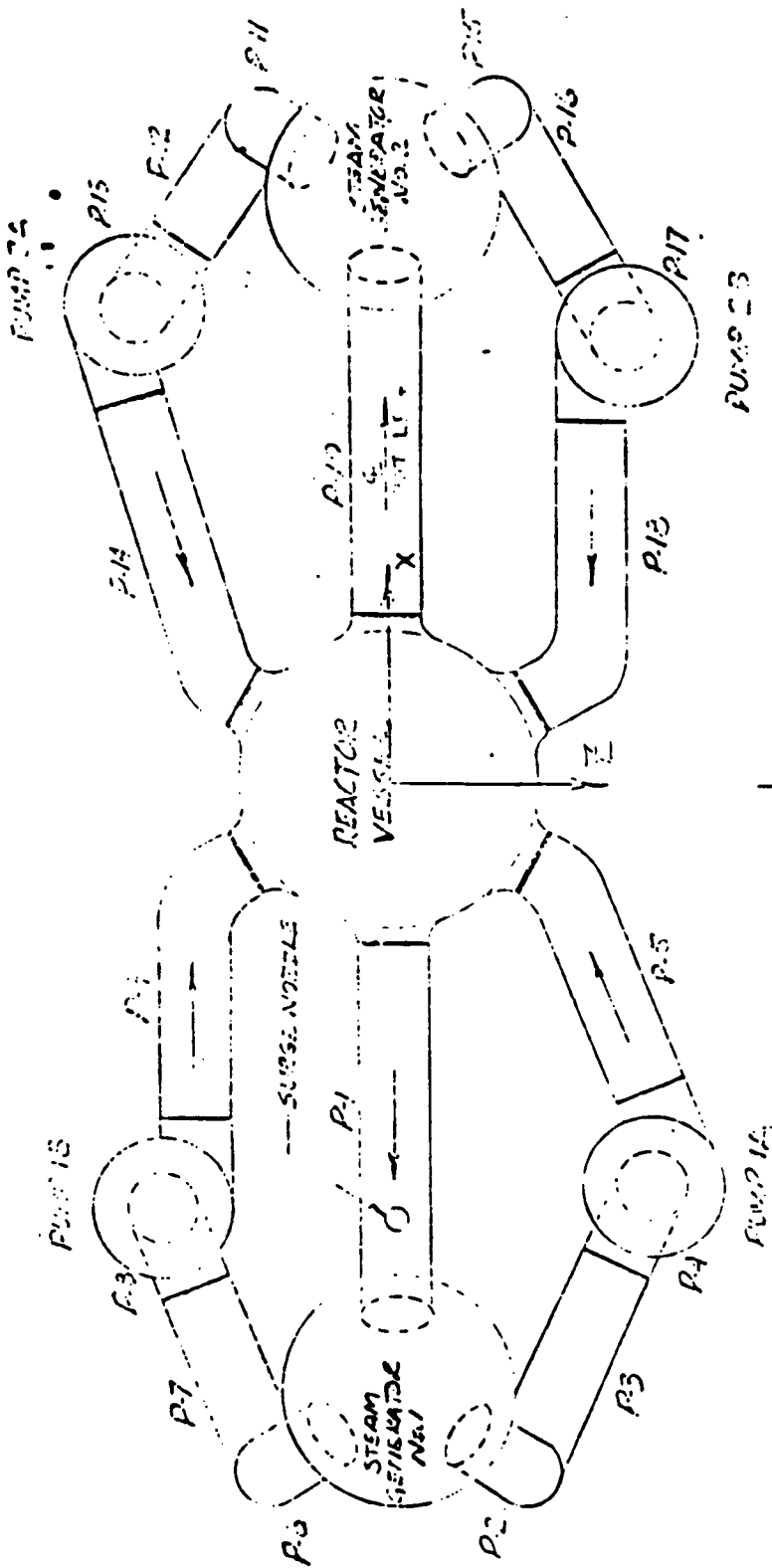
QUALITY
ACCEPTABLE

"THIS DOCUMENT HAS BEEN REVIEWED BY THE CE SAN
 ONOFRE UNITS 2 AND 3 PROJECT OFFICE AND IS CON-
 sidered TO BE HIGH CONFIDENCE LEVEL INFORMATION."

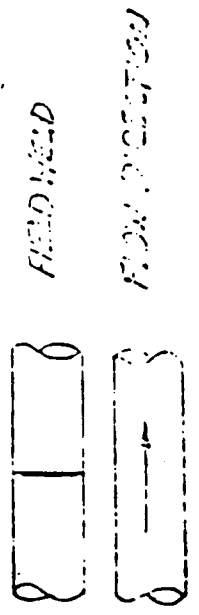
919-24-2

APPENDIX D (Con't)

Unit 3 RCS tributary nozzle movements (normal operation, ruptured line
and unruptured line)



Y



2

Title: REACTOR COOLANT PIPING ARRANGEMENT - PLAN VIEW

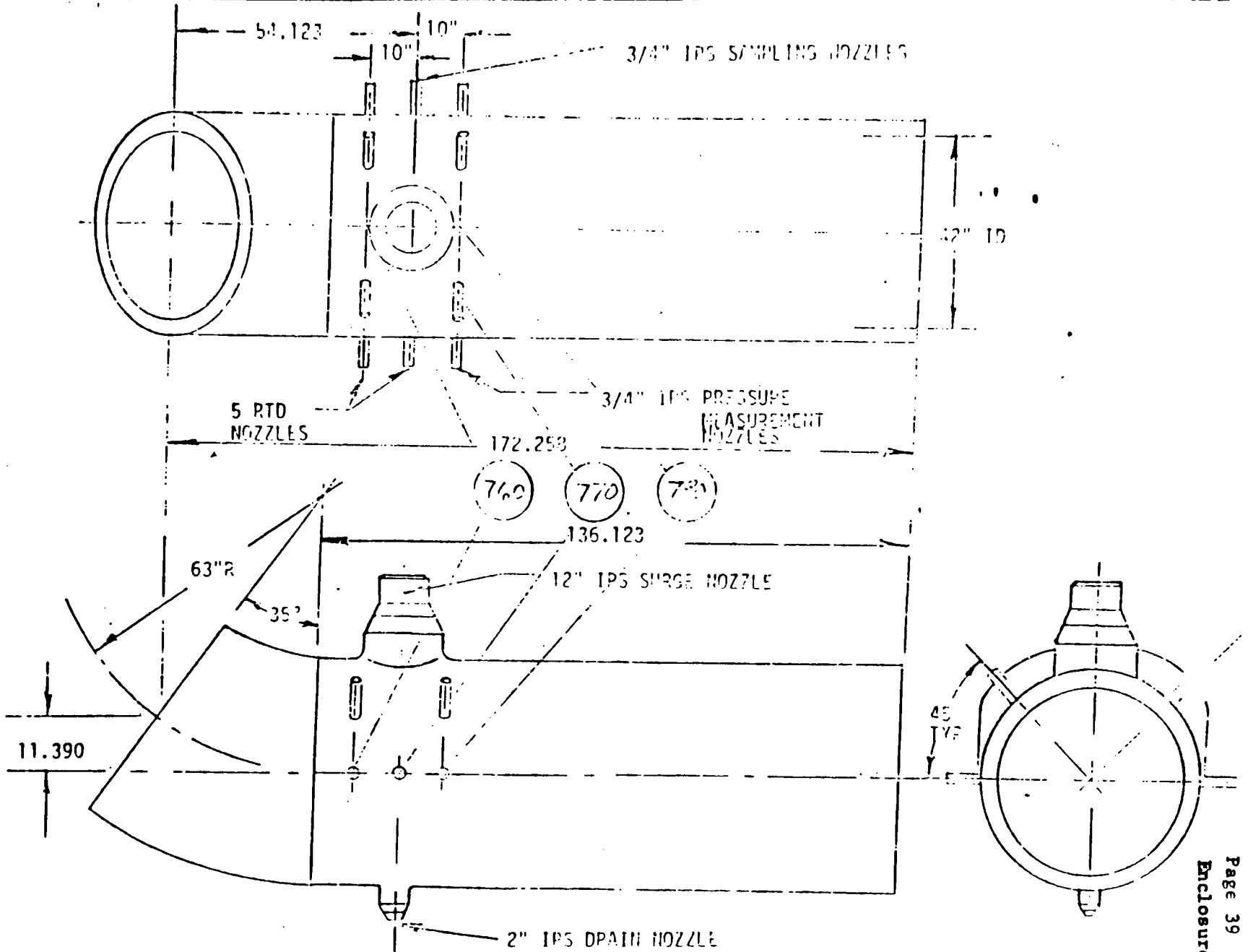
Specification No. 01470-PE-140

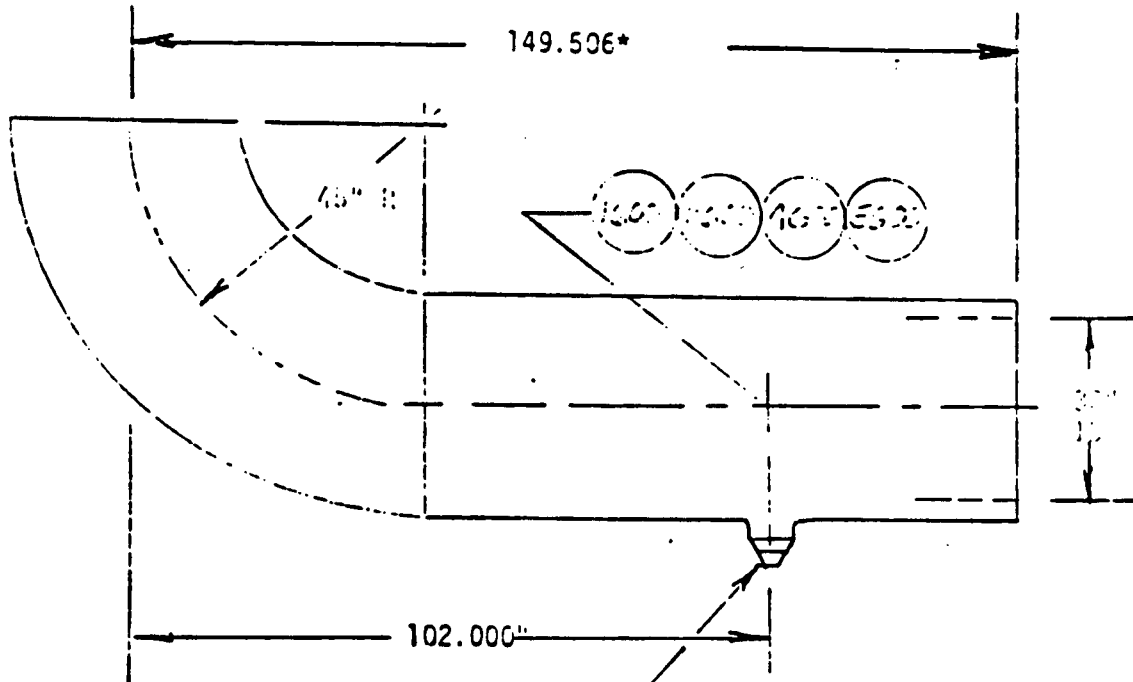
Revision 0

Figure 17 Sheet 1

Title: REACTOR CONTAINMENT FILTRATION DETAILS - Assembly P-1
Specification No. 01470-PE-140
Revision: 0

Figure 17 Sheet 3

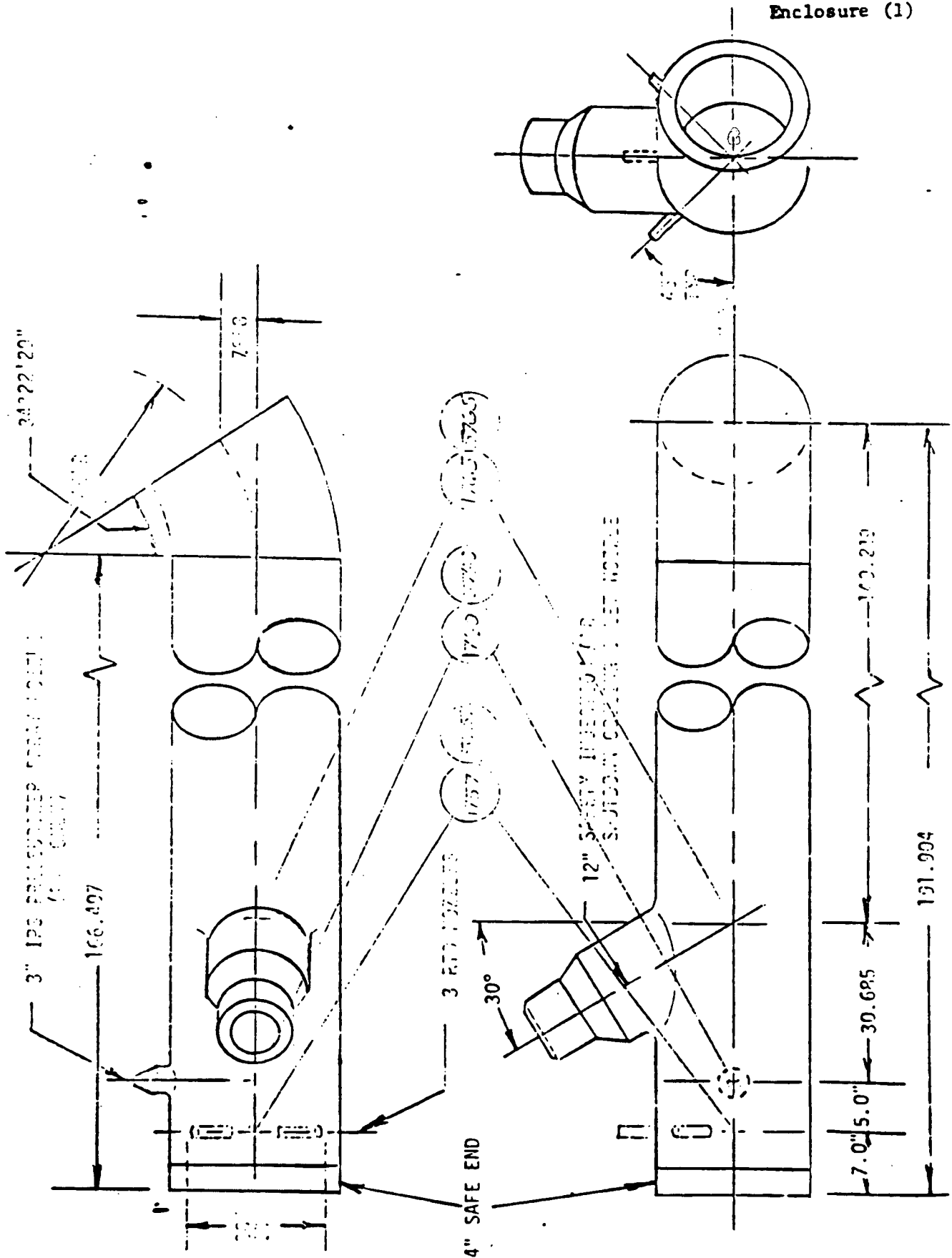


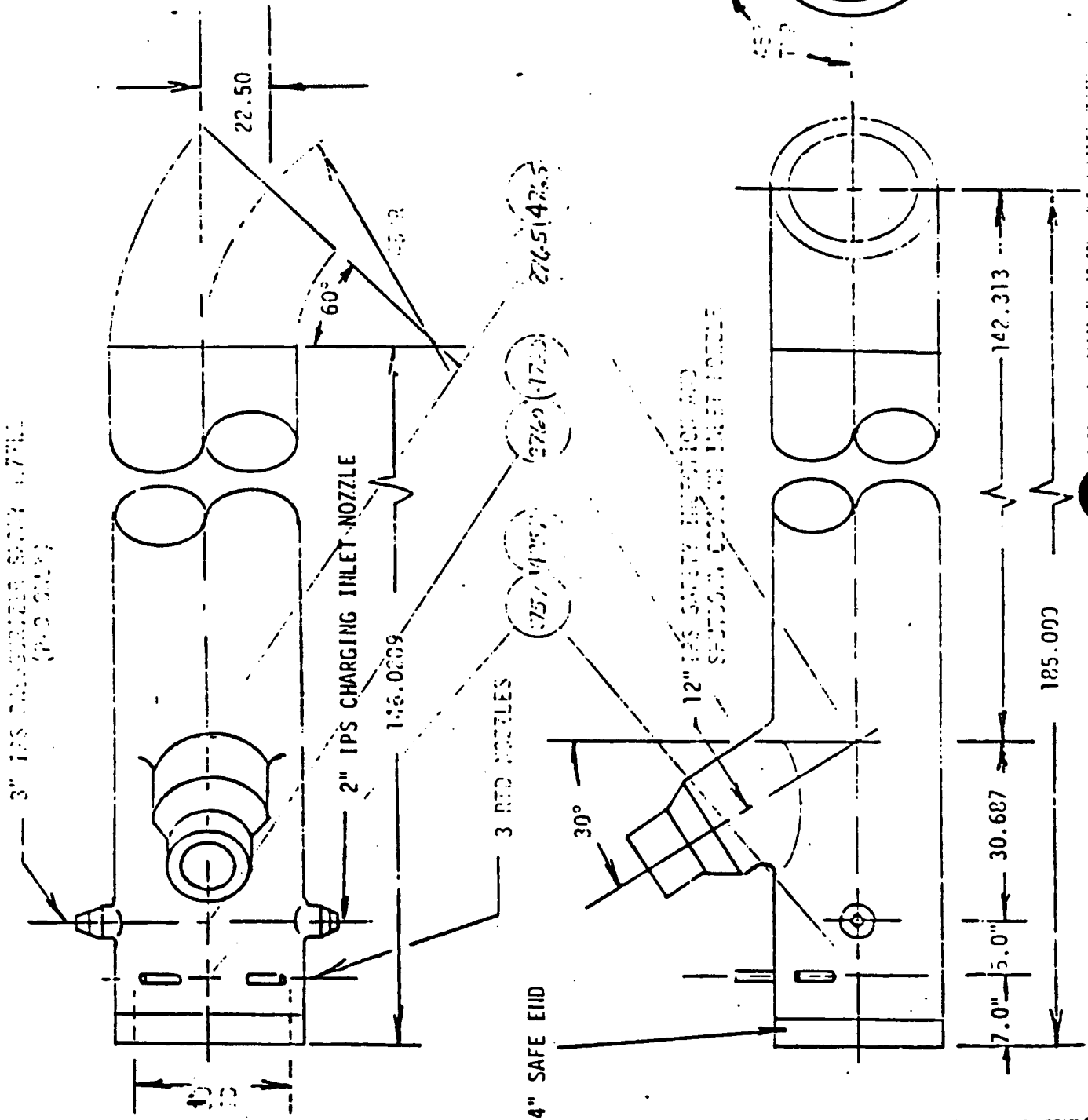


- 2" IPS Drain Nozzle (P-7, P-12, P-16)
- 2" IPS Nut and Drain Nozzle (P-3)

*this is a calculated dimension.
 Add 2" extra length per paragraph 4.9.2
 of Specification 01470-PE-140.

REACTOR LEAKAGE TYPING DETAILS - Assemblies P-3, 7, 12, 16		
Specification No. 01470-PE-140	REVISION 0	FIGURE 17





REACTOR REACTOR COMPONENTS - Assemblies P-3, 14

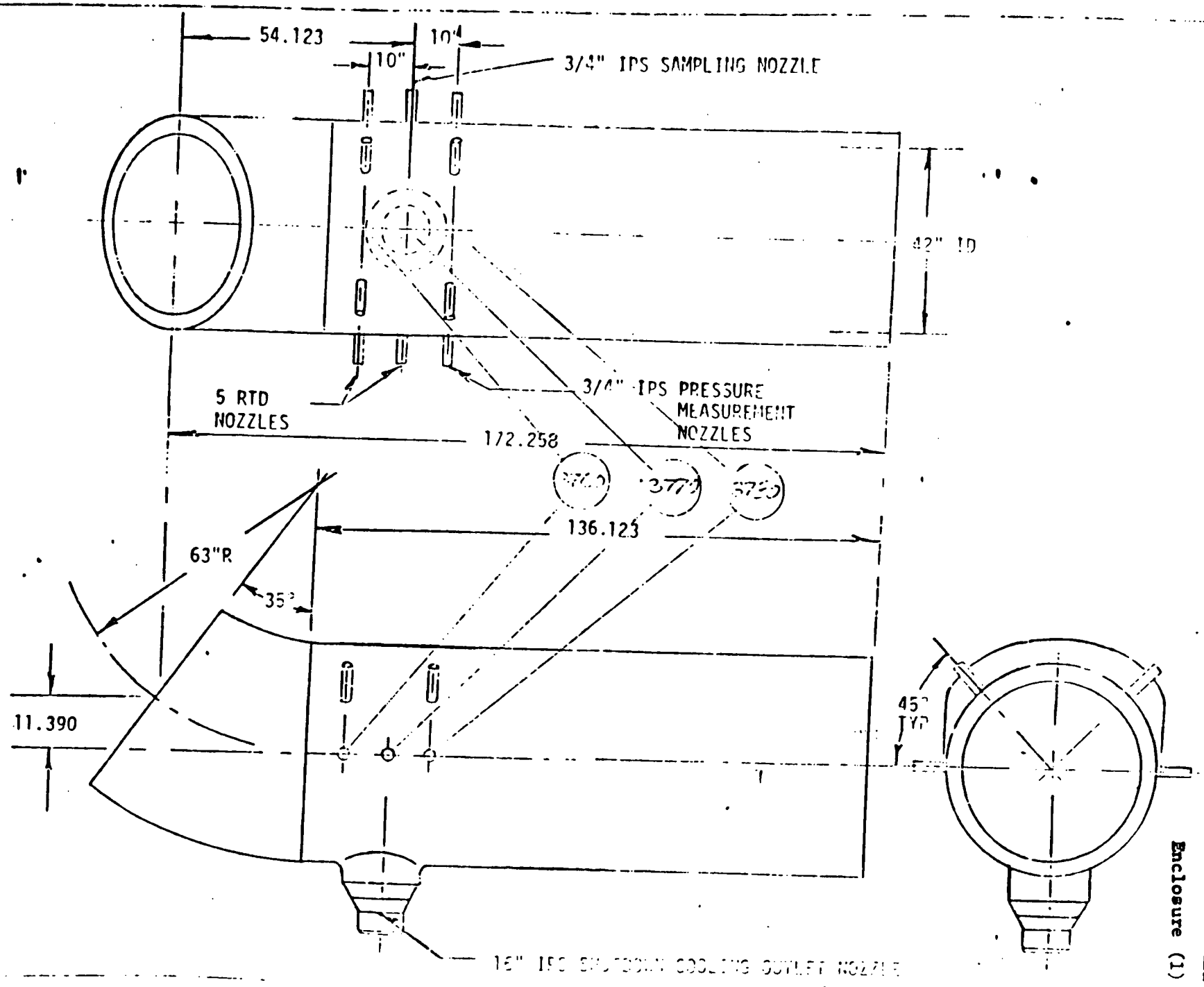
01470-PE-140

0

Page 17

TITLE: REACTOR COOLANT PIPING DETAILS - Assembly P-10
 Specification No. 01470-PE-140
 Revision 0

Figure 17 Sheet 9



RC Piping Tributary Nozzle Locations

Enclosure (2)

Piping Assembly See Fig. 17 Sheet 1		Reference Point	Reference Point Location With Respect to Coordinate System Shown on Figure 17 Sheet 1		
			X (feet)	Y (feet)	Z (feet)
See Fig. 17 Sheet 3	P-1	760	-21.222	0	0
		770	-20.389	0	0
		730	-19.556	0	0
See Fig. 17 Sheet 5	P-3	1600	-30.744	-6.635	10.281
	P-7	2600	-30.744	-6.635	-10.281
	P-12	5600	30.744	-6.635	-10.281
	P-16	4600	30.744	-6.635	10.281
See Fig. 17 Sheet 7	P-5	1757	-18.860	0	16.348
		1760	-18.484	0	16.168
		1765	-16.179	0	15.062
	P-14	5757	18.860	0	-16.348
		5760	18.484	0	-16.168
		5765	16.179	0	-15.062
See Fig. 17 Sheet 8	P-9	2757	-20.084	0	-10.969
		2760	-19.667	0	-10.969
		2765	-17.110	0	-10.969
	P-18	4757	+20.084	0	10.969
		4760	19.667	0	10.969
		4765	17.110	0	10.969
See Fig. 17 Sheet 9	P-10	3760	21.222	0	0
		3770	20.389	0	0
		3780	19.556	0	0

RC Piping Tributary Nozzle Movements - Normal Operation

Enclosure (2)

Piping Assembly See Fig. 17 Sheet 1		Reference Point	Reference Point Movement with Respect to Coordinate System Shown on Fig. 17 Sheet 1					
			Displacement (inches)			Rotations (radians)		
			ΔX	ΔY	ΔZ	ΘX	ΘY	ΘZ
See Fig. 17 Sheet 3	P-1	760	-.999	.272	.001	0	-.00001	.00133
		770	-.960	.287	.001	0	0	.00132
		780	-.921	.302	.001	0	0	.00130
See Fig. 17 Sheet 5	P-3	1600	-1.341	-.162	.410	.00064	.00030	.00040
	P-7	2600	-1.344	-.163	-.411	-.00065	-.00024	.00039
	P-12	5600	1.341	-.162	-.410	-.00064	.00030	-.00040
	P-16	4600	1.344	-.163	.411	.00065	-.00024	-.00039
See Fig. 17 Sheet 7	P-5	1757	-.798	.180	.732	.00058	-.00007	.00081
		1760	-.782	.185	.725	.00060	-.00005	.00085
		1765	-.686	.224	.679	.00071	.00003	.00107
	P-14	5757	.798	.179	-.734	-.00058	-.00006	-.00081
		5760	.782	.185	-.725	-.00060	-.00005	-.00085
		5765	.686	.224	-.679	-.00071	.00003	-.00170
See Fig. 17 Sheet 8	P-9	2757	-.864	.204	-.440	-.00053	.00025	.00083
		2760	-.846	.208	-.441	-.00053	.00025	.00089
		2765	-.740	.243	-.450	-.00051	.00028	.00113
	P-18	4757	.864	.204	.440	.00053	.00025	-.00083
		4760	.846	.208	.441	.00053	.00025	-.00089
		4765	.740	.243	.450	.00051	.00028	-.00113
See Fig. 17 Sheet 9	P-10	3760	.999	.272	-.001	0	-.00001	-.00133
		3770	.960	.287	-.001	0	-.00001	-.00132
		3780	.921	.302	-.001	0	-.00001	-.00130

RC Piping Tributary Nozzle Movements - Unruptured Line

Enclosure (2)

Piping Assembly See Fig. 17 Sheet 1	Reference Point	Reference Point Movement with Respect to Coordinate System Shown on Fig. 17 Sheet 1						
		Displacement (inches)			Rotation (radians)			
		ΔX	ΔY	ΔZ	ΘX	ΘY	ΘZ	
See Fig. 17 Sheet 3	P-1	760	.074	.102	.064	.00015	.00079	.00074
		770	.074	.093	.073	.00014	.00080	.00075
		780	.075	.085	.083	.00013	.00081	.00074
See Fig. 17 Sheet 5	P-3	1600	.112	.132	.036	.00083	.00100	.00093
	P-7	2600	.113	.131	.030	.00078	.00106	.00097
	P-12	5600	.112	.132	.036	.00083	.00100	.00093
	P-16	4600	.113	.131	.030	.00078	.00106	.00097
See Fig. 17 Sheet 7	P-5	1757	.087	.022	.064	.00021	.00028	.00028
		1760	.086	.024	.066	.00022	.00033	.00033
		1765	.081	.043	.078	.00038	.00057	.00053
	P-14	5757	.087	.022	.064	.00021	.00028	.00028
		5760	.086	.024	.066	.00022	.00033	.00033
		5765	.081	.043	.078	.00038	.00057	.00053
See Fig. 17 Sheet 8	P-9	2757	.070	.028	.044	.00020	.00029	.00033
		2760	.070	.030	.046	.00019	.00034	.00038
		2765	.070	.049	.059	.00023	.00062	.00064
	P-18	4757	.070	.028	.044	.00020	.00029	.00033
		4760	.070	.030	.046	.00019	.00034	.00038
		4765	.070	.049	.059	.00023	.00062	.00064
See Fig. 17 Sheet 9	P-10	3760	.074	.102	.064	.00015	.00079	.00074
		3770	.074	.093	.073	.00014	.00080	.00075
		3780	.075	.085	.083	.00013	.00081	.00074

- NOTES: 1. Tabulated displacements and rotations can be positive or negative.
 2. Displacements and rotations due to LOCA only.

RC Piping Tributary Nozzle Movements - Ruptured Line

Enclosure (2)

Piping Assembly See Fig. 17 Sheet 1		Reference Point	Reference Point Movement with Respect to Coordinate System Shown on Fig. 17 Sheet 1					
			Displacement (inches)			Rotations (radians)		
			ΔX	ΔY	ΔZ	ΘX	ΘY	ΘZ
See Fig. 17 Sheet 3	P-1	760						
		770	.256	1.181	.170	.00013	.00116	.01208
		780						
See Fig. 17 Sheet 5	P-3	1600						
	P-7	2600						
	P-12	5600						
	P-15	4600						
See Fig. 17 Sheet 7	P-5	1757						
		1760						
		1765	.432	.186	.644	.00138	.00606	.00195
	P-14	5757						
		5760						
		5765	.432	.186	.644	.00138	.00606	.00195
See Fig. 17 Sheet 8	P-9	2757						
		2760						
		2765	.436	.229	.533	.00105	.00718	.00213
	P-18	4757						
		4760						
		4765	.436	.229	.533	.00105	.00718	.00213
See Fig. 17 Sheet 9	P-10	3760						
		3770	.256	1.181	.170	.00013	.00116	.01208
		3780						

NOTES: 1. Tabulated displacements and rotations can be positive or negative.
2. Displacements and rotations due to LOCA only.

APPENDIX E

Code Class 2, Instrument Sensing Line List

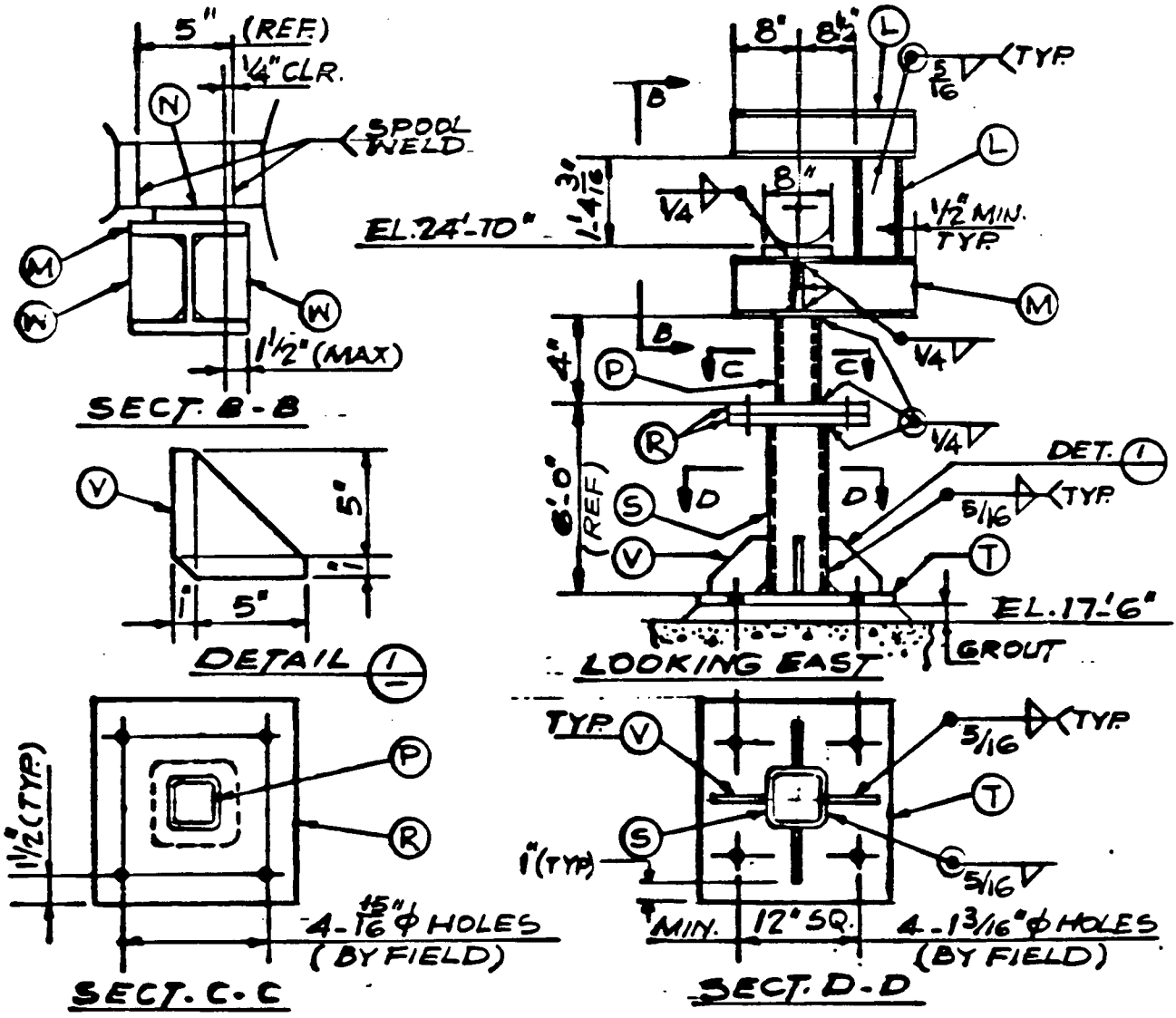
Code Class 2, Instrument Sensing line List

<u>Code Class 2 Instrument Sensing Line</u>	<u>Equipment</u>
PT-0100X	Pressurizer
PT-0100Y	S2-1201-ME087-Unit 2
PT-0101-1	S2-1201-ME-087-Unit 3
PT-0101-2	
PT-0101-3	
PT-0101-4	
PT-0102-1	
PT-0102-2	
PT-0102-3	
PT-0102-4	
LT-0103	
PT-0103-1	
PT-0104-2	
PT-0105-3	
PT-0106-4	
LT-0110-1	
LT-0110-2	

"Tagging", (line numbers), of the Code Class 2 instrument sensing lines on Code Class 1 equipment (pressurizer) within the process piping system, shall be the same as the corresponding instrument number. This shall be typical for Units 2 and 3.

S.U.S. 28BB

ITEM NO	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
L	2		W6X20X2'-0"			X	BY FIELD
M	1		W8X40X2'-0"			X	
N	1		Æ-1/2X3X0'-8"			X	
P	1		TS 6X6X.375X0'-4			X	
R	2		Æ 3/4X14X1'-2"			X	
S	1		TS 8X8X.375X6'-3"			X	
T	1		Æ-1X22X1'-10"			X	
V	4		3/8" GUSSET Æ			X	
W	2		3/8" STIFF. Æ			X	
	4		3/4" φ BOLTS W/NUTS & WASHERS			X	
	4		US-B-HC-LCSF-175				



1201 SHT 2 OF 2
TAG NO. S2-RC-016-H001 REV 2

BECHTEL POWER CORPORATION BORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION		
JOB NO. 10079			FILE	PIPE SUPPORT ASSEMBLY		
DATE	APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.			



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-5104
DATE 4-26-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 05
12D. DATE MAY 14 1980
12E. SCN NO.

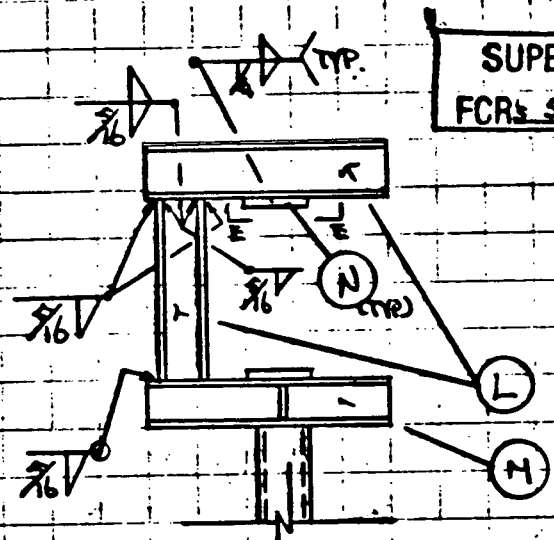
ARQCI) 2888 JOB NO. 10079 (I.C.)
REF. DWG. OR SPEC. SHEET NO. 2 REV. 2 (286-2)
5. TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

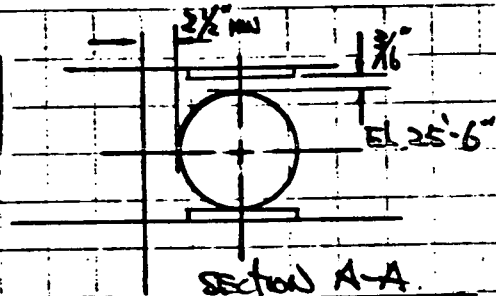
7. EXISTING CONDITION: CLR DIMENSION SHOWN INCORRECT.
CHANGE BILL OF MATH

THIS FCR SUPERSEDES: FCR S-4726, S-5011

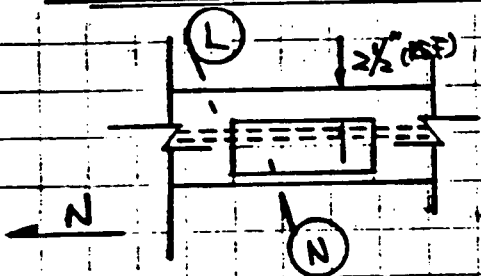
8. CHANGE REQUEST/SKETCH



LOOKING EAST (PARTIAL)



SECTION D-D (PARTIAL)



SECTION E-E

BILL OF MATH (BY FIELD)
1. CHANGE QUANTITY OF ITEM N FROM 1 TO 2

PL. 5469

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY _____ DATE _____
CIVIL _____ PIPF 4-30-80
ELEC _____ INSTR _____
MECH _____ NUC _____
WELD _____ GAE 4-30-80

PREPARED BY Kia Ching Wang
11. APPROVAL OF FLD DISPOSITION
Doris J. Lane
PROJECT FIELD ENGINEER
DATE APR 30 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/RL DATE 4-29-80

REMARKS: **CONVERT TO DCN** Void DCN 344

QUALITY ASSURANCE ENGINEER (FIELD): John Steppard DATE 4-30-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE John Steppard DATE 5-18-80

16. ADDITIONAL DISTRIBUTION _____

VOID FCR S-4726/DCN S-5011

APR 24 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 8-5011
DATE 4-11-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

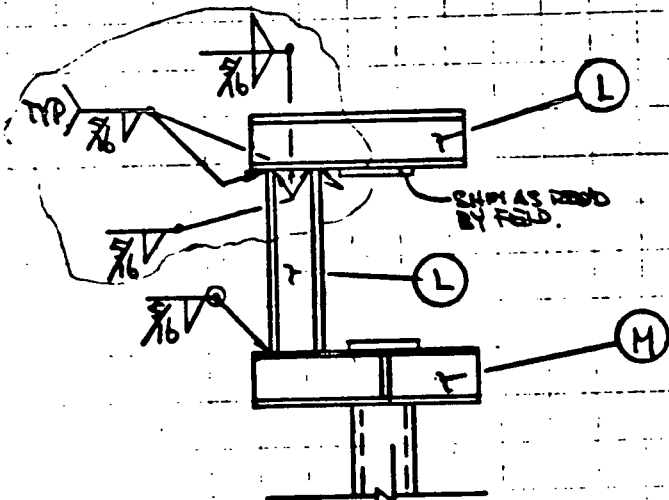
12C. DCN SUB NO. 04
APR 30 1980
12E. SCN NO.

A(QCI) QRRR JOB NO. 10079
REF. DWG. OR SPEC. SHEET NO. REV. 2 S. TITLE WPS SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION: WELD SYMBOL SHOWN INCORRECT

8. CHANGE REQUEST/SKETCH



NO NEW MATL REQ'D

LOOKING EAST (PARTIAL)

PL5398

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY _____ DATE _____
CIVIL _____ PIP _____
ELEC _____ INSTR _____
MECH _____ NUC _____
WELD _____ QA _____

9. Steve Olin Phang
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
Donnie Olin
PROJECT FIELD ENGINEER
DATE 4-14-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Kogua/lt DATE 4-11-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): g.w. Sheppard DATE 4-14-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE g.w. Sheppard DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 54726
DATE 3-11-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

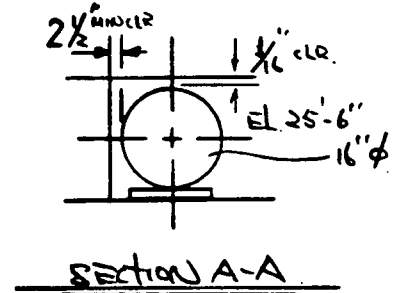
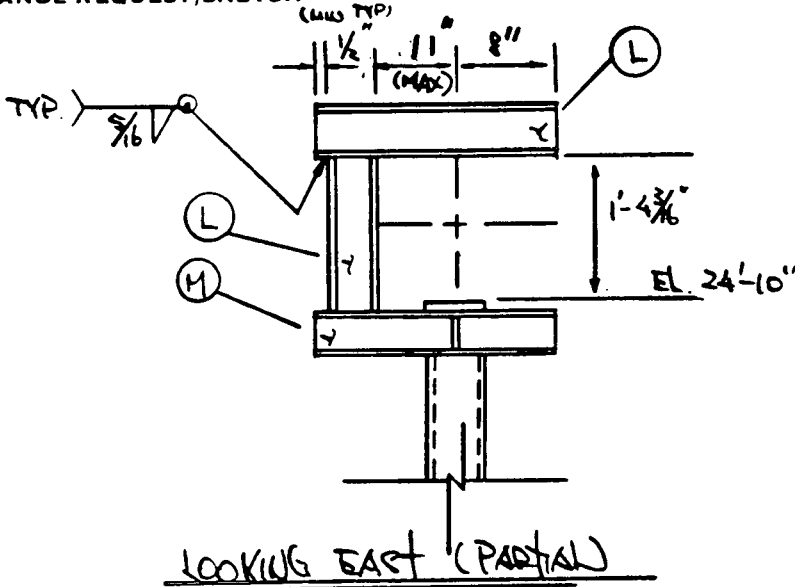
12C. DCN SUB NO. 3
12D. DATE MAR 25 1980
12E. SCN NO.

A (CCI)
RRR
JOB NO. 10079 (I.C.)
REV. 2 (C06-2)

5. TITLE PIPE SUPPORT ASSEMBLY
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: MEMBER TOO CLOSE TO THE WALL
WELD CAN NOT BE ACCOMPLISHED

8. CHANGE REQUEST/SKETCH



NO NEW MAT'L REQ'D

PL 5125

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 3-13-80
ELEC _____
MECH _____
WELD _____
PIPE INSTR _____
NUC _____
QA 3-14-80

11. APPROVAL OF FLD DISPOSITION
PREPARED BY [Signature]
PROJECT FIELD ENGINEER
DATE MAR 14 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: **CONVERT TO DCN**
P.E. R.L. Rogers/ML DATE 3-12-80

13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-14-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-25-80

16. ADDITIONAL DISTRIBUTION _____

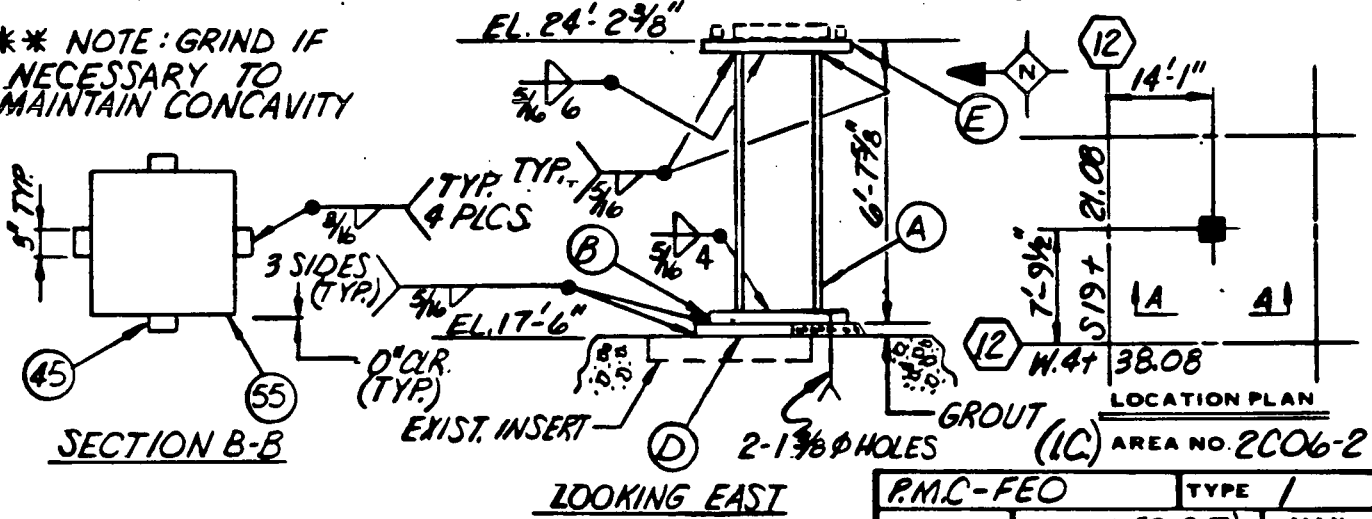
Lee

SUS-3888

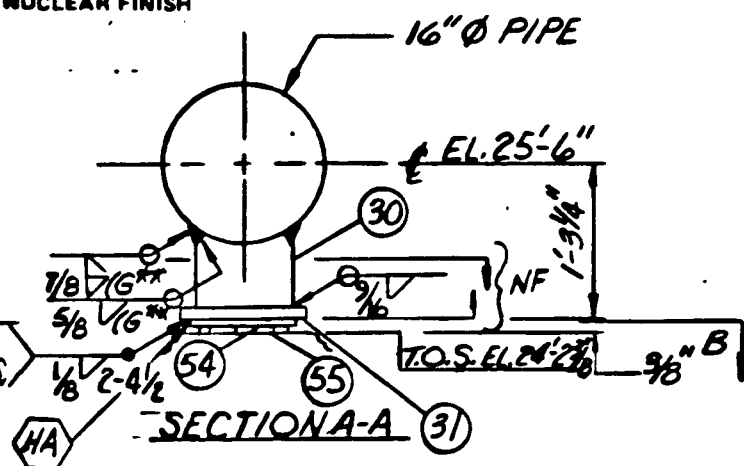
ITEM NO.	NO REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	8" SCH. 140 S.S. DUMMY PIPE		X		BY KELLOGG
31	1	-	12"x1 1/4"x12" C.S. P		X		BY KELLOGG
54	1	-	UPPER SLIDE BEARING R 10 GA. S.S. 11 1/2" x 11 1/2"				BY FIELD
55	1	-	LOWER SLIDE BEARING R BRONZITE 1/4"x11"x11"				BY FIELD
D	1	-	R 3/4 x 10 x 1'-5"				
A	1	-	W 8 x 31				SPEC.
B	1	-	R 3/4 x 16 x 1'-4"				S023-206-1B
E	1	-	R 1 1/4 x 1'-0 1/4 x 1'-0 1/4"				BY FIELD
45	4	-	C.S. BAR 3/16" x 3/16" x 3"				BY FIELD
	2	-	US-8-HC-LCSF-175				

* INTEGRAL ATTACH. USE ASME SECT. III, SUBSECTION 'NB' MAT'L.

** NOTE: GRIND IF NECESSARY TO MAINTAIN CONCAVITY



COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH



P.M.C.-FEO		TYPE I		
PROJ CL	PIPE A(Q.C.I)	MAX. TEMP		
QUAL CL	STEEL II	650-F		
DESIGN		X	Y	Z
	M +	—	—	—
	(FT-LBS)	—	—	—
	P +	—	0	—
(LBS)	—	28914	—	—

PROB. NO. 52 FT. NO. 104
 SPOOL NO. 2-RC-016-5
 ISO 1201-016-1
 PIPE 40400
 REF. DWGS. STEEL

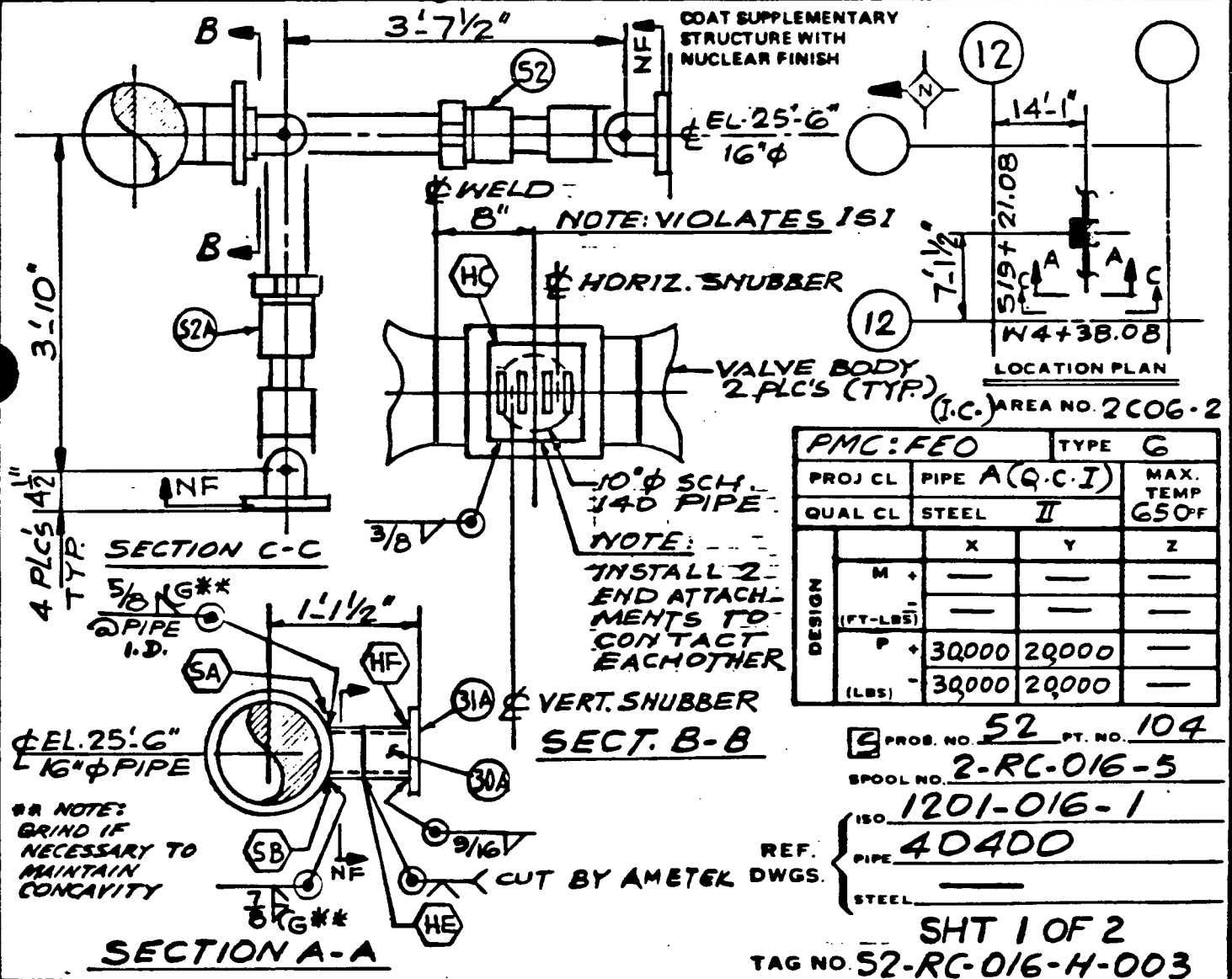
TAG NO. S2-RC-016-H-002

3	REDRAWN + INCORP. DCN'S #1,2	2-26-80	DR.	CHK.	KG R AB	E.G.S.	P.E.	C.A.E.
---	------------------------------	---------	-----	------	---------	--------	------	--------

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY			LOS ANGELES, CALIF.		

S.U.S. 28HA

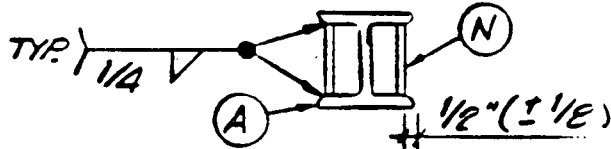
ITEM NO.	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
52	1	307	35-6"	MECH. SHOCK SUPPRESSOR, NUCLEAR CLASS T, C.S. F.B.D. H.S. 2.21" W=8.75, LOAD=2956# W/ADDITIONAL REAR BRACKET	X		BY GRINNELL
52A	1	307	35-6"	MECH. SHOCK SUPPRESSOR W/OPTION NUCLEAR CLASS T, C.S. F.B.D. H.S. 2.21" W=8.75, LOAD=18,000# (USE SURPLUS SNUBBER FROM 52-RC-017-H-030 (NE))	X		BY FIELD
30A	1		10" φ SCH. 140 B.S. DUMMY PIPE		X		
31A	1		# 1/4" X 1/4" X 1'-2" C.S.		X	X	BY FIELD
L	1		# 1/2" X 1/2" X 1'-2" C.S.		X	X	BY FIELD
				* INTEGRAL ATTACH. USE ASME SUBJECT 'NB' MAT'L			
A	2		W 10 X 49	US-B-HC-LCSF-115		X	SPEC. 2025-206-18
D	2		3/8" STIFF. B			X	
K	1		B=1X1B X 1'-6"			X	
M	1		W 10 X 49			X	BY FIELD
N	1		B=1/2" STIFF.			X	
X	2		B=1/2 X B 1/2 X 1'-2"			X	



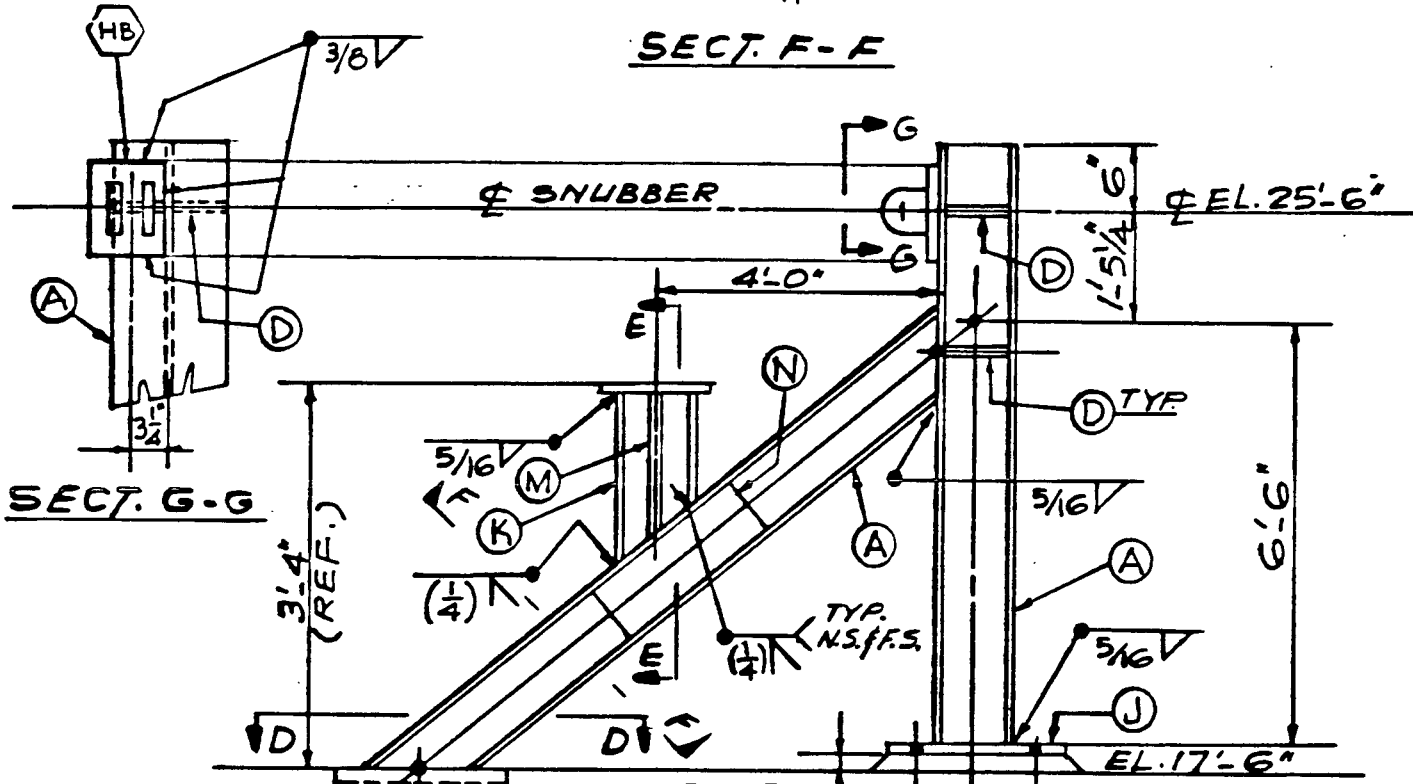
NO.	INCORP. DEN 1, 2, 3, 4, 5	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	O.A.E.
			2-28-80	D.P.	DAR	ST MB		

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					

S.U.S. 2BMA

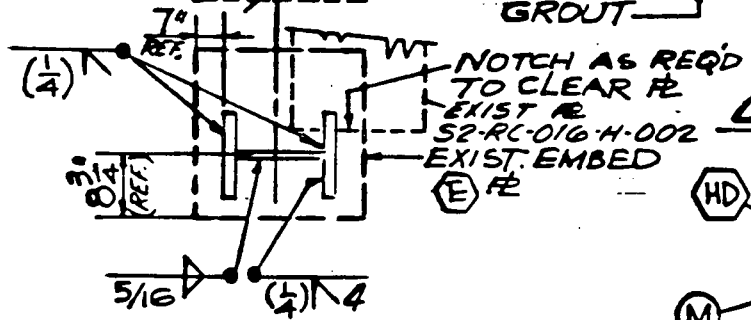


SECT. F-F



SECT. G-G

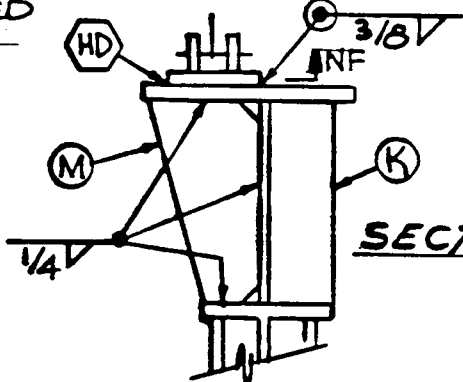
3'-4\"/>



SECT. D-D

1 1/2\"/>

LOOKING EAST



SECT. E-E

1201 SHT. 2 OF 2
 S2-RC-016-H-003 REV. 4

BECHTEL POWER CORPORATION BERKELEY, CALIFORNIA			10. NO.	SAR ONOFRE NUCLEAR GENERATIVE STATION	
			FILE	PWT SUPPORT ASSEMBLY	
DESIGN 10079	DATE	APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY SCALE NTS LOS ANGELES, CALIF.	

APR 24 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-5024
DATE 4-16-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 09
12D. DATE APR 30 1980
12E. SCN NO.

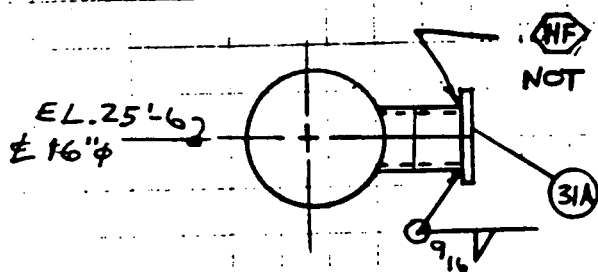
JOB NO. 10079 IC 2062

REF. DWG. OR SPEC. S2-RC-016-H-003 SHEET NO. 4 REV. 4 5. TITLE PIPE SUPPORT ASSEMBLY

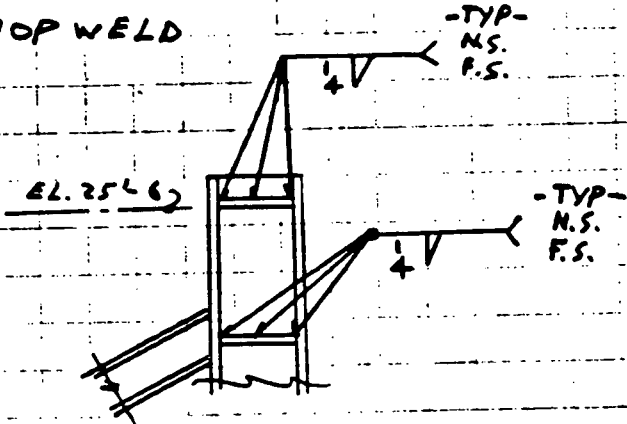
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: CHANGE B/M QTY
WELD - FROM FIELD TO SHOP
WELD IDENTIFIER NOT REQ'D

8. CHANGE REQUEST/SKETCH
B/M ITEM # D CHANGE QTY TO 4



SECTION A-A
(PARTIAL)



LOOKING EAST
(PARTIAL)

NO NEW MATERIAL REQ'D

PL-5411

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY _____ DATE _____
CIVIL _____ PIPE M.S. 4-17-80
ELEC _____ INSTR _____
MECH _____ NUC _____
WELD _____ GAS 4-17-80

MARIO CAMPANILE
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
Dennis J. Hayes
PROJECT FIELD ENGINEER
DATE APR 19 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers DATE 4-16-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): B. Salomon DATE 4-17-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE J.W. Sheppard DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____

APR 4 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 51869
DATE 3/25/80
2. PAGE 1 OF 1
3. UNIT NO. II

12A. QUALITY CLASS I
12B. SPEC ADDENDUM NO.

12C. DCN SUBNO. 07
12D. DATE APR 15 1980
12E. SCN NO.

DBHA
A

JOB NO. 10079 (I.C.) 20061

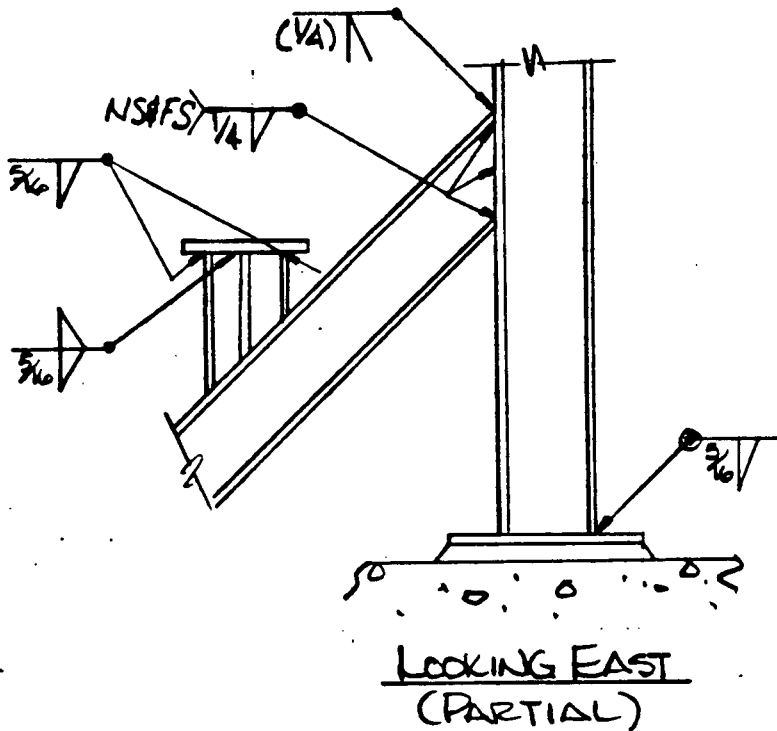
REF. DWG. OR SPEC. SHEET NO. REV. 3. TITLE
52-RC-C16-H-003 4 PIPE SUPT. ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

INCOMPLETE WELD REQ'MENTS. CALLED FOR ON DWG.

8. CHANGE REQUEST/SKETCH



APR 5 1980 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE
CIVIL _____	PIPE <u>H.S.</u> <u>3-29-80</u>
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QA <u>Approved</u> <u>3-27-80</u>

PREPARED BY	DATE
<u>C.W. GREER</u>	<u>MAR 27 1980</u>
11. APPROVAL OF FLD DISPOSITION	
<u>David J. Blaney</u>	
PROJECT FIELD ENGINEER	

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers / JRM DATE 3-27-80

REMARKS: CONVERT TO DCN.

13. QUALITY ASSURANCE ENGINEER (FIELD):	DATE
<u>[Signature]</u>	<u>3-27-80</u>
14. SCE ENGINEERING APPROVAL	DATE
<u>[Signature]</u>	<u>4-11-80</u>
15. BECTHEL QUALITY ENGINEER/QUALITY ASSURANCE	DATE
<u>[Signature]</u>	
16. ADDITIONAL DISTRIBUTION	

APR 16 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-2552
DATE 4.8.80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 08
12D. DATE APR 30 1980
12E. SCN NO.

A JOB NO. 10079 (1.L.) 2106.2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
RC.016.H.003 4 PIPE SUPT ASSEMBLY

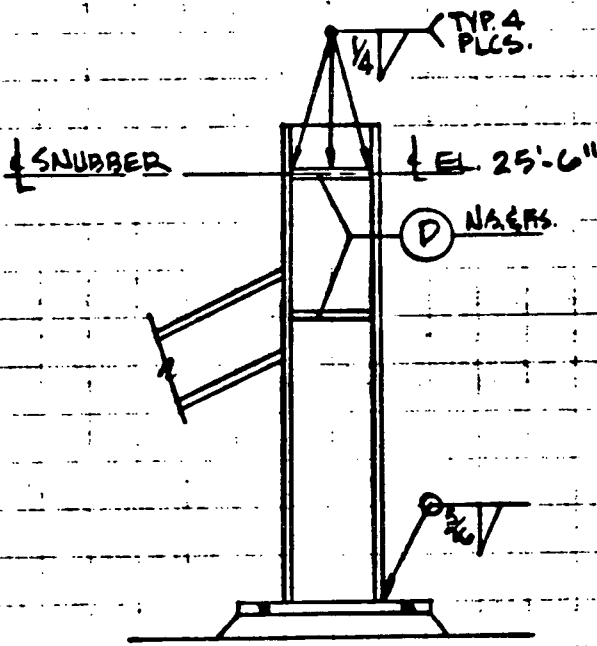
DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

12c1

7. EXISTING CONDITION:

- 1. WELD CALL-OUT FOR ITEM "D" MISSING
- 2. SHOP WELD SHOWN AS FIELD WELD
- 3. WRONG AMOUNT SHOWN FOR ITEM "D"

8. CHANGE REQUEST/SKETCH



CHG. DOWM TO READ:
ITEM "D" - NO. REQ'D. 4

LOOKING EAST
(PARTIAL)

PL# 5353 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE

CIVIL _____ DATE _____

ELEC _____ DATE _____

MECH _____ DATE _____

WELD _____ DATE _____

PIPE M.S. 4-7-80

INSTR. _____

NUC _____

QA approved 4-8-80

PREPARED BY C.W. GREER

11. APPROVAL OF FCD DISPOSITION

Dennis O'Hara

PROJECT FIELD ENGINEER

DATE APR 08 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____

REMARKS: CONVERT TO DCN

P.E. R.L. Rogen DATE 4-7-80

QUALITY ASSURANCE ENGINEER (FIELD): approved DATE 4-8-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE BB DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____

X



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-470
DATE 3-8-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 06
12D. DATE MAR 25 1980
12E. SCN NO.

A(DCI)
ZBLA JOB NO. 10079 C
REF. DWG. OR SPEC. SHEET NO. REV 4/3 5. TITLE PIPE SUPPORT ASSEMBLY
S2-RC-016-H-003

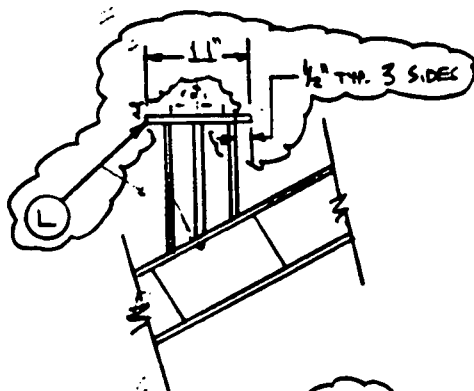
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: WELDS NOT REQUIRED, PLATES EITHER NOT IDENTIFIED OR IDENTIFIED INCORRECTLY ON DCN #04 (PLATE UNDERLINED)

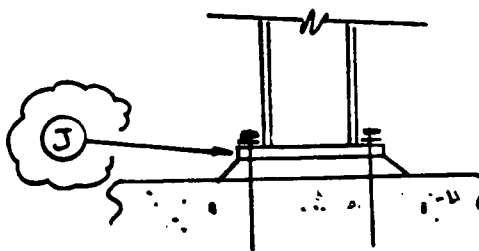
8. CHANGE REQUEST/SKETCH

R5110

NOTE: FROM SECTION "A-A" (REV. 3 DRAWING), DELETE WELD IDENTIFIER "HA"



LOOKING EAST (CHANGES ONLY)



BILL OF MATERIAL

1. CHANGE SIZE ON ITEM # L FROM 1" x 10" x 10" TO 1" x 11" x 1'-0"

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 3-11-80
ELEC _____
MECH _____
WELD _____
PIPE RS
ELEC RS
NUC RS
DATE 3-12-80

9. R.L. ELLINGTON
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
Louis J. Gentry
PROJECT FIELD ENGINEER
DATE MAR 12 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/KH DATE 3-11-80

REMARKS: **CONVERT TO DCN**

QUALITY ASSURANCE ENGINEER (FIELD): J.W. Sheppard DATE 3-12-80

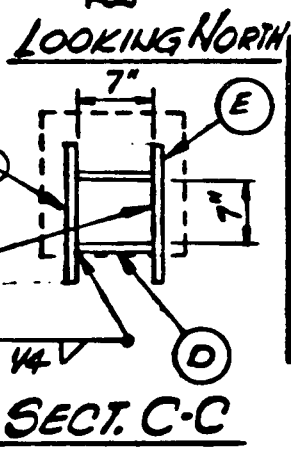
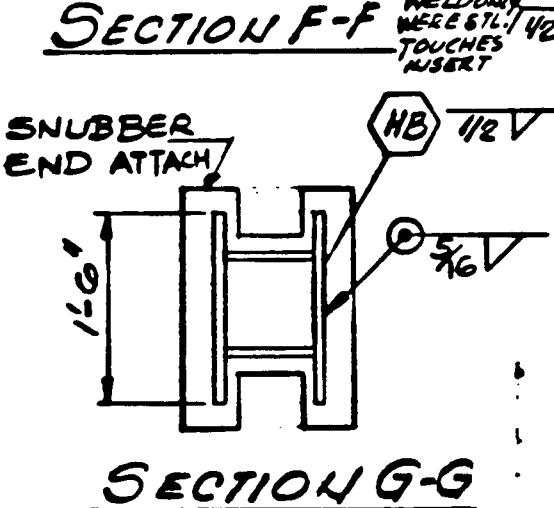
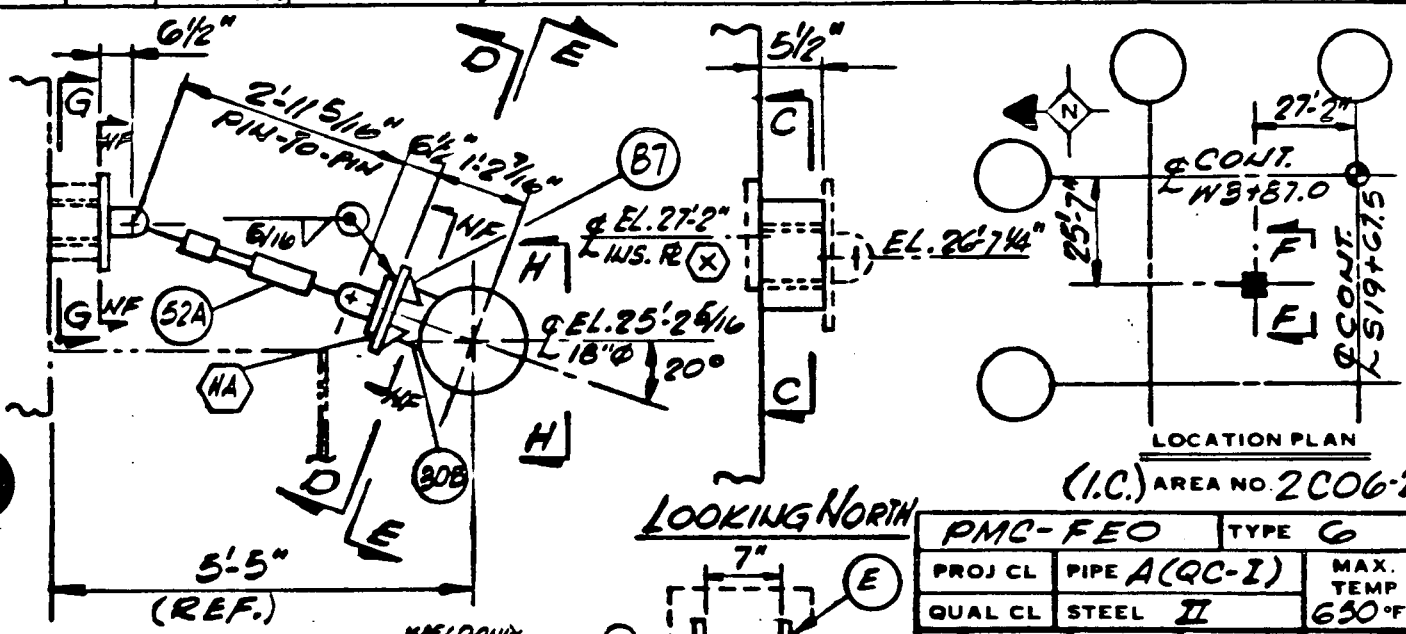
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE J.W. Sheppard DATE 3-25-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO	NO REC'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
30B	1	-	10" ϕ SCH. 160 S.S. DUMMY STUB		*		SPEC. 5023-
31A	1	-	R 1 1/4 X 12 X 1-10"		X		409-23.
37	4	-	1/2" GUSSET R		X		"
52A	1	-	PSA 100-G PART NO. 1811 SERIAL 021-02	SHOCK ARRESTOR KIT NUCLEAR CLASS I	X		PSC
				H.S. = 3.473" C.S. = 2.528",			
				LOAD = 132,237#			
D	2	-	R 3/4 X 7 X 0-55/8"			X	BY FIELD
E	2	-	R 3/4 X 5 5/8 X 1-6"			X	"

* INTEGRAL ATTACHMENT, USE ASME SECT. III SUBSECTION 'NB' MAT'L.



PMC-FEO		TYPE G	
PROJ CL	PIPE A(QC-1)	MAX. TEMP 650°F	
QUAL CL	STEEL II		
DESIGN	M +	X	Y
	(FT-LBS)	-	-
(LBS)	P +	23307	132241
	-	23307	132241

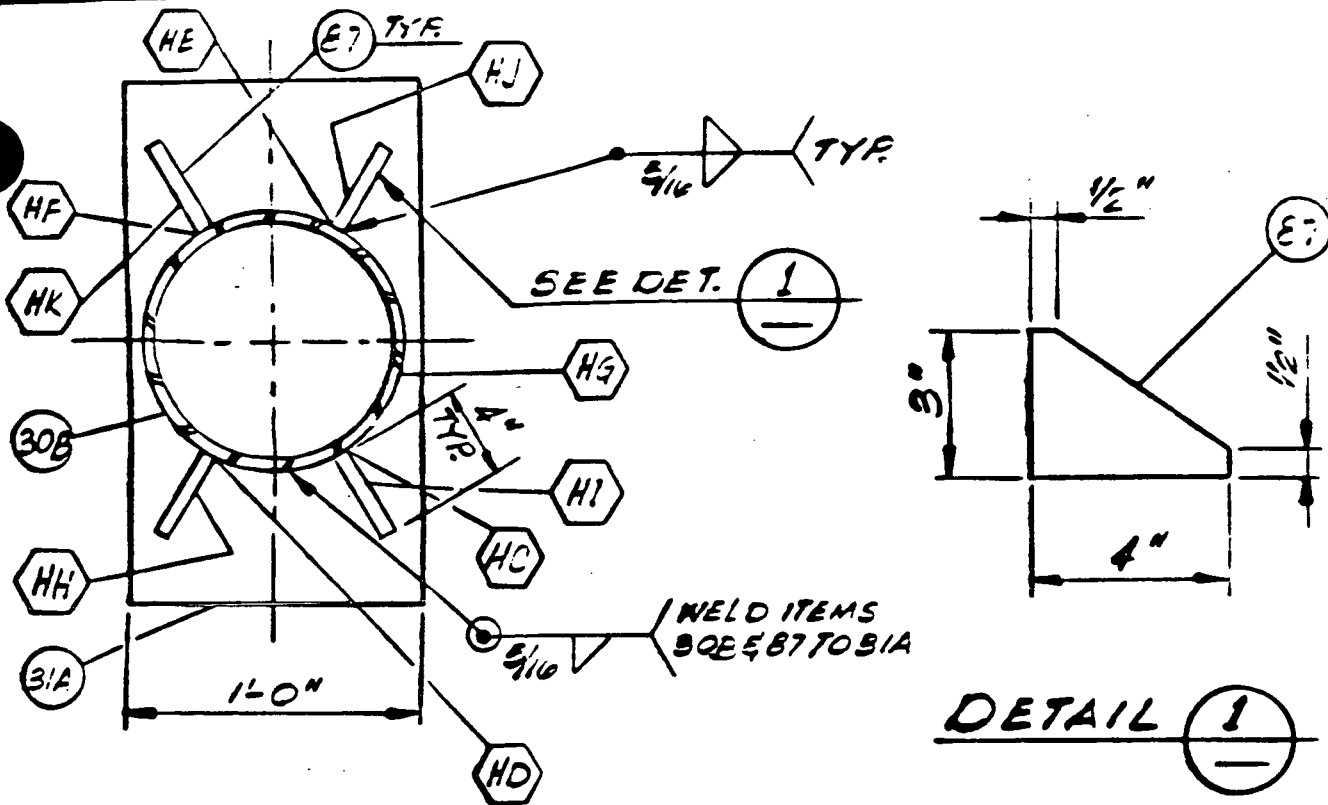
PROB. NO. 52 FT. NO. 253
 SPOOL NO. 2-RC-016-3
 ISO 1201-016-1
 PIPE 40400
 STEEL
 SHT 1 OF 2
 TAG NO. S2-RC-016-H004

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

2	REDRAWING INC. DCN 1,253	2-28-80	YL	ST	KG MB	RLR/SAR/RS
	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E. O.A.E.

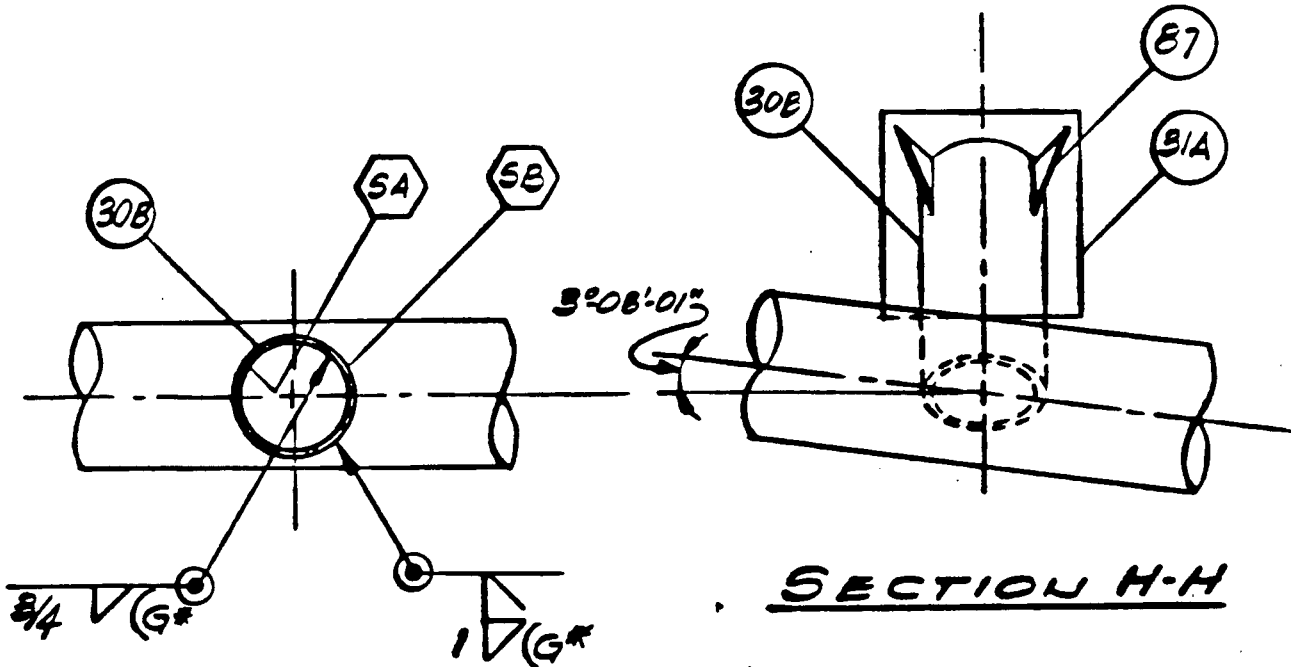
BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
		FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.			

S.U.S. 2 B



SECTION D-D

*GRIND IF NECESSARY TO MAINTAIN CONCAVITY.



SECTION E-E

SECTION H-H

1201 SHT 2 OF 2
 S2-RC-016-H-004 REV.2

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
			FILE	PIPE SUPPORT ASSEMBLY	
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.		

APR 4 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4877
DATE 3-26-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 05
12D. DATE APR 15 1980
12E. SCN NO.

A(QCI) 2BBB JOB NO. 10079 (1.C) 200-2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE

S3-RC-016-H-008 SHEET NO. 2 TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: CHANGE BILL OF MATL

8. CHANGE REQUEST/SKETCH

BILL OF MATL (BY FIELD)

1. CHANGE ITEM 52B TO 52C.
USE S3-ST-001-H-008.
306.100-6"
C.S = 2.52" H.S = 3.47"

PL 5289

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE M.S. 3-27-80
INSTR _____
NUC _____
QAE E. B. Lutz 3/27/80

9. K. C. ... PREPARED BY
11. APPROVAL OF FLD DISPOSITION
R. L. ... PROJECT FIELD ENGINEER
DATE 3-28-80

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: **CONVERT TO DCN**
P.E. R. L. ... DATE 3-27-80


QUALITY ASSURANCE ENGINEER (FIELD): E. B. Lutz DATE 3/27/80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE R. L. ... DATE 4-11-80

16. ADDITIONAL DISTRIBUTION _____

MAR 31 1980

 SAN ONOFRE NUCLEAR GENERATING STATION UNITS 2 & 3 FIELD CHANGE REQUEST/DCN/SCN	1. FCR NO. <u>S-4849</u>	12A. QUALITY CLASS <u>I</u>	12C. DCN SUB NO. <u>04</u>
	DATE <u>3-21-80</u>	12B. SPEC ADDEND. NO.	12D. DATE <u>APR 8 1980</u>
	2. PAGE <u>1</u> OF <u>1</u>	3. UNIT NO. <u>2</u>	12E. SCN NO.

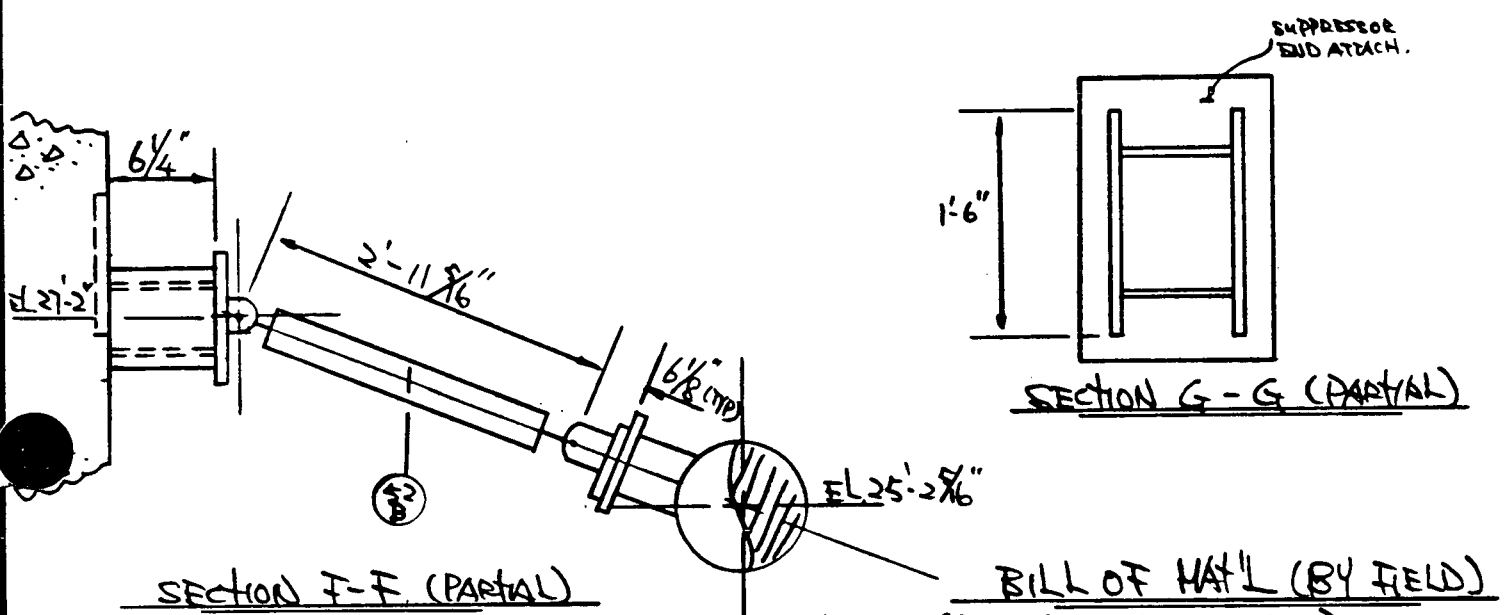
A (OCI) ORRR JOB NO. 10079 (I.C.) 2062

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: CHANGE BILL OF MATL

8. CHANGE REQUEST/SKETCH



- CHANGE ITEM 52A TO 52 B
USE SS-ST-001-H-007.
306 100 - 6" STROKE SUPPRESSOR.
C.S = 2.52" H.S = 341.
- CHANGE DIMENSION OF ITEM D
(2 REQ'D) FROM $R \frac{3}{4} \times 7 \times 0'-5 \frac{7}{8}"$ TO $R \frac{3}{4} \times 7 \times 6 \frac{1}{4}"$
- CHANGE DIMENSION OF ITEM E FROM
 $R \frac{3}{4} \times 5 \frac{7}{8} \times 1'-6"$ TO $R \frac{3}{4} \times 6 \frac{1}{4} \times 1'-6"$ (2 REQ'D)

PL 255

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PREPARED BY
CIVIL _____	_____	<u>Hui Chi Shing</u>
ELEC _____	_____	APPROVAL OF FIELD DISPOSITION
MECH _____	_____	<u>Royce Harvey</u>
WELD _____	_____	PROJECT FIELD ENGINEER
PIF <u>GS-5</u>	<u>3-24-80</u>	DATE <u>3-24-80</u>
INSTR _____	_____	
NUC _____	_____	
QAE <u>planned</u>	<u>3-24-80</u>	

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/RH DATE 3-24-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): planned DATE 3-24-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE R. L. Rogers DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

APR 17 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4933
DATE 4-3-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDENDUM NO.

12C. DCN SUB NO. 06
12D. DATE APR 30 1980
12E. SCN NO.

A(OCI) 2288 (I.C.)
JOB NO. 10079 206-2

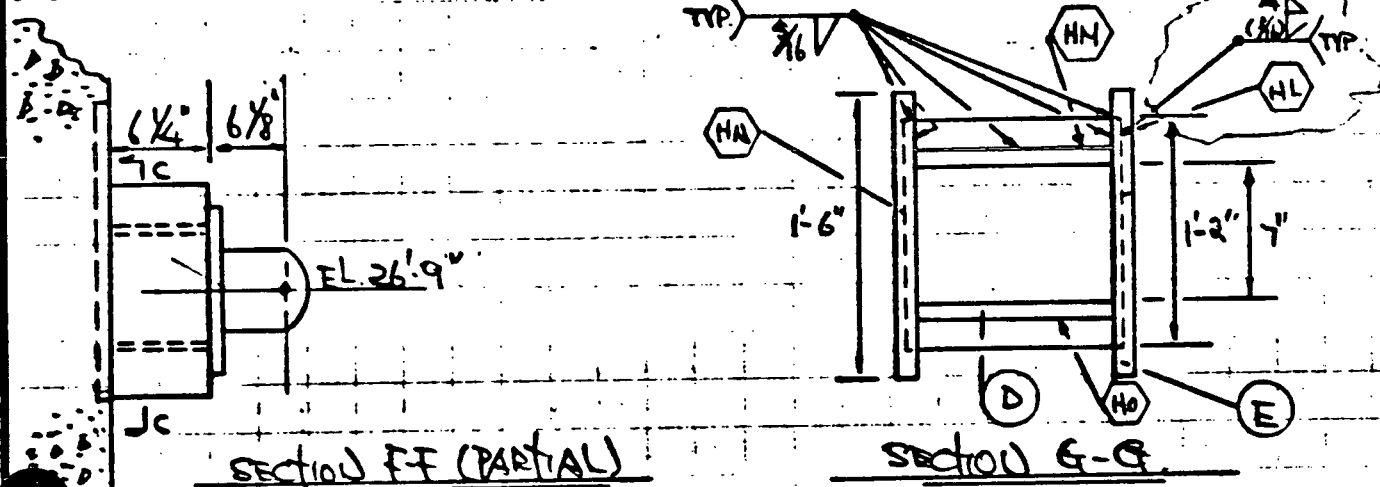
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
RC-016-H-004 2 PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: CLARIFICATION OF DWGS

THIS FCR SUPERSEDES FCR S-4877, S-4849

8. CHANGE REQUEST/SKETCH

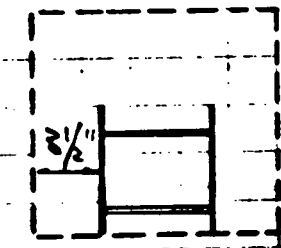


SECTION FF (PARTIAL)

SECTION G-G

BILL OF MATERIAL (BY FIELD)

- 1. DELETE WELD ID HB & VIEW LOOKING NORTH
- 2. CHANGE ITEM 52B TO 52C
- USE S8-ST-001-H-008
- 306 100-6"
- C.S = 2.52" H.8 = 3.47"



SECTION C-C (PARTIAL)

PL 5349

SUPERSEDES
FCR 5-4877-5-4849

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
 CIVIL _____ DATE _____
 ELEC _____ DATE _____
 MECH _____ DATE _____
 WELD _____ DATE _____
 PIPE M.S. 4-4-80
 INSTR _____
 NUC _____
 GAE E.B. L. 4/4/80

11. APPROVAL OF FLD DISPOSITION
 PREPARED BY [Signature]
 PROJECT FIELD ENGINEER
 DATE APR 04 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers DATE 4-9-80

REMARKS: **CONVERT TO DCN** VOID DCN 445

QUALITY ASSURANCE ENGINEER (FIELD): E.B. L. DATE 4/4/80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____

X

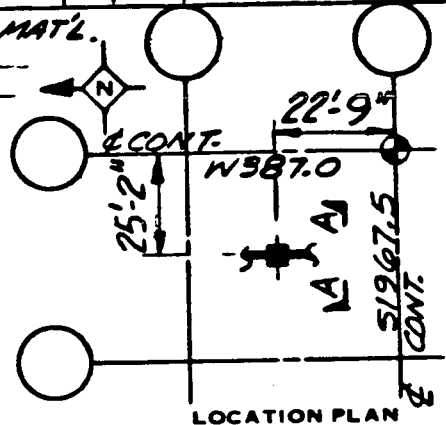
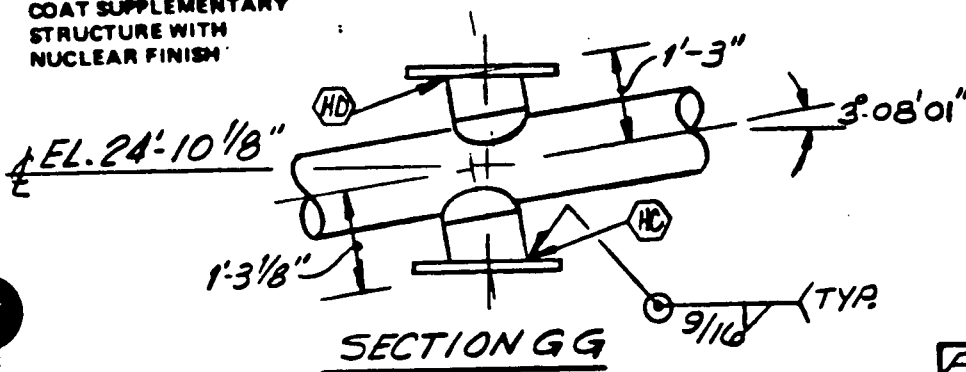
VOID FCR S-4877, S-4849
VOID DCN 445

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
31	2	-	14"X14"X1 1/4 C.S. R.		X		BY KELLOGG
30	2	-	10" SCH. 140 S.S. DUMMY PIPE		*		" "
54	1	-	10 GA. S.S. 13 1/2" X 13 1/2" UPPER SLIDE BEARING				BY FIELD
55	1	-	1/4 X 13" X 13" BRONZITE LOWER SLIDE R.				
45	4	-	C.S. BAR 3/16" X 3/16" X 3"				
F	2	-	R 1/2 X 14 X 1'-2"			X	
G	8	-	1/2" R.			X	
H	8	-	1/2" STIFF. R.			X	
J	1	-	R 1/2 X 10 X 0'-10"			X	
K	5	-	W 8 X 5 8			X	
L	1	-	W 6 X 2 5			X	
M	1	-	R 2" X 2 8" X 2'-4"			X	
N	1	-	R 1 1/4 X 1 7" X 1'-5"			X	
	12	-	US-B-HC-LCSF-175				

* INTEGRAL ATTACHMENT, USE ASME SECT. III SUBJECT 'NB' MAT'L.

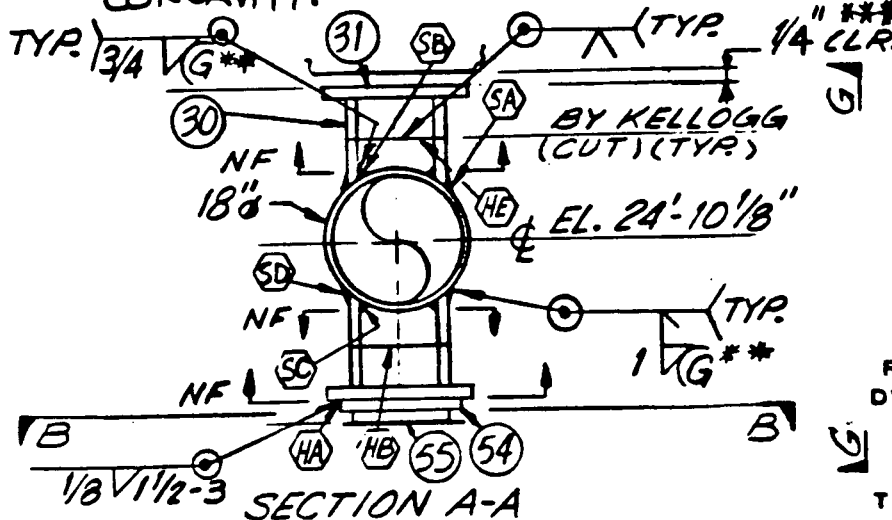
*** NOTE: MIN TOTAL CLRC. REQ'D. IS 3/16"

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH



I.C. AREA NO. 2C062

** GRIND IF NECESSARY TO MAINTAIN CONCAVITY.



PMC: FEO		TYPE 2		
PROJ CL	PIPE A (QCI)	MAX. TEMP		
QUAL CL	STEEL II	650°F		
DESIGN	(FT.-LBS)	X	Y	Z
	(LBS)	0	88071	0
		0	109510	0

PROB. NO. 52 FT. NO. 53

SPOOL NO. 2RC-016-3

ISO 1201-016-1

PIPE 40400

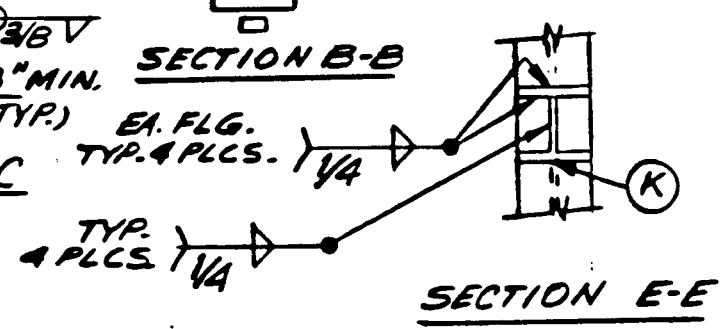
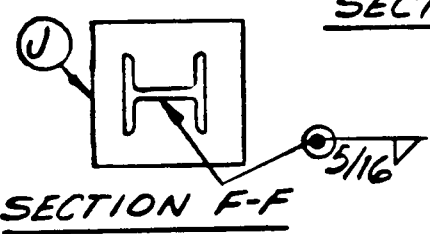
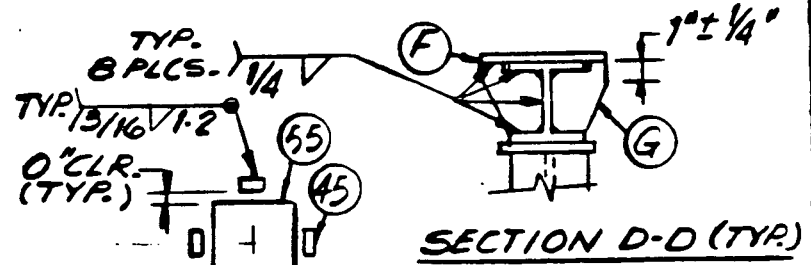
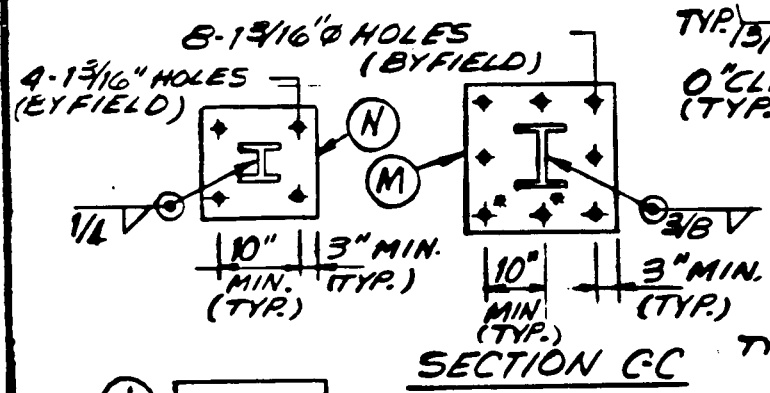
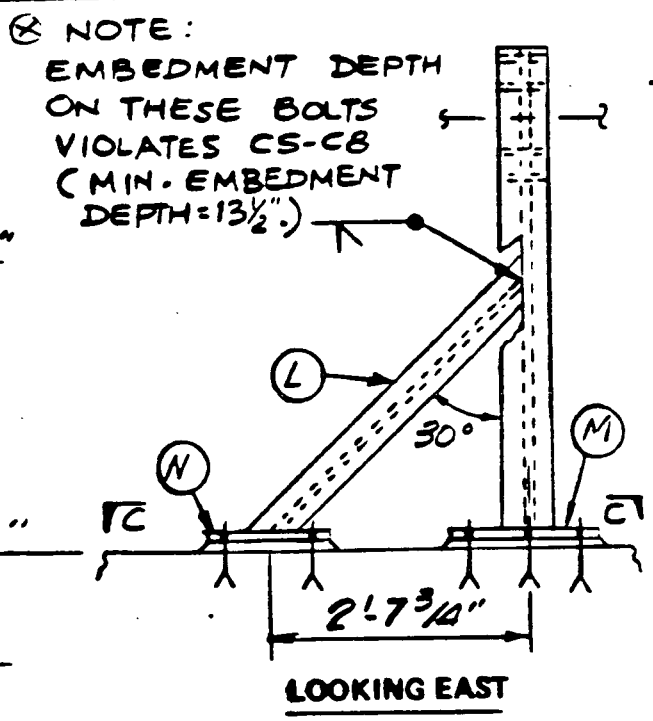
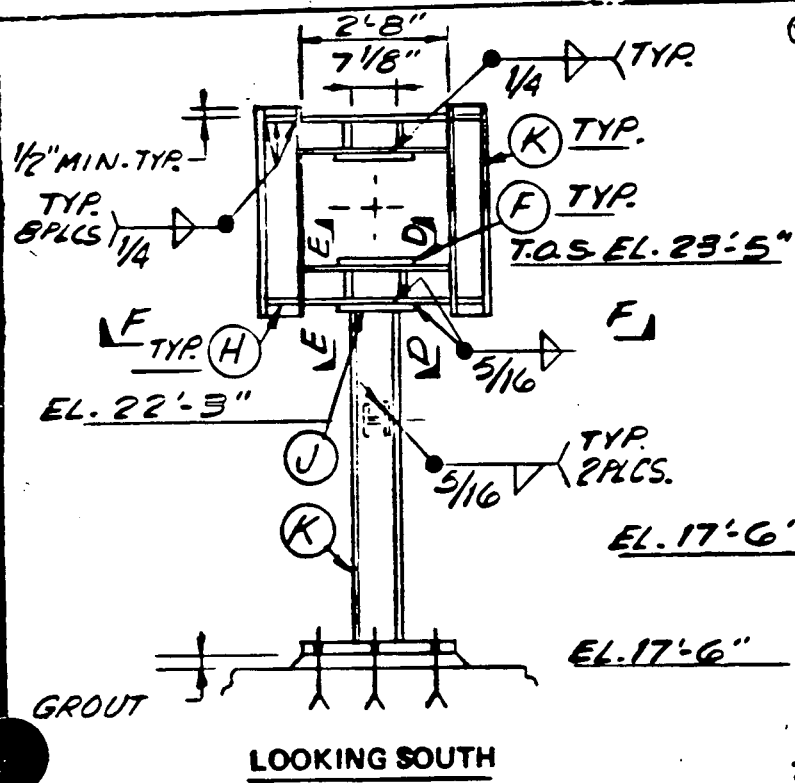
STEEL SHT 10F2

TAG NO. S2-RC-016-H-005

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	G.A.E.
4	INCORR DCN 1, 2, 3, 4 & REDRAWN	2-28-80	18	SA	KG MB		

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
		FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

ITEM NO.	QTY	ART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES



NOTE:
 EMBEDMENT DEPTH
 ON THESE BOLTS
 VIOLATES CS-CB
 (MIN. EMBEDMENT
 DEPTH = 13 1/2")

12c1 SHT 2 OF 2
 S2-RC-016-H-005 REV4

BECHTEL POWER CORPORATION DORWALK, CALIFORNIA			LD NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
			FILE	PIPE SUPPORT ASSEMBLY	
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON SCALE NTS LOS ANGELES CALIF.		

APR 7 1980

A=24 S=409 I=112.0

100 C



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S4868
DATE 3-25-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 05
12D. DATE APR 15 1980
12E. SCN NO.

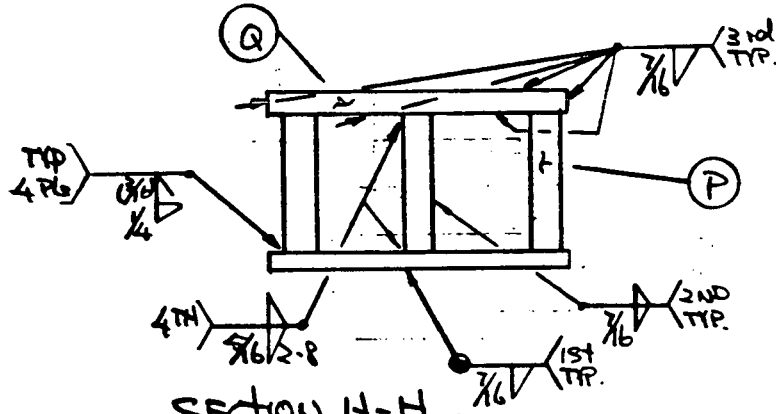
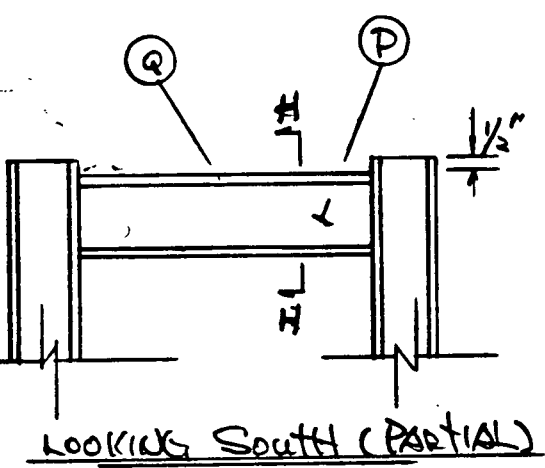
JOB NO. 10079 (I.C.) 2006-2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2 RC-016-H-005 4 PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)
1201

7. EXISTING CONDITION: 1" CLR BETWEEN R.C. PUMP EXTRACT TO THE TOP OF DUMMY PIPE. MODIFICATION REQ'D BY FIELD

8. CHANGE REQUEST/SKETCH



SECTION H-H
BILL OF MATERIAL (BY FIELD)

1. CHANGE ITEM K FROM 5 TO 4.
2. CHANGE ITEM G FROM 8 TO 4.
3. ADD ITEM Q TR 1" X 8" X 2'-8" (2 REQ'D)
4. ADD ITEM P TR 1" X 4" X 2'-8" (3 REQ'D)

PLS 278

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY _____ DATE _____

CIVIL _____ PIPF L.S. 4-2-80

ELEC _____ INSTR _____

MECH _____ NUC _____

WELD _____ QA B.L. Johnson 4-2-80

9. Mr. Chi Shing PREPARED BY

11. APPROVAL OF FIELD DISPOSITION

Dennis J. Laney PROJECT FIELD ENGINEER

DATE APR 02 1980

2. PROJECT ENGRG APPROVAL: YES NO EGS. P.E. R.L. Keyser-RH DATE 4-2-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): B.L. Johnson DATE 4-2-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B.L. Johnson DATE 4-11-80

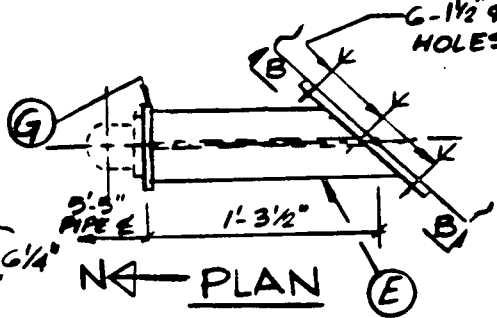
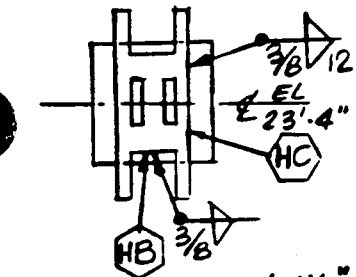
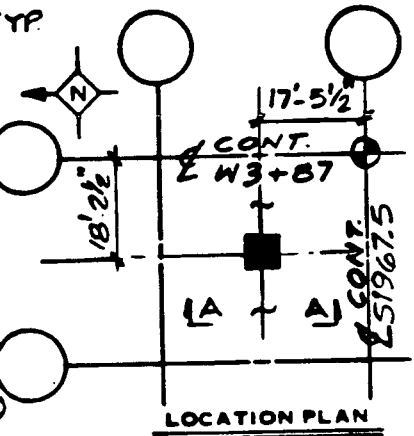
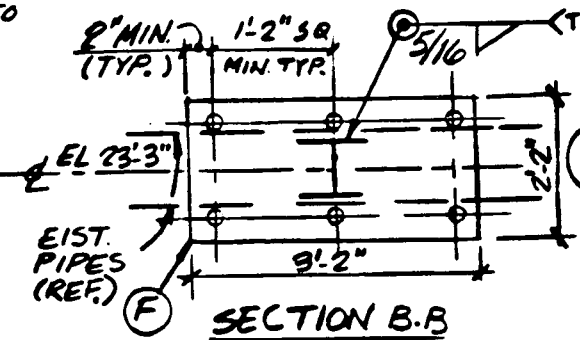
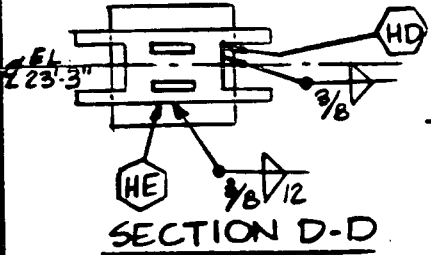
16. ADDITIONAL DISTRIBUTION _____

2

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	10" SCH. 140 S.S. DUMMY PIPE		*		BY KELLOGG
31	1	-	14" x 14" x 1/4" C.S. PL.		X		"
52A	1	306	PSA-#100-6 P/N 1B11021-02 SNOCK		X		BY GRINNEL
			ARRESTOR KIT. CPS. = 3.45" H.P.S. = 2.55"				
			LOAD = 91368"				
E	1		W10 x 49			X	BY FIELD.
F	1		PL 1/4" x 26" x 9'-2"			X	
G	1		PL 1" x 14" x 1'-2"			X	
	6		US-11-HC-LCSF-225			X	
							COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH.
* INTEGRAL ATTACHMENT - USE ASME SUBSECTION 'NB' MATERIAL.							

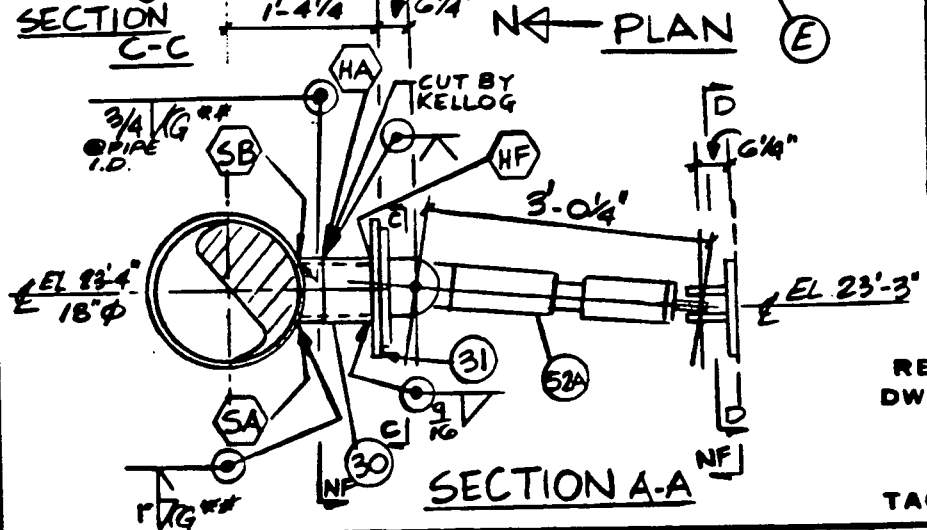
SUS-2BBB

* GRIND ONLY AS REQ'D TO INSURE CONCAVITY.



I.C. AREA NO. 2C062

PMC: FEO		TYPE G		
PROJ CL	PIPE A (QCI)	MAX. TEMP		
QUAL CL	STEEL II	650°F		
DESIGN		X	Y	Z
	M +	⊖	⊖	⊖
	(FT-LBS)	⊖	⊖	⊖
	P +	91368	⊖	⊖
	(LBS)	91368	⊖	⊖



5 PROB. NO. 52 FT. NO. 36
 SPOOL NO. 2-RC-016-2
 ISO 1201-016-1
 REF. DWGS. PIPE 40400
 STEEL

TAG NO. 52-RC-016-H-008

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
1	INC. 2' 3" DEN. VOIDED DEN. REDRAWN	2-26-80	KG		RB		

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
JOB NO. 10079		FILE	PIPE SUPPORT ASSEMBLY				
DATE		APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.			
SCALE: NTS		01-02-01					

MAR 31 1980

<p>SAN ONOFRE NUCLEAR GENERATING STATION UNITS 2 & 3 FIELD CHANGE REQUEST/DCN/SCN</p>	1. FCR NO. <u>8-4810</u>	12A. QUALITY CLASS <u>I</u>	12C. DCN SUB NO. <u>04</u>
	DATE <u>3-19-80</u>	12B. SPEC ADDEND. NO.	12D. DATE <u>APR 8 1980</u>
	2. PAGE <u>1</u> OF <u>1</u>	3. UNIT NO. <u>2</u>	12E. SCN NO.

AC(QCI) 2RBR JOB NO. 10079 (I.C.) 2206-2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: 12c1 ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: DIMENSION SHOWING INCORRECT
CHANGE BILL OF MAT'L

8. CHANGE REQUEST/SKETCH

SECTION A-A (PARTIAL)

SECTION B-B (PARTIAL)

SECTION D-D

BILL OF MAT'L (BY FIELD)

- CHANGE 52A TO 52 B. 306
100 - 6" SHOCK SUPPRESSOR
C.S = 3.45" H.S = 2.55"
USE S3-ST-001-14-009.
- CHANGE ITEM F DIMENSION FROM
1/4" X 3'-2" X 2'-2" TO 1/4" X 28" X 4'-1 1/2"
(REQ'D)

PL 5213

PROJECT ENGINEERING APPROVAL PER _____

10. REVIEWED BY	DATE	9. PREPARED BY
CIVIL _____	_____	<u>Steve Chi Shing</u>
ELEC _____	_____	11. APPROVAL OF FLD DISPOSITION
MECH _____	_____	<u>James J. Murray</u>
WELD _____	_____	PROJECT FIELD ENGINEER
PIPF <u>M.S.</u>	<u>3-21-80</u>	DATE <u>3-21-80</u>
INSTR _____	_____	
NUC _____	_____	
QA <u>approved 3-24-80</u>	_____	

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/PLH DATE 3-21-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): John J. ... DATE 3-24-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B. J. ... DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 4844
DATE 3-23-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 05
12D. DATE APR 8 1980
12E. SCN NO.

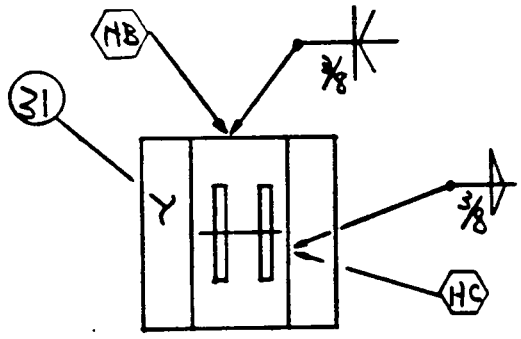
JBBB (QCI) JOB NO. 10079 (I.C.) 206-2

4. REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-016-A-008 1 PIPE SUPPORT ASSEMBLY

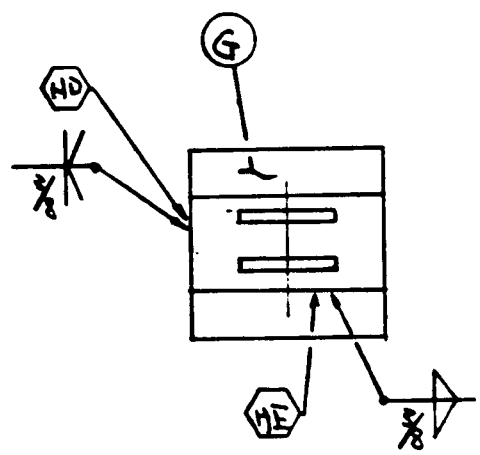
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION: DUMMY TR & END BRACKET ARE THE SAME SIZE.

8. CHANGE REQUEST/SKETCH



SECTION C-C



SECTION D-D

NO NEW MATH REQD

TR 5265

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE R.L.S. 3-24-80
INSTR _____
NUC _____
QA Stephenson 3-24-80

9. Stephenson
PREPARED BY
11. APPROVAL OF FLD DEPOSITION
Stephenson
PROJECT FIELD ENGINEER
DATE 3-24-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Royer/RH DATE 3-24-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): Stephenson DATE 3-24-80

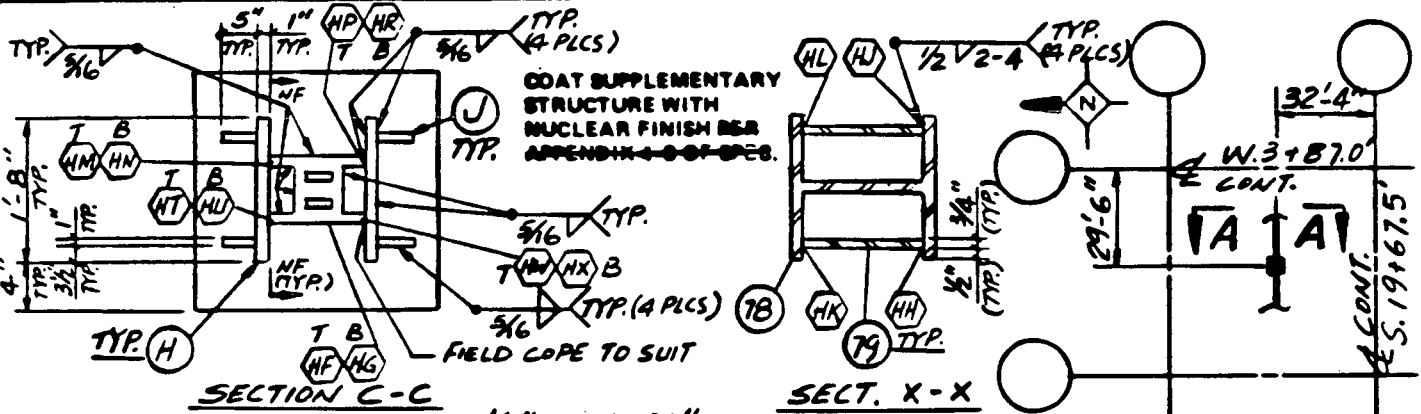
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE Stephenson DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES	
30	1		8" ϕ SCH 160	S.S. DUMMY PIPE	**		AMETEK	
31	1		1/4" x 12" x 1'-0"	C.S. R			5023-409-23	
78	1		WB x 35 x 4'-0"				BY FIELD	
79	2		R 3/4" x 7/8" x 4'-0"					
80	1		WB x 35 x 0'-5 3/4"					
52A	2		PSA-35-6" STROKE	P/N 1B11021-02			BY PSC	
			SHOCK ARRESTOR KIT, C.S. = 2.13", H.S. = 3.85"					
			LOAD = 40757" EACH.					
H	4		BAR 1" x 4" x 1'-8"				BY FIELD	
J	8		BAR 1" x 4" x 0'-5"					
** INTEGRAL ATTACH. USE ASME SUBSECT. "NB" MAT'L								

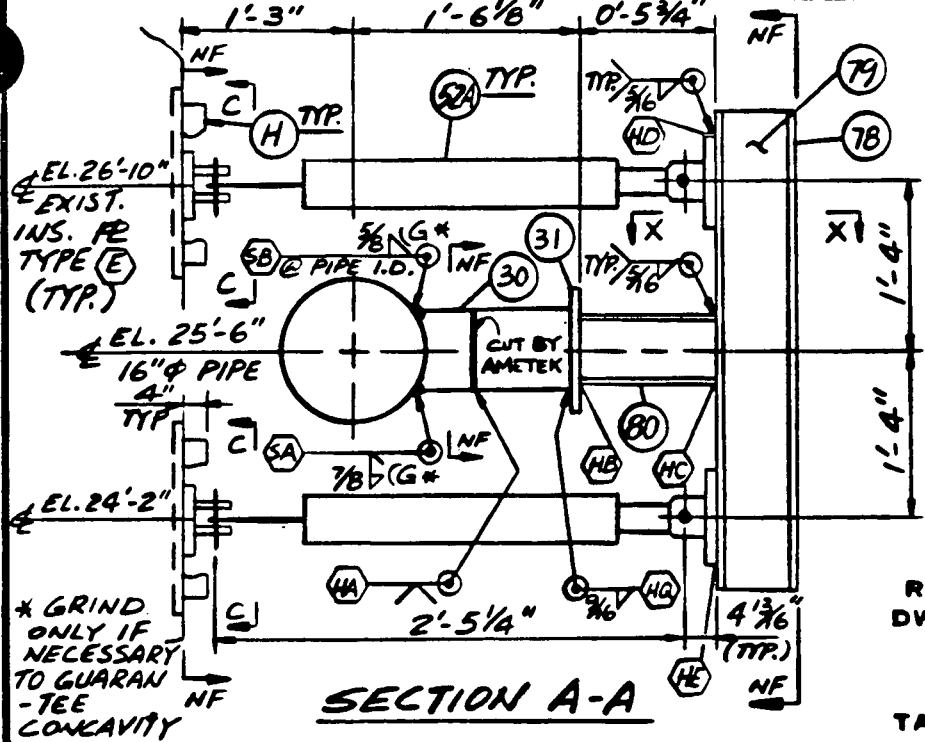
SUS-288B



PMC-FEO		TYPE 6		
PROJ CL	PIPE A(QCI)	MAX. TEMP		
QUAL CL	STEEL II	650°F		
DESIGN	M +	X	Y	Z
	(FT-LBS)	-	-	-
P +	81413	-	-	-
	(LBS)	81413	-	-

[S] PROB. NO. 52 PT. NO. 69
 SPOOL NO. 2-RC-016-3
 ISO. 1201-016-1
 REF. DWGS. PIPE 40400
 STEEL _____

TAG NO. 52-RC-016-H-009



NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	O.A.E.
1	INCORP. DCN 1, 2 & 3 & REDRAWN	2-26-80	QT	KG	RL		

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4025
DATE 3-19-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

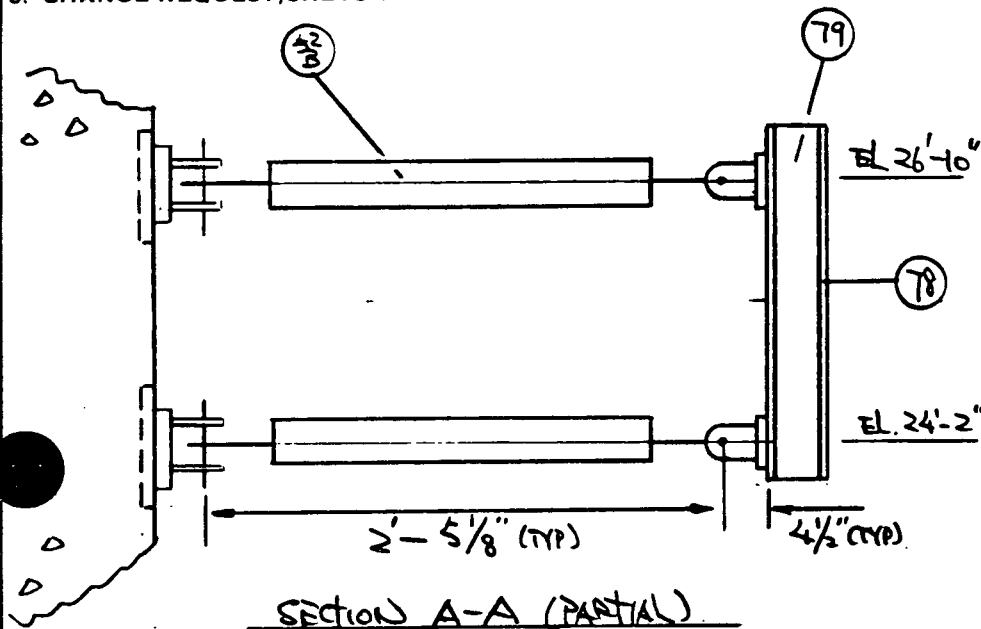
12C. DCN SUB NO. 04
DATE APR 8 1980
12E. SCN NO.

A(QC) ORBR JOB NO. 10079 (I.C.) 206-2
REF. DWG. OR SPEC. SHEET NO. REV. 1 5. TITLE PIPE SUPPORT ASSEMBLY
S2-RC-016-H-009

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: CHANGE BILL OF MAT'L

8. CHANGE REQUEST/SKETCH



PL 5218

BILL OF MAT'L (BY FIELD)

1. CHANGE ITEM 52A TO 52B (2 REQD)
USE S3-S1-059-H-005 +
S3-S1-062-H-005.
35-6" SHOCK SUPPRESSOR 306
C.S = 2.13" H.8 = 3.85"

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPF W.S. 3-21-80
INSTR _____
NUC _____
QA W.S. 3-24-80

9. Hui Chi Shing
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
Hui Chi Shing
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS P.E. R.L. Rogers/164 DATE 3-21-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. Sleep DATE 3-24-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B.L. Hansen DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

APR 7 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4867
DATE 3-25-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

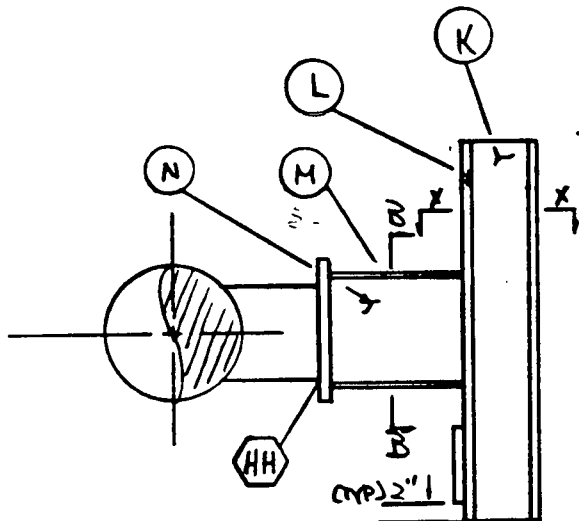
12C. DCN SUB NO. 05
12D. DATE APR 15 1980
12E. SCN NO.

A(QCI)
DBBB JOB NO. 10079
REF. DWG. OR SPEC. SHEET NO. 206-2 REV. 1 TITLE PIPE SUPPORT ASSEMBLY

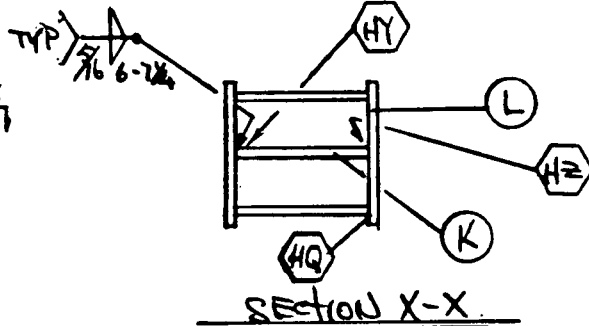
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION: NAT'L NOT IN STOCK.

8. CHANGE REQUEST/SKETCH

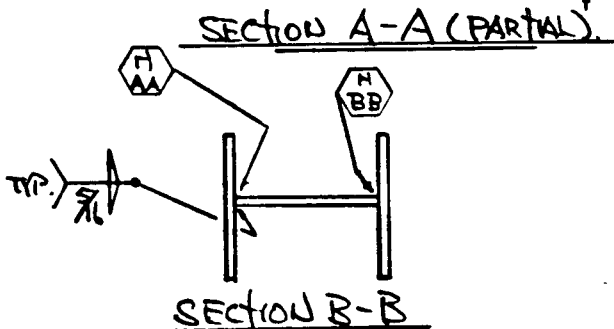


PL 5277



BILL OF MAT'L (BY FIELD)

1. DELETE ITEM 78, 80.
- * 2. ADD ITEM L TR 1/2" X 8 1/2" X 3'-8 3/4" L.G. (2 REQ'D)
- * 3. ADD ITEM K. TR 1/2" X 7 1/8" X 3'-8 3/4" L.G. (1 REQ'D)
- * 4. ADD ITEM M. TR 1/2" X 8 1/8" X 0'-5 3/4" L.G. (2 REQ'D)
- * 5. ADD ITEM N. TR 1/2" X 7 1/8" X 0'-5 3/4" L.G. (1 REQ'D)



NOTE: REVERSE WELD IDENTIFYS HF. HF. NF MAT'L.

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE
CIVIL _____	PIPE <u>RF</u> 4-1-80
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QAE <u>RF</u> 4-1-80

11. APPROVAL OF FLD DISPOSITION
PREPARED BY <u>Chi Shih</u>
PROJECT FIELD ENGINEER
DATE <u>4-1-80</u>

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. P.L. Rogers/RH DATE 3-31-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): RF DATE 4-1-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE RF DATE 4-1-80

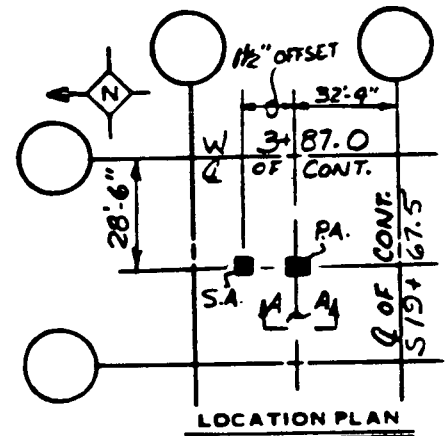
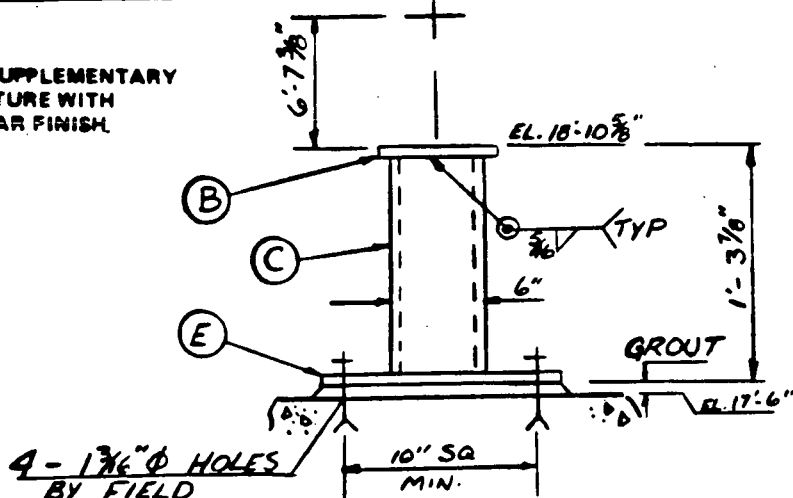
16. ADDITIONAL DISTRIBUTION _____

X

SUS-2888

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	1	-	8" ϕ SCH. 160	S.S. DUMMY STUB	*		AMETEK
31A	1	-	1/4 x 12 x 1'-0"	C.S. PL	X		FIELD
32A	1	307	35-6" STROKE	MECH. SHOCK SUPPRESSOR	X		FROM U-3 TAG
				NUCLEAR CLASS 1, CS = 3.00", HS = 3.00"			SS-SI-044-H-003
				W = 1'-5 3/8", w/ADD. REAR BRACKET			
				LOAD = 35,738 lbs.			
B	1	-	PL 1 x 5 x 0'-7"			X	FIELD
C	1	-	TS 6 x 4 x 3/8 x 1'-4"			X	"
E	1	-	PL 1/2 x 20 x 1'-8"			X	"
	4	-	US-B-HC-LCSF-175			X	"
(FROM SURPLUS S2-RC-016-H-004)							
*INTEGRAL ATTACH. USE ASME SUBSECT. NB MAT'L.							

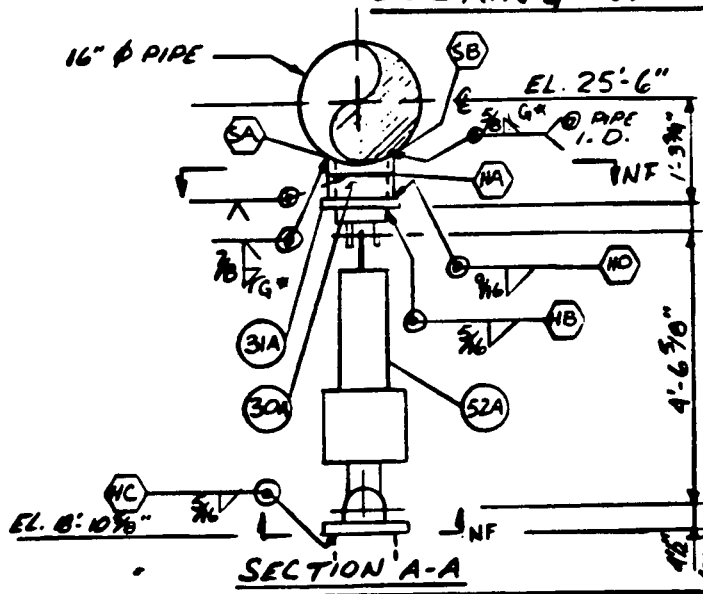
COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH



LOCATION PLAN

(I.C.) AREA NO. 2C06-2

LOOKING WEST



*GRIND ONLY IF NECESSARY TO GUARANTEE CONCAVITY

PMC-FEO		TYPE 6	
PROJ CL	PIPE A(QCI)	MAX. TEMP	
QUAL CL	STEEL II	650°F	
DESIGN		X	Y
	M +		
	(FT-LBS)		
P +		35,738	-
(LBS)		35,738	-

PROB. NO. 52 PT. NO. 69
 SPOOL NO. 2-RC-016-3
 ISO. 1201-016-1
 REF. DWGS. PIPE 40400
 STEEL 23168

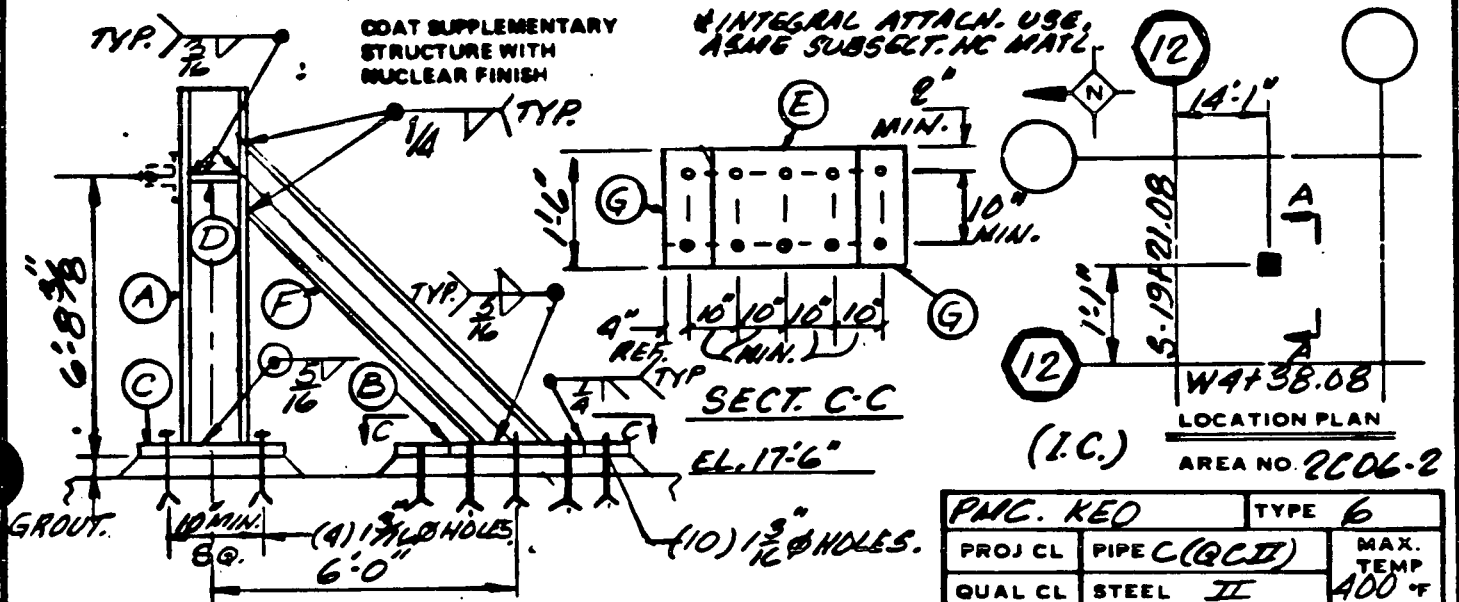
TAG NO. S2-RC-016-H-010

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
	2 INCORP DCN OLDR S-44370 REDRAWN	2-21-80	B	VG	U		

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO.	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY				
10079			LOS ANGELES, CALIF.				

SUS-2BBA

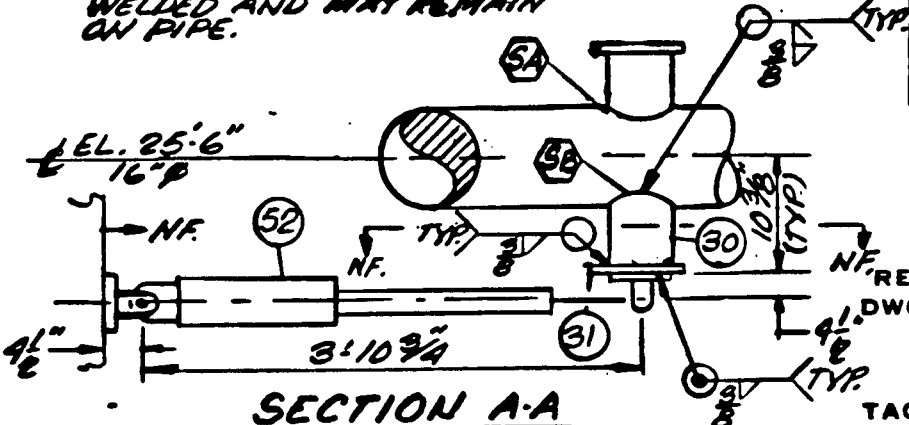
ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	2	—	10"Ø SCH. 40S DUMMY PIPE		✗		BY KELLOGG.
31	2	—	12"X12"X1/2" C.S. PLATE.		✗		" "
52	1	307	35-6 MECH. SHOCK SUPPRESSOR W/OPTION I. C.S.=3.789", H.S.=2.219" W.=8 3/4" LOAD: 10,945		✗		BY GRINNELL.
A	1	—	W10X49		✗		5023-206-18
E	1	—	R. 1 1/4" X 2 1/2" X 1/2"		✗		BY FIELD
F	1	—	W10X49		✗		"
D	2	—	3/8" STIFF. R.		✗		5023-206-18
G	2	—	R. 1 1/4" X 1 1/2" X 1/2"		✗		BY FIELD
	1A	—	US-B-HC-LCSF-175		✗		"
C	1	—	R. 1 1/4" X 1 1/2" X 1/2"		✗		SPEC 5023-206-18



LOOKING SOUTH

NOTE: UPPER DUMMY STUB SHD WELDED AND MAY REMAIN ON PIPE.

P.M.C. REQ		TYPE 6		
PROJ CL	PIPE C (Q.C.I)	STEEL II		MAX. TEMP
		X	Y	Z
		—	—	—
DESIGN	(FT-LBS)	—	—	—
	(LBS)	0	0	75037
		0	0	75037



SECTION A-A

PROB. NO. 52 FT. NO. 109
 SPOOL NO. 2-RC-017-H-028
 ISO 1201-016-1
 PIPE 40400
 STEEL
 TAG NO. 52-RC-017-H-030

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	O.A.E.
2	INC. DCN 1,2, FCR 22146, 4422 REDRAWN	2-26-80	And	KS	KG	RR	—

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO. FILE	SAN ONOFRE NUCLEAR GENERATING STATION PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

MAR 26 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4774
DATE 3/14/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 03
DATE MAR 31 1980
12E. SCN NO.

C(QCII) JOB NO. 10079 (I.C.) 2C06-2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
52-RC-017-H-030 2 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Weld symbols incorrect

8. CHANGE REQUEST/SKETCH

Delete weld Identifier SA & SB

PL # 5163

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPF H.P.S. 3-14-80
INSTR _____
NUC _____
QA [Signature] 3-17-80

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE 3-15-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers DATE 3-14-80
REMARKS: CONVERT TO DCN

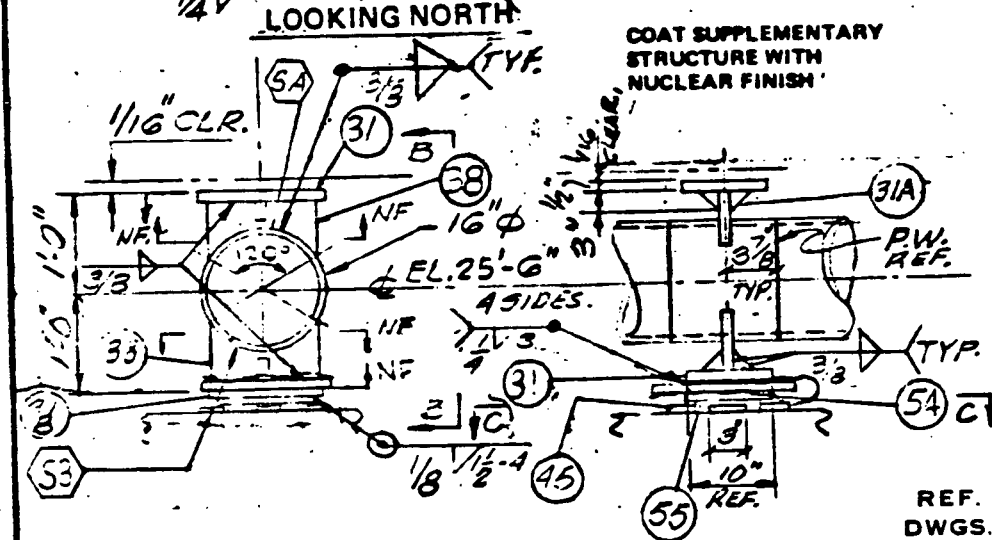
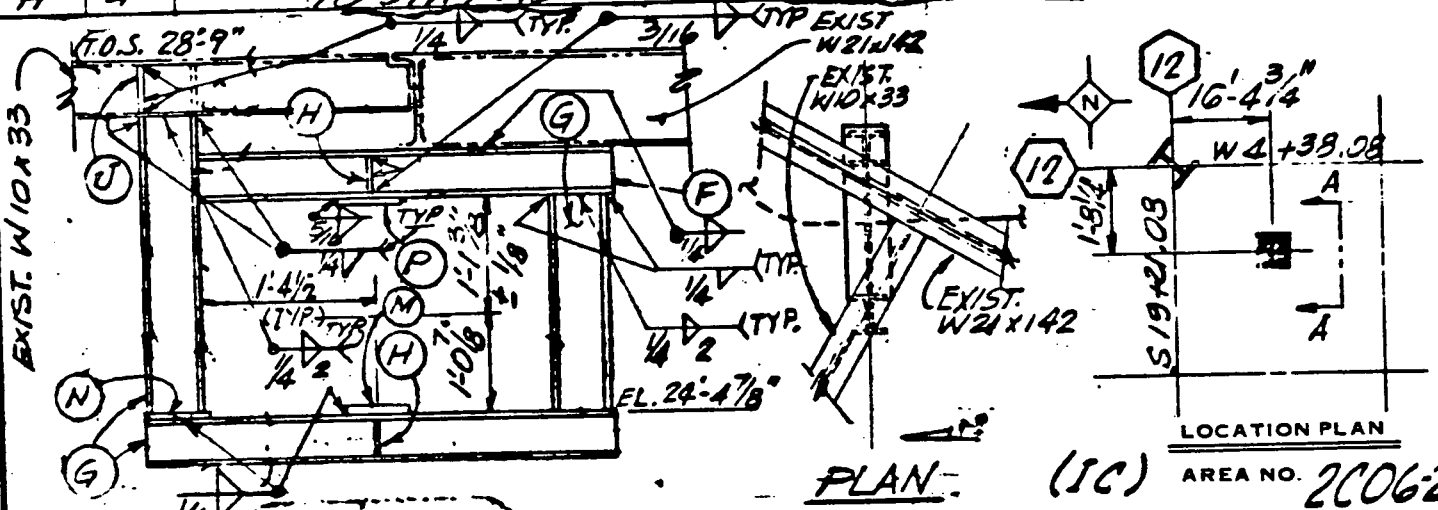
13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-18-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-28-80

16. ADDITIONAL DISTRIBUTION _____

S.U.S. 2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
39	2	-	14" x 4" HIGH x 2 1/4" S.S. PL (SHIP LOOSE)	*			BY KELLOGG
31	2	-	16" x 10" x 1/2" C.S. PL	X			BY KELLOGG
31A	4	-	3" x 3" x 1/2" C.S. PL	X			BY KELLOGG
54	1	-	UPPER SLIDE BEARING PL 10 GA. S.S. 9 1/2" x 9 1/2"				BY FIELD
55	1	-	LOWER SLIDE BEARING PL BRONZITE 1/4" x 9" x 9"				BY FIELD
45	4	-	C.S. BAR 3/16" x 3/16" x 3"				"BY FIELD"
31B	1	-	R. 3/4 x 12 x 1'-0"				
F	1	-	W4 x 13 x 3'-3 1/2"				
G	3	-	W6 x 15.5				
H	4	-	3/8" STIFF. PL.				



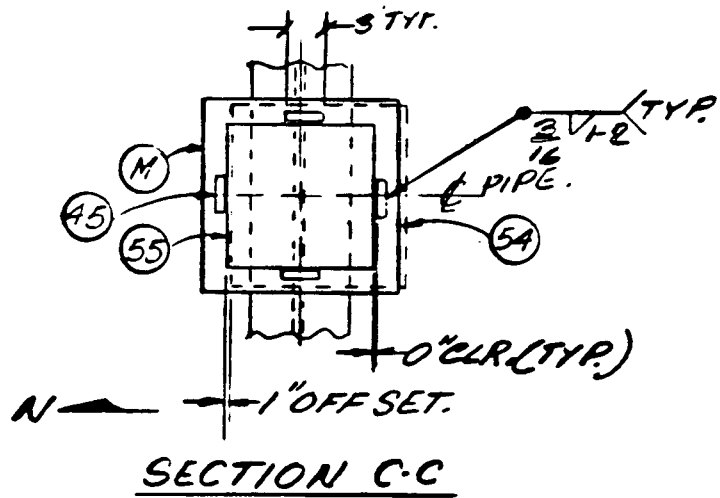
DESIGN CODE: C
 TYPE: 2
 PROJ. CLASS C(QCII)
 MAX. TEMP. 400 °F
 OPER. LOAD (LBS.) —
 DESIGN LOAD (LBS) Y: +4000, -7000
 5 PROB. NO. 52 FT. NO. 111
 SPOOL NO. 2-RC-017-28
 ISO 1201-016-1
 PIPE 40400
 STEEL —
 SHT 1 OF 2
 TAG NO. S2-RC-017-H-031

6 REVISED PER DSN. NO. 1 & 2 & REDRAWN 2-28-53 [Signature] P.A.E.M. KG MB 1201 4 1/2" [Signature]

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	Q. A. E.
BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.		SAN ONOFRE NUCLEAR GENERATING STATION				
		FILE		PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

ITEM NO.	QTY.	SIZE	DESCRIPTION	IF AISC	NOTES
J	2	3/8" STIFF. PL.			BY FIELD.
M	1	R 3/4" x 10" x 0.10"			"
N	1	R 3/4" x 7" x 0.17"			"
P	1	R 7/8" x 10" x 0.10"			"

* FOR INTEGRAL ATTACH. USE ASME SUB SECT. NC MATL.



1201 SHT 2 OF 2
S2-RC-017-H-031 REV 6

BECHTEL POWER CORPORATION DORRIS, CALIFORNIA			LG NO.	BAR 0000-E NUCLEAR GENERATING STATION
			PL	PIPE SUPPORT ASSEMBLY
APP. NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE NTS LOS ANGELES, CALIF.	

FEB 12 1980

SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4637
DATE 2-29-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 03
12D. DATE FEB 24 1980
12E. SCN NO.

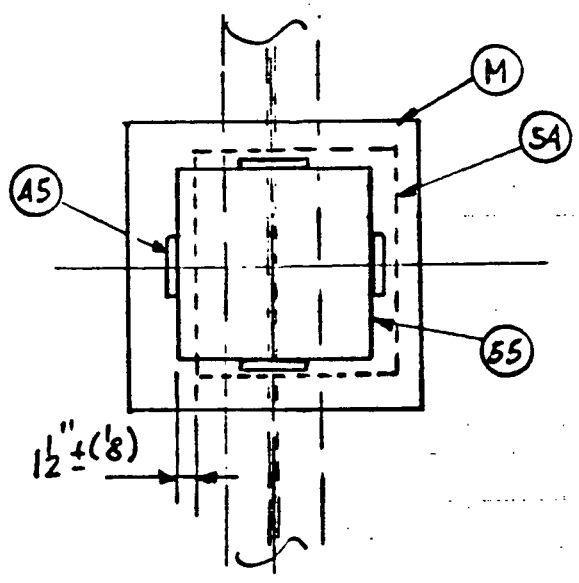
CRCT) JOB NO. 10079 (1.C)
REV. 5 SHEET NO. 206-2

5. TITLE Pipe Support Assembly

6. DESIGN ORIGIN: 1201 ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:
ACTUAL OFF SET DISTANCE LESS THAN AS SHOWN IN
DWG

8. CHANGE REQUEST/SKETCH



PL# 5055

No new material req'd

SECT. C-C (PARTIAL)

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPF NLS 3-1-80
INSTR _____
NUC _____
QAE gws 3-3-80

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FAD DISPOSITION
B. Chuteiman
PROJECT FIELD ENGINEER
DATE FEB 02 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: **CONVERT TO DCN**
P.E. R.L. Vogt/PL DATE 3-1-80

QUALITY ASSURANCE ENGINEER (FIELD): gws DATE 3-3-80

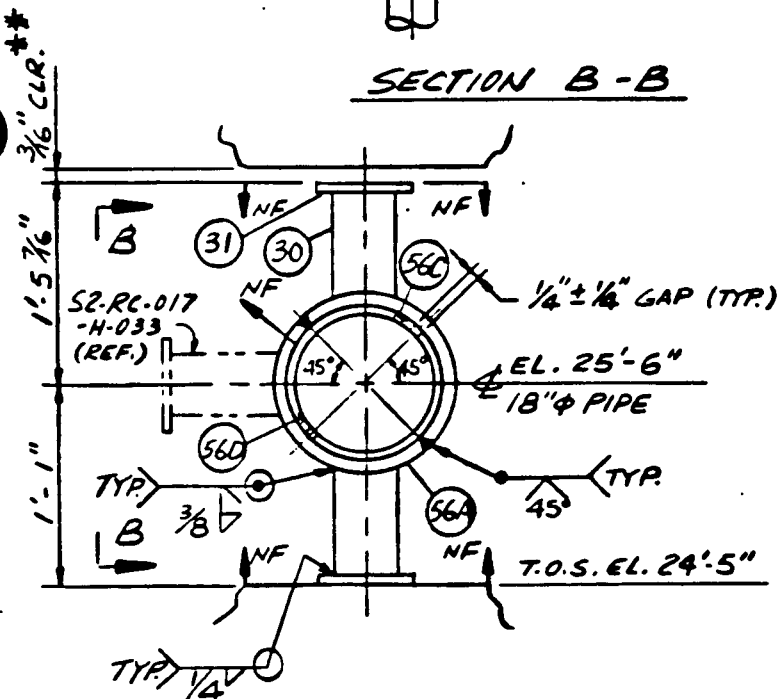
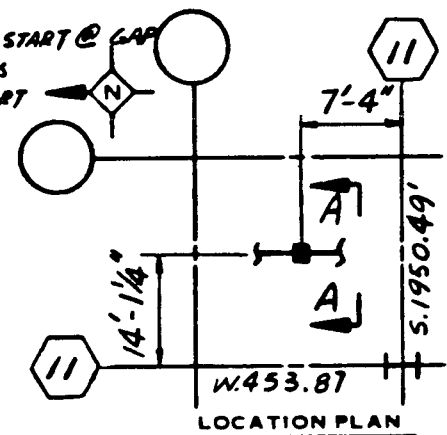
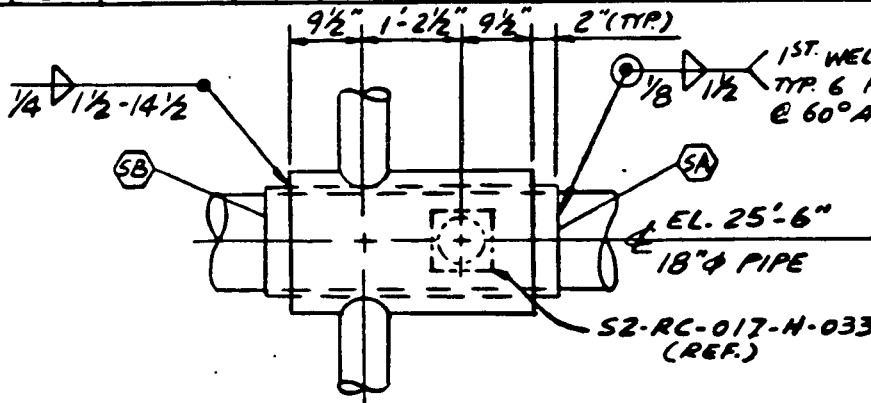
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE gws DATE 3-21-80

16. ADDITIONAL DISTRIBUTION _____

SUS - 2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	2	-	10"φ SCH. 40S DUMMY PIPE S.S.		X		BY KELLOGG
31	2	-	12" x 12" x 1/2" C.S. PLATE		X		" "
56A	2	-	1/4 x 2'-9 1/2" CURVE C.S. PLATE		X		BY AMETEK
56C	1	-	1/8 x 3'-1 1/2" CURVE S.S. PLATE		*		" "
56D	1	-	1/8 x 3'-1 1/2" CURVE S.S. PLATE		*		" "
* INTEGRAL ATTACH. USE ASME SECT. III SUBSECT. "NC" NAT'L.							
A	1	-	W6 x 20		X		
B	1	-	W8 x 35		X		SPEC.
C	2	-	PL 3/8 x 4 x 0'-6"		X		S023-206-18
D	1	-	W6 x 20		X		
E	1	-	PL 3/8 x 4 x 0'-6"		X		
	6	-	1"φ HEX BOLTS		X		



PMC - KEO		TYPE 2		
PROJ CL	PIPE C (QC II)	MAX. TEMP 400°F		
QUAL CL	STEEL II	X	Y	Z
DESIGN	M +	-	-	-
	(FT-LBS)	-	-	-
(LBS)	P +	-	3491	-
	-	-	11237	-

[S] PROB. NO. 52 FT. NO. 114
 SPOOL NO. 2-RC-017-29
 ISO 1201-016-2
 REF. DWGS. PIPE 40400
 STEEL _____
 SHT 1 OF 2

TAG NO. S2-RC-017-H-032

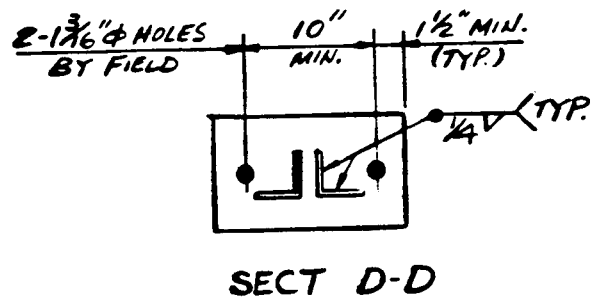
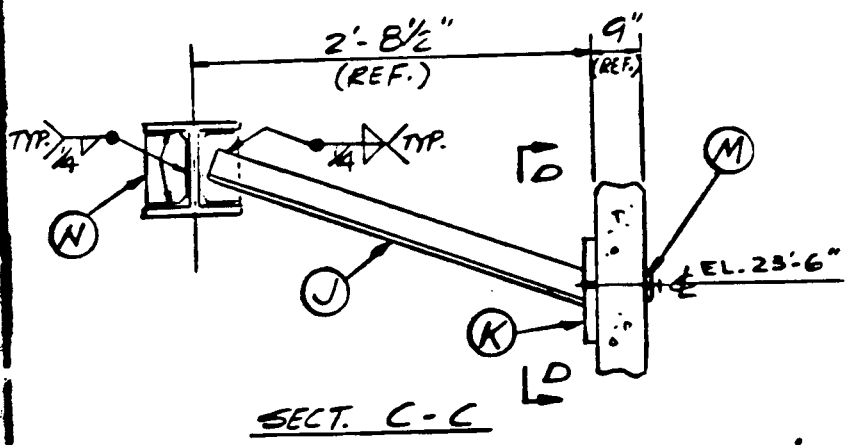
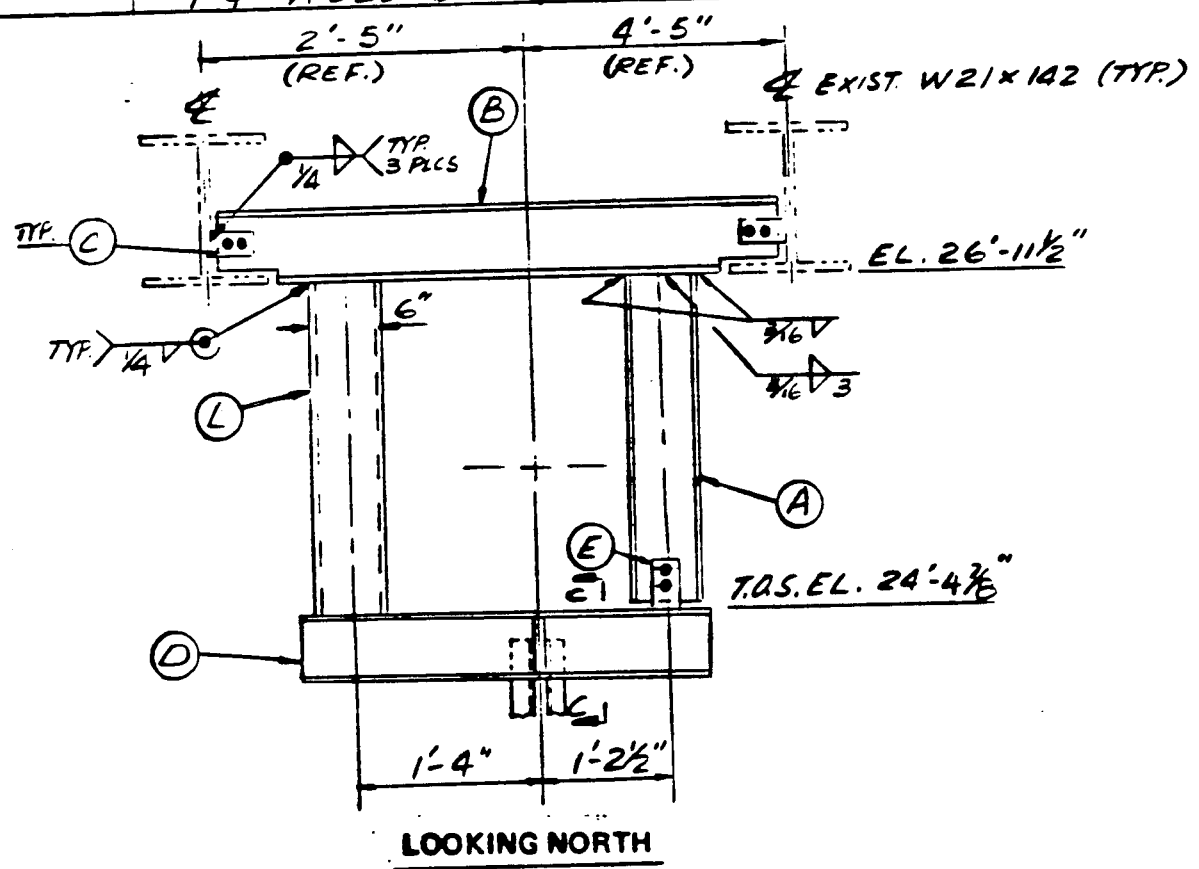
COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

SECTION A - A

						1201			
3	INCORP. DCN 1, 2, 3, 4 & REDRAWN	2-28-80	RT	DAR	KG	MB			R. J. A. J. M. S.
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.				P.E. Q.A.E.

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION					
			FILE	PIPE SUPPORT ASSEMBLY					
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS						LOS ANGELES, CALIF.

REV NO	NO	PART NO	DESCRIPTION	WF BISC	NOTES
		5-7F			
J	2		L 2 1/2 x 2 1/2 x 3/8 x 3'-0" (±)		
K	1		P 1 x 8 x 1'-2"		BY FIELD
L	1		T.S. 6 x 4 x 3/8		
	2		P 3/4 x 4 x 0'-4"		
	2		3/8" STIFF. P		
	2		1" φ A-325 BOLTS/NUTS		



**NOTE: MIN. TOTAL CLRC. REQ'D. IS 1/8"

1201- SHT 2 OF 2
S2-RC-017-H-032 REV 3

BECHTEL POWER CORPORATION DOWNEY, CALIFORNIA			16 NO	SAN ONOFRE NUCLEAR GENERATING STATION	
			PLP	PIPE SUPPORT ASSEMBLY	
APP NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.		

APR 10 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 24900
DATE 3-28-80
2. PAGE 1 OF 1
3. UNIT NO. II

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 05
12D. DATE APR 22 1980
12E. SCN NO.

JOB NO. 10079 (I.C.) 21062

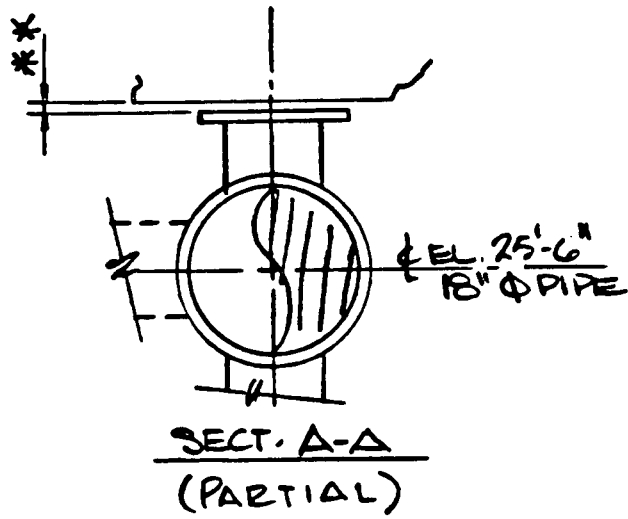
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-017-H-032 3 PIPE SUPT. ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

MIN./MAX. CLEARANCE REQ'D. CHG.

8. CHANGE REQUEST/SKETCH



**** NOTE:**

1. MIN. TOTAL CLR. REQ'D IS $\frac{1}{8}$ "
2. MAX TOTAL CLR IS $\frac{5}{16}$ "

PL# 5310 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE

CIVIL _____	PIPF <u>14.5</u> <u>3-1-80</u>
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QA <u>step</u> <u>4-1-80</u>

11. APPROVAL OF FLD DISPOSITION

PREPARED BY C.W. GREER / S. Tampa

PROJECT FIELD ENGINEER Harris Johnson

DATE APR 01 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogus / R.H. DATE 3-31-80

REMARKS: CONVERT TO DCN

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. Steppard DATE 4-1-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

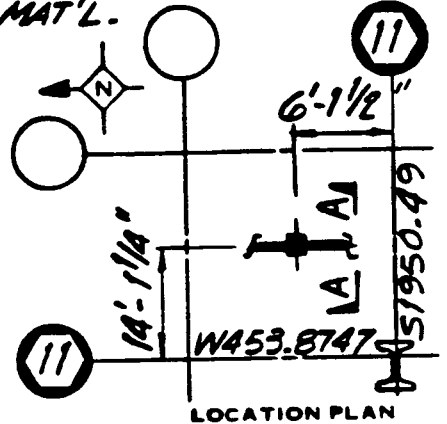
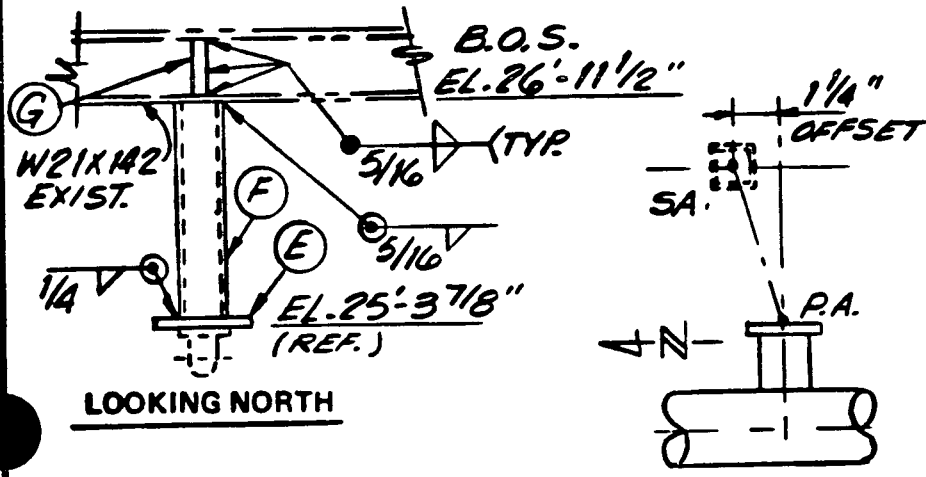
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE J.W. Steppard DATE 4-16-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	—	10" SCH. 40S DUMMY PIPE S.S.		X		BY KELLOGG
31	1	—	R 1/2 X 12 X 1'-0" CARBON STEEL		X		"
52A	1	307	#3-5" STROKE MECH. SHOCK SUPPRESSOR W/ADDITIONAL REAR BRACKET, CS = 1 1/2", HS = 3 3/8", W = 8 3/8", LOAD = 944#				SURPLUS FROM 52-51-003-H-015
E	1		R 1/2 X 6 X 0'-6"		X		BY FIELD
F	1		TS 4 X 4 X 1/2		X		
G	2		1/2" STIFF R		X		

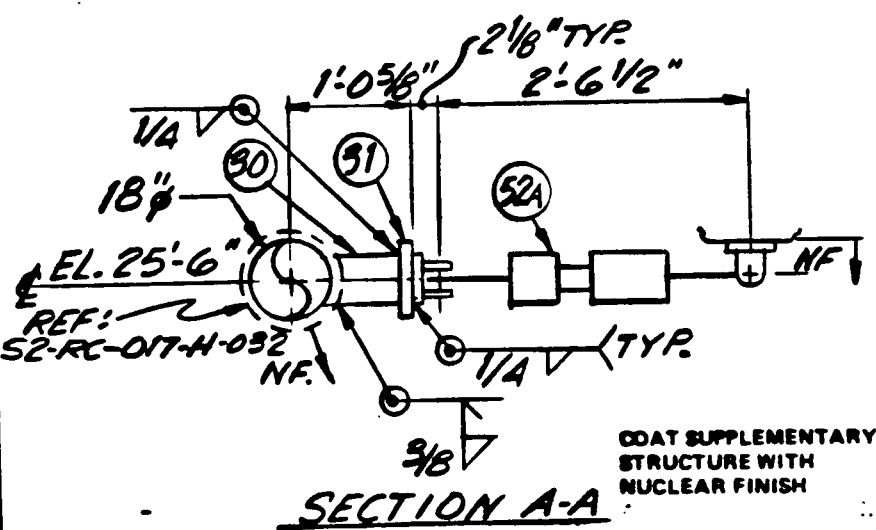
2BHA

* INTEGRAL ATTACH. USE ASME SECT III SUBSECT. 'NC' MAT'L.



(I.C.) AREA NO. 2C06-2

PMC: KEO		TYPE 6	
PROJ CL	PIPE C (QC II)	MAX. TEMP	
QUAL CL	STEEL II	400 °F	
DESIGN		X	Y
	M +	—	—
	(FT-LBS)	—	—
	P +	⊖	944
	(LBS)	⊖	944



PROB. NO. 52 FT. NO. 114
 SPOOL NO. 2RC-017-29
 ISO. 1201-016-2
 REF. DWGS. PIPE 40400
 STEEL 23211

TAG NO. 52-RC-017-H-033

NO. 4	INC. FCR 22174, 19201, DCN 142 REDRAWN	DATE 2-26-80	DR. P. J. H.	CHK. K. G. U. H. B.	E.G.S.	P.E. R. L. K. A. S.	Q.A.E.
-------	--	--------------	--------------	---------------------	--------	---------------------	--------

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

MAR 26 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4770
DATE 3/14/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 05
MAR 31 1980
12E. SCN NO.

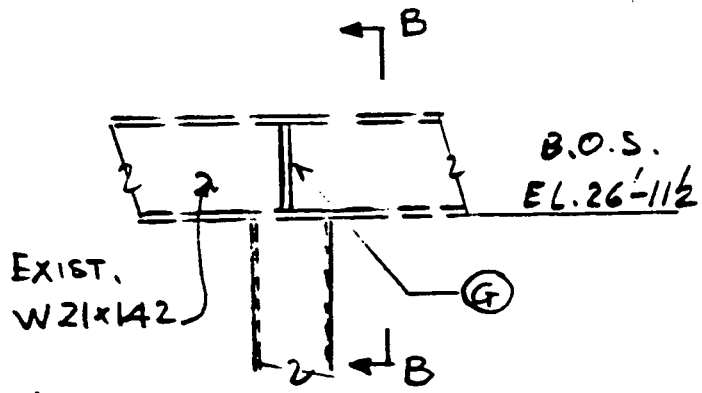
REF. DWG. OR SPEC. S2-RC-017-H-033 SHEET NO. 4 REV. 4 5. TITLE Pipe Support Assembly
JOB NO. 10079 (I.C.) 2C06-2

NAME

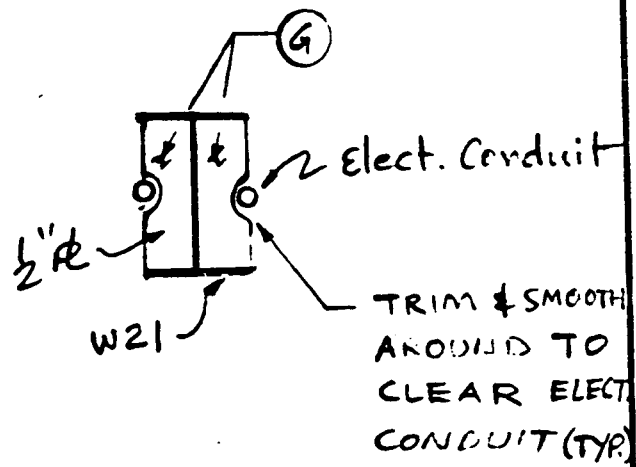
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION:
1/2" stiffener & interfere with Elect. Conduit

8. CHANGE REQUEST/SKETCH



LOOKING NORTH
(PARTIAL)



SECT. B-B

P# 5159

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPF Y.J.S. 3-14-80
INSTR _____
NUC _____
QA g.w. Slapnick 3-17-80

9. P. Tanniyat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
A. Christman
PROJECT FIELD ENGINEER
DATE 3-15-80

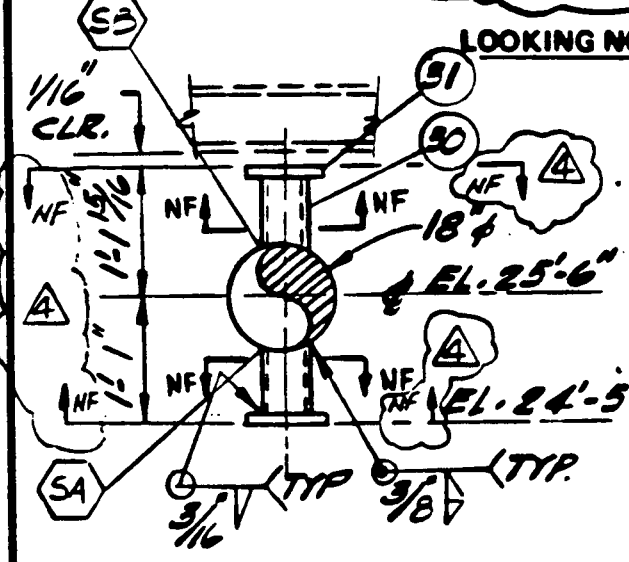
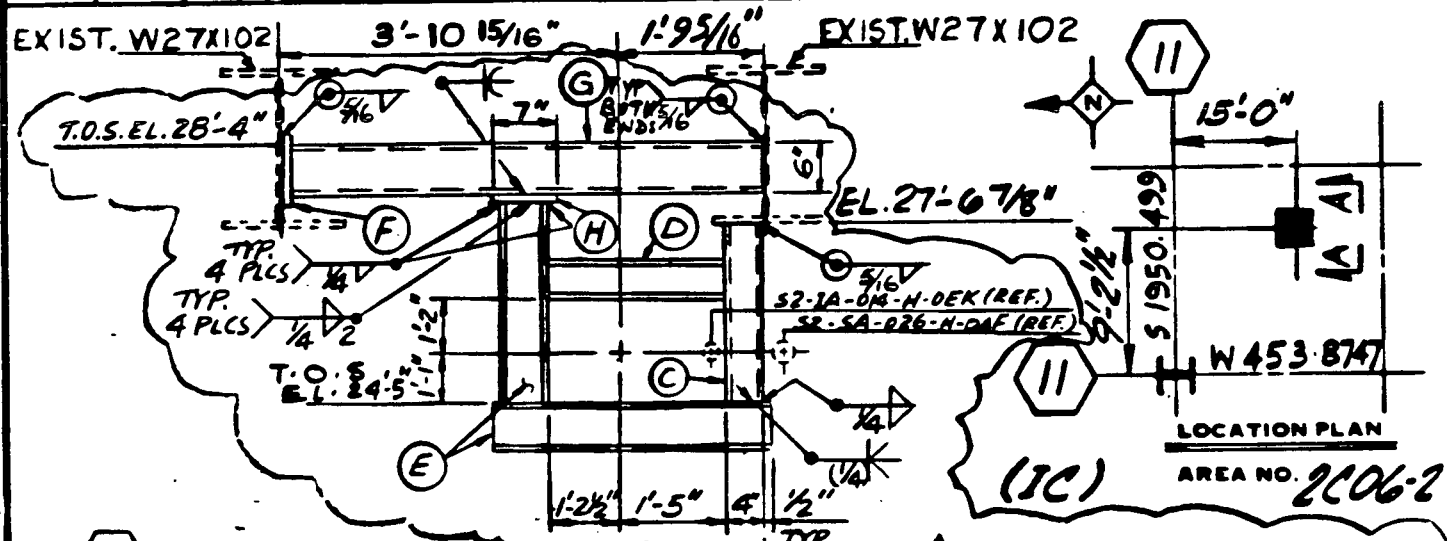
12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogerson DATE 3-14-80
REMARKS: CONVERT TO PLN

13. QUALITY ASSURANCE ENGINEER (FIELD): g.w. Slapnick DATE 3-18-80
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE g.w. Slapnick DATE 3-26-80
16. ADDITIONAL DISTRIBUTION _____

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF AISC	NOTES
30	2	-	10" SCH. 40 DUMMY PIPE S.S.	#		BY KELLOGG
31	2	-	R 1/2 x 11 1/4 x 0'-11 1/4" C.S.	X		"
C	1		T.S. 6 x 4 x 1/2 x 3'-1 7/8"			BY FIELD
D	1		W4 x 13 x 2'-7 1/2"			
E	2		W6 x 20			
F	1		R 3/4 x 5 x 0'-7" A			
G	1		T.S. 6 x 4 x 1/2 x 5'-7"			
H	1		R 3/4 x 6 1/2 x 0'-7"			

INTEGRAL ATTACHMENT USE AS ME SUBSECTION 'NC' MAT'L

SUS-2BHA



COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

PM-C-KED STEEL II TYPE: 2

PROJ. CLASS. C(OC II)
 MAX. TEMP. 400 F
 OPER. LOAD (LBS.)
 DESIGN LOAD (LBS) 13283
 5 PROB. NO. 52 FT. NO. 120
 SPOOL NO. 2-RC-017-38
 ISO 1201-016-2
 REF. DWGS. PIPE 40400 & (40386)
 STEEL

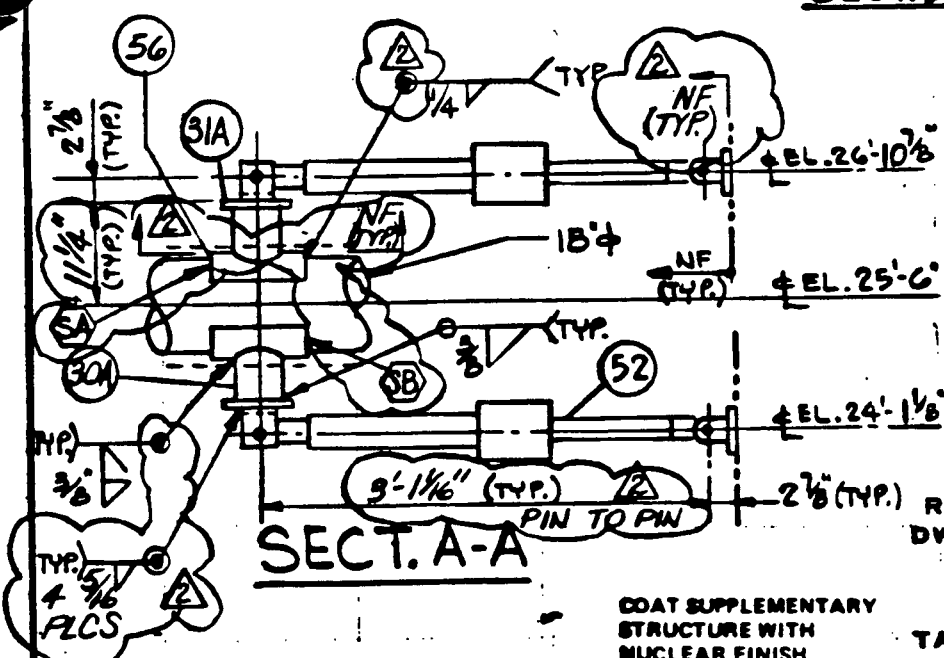
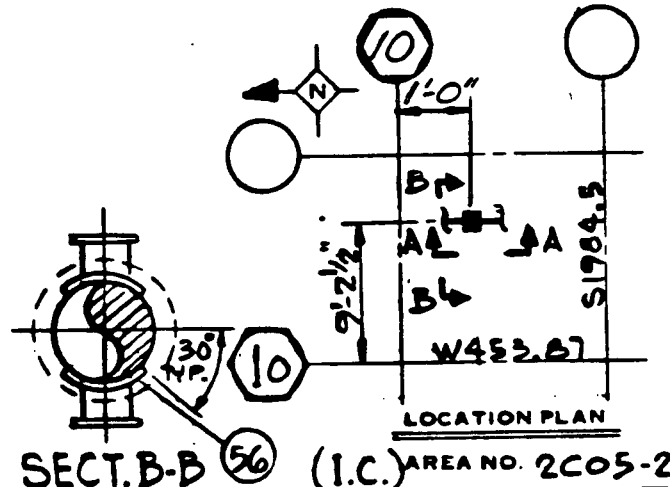
TAG NO. S2-RC-017-H-035

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHK. E.	P. E.	Q. A. E.
4	INCORP. DCN 3	2-26-80	QT	KG	RE HB 1201			
3	INCORP. DCN # 122	6-29-79	NS					
0	ISSUED FOR CONSTRUCTION	2-8-77	MR	DAI	LA MDC			

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					

SUS:2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	2	-	10" ϕ SCH. 40S	DUMMY PIPE	X		BY FIELD
31A	2	-	3/4 x 12 3/4 x 1-0 3/4"	S.S. PLATE	X		" "
52	2	307	NO 10, 6" STROKE	MECH. SHOCK SUPPRESSOR NUCLEAR CLASS 2, W=10", CS=2 1/16", HS=3 3/16" W/ADDITIONAL REAR BRACKET, LOAD=12124"	X		BY GRINNELL
56	2	-	1/4" x 120" x 14 1/4"	S.S. CURVED PLATE	*		BY KELLOGG
							* INTEGRAL ATTACHMENT - USE CODE SUB-SEC. NC MATERIAL.



DESIGN CODE	C	TYPE	6
PROJ CL	PIPE C (QC II)	MAX. TEMP 400°F	
QUAL CL	STEEL		
DESIGN (FT-LBS)		X	Y
	M	-	-
	P	24248	-
(LBS)		24248	-

PROB. NO. 22 FT. NO. 125
 SPOOL NO. 2-RC-017-16
 ISO 1201-016-1
 PIPE 40386
 STEEL 20075

TAG NO. S2-RC-017-H-036

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	Q. A. E.
2	INCORPORATED DCNS 1,2,3	2-26-80	TM	KG	LR MB	1201	-	RL/SW/CS
1	CHANGED DIM. OF ITEM 56	7-11-79	RK	A2	Amal		-	JDH/AM/KM
0	ISSUED FOR CONSTRUCTION	5-18-79	HW	W/AC	ENK/RT	Am	-	JDH/AM/JRM

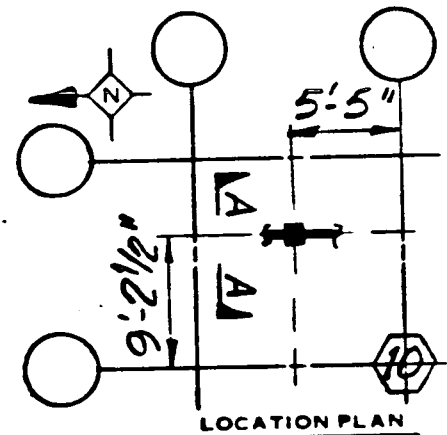
BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					

CALC. C-270-3.0

SUS 2BHA

ITEM NO.	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	1		10" SCH 40S DUMMY STUB		X		BY FIELD
31A	1		PL 3/4 X 12 X 1'-0" CARBON STEEL		X		
36	1		1/4 X 120 X 14 3/4" S.S. CURVED PLATE		X		BY KELLOSS
D	1		W6 X 15.5 X 5'-6 3/4" LG		X	X	
E	2		L3 X 3 X 1/4 X 0'-4" LG		X	X	
F	1		W6 X 15.5 X 1'-10 7/16 LG		X	X	
G	1		1/2 X 9 X 0'-9" C.S. PLATE		X	X	BY FIELD.
H	1		PL 1/2 X 12 X 1'-0"		X	X	
J	1		W6 X 15.5		X	X	
K	1		PL 3/4 X 14 X 2'-0" LG		X	X	
	4		US-8-HC-LCSF-175				

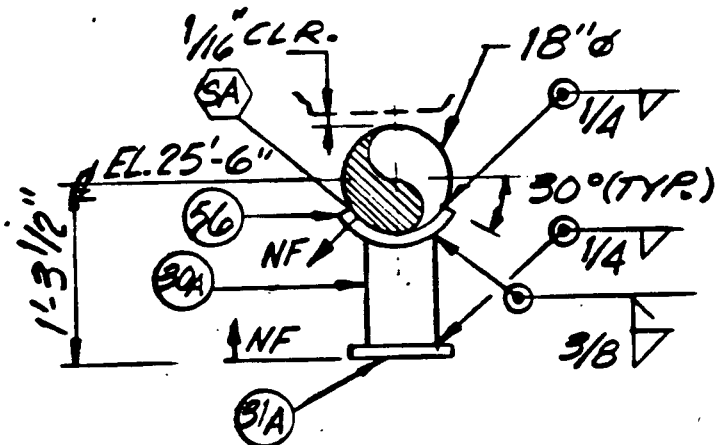
* INTEGRAL ATTACHMENT-USE ASME SECT III SUBSECT NC' MAT'L.



LOCATION PLAN

(I.C.) AREA NO. 2C05-2

PMC: KEO		TYPE 2	
PROJ CL	PIPEC (QCII)	MAX. TEMP	
QUAL CL	STEEL II	400°F	
DESIGN		X	Y
	M +	—	—
	(FT-LBS)	—	—
	P +	Ø	1384
	(LBS)	Ø	1384



SECTION A-A

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

PROB. NO. 52 PT. NO. 125
 SPOOL NO. 2RC-017-16
 ISO 1201-016-1
 PIPE 40386
 STEEL 12c1
 SHT 1 OF 2

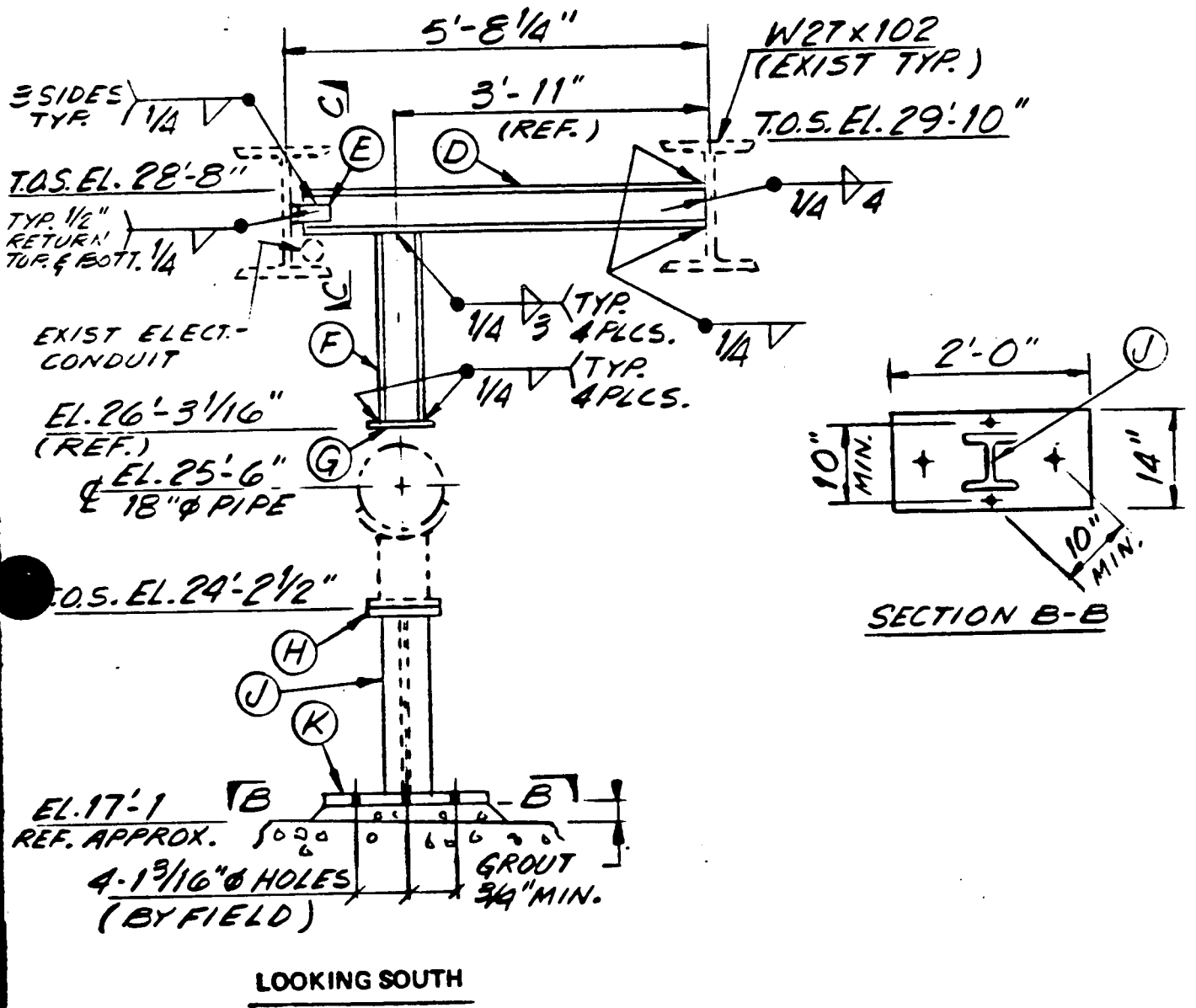
REF. DWGS.

TAG NO. S2-RC-017-H-037

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	O.A.E.
3	INCORP. DCN 1, 2, 3 & 4 REDRAWN	2-28-80	LD	ST	KG MB		RIF/MS/S

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
JOB NO. 10079		FILE	PIPE SUPPORT ASSEMBLY	
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.		
		SCALE: NTS		

ITEM NO.	NO. REQ.	PART NO.	SIZE	DESCRIPTION	NF AISC	NOTES

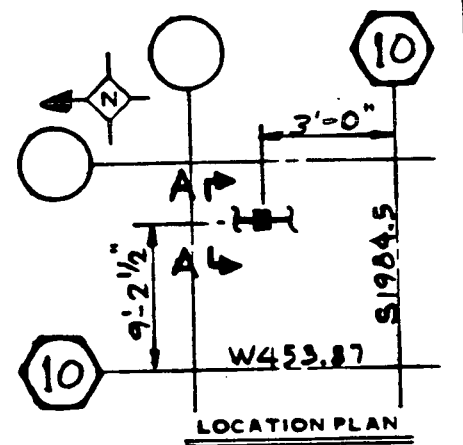
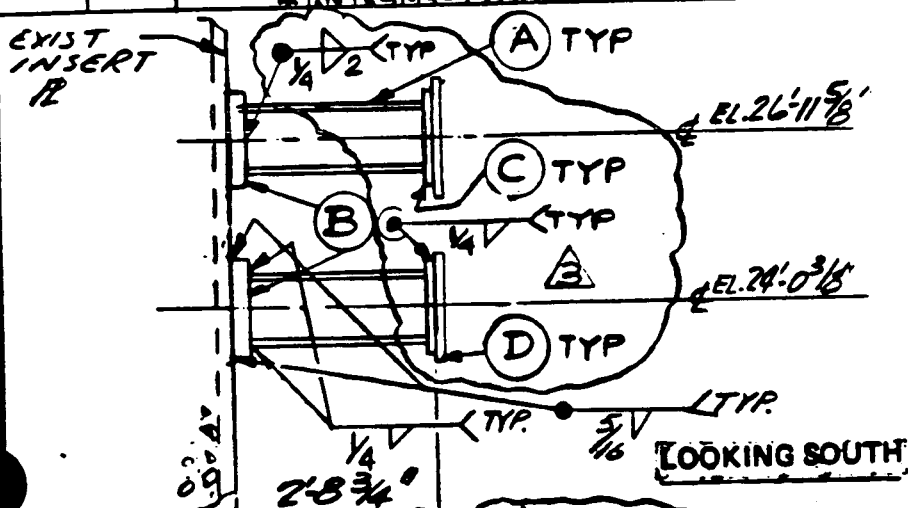


1201 SHT 2 OF 2
S2-RC-017-H-037 REV 3

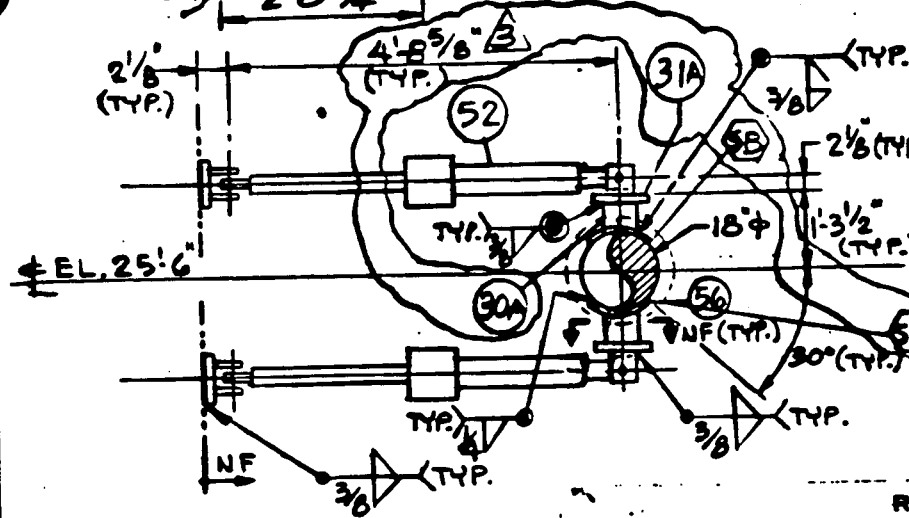
BECHTEL POWER CORPORATION DORNALE, CALIFORNIA			1 & 2	SAN ONOFRE NUCLEAR GENERATING STATION	
10079			FILE	PP. SUPPORT ASSEMBLY	
DATE	APPROVED		SOUTHERN CALIFORNIA Edison COMPANY SCALE NTS LOS ANGELES, CALIF.		

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	2	-	10" ϕ SCH. 40 S-55 DUMMY PIPE		X		BY FIELD
31A	2	-	1/2" x 12" x 1'-0" C.S. PLATE		X		" "
52	2	307	NO. 3, 5" STROKE, MECH. SHOCK SUPPRESSOR, W=34 1/8", CS=1 1/8", HS=3 1/8"				
			W/ADDITIONAL REAR BRACKET, LOAD = 220 LB*				BY GRINNELL
56	2	-	1/4" x 120" x 14 3/4" S.S. CURVED PLATE (SHTP 10050)*				BY KELLOGG
A	2	-	W 4 x 13				SPEC.
B	2	-	R 3/4 x 6 x 0'-6"				5023-206-15
C	2	-	R 1/2 x 5 x 0'-5"				
D	2	-	R 1/2 x 6 x 0'-6"				X BY FIELD

* INTEGRAL ATTACHMENT - USE CODE SUB. SEC. NC MATERIAL



LOCATION PLAN (I.C.) AREA NO. 2C05-2



SECT. A-A

DESIGN CODE	C	TYPE	G
PROJ CL	PIPE C (QC II)	MAX. TEMP	400°F
QUAL CL	STEEL		
DESIGN	M +	-	-
	(FT-LBS)	-	-
	P +	-	4416
	(LBS)	-	4416

PROB. NO. 52 PT. NO. 125
 SPOOL NO. 2-RC-017-16
 ISO 1201-016-1
 PIPE 40386
 STEEL 1201

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH PER APPENDIX 4-C OF SPEC.

TAG NO. 52-RC-017-H-038

658

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	Q. A. E.
2	REVISED AS SHOWN	4-18-76	RJS	RT	RT, HSN	RJR	-	RR/SJS
3	INCORPORATED DCNS 1, 2 & 3	2-26-80	KG	LL	MB		-	RLP/SAM
0	ISSUED FOR CONSTRUCTION	5-12-77	WJ	WJ	HSN	RT, HSN	-	JDA/ADJ/SJM

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO.	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS					
10079			LOS ANGELES, CALIF.					

CA/C-C-270-3.0

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-478B
DATE 3/15/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 04
12D. DATE APR 8 1980
12E. SCN NO.

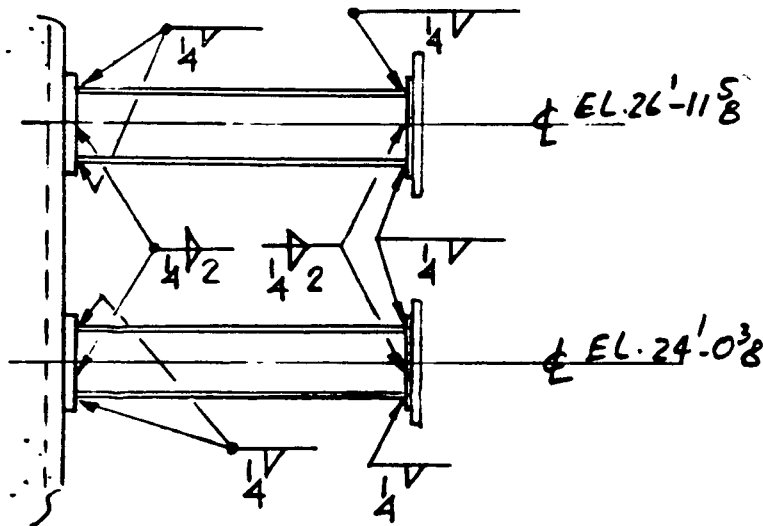
C(OCT II)
R3HA JOB NO. 10079 (1-C)
2C05-2
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-017-H-03B 3 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Incorrect weld symbols.

8. CHANGE REQUEST/SKETCH



PL # 5178

No new material req'd

LOOKING SOUTH
(PARTIAL)

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE NT-5 2-18-80
INSTR _____
NUC _____
QAE [Signature] 3-19-80

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE 3-19-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. P.L. Rogers/NT DATE 3-18-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-19-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

APR 7 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5.4844
DATE 4.2.80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS
II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 05
12D. DATE APR 15 1980
12E. SCN NO.

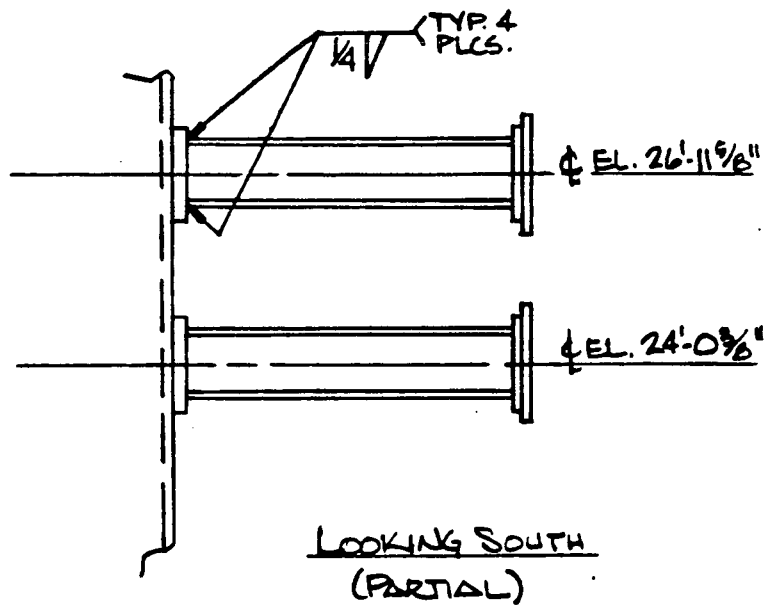
JOB NO. 10079 (I.L.)
2005.2

REF. DWG. OR SPEC. S2.R.017.H.038 SHEET NO. 3 REV. 3 5. TITLE PIPE SUPT. ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:
EXISTG SHOP WELDS SHOWN AS FIELD WELDS
WORK WITH FCR# 5.4788

8. CHANGE REQUEST/SKETCH TO:



PL# 5344 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPF R.L.S. 4-3-80
INSTR _____
NUC _____
QA approved 4-4-80

9. C.W. GREER
PREPARED BY
11. APPROVAL OF FLD. DISPOSITION
Louis Johnson
PROJECT FIELD ENGINEER
DATE APR 04 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers DATE 4-3-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): C.W. Greer DATE 4-4-80

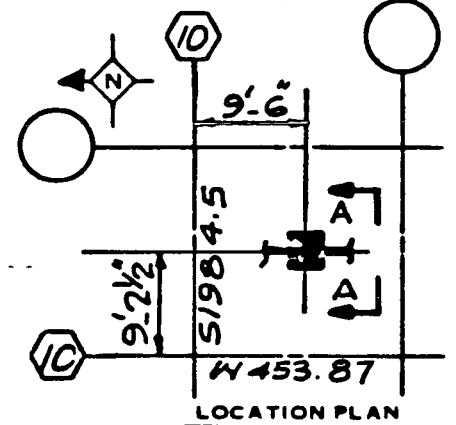
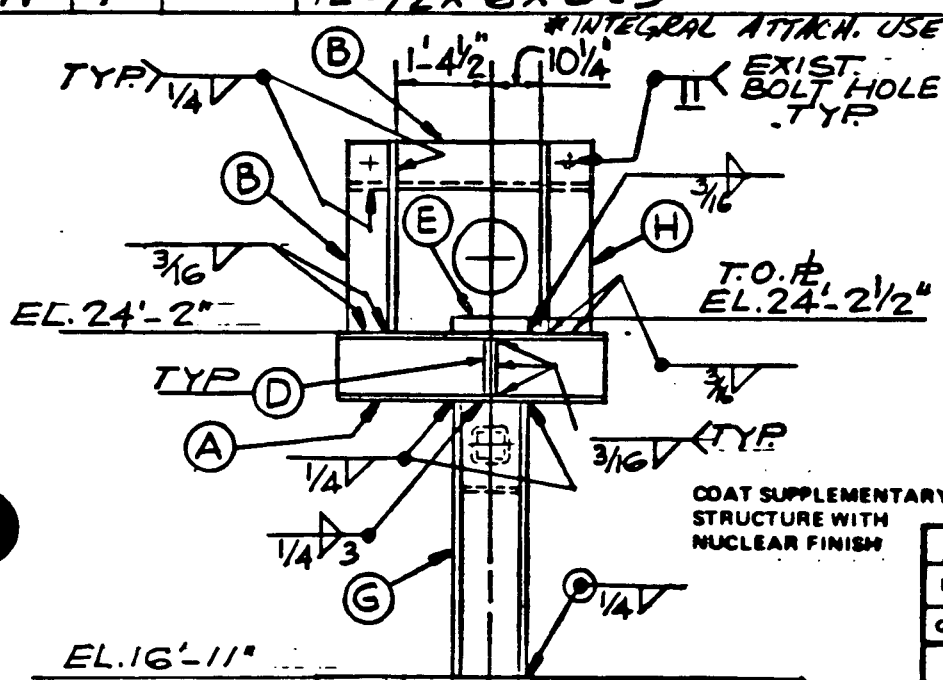
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B. Halman DATE 4-1-80

16. ADDITIONAL DISTRIBUTION _____

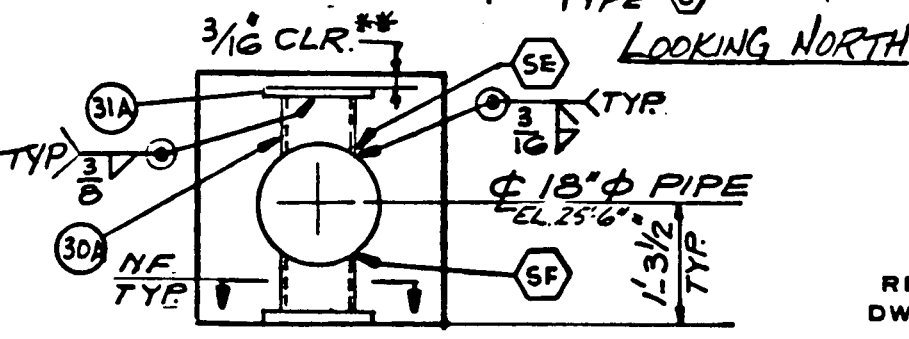
SUS-2BHC

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	2		10" ϕ SCH. 40 S DUMMY STUB		*		FIELD
31A	2		3/4" X 12" X 1'-0" CS PLATE		X		"
A	1		WG X 15.5			X	S023-206-18
B	2		Ls 3 X 3 X 3/8			X	"
D	2		3/8" STIFF. PL			X	"
E	1		PL-1/2 X 11 X 0'-11"			X	"
G	1		WG X 15.5 X 6'-9"			X	FIELD
H	1		L 3 X 3 X 3/8 X 2'-10 5/16"			X	"
U	1		TS 3 X 3 X .250			X	"
L	1		PL-3/8" STIFF. PL			X	"
M	1		PL-1/2 X 5 1/2 X 0'-9"			X	"
N	1		PL-1/2 X 6 X 0'-9"			X	"



(IC) AREA NO. 2C05-2

PMC = KEO		TYPE 2	
PROJ CL	PIPE C (QC II)	MAX. TEMP	
QUAL CL	STEEL II	400 °F	
DESIGN		X	Y
	M +	—	—
	(PT-LBS)	—	—
	P +	111	—
	(LBS)	—	5443

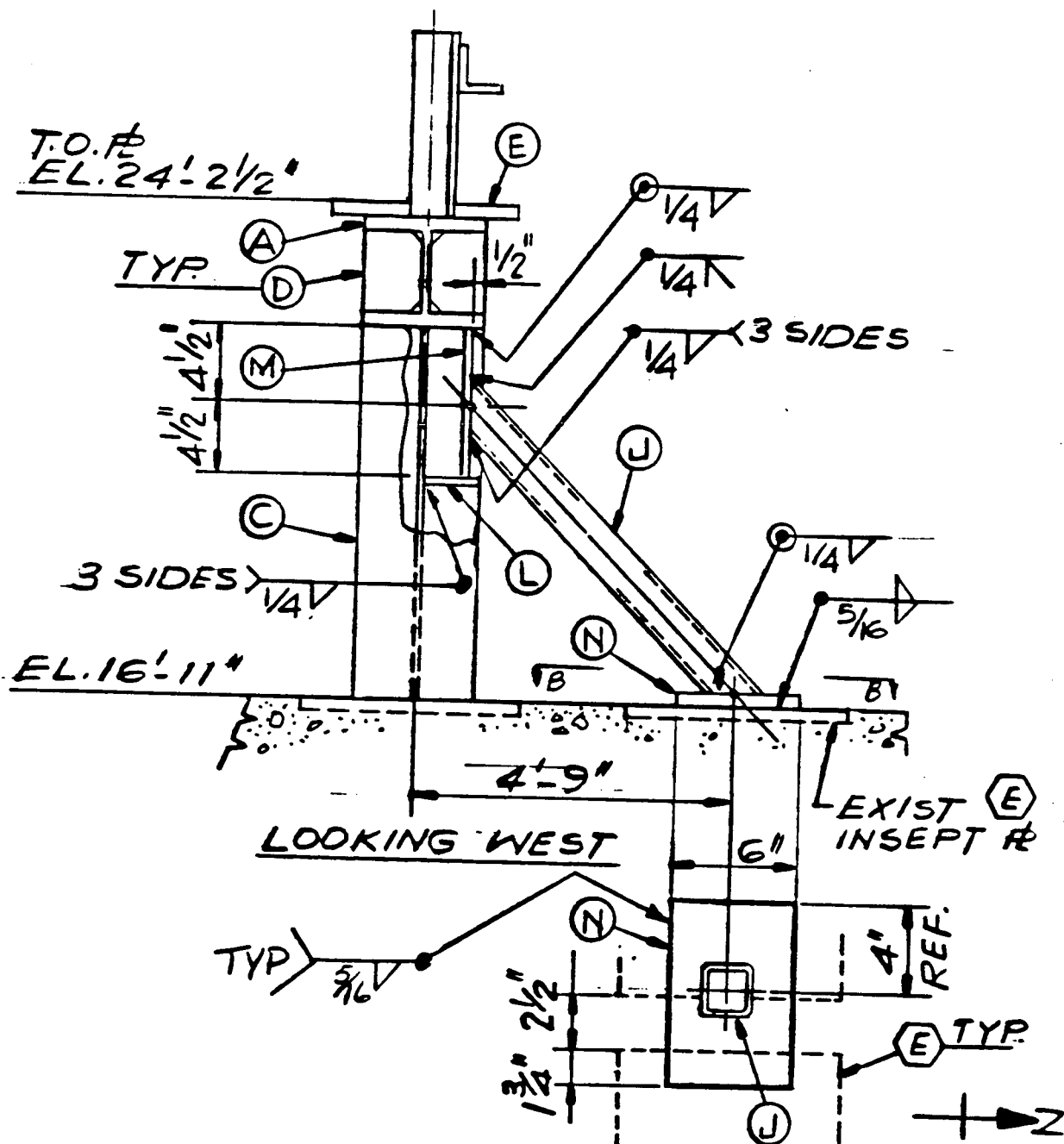


PROB. NO. 52 PT. NO. 130
 SPOOL NO. 2-RC-017-17
 ISO 1201-016-1
 REF. DWGS. PIPE 40386
 STEEL —

SHT 1 OF 2
 TAG NO. 52-RC-017-H-039

5 INCRP. DCN 01 THRU 09, REDRAWN 2-28-80		D.P.	ST	KG	YB		
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.		P.E. YQ.A.E.

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE NTS				
			LOS ANGELES, CALIF.				



** NOTE: MIN TOTAL CLRC. REQ'D IS 1/8" SECT. E-B

1201 SHT 2 OF 2
S2-RC-017-H-039 REV. 5

BECHTEL POWER CORPORATION BORWALK, CALIFORNIA			LOG NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
			FILE	PIPE SUPPORT ASSEMBLY	
JOB NO. 10079	DATE	BY		SOUTHERN CALIFORNIA EDISON COMPANY SCALE NTS LOS ANGELES CALIF.	

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4800
DATE 3-18-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 10
DATE APR 8 1980
12E. SCN NO.

(QC II) (I.C)
2BHA JOB NO. 10079 2COS-2

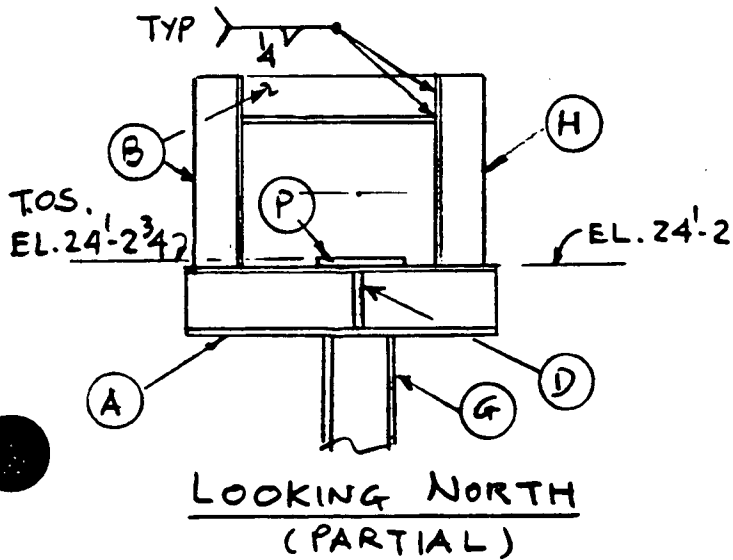
REF. DWG. OR SPEC. SHEET NO. REV. 5 TITLE Pipe Support Assembly
S2-RC-017-H-039

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Need to revise Framing & Weld Symbols.

8. CHANGE REQUEST/SKETCH



PL 5197

- Delete Item © on Sect. Looking WEST.

- No new material req'd

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE	DATE
CIVIL			
ELEC		INSTR	
MECH		NUC	
WELD		QA	<u>3-20-80</u>

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD/DISPOSITION
James J. Harvey
PROJECT FIELD ENGINEER
DATE MAR 20 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS P.E. P.L. Rogers/PLH DATE 3-19-80

REMARKS: **CONVERT TO DCN**

QUALITY ASSURANCE ENGINEER (FIELD): James J. Harvey DATE 3-20-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B. Balaban DATE 4-2-80

16. ADDITIONAL DISTRIBUTION _____

X

APR 17 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4752
DATE 4-3-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 11
12D. DATE APR 30 1980
12E. SCN NO.

2BHA
C

JOB NO. 10079 (I.C.) 2105.2

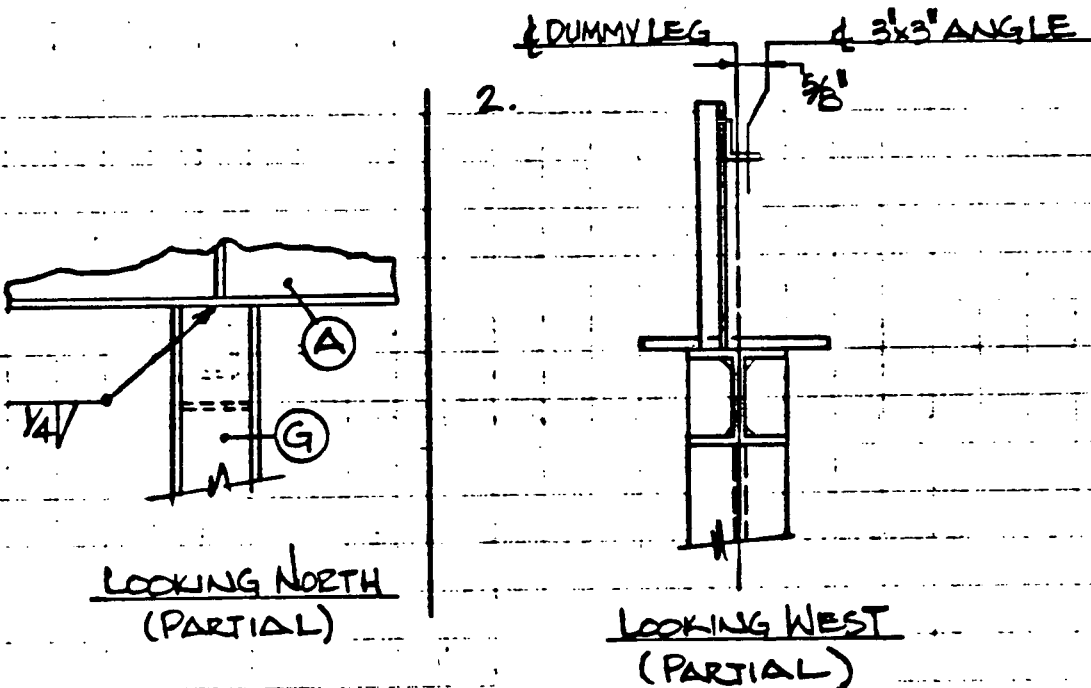
REF. DWG. OR SPEC. SHEET NO. REV. 5 TITLE
2. P.C. 017 H.C. 29 5 PIPE SUPT. ASSEMBLY

DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

1. WELD BOTH SIDES OF WEB TO MEMBER 'G' NOT REQ'D.
2. MISMATCH BETWEEN TOP DUMMY LEG AND 3"x3" ANGLE

8. CHANGE REQUEST/SKETCH TO:



PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
 CIVIL _____ DATE _____
 ELEC _____ DATE _____
 MECH _____ DATE _____
 WELD _____ DATE _____
 INSTR. M.S. 4-7-80
 NUC _____
 QA 4-8-80

PREPARED BY C.W. GREER
 APPROVAL OF FCD DISPOSITION
Dennis J. Lang
 PROJECT FIELD ENGINEER
 DATE APR 08 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____
 P.E. R.L. Rogers DATE 4-7-80
 REMARKS: CONVERT TO DCN.

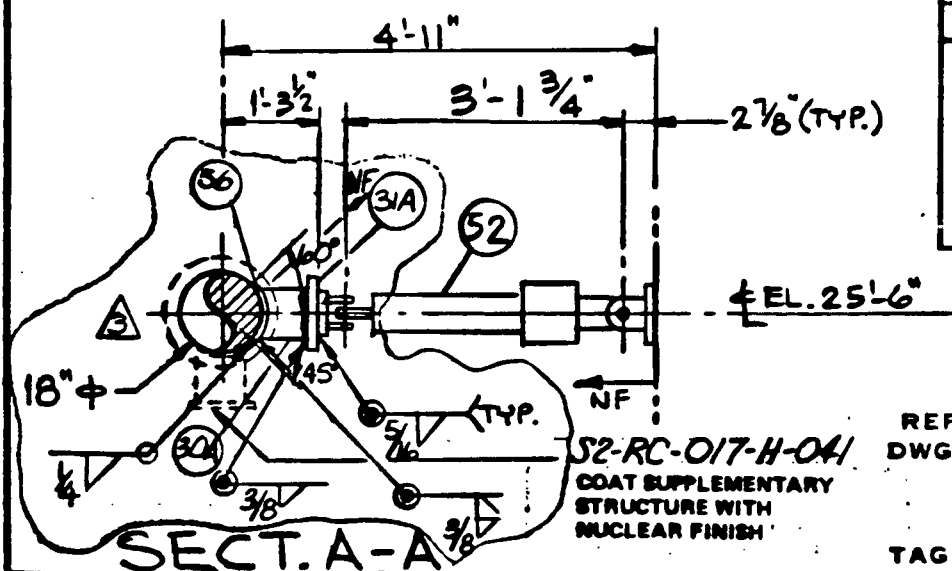
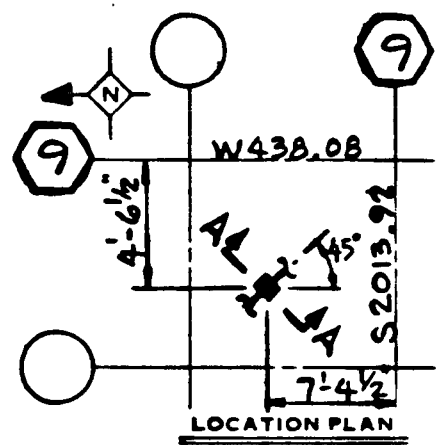
QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 4-8-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
 15. BECTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 4-28-80
 16. ADDITIONAL DISTRIBUTION _____

X

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	1	-	10" ϕ SCH. 40 S.S. DUMMY PIPE		X		BY FIELD
31A	1	-	3/4" x 12" x 10" C.S. RATE		X		" "
52	1	307	10, 6" STROKE, MECH. SHOCK SUPPRESSOR, CS = 3/4", HS = 2 3/4", W = 10"		X		
56	1	-	1/4" x 105 x 1'-2 3/4" S.S. CURVED RATE		*		BY GRINWELL BY KELLOGG
				W/ADDITIONAL REAR BRACKET, LOAD = 16,734#			
				INTEGRAL ATTACHMENT — USE CODE SUB. SEC. NC MATERIAL.			
				† FAULTED CONDITION			

SUS-2



P.M.C. - REQ		TYPE 6			
PROJ CL	PIPE C (QC II)	MAX. TEMP			
QUAL CL	STEEL II	400°F			
DESIGN	(FT-LBS)	X	Y	Z	
		M +	-	-	-
		P	11833	11833	11833
	(LBS)	11833	-	11833	

PROB. NO. 52 PT. NO. 140

SPOOL NO. 2-RC-017-18

ISO 1201-016-1

PIPE 40386

STEEL S2-RC-017-H-041

TAG NO. S2-RC-017-H-040

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	Q. A. E.
2	CHANGED 2'-11 3/4" TO 3'-1 1/4"	7-21-11	RK	AR	12/1			
3	INCORP. DCN #3 VOID DCN 5 01/5 02	2-26-80	TM	KG	PL HB			
0	ISSUED FOR CONSTRUCTION	5-12-77						

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					

MAR 12 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 2-4557
DATE 2-27-80
2. PAGE 1 OF 1
3. UNIT NO. 2

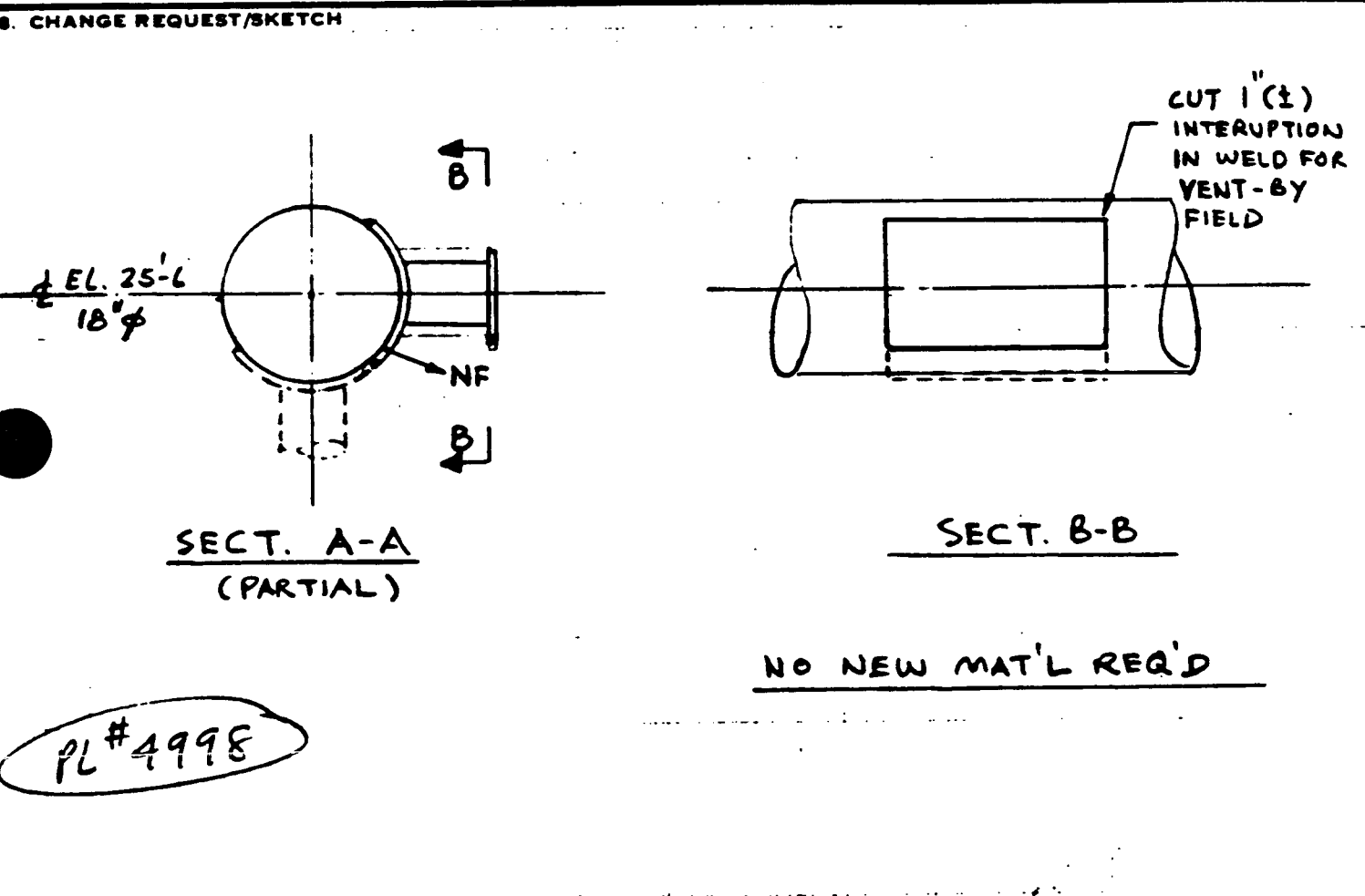
12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 04
12D. DATE MAR 24 1980
12E. SCN NO.

(QC II) JOB NO. 10079 (I.C.)
ZBHA 05-2
4. REF. DWG. OR SPEC. SHEET NO. 25 5. TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:
wrapper & weep hole was sealed by welding wrapper & of S2-RC-017-H-041



PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE H.S. 2-25-80
INSTR _____
NUC _____
QA g.w. stephens 2-26-80

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FWD DISPOSITION
g.w. stephens
PROJECT FIELD ENGINEER
DATE 2/26/80

12. PROJECT ENGRG APPROVAL: YES NO EGS
P.E. R.L. Rogers 1/14 DATE 2-25-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): g.w. stephens DATE 2-26-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE g.w. stephens DATE 2-27-80

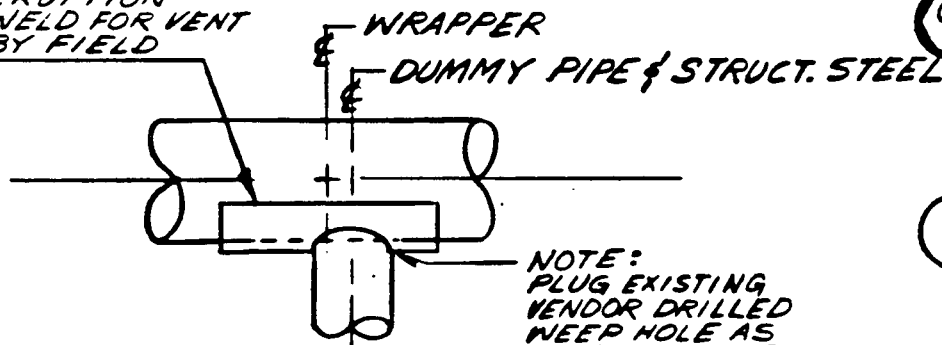
16. ADDITIONAL DISTRIBUTION _____

S.U.S.: 2BHA

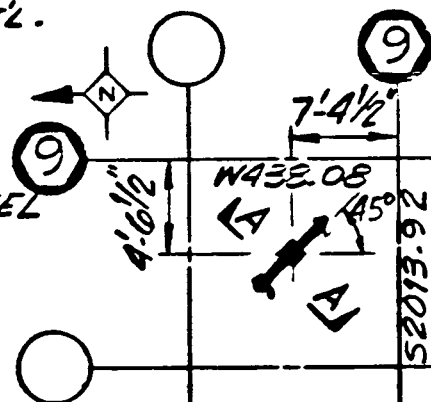
ITEM NO	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
30A	1		10" O.SCH. 40S DUMMY PIPE		X		BY FIELD
31B	1		R 3/4" X 12 X 1'-0" C.S. PLATE		X		"
6	1		1/4" X 105° X 14 3/4" S.S. CURVED PLATE		X		BY KELLOGG
A	2		W 6 X 15.5			X	BY FIELD
C	1		R 1/2 X 12 X 1'-0"			X	5023-206-1E
H	4		3/8" STIFF R			X	
J	1		R 3/4" X 14 X 2'-2 1/2"			X	
L	1		W 14 X 95 X 8'-6 1/2"			X	
M	1		R 1 X 17 1/2 X 2'-2 1/2"			X	BY FIELD
Q	1		W 4 X 13 X 1'-10"			X	
R	1		W 4 X 13 X 3'-0"			X	
S	1		W 4 X 13 X 0'-9"			X	

* INTEGRAL ATTACHMENT - USE CODE SUBJECT. 'NC' MAT'L.

NOTE:
CUT 1" (+ OR -)
INTERRUPTION
IN WELD FOR VENT
BY FIELD



SECTION F-F

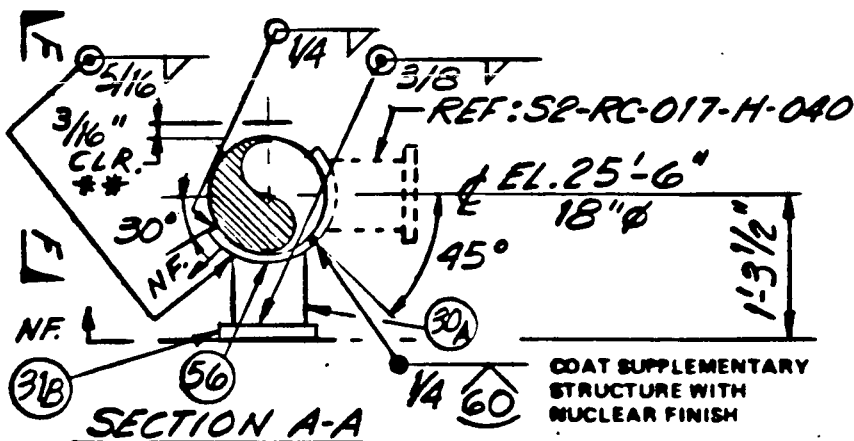


LOCATION PLAN

(I.C.) AREA NO. 2C05-2

PMC: KEO		TYPE 1		
PROJ CL	PIPE C (QC II)	MAX. TEMP		
QUAL CL	STEEL II	400 °F		
DESIGN		X	Y	Z
	M +	—	—	—
	(FT-LBS)	—	—	—
	P +	⊕	1662	⊕
	(LBS)	⊕	6721	⊕

** NOTE: MIN. TOTAL CLRC. REQ'D IS 1/8"



SECTION A-A

PROB. NO. 52 PT. NO. 140

SPOOL NO. 2-RC-017-18

ISO 1201-016-1

PIPE 40386

SHT 1 OF 2

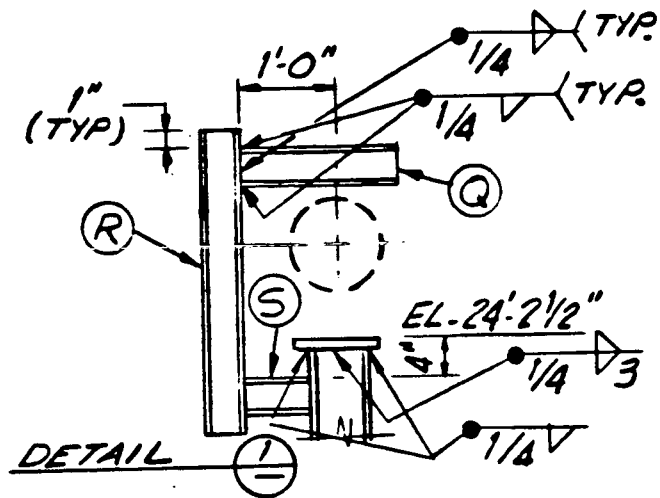
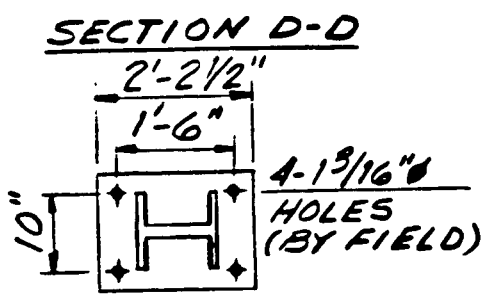
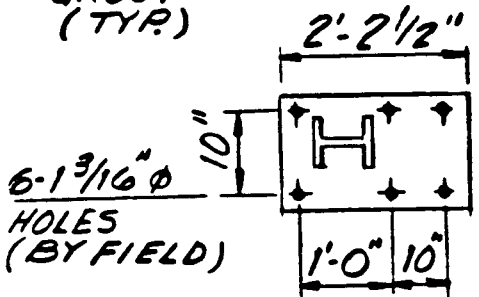
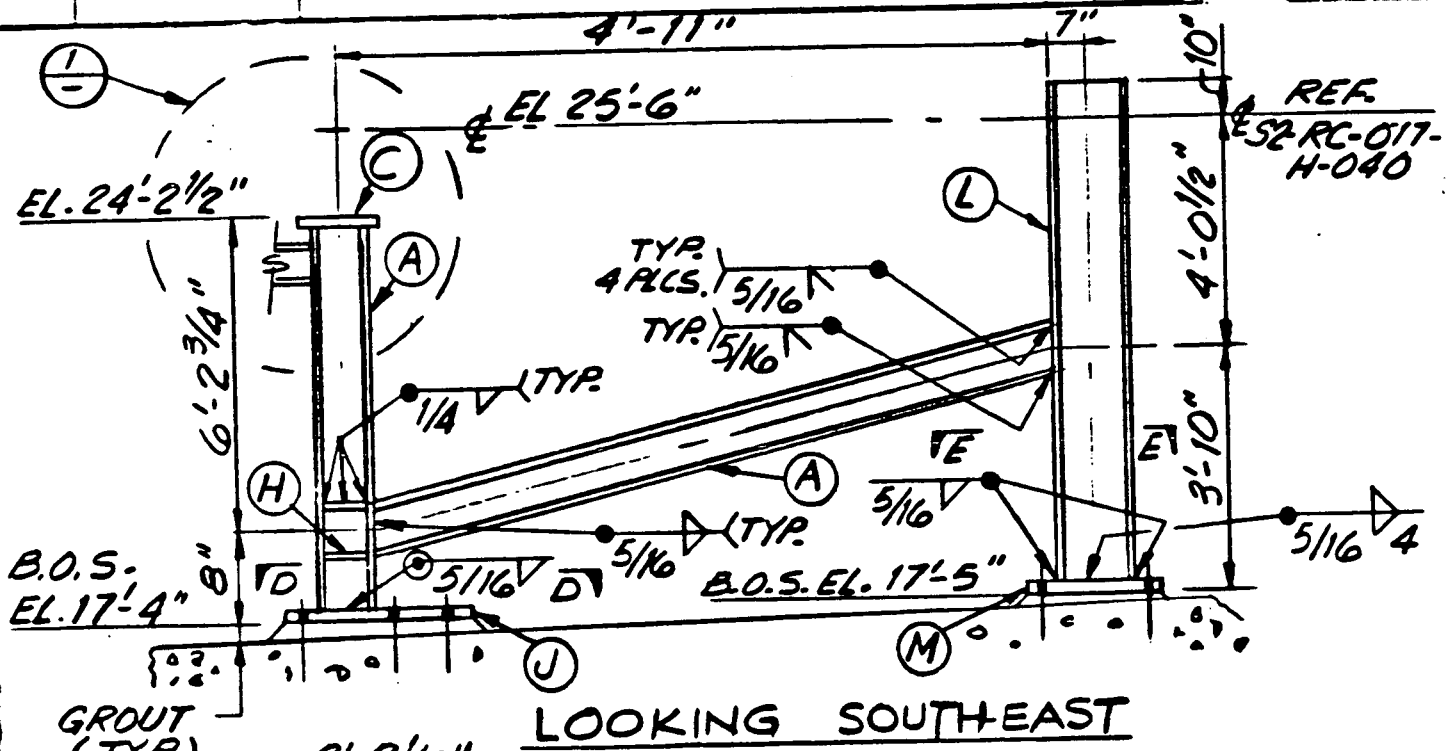
TAG NO. S2-RC-017-H-041

1201

3 INC. DCN 01, 02, 03, 04, 05, 06, 07	2-28-80	180	ST	KG		REF. P. 205
NO. REVISIONS	DATE	DR.	CHK.	E.G.S.		P.E. QAE

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
		FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.			

ITEM NO	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF A-5C	NOTES
	10		US-8-HC-LCSF-175			BY FIELD



1201 SHT 2 OF 2
S2-RC-017-H-041 REV 3

BECHTEL POWER CORPORATION SANTA MONICA, CALIFORNIA		DATE	SAN ONOFRE NUCLEAR GENERATING STATION	
10079		FILE	PIPE SUPPORT ASSEMBLY	
APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY SANTA MONICA, CALIFORNIA		

APR 10 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-495A
DATE 4-3-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND NO.

12C. DCN SUB NO. 11
12D. DATE APR 30 1980
12E. SCN NO.

2 BHA
C

JOB NO. 10079

(I.C.)
2105.2

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
2105.2 H-041 3 PIPE SUPT ASSEMBLY

DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

12c1

7. EXISTING CONDITION:

WRONG SIZE FE CALL-OUT FOR FE "M" ON
REV. 3 DWG.

8. CHANGE REQUEST/SKETCH

CHANGE BILL OF MAT'L. TO READ:

ITEM "M" - FE 1" x 1 7/2" x 2' - 1 1/2"

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIP MS 4-7-80
INSTR _____
NUC _____
QA 4-8-80

PREPARED BY C.W. GREER
11. APPROVAL OF FLD DISPOSITION
Project Field Engineer
DATE APR 08 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS
P.E. R.L. Rogers/KH DATE 4-7-80

REMARKS: CONVERT TO DCN 0511034

QUALITY ASSURANCE ENGINEER (FIELD): Proskop DATE 4-8-80

14. SCE ENGINEERING APPROVAL P.E. Bob DATE 4-28-80

15. BECTEL QUALITY ENGINEER/QUALITY ASSURANCE DATE 4-28-80

16. ADDITIONAL DISTRIBUTION

X

APR 10 1980

C/S



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 54842
DATE 3-20-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 09
12D. DATE APR 22 1980
12E. SCN NO.

(QCI) BHA JOB NO. 10079 (I.C.) 2C05-2

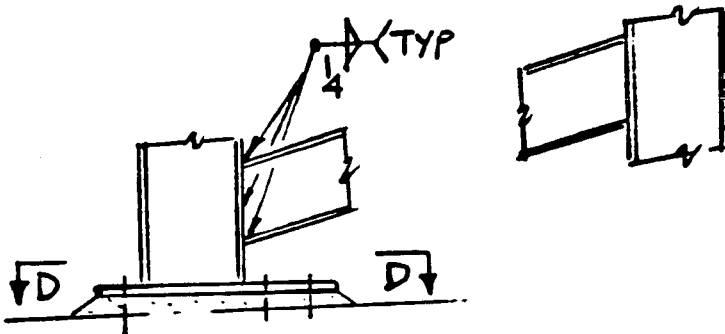
4. REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-017-H-041 3 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

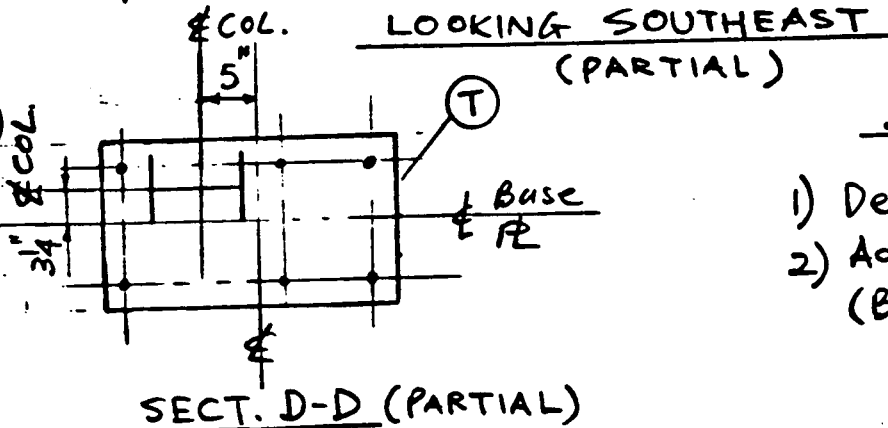
7. EXISTING CONDITION:

Need Col. Location on Sect. D-D & weld symbols
Incorrect.

8. CHANGE REQUEST/SKETCH



PL # 5246



BILL OF MAT'L REQ'D

- 1) Delete Item D
- 2) Add Item T 1ea R 1x14x2-22 (By Field)

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE JS 3-21-80
INSTR _____
NUC _____
QAEG W. S. P. J. 3-24-80

9. P. Tannirat (Signature)
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
Dennis J. Loney (Signature)
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers / RLR DATE 3-21-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): W. S. P. J. DATE 3-24-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE W. S. P. J. DATE 4-16-80

16. ADDITIONAL DISTRIBUTION _____

X

APR 24 1980

CS E H O A O



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-5025
DATE 4-16-80
2. PAGE 1 OF 1
3. UNIT NO. 3

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 12
APR 30 1980
12E. SCN NO.

C(RC-II) BHA JOB NO. 10079 IC 2C05-2

REF. DWG. OR SPEC. SHEET NO. REV. B. TITLE
52-RC-017-H-041 3 PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:
CHANGE B/M

8. CHANGE REQUEST/SKETCH

CHANGE ITEM * T TO R 3/4" X 14 X 2'-2 1/2"

NO NEW MATERIAL REQ'D

PL-5412

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 4-17-80
ELEC _____
MECH _____
WELD _____
PIPE _____
INSTR _____
NUC _____
GAE [Signature] 4-18-80

9. MARIO CAMPANILE
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE APR 18 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS P.E. R.L. [Signature] DATE 4-17-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 4-18-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____

APR 10 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 24880
DATE 3-26-80
2. PAGE 1 OF 1
3. UNIT NO. II

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. LO
12D. DATE APR 22 1980
12E. SCN NO.

JOB NO. 10079 (I.C.) 2105.2

4. REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
52-PL017-H-0A1 3 PIPE SUPT. ASSEMBLY

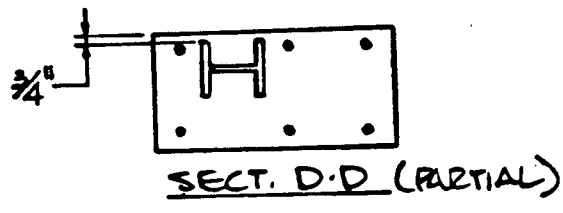
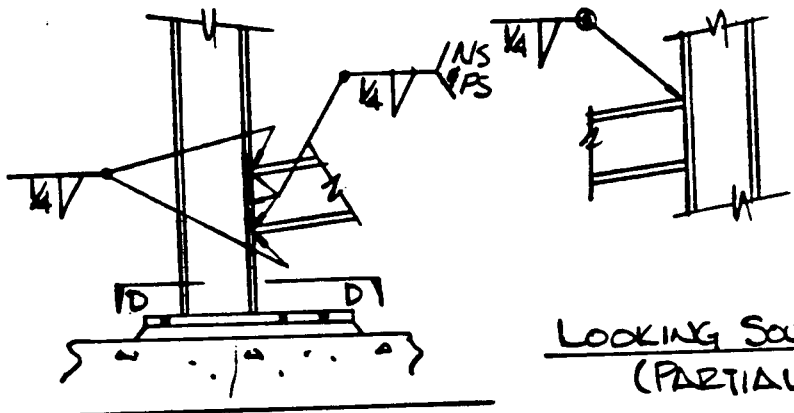
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION:

- 1. INCORRECT WELD SYMBOLS CALLED FOR
- 2. VERT. BEAM "A" FALLS OUTSIDE BOLT PATTERN OF R "J"

8. CHANGE REQUEST/SKETCH

NO NEW MAT'L. REQ'D.



SUPERSEDES
FCR 5-4719

PL# 5291 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY _____ DATE _____
 CIVIL _____
 ELEC _____
 MECH _____
 WELD _____
 PIPE M.S. 27
 INSTR 3-27-80
 NUC _____
 QA W. J. ... 3-27-80

PREPARED BY C.W. GREER
 11. APPROVAL OF FLD DISPOSITION
Howard Greer
 PROJECT FIELD ENGINEER
 DATE MAR 27 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Royce DATE 3-27-80

REMARKS: CONVERT TO D.C.N. VOID DCN 8

13. QUALITY ASSURANCE ENGINEER (FIELD): W. J. ... DATE 3-27-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE W. J. ... DATE 4-16-80

16. ADDITIONAL DISTRIBUTION _____

CIVIL PROJECT # 5291

MAR 26 1980

BOTH SIDES OF W.C.P.



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 3-4719
DATE 3-10-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 08
DATE MAR 31 1980
12E. SCN NO.

C(QCZ)
2BHA
JOB NO. 10079
REF. DWG. OR SPEC. SHEET NO. 23
5. TITLE Pipe Support Assembly

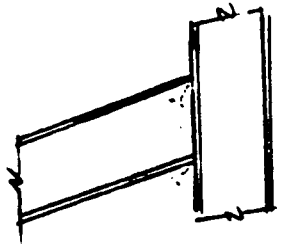
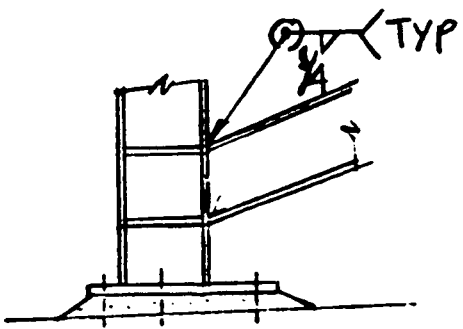
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION:

WELD SYMBOLS INCORRECT

8. CHANGE REQUEST/SKETCH

PL # 5117



NO NEW MAT'L REQ'D

LOOKING SOUTHEAST (PARTIAL)

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE M.S. 3-13-80
INSTR _____
NUC _____
QA 3-14-80

9. P. Tanniraj
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
R. L. Rogers
PROJECT FIELD ENGINEER
DATE MAR 14 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____
REMARKS: CONVERT TO DCN P.E. R.L. Rogers DATE 3-13-80

13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-14-80

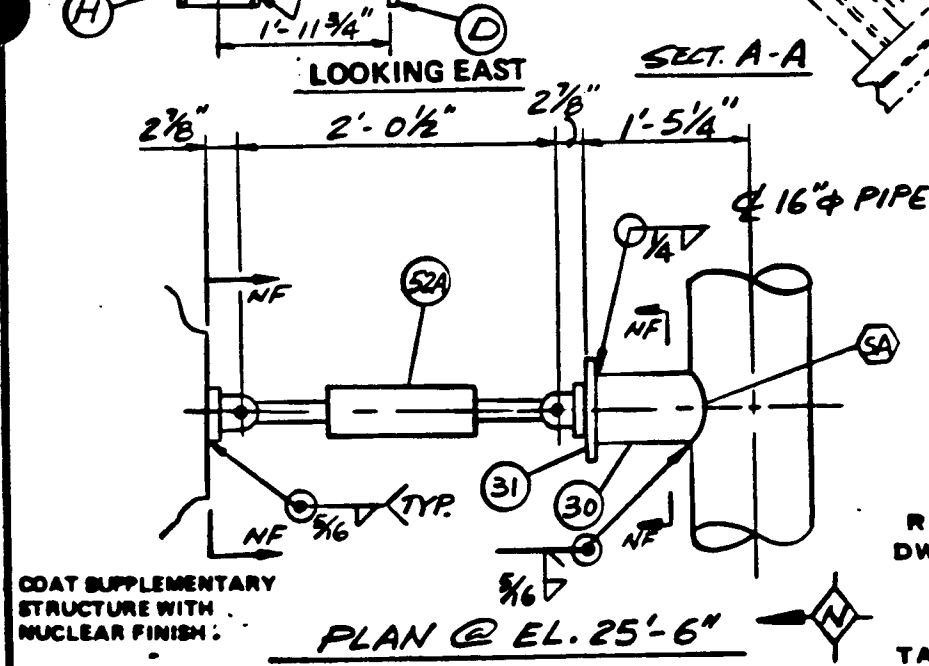
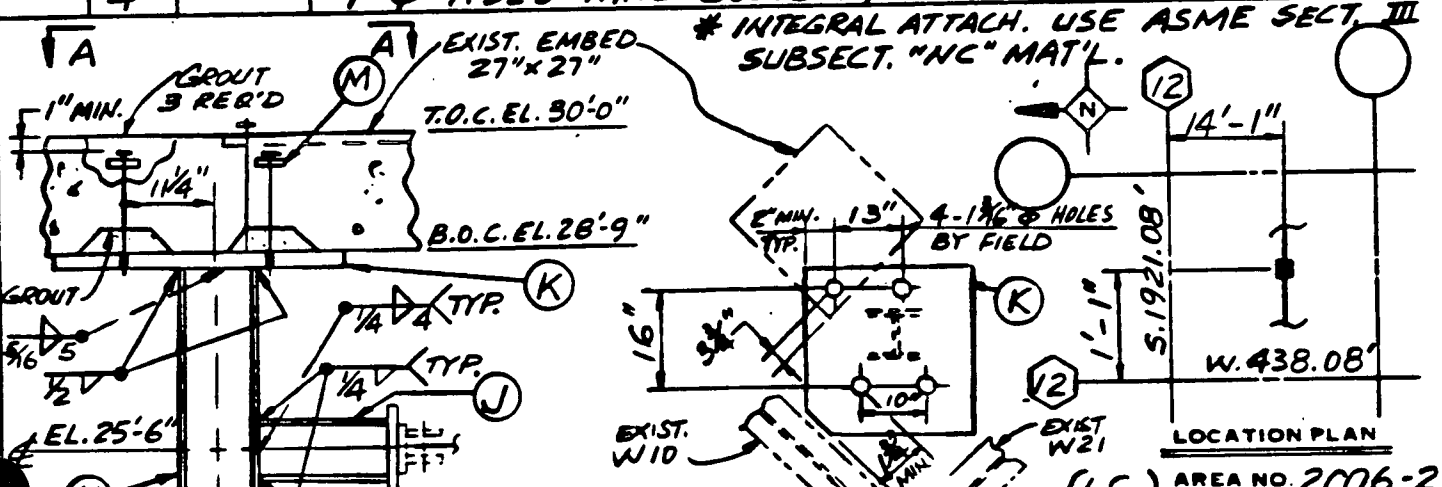
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-28-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1		8"φ SCH. 40 S.S. DUMMY PIPE		*		5023-409-23
31	1		3/4" x 12" x 1'-0" C.S. PL		X		5023-409-23
52A	1	FIG. 306	#10 - 6" STROKE MECH. SHOCK SUP. PRESSOR W/ADDITIONAL REAR BRACKET, C.S. = 4 5/16", H.S. = 1 9/16", LOAD = 11501*		X		SURPLUS FROM TAG NO. 52-TC-027-H-013
D	1		PL 3/4" x 9 x 0'-9"		X		5023-206-18
H	1		W10 x 49 x 3'-6"		X		
J	1		WB x 31 x 1'-6 3/4"		X		BY FIELD
K	1		PL 1 1/2" x 22" x 2'-2"		X		
M	3		PL 1/2" x 4" x 0'-4"		X		
	4		1"φ A325 THRU BOLTS W/WASHERS				

SUS - 2BHA



PMc-KEO		TYPE 6		
PROJ CL	PIPE C(QC II)	MAX. TEMP 400°F		
QUAL CL	STEEL II			
DESIGN	M +	X	Y	Z
	(FT-LBS)	-	-	-
	P +	11501	-	-
(LBS)	-	11501	-	-

PROB. NO. 52 FT. NO. 109

SPOOL NO. 2-RC-017-28

ISO 1201-016-1

PIPE 40400

STEEL 23211

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E. Q.A.E.
1	INCORP. DCN 1.2 & FR-S4423 & REDRAWN	2-26-80	GT	KG	RE	RP/AN R/S

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
JOB NO. 10079		FILE	PIPE SUPPORT ASSEMBLY			
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

APR 1 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4923
DATE 3-31-80
2. PAGE 1 OF 1
3. UNIT NO. II

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 03
12D. DATE APR 15 1980
12E. SCN NO.

2 BHA
JOB NO. 10079 (I.C.)
20062

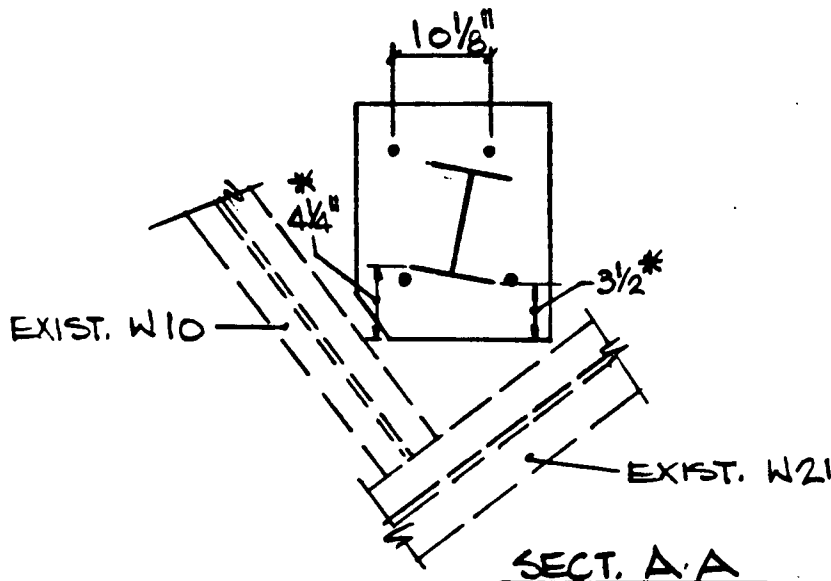
REF. DWG. OR SPEC. S2.RL.017.H.080 SHEET NO. 1 REV. 1 TITLE PIPE SUPT. ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

CLARIFICATION OF VERT. ITEM "H" LOCATION
REQ'D.

8. CHANGE REQUEST/SKETCH



*NOTE:
THESE ARE REF.
DIM. ONLY.

PL# 5324 PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE
CIVIL _____	PIPF <u>W.S.</u> <u>4-1-80</u>
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QA <u>B. Baham</u> <u>4-2-80</u>

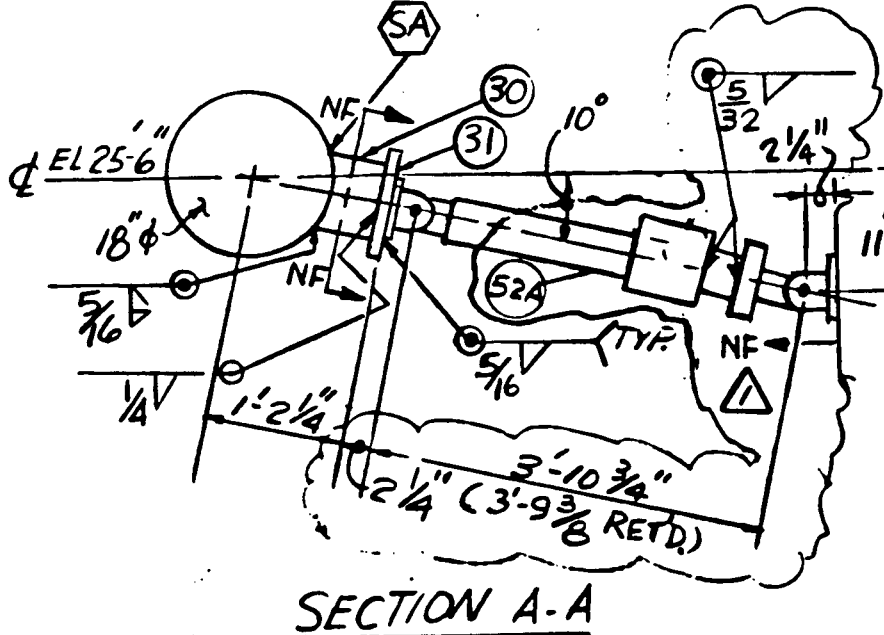
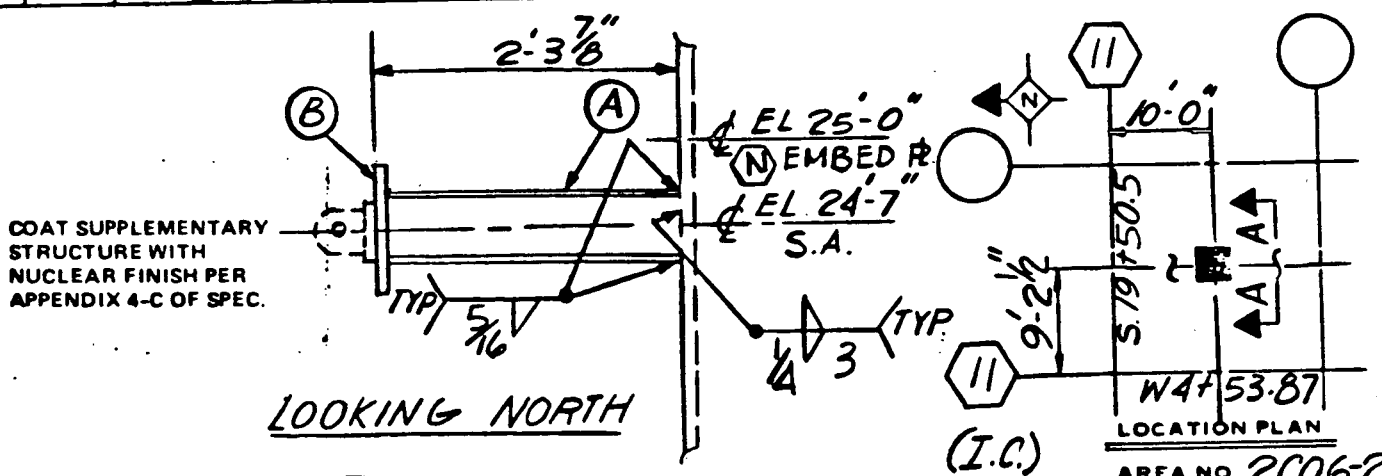
9. C.W. GREER JR.
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
Davis J. Haney
PROJECT FIELD ENGINEER
DATE APR 02 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS. P.E. R.L. Poppe/RLP DATE 4-1-80
REMARKS: CONVERT TO DCN.

13. QUALITY ASSURANCE ENGINEER (FIELD): B. Baham DATE 4-2-80
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE B. Baham DATE 4-11-80
16. ADDITIONAL DISTRIBUTION _____

DUP-CDDA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	8" SCH. 40 SS. DUMMY PIPE		*		BY SPEC.
31	1	-	3/4" X 10" X 0-10" C. STEEL PLATE		X		5023-409-23
52A	1	-	PSA-3-5" STROKE PIN-1811011-46		X		BY PSC
				SHOCK ARRESTOR KIT NUCLEAR CLASS-II CPS=1 7/8" HPS=3 1/2" LOAD: 2194 #			
A	1	-	WB X 24			X	BY SPEC.
B	1	-	1" X 9" X 0-9" PLATE			X	5023-206-18
* INTEGRAL ATTACH. - USE ASME SUBSECTION NC MAT'L							



PMC - KEO		TYPE 6	
PROJ CL	PIPE C (QCII)	MAX. TEMP 400°F	
QUAL CL	STEEL		
DESIGN		X	Y
	M +	-	-
	(FT-LBS)	-	-
	P +	-	2194
	(LBS)	-	2194

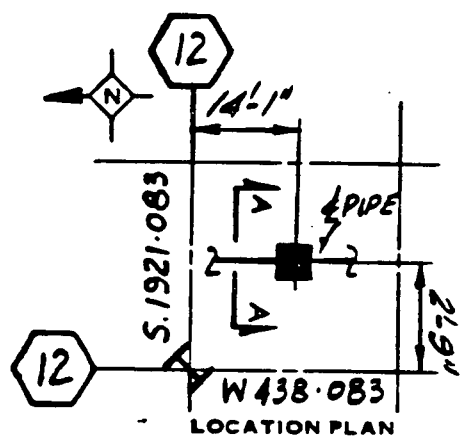
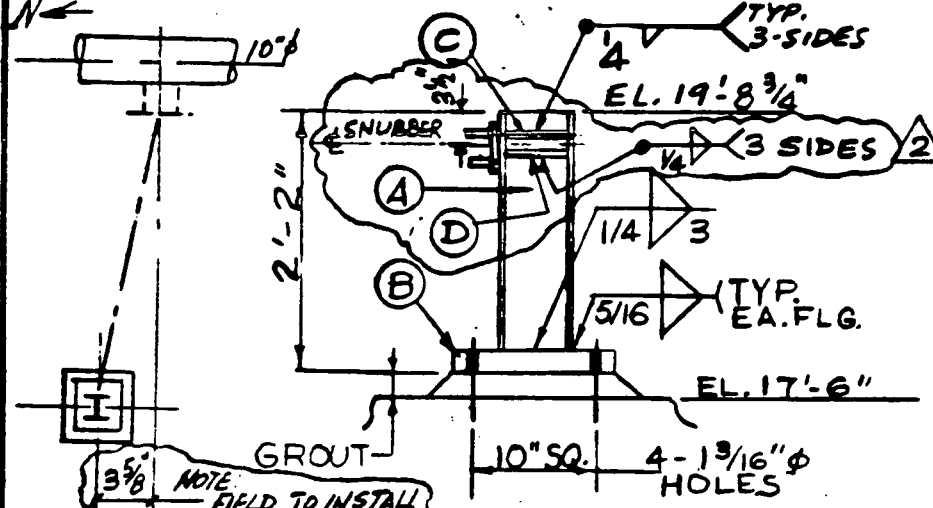
S PROB. NO. 52 PT. NO. 122
 SPOOL NO. 2-PC-017-16
 ISO 1201-016-2
 PIPE 40400
 STEEL 23177

REF. DWGS. TAG NO. 52-PC-017-H-081

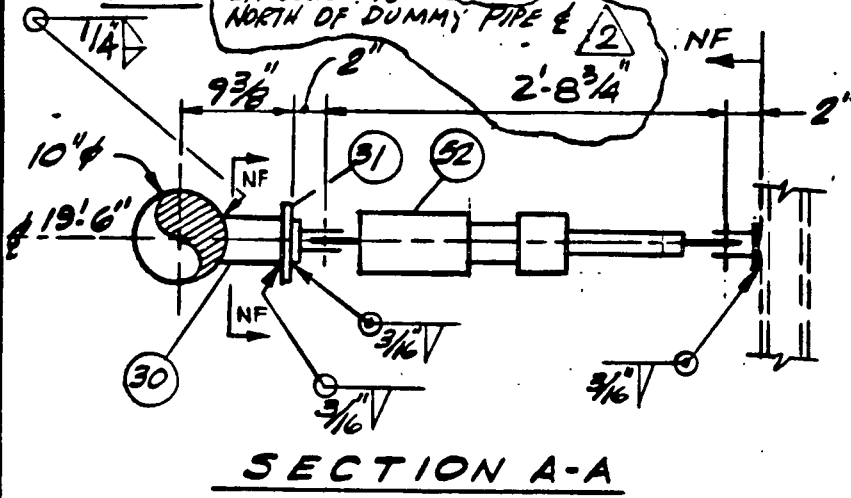
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
1	SNUBBER VENDOR CHANGE	10-16-79	NY	SBP	4m MB		
0	ISSUED FOR CONSTRUCTION	6-6-79	RSS	RY	HSN RWS MB		

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
		FILE	PIPE SUPPORT ASSEMBLY				
JOB NO.	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				
10079							

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	—	6" SCH. 40S DUMMY PIPE S.S.		*		BY KELLOGG
31	1	—	8" x 8" x 3/8" C.S. PLATE		X		" "
52	1	307	3-5 MECH. SHOCK SUPPRESSOR		X		BY GRINNELL
			W/ OPTION J CPS. = 3.2905"				
			H.P.S. = 1.7095 W = 8.88" LOAD = 1150 #				
* INT. ATTACH. USE ASME SECT. III SUBJECT. 'NC' MAT'L							
D	2	2	3/8" STIFF. R			X	BY FIELD
A	1		W 6 X 20			X	SPEC.
B	1		# 3/4 X 14 X 1'-2"			X	5023-206-1F
C	2		3/8" STIFF. R				
	4		US-8-HC-LCSF-175				BY FIELD



NOTE: FIELD TO INSTALL THIS END OF SNUBBER 9 5/8\"/>



PMC: KEO
 TYPE: G
 PROJ. CLASS: C (QC II)
 MAX. TEMP: 400 °F
 OPER. LOAD (LBS.):
 DESIGN LOAD (LBS): 1150
 PROB. NO. 52 PT. NO. 91
 SPOOL NO. 2-RC-071-1
 ISO 1201-016-1
 PIPE 40400
 STEEL

TAG NO. 52-RC-071-H-001

2	INCORPORATED DCNS 162 & RR 4434	2-26-80	KG	PR	1201		
1	ADDED STIFF.	7-11-77	CL	GB			
0	ISSUED FOR CONSTRUCTION	2-8-77	MM	MDA/AL			

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4722
DATE 3/10/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 03
12D. DATE MAR 25 1980
12E. SCN NO.

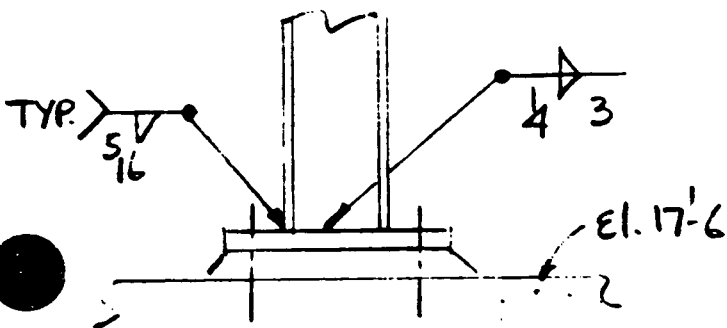
C(QCI)
BHA JOB NO. 10079
F. DWG. OR SPEC. SHEET NO. 12 REV. 1 5. TITLE Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:
WELD SYMBOLS INCORRECT

8. CHANGE REQUEST/SKETCH

PL# 5120



LOOKING SOUTH (PARTIAL)

NO NEW MAT'L REQ'D

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 3-11-80
ELEC _____ INSTR. R.J.S.
MECH _____ NUC _____
WELD _____ QAE [Signature] 3-12-80

9. P. Terrazano
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE MAR 12 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS. P.E. R.L. Kogers/PL DATE 3-11-80

REMARKS: **CONVERT TO DCN**

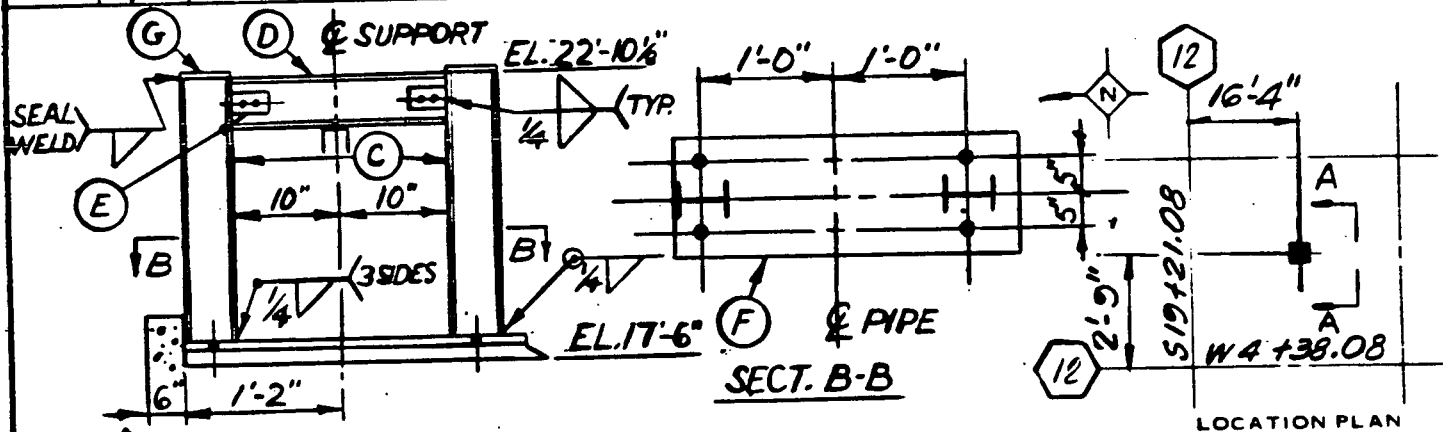
13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-12-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

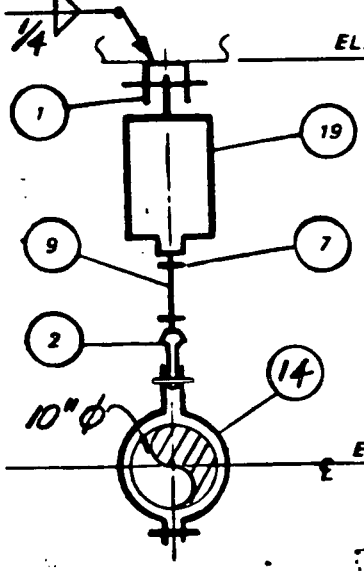
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-25-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
1	1	66	1 1/8"	BEAM ATTACHMENT WITH PIN & COTTER	X		BY FIELD
2	1	290	1 1/8"	WELDLESS EYENUT W/R.H. TAP	X		BY GRINNELL
7	2	-	1 1/8"	HEX NUT	X		"
9	1	140N	1 1/8" φ	ROD W/R.H.T. BOTH ENDS 1'-2 3/4" LG.; W/ 4 TBE	X		"
14	1	295H	10" φ	DOUBLE BOLT CLAMP	X		"
19	1	C-82	#3	TYPE "B" VARIABLE SPRING HL-2574* CL 2290*	X		BY GRINNELL
				MVT. .237" DN :WTS			
C	2	-	1 1/2" x 1 1/2" x .25"				SPEC. 5023-206-1B
D	2	-	1 1/2" x 2 1/2" x 1/4"				
F	2	-	1 1/2" x 2 1/2" x 1/4"				
G	2	-	1 1/2" x 4 x 1/4"				
	4			5/8" φ HEX. BOLTS			"BY FIELD"
	4			US-B-HC-LCSF-175			



LOCATION PLAN
(I.C.) AREA NO. 2C06-2



NOTE:
SPRING TO BE LOCKED
DURING HYDRO TEST

COAT SUPPLEMENTARY
STRUCTURE WITH
NUCLEAR FINISH PER
APPENDIX 4-C OF SPEC.

DESIGN CODE C		TYPE 5	
PROJ CL	PIPE C(QC II)	MAX. TEMP 400°F	
QUAL CL	STEEL		
DESIGN		X	Y
	M +	-	-
	(FT-LBS)	-	-
	P +	-	-
	(LBS)	-	2660

PROB. NO. 52 PT. NO. 91
SPOOL NO. 2-RC-071-1
1201-016-1
REF. DWGS. PIPE 40400
STEEL 1201

TAG NO. S2-RC-071-H-002

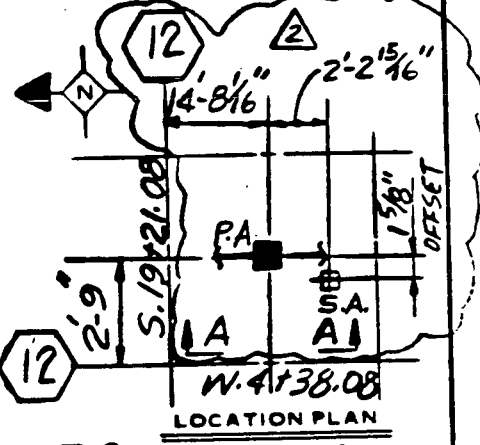
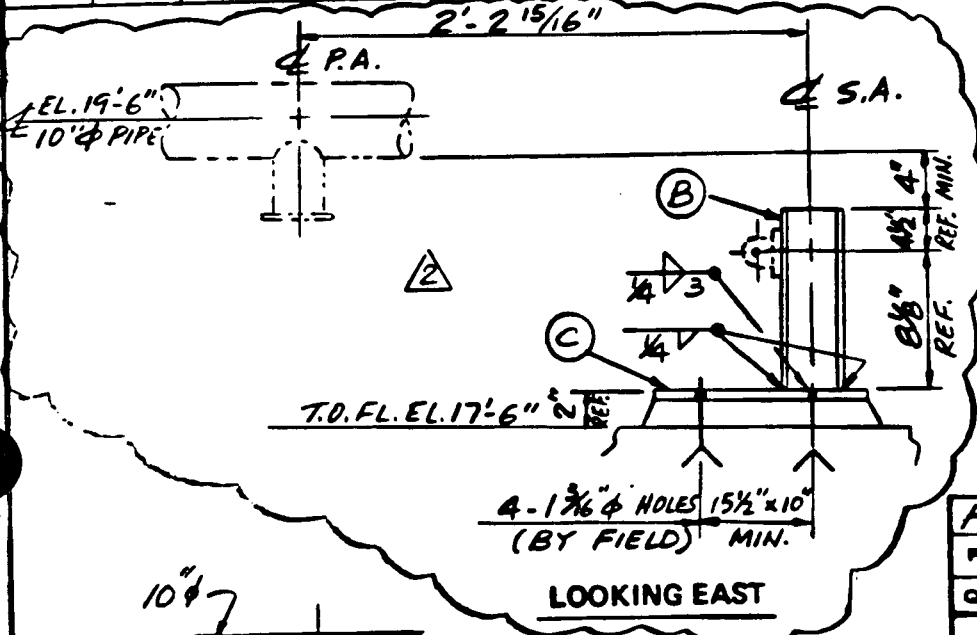
2	INCORP. DCN'S 1-1, 3 ISSUE VOID/STRESS 5-24-77 DWH FSM HSN	5-24-77	DR.	CHK.	EGS.	P.E.	OAE
1	REV. SECT. B-B ELEVATION B/M	8-25-77	DR.	CHK.	EGS.	P.E.	OAE
0	ISSUED FOR CONSTRUCTION	3-12-77	DR.	CHK.	EGS.	P.E.	OAE

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS				
			LOS ANGELES, CALIF.				

ITEM NO	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	6" SCH. 80S DUMMY PIPE		#		BY SPEC.
31	1	-	1/2" x 9" x 0'-9" C.S. BASE PL		X		S023-409-23
52A	1	F16306	#10-6" STROKE, MECH. SHOCK SUPPRESSOR. CS=1.671" H.S.=4.33"		X		USE SURPLUS MAT'L FROM S2-FW-294-H-005
				W/ADDITIONAL REAR BRACKET			
				LOAD = 7686"			
B	1	-	W6 x 15.5				BY FIELD
C	1	-	PL 1/2" x 22 x 2'-6"				
	4	-	US-B-HC-LCSF-175				

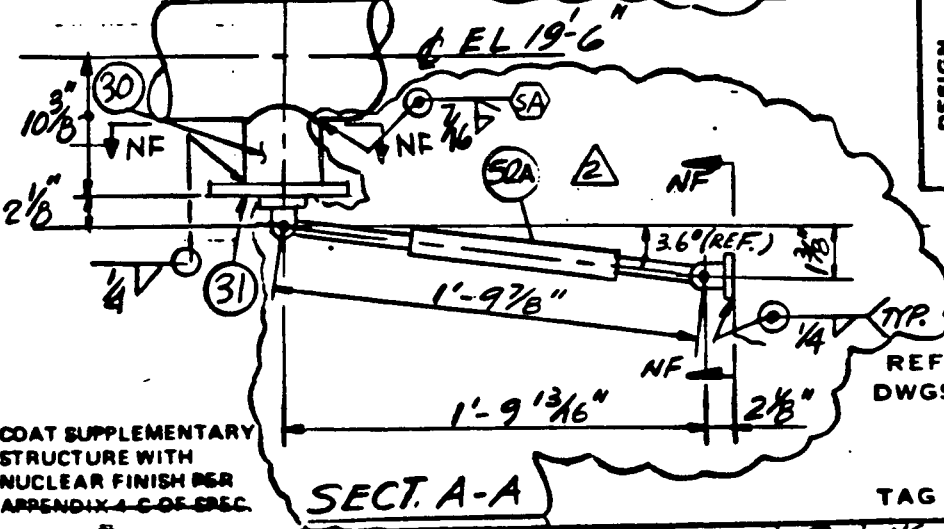
* INTEGRAL ATTACH - USE ASME SUBSECTION NC MAT'L

SLIS-2BHA



I.C. AREA NO. 2C06-2

PMC-KEO		TYPE	6
PROJ CL	PIPE C(QCD)	MAX. TEMP	
QUAL CL	STEEL II	400°F	
DESIGN		X	Z
	M +	-	-
	(FT-LBS)	-	-
	(LBS)	7686	-



PROB. NO. 52 PT. NO. 91
 SPOOL NO. 2-RC-071-1
 ISO. 1201-016-1
 PIPE 40400
 STEEL -

TAG NO. S2-RC-071-H-003

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
2	IN CORP. DCN 1, 2, 3, 4 & 5	2-26-80	GT	Y4	PL. MB 1201	-	FURMAN
1	REVISED AS NOTED (Q.E. TO Q.A.E.)	3-2-79	CH	PL		-	PL
0	ISSUED FOR CONSTRUCTION	2-9-79	RSS	PL	HSN 1005	-	PL

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
JOB NO. 10079			FILE	PIPE SUPPORT ASSEMBLY			
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.					
SCALE: NTS			01-02-01				



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 24095
DATE 4.8.80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 06
DATE APR 30 1980
12E. SCN NO.

2 DHA
C

JOB NO. 10079

(I.C.)
21062

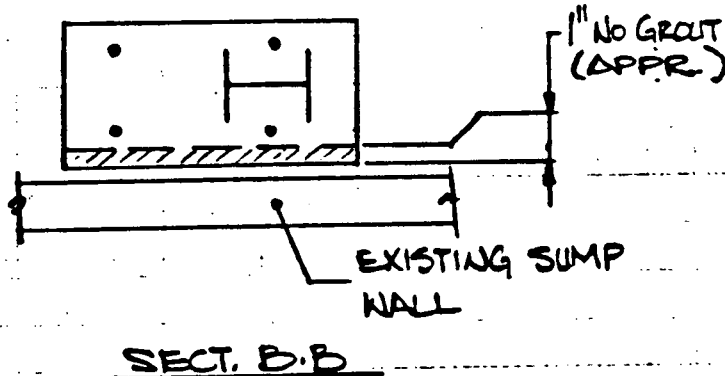
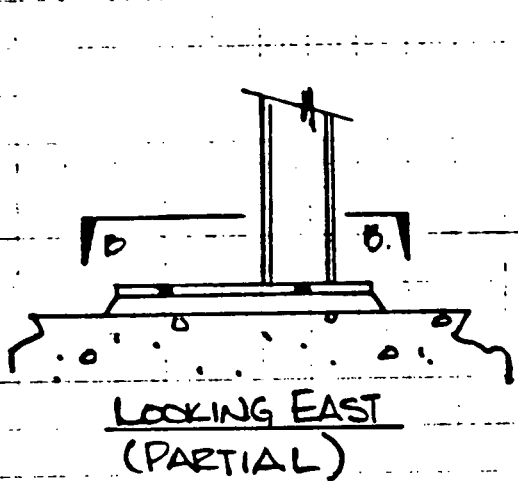
F. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
RC-071-H-003 2 PIPE SUPT. ASSEMBLY

DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

1. GROUTING OF BASE P AS CALLED FOR WILL NOT ALLOW WATER DRAINAGE TO PROXIMITY OF SUMP WALL. 2 SECT. B-B REQ'D.

8. CHANGE REQUEST/SKETCH TO



PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 4-9-80
ELEC _____ INSTR. 14.5
MECH _____ NUC _____
WELD _____ QAE approved 4-10-80

PREPARED BY C.W. GREER
11. APPROVAL OF FLD/DISPOSITION
David J. [Signature]
PROJECT FIELD ENGINEER
DATE 4-10-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____
REMARKS: CONVERT TO DCN P.E. R.L. Pagen/Kth DATE 4-9-80

QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 4-10-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 4-28-80

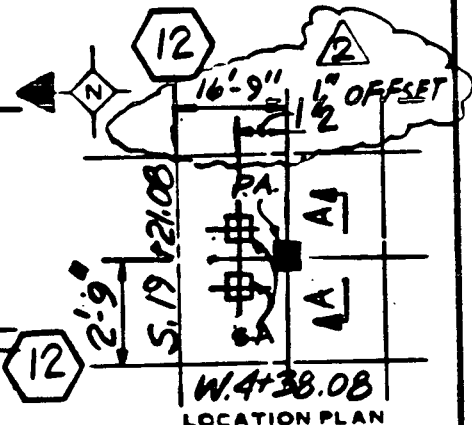
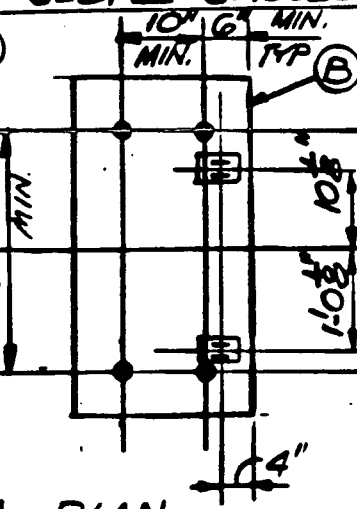
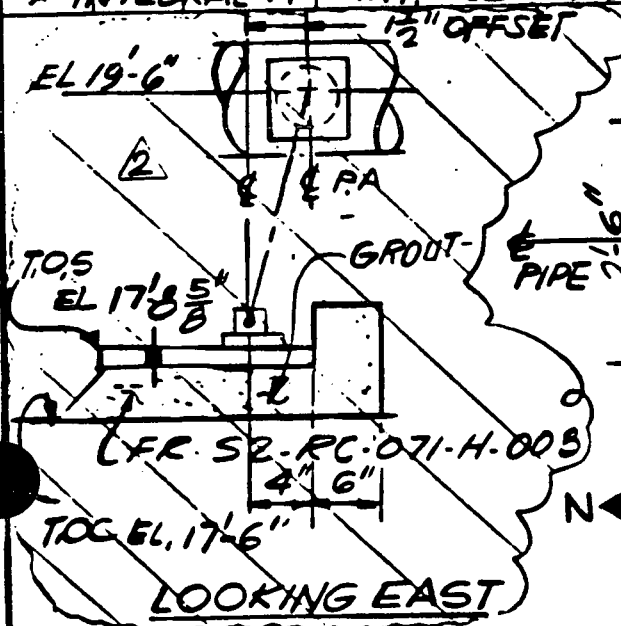
16. ADDITIONAL DISTRIBUTION _____

X

SUS-2BHA

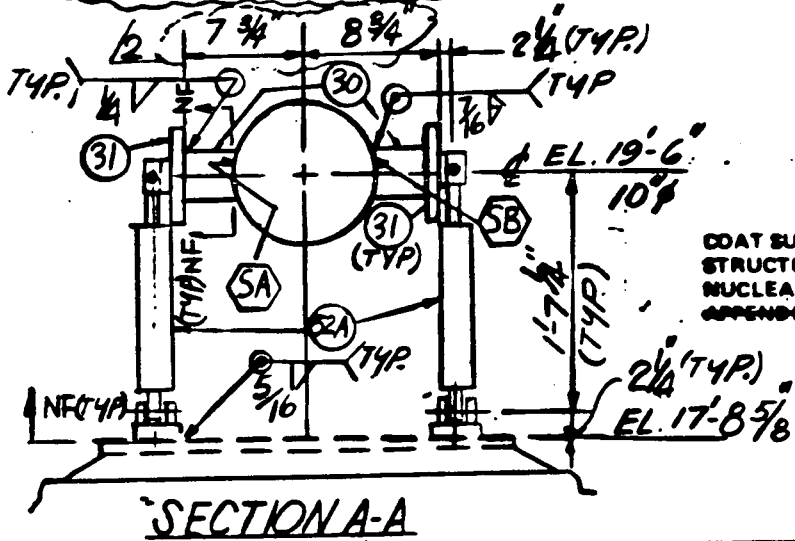
ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	2	-	6" SCH. 80S DUMMY PIPE		#		BY SPEC.
31	2	-	1/2" X 9" X 0.9" C.S. BASE PLATE		X		5023-409-23
52A	2	-	PSA 3-5 STROKE PIN 1B11012-02		X		BY PSC
				SHOCK ARRESTOR KIT, NUC. CLASS 2, CPS = 2 3/4" H.P.S. = 2 1/2" LOAD = 2549*			
				EACH			
B	1	-	R 1 X 22" X 3 1/2" G			X	BY FIELD
	4	-	US-8-HC-LCSF-175				BY FIELD

* INTEGRAL ATTACH-USE ASME SECT. III SUBJECT, "NC" MAT'L



I.C. AREA NO. 2C06-2

PMC-KEO		TYPE 6		
PROJ. CL.	PIPE C(OCL)	MAX. TEMP		
QUAL. CL.	STEEL -	400°F		
DESIGN		X	Y	Z
M +		-	-	-
(FT-LBS)		-	-	-
P +		5100	-	-
(LBS)		5100	-	-



COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH PER APPENDIX 4 OF SPEC.

PROB. NO. 52 PT. NO. 291
 SPOOL NO. 2-RC-071-1
 ISO. 1201-016-1
 PIPE 40400
 STEEL S2-RC-071-H-003

TAG NO. S2-RC-071-H-004

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.E.
2	INCORP. DCN #3, 4 FOR 4532	2-26-80	TM				
1	SNUB. VIB. D. CHG'D. EING. DCN. #152	10-16-79	JL				
0	ISSUED FOR CONSTRUCTION	6-6-79	PSS				

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
		FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.				
			SCALE: NTS				

MAR 19 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 3-4675
DATE 3-3-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 05
12D. DATE MAR 27 1980
12E. SCN NO.

4. REF. DWG. OR SPEC. S2-RC-071-H-004 SHEET NO. 12 REV. 1 5. TITLE Pipe Support Assembly

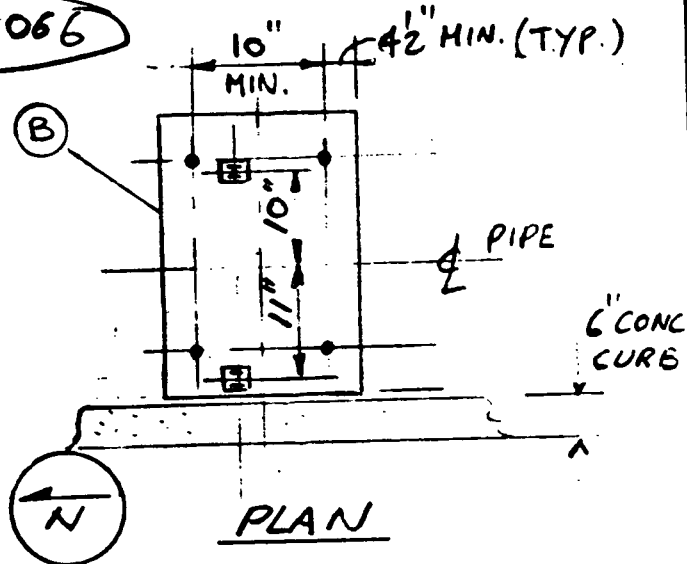
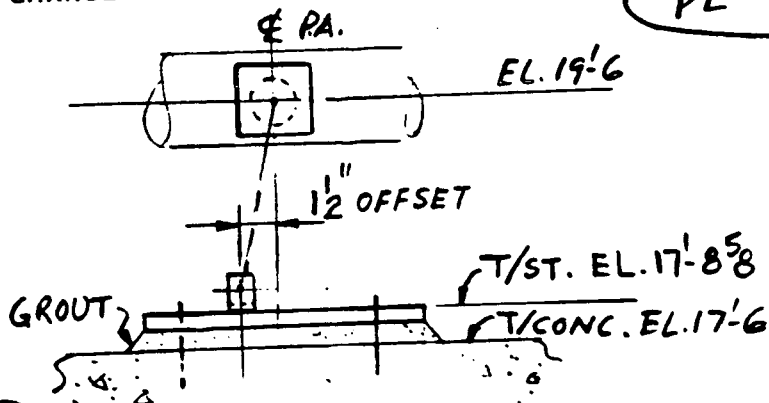
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION:

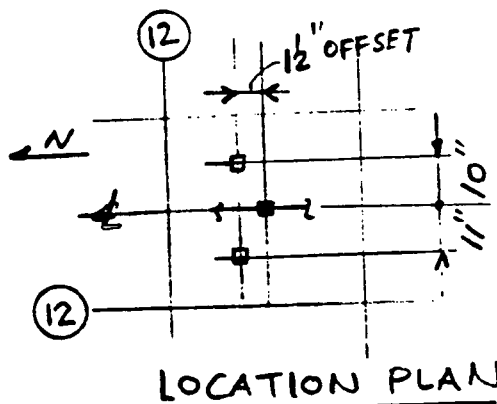
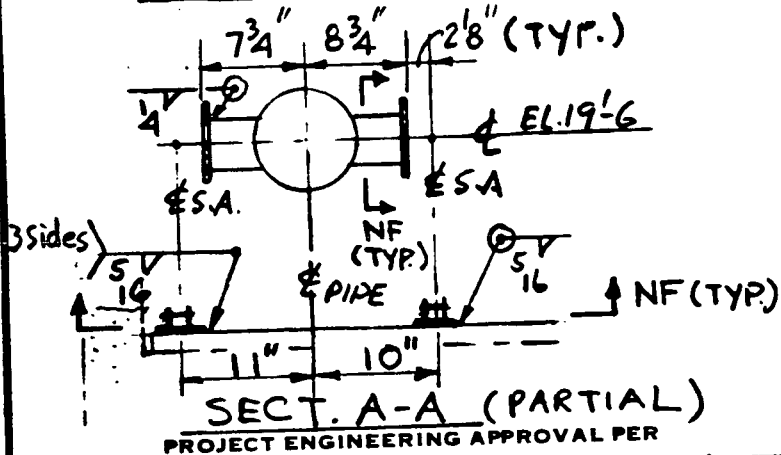
DIMENSIONS SHOWN INCORRECT.
NO NEW MATERIAL REQ'D

8. CHANGE REQUEST/SKETCH

PL #5066



LOOKING EAST



10. REVIEWED BY _____ DATE _____
CIVIL _____
ELEC _____
MECH _____
WELD _____

PIPE PLS 3-4-80
INSTR. _____
NUC _____
QA W. Stepp 3-5-80

9. P. Tannir
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
Darin [Signature]
PROJECT FIELD ENGINEER
DATE MAR 05 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS _____

P.E. R.L. Poyen/RA DATE 3-4-80

REMARKS:

CONVERT TO DCN

~~NO VOID FOR S453A~~

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. Stepp DATE 3-5-80
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE J.W. Stepp DATE 3-26-80
16. ADDITIONAL DISTRIBUTION _____

MAR 19 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 54672
DATE 3-5-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 06
12D. DATE MAR 27 1980
12E. SCN NO.

RC II)
2BHA JOB NO. 10079 (I.C.)
2C06-2

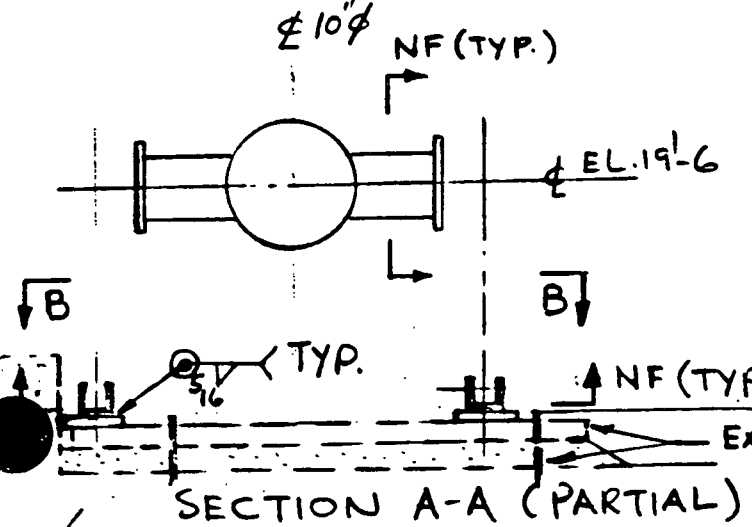
4. REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-071-H-004 2 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)
1201

7. EXISTING CONDITION:
Not adequate projection for rock bolts

8. CHANGE REQUEST/SKETCH

PL#5091



BILL OF MATERIAL
- Add item C 2 ea - $\Phi 4 \times 3 \times \frac{3}{4}$
(by field)
- Delete item B

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE R.L.S. 3-11-80
INSTR _____
NUC _____
GAE [Signature] 3-12-80

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE MAR 12 1980

12. PROJECT ENGRG APPROVAL: YES NO EGS
P.E. R.L. Hoyer/124 DATE 3-11-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-12-80

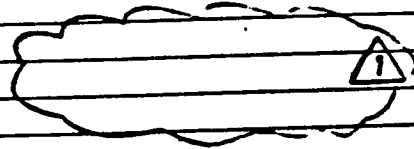
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-26-80

16. ADDITIONAL DISTRIBUTION _____

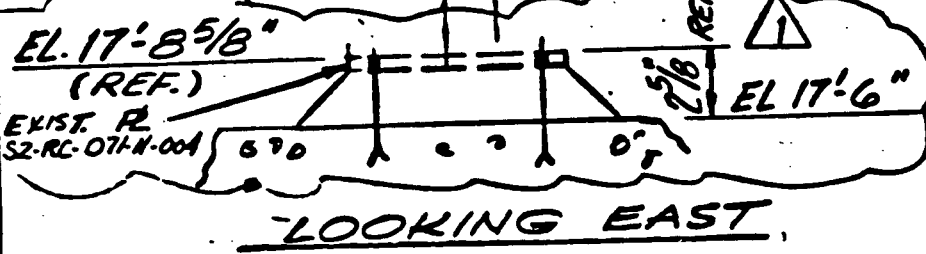
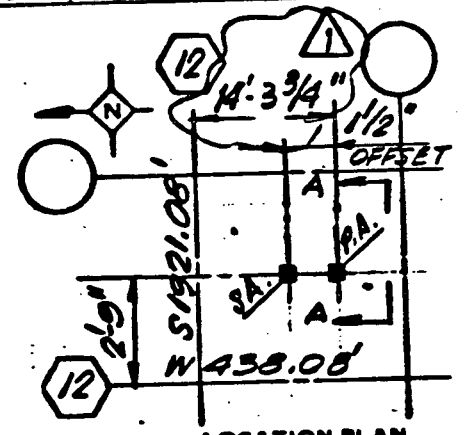
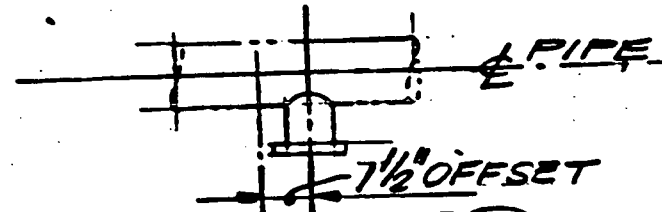
LCC

SUS-2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1		4" ϕ SCH. 80S DUMMY PIPE	}	*		SPEC
31	1		1 X 10 X 0'-10" C.S.P.		X		S023-409-23
23	1	TVS1	13 TYPE "F" VARIABLE SPRING H.L. = 2614", C.L. = 2357", MVT. = .26" DN		X		BY STC

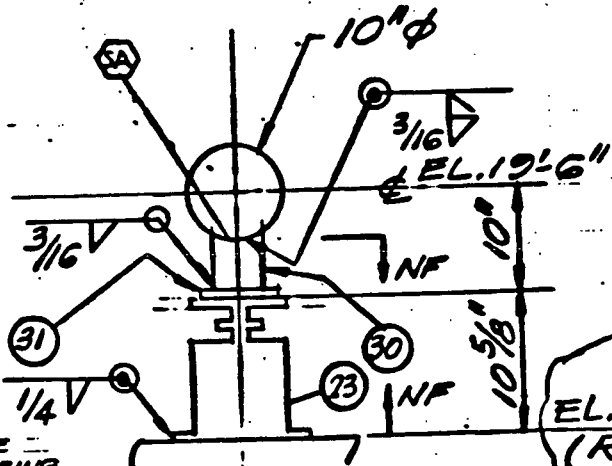


*INTEGRAL ATTACHMENT-USE ASME SECT. III SUBSECTION "NC" MAT'L



I.C. AREA NO. 2006-2

PMC-KEO		TYPE 5		
PROJ CL	PIPE C(QC II)	MAX. TEMP		
QUAL CL	STEEL II	400°F		
DESIGN	M	X	Y	Z
	(FT-LBS)	-	-	-
	P	⊗	⊗	⊗
	(LBS)	⊗	(3301)	⊗



PROB. NO. 52 FT. NO. 291
 SPOOL NO. 2RC-071-1
 ISO 1201-016-1
 PIPE 40400
 STEEL S2-RC-071-H-004
 TAG NO. S2-RC-071-H-005

NOTE: SPRINGS TO BE LOCKED DURING HYDRO TEST

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH

1	INCORP. DCN 01, 02, 03 & 04	3-5-80	B/SB	KG	KG	1201	AKM/LS
0	ISSUED FOR CONSTRUCTION	7-13-79	GC	VM	PL	93	RS/SLS CT
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.		SAN ONOFRE NUCLEAR GENERATING STATION			
JOB NO. 10079		DATE		FILE		PIPE SUPPORT ASSEMBLY	
APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY		LOS ANGELES, CALIF.			
		SCALE: NTS		01-02-01			

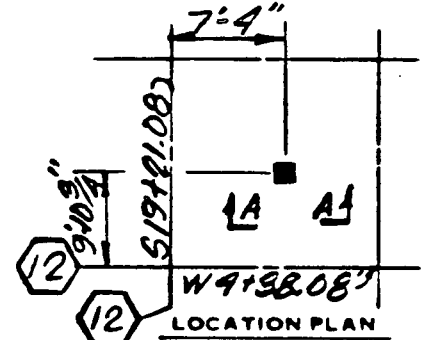
ITEM NO.	NO REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
31	2	-	8"x8"x1/4" CS. R.		X		BY KELLOGG.
30	2	-	6" SCH. 1205 DUMMY PIPE.		*		"
5A	1	-	UPPER SLIDE BEARING 10GA. S.S. 7 1/2"x7 1/2" R.				BY FIELD.
55	1	-	LOWER SLIDE BEARING BRONZITE 1/4"x7"x7" R.				"
15	4	-	C.S. BEAR 3/16"x3/16"x3"				
A	2	-	W8X35.		X		
B	2	-	W4X13.				
C	1	-	R 3/4"x16"x1'-9"				SPEC.
D	2	-	R 1/2"x8"x0'-8"				5023-206-18
E	6	-	3/8" STIFF. R.				
F	2	-	R. 3/8"x2 1/2"x0'-6"				
G	1	-	TS 3x6x1/2.				
J	2	-	R 1/8"x4"x0'-7"				BY FIELD.
	4	-	3/4" HEX BOLTS.				5023-206-18
	4	-	US-B-HC-LCSF-175		X		BY FIELD

* INTEGRAL ATTACH. USE ASME SECT. III
SUBSECT. NB. MATL.

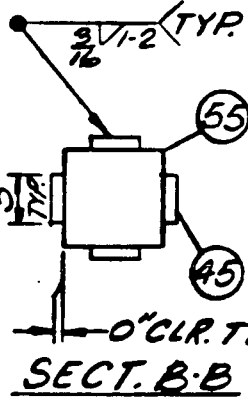
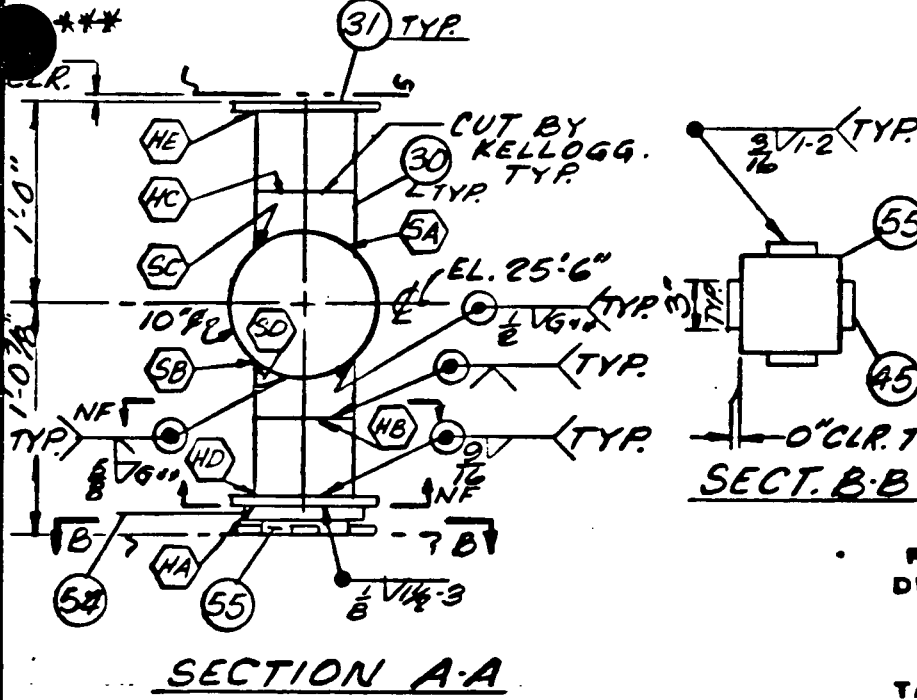
** GRIND ONLY AS NECESSARY
TO INSURE CONCAVITY.

*** NOTE: MIN. TOTAL CLRC. REQD. IS 3/16"

COAT SUPPLEMENTARY
STRUCTURE WITH
NUCLEAR FINISH



P.M.C.-FEO		TYPE 2	
PROJ CL	PIPE A(QC1)	MAX. TEMP	
QUAL CL	STEEL II	650 °F	
DESIGN		X	Y
	M +	—	—
	(FT-LBS)	—	—
	P +	0	502
	(LBS)	0	10283



PROB. NO. 52 FT. NO. 278
SPOOL NO. 2-RC-072-1
ISO 1201-016-1
PIPE 40400.
STEEL

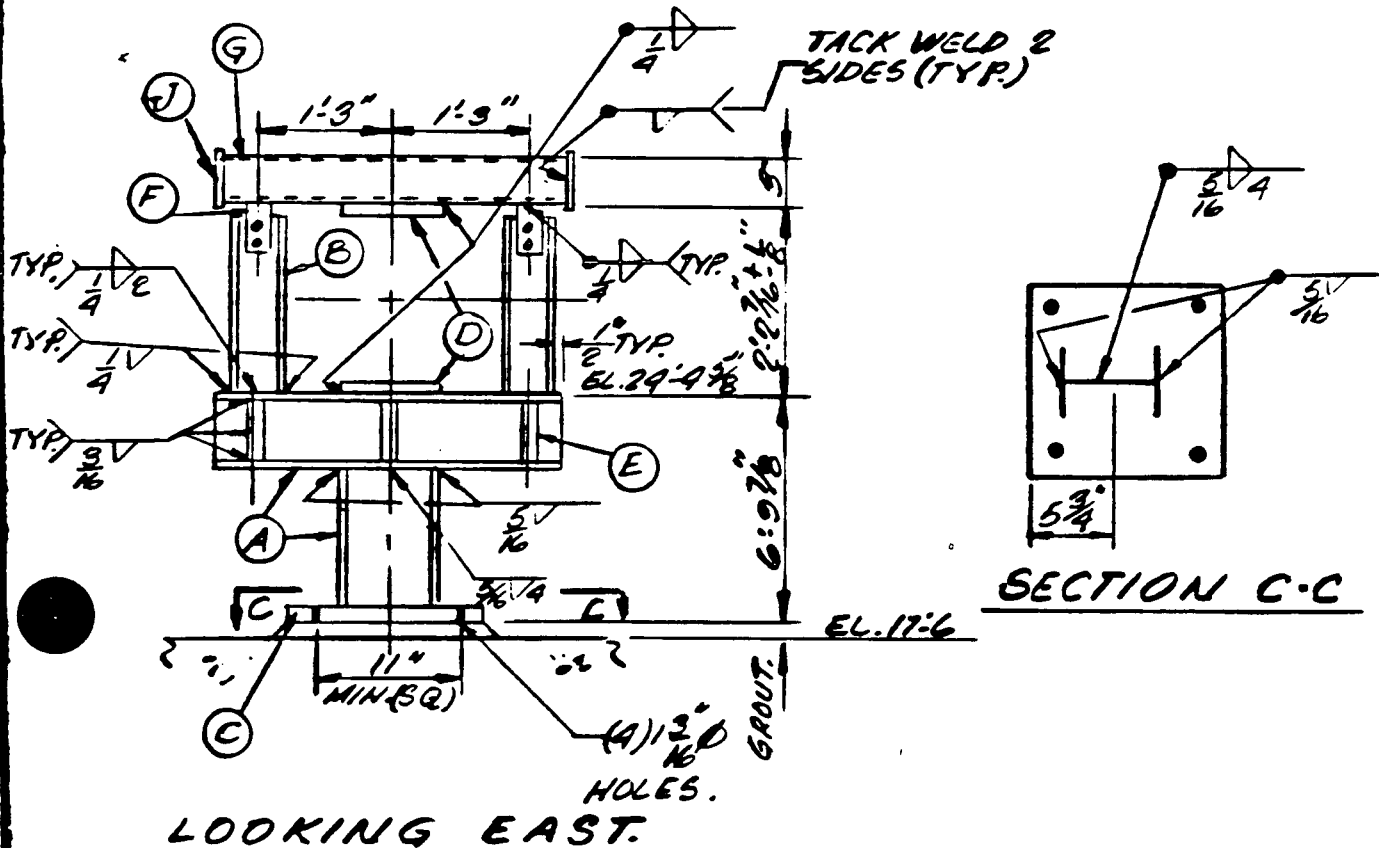
SHT 1 OF 2
TAG NO. 52-RC-072-H-001

3	REDRAWN INC. DCN'S. 01, 02 & 03	2-28-80	DR.	JB	CHK.	MB	E.G.S.	REVISIONS	P.E. Q.A.E.
---	---------------------------------	---------	-----	----	------	----	--------	-----------	-------------

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION					
			FILE	PIPE SUPPORT ASSEMBLY					
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY			LOS ANGELES, CALIF.			

SUS. 2888.

ITEM NO	NO REC'D	PART NO	SIZE	DESCRIPTION	WF AISC	NOTES



1201 SHT 2 OF 2
 S2-RC-072-H001 REV.3

BECHTEL POWER CORPORATION BERTHLE, CALIFORNIA			LG NO	SAN ONOFRE NUCLEAR GENERATING STATION
10079			FILE	PIPE SUPPORT ASSEMBLY
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.		

MAR 26 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4763
DATE 3-13-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 04
12D. DATE MAR 31 1980
12E. SCN NO.

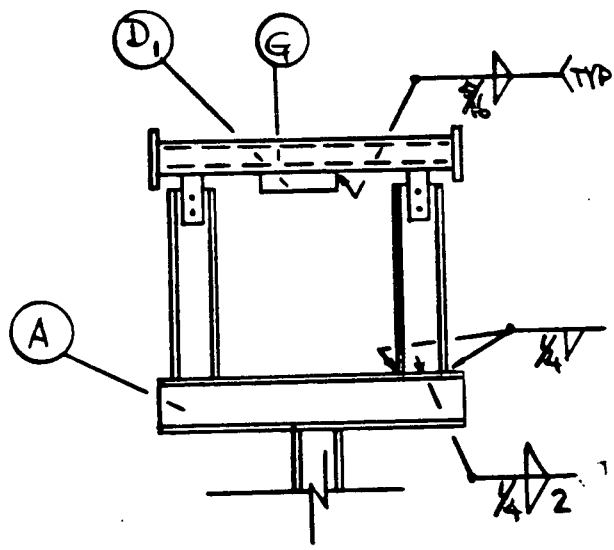
A(001)
JOB NO. 10079 (1.0)
REV. 3 SHEET NO. 206-2

REF. DWG. OR SPEC. 2-RC-072-H-001
5. TITLE PIPE SUPPORT ASSEMBLY
NAME

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION: CHANGE SHOP WELD TO FIELD WELD.
EXCESSIVE CLR THICKER TR REQ'D BY FIELD

8. CHANGE REQUEST/SKETCH



LOOKING EAST (PARTIAL)

BILL OF MAT'L (BY FIELD)

- 1. CHANGE QUANTITY OF ITEM D FROM 2 TO 1.
- 2. ADD ITEM D, TR 1 1/2" X 8 X 8. (REQ'D)
- 3. CHANGE ITEM G FROM T.S. 3 X 6 X 1/2 TO T.S. 6 X 4 X 1/2"

PL. 5152

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE
CIVIL _____	PIPF <u>R.J.S.</u> <u>3-15-80</u>
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QA <u>[Signature]</u> <u>3-17-80</u>

11. APPROVAL OF FCD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE 3-15-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/MLH DATE 3-15-80

REMARKS: **CONVERT TO DCN**

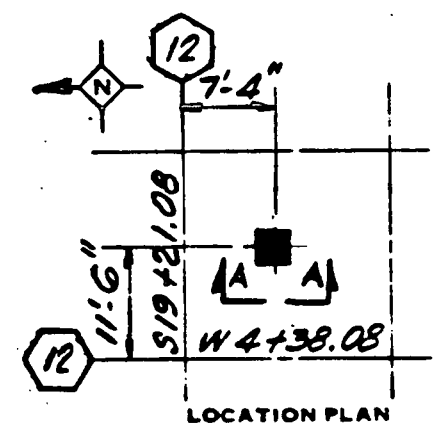
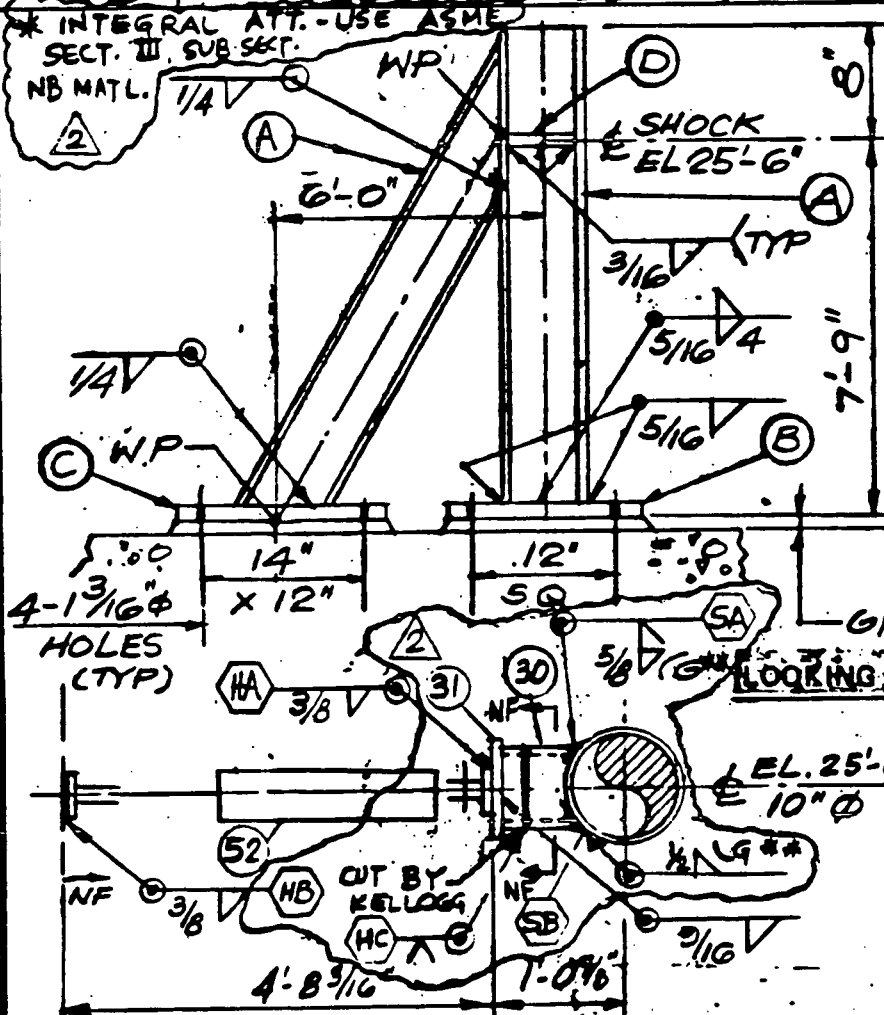
13. QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-17-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE [Signature] DATE 3-28-80

16. ADDITIONAL DISTRIBUTION _____

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
45	4		C.S. BAR 3/16" x 3/16" x 3"				"BY FIELD"
52	1	307	35-G MECH. SHOCK SUPPRESSOR		X		BY GRINNELL
			W/ OPTION 1, C.S. = 4.205"				
			H.S. = 1.795", W = 8.75"				
			LOAD = 29 200				
30	1	-	6" SCH. 120 S.S. DUMMY PIPE		*		BY KELLOGG
31	1	-	12" x 12" x 1/4" C.S. PL		X		BY KELLOGG
A	2		W 8 x 31				SPEC. 5023-206-18
B	1		PL 7 x 16 x 1'-4"				
C	1		PL 3/4 x 16 x 1'-6"				
D	2		3/8" STIFF. PL'S				
	8		US-B-HC-LCSF-175				



EL 17'-6" (IC) AREA NO. 2006-2
 H.P. FL. DESIGN CODE: C
 TYPE: G
 PROJ. CLASS A (QC I)
 MAX. TEMP. 650°F
 OPER. LOAD (LBS.)
 DESIGN LOAD (LBS.) 1.93456 (X-DIS)
 PROB. NO. 52 FT. NO. 7B
 SPOOL NO. 2-RC-072-1
 ISO 1201-016-1
 PIPE 40400
 STEEL

SECT. A-A

** GRIND ONLY IF NECESSARY TO GUARANTEE CONCAVITY.

REF. COAT SUPPLEMENTARY DWGS. STRUCTURE WITH NUCLEAR FINISH

TAG NO. 52-RC-072-H-002

2	INCORPORATED DCNS 1 & 2	2-26-80	RS	H	1201		RIP/SAM/MS
1	INCORP. PER FCR # 12149-5	5-24-78	MS	R.T.MSN			RIP/SAM/MS
0	ISSUED FOR CONSTRUCTION	5-12-77	MS	SLB/RAE/WL/MHW/RT/W			JDY/AR/JEM

REVISIONS			DATE	DR.	CHK.	E.G.S.	CHF. E.	P. E.	Q.A.E.
BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.		SAN ONOFRE NUCLEAR GENERATING STATION				
JOB NO. 10079			FILE		PIPE SUPPORT ASSEMBLY				
DATE			APPROVED		SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 24955
DATE 4-3-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. 03
12D. DATE APR 30 1980
12E. SCN NO.

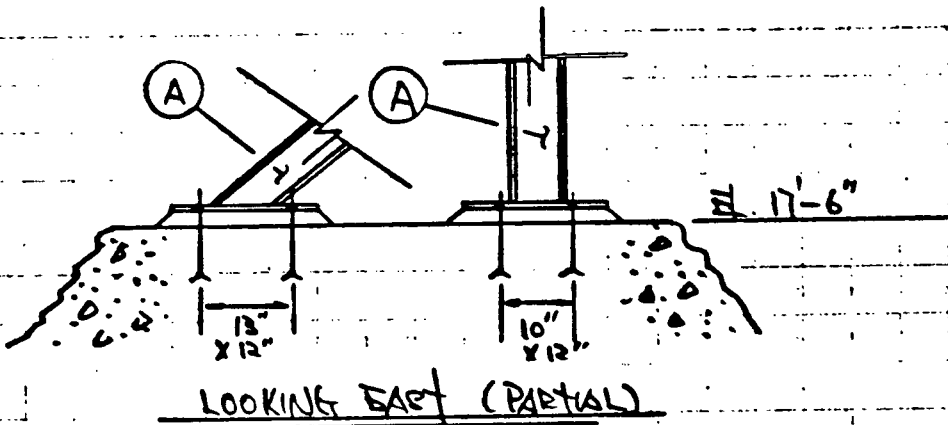
A(OC) 2PPR JOB NO. 10079 (I.C.) 2062

REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
PC-072-A-002 2 PIPE SUPPORT ASSEMBLY

DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION: ROCKBOLTS HIT REBAR

8. CHANGE REQUEST/SKETCH



NO NEW MATL REQ'D

PL5356

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE 4-7-80
ELEC _____ INSTR _____
MECH _____ NUC _____
WELD _____ QA 4-8-80

11. APPROVAL OF FLD DISPOSITION
PREPARED BY Chris King
DATE APR 08 1980
PROJECT FIELD ENGINEER
Louis J. Gandy

12. PROJECT ENGRG APPROVAL: YES NO EGS
P.E. R.L. Rogers/RH DATE 4-7-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. Sheppard DATE 4-5-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE 4-28-80

16. ADDITIONAL DISTRIBUTION _____

X



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-5051
DATE 4-18-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS I
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 02
MAY 13 1980
12E. SCN NO.

JOB NO. 10079
REF. DWG. OR SPEC. SHEET NO. 2 REV. 2 (1.e) 206-3
5. TITLE PIPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY)

7. EXISTING CONDITION: ITEM 45. NOT REV'D

8. CHANGE REQUEST/SKETCH

BILL OF MAT'L
1. DELETE ITEM 45.

PL 5425

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY DATE
CIVIL _____ DATE _____
ELEC _____ DATE _____
MECH _____ DATE _____
WELD _____ DATE _____
PIPE N.S. 4-24-80
INSTR _____
NUC _____
QAE stepped 4-25-80

9. Alan Chi Shing
PREPARED BY
11. APPROVAL OFFIELD DISPOSITION
Darin Henry
PROJECT FIELD ENGINEER
DATE 4-25-80

12. PROJECT ENGRG APPROVAL: YES NO EGS. P.E. R.L. Rogue/RA DATE 4-24-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): stepped DATE 4-25-80

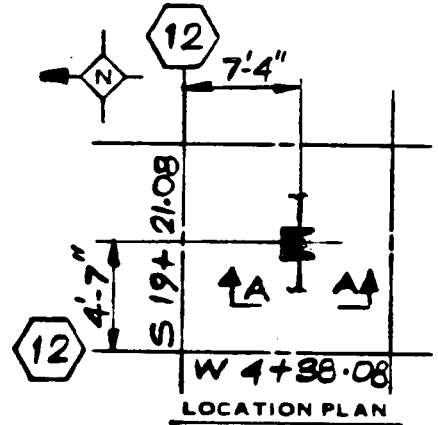
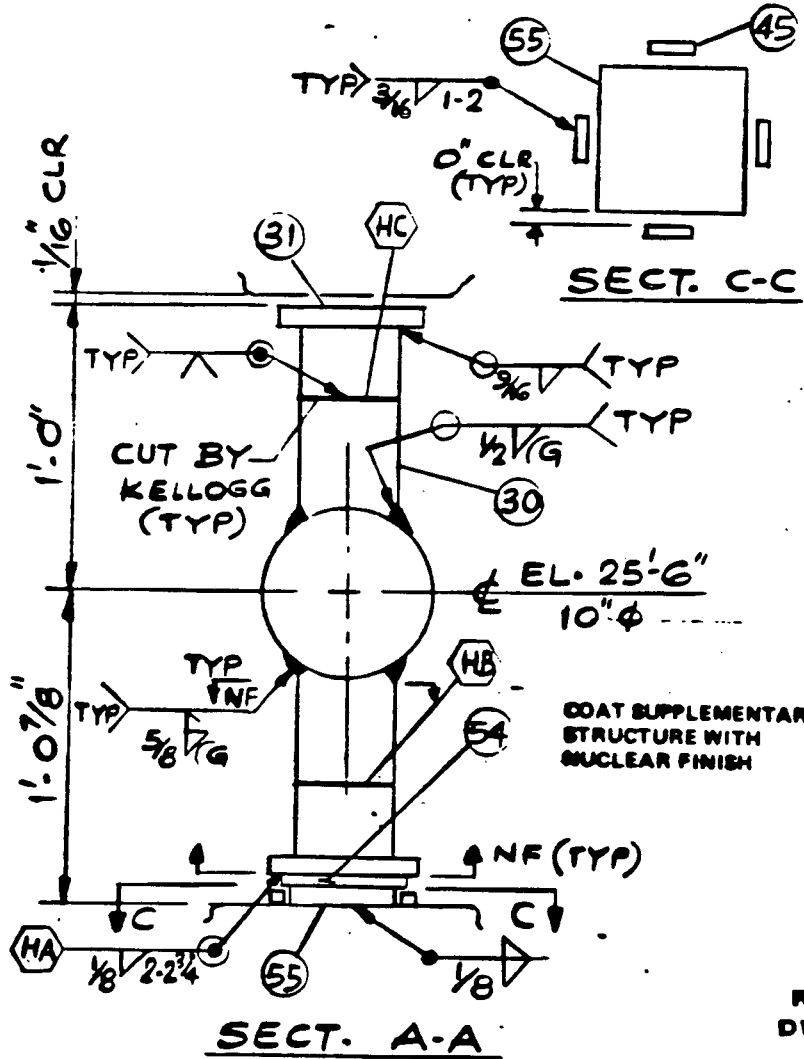
14. SCE ENGINEERING APPROVAL P.E. stepped DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE stepped DATE 5-9-80

16. ADDITIONAL DISTRIBUTION

S.U.S. 2 BH

ITEM NO	NO. REQ'D	PART NO	SIZE	DESCRIPTION	NF	AISC	NOTES
31	2	-	1/2" X 6" X 0'-8" C.S. R		X		BY KELLOGG
30	2	-	6" Ø SCH. 120 S.S. DUMMY PIPE		*		" "
54	1	-	UPPER SLIDE BEARING R				BY FIELD
			10 GA. S.S. 7 1/2" X 7 1/2"				
55	1	-	LOWER SLIDE BEARING R				" "
			BRONZITE 1/4" X 7" X 7"				
45	4	-	3/16" X 3/16" X 3" C.S. BAR				" "
* INTEGRAL ATTACH. USE ASME SECT. III, SUB SECT 'NB' MAT'L							

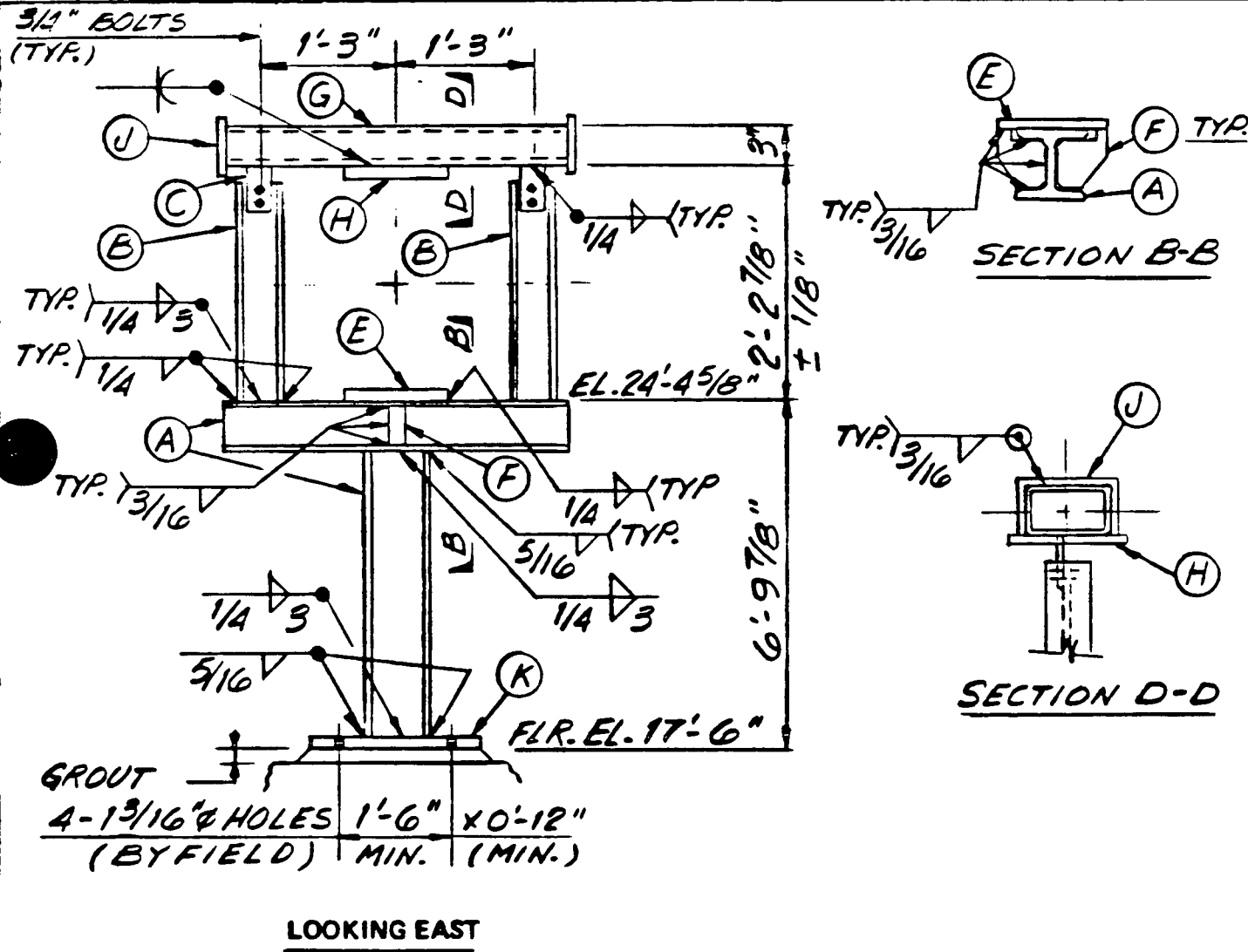


PMC : FEO		TYPE 2	
PROJ CL	PIPE A (O.C.I)	MAX. TEMP	
QUAL CL	STEEL II	650°F	
DESIGN		X	Y
	M +	-	-
	(FT-LBS)	-	-
	P +	0	2777
	(LBS)	0	4536

5 PROB. NO. 52 FT. NO. 83
 SPOOL NO. 2-RC-072-2
 ISO 1201-016-1
 REF. DWGS. PIPE 40400
 STEEL 1201 SHT 1 OF 2
 TAG NO. S2-RC-072-H-003

4 REDRAWN & INC. DCN 122		2280	KG	JB	ST	MB	
REVISIONS		DATE	DR.	CHK.	E.G.S.		P.E. & O.A.E.
BECHTEL POWER CORPORATION BORWALK, CALIFORNIA		J.O. NO. SAN ONOFRE NUCLEAR GENERATING STATION					
JOB NO. 10079		FILE PIPE SUPPORT ASSEMBLY					
DATE		SOUTHERN CALIFORNIA EDISON COMPANY					
APPROVED		SCALE: NTS LOS ANGELES, CALIF.					

ITEM NO	DESCRIPTION	QTY	UNIT	REMARKS
A	W6X25	2		SPEC. S023-206-1E
B	W4X13	2		
C	R 5/8 X 2 1/2 X 0'-6"	2		
D	R 1/2 X 8 X 0'-8"	1		
E	5/8" GUSSET PLATE	2		
G	T.S. 3X6X.50	1		
H	R 1/2 X 8 X 0'-8"	1		
J	R 1/4 X 4 X 0'-7"	2		BY FIELD
K	R 3/4 X 16 1/2 X 1'-10"	1		
	3/4" Ø HEX BOLTS	4		
	US-8-HC-LCSF-175	4		

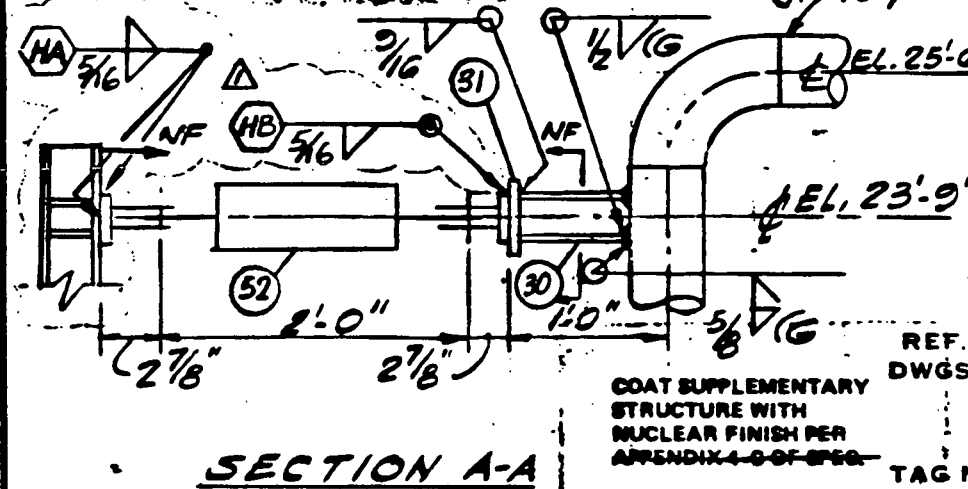
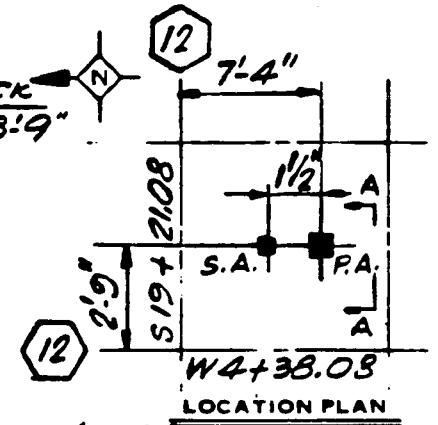
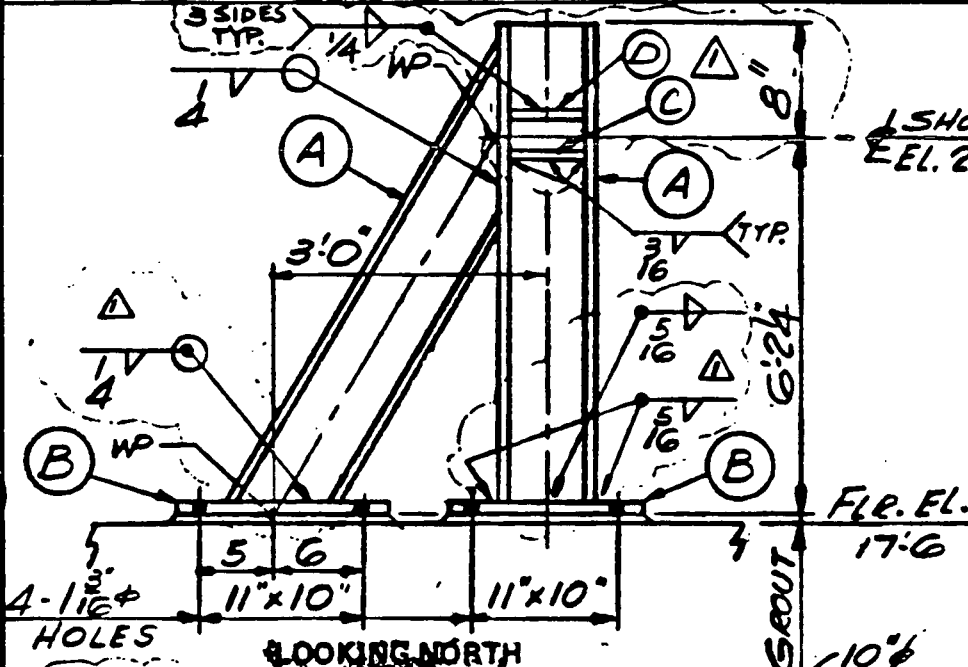


1201 SHT 2 OF 2
S2-RC-072-H-003 REV.4

BECHTEL POWER CORPORATION BORNEAL, CALIFORNIA			A & NO SAN ONOFRE NUCLEAR GENERATING STATION
JOB NO. 10079			FILE PIPE SUPPORT ASSEMBLY
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON CO. SCALE NTS LOS ANGELES	

SUS - 2 BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	ALSC	NOTES	
32	1	306	10-6 MECH. SHOCK SUPPRESSOR	X			BY GRINNELL	
			W/ OPTION 1 C.S. = 3.83"					
			H.S. = 2.17					
30	1	-	6" SCH. 120 S.S. DUMMY PIPE	*			BY KELLOGG	
31	1	-	8" x 8" x 1/4" C.S. FL	X			BY KELLOGG	
			* INTEGRAL ATTACH. USE ASME SUBJECT. "NB" MAT'L.					
A	2	-	WG x 25				SPEC.	
B	2	-	FL - 1" x 14 x 1/3"				5023-206-18	
C	2	-	3/8" STIFF. FL					
D	2	-	3/8" STIFF. FL				BY FIELD.	
8	-	-	US-8-HC-LCSF-175				"BY FIELD"	



(JC) AREA NO. 2006-2
 PMC-FED Δ
 TYPE: G
 PROJ. CLASS A(QC1)
 MAX. TEMP. 650°F
 OPER. LOAD (LBS.) -
 DESIGN LOAD (LBS.) P₂ = ±5151
 5) PROB. NO. 52 PT. NO. 83
 SPOOL NO. 2-RC-072-2
 ISO. 1201-016-1
 PIPE 40400
 STEEL -
 TAG NO. S2-RC-072-H-004

NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	Q. A. E.
1	INCORP. DCN 1, 2 & 3	2-21-80	OT	Y. G.	RF			
0	ISSUED FOR CONSTRUCTION	5-17-77						

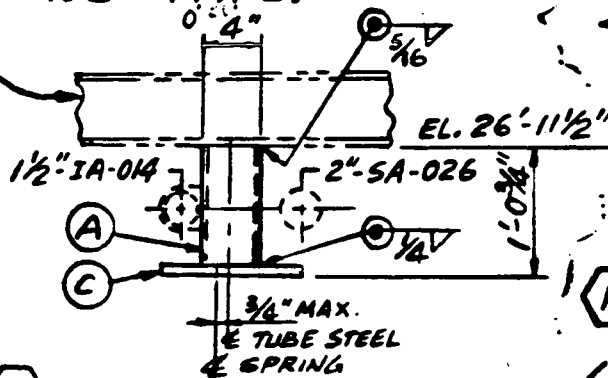
BECHTEL POWER CORPORATION NORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
JOB NO. 10079		FILE	PIPE SUPPORT ASSEMBLY	
DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.		

CALC. NO. C-270-3.0

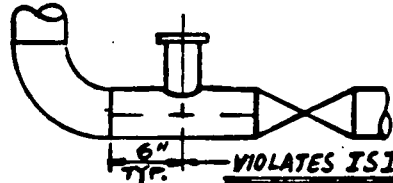
ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	BY	DATE	NOTES
1	2	66	1 1/8"	BEAM ATTACHMENT	X		BY FIELD
2A	1	290	1 1/8"	WELDLESS EYENUT W/R.H. TAP	X		BY GRINNELL
7A	2	-	1 1/8"	HEX NUT	X		"
9A	1	140N	1 1/8" φ	ROD W/R.H.T. BOTH ENDS	X	3'-7" LG. WI	7" TBE BY FIELD
19A	1	B.268	14	TYPE "B" VARIABLE SPRING	X	HL-4065*CL-3873*	BY GRINNELL
				MVT. 1/4" ↓ W/TS			
30	1	-	6" φ	SCH. 120 S.S. DUMMY PIPE	X		BY KELLOGG
31	1	-	8" x 8" x 1/4"	C.S. PL	X		BY KELLOGG
A	1	-	T.S. 6 x 4 x 1/2 x 1'-0"		X		BY FIELD
C	1	-	PL 3/4 x 8 x 0'-8"		X		U

* INTEGRAL ATTACH. USE ASME SECTION III
SUBJECT. "NB" MAT'L.

EXIST. W21 x 142

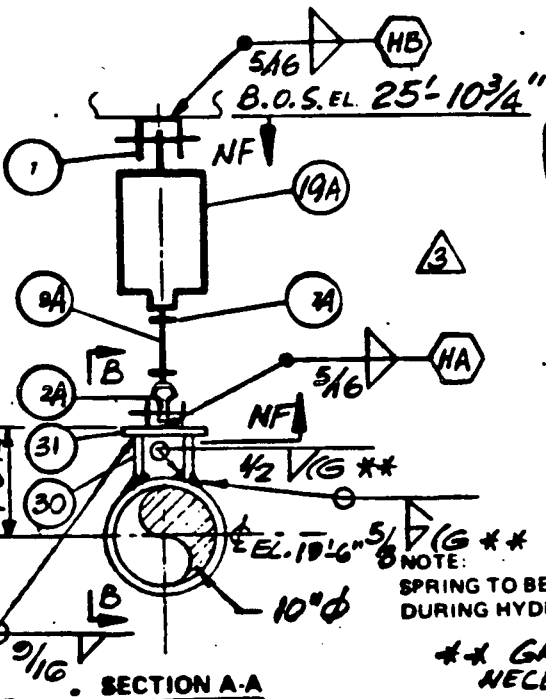


LOOKING EAST



SECTION B-B

COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH.



SECTION A-A

** GRIND ONLY AS NECESSARY TO INSURE CONCAVITY

LOCATION PLAN
(1C) AREA NO. 2C06-2

PMC-FED STEEL II
TYPE: 5

PROJ. CLASS. A (QC 1)

MAX. TEMP. 650 °F

OPER. LOAD (LBS.) SEE ITEM 19

DESIGN LOAD (LBS) 4065

PROB. NO. 52 PT. NO. 86

SPOOL NO. 2-RC-072-2

ISO 1201-016-1

PIPE 40400

STEEL

TAG NO. 52-RC-072-H-005

2A1

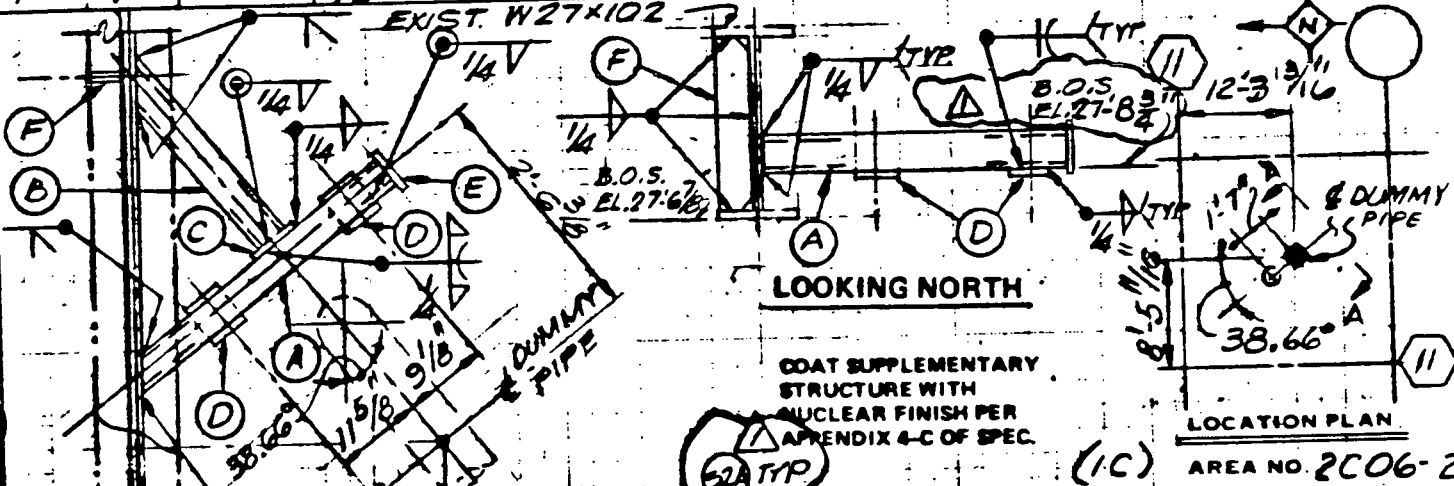
NO.	REVISIONS	DATE	DR.	CHK.	EGS.	CHF. E.	P. E.	G.A.E.
2	ADDED BOTTOM OF EXIST W21 x 142	10-10-71	AN	RM	HH	1201	-	JDH/OK/TT
3	INCORP. DCN 1, 2 & 3	2-26-80	GT	CH	KG	PL	MB	RL/AM/TJS
0	ISSUED FOR CONSTRUCTION	5-12-71	W/EL	BP/AR	CV/LM	HSN	PT.	JDH/OK/JJA

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
		FILE	PIPE SUPPORT ASSEMBLY				
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

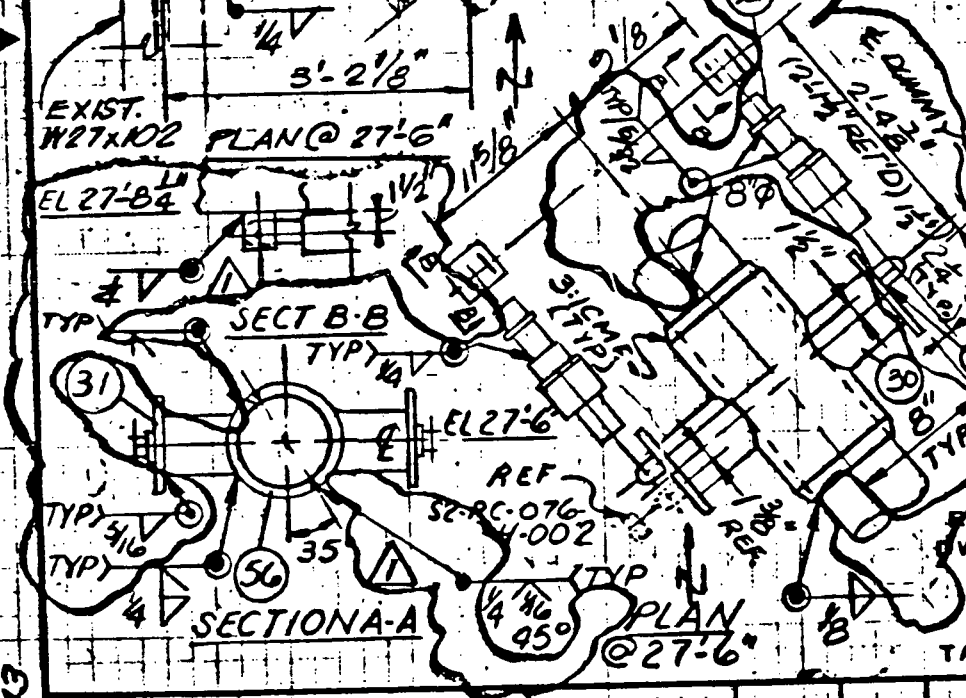
SUS-2BBA

SUS-2 BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	2	-	4" ϕ SCH 40 S	DUMMY PIPE S.S.			SPEC
31	2	-	R 3/4 x 7" x 0-7"	CS END PLATE			5023-409-23
56	2	-	3/8 x 10"	S.S. CURVED PLATE			
52A	2	-	PSA 3-5"	STROKE PIN 1811023-26 SHOCK ARRESTOR KIT, CPS = 3 3/8", HPS = 1 5/8" LOAD = 36.66# FA.			BY PSC
A	7	-	T.S. 4 x 4 x .375				
B	1	-	T.S. 4 x 4 x .375			X	SPEC
C	1	-	R 1/2 x 5 x 0-5"				5023-206-18
D	2	-	R 1/2 x 5 1/2 x 0-5 1/2"				
E	1	-	R 1/4 x 5 x 0-5"				
F	1	-	3/8" STIFF. R				



PMC: LLO		TYPE 6	
PROJ CL	PIPE J (QCIII)	MAX. TEMP 220°F	
QUAL CL	STEEL II	X	Z
DESIGN	M +	-	-
	(FT-LBS)	-	-
	P +	3162	2580
	(LBS)	3162	2580
PROB. NO. 52		PT. NO. 176	
POOL NO. 2-RC-076-1		ISO 1201-076-1	
PIPE 40900		STEEL 23211	



NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	QAE
1	SNUBBER VENDOR CHANGED	0-30-79	JL	AG	Qm NB	-	RLH/AIS
0	ISSUED FOR CONSTRUCTION	7-11-79	GC	YL	Qm NB	-	RLH/AIS

BECHTEL POWER CORPORATION
 NORWALK, CALIFORNIA

J.O. NO. SAN ONOFRE NUCLEAR GENERATING STATION
 FILE PIPE SUPPORT ASSEMBLY

SOUTHERN CALIFORNIA EDISON COMPANY
 LOS ANGELES, CALIF.

JOB NO. DATE APPROVED

MAR 1 1980



SAN ONOFRE NUCLEAR GENERATING STATION

UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4837
DATE 3-20-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS III

12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 02

12D. DATE APR 8 1980

12E. SCN NO.

J(QC III) (U.C.)
QBHA JOB NO. 10079 2C06-2

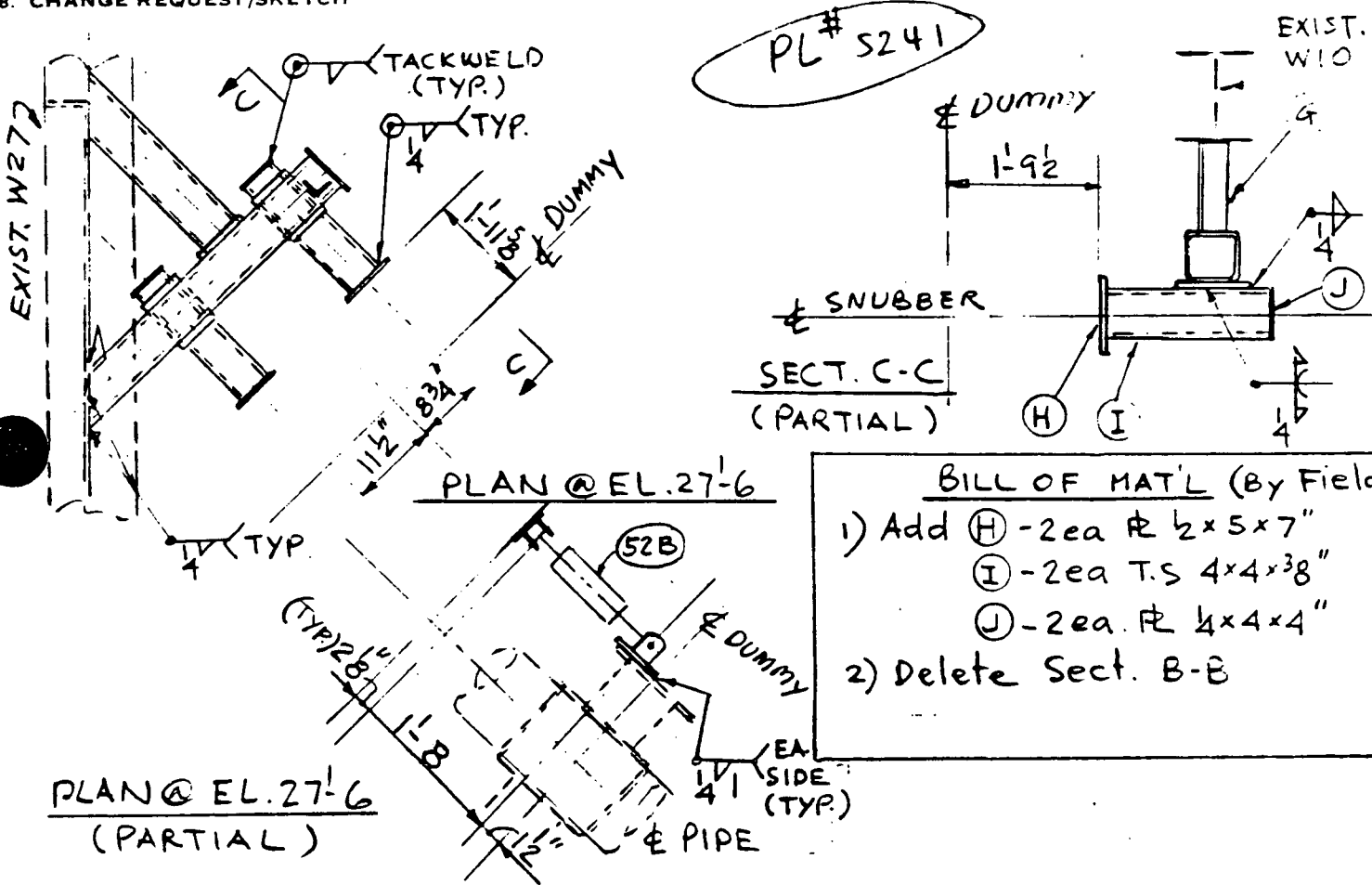
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-076-H-001 1 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Need to revise Framing

8. CHANGE REQUEST/SKETCH



PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE	DATE
CIVIL		INSTR	
ELEC		NUC	
MECH		QAE	
WELD			

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
Dennis J. [Signature]
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/PLH DATE 3-21-80

REMARKS: **CONVERT TO DCN**

13. QUALITY ASSURANCE ENGINEER (FIELD): N/A DATE 3-21-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

MAR 26 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-4736
DATE 3/12/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS III
12B. SPEC ADDEND. NO.

12C. DCN SUBNO. DL
12D. DATE MAR 31 1980
12E. SCN NO.

J(QC III)
26HA JOB NO. 10079 (I.C.)
206-2

4. REF. DWG. OR SPEC. S2-RC-076-H-001 SHEET NO. 1 REV. 1 5. TITLE Pipe Support Assembly

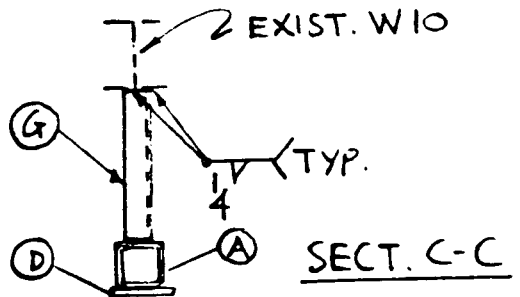
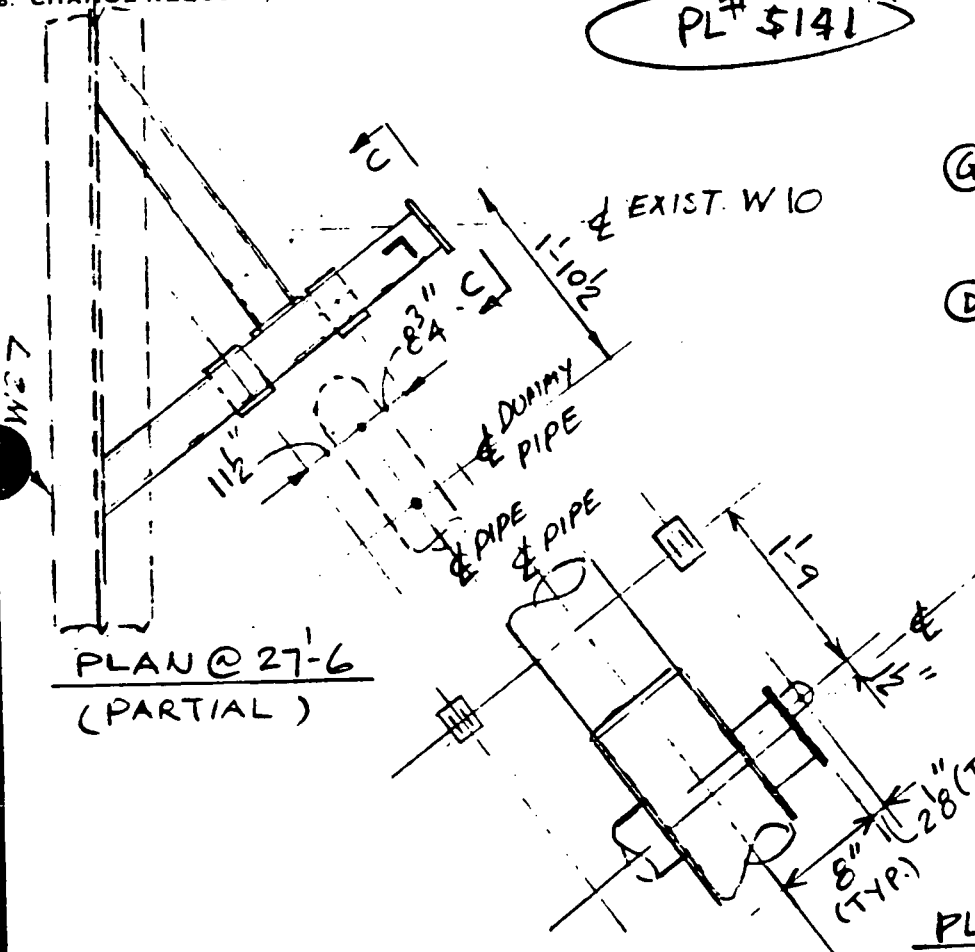
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Item (52A) Suppressor not in stock

8. CHANGE REQUEST/SKETCH

PL# 5141



BILL OF MATERIAL (By Field)

- 1) Delete Item (52A)
- 2) Add Item (52B) use Mech Shock Arrestor retag 2-aa from S2-RC-147-H-001 - Fig. 306 No 3-5" stroke CPS=338, HPS=158 Load=3666# ea.
- 3) Add item (G) 1-L 3x3x1/4

PLAN @ 27-6 (PARTIAL)

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE
CIVIL		
ELEC		
MECH		
WELD		
		INSTR
		NUC
		QA

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD/ DISPOSITION
P. Christman
PROJECT FIELD ENGINEER
DATE 3-15-80

12. PROJECT ENGRG APPROVAL: YES NO EGS P.E. P.L. Rogers/Bom DATE 3-14-80

REMARKS CONVERT TO PLAN

13. QUALITY ASSURANCE ENGINEER (FIELD): g.w. sleepman DATE 3-18-80

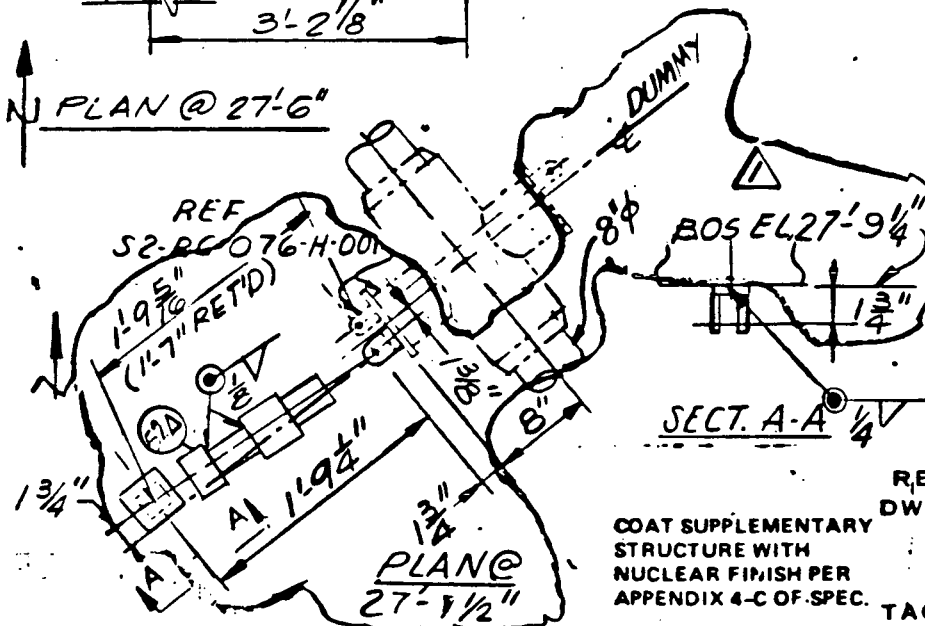
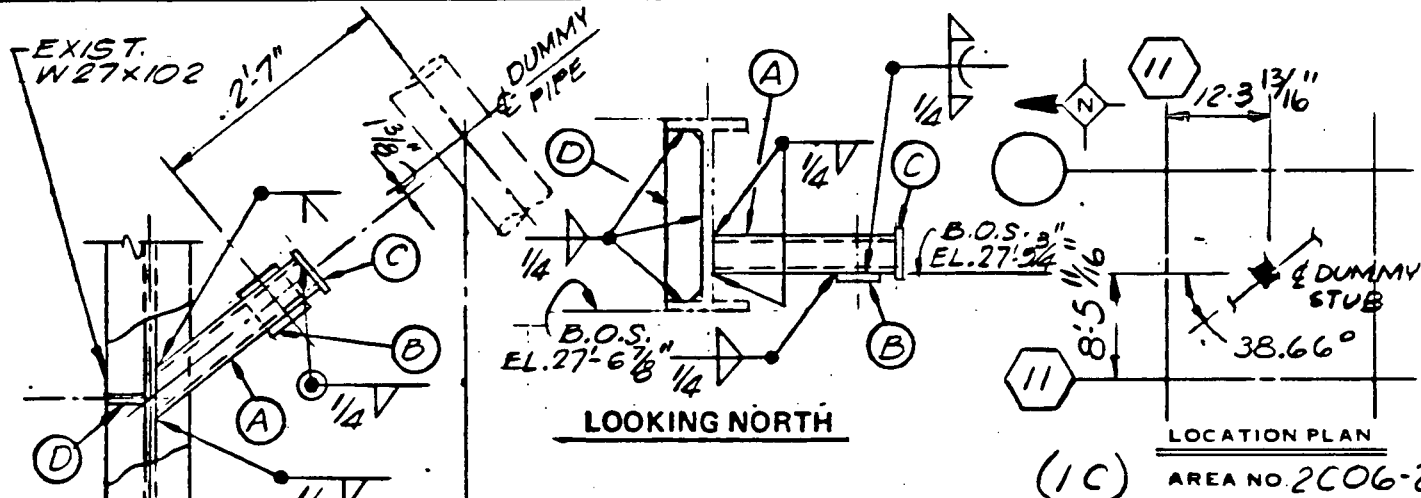
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

ITEM NO	NO REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
52A	1			PSA 1-4" STROKE PIN 1811008-19			BY PSC
				SHOCK ARRESTOR KIT, NON-NUCLEAR CPS = 2 5/16", HPS = 1 1/16" LOAD = 147#			
A	1		TS 4 x 4 x .375	}			SPEC. S023-206-18
B	1		1/2 x 5 1/2 x 0.5 1/2"				
C	1		1/4 x 5 x 0.5"				
D	1		3/8" STIFF. PL				

SUS:2BHA



PMC:LLO		TYPE 6	
PROJ CL	PIPE J(QCIII)	MAX. TEMP	
QUAL CL	STEEL II	220°F	
DESIGN		X	Y
	M +	-	-
	(FT-LBS)	-	-
	P +	885	1107
	(LBS)	885	1107

PROB. NO. 52 PT. NO. 176
 SPOOL NO. 2-RC-076-1
 ISO. 1201-076-1
 PIPE 40400
 STEEL 23211
 TAG NO. S2-RC-076-H-002

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	Q.A.E.
1	SNUBBER VENDOR CHANGED	11-9-79	JL	AG	Can MB	ent/sus	Michael P. G
0	ISSUED FOR CONSTRUCTION	7-11-79	JL	AG	Can MB		Michael P. G

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS				LOS ANGELES, CALIF.

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 524839
DATE 3-19-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS III
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 02
12D. DATE APR 8 1980
12E. SCN NO.

J(QCT III)
ZBHA JOB NO. 10079 (I.C.)
2C06-2

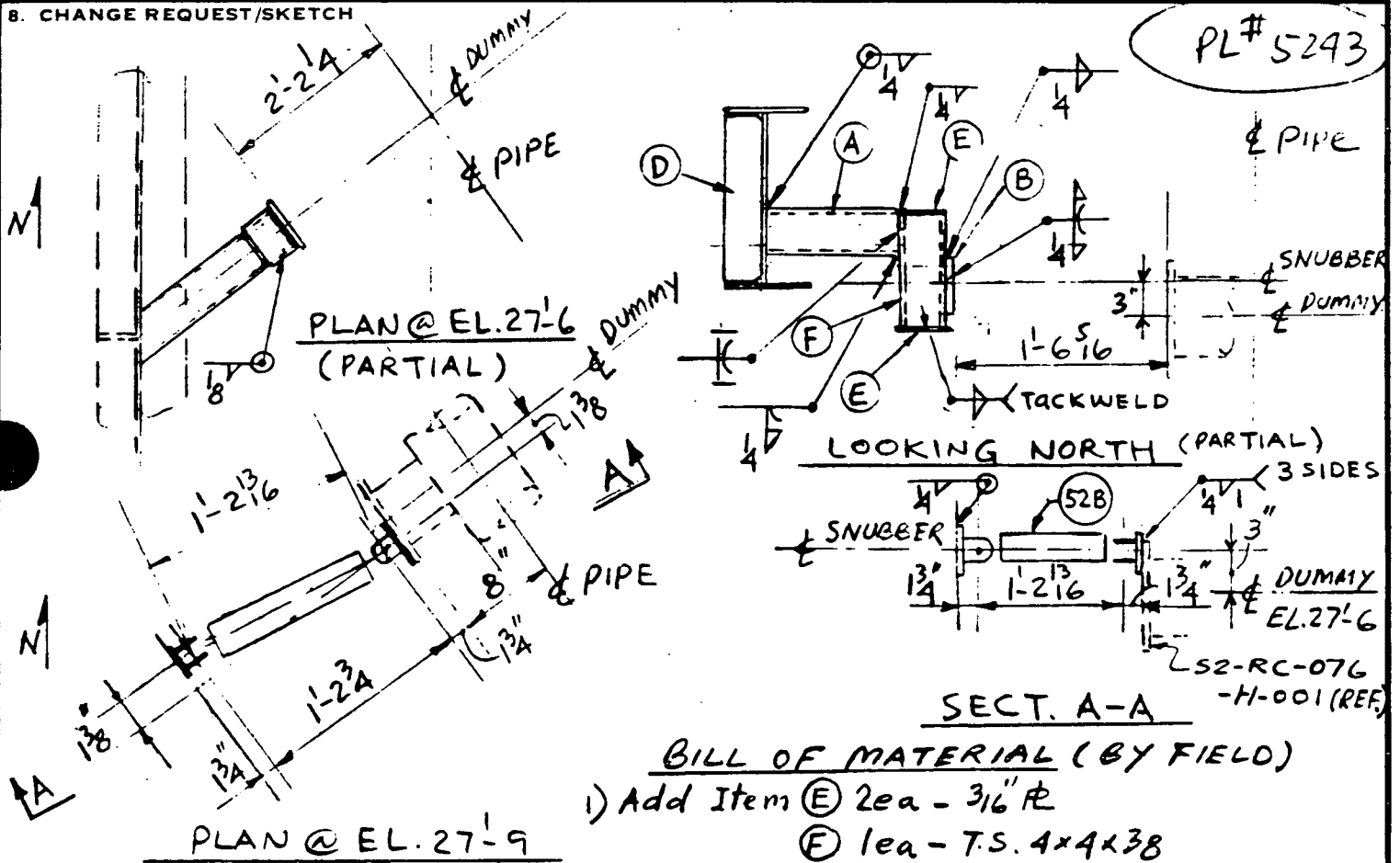
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-076-H-002 1 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Need to revise Support Framing

8. CHANGE REQUEST/SKETCH



PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPF	DATE
CIVIL _____	_____	<u>N.T.S.</u>	<u>3-21-80</u>
ELEC _____	_____	INSTR _____	_____
MECH _____	_____	NUC _____	_____
WELD _____	_____	QAE _____	_____

9. P. Tannirath
PREPARED BY
11. APPROVAL OF FIELD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: CONVERT TO DCN
P.E. R.L. Rogers/11th DATE 3-21-80

13. QUALITY ASSURANCE ENGINEER (FIELD): N/A-108 DATE 3-21-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

MAR 26 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3
FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4733
DATE 3/12/80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS III
12B. SPEC ADDEND NO.

12C. DCN SUB NO. 01
12D. DATE MAR 31 1980
12E. SCN NO.

J(CQC II)
26HA JOB NO. 10079 (I.C.)
2C06-2

4. REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-076-H-002 1 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Item (S2A) suppressor not in stock

8. CHANGE REQUEST/SKETCH

PL # 5138

BILL OF MATERIAL

1. DELETE ITEM #S2A
2. ADD ITEM #S2B - 1 REQD - No. 1 - 4" ST-PIPE
MECHANICAL STOCK APPROX. 2
CPS = 2 5/16", HPS = 1 1/16" LEAS = 14 1/2"
USE SURPLUS NUMBER - S2-RC-076-H-002?

NOTE: IN PLAN @ 27'-1 1/2" CHANGE "S2A" TO S2B

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE	INSTR	NUC	QAE
CIVIL					
ELEC					
MECH					
WELD					

M.S. 3-15-80

9. P. Tamirat
PREPARED BY

11. APPROVAL OF FLD DISPOSITION
P. Christman
PROJECT FIELD ENGINEER
DATE 3-15-80

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: CONVERT TO DCN
P.E. R.L. Rogers/KH DATE 3-15-80

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. [Signature] DATE 3-15-80

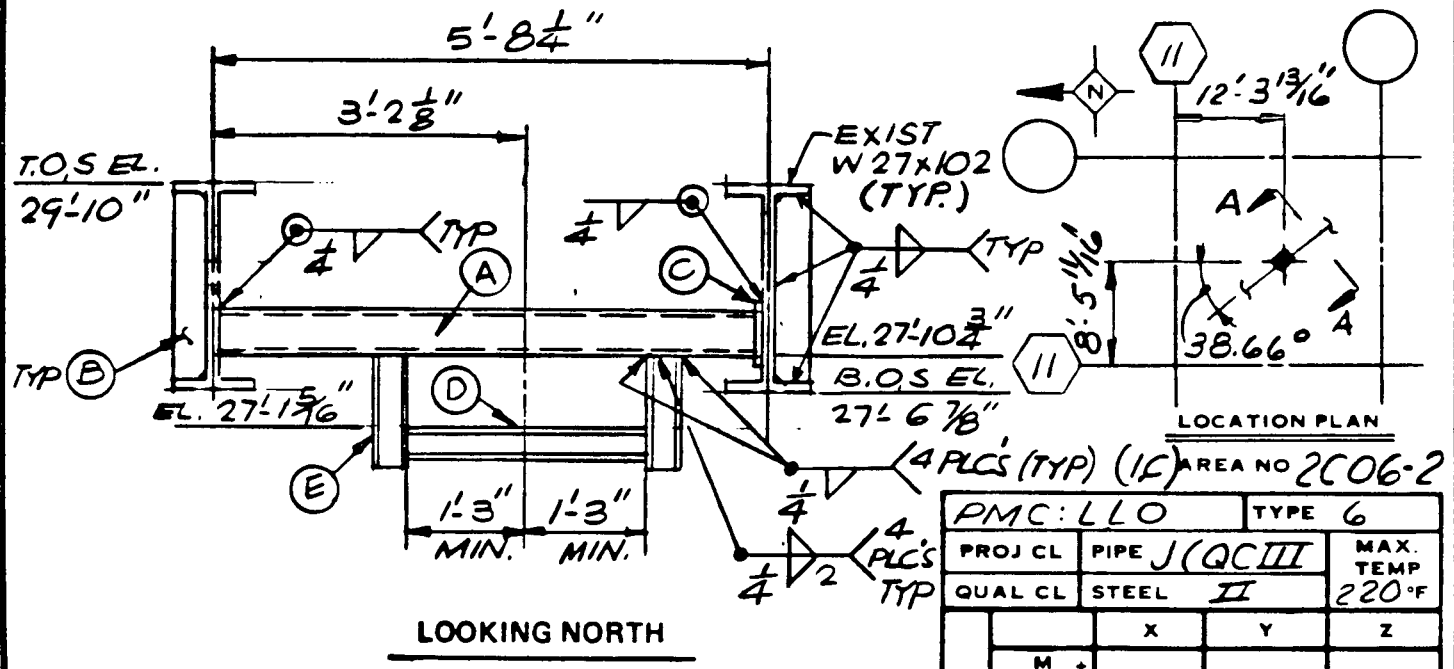
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

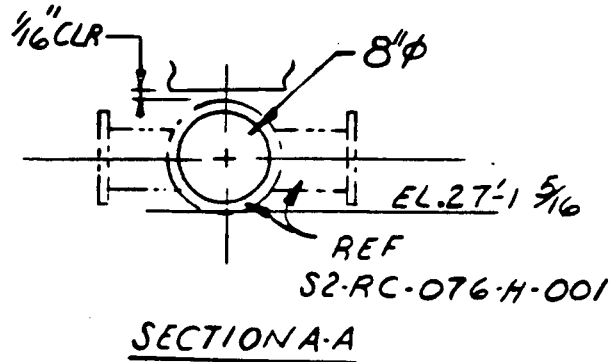
SUS: 2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
A	1		TS 6x6x.375x 5'-9"	}		X	
B	2		3/8" STIFF. PL		X		
C	1		E 1/2 x 7 x OL-7"		X	SPEC	
D	1		W4x13		X	5023-206-18	
E	2		W4x13		X		



LOOKING NORTH

PMC: LLO		TYPE 6	
PROJ CL	PIPE J(QCIII)	MAX. TEMP	
QUAL CL	STEEL II	220°F	
DESIGN		X	Y
	M +	—	—
	(FT-LBS)	—	—
	P +	6173	—
	(LBS)	2563	—



COAT SUPPLEMENTARY STRUCTURE WITH NUCLEAR FINISH PER APPENDIX 4-C OF SPEC.

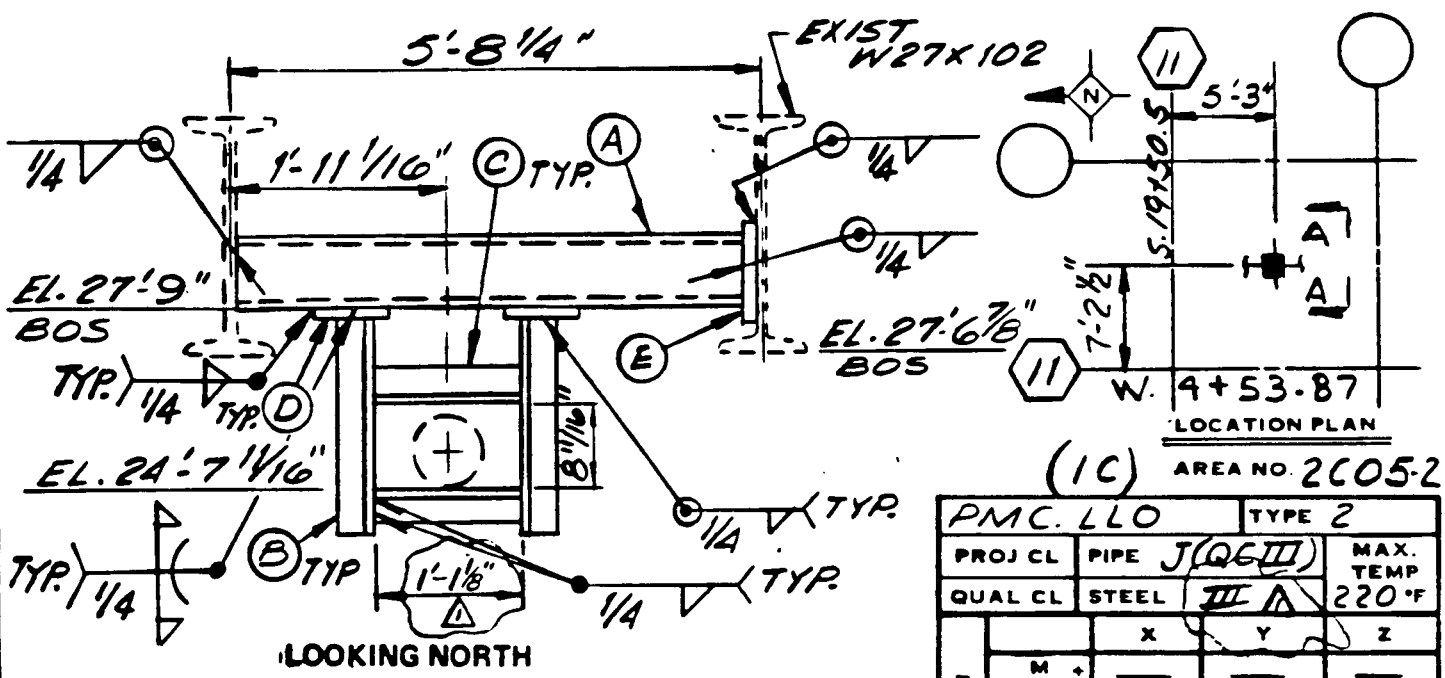
PROB. NO. 52 PT. NO. 176
 SPOOL NO. 2-RC-076-1
 ISO 1201-076-1
 REF. DWGS. PIPE 40400
 STEEL 23211

TAG NO. S2-RC-076-H-003

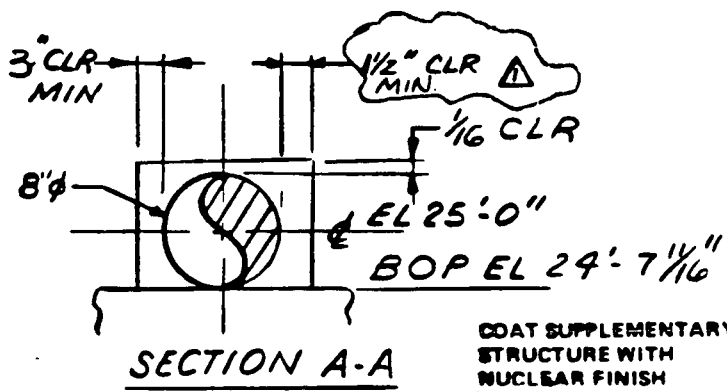
0 ISSUED FOR CONSTRUCTION		7-11-79	JM	PA	PA	PA	PA	PA
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	QAE	
BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION				
			FILE	PIPE SUPPORT ASSEMBLY				
JOB NO.	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.					
10079								

SUS:2BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
A	1		TS 4x4x 1/2				SPEC
B	2		L 3x3x 5/8x3'-6"				5029-206-1B
C	2		L 3x3x 5/8				
D	2		R 3/8x5x0'-5"				
E	1		R 1/2x5x0'-5"				



PMC. LLO		TYPE 2	
PROJ CL	PIPE J(Q6II)	MAX. TEMP	
QUAL CL	STEEL III A	220°F	
DESIGN		X	Y
	M +	—	—
	(FT-LBS)	—	—
	P +	⊕ 500	⊕
	(LBS)	⊕ 776	⊕



[S] PROB. NO. 52 PT. NO. 183
 SPOOL NO. 2-RC-076-1
 ISO. 1201-076-1
 REF. DWGS. PIPE 40400
 STEEL 23211

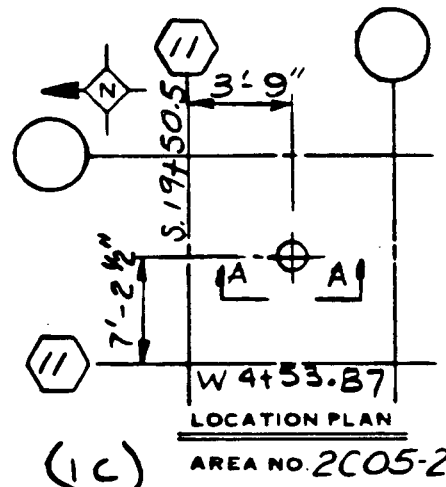
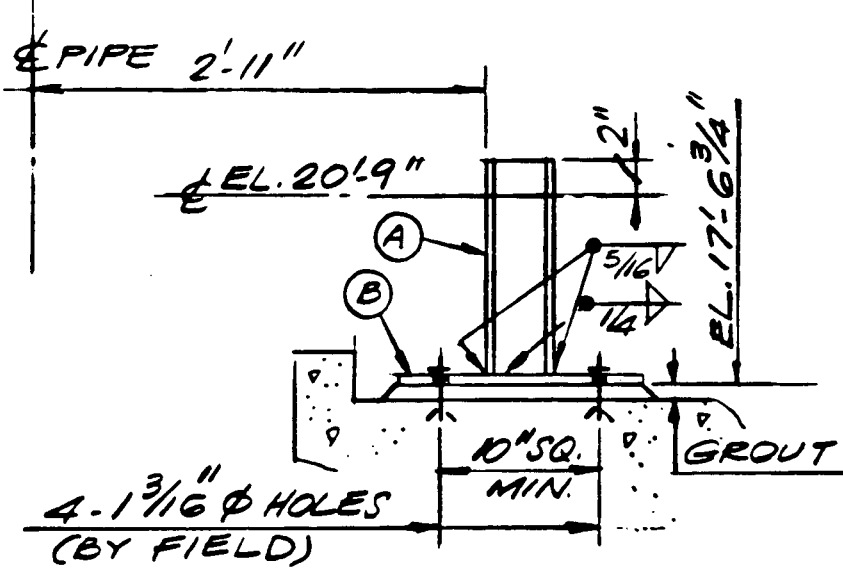
TAG NO. S2-RC-076-H-004

1	INCORPORATED DCN 01	2-26-80	JB	KG	RL HB	—	RIP/MA/CS
0	ISSUED FOR CONSTRUCTION	7-10-79	IM/EX	PMY/LL	J. P.A. JS/HB	—	RG/CS/CZ
NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.		P.E. QAE

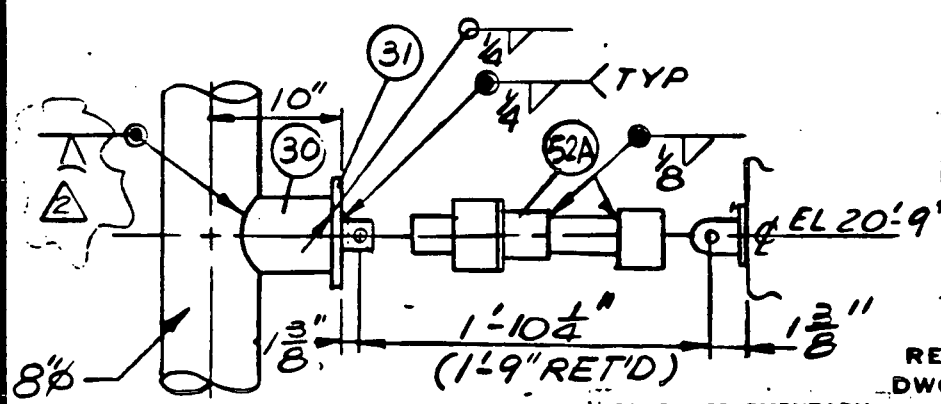
BECHTEL POWER CORPORATION MORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS				
			LOS ANGELES, CALIF.				

SUS: BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	4"Ø SCH. 40S DUMMY PIPE S.S.				SPEC
31	1	-	R 1/2 x 6 x 0'-6" CS END PLATE				S023-409-23
52A	1		PSA 1/4-4" STROKE PIN 1811002-21				BY PSC
			SHOCK ARRESTOR KIT, CPS=1 1/4"				
			H.P.S.=3 1/2", LOAD=32#				
A	1		W4 x 13 x 3'-5"	}		X	SPEC
B	1		R 1 x 22 x 1'-10"			X	S023-206-18
	4		1" Ø CONC. FASTENERS				BY FIELD



LOOKING EAST



PMC: LLO		TYPE 2	
PROJ CL	PIPE J (QCT III)	MAX. TEMP 220°F	
QUAL CL	STEEL III		
DESIGN		X	Y 2
	M +	-	-
	(FT-LBS)	-	-
	P +	500	Ø
	(LBS)	500	Ø

PROB. NO. 52 PT. NO. 186
 SPOOL NO. 2-RC-076-1
 ISO 1201-076-1
 PIPE 40400
 STEEL 23110

TAG NO. S2-RC-076-H-005

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	QAE
2	INCORPORATED DCN 01	2-26-80	JB	KG	RE HB	-	RLP/AM
1	SNUBBER VENDOR CHANGED	10-30-79	JL	AG	RE HB	-	REHE/MS
0	ISSUED FOR CONSTRUCTION	7-10-79	MS	GC	RE HB	-	REHE/MS

BECHTEL POWER CORPORATION NORWALK, CALIFORNIA			J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION			
			FILE	PIPE SUPPORT ASSEMBLY			
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY SCALE: NTS LOS ANGELES, CALIF.				

3445

MAR 31 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. S-4840
DATE 3-20-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 02
12D. DATE APR 8 1980
12E. SCN NO.

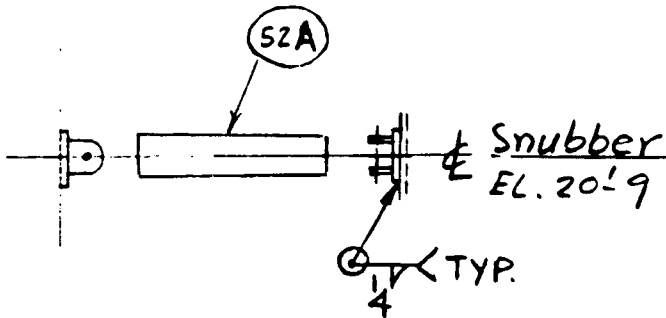
J(QC II) (I.C)
ZBHA JOB NO. 10079 2C05-2
REF. DWG. OR SPEC. SHEET NO. REV. 5. TITLE
S2-RC-076-H-005 2 Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Need to rotate snubber bracket

8. CHANGE REQUEST/SKETCH



PL# 5244

SECT. A-A
(PARTIAL)

No new Material Req'd

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE
CIVIL _____	PIPE <u>M.S.</u> <u>3-21-80</u>
ELEC _____	INSTR _____
MECH _____	NUC _____
WELD _____	QAE _____

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
[Signature]
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers/RA DATE 3-21-80

REMARKS: **CONVERT TO DCN**


13. QUALITY ASSURANCE ENGINEER (FIELD): N/A DATE 3-21-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

MAR 31 1980

 SAN ONOFRE NUCLEAR GENERATING STATION UNITS 2 & 3 FIELD CHANGE REQUEST/DCN/SCN	1. FCR NO. <u>S-4715</u>	12A. QUALITY CLASS <u>III</u>	12C. DCN SUB NO. <u>03</u>
	DATE <u>3-8-80</u>	12B. SPEC ADDEND. NO.	APR 8 1980
	2. PAGE <u>1</u> OF <u>1</u>	3. UNIT NO. <u>2</u>	12E. SCN NO.

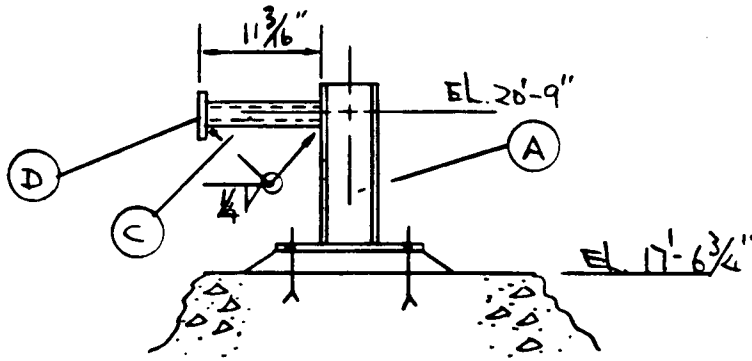
(I.P.)
 (J. Q. G.)
 (R. H. A.)
 JOB NO. 10079 REF. DWG. OR SPEC. S2-DC-016-A-005 SHEET NO. 12 5. TITLE RPE SUPPORT ASSEMBLY

6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

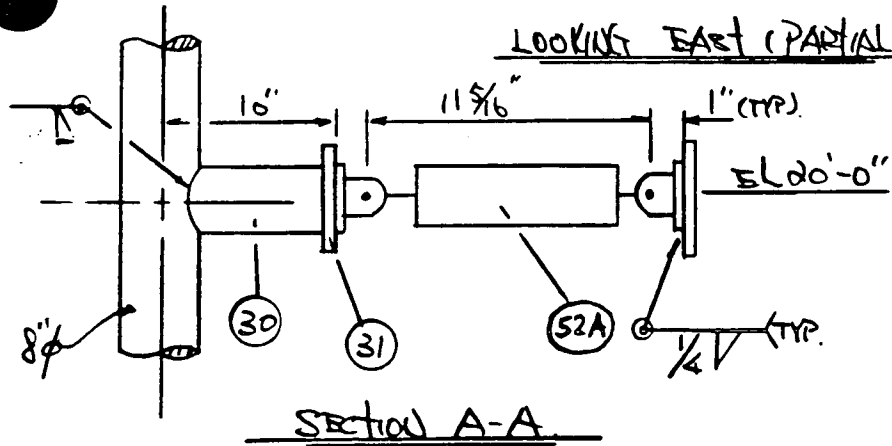
7. EXISTING CONDITION: SUPPRESSOR WORKING IN FIELD.

8. CHANGE REQUEST/SKETCH

PL 5113



LOOKING EAST (PARTIAL)



SECTION A-A

Bill of Mat'l (by Field)

- Delete Item (52)
- Add (52A) 1 ea Fig 306 4-4" stroke Mech. arrestor CPS = 14
HPS = 3 1/2
Load = 32#
(retag from S3-SI-077-H-002)
- Add item (C) 1-T.S. 3"x3"x3/16"
- Add item (D) 1-PL 1/2"x5"x5"

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PREPARED BY
CIVIL _____	_____	<u>Steve Chi King</u>
ELEC _____	_____	INSTR _____
MECH _____	_____	NUC _____
WELD _____	_____	QAE _____
		11. APPROVAL OF FLD DISPOSITION
		<u>R. Christman</u>
		PROJECT FIELD ENGINEER
		DATE <u>3-15-80</u>

12. PROJECT ENGRG APPROVAL: YES NO EGS _____ P.E. R.L. Rogers DATE 3-14-80

REMARKS: CONVERT TO DCN

13. QUALITY ASSURANCE ENGINEER (FIELD): g. w. step DATE 3-15-80

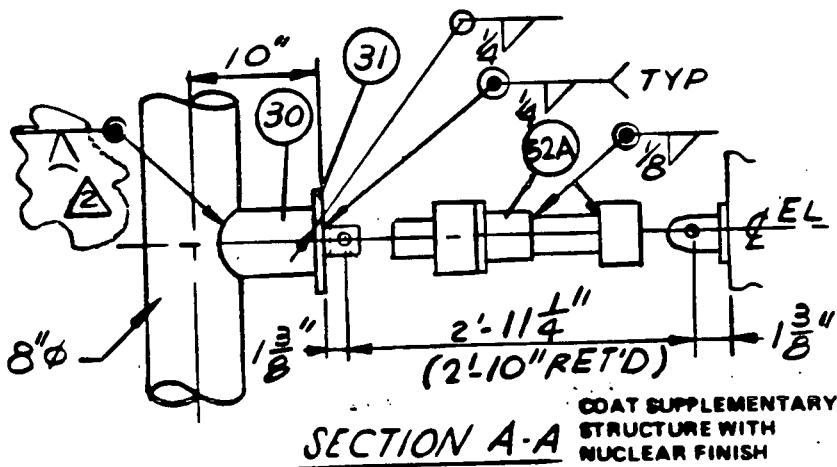
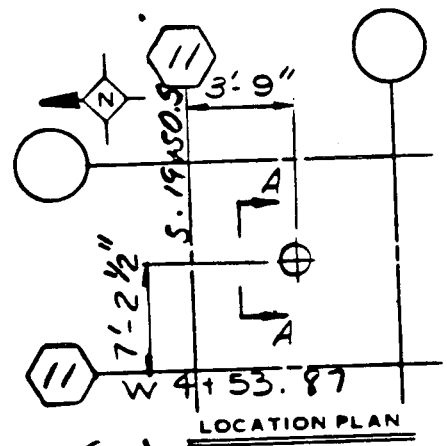
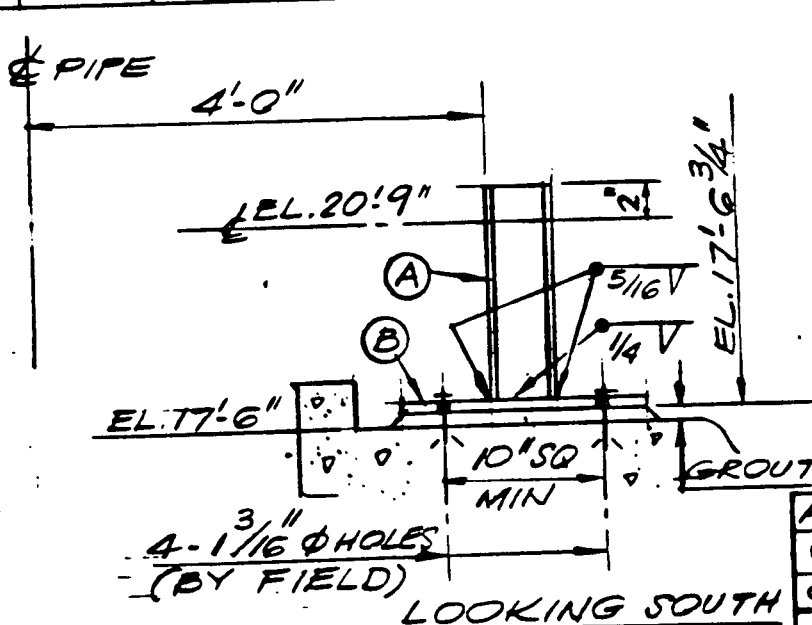
14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

SUS : BHA

ITEM NO.	NO. REQ'D	PART NO.	SIZE	DESCRIPTION	NF	AISC	NOTES
30	1	-	4"Ø SCH. 40S DUMMY PIPE S.S.				SPEC
31	1	-	R 1/2 x 6 x 0.6" CS END PLATE				S023-409-23
52A	1	-	PSA 1/4 4" STROKE PIN 1811002-34		X		BY PSC
				SHOCK ARRESTOR KIT, CPS = 1 1/4"			
				HPS = 3 1/2", LOAD = 194#			
A	1		W 4 x 13 x 3'-5"			X	SPEC
B	1		R 1" x 22 x 1'-10"			X	S023-206-18
							BY FIELD
	4		1"Ø CONC. FASTENERS				



PMC: LLO		TYPE 2		
PROJ CL	PIPE J (QC III)	MAX. TEMP		
QUAL CL	STEEL III	220°F		
DESIGN		X	Y 2	
	M +	-	-	
	(FT-LBS)	-	-	
	P +	Ø	Ø	500
	(LBS)	Ø	Ø	500

PROB. NO. 52 FT. NO. 186
 SPOOL NO. 2-RC-076-1
 ISO 1201-076-1
 PIPE 40400
 STEEL 23110

TAG NO. S2-RC-076-H-006

NO.	REVISIONS	DATE	DR.	CHK.	E.G.S.	P.E.	QAE
2	INCORPORATED DCN 01	2-26-80	B	KG	RR	MB	
1	SNUBBER VENDOR CHANGED	10-30-79	JL	AG	RR	MB	
0	ISSUED FOR CONSTRUCTION	7-10-79	MM	GC	RR	MB	

BECHTEL POWER CORPORATION MORWALK, CALIFORNIA		J.O. NO.	SAN ONOFRE NUCLEAR GENERATING STATION	
		FILE	PIPE SUPPORT ASSEMBLY	
JOB NO. 10079	DATE	APPROVED	SOUTHERN CALIFORNIA EDISON COMPANY LOS ANGELES, CALIF.	

PC 3446

MAR 21 1980



SAN ONOFRE NUCLEAR GENERATING STATION
UNITS 2 & 3

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 54841
DATE 3-20-80
2. PAGE 1 OF 1
3. UNIT NO. 2

12A. QUALITY CLASS II
12B. SPEC ADDEND. NO.

12C. DCN SUB NO. 04
12D. DATE APR 8 1980
12E. SCN NO.

J(QC III)
BHA JOB NO. 10079 (I.C.)
2COS-2
REF. DWG. OR SPEC. SHEET NO. 2 REV. 2 5. TITLE

Pipe Support Assembly

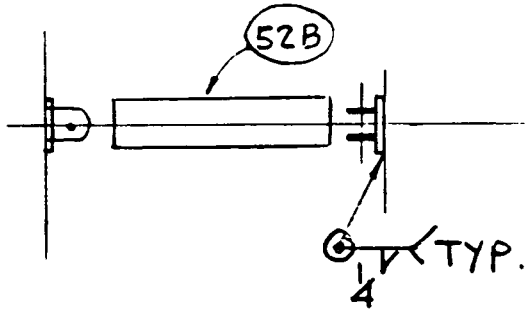
6. DESIGN ORIGIN: ENGRG VENDOR (IDENTIFY) NAME

7. EXISTING CONDITION:

Need to rotate snubber bracket

8. CHANGE REQUEST/SKETCH

PL# 5245



- 1) Change Item (52A) to (52B) in BILL OF MAT'L (FCR# S-4734)
- 2) No new Material Req'd

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE	INSTR.	NUC.	QAE
CIVIL					
ELEC					
MECH					
WELD					

9. P. Tannirat
PREPARED BY
11. APPROVAL OF FLD DISPOSITION
Harris J. [Signature]
PROJECT FIELD ENGINEER
DATE 3-21-80

12. PROJECT ENGRG APPROVAL: YES NO EGS
REMARKS: **CONVERT TO DCN**
P.E. R.L. Koger/MLT DATE 3-21-80

QUALITY ASSURANCE ENGINEER (FIELD): [Signature] DATE 3-21-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____
15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____
16. ADDITIONAL DISTRIBUTION _____

26 1980

SAN ONOFRE NUCLEAR GENERATING STATION

FIELD CHANGE REQUEST/DCN/SCN

1. FCR NO. 5-434

DATE 3/1/80

2. PAGE 1 OF 1

3. UNIT NO. 2

12A. QUALITY CLASS III

12C. DCN SUB NO. 03

12D. DATE MAR 31 1980

12E. SCN NO.

J(QC III)

ZBHA

JOB NO. 10679

(I.C)

2 COS-2

4. REF. DWG. OR SPEC. S2-RC-076-H-006

SHEET NO. 2

REV. 2

5. TITLE

Pipe Support Assembly

6. DESIGN ORIGIN: ENGRG

VENDOR (IDENTIFY)

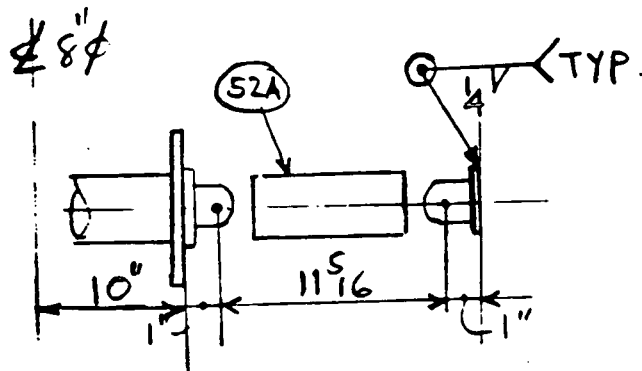
NAME

7. EXISTING CONDITION:

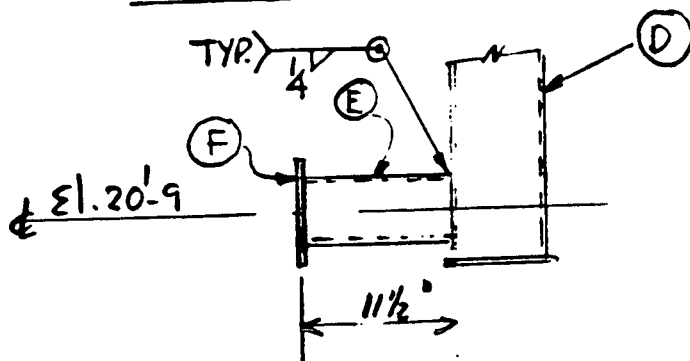
Item (S2) suppressor not in stock

8. CHANGE REQUEST/SKETCH

PL# 5139



SECT. A-A



LOOKING NORTH (PARTIAL)

Bill of Mat'l (by Field)

- 1) Delete Item (S2)
- 2) Add item (S2A) 1 ea - Fig 306
1/4 - 4" stroke Mech. shock
arrestor CPS = 14, HPS = 32
Load = 194#
(Retag from S3-SI-168-H-003)
- 3) Add Item (E) 1 - T.S. 3x3x3/16
- 4) Add Item (F) 1 - PL 1/2 x 5 x 5"

PROJECT ENGINEERING APPROVAL PER

10. REVIEWED BY	DATE	PIPE	3-14-80
CIVIL		INSTR	
ELEC		NUC	
MECH		QAE	
WELD			

9. P. Tannirat
PREPARED BY

11. APPROVAL OF FLD DISPOSITION
A. Christman
PROJECT FIELD ENGINEER
DATE 3-15-80

12. PROJECT ENGRG APPROVAL: YES NO EGS _____
REMARKS: CONVERT TO DCN
P.E. R.L. Rogers Date 3-14-80

13. QUALITY ASSURANCE ENGINEER (FIELD): J.W. Clifford DATE 3-15-80

14. SCE ENGINEERING APPROVAL _____ P.E. _____ DATE _____

15. BECHTEL QUALITY ENGINEER/QUALITY ASSURANCE _____ DATE _____

16. ADDITIONAL DISTRIBUTION _____

MAR 12 1980

PH

SAN ONOFRE NUCLEAR GENERATOR STATION UNITS 2 & 3
DRAWING CHANGE NUMBER (DCN) (IC)
JOB NO. 10079-003

2005-2
"RLE"

DCN NUMBER				
DRAWING NO.	SHEET NO.	REV. NO.	DCN SUB NO.	QUALITY CLASS
S2-R2-076-H-006	—	2	02	III

STARTUP SYSTEMS AFFECTED: 2BHA

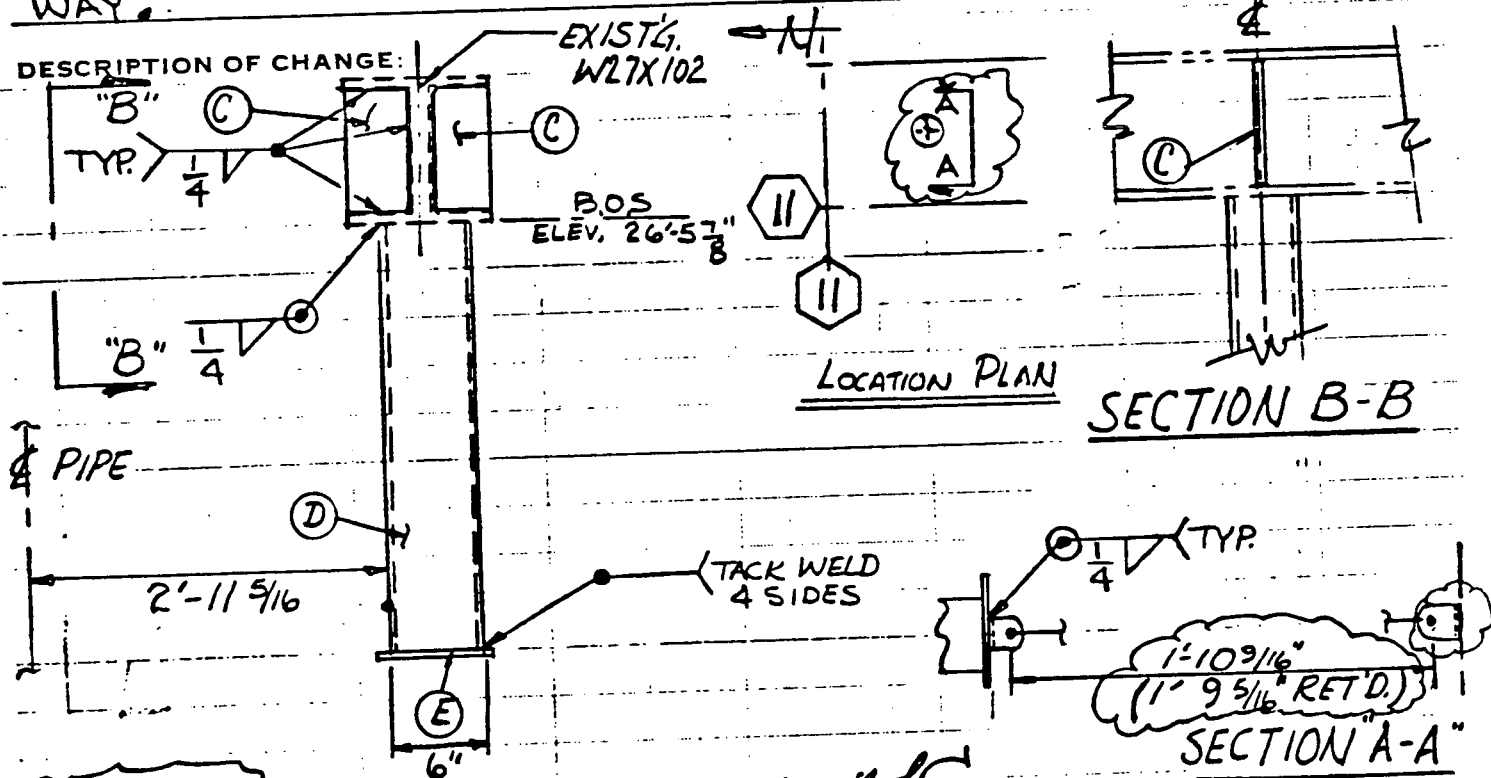
JOB NO. 10079-003 PAGE 1 OF 2 PAGE

DATE: FEB. 28, 1980 BY: R. MEJIANO

CHANGE REQUESTED BY: CLIENT ENG'R'G FIELD SUPPLIER/CONTRACTOR

REASON FOR CHANGE: REDESIGNED PIPE SUPPORT TO CLEAR PASSAGE WAY.

DESCRIPTION OF CHANGE:



PL# 4911

LOOKING NORTH N/S. 2-29-80

MATERIAL PROCUREMENT RESPONSIBILITY

- BECHTEL OFFICE
- BECHTEL FIELD
- SCE

AFFECTED PURCHASE ORDERS

NONE

REVISED FOR DCN CHANGE
YES NO

✓

APPROVAL SIGNATURES:

BECHTEL ENGINEERING _____ EGS

R.L. Rogers/PH
PE

DATE
2-29-80
DATE

SCE ENGINEERING APPROVAL _____ PE

DATE

BECHTEL QUALITY ENGINEER _____

DATE

BECHTEL QUALITY ASSURANCE _____

ADDITIONAL DISTRIBUTION: _____



SAN ONOFRE NUCLEAR GENERATING STATION UNITS 2 & 3
DRAWING CHANGE NOTICE (DCN)
JOB NO. 10079

MAR 12 1980

SUPPLEMENTAL PAGE

DCN NUMBER			
DRAWING NO.	SHEET NO.	REV.	DCN SUB NO.
S2-RC-076-H-006	—	2	02

JOB NO. 10079-003 PAGE 2 OF 2 PAGE
DATE: FEB. 28, 1980 BY: R. MEJIANO

CHANGE: STL. REF DNG TO: 23211

DESCRIPTION OF CHANGE

VENDOR	ADD	CHNG	DELETE	INFO	N/A
KELLOGG					✓
PIPE FAB					✓
GRINNELL					✓
409-23					✓
206-18			A&B		✓
206-1					
OTHER PSC		52A			
FIELD	C, D & E		(4) 1/8" CONC. FASTENERS		
COMBUSTION	INFORMATION ONLY			YES	NO
					✓

ADDITIONS AND CHANGES ONLY

ADD
↓
CHG.

ITEM	QTY	PART NO.	DESCRIPTION	AISC	NF
C	2	—	3/8" STIFFENER P'S.		
D	1	—	T.S. 6"X4"X1/2"X 6'-0" LG.		
E	1	—	R 1/4X4 1/2 X 0'-6 1/2"		
52A			PN 1811002 (22) "FIELD MODIFY"		