

February 8, 1989

Docket Nos.: 50-361 and 50-362

FACILITY: San Onofre Nuclear Generating Station, Unit Nos. 2 and 3  
LICENSEE: Southern California Edison Company (SCE)  
SUBJECT: SUMMARY OF MEETING HELD ON DECEMBER 7, 1988  
RE: SPENT FUEL POOL RERACKING

On December 7, 1988, Southern California Edison Company (SCE) and representatives of their subcontractors, Westinghouse Electric Corporation (WEC) and Bechtel Power Corporation (BPC), met with NRR staff to discuss their plans to rerack the spent fuel pools of San Onofre Units 2 and 3. The list of attendees is provided in Enclosure 1.

The meeting consisted of a presentation by SCE and their subcontractors with questions, comments and discussion by the staff. Enclosure 2 provides the briefing slides prepared by SCE.

A list of issues to be addressed in the amendment request is provided as Enclosure 3.

original signed by

Donald E. Hickman, Project Manager  
Project Directorate V  
Division of Reactor Projects - III,  
IV, V and Special Projects

Enclosures:  
As stated

DISTRIBUTION

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PD #5 Reading  
JLee  
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OGC (f/info only)  
EJordan  
BGrimes  
ACRS (10)  
MRJohnson (Region V)  
NRC Participants

DRSP/PD5  
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2/7/89

*for* DRSP/D:PD5  
GKnighton  
2/8/89

8902230114 890208  
PDR ADOCK 05000361  
F PDC

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UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

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A handwritten signature in cursive script, reading "Donald E. Hickman", is written over the typed name.

Donald E. Hickman, Project Manager  
Project Directorate V  
Division of Reactor Projects - III,  
IV, V and Special Projects

Enclosures:  
As stated

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Southern California Edison Company

San Onofre Nuclear Generating  
Station, Units 2 and 3

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## SPENT FUEL POOL RERACKING MEETING

SAN ONOFRE UNITS 2 AND 3

DECEMBER 7, 1988

## LIST OF ATTENDEES

<u>NAME</u>	<u>AFFILIATION</u>	<u>FUNCTION</u>
Fred Nandy	SCE	Licensing
Jack Rainsberry	SCE	Licensing
Derrick Mercurio	SCE	Licensing
Raymond Baker	SCE	Project Engineering
Richard Blaschke	SCE	Civil Engineering
Richard Miller	SCE	Civil Engineering
Dennis Ostrom	SCE	Civil Engineering
Tom Watson	WEC	Engineering Analysis
Keith Matthews	WEC	Licensing
Harry Flanders	WEC	NCD Analysis
Don Green	WEC	NCD Analysis
William Guerin	WEC	Nuclear Safety
Richard Day	BPC	Structural Engineering
Selcuk Atalik	BPC	Task Engineering
Don Hickman	NRR	Project Manager
Charles Trammell	NRR	Project Manager
Jerry Wermiel	NRR	Plant Systems
Norman Wagner	NRR	Plant Systems
Neil Thompson	NRR	Structural Engineering
Hans Asher	NRR	Structural Engineering
David Jeng	NRR	Structural Engineering
Herman Graves	NRC	Research
Giuliano DeGrassi	NRC	Brookhaven National Lab

SPENT FUEL POOL RERACKING

HEAVY LOADS EVALUATION

SAN ONOFRE UNITS 2 AND 3

DECEMBER 7, 1988

## AGENDA

I. INTRODUCTION (SCE)  
DERRICK MERCURIO

II. HEAVY LOADS (BECHTEL)  
RICHARD DAY

## I. INTRODUCTION

### A. SCOPE

#### 1. INCREASE SPENT FUEL STORAGE CAPACITY

A. INCREASE FROM 800 TO APPROXIMATELY 1572  
ASSEMBLIES PER UNIT

B. STORAGE CAPACITY TO YEAR 2002 WITH CORE OFF-LOAD

## I. INTRODUCTION

### B. PROJECT SCHEDULE AND MILESTONES

- 6/3/88 - INITIAL MEETING WITH NRC
- 12/7/88 - MEETING WITH NRC
- 2/1/89 - SUBMITTAL OF PROPOSED LICENSE AMENDMENT
- 3/30/89 - BEGIN RACK FABRICATION FOR UNIT 2
- 8/1/89 - LICENSE AMENDMENT ISSUED BY NRC
- 10/2/89 - RACK DELIVERY FOR UNIT 2
- 10/89 - BEGIN RACK INSTALLATION IN UNIT 2 (COMPLETE  
RACK INSTALLATION DURING CYCLE 5 OPERATION)



## C. HEAVY LOADS CONSIDERATIONS

### 0 CONSTRUCTION SEQUENCING

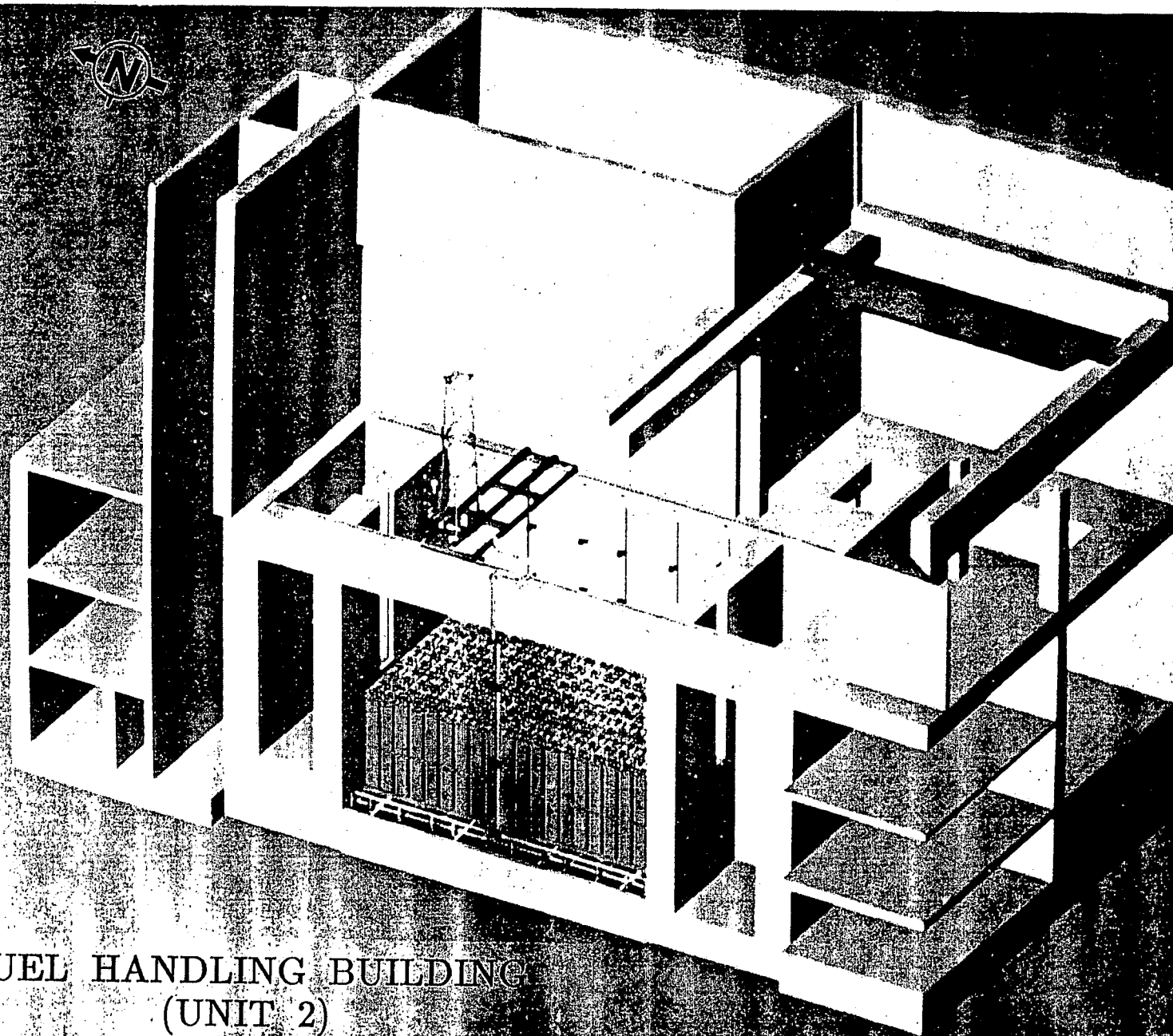
- TEMPORARY SPENT FUEL STORAGE IN CASK POOL

### 0 TEMPORARY CRANE - JANUARY 15, 1989 AWARD

### 0 NUREG-0612 EVALUATION

## **AGENDA**

- 1. RACK REMOVAL/INSTALLATION SEQUENCING**
- 2. SAFE LOAD PATHS**
- 3. TEMPORARY CONSTRUCTION CRANE**
- 4. CONTROL OF HEAVY LOADS (NUREG 0612)**
- 5. POSTULATED CONSTRUCTION LOAD DROP**
- 6. CASK POOL COVER DESIGN FUNCTIONS**



FUEL HANDLING BUILDING  
(UNIT 2)

# **RACK REMOVAL/INSTALLATION SEQUENCING**

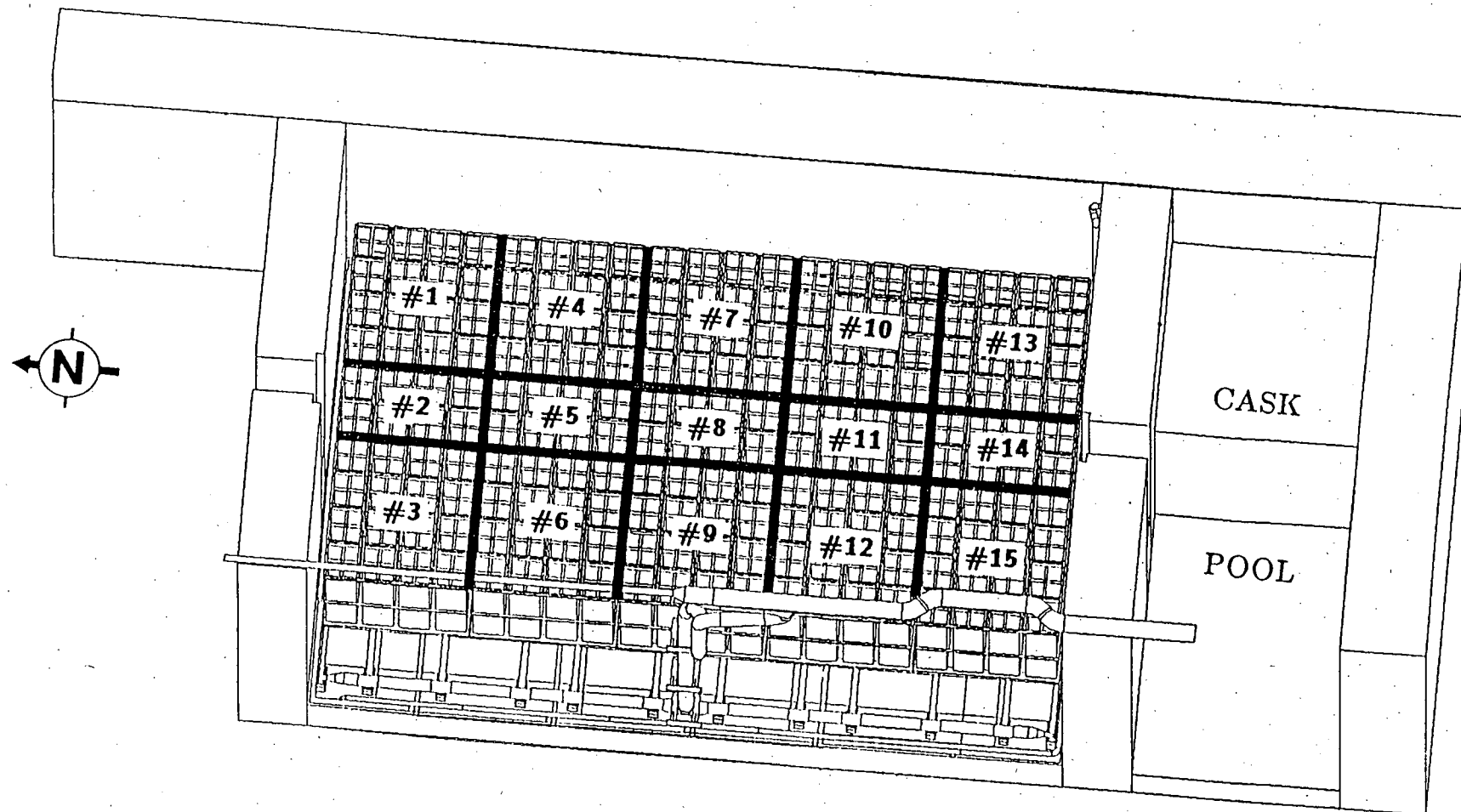
## **APPROACH**

- **SPENT FUEL STORED IN CASK POOL (DURING RERACKING)**

## **SIGNIFICANT CRITERIA**

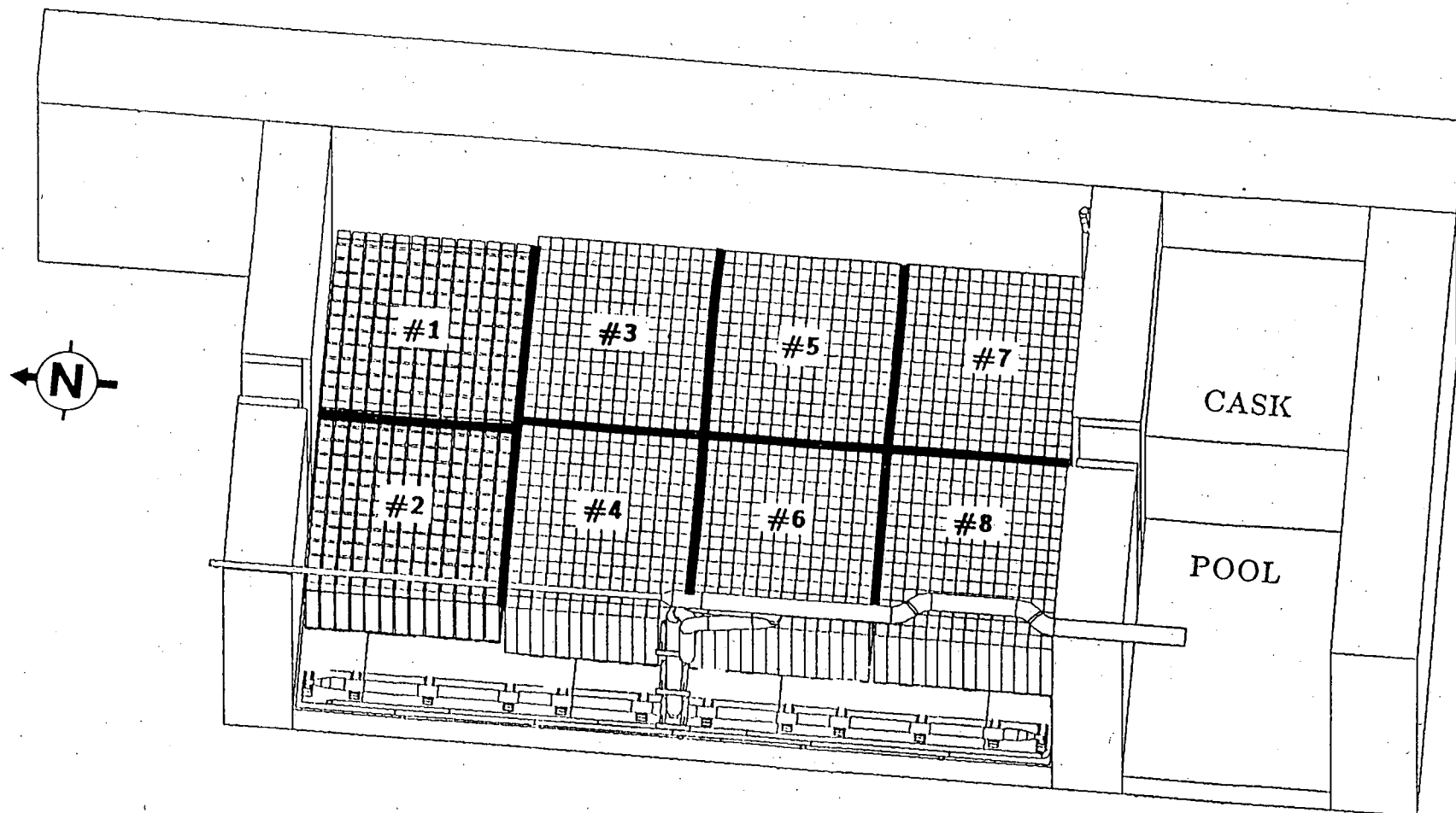
- **MAINTAIN SAFE LOAD PATH**
- **PROVIDE MINIMUM 3 EMPTY ROWS OF CELLS (NO SPENT FUEL) ADJACENT TO WORK AREA**
- **PROVIDE FLEXIBILITY IN SPENT FUEL LOCATIONS**
- **MINIMIZE REQUIRED FUEL SHUFFLING**

# SPENT FUEL POOL (UNIT 2 )



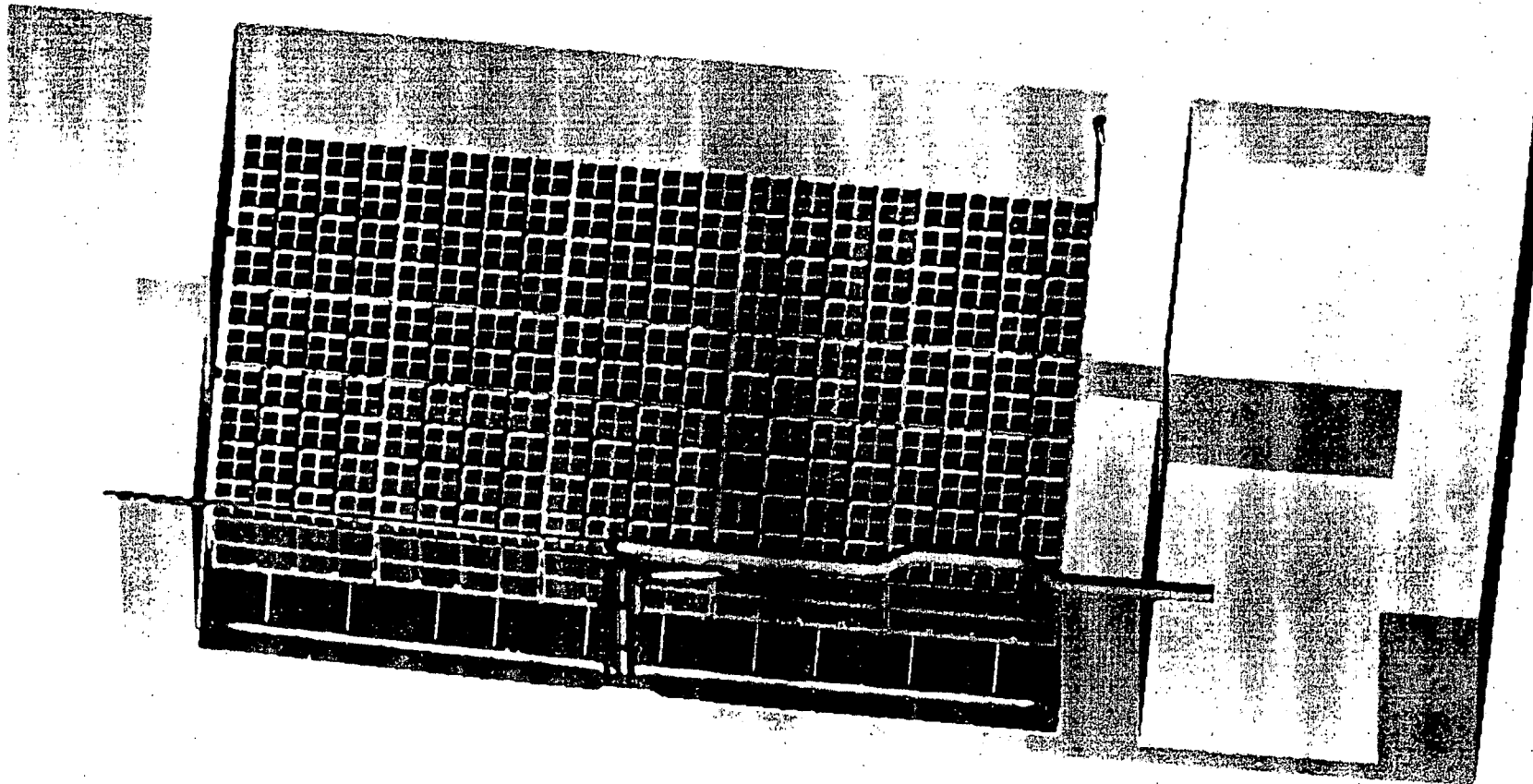
ORIGINAL CONDITION

# SPENT FUEL POOL (UNIT 2)



FINAL CONFIGURATION

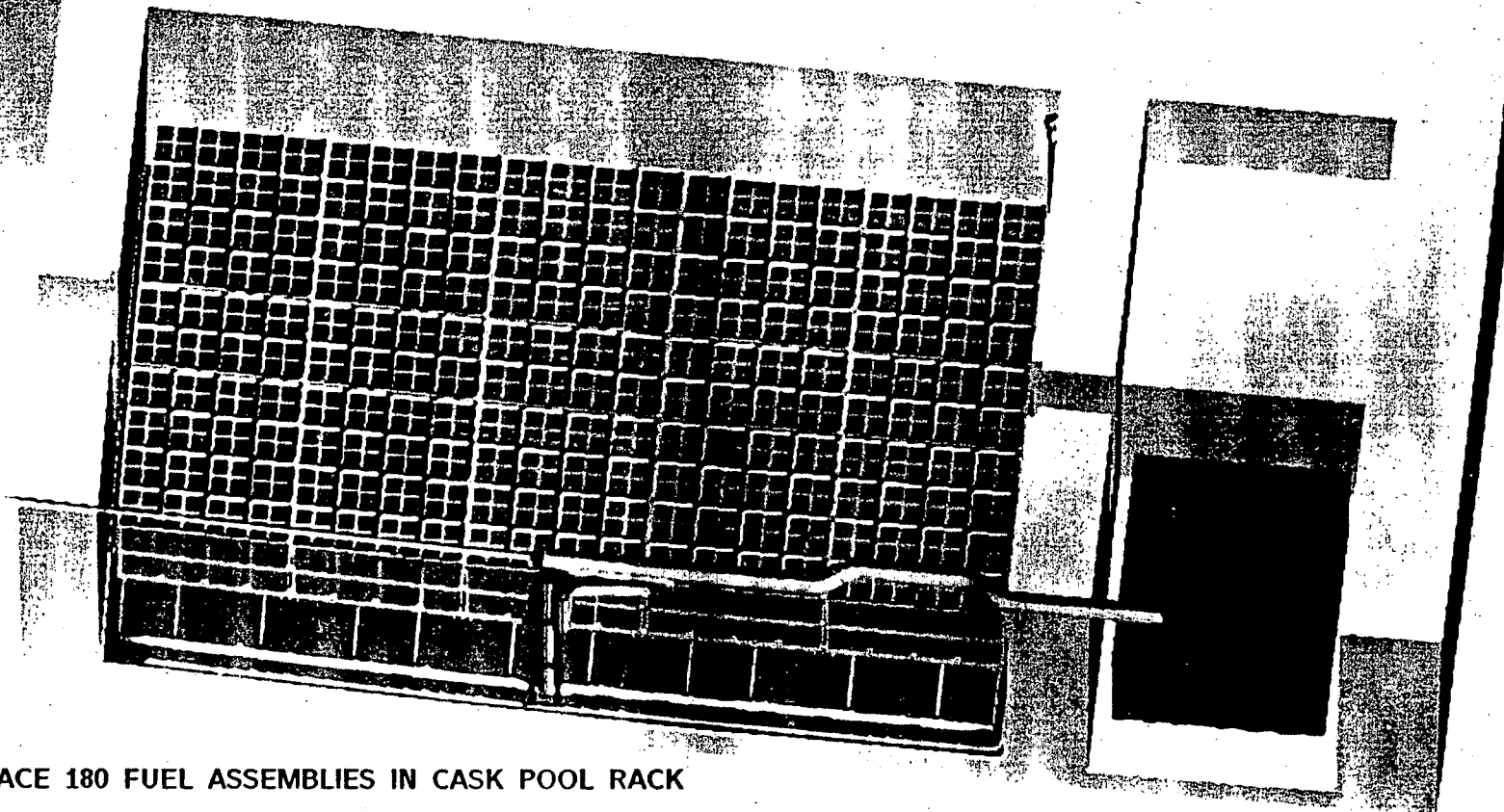
# RERACK SEQUENCING SPENT FUEL POOL (UNIT 2)



- \* 800 FUEL STORAGE LOCATIONS IN EXISTING RACKS
- \* 480 FUEL ASSEMBLIES STORED IN POOL (POST CYCLE 5 REFUELING)
- \* 320 EMPTY FUEL STORAGE LOCATIONS

ORIGINAL CONDITION

## PROPOSED RERACK SEQUENCING

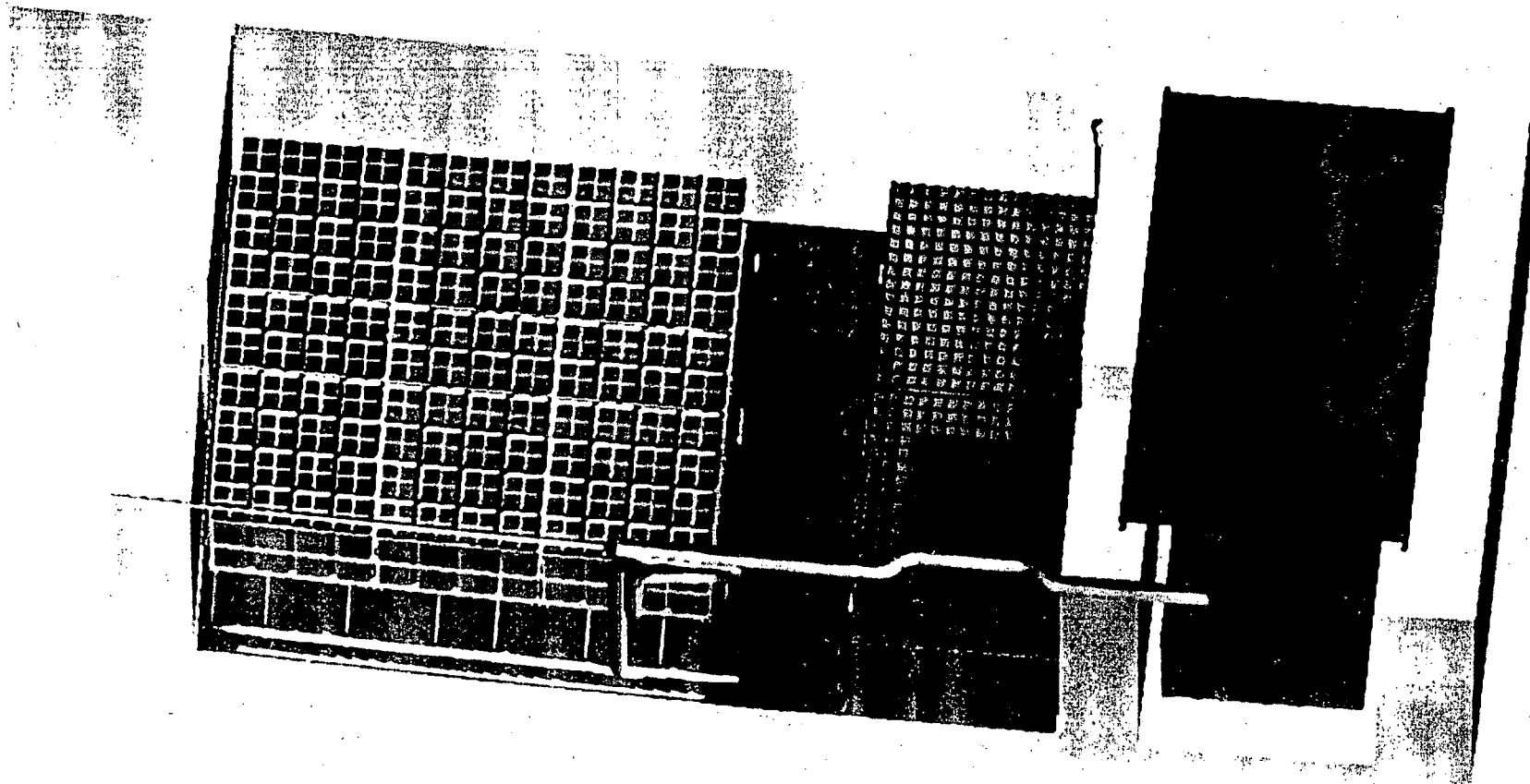


- \* PLACE 180 FUEL ASSEMBLIES IN CASK POOL RACK
- \* PLACE PROTECTIVE COVER OVER CASK HANDLING POOL
- \* LOCATE REMAINING 300 FUEL ASSEMBLIES AT NORTH END
- \* REMOVE NES RACKS #10-15
- \* REMOVE PIPING AND SUPPORTS FROM VACATED AREA

STEP 1



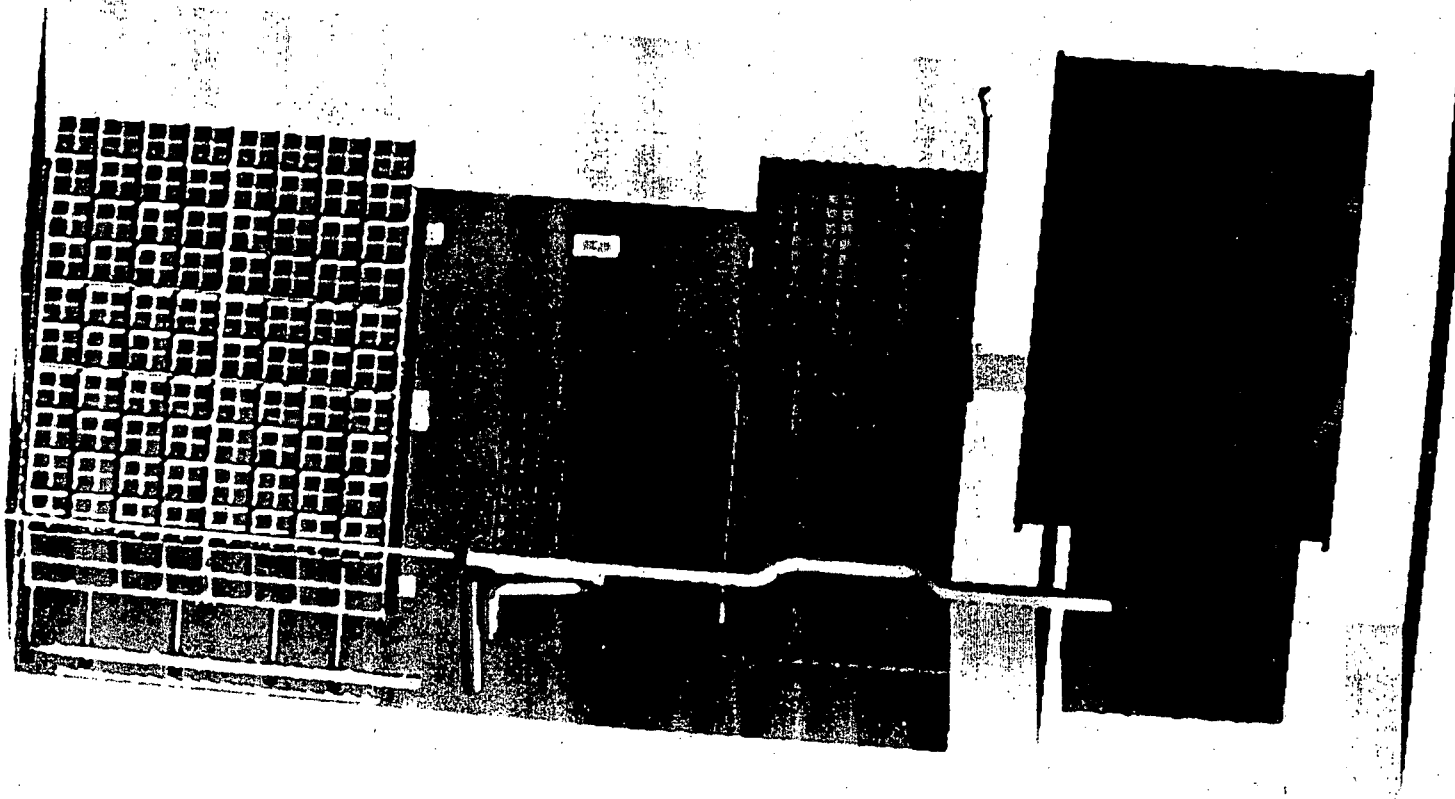
## PROPOSED RERACK SEQUENCING



- \* INSTALL W RACKS #7 & 8
- \* SHIFT 132 FUEL ASSEMBLIES INTO W RACK #8
- \* REMOVE NES RACKS #7-9
- \* REMOVE PIPING AND SUPPORTS FROM VACATED AREA

STEP 2

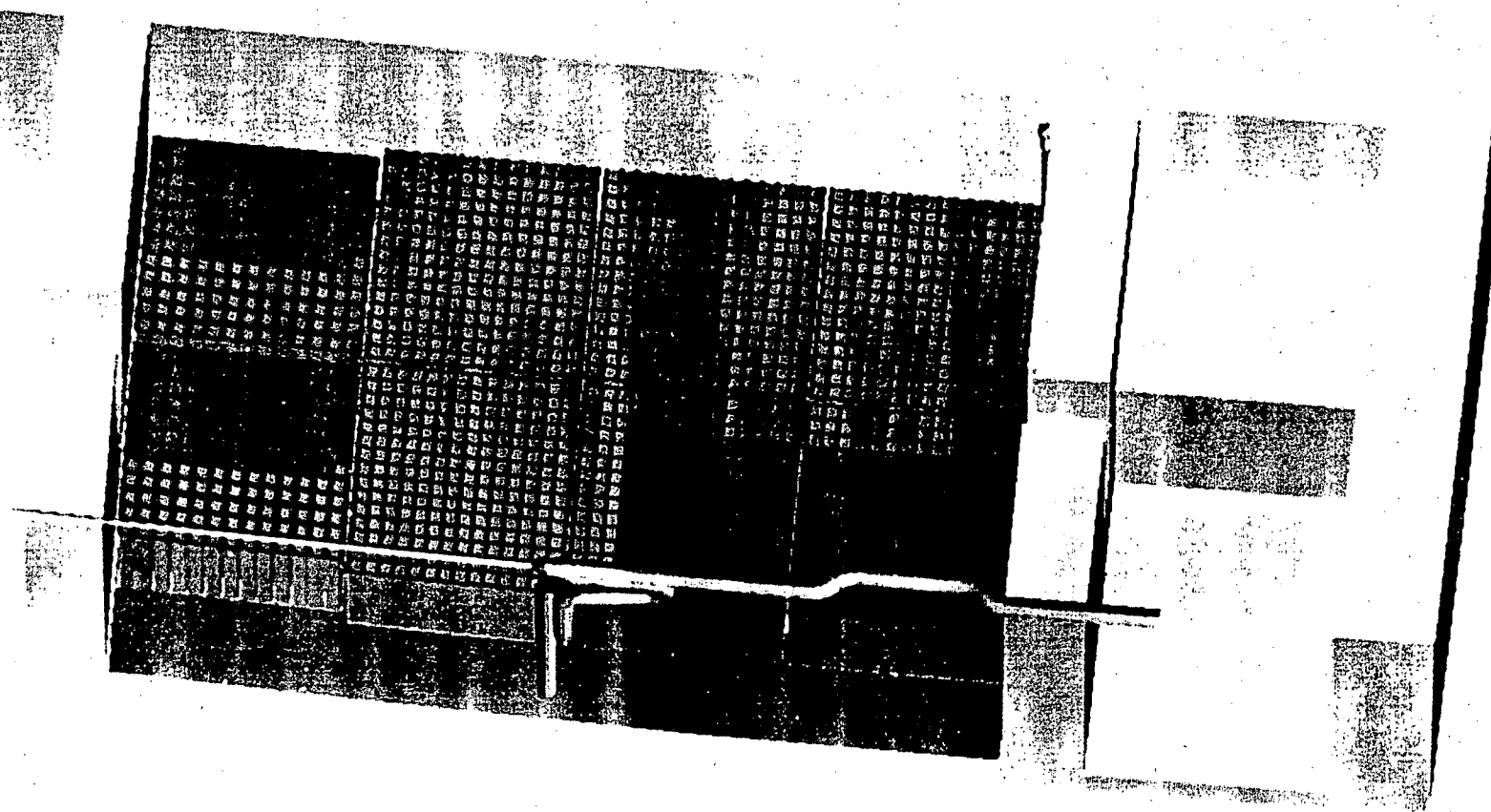
## PROPOSED RERACK SEQUENCING



- \* INSTALL W RACK #6
- \* PLACE ALL FUEL ASSEMBLIES IN W RACKS #6 & 8
- \* REMOVE NES RACKS #1-6
- \* REMOVE REMAINING PIPING AND SUPPORTS

STEP 3

## PROPOSED RERACK SEQUENCING

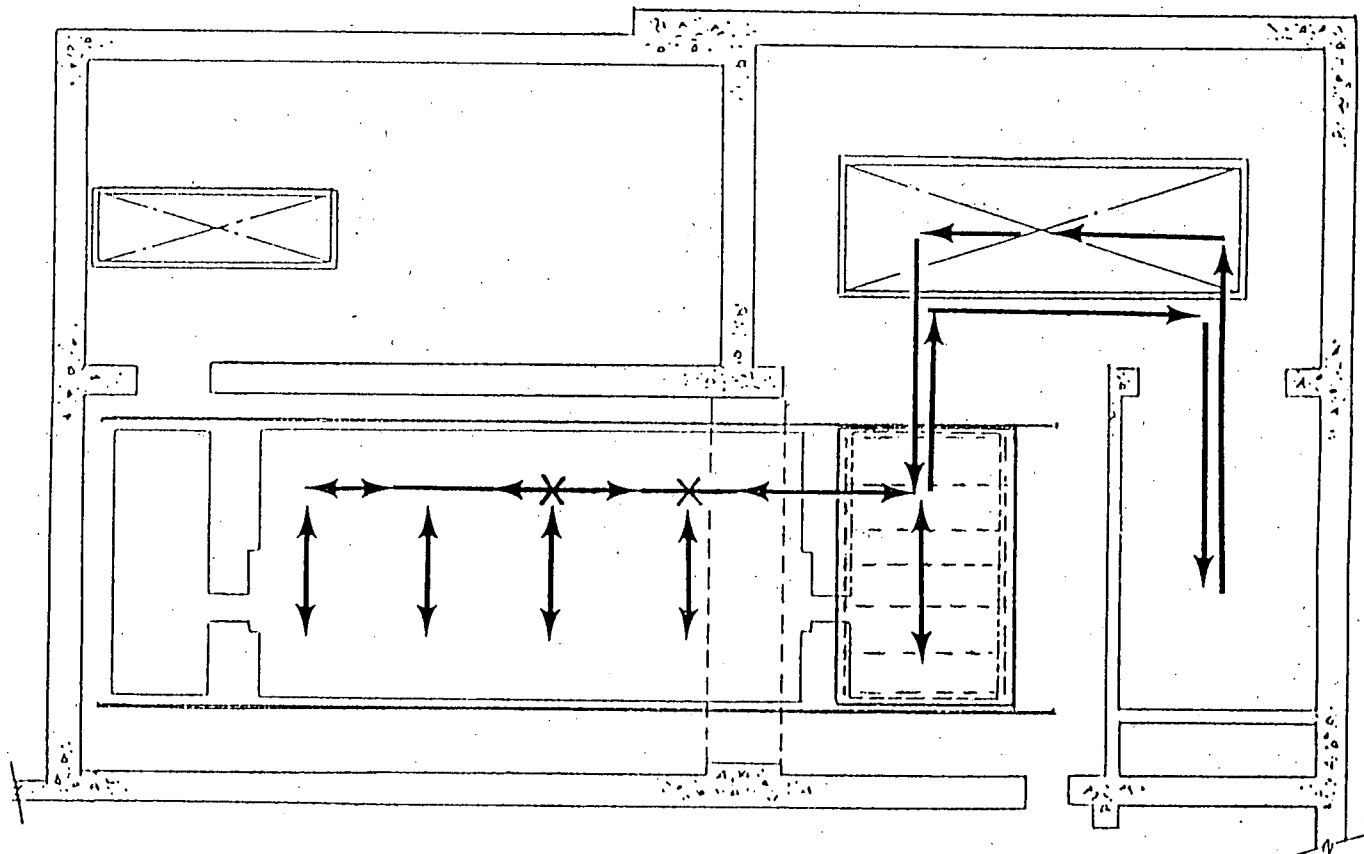
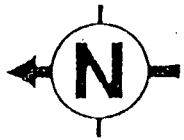


- \* INSTALL W RACKS #1-4
- \* REMOVE PROTECTIVE COVER FROM CASK HANDLING POOL
- \* SHIFT 180 FUEL ASSEMBLIES FROM CASK POOL TO SPENT FUEL POOL
- \* PLACE W RACK #7 IN SPENT FUEL POOL

STEP 4

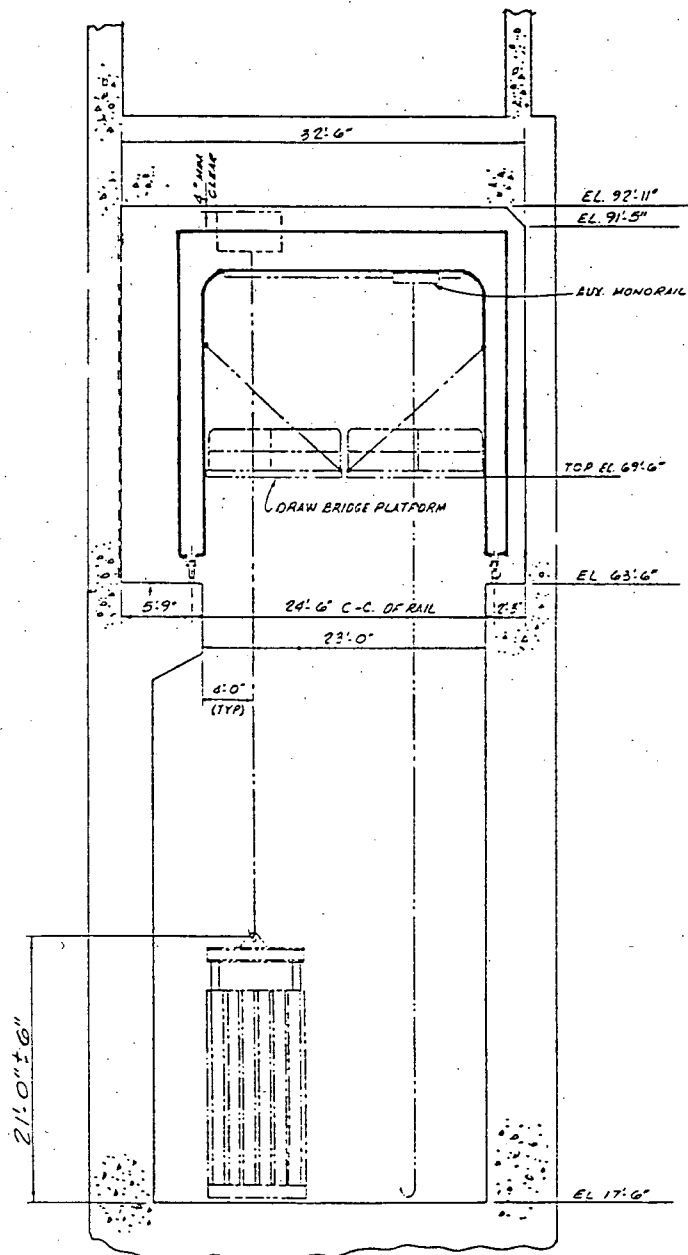
# SAFE LOAD PATHS

## FUEL HANDLING BUILDING (UNIT 2)



PARTIAL PLAN AT ELEV. 63'-6"  
POOL DECK

# TEMPORARY CONSTRUCTION GANTRY CRANE



SECTION - SPENT FUEL POOL  
(UNIT 2)

# **TEMPORARY GANTRY CRANE**

- **35 TON UPGRADED COMMERCIAL CLASS C**
- **MEET CMAA-70 AND CHAPTER 2-1 OF ANSI B30.2 REQUIREMENTS**
- **FACTOR OF SAFETY FOR LOAD BEARING MEMBERS**
  - **3 AGAINST MINIMUM TENSILE YIELD STRENGTH**
  - **5 AGAINST AVERAGE ULTIMATE STRENGTH**
- **MEET SRP LOAD COMBINATIONS (INCLUDES DBE)**
- **DUAL HOLDING BRAKES ON HOISTS (MAIN AND AUXILIARY) RATED AT 150% OF MOTOR TORQUE**
- **GANTRY AND TROLLEY BRAKES RATED AT 150% MOTOR TORQUE**
- **HOOKS TESTED AT TWICE RATED CAPACITY**

## **NUREG 0612**

# **CONTROL OF HEAVY LOADS AT NUCLEAR POWER PLANTS**

### **SECTION**

### **TITLE**

<b>5</b>	<b>GUIDELINES FOR CONTROL OF HEAVY LOADS</b>
<b>5.1.1</b>	<b>GENERAL (GUIDELINES)</b>
<b>5.1.2</b>	<b>SPENT FUEL POOL AREA - PWR</b>

NUREG 0612

SECTION 5.1.1 GENERAL (GUIDELINES)

<u>REQUIREMENTS</u>	<u>EXTENT OF COMPLIANCE</u>
<u>2. PROCEDURES</u>	COMPLY
<u>3. CRANE OPERATORS</u>	COMPLY
<u>4. SPECIAL LIFTING DEVICES</u>	COMPLY
<u>5. LIFTING DEVICES THAT ARE NOT SPECIALLY DESIGNED (SLINGS)</u>	COMPLY
<u>7. CRANE DESIGN</u>	COMPLY



NUREG 0612

SECTION 5.1.2 (GUIDELINES FOR)  
SPENT FUEL POOL AREA - PWR

REQUIREMENTS

EXTENT OF  
COMPLIANCE

(3) (a) "HOT" SPENT FUEL AT ONE  
LOCATION WITH MAXIMUM  
SEPARATION FROM LOAD PATH

COMPLY  
(NO "HOT" FUEL)

(b) PREVENT LOAD BLOCK MOVEMENT  
WITHIN 25' (HORIZ) OF "HOT" FUEL

COMPLY  
(NO "HOT" FUEL)

NUREG 0612

SECTION 5.1.2 (GUIDELINES FOR)  
SPENT FUEL POOL AREA - PWR

REQUIREMENTS

EXTENT OF  
COMPLIANCE

(3) (c) MECHANICAL STOP/ELECTRICAL  
INTERLOCK TO PREVENT TRAVEL  
WHERE DROP COULD DAMAGE  
EQUIPMENT (SAFE SHUTDOWN)

COMPLY  
(NOT APPLICABLE)

- ANALYZE DROPS IN  
UNRESTRICTED TRAVEL AREAS  
TO ENSURE NOT CAUSE OF  
CRITICALITY, LEAKAGE  
UNCOVERING FUEL, OR LOSS  
OF SAFE SHUTDOWN EQUIPMENT

COMPLY

NUREG 0612

SECTION 5.1.1 GENERAL (GUIDELINES)

REQUIREMENTS

EXTENT OF  
COMPLIANCE

1. SAFE LOAD PATHS

**COMPLY -  
EXCEPT MARKINGS  
OF FLOOR**

6. CRANES

- INSPECTION, TESTING, AND  
MAINTENANCE PER CHAPTER  
2-2 OF ANSI B30.2-1976

**COMPLY -  
EXCEPT LOAD TESTS  
(2-2.2.2) PERFORMED AT  
SHOP AND SITE PRIOR TO  
INSTALLATION**

# **TEMPORARY GANTRY CRANE TESTING**

**PER ANSI B30.2-1976**

- **OPERATIONAL TESTS (SECTION 2-2.2.1)**
  - AT FACTORY PRIOR TO SHIPMENT**
  - AT SITE PRIOR TO FINAL INSTALLATION**
  - IN PLACE (OVER POOLS) PRIOR TO INITIAL USE**
- **RATED LOAD TEST (SECTION 2-2.2.2)**
  - AT FACTORY PRIOR TO SHIPMENT (1.25 X 35 TON)**
  - AT SITE PRIOR TO FINAL INSTALLATION (1.25 X 35 TON)**
- **MODIFIED LOAD TEST (HOIST & TROLLEY ONLY)**
  - IN PLACE (OVER CASK POOL ONLY) PRIOR TO INITIAL USE  
(1.25 X MAX. ANTICIPATED LOAD)**

NUREG 0612

SECTION 5.1.2 (GUIDELINES FOR)  
SPENT FUEL POOL AREA - PWR

REQUIREMENTS

EXTENT OF  
COMPLIANCE

(3) (b) LOAD BLOCK MOVEMENT  
WITHIN 25' (HORIZ) OF FUEL

- SUFFICIENT FUEL DECAY
- APPROVAL OF SHIFT  
SUPERVISOR

COMPLY

MEET INTENT BY  
PROCEDURE  
APPLICATION AND  
SCHEDULED WORK  
ACTIVITIES

MECHANICAL STOP/ELECTRICAL  
INTERLOCK IN PLACE PRIOR TO  
PLACING "HOT" FUEL IN POOL

COMPLY

NUREG 0612

SECTION 5.1.2 (GUIDELINES FOR)  
SPENT FUEL POOL AREA - PWR

REQUIREMENTS

EXTENT OF  
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ACTIVITIES

MECHANICAL STOP/ELECTRICAL  
INTERLOCK IN PLACE PRIOR TO  
PLACING "HOT" FUEL IN POOL

COMPLY  
(NOT APPLICABLE)

**NUREG 0612**

**SECTION 5.1.2 (GUIDELINES FOR)  
SPENT FUEL POOL AREA - PWR**

**REQUIREMENTS**

**EXTENT OF  
COMPLIANCE**

**(3) (d) CARRY LOAD (CASK) MAXIMUM  
6 INCHES, OR LESS, ABOVE FLOOR**

**MAXIMUM 24 INCHES  
IN POOL  
(RACK WEIGHT << CASK)  
EXCEPT WHEN ENTERING/  
LEAVING ALL OTHER  
AREAS 12 INCH MAXIMUM**

**(3) (e) ANALYZE POSTULATED LOAD  
DROPS PER NUREG APPENDIX A**

**COMPLY - APPLYING  
DROP ANALYSES TO  
NORMAL TRAVEL PATHS**

# **POSTULATED CONSTRUCTION LOAD DROP**

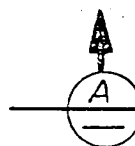
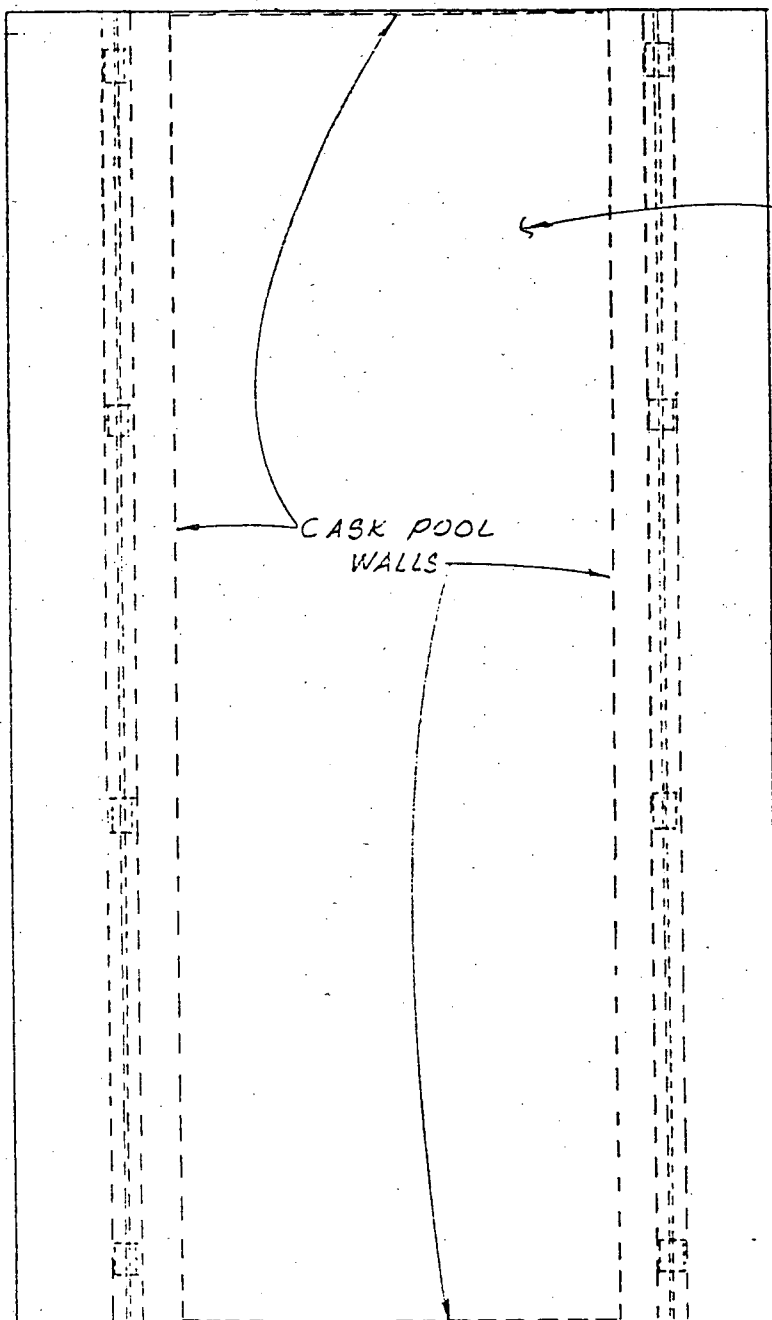
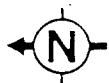
## **SPENT FUEL POOL**

- RESULTS:**
- 1) LINER (3/16" THICK) AND RELINER (1/8" THICK)  
PENETRATED**
  - 2) CONCRETE BASEMAT PENETRATED ABOUT  
5 3/4 INCHES (7% OF THICKNESS)**
  - 3) LEAKAGE CONFINED TO LEAK CHASE SYSTEM  
(MAXIMUM FLOW RATE < 60 GPM)**
  - 4) MAKEUP WATER SUPPLY (150 GPM)**
  - 5) TECHNICAL SPECIFICATION WATER LEVEL  
MAINTAINED**

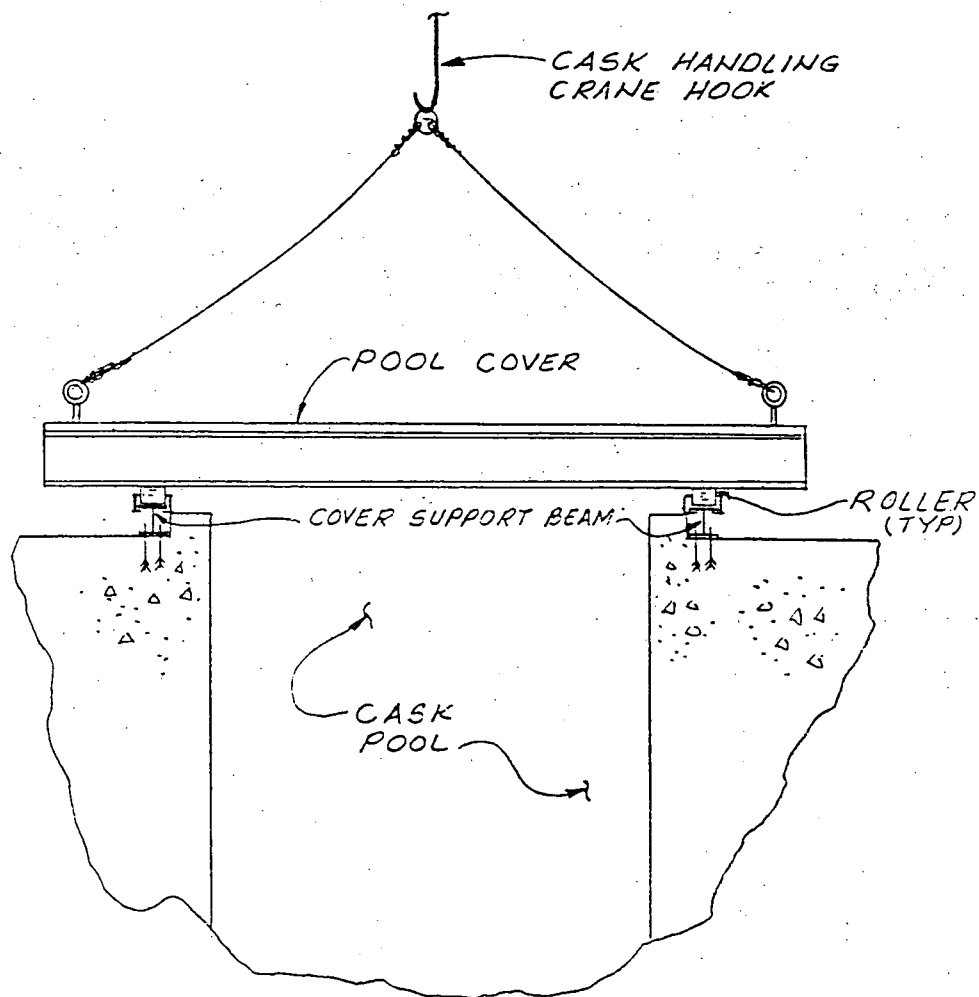


## **CASK POOL COVER DESIGN FUNCTIONS**

- **PRECLUDE COVER DROP IN CASK POOL DURING  
INSTALLATION/REMOVAL**
- **WITHSTAND POSTULATED CONSTRUCTION LOAD  
DROPS (COMPLY WITH NUREG 0612 APPENDIX A)**
- **ANCHOR COVER TO POOL DECK**
- **PROVIDE UNIFORM WORKING SURFACE  
(LAYDOWN AREA)**



PLAN (CASK POOL COVER)



SECTION (A)

SAN ONOFRE NUCLEAR GENERATING STATION

UNITS 2 AND 3

SPENT FUEL POOL RERACK

PRESENTATION

DECEMBER 7, 1988

AGENDA

I. INTRODUCTION (SCE)  
DERRICK MERCURIO

II. SEISMIC ANALYSES OF SPENT FUEL RACKS (WESTINGHOUSE)  
HARRY FLANDERS

## I. INTRODUCTION

### A. SCOPE

#### 1. INCREASE SPENT FUEL STORAGE CAPACITY

A. INCREASE FROM 800 TO APPROXIMATELY 1572  
ASSEMBLIES PER UNIT

B. STORAGE CAPACITY TO YEAR 2002 WITH CORE OFF-LOAD

## I. INTRODUCTION

### B. RACK DESIGN PARAMETERS

1. FREE STANDING RACKS
2. FIXED BORAFLEX POISON
3. 2 REGION DESIGN
  - A. 312 LOCATIONS (APPROXIMATE) - NEW AND RECENTLY IRRADIATED FUEL
  - B. 1260 LOCATIONS (APPROXIMATE) - IRRADIATED FUEL
4. LICENSE FOR 4.1% ENRICHED FUEL (5.1% DESIGN)
5. STORE UNITS 1, 2 AND 3 FUEL

## I. INTRODUCTION

### C. PROJECT SCHEDULE AND MILESTONES

- 6/3/88 - INITIAL MEETING WITH NRC
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RACK INSTALLATION DURING CYCLE 5 OPERATION)

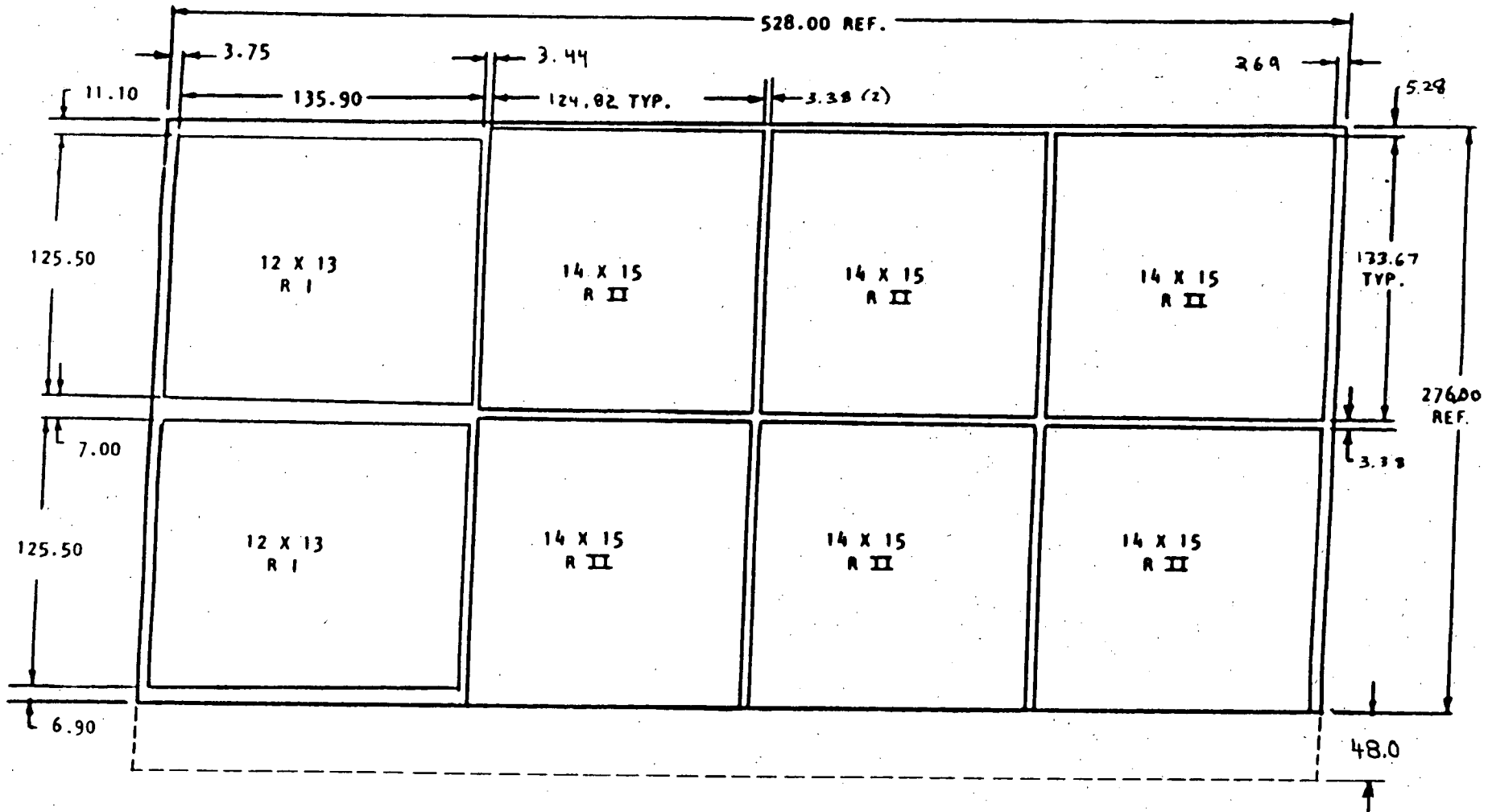


## **SAN ONOFRE UNITS 2 & 3 FUEL RACKS SEISMIC ANALYSIS**

- o Pool Layout**
- o Background Information**
- o Fuel Rack Structural Model**
- o Single Rack Seismic Models**
  - Full Fuel Loading**
  - Partial Fuel Loading (Quadrant)**
  - Partial Fuel Loading (4 Rows)**
  - Partial Fuel Loading (1 Row)**
  - Empty Rack**
  - Displacement Results**
- o Multiple Rack Seismic Models**
  - Full/Full**
  - Full/Empty**
- o Displacement Results**
  - Rack Absolute Displacements**
  - Rack Relative Displacements**
  - Displacement Characteristics**
- o Conservatisms**

SAN ONOFRE UNIT 2 OR UNIT 3  
SPENT FUEL POOL LAYOUT

N 



## **BACKGROUND INFORMATION**

## BACKGROUND INFORMATION

### Friction

- .8 Maximum/.2 Minimum
- Reference: Rabinowicz, E., Friction Coefficients of Water - Lubricated Stainless Steels for a Spent Fuel Rack Facility, Report Q 23.1.3 to Boston Edison Co., November 1976

### Finite Element Code

- WECAN, Westinghouse Electric Computer Aalysis. Configuration control under strict QA standards. Generic review by NRC and reviewed 2 times by Franklin Institute for fuel rack application.

### Hydrodynamic Mass

- Potential flow theory
- Reference: Fritz, R. J., The Effects of Liquids on the Dynamic Motions of Immersed Solids, Transactions of the ASME, February 1972

### Time History

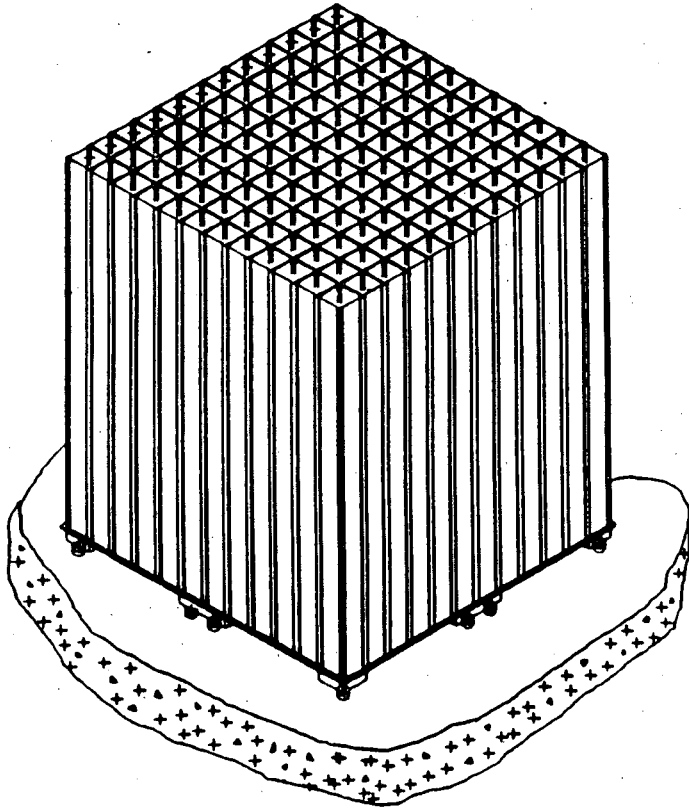
- Developed by Bechtel
- Three statistically independent components
- 80 seconds duration

### Standard Fuel Characteristics

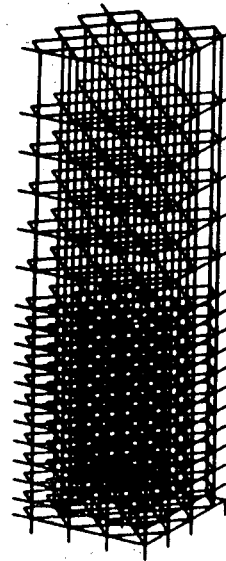
- Dynamic properties supplied by fuel vendor

## FUEL RACK STRUCTURAL MODEL

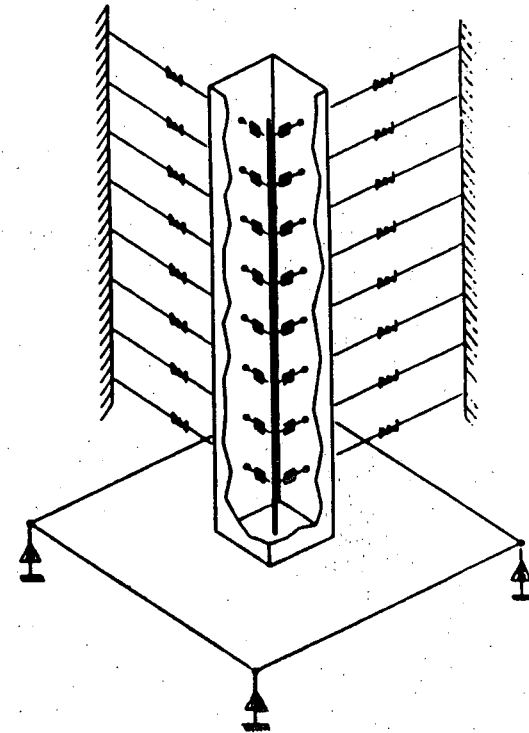
## SEISMIC MODEL DEVELOPMENT



FUEL RACK MODULE

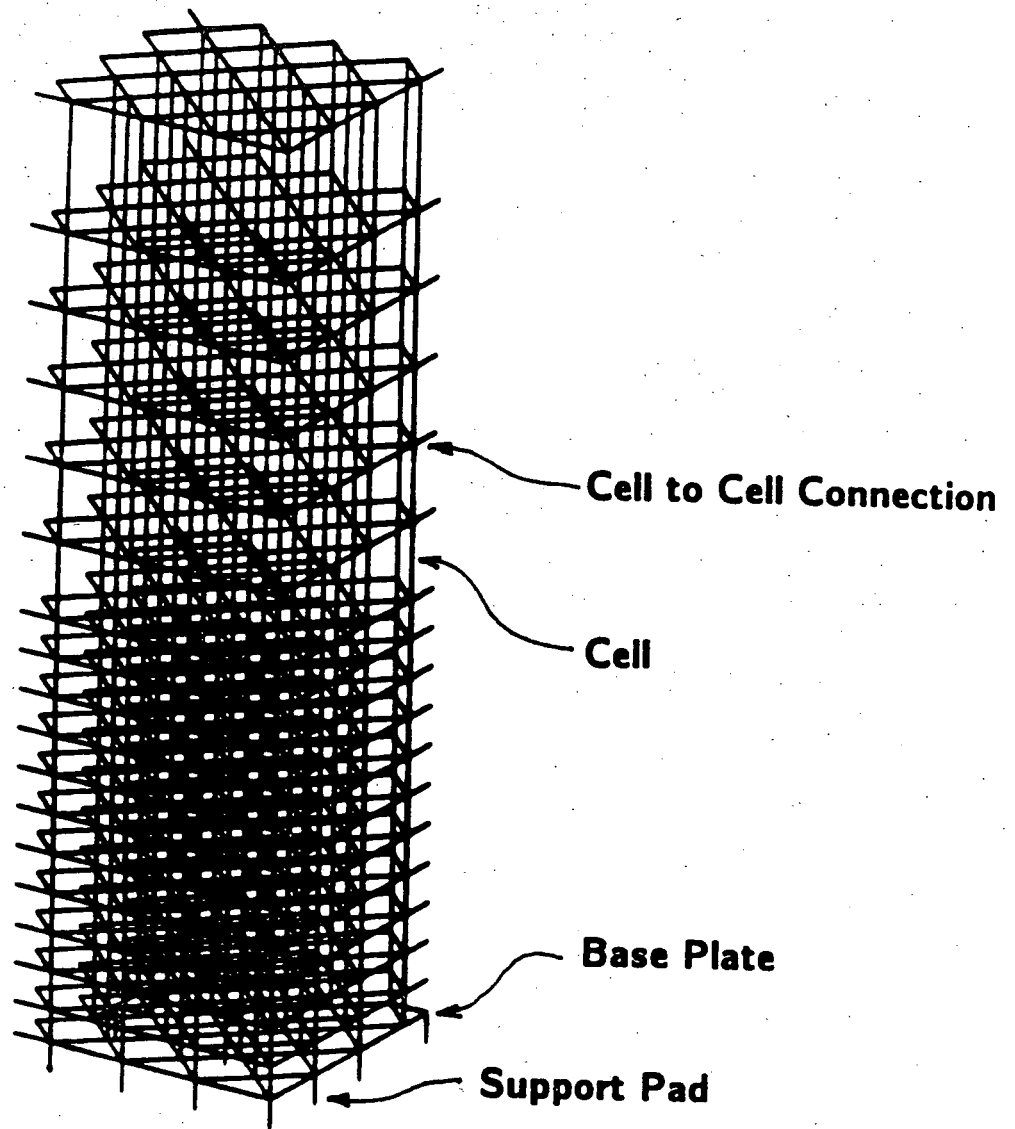


STRUCTURAL MODEL

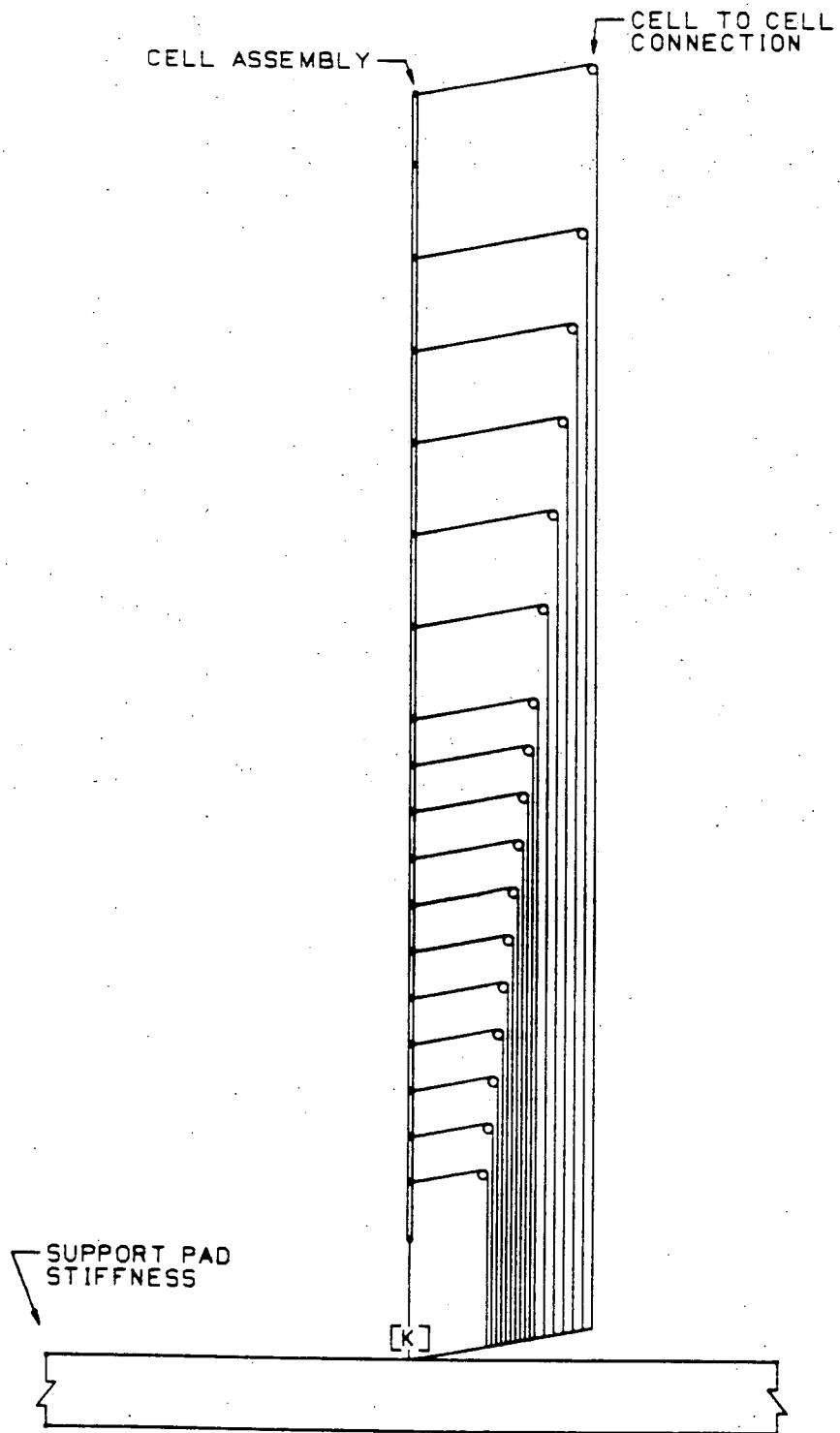


SEISMIC MODEL

# FUEL RACK STRUCTURAL MODEL REGION II



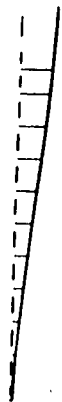
# EFFECTIVE STRUCTURAL PROPERTIES





# EQUIVALENT STRUCTURAL MODEL

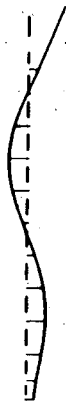
## MODE SHAPES



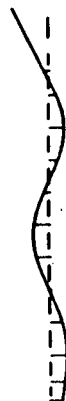
1ST MODE  
12.7 Hz



2ND MODE  
40.4 Hz



3RD MODE  
74.5 Hz



4TH MODE  
116.3 Hz



5TH MODE  
165.8 Hz



6TH MODE  
226.8 Hz

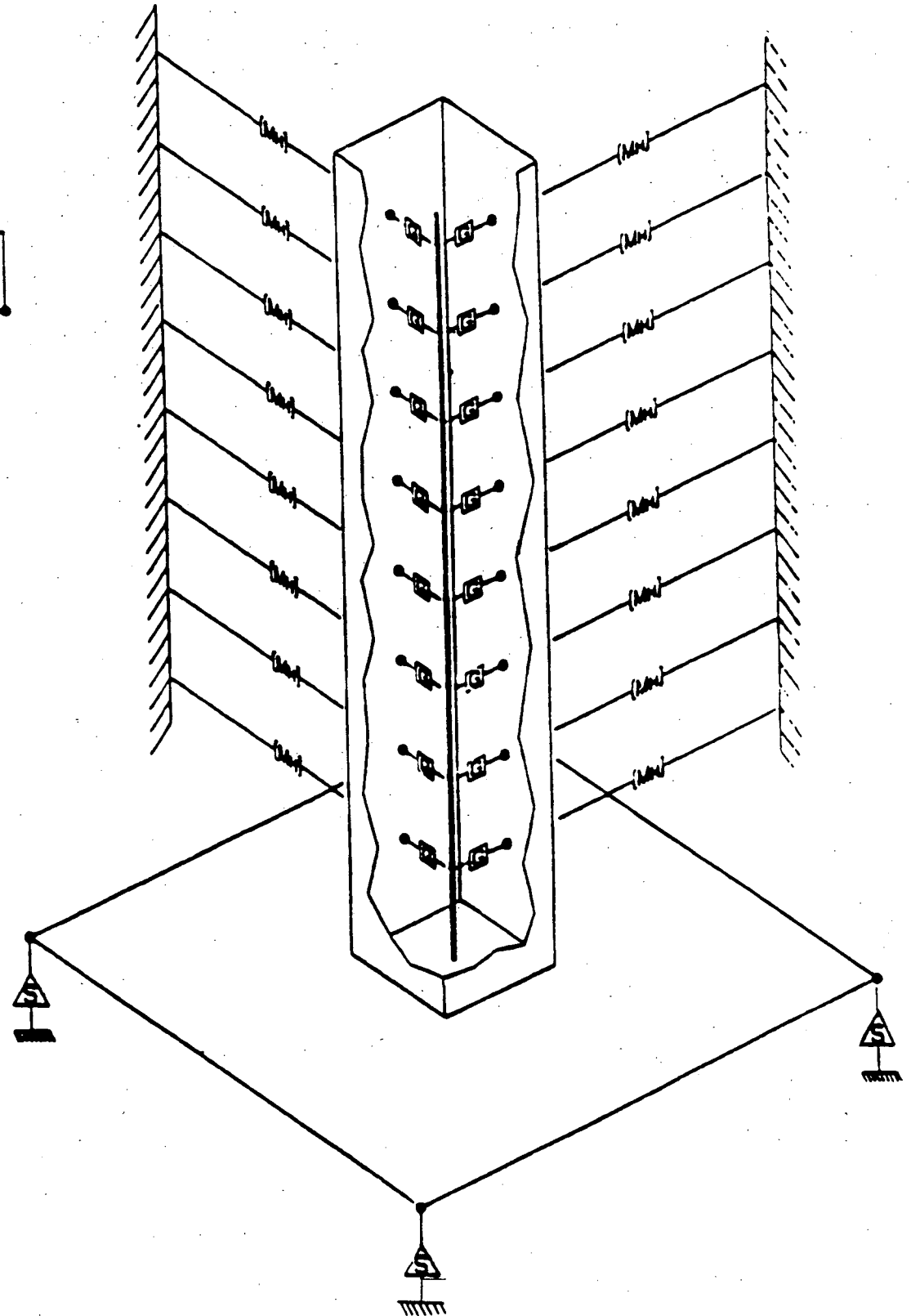
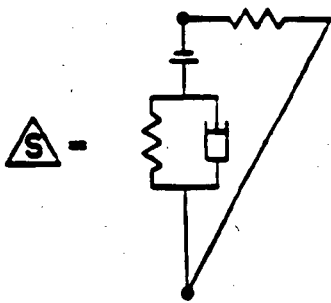
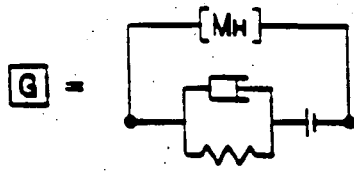


7TH MODE  
304.2 Hz

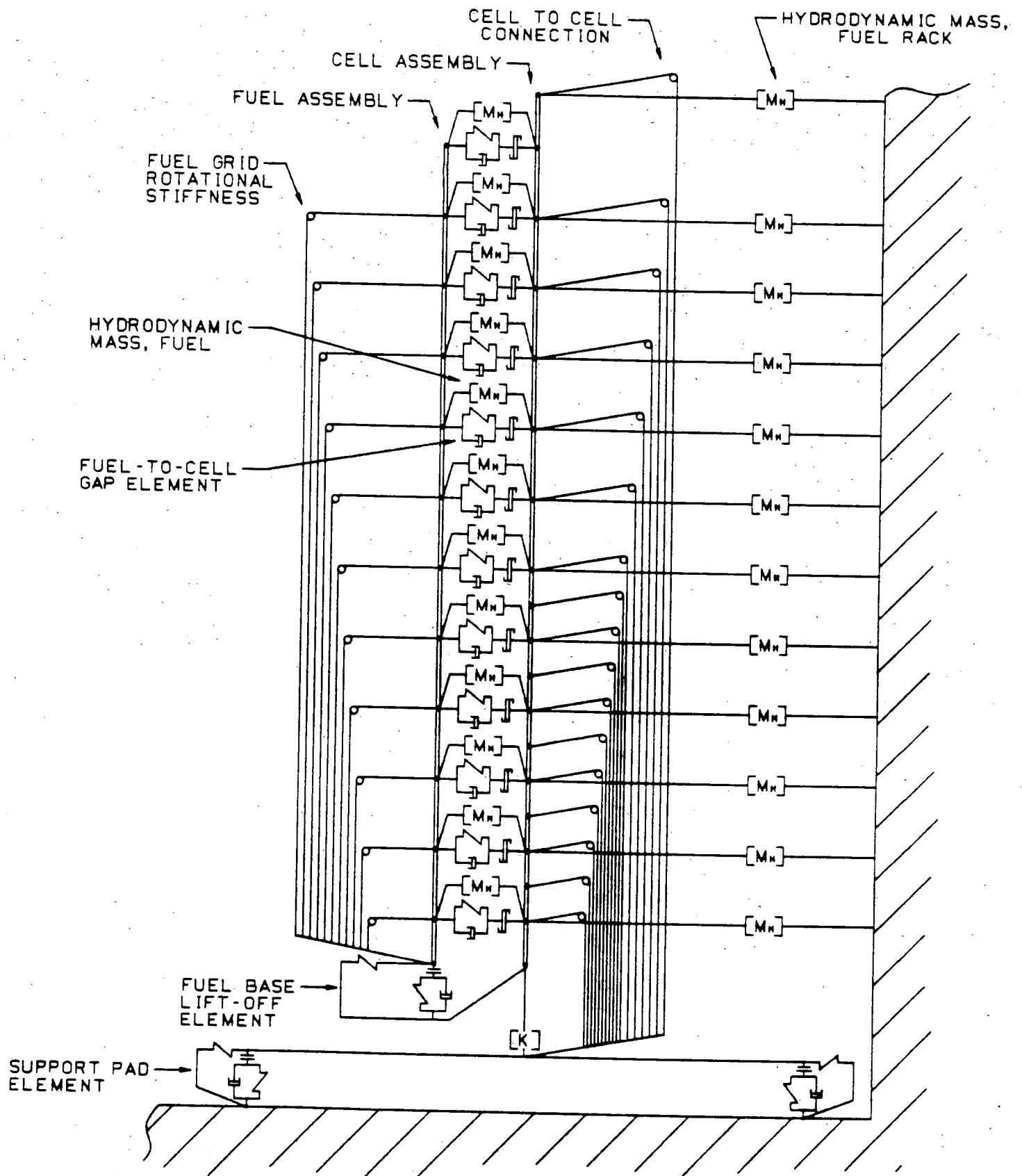
## **SINGLE RACK SEISMIC MODELS**

- **FULL FUEL LOADING**
- **PARTIAL FUEL LOADING (QUADRANT)**
- **PARTIAL FUEL LOADING (4 ROWS)**
- **PARTIAL FUEL LOADING (1 ROW)**
- **EMPTY RACK**
- **DISPLACEMENT RESULTS**

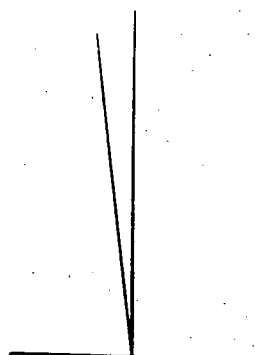
# THREE DIMENSIONAL NONLINEAR SEISMIC MODEL



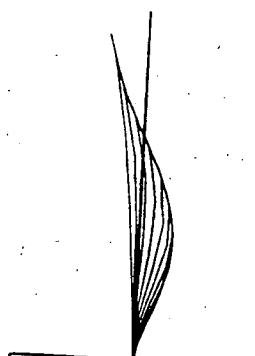
# NONLINEAR SEISMIC MODEL, SINGLE RACK (2-D VIEW OF 3-D MODEL)



FUEL AND CELL MODE SHAPES  
REGION 2 STANDARD FUEL



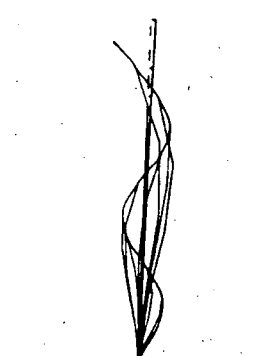
FUEL 1ST



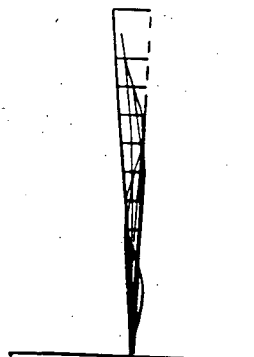
FUEL 2ND



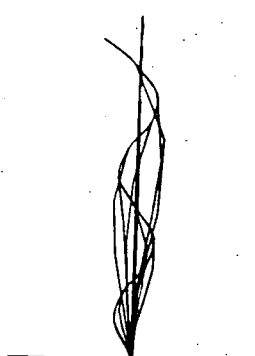
FUEL 3RD



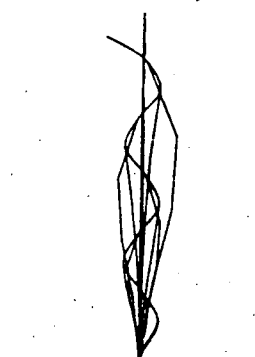
FUEL 4TH



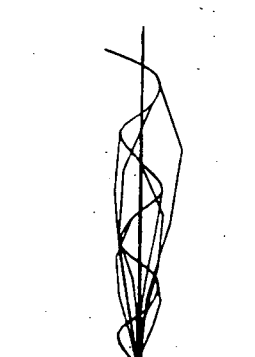
CELL 1ST



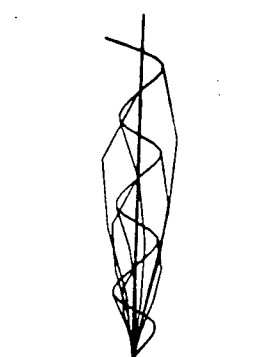
FUEL 5TH



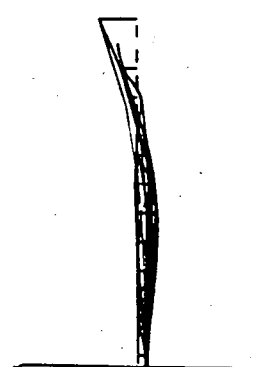
FUEL 6TH



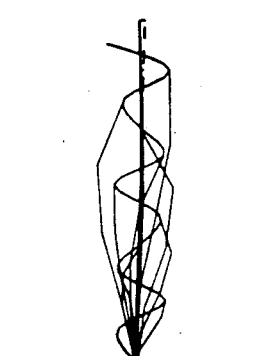
FUEL 7TH



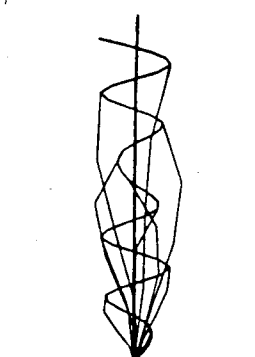
FUEL 8TH



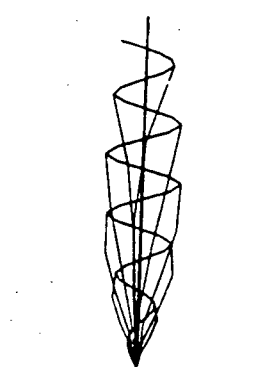
CELL 2ND



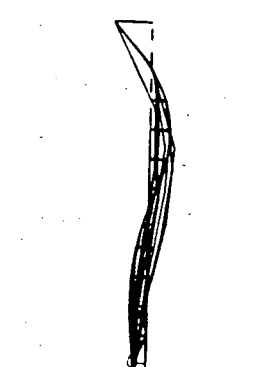
FUEL 9TH



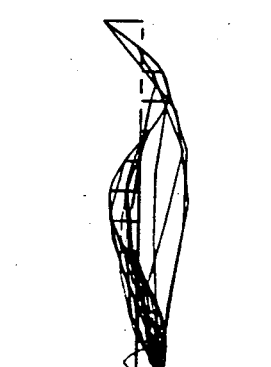
FUEL 10TH



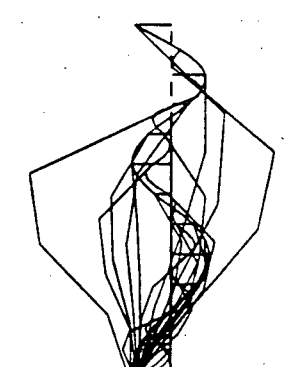
FUEL 11TH



CELL 3RD

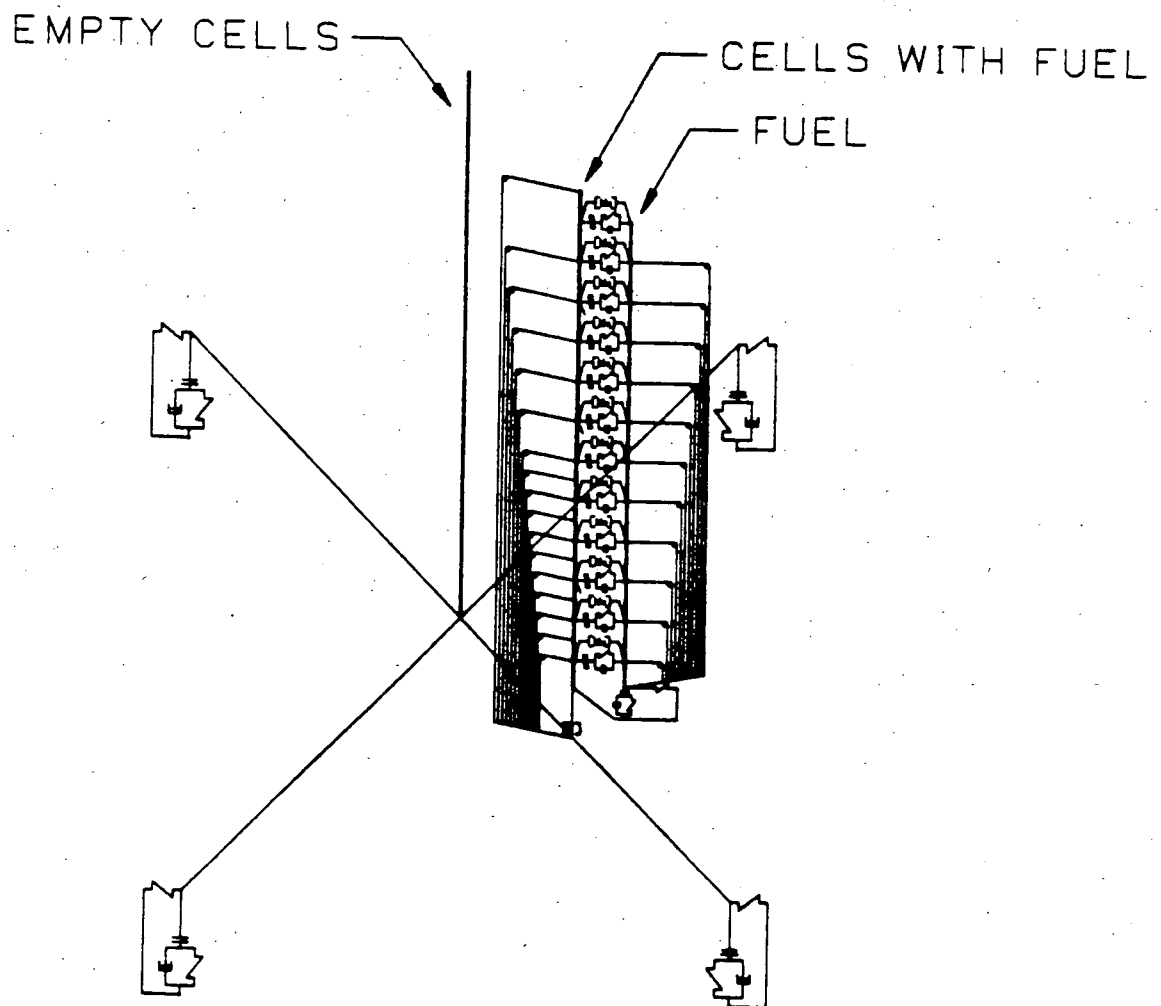


CELL 4TH

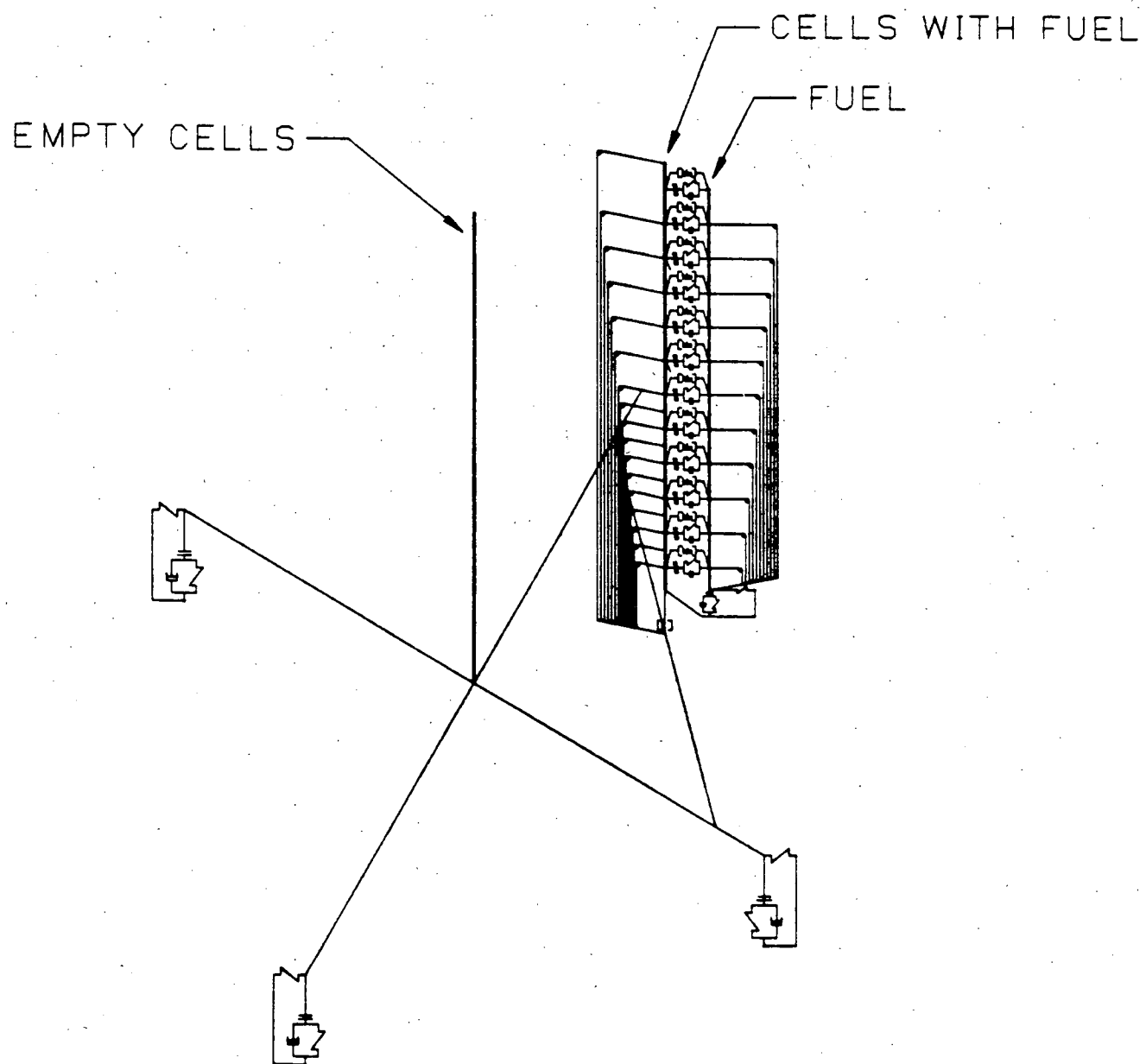


CELL 5TH

PARTIAL FUEL LOADING MODEL  
(QUADRANT LOADING)



PARTIAL FUEL LOADING MODEL  
(4 ROW LOADING)

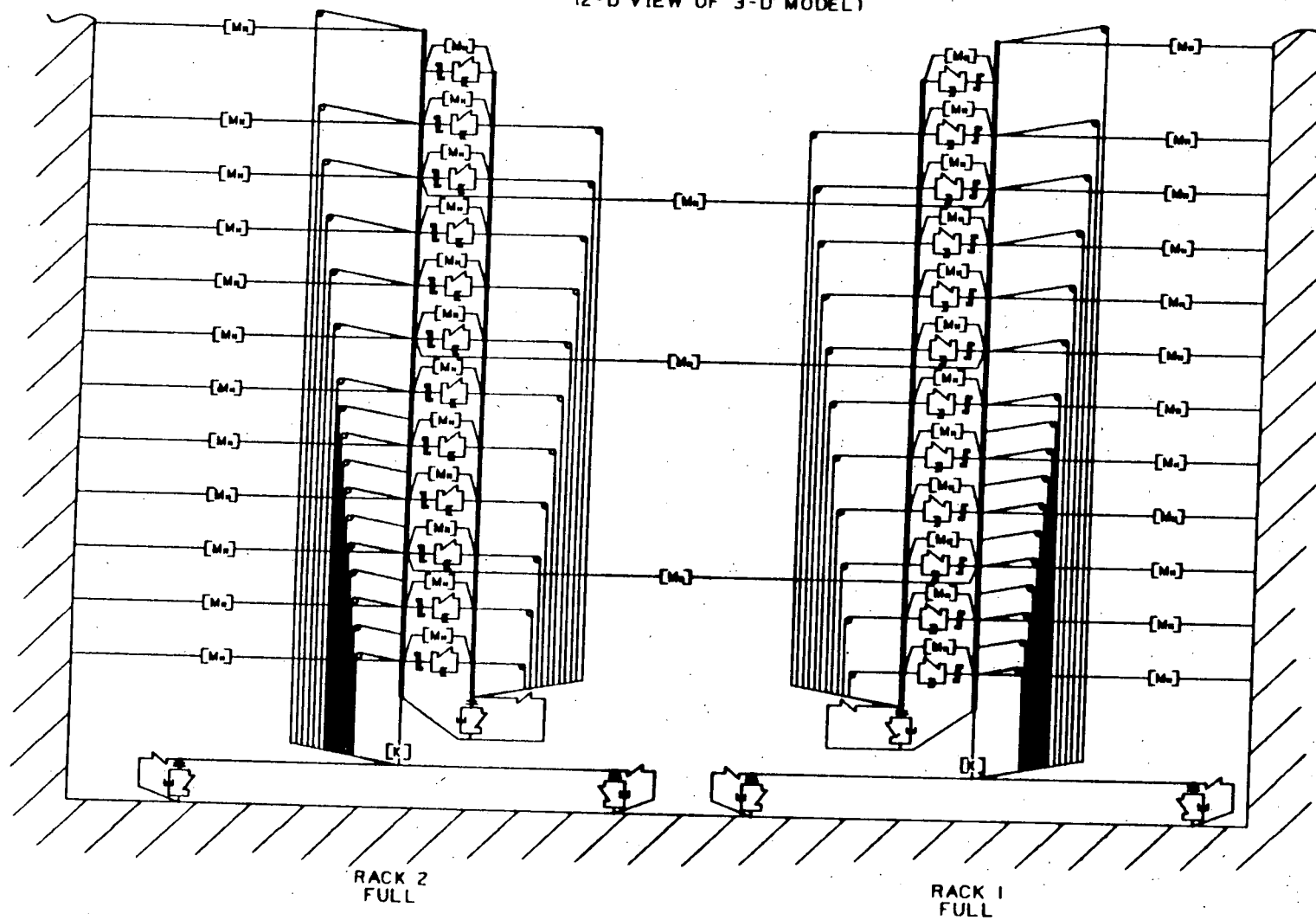


## **MULTIPLE RACK SEISMIC MODELS**

- **FULL/FULL**
- **FULL/EMPTY**



MULTIPLE RACK POOL MODEL, FULL/FULL  
(2-D VIEW OF 3-D MODEL)

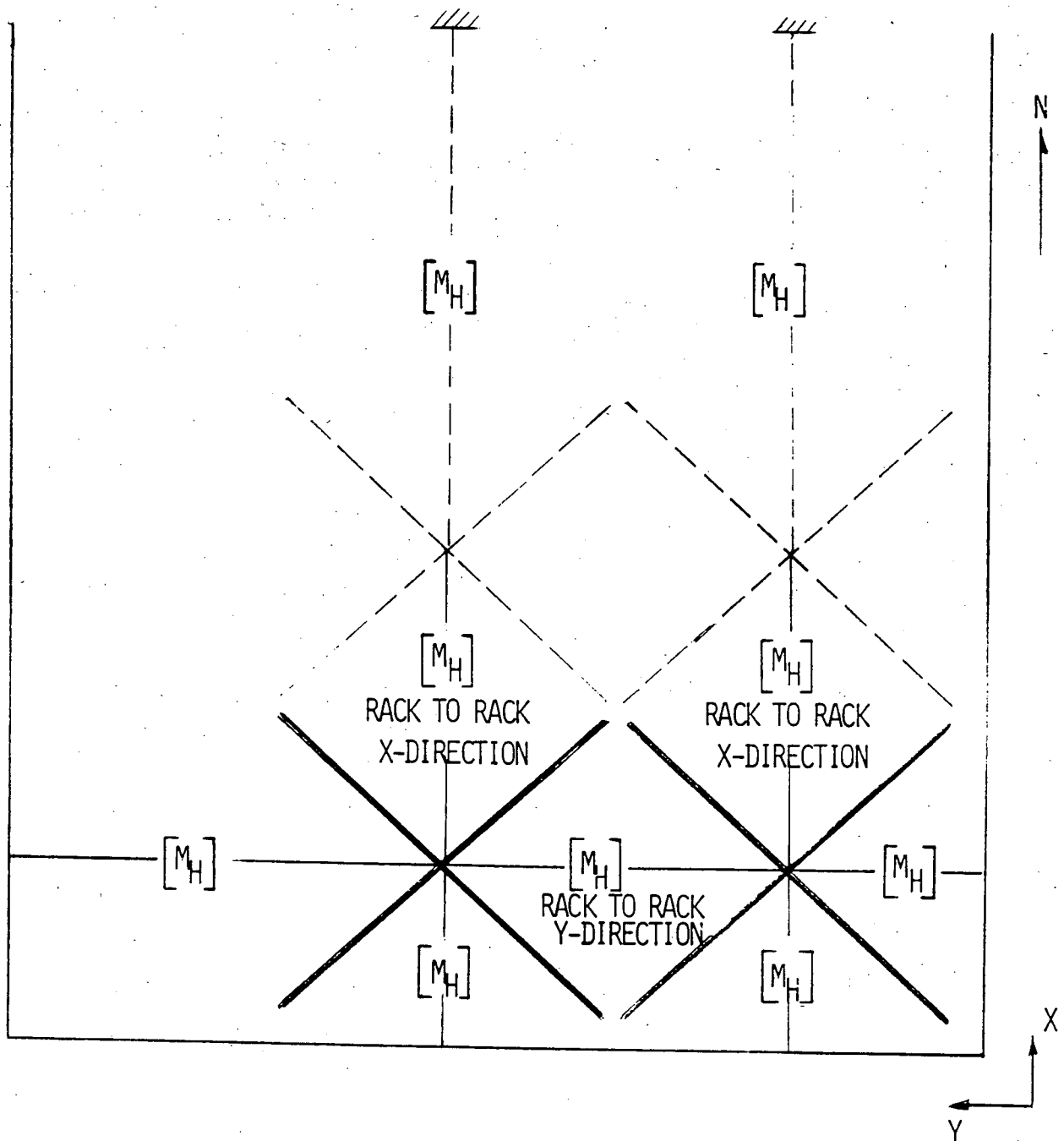


RACK 2  
EMPTY

RACK 1  
FULL

# MULTIPLE RACK POOL MODEL

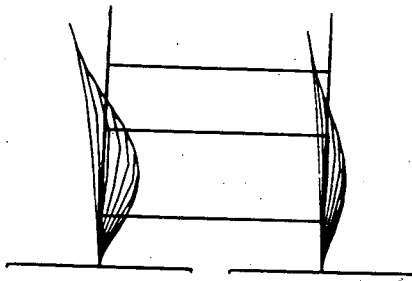
(PLAN VIEW)



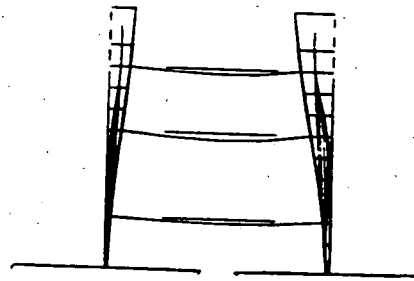
# MULTIPLE RACK MODULE MODE SHAPES

## REGION 2 STANDARD FUEL

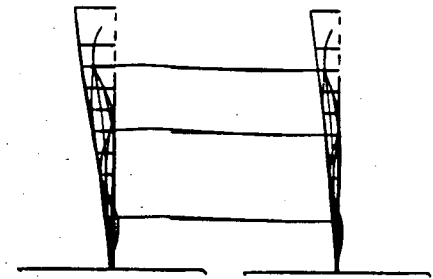
### FULL/FULL CONDITION



FUEL 2ND MODE  
4.6 Hz

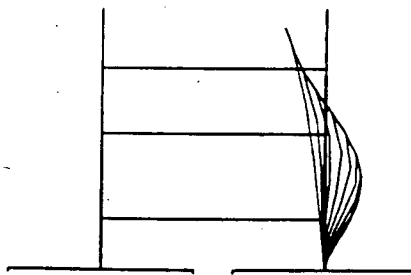


CELLS OUT-OF-PHASE  
8.3 Hz

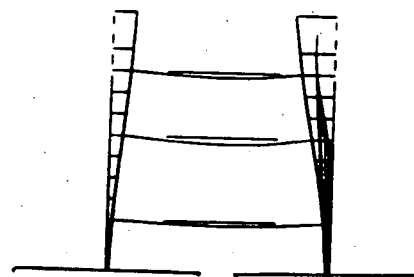


CELLS IN-PHASE  
14.5 Hz

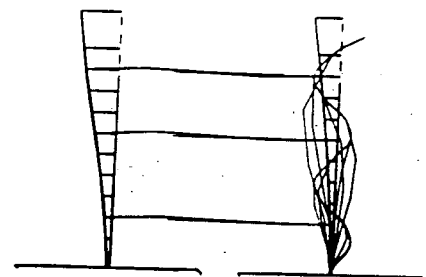
### EMPTY/FULL CONDITION



FUEL 2ND MODE  
4.6 Hz



CELLS OUT-OF-PHASE  
8.4 Hz



CELLS IN-PHASE  
15.2 Hz

## **DISPLACEMENT RESULTS**

- **RACK ABSOLUTE DISPLACEMENTS**
- **RACK RELATIVE DISPLACEMENTS**
- **DISPLACEMENT CHARACTERISTICS**

# SAN ONOFRE RACK DISPLACEMENT SUMMARY

MODEL TYPE*	Mu	Max Disp (in)		Rel Disp (in)		LOCATION	Frequency (Hz)	
		NS	EW	NS	EW		NS	EW
Reg. 1, Std, Full	.2	1.50	1.80	.33	.41	Top/Top	14.1	17.0
Reg. 1, Std, Full	.8	1.49	1.37	.84	.44	Top/Top	14.1	17.0
Reg. 1, Std, E/F	.2	1.30	1.51	1.39	.96	Top/Top	14.7	18.6
Reg. 1, Std, E/F	.8	1.42	1.60	.99	.90	Top/Top	14.7	18.6
Reg. 1, Std, Quad	.2	.39	.43	**	**	Top/Top	15.1	17.1
Reg. 1, Std, Quad	.8	.67	.33	**	**	Top/Top	15.1	17.1
Reg. 1, Std, Rows	.2	.33	.60	**	**	Top/Top	15.1	17.2
Reg. 1, Std, Rows	.8	.35	.64	**	**	Top/Top	15.1	17.2
Reg. 2, Std, Full	.2	1.00	1.39	.26	.59	Top/Top	13.8	14.1
Reg. 2, Std, Full	.8	1.44	1.36	.68	.76	Top/Top	13.8	14.1
Reg. 2, Std, E/F	.2	1.09	1.05	.99	.83	Top/Bot	14.2	15.2
Reg. 2, Std, E/F	.8	1.39	1.33	1.17	.96	Top/Top	14.2	15.2
Reg. 2, 2xStd, Full	.2	2.28	2.38	.44	.38	Bot/Top	11.7	12.0
Reg. 2, 2xStd, Full	.8	1.33	1.34	.87	.83	Top/Top	11.7	12.0
Reg. 2, 2xStd, E/F	.2	1.29	1.37	1.27	1.22	Bot/Bot	13.1	14.5
Reg. 2, 2xStd, E/F	.8	1.40	1.14	.98	.79	Top/Top	13.1	14.5

## \* Loading Conditions

Four terms are used to define the different loading conditions. They are defined as follows. Full is used to describe the fully loaded situation. E/F describes a case where one rack is full and another is empty. Quad represents a single rack case where one quadrant only is loaded. Rows describes a case where only four rack rows are loaded. Finally, 2xStd represents a fuel assembly with double mass, increased beam stiffness, and increased hydrodynamic mass.

\*\* These are single rack cases. Relative Displacements do not apply.

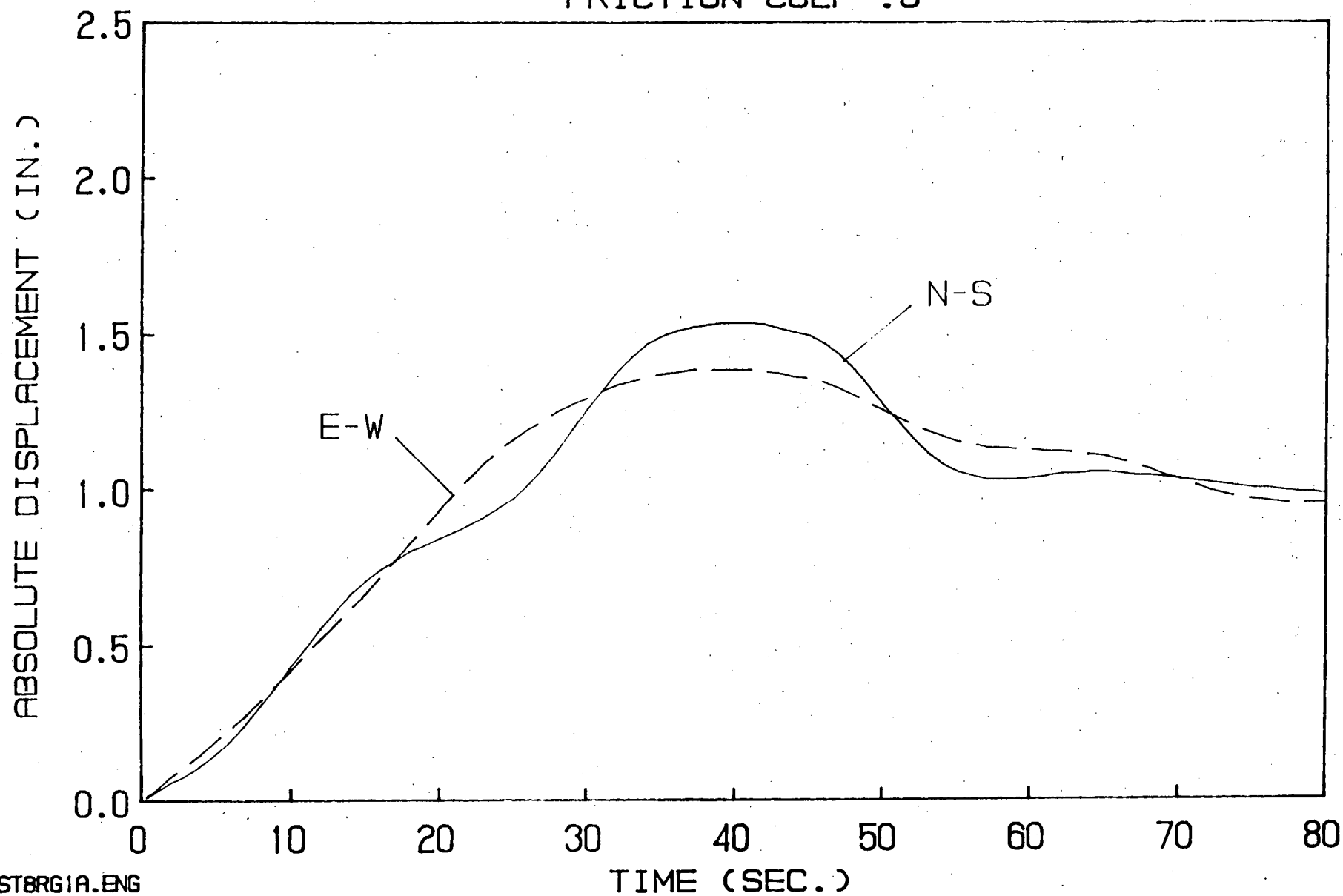
**MAXIMUM ABSOLUTE DISPLACEMENTS  
UNITS (IN.)**

Friction Coefficient	Region 1		Region 2			
	Standard Fuel		Standard Fuel		2xStandard Fuel	
	Full-Full		Full-Full		Full-Full	
	N-S	E-W	N-S	E-W	N-S	E-W
.2	1.50	1.80	1.09*	1.39	2.28	2.38
.8	1.49	1.60*	1.44	1.36	1.33	1.34

\* Empty-Full Condition

# MAXIMUM ABSOLUTE DISPLACEMENT PLOT

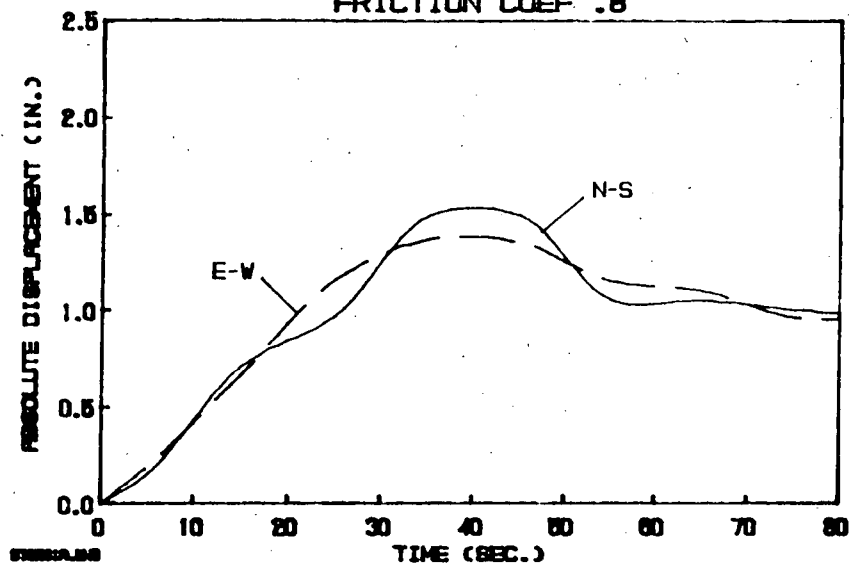
REGION 1  
STANDARD FUEL  
FULL/FULL  
FRICTION COEF .8



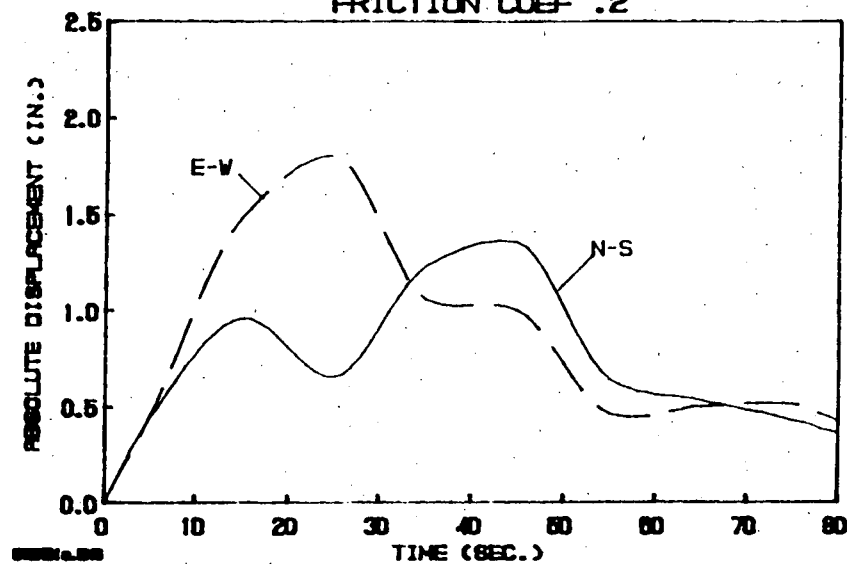


# MAXIMUM ABSOLUTE DISPLACEMENT PLOTS

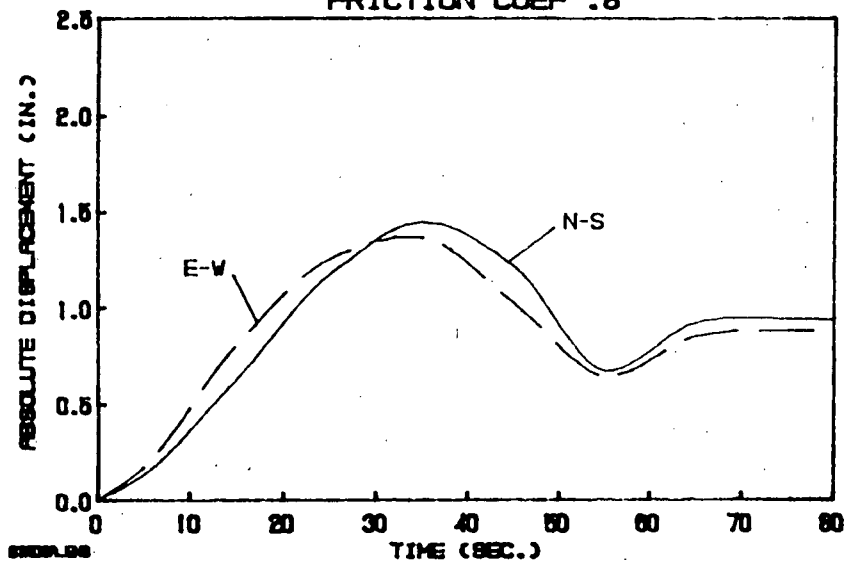
REGION 1  
STANDARD FUEL  
FULL/FULL  
FRICTION COEF .8



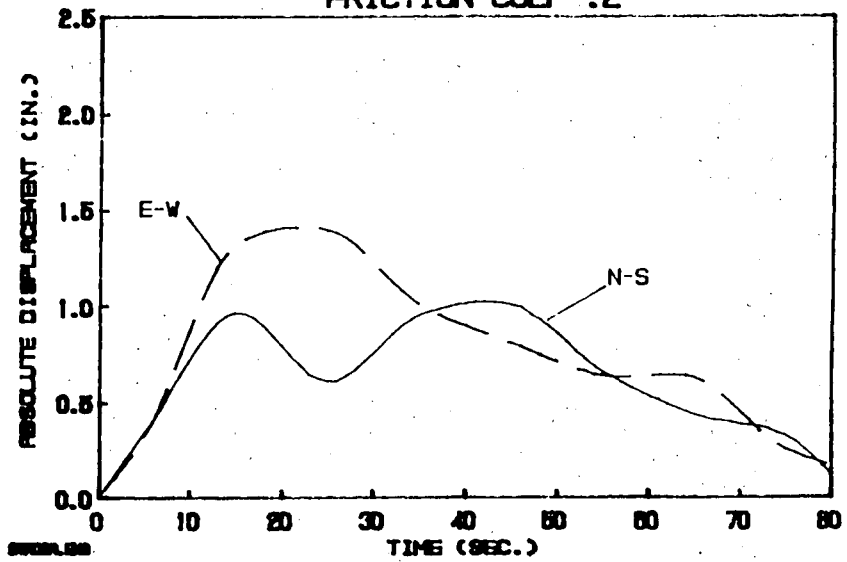
REGION 1  
STANDARD FUEL  
FULL/FULL  
FRICTION COEF .2



REGION 2  
STANDARD FUEL  
FULL/FULL  
FRICTION COEF .8



REGION 2  
STANDARD FUEL  
FULL/FULL  
FRICTION COEF .2



**MAXIMUM RELATIVE DISPLACEMENTS  
UNITS (IN.)**

Friction Coefficient	Region 1		Region 2			
	Standard Fuel		Standard Fuel		2xStandard Fuel	
	Empty-Full		Empty-Full		Empty-Full	
	N-S	E-W	N-S	E-W	N-S	E-W
.2	1.39	.96	.99	.83	1.27	1.22
.8	.99	.90	1.17	.96	.98	.83*

\* Full-Full Condition

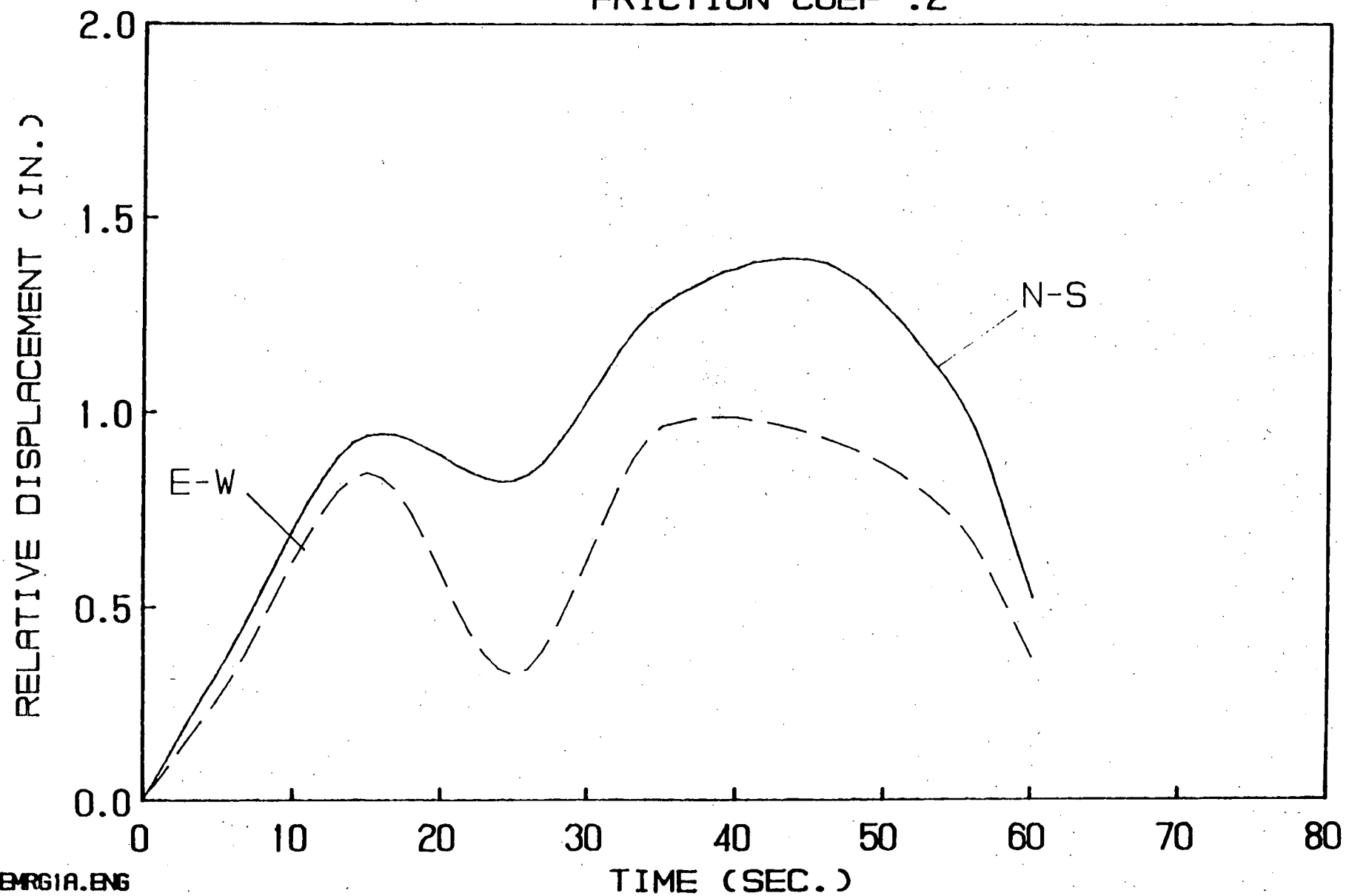
# MAXIMUM RELATIVE DISPLACEMENT PLOT

REGION 1

STANDARD FUEL

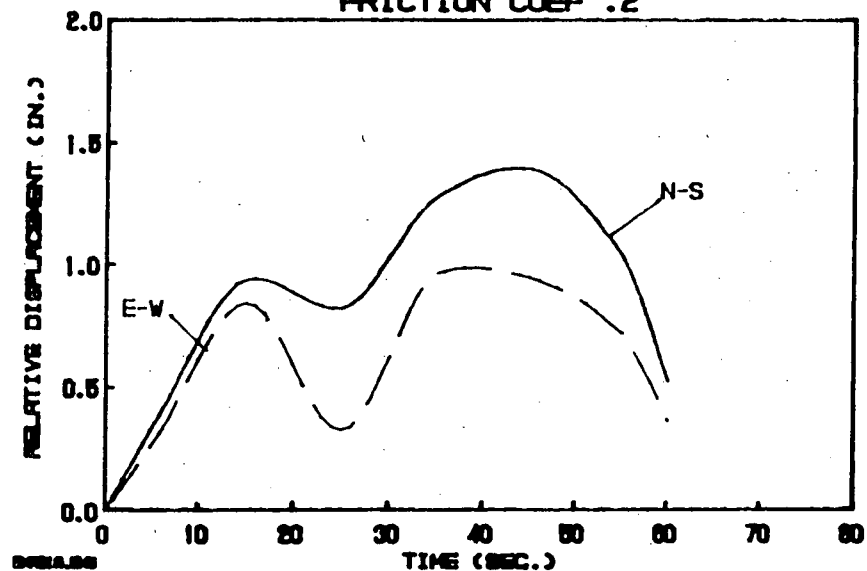
EMPTY/FULL

FRICTION COEF .2

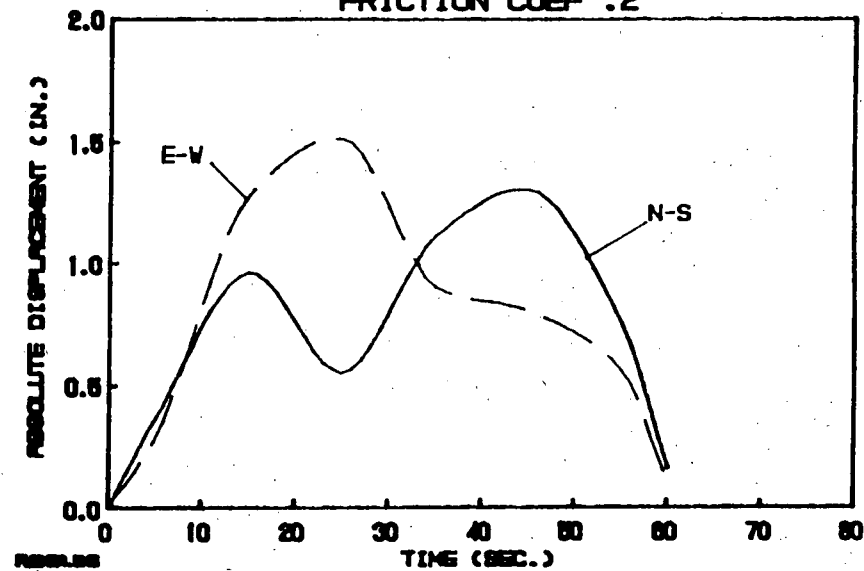


# MAXIMUM RELATIVE/ABSOLUTE DISPLACEMENT PLOTS

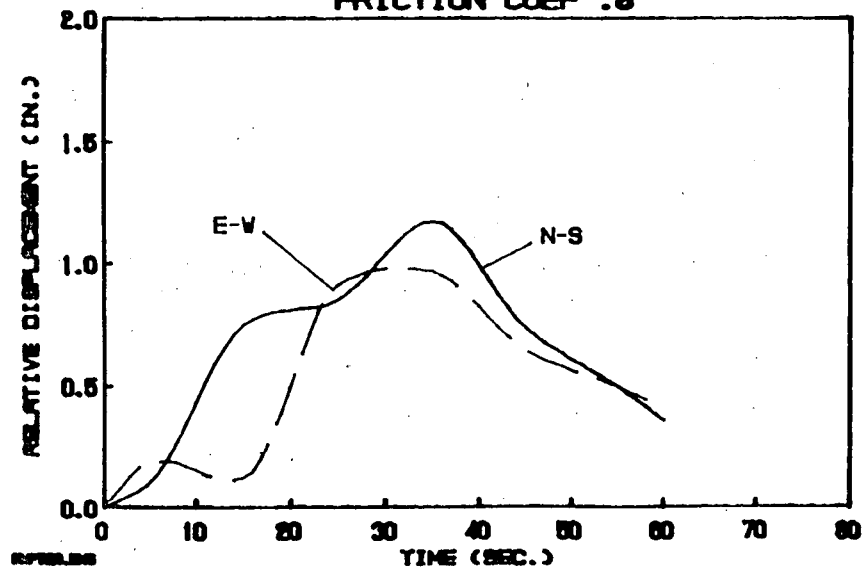
REGION 1  
STANDARD FUEL  
EMPTY/FULL  
FRICTION COEF .2



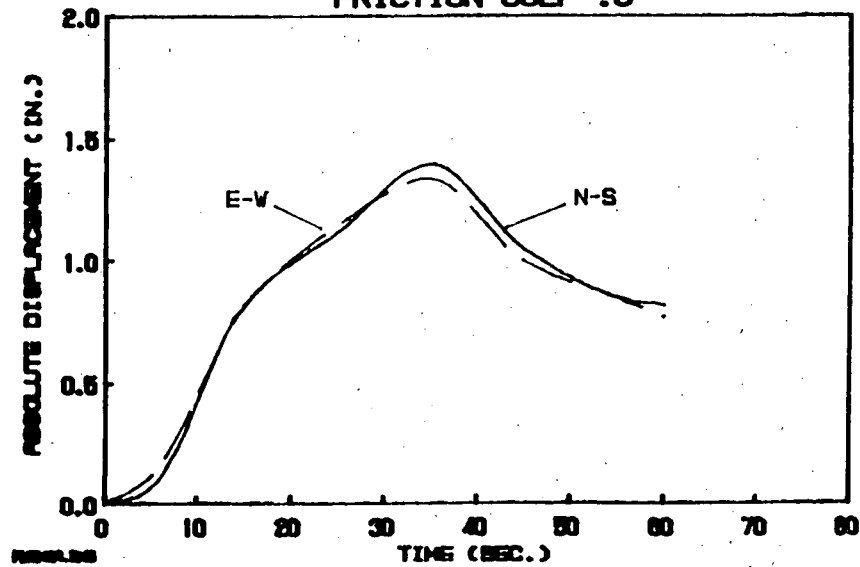
REGION 1  
STANDARD FUEL  
EMPTY/FULL  
FRICTION COEF .2



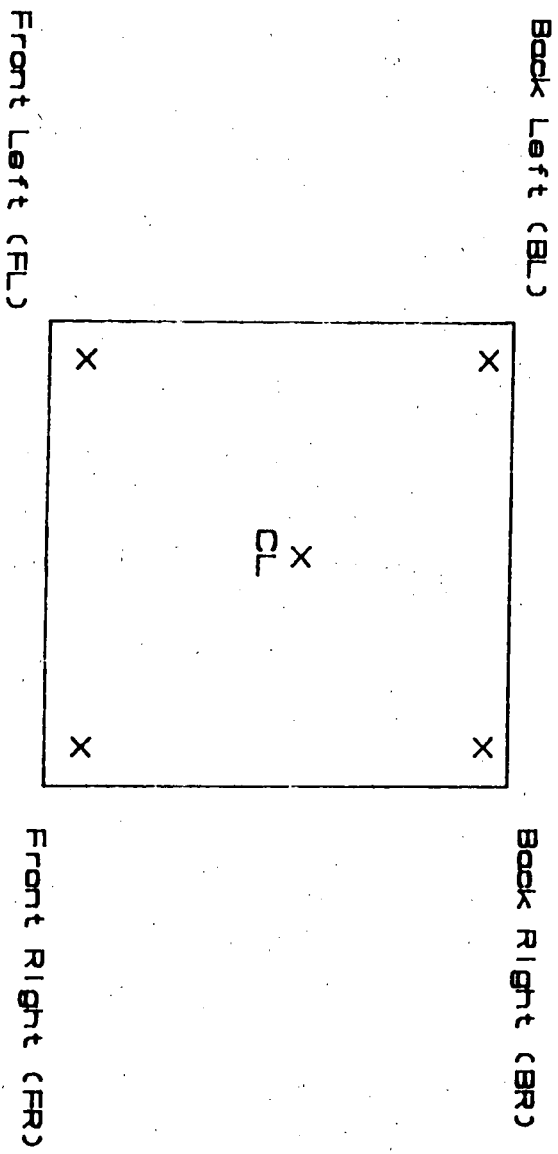
REGION 2  
STANDARD FUEL  
EMPTY/FULL  
FRICTION COEF .8



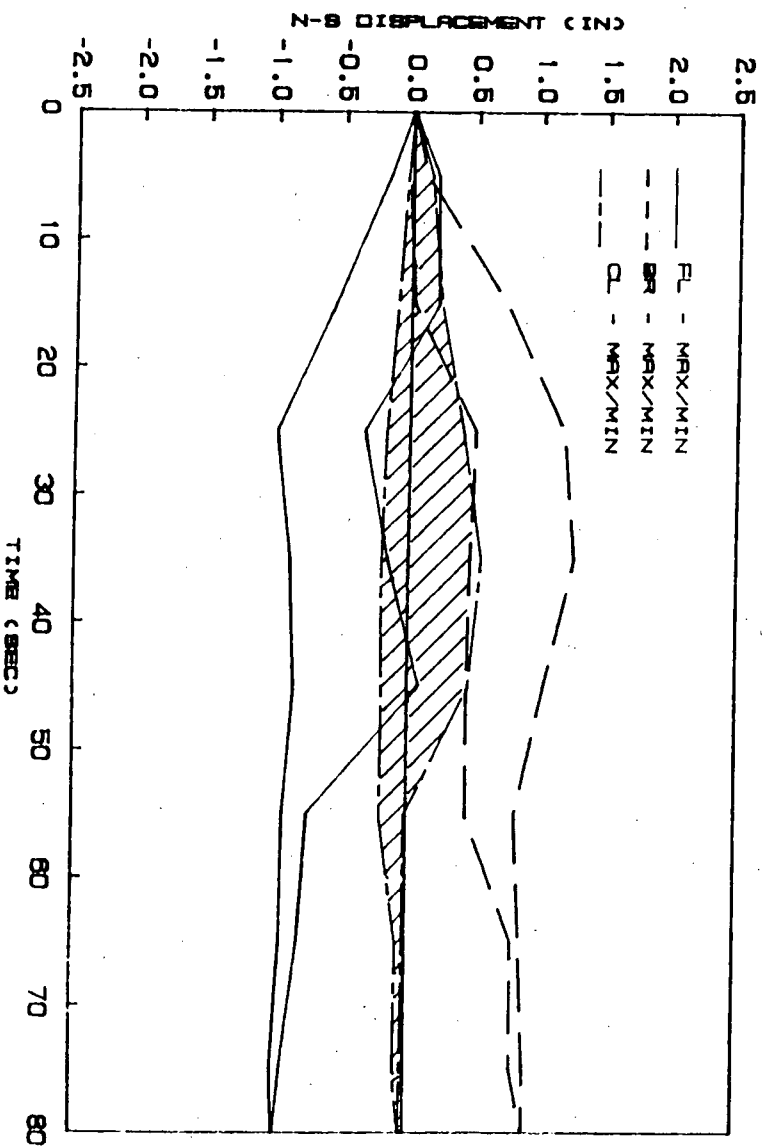
REGION 2  
STANDARD FUEL  
EMPTY/FULL  
FRICTION COEF .8



# TORSIONAL VS SLIDING MOTION



RACK 1  
STANDARD FUEL  
FULL/FULL. FRICTION COEF. = 0.8

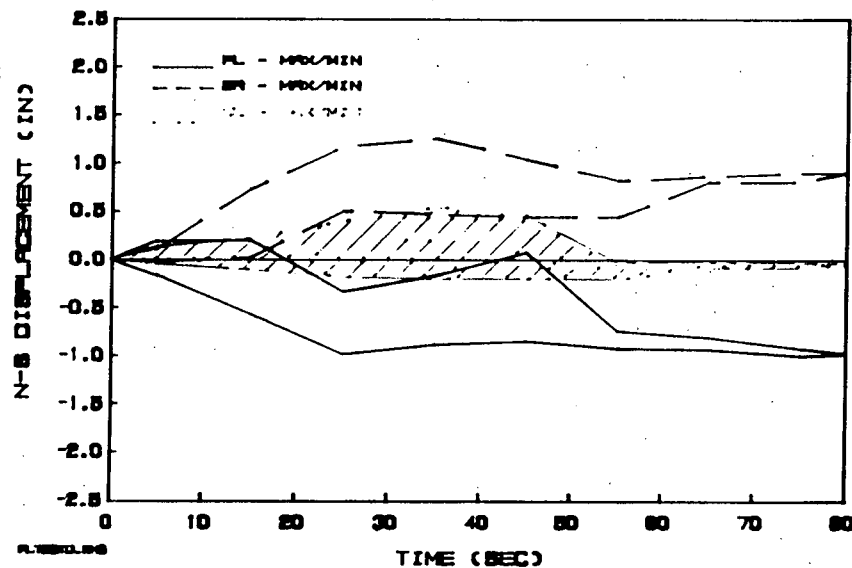


# SLIDING/TORSION DISPLACEMENT CHARACTERISTICS

RACK 1

STANDARD FUEL

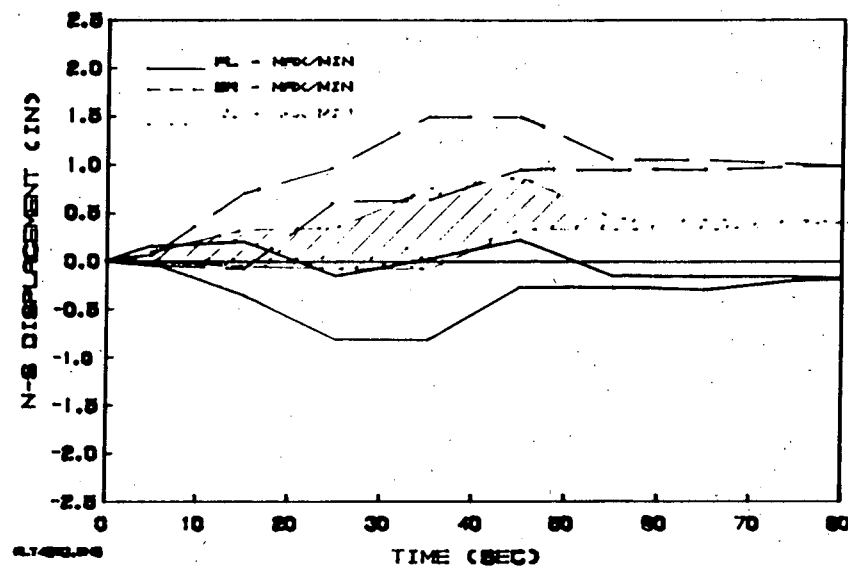
FULL/FULL. FRICTION COEF. - 0.8



RACK 2

STANDARD FUEL

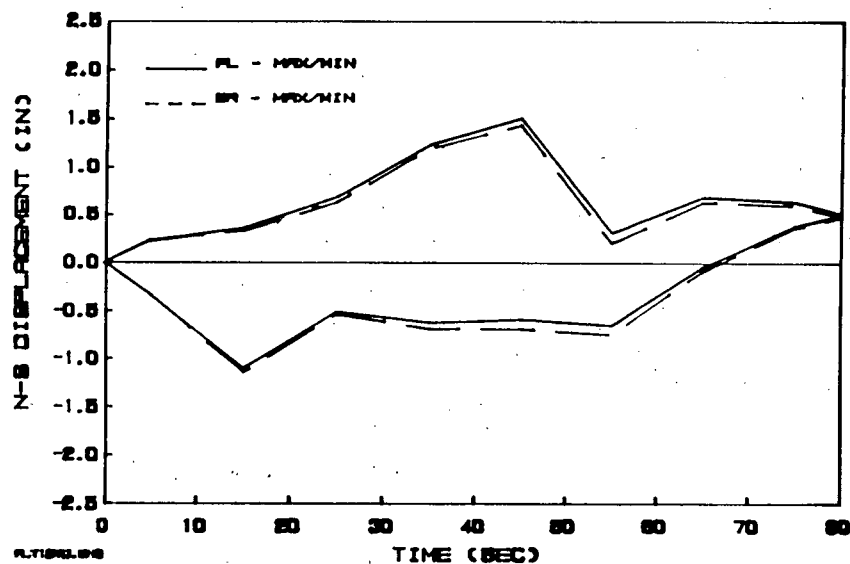
FULL/FULL. FRICTION COEF. - 0.8



RACK 1

STANDARD FUEL

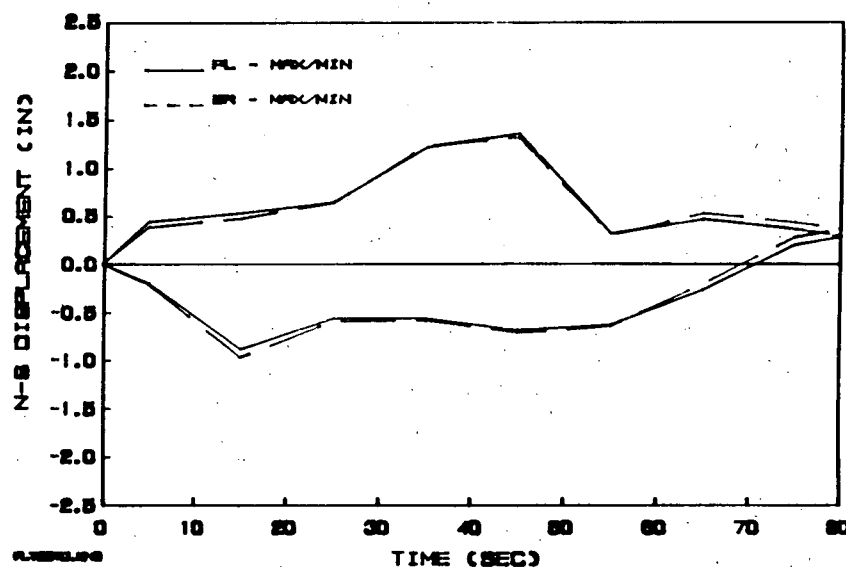
FULL/FULL. FRICTION COEF. - 0.2



RACK 2

STANDARD FUEL

FULL/FULL. FRICTION COEF. - 0.2



## **CONSERVATISMS**

## CONSERVATISMS

1. ALL FUEL ASSEMBLIES RESPOND IN PHASE.
2. FRICTION COEFFICIENTS OF 0.8 MAXIMUM AND 0.2 MINIMUM.
3. FUEL ASSEMBLY GRID IMPACT DAMPING OF 4.4%.
4. HYDRODYNAMIC MASS BASED UPON CONSTANT GAPS. AS GAP DECREASES THE HYDRODYNAMIC MASS RESTORING FORCE INCREASES, BUT SINCE THE ANALYSIS IS BASED UPON CONSTANT GAPS, THE DISPLACEMENTS WHICH CLOSE THE GAPS ARE CONSERVATIVE.
5. THE SEISMIC MODEL, WHICH USES 4 EFFECTIVE SUPPORT PADS TO REPRESENT THE 26 TO 33 ACTUAL SUPPORT PADS, ROCKED ONTO ONE SUPPORT PAD AND PRODUCED ROTATIONAL MOTION. SINCE THE ACTUAL RACK MODULE HAS MULTIPLE INTERIOR SUPPORT POINTS AND WILL NOT LIFT OFF ONTO ONE SUPPORT POINT, THE SUPPORT PADS IN CONTACT WILL RESIST THE ROTATIONAL MOTION.
6. NO FRICTION USED IN SUPPORT PAD BALL JOINT TO RESIST ROTATION WHEN RACK ROCKS ONTO ONE PAD.
7. GAPS BETWEEN FUEL AND CELL WERE MAXIMIZED AND PRODUCE THE MAXIMUM IMPACT FORCES.
8. MARGIN OF SAFETY AGAINST RACK IMPACT BASED UPON THE MINIMUM GAP DURING SEISMIC EVENT.



## **SUMMARY/CONCLUSIONS**

- **SOPHISTICATED AND REALISTIC DYNAMIC MODEL USED IN ANALYSIS**
- **EVALUATED MANY CASES AND DETERMINED BOUNDING CASES**
- **DESIGN BASIS IS FROM MULTIPLE RACK MODEL**
- **RACK TO RACK AND RACK TO WALL IMPACT DOES NOT OCCUR**
- **REMAINING SEPARATION RESULTS IN COMFORTABLE MARGIN OF SAFETY**

IV. SUMMARY

(SCE)

DERRICK MERCURIO

NRC SEISMIC DESIGN INFORMATION REQUESTS  
FROM THE JUNE 3, 1988 NRC MEETING  
SAN ONOFRE UNITS 2 AND 3

1. PROVIDE A STRENGTH EVALUATION FOR THE GROUND MOTION DBE TIME HISTORY.
2. DESCRIBE THE CHANGES IN RACK FREQUENCY WITH WELD SIZE AND CLIPS, AND INCLUDE DESCRIPTIONS OF THE SIZES AND NUMBERS OF WELDS AND CLIPS.
3. PROVIDE ASSURANCE THAT RACK-TO-RACK SPACING IS MAINTAINED.
4. COMPLETELY ADDRESS RACK-TO-RACK AND RACK-TO-WALL INTERACTIONS.
5. EXPLAIN ANY EFFECT OF THE RACK LEVELING PAD ON ROCKING OR LIFTING FROM SEISMIC INPUTS.
6. JUSTIFY SRSS COMBINATIONS OF ADJACENT RACK DISPLACEMENTS.
7. INCLUDE ROTATION ABOUT ONE RACK SUPPORT FOOT AS A POTENTIAL WORST CASE DISPLACEMENT.
8. EXPLAIN HOW HIGH FREQUENCY IMPACT LOADS ARE CALCULATED WITH THE PROPOSED RACK MODEL.
  - A. DESCRIBE IN DETAIL HOW THE RACK CELL WALLS ARE DESIGNED INCLUDING THE FUEL ELEMENT/CELL WALL IMPACT MODEL.
  - B. IN MODELING THE FUEL ASSEMBLY-RACK CELL GAP WIDTH, THE GAP SHOULD BE MAXIMIZED BY INCLUDING TOLERANCES.
  - C. DEMONSTRATE THAT THE ANALYSES ENVELOPE DIFFERENT HYDRODYNAMIC MASS AND GAP SIZE CONDITIONS.
9. ADDRESS ANALYSES UNCERTAINTIES TO VERIFY THE RACK MODEL DYNAMIC CHARACTERISTICS.
10. IF VERTICAL ACCELERATION EXCEEDS 1G, INCLUDE THE IMPACT EFFECTS IN THE FUEL CELL ANALYSES.
11. INCLUDE AN ADEQUATE RANGE OF FUEL ASSEMBLY STIFFNESS (INCLUDING IMPACT STIFFNESS) TO ENCOMPASS CURRENT AND FUTURE FUEL.

#### IV. SUMMARY

- 0 2/1/89 - SUBMITTAL OF PROPOSED LICENSE AMENDMENT
  - PROVIDE COMPLETE RERACKING ANALYSES AND LICENSE AMENDMENT REQUEST
- 0 3/30/89 - BEGIN RACK FABRICATION
- 0 8/1/89 - NRC ISSUE LICENSE AMENDMENT

SPENT FUEL POOL RERACKING

SAN ONOFRE UNITS 2 AND 3

December 7, 1988

Issues to be Addressed in the License Amendment Request

1. Structural and Effective Structural Properties.
  - A. Analysis method and calculation to determine the structural properties of the cell-to-cell weld shear connection for the structural model.
  - B. Analysis method and calculation to determine the effective rotational stiffness properties of the cell-to-cell connections for the effective structural model.
  - C. Analysis method and calculation to determine the effective rotational stiffness properties of the fuel rack base for the effective structural model.
  - D. The basis for the use of rigid beams in the base of the nonlinear model. "Rigid base plate"
2. Hydrodynamic Mass.
  - A. Details of the hydrodynamic mass calculation.
  - B. Justification of the hydrodynamic mass simulation in the N-S direction (4 rack configuration).
3. Maximum support pad lift-off and margin against overturn.
4. Uncertainties and conservatisms.
5. WECAN Code.
  - A. Information on method and verification solutions on the nonlinear model superposition method. Justify its validity in case of multiple non-linearities.
  - B. List of licensees where WECAN was reviewed by NRC.
6. Engineering explanation of the relationship between the values of rack relative displacements for the N-S and E-W directions. Why does N-S exceed E-W?
7. Reference test data which may be used to substantiate rack parameters.

8. Stresses in rack components.
9. Interface loads and effects on pool.
10. Confirm earthquake time history inputs are compatible with FSAR.
11. Rack-to-rack and rack-to-wall gap adequacy, including installation tolerances
12. Walkdown requirements after a seismic event.

TDM:0633n