

ENCLOSURE 1

LOSS OF SECONDARY COOLANT

**REGULATORY DOCKET FILE COPY**

BASIC ACTIONS

GENERIC SECONDARY LINE BREAK

1. VERIFY STEAMLINE ISOLATION
2. IDENTIFY FAULTED STEAM GENERATOR
3. ISOLATE AFW TO FAULTED STEAM GENERATOR
4. RESTORE LEVEL IN NON-FAULTED STEAM GENERATORS
5. TERMINATE SAFETY INJECTION
  - . PTS CONCERN
  - . HEATUP CONCERN
6. GO TO COLD SHUTDOWN CONDITIONS USING RHR SYSTEM

SI TERMINATION CRITERIA

	<u>PTS</u>	<u>HEATUP</u>
RCS PRESSURE	X	X
PRESSURIZER LEVEL	X	X
RCS SUBCOOLING	X	X
SECONDARY HEAT SINK *	X	X

\* STEAM GENERATOR LEVEL OR AFW FLOW

## BASIC ACTIONS

### SONGS #1 SECONDARY LINE BREAK

1. VERIFY AFW FLOW TO STEAM GENERATOR
2. IDENTIFY (IF POSSIBLE) TYPE AND LOCATION OF BREAK  
- ISOLATE AFW TO STEAM GENERATOR WITH FEEDLINE BREAK
3. ATTEMPT TO RESTORE LEVEL IN STEAM GENERATORS
4. REGULATE AFW TO ALL STEAM GENERATORS TO MAINTAIN 100 DEGREES PER HOUR COOLDOWN
5. TERMINATE SI/REGULATE CHARGING
  - . PTS CONCERN
  - . HEATUP CONCERN
6. GO TO COLD SHUTDOWN CONDITIONS USING RHR SYSTEM

### SI TERMINATION CRITERIA

	<u>PTS</u>	<u>HEATUP</u>
RCS PRESSURE	X	X
PRESSURIZER LEVEL	X	X
RCS SUBCOOLING	X	X
SECONDARY HEAT SINK *	X	X

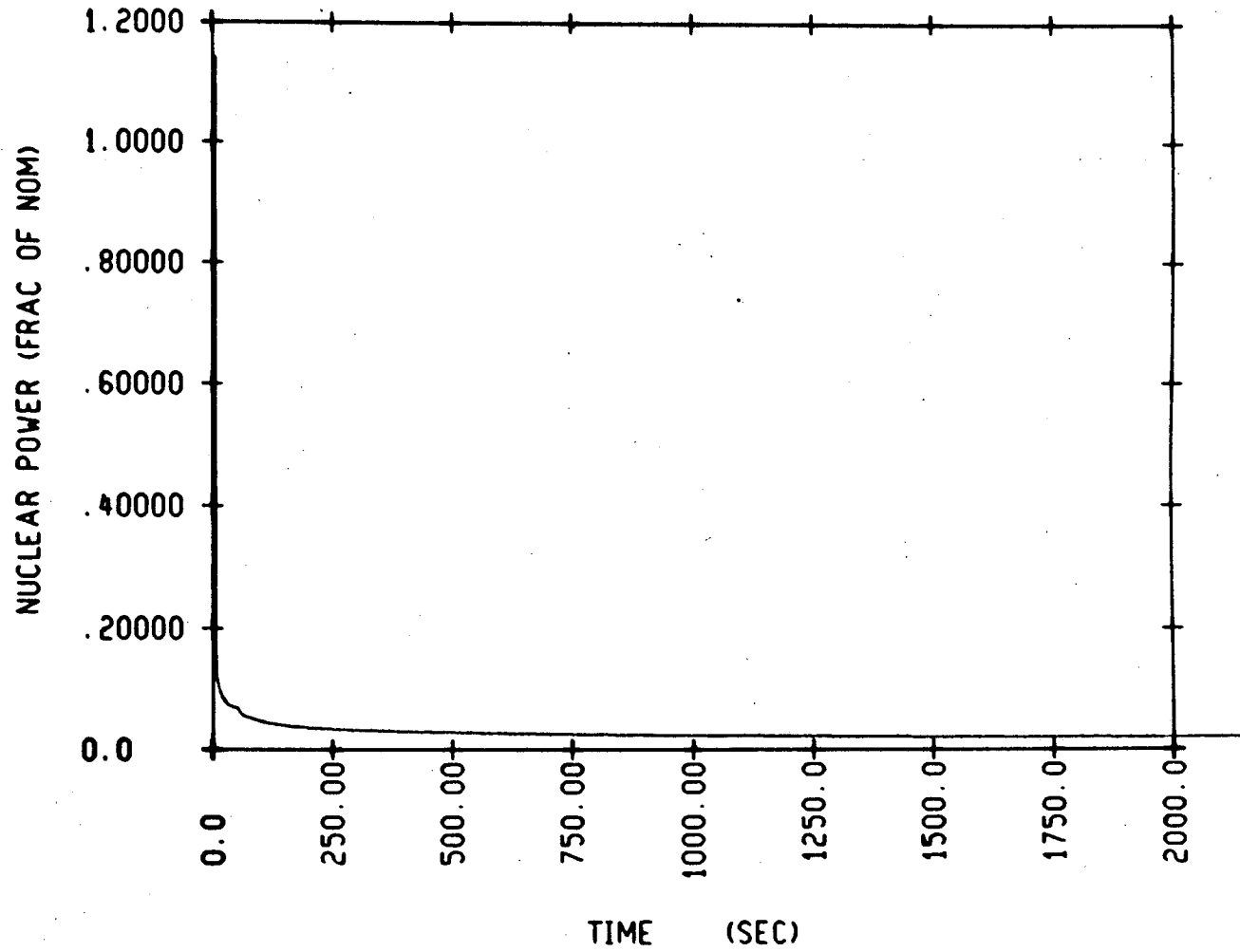
\* AFW FLOW AND RCS TEMPERATURES STABLE OR DECREASING

## FULL POWER DE STEAMLINE BREAK

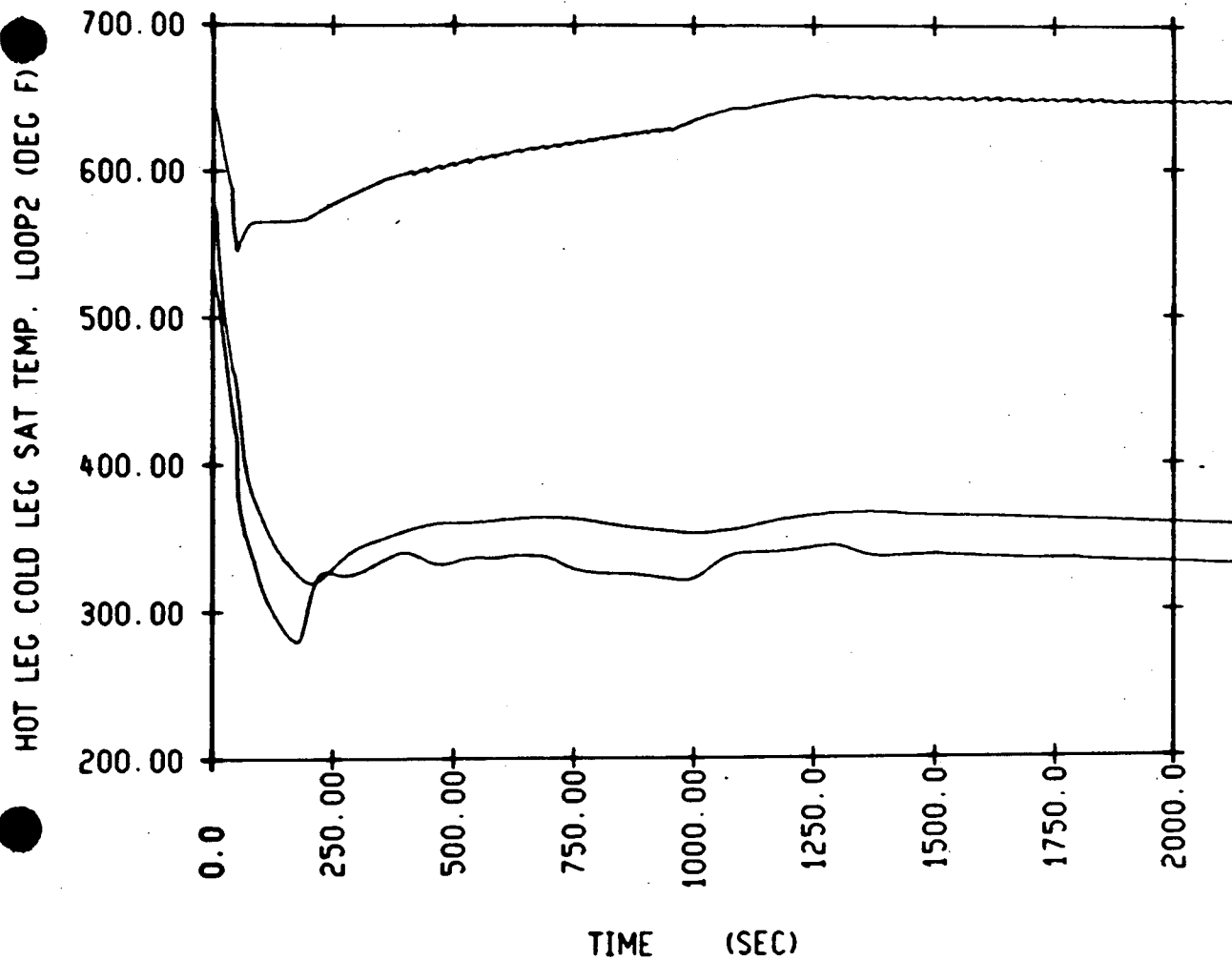
<u>EVENT</u>	<u>TIME</u>
PIPE RUPTURE	0
REACTOR TRIP (HIGH NEUTRON FLUX)	4.8
ROD MOTION	5.3
SI INITIATION (LOW PRESSURIZER PRESSURE)	20.5
RCP TRIP	22.5
MFW ISOLATION	22.5
SI SYSTEM ALIGNED AND RUNNING	42.5
STEAM GENERATOR DRYOUT	200.0
M/D AFW PUMPS STARTED (300 GPM)	322.5
MAIN FEEDLINES PURGED	650.0
OPERATOR ACTION (AFW TROTTLED TO 75 GPM)	950.0
OPERATOR ACTION (AFW TROTTLED TO 200 GPM)	1250.0

$$DE = 1.12 \text{ FT}^2/\text{LOOP}$$

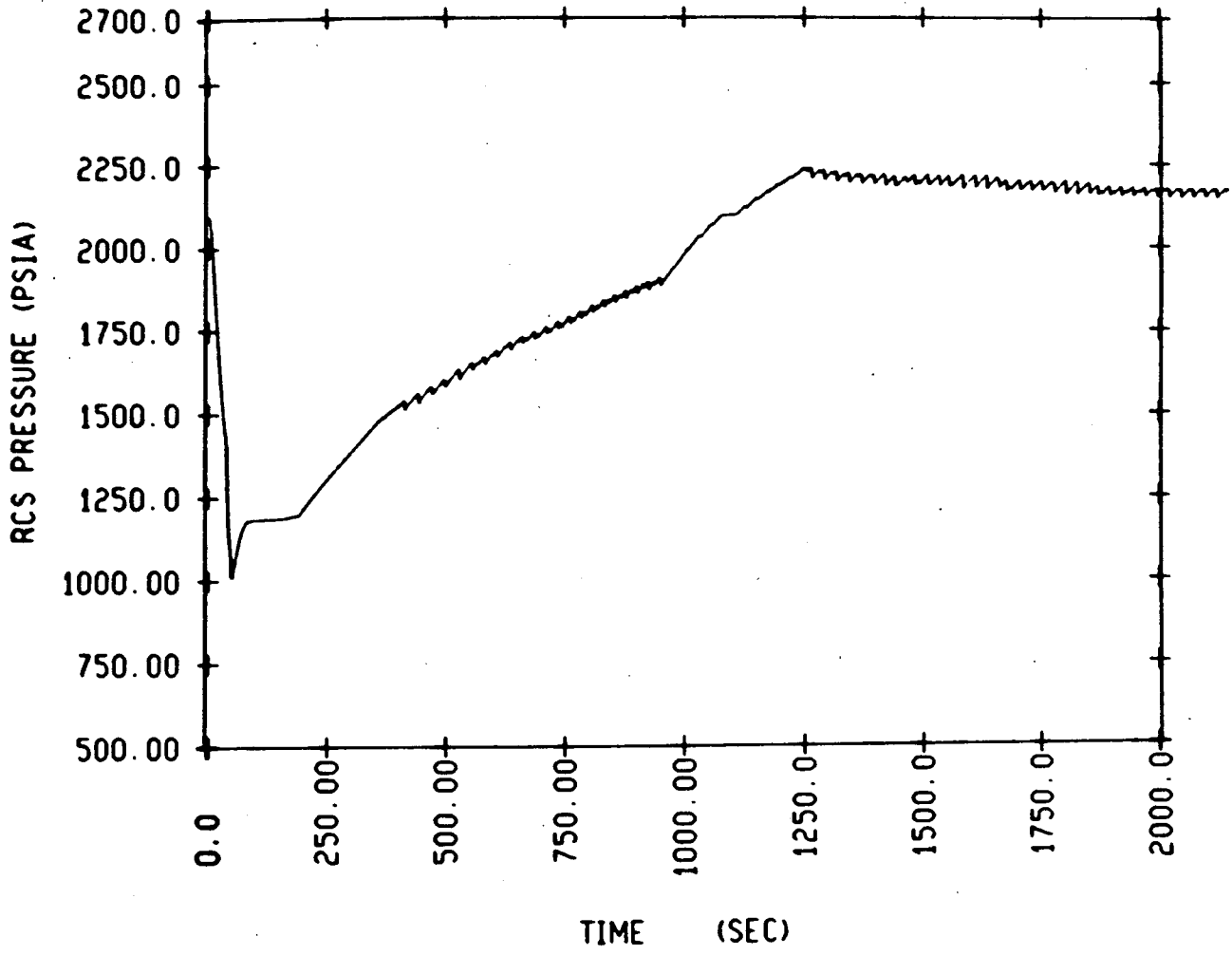
SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT27 RUN 1



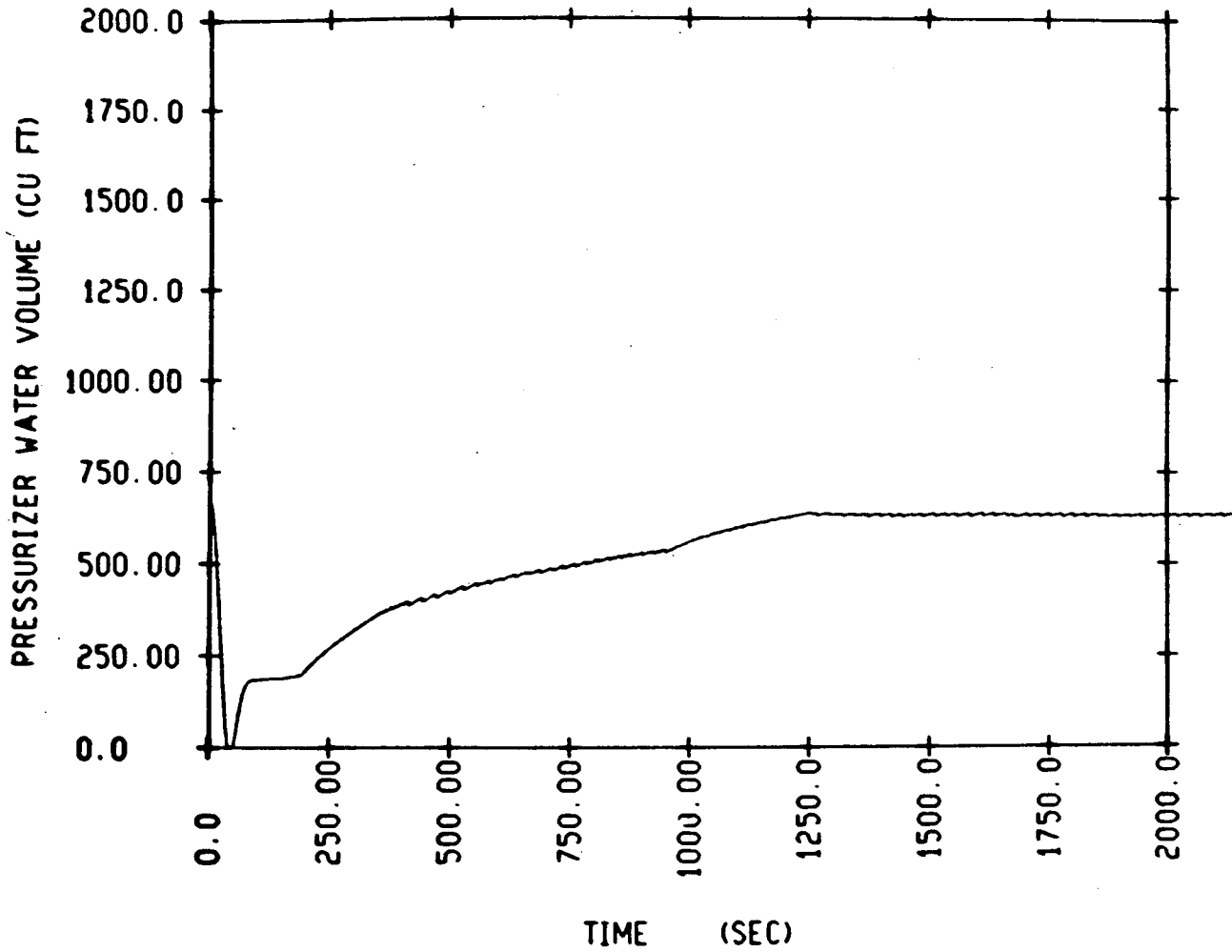
SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT42 RUN 1



SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT29 RUN 1

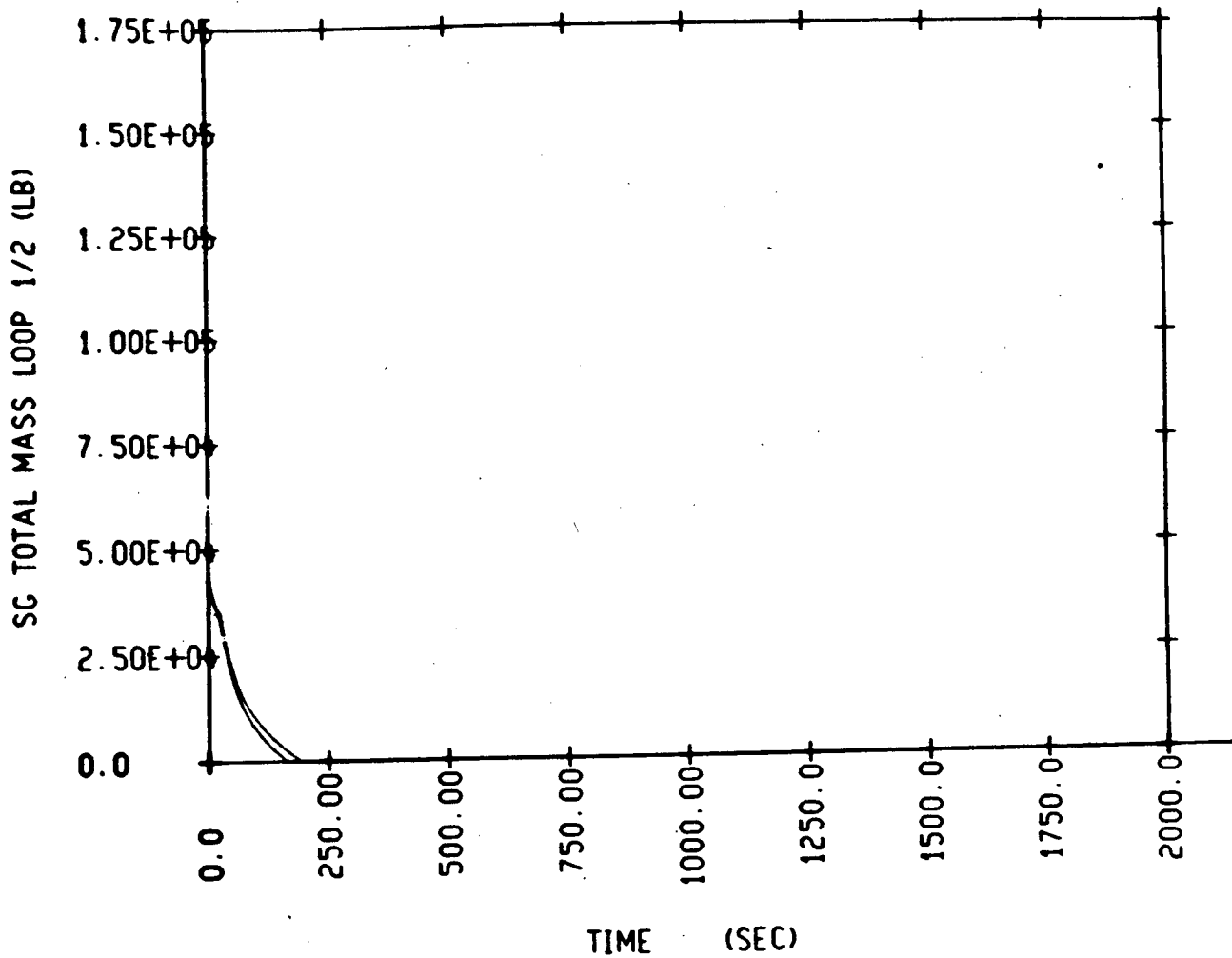


SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT31 RUN 1

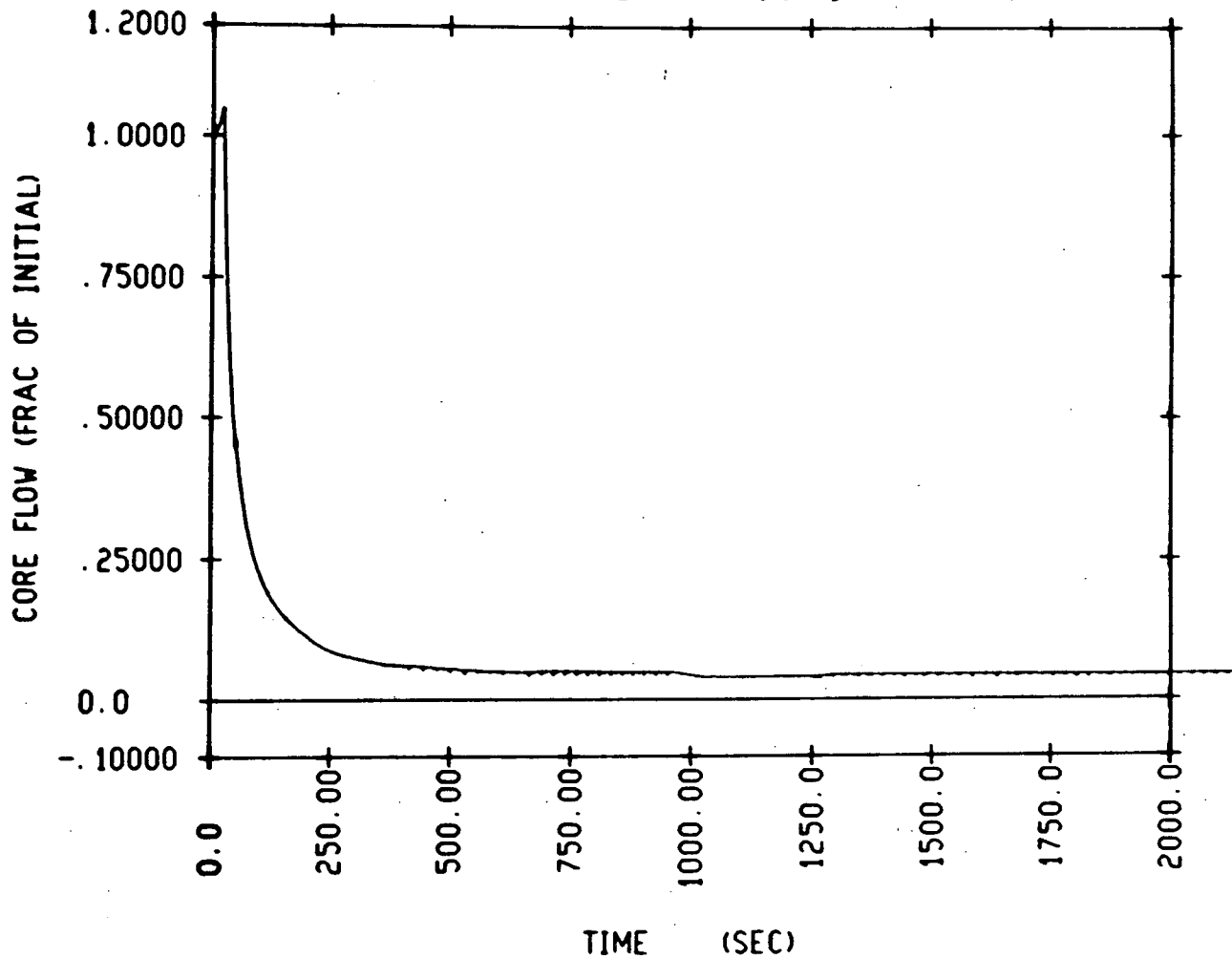




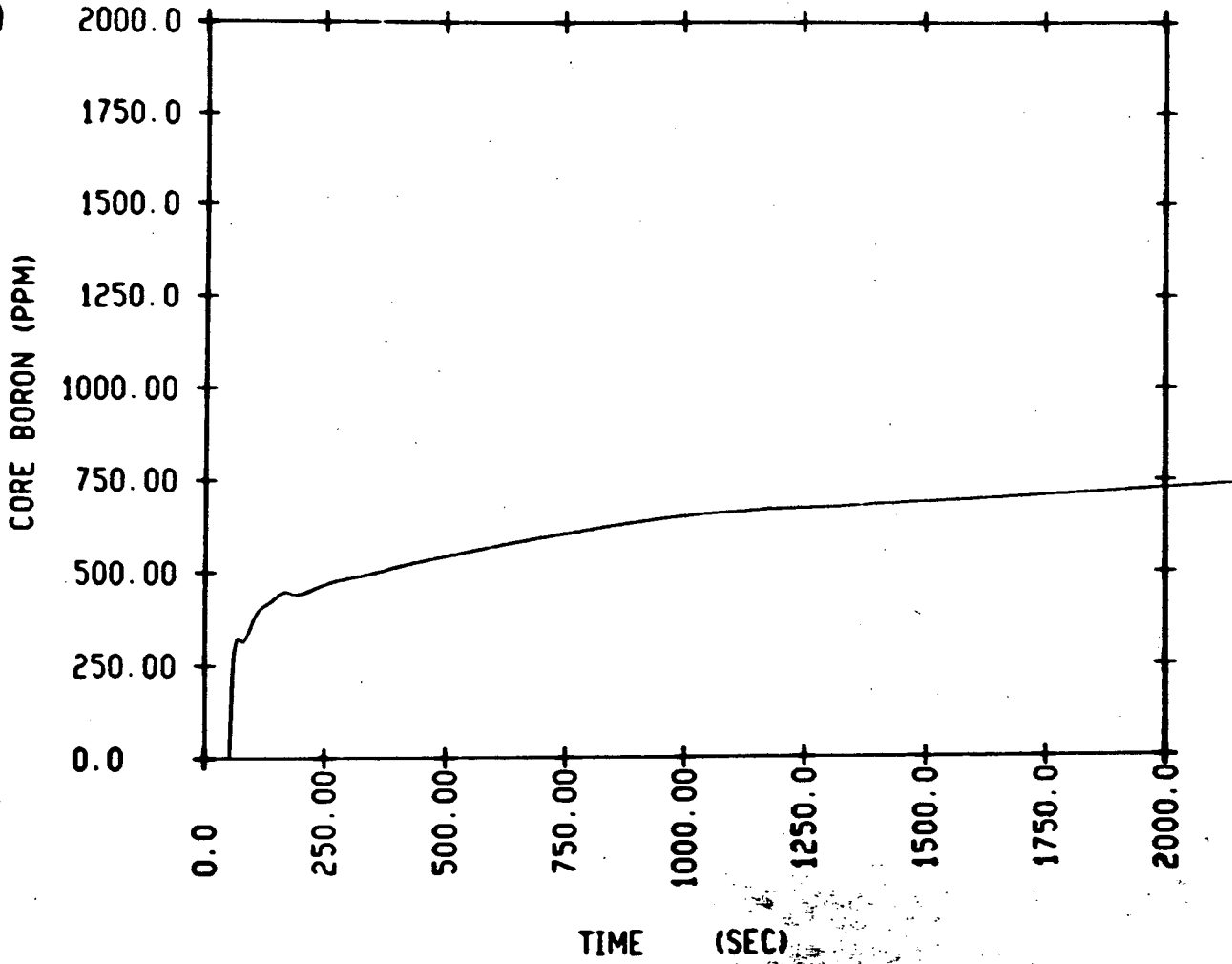
SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT45 RUN 1



SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT32 RUN 1



SCE BETTER EST. STMBRK AT 100 PC POW OUTSIDE W/POW  
SCE BASE DECK  
PLOT50 RUN 1

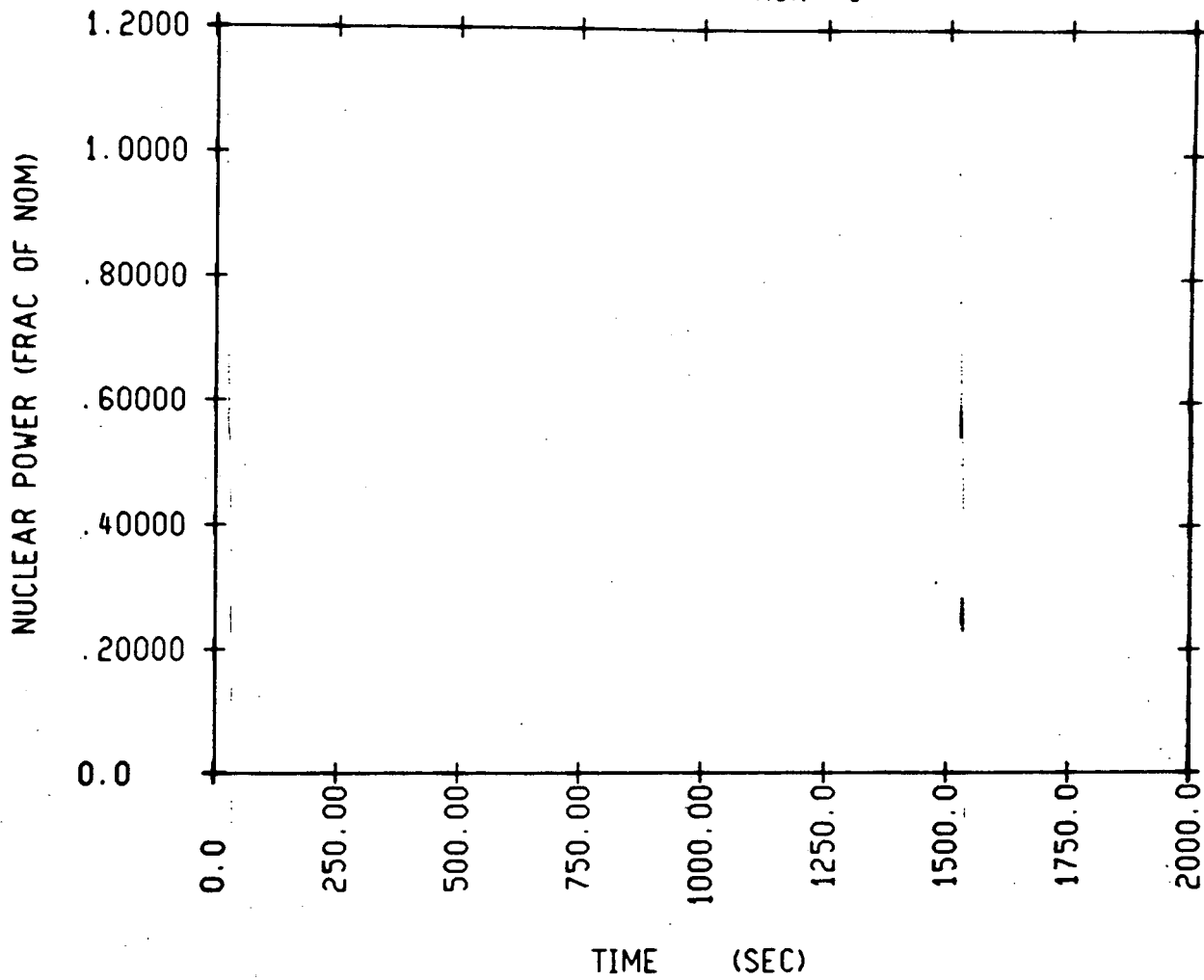


## ZERO POWER DE STEAMLINE BREAK

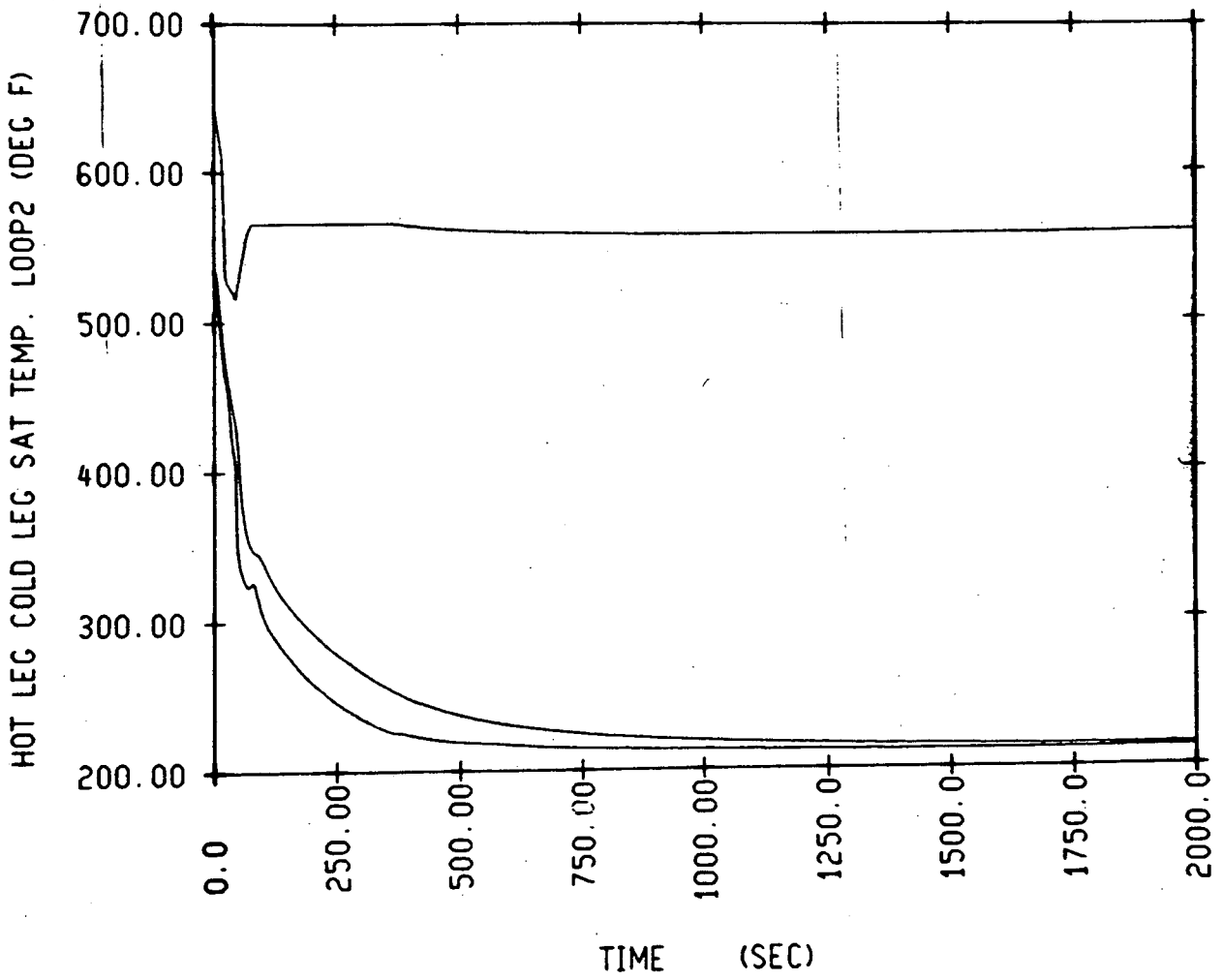
<u>EVENT</u>	<u>TIME</u>
PIPE RUPTURE	0
SI INITIATION	15.5
RCP TRIP	17.5
MFW ISOLATION	17.5
PRESSURIZER EMPTY	18.0
SI SYSTEM ALIGNED AND RUNNING	37.5
M/D AFW PUMPS STARTED (75 GPM)	317.0
SI TERMINATED	317.0
NORMAL CHARGING AND LETDOWN RESTORED	317.0
STEAM GENERATOR MINIMUM MASS	600.0

$$DE = 1.12^2/\text{LOOP}$$

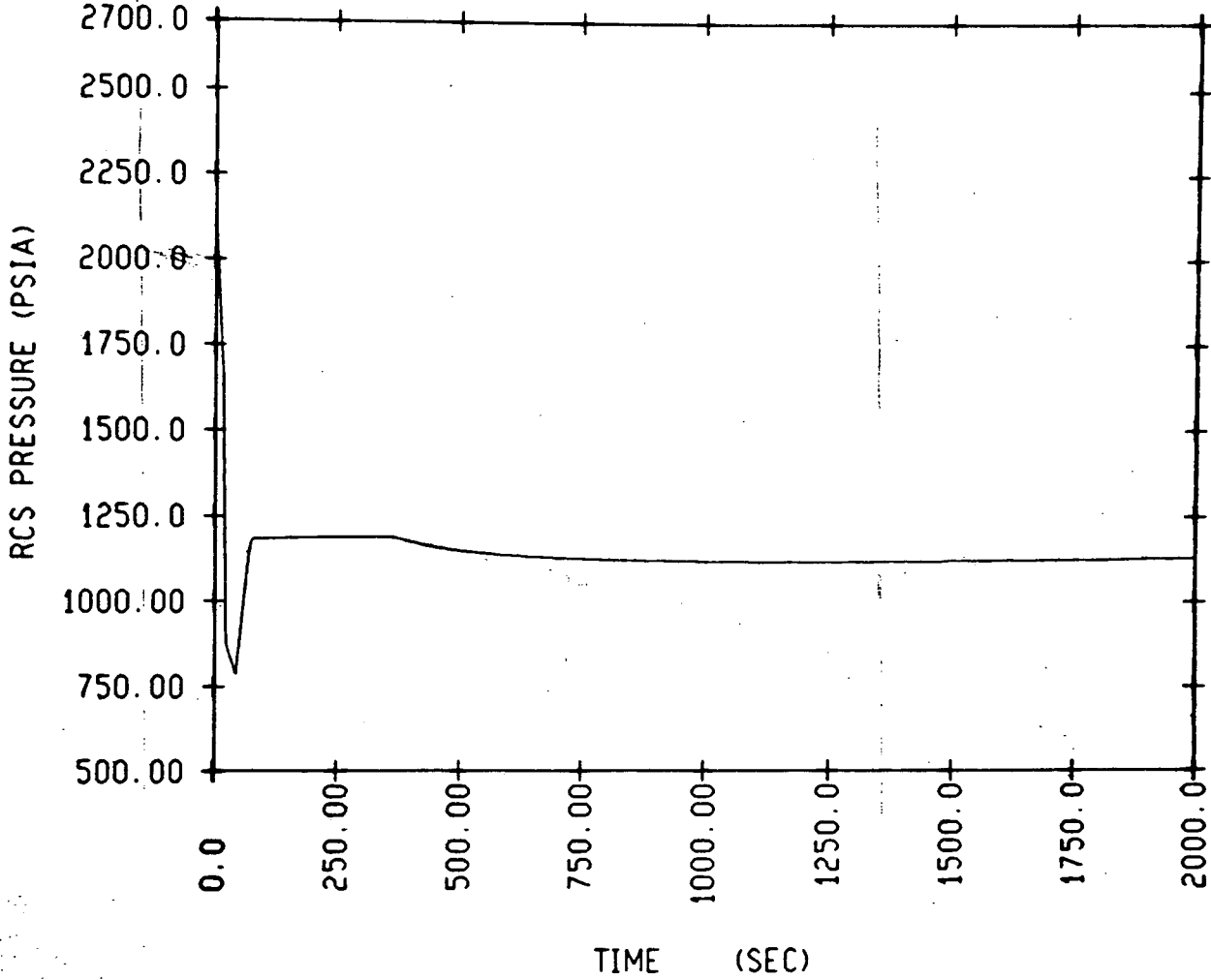
SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT27 RUN 1



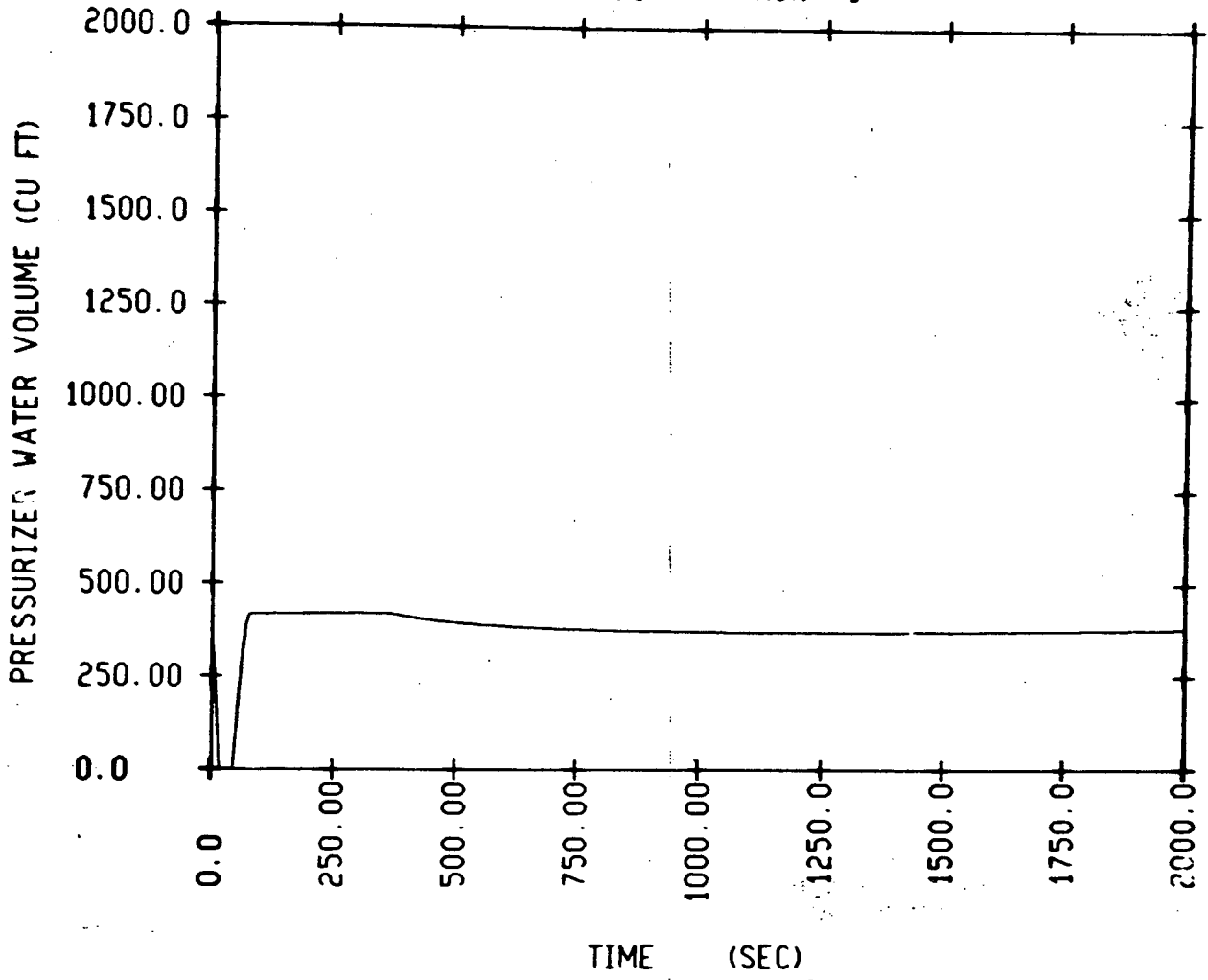
SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT42 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT29 RUN 1

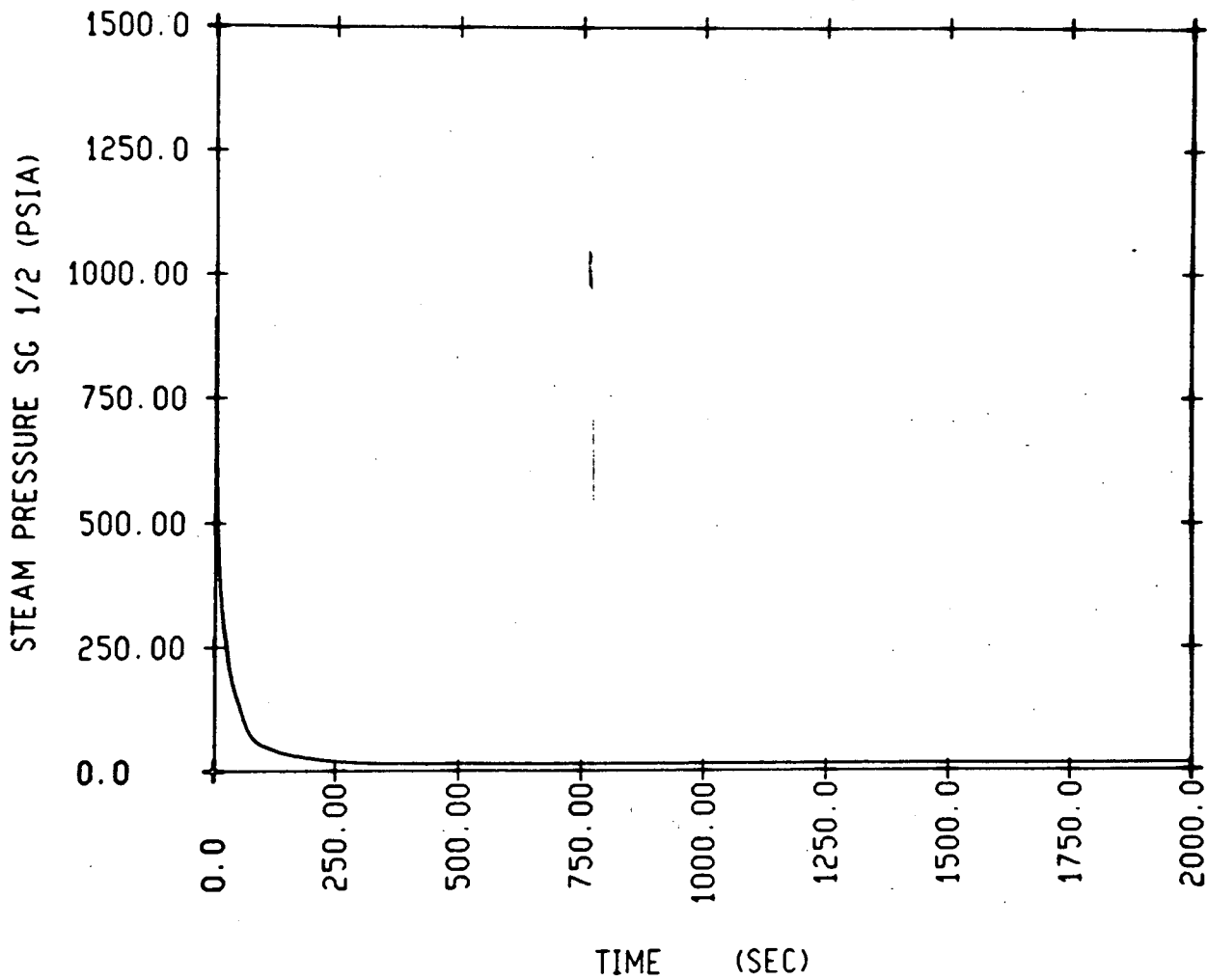


SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT31 RUN 1

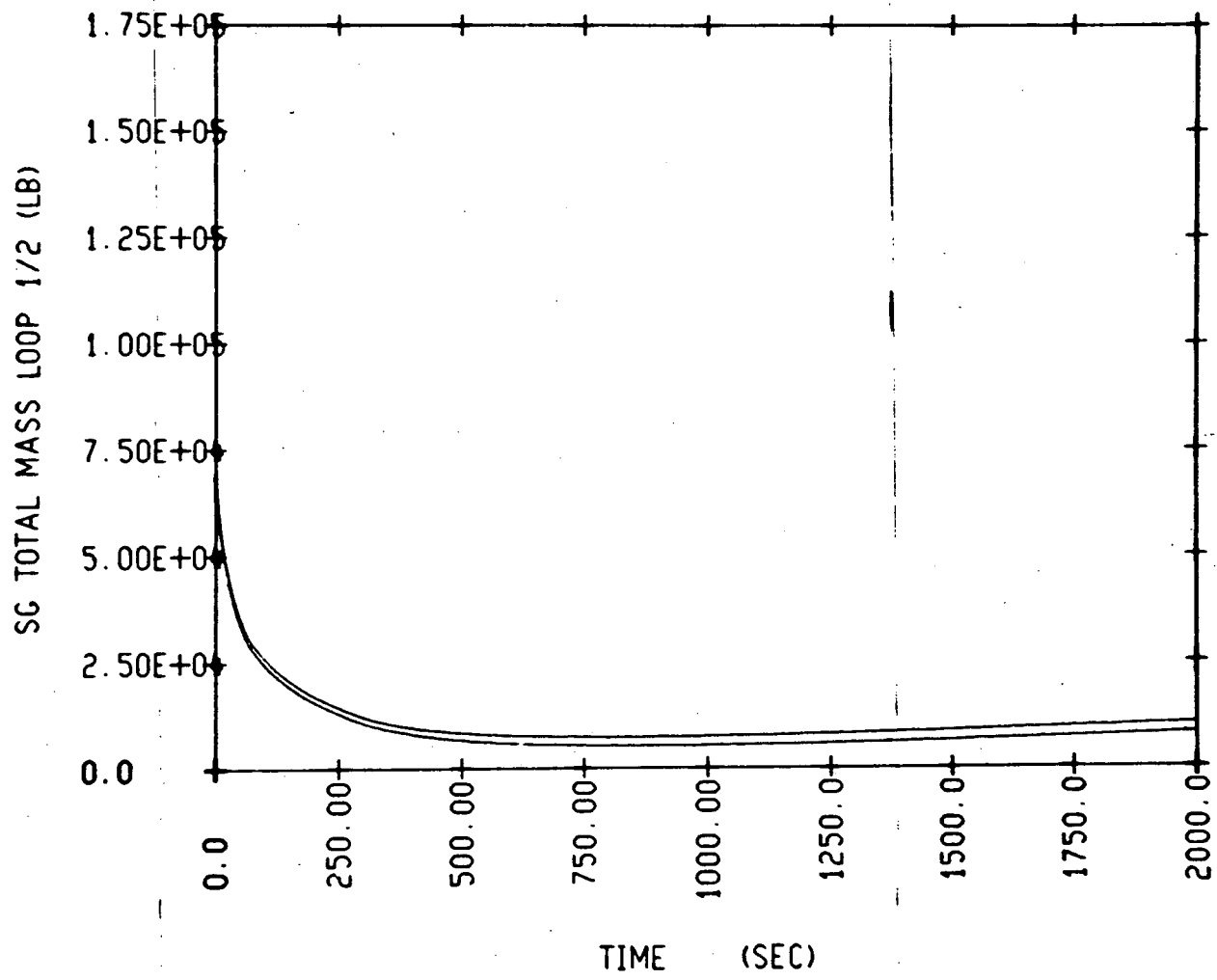




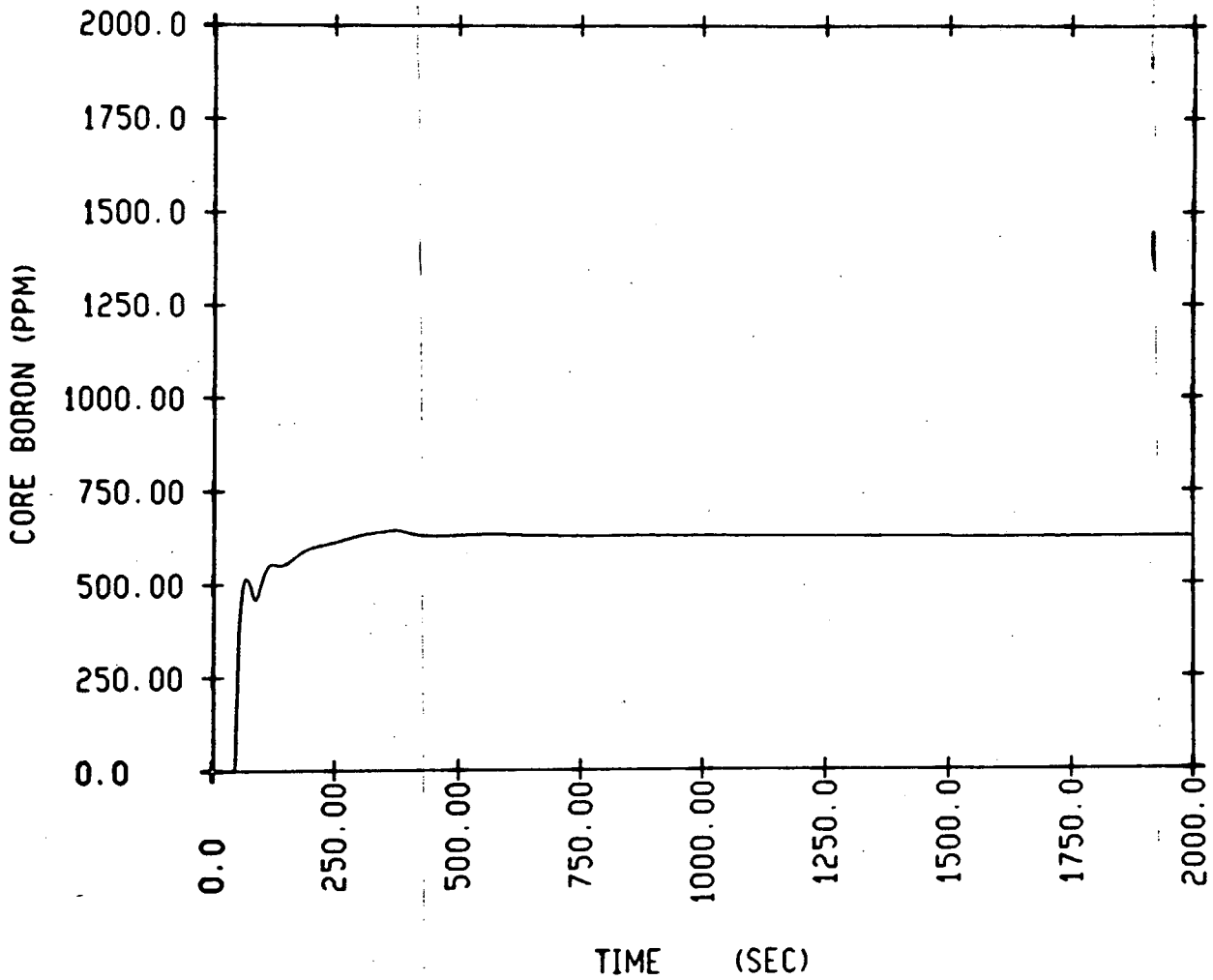
SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT48 RUN 1



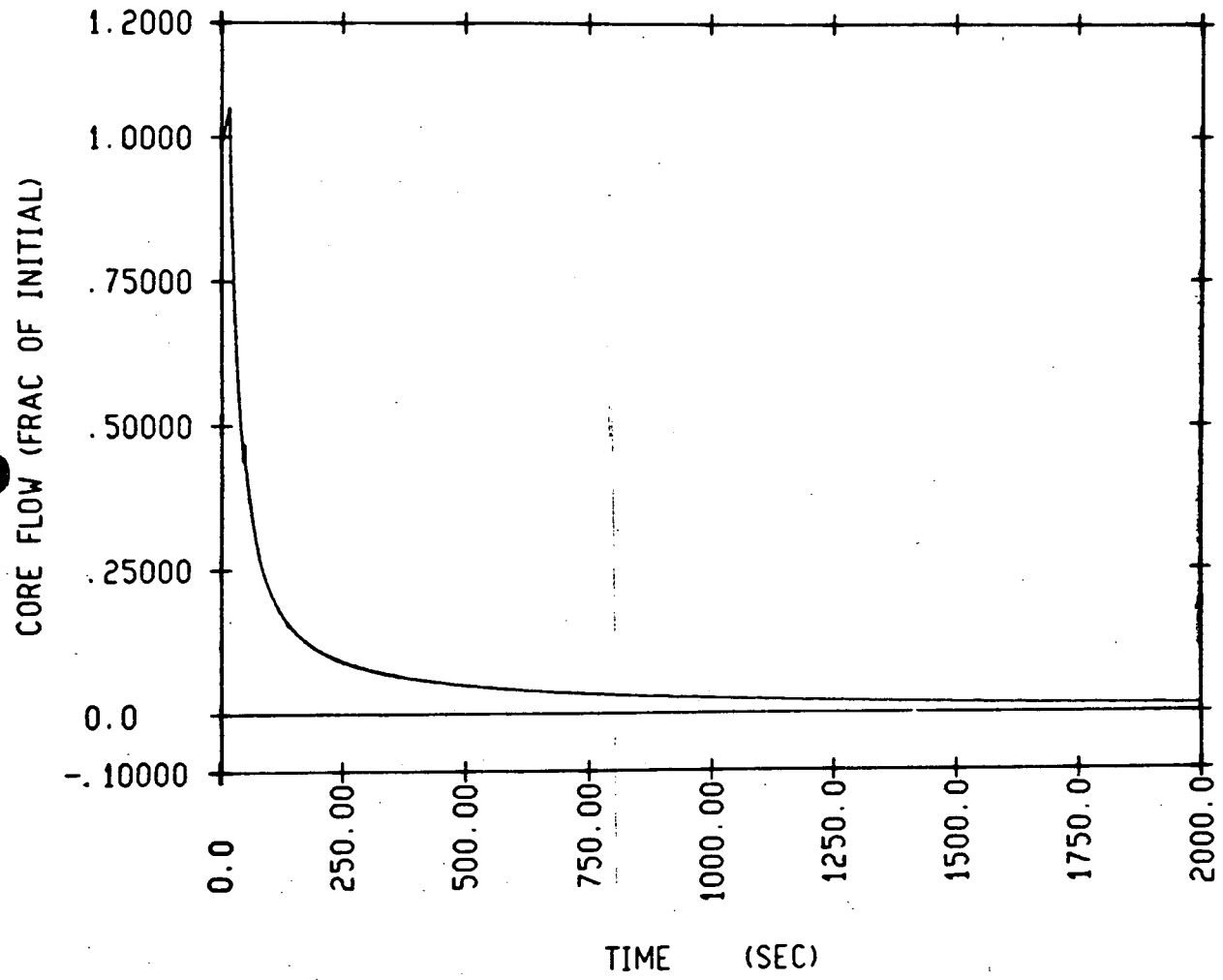
SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT45 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT50 RUN 1



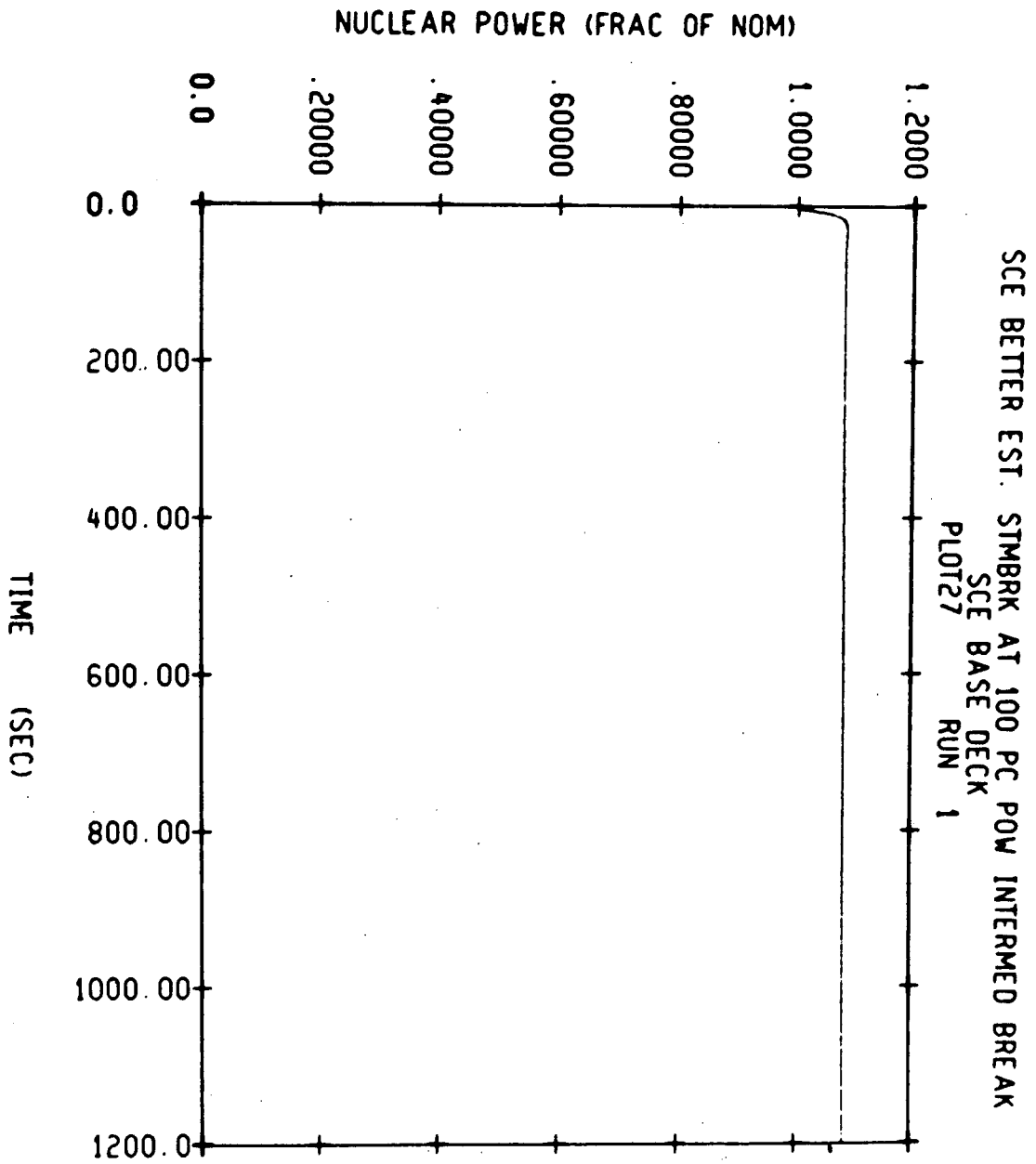
SCE BEST ESTIMATE STMBRK AT ZERO POWER W/ OFFSITE POW  
SCE BASE DECK  
PLOT32 RUN 1



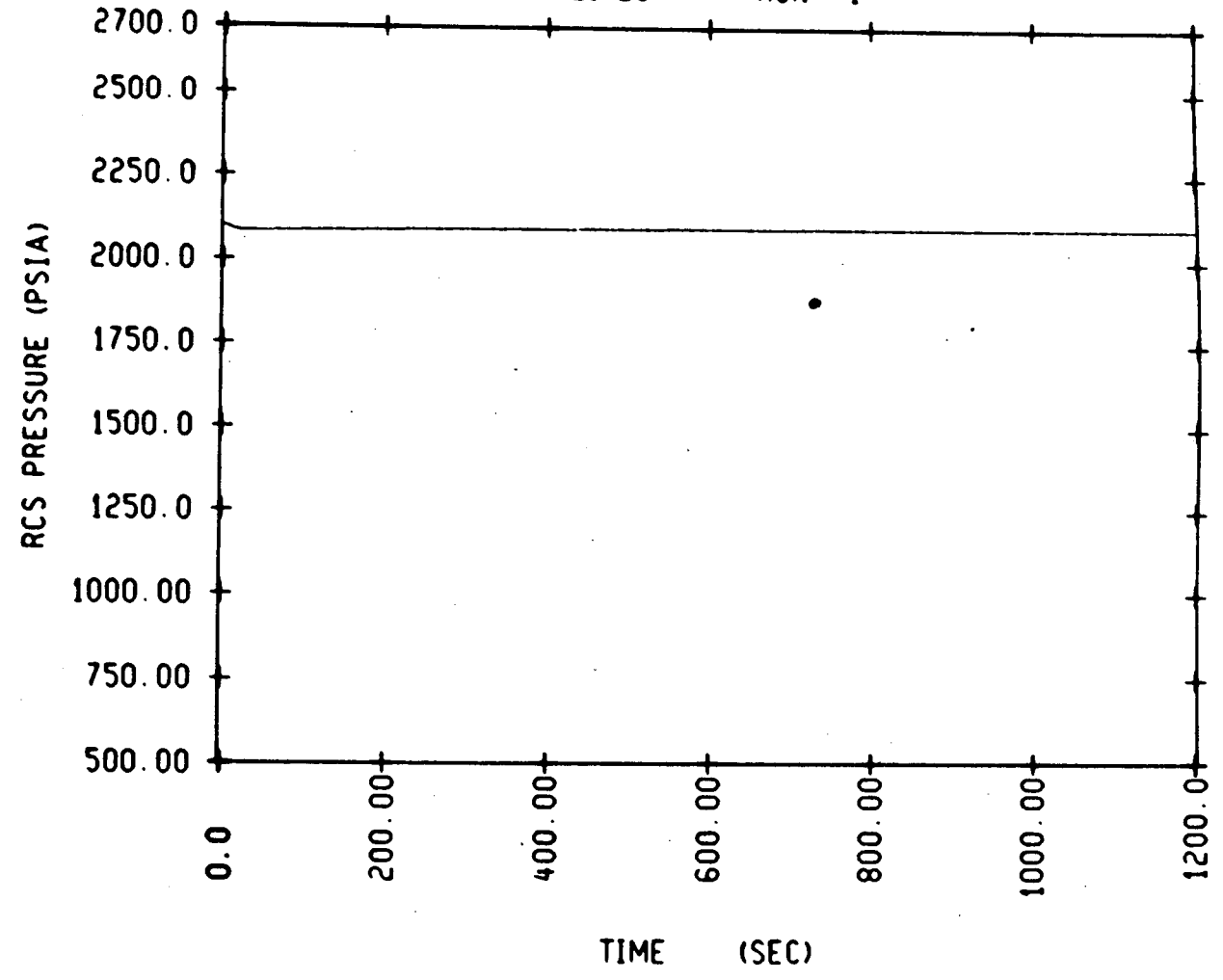
# INTERMEDIATE FULL POWER STEAMLINER BREAK

<u>EVENT</u>	<u>TIME</u>
PIPE RUPTURE	0
PLANT STABILIZED	60

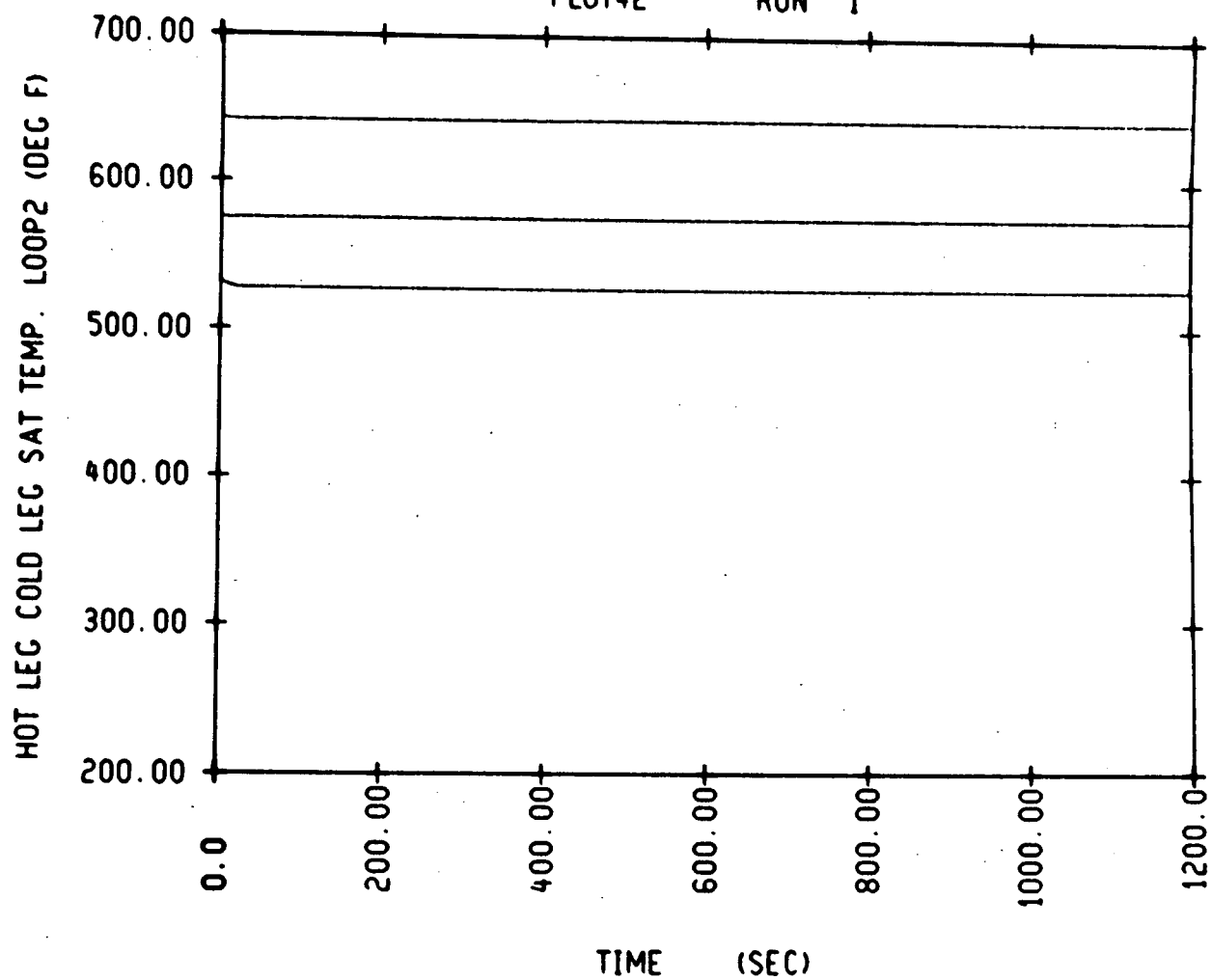
INTERMEDIATE = 0.1 FT<sup>2</sup>/LOOP



SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT29 RUN 1

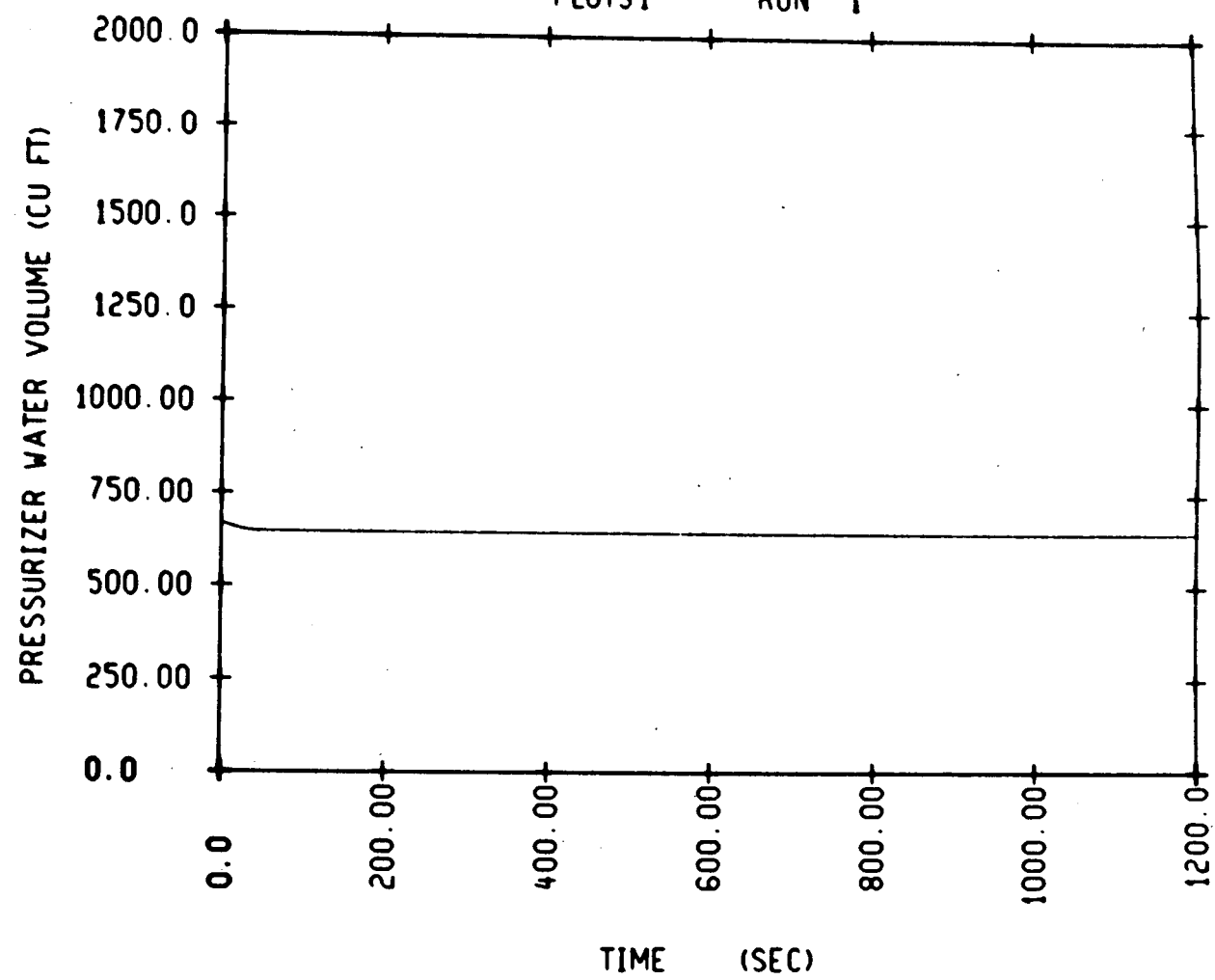


SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT42 RUN 1

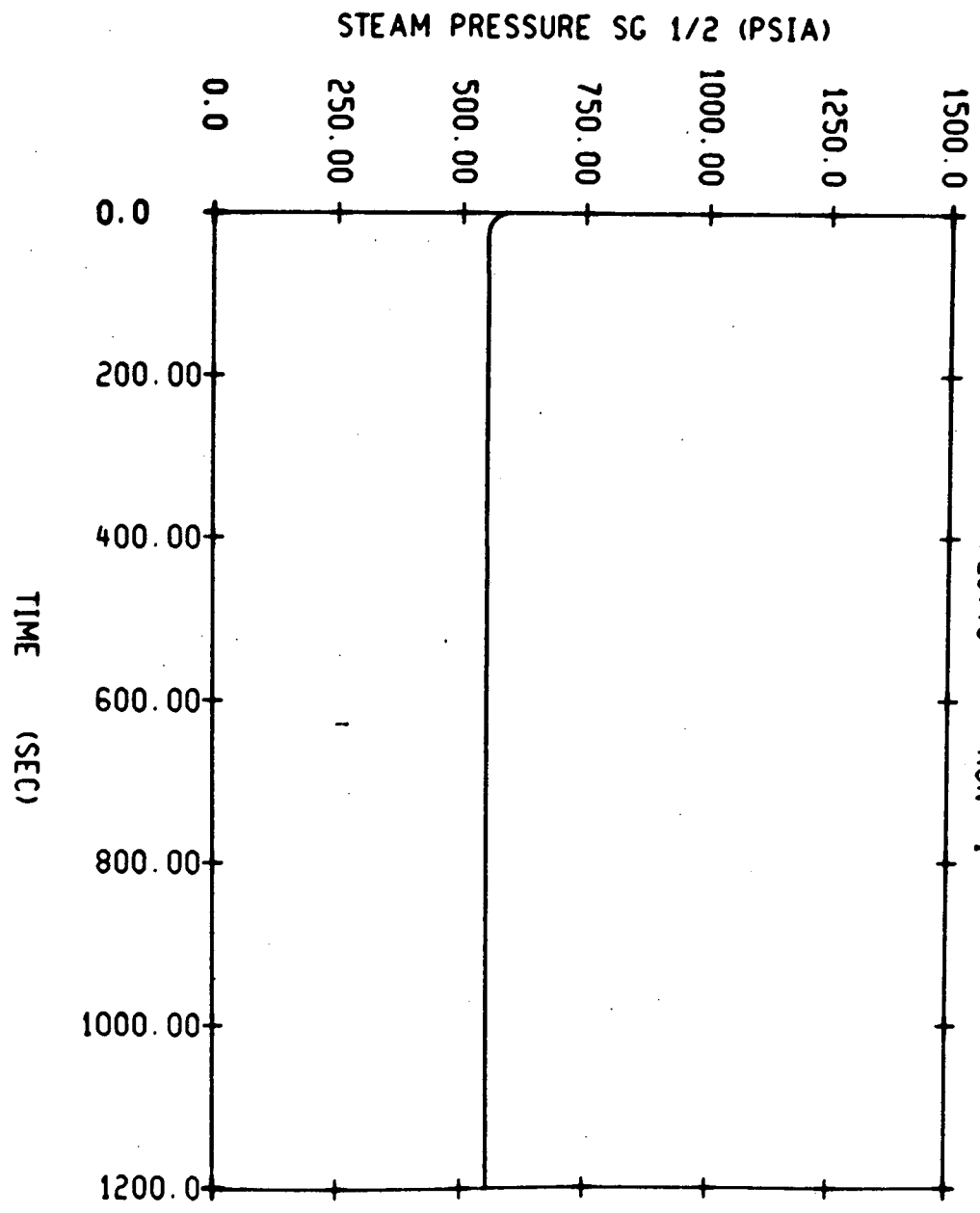




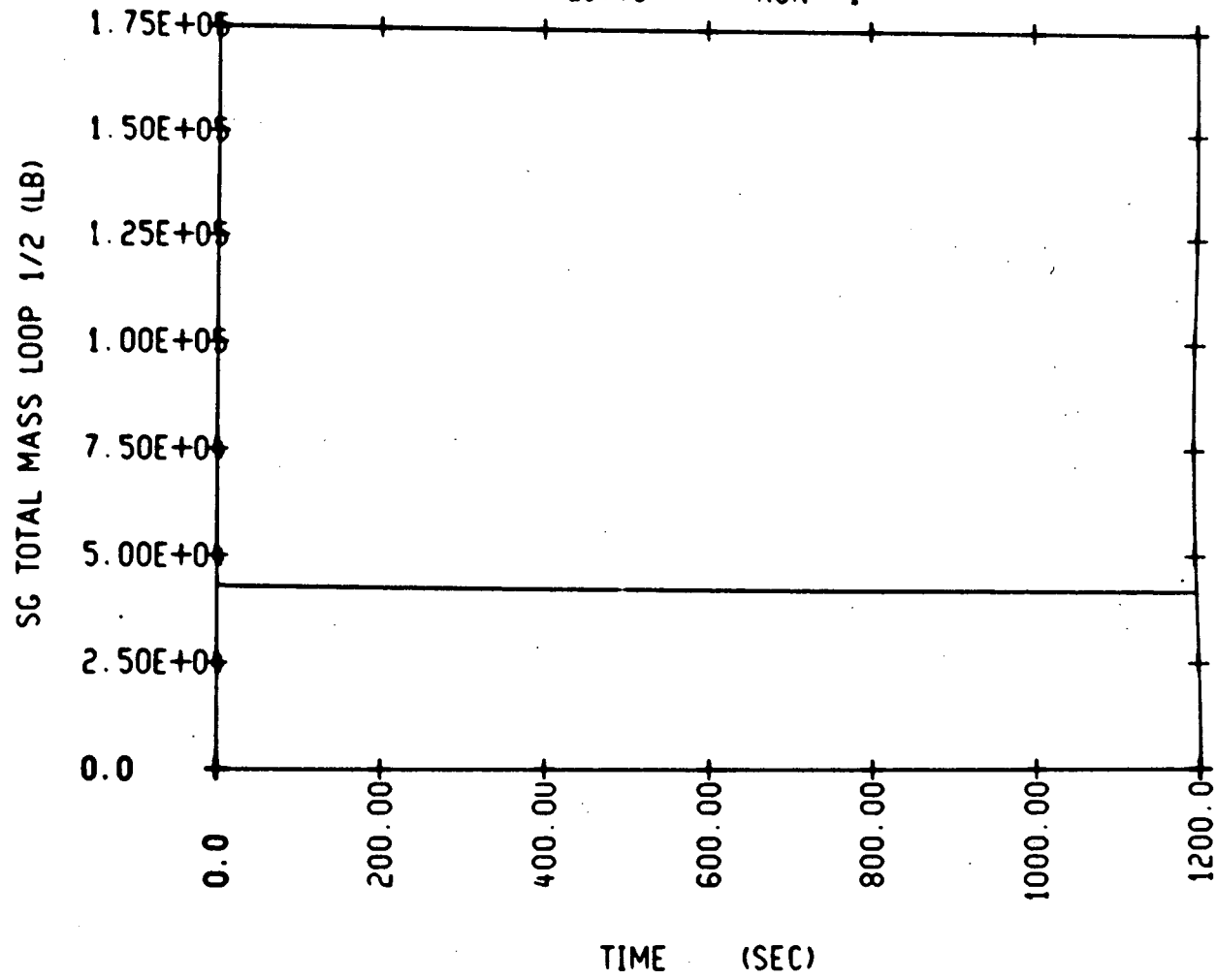
SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT31 RUN 1



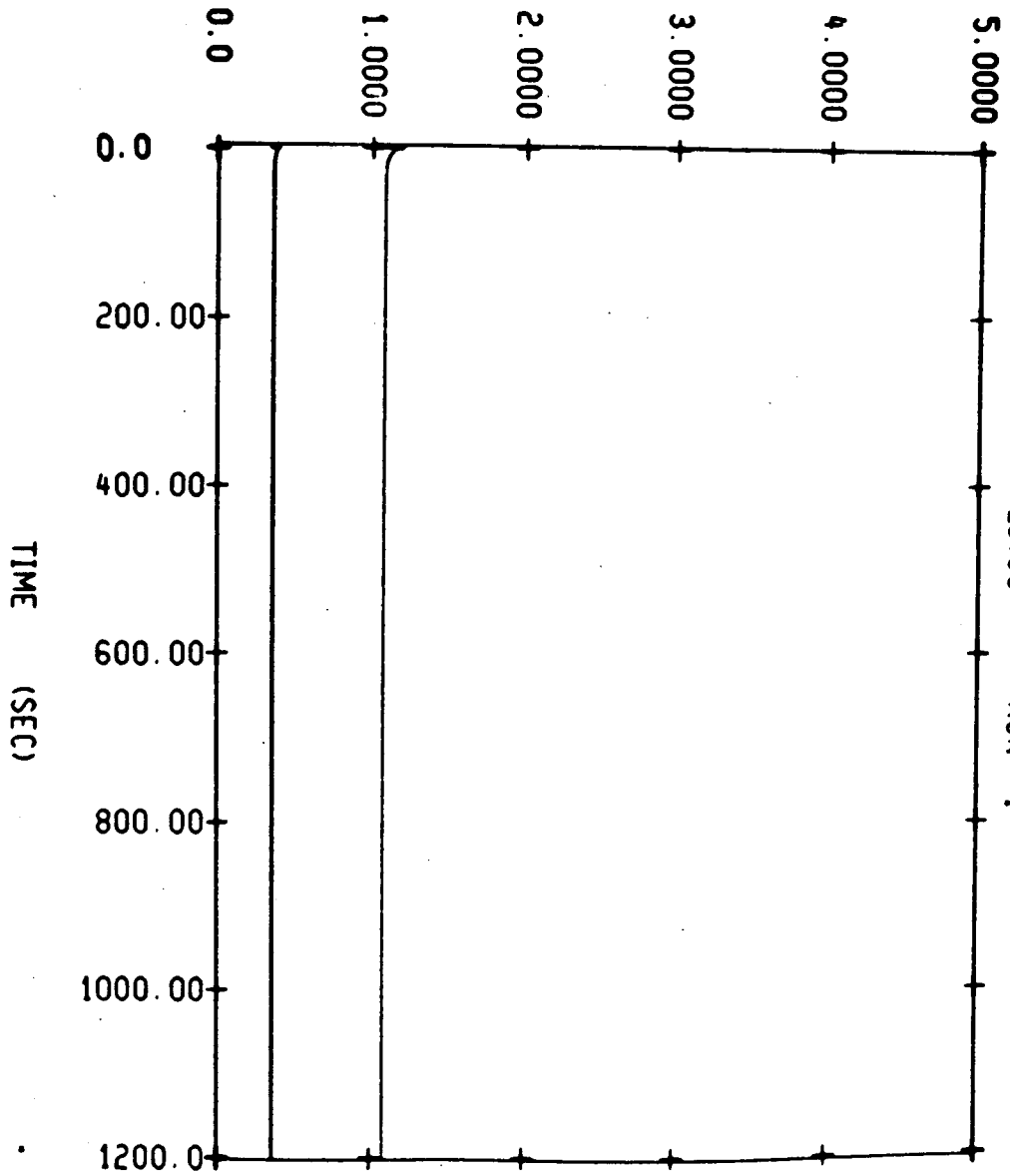
SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT#8  
RUN 1



SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT45 RUN 1

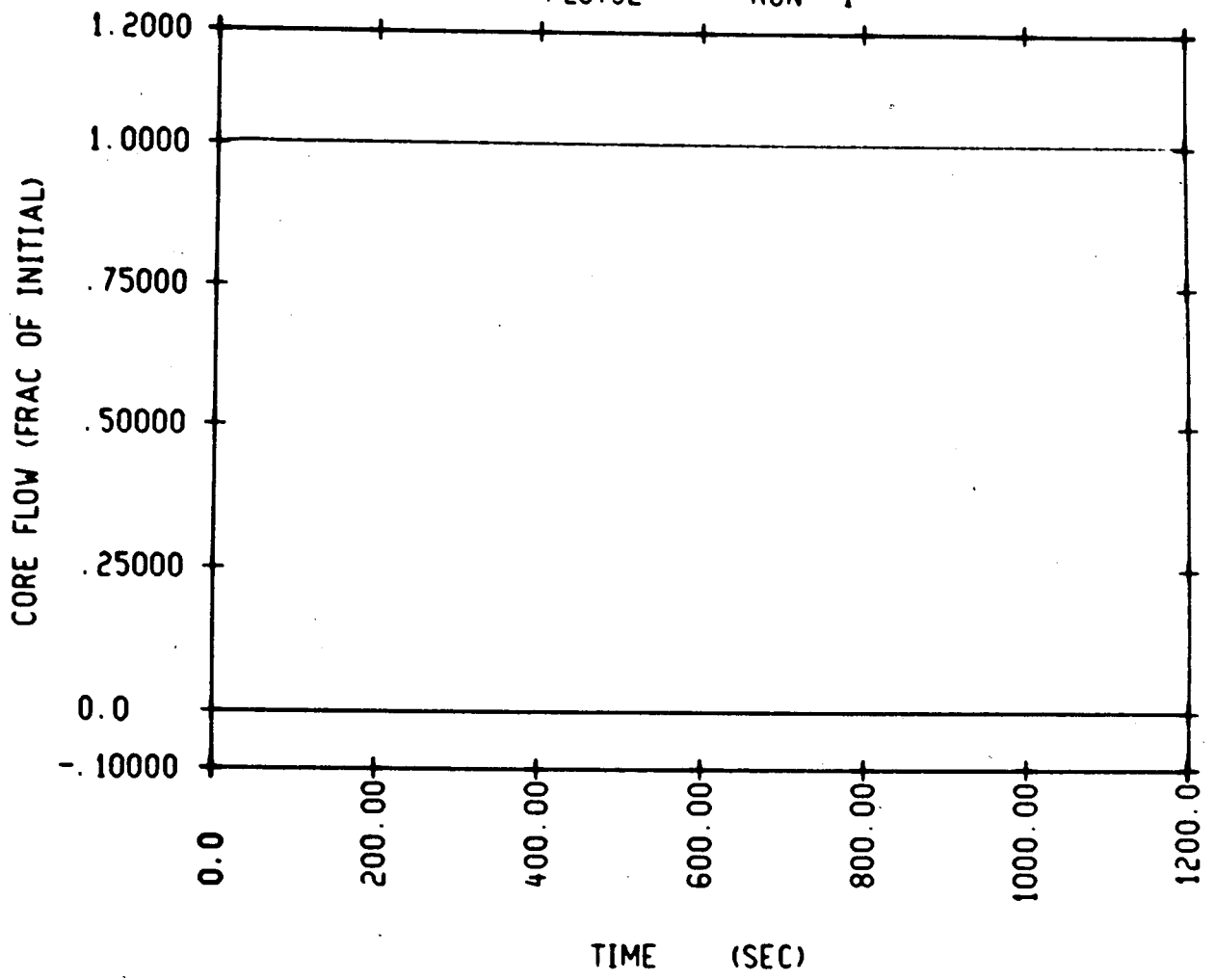


STEAM FLOW PLANT L1 L2  
(FRAC OF PLANT NOM)

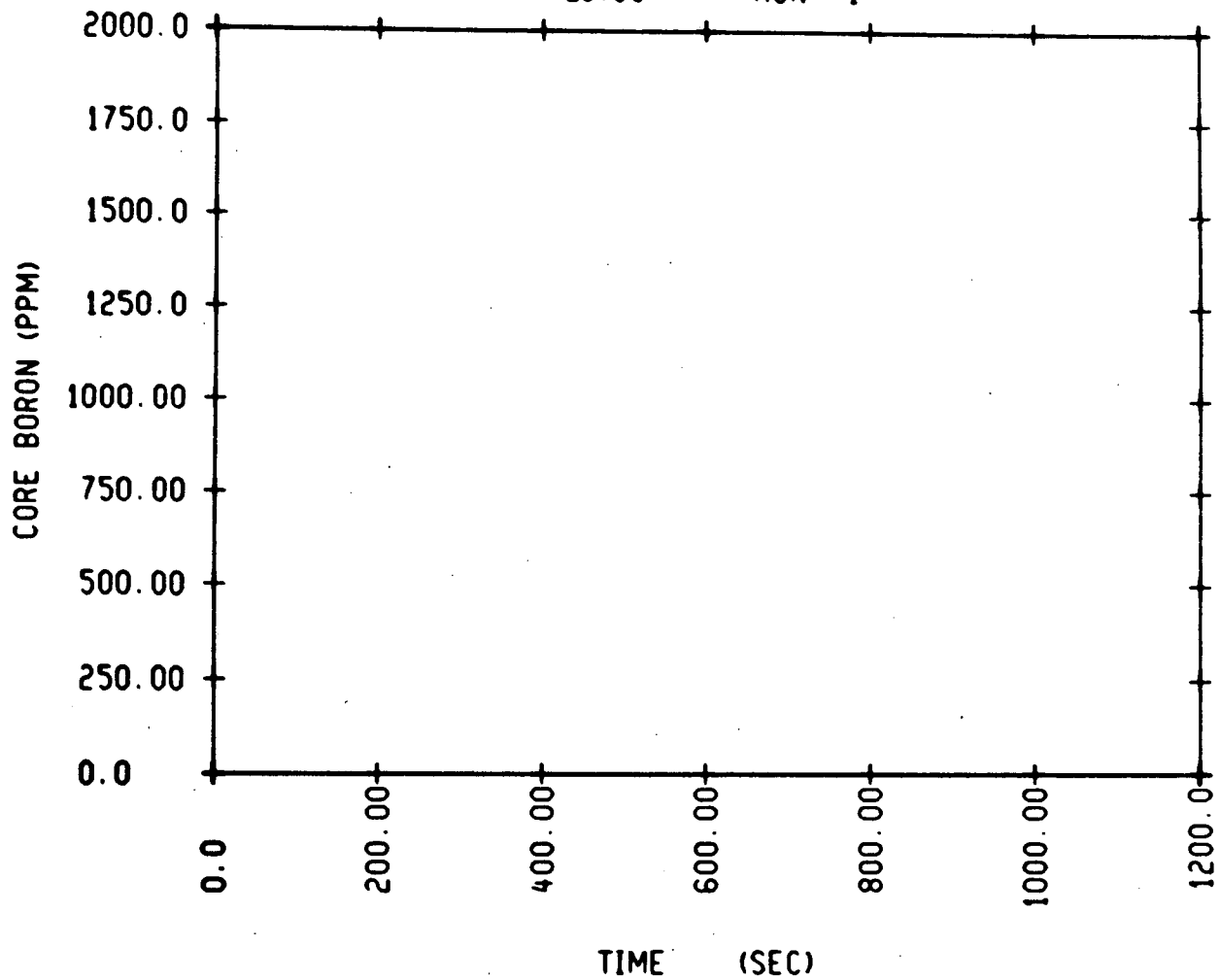


SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT36  
RUN 1

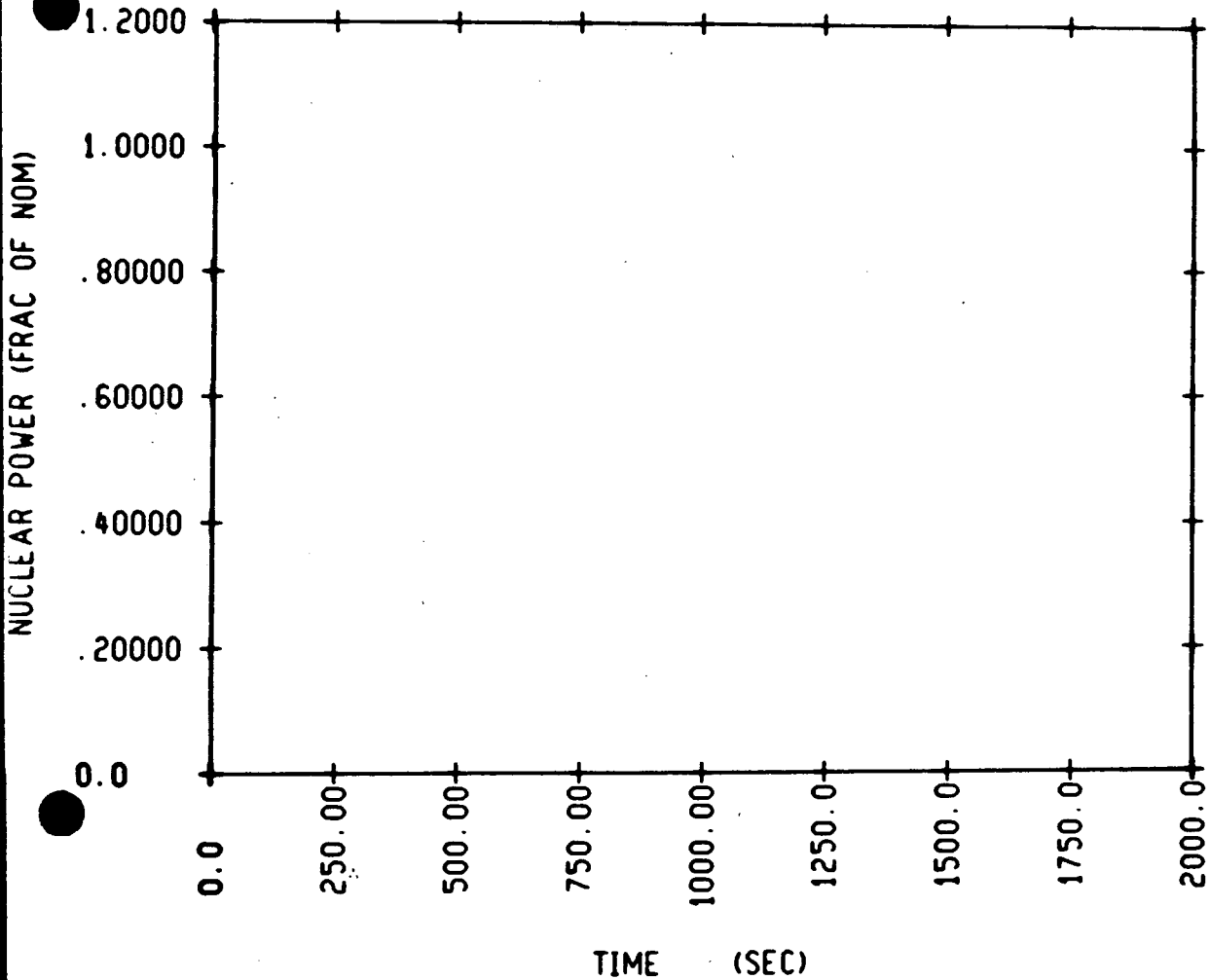
SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT32 RUN 1



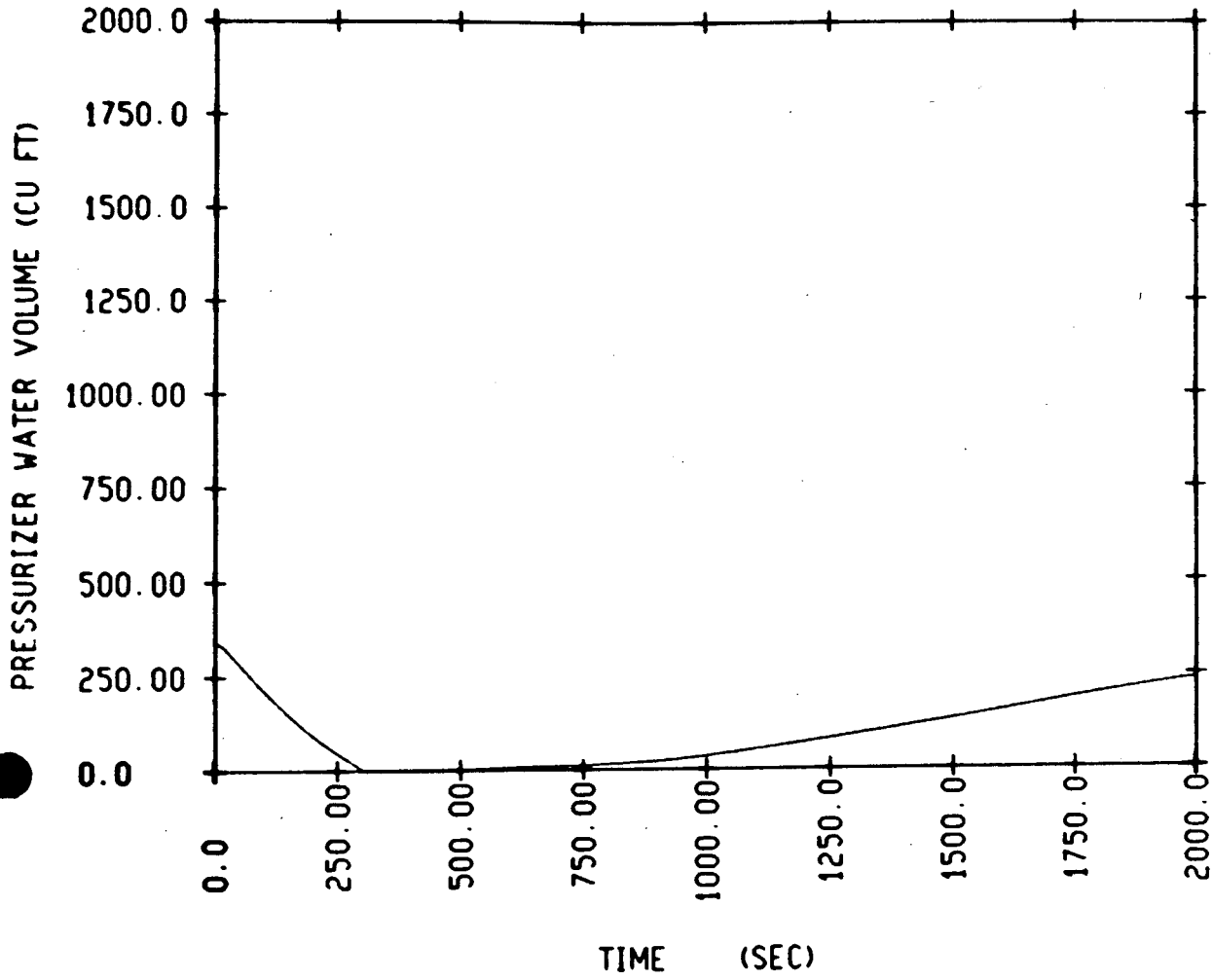
SCE BETTER EST. STMBRK AT 100 PC POW INTERMED BREAK  
SCE BASE DECK  
PLOT50 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT27 RUN 1

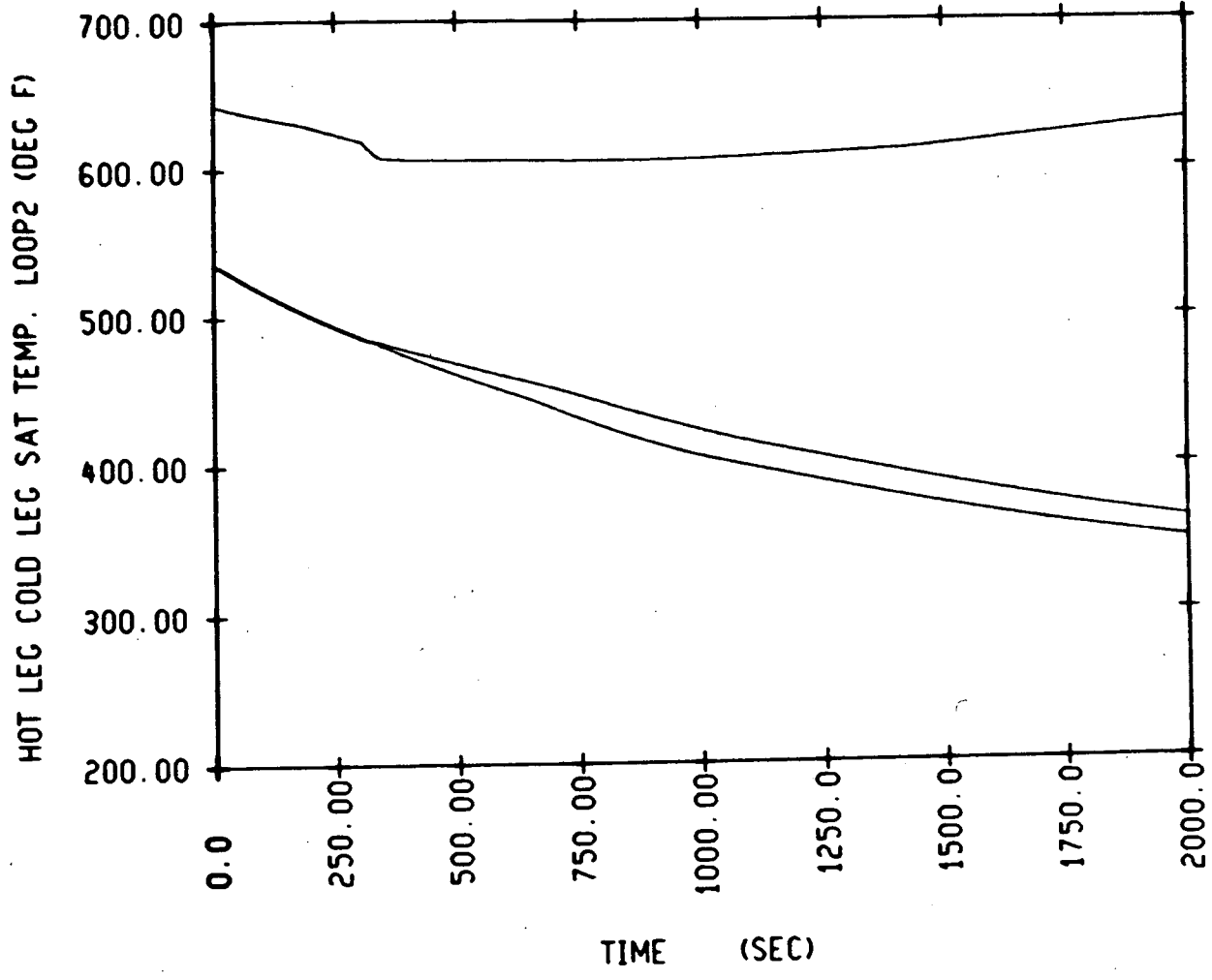


SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT31 RUN 1

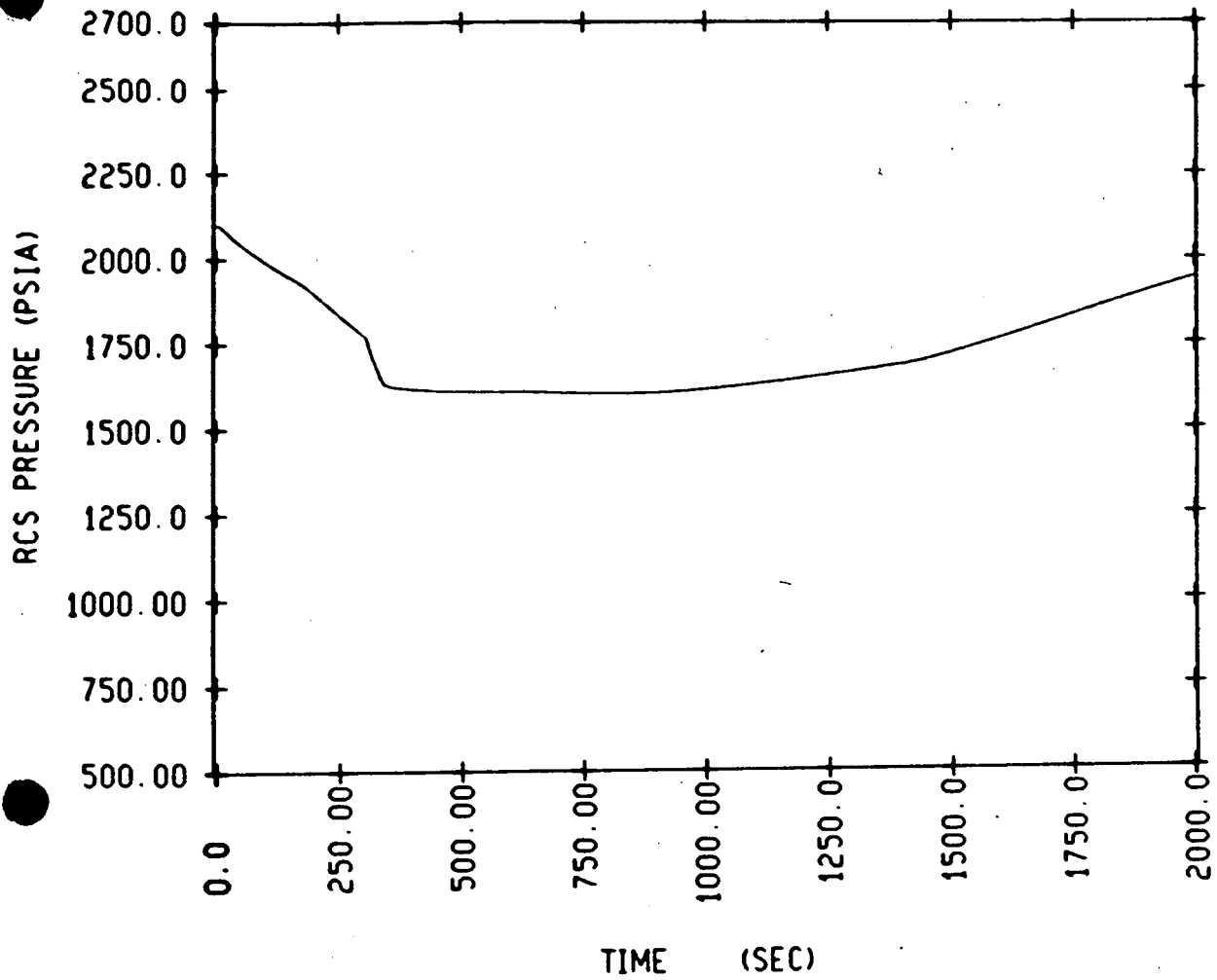




SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT42 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT29 RUN 1

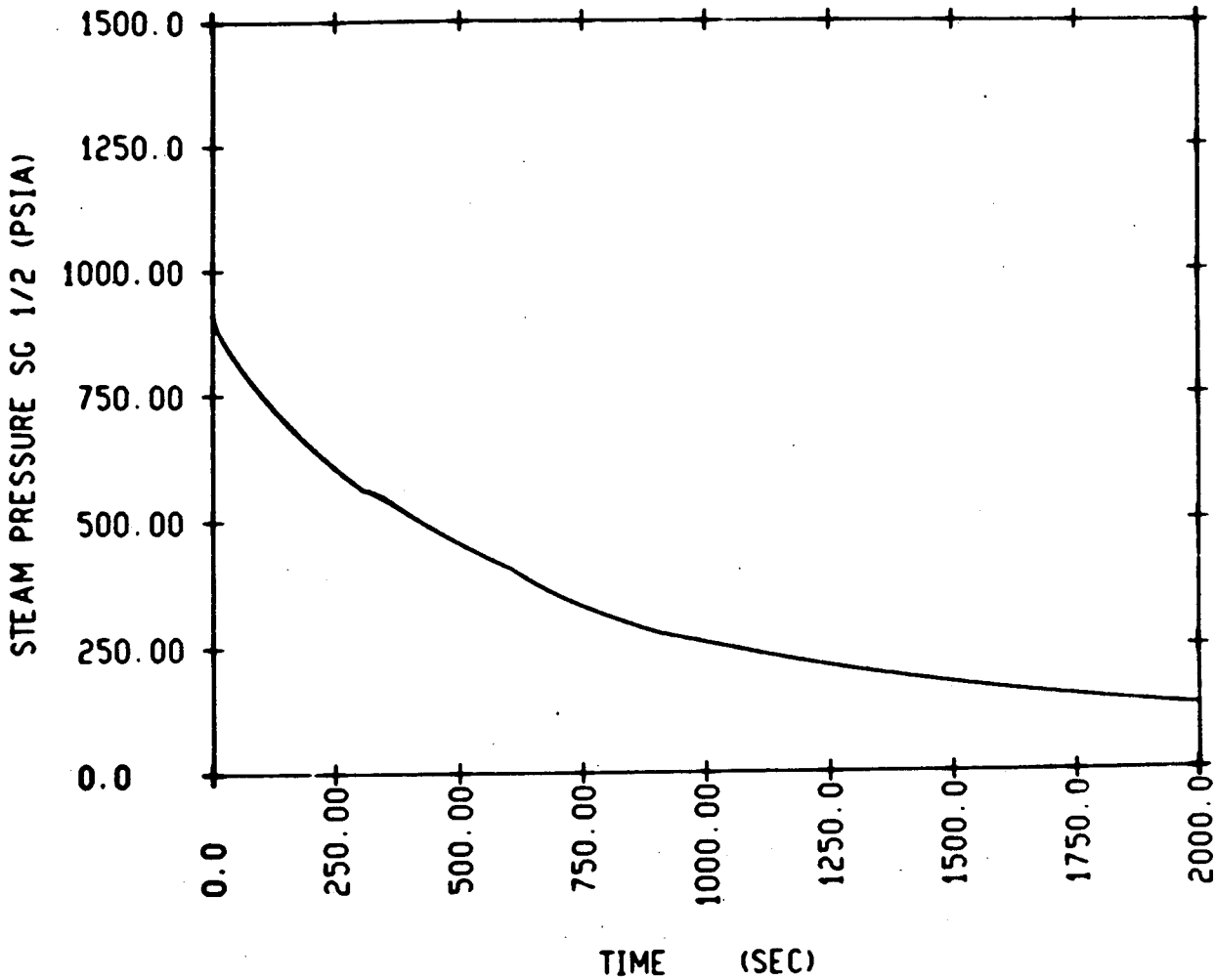


## CREDIBLE ZERO POWER STEAMLINE BREAK

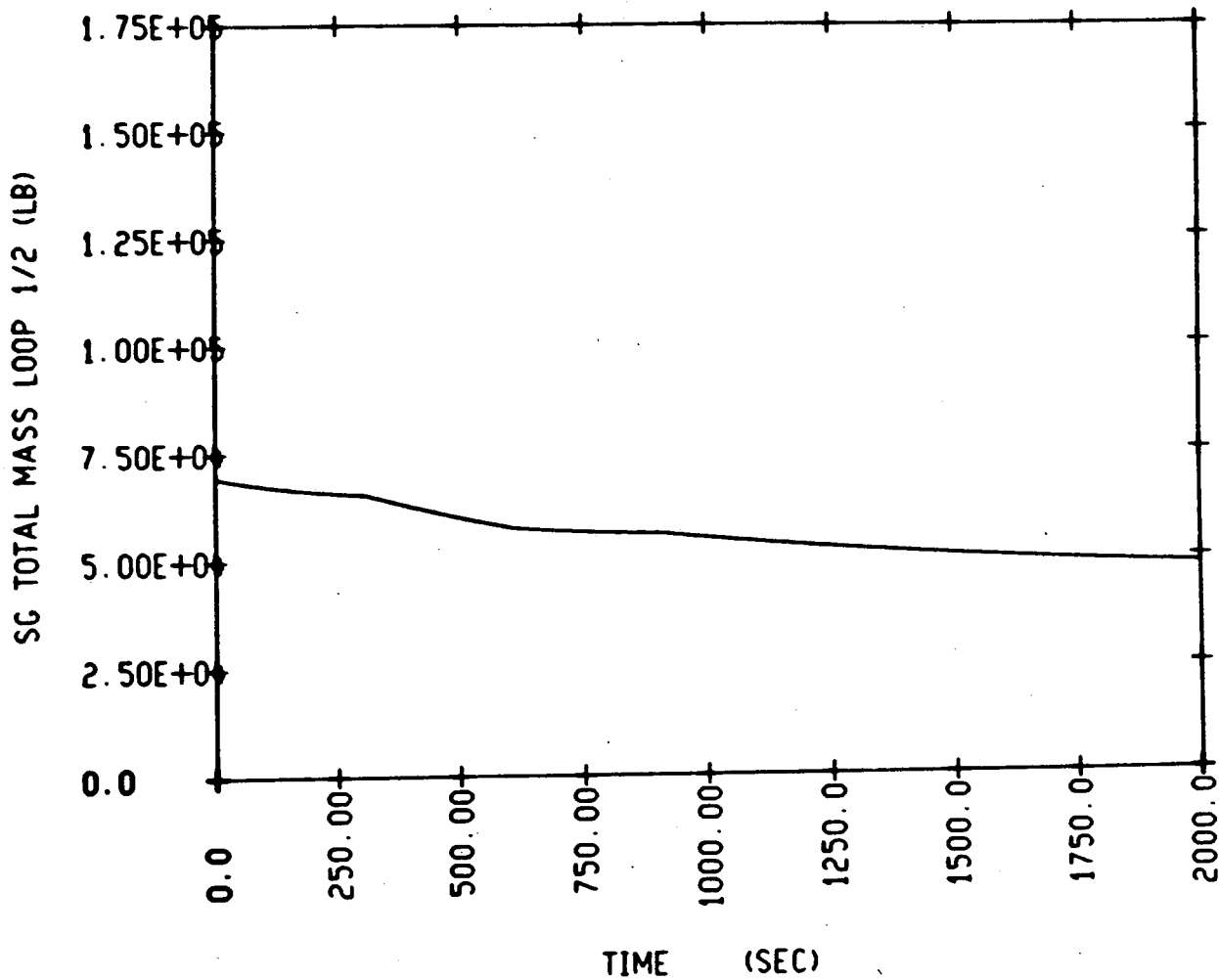
<u>EVENT</u>	<u>TIME</u>
PIPE RUPTURE	0
REACTOR TRIP (LOW PRESSURIZER PRESSURE)	236.5
RCP TRIP	238.5
PRESSURIZER EMPTIES	305.0
SI INITIATION (LOW PRESSURIZER PRESSURE)	310.4
MFW ISOLATION	312.4
SI SYSTEM ALIGNED AND OPERATING	332.4
M/D AFW PUMPS STARTED	610.4
M/D AFW PUMPS THROTTLED	910.4

CREDIBLE =  $0.02 \text{ FT}^2/\text{LOOP}$

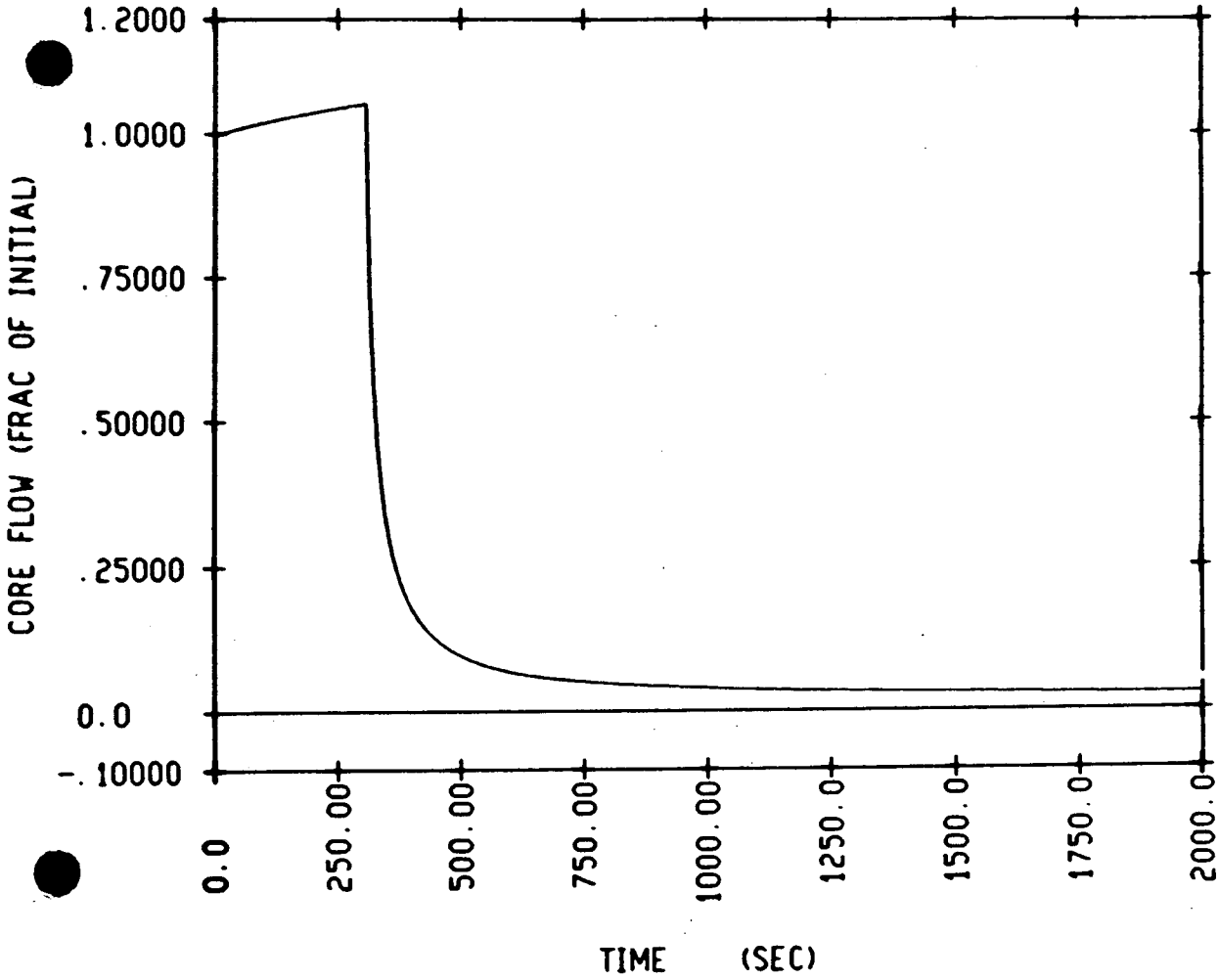
SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT48 RUN 1



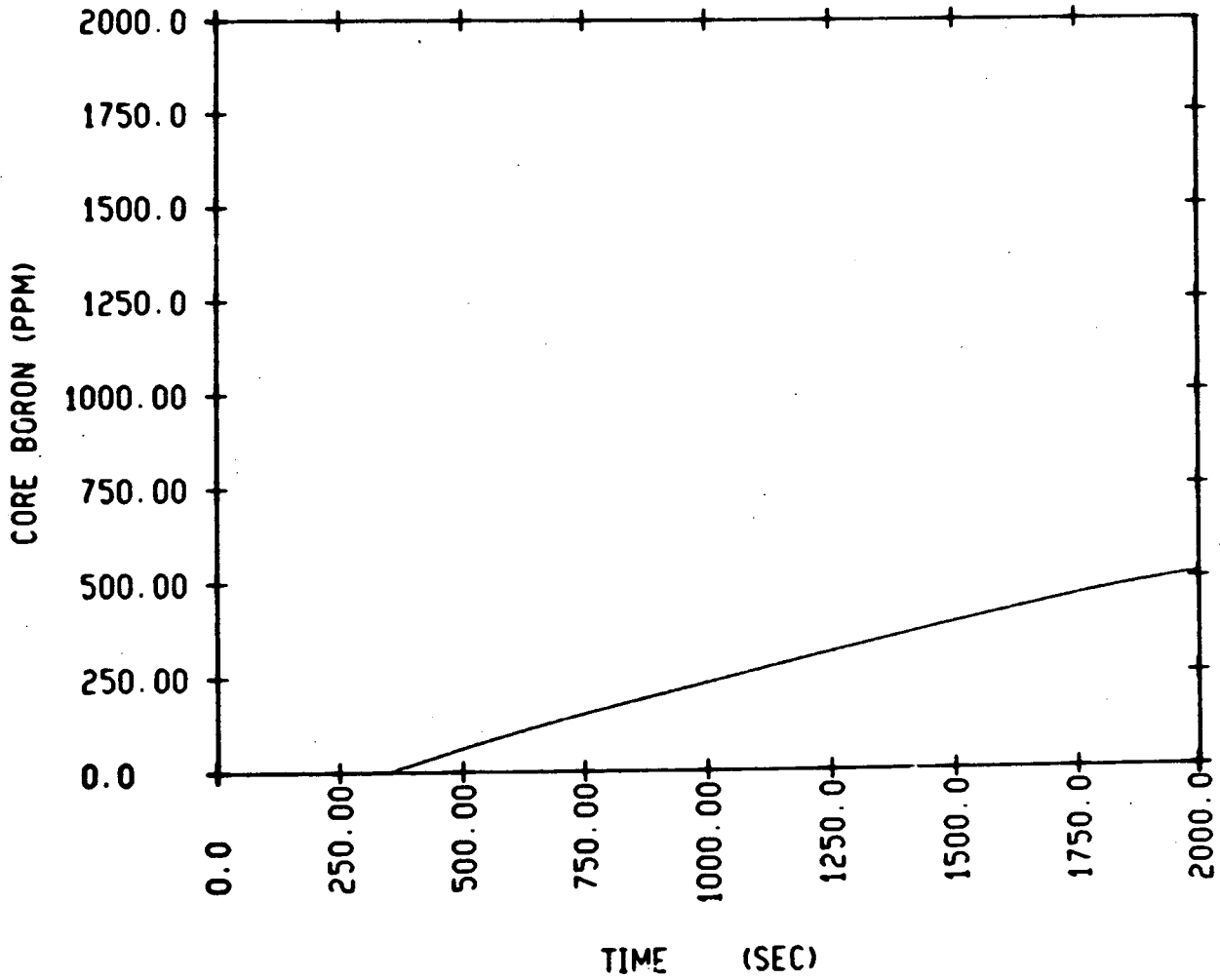
SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT45 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT32 RUN 1



SCE BEST ESTIMATE STMBRK AT ZERO POWER CREDIBLE BREAK  
SCE BASE DECK  
PLOT50 RUN 1



ENCLOSURE 2

STEAM GENERATOR TUBE RUPTURE



## BASIC ACTIONS

### GENERIC STEAM GENERATOR TUBE RUPTURE

1. IDENTIFY RUPTURED STEAM GENERATOR
2. ISOLATE RUPTURED STEAM GENERATOR
3. USE NON-RUPTURED STEAM GENERATORS TO COOL DOWN  
RCS TO 50 degrees BELOW NO-LOAD TEMPERATURE
4. DEPRESSURIZE RCS TO RUPTURED STEAM GENERATOR  
PRESSURE
5. TERMINATE SAFETY INJECTION FLOW
6. COOL DOWN AND DEPRESSURIZE RCS TO RHR CONDITIONS
7. CONTINUE COOLDOWN ON RHR TO COLD SHUTDOWN CONDITIONS

AREAS OF CONCERN FOR SAN ONOFRE

1. CANNOT ISOLATE RUPTURED STEAM GENERATOR
2. OVERFILL OF RUPTURED STEAM GENERATOR
3. VOIDING OF UPPER HEAD REGION
4. HIGH CAPACITY OF MAIN FEED (SI) PUMPS
5. RCPS TRIPPED ON REACTOR TRIP

## BASIC ACTIONS

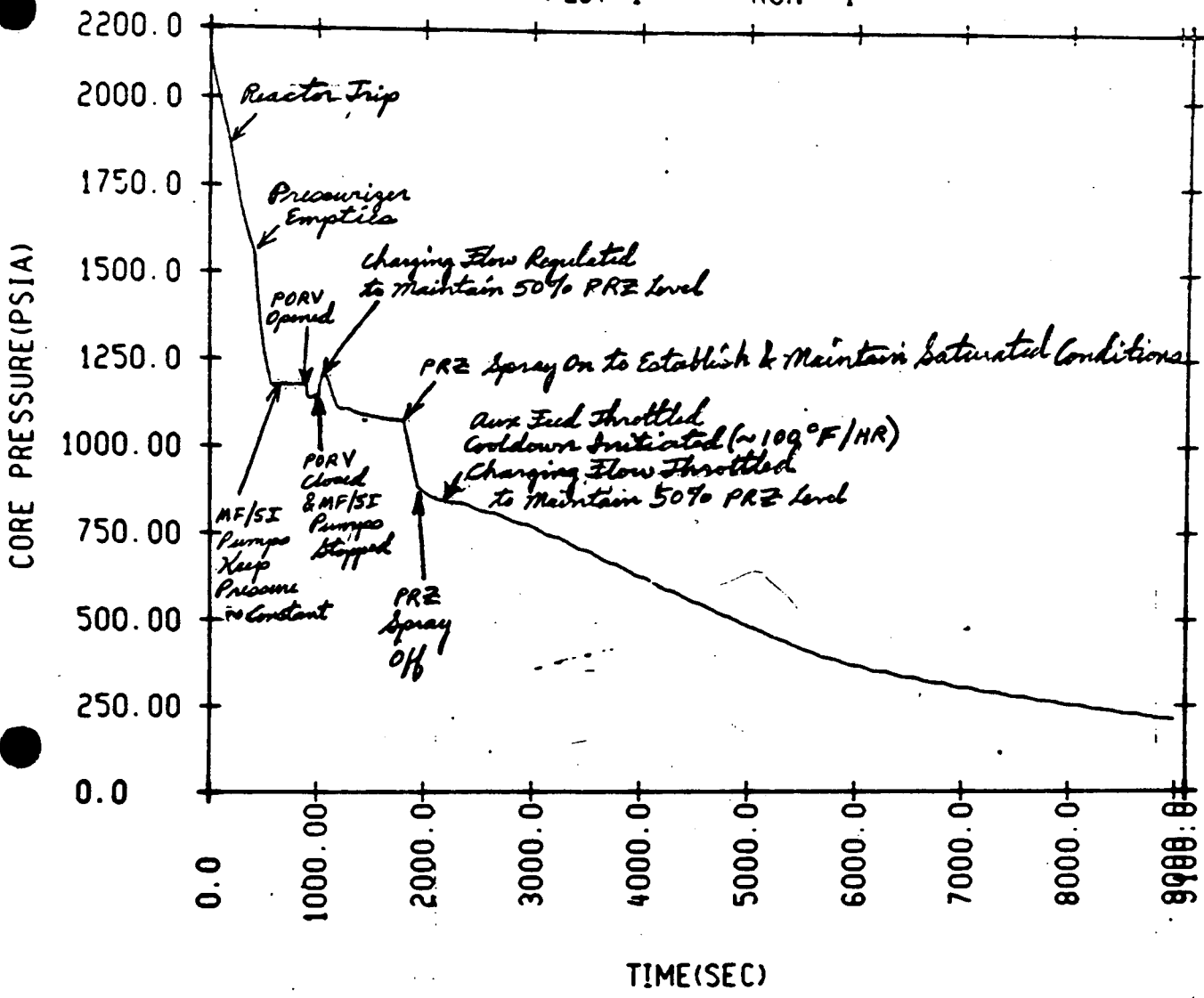
### SONGS #1 STEAM GENERATOR TUBE RUPTURE

1. IDENTIFY RUPTURED STEAM GENERATOR
2. ISOLATE AFW TO RUPTURED STEAM GENERATOR
3. INITIATE MAX CHARGING FLOW TO RCS
4. DEPRESSURIZE RCS TO REFILL PRESSURIZER
5. START REACTOR COOLANT PUMPS
6. STOP SAFETY INJECTION PUMPS
7. COOL DOWN RCS AT MAXIMUM RATE WHILE MINIMIZING  
PRIMARY TO SECONDARY DELTA P
8. INITIATE RHR OPERATION
9. COOL RCS TO COLD SHUTDOWN CONDITIONS WITH RHR  
(MAINTAIN RCS PRESSURE APPROXIMATELY EQUAL TO  
STEAM PRESSURE)

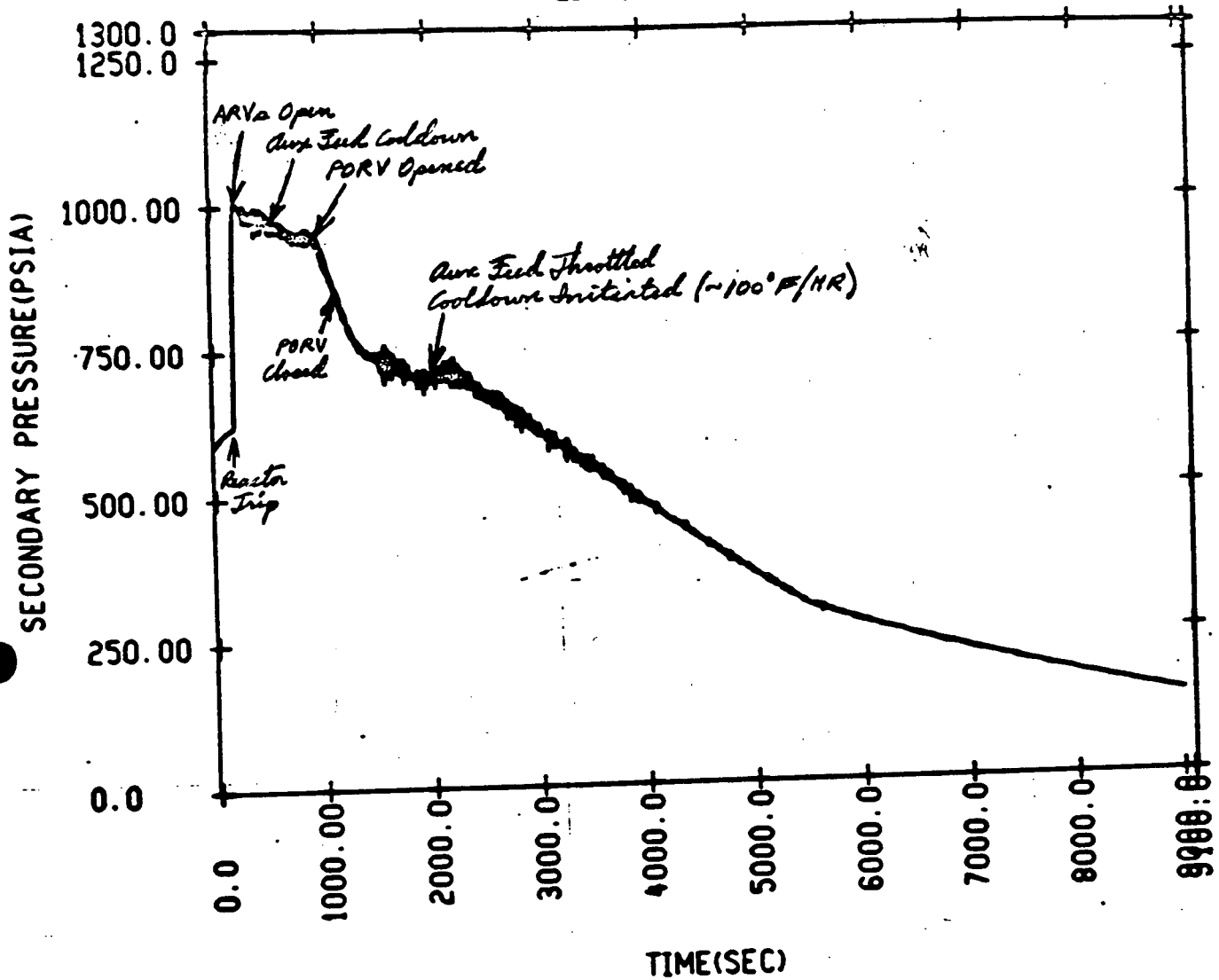
OFFSITE POWER LOST - SATURATED COOLDOWN

<u>EVENT</u>	<u>TIME (SEC)</u>
REACTOR TRIP	182.3
SI INITIATION	272.0
AUX. FEEDWATER INITIATION	310.0
AUX. FEEDWATER TERMINATED TO RUPTURED SG	815.0
PRESSURIZER PORV OPENED	900.0
PRESSURIZER PORV CLOSED	1016.0
MF/SI PUMPS STOPPED	1023.0
CHARGING FLOW THROTTLED TO MAINTAIN 50% LEVEL IN PRESSURIZER	1052.0
PRESSURIZER SPRAY ON	1800.0
~100°F/HR COOLDOWN INITIATED	1800.0
AUX. FEEDWATER THROTTLED TO INTACT SGS	~2100.0

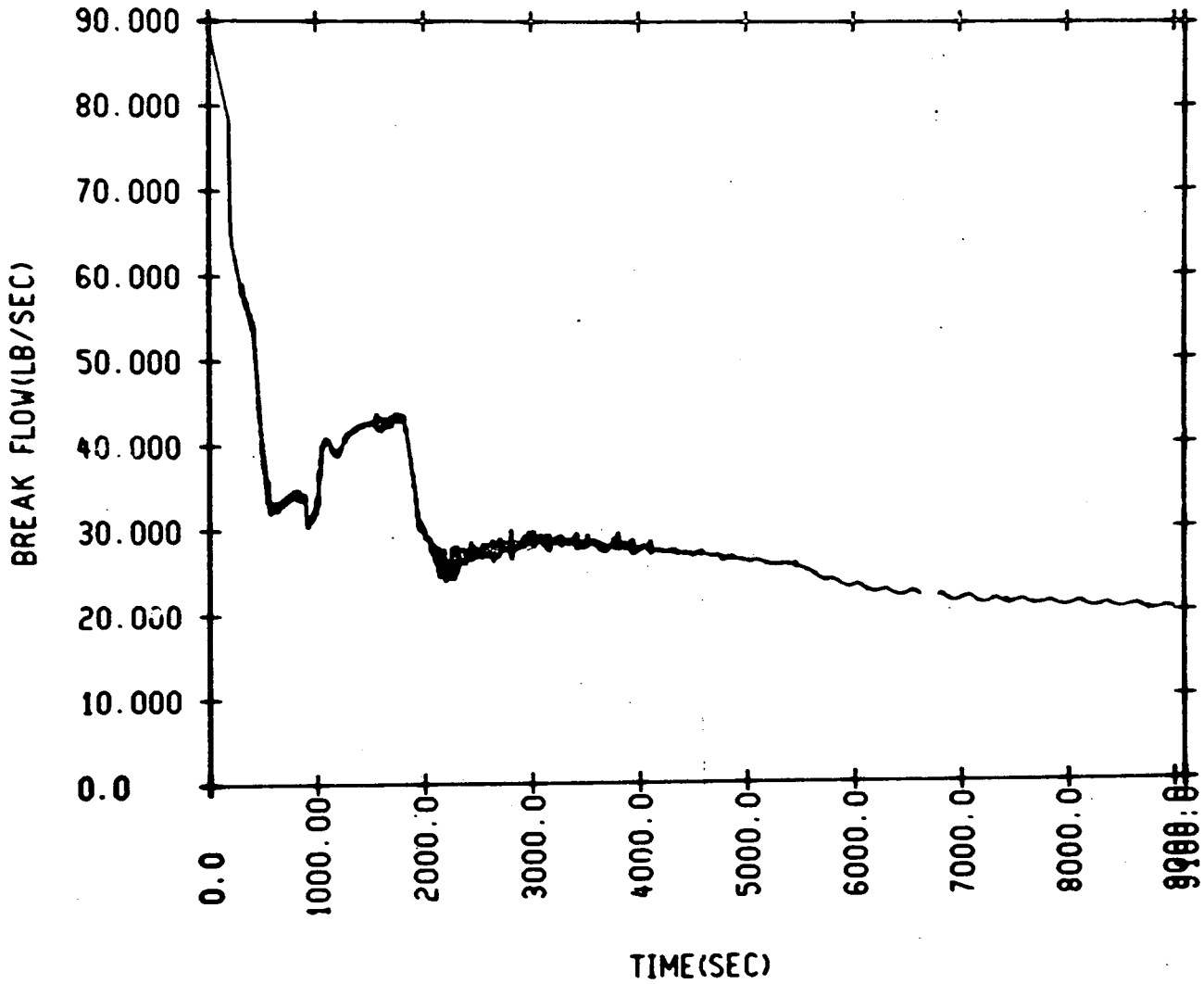
LOFT-4 STEAM GENERATOR TUBE RUPTURE  
 SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
 PLOT 1 RUN 1



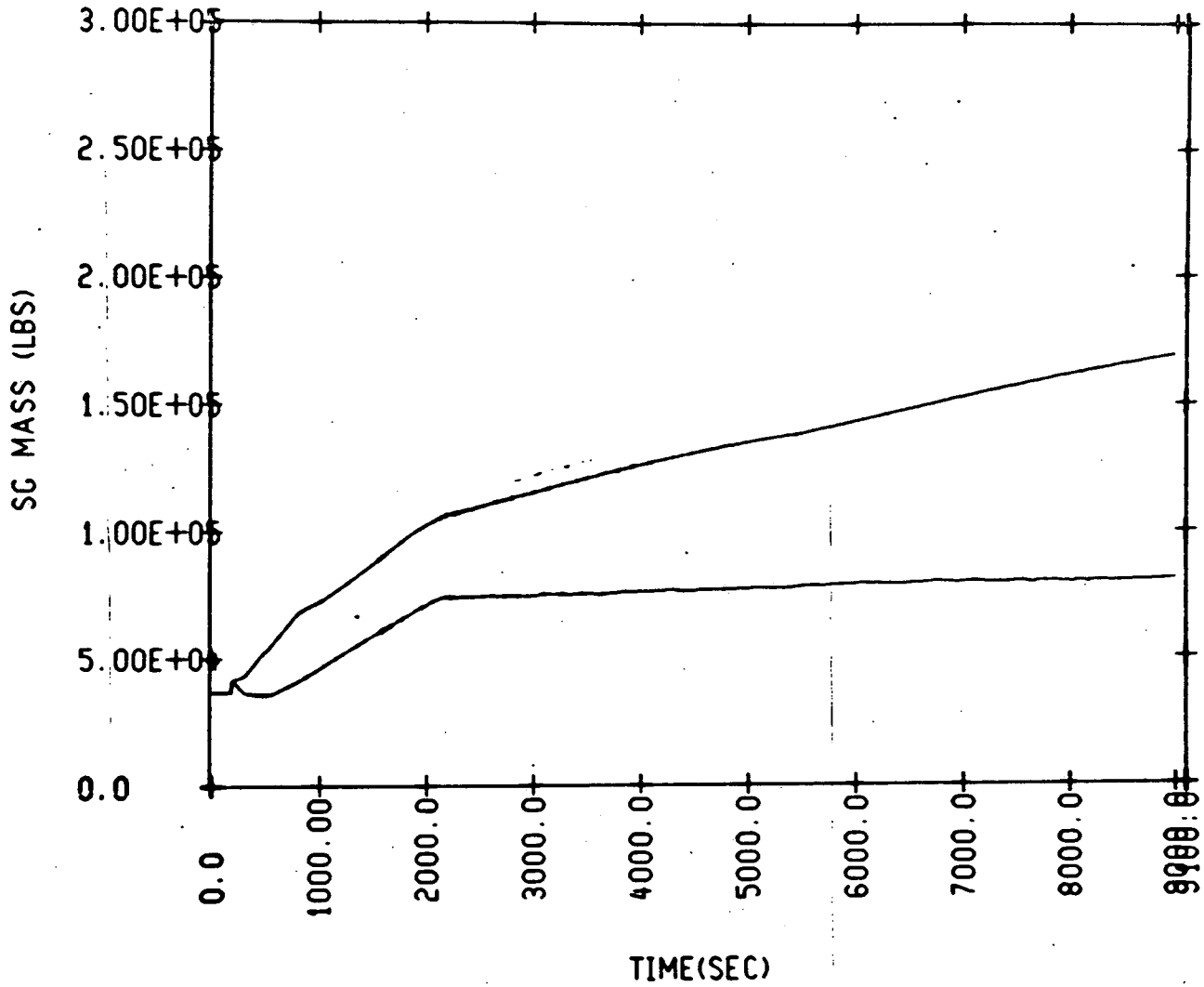
LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
PLOT 5 RUN 1



LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
PLOT 9 RUN 1

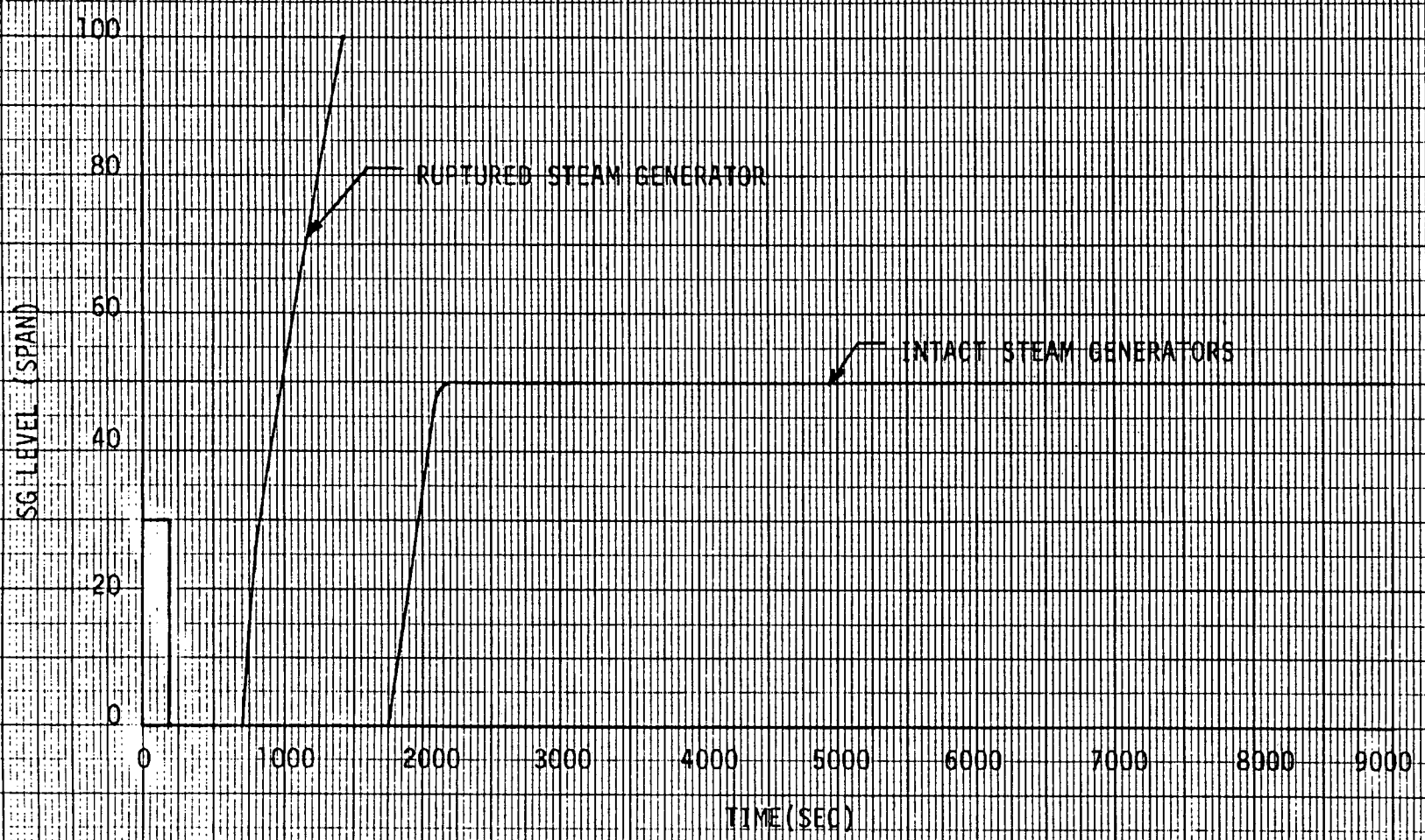


LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
PLOT11 RUN 1

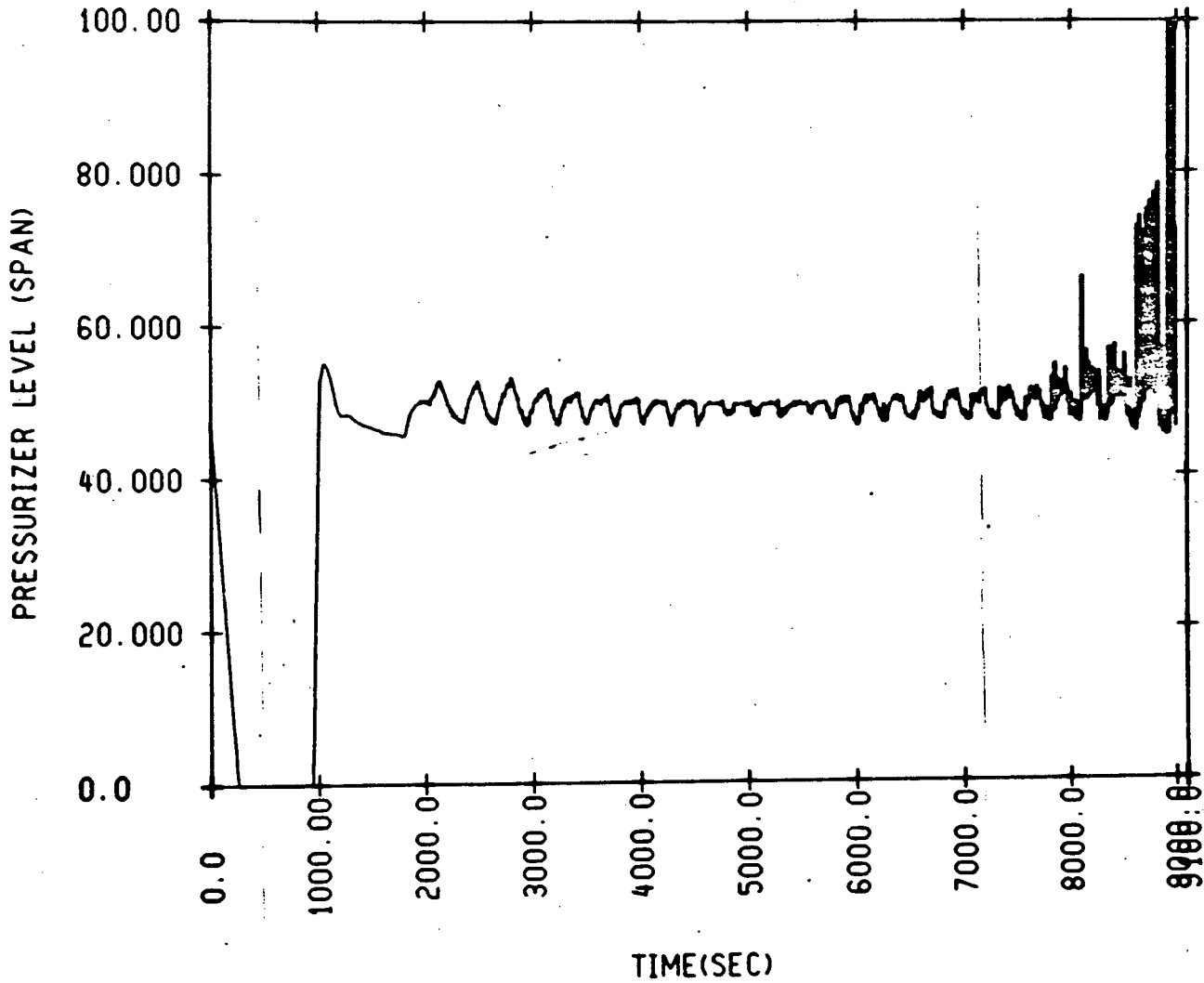




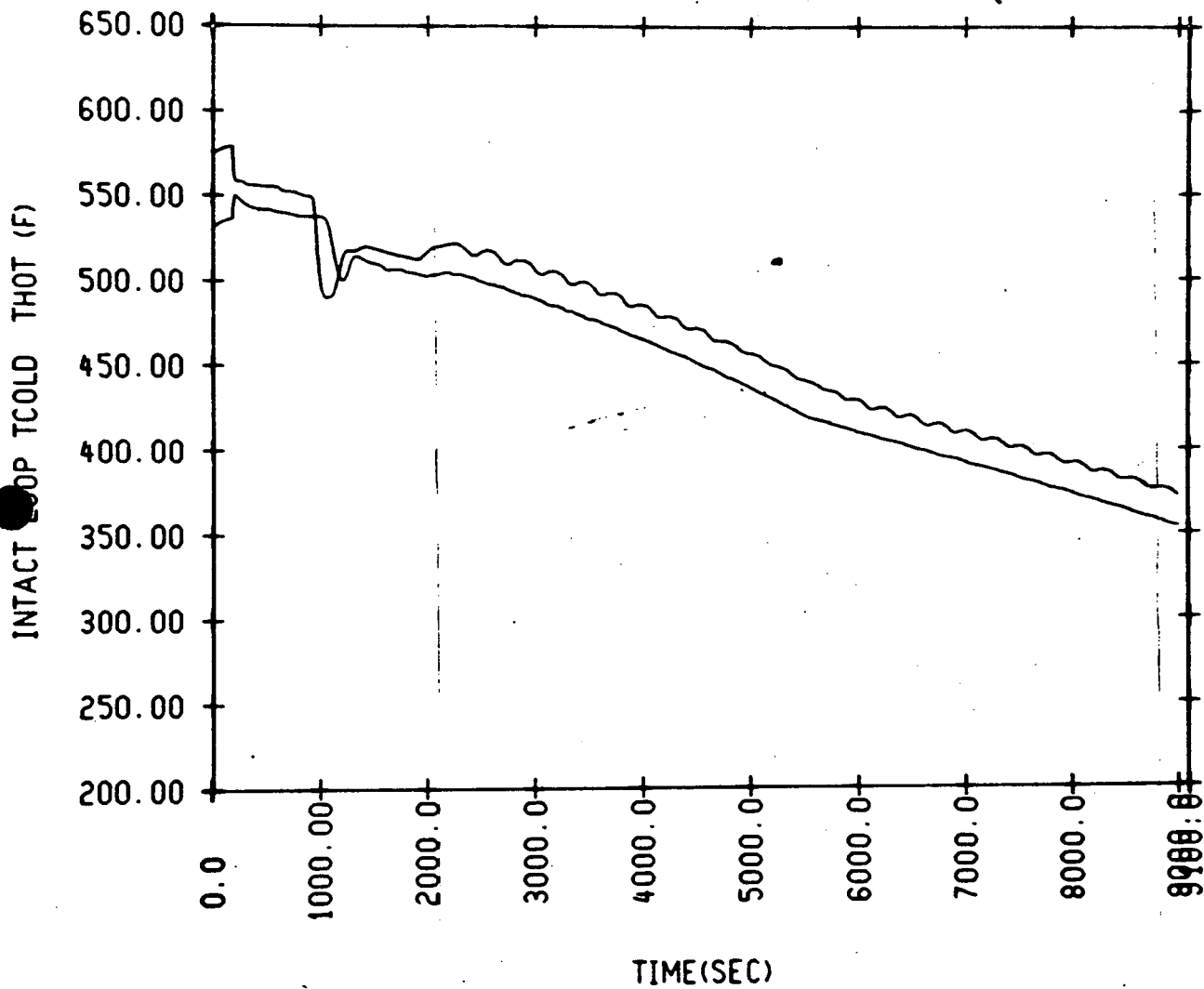
OFFSITE POWER LOST



LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
PLOT13 RUN 1



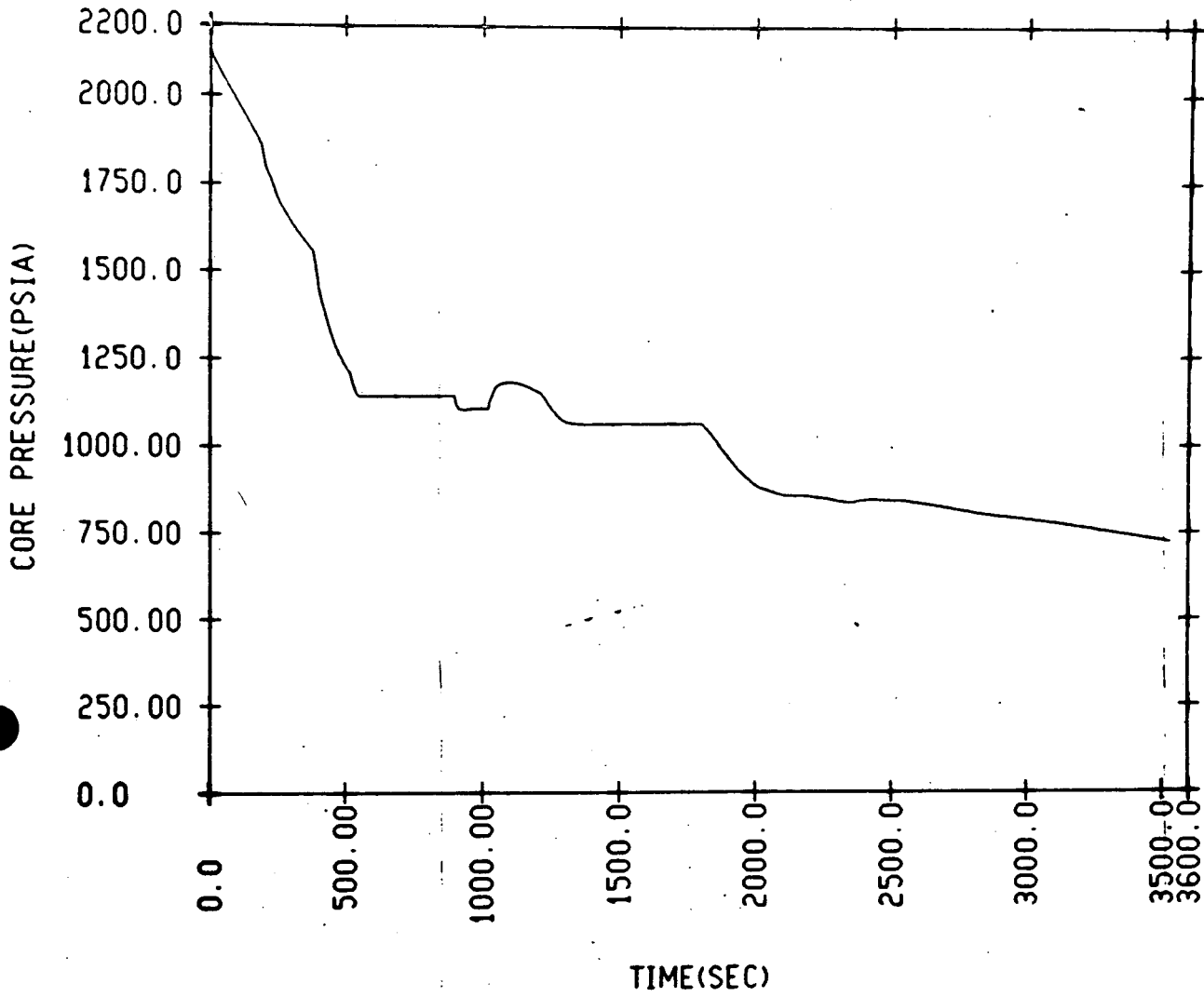
LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BEST ESTIMATE SGTR - OFFSITE POWER LOST  
PLOT16 RUN 1



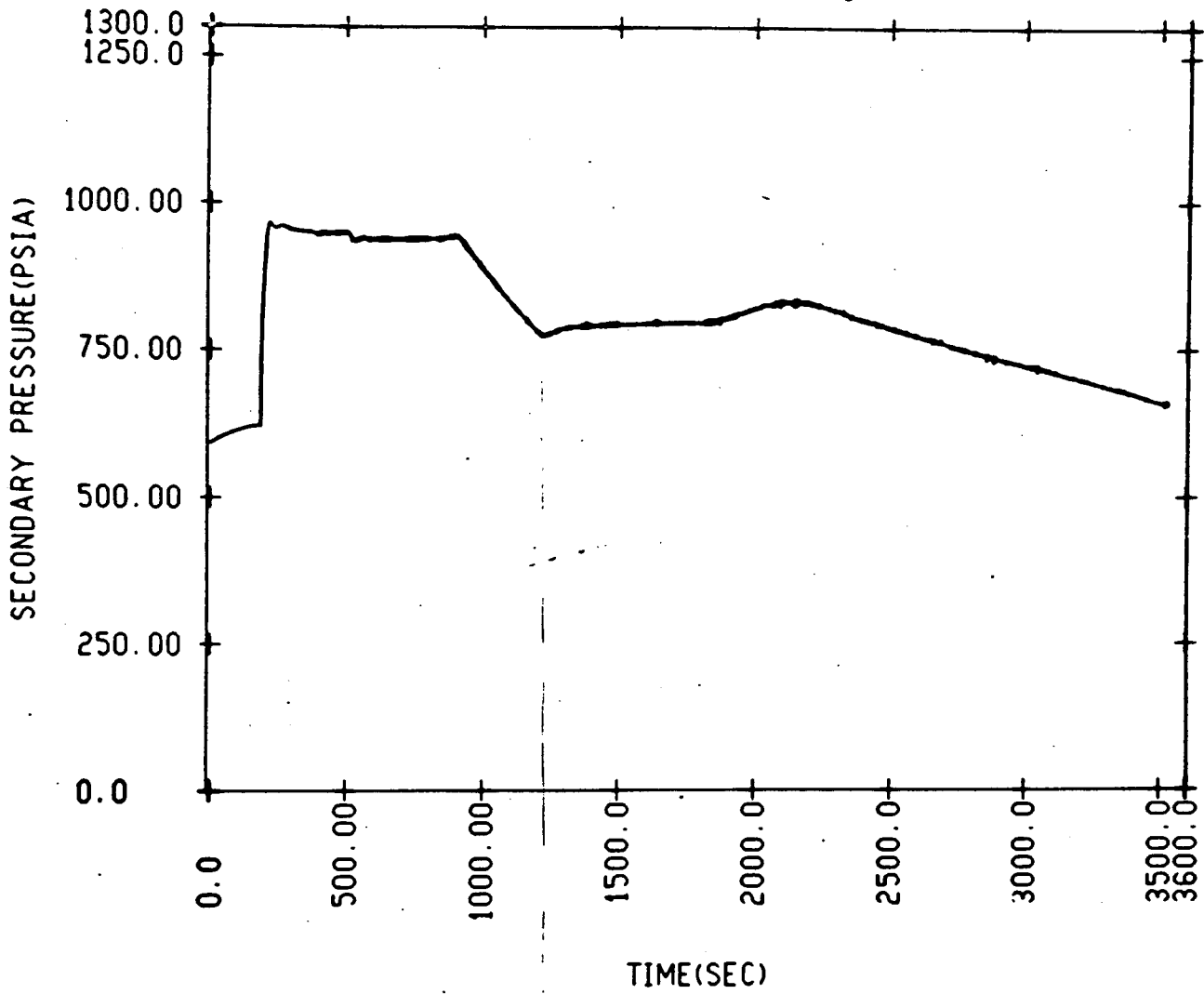
OFFSITE POWER AVAILABLE - SATURATED COOLDOWN - RCPS RUNNING

<u>EVENT</u>	<u>TIME (SEC)</u>
REACTOR TRIP	182.8
SI INITIATION	248.0
AUX. FEEDWATER INITIATION	286.0
AUX. FEEDWATER TERMINATED TO	870.0
PRESSURIZER PORV OPENED	900.0
PRESSURIZER PORV CLOSED	1023.0
MF/SI PUMPS STOPPED	1026.0
CHARGING FLOW THROTTLED TO MAINTAIN 50% LEVEL IN PRESSURIZER	1047.0
PRESSURIZER SPRAY ON	1800.0
~100°F/HR COOLDOWN INITIATED	1800.0
AUX. FEEDWATER THROTTLED TO INTACT SGS	~2100.0

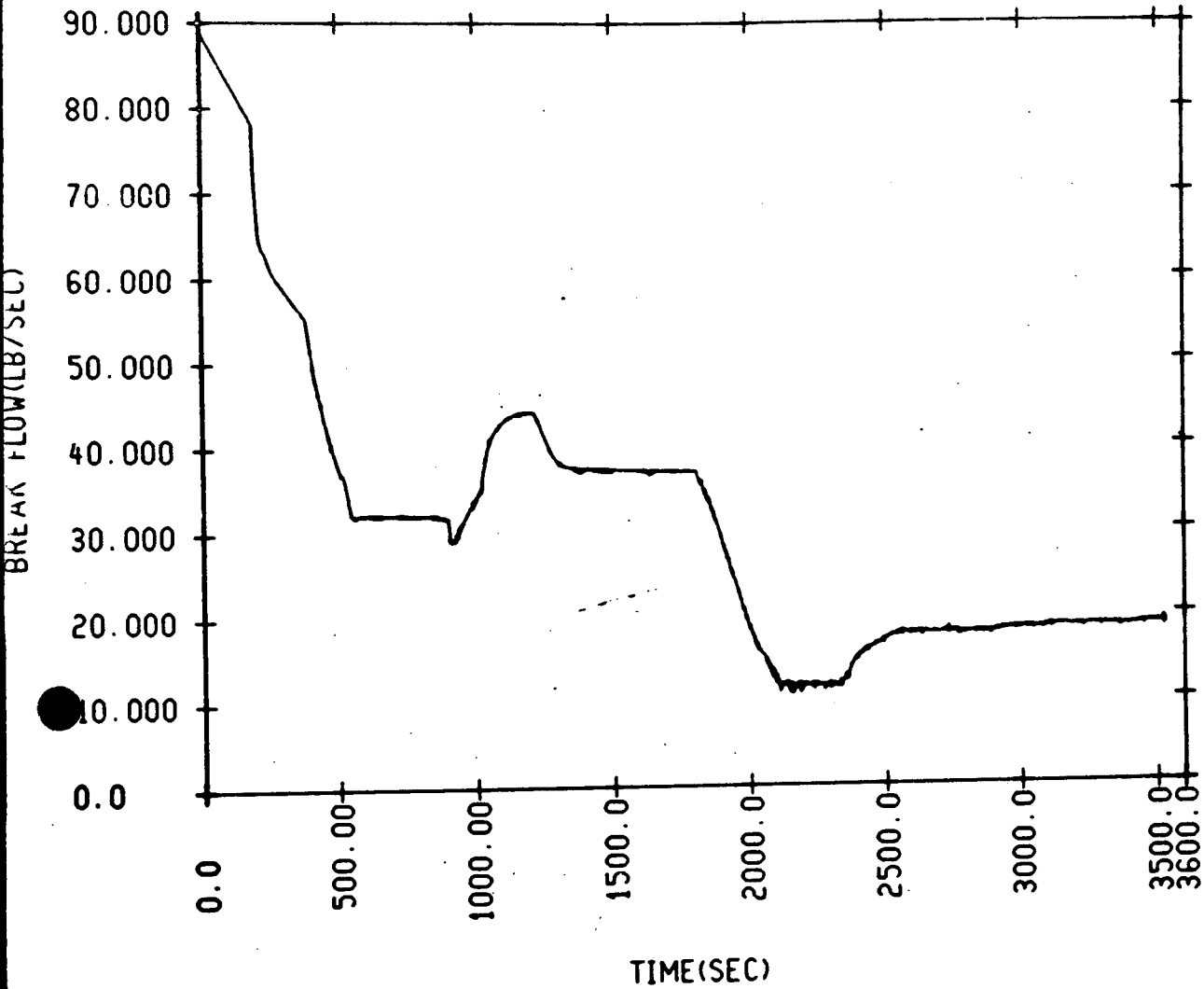
LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SGTR-OFF. POWER AVAIL.-RCPS RUNNING  
PLOT 1 RUN 1



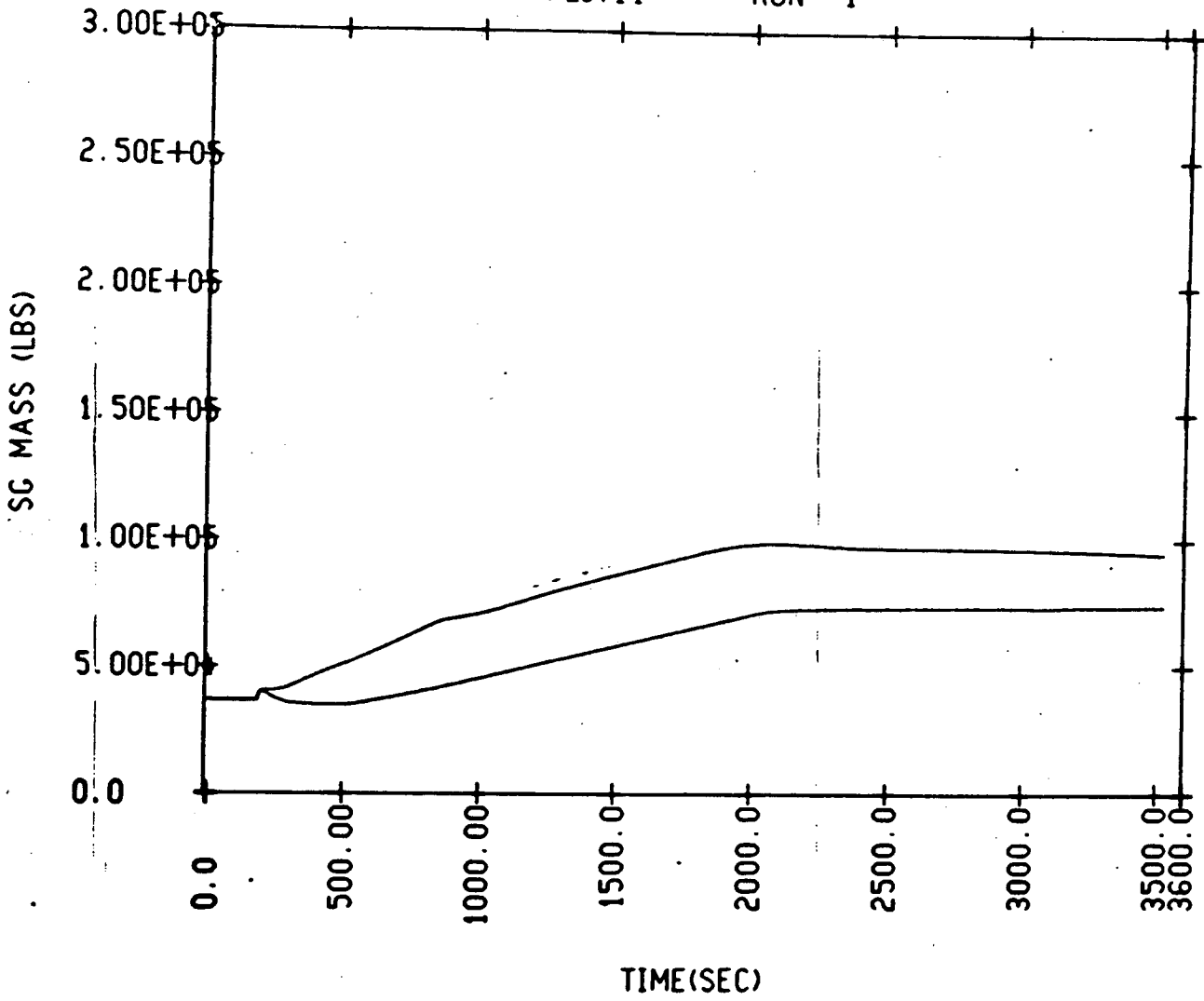
LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SGTR-OFF. POWER AVAIL. RCPS RUNNING  
PLOT 5 RUN 1



LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SCGR-OFF. POWER AVAIL. -RCPS RUNNING  
PLOT 9 RUN 1

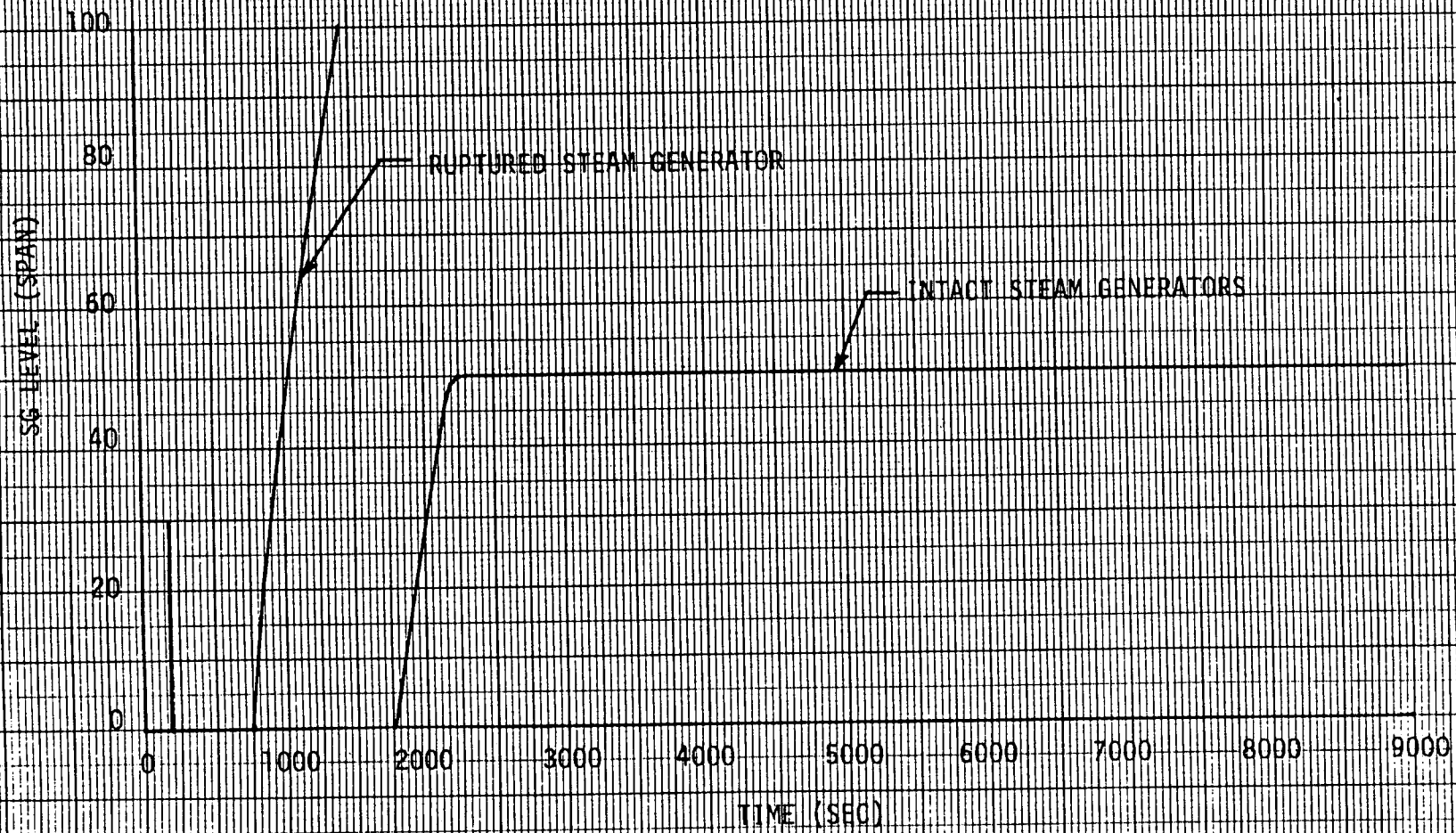


LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SGTR-OFF. POWER AVAIL. -RCPS RUNNING  
PLOT11 RUN 1

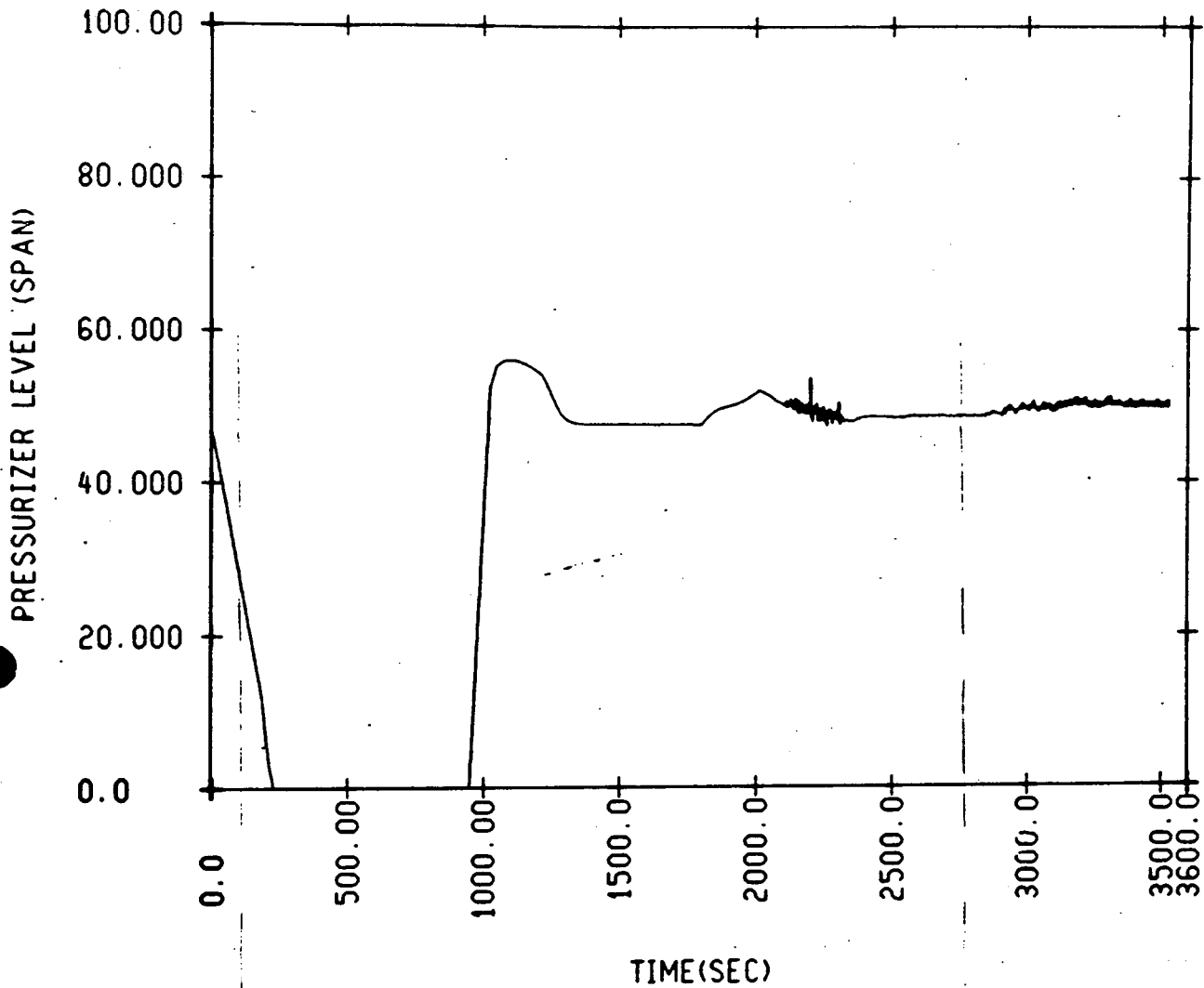




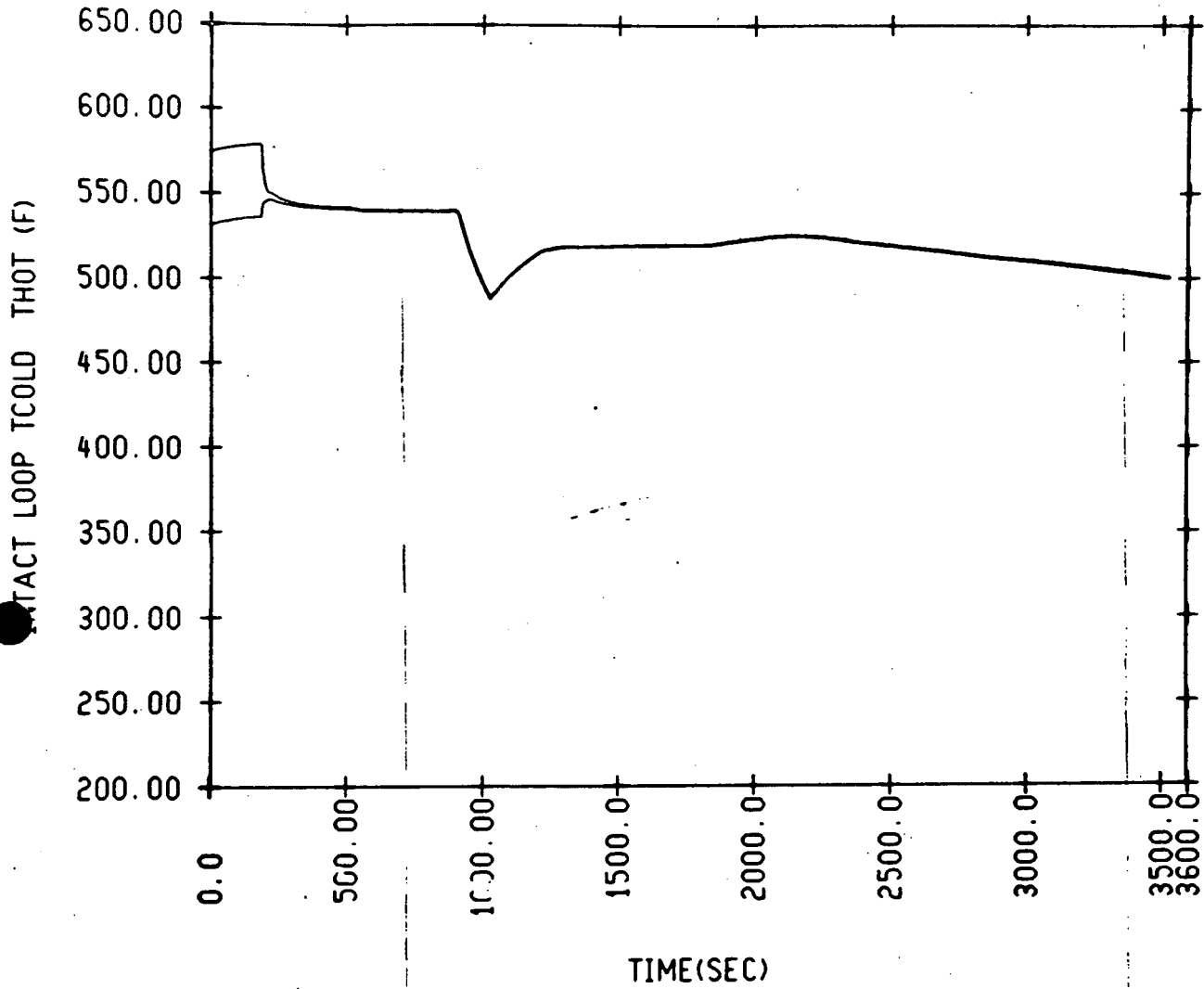
OFFSITE POWER AVAILABLE - RCP RUNNING



LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SGTR-OFF. POWER AVAIL. -RCPS RUNNING  
PLOT13 RUN 1



LOFT-4 STEAM GENERATOR TUBE RUPTURE  
SCE BE SGTR-OFF. POWER AVAIL.-RCPS RUNNING  
PLOT16 RUN 1



ENCLOSURE 3

FEED AND BLEED ANALYSIS

E<sup>2</sup>01-2

INSTRUCTIONS TO MITIGATE  
INADEQUATE CORE COOLING (ICC) RESULTING  
FROM A LOSS OF SECONDARY COOLING

- ASSUMES HIGH HEAD SAFETY INJECTION  
IS AVAILABLE
  - A LOW PRESSURE WATER SOURCE IS AVAILABLE  
TO DEPRESSURIZED STEAM GENERATOR'S
-

PERFORM VITAL STEPS  
OF INITIATING EVENT  
OPERATING INSTRUCTION

ATTEMPT TO RESTORE  
SECONDARY COOLING

- A) AUX FEED
- B) MAIN FEED
- C) CONDENSATE

MANUALLY START SAFETY  
INJECTION WHEN  
RCS PARAMETERS INCREASE

OPEN PRESSURIZER PORV'S  
TO DEPRESSURIZE THE RCS AND  
INCREASE SI FLOW

TRIP ALL REACTOR  
COOLANT PUMPS TO  
MAINTAIN INVENTORY

**CLOSE PRESSURIZER PORV'S**

**WHEN:**

- A) S/G LEVEL**
- B) RCS SUBCOOLING**

**TERMINATE SI WHEN:**

- A) PRESSURE**
- B) PRESSURIZER LEVEL**
- C) SUBCOOLING**

**SI REINITIATION**

- A) PRESSURE**
- B) PRESSURIZER LEVEL**
- C) SUBCOOLING**

**RE-ESTABLISH NORMAL PRESSURE AND LEVEL CONTROL**

**FOLLOW NORMAL COOLDOWN PROCEDURES**

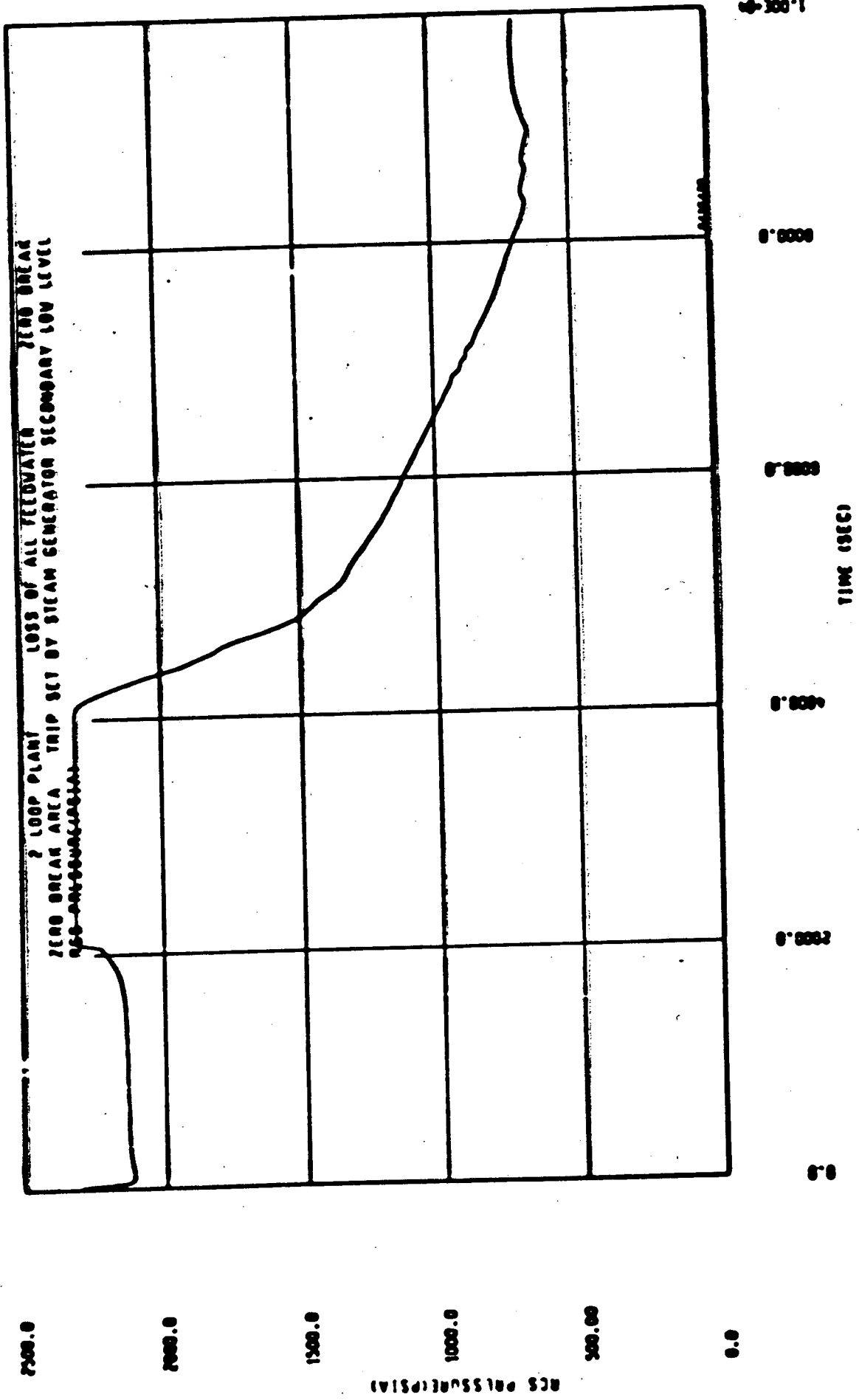
LOSS OF HEAT SINK

Differences of SCE Versus Generic Guidelines

- . REALIGN AND MAXIMIZE CHARGING FLOW
- . ELIMINATION OF COLD LEG ACCUMULATOR CONSIDERATION
- . CONTINGENCY FOR COMPLETE LOSS OF MF/SI AND MF

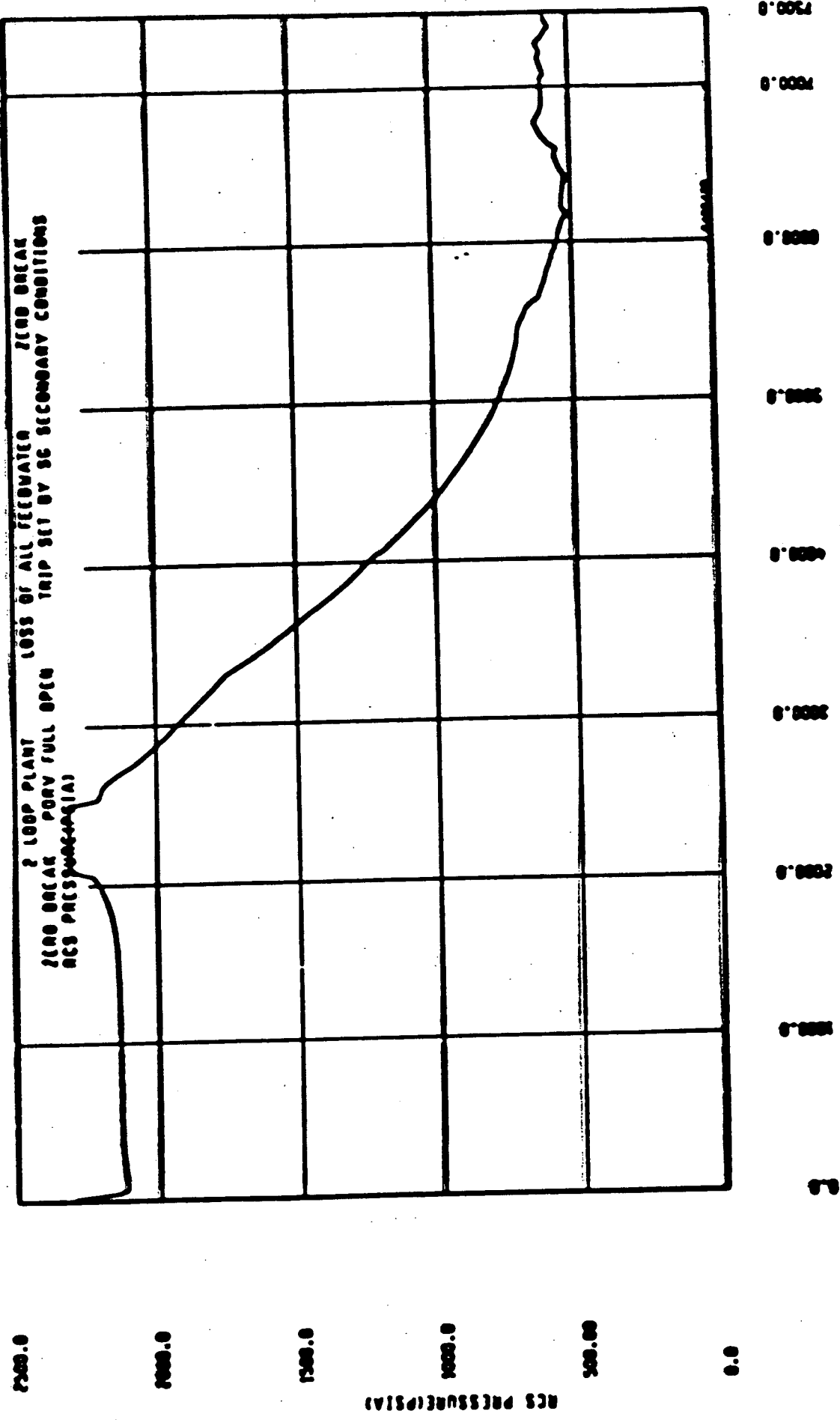


CASE 1: LOSS OF FEEDWATER  
AUXILIARY FEEDWATER INITIATED AT 4000 SECONDS  
GENERIC TWO-LOOP PLANT  
CASE A SECTION 4.2 WCAP-9600



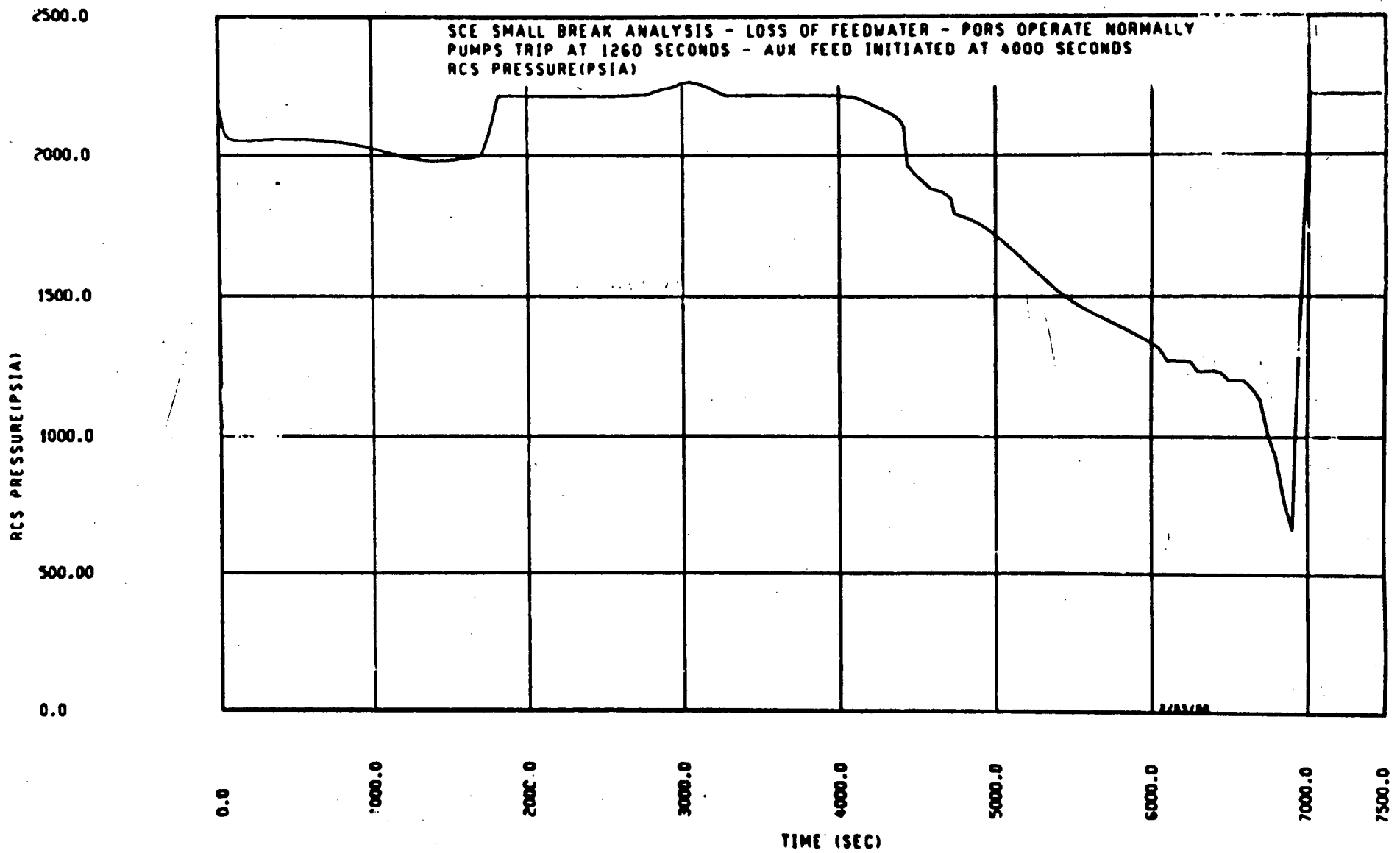
Loss of Feed  
Zero Brk  
Aux Feed on  
@ 4000 sec

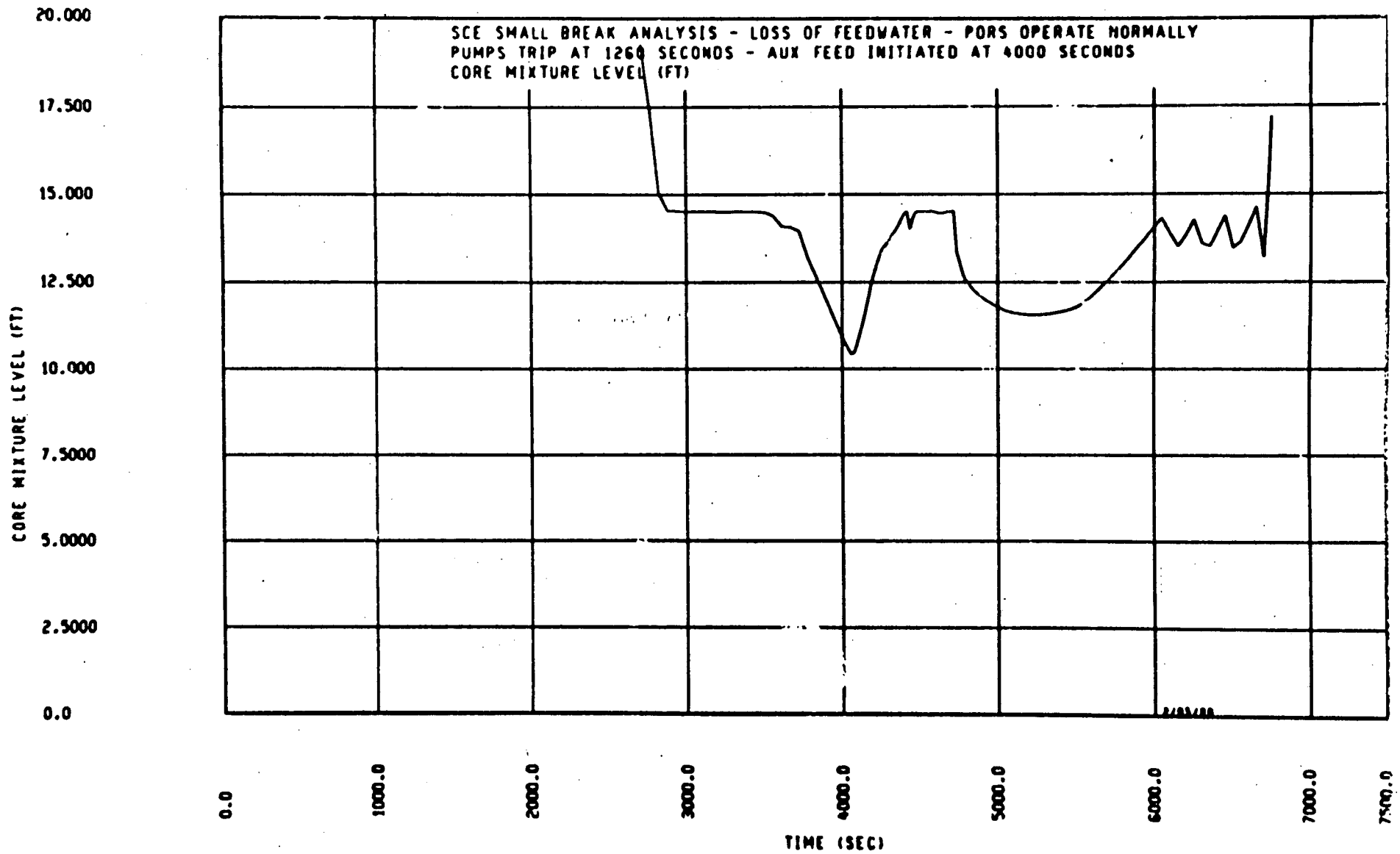
CASE 2: LOSS OF FEEDWATER  
PORVs OPEN AT 2500 SECONDS  
GENERIC TWO-LOOP PLANT  
CASE B SECTION 4.2 WCAP-9600



Loss of Feed  
 Zero Brk  
 PORV open @  
 2500 sec

CASE 3: LOSS OF FEEDWATER  
AUXILIARY FEEDWATER INITIATED AT 4000 SECONDS  
SAN ONOFRE UNIT 1  
SECTION 4.1 STUDY OF SMALL LOSS OF COOLANT  
ACCIDENTS FOR THE SAN ONOFRE NUCLEAR GENERATING STATION UNIT 1





60.000

50.000

40.000

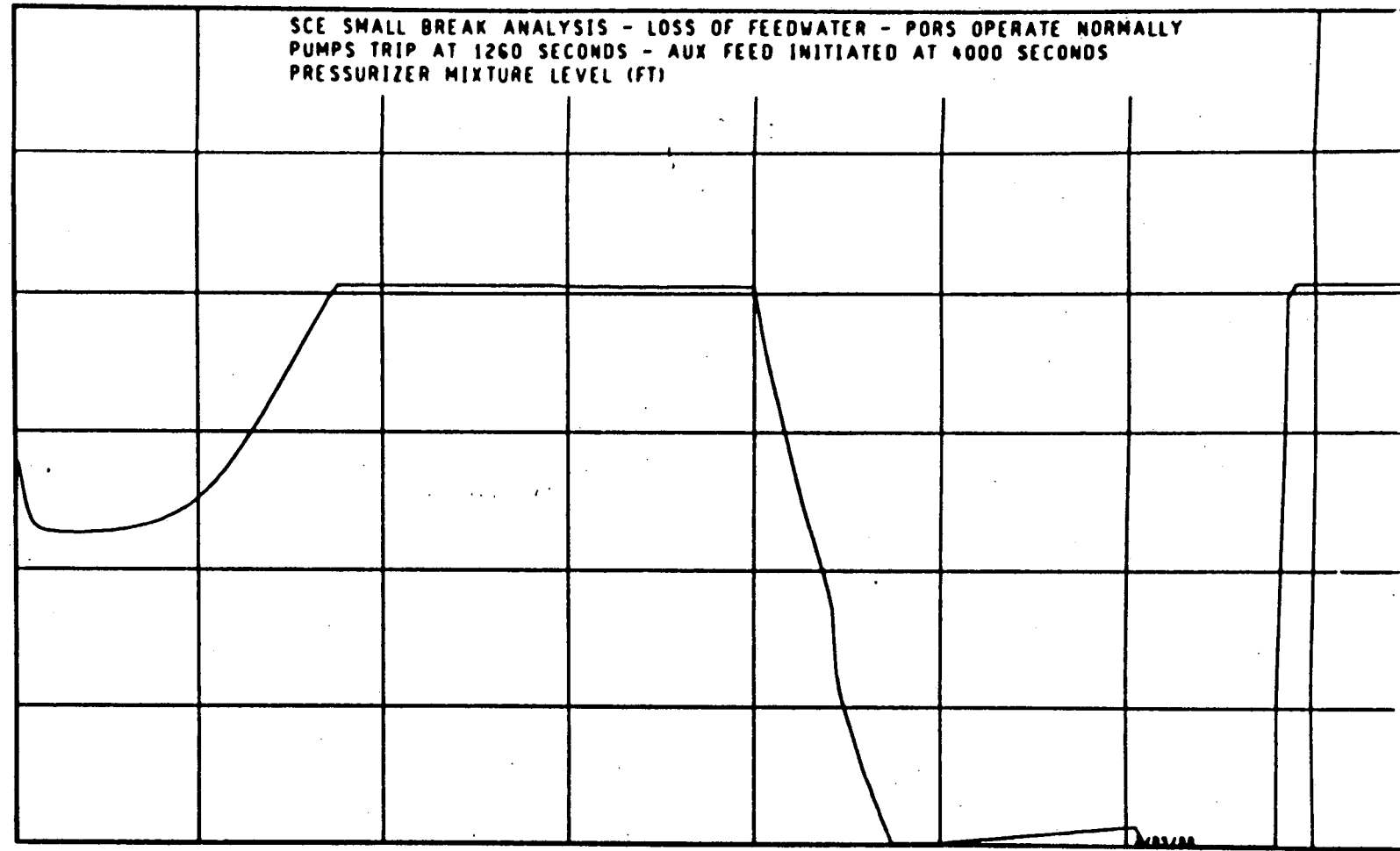
30.000

20.000

10.000

0.0

PRESSURIZER MIXTURE LEVEL (FT)



0.0

1000.0

2000.0

3000.0

4000.0

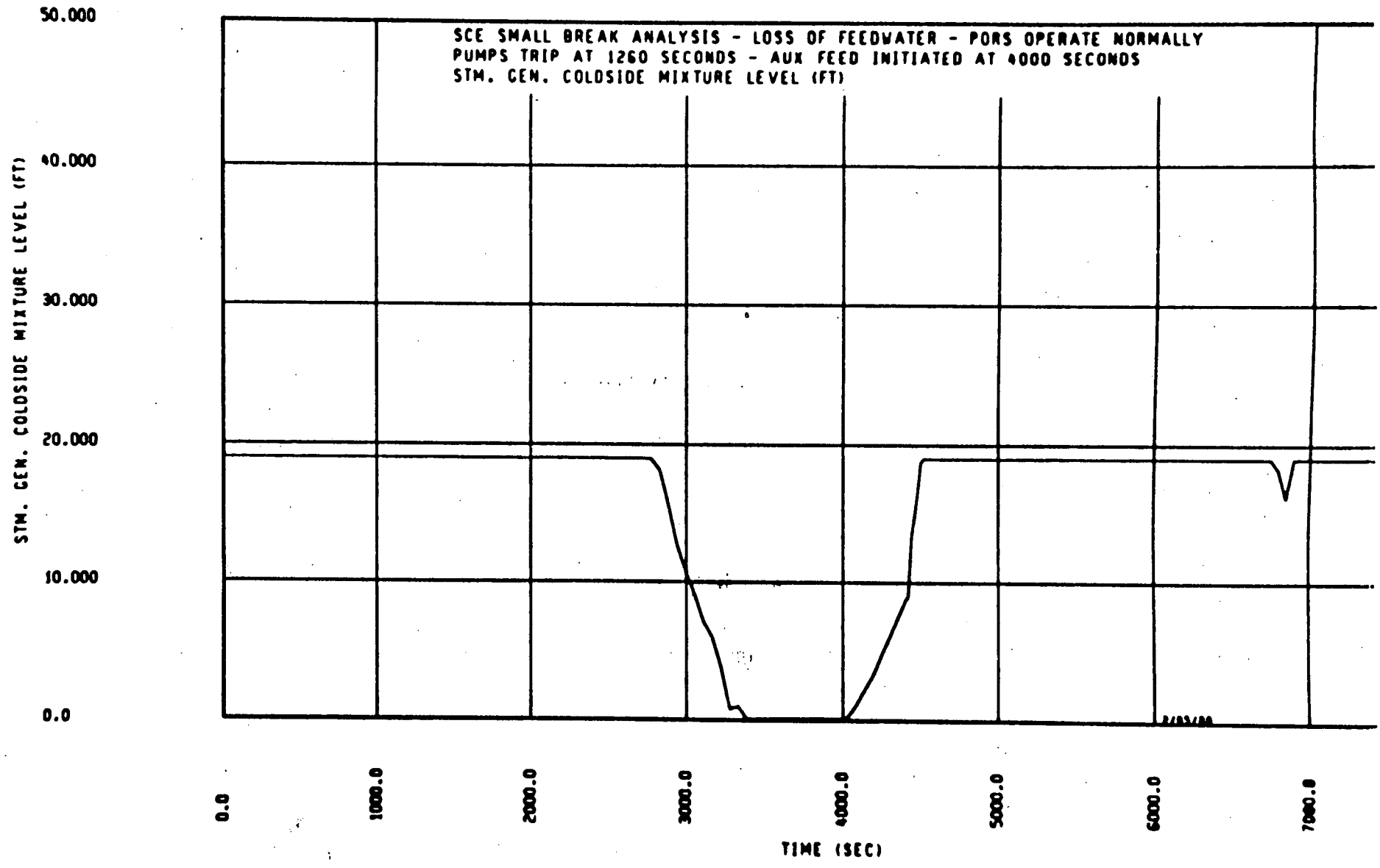
5000.0

6000.0

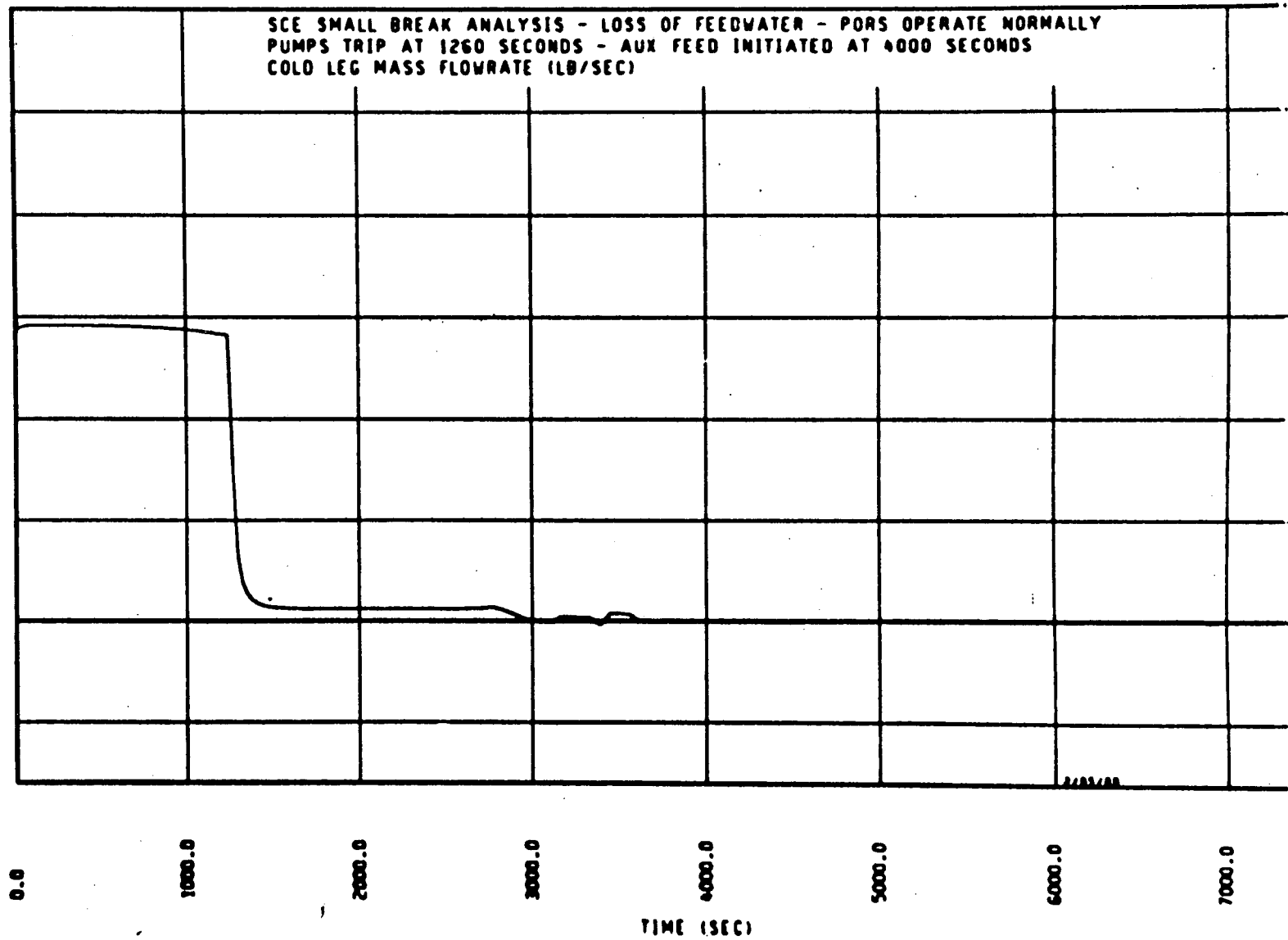
7000.0

TIME (SEC)



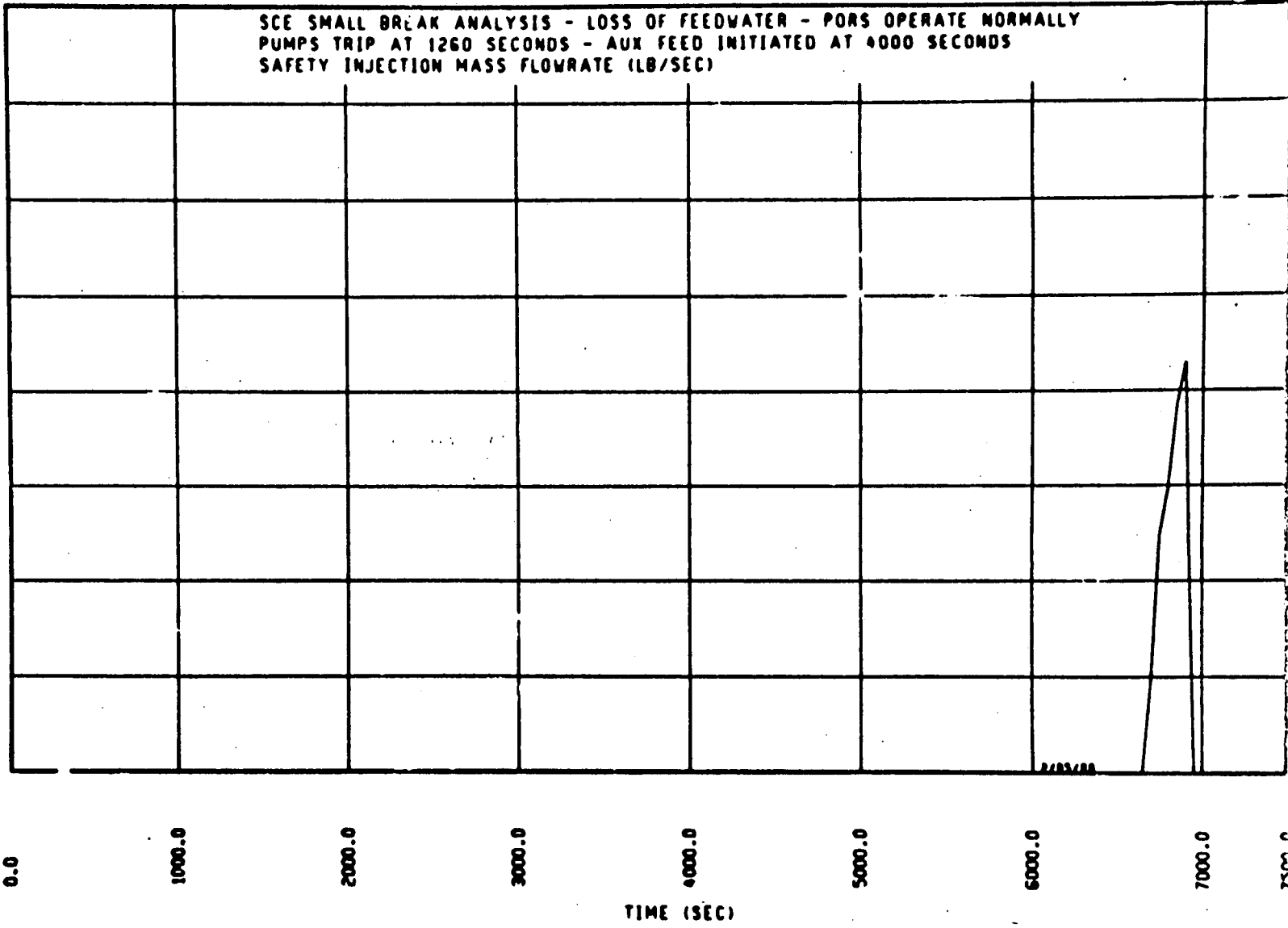


COLD LEG MASS FLOWRATE (LB/SEC)

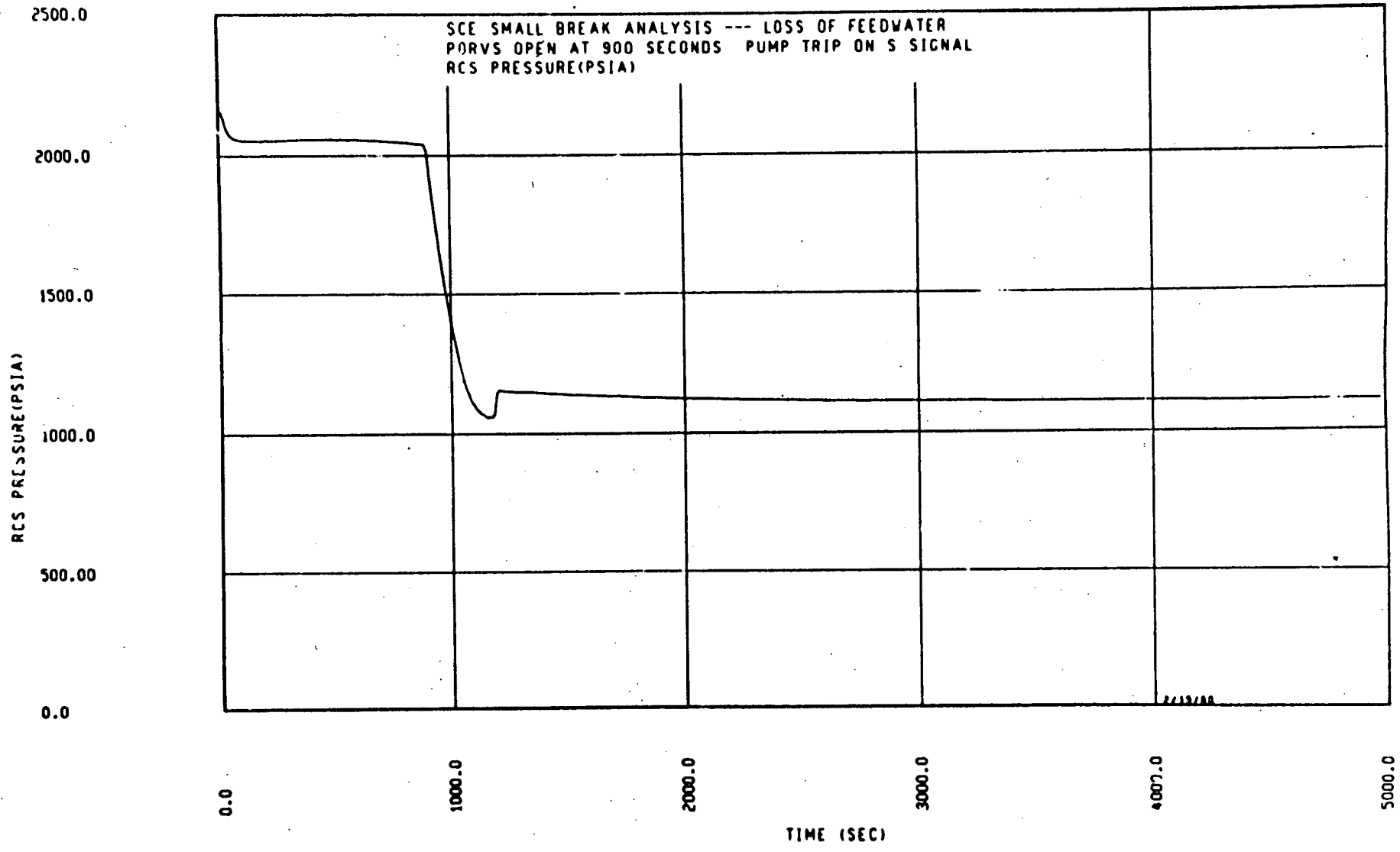


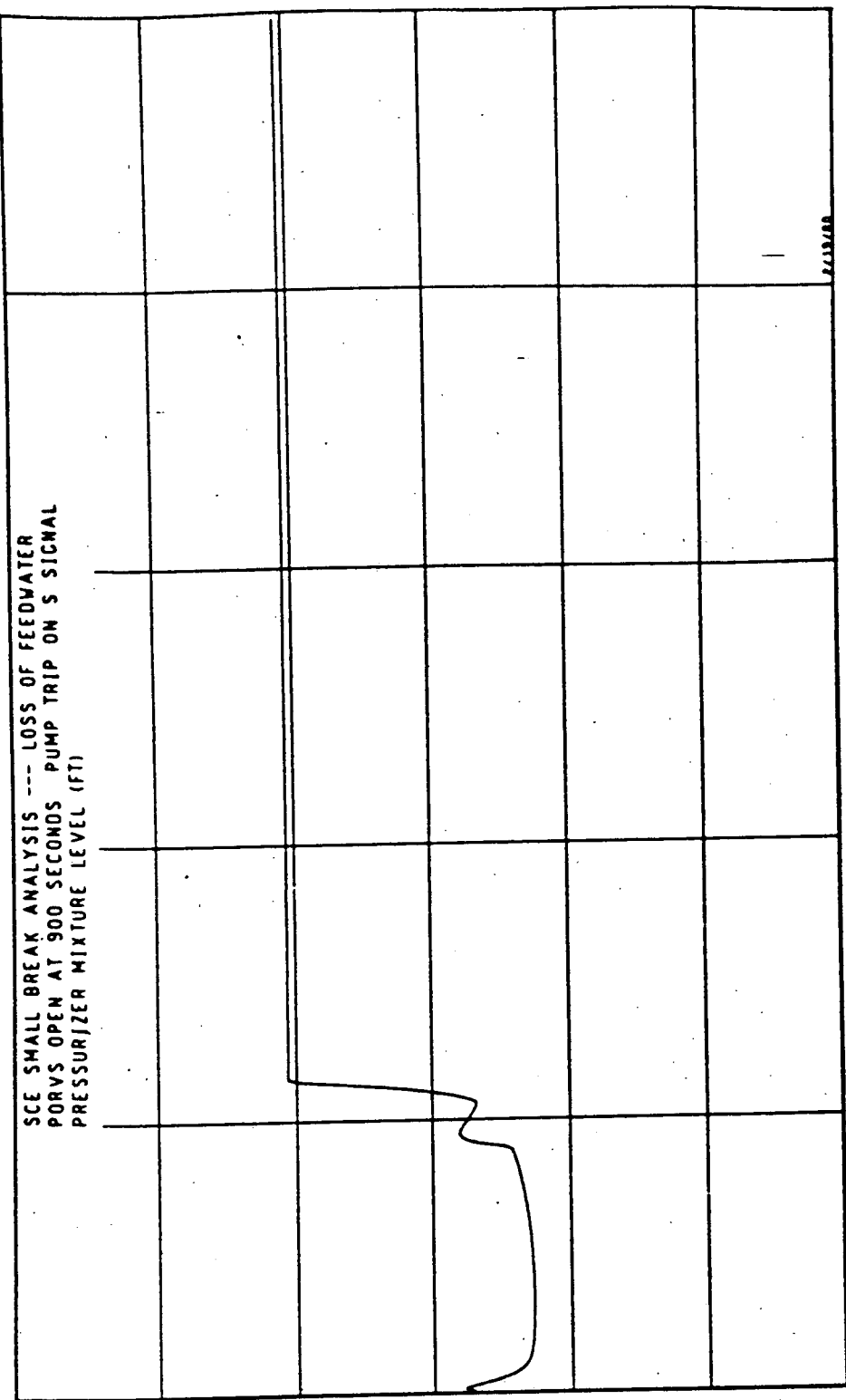
2000.0  
1750.0  
1500.0  
1250.0  
1000.0  
750.0  
500.0  
250.0  
0.0

SAFETY INJECTION MASS FLOWRATE (LB/SEC)



CASE 4: LOSS OF FEEDWATER  
PORVs OPEN AT 900 SECONDS  
SAN ONOFRE UNIT 1  
SECTION 4.1 STUDY OF SMALL LOSS OF COOLANT  
ACCIDENTS FOR THE SAN ONOFRE NUCLEAR GENERATING STATION UNIT 1





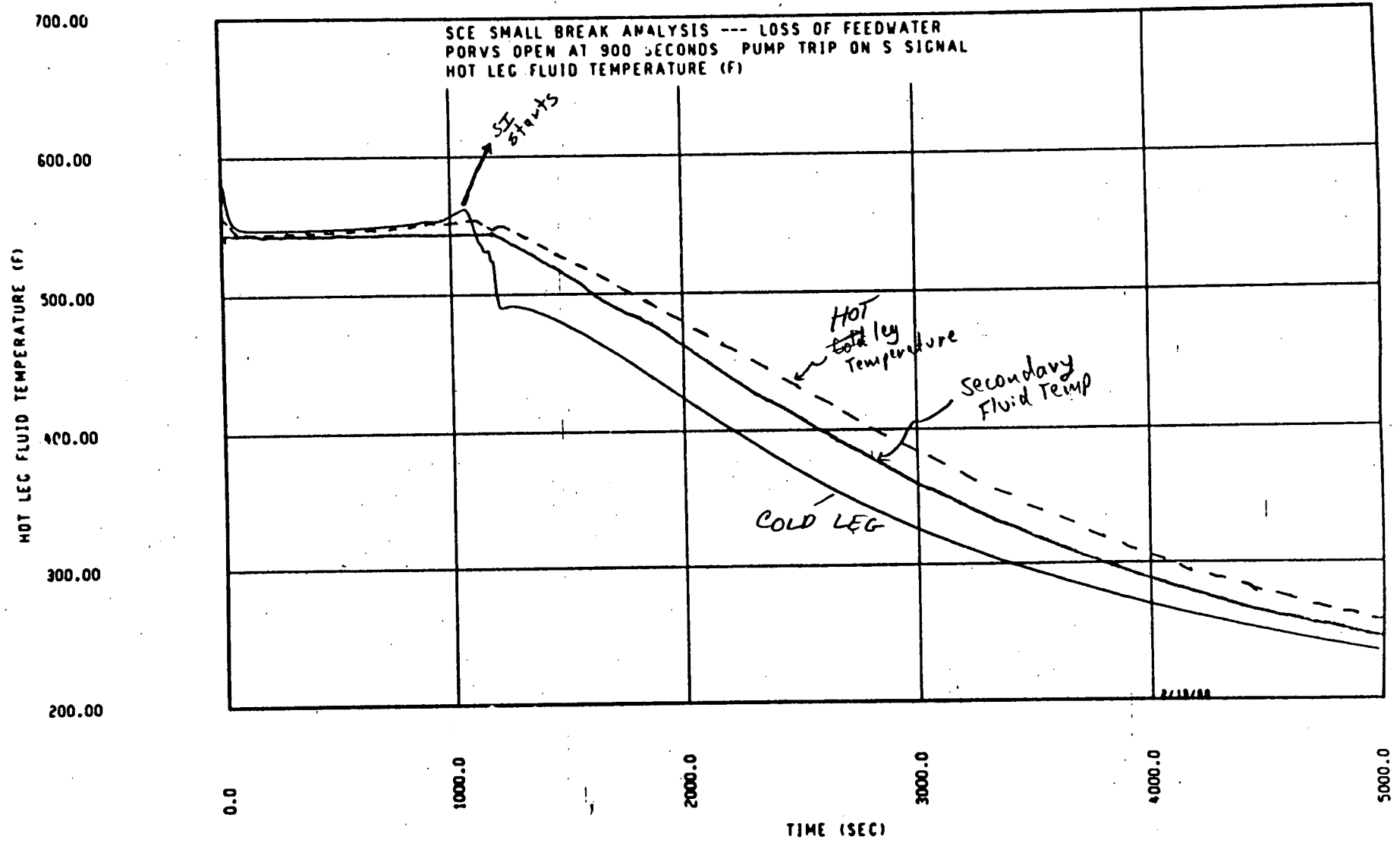
SCE SMALL BREAK ANALYSIS --- LOSS OF FEEDWATER  
 PORVS OPEN AT 900 SECONDS PUMP TRIP ON S SIGNAL  
 PRESSURIZER MIXTURE LEVEL (FT)

60.000  
 50.000  
 40.000  
 30.000  
 20.000  
 10.000  
 0.0

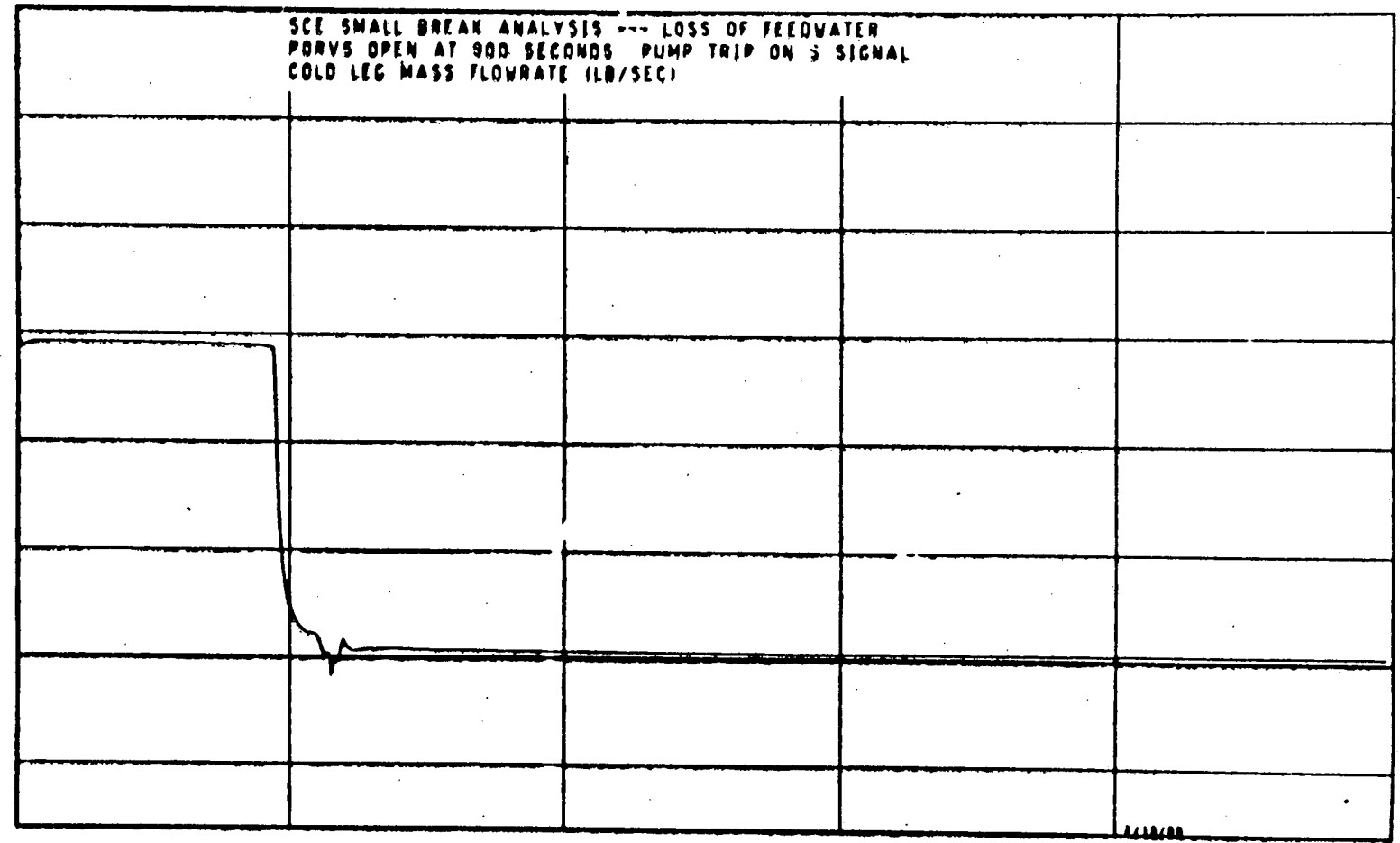
PRESSURIZER MIXTURE LEVEL (FT)

5000.0  
 4000.0  
 3000.0  
 2000.0  
 1000.0  
 0.0

TIME (SEC)



1.50E+04  
1.25E+04  
1.00E+04  
7500.0  
5000.0  
2500.0  
0.0  
-2500.0  
-5000.0



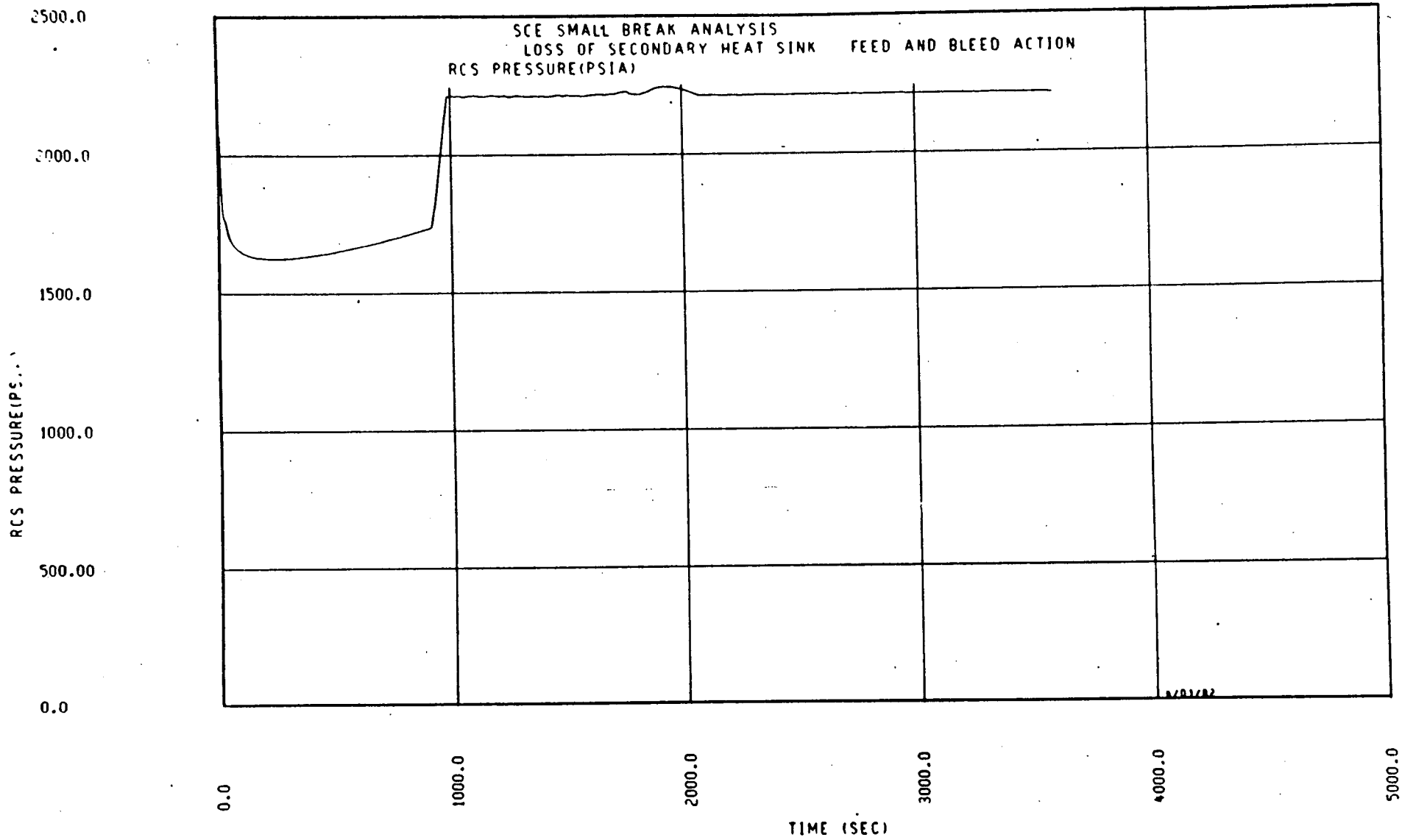
0.0 1000.0 2000.0 3000.0 4000.0 5000.0

TIME (SEC)



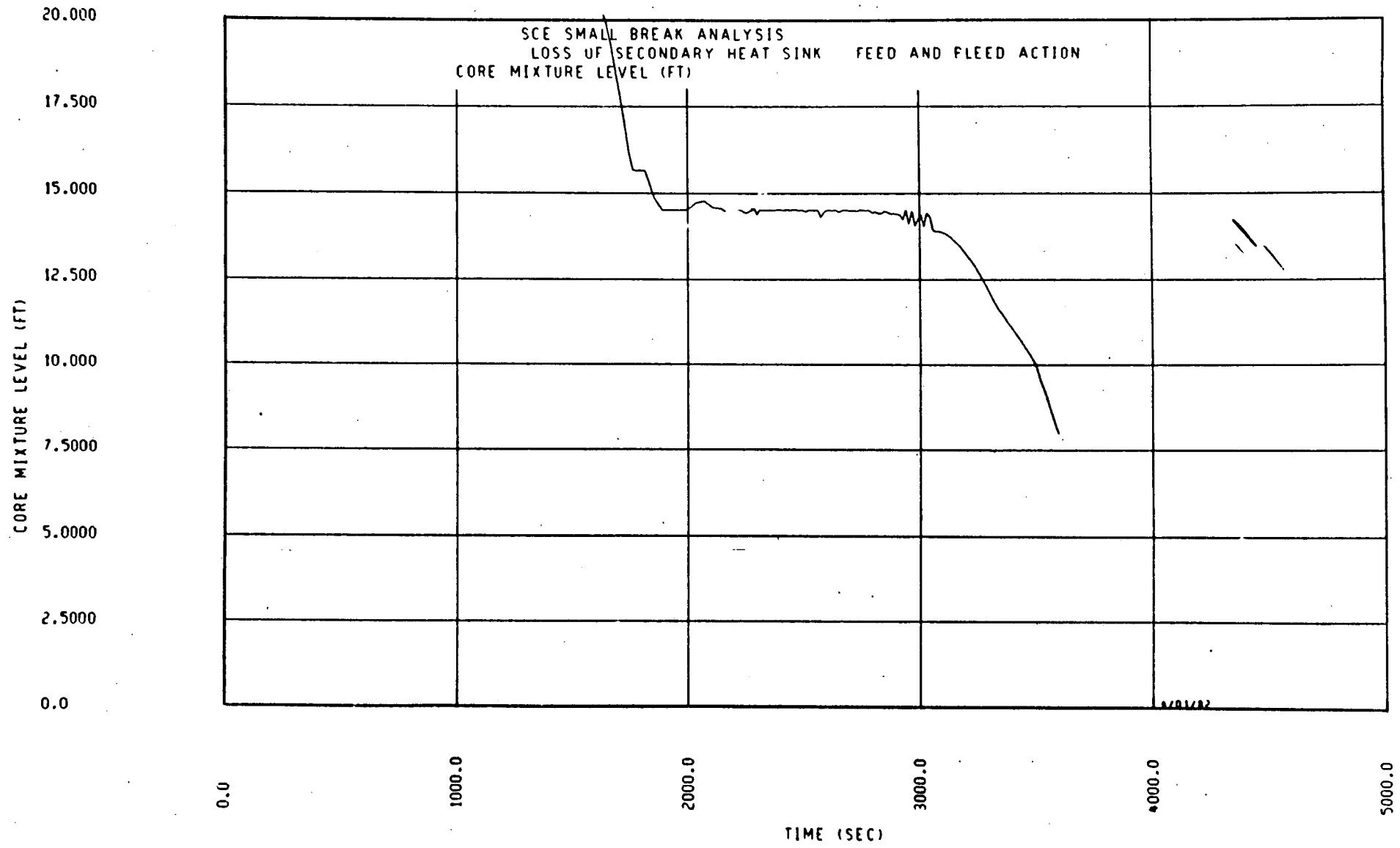
CASE 5: COINCIDENT STEAMLINER BREAK, FEEDLINE BREAK,  
LOSS OF SAFETY INJECTION, LOSS OF AUXILIARY FEEDWATER  
SAN ONOFRE UNIT 1  
NO BLEED AND FEED ACTION

SCE SMALL BREAK ANALYSIS  
LOSS OF SECONDARY HEAT SINK FEED AND BLEED ACTION  
RCS PRESSURE(P.S.I.A)



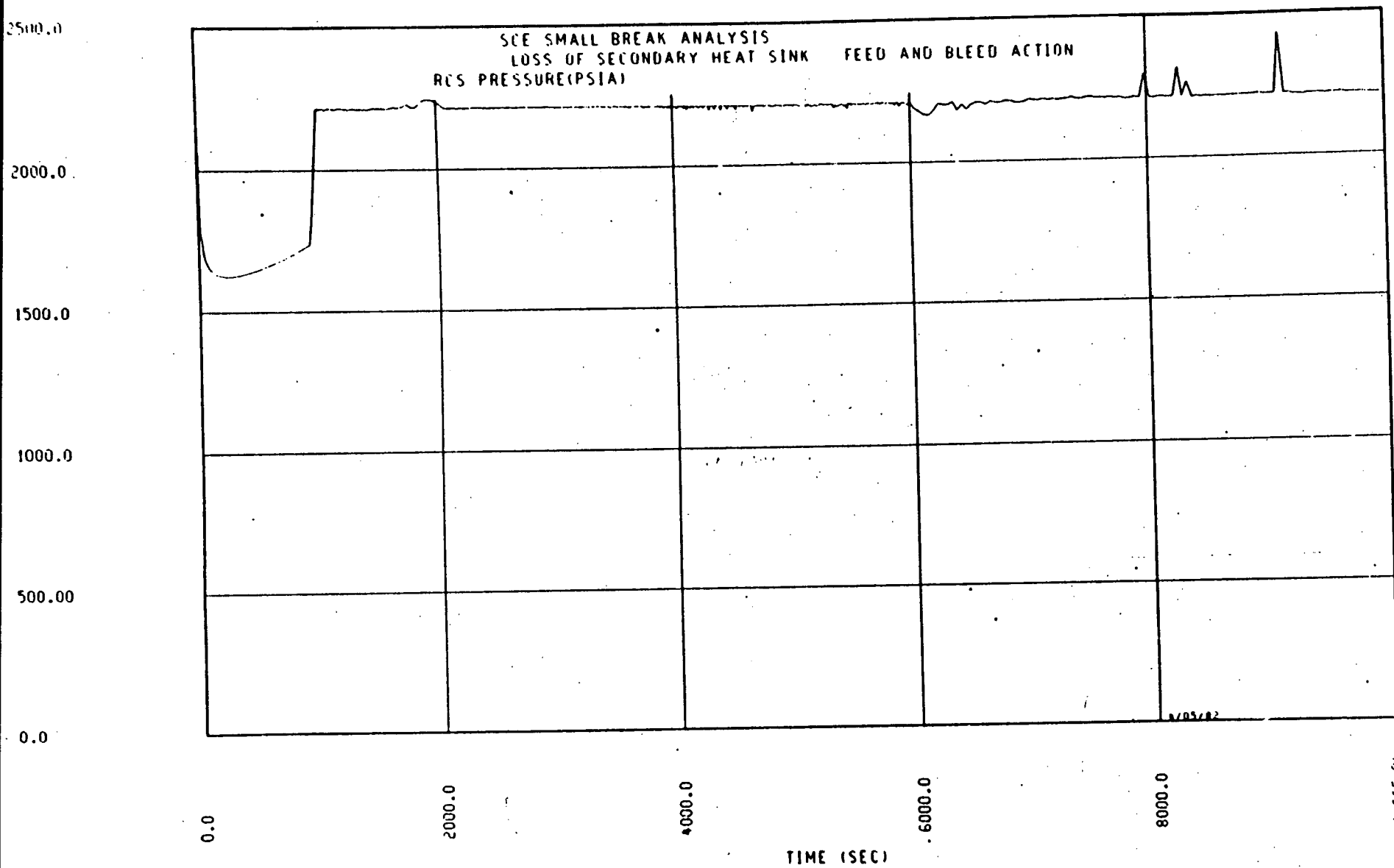
4/01/82

SCE SMALL BREAK ANALYSIS  
LOSS OF SECONDARY HEAT SINK FEED AND FLEED ACTION  
CORE MIXTURE LEVEL (FT)

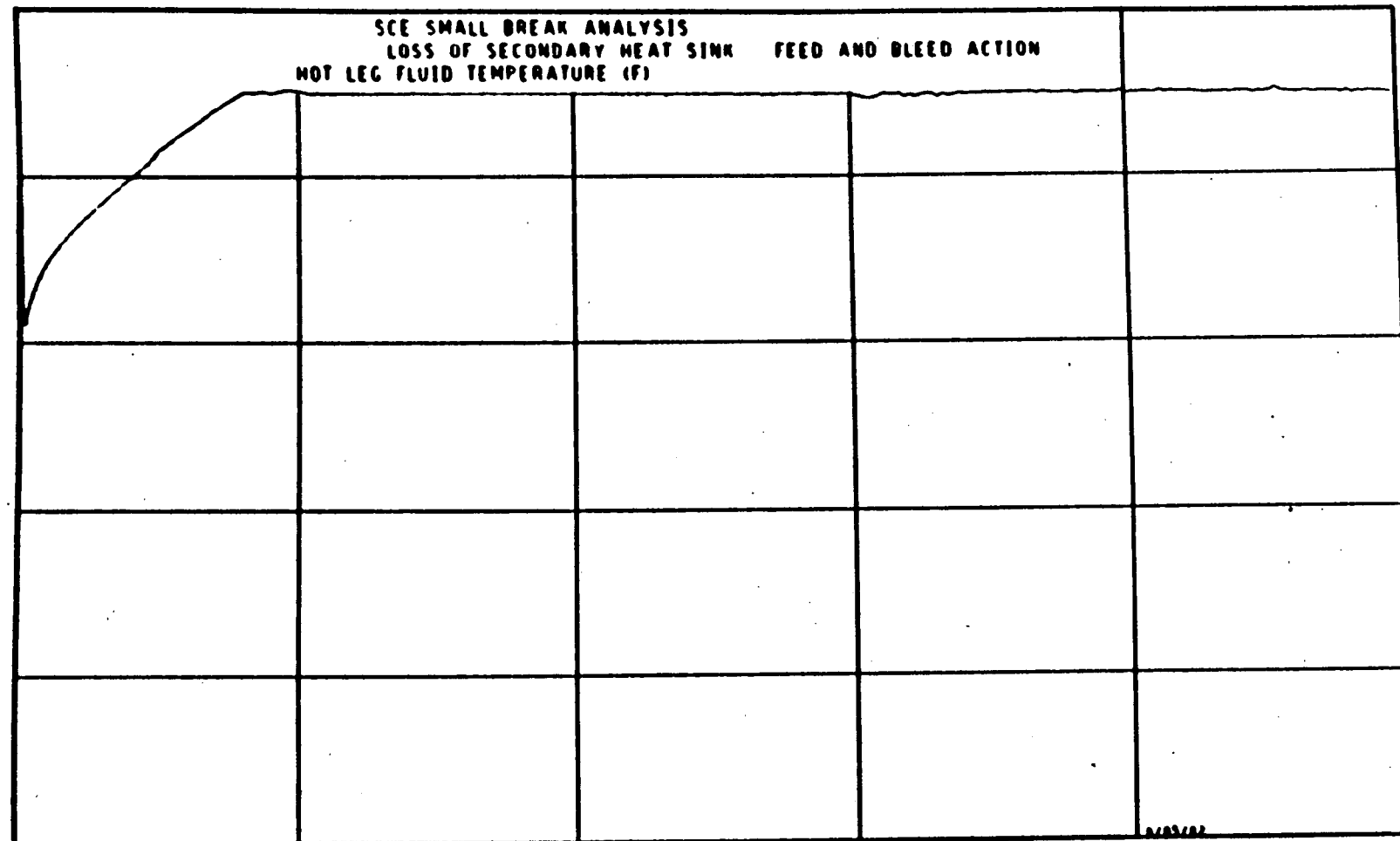


4/8/82

CASE 6: COINCIDENT STEAMLINE BREAK, FEEDLINE BREAK,  
LOSS OF SAFETY INJECTION, LOSS OF AUXILIARY FEEDWATER  
SAN ONOFRE UNIT 1  
BLEED AND FEED ACTION INITIATED AT 3000 SECONDS



SCE SMALL BREAK ANALYSIS  
LOSS OF SECONDARY HEAT SINK FEED AND BLEED ACTION  
HOT LEG FLUID TEMPERATURE (F)



1.4000  
1.2500  
1.0000  
0.7500  
0.5000  
0.2500  
0.0

STM. GEN. COLD SIDE MIXTURE QUALITY (-)

0.0

2000.0

4000.0

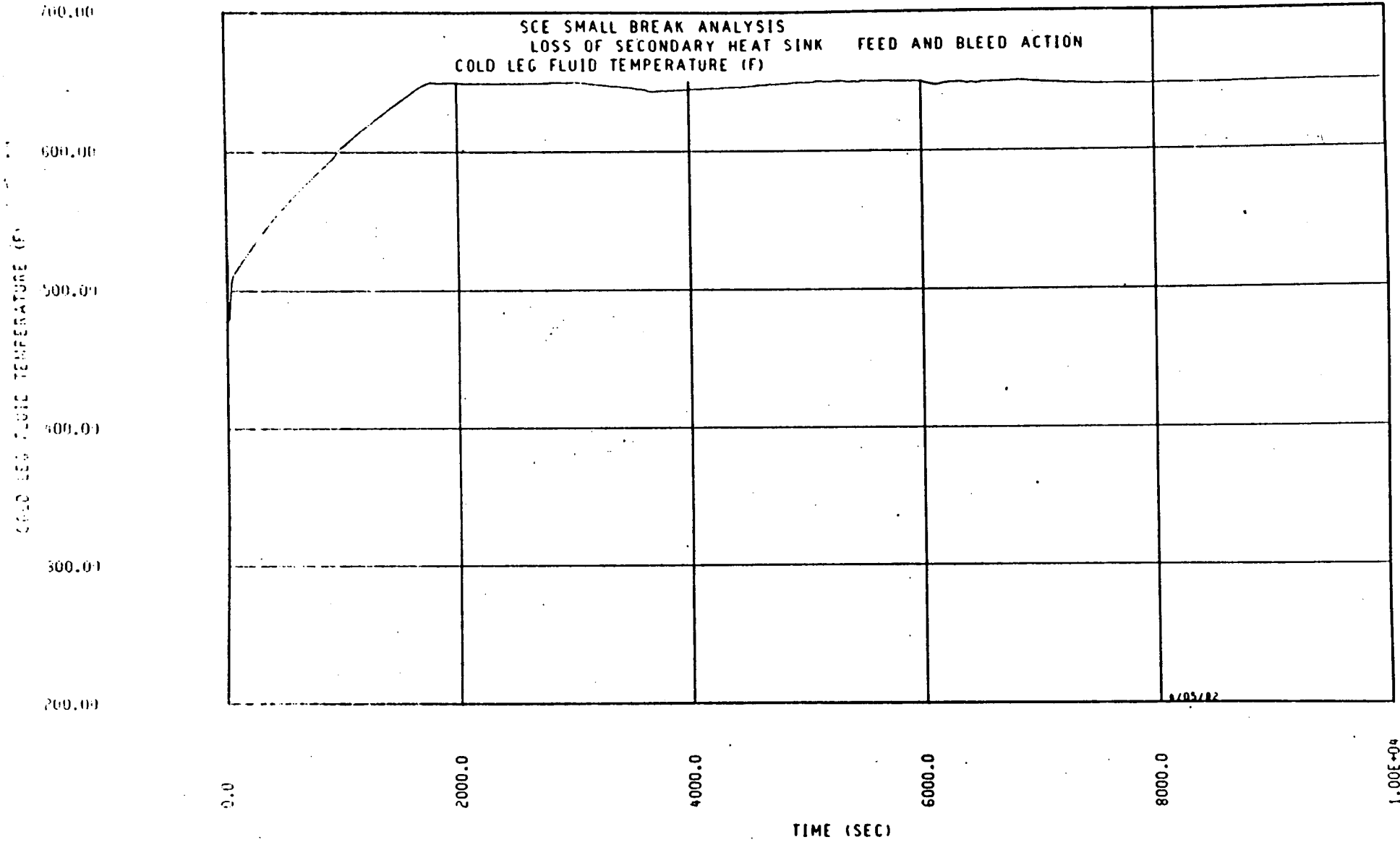
TIME (SEC)

6000.0

8000.0

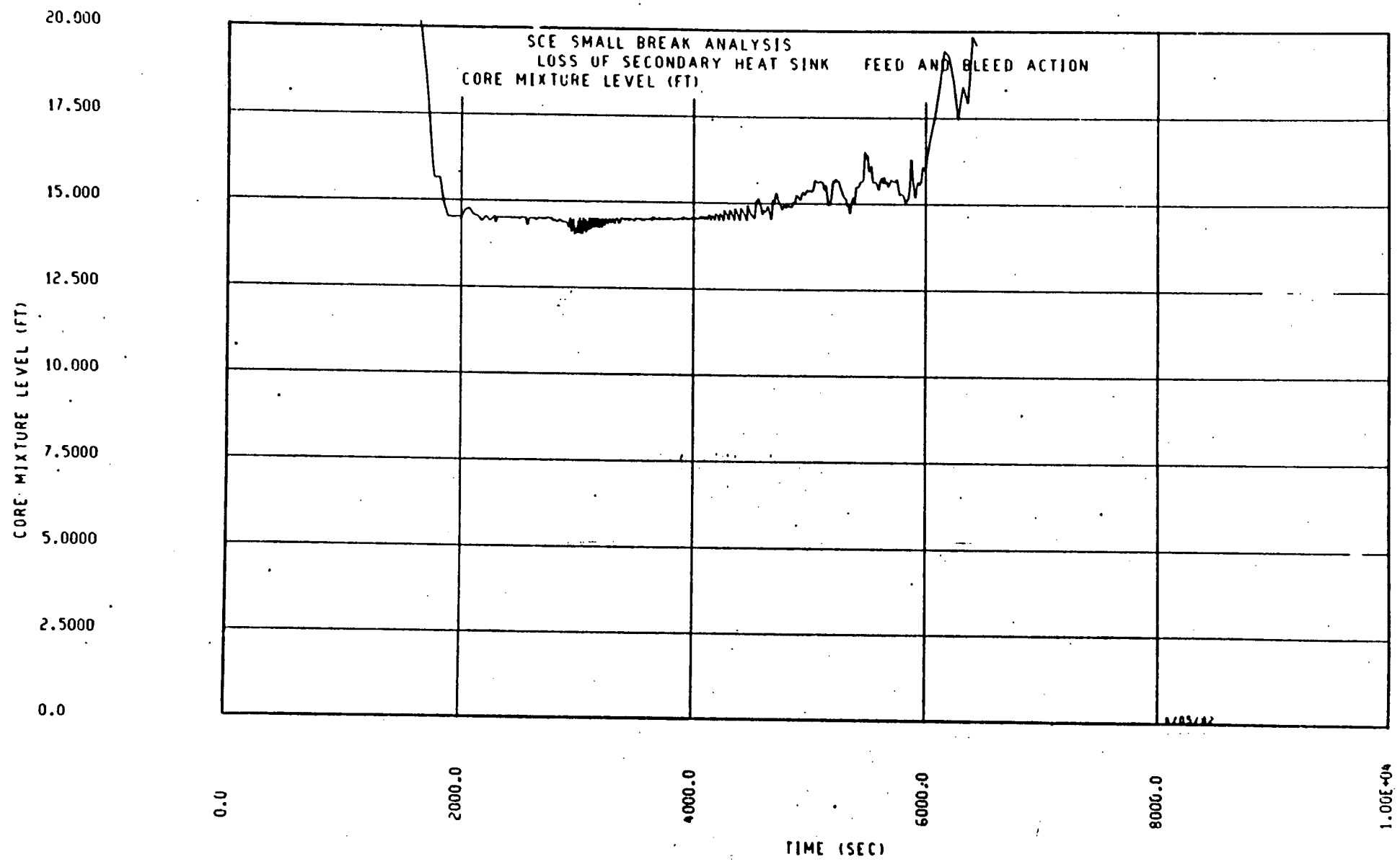
1.00E+04

SCE SMALL BREAK ANALYSIS  
LOSS OF SECONDARY HEAT SINK FEED AND BLEED ACTION  
COLD LEG FLUID TEMPERATURE (F)



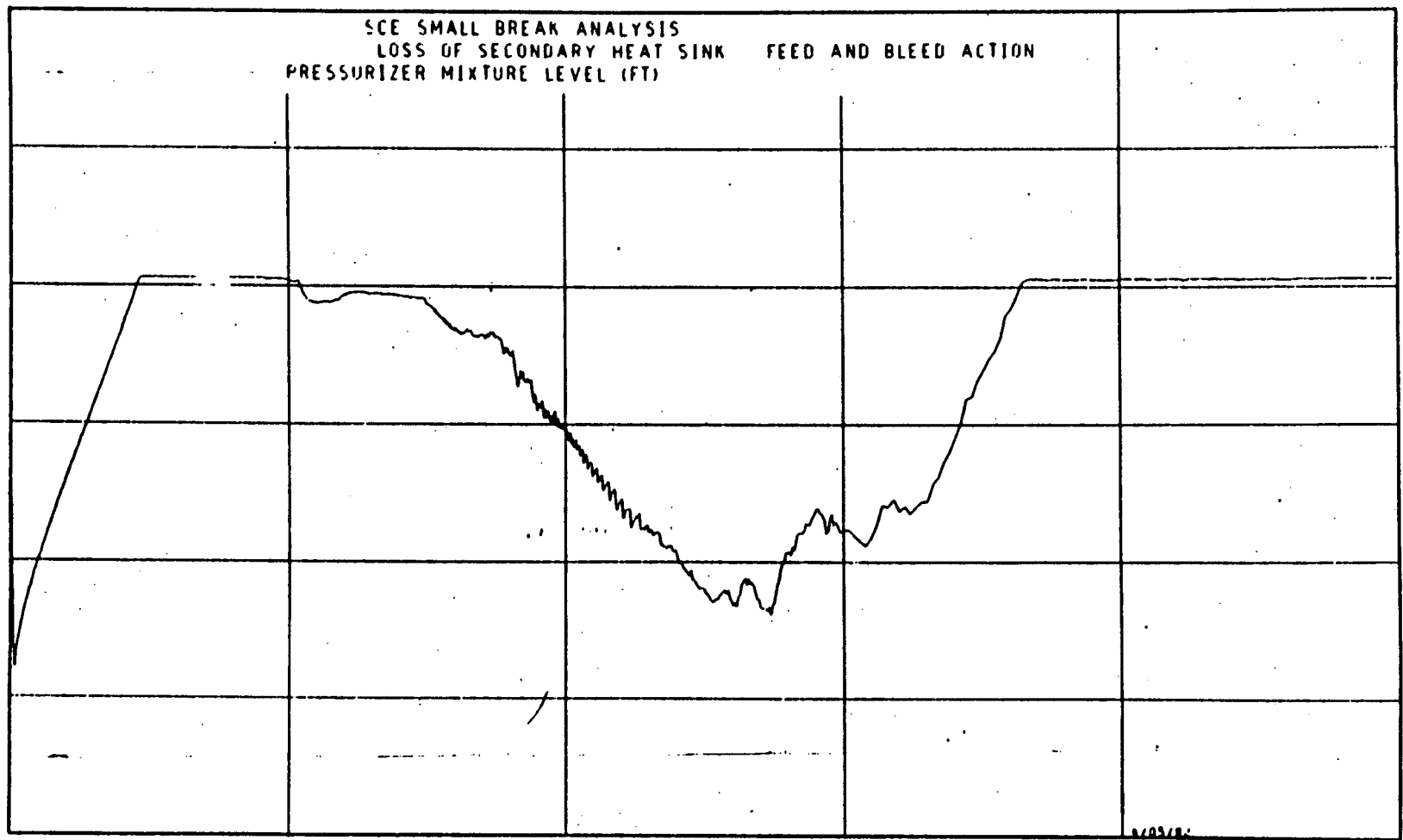
4/05/82

1.00E+04



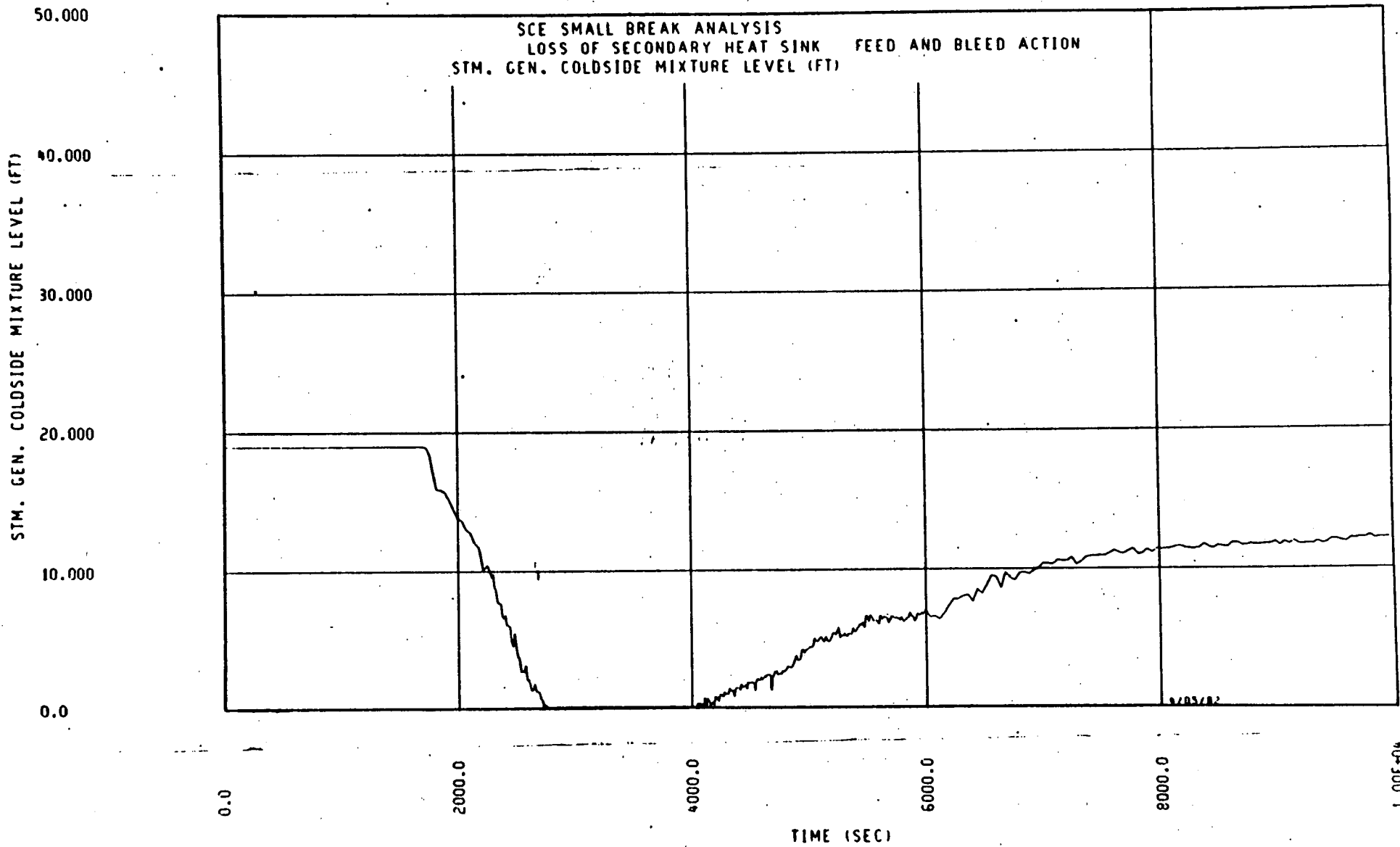


PRESSURIZER MIXTURE LEVEL (FT)

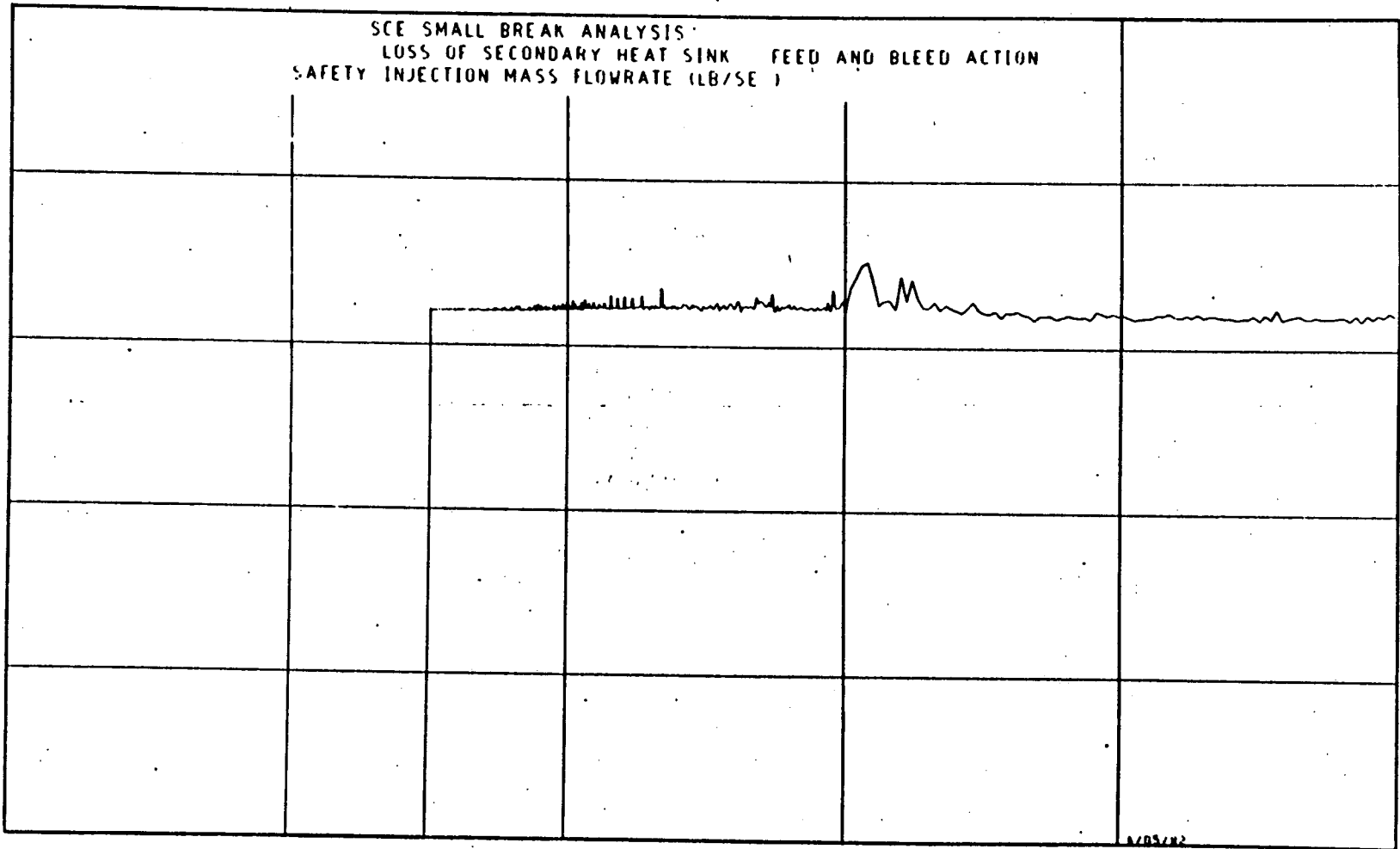


TIME (SEC)

0.0 2000.0 4000.0 6000.0 8000.0 1.00E+04



0.000  
0.000  
0.000  
0.000  
0.000  
0



0.0

2000.0

4000.0

6000.0

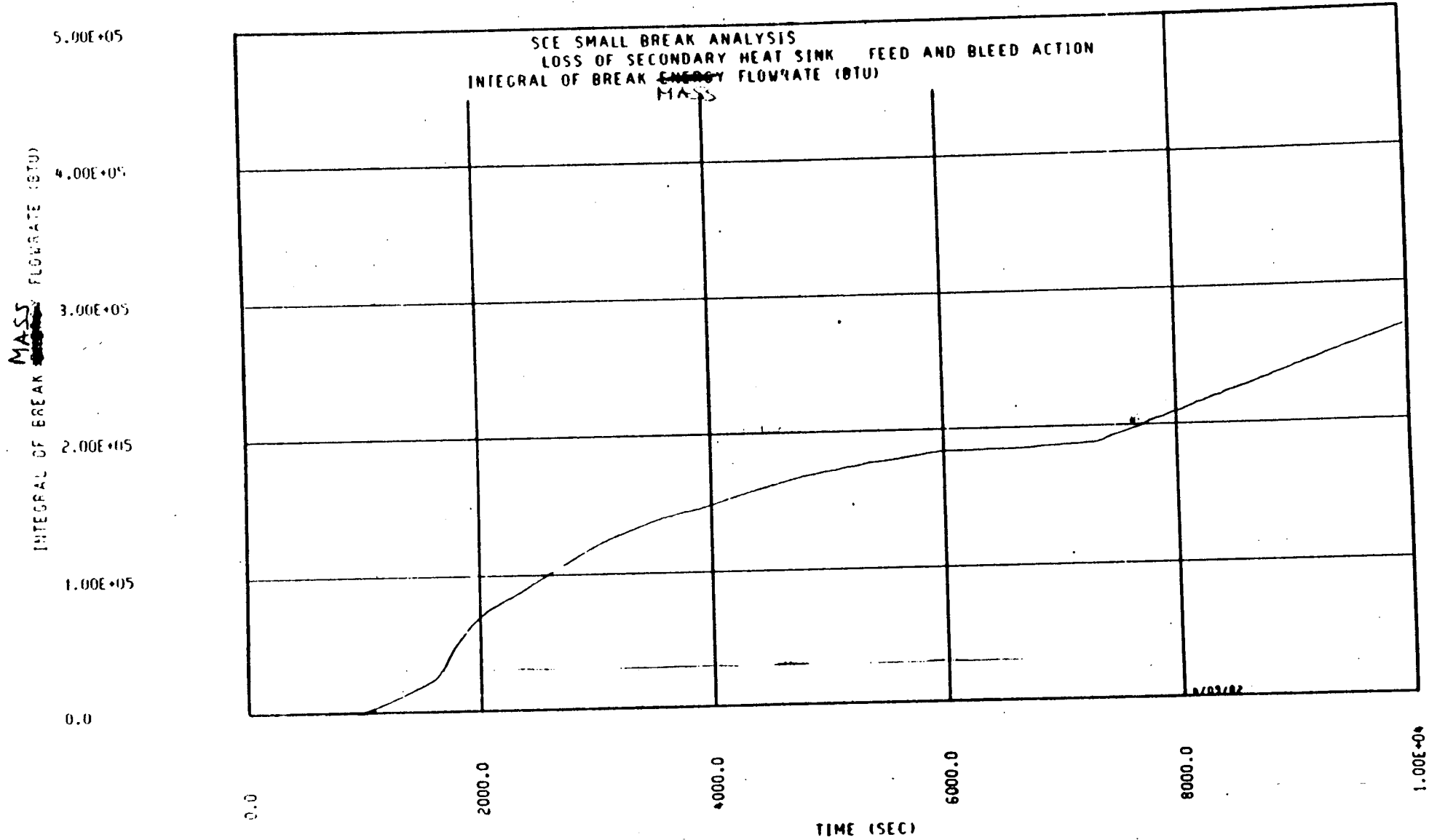
8000.0

1.00E+04

TIME (SEC)

CONTAINMENT PRESSURE RESPONSE

POW MASS & ENERGY RELEASE  
CASE # 4 BLEED & FEED



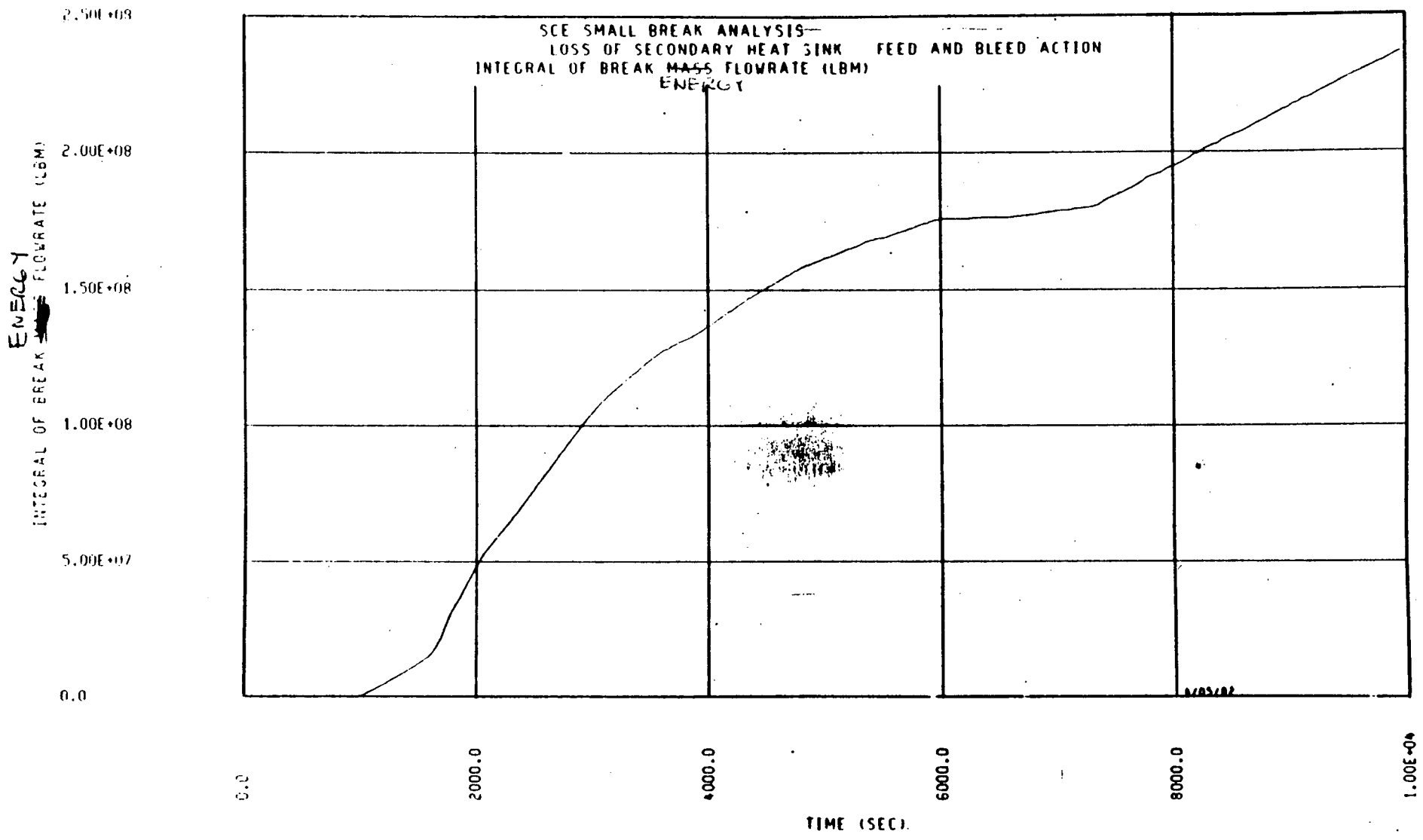
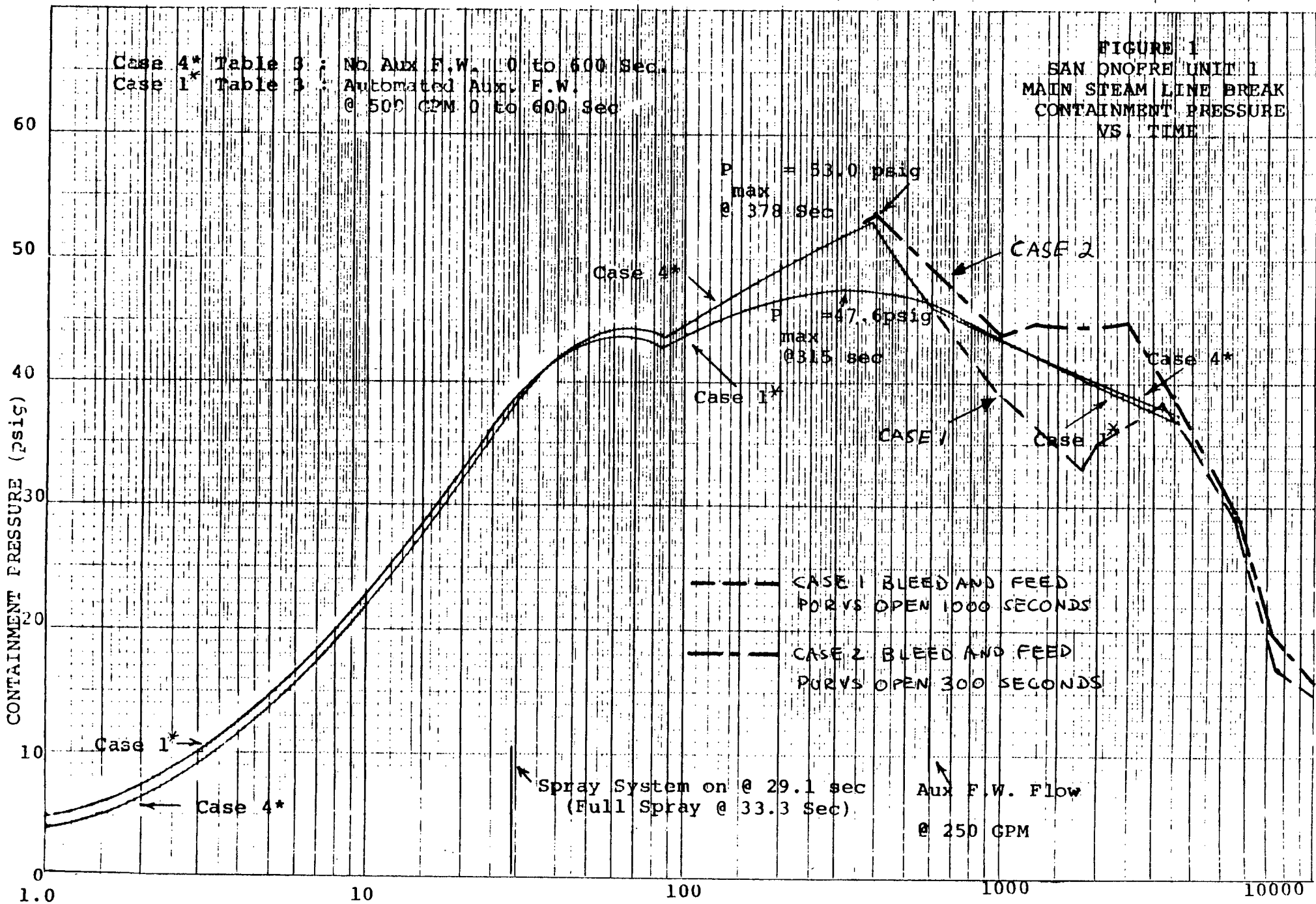


FIGURE 1  
SAN ONOFRE UNIT 1  
MAIN STEAM LINE BREAK  
CONTAINMENT PRESSURE  
VS. TIME

Case 4\* Table 3 : No Aux F.W. 0 to 600 Sec.  
Case 1\* Table 3 : Automated Aux. F.W.  
@ 500 GPM 0 to 600 Sec



ENCLOSURE 4

PRESSURIZED THERMAL SHOCK ANALYSIS

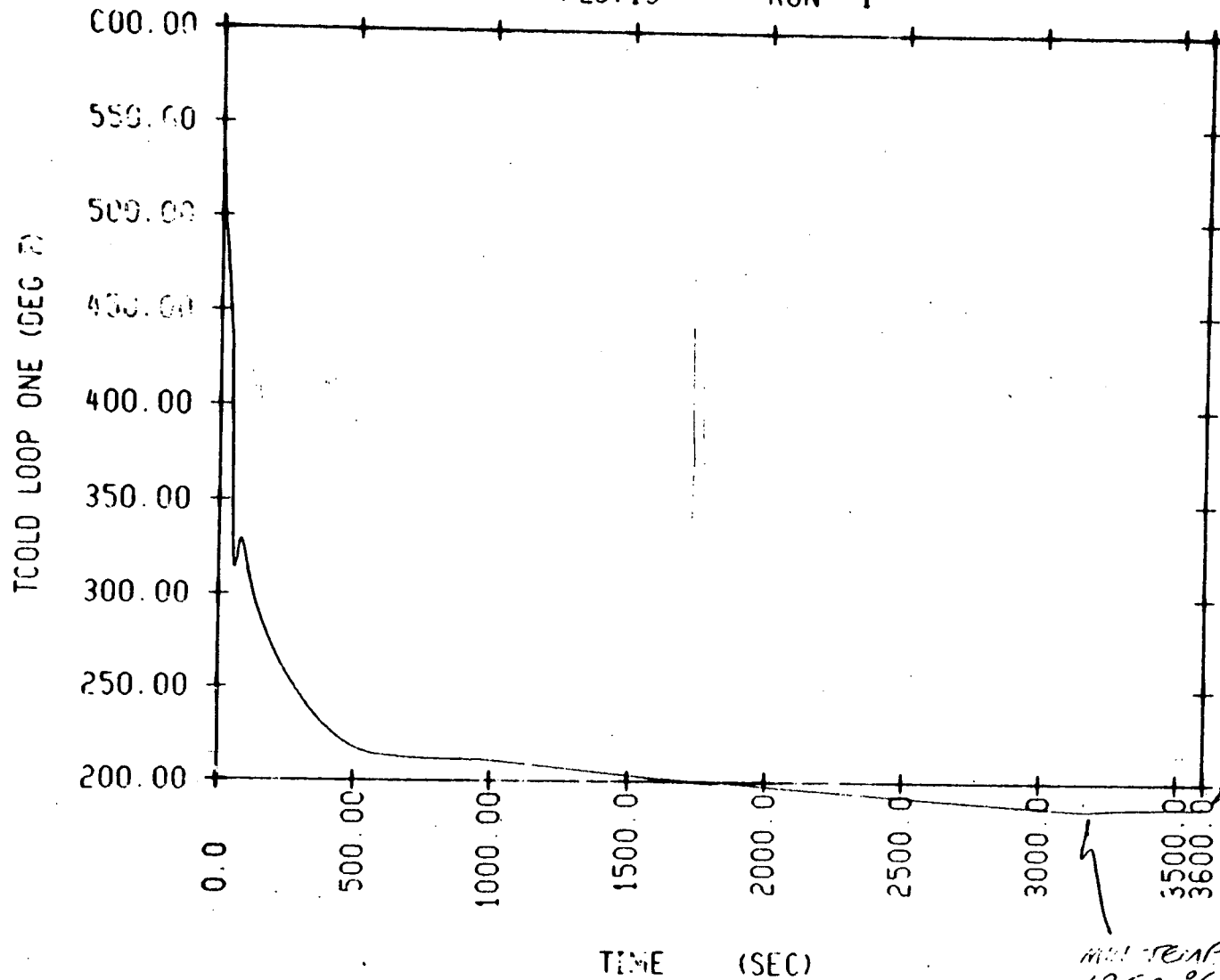


The following transient development assumptions were used in the final simulation of the hypothetical LSB accident as input to the LOFTMAN computer code:

1. Break area is 1.12 Square Feet
2. Initially at hot zero power conditions
3. No decay heat
4. Thick metal was modeled
5. 450 GPM aux feed flow to all SG's until termination
6. Feedwater, aux feed and SI temp is 60°F
7. Initial steam generator mass is 70491 lbm/SG (50% narrow range span)
8. Initial pressurizer water volume is 345 cubic feet (10% of span)
9. Steambreak back pressure is 14.7 psia
10. SI terminated at 10, 20, and 30 min.
11. RCP's are tripped at 10 sec.
12. SI pumps started at 10 sec.
13. No pressurizer heaters or spray modeled
14. Charging flow terminated at 10, 20, and 30 min.
15. Aux feed terminated when SG's reached 50% narrow range span (3110 sec.)

FIGURE 1

SCE LARGE STEAM BREAK FOR P1S  
30 MIN TERM CHRGING AND SI/ 3100 SEC TERM AFW  
PLOT19 RUN 1



FOR P1S CONSIDERATIONS,  
ASSUME CONSTANT  
185.3 °F AFTER  
3170 SEC

MIN TEMP  
185.3 °F  
AT TIME 3170 SEC

Figure 3

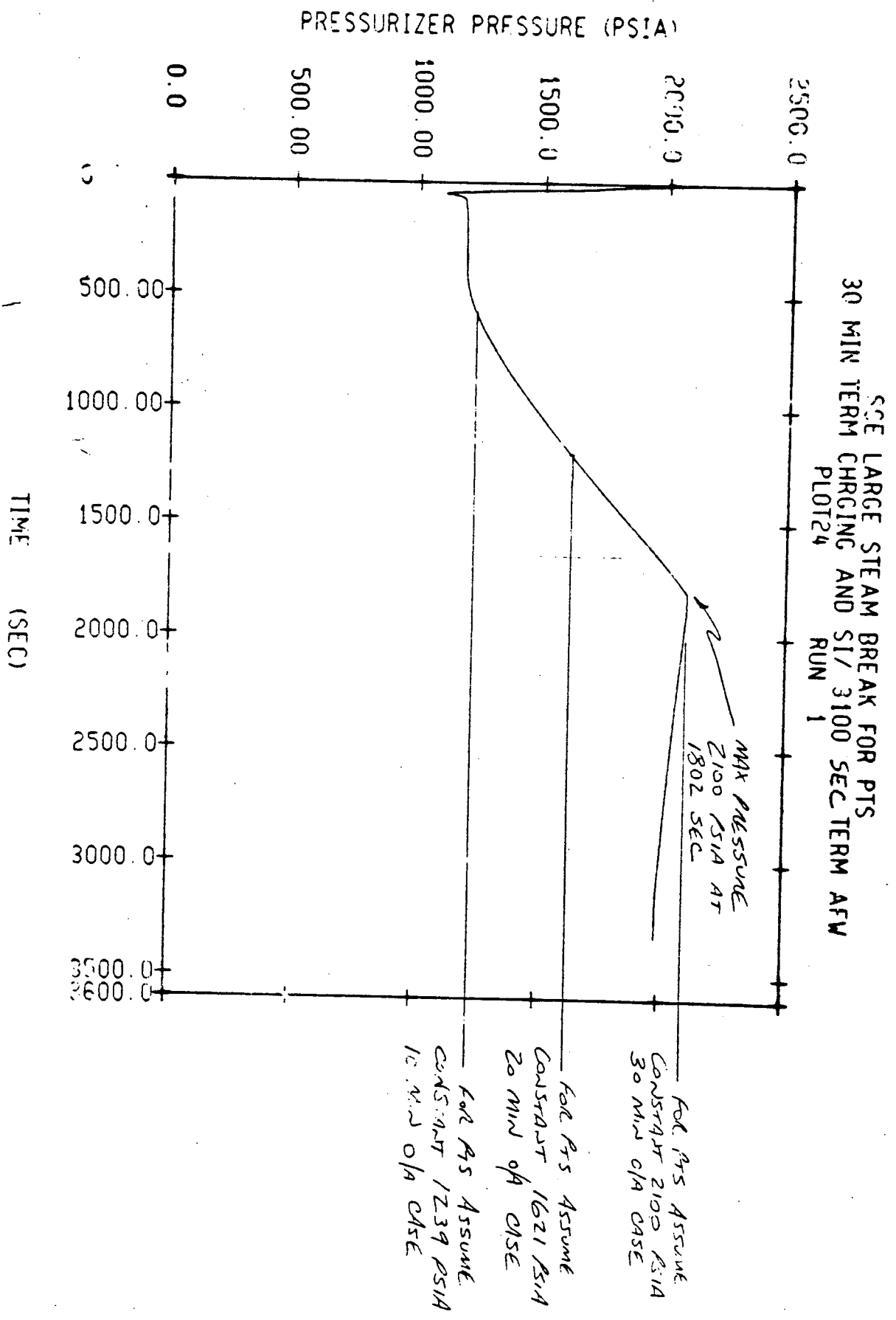


Figure 8

SCE LARGE STEAM BREAK FOR PTS  
30 MIN TERM CHRGING AND SI/ 3100 SEC TERM AFW  
PLOT06 RUN 1

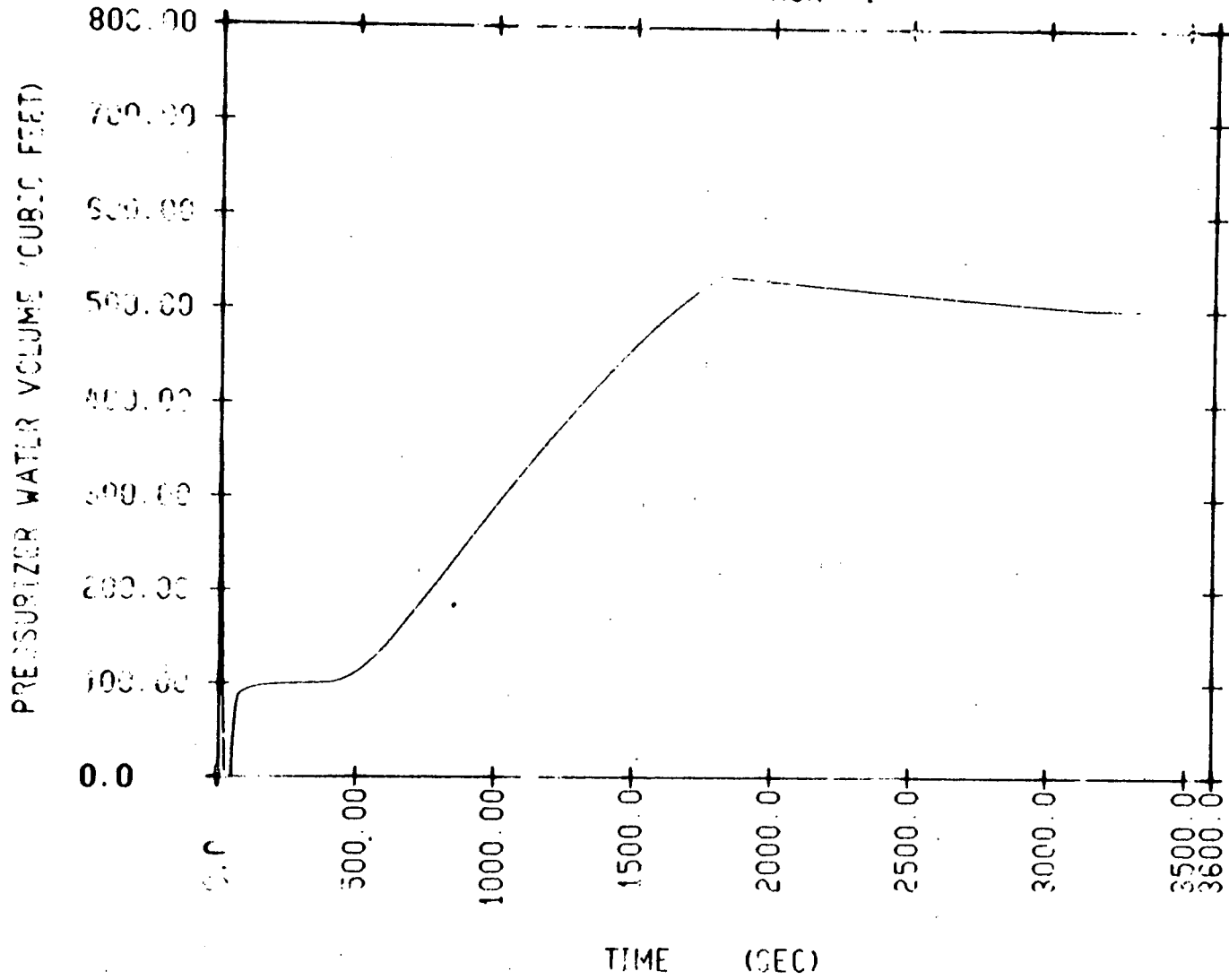


TABLE 1

RESULTS OF SAN ONOFRE - UNIT 1 FRACTURE ANALYSIS FOR A POSTULATED  
LARGE STEAMLINE BREAK ACCIDENT EVENT

Analysis Case	Operator Action Time	Flaw Location	Minimum Total Number of Acceptable Effective Full Power Years (EFPY) of Operation <sup>(a)</sup>	
			With Benefit of Warm Prestressing (WPS)	Without Benefit of Warm Prestressing (WPS)
1	10 min (215°F, 1239 psia)	Base Metal	24 <sup>(b)</sup>	22*
		Longitudinal Weld	WPS Not Required	24
2	20 min (210°F, 1621 psia)	Base Metal	24	14*
		Longitudinal Weld	24	21*

NOTE: (a) The results shown reflect the minimum total of EFPY of plant operation before conservative acceptance criteria [Ref. 1,2] are exceeded. The accumulated EFPY for the San Onofre vessel was 8.97 years as of 10/31/81. No crack initiation occurred for any of the results reported. That is, cracks less than 1" did not initiate. For those values marked with an asterik(\*), one more additional EFPY resulted in cracks less than 1" initiating and not arresting within 75% of the vessel wall thickness.

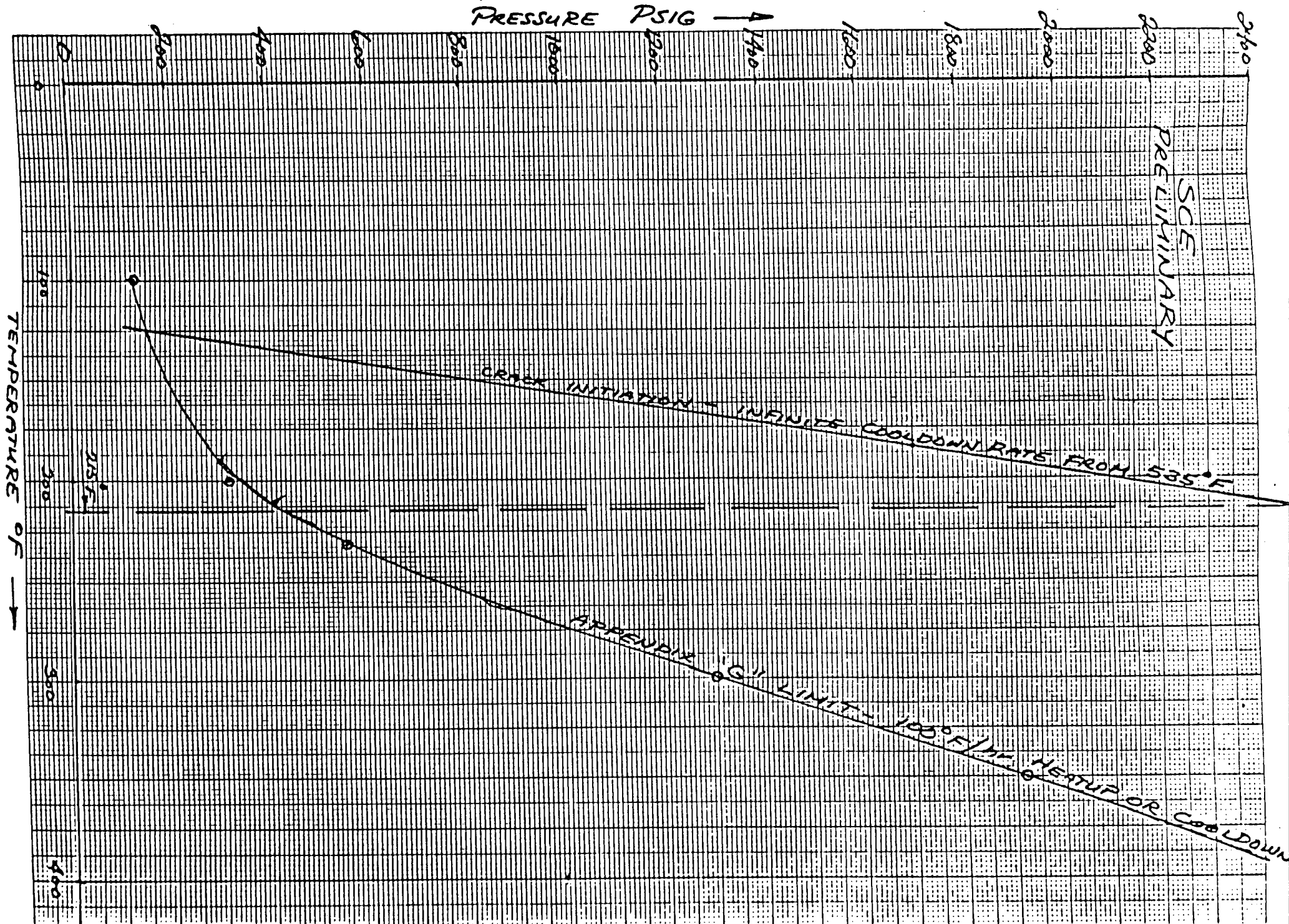
(b) 24 EFPY corresponds to 30 calendar year of operation at a 0.8 plant usage factor (capacity factor).

TABLE 3-1  
RESULTS OF SAN ONOFRE UNIT 1 FRACTURE ANALYSES FOR POSTULATED  
THERMAL SHOCK TRANSIENTS

Transient	Minimum Number of Additional Years Acceptability Demonstrated	Benefits of Warmprestressing Used	Vessel Geometry	Location	Material Properties	Inputs to Analysis Transient Characteristic	Fluence Profile	Trend Curve
Large LOCA	18*	YES	plant specific	plant specific	plant specific	plant specific (2)	plant specific	low nickel
Small LOCA	18*	YES	"	"	"	limiting generic 3 loop, 2" break no mixing	"	"
Large Steam Break	18*	NO	"	"	"	quasi-plant specific (2)	"	"
Small Steam Break	18*	NO	"	"	"	generic	"	"
Rancho Seco	18*	NO	"	"	"	--	"	"

\*This number of year corresponds to the remaining vessel design lifetime, assuming a plant design life of 30 calendar years and load factor of 0.8. As indicated in Section 5, fracture mechanics analyses were also completed for a design life of 40 calendar years which showed that vessel integrity criteria are met. Hence the useful life of the vessel is not limited by vessel integrity considerations.

WF:3163



ENCLOSURE 5

EMERGENCY OPERATING INSTRUCTIONS



PROCEDURE

SONGS 1 NUMBER

Reactor Trip OR SI	S01-1.2-1.0
Reactor Trip Response	S01-1.2-1.01
SI Termination Following Spurious Safety Injection	S01-1.2-1.03
Loss of Reactor Coolant	S01-1.2-1.1
SI Termination Following Loss of Reactor Coolant	S01-1.2-1.11
Post-LOCA Cooldown and Depressurization	S01-1.2-1.12
Transfer to Cold Leg Injection and Recirculation	S01-1.2-1.13
Transfer to Hot Leg Recirculation	S01-1.2-1.14
Loss of Secondary Coolant	S01-1.2-1.2
SI Termination Following Loss of Secondary Coolant	S01-1.2-1.21
Containment Spray Recirculation Following Loss of Secondary Coolant	S01-1.2-1.22
Loss of RHR Due to Loss of Secondary Coolant In Containment	S01-1.2-1.23
Steam Generator Tube Rupture	S01-1.2-1.3
Response to Inadequate Core Cooling	S01-1.2-14
Response to Loss of Secondary Heat Sink	S01-1.2-15
Anticipated Transient Without Scram	S01-1.2-16