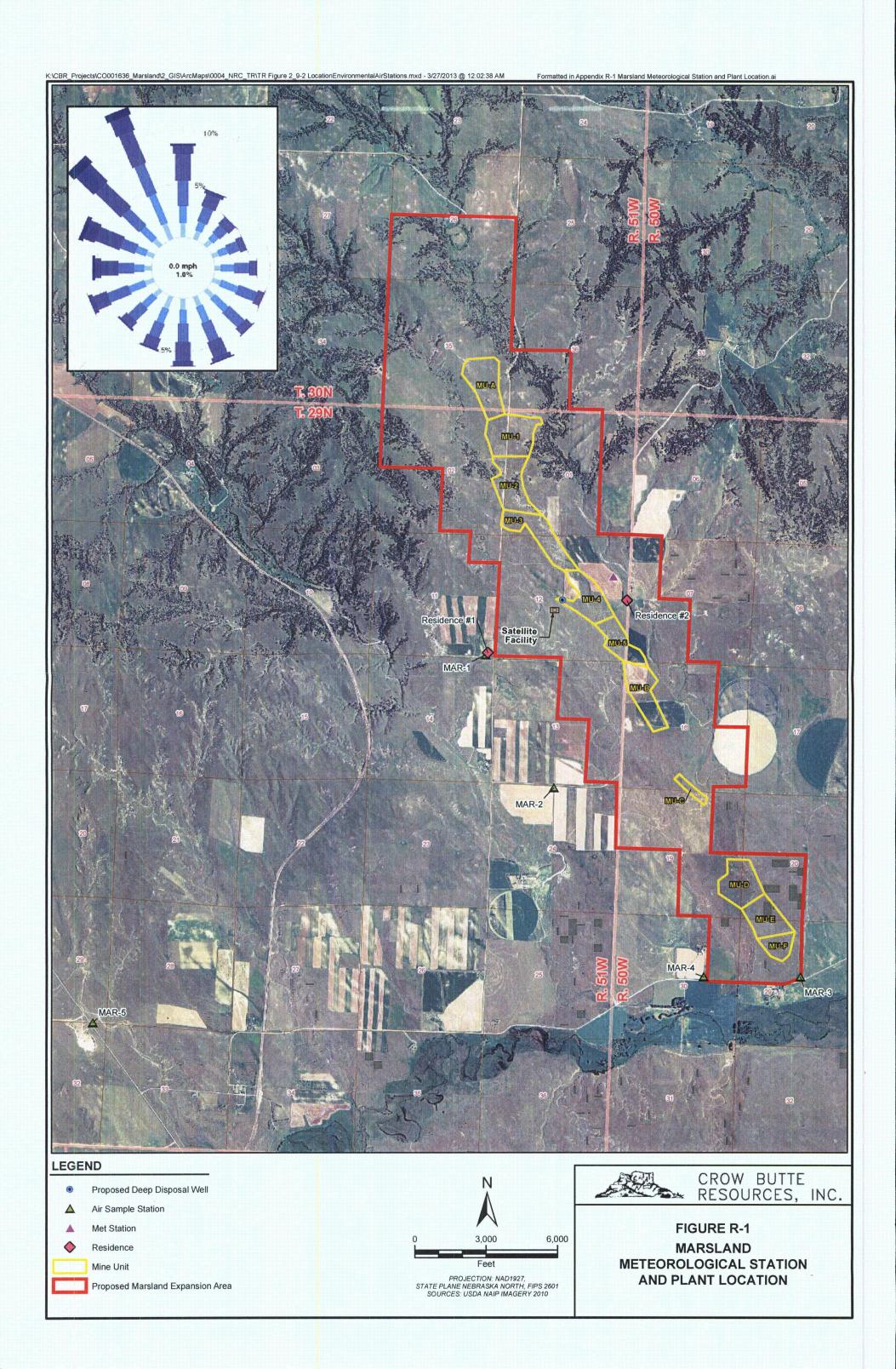
Appendix R Siting of Meteorological Instruments

NRC Regulatory Guide 3.63 provides guidance acceptable to the NRC regarding the siting of meteorological instruments. The siting of the Marsland Expansion Area meteorological tower followed guidance in NRC Regulatory Guide 3.63, which states:

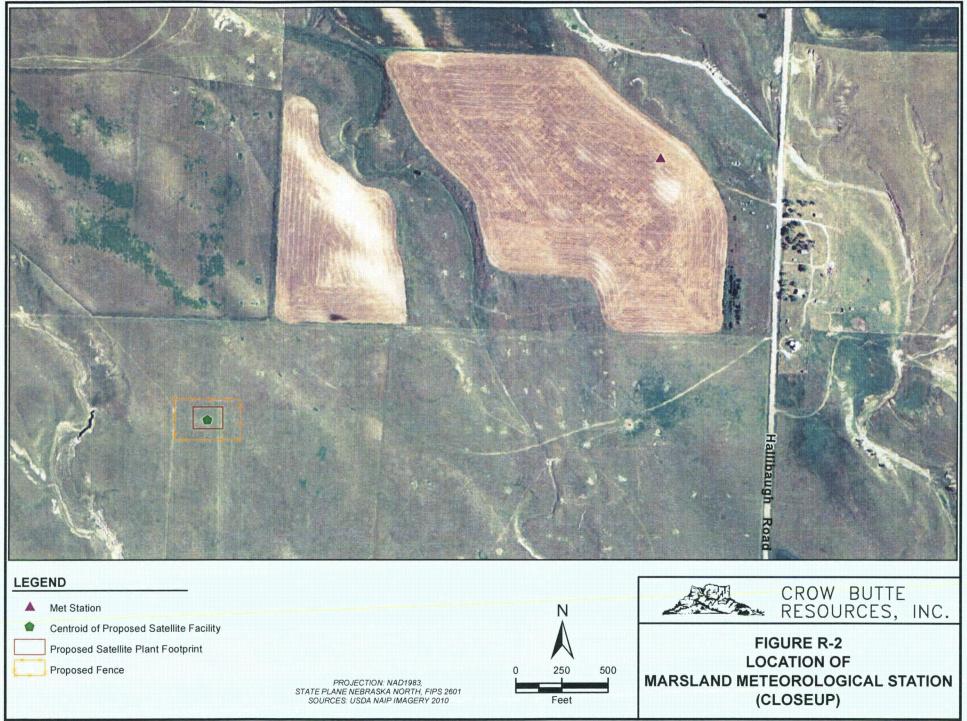
"The location of the meteorological instruments should represent as closely as possible the longterm meteorological characteristics of the area for which the measurements are being made. Whenever possible, the base of the instrument tower or mast should be sited at approximately the same elevation as the facility operation. Ideally, the instruments should be located in an area where localized singular natural or man-made obstructions (e.g., trees, buildings) will have little or no influence on meteorological measurements. Measurements of wind speed, wind direction and sigma theta...should be made at least 10 obstruction heights away from the nearest obstruction. To the extent practicable, these instruments should not be located in the prevailing downwind direction of an obstruction." In addition to criteria related to wind measurement, the guide also addresses solar radiation. "If instrumentation is used to measure incoming solar radiation, it should be located in an area as free as possible from terrestrial shadows."

Accordingly, the following siting issues were considered:

- 1. **Elevation** The meteorological monitoring tower, at 4,240 ft. above sea level, is near the elevation of the proposed satellite plant (4,245 ft.). The meteorological site elevation is also representative of the entire Marsland Expansion Area, in which surface elevations range generally between 4,100 and 4,300 ft. above sea level.
- 2. **Proximity** The meteorological monitoring tower is located 0.4 miles east-northeast of the proposed plant site. **Figure R-1** shows the location of the tower relative to the plant site.
- 3. **Topography** Both the meteorological monitoring tower and the proposed plant site are surrounded by relatively flat topography. A small drainage runs through the area, but the monitoring tower is situated on a flat area above the stream channel.
- 4. **Obstructions Figure R-2** depicts the area surrounding the Marsland meteorological tower and proposed plant site. The area is relatively flat with no trees, structures or other obstructions in the vicinity of the meteorological tower.
- 5. **Shadows** There are no trees, large rocks or other obstructions in the immediate vicinity that would compromise solar radiation exposure at the meteorological station.



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Appendix S Justification for Use of 15 Years of Scottsbluff's Meteorological Data

The regression analyses for wind parameters at the Scottsbluff meteorological station are repeated below with p-values as requested in NRC Comment #4 a). As seen in **Figure S-1**, the wind direction correlation produced a very high coefficient of determination, or R^2 . In the wind direction regression analysis below, the p-value of 0.000 indicates virtually no chance that this R^2 value is accidental. In other words, the 1-year distribution of wind directions is strongly correlated with the 15-year distribution, to a high degree of confidence.

Scottsbluff Regression Analysis: 15-Year Directions versus 1-Year Directions

The regression equation is:

15-Year Directions = 0.006077 + 0.90281-Year DirectionsS = 0.00689141R-Sq = 97.5%R-Sq(adj) = 97.4%

Analysis of Variance

| Source | DF | SS | MS | F | Р |
|------------|----|-----------|-----------|--------|-------|
| Regression | 1 | 0.0262411 | 0.0262411 | 552.54 | 0.000 |
| Error | 14 | 0.0006649 | 0.0000475 | | |
| Total | 15 | 0.0269060 | | | |

In similar fashion, the wind speed correlation produced a very high coefficient of determination (**Figure S-2**). The p-value of 0.001 shown in the regression analysis below indicates a 99.9% confidence that this R^2 value is not accidental. In other words, the 1-year distribution of wind speeds is strongly correlated with the 15-year distribution, to a high degree of confidence.

Scottsbluff Regression Analysis: 15-Year Speeds versus 1-Year Speeds

The regression equation is:

 $15-Year Speeds = 0.00959 + 0.9425 \qquad 1-Year Speeds \\ S = 0.0321279 \quad R-Sq = 94.8\% \quad R-Sq(adj) = 93.5\%$

Analysis of Variance

| Source | DF | SS | MS | F | Р |
|------------|----|-----------|-----------|-------|-------|
| Regression | 1 | 0.0748612 | 0.0748612 | 72.53 | 0.001 |
| Error | 4 | 0.0041288 | 0.0010322 | | |
| Total | 5 | 0.0789900 | | | |

In response to NRC Comment #4 b), hourly wind data were retrieved from the Chadron airport meteorological station. **Figures S-3** and **S-4** illustrate strong similarities between the baseline year and the 12-year period from 2001 through 2012.

The similarities in **Figures S-5** and **S-6** are further illustrated by comparing the bar graphs of wind direction and wind speed distributions between the baseline year and the 12-year period (**Figures S-5** and **S-6**).

The regression analyses for wind parameters at the Chadron meteorological station are presented below with p-values as requested in NRC Comment #4 a). **Figure S-7** shows the wind direction correlation produced a very high coefficient of determination, or R^2 . As seen in the regression analysis below, the p-value of 0.000 indicates virtually no chance that this R^2 value is accidental. In other words, the 1-year distribution of wind directions is strongly correlated with the 12-year distribution, to a high degree of confidence.

Chadron Regression Analysis: 12-Year Directions versus 1-Year Directions

The regression equation is:

12-Year Directions = 0.002237 + 0.96181-Year DirectionsS = 0.00685647R-Sq = 95.8%R-Sq(adj) = 95.5%

Analysis of Variance

| Source | DF | SS | MS | F | Р |
|------------|----|-----------|-----------|--------|-------|
| Regression | 1 | 0.0160024 | 0.0160024 | 340.39 | 0.000 |
| Error | 15 | 0.0007052 | 0.0000470 | | |
| Total | 16 | 0.0167075 | | | |

In similar fashion, the wind speed correlation for Chadron produced a very high coefficient of determination (**Figure S-8**). The p-value of 0.000 shown in the regression analysis below indicates virtual certainty that this R^2 value is not accidental. In other words, the 1-year distribution of wind speeds is strongly correlated with the 12-year distribution, to a high degree of confidence.

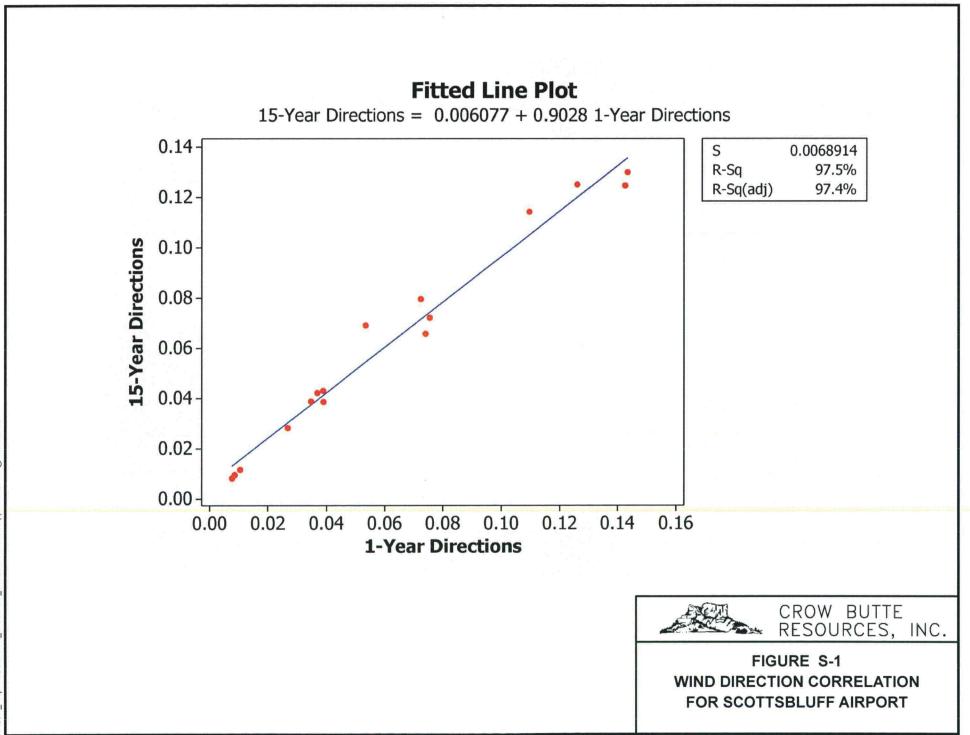
Chadron Regression Analysis: 12-Year Speeds versus 1-Year Speeds

The regression equation is:

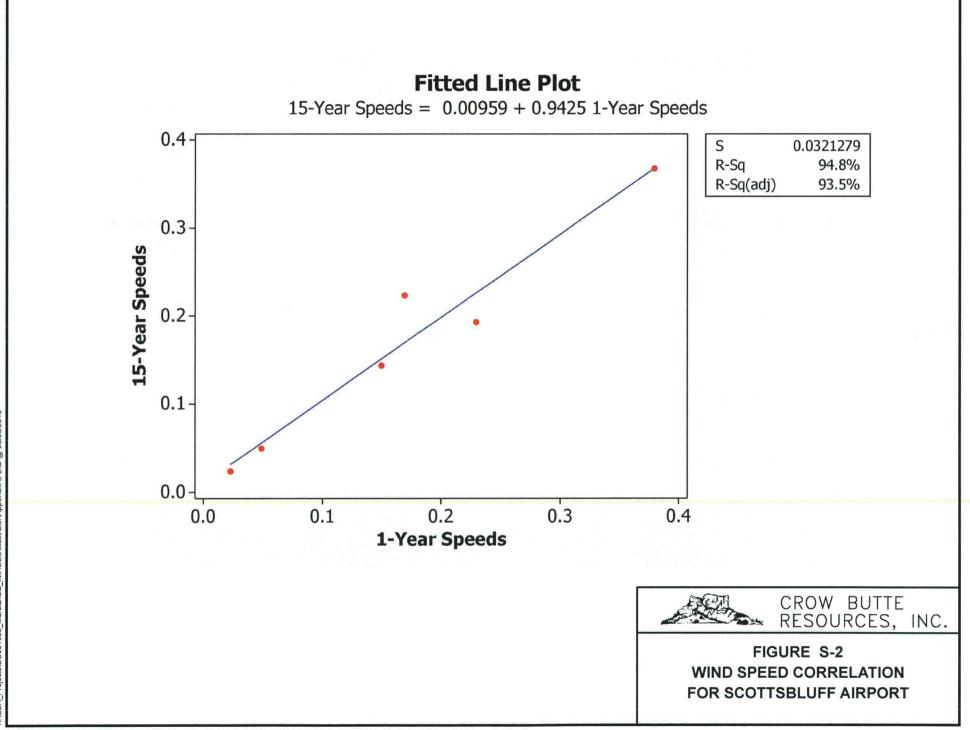
12-Year Speeds = -0.00580 + 1.04 1-Year Speeds S = 0.0146045 R-Sq = 98.2% R-Sq(adj) = 97.9%

Analysis of Variance

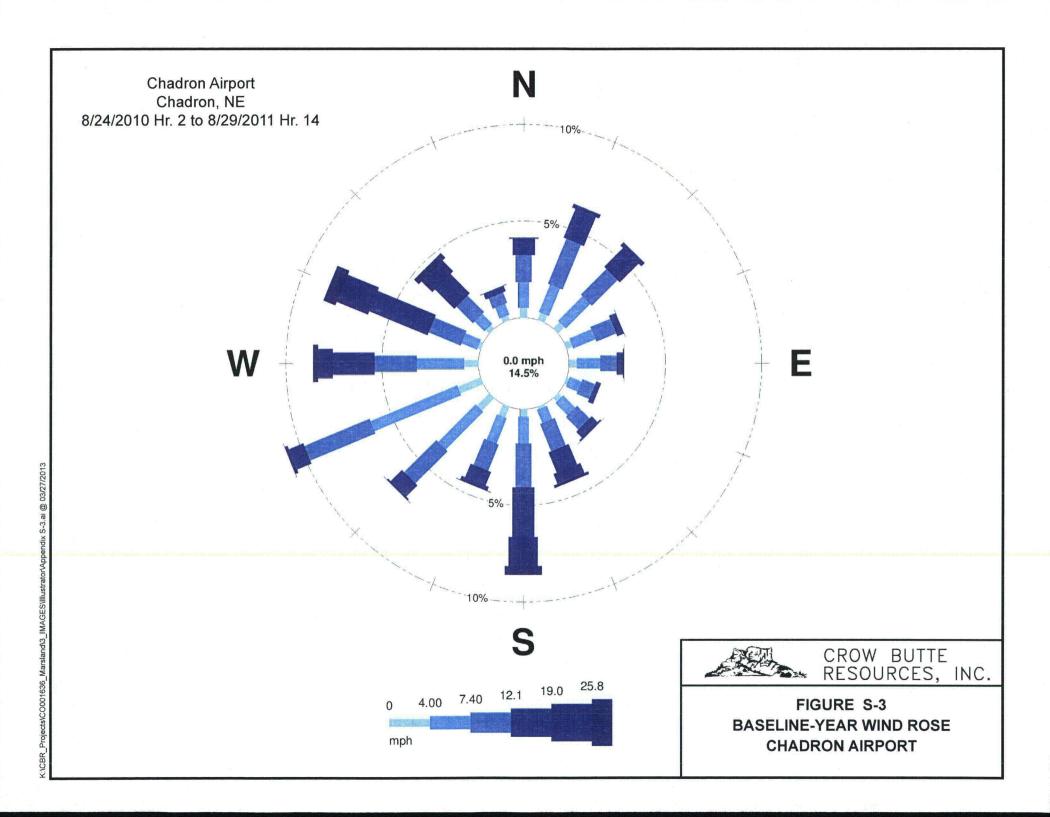
| Source | DF | SS | MS | F | Р |
|------------|----|-----------|-----------|--------|-------|
| Regression | 1 | 0.0590527 | 0.0590527 | 276.86 | 0.000 |
| Error | 5 | 0.0010665 | 0.0002133 | | |
| Total | 6 | 0.0601191 | | | |

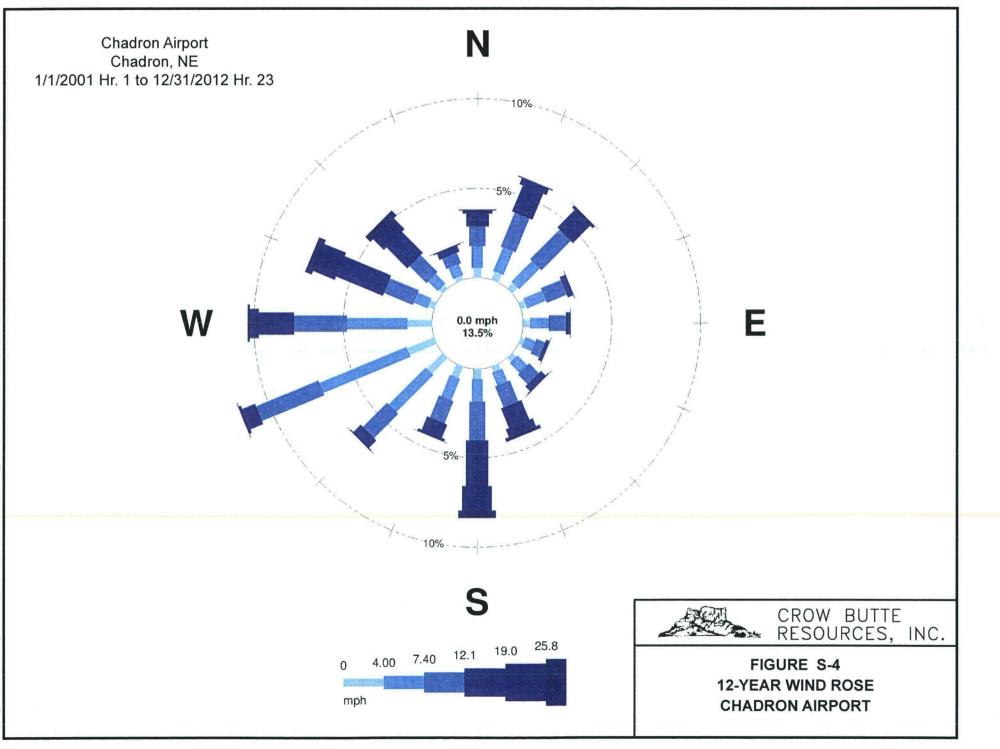


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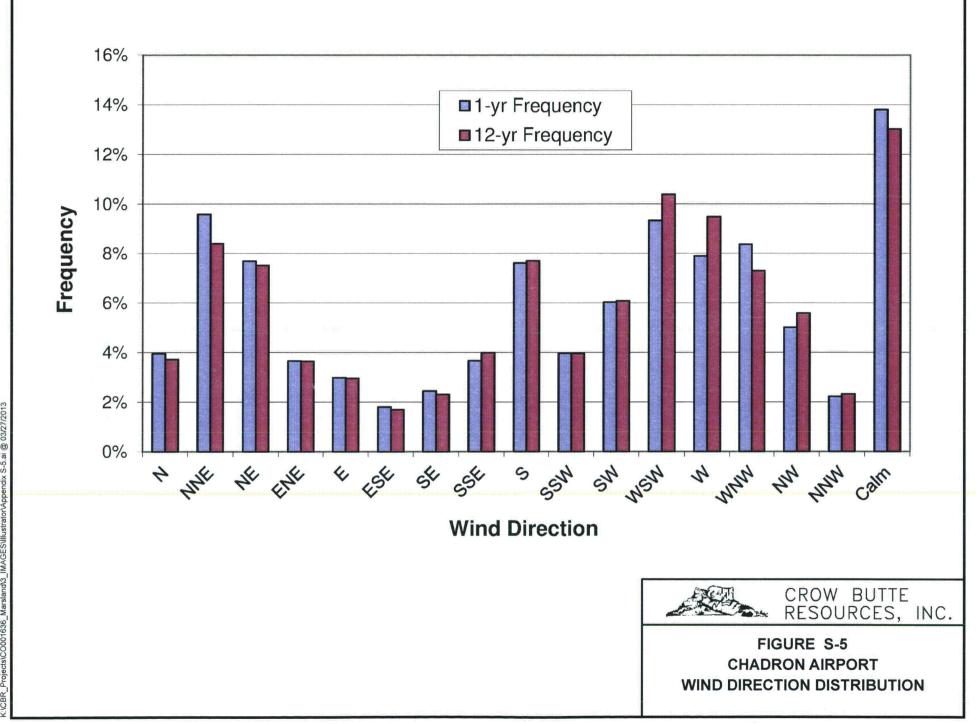


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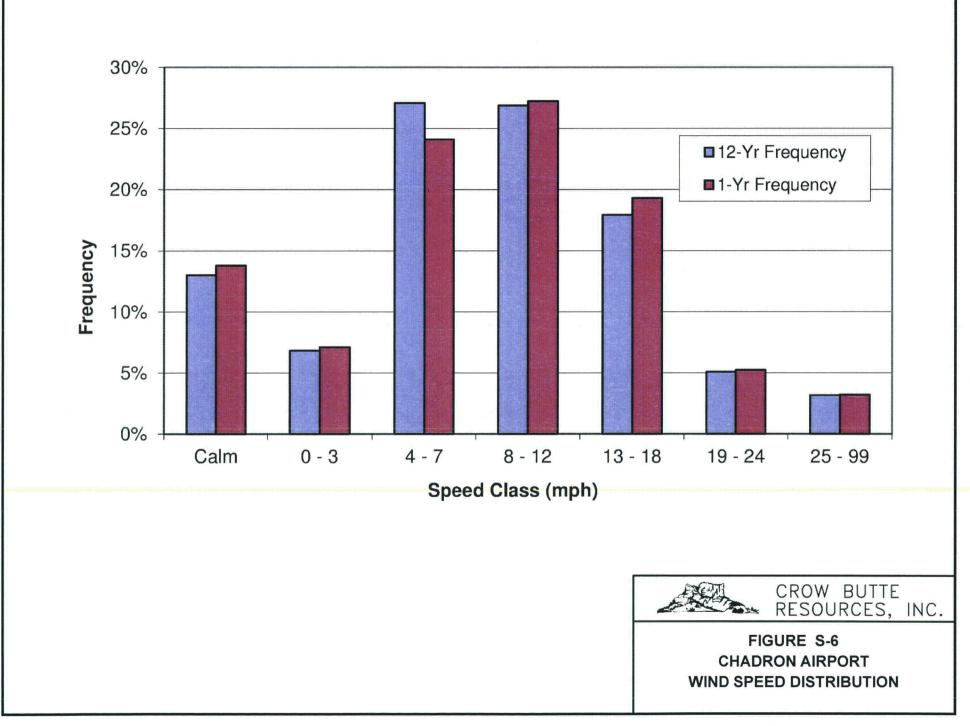




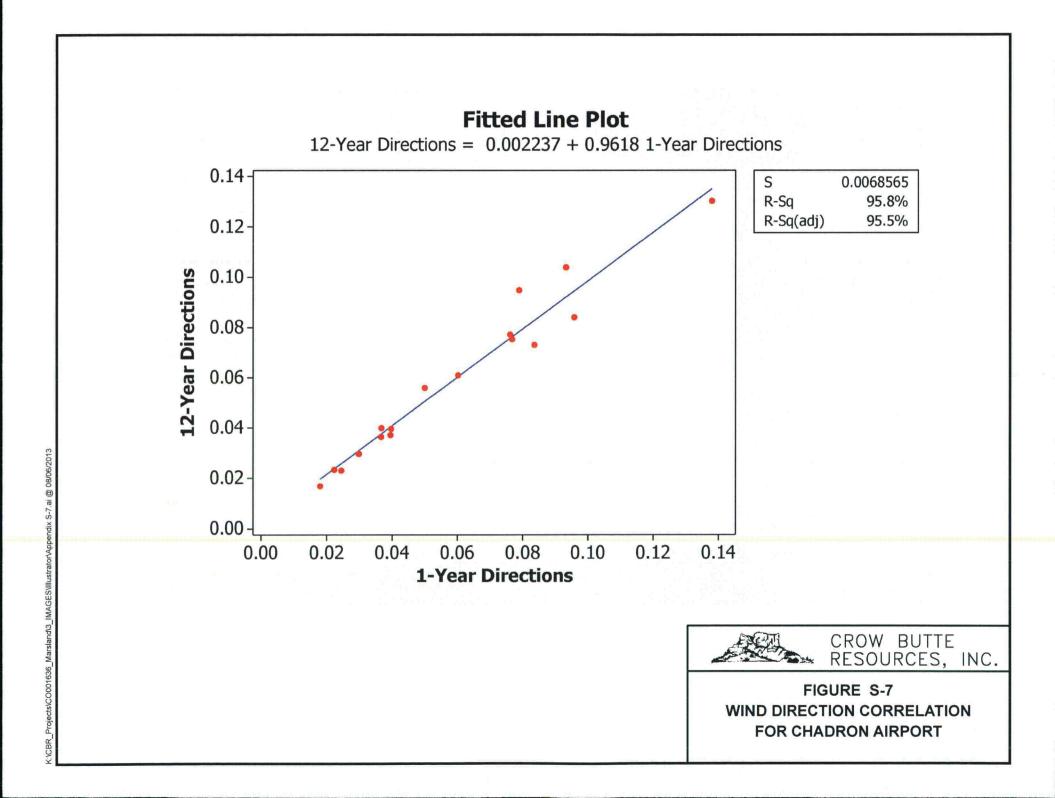
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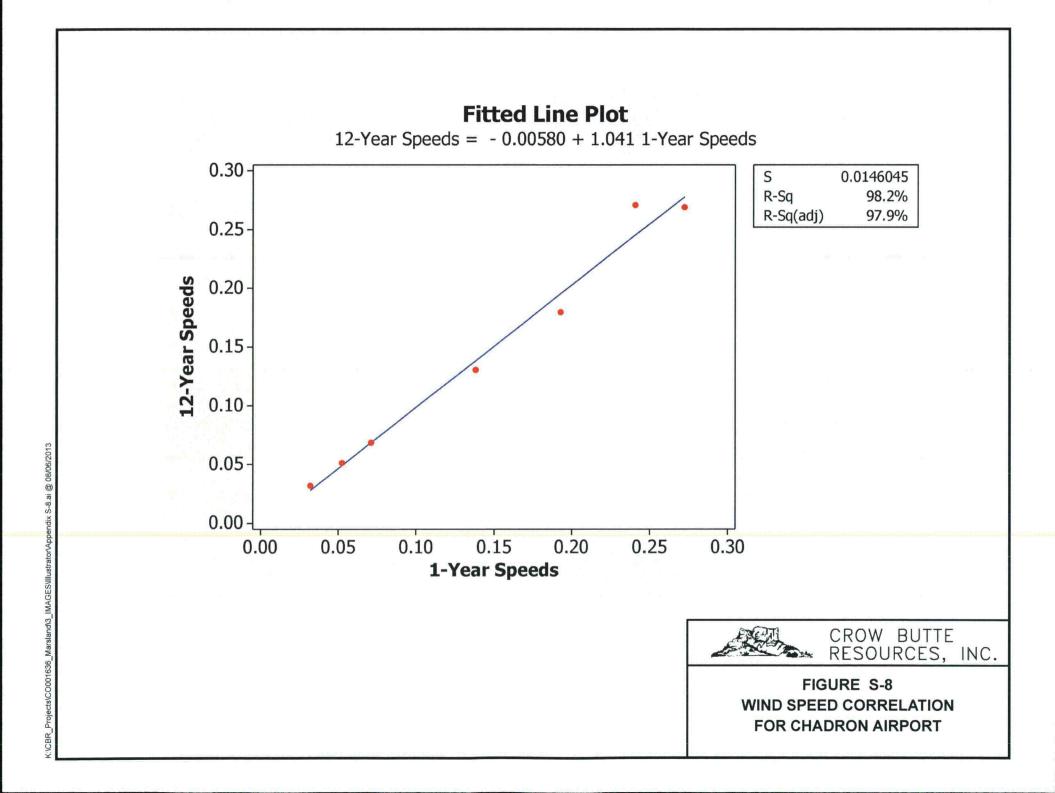


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APPENDIX T MARSLAND WATER BALANCE (PRODUCTION, RESTORATION, AND STABILIZATION SAMPLING)

| MINE UNIT 1 IX Treatment/Reinjection Perm Recirculation STABILIZATION SAMPLING MINE UNIT 2 IX Treatment/Reinjection Perm Recirculation | Q1 1100 | Q2 1700 | Q3 C 1700 1 | Q4 Q1 1600 150 | 00 1500 | Q3 10 1400 | Q4 1400 | Q1 0 | | | Q1 0 1000 | | | Q4 Q1 700 6 | | Q3 400 | Q4 | Q1 Q | 12 Q3 | Q4 | Q1 | Q2 Q3 | Q4 | Q1 Q | 2 Q3 | Q4 | Q1 Q | 2 Q3 | Q4 | Q1 Q2 | Q3 | Q4 | Q1 Q | 12 Q3 | Q4 | Q1 (| Q2 Q3 | 3 Q4 | Q1 (| Q2 Q3 | 3 (|
|--|------------|------------|--|-----------------------|---------|----------------|------------|--------|---------|------------------|----------------|------|--------|----------------|------------------|--------|--------------------------|---------|----------------------------|--------------|--|----------|-------------------|--|----------------|--------------|---------|------------------|---|---|---------------------|-------|-----------------------|-----------------------|----------------|--------|---------|----------------------------|------------------------------|------------------|------|
| IX Treatment/Reinjection Perm Recirculation STABILIZATION SAMPLING MINE UNIT 2 IX Treatment/Reinjection Perm | | | | 1000 150 | 00 150. | 10 1400 | 1400 | 1300 | 1200 11 | 110 | 0 1000 | 900 | 800 | 100 0 | 00 50 | 0 400 | 400 | | and an and a second second | | and the second s | | The second second | | ALC: NO. | | | | 10 TO | | A 2. 3 | S | | | - | | | | | Sec. 10. 10. 10. | |
| Recirculation STABILIZATION SAMPLING MINE UNIT 2 X Treatment/Reinjection Perm | | | | | | | | | | 1.10 | | | | | | | | 2.79 | 800 80 | 0 800 | 200 | | | | | | | | | | - | | | | | | | and a second second second | | | - |
| STABILIZATION SAMPLING MINE UNIT 2 IX Treatment/Reinjection Perm | | | | | | | | | | | | | | | | | | | | | | 500 50 | 00 500 | 500 | 500 500 | 500 | 500 | | | | | | | | + | _ | | | | | + |
| MINE UNIT 2 IX Treatment/Reinjection Perm | | | | | | | | | | | | | | | | | | | | | | | | | | | 8 | 008 000 | | | | | | | | | | | | | _ |
| IX Treatment/Reinjection Perm | | | | | | | | | | | | | - | | - | | | | | - | | | | | | | | | 1 | 1 | 1 1 | 1 | | | | | | | | | |
| IX Treatment/Reinjection Perm | | | 400 | 500 60 | 00 120 | 0 1600 | 1700 | 1600 1 | 1500 14 | 00 140 | 0 1300 | 1200 | 1100 1 | 1100 10 | 00 90 | 800 | 700 | 600 | 500 40 | 0 300 | | - | | | | | | - | | | | | | - | ++ | | | | | | |
| | | | | | | | | | | | | | | | | | | | | 1 | | 800 80 | 008 00 | 400 | | | | - | | | | | | | + | | | - Salar | | | - |
| Recirculation | | | | | | | | | | | | | | | | | | | | | | | | 250 | 250 250 | 250 | 250 5 | 00 500 | 500 | 500 50 | 0 500 | 500 | | | | | | | | | |
| STABILIZATION SAMPLING | | | | | _ | | | | | | | | | | | | | _ | | | | | | | | | | | | | | | 800 | and the second second | | | | | - | | |
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| MINE UNIT 4 | | | | | | - | | | 4 | 00 50 | 0 600 | 1200 | 1600 1 | 1700 160 | 00 150 | 1400 | 1400 | 1300 13 | 200 110 | 0 1100 | 1000 | 900 80 | 0 700 | 600 | 500 400 | 300 | | | | | - | | | | ++ | | | | | | |
| IX Treatment/Reinjection | | | | | | | | | | | | | | | 1 | 1 | | | | | | | | | | ,Г | 4 | 00 400 | 400 | 400 40 | 0 400 | 3 400 | | | - | | | - | | | + |
| Perm | | | | | | | | | | | | | | et | | | | | | | | | | | | | | | | | | | 250 | 250 250 | 0 250 | 250 | 250 5 | 00 500 | 500 | 500 50 | 00 |
| Recirculation | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| STABILIZATION SAMPLING | | | | | | | | | | | - | | | | | | | | | _ | | | _ | | | | | | | | _ | | | | | | | | | | _ |
| MINE UNIT 5 | | | | | | - | | | | - | ++ | | 400 | 500 60 | 00 120 | 1600 | 1700 | 1600 15 | 500 140 | 0 1400 | 1300 | 1200 110 | 0 1100 | 1000 | 900 800 | 700 | 600 | 00 400 | 300 | | + | - | | | ++ | | | | + | | |
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| MINE UNIT 6 | | | | | | | | | | | | | | | - | + - | | | 400 50 | 0 000 | 1200 | 1600 17 | 10 1000 | 1500 | 400 1400 | 1300 | 1200 11 | 00 1100 | 1000 | 000 | | | 500 | 400 | | | | | <u> </u> | | |
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| Recirculation | | | - | | | | | | | | - | | | | | | | | - | | | | | | | | | | | | | 1 | | | | | | | | | - |
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| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| STABILIZATION SAMPLING | | | | | _ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Prod Flow | 1100 | 1700 | 2100 2 | 2100 244 | 20 2704 | 2400 | 2600 | 2500 | 2000 15 | 170 | 4500 | 4900 | 5200 | 400 51 | 0 500 | 5000 | 5200 | 4500 | 00 100 | | | | | 1000 | | | 1500 | | | 1000 | 1 | | | | | | | | 3400 3 | | _ |
| Prod Flow Prod Bleed 1.2% | 1100 | 20 | 2100 21 | 2100 2100 | 25 32 | 0 3400 2 41 | 3600 | 3500 3 | 47 47 | 00 4700 54 56 | 0 4500 6 54 | | | | 00 5300 51 64 | | | | | 0 4100 | | | 00 4300 54 52 | | | 4500 3 54 | | 00 5100 60 61 | | | 0 5400 | | | | 0 4700 2 56 | | | | 3400 3 3 41 | | |
| Mine Unit 1 IX Bleed | 0 | 0 | 0 | 0 2 | 0 0 | 0 0 | | 92 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 04 | 0 | | 0 49 6 16 | | | 0 0 | 52 | 58 58 | | 54 | 60 61 0 0 | | a des si and | 4 65 | 5 61 | 64 | | 2 56 | 52 | 44 | 47 43 0 0 | | | 47 |
| Mine Unit 1 RO Bleed | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | | 0 | 0 | 0 | 0 0 | | - | 67 167 | | 167 167 | | 167 | 0 0 | 0 | | 0 0 | | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | | 0 |
| Mine Unit 2 RO Bleed | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | and the second sec | 83 83 | | | 67 167 | 167 | 167 16 | Contraction and the | 7 167 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | | 0 |
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| line Unit 8 RO Bleed | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | | 0 |
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| line Unit 11 RO Bleed | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 0 | 0 C | 0 | 0 | 0 0 | 0 | 0 | 0 |
| otal DW needed capacity | 40 | 20 | 25 | 25 - | 15 | 2 41 | 43 | 10 | 47 | | | | | 05 | | | - | | 70 | | | | | | | | | | | | | | | | | | | | | | |
| otal Day needed capacity | 13 | 20 | 20 | 25 2 | 25 32 | 41 | 43 | 42 | 4/ | 54 56 | 6 54 | 58 | 64 | 65 6 | 51 64 | 64 | 64 | 54 | 70 6 | 6 65 | 220 | 222 22 | 21 218 | 302 | 308 308 | 304 | 304 3 | 10 311 | 308 | 308 31 | 4 315 | 5 311 | 314 | 314 312 | 2 306 | 302 | 294 2 | 97 293 | 3 291 | 294 25 | 97 |
| X Flow | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 8 | 300 80 | 0 800 | 200 | 800 80 | 008 00 | 400 | 800 800 | 800 | 800 4 | 00 400 | 400 | 400 80 | 0 800 | 008 0 | 400 | 400 400 | 0 400 | 400 | 400 4 | 00 400 | 400 | 400 40 | 400 |
| | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | | 0 0 | | | 0 500 | | 750 750 | | | 50 750 | | 750 75 | | | | 400 400 750 750 | | | | 50 750 | | | 750 |
| PERM Flow | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | | | | | - | 1 | | - | | - | | | | | | - | | | | and the second data in the second data in | | - | | | | | | | | | |
| PERM Flow Recirculation Flow | - | | | and the second second | - | | | 0 | 0 | 0 1 | | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 0 | 0 8 | 00 800 | 0 | 0 | 0 0 | 0 0 | 800 | 800 0 | 0 0 | 0 | 0 8 | 00 800 | 0 0 | 0 | 0 |
| PERM Flow | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | | 0 | 0 | 0 | 0 0 | 1 1 | 0 | 0 | 0 | 0 0 | 167 | | 0 0 67 167 | | 0 0 250 250 | | | 00 800 50 250 | | 250 25 | C | 1 | | 800 0 250 250 | | | | 00 800 50 250 | | 250 25 | |

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| | | 28 | | 2029 | | | 2030 | | | 2031 | | | 2032 | | | 203 | | | | 2034 | | | 35 | | 203 | | | 2037 | | 203 | | 2039 |
|--|--------------------|------|----------|--------------|------------------|------|----------|----------------|--|------------|----------------|-----------------|----------|---------|-----------------|------|-----------|-----------|---------|----------------|----------|----------|------|---------------|-----------------------|-----------|--------|------------------|------|---------|-------|---------------------------|
| NIT 1 | Q1 Q2 | Q3 | 14 Q1 | Q2 Q3 | Q4 | Q1 | Q2 Q | 3 Q4 | Q1 | Q2 (| Q3 Q4 | Q1 | Q2 | Q3 Q4 | Q1 | Q2 | Q3 | Q4 Q | 1 Q2 | Q3 | Q4 C | Q1 Q2 | Q3 | Q4 Q1 | Q2 | Q3 Q4 | Q1 | Q2 Q3 | Q4 Q | 1 Q2 | Q3 Q4 | 4 Q1 (|
| ent/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - |
| ion | | | | | | | | | | | | | | | - | | | | | - | | _ | | | | | | | | | | - |
| ZATION SAMPLING | | | | | | | | | | | | | | | | | | - | - | | | | | | | | | | | | | - |
| VIT 2 | | | | | - | | | _ | | | | | | | _ | | | - | | | | | | | | | - | _ | | | | |
| ment/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - |
| lation | | | | | | | | - | | | | | | | | | | _ | | | | | | | | | | | | | | _ |
| ZATION SAMPLING | | | | | | | | | | | | | | | | | | | | | | | | - | | | | | | | | |
| JNIT 3 | | - | | | | | | _ | | | | | | | | | | | | | | _ | | | - | - | | | | | | - |
| ment/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ulation | | - | | | | | | | | | | | | | | | | | | | | | | | | - | | | | | | |
| LIZATION SAMPLING | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| UNIT 4 | | | | | - | | | _ | | | | - | | | | | | | | | | | | | | | | | | | | |
| atment/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| culation | 800 800 | L | - | | - | | <u> </u> | | | | _ | - | | | - | | - | | - | | | | | | | | | _ | | | | |
| LIZATION SAMPLING | | | 1 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| JNIT 5 | | | | | | | | | | | | | | - | | | | | - | | | | | | - | | | | | | | |
| eatment/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| culation | 500 500 | 500 | 500 500 | | 008 00 | | | | | | | | - | | | | | | | | | | | | | | | | | | | |
| ILIZATION SAMPLING | | | | | | | 1 | 1 1 | | | | | | | | | | | | | | | | | | | | | | | | |
| UNIT 6 | | | | | | | | | + | | | | | | - | | | | | | | | | | + + | | | | | | | + |
| tment/Reinjection | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| lation | 250 250 | 250 | 250 250 | 250 5 | 00 500 | 500 | 500 | 500 500 | and the second s | 800 | | | | | - | | | | | - | | | | | + | | | - | | | | - |
| LIZATION SAMPLING | | | | | | | | | | | 1 | 1 1 | 1 | | | | | | | | | | | | | | | | | | | |
| UNIT 7 | | | - | | | | | _ | | | | | | | - | | | | | | - | - | | | | | | | | - | | |
| eatment/Reinjection | 400 400 | 400 | 400 400 | | | | | | | | | | | | | | - | | | | | | | | | | | | | | | |
| n rculation | | | | 2 | 50 250 | 250 | 250 | 250 250 | 500 | 500 | 500 50 | 0 500 | 500 | 800 8 | 00 | | | | | - | | - | | | | | | | | | | - |
| BILIZATION SAMPLING | | | | | | | | | | | | | | | 1 | 1 | 1 | 1 | | | | | | | | | | | | | | |
| E UNIT 8 | 200 200 | 200 | 200 200 | | | | | | | | | | | | | | | | - | - | | | | | | | | _ | | | | |
| eatment/Reinjection | | | | 4 | 00 400 | 400 | 400 | 400 400 | | | | | | | | | | | | | | | | | | | | | | | | |
| culation | | | | | | | | | 250 | 250 | 250 25 | 0 250 | 250 | 500 5 | 00 500 | 500 | 500 | | 800 80 | 00 | | | | | | | | | | | | - |
| LIZATION SAMPLING | | | | | | | | - | | | | | | | _ | | | | | 1 | 1 | 1 1 | | | | | | | | | | |
| UNIT 9 | 500 400 | 300 | 200 200 | 200 2 | 200 | 200 | 200 | 200 | | | | | | | | | | | | | | | | | | | | | | | | |
| eatment/Reinjection | | | - | | | | | | 400 | 400 | 400 40 | 0 400 | 400 | 250 2 | 50 050 | 250 | 250 | 050 | 500 50 | 00 500 | 500 | 500 500 | | | | | | | | | | _ |
| culation | | | | | - | | | | | | | | | 250 2 | 50 250 | 250 | 200 | 200 | 500 50 | 0 500 | 000 | 500 500 | 800 | 800 | and the second second | | | | | | | |
| BILIZATION SAMPLING | | | | | | | | | | | | | | | _ | - | | | | | | | | 1000 | 1 1 | 1 1 | 1 | | | | | |
| EUNIT 10 | 900 800 | 700 | 500 500 | 400 3 | 200 | 200 | 200 | 200 200 | 200 | 200 | 200 20 | 200 | | | | | | | - | | | | | | | | | | | | | |
| reatment/Reinjection | | | | | | | | | | | _ | | | 400 4 | | | 400 | | 250 25 | 50 250 | 250 | 250 250 | 500 | E00 E0 | D 500 | 500 500 | 0 | | | _ | | |
| circulation | | | | | - | | | | | | | | | | | | | | 200 20 | | 200 | 250 250 | 500 | 500 50 | | 500 500 | 800 | 800 | | | | and a state of the second |
| BILIZATION SAMPLING | | | | | | | | - | | | | | | | | | | | | | | | 1 | - | | | | 1 | 1 | 1 1 | | |
| IE UNIT 11 | 1600 1500 | 1400 | 400 1300 | 1200 11 | 1100 | 1000 | 900 | 800 700 | 600 | 500 | 400 30 | 200 | 200 | 200 2 | 00 200 | 200 | 200 | | | | | | | | | | | | | | | |
| Freatment/Reinjection m | | | - | | | | | | | | | - | | | | | - | 512 | 400 40 | 00 400 | 400 | 400 400 | | 250 25 | 0 250 | 250 250 | 0 750 | 750 750 | 750 | | | |
| circulation | | | | | | | | | | | | | | | | | | | | | | | 200 | 250 25 | | 200 200 | | /50 /50 | | 008 000 | | |
| ABILIZATION SAMPLING | | | - | | | | | | | | | - | | | | | | | | - | | | | | | | | | | _ | 1 | 1 1 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow Bleed 1.2% | 3200 2900 38 35 | | | | 00 1500 19 18 | | | 200 900 | | 700 | 600 50 | 6 5 | 200 | 200 2 | 200 | 200 | 200 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 1 IX Bleed | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 1 RO Bleed Unit 2 RO Bleed | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 3 RO Bleed | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 4 RO Bleed Unit 5 RO Bleed | 0 0 | 0 | 0 0 | | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 6 RO Bleed | 83 83 | | | | 67 167 | 167 | 167 | 167 167 | | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 7 RO Bleed Unit 8 RO Bleed | 0 0 | 0 | 0 0 | 0 | 83 83 | 83 | 83 | 83 83 | 8 167) 83 | 167 83 | 167 16 83 6 | 67 167 13 83 | | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Jnit 9 RO Bleed | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 | | 67 167 83 83 | | 167 83 | 167 83 | 167 16 | 0 0 57 167 | 167 | 167 167 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| e Unit 10 RO Bleed e Unit 11 RO Bleed | 0 0 | | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 83 8 | 83 83 | 83 | 83 83 | | | 67 167 | | | 0 0 | 0 | 0 0 | 0 | 0 0 |
| Unit 11 RO bleed | 0 0 | U | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 83 | 83 8 | 3 83 | 83 83 | 3 250 | 250 250 | 250 | 0 0 | 0 | 0 0 |
| I DW needed capacity | 288 285 | 281 | 279 276 | 272 20 | 69 268 | 267 | 266 | 264 261 | 260 | 258 | 257 25 | 6 255 | 252 | 252 2 | 52 252 | 252 | 252 | 250 | 250 25 | 50 250 | 250 | 250 250 | 250 | 250 25 | 60 250 | 250 250 | 0 250 | 250 250 | 250 | 0 0 | 0 | 0 0 |
| low | 400 400 | 400 | 400 400 | 400 44 | 00 400 | 400 | 400 | 400 400 | 400 | 400 | 400 40 | 0 400 | 400 | 400 4 | 00 400 | 400 | 400 | 400 | 400 40 | 00 400 | 400 | 400 400 | 0 | 0 | 0 0 | 0 (| 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 |
| M Flow | 750 750 | 750 | 750 750 | 750 7 | 50 750 | 750 | 750 | 750 750 | 750 | 750 | 750 75 | | 750 | 750 7 | 50 750 | | 750 | 750 | 750 75 | 50 750 | 750 | 750 750 | 750 | 750 75 | 0 750 | 750 750 | 0 750 | 750 750 | 750 | 0 0 | 0 | 0 0 |
| E TO DDW | 800 800 250 250 | | | 0 8 250 2 | | | | 0 0 250 250 | | 800 250 | 250 25 | 0 0 | 0 250 | | 00 0 50 250 | 250 | 250 | | | 00 0 50 250 | 0 250 | 0 0 | | 800 250 25 | 0 0 | 0 0 | 0 800 | 800 0 250 250 | | 008 008 | 0 | 0 0 |
| 0 | | | | | | | | | | | | - | | | | | | | | | | | | | | | | | | | | |
| | 1400 1400 | 1400 | 400 1400 | 1400 14 | 1400 | 1400 | 1400 1 | 400 1400 | 1400 | 1400 1 | 1400 140 | 1400 | 1400 | 1400 14 | 00 1400 | 1400 | 1400 | 1400 1 | 400 140 | 00 1400 | 1400 1 | 400 1400 | 1000 | 1000 100 | 0 1000 | 1000 1000 | 0 1000 | 1000 1000 | 1000 | 0 0 | 0 | 0 0 |

APPENDIX T MARSLAND WATER BALANCE (PRODUCTION, RESTORATION, AND STABILIZATION SAMPLING)

| | - | - | PV size | Surety PV | Flow GPM | Days | PV Needeo | Total Dave | 91 Day Quarters | | Total Gal Needed | Plan Callen | Difference | PV Diff |
|--------------------------------------|------------|----------|----------------------|---|------------|------------------------|-----------|--------------|-----------------|------|---|------------------------|---|------------|
| MINE UNIT 1 | | | FV SIZE | PV | FIOW GPM | Days | PV Needed | i Total Days | 91 Day Quarters | | Total Gal Needed | Plan Gallons | Difference | PV Din |
| X Treatment/Reinjection | MU1 | IX | 95017565 | 95017565 | 800 | 82.480525 | 3 | 247 | 2.72 | 2600 | 285052695.1 | 336960000 | -51907304.9 | -0.5462916 |
| Perm | MU1 | RO | 95017565 | 95017565 | | 131.96884 | 6 | | 8.70 | 4500 | 570105390.2 | | -13094609.8 | -0.137812 |
| Recirculation | MU1 | RC | 95017565 | 95017565 | 800 | 82.480525 | 2 | 165 | 1.81 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| STABILIZATION SAMPLING | | | | | | | | | | | | | | |
| AINE UNIT 2 | | | | | | | | | | - | | | | |
| X Treatment/Reinjection | MU2 | IX | 95017565 | 95017565 | 220 | 299.92918 | 3 | 900 | 9.89 | 2800 | 285052695.1 | 362880000 | -77827304.9 | -0.819083 |
| Perm | MU2 | RO | 95017565 | 95017565 | 225 | 293.26409 | 6 | 1760 | 19.34 | 4750 | 570105390.2 | 615600000 | -45494609.8 | -0.47880 |
| Recirculation | MU2 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| STABILIZATION SAMPLING | | - | | | | | | | | | | | | _ |
| MINE UNIT 3 | - | | | | | | | | | | | | | |
| X Treatment/Reinjection | MU3 | IX | 95017565 | 95017565 | 220 | 299.92918 | 3 | 900 | 9,89 | 3200 | 285052695.1 | 414720000 | -129667305 | -1.364666 |
| Perm | MU3 | RO | 95017565 | 95017565 | 225 | 293.26409 | 6 | | 19.34 | 4750 | 570105390.2 | 615600000 | | -0.47880 |
| Recirculation | MU3 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| STABILIZATION SAMPLING | | | | | | | | | | | | | | |
| MINE UNIT 4 | | - | | | | | - | | | - | | | | - |
| X Treatment/Reinjection | MU4 | IX | 95017565 | 95017565 | 172 | 383.63035 | 3 | 1151 | 12.65 | 2800 | 285052695.1 | 362880000 | -77827304.9 | -0.819083 |
| Perm | MU4 | RO | 95017565 | 95017565 | 250 | 263.93768 | | 1583.62608 | 17.40 | 4500 | 570105390.2 | 583200000 | | -0.137812 |
| Recirculation | MU4 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | | 3.63 | 1600 | 190035130.1 | | -17324869.9 | -0.182333 |
| TABILIZATION SAMPLING | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| AINE UNIT 5 | 141.15 | IX | 05047505 | 05047565 | 0.00 | 100 5005 | - | ECO | 6.00 | 2000 | 295052005 4 | 400500000 | 101507005 | 1.040050 |
| X Treatment/Reinjection | MU5 MU5 | IX RO | 95017565 95017565 | 95017565 95017565 | 350 225 | 188.52691 293.26409 | 3 | | 6.22 19.34 | 3600 | 285052695.1 570105390.2 | 466560000 583200000 | | -1.910250 |
| Recirculation | MU5 | RC | 95017565 | 95017565 | 400 | 293.26409 164.96105 | 2 | | 3.63 | 1600 | 190035130.1 | 207360000 | | -0.137612 |
| TABILIZATION SAMPLING | | | _0011000 | | | | | 0.00 | 0.00 | | | 20,00000 | 1102-1000.0 | 0.102000 |
| | | | | | | | | | | | | | | |
| MINE UNIT 6 | | | | | | | | | | | 005050 | 01/01/01 | | 0.000 |
| X Treatment/Reinjection | MU6 | IX | 95017565 | | 1000 | 65.98442 | 3 | | 2.18 | 2400 | 285052695.1 | | -25987304.9 | -0.273500 |
| Recirculation | MU6 MU6 | RO RC | 95017565 95017565 | 95017565 95017565 | 800 400 | 82.480525 164.96105 | 6 | | 5.44 | 4500 | 570105390.2 190035130.1 | 583200000 207360000 | | -0.137812 |
| STABILIZATION SAMPLING | WUO | 1 | 90011005 | 0001/005 | 400 | 104.90105 | 2 | 330 | 3.03 | 1000 | 130033130.1 | 201300000 | -11324009.9 | -0.102333 |
| | | | | | | | | | | | Part of the second s | | | |
| AINE UNIT 7 | | | | | | | | | | | | | | |
| X Treatment/Reinjection | MU7 | IX | 95017565 | | 1000 | 65.98442 | 3 | | 2.18 | 2400 | 285052695.1 | | -25987304.9 | -0.273500 |
| Perm | MU7 | RO | 95017565 | 95017565 | 800 | 82.480525 | 6 | | 5.44 | 4500 | 570105390.2 | 583200000 | | -0.137812 |
| Recirculation | MU7 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| | | | | | | | | | | 1 | | | | |
| AINE UNIT 8 | | | | | | | | | | | | | | |
| X Treatment/Reinjection | MU8 | IX | 95017565 | and the second se | 1000 | 65.98442 | 3 | | 2.18 | 2400 | 285052695.1 | | -25987304.9 | -0.273500 |
| ² em | MU8 | RO | 95017565 | 95017565 | 800 | 82.480525 | 6 | | 5.44 | 4500 | 570105390.2 | 583200000 | | -0.137812 |
| Recirculation STABILIZATION SAMPLING | MU8 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| | | | | | | | | | | | | | | |
| AINE UNIT 9 | | | | | | | | | | | | | | |
| X Treatment/Reinjection | MU9 | IX | 95017565 | 95017565 | 1000 | 65.98442 | 3 | | 2.18 | 2400 | 285052695.1 | | -25987304.9 | -0.273500 |
| Perm | MU9 | RO | 95017565 | 95017565 | 800 | 82.480525 | 6 | | 5.44 | 4500 | 570105390.2 | 583200000 | | -0.137812 |
| Recirculation | MU9 | RC | 95017565 | 95017565 | 400 | 164,96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.1823333 |
| TABILIZA HON SAMPLING | - | | | | | | | | | | | | | |
| MINE UNIT 10 | | | | | | | | | | | | | | |
| X Treatment/Reinjection | MU10 | IX | 95017565 | 95017565 | 1000 | 65.98442 | 3 | 198 | 2.18 | 2400 | 285052695.1 | 311040000 | -25987304.9 | -0.273500 |
| Perm | MU10 | RO | 95017565 | 95017565 | 800 | 82.480525 | 6 | | 5.44 | 4500 | 570105390.2 | 583200000 | and the second second second second second second | -0.137812 |
| | MU10 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| STABILIZATION SAMPLING | | | | | | | | | | | | | | - |
| MINE UNIT 11 | | + | | | | | | | | | | | | |
| X Treatment/Reinjection | MU11 | IX | 95017565 | 95017565 | 1000 | 65.98442 | 3 | 198 | 2.18 | 2400 | 285052695.1 | 311040000 | -25987304.9 | -0.2735000 |
| Perm | MU11 | RO | 95017565 | 95017565 | 800 | 82.480525 | 6 | 495 | 5.44 | 4500 | 570105390.2 | 583200000 | -13094609.8 | -0.137812 |
| | MU11 | RC | 95017565 | 95017565 | 400 | 164.96105 | 2 | 330 | 3.63 | 1600 | 190035130.1 | 207360000 | -17324869.9 | -0.182333 |
| TABILIZATION SAMPLING | | | | | | | - | | | | | | | |
| | | | | | | | | | | | | | | |
| Prod Flow | | | | | | | | | | | | | | + |
| Prod Bleed 1.2% | | 1 | | | | | | | | | | | | |
| line Unit 1 IX Bleed | | | | | | | | | | | | | | |
| line Unit 1 RO Bleed | | | | | | | | | | | | | | |
| line Unit 2 RO Bleed | | - | | | | | | | | | | | | - |
| Aine Unit 3 RO Bleed | - | | | | | | | | | + | | | | - |
| line Unit 5 RO Bleed | | | | | | | | | | 1 | | | | + |
| line Unit 6 RO Bleed | | | | | | | | | | | | | | |
| line Unit 7 RO Bleed | | | | | | | | | | | | | | |
| line Unit 8 RO Bleed | | | | | | | | | | | | | | |
| Nine Unit 9 RO Bleed | | - | | | | | | | | | | | | |
| fine Unit 10 RO Bleed | | | | | | | | | | | | | | |
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| otal DW needed capacity | | | | | | | | | | | | | | |
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| X Flow | | | | | | | | | | | | | | |
| PERM Flow | | | | | | | | | | | | | | |
| Recirculation Flow | | | | | | | | | | | | | | |
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