

Appendix R

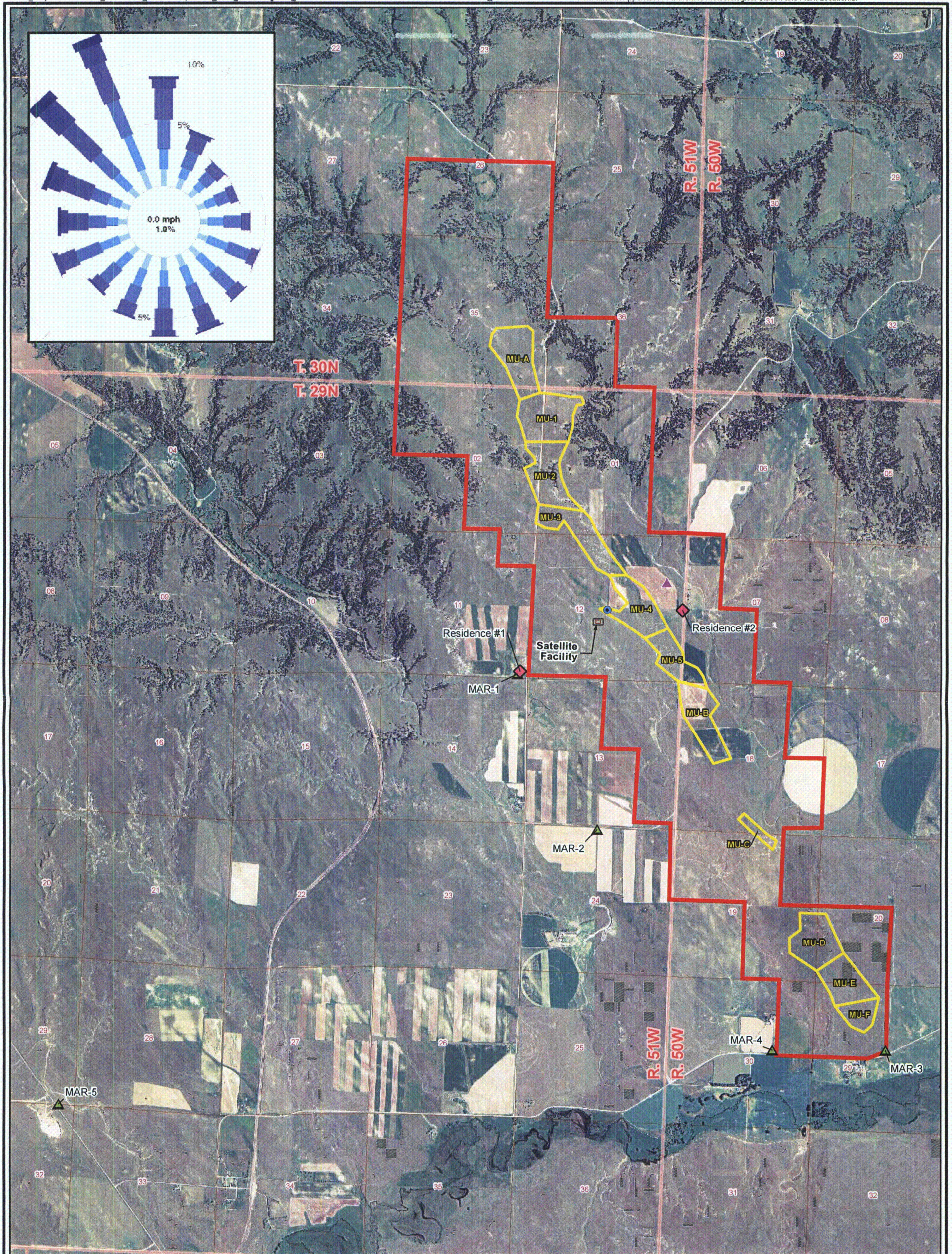
Siting of Meteorological Instruments

NRC Regulatory Guide 3.63 provides guidance acceptable to the NRC regarding the siting of meteorological instruments. The siting of the Marsland Expansion Area meteorological tower followed guidance in NRC Regulatory Guide 3.63, which states:

“The location of the meteorological instruments should represent as closely as possible the long-term meteorological characteristics of the area for which the measurements are being made. Whenever possible, the base of the instrument tower or mast should be sited at approximately the same elevation as the facility operation. Ideally, the instruments should be located in an area where localized singular natural or man-made obstructions (e.g., trees, buildings) will have little or no influence on meteorological measurements. Measurements of wind speed, wind direction and sigma theta...should be made at least 10 obstruction heights away from the nearest obstruction. To the extent practicable, these instruments should not be located in the prevailing downwind direction of an obstruction.” In addition to criteria related to wind measurement, the guide also addresses solar radiation. “If instrumentation is used to measure incoming solar radiation, it should be located in an area as free as possible from terrestrial shadows.”

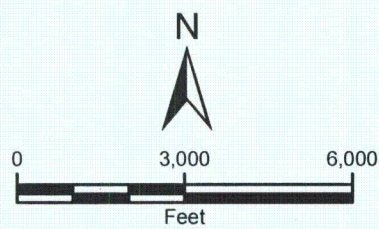
Accordingly, the following siting issues were considered:

1. **Elevation** – The meteorological monitoring tower, at 4,240 ft. above sea level, is near the elevation of the proposed satellite plant (4,245 ft.). The meteorological site elevation is also representative of the entire Marsland Expansion Area, in which surface elevations range generally between 4,100 and 4,300 ft. above sea level.
2. **Proximity** – The meteorological monitoring tower is located 0.4 miles east-northeast of the proposed plant site. **Figure R-1** shows the location of the tower relative to the plant site.
3. **Topography** – Both the meteorological monitoring tower and the proposed plant site are surrounded by relatively flat topography. A small drainage runs through the area, but the monitoring tower is situated on a flat area above the stream channel.
4. **Obstructions** – **Figure R-2** depicts the area surrounding the Marsland meteorological tower and proposed plant site. The area is relatively flat with no trees, structures or other obstructions in the vicinity of the meteorological tower.
5. **Shadows** – There are **no trees**, large rocks or other obstructions in the immediate vicinity that would compromise solar radiation exposure at the meteorological station.



LEGEND

- Proposed Deep Disposal Well
- Air Sample Station
- Met Station
- Residence
- Mine Unit
- Proposed Marsland Expansion Area



PROJECTION: NAD1927,
STATE PLANE NEBRASKA NORTH, FIPS 2601
SOURCES: USDA NAIP IMAGERY 2010







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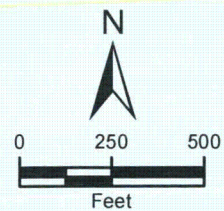
**FIGURE R-1
MARSLAND
METEOROLOGICAL STATION
AND PLANT LOCATION**



LEGEND

-  Met Station
-  Centroid of Proposed Satellite Facility
-  Proposed Satellite Plant Footprint
-  Proposed Fence

PROJECTION: NAD1983,
STATE PLANE NEBRASKA NORTH, FIPS 2601
SOURCES: USDA NAIP IMAGERY 2010



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**FIGURE R-2
LOCATION OF
MARSLAND METEOROLOGICAL STATION
(CLOSEUP)**

Appendix S

Justification for Use of 15 Years of Scottsbluff's Meteorological Data

The regression analyses for wind parameters at the Scottsbluff meteorological station are repeated below with p-values as requested in NRC Comment #4 a). As seen in **Figure S-1**, the wind direction correlation produced a very high coefficient of determination, or R^2 . In the wind direction regression analysis below, the p-value of 0.000 indicates virtually no chance that this R^2 value is accidental. In other words, the 1-year distribution of wind directions is strongly correlated with the 15-year distribution, to a high degree of confidence.

Scottsbluff Regression Analysis: 15-Year Directions versus 1-Year Directions

The regression equation is:

$$15\text{-Year Directions} = 0.006077 + 0.9028 \quad 1\text{-Year Directions}$$

$$S = 0.00689141 \quad R\text{-Sq} = 97.5\% \quad R\text{-Sq(adj)} = 97.4\%$$

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	0.0262411	0.0262411	552.54	0.000
Error	14	0.0006649	0.0000475		
Total	15	0.0269060			

In similar fashion, the wind speed correlation produced a very high coefficient of determination (**Figure S-2**). The p-value of 0.001 shown in the regression analysis below indicates a 99.9% confidence that this R^2 value is not accidental. In other words, the 1-year distribution of wind speeds is strongly correlated with the 15-year distribution, to a high degree of confidence.

Scottsbluff Regression Analysis: 15-Year Speeds versus 1-Year Speeds

The regression equation is:

$$15\text{-Year Speeds} = 0.00959 + 0.9425 \quad 1\text{-Year Speeds}$$

$$S = 0.0321279 \quad R\text{-Sq} = 94.8\% \quad R\text{-Sq(adj)} = 93.5\%$$

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	0.0748612	0.0748612	72.53	0.001
Error	4	0.0041288	0.0010322		
Total	5	0.0789900			

In response to NRC Comment #4 b), hourly wind data were retrieved from the Chadron airport meteorological station. **Figures S-3** and **S-4** illustrate strong similarities between the baseline year and the 12-year period from 2001 through 2012.

The similarities in **Figures S-5** and **S-6** are further illustrated by comparing the bar graphs of wind direction and wind speed distributions between the baseline year and the 12-year period (**Figures S-5** and **S-6**).

The regression analyses for wind parameters at the Chadron meteorological station are presented below with p-values as requested in NRC Comment #4 a). **Figure S-7** shows the wind direction correlation produced a very high coefficient of determination, or R^2 . As seen in the regression analysis below, the p-value of 0.000 indicates virtually no chance that this R^2 value is accidental. In other words, the 1-year distribution of wind directions is strongly correlated with the 12-year distribution, to a high degree of confidence.

Chadron Regression Analysis: 12-Year Directions versus 1-Year Directions

The regression equation is:

$$12\text{-Year Directions} = 0.002237 + 0.9618 \quad 1\text{-Year Directions}$$

$$S = 0.00685647 \quad R\text{-Sq} = 95.8\% \quad R\text{-Sq(adj)} = 95.5\%$$

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	0.0160024	0.0160024	340.39	0.000
Error	15	0.0007052	0.0000470		
Total	16	0.0167075			

In similar fashion, the wind speed correlation for Chadron produced a very high coefficient of determination (**Figure S-8**). The p-value of 0.000 shown in the regression analysis below indicates virtual certainty that this R^2 value is not accidental. In other words, the 1-year distribution of wind speeds is strongly correlated with the 12-year distribution, to a high degree of confidence.

Chadron Regression Analysis: 12-Year Speeds versus 1-Year Speeds

The regression equation is:

$$12\text{-Year Speeds} = - 0.00580 + 1.04 \quad 1\text{-Year Speeds}$$

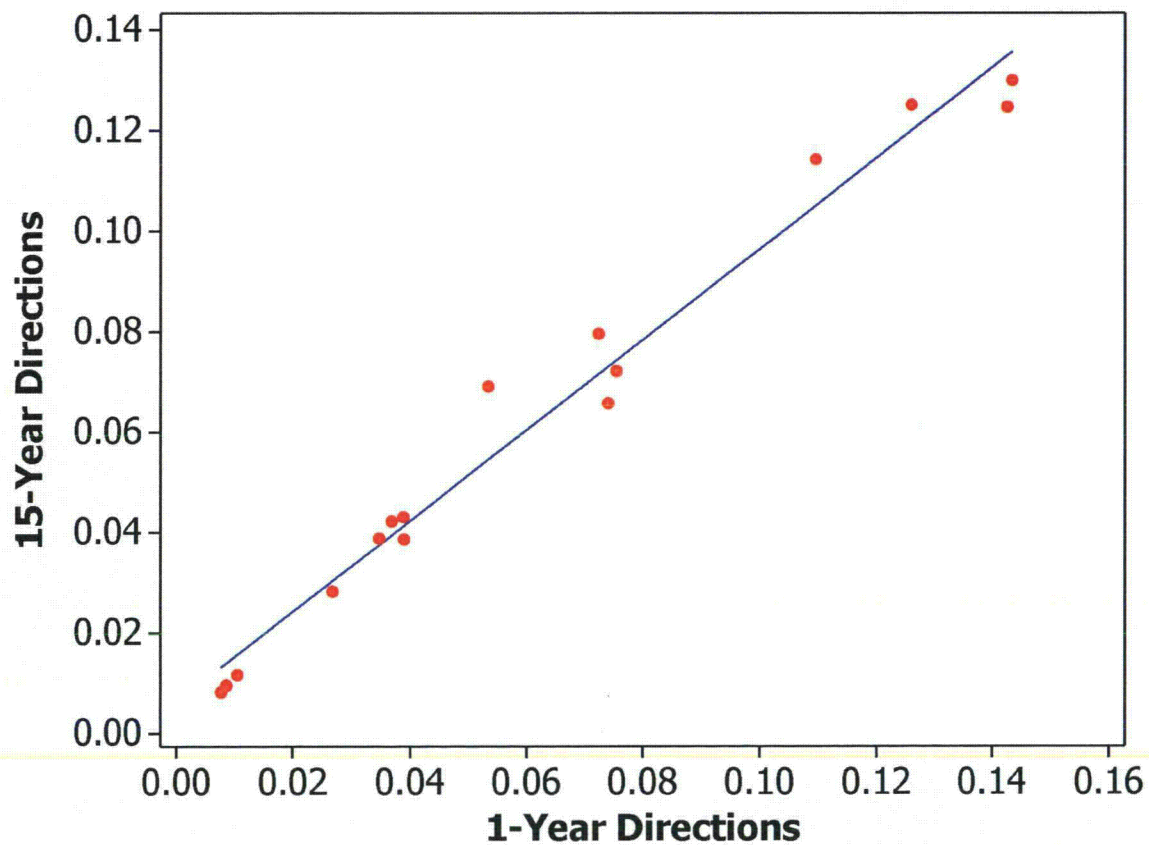
$$S = 0.0146045 \quad R\text{-Sq} = 98.2\% \quad R\text{-Sq(adj)} = 97.9\%$$

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	0.0590527	0.0590527	276.86	0.000
Error	5	0.0010665	0.0002133		
Total	6	0.0601191			

Fitted Line Plot

$$15\text{-Year Directions} = 0.006077 + 0.9028 \text{ 1-Year Directions}$$

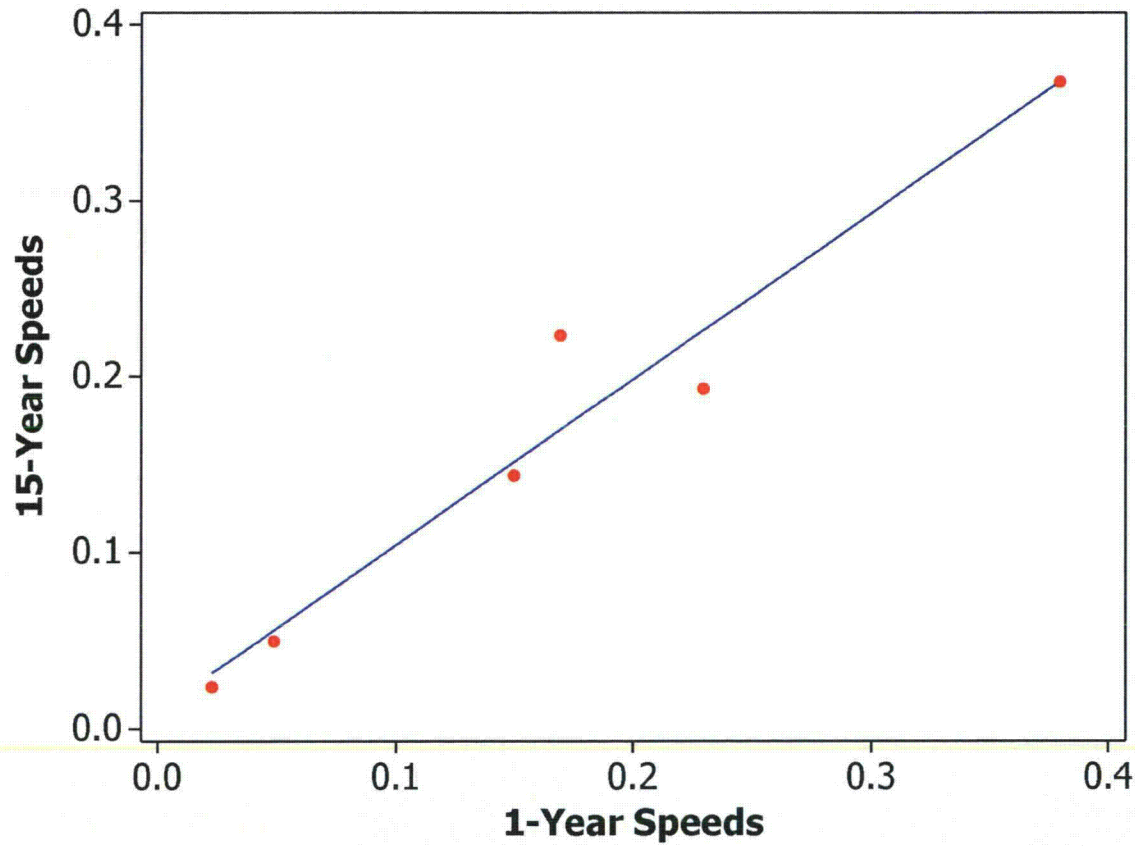


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FIGURE S-1
WIND DIRECTION CORRELATION
FOR SCOTTSBLUFF AIRPORT

Fitted Line Plot

$$15\text{-Year Speeds} = 0.00959 + 0.9425 \text{ 1-Year Speeds}$$



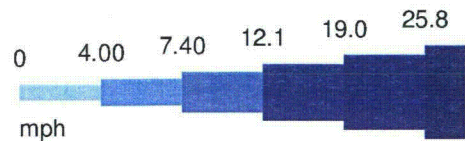
S	0.0321279
R-Sq	94.8%
R-Sq(adj)	93.5%



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FIGURE S-2
WIND SPEED CORRELATION
FOR SCOTTSBLUFF AIRPORT

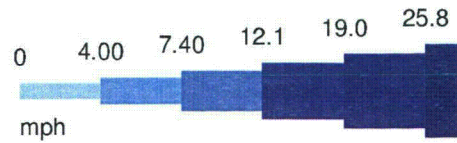
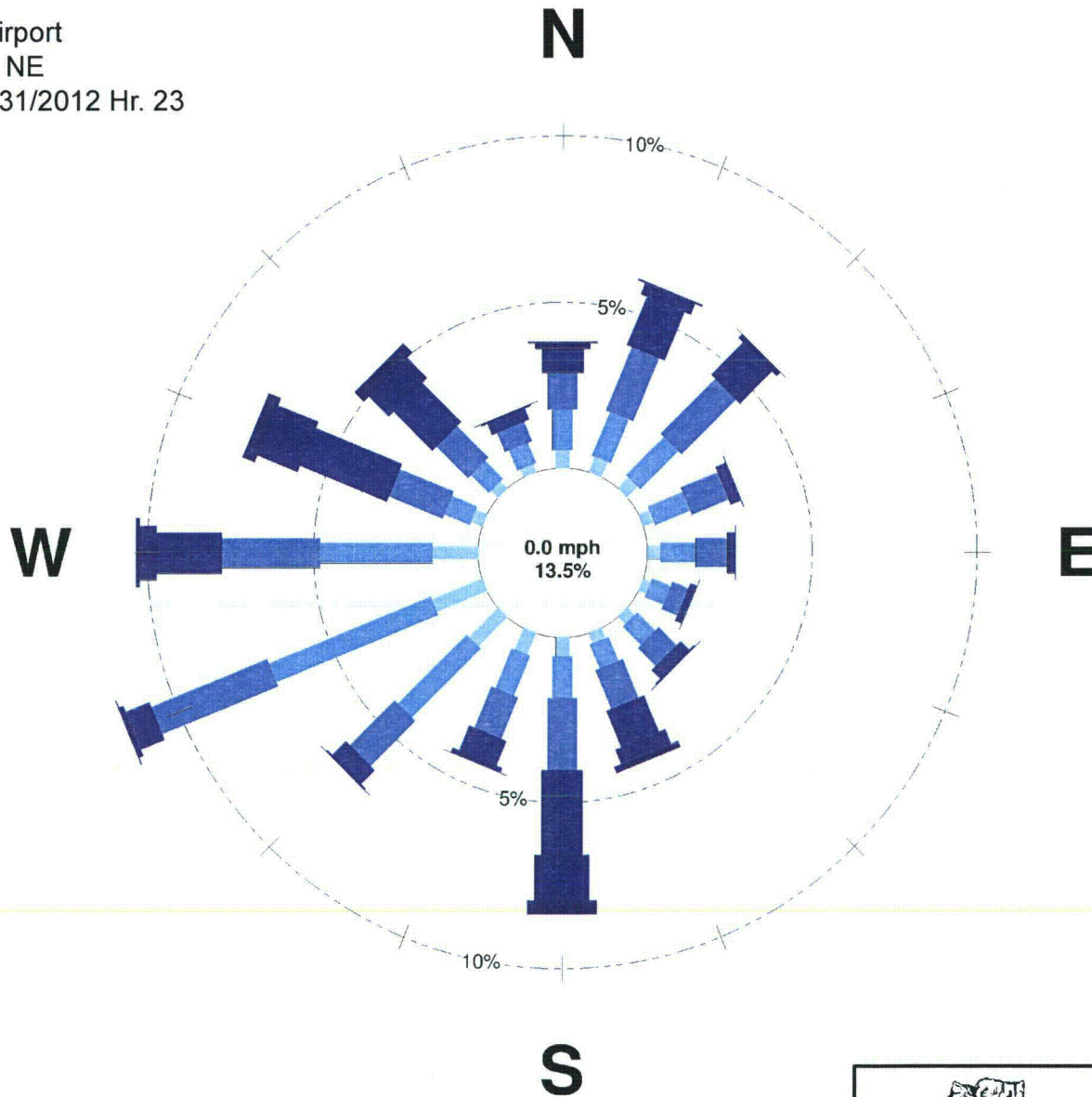
Chadron Airport
 Chadron, NE
 8/24/2010 Hr. 2 to 8/29/2011 Hr. 14



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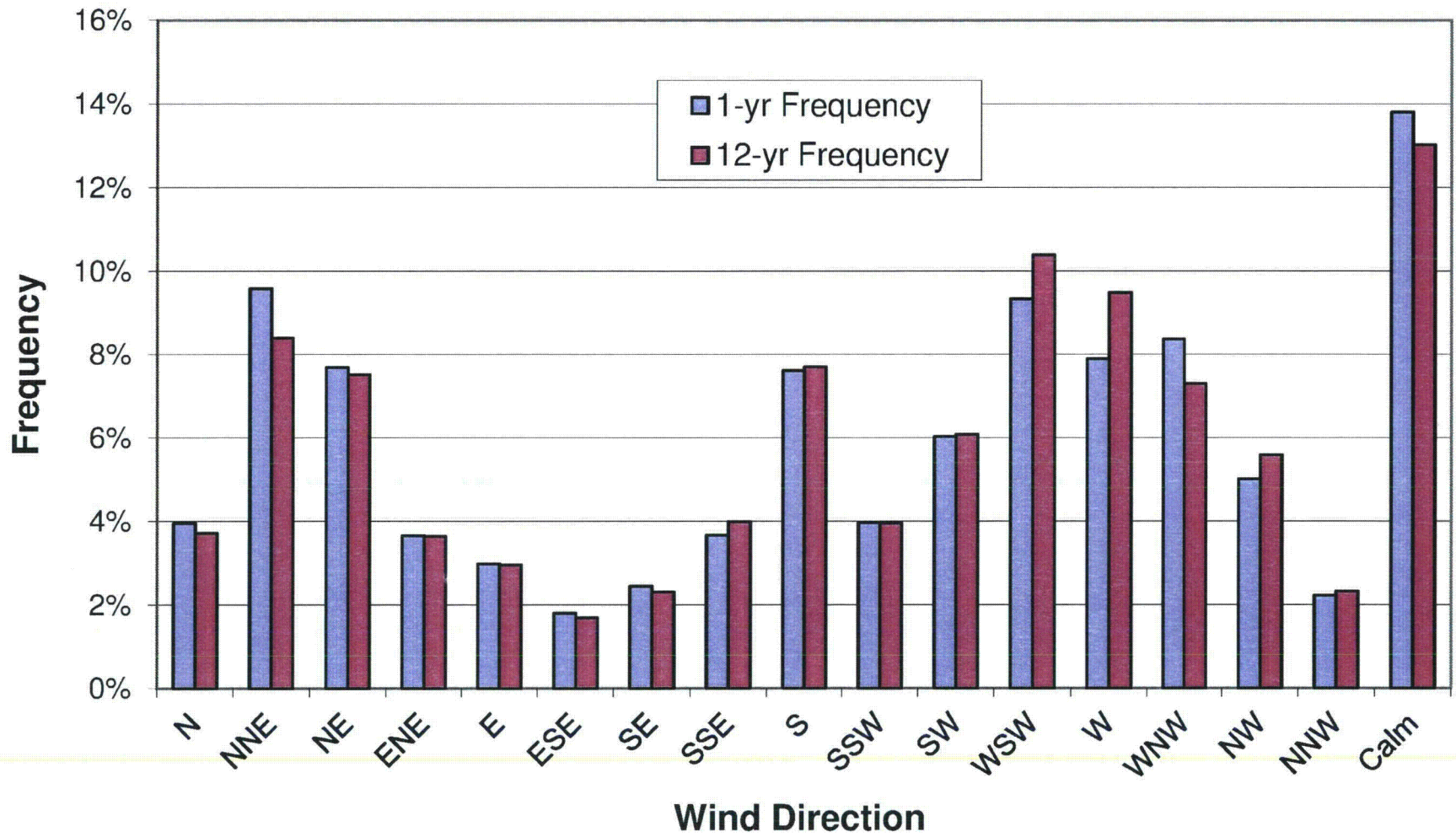
FIGURE S-3
BASELINE-YEAR WIND ROSE
CHADRON AIRPORT

Chadron Airport
 Chadron, NE
 1/1/2001 Hr. 1 to 12/31/2012 Hr. 23



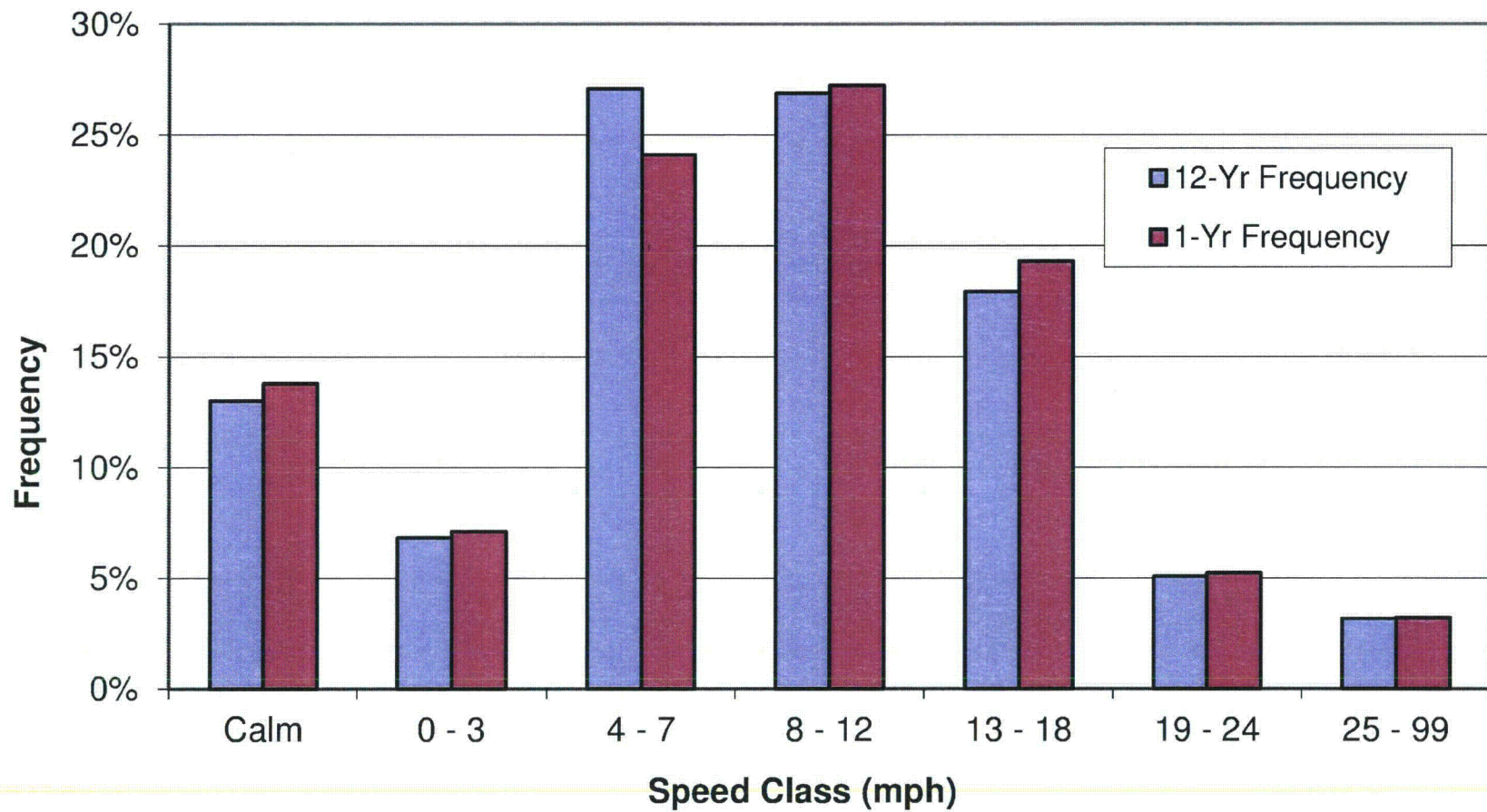
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FIGURE S-4
12-YEAR WIND ROSE
CHADRON AIRPORT



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FIGURE S-5
CHADRON AIRPORT
WIND DIRECTION DISTRIBUTION

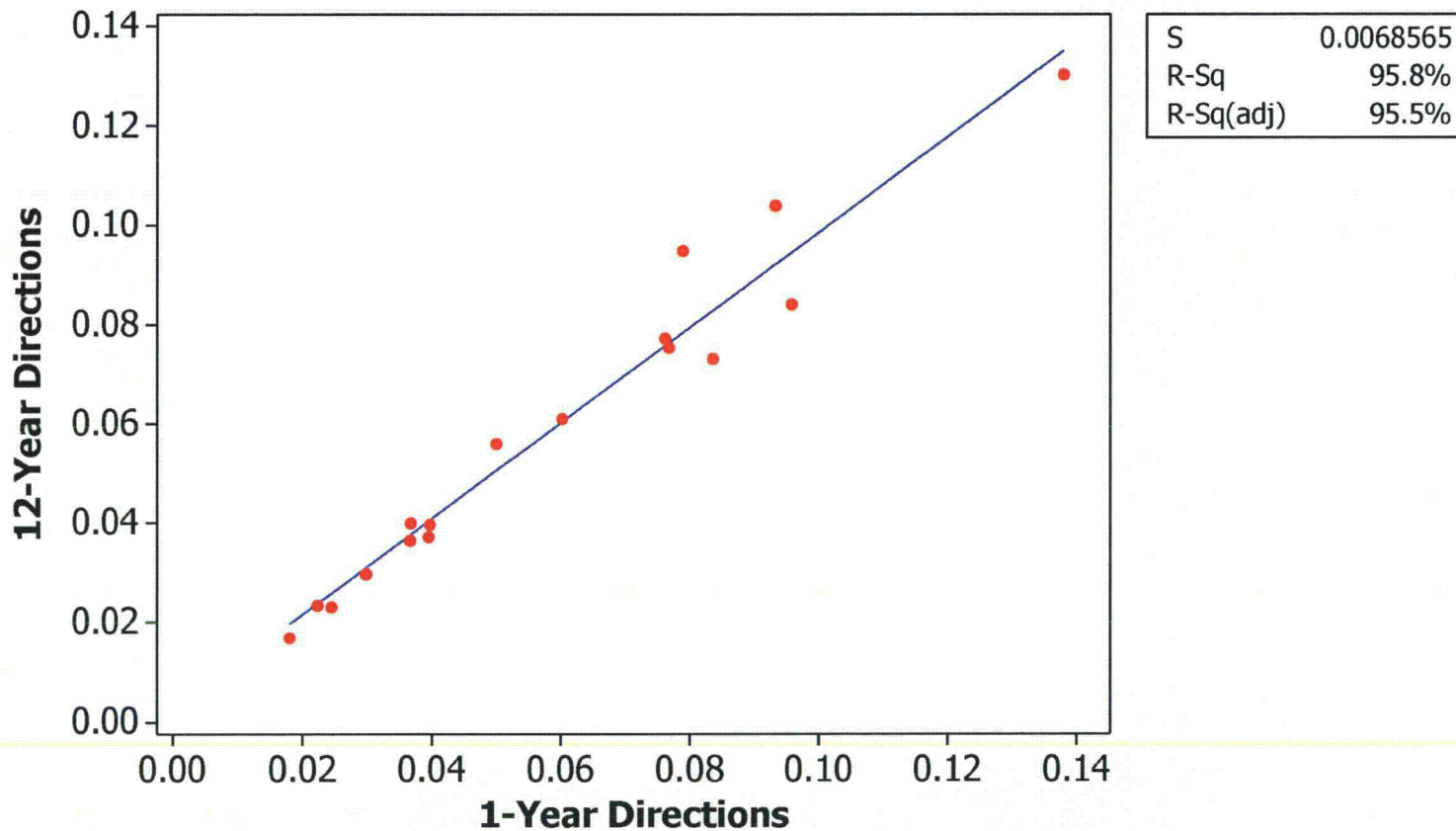


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FIGURE S-6
CHADRON AIRPORT
WIND SPEED DISTRIBUTION

Fitted Line Plot

$$12\text{-Year Directions} = 0.002237 + 0.9618 \text{ 1-Year Directions}$$

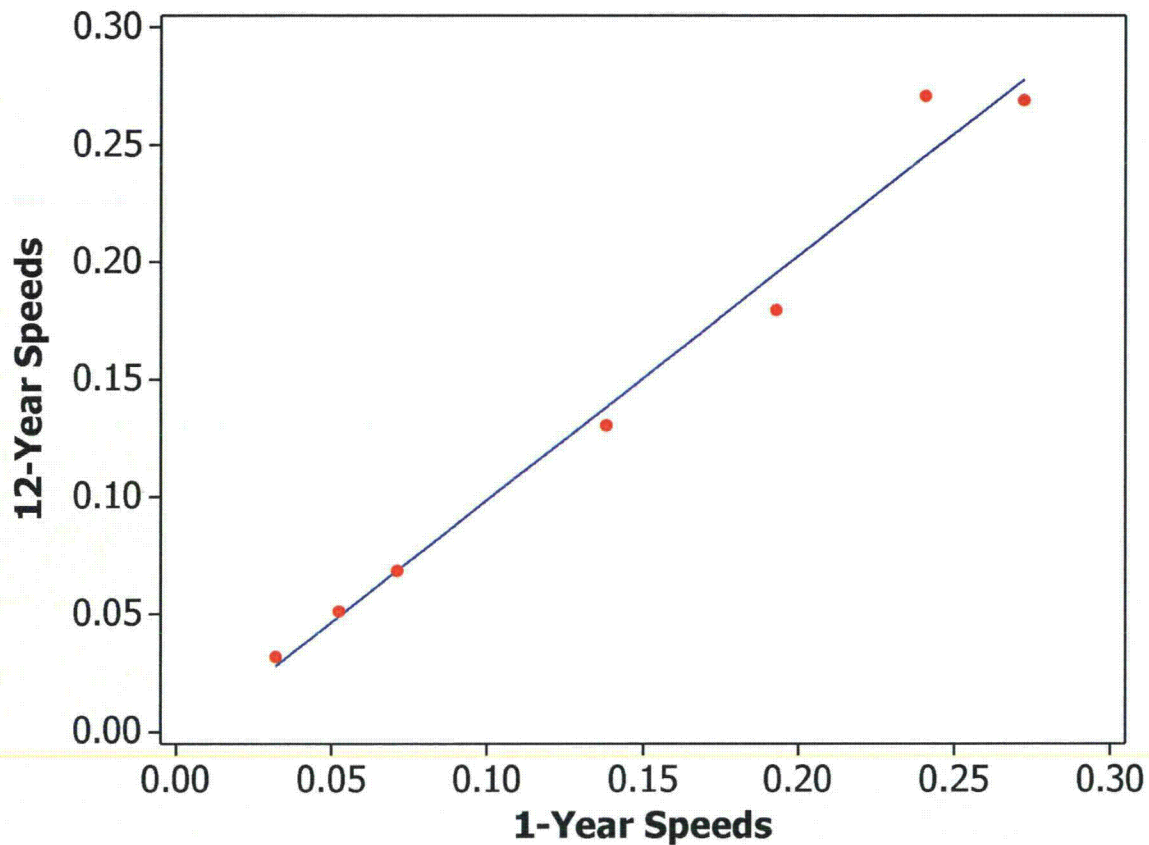


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FIGURE S-7
WIND DIRECTION CORRELATION
FOR CHADRON AIRPORT

Fitted Line Plot

$$12\text{-Year Speeds} = -0.00580 + 1.041 \text{ 1-Year Speeds}$$



S	0.0146045
R-Sq	98.2%
R-Sq(adj)	97.9%



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FIGURE S-8
WIND SPEED CORRELATION
FOR CHADRON AIRPORT

APPENDIX T MARSLAND WATER BALANCE (PRODUCTION, RESTORATION, AND STABILIZATION SAMPLING)

			Surety														
			PV size	PV	Flow GPM	Days	PV Needed	Total Days	#1 Day Quarters		Total Gal Needed	Plan Gallons	Difference	PV Diff			
MINE UNIT 1																	
IX Treatment/Reinjection Perm	MU1	IX	95017565	95017565	800	82.480525	3	247	2.72	2600	285052695.1	336960000	-51907304.9	-0.54629168			
Recirculation	MU1	RO	95017565	95017565	500	131.96984	6	792	8.70	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU1	RC	95017565	95017565	800	82.480525	2	165	1.81	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 2																	
IX Treatment/Reinjection Perm	MU2	IX	95017565	95017565	220	299.92918	3	900	9.89	2800	285052695.1	362880000	-77827304.9	-0.81908334			
Recirculation	MU2	RO	95017565	95017565	225	293.26409	6	1760	19.34	4750	570105390.2	615600000	-45494609.8	-0.4788021			
STABILIZATION SAMPLING	MU2	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 3																	
IX Treatment/Reinjection Perm	MU3	IX	95017565	95017565	220	299.92918	3	900	9.89	3200	285052695.1	414720000	-129667305	-1.36466668			
Recirculation	MU3	RO	95017565	95017565	225	293.26409	6	1760	19.34	4750	570105390.2	615600000	-45494609.8	-0.4788021			
STABILIZATION SAMPLING	MU3	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 4																	
IX Treatment/Reinjection Perm	MU4	IX	95017565	95017565	172	383.63035	3	1151	12.65	2800	285052695.1	362880000	-77827304.9	-0.81908334			
Recirculation	MU4	RO	95017565	95017565	250	283.93768	6	1583.62608	17.40	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU4	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 5																	
IX Treatment/Reinjection Perm	MU5	IX	95017565	95017565	350	188.52691	3	566	6.22	3600	285052695.1	466560000	-181507305	-1.91025001			
Recirculation	MU5	RO	95017565	95017565	225	293.26409	6	1760	19.34	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU5	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 6																	
IX Treatment/Reinjection Perm	MU6	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU6	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU6	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 7																	
IX Treatment/Reinjection Perm	MU7	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU7	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU7	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 8																	
IX Treatment/Reinjection Perm	MU8	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU8	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU8	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 9																	
IX Treatment/Reinjection Perm	MU9	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU9	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU9	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 10																	
IX Treatment/Reinjection Perm	MU10	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU10	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU10	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
MINE UNIT 11																	
IX Treatment/Reinjection Perm	MU11	IX	95017565	95017565	1000	65.98442	3	198	2.18	2400	285052695.1	311040000	-25987304.9	-0.27350001			
Recirculation	MU11	RO	95017565	95017565	800	82.480525	6	495	5.44	4500	570105390.2	583200000	-13094609.8	-0.13781252			
STABILIZATION SAMPLING	MU11	RC	95017565	95017565	400	164.96105	2	330	3.63	1600	190035130.1	207360000	-17324869.9	-0.18233334			
Prod Flow																	
Prod Bleed 1.2%																	
Mine Unit 1 IX Bleed																	
Mine Unit 1 RO Bleed																	
Mine Unit 2 RO Bleed																	
Mine Unit 3 RO Bleed																	
Mine Unit 4 RO Bleed																	
Mine Unit 5 RO Bleed																	
Mine Unit 6 RO Bleed																	
Mine Unit 7 RO Bleed																	
Mine Unit 8 RO Bleed																	
Mine Unit 9 RO Bleed																	
Mine Unit 10 RO Bleed																	
Mine Unit 11 RO Bleed																	
Total DW needed capacity																	
IX Flow																	
PERM Flow																	
Recirculation Flow																	
BRINE TO DDW																	
IX + RO																	