UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

February 13, 2013

Mr. William G. Gideon, Vice President
H. B. Robinson Steam Electric Plant
Carolina Power & Light Company
3581 West Entrance Road
Hartsville, SC 29550

SUBJECT: H. B. ROBINSON STEAM ELECTRIC PLANT, UNIT NO. 2 - ISSUANCE OF AN AMENDMENT ON TECHNICAL SPECIFICATION CHANGE REGARDING CORRECTIONS TO TABLE 3.3.1-1 NOTE 1 (TAC NO. ME8225)

Dear Mr. Gideon:

The Nuclear Regulatory Commission has issued the enclosed Amendment No. 231 to Renewed Facility Operating License No. DPR-23 for the H. B. Robinson Steam Electric Plant, Unit No. 2 (HBRSEP). This amendment changes the HBRSEP Technical Specifications (TSs) in response to your application dated March 16, 2012 (Agencywide Documents Access and Management System (ADAMS) Accession No. ML12083A292), as supplemented by letter dated August 16, 2012 (ADAMS Accession No. ML12242A242).

The amendment changes HBRSEP TS Table 3.3.1-1 for Overtemperature Delta Temperature to be consistent with NUREG-1431, Revision 3, "Standard Technical Specifications - Westinghouse Plants."

A copy of the related Safety Evaluation is enclosed. Notice of Issuance will be included in the Commission's biweekly *Federal Register* notice.

Sincerely,

Araceli T. Billoch Colón

Araceli T. Billoch Colón, Project Manager
Plant Licensing Branch II-2
Division of Operating Reactor Licensing
Office of Nuclear Reactor Regulation

Docket No. 50-261

Enclosures:
1. Amendment No. 231 to DPR-23
2. Safety Evaluation

cc w/enclosures: Distribution via ListServ

UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

CAROLINA POWER & LIGHT COMPANY

DOCKET NO. 50-261

H. B. ROBINSON STEAM ELECTRIC PLANT, UNIT NO. 2

AMENDMENT TO RENEWED FACILITY OPERATING LICENSE

Amendment No. 231
Renewed License No. DPR-23

1. The Nuclear Regulatory Commission (the Commission) has found that:

   A. The application for amendment by Carolina Power & Light Company (the licensee), dated March 16, 2012, as supplemented by letter dated August 16, 2012, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act), and the Commission's rules and regulations set forth in 10 CFR Chapter I;

   B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;

   C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;

   D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and

   E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.

2. Accordingly, the license is amended by changes to the Technical Specifications, as indicated in the attachment to this license amendment; and paragraph 3.B. of Renewed Facility Operating License No. DPR-23 is hereby amended to read as follows:

   B. Technical Specifications

   The Technical Specifications contained in Appendix A, as revised through Amendment No. 231 are hereby incorporated in the license.

   The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of the date of its issuance and shall be implemented within 120 days.

FOR THE NUCLEAR REGULATORY COMMISSION

Jessie F. Quichocho, Chief
Plant Licensing Branch II-2
Division of Operating Reactor Licensing
Office of Nuclear Reactor Regulation

Attachment:
Changes to Operating License No. DPR-23
and the Technical Specifications

Date of Issuance: February 13, 2013

ATTACHMENT TO LICENSE AMENDMENT NO. 231

RENEWED FACILITY OPERATING LICENSE NO. DPR-23

DOCKET NO. 50-261

Replace the following pages of the Renewed Facility Operating License and Appendix "A" Technical Specifications with the enclosed pages. The revised pages are identified by amendment number and contain marginal lines indicating the areas of change.

Remove	Insert
License DPR-23 Page 3	License DPR-23 Page 3
TSs 3.3-18	TSs 3.3-18

neutron sources for reactor startup, sealed sources for reactor instrumentation and radiation monitoring equipment calibration, and as fission detectors in amounts as required;

D. Pursuant to the Act and 10 CFR Parts 30, 40 and 70, to receive, possess, and use in amounts as required any byproduct, source, or special nuclear material without restriction to chemical or physical form for sample analysis or instrument and equipment calibration or associated with radioactive apparatus or components;

E. Pursuant to the Act and 10 CFR Parts 30 and 70, to possess, but not separate, such byproduct and special nuclear materials as may be produced by operation of the facility.

3. This renewed license shall be deemed to contain and is subject to the conditions specified in the following Commission regulations: 10 CFR Part 20, Section 30.34 of 10 CFR Part 30, Section 40.41 of 10 CFR Part 40, Section 50.54 and 50.59 of 10 CFR Part 50, and Section 70.32 of 10 CFR Part 70; and is subject to all applicable provisions of the Act and to the rules, regulations, and orders of the Commission now or hereafter in effect; and is subject to the additional conditions specified or incorporated below:

A. Maximum Power Level

The licensee is authorized to operate the facility at a steady state reactor core power level not in excess of 2339 megawatts thermal.

B. Technical Specifications

The Technical Specifications contained in Appendix A, as revised through Amendment No. 231 are hereby incorporated in the license.

The licensee shall operate the facility in accordance with the Technical Specifications.

(1) For Surveillance Requirements (SRs) that are new in Amendment 176 to Final Operating License DPR-23, the first performance is due at the end of the first surveillance interval that begins at implementation of Amendment 176. For SRs that existed prior to Amendment 176, including SRs with modified acceptance criteria and SRs whose frequency of performance is being extended, the first performance is due at the end of the first surveillance interval that begins on the date the Surveillance was last performed prior to implementation of Amendment 176.

Table 3.3.1-1 (page 6 of 7)
Reactor Protection System Instrumentation

Note 1: Overtemperature ΔT

The Overtemperature ΔT Function Allowable Value shall not exceed the following Nominal Trip Setpoint by more than 2.96% of ΔT span.

$$\Delta T_{setpoint} \leq \Delta T_0 \{ K_1 - K_2 [(1 + \tau_1 S) / (1 + \tau_2 S)] (T - T') + K_3(P - P') - f(\Delta I) \}$$

Where: ΔT_0 is the indicated ΔT at RTP, °F.
s is the Laplace transform operator, sec^{-1}.
T is the measured RCS average temperature, °F.
T' is the reference T_{avg} at RTP, ≤ 575.9°F.

P is the measured pressurizer pressure, psig
P' is the nominal RCS operating pressure, ≥ 2235 psig

$K_1 \leq 1.1265$ $K_2 = 0.01228/°F$ $K_3 = 0.00089/psig$
$\tau_1 \geq 20.08$ sec $\tau_2 \leq 3.08$ sec

$f(\Delta I) =$ $2.4\%\{(q_b - q_t) - 17\}$ when $q_t - q_b < -17\%$ RTP
0% of RTP when $-17\% \text{ RTP} \leq q_t - q_b \leq 12\%$ RTP
$2.4\%\{(q_t - q_b) - 12\}$ when $q_t - q_b > 12\%$ RTP

Where q_t and q_b are percent RTP in the upper and lower halves of the core, respectively, and $q_t + q_b$ is the total THERMAL POWER in percent RTP.

UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

RELATED TO AMENDMENT NO. 231 TO

RENEWED FACILITY OPERATING LICENSE NO. DPR-23

CAROLINA POWER & LIGHT COMPANY

H. B. ROBINSON STEAM ELECTRIC PLANT, UNIT NO. 2

DOCKET NO. 50-261

1.0 INTRODUCTION

By letter to the U.S. Nuclear Regulatory Commission (NRC) dated March 16, 2012 (Agencywide Documents Access and Management System (ADAMS) Accession No. ML12083A292), as supplemented by letter dated August 16, 2012 (ADAMS Accession No. ML12242A242), Carolina Power & Light Company (the licensee), doing business as Progress Energy Carolinas, Inc., submitted a license amendment request for changes to the H. B. Robinson Steam Electric Plant, Unit No. 2 (HBRSEP), Technical Specifications (TSs). The requested changes would make corrections in TS Table 3.3.1-1 for Overtemperature Delta Temperature (OTΔT) consistent with NUREG-1431, Revision 3, "Standard Technical Specifications [STSs] - Westinghouse Plants."

The supplement dated August 16, 2012, provided additional information that clarified the application, did not expand the scope of the application as originally noticed, and did not change the staff's initial proposed no significant hazards consideration determination as published in the *Federal Register* on April 17, 2012 (77 FR 22811).

2.0 REGULATORY EVALUATION

The purposes of the reactor protection system (RPS) are to: 1) initiate a reactor trip if safe operating limits are exceeded, and 2) initiate engineered safety features action(s) if an accident occurs. The initiation of a reactor trip by the RPS prevents the core from operating in a condition that could cause damage to the core. The reactor plant operating limits are determined and set by the utility's Final Safety Analysis Report, and are incorporated into the plant TSs.

Section 182a of the Atomic Energy Act requires applicants for nuclear power plant operating licenses to include TSs as part of the license. The NRC regulatory requirements related to the content of the TSs are contained in Title 10, *Code of Federal Regulations* (10 CFR), Part 50, Section 50.36, "Technical Specifications." The TS requirements in 10 CFR 50.36 include the following categories: 1) safety limits, limiting safety systems settings and control settings;

2) limiting conditions for operation; 3) surveillance requirements; 4) design features; 5) administrative controls; 6) decommissioning; 7) initial notification; and 8) written reports.

HBRSEP Updated Final Safety Analysis Report (UFSAR) Section 3.1.2.6, "Reactor Core Design," states that "the reactor core with its related controls and protection systems shall be designed to function through its design lifetime without exceeding acceptable fuel damage limits which have been stipulated and justified." It also states that "the core and related auxiliary systems designs shall provide this integrity under all expected conditions of normal operation with appropriate margins for uncertainties and specified transient conditions which can be anticipated."

HBRSEP UFSAR Section 3.1.2.14, "Core Protection System," states that "core protection systems, together with associated equipment, shall be designed to prevent or to suppress conditions that could result in exceeding acceptable fuel damage limits."

The NRC staff reviewed the licensee TS changes request to ensure that the proposed changes are consistent with these UFSAR sections and provide reasonable assurance that the core protection systems would continue to be capable of performing their safety function and the acceptable fuel damage limits would not be exceeded.

3.0 TECHNICAL EVALUATION

HBRSEP UFSAR Section 15.0.7, "Trip Setpoints and Time Delays," states that the OTΔT reactor trip setpoint is designed to provide a 95-percent probability with a 95-percent confidence that neither bulk boiling in the Reactor Coolant System (RCS) hot-leg, nor departure from nucleate boiling (DNB) will occur during normal operation and design transients.

The equation of the OTΔT reactor trip settings is specified in TS Table 3.3.1-1 Note 1, "Overtemperture ΔT," which expresses the OTΔT reactor trip setpoints by the following four items:

- Item 1 is a preset adjustable value, K_1, independent of the process variables
- Item 2 includes the effects of temperature on the safety limits, and is compensated for instrumentation and piping delays
- Item 3 contains the effects of pressure on the safety limits, and
- Item 4 accounts for the effects of adverse power distribution, and is dependent on the axial flux difference

The TS changes will affect above Items 3 and 4. The NRC staff reviewed the proposed TS changes and provides its evaluation in subsections 3.1 and 3.2 for changes to Items 3 and 4, respectively.

3.1 TS Change for the Value of P' from < 2235 psig to > 2235 psig

The proposed change to TS 3.3.1, "Reactor Protection System Instrumentation," Table 3.3.1-1 Note 1 corrects the inequality symbol associated with the nominal RCS operating pressure (P'). The P' provided in Note 1 was incorrectly specified as less than or equal to (≤) 2235 pounds per square inch gage (psig) and is being corrected to greater than or equal to (≥) 2235 psig. HBRSEP was issued Improved Technical Specifications (ITSs) on October 24, 1997 (ADAMS Accession No. ML020560172). The improved Technical Specifications were based on NUREG-1431, "Standard Technical Specifications - Westinghouse Plants," Revision 0. This revision of NUREG-1431 included the typographical error in TS Table 3.3.1-1 Note 1 for OTΔT. The correction to the inequality symbol for P' from ≤ to ≥ was incorporated into NUREG-1431, Revisions 2 and 3.

The OTΔT trip function is provided to ensure that the DNB ratio (DNBR) is met. This trip function also limits the range over which the Overpower ΔT trip function must provide protection. The inputs to the OTΔT trip include all pressure, coolant temperature, axial power distribution, and reactor power as indicated by loop ΔT assuming full reactor coolant flow. Protection from violating the DNBR limit is assured for those transients that are slow with respect to delays from the core to the measurement system. The OTΔT function monitors both variation in power and flow since a decrease in flow has the same effect on ΔT as a power increase. The Overtemperature ΔT trip function uses each loop's ΔT as a measure of reactor power and is compared with a setpoint that is automatically varied with the following parameters:

- Reactor coolant average temperature - The OTΔT trip setpoint is varied to correct for changes in coolant density and specific heat capacity with changes in coolant temperature.

- Pressurizer pressure - The OTΔT trip setpoint is varied to correct for changes in system pressure.

- Axial power distribution - f(ΔI), The OTΔT trip setpoint is varied to account for imbalances in the axial power distribution as detected by the nuclear instrumentation system (NIS) upper and lower power range detectors. If axial peaks are greater than the design limit, as indicated by the difference between the upper and lower NIS power range detectors, the Trip Setpoint is reduced in accordance with Note 1 of Table 3.3.1-1.

HBRSEP TS 3.3.1, "Reactor Protection System Instrumentation," Table 3.3.1-1 Note 1 currently states:

> Note 1: Overtemperature ΔT
>
> The Overtemperature ΔT Function Allowable Value shall not exceed the following Nominal Trip Setpoint by more than 2.96% of ΔT span.
>
> $$\Delta T_{setpoint} \leq \Delta T_0 \{K_1 - K_2 \frac{(1+\tau_1 S)}{(1+\tau_2 S)}(T - T') + K_3 (P - P') - f(\Delta I)\}$$
>
> Where: ΔT_0 is the indicated ΔT at RTP, °F.

s is the Laplace transform operator, sec^{-1}.
T is the measured RCS average temperature, °F.
T' is the reference T_{avg} at RTP, ≤ 575.9°F.

P is the measured pressurizer pressure, psig
P' is the nominal RCS operating pressure, ≤ 2235 psig

$K_1 \leq 1.1265$ $K_2 = 0.01228/°F$ $K_3 = 0.00089/psig$
$\tau_1 \geq 20.08$ sec $\tau_2 \leq 3.08$ sec
$f(\Delta I) = 2.4\{(q_b - q_t) - 17\}$ when $q_t - q_b < -17\%$ RTP
0% of RTP when $-17\% \text{ RTP} \leq q_t - q_b \leq 12\%$ RTP
$2.4\{(q_t - q_b) - 12\}$ when $q_t - q_b > 12\%$ RTP

Where q_t and q_b are percent RTP in the upper and lower halves of the core, respectively, and $q_t + q_b$ is the total THERMAL POWER in percent RTP.

The HBRSEP UFSAR section 7.2.1.1.2.d, "Overtemperature ΔT Trip" states:

The purpose of this trip is to protect the core against DNB. This circuit trips the reactor on coincidence of two out of the three signals, with one set of temperature measurements per loop. The setpoint for this reactor trip is continuously calculated for each loop by solving the following equation:

$$\Delta T_{setpoint} \leq \Delta T_0 \{K_1 - K_2 \frac{(1+\tau_1 S)}{(1+\tau_2 S)}(T - T') + K_3 (P - P') - f(\Delta I)\}$$

Where: ΔT_0 = indicated ΔT at rated thermal power;
T = average temperature, °F;
P = pressurizer pressure, psig;
K_1 = set point bias (°F)
K_2, K_3 = constants based on the effect of temperature and pressure on the DNB limits, (°F/°F), (°F /psia)
$\frac{1+\tau_1 S}{1+\tau_2 S}$ = the function generated by the lead-lag controller for T_{avg} dynamic compensation;
τ_1 & τ_2 = time constants utilized in the lead-lag controller for T_{avg}
T' = reference T_{avg} at rated thermal power;
P' = nominal RCS Operating Pressure;
S = Laplace transform operator, sec^{-1};
and f(ΔI) is a function of the indicated difference between top and bottom detectors of the power--range nuclear ion chambers; with gains to be selected based on measured instrument response during plant start-up tests.

Values for each of the parameters are given in the TSs.

As indicated by the licensee in Section 3.0 of the application, the pressure basis for OTΔT reactor trip settings is a reference pressure (P' used in the equation of the OTΔT trip setpoints) of 2235 psig, which is also the RCS pressure used in the HBRSEP UFSAR Chapter 15 analyses. The proposed change to the value of P' from $\leq$ 2235 psig to $\geq$ 2235 psig will decrease the value of Item 3, K_3 (P-P'), in the equation for the OTΔT reactor trip setpoints. As a result, the OTΔT reactor trip setpoint will decrease, resulting in an earlier reactor trip, compared to that assumed in the Chapter 15 analyses. The resulting earlier reactor trip will limit the energy generated in the reactor and reduce the risk of bulk boiling in the RCS hot-leg and DNB occurrence of fuel damage during normal and design transients. Therefore, the revised value is conservative with respect to the HBRSEP UFSAR Section 15 analyses.

Based on the evaluation discussed above, the NRC staff finds that the proposed change to the inequality sign for P' from $\leq$ to $\geq$ is (1) consistent with the NUREG-1431, Revisions 2 and 3, and the STSs for Westinghouse plants (applicable to HBRSEP, a Westinghouse plant), and (2) conservative with respect to the OTΔT reactor trip setpoint assumed in the HBRSEP UFSAR Chapter 15 design transients analyses. Therefore, the NRC staff concludes that the change is acceptable.

3.2 TS Change for Value of 2.4 in f(ΔI) to 2.4%

In the existing TS for HBRSEP, Item 4 in the equation of the OTΔT reactor trip setpoints is expressed as follows:

$$f(\Delta I) = \begin{cases} 2.4\{(q_b - q_t) - 17\} & \text{when } q_t - q_b < -17\% \text{ Rated Thermal Power (RTP)} \\ 0\% \text{ of RTP} & \text{when } -17\% \text{ RTP} \leq q_t - q_b \leq 12\% \text{ RTP} \\ 2.4\{(q_t - q_b) - 12\} & \text{when } q_t - q_b > 12\% \text{ RTP} \end{cases}$$

Where q_t and q_b are percent RTP in the upper and lower halves of the core, respectively, and $(q_t + q_b)$ is the total thermal power in percent RTP.

The f(ΔI) penalty factor is to reduce OTΔT reactor trip setpoint to account for skewed axial power shape conditions. The proposed TS will change the value of 2.4 in the f(ΔI) penalty factor to 2.4 percent.

In Reference 1, the licensee stated that prior to ITS implementation, the custom TSs for HBRSEP expressed the f(ΔI) penalty factor as: "For each percent that the magnitude of $(q_t - q_b)$ exceeds 12 percent in a positive direction, the ΔT trip setpoint shall be automatically reduced by 2.4 percent of the value of ΔT at rated power (2300 MWt)." Similar expression was used for the f(ΔI) penalty when $(q_t - q_b)$ exceeds -17 percent in the negative direction. The licensee indicated that during the ITS conversion, the unit of percent associated with the 2.4 percent was dropped in adopting NUREG-1431, Revision 1, which did not express the f(ΔI) penalty factor as a percent.

During the review, the NRC staff found that in NUREG-1431, Revision 1, the first three items (K_1, K_2, and K_3 terms) on the right hand side of the equation of the OTΔT reactor trip setpoints are presented in fractions of full power units, and thus, finds that the f(ΔI) penalty factor (the fourth item) should be in the same units. Also, the OTΔT reactor trip setpoints in NUREG-1431, Revision 1 shows that for the region with no penalty applied (-17% RTP $\leq q_t - q_b \leq$ 12% RTP),

Accordingly, in applying NUREG-1431, Revision 1 to HBRSEP, the f(ΔI) penalty factor should be expressed as either a fractional 0.024 value, or 2.4 percent. The NRC staff found that the licensee proposed value of 2.4 percent is consistent with the requirement of the f(ΔI) penalty factor in the custom TSs for HBRSEP, and changing the value from 2.4 to 2.4 percent is consistent with the intent of NUREG-1431, Revision 1.

Further, the current TS Bases 3.3.1 states that "For every % that (q_b- q_t) exceeds 17%, the OTΔT setpoint is reduced by 2.4% and for every % that (q_t - q_b) exceeds 12%, OTΔT setpoint is reduced by 2.4%." The statement in the current TS Bases clarifies the use of the value of 2.4 percent for the f(ΔI) penalty factor.

Based on the discussion above, the NRC staff finds that the proposed TS changing the value of 2.4 in the f(ΔI) penalty factor to 2.4 percent is acceptable, because the TS change is consistent with (1) the requirement of the f(ΔI) penalty factor in the Custom TSs for HBRSEP, (2) the intent of NUREG-1431, Revision 1 regarding use of the unit in the f(ΔI) penalty factor, and (3) the clarification in current TS Bases 3.3.1 for the expression of the f(ΔI) penalty factor.

The NRC staff also reviewed the information in the August 16, 2012, letter providing the bases for the K_2 and K_3 used in the equation of the OTΔT trip setpoints. The NRC staff finds that the proposed TS maintaining the equality sign (=) unchanged for both the K_2 and K_3 constants is acceptable, because the proposed TS (1) provides reasonable assurance that the core protection systems would continue to perform their safety functions consistent with the current HBRSEP UFSAR analysis, and (2) is consistent with the corresponding TSs for similar Westinghouse plants.

3.3 Conclusion

The NRC staff reviewed the proposed TS and finds that: 1) the proposed change to the inequality sign for P' from $\leq$ to $\geq$ is conservative with respect to the OTΔT reactor trip setpoints assumed in the HBRSEP UFSAR Chapter 15 analyses; 2) the proposed TS revision that changes the value of 2.4 in the f(ΔI) penalty factor to 2.4 percent is consistent with the requirement of the f(ΔI) penalty factor in the original custom TS for HBRSEP, and the clarification presented in the current TS Bases 3.3.1 for the OTΔT trip setpoints; and 3) the proposed TS that maintains the equality sign (=) unchanged for both the K_2 and K_3 constants in the equation of the OTΔT trip setpoints, is consistent with the current HBRSEP licensing basis. Therefore, the NRC staff concludes that the proposed TS revisions provides reasonable assurance that the core protection systems (including the OTΔT trip) would continue to be capable of performing their safety function in avoiding fuel damage, meeting the requirements of UFSAR Sections 3.1.2.6, "Reactor Core Design" and 3.1.2.14, "Core Protection Systems," therefore the TS changes are acceptable.

4.0 STATE CONSULTATION

In accordance with the Commission's regulations, the State of South Carolina official was notified of the proposed issuance of the amendment. The State official had no comments.

5.0 ENVIRONMENTAL CONSIDERATION

The amendments change a requirement with respect to installation or use of a facility component located within the restricted area as defined in 10 CFR Part 20. The NRC staff has determined that the amendment involves no significant increase in the amounts, and no significant change in the types, of any effluents that may be released offsite, and that there is no significant increase in individual or cumulative occupational radiation exposure. The Commission has previously issued a proposed finding that the amendment involves no significant hazards consideration, and there has been no public comment on such finding (77 FR 22811). Accordingly, the amendment meets the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9). Pursuant to 10 CFR 51.22(b), no environmental impact statement or environmental assessment need be prepared in connection with the issuance of the amendment.

6.0 CONCLUSION

The Commission has concluded, based on the considerations discussed above, that (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) there is reasonable assurance that there is reasonable assurance that such activities will be conducted in compliance with the Commission's regulations, and (3) the issuance of the amendment will not be inimical to the common defense and security or to the health and safety of the public.

Principal Contributors: K. Bucholtz
S. Sun

Date: February 13, 2013

February 13, 2013

Mr. William G. Gideon, Vice President
H. B. Robinson Steam Electric Plant
Carolina Power & Light Company
3581 West Entrance Road
Hartsville, SC 29550

SUBJECT: H. B. ROBINSON STEAM ELECTRIC PLANT, UNIT NO. 2 - ISSUANCE OF AN AMENDMENT ON TECHNICAL SPECIFICATION CHANGE REGARDING CORRECTIONS TO TABLE 3.3.1-1 NOTE 1 (TAC NO. ME8225)

Dear Mr. Gideon:

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The amendment changes HBRSEP TS Table 3.3.1-1 for Overtemperature Delta Temperature to be consistent with NUREG-1431, Revision 3, "Standard Technical Specifications - Westinghouse Plants."

A copy of the related Safety Evaluation is enclosed. Notice of Issuance will be included in the Commission's biweekly *Federal Register* notice.

Sincerely,

/RA/

Araceli T. Billoch Colón, Project Manager
Plant Licensing Branch II-2
Division of Operating Reactor Licensing
Office of Nuclear Reactor Regulation

Docket No. 50-261
Enclosures:
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ADAMS Accession No.: ML13014A641 *** Via Memo**

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