

WOLF CREEK

NUCLEAR OPERATING CORPORATION

December 20, 2012

John P. Broschak
Vice President Engineering

ET 12-0033

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555

- Reference:
- 1) Letter ET 10-0026, dated September 22, 2010, from T. J. Garrett, WCNOG, to USNRC
 - 2) Letter ET 10-0031, dated November 22, 2010, from T. J. Garrett, WCNOG to USNRC
 - 3) Letter dated May 24, 2011, from J. R. Hall, USNRC, to M. W. Sunseri, WCNOG, "Wolf Creek Generating Station – Request for Additional Information Regarding License Amendment Request to Revise the Fire Protection Program (TAC NO. ME4757)"
 - 4) Letter ET 11-0005, dated June 30, 2011, from R. P. Clemens, WCNOG to USNRC

Subject: Docket No. 50-482: License Amendment Request (LAR) for Deviation from Fire Protection Requirements

Gentlemen:

Pursuant to 10 CFR 50.90, "Application for amendment of license, construction permit, or early site permit," and 10 CFR 50.91, "Notice for public comment; State consultation," Wolf Creek Nuclear Operating Corporation (WCNOG) hereby requests an amendment to the Renewed Facility Operating License No. NPF-42 for the Wolf Creek Generating Station (WCGS). This license amendment request (LAR) is seeking approval by the Commission, pursuant to License Condition 2.C.(5), to make changes to the approved fire protection program as described in the Updated Safety Analysis Report (USAR).

A006
MRR

The proposed changes to the approved fire protection program are based on the Reactor Coolant System (RCS) thermal-hydraulic response (Evaluation SA-08-006) for a postulated control room fire performed for changes to the alternative shutdown methodology outlined in letter SLNRC 84-0109, "Fire Protection Review." Drawing E-1F9915, "Design Basis Document for OFN RP-017, Control Room Evacuation," Revision 4, and Evaluation SA-08-006, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 3, demonstrate the adequacy of the revised alternative shutdown procedure, OFN RP-017. The results of the RCS thermal-hydraulic response identified required changes to the fire protection program as follows:

1. Deviation from the 10 CFR 50, Appendix R, Section III.L.1 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining RCS process variables within those predicted for a loss of normal AC power.
2. Deviation from the 10 CFR 50, Appendix R, Section III.L.2 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining pressurizer level on scale.
3. Revision to USAR Appendix 9.5B include incorporation of drawing E-1F9915 and a deviation from Calculation XX-E-013. Deviation from Calculation XX-E-013, Revision 2, "Post-Fire Safe Shutdown (PFSSD) Analysis," Assumption 3-A-4 regarding application of loss of automatic functions, specific to automatic feedwater isolation in the event of a control room fire. Calculation XX-E-013 is incorporated by reference in USAR Appendix 9.5B, "Fire Hazards Analyses."

Attachment I provides the evaluation and justification for the proposed license amendment. Attachment II provides a markup of License Condition 2.C.(5) reflecting the issuance of an amendment to the license condition. Attachment III provides markups of the USAR including Appendix 9.5B and 9.5E. USAR Appendix 9.5E provides a design comparison to 10 CFR 50 Appendix R. Attachment IV provides markups of the changes to Calculation XX-E-013. Attachment V provides a drawing of the control room layout. The Enclosure provides a copy of drawing E-1F9915, Revision 4.

Reference 1 provided WCNOC's LAR to make changes to the approved fire protection program as described in the WCGS USAR. Specifically, a revision to USAR Table 9.5E-1 was proposed to include information on RCS process variables not maintained within those predicted for a loss of normal AC power as evaluated in Evaluation SA-08-006, Revision 1. Reference 2 provided supplemental information necessary to enable the Nuclear Regulatory Commission (NRC) staff to make an independent assessment regarding the acceptability of the proposed amendment. Reference 3 provided a request for additional information related to the LAR. In preparing the information to support a response to Reference 3, further review of Evaluation SA-08-006, Revision 1, identified a number of discrepancies with the assumptions utilized. Based on these discrepancies, Reference 4 withdrew that LAR.

It has been determined that this amendment application does not involve a significant hazard consideration as determined per 10 CFR 50.92 "Issuance of amendment." Pursuant to 10 CFR 51.22, "Criterion for categorical exclusion; identification of licensing and regulatory actions eligible for categorical exclusion or otherwise not requiring environmental review," Section (b),

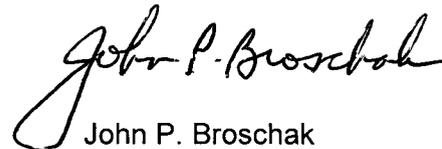
no environmental impact statement or environmental assessment needs to be prepared in connection with the issuance of this amendment.

The amendment application was reviewed by the WCNOG Plant Safety Review Committee. In accordance with 10 CFR 50.91, a copy of this application is being provided to the designated Kansas State official.

WCNOG requests approval of this proposed amendment by December 31, 2013. Once approved, the amendment will be implemented within 90 days of issuance.

This letter contains no commitments. If you have any questions concerning this matter, please contact me at (620) 364-4085, or Mr. Michael J. Westman at (620) 364-8831 ext. 4009.

Sincerely,



John P. Broschak

JPB/rit

Attachment I - Evaluation of Proposed Change
Attachment II - Markup of Renewed Facility Operating License
Attachment III - Markup of USAR Pages
Attachment IV - Markup of Calculation XX-E-013
Attachment V - Control Room Layout

Enclosure Drawing E-1F9915, Revision 4, "Design Basis Document for OFN RP-017, Control Room Evacuation"

cc: E. E. Collins (NRC), w/a, w/e
T. A. Conley (KDHE), w/a, w/e
C. F. Lyon (NRC), w/a, w/e
N. F. O'Keefe (NRC), w/a, w/e
Senior Resident Inspector (NRC), w/a, w/e

STATE OF KANSAS)
) SS
COUNTY OF COFFEY)

John P. Broschak, of lawful age, being first duly sworn upon oath says that he is Vice President Engineering of Wolf Creek Nuclear Operating Corporation; that he has read the foregoing document and knows the contents thereof; that he has executed the same for and on behalf of said Corporation with full power and authority to do so; and that the facts therein stated are true and correct to the best of his knowledge, information and belief.

By John P. Broschak
John P. Broschak
Vice President Engineering

SUBSCRIBED and sworn to before me this 20th day of December, 2012.

Gayle Shepherd
Notary Public



Expiration Date 7/24/2015

Evaluation of Proposed Change

Subject: License Amendment Request (LAR) for Deviation from Fire Protection Requirements

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EVALUATION

1. SUMMARY DESCRIPTION

The proposed amendment request is requesting Nuclear Regulatory Commission (NRC) approval, pursuant to License Condition 2.C.(5), to make changes to the approved fire protection program as described in the Updated Safety Analysis Report (USAR). This evaluation supports a request to amend Renewed Facility Operating License NPF-42 for the Wolf Creek Generating Station (WCGS). The proposed changes to the approved fire protection program are based on the Reactor Coolant System (RCS) thermal-hydraulic response (Evaluation SA-08-006) for a postulated control room fire performed for changes to the alternative shutdown methodology outlined in letter SLNRC 84-0109 (Reference 1), "Fire Protection Review." Drawing E-1F9915 (Reference 2), "Design Basis Document for OFN RP-017, Control Room Evacuation," Revision 4, and Evaluation SA-08-006 (Reference 3), "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 3, demonstrate the adequacy of the revised alternative shutdown procedure, OFN RP-017 (Reference 4). The results of the RCS thermal-hydraulic response identified required changes to the fire protection program as follows:

- Deviation from the 10 CFR 50, Appendix R, Section III.L.1 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining RCS process variables within those predicted for a loss of normal AC power.
- Deviation from the 10 CFR 50, Appendix R, Section III.L.2 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining pressurizer level on scale.
- Revision to USAR Appendix 9.5B to include incorporation of drawing E-1F9915 and a deviation from Calculation XX-E-013. Deviation from Calculation XX-E-013 (Reference 5), Revision 2, "Post-Fire Safe Shutdown (PFSSD) Analysis," Assumption 3-A-4 regarding application of loss of automatic functions, specific to automatic feedwater isolation in the event of a control room fire. Calculation XX-E-013 is incorporated by reference in USAR Appendix 9.5B, "Fire Hazards Analyses."

The proposed changes have been determined to adversely affect the ability to achieve and maintain safe shutdown in the event of a fire. Therefore, prior Commission approval is required as Section III.L.1 and Section III.L.2 of Appendix R is not directly satisfied.

2. DETAILED DESCRIPTION

This amendment application contains a proposed change to the Renewed Facility Operating License and changes to the fire protection program as described in the USAR.

2.1 Proposed changes to License Condition 2.C.(5)

License Condition 2.C.(5)(a) currently states:

- (a) The Operating Corporation shall maintain in effect all provisions of the approved fire protection program as described in the SNUPPS Final Safety Analysis Report for the facility through Revision 17, the Wolf Creek site addendum through Revision 15, as approved in the SER through Supplement 5, Amendment No. 191, and Amendment No. 193 subject to provisions b and c below.

License Condition 2.C.(5)(a) is revised to state:

- (a) The Operating Corporation shall maintain in effect all provisions of the approved fire protection program as described in the SNUPPS Final Safety Analysis Report for the facility through Revision 17, the Wolf Creek site addendum through Revision 15, as approved in the SER through Supplement 5, Amendment No. 191, Amendment No. 193, and Amendment No. XXX subject to provisions b and c below.

The proposed change reflects the approved fire protection program based on the issuance of the license amendment approving the proposed change. The amendment number will be reflected in the license condition upon the issuance of the amendment.

2.2 Proposed Change to USAR Appendix 9.5E, Response to Section III.L.1.

The WCGS response to Section III.L.1 in USAR Table 9.5E-1 (Sheet 25), is revised by adding the following statement:

The performance criteria of III.L.1 are satisfied, with the exception of maintaining reactor process variables within those predicted for a loss of normal ac power. This is acceptable, as long as a control room fire will not result in the plant reaching an unrecoverable condition, which could lead to core damage. The criteria for "not reaching an unrecoverable condition" are that 1) natural circulation is maintained, and 2) adequate core cooling is maintained (average hot leg temperature remains at or below normal full power temperature ~630°F).

2.3 Proposed Change to USAR Appendix 9.5E, Response to Section III.L.2

The WCGS response to Section III.L.2 in USAR Table 9.5E-1 (Sheet 25), is revised by adding the following statement:

In general, the performance goals of III.L.2 are satisfied except that in some cases pressurizer water level is not maintained within level indication. This is acceptable since the evaluation demonstrates that unrecoverable conditions are not reached.

2.4 Proposed Change to Calculation XX-E-013 (USAR Appendix 9.5B)

Calculation XX-E-013, Assumption 3-A-4 currently states:

For fire in areas requiring alternative shutdown capability (i.e., where control room evacuation may be necessary), a loss of automatic functions is assumed. For example, in the event of a loss of offsite power the emergency diesel generators will normally start automatically on undervoltage. However, in developing the alternative shutdown, capability of this automatic feature to operate is not assumed.

Basis: NRC Generic Letter 86-10, Response to Question 3.8.1; NEI 00-01, Rev. 2, Paragraph 3.3.1.1.4.1

Assumption 3-A-4 is revised as follows:

For a fire in areas requiring alternative shutdown capability (i.e., control room), loss of automatic function of valves and pumps with control circuits that could be affected by a control room fire is assumed, except that an automatic feedwater isolation signal (FWIS) is unaffected by a fire in the control room.

Basis: NRC Generic Letter 86-10, Response to Question 3.8.4; NEI 00-01, Rev. 2, Paragraph 3.3.1.1.4.1; License Amendment XXX (amendment number to be incorporated based on NRC approval of this application)

3. TECHNICAL EVALUATION

Letter SLNRC 84-0109 is the original response strategy for shutting down the plant and maintaining a safe hot standby condition from outside the control room in the event of a fire in the control room. This letter is part of the approved fire protection program because the response strategy is described, in detail, in NUREG 0881 Supplement 5, "Safety Evaluation Report related to the operation of the Wolf Creek Generating Station Unit No. 1," (Reference 6), Section 9.5.1.5. However, there was no technical basis supporting the actions and response times. The strategy was developed based on operator knowledge and experience at the time.

Procedure OFN RP-017 implements the response plan for fire in the control room but differs from letter SLNRC 84-0109 and the response strategy in NUREG 0881 Supplement 5. The technical basis for the response plan in OFN RP-017 is documented in drawing E-1F9915, "Design Basis Document for OFN RP-017, Control Room Evacuation," Revision 4. This drawing, along with various inputs, provides the technical basis for each action step and response time in the procedure and shows that the plant can be safely brought to a hot standby condition using procedure OFN RP-017.

WCNOC proposes to establish drawing E-1F9915 as the new license basis for the procedure OFN RP-017 for shutting down the plant from outside the control room in case of a fire. Drawing E-1F9915 maintains the original philosophical approach for achieving and maintaining safe shutdown as discussed in letter SLNRC 84-0109 by manually manipulating equipment per an approved procedure. The procedure directs operators to take actions, regardless of the status of plant equipment, to avoid or mitigate undesirable events.

The approved fire protection program is revised to modify the response strategy described in NUREG 0881 Supplement 5 to the response strategy described in drawing E-1F9915. The response strategy is encompassed in procedure OFN RP-017 with the technical basis provided in drawing E-1F9915.

Additionally, as a result of the development of drawing E-1F9915 and supporting evaluation, it has been identified that some requirements of Section III.L of Appendix R are not met. WCNOG proposes to revise USAR Table 9.5E-1 to document the deviations from the requirements of Appendix R. The proposed changes have been determined to adversely affect the ability to achieve and maintain safe shutdown in the event of a fire. Therefore, prior Commission approval is required as Section III.L.1 and Section III.L.2 of Appendix R are not directly satisfied.

Design Basis Function

The post-fire safe shutdown design basis for WCGS is the cold shutdown operational mode (Mode 5). In the event that a fire occurs in the plant, which is determined to warrant the plant being brought to a cold, depressurized condition, the plant will be taken immediately to a hot standby condition and then taken to cold shutdown. The time to achieve cold shutdown is 72 hours for control room fires. For fires outside the control room, repairs to cold shutdown equipment need to be made within 72 hours.

10 CFR 50 Appendix R, Section III.L, "Alternative and dedicated shutdown capability," specifies that alternative or dedicated shutdown capability provided for a specific fire area shall be able to:

- (a) achieve and maintain subcritical reactivity conditions in the reactor;
- (b) maintain reactor coolant inventory;
- (c) achieve and maintain hot standby conditions for a PWR
- (d) achieve cold shutdown conditions within 72 hours; and
- (e) maintain cold shutdown conditions thereafter.

In order to meet the above criteria, the following functions must be available following any fire in the plant:

- 1. reactivity control function;
- 2. reactor inventory makeup function; and
- 3. decay heat removal function.

Associated with the above functions is process monitoring instrumentation and other support systems needed to make the function available.

Background

The WCGS USAR, Appendix 9.5E, provides a comparison of the WCGS Fire Protection Program against the requirements of Section III of Appendix R to 10 CFR 50. Although WCGS obtained its operating license after January 1, 1979, the NRC stated, in NUREG 0881 (Reference 7), "Safety Evaluation Report related to the operation of Wolf Creek Generating Station, Unit No. 1,"

that they will condition the WCGS operating license to require WCGS to meet the technical requirements of Appendix R to 10 CFR 50, or provide equivalent protection. However, the license condition never appeared in the WCGS full power operating license when it was issued on June 4, 1985. Therefore, although Appendix R does not apply, WCGS's commitment to Appendix R is established in Appendix 9.5E as part of the approved fire protection program documented in the USAR.

During an NRC audit of fire protection during the week of July 30, 1984 assumptions applied in the control room fire hazards analysis were questioned. The concern resulted in meetings involving Standardized Nuclear Unit Power Plant System (SNUPPS), WCGS, Callaway Plant, and the NRC in August 1984 to resolve the issues. Meetings were on August 10, 14, 15, and 22. As a result of the meetings, SNUPPS developed letter SLNRC 84-0109 (Reference 1) which documented the SNUPPS "Response Plan for Immediate Evacuation of the Control Room Due to Fire." Letter SLNRC 84-109 addressed spurious actuations and established Phases A through F actions to be taken to mitigate the consequences of a fire in the control room.

After the 2005 NRC triennial fire protection inspection, significant changes to the alternative shutdown methodology were implemented in procedure OFN RP-017. Additionally, drawing E-1F9915, Revision 0, and Evaluation SA-08-006, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 0, were developed to demonstrate the adequacy of the revised alternative shutdown procedure. These evaluations predicted that a fire in the control room, which led to control room abandonment and caused a single pressurizer power operated relief valve (PORV) to spuriously open, could cause a steam bubble and subsequent void in the reactor vessel head. USAR Table 9.5E-1 was revised to include the following paragraph:

Analysis demonstrates that the performance goals of III.L.2 are satisfied. The performance criteria of III.L.1 are also satisfied, with the exception of maintaining reactor process variables within those predicted for a loss of normal ac power. This is acceptable, as long as a control room fire will not result in the plant reaching an unrecoverable condition, which could lead to core damage.

During the 2008 NRC triennial fire protection inspection, the team identified an unresolved item related to this change to the fire protection program. The team was concerned that the licensee changed the fire protection program in a manner that could adversely affect the ability to achieve and maintain safe shutdown in the event of a fire without prior NRC approval. Subsequently, the NRC identified this as noncited violation 05000482/2009004-08 (Reference 8).

In response to the NRC finding, WCNOG submitted a license amendment request (Reference 12) to make changes to the approved fire protection program as described in the WCGS USAR. Specifically, a revision to USAR Table 9.5E-1 was proposed to include information on RCS process variables not maintained within those predicted for a loss of normal AC power as evaluated in Evaluation SA-08-006, Revision 1. WCNOG letter ET 10-0031 (Reference 13) provided supplemental information necessary to enable the NRC staff to make an independent assessment regarding the acceptability of the proposed amendment. On May 24, 2011, a request for additional information (Reference 14) was issued related to the amendment request. In preparing the information to support a response to request for additional information, further review of Evaluation SA-08-006, Revision 1, identified a number of discrepancies with the assumptions utilized. Based on these discrepancies, WCNOG letter ET 11-0005 withdrew the license amendment request.

WCGS Fire Protection Program License Basis

The WCGS fire protection program license basis for alternative shutdown can be found in the following documents:

1. WCGS Renewed Facility Operating License NPF-42, Condition 2.C.(5), Fire Protection,
2. NUREG 0881 Supplement No. 5, and
3. WCGS USAR, Section 9.5.1, Appendix 9.5B, and Appendix 9.5E.

WCGS Renewed Facility Operating License NPF-42, Section 2.C.(5) conditions the operating license as follows regarding fire protection:

(5) Fire Protection (Section 9.5.1, SER, Section 9.5.1.8, SSER #5)

- (a) The Operating Corporation shall maintain in effect all provisions of the approved fire protection program as described in the SNUPPS Final Safety Analysis Report for the facility through Revision 17, the Wolf Creek site addendum through Revision 15, and as approved in the SER through Supplement 5, Amendment No. 191, and Amendment No. 193 subject to provisions b and c below.
- (b) The licensee may make changes to the approved fire protection program without prior approval of the Commission only if those changes would not adversely affect the ability to achieve and maintain safe shutdown in the event of a fire.
- (c) Deleted

The changes described herein adversely affect the ability to achieve and maintain safe shutdown in the event of a fire and, therefore, prior Commission approval is required.

NUREG 0881 (referred to as SER), Section 9.5.1.7, states the following regarding compliance with 10 CFR 50, Appendix R:

"9.5.1.7 Appendix R Statement

On October 27, 1980, the Commission approved a rule concerning fire protection. Although this rule and its Appendix R are not directly applicable to Wolf Creek, the requirements set forth in Appendix R are being used as guidelines in licensing plants after January 1, 1979. On April 27, 1981, the Commission required that Operating Licenses issued after January 1, 1979, contain a condition requiring compliance with commitments made by an applicant and agreed to by the staff after differences between the applicant's program and the guidelines set forth in Appendix A to BTP 9.5-1 and Appendix R to 10 CFR 50 have been identified and evaluated.

The applicant has provided in the FSAR an evaluation of how he meets Appendix R and identified any exceptions. The staff is continuing to review the information. The staff will

condition the operating license to require the applicant to meet the technical requirements of Appendix R to 10 CFR 50, or provide equivalent protection."

Although the fire protection conditions in Section 2.C.(5) were not revised to include a specific Appendix R license condition, Section 2.C.(5)(a) references the SER, through Supplement 5 and, therefore, the above SER statement is considered a license condition by reference.

3.1 Proposed Change to License Condition 2.C.(5)

The proposed change reflects the approved fire protection program based on the issuance of the license amendment approving the proposed change. The amendment number will be reflected in the license condition upon the issuance of the amendment.

3.2 Proposed Change to USAR Appendix 9.5E, Response to Section III.L.1

Appendix R, Section III.L.1 states the following:

"Alternative or dedicated shutdown capability provided for a specific fire area shall be able to (a) achieve and maintain subcritical reactivity conditions in the reactor; (b) maintain reactor coolant inventory; (c) achieve and maintain hot standby² conditions for a PWR (hot shutdown² for a BWR); (d) achieve cold shutdown conditions within 72 hours; and (e) maintain cold shutdown conditions thereafter. During the postfire shutdown, the reactor coolant system process variables shall be maintained within those predicted for a loss of normal AC power, and the fission product boundary integrity shall not be affected; i.e., there shall be no fuel clad damage, rupture of any primary coolant boundary, or rupture of the containment boundary.

²As defined in the Standard Technical Specifications."

One of the requirements listed in Appendix R, Section III.L.1 is that the process variables shall be maintained within those predicted for a loss of normal AC power. This general requirement may not be met for all transients for two reasons:

- 1) Some of the transients evaluated have off-site power available and do not represent the transient characteristics of a normal loss of AC power.
- 2) The PFSSD analysis assumes a loss of off-site power in some scenarios coupled with one spurious operation (failure) and no automatic actuation of safety components. These two additional conservative assumptions ensure the transient will be more severe than a loss of normal AC power.

Thus, the response of the process variables to these accident conditions cannot be bounded by the loss of normal AC transient results. However, in all scenarios, adequate core cooling is maintained, natural circulation flow through the core is maintained, and the plant reaches safe shutdown conditions.

3.3 Proposed Change to USAR Appendix 9.5E, Response to Section III.L.2

Appendix R, Section III.L.2 states the following:

"The performance goals for the shutdown functions shall be:

- a. The reactivity control function shall be capable of achieving and maintaining cold shutdown reactivity conditions.
- b. The reactor coolant makeup function shall be capable of maintaining the reactor coolant level above the top of the core for BWRs and be within the level indication in the pressurizer for PWRs.
- c. The reactor heat removal function shall be capable of achieving and maintaining decay heat removal.
- d. The process monitoring function shall be capable of providing direct readings of the process variables necessary to perform and control the above functions.
- e. The supporting functions shall be capable of providing the process cooling, lubrication, etc., necessary to permit the operation of the equipment used for safe shutdown functions."

Evaluation SA-08-006, Revision 3, demonstrates that the performance goals of Appendix R, Section III.L.2, are generally satisfied. Section 3.5 provides the results of Evaluation SA-08-006. In one evaluated event (Scenario 3A), pressurizer water level is not maintained within level indication as required by Section III.L.2.b. This is acceptable since the evaluation demonstrates natural circulation is maintained and adequate core cooling is maintained. As such, an unrecoverable condition is not reached.

3.4 Revision to USAR Appendix 9.5B

USAR Appendix 9.5B is being revised to include incorporation of drawing E-1F9915 and a deviation from Calculation XX-E-013. Incorporation of drawing E-1F9915 into USAR Appendix 9.5B incorporates the revised alternate shutdown methodology into the fire protection program.

Calculation XX-E-013, Revision 2, Assumption 3-A-4 states:

"For fire in areas requiring alternative shutdown capability (i.e., where control room evacuation may be necessary), a loss of automatic functions is assumed. For example, in the event of a loss of offsite power the emergency diesel generators will normally start automatically on undervoltage. However, in developing the alternative shutdown, capability of this automatic feature to operate is not assumed.

Basis: NRC Generic Letter 86-10, Response to Question 3.8.1; NEI 00-01, Rev. 2, Paragraph 3.3.1.1.4.1"

Contrary to this assumption, Evaluation SA-08-006 assumes that an automatic feedwater isolation signal (FWIS) will occur in response to a reactor trip with low T_{avg} or abnormal steam generator level. As a result of a non-cited violation documented in the 2011 NRC Triennial Fire

Protection Inspection Report 05000482/2011007 (Reference 9), the WCGS fire protection program cannot take sole credit for main steam isolation valve (MSIV) closure using the hand switches in the main control room. Closing the MSIVs stops main steam flow to the feedwater pump turbines and stops the main feedwater pumps. However, with the main feedwater pumps continuing to operate, the steam generators overfill in a matter of minutes, which is insufficient time for operators to take action to stop the pumps. Therefore, WCNOG requests a deviation to credit the automatic FWIS for closure of the feedwater isolation valves to stop main feedwater flow and prevent steam generator overfill. The basis for acceptance of this deviation is discussed below.

A FWIS occurs on one of the following signals:

- Reactor Trip with 2/4 Low T_{avg} (564°F)
- 2/4 Hi-Hi (78 %) Steam Generator Level on 1/4 Steam Generators
- 2/4 Lo-Lo (23½ %) Steam Generator Level on 1/4 Steam Generators
- Safety Injection Signal (SIS)

The control room cabinets that contain controls associated with the FWIS are:

- SB038 – Protection Set I
- SB042 – Protection Set II
- SB037 – Protection Set III
- SB041 – Protection Set IV
- SB029A/B/C – Train A Solid State Protection System (SSPS)
- SB030A/B – Train A SSPS Test Cabinet
- SB032A/B/C – Train B SSPS
- SB033A/B - Train B SSPS Test Cabinet

RCS temperature is monitored by the following temperature elements:

- Loop 1 – BBTE0411B (Cold Leg), BBTE0411A1 (Hot Leg), BBTE0411A2 (Hot Leg) and BBTE0411A3 (Hot Leg)
- Loop 2 – BBTE0421B (Cold Leg), BBTE0421A1 (Hot Leg), BBTE0421A2 (Hot Leg) and BBTE0421A3 (Hot Leg)
- Loop 3 – BBTE0430B (Cold Leg), BBTE0431A1 (Hot Leg), BBTE0431A2 (Hot Leg) and BBTE0431A3 (Hot Leg)
- Loop 4 – BBTE0441B (Cold Leg), BBTE0441A1 (Hot Leg), BBTE0441A2 (Hot Leg) and BBTE0441A3 (Hot Leg)

Signals from these temperature elements are processed in the applicable protection cabinet for that loop (SB038 – Loop 1, SB042 – Loop 2, SB037 – Loop 3, SB041 – Loop 4). The average temperature of each loop is calculated within the protection cabinet and the output is sent to both trains of SSPS cabinets (SB029A/B/C – Train A and SB032A/B/C – Train B). Low T_{avg} on two out of four loops coincident with a reactor trip generates a FWIS.

A credible fire in the control room could affect two of the four protection cabinets or one of the SSPS sets based on the control room layout (see Attachment V for the control room layout). The remaining two protection cabinets and remaining SSPS set would be unaffected by the fire. Therefore, a FWIS would be generated in the event of a reactor trip with Low T_{avg} on 2/4 loops and the feedwater isolation valves close.

Steam generator (SG) level is monitored by the following level instruments:

- SG 'A' - AELT0517, AELT0518, AELT0519, AELT0551
- SG 'B' - AELT0527, AELT0528, AELT0529, AELT0552
- SG 'C' - AELT0537, AELT0538, AELT0539, AELT0553
- SG 'D' - AELT0547, AELT0548, AELT0549, AELT0554

Signals from AELT0551, AELT0529, AELT0539 and AELT0554 are processed in Protection Set I cabinet SB038.

Signals from AELT0519, AELT0552, AELT0553 and AELT0549 are processed in Protection Set II cabinet SB042.

Signals from AELT0518, AELT0528, AELT0538 and AELT0548 are processed in Protection Set III cabinet SB037.

Signals from AELT0517, AELT0527, AELT0537 and AELT0547 are processed in Protection Set IV cabinet SB041.

Each protection cabinet sends an output signal to both trains of SSPS cabinets (SB029A/B/C – Train A and SB032A/B/C – Train B). Loss of 1 train of protection cabinets or 1 train of SSPS cabinets would not prevent a FWIS on Hi-Hi or Lo-Lo SG level. Based on the control room layout, these cabinets have physical separation that would prevent a credible fire from affecting both trains. Therefore, there is reasonable assurance that a credible fire in the control room will not affect both trains of SG level FWIS.

The physical separation between redundant divisions of FWIS circuits in the control room meets the requirements of IEEE 384-1974. The NRC in Regulatory Guide 1.75, "Physical Independence of Electrical Systems," dated September 1978, has endorsed this standard. The physical separation provides reasonable assurance that a single spurious operation or signal due to a fire will not affect both divisions of FWIS and that one division of FWIS will remain available to isolate feedwater upon receipt of one of the four feedwater isolation signals.

Control Room Cabinet Fire Testing

Fire tests of representative samples of control room cabinets were conducted in the mid-1980s and the results are reported in NUREG/CR-4527 (Reference 16), "An Experimental Investigation of Internally Ignited Fires in Nuclear Power Plant Control Cabinets: Part 1: Cabinet Effects Tests." The results of this test program show that severe fires in vertical control cabinets will not spread to adjacent cabinets where IEEE-383 qualified and unqualified cable is used and where the cabinets are separated only by the metal enclosure of each cabinet forming a double wall metal barrier. In these tests, the cabinets were placed side-by-side leaving only a 1-inch air gap between cabinets.

The following observation was made in NUREG/CR-4527 regarding test Preliminary Cabinet Test (PCT) #2:

"PCT #2 demonstrated that for a vertical cabinet with open doors and with an in situ fuel loading of unqualified cable that appears similar to real fuel loadings in nuclear power plants, the fire will develop and spread rapidly throughout the burning cabinet. However,

even a fire as large as this did not have a significant thermal effect (i.e. temperature rise that could result in melting of cables or components) on the adjacent cabinets in the configuration tested."

During PCT #2, thermocouple readings inside the test cabinet reached as high as 1,742°F, whereas the adjacent cabinet wall temperature only reached 536°F. The air temperature inside the adjacent cabinet reached 180°F. IEEE-383 qualified cable has a damage threshold of approximately 700°F. Therefore, the temperatures experienced in the adjacent cabinet would not have been sufficient to damage the cables in that cabinet.

It should be noted that PCT #2 was performed with the cabinet doors open, which results in a higher heat release rate (HRR) than with the doors closed. This represents the most severe condition for the test. At WCGS, the cabinet doors are not open during normal operation and are alarmed to alert operators of them being opened. Also, WCGS uses IEEE-383 qualified cable, which resulted in a much lower fire severity when compared to the tests that used unqualified cable. Test PCT #3 studied the effects of a control cabinet fire that uses IEEE-383 qualified cable. The following observation was made regarding this test:

"Preliminary Cabinet Test #3 again showed that a cabinet fire in a vertical cabinet with qualified cable has little potential to propagate and spread throughout a single vertical cabinet. ... with the in situ fuel and configurations tested, a fire in a vertical cabinet with qualified cable is not likely to propagate or result in damage to cable components or equipment outside the cabinet as a result of the thermal environment."

During PCT #3, thermocouple readings were much lower than in test PCT #2. Inside the test cabinet, the air temperature only reached 423°F and the adjacent cabinet wall temperature only reached about 212°F. The air temperature inside the adjacent cabinet reached 140°F. Therefore, the temperatures experienced in the adjacent cabinet were not sufficient to damage the cables in that cabinet.

The test results in NUREG/CR-4527 provide valuable insight for the control room fire scenario discussed in this evaluation. The test results clearly show that under the test configuration studied, a severe fire in one cabinet will not propagate to adjacent cabinets as long as there is at least a double wall metal barrier and 1-inch air gap between the cabinets. It is reasonable to conclude that additional spatial separation further reduces the potential for thermal propagation between cabinets.

The ignition source used in most of the tests was a 2.5 gallon polyethylene bucket containing a 16 oz box of kimwipes and 1 quart of acetone. Some of the kimwipes were crumpled and placed in the bucket and some of the acetone was dumped into the bottom of the bucket to represent a spill. The total heat content of the ignition source was about 68,500 BTUs. This ignition source is extreme compared to the conditions present at WCGS. Administrative controls are in place to prevent the presence of this fuel load inside control room cabinets at WCGS. The only ignition sources inside these cabinets are the IEEE-383 qualified cables that terminate in the cabinets and other cabinet mounted equipment.

The testing also showed that ignition and sustained combustion of qualified cable was difficult even with the ignition source used. A series of 11 smaller scale scoping tests (ST) were performed to evaluate the ability of the selected ignition source fuels to ignite and propagate a fire in a cable bundle and to select credible in situ fuel packages. These scoping tests also

provide valuable insight of the potential fire hazard of qualified and unqualified cable. In test ST #2, only 1 pint of acetone was used in the ignition source package and the fire was not adequate to ignite and propagate a fire in a vertical bundle of qualified cable. In test ST #3, the full quart of acetone was included in the ignition source package and the vertical qualified cable bundle had to be loosened to allow additional air flow and flames through the cables. In this test, the cables ignited and flames propagated up the bundle. As was demonstrated in this test, it was necessary to increase the ignition source fuel and modify the configuration of the cables to achieve the desired test results. At WCGS, cables within control room cabinets are tightly bundled and run in raceway where possible. Therefore, the testing is conservative compared to the WCGS configuration.

Based on the testing reported in NUREG/CR-4527, a credible fire in the control room will not spread out of the cabinet of origin and will not adversely affect cables and components in adjacent cabinets as long as there is a double metal barrier and one inch air gap between cabinets.

A fire starting outside a cabinet was not considered because there are no significant ignition sources or combustibles located outside the cabinets. The back portion of the control room where the critical cabinets are located needs to remain accessible during operation. This along with administrative controls prevents the accumulation of transient combustibles in the area.

Based on a review of the control room layout, a credible fire will not affect both Train A FWIS and Train B FWIS. Therefore, there is reasonable assurance that a FWIS will occur resulting in closure of the feedwater isolation valves.

Licensing Basis for Feedwater Isolation

Section 9.5.1.5 of NUREG 0881 Supplement 5 (Reference 6), provides NRC acceptance of the alternative shutdown strategy for a control room fire. The strategy was presented in letter SLNRC 84-0109 dated August 23, 1984 (Reference 1). In that letter, SNUPPS outlined the strategy for bringing the reactor to a safe and stable hot standby condition from outside the control room. Key observations from that letter related to feedwater are listed below:

1. The alternative shutdown strategy in SLNRC 84-0109 took no actions to isolate main feedwater.
2. MSIVs are closed in Phase D, which is a 30 minute action.
3. Isolation of the MSIVs was the only action taken in SLNRC 84-0109 that would have isolated main feedwater.
4. SG overfill did not appear to be an immediate concern in SLNRC 84-0109.

The NRC, in NUREG 0881 Supplement 5, accepted the alternative shutdown strategy with no specific actions taken to isolate main feedwater by the closure of the feedwater isolation valves. In addition, isolation of MSIVs was accepted as a 30 minute action. WCNO procedure OFN RP-017 currently isolates the main steam and main feedwater isolation valves in less than 3 minutes.

As discussed above, feedwater isolation is not part of the WCGS license basis for alternative shutdown because it was not included as an action in SLNRC 84-0109. Furthermore, the NRC accepted the safe shutdown procedure presented in SLNRC 84-0109 as indicated in NUREG 0881, Supplement 5.

3.5 Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation

Evaluation SA-08-006, Revision 3, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," (Reference 3) documents the basis of the WCGS RCS thermal-hydraulic response to different scenarios potentially caused by a fire in the control room. Twenty-four control room fire scenarios were chosen to address a spurious actuation that could result in significant RCS mass inventory loss, significant RCS pressure reduction, and pressurizer overflow. These scenarios were developed by evaluating various potential scenarios on the simulator, iterating on assumed failures, and selecting the cases that would result in a maximum RCS mass inventory loss and pressure reduction following an uncontrolled cool down of the primary system.

All scenarios assume a single spurious operation failure in conjunction with and without a loss of off-site power and with and without an auxiliary feedwater actuation signal (AFAS). The AFAS was modeled since it could adversely impact PFSSD due to the potential for uncontrolled cool down. No automatic actions were assumed unless it adversely impacted the transient except for automatic feedwater isolation.

The 24 bounding scenarios evaluated, shown in Table 1, can be grouped into three categories and are summarized as follows:

1. Spurious behavior of pressurizer PORV failed open;
2. Spurious behavior of SG atmospheric relief valves (ARVs) failed open; and
3. Spurious uncontrolled letdown.

Table 1 – Summary of Transient Scenarios				
Scenario	Spurious Operation Failure	AFW Pump Auto Start	Off-Site Power Available	Automatic Safety Injection Signal Available
1	Failed Open Pressurizer PORV			
1A	Failed Open Pressurizer PORV	X		
1B	Failed Open Pressurizer PORV			X
1C	Failed Open Pressurizer PORV	X		X

Table 1 – Summary of Transient Scenarios (cont.)				
Scenario	Spurious Operation Failure	AFW Pump Auto Start	Off-Site Power Available	Automatic Safety Injection Signal Available
2	Failed Open Pressurizer PORV		X	
2A	Failed Open Pressurizer PORV	X	X	
2B	Failed Open Pressurizer PORV		X	X
2C	Failed Open Pressurizer PORV	X	X	X
3	Failed Open SG ARV			
3A	Failed Open SG ARV	X		
3B	Failed Open SG ARV			X
3C	Failed Open SG ARV	X		X
4	Failed Open SG ARV		X	
4A	Failed Open SG ARV	X	X	
4B	Failed Open SG ARV		X	X
4C	Failed Open SG ARV	X	X	X
5	Letdown Open			
5A	Letdown Open			X
6	Letdown Open		X	
6A	Letdown Open, No Pressurizer Heaters		X	
6B	Letdown Open, No Pressurizer Heaters, Pressurizer Spray On		X	
6C	Letdown Open		X	X
6D	Letdown Open, No Pressurizer Heaters		X	X
6E	Letdown Open, No Pressurizer Heaters, Pressurizer Spray On		X	X

The RETRAN-3D Input Model

The results presented in Evaluation SA-08-006 were developed using a four-loop best-estimate RETRAN-3D model of the plant used in the RETRAN-02 mode. The only exception to the RETRAN-02 mode was that the Chexal-Lellouche drift flux model option was used to better represent depleted mass distributions on the steam generator secondary and to simulate vapor collecting in the upper regions of the RCS should boiling occur. By using a model to simulate vapor and liquid phase separation (unequal velocities), the evaluation allows the vapor to collect in the upper tube primary region, and RCS vessel, which enhance the possibility of loop flow stagnation.

The NRC approved the use of RETRAN-02 in the Safety Evaluation Report dated September 30, 1993 (Reference 17), for the WCNOG Topical Report NSAG-006 "Transient Analysis Methodology for the Wolf Creek Generating Station." The NRC has accepted the RETRAN-3D computer code for use in analyzing Chapter 15 accidents and transients subject to some conditions and limitations. This acceptance is documented in a letter from Stuart Richards, NRC, to Gary Vine, EPRI, dated January 25, 2001, entitled "Safety Evaluation Report (SER) on EPRI Topical Report NP-7450(P), Revision 4, "RETRAN-3D – A Program for Transient Thermal-Hydraulic Analysis of Complex Fluid Flow Systems" (TAC No. MA4311)," (Reference 10). Specifically, Condition 40 of the NRC Safety Evaluation Report states:

40. Organizations with NRC-approved RETRAN-02 methodologies can use the RETRAN-3D code in the RETRAN-02 mode, without additional NRC approval, provided that none of the new RETRAN-3D models listed, in the definition are used. Organizations with NRC-approved RETRAN-02 methodologies must obtain NRC approval prior to applying any of the new RETRAN-3D models listed above for UFSAR Chapter 15 licensing basis applications. Organizations without NRC approved RETRAN-02 methodologies must obtain NRC approval for such methodologies or a specific application before applying the RETRAN-02 code or the RETRAN-3D code for UFSAR Chapter 15 licensing basis applications. Generic Letter 83-11 provides additional guidance in this area. Licensees who specifically reference RETRAN-02 in their technical specifications will have to request a Technical Specification change to use RETRAN-3D.

Section 8.0 of the NRC Safety Evaluation Report indicates that use of the Chexal-Lellouche drift flux model will result in the need to assure its use is in conformance with Condition 16. Condition 16 indicates that the results of the analysis using the model must be carefully reviewed. WCNOG has reviewed the results of the model. Additionally, as noted in Condition 40, Evaluation SA-08-006 is not a USAR Chapter 15 licensing basis analysis.

Evaluation SA-08-006, Revision 3 Results

The key results of this evaluation are shown in Table 2. Although not an Appendix R requirement, it is noted in Table 2 whether boiling in the RCS occurs. In Scenarios 1, 1A and 1C minimal boiling occurred in the upper core region for a short period. The only transient scenario that does not meet the Appendix R, Section III.L.2 performance goals is Scenario 3A in which, for a brief period, the pressurizer water level is not maintained within level indication. Scenarios 1, 1A, 1C, and 3A are discussed in further detail below.

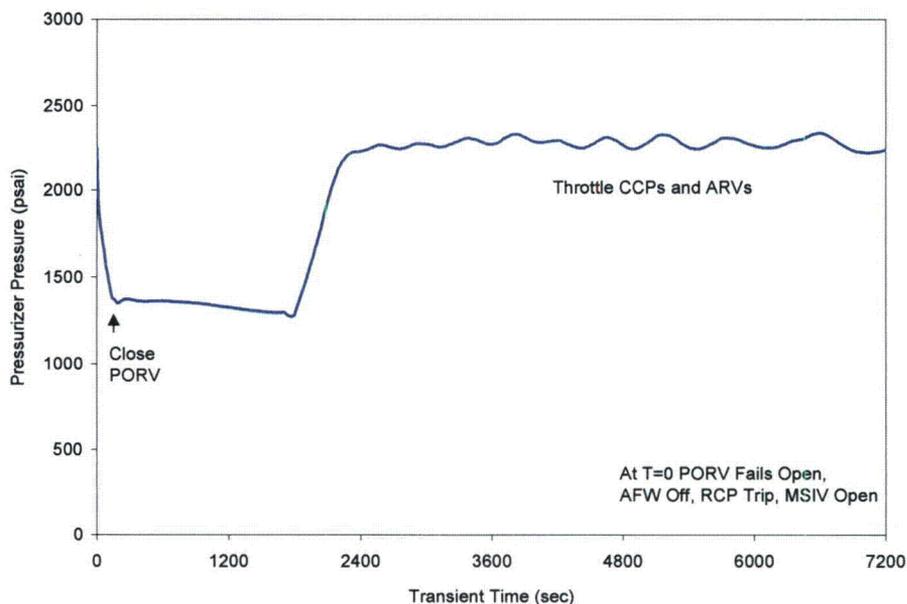
Table 2 - Results of the Transient Scenarios					
Scenario	Cold Shutdown Achieved	Core Remains Covered	Pressurizer Level Maintained	Natural Circulation Maintained	RCS Boiling Prevented
1	Yes	Yes	Yes	Yes	No
1A	Yes	Yes	Yes	Yes	No
1B	Yes	Yes	Yes	Yes	Yes
1C	Yes	Yes	Yes	Yes	No
2	Yes	Yes	Yes	Yes	Yes
2A	Yes	Yes	Yes	Yes	Yes
2C	Yes	Yes	Yes	Yes	Yes
2D	Yes	Yes	Yes	Yes	Yes
3	Yes	Yes	Yes	Yes	Yes
3A	Yes	Yes	No	Yes	Yes
3B	Yes	Yes	Yes	Yes	Yes
3C	Yes	Yes	Yes	Yes	Yes
4	Yes	Yes	Yes	Yes	Yes
4A	Yes	Yes	Yes	Yes	Yes
4B	Yes	Yes	Yes	Yes	Yes
4C	Yes	Yes	Yes	Yes	Yes
5	Yes	Yes	Yes	Yes	Yes
5A	Yes	Yes	Yes	Yes	Yes
6	Yes	Yes	Yes	Yes	Yes
6A	Yes	Yes	Yes	Yes	Yes
6B	Yes	Yes	Yes	Yes	Yes
6C	Yes	Yes	Yes	Yes	Yes
6D	Yes	Yes	Yes	Yes	Yes
6E	Yes	Yes	Yes	Yes	Yes

Scenario 1 Discussion

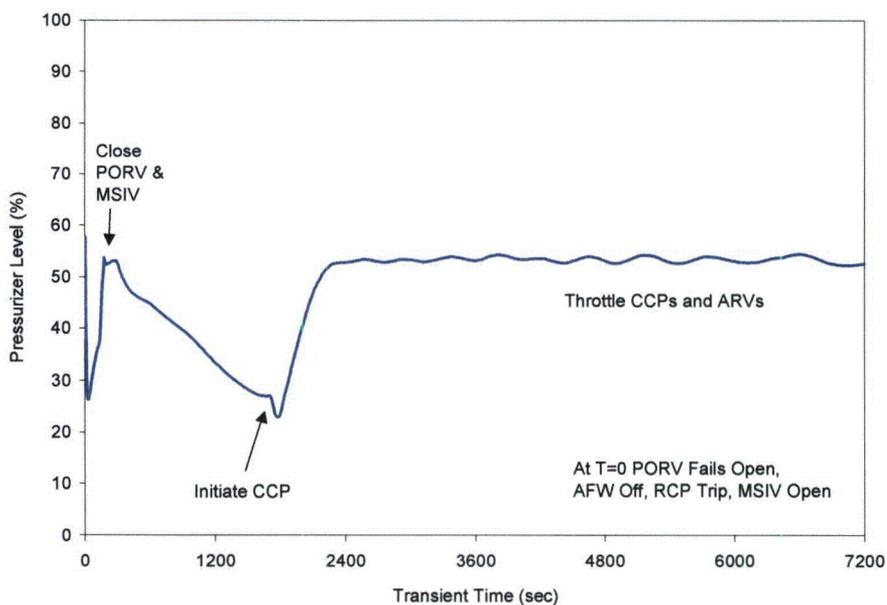
Scenario 1 assumes a loss of offsite power with one pressurizer PORV stuck open. A reactor trip occurs at time zero when operators press the reactor trip pushbuttons. The MSIVs are closed by manual operation within 180 seconds after reactor trip. Automatic feedwater isolation occurs on reactor trip with low T_{avg} (564°F). A rapid RCS depressurization occurs due to the reactor trip and the failed open PORV. With the PORV open, a rapid decrease in pressurizer level occurs followed by RCS coolant drawn into the pressurizer creating an increase in pressurizer level. When the PORV is closed at 180 seconds by operator action the RCS begins to repressurize and

the pressurizer level decreases. The following figures from Evaluation SA-08-006 show the pressurizer level and pressure during the Scenario 1 transient.

Scenario 1, Figure 2: Pressurizer Pressure



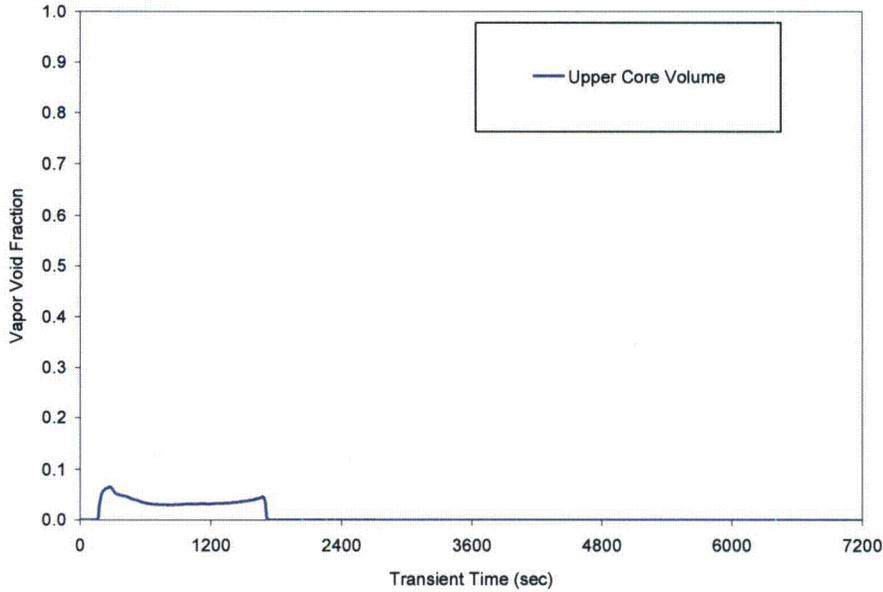
Scenario 1, Figure 3: Pressurizer Level



The rapid depressurization of the RCS results in minimal upper core boiling between 160 seconds and 770 seconds. The maximum void fraction achieved in the upper core is less than 6.6%. All of the voids are collapsed due to cooling and elevation head prior to reaching the top of the SG tubes so natural circulation is maintained.

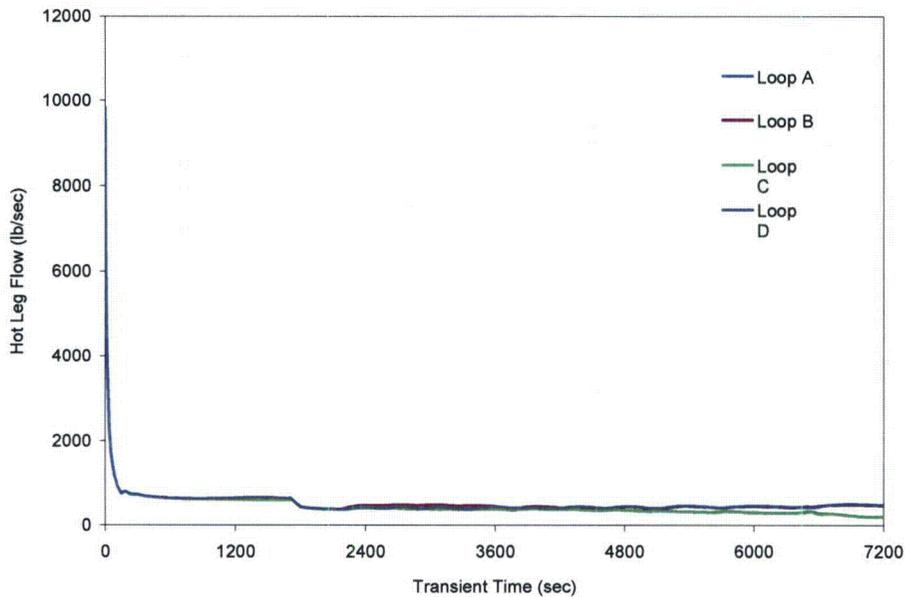
The following figure from Evaluation SA-08-006 shows the upper core void fraction during the Scenario 1 transient.

Scenario 1, Figure 8: Upper Core Void Fraction

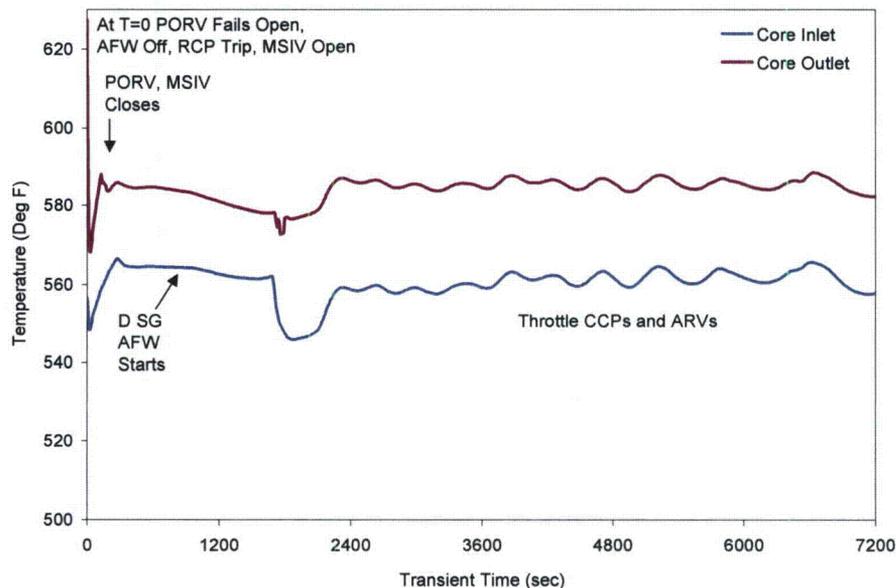


The following figures from Evaluation SA-08-006 demonstrate that, during the Scenario 1 transient, the RCS loop flows remain in natural circulation and RCS temperature stabilizes.

Scenario 1, Figure 5: Hot Leg Loop Flow



Scenario 1, Figure 4: Core Inlet and Exit Temperature



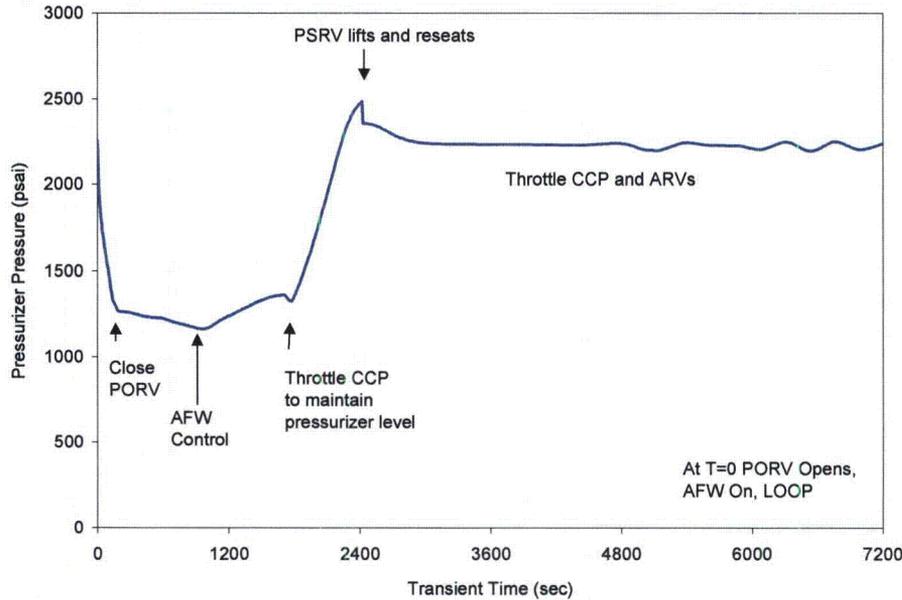
After 3000 seconds the RCS pressure, temperature, and pressurizer level have stabilized indicating a safe shutdown condition.

Scenario 1A Discussion

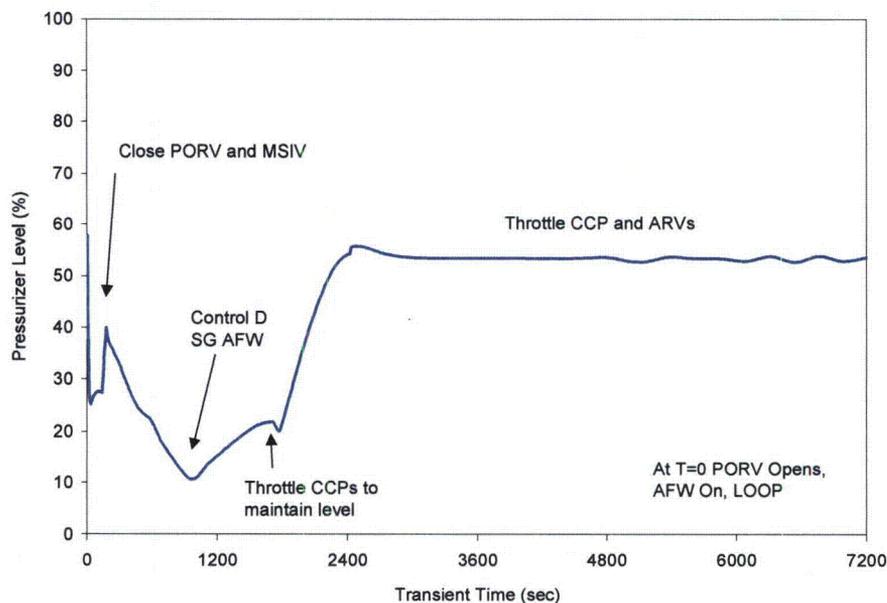
Scenario 1A is similar to Scenario 1 with the exception of the AFW pumps auto start for an unplanned cooldown. With the loss of power, the reactor trip occurs at time zero and the reactor coolant pumps (RCPs) coast down. Automatic feedwater isolation occurs on reactor trip with low T_{avg} (564°F). The MSIVs are closed by manual operation within 180 seconds after reactor trip. A rapid RCS depressurization occurs due to the reactor trip and the failed open PORV. With the PORV open, a rapid decrease in pressurizer level occurs followed by RCS coolant drawn into the pressurizer creating an increase in pressurizer level. When the PORV is closed at 180 seconds by operator action the RCS begins to repressurize and the pressurizer level decreases.

The following figures from Evaluation SA-08-006 show the pressurizer level and pressure during the Scenario 1A transient.

Scenario 1A, Figure 2: Pressurizer Pressure



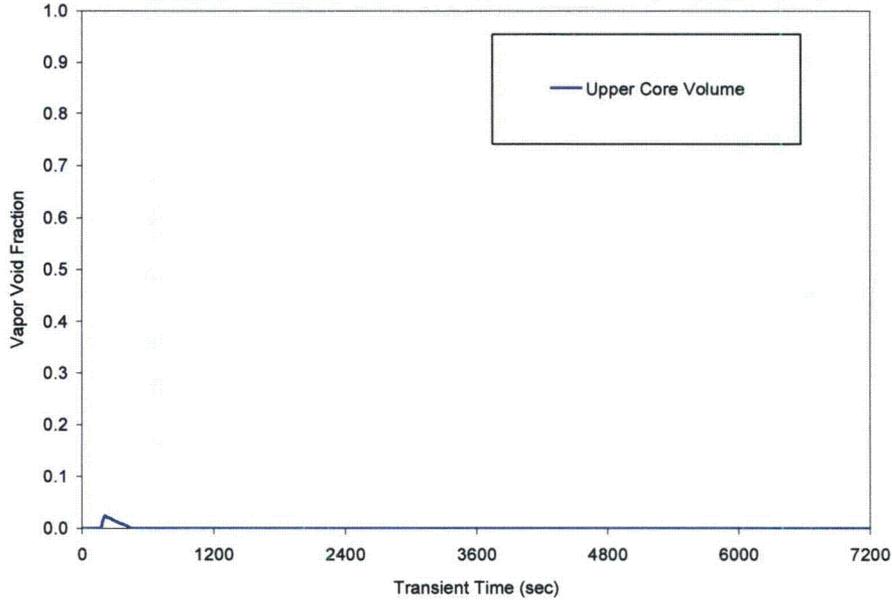
Scenario 1A, Figure 3: Pressurizer Level



The rapid depressurization of the RCS results in minimal upper core boiling between 180 seconds and 450 seconds. The maximum void fraction achieved in the upper core is less than 2.35%. All of the voids are collapsed prior to reaching the top of the SG tubes so natural circulation is maintained.

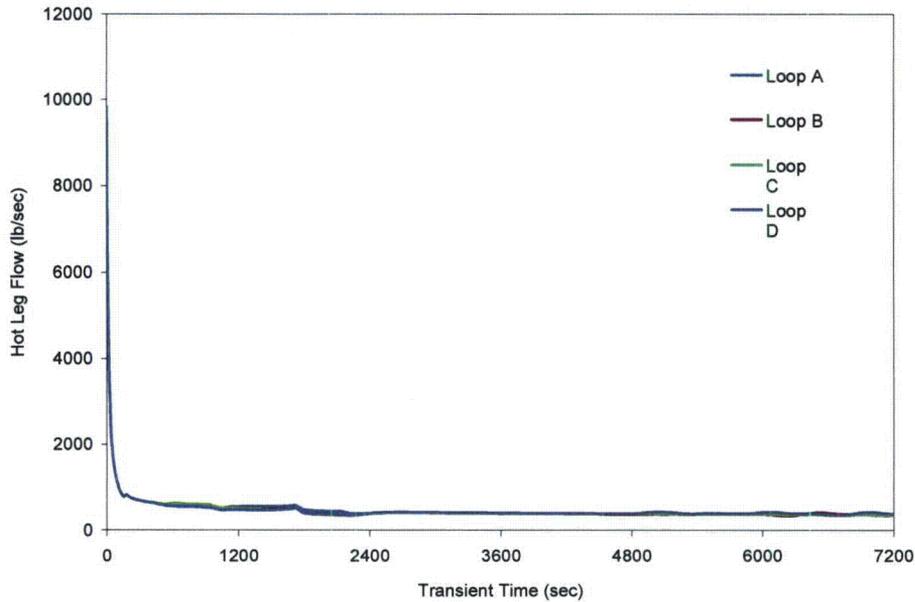
The following figure from Evaluation SA-08-006 shows the upper core void fraction during the Scenario 1A transient.

Scenario 1A, Figure 8: Upper Core Void Fraction

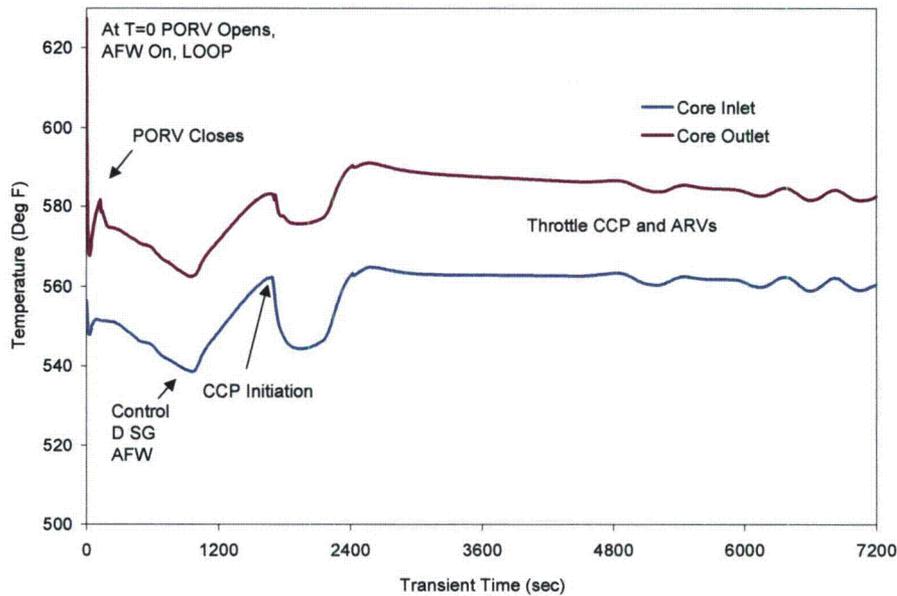


The following figures from Evaluation SA-08-006 demonstrate that, during the Scenario 1A transient, the RCS loop flows remain in natural circulation and RCS temperature stabilizes.

Scenario 1A, Figure 5: Hot Leg Loop Flow



Scenario 1A, Figure 4: Core Inlet and Exit Temperature



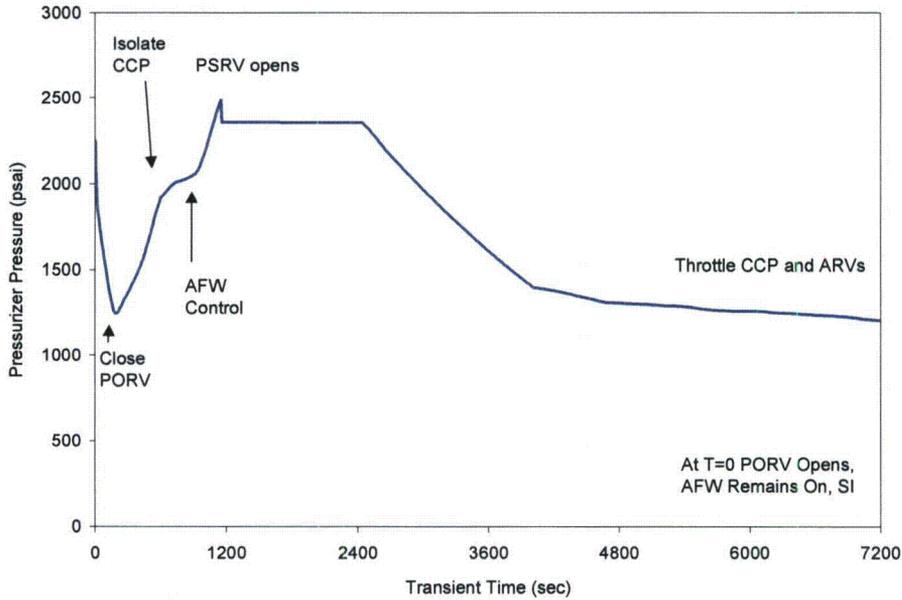
After 3000 seconds the RCS pressure, temperature, and pressurizer level have stabilized indicating a safe shutdown condition.

Scenario 1C Discussion

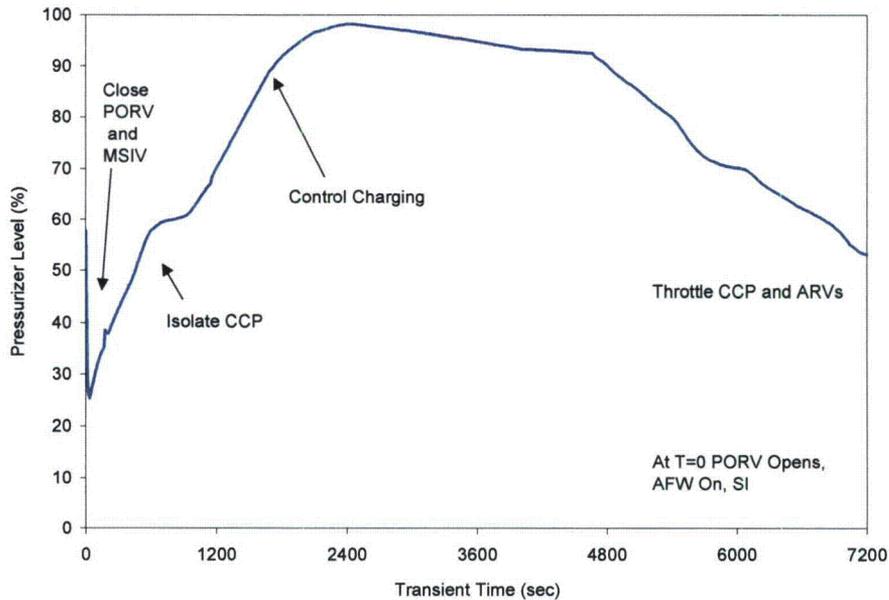
Scenario 1C is similar to Scenario 1A with the exception of the AFW pumps auto start for an unplanned cooldown and safety injection is available if required. With the loss of power, the reactor trip occurs at time zero and the RCPs coast down. The MSIVs are manually closed within 180 seconds of reactor trip. Automatic feedwater isolation occurs on reactor trip with low T_{avg} (564°F). A rapid RCS depressurization occurs due to the reactor trip and the failed open PORV. This is followed by a safety injection signal which initiates the centrifugal charging pumps (CCPs) increasing pressurizer level as shown in Scenario 1C, Figure 3.

The following figures from Evaluation SA-08-006 show the pressurizer level and pressure during the Scenario 1C transient.

Scenario 1C, Figure 2: Pressurizer Pressure



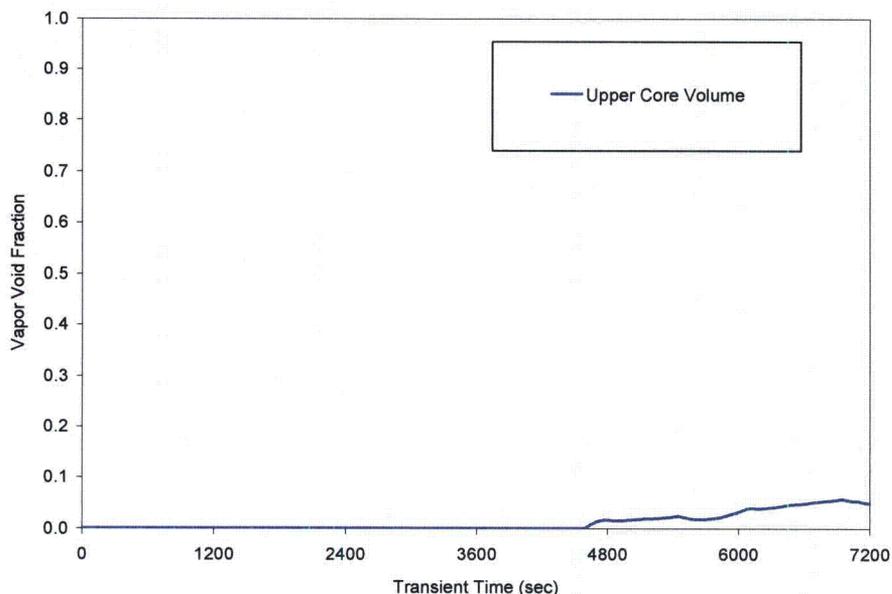
Scenario 1C, Figure 3: Pressurizer Level



Low RCS pressure after 4800 seconds results in minimal upper core boiling for the period after that time.

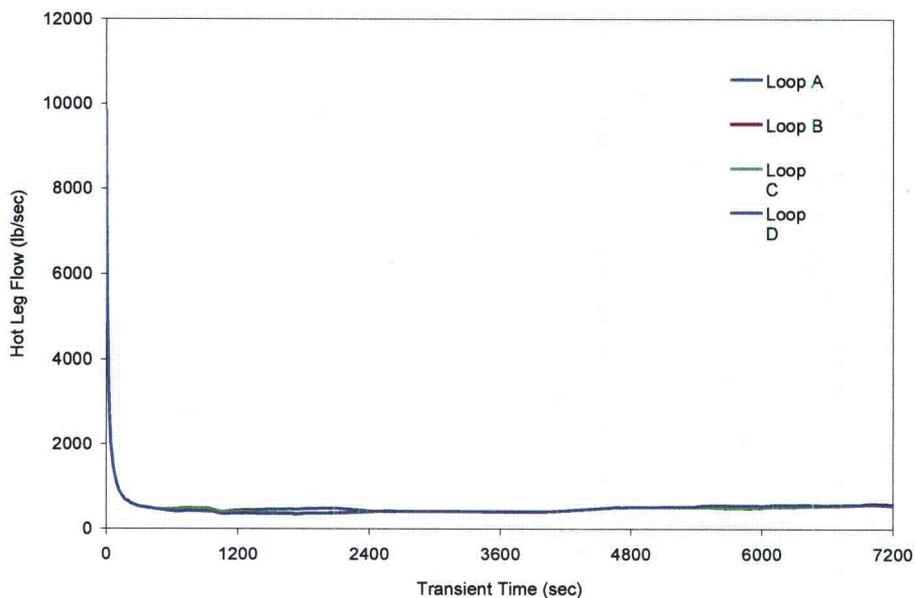
The maximum void fraction achieved in the upper core is less than 11.2% as shown in the following figure from Evaluation SA-08-006. All of the voids are collapsed prior to reaching the top of the SG tubes.

Scenario 1C, Figure 8: Upper Core Void Fraction

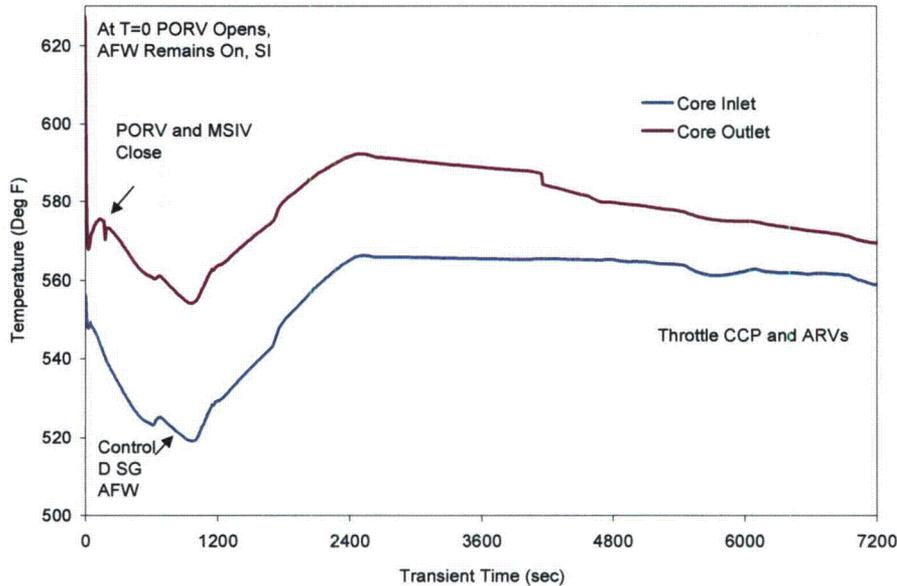


The following figures from Evaluation SA-08-006 demonstrate that, during the Scenario 1C transient, the RCS loop flows remain in natural circulation and RCS temperature stabilizes.

Scenario 1C, Figure 5: Hot Leg Loop Flow



Scenario 1C, Figure 4: Core Inlet and Exit Temperature



After 6000 seconds the RCS pressure, temperature, and pressurizer level have stabilized indicating a safe shutdown condition.

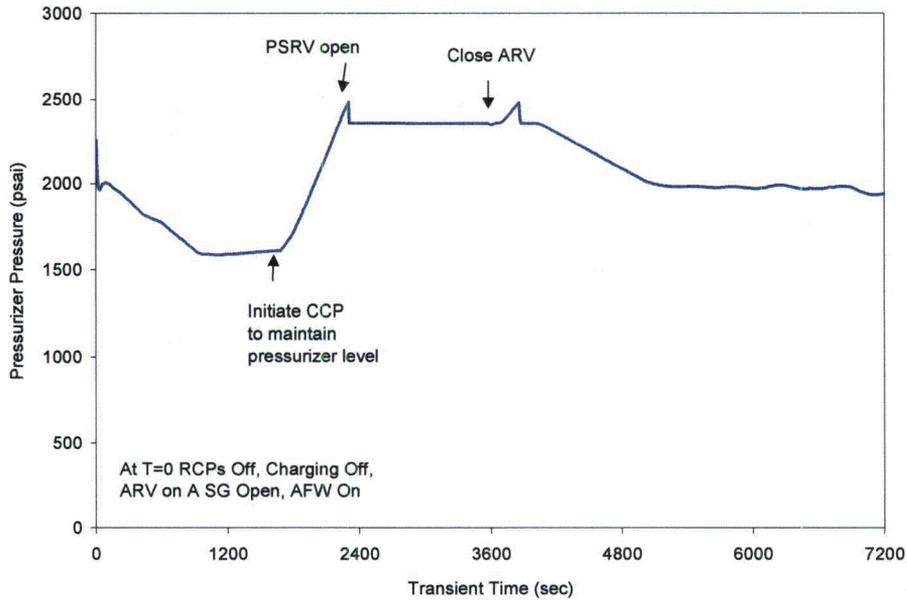
Scenario 3A Discussion

Scenario 3A assumes a loss of offsite power with the SG 'A' ARV stuck open and closes at 3600 seconds. The AFW pumps auto start. A reactor trip occurs at time zero and automatic feedwater isolation occur on reactor trip with low T_{avg} (564°F). The MSIVs are manually closed within 180 seconds of reactor trip. The stuck open ARV with AFW flow to the SGs result in a RCS cooldown.

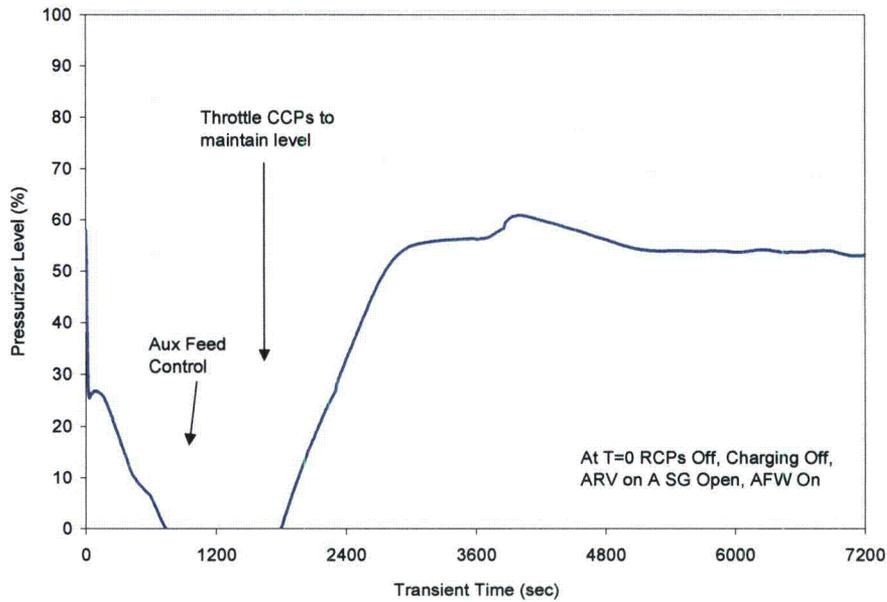
The RCS pressure, temperature, and pressurizer water level initially decrease due to the reactor trip followed by a small rise after the MSIVs close increasing SG pressure and cooling capability. The uncontrolled AFW flow and stuck open SG 'A' ARV causes excess SG cooling and these RCS parameters continue to decline. Through the first 2000 seconds, SG 'A' pressure is decreasing and is the primary reason the RCS cools. At 840 seconds pressurizer level goes off scale low and returns on scale at 1780 seconds. To verify no voiding occurred in the RCS hot leg, the water level in the pressurizer surge line was examined. The water level in the surge line reached a minimum height of 67% volume for a short period of time and increases with the initiation of CCP flow. Natural circulation is maintained through this time period and the core remains in a controlled safe shutdown condition.

The following figures from Evaluation SA-08-006 show the pressurizer level and pressure during the Scenario 3A transient.

Scenario 3A, Figure 2: Pressurizer Pressure

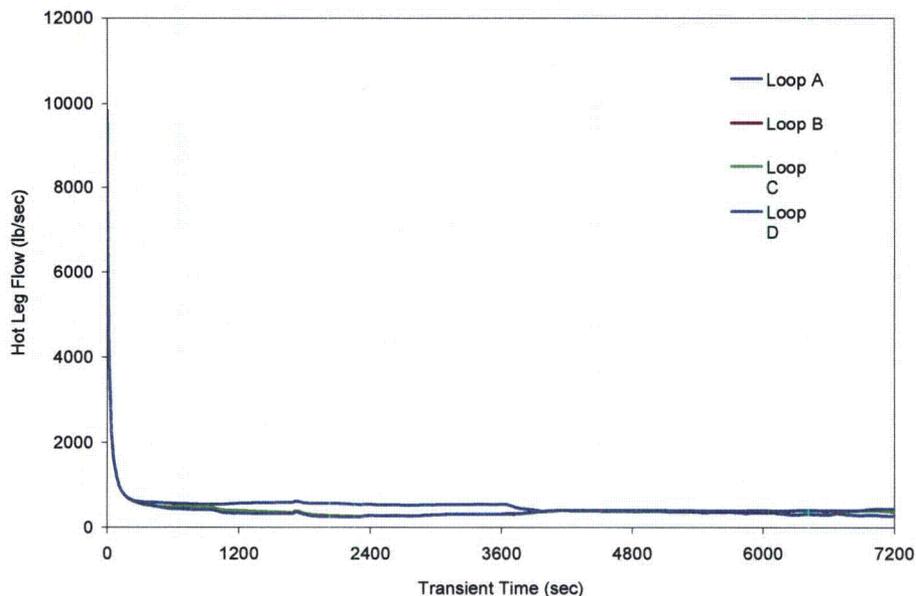


Scenario 3A, Figure 3: Pressurizer Level

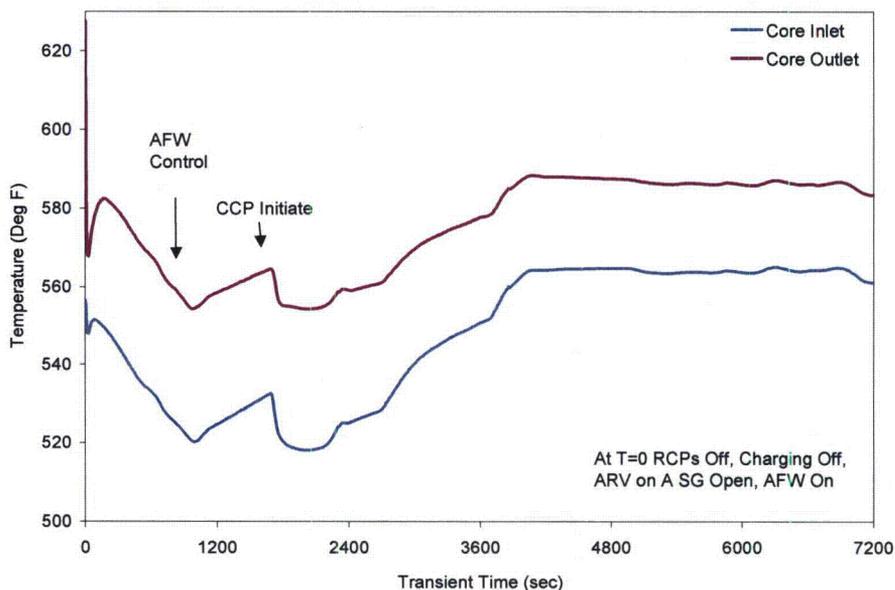


The following figures from Evaluation SA-08-006 demonstrate that, during the Scenario 3A transient, the RCS loop flows remain in natural circulation and RCS temperature stabilizes.

Scenario 3A, Figure 5: Hot Leg Loop Flow



Scenario 3A, Figure 4: Core Inlet and Exit Temperature



After 4800 seconds the RCS temperature and pressurizer level have stabilized indicating a safe shutdown condition.

Summary

Based on the control room fire scenarios investigated in Evaluation SA-08-006, Revision 3, coupled with the procedural guidance of OFN RP-017 (Reference 4) and OFN RP-017A, "Hot Standby to Cold Shutdown From Outside the Control Room due to a Fire" (Reference 11), the plant will not reach unrecoverable conditions, which could lead to core damage. The pressurizer level remains on scale for all scenarios except Scenario 3A, natural circulation flow is maintained, and average hot leg temperature remains below 628°F (approximately 100% power steady-state temperature). This demonstrates that safe hot standby and inventory levels can be achieved and maintained using the timing limitations defined in Evaluation SA-08-006. In all cases the reactor core remains cooled and no core damage is indicated, no pressure vessel limits are exceeded, and the reactor reaches a new stable steady-state condition representing safe shutdown.

The results of these transient evaluations may not be bounded by the normal loss of AC power transient because of an additional spurious operation (failure) and no automatic actuation of safety components assumptions. These two additional conservative assumptions ensure the transient will be more severe than a loss of normal AC power. In addition, some of the transients have off-site power available and will have much different results than an AC power loss transient. Thus, they cannot be directly compared.

In only two scenarios, small amounts of voiding occur for a short period of time with a loss of off-site power and a stuck open PORV. Natural circulation and adequate core cooling is maintained throughout the duration of the transient.

3.6 Conclusions

It is acceptable to re-baseline the license basis for shutdown of the plant from outside the control room in the case of a fire in the control room from letter SLNRC 84-0109 referenced in NUREG 0881 Supplement 5 to drawing E-1F9915. The present license basis is a letter that has no documented technical basis for the sequence of operator actions. Drawing E-1F9915 is a comprehensive and documented technical basis for the sequence of operator actions in procedure OFN RF-017.

The thermal-hydraulic evaluation results in Evaluation SA-08-006 demonstrate that the control room shutdown capability meets the Appendix R, III.L.1 criteria with one exception. The RCS process variables are not maintained within those predicted for a loss of normal ac power. Specifically, some voiding is observed in the upper core region in three (Scenarios 1, 1A, and 1C) of the 24 scenarios modeled. However, this is acceptable since the evaluation shows that the plant does not reach unrecoverable conditions.

The thermal-hydraulic evaluation also demonstrates that the performance goals of Appendix R, Section III.L.2, are met with one exception. In one analyzed event (Scenario 3A), pressurizer water level falls below the indicated level for a short period of time. This is acceptable because the evaluation also shows that the core remains covered and the plant does not reach unrecoverable conditions.

It is acceptable to credit an automatic FWIS in the event of a fire in the control room. The redundancy and diversity of FWIS initiators in the control room, the physical location of redundant protection cabinets in the control room as well as fire test data associated with control cabinet

fires provides reasonable assurance that a single credible fire in the control room will not adversely affect both trains of components necessary to actuate an automatic FWIS.

Based on the above discussion, the proposed changes to the approved fire protection program discussed herein are acceptable as there is reasonable assurance that safe shutdown can be achieved.

4. REGULATORY EVALUATION

4.1 Applicable Regulatory Requirements/Criteria

10 CFR 50, Section 48, Fire Protection, paragraph (a)(1) states, in part: "Each holder of an operating license issued under this part or a combined license issued under part 52 of this chapter must have a fire protection plan that satisfies Criterion 3 of appendix A to this part." Paragraph (b) states, in part: "Appendix R to this part establishes fire protection features required to satisfy Criterion 3 of appendix A to this part with respect to certain generic issues for nuclear power plants licensed to operate before January 1, 1979."

10 CFR 50, Appendix R, Section III.L.1, states: "Alternative or dedicated shutdown capability provided for a specific fire area shall be able to (a) achieve and maintain subcritical reactivity conditions in the reactor; (b) maintain reactor coolant inventory; (c) achieve and maintain hot standby² conditions for a PWR (hot shutdown² for a BWR); (d) achieve cold shutdown conditions within 72 hours; and (e) maintain cold shutdown conditions thereafter. During the postfire shutdown, the reactor coolant system process variables shall be maintained within those predicted for a loss of normal a.c. power, and the fission product boundary integrity shall not be affected; i.e., there shall be no fuel clad damage, rupture of any primary coolant boundary, of rupture of the containment boundary."

10 CFR 50, Appendix R, Section III.L.2, states: "The performance goals for the shutdown functions shall be:

- a. The reactivity control function shall be capable of achieving and maintaining cold shutdown reactivity conditions.
- b. The reactor coolant makeup function shall be capable of maintaining the reactor coolant level above the top of the core for BWRs and be within the level indication in the pressurizer for PWRs.
- c. The reactor heat removal function shall be capable of achieving and maintaining decay heat removal.
- d. The process monitoring function shall be capable of providing direct readings of the process variables necessary to perform and control the above functions.
- e. The supporting functions shall be capable of providing the process cooling, lubrication, etc., necessary to permit the operation of the equipment used for safe shutdown functions."

10 CFR 50, Appendix A, *Criterion 3—Fire protection*. Structures, systems, and components important to safety shall be designed and located to minimize, consistent with other safety requirements, the probability and effect of fires and explosions. Noncombustible and heat resistant materials shall be used wherever practical throughout the unit, particularly in locations such as the containment and control room. Fire detection and fighting systems of appropriate capacity and capability shall be provided and designed to minimize the adverse effects of fires on structures, systems, and components important to safety. Firefighting systems shall be designed to assure that their rupture or inadvertent operation does not significantly impair the safety capability of these structures, systems, and components.

4.2 Significant Hazards Consideration

The proposed amendment request is requesting Nuclear Regulatory Commission (NRC) approval, pursuant to License Condition 2.C.(5), to make changes to the approved fire protection program as described in the Updated Safety Analysis Report (USAR). The proposed changes to the approved fire protection program are based on the Reactor Coolant System (RCS) thermal-hydraulic response (Evaluation SA-08-006) for a postulated control room fire performed for changes to the alternative shutdown methodology outlined in letter SLNRC 84-0109, "Fire Protection Review." Drawing E-1F9915, "Design Basis Document for OFN RP-017, Control Room Evacuation," Revision 4, and Evaluation SA-08-006, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 3, demonstrate the adequacy of the revised alternative shutdown procedure, OFN RP-017, "Control Room Evacuation." The results of the RCS thermal-hydraulic response identified required changes to the fire protection program as follows:

- Deviation from the 10 CFR 50, Appendix R, Section III.L.1 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining RCS process variables within those predicted for a loss of normal AC power.
- Deviation from the 10 CFR 50, Appendix R, Section III.L.2 comparison response, as described in Appendix 9.5E of the WCGS USAR, specific to maintaining pressurizer level on scale.
- Revision to USAR Appendix 9.5B to include incorporation of drawing E-1F9915 and a deviation from Calculation XX-E-013. Deviation from Calculation XX-E-013, "Post-Fire Safe Shutdown (PFSSD) Analysis," Revision 2, Assumption 3-A-4 regarding application of loss of automatic functions, specific to automatic feedwater isolation in the event of a control room fire. Calculation XX-E-013 is incorporated by reference in USAR Appendix 9.5B, "Fire Hazards Analyses."

The proposed changes have been determined to adversely affect the ability to achieve and maintain safe shutdown in the event of a fire. Therefore, prior Commission approval is required as Section III.L.1 and Section III.L.2 of Appendix R is not directly satisfied.

WCNOC has evaluated whether or not a significant hazards consideration is involved with the proposed amendment(s) by focusing on the three standards set forth in 10 CFR 50.92, "Issuance of amendment," as discussed below:

1. **Does the proposed amendment involve a significant increase in the probability or consequences of an accident previously evaluated?**

Response: No.

The design function of structures, systems and components (SSCs) are not impacted by the proposed deviations from Appendix R, Sections III.L.1 and III.L.2, and Calculation XX-E-013. The proposed changes to the approved fire protection program are based on the RCS thermal-hydraulic response (Evaluation SA-08-006) for a postulated control room fire performed for changes to the alternative shutdown methodology outlined in letter SLNRC 84-0109, "Fire Protection Review." Drawing E-1F9915, "Design Basis Document for OFN RP-017, Control Room Evacuation," Revision 4, and Evaluation SA-08-006, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 3, demonstrate the adequacy of the revised alternative shutdown procedure, OFN RF-017. The proposed changes do not alter or prevent the ability of SSCs from performing their intended function to mitigate the consequences of an initiating event within the assumed acceptance limits. Therefore, the probability of any accident previously evaluated is not increased. Equipment required to mitigate an accident remains capable of performing the assumed function.

2. **Does the proposed amendment create the possibility of a new or different kind of accident from any accident previously evaluated?**

Response: No.

The proposed changes will not alter the requirement or function for systems required during accident conditions. The design function of structures, systems and components are not impacted by the proposed change. The thermal-hydraulic evaluation of the RCS determined natural circulation is maintained and adequate core cooling is maintained. The fission product boundary integrity is not affected and safe shutdown capability is maintained.

Therefore, the proposed change does not create the possibility of a new or different kind of accident from any accident previously evaluated.

3. **Does the proposed amendment involve a significant reduction in a margin of safety?**

Response: No.

There will be no effect on the manner in which safety limits or limiting safety system settings are determined nor will there be any effect on those plant systems necessary to assure the accomplishment of protection functions. The revised alternative shutdown methodology provides the ability to achieve and maintain safe shutdown in the event of a fire. The thermal-hydraulic evaluation of the RCS determined natural circulation is maintained and adequate core cooling is maintained.

Therefore, the proposed change does not involve a significant reduction in a margin of safety.

Based on the above, WCNOC concludes that the proposed amendment does not involve a significant hazards consideration under the standards set forth in 10 CFR 50.92(c), and, accordingly, a finding of "no significant hazards consideration" is justified.

4.3 Conclusions

In conclusion, based on the considerations discussed above, (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) such activities will be conducted in compliance with the Commission's regulations, and (3) the issuance of the amendment will not be inimical to the common defense and security or to the health and safety of the public.

5. ENVIRONMENTAL CONSIDERATION

WCNOC has evaluated the proposed changes and determined that the changes do not involve (i) a significant hazards consideration, (ii) a significant change in the types or a significant increase in the amounts of any effluents that may be released offsite, or (iii) a significant increase in individual or cumulative occupational radiation exposure. Accordingly, the proposed amendment meets the eligibility criterion for categorical exclusion set forth in 10 CFR 51.22(c)(9). Therefore, pursuant to 10 CFR 51.22(b), no environmental impact statement or environmental assessment need be prepared in connection with the proposed amendment.

6. REFERENCES

1. SNUPPS letter SLNRC 84-0109, "Fire Protection Review," from N. A. Petrick, SNUPPS, to H. R. Denton, USNRC, August 23, 1984.
2. Drawing E-1F9915, Revision 4, "Design Basis Document for Procedure OFN RP-017, Control Room Evacuation."
3. Evaluation SA-08-006, "RETRAN-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire," Revision 3, October 17, 2012.
4. Procedure OFN RP-017, Revision 40, "Control Room Evacuation," January 30, 2012.
5. Calculation XX-E-013, Revision 2, "Post Fire Safe Shutdown Analysis," April 11, 2010.
6. NUREG 0881, "Safety Evaluation Report related to the operation of Wolf Creek Generating Station, Unit No. 1," Supplement No. 5, March 1985.
7. NUREG 0881, "Safety Evaluation Report related to the operation of Wolf Creek Generating Station, Unit No. 1," April 1982.
8. NRC letter, "Wolf Creek Generation Station – NRC Integrated Inspection Report 05000482/2009004," November 10, 2009. ADAMS Accession No. ML093140803.
9. NRC letter, "Wolf Creek Generating Station - NRC Triennial Fire Protection Inspection Report (05000482/2011007)," December 27, 2011. ADAMS Accession No. ML11361A427.

10. NRC letter from Stuart Richards, NRC, to Gary Vine, EPRI, "Safety Evaluation Report on EPRI Topical Report NP-7450(P), Revision 4, "RETRAN-3D – A Program for Transient Thermal-Hydraulic Analysis of Complex Fluid Flow Systems" (TAC No. MA4311)," January 25, 2001.
11. Procedure OFN RP-017A, Revision 5, "Hot Standby to Cold Shutdown From Outside the Control Room due to a Fire," June 6, 2012.
12. WCNOG letter ET 10-0026, "License Amendment Request (LAR) for Deviation from Fire Protection Requirements - Reactor Coolant System Subcooling During Alternative Shutdown," September 22, 2010. ADAMS Accession No. ML102720417.
13. WCNOG letter ET 10-0031, "Response to Supplemental Information Request for License Amendment Request Deviation from Fire Protection Requirements - Reactor Coolant System Subcooling During Alternative Shutdown (TAC NO. ME4757)," November 22, 2010. ADAMS Accession No. ML103340290.
14. NRC letter from J. R. Hall, USNRC, to M. W. Sunseri, WCNOG, "Wolf Creek Generating Station – Request for Additional Information Regarding License Amendment Request to Revise the Fire Protection Program (TAC NO. ME4757)," May 24, 2011. ADAMS Accession No. ML111380215.
15. WCNOG letter ET 11-0005, "Withdrawal of License Amendment Request to Revise the Fire Protection Program (TAC NO. ME4757)," June 30, 2011. ADAMS Accession No. ML11188A074.
16. NUREG/CR-4527 (Reference 16), "An Experimental Investigation of Internally Ignited Fires in Nuclear Power Plant Control Cabinets: Part 1: Cabinet Effects Tests," April 1987.
17. NRC letter from W. D. Reckley, USNRC, to N. S. Carns, WCNOG, "Wolf Creek Nuclear Operating Corporation - Transient Analysis Methodology for the Wolf Creek Generating Station (TAC NO. M79740)," September 30, 1993.

Markup of Renewed Facility Operating License

- (5) Fire Protection (Section 9.5.1, SER, Section 9.5.1.8, SSER #5)
- (a) The Operating Corporation shall maintain in effect all provisions of the approved fire protection program as described in the SNUPPS Final Safety Analysis Report for the facility through Revision 17, the Wolf Creek site addendum through Revision 15, as approved in the SER through Supplement 5, Amendment No. 191, and Amendment No. 193 subject to provisions b and c below.
- (b) The licensee may make changes to the approved fire protection program without prior approval of the Commission only if those changes would not adversely affect the ability to achieve and maintain safe shutdown in the event of a fire.
- (c) Deleted.
- (6) Qualification of Personnel (Section 13.1.2, SSER #5, Section 18, SSER #1)
- Deleted per Amendment No. 141.
- (7) NUREG-0737 Supplement 1 Conditions (Section 22, SER)
- Deleted per Amendment No. 141.
- (8) Post-Fuel-Loading Initial Test Program (Section 14, SER Section 14, SSER #5)
- Deleted per Amendment No. 141.
- (9) Inservice Inspection Program (Sections 5.2.4 and 6.6, SER)
- Deleted per Amendment No. 141.
- (10) Emergency Planning
- Deleted per Amendment No. 141.
- (11) Steam Generator Tube Rupture (Section 15.4.4, SSER #5)
- Deleted per Amendment No. 141.
- (12) LOCA Reanalysis (Section 15.3.7, SSER #5)
- Deleted per Amendment No. 141.

and Amendment No. XXX

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WOLF CREEK

APPENDIX 9.5B
FIRE HAZARDS ANALYSES

The USAR FHA has been superseded by the following documents:

- E-1F9905, Fire Hazard Analysis.
- E-1F9900, Post-Fire Safe Shutdown Manual Actions.
- E-1F9910, Post-Fire Safe Shutdown Fire Area Analysis.
- XX-E-013, Post-Fire Safe Shutdown (PFSSD) Analysis.
- M-663-00017A, Fire Protection Evaluations for Unique or Unbounded Fire Barrier Configurations.

The above documents are incorporated by Reference within the USAR.

- E-1F9915, Design Basis Document for OFN RP-017, Control Room Evaluation

WOLF CREEK

No changes this page
For information only

TABLE 9.5E-1 (Sheet 25)

10CFR50 Appendix R

WCGS

covered by any complete shift personnel complement. These duties include command control of the brigade, transporting fire suppression and support equipment to the fire scenes, applying the extinguishant to the fire, communication with the control room, and coordination with outside fire departments.

g. Potential radiological and toxic hazards in fire zones.

h. Ventilation system operation that ensures desired plant air distribution when the ventilation flow is modified for fire containment or smoke clearing operations.

i. Operations requiring control room and shift engineer coordination or authorization.

j. Instructions for plant operators and general plant personnel during fire.

III. L. Alternative and Dedicated Shutdown Capability

1. Alternative or dedicated shutdown capability provided for a specific fire area shall be able to (a) achieve and maintain subcritical reactivity conditions in the reactor, (b) maintain reactor coolant inventory (c) achieve and maintain hot standby⁽¹⁾ conditions

An auxiliary shutdown panel, described in Section 7.4, in conjunction with certain local controls, provides a means of achieving and maintaining hot standby in the event that the main control room is uninhabitable.

WOLF CREEK

TABLE 9.5E-1 (Sheet 26)

10CFR50 Appendix R

WCGS

for PWR (hot shutdown⁽⁷⁾ for a BWR); (d) achieve cold shutdown conditions within 72 hours; and (e) maintain cold shutdown conditions thereafter. During the postfire shutdown, the reactor coolant system process variables shall be maintained within those predicted for loss of normal ac power and the fission product boundary integrity shall not be affected i.e., there shall be no fuel clad damage, rupture of any primary coolant boundary, or rupture of the containment boundary.

The auxiliary shutdown panel contains the controls and indication necessary to maintain reactor coolant system inventory, remove decay heat, and provide the required boration for hot standby. Adequate operations shift staffing is provided to achieve and maintain post-fire safe shutdown "Hot Standby Conditions" in the event of a fire. Cold shutdown can be achieved and maintained from outside the control room by additional manual operator action at local control sites.

The auxiliary shutdown panel is included in the fire hazards analysis, Appendix 9.5B.

2. The performance goals for the shutdown functions shall be:

a. The reactivity control function shall be capable of achieving and maintaining cold shutdown reactivity conditions.

The performance criteria of III.L.1 are satisfied, with the exception of maintaining reactor process variables within those predicted for a loss of normal ac power. This is acceptable, as long as a control room fire will not result in the plant reaching an unrecoverable condition, which could lead to core damage. The criteria for "not reaching an unrecoverable condition" are that 1) natural circulation is maintained, and 2) adequate core cooling is maintained (average hot leg temperature remains at or below normal full power temperature - 630°F).

7 - As defined in the Standard Technical Specifications.

WOLF CREEK

TABLE 9.5E-1 (Sheet 27)

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WCGS

b. The reactor coolant makeup function shall be capable of maintaining the reactor coolant level above the top of the core for BWRs and be within the level indication in the pressurizers for PWRs.

c. The reactor heat removal function shall be capable of achieving and maintaining decay heat removal.

d. The process monitoring function shall be capable of providing direct readings of the process variables necessary to perform and control the above functions.

e. The supporting functions shall be capable of providing the process cooling, lubrication, etc., necessary to permit the operation of the equipment used for safe shutdown functions.

3. The shutdown capability for specific fire areas may be unique for each such area or it may be one unique combination

In general, the performance goals of III.L.2 are satisfied except that in some cases pressurizer water level is not indicated within level indication. This is acceptable since the evaluation demonstrates that unrecoverable conditions are not reached.

Markup of Calculation XX-E-013

CALCULATION SHEET		CALCULATION NO. <u> XX-E-013 </u>
		REVISION NO. <u> 2 </u> Page 15
Area of change	<p>Basis: NRC Generic Letter 86-10, Response to Question 7.2; NEI 00-01, Rev. 2, Paragraph 3.1.1.6.</p> <p>3-A-3 Design basis fires are not assumed to occur concurrently with non-fire related failures in safety systems, plant accidents, or the most severe natural phenomena.</p> <p>Basis: NRC Generic Letter 86-10, Response to Question 7.2; NUREG 0800, Section 9.5-1, Rev. 3, paragraph C.1.b.</p>	
	<div style="border: 1px solid black; padding: 5px;"><p>3-A-4 For fire in areas requiring alternative shutdown capability (i.e., where control room evacuation may be necessary), a loss of automatic functions is assumed. For example, in the event of a loss of offsite power the emergency diesel generators will normally start automatically on undervoltage. However, in developing the alternative shutdown, capability of this automatic start feature to operate is not assumed.</p><p>Basis: NRC Generic Letter 86-10, Response to Question 3.8.4; NEI 00-01, Rev. 2, Paragraph 3.3.1.1.4.1.</p><p>For a fire in areas requiring alternative shutdown capability (i.e., control room), loss of automatic function of valves and pumps with control circuits that could be affected by a control room fire is assumed, except that an automatic feedwater isolation signal (FWIS) is unaffected by a fire in the control room.</p><p>Basis: NRC Generic Letter 86-10, Response to Question 3.8.4; NEI 00-01, Rev. 2, Paragraph 3.3.1.1.4.1; License Amendment XXX (LAR number will be assigned after approval of LAR)"</p></div>	
	<p>3-A-5 For fire areas not requiring an alternative shutdown capability, automatic operation of components and logic circuits is credited in the analysis only where the control circuits associated with the automatic operation are known to be unaffected by the postulated fire (i.e., III.G.2 separation requirements are satisfied).</p> <p>Basis: 10 CFR 50, Appendix R, Specific Requirements Sections III.G.1 and III.G.2; NEI 00-01, Rev. 2, Paragraphs 3.1.1.10 and 3.3.1.1.4.1.</p> <p>3-A-6 Off-site power may or may not be available. The maximum duration of any loss of offsite power event is assumed to be 72 hours.</p> <p>Basis: 10 CFR 50, Appendix R, Section III.L.3; NUREG 0800, Section 9.5-1, Rev. 3, paragraph C.1.b.</p> <p>3-A-7 Loss of offsite power has been specifically evaluated for every fire area to demonstrate where a LOOP may occur as a result of a fire. For alternate shutdown, a LOOP is considered as a simultaneous event. (Appendix 2 identifies fire areas where a fire may cause a LOOP)</p> <p>Basis: 10 CFR 50, Appendix R, Section III.L.3; NUREG 0800 Position C5.c.(3); NEI 00-01, Rev. 2 paragraph 3.1.1.7.</p> <p>3-A-8 Failure of onsite power supplies is not assumed unless it is caused as a direct consequence of a fire.</p> <p>Basis: 10 CFR 50, Appendix R, Section III.L.3; NUREG 0800 Position C5.c.(4); NEI 00-01, Rev. 2, Paragraph 3.1.1.7.</p>	

Control Room Layout

Enclosure to ET 12-0033

**Drawing E-1F9915, Revision 4, "Design Basis Document for Procedure OFN RP-017,
Control Room Evacuation"**
(167 pages)

COVER SHEET

DRAFT MARKUP ASSOCIATED WITH
LICENSE AMENDMENT REQUEST
LETTER
ET 12-0033

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THIS DWG. SUPERSEDED BY	REV.	THIS DWG SUPERSEDES	REV.
REVISION NOTES:			
		ELECTRONIC APPROVAL	
DESIGN BASIS DOCUMENT FOR OFN RP-017, CONTROL ROOM EVACUATION			
SCALE	DRAWING NUMBER	SHEET	REV
NONE	E-1F9915	1	4

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Appendix 1 – OFN RP-017 Credited Component Evaluation

Appendix 2 – Control Room Fire Consequence Evaluation for Motor Operated Valves

1.0 Purpose

The purpose of this document is to provide a technical basis for procedure OFN RP-017, Control Room Evacuation (due to fire) and define the timing basis for each action step within OFN RP-017.

2.0 Scope and Assumptions

2.1 Scope

This document applies to procedure OFN RP-017.

2.2 Assumptions

The following assumptions are applied when developing the Wolf Creek strategy for shutting down and maintaining hot standby using procedure OFN RP-017.

- 2.2.1 Only fire-induced failures are postulated to occur and all equipment is in normal operating state at the time of the fire.
- 2.2.2 Response Not Obtained (RNO) actions are included as operator aids and exceeds the procedural guidance required by regulation. It is not expected that the RNO actions will be necessary unless the primary action is affected by the fire.
- 2.2.3 Prior to transfer of control to the Auxiliary Shutdown System only a single spurious actuation is assumed to occur at a time, except in the case of two redundant valves in a high/low pressure interface line. All potential spurious actuations are mitigated/prevented using OFN RP-017 but timing is based on the spurious actuations occurring one at a time, or two at a time in the case of high/low pressure interface lines.
- 2.2.4 The Wolf Creek Fire Protection licensing basis, as described in USAR, Section 9.5.1, requires that a loss of off-site power be assumed in conjunction with a control room fire. However, a loss of offsite power may not be the most conservative assumption for every fire scenario. Therefore, the thermal hydraulic calculations were performed assuming off-site power is available and off-site power is not available to determine the most conservative outcome. The results of the thermal hydraulic calculation are presented in evaluation SA-08-006.
- 2.2.5 Automatic functions capable of mitigating spurious actuations are assumed to be defeated by damage to cables located in the area associated with the automatic function.
- 2.2.6 The reactor is tripped prior to evacuation of the control room. This is the only action assumed to work prior to evacuation. Tripping the reactor is considered to be $t = 0$ seconds for the purpose of timing subsequent steps.
- 2.2.7 Transfer of control to the alternative or dedicated shutdown system is assumed to occur when all isolation and transfer switches have been manipulated per procedure OFN RP-017. These switches are either located at the Auxiliary Shutdown Panel or at the local equipment.

3.0 Methodology

The methodology for completing this document is described in this section.

Each section and step within OFN RP-017 was reviewed and a technical basis for the section or step was documented.

Section 1.0 describes the purpose of E-1F9915. Section 2.0 identifies the scope. Section 4.0 lists the references used to compile E-1F9915.

Section 5.0 provides background information on OFN RP-017.

Section 6.0 is a summary of each PFSSD function and the major equipment associated with the function. In addition, Section 6.0 summarizes the timing requirement to ensure the function is satisfied per the times justified in Section 7.0.

Section 7.0 provides a technical review of each section in OFN RP-017. First, the front-end sections are discussed and a technical basis provided. These front-end sections include the Purpose, Symptoms or Entry Conditions, and References and Commitments.

Next, each Action/Expected Response and Response Not Obtained step within OFN RP-017 is tabulated in Table 7.1. The columns and the information provided in each column are described below.

- Step Number - The step number identified in OFN RP-017, revision 31.
- Step Description - The Step wording taken verbatim from the procedure.
- PFSSD Function - This column describes the PFSSD function that is satisfied by performing the Step. Functions are as follows: R - Reactivity Control; M - Reactor Coolant Makeup and Inventory Control; D - Decay Heat Removal; P - Process Monitoring; S - Support. If the step does not satisfy a specific function, then N/A is placed in the column.
- Basis - This column provides useful information about the step and why it is included in the procedure.
- Required Time to Complete - This column describes the maximum time that the operator has to complete the step to ensure the function supported by the step is satisfied. Completion of a step after the time indicated does not necessarily mean unrecoverable conditions would be reached but it would be beyond that which has been analyzed. Further analysis would be needed to determine the impact of not meeting a time limit identified in this document.
- Timing Basis - This column describes the basis for the maximum allowed operator response time given in the previous column. The basis is derived from a number of calculations and evaluations as described in the column.
- Control Room Fire Impact - This column describes whether a fire in the control room could cause the component to spuriously operate after the Step and any identified pre-requisite Steps are complete. If yes, then further discussion is provided for why it is acceptable.
- Prerequisite Steps - This column identifies the Step(s) that are required to be completed prior to completing the Step. Prerequisites are steps that must be completed before the current step to prevent potential damage to equipment or prevent spurious operation of the equipment after the step is completed and the Operator moves on. A step that restores power to a component is not considered a prerequisite. These pre-requisites are listed to provide reasonable assurance that future procedure changes will not improperly re-order the steps.

4.0 References

4.1 Wolf Creek Documents

4.1.1 Procedure OFN RP-017, Revision 40 - Control Room Evacuation

4.1.2 Wolf Creek Operating License NPF-42

4.1.3 Wolf Creek Safety Evaluation Report including Supplements 1 through 5

4.1.4 Wolf Creek Technical Requirements Manual (TRM), Revision 38

4.1.5 SNUPPS Letter SLNRC 84-0109 - Fire Protection Review

4.1.6 Memo from NRC to KG&E dated August 31, 1984 - Minutes of August 22, 1984 Meeting with

Kansas Gas and Electric and Union Electric Company

- 4.1.7 Calculation XX-E-013, Post-Fire Safe Shutdown Analysis
- 4.1.8 Safety Analysis Evaluation SA-08-006, Rev. 2 - Retran-3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire
- 4.1.9 Calculation Change Notice AN-02-10-000-02 - EDG Room Temperature at Various Outside Air Temperatures for the NRC Triennial Fire Protection Inspection
- 4.1.10 Calculation EF-10 - ESW System Flow Requirements
- 4.1.11 Drawing M-018-000155 - Operation of Diesel Engine without Cooling Water
- 4.1.12 Drawing J-14001 - Control Room Equipment Arrangement
- 4.1.13 Drawing E-13EF06A - Schematic Diagram ESW to Ultimate Heat Sink Isolation Valves
- 4.1.14 Drawing E-025-00007, Sheet 185 - EFHV0038 Design Configuration Document
- 4.1.15 Document E-10NK - Class 1E 125 VDC System Description
- 4.1.16 Specification M-018 - Standby Diesel Generator
- 4.1.17 PIR 2005-3314/CR2007-003037 - Issues involving NRC Information Notice 92-18
- 4.1.18 CR 00012368 – Timing Basis for Re-Establishing Room Cooling
- 4.1.19 CR 00016481 – Guidance for Control Room Re-Entry After Fire
- 4.1.20 CR 00019239 – Time to Close Valve BNHV8812A
- 4.1.21 CR 00019242 – Train B Emergency Diesel Generator Potential Failure to Start
- 4.1.22 CR 00020612 – Amphenol Connectors for MSIVs cannot be Removed by Hand
- 4.1.23 CR 00023410 – Issues with the Train B Emergency Diesel Generator Voltage Regulator
- 4.1.24 CR 00030350 – Post-Fire Safe Shutdown Concern with Train B Diesel Generator Field Flashing
- 4.1.25 CR 00030376 – Revise E-1F9915 to Document Time to Establish Diesel Engine Cooling
- 4.1.26 CR 2008-004708 – Determine Time to Establish Diesel Engine Cooling
- 4.1.27 CR 00041746 – Spurious Operation of Valve EFHV0060
- 4.1.28 Calculation KJ-M-017, Rev. 0 - Emergency Diesel Standby Generator (KKJ01B) Runtime Without ESW Flow
- 4.1.29 CR 00041746 - Potential for EFHV0060 to Open Due to Control Room Fire
- 4.1.30 CR 00044460 – Add OFN RP-017 Component Evaluation to E-1F9915
- 4.1.31 CR 00046642 – RCP Seal Return Valves
- 4.1.32 CR 00046702 – Auxiliary Shutdown Panel Controls for B Motor Driven Auxiliary Feedwater Pump
- 4.1.33 CR 00046707 – Review Reactor Trip Switch Circuits for Alternative Shutdown

4.2 Nuclear Regulatory Commission Documents

- 4.2.1 10 CFR 50.48 - Fire Protection
- 4.2.2 10 CFR 50, Appendix R - Fire Protection Program for Nuclear Power Facilities Operating Prior to January 1, 1979
- 4.2.3 NRC Generic Letter 86-10 - Implementation of Fire Protection Requirements
- 4.2.4 NRC Information Notice 2005-14 - Fire Protection Findings on Loss of Seal Cooling to Westinghouse Reactor Coolant Pumps
- 4.2.5 Regulatory Guide 1.189, Rev. 2 – Fire Protection for Nuclear Power Plants

4.3 Other Documents

- 4.3.1 Westinghouse WCAP-16396-NP, Westinghouse Owners Group Reactor Coolant Pump Seal Performance for Appendix R Assessments.
- 4.3.2 Westinghouse Technical Bulletin TB-04-22, Rev. 1, Reactor Coolant Pump Seal Performance – Appendix R Compliance and Loss of All Seal Cooling.
- 4.3.3 NEI 00-01, Rev. 2 – Guidance for Post-Fire Safe Shutdown Circuit Analysis
- 4.3.4 Westinghouse Letter LTR-RAM-I-10-053 dated October 15, 2010. Subject: White Paper Westinghouse Reactor Coolant Pump Seal Behavior For Fire Scenarios, Revision 2.

5.0 Background

The Control Room evacuation and plant shutdown procedure is documented in OFN RP-017 (power operation to hot standby) and OFN RP-017A (hot standby to cold shutdown). The original basis for procedure OFN RP-017 is SLNRC 84-0109, which documents a phased approach to shutting down the plant and maintaining it in a safe hot standby condition if control room evacuation is required following a fire. This phased approach was approved by the NRC in Supplement 5 of the Wolf Creek Safety Evaluation Report.

Although SLNRC 84-0109 formed the original licensing basis for hot shutdown from outside the control room at SNUPPS facilities, its basis is not clearly defined nor understood. Some of the step sequences and actions are questionable by today's operational and regulatory standards. Over the years, changes have been made to OFN RP-017, which were not in literal compliance with the letter. The changes were subsequently determined to not have an adverse impact on the health and safety of the public. However, because of the confusing nature of the letter, it was decided that a design basis document that clearly describes the basis for OFN RP-017 is needed.

License Amendment **XXX** approved superseding letter SLNRC 84-0109 with document E-1F9915 as the basis for alternative shutdown in the event of a fire in the control room. Therefore, letter SLNRC 84-0109 is considered historical and is no longer part of the approved fire protection program.

6.0 Summary of Timing Basis

This Section includes a summary of the major equipment credited in OFN RP-017 for satisfying each PFSSD function (Reactivity Control, Reactor Coolant Makeup and Inventory Control, Decay Heat Removal, Process Monitoring and Support). In addition, operator response timing, to ensure the function is satisfied prior to reaching unrecoverable conditions, is discussed.

6.1 Reactivity Control

Reactivity control is achieved by tripping the reactor prior to leaving the control room. Tripping the reactor is considered to be $t = 0$ seconds for the OFN RP-017 timeline. (Assumption 2.2.6)

The main steam isolation valves (MSIVs) and steam generator (SG) blowdown valves are isolated to prevent return to criticality due to uncontrolled cooldown. The MSIVs are assumed to remain open until action is taken outside the control room within 3 minutes to close them. Prior to evacuating the control room, operators attempt to close the MSIVs using the all-close hand switches, but this action is assumed to fail. In these cases, the steam dumps are assumed to operate properly to control temperature to 557°F, then the steam dumps are isolated within 7 minutes by de-energizing power to the valves, at which time the ARVs are used for temperature control. All components located downstream of the MSIVs are assumed to be unaffected by the fire.

Plant cooldown is controlled using SGs B and D atmospheric relief valves (ARVs) while SGs A and C ARVs are closed. Based on Calculation SA-08-006, a single SG ARV can remain open for 1 hour with no adverse impact on safe shutdown. Otherwise, all SG ARVs are assumed to function normally at time 0, controlling pressure less than 1184.7 psia. Steam generators B & D ARVs are assumed to close at 7 min then control as necessary at 561 degrees F after the operator takes manual control of the B & D ARVs from the auxiliary shutdown panel (ASP). Steam generators A & C ARVs are assumed to close at 7 minutes, then stay closed after the operator at the ASP closes them per procedure.

The main turbine trips in response to a reactor trip through an interlock from the reactor trip breakers that is unaffected by a fire in the control room. Therefore, steam loss through the turbine is prevented.

The Train B Chemical and Volume Control System (CVCS) is used to provide borated water to the RCS to maintain negative reactivity conditions. This is accomplished using the Train B centrifugal charging pump (CCP) taking suction from the borated refueling water storage tank (RWST) and injecting to the RCS through the boron injection tank (BIT). Calculation SA-08-006 assumes the Train B CVCS is lined up and injecting through the BIT within 28 minutes.

6.2 Reactor Coolant Makeup/Inventory Control

Reactor coolant makeup and inventory control is achieved by first isolating all potential RCS leakage and inventory reduction paths including pressurizer power operated relief valves (PORVs), normal letdown, excess letdown, reactor vessel head vents, reactor coolant pump seals, MSIVs, steam generator blowdown, steam generator ARVs, and residual heat removal (RHR) suction from the RCS. Leakage through the RHR system is not credible since the RHR pump suction valves are normally closed and de-energized. The reactor coolant pumps (RCPs) are stopped to prevent loss of inventory through the RCP seals.

Based on Calculation SA-08-006, pressurizer PORVs are assumed isolated within 3 minutes and normal letdown is assumed isolated within 7 minutes. Charging flow to the reactor coolant pump seals is assumed to be isolated within 10 minutes. The reactor coolant pumps are assumed to be stopped within 7 minutes. Steam generator ARVs and MSIVs are isolated as discussed in Section 6.1.

Letdown flow is assumed to be isolated within 7 minutes. In all scenarios where letdown is unaffected, initial flow is 120 gpm until isolated. The 120 gpm flow rate is based on normal letdown of 75 gpm plus an additional 45 gpm that could be flowing for Chemistry concerns (this rarely occurs). In the scenarios where letdown valves fail open, letdown flow goes to 195 gpm for 7 minutes, which is the maximum letdown flow. The automatic letdown isolation signal on low pressurizer water level (17%) is assumed to fail.

Pressurizer heater backup group B is cycled to maintain pressurizer pressure within 2000 to 2300 psig. In the loss of off-site power scenarios, Calculation SA-08-006 assumes pressurizer heaters fail to operate at time zero. At 11.5 minutes, backup group B is controlled at the ASP. In the non loss of off-site power scenarios, all three heater groups operate normally but power to backup group B is lost by procedure

within 7 minutes. Power is restored within 11.5 minutes and control on backup group B is available from the ASP.

Calculation SA-08-006 assumes the steam generator blowdown valves function normally except in the scenarios where the blowdown valves are assumed to remain open. In these scenarios, the blowdown valves remain open for the duration of the modeled run (1-hour).

Calculation SA-08-006 assumes the pressurizer and auxiliary pressurizer spray valves operate normally except in those scenarios where the pressurizer spray is assumed to fail. In those scenarios, the pressurizer spray valves are assumed to open at time zero and pressurizer spray stops at 7 minutes when the RCPs are stopped. Auxiliary spray is assumed to operate at time zero and stops in 7 minutes when PK5117 is opened in Step D1.

The Train B CVCS is used for makeup and inventory control by taking suction from the RWST and injecting through the BIT. Calculation SA-08-006 assumes the Train B CVCS is lined up and injecting through the boron injection tank (BIT) within 28 minutes.

A potential concern with inventory control is that a control room fire could cause the number 1 seal return valves (BBHV8141A, B, C and D) to close, which could cause excessive RCS leakage. OFN RP-017 isolates RCP seal cooling, contributing to this event. OFN RP-017 also trips the RCPs, which minimizes the impact of this event.

A white paper prepared by Westinghouse and distributed as letter number LTR-RAM-I-10-053 (Reference 4.3.4) summarizes RCP seal behavior for fire scenarios. This white paper is a compilation of several WCAPs and Technical Bulletins on the subject.

Table 1 in the letter is a scenario matrix that identifies the number 1 and number 2 RCP seal behavior and resultant leakage given RCPs running or not running and seal cooling available or not available. For the scenario postulated here (Number 1 seal return line isolated, RCPs not running and no seal cooling), the resultant leakage from Table 1 is 21 gpm per seal or 84 gpm total. This leakage is well within the makeup capability of the charging pump, which has a design flow rate of 150 gpm at 2800 psi and a runout flow of 550 gpm at 606 psi. Therefore, this condition does not pose a concern for PFSSD at Wolf Creek.

6.3 Decay Heat Removal

Hot standby decay heat removal is achieved using Train B motor driven auxiliary feedwater pump (MDAFP), taking suction from the condensate storage tank (CST), to supply feedwater to steam generator D and the turbine driven auxiliary feedwater pump (TDAFP), taking suction from the condensate storage tank (CST), to supply feedwater to steam generator B.

Calculation SA-08-006 assumes the Train B MDAFP is lined up and supplying steam generator D within 15 minutes and the TDAFP is lined up and supplying steam generator B within 35 minutes. Steam generators B and D atmospheric relief valves are used to control reactor coolant system (RCS) temperature. Steam generators A and C atmospheric relief valves are isolated. See Section 6.1 for discussion about steam generator ARVs.

The reactor is tripped at $t = 0s$ when operators actuate the reactor trip push buttons prior to evacuating the control room. The reactor trip causes a low T_{avg} signal within 5 seconds and initiates a feedwater isolation signal, which stops main feedwater flow and prevents steam generator overfill from main feedwater.

To prevent steam generator overfill in cases where the fire causes a spurious auxiliary feedwater actuation signal (AFAS), the Train A MDAFP is stopped by operator action within 15 minutes. The TDAFP is taken to minimum output within 15 minutes and remains there until valves in the AFW discharge line are closed, which takes 35 minutes. At that point, the TDAFP is started to supply SG B.

Main steam isolation valves are required to be closed for decay heat removal to control cooldown. See Section 6.1 for discussion about MSIVs.

Cold shutdown decay heat removal is not included in OFN RP-017.

6.4 Process Monitoring

Process monitoring ensures RCS variables are within specified limits. The ASP contains all the required process monitoring instruments to verify reactivity conditions, pressurizer level, pressurizer pressure, RCS temperature and steam generator level. Source range indicator SENI0061X indicates reactivity level. Pressurizer level is determined by BBLI0460B. Pressurizer pressure is determined using reactor vessel pressure instrument BBPI0406X. RCS temperature is determined using RCS loop 2 cold leg temperature indicator BBTI0423X and loop 4 hot leg temperature indicator BBTI0443A. Steam generator level is determined using steam generators B and D narrow range level indicators AELI0502A and AELI0504A, respectively. These process monitors are unaffected by a fire in the control room.

6.5 Support

The post fire safe shutdown support function provides the necessary cooling, ventilation and electrical power required by the reactivity control, reactor makeup, decay heat removal and process monitoring functions. The support function supports all the other post fire safe shutdown functions and includes component cooling water (CCW), essential service water (ESW), room cooling and ventilation, control room isolation and electrical power distribution.

Component cooling water is required for OFN RP-017 to supply cooling to the Train B charging pump oil cooler and the seal water heat exchanger. Both of these components support centrifugal charging pump (CCP) operability. Therefore, CCW is required to be operable prior to the need for charging. Based on Calculation SA-08-006, charging needs to be lined up and injecting within 28 minutes.

Essential service water is required to provide cooling to the CCW heat exchanger, emergency diesel engine coolers and various room coolers. In addition, ESW is a backup source of auxiliary feedwater.

Emergency diesel engine cooling is required to maintain the engine jacket water temperature below the trip setpoint of 195°F. The engine is started in Step C6 when the offsite power feeder breakers are opened, which provides an automatic start signal to the engine. Step C8.e closes the Train B emergency diesel generator (EDG) output breaker and step C9 starts the ESW pump. The combined generator loading of the non-shed loads and the ESW pump is 3,615.9 kW per calculation KJ-M-017, which is 58.3% of the EDG rating of 6,201 kW. At this point, service water (SW) crosstie valve EFHV0026 is not closed and it is assumed that the ESW flow is diverted to the SW system. Therefore, no EDG cooling benefit is assumed after the start of the ESW pump. Step C12 closes EFHV0026, at which point EDG cooling can be credited.

Table 1 in Calculation KJ-M-017 identifies the allowable time to establish EDG cooling given various values of unloaded times from 1 minute to 5 minutes in 15 second increments. The table shows that, as the time to complete steps C6 through C8 increases, the time to complete Steps C9 through C12 decreases. For example, if step C8 is completed in 2.5 minutes after step C6, operators have 2.51 minutes to complete Steps C9 through C12 and close EFHV0026. However, if the operator takes 3.5 minutes to complete Step C8 after Step C6 is completed, then they only have 2.22 minutes to complete Steps C9 through C12 and close EFHV0026. Table 1 from Calculation KJ-M-017 follows.

Time Unloaded (Min)	Allowable Time Loaded (Min)	Time Unloaded (Min)	Allowable Time Loaded (Min)
1	2.80	3.25	2.28
1.25	2.75	3.5	2.22
1.5	2.69	3.75	2.12
1.75	2.63	4	1.98
2	2.57	4.25	1.85
2.25	2.51	4.5	1.71
2.5	2.45	4.75	1.58
2.75	2.39	5	1.44
3	2.33		

Room coolers and ventilation fans are used to maintain a suitable environment for the equipment within the room to ensure long term operation of the equipment. Room coolers credited in the event of a control room fire are as follows:

1. Train B Class 1E Electrical Equipment Room A/C Unit (SGK05B)
2. Train B Electrical Penetration Room Cooler (SGL15B)
3. Train B Component Cooling Water Pump Room Cooler (SGL11B)
4. Train B Auxiliary Feedwater Pump Room Cooler (SGF02B)
5. Train B Centrifugal Charging Pump Room Cooler (SGL12B)
6. Train B Containment Coolers (SGN01B and SGN01D)
7. Train B ESW Pump Room Supply Fan (CGD01B) and Dampers (GDTZ11A and GDTZ11C)

Procedure SYS GK-200 allows up to 2 hours to pass after loss of one Train of Class 1E Electrical Equipment Room A/C before compensatory measures are established to restore cooling to the affected Train. For conservatism, this design basis document uses 60 minutes as the requirement to restore Class 1E Electrical Equipment Room A/C.

The timing basis for establishing electrical penetration room cooling is documented in CR 012638. Based on the evaluation in CR 012638, 1 hour should be used as the maximum time to restore cooling to the electrical penetration rooms. This time is based on the Wolf Creek Technical Requirements Manual (TRM), TR 3.7.22-1 which states that operators have 8 hours to restore room temperatures to within allowable limits given in Table TR 3.7.22-1. (Note that the TRM revision in effect when the CR was evaluated (Revision 35) required equipment to be declared inoperable if temperatures were not restored within 4 hours. The current revision of the TRM (38) does not require equipment to be declared inoperable). For conservatism, 1-hour is used as the timing basis in E-1F9915. The allowable temperature limit for the electrical penetration rooms is 101 degrees F per Table TR 3.7.22-1. Based on operator timing, the electrical penetration room cooler is started within 13 minutes. Therefore, the time to restore electrical penetration room cooling is well within the 1-hour limit established in E-1F9915.

The pump room coolers (SGL11B, SGF02B and SGL12B) automatically start when the pump starts. Procedure OFN RP-017 lines up power and ESW flow to the pump room coolers prior to starting the pumps. Therefore, pump room cooling will be provided as soon as each pump starts.

The containment coolers maintain containment temperature within acceptable limits but are not directly required for safe shutdown after a fire in the control room. There are no post-fire safe shutdown components in containment that will adversely impact the ability to achieve safe shutdown if the coolers are not started. Therefore, the timing for this step is not critical and, therefore, no time limit has been established.

The timing basis for establishing ESW pump room ventilation is documented in CR 012638. Based on the evaluation in CR 012638, 1 hour should be used as the maximum time to restore cooling to the ESW pump room. This time is based on the Wolf Creek Technical Requirements Manual (TRM), TR 3.7.22-1 which states that operators have 8 hours to restore room temperatures to within allowable limits given in

Table TR 3.7.22-1. (Note that the TRM revision in effect when the CR was evaluated (Revision 35) required equipment to be declared inoperable if temperatures were not restored within 4 hours. The current revision of the TRM (38) does not require equipment to be declared inoperable). For conservatism, 1-hour is used as the timing basis in E-1F9915. The allowable temperature limit for the ESW pump rooms is 119 degrees F per Table TR 3.7.22-1. Based on operator timing, the ESW pump room supply fan is started approximately 12 to 15 minutes after the ESW pump is started. In addition, Step A16 directs an available operator to check ESW pump room temperature. Based on operator timing, Step A16 is reached in less than 20 minutes. At this point, the Site Watch, who has no fire brigade or OFN RP-017 duties, could be dispatched to the ESW pumphouse to check room temperatures and make adjustments as necessary per the Step A16 RNO column. Therefore, the time to restore room cooling in the ESW pump room is well within the 1-hour limit established in E-1F9915.

7.0 Section-by-Section Review

7.1 OFN RP-017, Section 1.0 - Purpose

7.1.1 OFN RP-017, Section 1.1

- 1.1 *To provide operator actions for evacuating the Control Room due to fire, establishing plant control from the Auxiliary Shutdown Panel (ASP), and reactor shutdown to Hot Standby conditions.*

Basis – 10 CFR 50, Appendix R, Section III.L.3 requires procedures to be in effect to implement the alternative and dedicated shutdown capability for any fire area utilizing the provisions in Appendix R, Section III.G.3. Wolf Creek took no exception to this requirement in the Appendix R comparison documented in the USAR, Table 9.5E. Letter SLNRC 84-0109 (August 23, 1984), Section 2.0 Response Plan Summary states, in part, "Procedures will be developed to implement this plan at Callaway and Wolf Creek." The Wolf Creek SER, Supplement 5, Page 9-12 states, in part, "(1) The applicant will revise the procedures for a fire in the control room in accordance with the SNUPPS letter of August 23, 1984 ..." Therefore, Wolf Creek is committed to maintain in effect procedure OFN RP-017 to achieve hot standby conditions. Cold shutdown is achieved from outside the control room using OFN RP-017A.

7.1.2 OFN RP-017, Section 1.2

- 1.2 *This procedure should only be used when the Control Room is uninhabitable and damage to controls or Control Room equipment has occurred or is imminent.*

Basis - This statement emphasizes that control room evacuation should only take place when control from the control room is lost or will be lost. Shutting down from outside the control room is not desired and evacuation should only be done when the plant cannot be controlled from inside the control room.

7.1.3 OFN RP-017, Section 1.3

- 1.3 *Since the Control Room is uninhabitable, this procedure includes actions to:*

- *Prevent subsequent fire/physical damage to Control Room circuits from adversely affecting systems needed to maintain Hot Standby*
- *Transfer critical Train B controls to the ASP*
- *Maintain the plant in Hot Standby from the ASP*

Basis - This step identifies the objectives for OFN RP-017. It clearly states that the procedure is only intended to maintain hot standby from outside the control room using Train B components. Cold shutdown is achieved using procedure OFN RP-017A.

7.2 OFN RP-017, Section 2.0 - Symptoms or Entry Conditions

Section 2.0 provides conditions in which operators may deem entering OFN RP-017 to be necessary. These entry conditions are not licensing commitments but rather guidance for operators to use when determining the need to enter OFN RP-017. The decision is a judgment call made by operating staff with the final decision made by the Shift Manager. Step 1 in the procedure provides additional conditions to be considered prior to evacuating the control room. There are no NRC criteria for establishing the point at which operators evacuate the control room. Therefore, there is no licensing basis for when control room evacuation takes place.

7.3 OFN RP-017, Section 3.0 - References and Commitments

7.3.1 OFN RP-017, Section 3.1 - References

a. *Nuclear Safety Engineering Surveillance Report No. 1991-005*

Basis - This surveillance report, designated SSR 91-005, was performed by Wolf Creek Nuclear Safety department and was issued on 4/26/1991. The purpose of the surveillance was to determine the adequacy of 10CFR50.59 screenings on Operations procedures. OFN 00-017, Control Room Evacuation, Revision 13 was chosen for review. The review concluded that the 50.59 screenings were appropriate but made 12 recommendations for improvement of the procedure. Most of the recommendations were incorporated into revision 14 of OFN 00-017 and some were not with justification. The changes made to OFN 00-017 as a result of this surveillance that are still in effect today in OFN RP-017 are listed below:

1. NK4101 is no longer opened to remove control power from Train A bus NB01 breakers. The observer stated that by opening the switch, the Train A AFW pump would not be able to be controlled from the ASP. Operations removed the step due to there being no requirement to open the switch. Train A equipment is not required for OFN RP-017. However, it may be practical to open NK4101 to support Step C15 (Stopping the Train A Containment Spray Pump).
2. Fuse #46 in panel RP209 is pulled to fail close the MSIV bypass valves. The observer noted that opening the breaker would remove power from other equipment and felt that this is not a good idea. He also noted that Callaway pulls fuses to close the MSIV bypass valves. Step B12 pulls fuse #46 in RP209.
3. NK4411 is used to isolate steam generator blowdown. This differs from SLNRC 84-0109, which says to use the switches in the Radwaste Control Room. Use of NK4411 will achieve the desired result faster than sending an operator to the Radwaste Control Room. See Step C27.
4. As a result of recommendation 12, an attachment was added to give operators instruction to protect Train A equipment after all other critical steps are completed. Attachment F provides guidance based on this recommendation.

b. *USAR 7.4.6, Safe Shutdown From Outside The Control Room*

Basis - USAR Section 7.4.6 describes the capability of Wolf Creek to shutdown from outside the control room using the Auxiliary Shutdown Panel (ASP), switchgear and motor control centers. The mitigating actions for a fire in the control room use Train B ASP and equipment. Train B was selected because instrumentation and controls for the turbine driven auxiliary feedwater pump are located on the Train B ASP.

c. *USAR Appendix 9.5B, Fire Hazards Analyses*

Basis - The Fire Hazards Analysis is now located in document E-1F9905, which is incorporated into the USAR, Appendix 9.5B by reference.

d. *PIR 1997-2819, EDG Master Transfer Switch In Auto With Fire In The Control Room*

Basis – PIR 1997-2819 identified a concern where OFN RP-017 did not previously require placing master transfer Switch KJHS0109 in Local/Manual position. The initiator stated that if the switch were left in Auto position, a control room fire could affect the circuits and shut down the diesel generator. After review of the circuits, OFN RP-017 was revised to require operators to place KJHS0109 in Local/Manual. Step C.8.b proceduralized this action. Also see PIR 2006-000860 discussion below.

e. *PIR 1997-2453, Enter OFN RP-013 At 2 mR/hr Submersion Dose Rate*

Basis – PIR 1997-2453 identified a concern where OFN RP-017 previously required evacuation of the control room if radiation reached certain levels. As a result, OFN RP-017 was revised to allow Health Physics and Shift Supervisor discretion on whether to evacuate. PIR 1997-3376 was also written to evaluate the need to evacuate the control room at all for radiation levels. OFN RP-017 was revised to remove the specific radiation levels and allow the Shift Supervisor to enter OFN RP-013 at his discretion.

f. *OP 1988-0190, Replacing BG HV-8105 with local valves within the NCP room*

Basis – This is an inter-office correspondence that requested a procedure change to OFN 00-017 (now OFN RP-017) to reduce the time to complete certain actions. The procedure required an operator to first open BGFCV0121 locally in the positive displacement pump (PDP) room (now the normal charging pump (NCP) room) on the 1974 elevation then the same operator had to ascend to the north pipe penetration room on the 2000 elevation to locally close BGHV8105. The memo requested that instead of closing BGHV8105, valves BG8402B and BGV0017 be manually closed or verified closed. These valves are located in the NCP room along with BGFCV0121. The change was made as requested and OFN RP-017 uses BG8402B and BGV0017.

g. *PIR 1999-109, Removing control power prior to rotating ESF bus #2 isolate switch*

Basis – This PIR identified 3 issues where OFN RP-017, Revision 11 was not consistent with the original response strategy for control room fires documented in SLNRC 84-0109 (Superseded by E-1F9915). These issues are discussed below:

Issue 1 – Note 10 in SLNRC 84-0109 states that FCHV0312 and ABHV0005 will not be opened until it is verified that ALHV0036 is open. There are two loop steam supply valves to the turbine driven auxiliary feedwater pump (TDAFP) (ABHV0005 (loop 2) and ABHV0006 (loop 3)). SLNRC 84-0109 only credited ABHV0005 to provide a steam supply to the TDAFP. OFN RP-017, Rev. 11 Step A9 required the operator at the ASP to open steam supply valve ABHV0006 using ABHIS0006B prior to verifying that suction valve ALHV0036 is open. However, OFN RP-017, Rev. 11 Steps A6 and A8 had the same operator at the ASP close the turbine trip and throttle valve (FCHV0312) using FCHIS0312B and the turbine governor valve (FCHV0313) using FCHS0313 and FCHIK0313. Step A7 required the operator at the ASP to isolate ABHV0005 using ABHIS0005B. The requirement in SLNRC 84-0109 has been met in that FCHV0312 and ABHV0005 are maintained closed until ALHV0036 is opened. However, ABHV0006 was added to the procedure at some later time. Since FCHV0312 is maintained closed, the TDAFP will not operate even with ABHV0006 open.

Issue 2 – This issue involves performing steps in the procedure in a different sequence than what was approved in SLNRC 84-0109. Note 2 in SLNRC 84-0109 states that DC power should be tripped after Action 9 [assure MCC and load center breakers are closed]

in room 3302 so that breakers can be electrically tripped by hand to the desired position. OFN RP-017, Rev 11 had operators' open the control power breakers to the NB02 bus and then rotate switch NBHS0014 to the isolate position. By opening the control power breaker before rotating NBHS0014, relay 195 will not energize and the control room will not be isolated.

Revision 18 of OFN RP-017 deleted NBHS0014 from the procedure. The hand switch would not have completely isolated the control room from the control circuit on the affected components. Also, a control room fire could have opened the control power fuse due to a hot short, thereby isolating control power prior to operation of the hand switch.

The current revision of OFN RP-017 requires operators to remove control power from the NB02 bus and not use NBHS0014. Isolating control power will prevent spurious operation of any of the breakers associated with NB02. The possibility still exists for the NB02 breakers to close prior to isolating control power. Therefore, to ensure the NB02 bus loads are shed, each pump breaker, except for the ESW pump, is verified open prior to opening the NB02 feeder breakers to simulate a LOSP and start EDG-B. Verifying each of these breakers is open also ensures the diesel will not fail to start due to overload.

On the basis of the above discussion, the concern raised in Issue 2 of this PIR is no longer valid. The use of NBHS0014 would never have fully isolated the control room and, therefore, its use was never required. Isolation of control power to NB02 ensures spurious operation of the breakers will not occur. All revisions of OFN RP-017 (OFN 00-017) required isolation of control power to NB02 in Phase A. The intent of SLNRC 84-0109 is met since isolation of control power effectively prevents spurious operation due to cable failures in the control room.

Issue 3 – The third issue involves the closure of the MSIVs using a portable air supply versus an electrical source, as delineated in SLNRC 84-0109. The MSIVs are closed prior to leaving the control room using ABHS0079 or ABHS0080. However, their closure cannot be guaranteed due to possible fire damage. Therefore, OFN RP-017 has steps to close the valves if they failed to close in response to the fast close signal.

SLNRC 84-0109, Note 6 states that the MSIVs will be closed with a portable 125 VDC source. Wires to the valves will then be cut to leave the valves in the closed position. Prior to revision 27, OFN RP-017 used a portable air source to close the MSIVs. This change was made in MA 93-0181 with insufficient documentation for the change. The PIR evaluation provides adequate justification for the change and RCMS 1985-118 documents the change in commitment. Since the use of air versus power to close the MSIVs is a more reliable and safe method, it met the intent of SLNRC 84-0109 and was therefore acceptable.

The MSIVs were replaced in refuel outage 16 (DCPs 09952 and 11608) with solenoid actuated system medium operated valves. These valves do not require an accumulator or external air supply so the portable air source and associated air hoses and fittings are not required. The new MSIVs are held open by six normally energized solenoid valves, three associated with Train A and three associated with Train B. Either train of solenoid valves can operate the associated valve, independent of the opposite train solenoids which provides for diversity and electrical independence. De-energizing either train of solenoids will cause the MSIVs to close. Amphenol connectors, 3 per MSIV per train, have been provided near each MSIV to provide a way for operators to disconnect power to the solenoids and close the MSIVs. This method for closing the MSIVs is utilized in the current version of OFN RP-017.

- h. PIR 1999-107, Concerns with meeting required time frame*

Basis – This PIR was written to document whether changes made in revision 12 of OFN RP-017 meet the commitments made in SLNRC 84-0109. The PIR concluded that commitments were met and no changes were required.

i. PIR 1999-3648 Procedure not matching plant labels

Basis – This PIR addressed labeling inconsistencies between OFN RP-017 and the plant labels. The procedure was revised to match plant labeling.

j. PIR 2002-1956, Failure to properly track and implement actions specified within Regulatory Correspondence SLNRC 84-0109 as referenced in USAR Appendix 9.5B.

Basis – This PIR identifies concerns with OFN RP-017, Rev. 16 not meeting commitments in SLNRC 84-0109. The evaluation shows a step-by-step comparison of OFN RP-017, Rev. 16 with SLNRC 84-0109 and provides justification for any deviations. The PIR evaluation found that the deviations would not have prevented the safe shutdown of the plant. The deviations were historical with no documented evaluation in some cases. In many cases, the deviations were a result of alternative methods to produce the desired result. The alternative methods were determined to be faster and/or safer than that specified by SLNRC 84-0109. Note that the contents of USAR Appendix 9.5B is now contained in E-1F9905.

k. PIR 2003-3479, Revisions to procedures need fire protection review

Basis – This PIR identified problems associated with emergency lighting for equipment required to implement OFN RP-017. Changes have been made to the procedure over the years with no consideration given to emergency lighting requirements. As components were added or deleted from the procedure, consideration was not always given to emergency lighting requirements. As a result of the PIR, a number of emergency lighting changes were made to ensure each OFN RP-017 action has sufficient lighting in accordance with Wolf Creek commitments.

l. Westinghouse Tech Bulletin TB-04-22, Reactor Coolant Pump Seal Performance - App R Compliance and Loss of All Seal Cooling and WCAP 10541, Reactor Coolant Pump Seal Performance Following A Loss of All AC Power, NRC IN 2005-14, FP Findings on Loss of Seal Cooling to Westinghouse RCPs.

Basis – These documents describe industry positions on reactor coolant pump seal cooling. Because of the uncertainty of where the NRC may go in the future with RCP seal cooling issues, Wolf Creek decided to deviate from SLNRC 84-0109 and not restore seal cooling in response to a control room fire. Rather, Wolf Creek will use a natural circulation cooldown and provide RCS makeup and boration through the Boron Injection Tank (BIT) flow path, rather than the seal injection flow path. Revision 22 of OFN RP-017 made this change. The use of natural circulation to cooldown will not adversely impact the ability to achieve and maintain safe shutdown.

m/n. PIR 2005-3314 (later converted to PIR 2007-003037 in PILOT), Failure to Address NRC Information Notice 92-18.

Basis - This PIR was written to address URI 2005008-06, which was given to Wolf Creek during the Fall, 2005, NRC Triennial Fire Protection Inspection. Wolf Creek has responded to this issue by modifying the control circuit on 36 motor operated valves so a hot short from a fire in the control room will not bypass the valve protective features and prevent operation of the valve.

NRC IN 92-18 identified a concern where a control room fire could cause the spurious operation of motor operated valves due to hot shorts that bypass the valve protective features. The hot short, if sustained, could cause valve damage in a manner that prevents the valve from being manually operated to its desired position. Therefore, the ability to achieve safe shutdown after a control room fire could be compromised.

Wolf Creek initially responded to the IN by crediting the modifications that were done prior to startup in which the NRC required the installation of a number of isolation switches. However, these modifications did not address the concerns raised in IN 92-18. In April 1999 the NRC conducted an inspection at Callaway and questioned their response to IN 92-18, which was the same response given by Wolf Creek. As a result, Wolf Creek initiated PIR 1999-1245 to take another look at the issue. The PIR was closed in March 2001 with no actions taken due to the ongoing industry discussions with the NRC on the issue of hot shorts, as well as a moratorium placed on circuit inspections by the NRC. The PIR closure statement said that a new PIR will be generated when the industry initiative to address the issue is completed.

The NEI and EPRI conducted testing in 2001 to gain a better understanding of the issue of hot shorts causing spurious actuations. The testing found that under certain fire conditions, spurious actuations could occur due to hot shorts. In January 2005 the NRC resumed inspections of fire-induced safe shutdown circuits. However, the IN 92-18 issue remained unresolved at Wolf Creek and, until PIR 2005-3314 was written, a new PIR was not written as stated in PIR 1999-1245.

- o. PIR 2007-003003, Potential Loss of Field Flashing on Train B Emergency Diesel Generator*

Basis - This PIR (originally PIR 2005-3333) was written to identify a condition where field flashing could be lost on the Train B EDG due to a fire in the control room. Since Train B is the protected train in the event of a control room fire, this could have an adverse impact on the ability to achieve safe shutdown. Change Package 12097 was prepared and implemented to modify the control circuit and add a control room isolation switch (KJHS0110) and redundant fuses on the circuit to ensure the availability of field flashing.

- p. PIR 2006-000860, Potential Loss of Train B Emergency Diesel Generator during Control Room Fire*

Basis - This PIR was written after it was discovered that a control room fire could cause a hot short in the EDG shutdown circuit that could stop the EDG during the event. Since Train B is the protected train in the event of a control room fire, this could have an adverse impact on the ability to achieve safe shutdown. The control room portion of the circuit was only partially isolated by hand switch KJHS0109, which left it vulnerable to a control room fire. Change Package 12097 was prepared and implemented to modify the circuit to provide full isolation from the control room.

- q. PIR 1998-3012, VCT Outlet Valve Did Not Have Redundant Control Power Fusing. LER 98-004-00, Verifying BG LCV 112C Closed*

Basis – This PIR identifies a concern where OFN RP-017 directed operators to close BGLCV0112C using local hand switch BGHS0112C. However, because the control power circuitry does not contain redundant fusing, control power could be lost, resulting in failure of the valve to close.

Prior to revision 27, OFN RP-017 had operators try the hand switch then open the breaker once sufficient time has passed for the valve to close. Another operator then followed up and verified the valve was closed and manually closed it if it was not closed.

DCP 12131 was implemented to add a redundant fuse to the circuit so that operation of BGHS0112C will close the valve. Therefore, the actions to open the breaker and manually close the valve have been removed from OFN RP-017.

- r. *E-1F9915, Design Basis Document for OFN RP-017, Control Room Evacuation*

This document describes the basis for OFN RP-017.

- s. *Engineering Disposition, PFSSD Issue With Voltage Regulator (CR 00023410)*

Basis – This CR identifies a concern where a fire in the control room could have affected the Train B EDG voltage regulator and could have energized the unit parallel relay, placing the EDG in droop mode of operation. The control circuitry was found to not have sufficient isolation capability to ensure the Train B EDG will be available in the event of a control room fire. A temporary modification (TMO 10-004-NE) was implemented and OFN RP-017 was revised to address the issue. A permanent modification will be implemented at a later date.

The temporary modification installed jumper in panel NE0106 to bypass the control room circuitry for the null meter and the Auto/Manual voltage regulator selector switch. This ensures a control room fire will not damage the voltage regulator.

The procedure change added Step C7 to remove the break glass cover from the emergency start pushbutton (KJ HS-101D) to energize the ESA and ESB relays to de-energize the UPR relay. This action will also energize relay 90 VEP which disables the control room auto/manual raise/lower voltage control switches and ensures a control room fire will not cause a hot short that sends a raise or lower signal to the voltage regulator.

- t. *Calculation SA-08-06, Rev. 2, Retran 3D Post-Fire Safe Shutdown (PFSSD) Consequence Evaluation for a Postulated Control Room Fire.*

Basis – This calculation demonstrates the thermal-hydraulic performance of the plant during a postulated control room fire that causes spurious operation of equipment. The results of the calculation are used to determine the maximum allowed time to mitigate a spurious operation. These times are utilized throughout Table 7.1.

7.3.2 OFN RP-017, Section 3.2 - Commitments

- a. *Letter SLNRC 84-0109, Fire Protection Review RCMS #1985-118 [Entire Procedure]*

Basis – SLNRC 84-0109 provides the original licensing basis for response to a control room fire and shutdown from outside the control room. The letter assigned 6 phases to the time critical actions within the letter. Procedure OFN RP-017 no longer uses phases. The timing is now based on thermal hydraulic calculations, which provide more realistic time response criteria to the potential spurious operations that could occur in the event of a fire in the control room. Therefore, all mention of phases has been removed from the procedure. The new timing requirements are described in Table 7.1.

Letter SLNRC 84-0109 should remain in this section because of other commitments within the letter. These commitments are described throughout this document where applicable.

- b. *SLNRC 84-0109 change to commitment RCMS #1988-201*

Basis – See 3.1.f above.

- c. *PIR 2005-3209, and LER 2005-006, Unanalyzed Condition Related To Loss Of RCP Seal Cooling During A Postulated Appendix R Fire Event. (Removes steps from procedure for RCP seal restoration)*

Basis – An Apparent Violation (AV) issued by the NRC during the 2005 Triennial Fire Protection Inspection identified a concern where Revision 21 of OFN RP-017 may not have been able to restore seal cooling prior to seal damage occurring. The current procedure does not restore seal cooling in response to a control room fire. Rather, the RCPs are stopped, the seal injection flow path is isolated, RCP thermal barrier is isolated from the CCW system, RCS makeup and boration is accomplished through the BIT flow path and natural circulation cooldown is used. The thermal hydraulic calculations show that stable hot standby conditions are achieved using OFN RP-017.

7.4 Step-by-Step Review

Table 7.1 provides a detailed evaluation for each Step in OFN RP-017 per the Methodology in Section 3.0.

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
NOTE	The fire brigade is dedicated to fighting the control room fire. They are not responsible for performing any of the operator actions described in this procedure.	N/A	<p>Wolf Creek USAR, Appendix 9.5E, Response to Section III.L states, in part: "...Adequate Operations shift staffing is provided to achieve and maintain post-fire safe shutdown..."</p> <p>10CFR50, Appendix R, Section III.L.4 states, in part, "...The number of operating shift personnel, exclusive of fire brigade members, required to operate such equipment and systems shall be on site at all times.</p> <p>The Wolf Creek Technical Requirements Manual (TRM), TR 5.2.1.b states in part: "A site Fire Brigade of at least 5 members shall be onsite at all times ... The Fire Brigade shall not include the Shift Manager (SM), and the two other members of the minimum shift crew necessary for safe shutdown of the Unit and any personnel required for other essential function during an emergency."</p> <p>Note that four operators, besides the SM, are required to complete OFN RP-017.</p>	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
1	<p>Check Control Room Evacuation Due To Fire - REQUIRED</p> <ul style="list-style-type: none"> * Annunciators and status panels - NOT READABLE FROM "AT THE CONTROLS" * Spurious equipment actuations - OBSERVED * Loss of Control Room controls - IMMINENT 	N/A	<p>The decision to evacuate is made by the Shift Manager based on environmental conditions and/or the ability to control the plant from the control room (CR). There is no regulatory basis for when the CR should be evacuated.</p> <p>The Wolf Creek SER, Supplement 5, page 9-10 states in part: "The new procedures assume that evacuation of the control room takes place when the fire starts..." It is not realistic to assume the control room operators will evacuate as soon as a fire starts. Only the control room staff can make the decision to evacuate based on conditions. Therefore, OFN RP-017 provides guidelines that the Shift Manager can use for deciding when to evacuate.</p>	N/A	N/A	N/A	N/A
2	<p>Trip The Reactor</p> <ul style="list-style-type: none"> • SB HS-1 • SB HS-42 	R	<p>Generic letter 86-10, response to question 3.8.4 states, in part: "...Note that the only manual action in the control room prior to evacuation usually given credit for is the reactor trip. For any additional control room actions deemed necessary prior to evacuation, a demonstration of the capability of performing such actions would have to be provided..."</p> <p>In a memo from the NRC to KG&E dated August 31, 1984, which documents the minutes of an August 22, 1984 meeting with KG&E and UEC, the NRC provided clarifications of staff positions discussed during the meeting. One of those positions is as follows:</p> <p><i>Credit can be taken only for a <u>manual</u> scram before leaving the control room.</i></p>	0	The reactor is assumed tripped at t=0.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>Based on this staff position, the NRC acknowledged that the reactor will trip when the switches are depressed prior to evacuating the control room.</p> <p>Hand switches SB HS-1 and SB HS-42 are located on separate panels. SB HS-1 is located on RL003 while SB HS-42 is located on RL006. There is a 2 foot air gap between the panels as well as metal outer covers that will restrict the spread of fire between panels. Automatic smoke detection is present in each panel, which will provide early warning of a fire. In addition, the control room is constantly attended. A fire in one panel is unlikely to spread to the other due to the physical separation present.</p> <p>Drawing E-13SB12A shows a schematic diagram of the reactor trip switch wiring. Each switch has two normally open contacts per train. Two out of four contact closures on one out of two trains actuates the reactor trip function at panel SB102A or SB102B, located outside the control room. Two contacts on each switch are on separation group 1 and two contacts are on separation group 4. Physical separation between each group is maintained in accordance with IEEE 384 to ensure a fire that affects one group will not affect the other.</p> <p>The positioning of the reactor trip switches on separate panels and the arrangement of the switch contacts and wiring provides reasonable assurance that one of the switches will successfully trip the reactor.</p>				

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
3	Close MSIVs <ul style="list-style-type: none"> • AB HS-79 <u>AND</u> • AB HS-80 	R, M, D	<p>Generic letter 86-10, response to question 3.8.4 states, in part: "...Note that the only manual action in the control room prior to evacuation usually given credit for is the reactor trip. For any additional control room actions deemed necessary prior to evacuation, a demonstration of the capability of performing such actions would have to be provided. Additionally, assurance would have to be provided that such actions could not be negated by subsequent spurious actuation signals resulting from the postulated fire."</p> <p>Hand switches AB HS-79 and AB HS-80 are located on RL006, which also has one of the two reactor trip hand switches (SB HS-42). Therefore, due to the close proximity between the reactor trip hand switch and the MSIV close hand switches, it is reasonable to conclude that actuating both hand switches is possible prior to exiting the control room.</p> <p>Credit is not given for actual MSIV closure since spurious actuation could occur as a result of the control room fire. Therefore, Step D15 provides instructions to close them if not already closed. For a single failure not involving the MSIVs, SA-08-006 assumes the MSIVs close in Step 3.</p>	5 sec	SA-08-006 assumes this step will be completed approximately 5 seconds after the reactor trip switches are depressed. See Section 6.1 for discussion on the timing basis for MSIV closure.	Yes. The MSIVs could spuriously open or remain open after the switches have been actuated. See Step D15.	N/A
4	Shift Manager proceed to ASP and direct personnel.	N/A	The Shift Manager (SM) proceeds directly to the ASP to direct performance of OFN RP-017.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
4.a	Announce the evacuation of the Control Room due to fire and entry into OFN RP-017 using Plant Gaitronics handset	N/A	The Gaitronics system is the preferred method to announce the fire and call out the fire brigade. The Gaitronics control panel is located in the back panel area of the control room on the far South wall, remote from the main control room area. A fire in the main control room area, in the absence of a loss of offsite power, will not affect the ability of the Gaitronics system to announce the fire and call out the fire brigade due to the physical separation of the control panel (QF076) and power cables. However, a loss of offsite power to NG01, NG02, PG19 and PG20 will prevent operation of the system. Therefore, an RNO is provided to ensure timely callout of the fire brigade and notification of control room evacuation.	N/A	N/A	N/A	N/A
4.a RNO	<u>IF</u> Gaitronics is not working, <u>THEN</u> perform the following: 1) Announce Evacuation using the public address system. 2) IF announcement cannot be made, <u>THEN</u> dispatch runners to notify OFN RP-017 personnel.	N/A	This RNO provides instructions to ensure all available means are used to call out the fire brigade and commence OFN RP-017 actions if the Gaitronics system is unavailable.	N/A	N/A	N/A	N/A
4.b	Repeat announcement.	N/A	The Operator repeats the announcement to ensure it is heard.	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
4.c	Check Fire Brigade - CALLED OUT	N/A	The Operator ensures the fire brigade has been called out successfully and, if not, performs the RNO actions.	N/A	N/A	N/A	N/A
4.c RNO	<p>Perform the following:</p> <ol style="list-style-type: none"> 1) Make the following announcement using the Public Address System <ul style="list-style-type: none"> • "Fire Fire Fire. Fire in Control Room. Fire Brigade members assemble at turnout lockers" 2) Repeat Public Address System Announcement. 3) <u>IF</u> Fire Brigade cannot be contacted, THEN dispatch runners to alert FB members. 4) Request assistance from Coffey County Fire Department. <ul style="list-style-type: none"> • Telephone number 911 	N/A	This RNO provides alternative methods to notify the fire brigade and provides instructions to ensure the off-site fire department is called out if the fire brigade is delayed or cannot be contacted.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
4.d	Classify the event using EPP 06-005, EMERGENCY CLASSIFICATION.	N/A	The SMs duty at this point is to classify the event and initiate the emergency plan.	N/A	N/A	N/A	N/A
4.e	Supervise performance of this procedure.	N/A	After the emergency plan has been initiated, the SM supervises performance of OFN RP-017.	N/A	N/A	N/A	N/A
5	SRO proceed to ASP via CAS and direct personnel.	N/A	The Senior Reactor Operator (SRO) is responsible for performing the actions of Attachment A in OFN RP-017.	N/A	N/A	N/A	N/A
5.a	Obtain the following equipment from Control Room emergency locker for personnel entering the RCA: <ul style="list-style-type: none"> • Low-Range PIC 0 – 500 mR • High-Range PIC 0-5 R • Record Dose Dosimeter (RDD) • Fire resistant Suit (SRO) • Leather gloves (SRO) • Hard hat 	N/A	This step ensures those exiting the CR through CAS obtain the proper radiation monitoring and safety gear. The SRO is required to operate 480 VAC breakers on his/her way to the ASP so it will be necessary to don a fire resistant suit and leather gloves.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
5.b	Direct CAS personnel to: 1. Transfer control to SAS 2. Evacuate CAS	N/A	CAS is evacuated to prevent security personnel from being overcome by smoke.	N/A	N/A	N/A	N/A
5.c	On NG03C, place the following breakers to OFF: <ul style="list-style-type: none"> • NG03CEF4 for AL HV-36, Supply From Cond Stor Tk Water • NG03CHF3 for EG HV-15, CCW Return From Nuclear Aux Components • NG03CKF3 for EG HV-61, CCW CTMT ISO VLV 	D, S	<p>The SRO proceeds to the ASP through CAS and enters room 1512, where NG03C is located. Therefore it is feasible for the SRO to perform these actions before proceeding to the ASP.</p> <p>These breakers are placed in the OFF position to ensure power is disconnected to the associated Train A valves. This will prevent the valves from spuriously operating prior to and after the valve is manually operated in another step.</p> <p>If, prior to performing this step, the valve spuriously operates to the undesired position, the valve can still be manually operated. Valve damage will not occur due to circuit modifications completed per change packages 12130 (EG HV-61) and 12170 (AL HV-36 and EG HV-15) in response to NRC IN 92-18 (PIR 2007-003037).</p> <p>For additional information on these specific valves see Steps B7, B10 and D5.</p>	N/A	See Section 6.3 for discussion of timing basis for aligning auxiliary feedwater. See Section 6.5 for discussion of timing basis for aligning component cooling water.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
5.d	Pick up radio from emergency locker outside ASP and select Channel 1.	N/A	Operators will generally communicate via radio. Therefore, the SRO obtains a radio from the emergency locker. The radio system is unaffected by a fire in the control room. Therefore, the radio system is a reliable means of communication. Channel 1 is used because it is the Operations channel.	N/A	N/A	N/A	N/A
5.e	Perform actions of ATTACHMENT A, SRO ACTIONS	N/A	The SRO is responsible for performing the actions of Attachment A in OFN RP-017.	N/A	N/A	N/A	N/A
6	On-Shift Personnel Perform Designated Actions:	N/A	N/A	N/A	N/A	N/A	N/A
6.a	Operator performing Turbine Building actions, proceed to PA01/PA02 and perform actions of ATTACHMENT B, TURBINE BUILDING ACTIONS	N/A	N/A	N/A	N/A	N/A	N/A
6.b	Reactor Operator, proceed to NK switchgear rooms and perform actions of ATTACHMENT C, REACTOR OPERATOR ACTIONS	N/A	N/A	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
6.c	Operator performing Aux Building actions, proceed to emergency locker 2026' level and perform actions of ATTACHMENT D, AUXILIARY BUILDING ACTIONS	N/A	N/A	N/A	N/A	N/A	N/A
6.d	Offsite Communicator, proceed to Aux Shutdown Panel until released by Shift Manager	N/A	The Wolf Creek emergency plan requires an offsite communicator.	N/A	N/A	N/A	N/A
6.e	Operator closing BN HV-8812A, RWST TO RHR PUMP A SUCTION ISOLATION VALVE proceed to ESF Switchgear Room B and perform actions of ATTACHMENT E, BN HV-8812A CLOSURE.	R, M	CR 00019239 identified an issue involving the time to close valve BN HV-8812A. The valve requires approximately 600 turns of the handwheel to close. Operations Standing Order #1 limits the handwheel speed to 60 revolutions per minute. Therefore, the minimum time to close is 10 minutes, but due to the location of the handwheel and potential fatigue of the operator, it will likely take longer. Therefore, it was decided to add an extra operator to this procedure to perform this action. This operator will also be responsible for opening the breaker to the valve. Due to the length of time necessary to close the valve, this operator should not be given any other OFN RP-017 duties prior to getting BN HV-8812A closed.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A1	<p>Place Following Switches in ISOLATE:</p> <ul style="list-style-type: none"> • RP HIS-1 CTRL ROOM ISO SWITCH - ISOLATE • RP HIS-2 CTRL ROOM ISO SWITCH - ISOLATE • RP HIS-3 CTRL ROOM ISO SWITCH - ISOLATE 	R, M, D, P, S	<p>These hand switches are used to isolate certain components from the control room. The switches, when placed in ISO. CTRL. ROOM position, energize lockout relays (LORs) and change the position on a number of contacts located in the control circuit for these components. This ensures a fire in the control room will not affect the isolated components after the hand switch is actuated.</p> <p>The LORs are powered from DC batteries (NK). The batteries are sized to supply power to all emergency loads for 200 minutes following loss of ac power per E-10NK. Loss of offsite power will not affect the LORs.</p> <p>RP HIS-1 performs the following functions:</p> <ul style="list-style-type: none"> • Isolates valve FC HV-312 (TDAFP Trip and Throttle Valve) from the control room. • Isolates main steam to TDAFP supply valves AB HV-5 and AB HV-6 from the control room. • Isolates AB PV-2 indication from the control room. AB PV-2 position indication at the ASP is independent of the control room. RP HIS-1 isolation is not required. ARV position indication is not credited for PFSSD. ARV position is determined by controlling the ARV using the controller at the ASP and monitoring RCS temperature. • Isolates FC FV-313 (TDAFP Speed Governing Valve) position indication from the control room. 	N/A	<p>This step establishes control of the isolated components from the auxiliary shutdown panel (ASP). The timing basis depends on when the isolated components are required to be operable, which is discussed in the steps that follow. Therefore, there is no timing basis for this step.</p>	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>RP HIS-2 performs the following functions:</p> <ul style="list-style-type: none"> • Isolates BG HV-8152 (Letdown Isolation Valve) from the control room. • Isolates the trip portion of NB0208 handswitch PG HIS-21. However, NB0208 could trip and the control power fuses could blow before RP HIS-2 is operated. This would prevent operation of pressurizer backup heater group B from the ASP. If this occurs, operators will need to manually close NB0208 to energize PG22. NB0208 is closed in Step C10. • Isolates valves AL HV-30, AL HV-33 and AL HV-34 from the control room and adds a redundant fuse in the circuit. • Isolates AB PV-4 indication from the control room. AB PV-4 position indication at the ASP is independent of the control room. RP HIS-2 isolation is not required. ARV position indication is not credited for PFSSD. ARV position is determined by controlling the ARV using the controller at the ASP and monitoring RCS temperature. • Isolates MDAFP B from the control room and adds redundant fuses in the circuit. However, this method of controlling the Train B motor driven auxiliary feedwater pump is not credited in OFN RP-017. Rather, the B MDAFP is started by closing breaker NB0205 in Step C14. 				

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>RP HIS-3 performs the following functions:</p> <ul style="list-style-type: none"> Isolates PG2201 control circuit from the control room. PG2201 supplies power to pressurizer heater backup group B. Isolation of the PG2201 control circuit using RP HIS-3 allows operation of the heater group using BB HIS-52B at RP118B. The heaters are used in Step A.7 RNO to maintain pressurizer pressure. Isolation of the heaters prevents spurious operation and ensures availability when needed. PG2201 is powered from NB0208 which is closed in Step C10. 				

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A2	<p>Close S/G A And C ARVs:</p> <p>a. AB HS-1 SG A STEAM DUMP CTRL XFR - LOCAL</p> <p>b. AB HS-3 SG C STEAM DUMP CTRL XFR - LOCAL</p> <p>c. AB PIC-1B SG A STEAM DUMP TO ATMS CTRL- CLOSED</p> <p>d. AB PIC-3B SG C STEAM DUMP TO ATMS CTRL- CLOSED</p>	R, M, D	<p>The control circuit for these valves is not isolated from the control room by operation of AB HS-1 and AB HS-3. Therefore, AB PV-1 and AB PV-3 could remain open. Steps D18 and D19 direct operators to isolate air and nitrogen to the valves then bleed air from the regulator to fail the valves closed. If this method fails, operators are directed to close AB-V018 and AB-V029. Isolating air and nitrogen provides a faster method of closing the valves.</p> <p>Control power to AB PIC-1B originates from NN0116, which is powered from the NK011 batteries. Therefore, power will be available to perform this action.</p> <p>Control power to AB PIC-3B originates from NN0303 which is powered from the NK013 batteries. Therefore, power will be available to perform this action.</p>	7	<p>SA-08-006 assumes this step will be completed within 7 minutes if a single failure occurs that does not involve an ARV circuit. Therefore, it is assumed that ARVs 1 and 3 will be closed in 7 minutes in this step and that the control room fire will not impact the ability to close the ARVs from the ASP. SA-08-006 also shows that a single failed open ARV can go unmitigated for at least 1-hour. See Section 6.1 for discussion of timing basis for controlling the steam generator ARVs.</p>	<p>Yes. A control room fire could prevent closure or cause the re-opening of ABPV1 and ABPV3.</p>	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A3	<p>Check RCS Cold Leg Temperatures:</p> <p>STABLE AT OR TRENDING TO 561 °F</p> <ul style="list-style-type: none"> BB TI-423X 	D	The steam generator ARVs, if unaffected by a fire, control temperature to 561 °F. Temperature instrument BB TI-423X is used to monitor cold leg temperature on loop 2. The circuits for this temperature indicator are independent of the control room.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A3 RNO	<p>Perform the following:</p> <p>a. IF temperature greater than 561 °F, THEN dump steam using S/G B and S/G D ARV's:</p> <ol style="list-style-type: none"> 1) AB HS-2 SG B STEAM DUMP CTRL XFR - LOCAL 2) AB HS-4 SG D STEAM DUMP CTRL XFR - LOCAL 3) AB PIC-2B – THROTTLED OPEN 4) AB PIC-4B – THROTTLED OPEN <p>b. IF temperature less than 561 °F AND temperature decreasing, THEN stop dumping steam.</p>	D	<p>ARVs AB PV-2 and AB PV-4 are isolated from the control room by placing AB HS-2 and AB HS-4 in LOCAL position. Auxiliary feedwater is assured to steam generators B and D using the Train B MDAFP and the TDAFP. The Train B MDAFP is started in Step C14. The TDAFP is started in Step A14.</p> <p>Control power for AB PIC-2B originates from NN0203 which is powered from NK02. Therefore, power will remain available from the NK012 batteries. Redundant power is available from NG02A which is energized in Step C11.</p> <p>Control power for AB PIC-3B originates from NN0404 which is powered from NK04. Therefore, power will remain available from the NK014 batteries. Redundant power is available from NG02A which is energized in Step C11.</p>	7	SA-08-006 assumes atmospheric steam dump control on steam generators B and D is established at the ASP within 7 minutes. See Section 6.1 for discussion about steam generator ARVs.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A4	<p>Check CST to MD AFP B – OPEN</p> <ul style="list-style-type: none"> • AL HIS-34B – OPEN 	D	<p>The control circuit for this valve is isolated from the control room by operating RP HIS-2 in Step A1. The control circuit has been modified to address NRC IN 92-18 (PIR 2005-3314).</p> <p>MDAFP B is lined up to supply feedwater to steam generator D. Step C13 restores power to AL HV-34 MCC cubicle NG04CNF1. The valve may not open until Step C13 is completed.</p>	15 minutes to start the pump and inject into steam generator D	See Section 6.3 for timing basis for establishing auxiliary feedwater using Train B MDAFP.	No	A1
A5	<p>Verify AFW Valve Lineup For MD AFP B:</p> <ul style="list-style-type: none"> a. SG D AUX FW XFR CTRL VLV <ul style="list-style-type: none"> o AL HS-5 - LOCAL b. SG D MD AFP AFW REG VLV CTRL <ul style="list-style-type: none"> o AL HK-5B - OPEN 	D	<p>Operation of AL HS-5 to the LOCAL position allows control of valve ALHV0005 from the ASP.</p> <p>Power to valve AL HV-5 is from NG04CCF2. The valve is normally full open and can be throttled to control flow into the steam generator. Loss of power will fail the valve as is and will prevent control of the valve from the ASP until power is restored to NG04C. Power is restored in step C13. This will have no adverse impact since the Train B MDAFP is not started until Step C14.</p>	15 minutes to start the pump and inject into steam generator D	See Section 6.3 for timing basis for establishing auxiliary feedwater using Train B MDAFP.	No	N/A
A6	Notify Reactor Operator That Motor Driven AFW Pump B Valve Lineup Steps A4 Through A5 Are Complete	D	The Reactor Operator, in Step C14, ensures Steps A4 and A5 are complete before starting the Train B motor driven auxiliary feedwater pump. Valve lineups in Steps A4 and A5 establish a suction source from the CST and a discharge path to SG D and need to be complete before Step C14 is complete.	15 minutes to start the pump and inject into steam generator D	See Section 6.3 for timing basis for establishing auxiliary feedwater using Train B MDAFP.	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A7	<p>Maintain Stable Plant Conditions:</p> <p>a. PZR pressure – BETWEEN 2000 PSIG AND 2300 PSIG</p> <ul style="list-style-type: none"> • BB PI-406X <p>b. PZR level – BETWEEN 25% AND 70%</p> <ul style="list-style-type: none"> • BB LI-460B <p>c. S/G Wide Range Levels BETWEEN 60% AND 62%</p> <ul style="list-style-type: none"> • AE LI-502A • AE LI-504A <p>d. RCS cold leg temperatures - BETWEEN 551°F AND 561°F</p> <ul style="list-style-type: none"> • BB TI-423X 	R, M, D, P	<p>Hot standby is maintained using procedure OFN RP-017 by ensuring parameters are within the ranges listed. Diagnostic instrumentation is available as described below.</p> <p>a. The only pressurizer pressure indicator at the ASP is on the Train A side (BB PI-455B), which is not protected from a control room fire. RCS pressure indicator BB PI-406X is located on the Train B ASP and is unaffected by a control room fire. Therefore, BB PI-406X is used in this step to verify RCS pressure.</p> <p>b. Pressurizer level is indicated by BB LI-460B on the Train B ASP and is unaffected by a control room fire.</p> <p>c. OFN RP-017 uses steam generators B and D for shutdown from outside the control room. Wide range level indicators AE LI-502A (SG B) and AE LI-504A (SG D) are located on the Train B ASP and are unaffected by a control room fire.</p> <p>d. RCS cold leg temperature is monitored at the Train B ASP using temperature indicator BB TI-423X (Loop 2 cold leg). This TI is unaffected by a fire in the control room.</p>	N/A	N/A	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A7 RNO	<p>a. Cycle PZR HTRS B/U GP B as necessary to restore PZR pressure</p> <ul style="list-style-type: none"> • BB HIS-52B <p>b. WHEN BIT is aligned, THEN direct Operator performing Turbine Building actions to control level locally:</p> <ul style="list-style-type: none"> • Throttle BIT outlet valve o EM HV-8801B 	R, M	<p>a. If pressurizer pressure is below 2000 psig, the backup group B pressurizer heaters are cycled to restore pressure. Step C10 restores power to the heaters and will need to be complete before this step can be completed.</p> <p>b. 10 CFR 50, Appendix R requires pressurizer level to remain on-scale. To maintain pressurizer level on scale, an operator needs to throttle the BIT outlet valve to control flow. The valve is throttled in Step B13.</p>	<p>a. 11.5</p> <p>b. 28</p>	<p>a. Per SA-08-006, pressurizer heater backup group B is assumed to be controlled within 11.5 minutes.</p> <p>b. SA-08-006 shows that the most challenging scenario for pressurizer level is a single steam generator ARV opening coincident with an immediate automatic AFAS(T) and a loss of offsite power. Pressurizer level does not drop off scale low as long as the CCP is started and BIT injection is lined up in 28 minutes. See Sections 6.1 and 6.2 for discussion about charging.</p>	No	<p>a. N/A</p> <p>b. D4</p>

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
N/A	<p>CAUTION</p> <p>o AL HV-6, AL HV-7, AL HV-8 and AL HV-12 are not isolated from the control room and may spuriously actuate. It may be necessary to manually isolate these valves.</p>	D	<p>If AL HV-6 opens, the TDAFP would supply AFW to steam generator D in addition to MDAFP B. Flow controller AL FC-5 will limit flow to the steam generator to 300 gpm and will throttle AL HV-5 accordingly. Circuits for this function are not run in the control room and, therefore, are unaffected by the fire. However, the controller will not function until power is restored to NG04C in Step C13. In this case, operators may have to manually close AL HV-6. The TDAFP is designed to supply all four steam generators so flow diversion to SG D will not impact PFSSD.</p> <p>If AL HV-7 opens, water would be directed to SG A via MDAFP B. The MDAFP B is sized to supply both SG A and SG D, so sufficient flow would be directed to SG D for safe shutdown. With flow being directed to SG A and with the SG A ARV not being used, the SG could fill solid. However, with the SG filled solid, PFSSD is still assured.</p> <p>If AL HV-8 opens, the same result would occur as with AL HV-7 opening, except the water would come from the TDAFP. The TDAFP is designed to supply all four steam generators. Therefore, if valve AL HV-8 spuriously opens, PFSSD is still assured.</p> <p>If AL HV-12 opens, water would be directed to SG C via the TDAFP. However, with flow being directed to SG C and with the SG C ARV not being used, the SG could fill solid, which is not desirable. However, with the SG filled solid, PFSSD is still assured. The</p>	N/A	<p>Closing valves ALHV-6, 7, 8 and 12 is not time critical as discussed in the Basis. Therefore, operators can mitigate spurious operation of these valves when all time critical actions are complete.</p>	<p>Yes. AL HV-6, AL HV-7, AL HV-8 and AL HV-12 are not isolated from the control room. This will not adversely impact PFSSD.</p>	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			TDAFP is designed to supply all four steam generators. Therefore, if valve AL HV-12 spuriously opens, PFSSD is still assured.				
A8	<p>Check ESW To TD AFW Pump Isolation Valve - CLOSED</p> <ul style="list-style-type: none"> o AL HIS-33B CLOSED 	D	<p>As stated earlier, AL HV-33 is isolated from the control room using RP HIS-2. Step C13 energizes valve cubicle NG04CCF4, so the valve may not close until Step C13 is completed.</p> <p>A failed open valve will not impact PFSSD. The preferred source of auxiliary feedwater is the CST. However, ESW is the safety-related source. This action is for commercial concerns to ensure raw untreated ESW water does not enter the SGs.</p>	N/A	This action is not time critical. As stated in the Basis, if the valve opens PFSSD is still assured.	No	A1
A9	<p>Contact Operator Performing Attachment B To Verify AL HV-36 Open</p> <ul style="list-style-type: none"> • AL HV-36 - OPEN 	D	The SRO ensures a suction supply from the CST is available before starting the TDAFP. Step B7 opens the valve after ensuring control power is de-energized in Step 5.c.	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A9 RNO	<p>Perform the following:</p> <ul style="list-style-type: none"> a. Close AFW Pump Turbine Mechanical Trip/Throttle Valve. <ul style="list-style-type: none"> • FC HIS-312B b. Close Loop 2 and Loop 3 Steam to AFP Turb. <ul style="list-style-type: none"> • AB HIS-5B • AB HIS-6B c. WHEN CST Supply To TD AFW Pump is open, THEN perform Steps A10 through A14. d. Observe note prior to Step A15 and continue with step A15. 	D	<p>If AL HV-36 is not open, this RNO directs the operator to ensure the steam supply to the TDAFP is isolated to protect the TDAFP.</p> <p>Valves AB HV-5, AB HV-6 and FC HIS-312B are isolated from the control room in Step A1.</p>	N/A	<p>If the TDAFP is running with no suction source, damage to the pump could occur. If the pump has no suction this RNO needs to be completed before damage occurs.</p>	No	A1

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A10	<p>Place TD AFP Governor Control to local:</p> <ul style="list-style-type: none"> FC HS-313 - LOCAL Adjust FC HIK-313B to Minimum Output 	D	<p>FC HS-313 transfers control of the TDAFP speed governing valve to the ASP. After the switch is manipulated, controller FC HIK-313B can be used to control the TDAFP.</p> <p>Control power originates from NN0203, which is powered from NK02. Therefore, power will remain available from the NK012 batteries. Redundant power is available from NG02A, which is energized in Step C11.</p>	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	N/A
A11	<p>Verify AFW Valve Lineup For TD AFP:</p> <p>a. SG B AUX FW XFR CTRL VLV LOCAL</p> <ul style="list-style-type: none"> AL HS-10 - LOCAL <p>b. SG B TD AFP AFW REG VLV CTRL OPEN</p> <ul style="list-style-type: none"> AL HK-10B - OPEN 	D	<p>AL HS-10 transfers control of AL HV-10 to the ASP, where AL HK-10B can be used to control valve position. This valve controls TDAFP flow to SG B, which is one of the credited AFW flowpaths.</p> <p>Control power originates from NN0404 which is powered from NK04. Therefore, power will remain available from the NK014 batteries. Redundant power is available from NG02A which is energized in Step C11.</p>	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	N/A
A12	<p>Ensure Loop B Steam Isolation To AFP Turbine Is - OPEN</p> <ul style="list-style-type: none"> AB HIS-5B - OPEN 	D	<p>Valve AB HV-5 is opened to ensure adequate steam supply to the TDAFP. RP HIS-1 isolates the valve from the control room and inserts a redundant fuse in the circuit. Therefore, the hand switch can be relied on to function.</p>	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	A1

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A13	<p>Ensure Loop C Steam Isolation To AFP Turbine Is - CLOSED</p> <ul style="list-style-type: none"> AB HIS-6B - CLOSED 	D	Valve AB HV-6 is closed because steam generator C is not credited for a control room fire. Continued steaming of this steam generator with no feedwater flow could result in the steam generator going dry. Valve AB HV-5 is opened in Step A12 to provide the required steam flow to the Turbine Driven Auxiliary Feedwater Pump. RP HIS-1 isolates the valve from the control room and inserts a redundant fuse in the circuit. The alternate power supply to the valve does not run through the control room. Therefore, the hand switch can be relied on to function.	N/A	N/A	No	A1
A14	<p>Ensure AFP Turbine Mechanical Trip/Throttle Valve Open</p> <ul style="list-style-type: none"> FC HIS-312B - OPEN 	D	Valve is isolated from the control room and redundant fuses are added using RP HIS-1 in Step A1.	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	A1, A9
A15	<p>Contact Operator Performing Attachment E, BN HV-8812A AND AUX FEEDWATER VALVE CLOSURE To Ensure AFW Valves Are closed.</p>	D	Auxiliary feedwater valves AL-V032, AL-V056, AL-V061 and AL-V071 are closed to prevent overfilling the steam generators. This step has the operator verify the valves are closed before starting the TDAFP.	35	Calculation SA-08-006 shows that the steam generators could overfill if the valves are not closed within 35 minutes.	No	N/A

TABLE 7.1
 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A15 RNO	Perform the following: a. <u>WHEN</u> AFW Valves are closed, <u>THEN</u> perform A15 b. Observe notes prior to step A16 and continue with step A16	D	If the AFW valves are not closed, The RNO directs the operator to continue to Step A16 until the valves are closed.	35	Calculation SA-08-006 shows that the steam generators could overflow if the valves are not closed within 35 minutes.	No	N/A
A16	Establish Turbine Driven AFW Pump Control: a. Adjust AFW Turbine Speed Governor CTRL Output to 60% • FC HIK-313B b. Adjust AFW pump speed as necessary to establish desired AFW flow	D	The TDAFP is credited for supplying AFW to SG B. FC HIK-313B is used to control TDAFP speed from the ASP. Step A10 transfers control of FC FV-313 to the ASP. Step E4 closes TDAFP to SGs A, C and D valves AL-V056, AL-V071 and AL-V061, respectively, to prevent overflow of these steam generators.	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	A1, A9, A10, E4

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A17	<p>Align Alternate AFW Pump Water Source:</p> <p>a. Check CST below minimum level:</p> <p>* CST level on ASP – LESS THAN 14%</p> <ul style="list-style-type: none"> • AP LI-4B <p style="text-align: center;">OR</p> <p>* Local CST level – LESS THAN 6' 5"</p> <p>b. Open ESW To MD AFW Pump B Isolation Valve</p> <ul style="list-style-type: none"> • AL HIS-30B - OPEN <p>c. Open ESW To TD AFP</p> <ul style="list-style-type: none"> • AL HIS-33B 	D	<p>This step aligns the ESW system to the AFW pumps in the event the CST reaches low level. RP HIS-2 isolates both AL HV-30 and AL HV-33 from the control room and adds redundant fuses to the control circuit for each valve.</p> <p>Step C13 needs to be complete to restore power to AL HV-30 and AL HV-33 MCC cubicles.</p>	N/A	<p>The CST contains sufficient inventory for PFSSD. This step is entered only when the CST reaches low level. There is no timing basis associated with this step.</p>	<p>Yes. CST level indicator AP LI-4B is not isolated from the control room. Local level instrument may need to be used.</p>	A1

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A17 RNO	<p>a. Perform the following:</p> <p>1) WHEN CST level decreases to less than minimum level, THEN do Steps A15.b and A15.c.</p> <p>2) Observe notes prior to Step A16 and continue with Step A16.</p>	D	<p>The RNO is entered when the CST is above minimum level. This is a continuous action step which means the operator at the ASP will continue to monitor CST level and initiate swapover to ESW when required.</p> <p>Per TS 3.7.6, the CST is required to contain 281,000 gallons of water, which is sufficient to provide water to the steam generators for 4 hours at hot standby followed by plant cooldown to RHR entry conditions. Therefore, it is not expected that ESW will be needed until several hours into the event.</p>	N/A	N/A	No	N/A
A18	<p>Direct Available Operator to Check B ESW Pumphouse Temperature</p> <p>a. Check room temperature greater than 65°F</p> <p>b. Check room temperature less than 90°F</p>	S	<p>This step was added in OTSC 10-0093 as a result of condition report 31408. Step C16 has operators fully open the B ESW pump room supply damper and start the supply fan. There are no operator actions taken for the recirculation damper. This lineup may not be adequate during all times of the year. In the winter months, drawing in 100% outside air with a closed recirculation damper could cause the room temperature to drop below freezing. In the summer months, with the recirculation damper open, the room could heat up to an undesired temperature. The temperature range of 65 to 90 degrees F ensures the room temperature remains within the required range. These are interim actions until a permanent resolution is determined. Condition Report Action 30350-02-06 is tracking the resolution of this issue.</p>	Prior to room reaching undesirable temperature	The timing basis depends on the time for the room to heat up or cool down to a point where the ESW pump and associated components will not operate. See Section 6.5 for discussion about room cooling.	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A18 RNO	<p>a. Perform the following:</p> <p>1) Open breaker NG06EEF4 to stop B ESW Pumphouse Supply Fan</p> <p>2) <u>WHEN</u> temperature reaches 100°F, <u>THEN</u> close breaker NG06EEF4 to start B ESW Pumphouse Supply Fan</p> <p>b. Perform the following:</p> <p>1) <u>WHEN</u> temperature reaches 110°F, <u>THEN</u> open breaker 8 on NG06EBF2 to fail Recirc Damper closed.</p> <p>2)) <u>WHEN</u> temperature reaches 65°F, <u>THEN</u> close breaker 8 on NG06EBF2 to energize Recirc Damper.</p>	S	<p>This RNO performs the necessary steps to ensure the Train B ESW pump room temperature remains within the required range. These steps are performed locally. Opening NG06EEF4 will de-energize the supply fan and allow the room to heat up if the temperature drops below 65°F. When the temperature reaches 100°F, the operator will re-start the fan.</p> <p>When the room temperature reaches 110°F, the operator will open breaker NG06EBF208 to fail the recirculation damper closed, allowing 100% outside air into the room to cool the room. When the temperature drops to 65°F, the operator will close breaker NG06EBF208 to re-energize the recirculation damper to allow it to open. If the recirc damper does not open due to the fire in the control room, then the operator can perform the RNO for Step A16.a to increase the room temperature.</p> <p>These are interim actions until a permanent resolution is determined. Condition Report Action 30350-02-06 is tracking the resolution of this issue.</p>	Prior to room reaching undesirable temperature	The timing basis depends on the time for the room to heat up or cool down to a point where the ESW pump and associated components will not operate. See Section 6.5 for discussion about room cooling.	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A19	Direct Available Operators To Perform Actions Of ATTACHMENT F, ACTIONS TO PROTECT TRAIN A EQUIPMENT	N/A	This step is used whenever extra operators are available to minimize damage to Train A equipment. Attachment F is not required by regulation, so its steps are not evaluated in this DBD.	N/A	N/A	N/A	N/A
A20	Check plant cooldown – NOT DESIRED	N/A	The purpose of OFN RP-017 is to maintain hot standby conditions until the fire is under control and operations can be resumed from the control room. If the event duration does not allow the plant to be maintained in hot standby, then OFN RP-017A is entered, per the RNO.	N/A	N/A	N/A	N/A
A20 RNO	Go to OFN RP-017A, HOT STANDBY TO COLD SHUTDOWN FROM OUTSIDE THE CONTROL ROOM	N/A	If necessary, OFN RP-017A is entered to bring the plant to safe cold shutdown.	N/A	N/A	N/A	N/A
A21	Check Fire Has Been Extinguished.	N/A	NRC Draft Regulatory Guide DG-1214 dated April 2009, which is a proposed revision to RG 1.189, Section 5.5.2 has guidance for re-entering and re-establishing control from the Control Room. Steps A-18 through A-22 were added to OFN RP-017 to identify this guidance. CR 00016481 identified the need to add guidance for re-entry into the Control Room.	N/A	N/A	N/A	N/A
A21 RNO	Do NOT continue until fire is extinguished.	N/A	Continuation in the procedure is not allowed until the fire is extinguished.	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
A22	Check Control Room Habitable	N/A	See Step A19 Basis	N/A	N/A	N/A	N/A
A22 RNO	Do NOT continue until Control Room is habitable.	N/A	Habitability must be established prior to allowing unprotected operators back into the control room.	N/A	N/A	N/A	N/A
A23	Assess Control Room Damage.	N/A	See Step A19 Basis	N/A	N/A	N/A	N/A
A24	Perform Corrective Actions To Restore Necessary Safety, Control And Information Systems To Functional.	N/A	See Step A19 Basis	N/A	N/A	N/A	N/A
A25	Contact TSC To Develop Procedures To Transfer Control From Aux Shutdown Panel To The Main Control Room And To Restore From Any Local Actions Taken Based On Review Of Actions Taken In The Procedures Performed.	N/A	See Step A19 Basis	N/A	N/A	N/A	N/A
A26	Proceed As Directed By Station Management.	N/A	N/A	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B1	<p>Locally Trip RCPs</p> <ul style="list-style-type: none"> • PA0107 for RCP A - TRIPPED • PA0108 for RCP B - TRIPPED • PA0205 for RCP C - TRIPPED • PA0204 for RCP D - TRIPPED 	M	<p>The RCPs are tripped to prevent damage to the seals upon loss of all seal cooling. Natural circulation is used to circulate coolant and to cooldown.</p> <p>The breakers are tripped by rotating the local hand switch to the STOP position. For this to work, control power needs to be available to each of the breaker control circuits. Control power is removed in Steps B4 and B5 after this step is completed.</p> <p>A fire in the control room could cause a loss of control power and prevent opening the breakers with the local hand switch. The fire would have to be located in either panel RL021, SB030A or SB033A for this to occur.</p>	7	Based on SA-08-006, the RCPs are assumed to be tripped within 7 minutes.	Yes. The breakers could spuriously close until Steps B4 and B5 are complete.	N/A
B2	Proceed To 2033 Turbine And Obtain A Copy Of This Procedure.	N/A	After the RCPs are tripped, the operator proceeds to the emergency equipment locker and obtains a copy of OFN RP-017.	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B3	<p>Perform the following:</p> <p>a. Obtain the following from emergency locker:</p> <ul style="list-style-type: none"> • Radio • Flashlight <p>b. Obtain pocket ion chambers and an RDD from the emergency locker for personnel entering the RCA</p> <ul style="list-style-type: none"> • Low-Range PIC 0-500 mR • High-Range PIC 0-5 R • RDD <p>c. Select Channel 1 on radio</p>	N/A	<p>A radio is required to ensure communication with the SRO at the ASP. Channel 1 is used by Operations for communication. A flashlight will supplement fixed Appendix R emergency lighting in the event of a loss of off-site power.</p> <p>Dosimetry is required for personnel entering the RCA.</p>	N/A	N/A	N/A	N/A
B4	<p>On PK41 OPEN breaker for DC control power to PA01</p> <ul style="list-style-type: none"> • PK4103 - OFF 	M	<p>Isolating DC control power to PA01 ensures cable damage will not cause the spurious closure of PA0107 or PA0108, causing the RCPs to start. Isolating control power before step B1 is complete will prevent opening the breakers using the local hand switch. Therefore, Step B4 shall be performed after Step B1.</p>	N/A	See Section 6.2 discussion about stopping the RCPs.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B5	<p>On PK62 Open breaker for DC control power to PA02</p> <ul style="list-style-type: none"> PK6204 - OFF 	M	Isolating DC control power to PA02 ensures cable damage will not cause the spurious closure of PA0204 or PA0205, causing the RCPs to start. Isolating control power before step B1 is complete will prevent opening the breakers using the local hand switch. Therefore, Step B5 shall be performed after Step B1.	N/A	See Section 6.2 discussion about stopping the RCPs.	No	N/A
B6	<p>Ensure RCP Breakers Are Tripped:</p> <ul style="list-style-type: none"> PA0107 for RCP A - TRIPPED PA0108 for RCP B - TRIPPED PA0205 for RCP C - TRIPPED PA0206 for RCP D - TRIPPED 	M	This step ensures the RCP breakers remain tripped after control power has been removed.	N/A	See Section 6.2 discussion about stopping the RCPs.	No	N/A
B7	<p>Check AL HV-36 CST to Turbine Driven AFP Suction Isolation Valve Open:</p> <p>a. Verify with SRO at ASP that Step 5.c is complete.</p> <p>b. Ensure AL HV-36 - OPEN</p>	D	Valve AL HV-36 is required to be open to ensure suction to the TDAFP from the CST. DCP 12170 modified the control circuit to ensure a control room fire will not damage the valve and prevent manual opening.	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAFP.	No	5.c

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B7 RNO	a. Do not continue until step 5.c is complete.	D	The operator completing step B7 RNO will not manually open AL HV-36 until it is verified that the breaker is off. With the breaker on, a spurious signal can close the valve after it has been opened.	35 minutes to start the pump and inject into steam generator B	See Section 6.3 for timing basis for the TDAPP.	No	5.c
B8	Descend To 1974' Elevation Via Ladders In AFW Valve Room And Enter The RCA.	N/A	This step provides the operator with the most efficient path to get to the Auxiliary Building. Dosimetry for entering the RCA is obtained in Step B3.	N/A	N/A	N/A	N/A
B9	In NCP Room, Close CCP To Regen Hx Valves a. Close Charging Header HCV-182 Inlet Isolation Valve • BG-8402B - CLOSED b. Close Charging Header BG HCV-182 Bypass Valve • BG-V017 - CLOSED	M	This step is required to prevent uncontrolled charging. Closing the valves ensures charging to the RCS through the Regen Hx is isolated.	14	See Section 6.2 for timing basis for isolating normal charging.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B10	<p>In North Mechanical Pent Room, Isolate CCW From RCP Thermal Barriers</p> <p>a. Verify with SRO that Step 5.c is complete.</p> <p>b. Ensure EG HV-61 - CLOSED</p> <p>c. Verify with Aux Bldg that Att D, Step D8 is complete.</p> <p>d. Ensure EG HV-133 - CLOSED</p>	S	<p>These valves are closed to prevent a steam bubble from migrating to the CCW piping when the CCW pumps are started. The valves are also closed to prevent cold CCW from being injected to the RCP thermal barrier when the CCW pump is started, which could cause damage to the RCP seals. The CCW pumps are not started until these valves are closed. As long as the valves are closed before starting the CCW pumps, then there is no possibility of water hammer or seal damage.</p> <p>a. Step 5.c opens the breaker associated with EG HV-61. After the breaker is open, control power is lost and the valve cannot spuriously actuate. If the breaker is confirmed open and the valve is closed, then it is in the desired position and will remain there throughout the event. If the valve is verified closed prior to ensuring Step 5.c is complete and the operator moves on to the next step, the valve could spuriously operate. Also see the discussion for Step 5.c.</p> <p>c. Step D8 opens the breaker associated with EG HV-133. After the breaker is open, control power is lost and the valve cannot spuriously actuate. If the breaker is confirmed open and the valve is closed, then it is in the desired position and will remain there throughout the event. If the valve is verified closed prior to ensuring Step D8 is complete and the operator moves on, the valve could spuriously operate. Also see the discussion for Step D8.</p>	Prior to the need for supported systems.	See Section 6.5 for discussion about support systems.	No	<p>b. 5.c</p> <p>d. D8</p>

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B10 RNO	<p>a. Do not continue until Step 5.c is complete.</p> <p>c. Do not continue until Att D, Step D8 is complete.</p>	S	The RNO ensures the operator does not continue until power is disconnected.	N/A	N/A	No	<p>b. 5.c</p> <p>d. D8</p>
B11	<p>In Aux Bldg Filter Alley, Locally Close Valves To Isolate RCP Seals:</p> <p>a. Seal Water Injection Filters Inlet Isolations.</p> <ul style="list-style-type: none"> • BG-V101 • BG-V105 <p>b. Inform Reactor Operator that Steps B10 and B11 are complete.</p>	M	Manual valves BG-V101 and BG-V105 isolate the seal injection lines and ensure spurious valve actuation will not restore seal injection. These valves are required to be closed before charging is restored to prevent RCP seal damage and loss of RCS inventory. The PFSSD strategy for a control room fire is to not restore seal cooling in order to prevent a seal LOCA if seal cooling is not restored promptly. Only one of these valves is open at a time but both are included because either one could be open at the time of the fire.	28 minutes to start the charging pump and inject to the RCS.	See Section 6.2 for timing basis for charging.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
B12	<p>At RP209 Across From North Mechanical Penetration Room Fail MSIV Bypass Valves Closed.</p> <ul style="list-style-type: none"> Fuse #46 - OFF 	R, M, D	<p>The action to pull this fuse was part of the original licensing basis strategy for control room fire. The strategy was approved by the NRC in Supplement 5 of the SER. Pulling the fuse removes control power from the MSIV bypass valve circuit and fails the valves closed. See Section 7.3.1 for more information.</p>	60	<p>SA-08-006 shows all four MSIVs can stay open for at least 1 hour as long as there are no other failures. This bounds the scenario where the bypass valves are open because the bypass lines are 2-inch diameter whereas the main steam lines are 28-inch diameter. See Section 6.1 for discussion about MSIVs.</p>	No	N/A
B13	<p>Verify BIT Isolation Valves open:</p> <p>a. Verify with person performing Aux Bldg actions that Attachment D, Steps D4 through D5 are complete.</p> <p>b. In the North Piping Penetration Room, locally Close "A" BIT OUTLET VALVE.</p>	M	<p>Step D4 opens the breaker for valve EM HV-8801B, ensuring the valve will not change position after it has been throttled.</p> <p>Step D5 opens the breaker for valve EM HV-8801A, ensuring the valve will not spuriously open after it has been closed.</p> <p>Valve EM HV-8801B is throttled manually to prevent overfilling the pressurizer. If the valve were to fully open with no letdown, the pressurizer would go solid and water would be lost to the PRT and eventually the floor of the reactor building. Therefore, the valve is manually throttled to control pressurizer level.</p>	<p>28 minutes to start the charging pump and control charging flow.</p> <p>The timing basis to close EM HV-8801A is being determined</p>	<p>See Section 6.2 for timing basis for charging.</p>	No	D4

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
	<ul style="list-style-type: none"> • EM HV-8801A CLOSED <p>c. In the North Piping Penetration Room locally throttle open BIT outlet isolation valve.</p> <ul style="list-style-type: none"> • EM HV-8801B THROTTLED OPEN <p>d. Notify the SRO that BIT is lined up for injection.</p> <p>e. Throttle EM HV-8801B as directed by the SRO to control PZR level.</p>		<p>Valve EM HV-8801A is closed to prevent overfilling the pressurizer. This step was added as a compensatory measure per CR 00045442, which identified the potential to overfill the pressurizer if this valve were to spuriously open as a result of a safety injection signal. Closing valve EM HV-8801A or ensuring it is closed will prevent the pressurizer from going water solid.</p>	<p>by CR 045442-02-04.</p>			
B13 RNO	<p>a. Do not continue until D4 through D5 are complete.</p>	M	<p>The RNO ensures the operator does not continue until power is disconnected to both valves.</p>	<p>28 minutes to start the charging pump and control charging flow.</p>	<p>See Section 6.2 for timing basis for charging.</p>	No	D4
B14	<p>Contact SRO At ASP For Further Direction</p>	N/A	N/A	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C1	Evacuate Control Room: a. Exit Control Room using north door b. Ensure Control Room outer doors - AT LEAST ONE CLOSED: * Normal outer door OR * Missile door c. Proceed to NK switchgear rooms.	N/A	The operator exits through the north door and retrieves his/her hard hat and proceeds to the NK switchgear room. Ensuring one of the control room doors is closed prevents the fire from spreading beyond the control room.	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C2	<p>Turn Off The Following NK Breakers:</p> <ul style="list-style-type: none"> • NK5108 for BB PCV-455A PZR PORV Control Power Breaker – OFF • NK5109 for Reactor Head Vent Valves – OFF • NK5119 for MSFIS Cab SA075A - OFF • NK4401 Breaker Control Power for NB02 - OFF • NK4413 MCB Control Panels RL019 and RL020 • NK4414 for Reactor Head Vent Valves - OFF • NK4416 SS Protection System: Out 2 Cabinet SB032D (Strm Dumps) – OFF 	M, D	<p>One pressurizer PORV is assumed to fail open. Both PORVs are failed closed by opening NK5108 and NK4421 to prevent loss of RCS inventory.</p> <p>NK5109 and NK4414 supply power to portions of RL021/RL022. Panel RL021/RL022 supplies power to a number of loads including the reactor head solenoid vent valves. Placing these switches in the OFF position will fail the solenoid valves closed, thereby preventing loss of inventory through the reactor head vents. Loss of power to the remaining loads supplied by these breakers will have no adverse impact on safe shutdown. Switches NK4414 and NK5109 are also opened to de-energize other potential Separation Group 1 and 4 125VDC power sources that could cause the pressurizer PORVs to open in the event of multiple proper polarity hot shorts within RL021/RL022.</p> <p>NK5119 supplies power to Train A MSFIS cabinet SA075A. Isolation of power to SA075A will close the main steam and main feedwater isolation valves. This action was added as a compensatory measure for CR 00045442, which identified the potential to overfill the steam generators if feedwater flow is not stopped in a timely manner.</p> <p>Control power for NB02 needs to be isolated before the NB02 breakers are manipulated in Step C5. Therefore, it makes sense to open the breaker in this step.</p>	3	<p>Based on SA-08-006, the pressurizer PORVs need to be closed within 3 minutes following reactor trip. This assumes a single PORV opens and no other spurious actuations. Therefore, NK5108, NK5109, NK4414 and NK4421 need to be opened within 3 minutes.</p> <p>The time required to open NK5119 is being analyzed by CR 045442-02-04.</p> <p>The time required to open the remaining switches in this step is greater than 3 minutes so opening them within 3 minutes will ensure PFSSD.</p>	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
	<ul style="list-style-type: none"> NK4421 for BB PCV-456A PZR PORV Control Power Breaker - OFF 		<p>NK4413 supplies power to the following PFSSD components: 1) Train B diesel generator room exhaust damper actuator GM HZ-19; 2) Solenoid actuators for radwaste building CCW supply/return header supply valves EG HV-70A and EG HV-70B; and, 3) Train B CCW temperature control valve EG TV-30. Loss of power to GM HZ-19 will fail the damper open, which is the desired position. Loss of power to EG HV-70A/B will fail the valves closed, which is the desired PFSSD position. Loss of power to EG TV-30 will fail the valve closed, allowing maximum cooling in the CCW system which will not adversely impact PFSSD. Loss of power to other components supplied by NK4413 will not adversely impact PFSSD.</p> <p>NK4416 supplies power to the steam dumps. Placing NK4416 in OFF isolates the steam dumps and prevents uncontrolled cooldown and return to criticality if the MSIVs fail to close.</p>				
C3	Proceed to NB02 Switchgear Room And Obtain A Copy Of This Procedure.	N/A	Prior to performing remaining steps, the Operator proceeds to the emergency locker and obtains a copy of OFN RP-017.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C4	<p>Perform the following:</p> <p>a. Obtain the following from the emergency locker:</p> <ul style="list-style-type: none"> • Radio • Flashlight <p>b. Select Channel 1 on radio.</p>	N/A	A radio is required to ensure communication with the SRO at the ASP and other operators. Channel 1 is used by Operations for communication. A flashlight supplements fixed battery powered emergency lights.	N/A	N/A	N/A	N/A
C5	<p>Ensure Train B Pump Breakers - OPEN</p> <ul style="list-style-type: none"> • NB0207 - OPEN • NB0206 - OPEN • NB0205 - OPEN • NB0204 - OPEN • NB0203 - OPEN • NB0202 - OPEN • NB0201 - OPEN 	S	<p>This step sheds large loads from the NB02 bus and is required prior to starting the Train B diesel generator in Step C6.</p> <p>Step C2 isolates control power to the NB02 bus and ensures the breakers do not spuriously close.</p>	Prior to the need for diesel generator	The timing for this step is based on the need for the supported PFSSD equipment.	No	C2

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C6	<p>Ensure Feeder Breakers To NB02 - OPEN</p> <ul style="list-style-type: none"> NB0209 - OPEN NB0212 - OPEN 	S	<p>This action isolates off site power to the NB02 bus and causes the diesel generator to automatically start on bus under voltage. The emergency generator is started to energize PFSSD equipment needed throughout this procedure.</p> <p>Step C2 isolates control power to the NB02 bus and ensures the breakers do not spuriously close.</p> <p>Step C5 needs to be completed to prevent overloading the diesel generator.</p>	Prior to the need for diesel generator	The timing for this step is based on the need for the supported PFSSD equipment. The most limiting time is restoring pressurizer backup group B heaters in Step A7 RNO.	No	C2, C5
C7	<p>Ensure ESA And ESB Relays - Energized</p> <p>a. Remove the break glass cover from the EMERGENCY START pushbutton, to energize the ESA and ESB relays.</p> <ul style="list-style-type: none"> KJ HS-101D - BREAK GLASS COVER REMOVED 	S	<p>This step energizes relays ESA and ESB on the Train B diesel generator engine control circuit (E-13KJ03A). The Wolf Creek licensing basis for control room fires assumes only a single spurious actuation occurs as a result of the fire. Therefore, it can be assumed that one of the two relays will energize.</p> <p>With at least one relay (ESA or ESB) energized, the unit parallel relay (UPR) will be de-energized (E-13NE13). Therefore, the diesel generator will not be in droop mode and will function properly as PFSSD loads are added.</p> <p>Also, with one relay (ESA or ESB) energized, relay 90 VEP will be energized which will switch the electronic voltage adjuster to a pre-determined setpoint and ignores signals from the control room auto/manual raise/lower switches. This ensures a fire in the control room will not affect the output voltage of the EDG during the event.</p>	Prior to the need for diesel generator	The timing for this step is based on the need for the supported PFSSD equipment. The most limiting time is restoring pressurizer backup group B heaters in Step A7 RNO.	No	C2, C5

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C8	<p>Align EDG B To Bus</p> <p>a. At panel KJ122, place CR Fire Iso Switch in isolate.</p> <ul style="list-style-type: none"> • KJ HS-110 - ISO <p>b. Check Diesel – STARTED</p> <p>c. Ensure Master Transfer Switch is in LOC/MAN</p> <ul style="list-style-type: none"> • KJ HS-109 - LOC/MAN <p>d. At Panel NE106 Check Indicator Light IL-8 - LIT</p> <p>e. Close EDG Output Breaker</p> <ul style="list-style-type: none"> • NB0211 - CLOSED <p>f. Check NB02 voltage on breaker NB0201 NORMAL</p>	S	<p>After loads are shed from the NB02 bus, and the NB02 feeder breakers are opened, the Train B diesel generator will automatically start and load to the bus when NB0211 is closed. Placing KJ HS-109 in LOC/MAN allows for local voltage regulation and also isolates portions of the control circuit from the control room. Local voltage regulation is not credited for PFSSD and is disabled by actuation of the emergency start switch in Step C7.</p> <p>DCP 12097 was implemented to add another KJ HS-109 contact to the control room stop circuit to ensure a control room fire will not shut the EDG down during the event. In addition, DCP 12097 added KJ HS-110 and redundant fuses to ensure power is available to the field flashing circuit. However, CR 30350 identified an issue where certain fuses located in NE106 could blow, preventing field flashing. Step C8.d and accompanying RNO was added to address this concern in the interim until a permanent modification is implemented. CR 30350-02-04 is tracking the implementation of the modification.</p> <p>Closing the EDG output breaker after the EDG is started energizes the NB02 bus.</p>	Prior to the need for diesel generator	See Section 6.5 for timing basis associated with EDG cooling.	Yes. A control room fire could prevent an automatic start of the Train B EDG. The RNO provides a method to start the engine if it does not auto start.	N/A

TABLE 7.1
 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C8 RNO	b. Perform the following: 1) Obtain handle from emergency locker 2) Place handle on either Air Start Valve: * Northeast end between cylinders and turbocharger <u>OR</u> * Southwest end between cylinders and generator 3) Pull handle down until diesel starts d. Perform the following: 1) Obtain new 15 amp fuses (two) from EDG emergency locker. 2) At panel NE106, open bottom cabinet third from left door.	S	The RNO for Step C8.a provides an assured method for starting the Train B diesel engine if it does not automatically start. Another method would be to use the emergency start switch, but this method may not work because of possible fire damage. Therefore, the RNO directs operators immediately to the assured method to minimize the time to start the engine. The RNO for Step C8.d provides instructions to restore power to the voltage regulator and excitation system circuit shown on drawing M-018-00636. Placing KJHS0109 in LOCAL/MAN in Step C8.c prevents the new fuses from blowing when they are inserted. Manual voltage control switches NEHS0014B and NEHS0016B are not used in OFN RP-017 and their contacts will remain open. This is an interim compensatory measure until a permanent modification is implemented.	Prior to the need for diesel generator	The timing for this step is based on the need for the supported PFSSD equipment.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
	3) Remove unmarked fuse block directly below Agastat. 4) Replace both 15 amp fuses and reinsert fuse block.						
C9	Ensure ESW Pump B Breaker - CLOSED • NB0215 - CLOSED	S	The ESW system supplies cooling water to the emergency diesel engine cooler, the component cooling water heat exchanger and various room coolers. The ESW system is also a backup source of auxiliary feedwater. NB0215 is normally open. Breaker control power is isolated in Step C2. If the breaker did not close in response to the load sequencer signal, Operators can close the breaker by pushing the manual close push button.	Prior to the need for supported components	This step starts the ESW pump. Step C12 closes the service water cross tie valve to prevent flow diversion from ESW to SW. See Section 6.5 for timing basis associated with EDG cooling.	No	C2
C9 RNO	Perform Attachment G to charge the closing springs and manually close NB0215.	S	Attachment G is included to provide instructions to operators to charge the closing springs if the breaker does not close. See the discussion regarding Attachment G basis at the end of this table.	N/A	This step starts the ESW pump. Step C12 closes the service water cross tie valve to prevent flow diversion from ESW to SW. See Section 6.5 for timing basis associated with EDG cooling.	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C10	<p>Ensure Load Center and ESW Pumphouse MCC Breakers – CLOSED:</p> <ul style="list-style-type: none"> • NB0208 – CLOSED • NB0210 – CLOSED • NB0213 – CLOSED • NB0216 – CLOSED 	S	<p>The Train B 480 VAC load centers and MCC breakers are not shed from the NB02 bus. Therefore, the listed breakers could remain closed. If the breakers open as a result of a control room fire, this step ensures they are closed.</p> <p>Step C2 disconnects control power from the NB02 bus and ensures the breakers do not spuriously open after they have been closed.</p> <p>NB0208 powers XPG022. PG2201 is cycled in Step A7 (RNO) to operate the pressurizer heater backup group B. See Step A7 RNO discussion for more information.</p> <p>NB0210 powers XNG04. NG0401 is closed in Step C13 to energize NG04. See Step C13 discussion for more information on NG04.</p> <p>NB0213 powers XNG02. NG0201 is closed in Step C11 to energize NG02. See Step C11 discussion for more information on NG02.</p> <p>NB0216 powers XNG06, which energizes Train B ESW pumphouse MCC NG006E. MCC NG006E powers a number of components required to ensure Train B ESW pump operability. The Train B ESW pump is directly powered from NB0215 and does not require NG006E to be energized.</p>	Prior to the need for supported components	The required time to complete this step is based on the time to place the supported systems in service. See Steps A7 RNO, C11, C13 and C17.	No	C2

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C10 RNO	Perform Attachment G to charge the closing springs and manually close the breakers.	S	Attachment G is included to provide instructions to operators to charge the closing springs if the breaker does not close. See discussion regarding Attachment G basis at the end of this table.	N/A	N/A	N/A	N/A
C11	<p>Isolate Control Power To NG02:</p> <p>a. Position NORMAL ISOLATE switch to ISOLATE</p> <ul style="list-style-type: none"> • NG HIS-15 - ISOLATE <p>b. On NG02, ensure Load Center NG02 Main Breaker - CLOSED</p> <ul style="list-style-type: none"> • NG0201 - CLOSED 	S	<p>This step is performed to ensure power is available to PFSSD components supplied by NG02. Power is provided to NG02 by NB0213. NB0213 is verified closed in Step C10. NG02 supplies power to a number of PFSSD components, but only a few are needed for OFN RP-017. These include:</p> <ul style="list-style-type: none"> • EF HV-32 • EF HV-34 • EF HV-46 • EF HV-50 • SGK05B • DSGL12B • XNN06 • BN HV-8812B • BG LCV-112C • EF HV-26 • EF HV-38 • BG HV-8111 • BN LCV-112E • DSGN01B • DSGL15B <p>Placing NG HIS-15 in isolate position will isolate the trip circuit and prevent a spurious breaker trip after the breaker has been closed. The hand switch needs to be operated first before manually closing the breaker to ensure a trip does not occur.</p>	Prior to the need for supported systems	The required time to complete this step is based on the time to place the supported systems in service. See Steps C12, C17, C18, C19, C20, C21, C23, D7, D10, D11, D12, D13, D20.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>EF HV-32, EF HV-34, EF HV-46 and EF HV-50 are opened in Steps D10 through D12 to provide a flow path to/from ESW to the Train B containment coolers.</p> <p>SGK05B is required to provide cooling to Class 1E electrical equipment rooms. The unit is started in Step D20 after all required lineups are made.</p> <p>DSGL12B is the Train B CCP room cooler fan motor. The pump room cooler provides a suitable ambient air temperature for the CCP motor. The cooler starts automatically when the pump motor starts. Failure of the room cooler to start does not prevent operation of the pump. The CCP is started in Step C23. ESW is lined up in Step C17.</p> <p>XNN06 is required to energize NN02 to provide long-term power to panels RP147A and RP147B. 125 VDC battery sets NK012 and NK014 provide the short-term power needs for these panels. The batteries are sized to supply power to all emergency loads for 200 minutes following loss of AC power per E-10NK, at which time the alternate power source will need to be lined up.</p> <p>BN HV-8812B is closed in Step C18 using BN HS-8812B. Step C11 is performed prior to C18, so power will be available when the operator performs Step C18.</p> <p>BG LCV-112C needs to be closed prior to starting</p>				

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>Train B CCP to ensure hydrogen is not introduced into the CCP suction. The valve is closed in Step C20 using BG HS-112C. Train B CCP is started in Step C23.</p> <p>EF HV-26 is closed in Step C12 using ISO/CLOSE switch EF HS-26A to prevent ESW flow diversion to the service water piping.</p> <p>EF HV-38 needs to be open to ensure a full flow return path from ESW to the UHS. EF HV-38 is fully opened in Step C17 by placing EF HS-38A in ISO/OPEN position. Power needs to be restored prior to the need for this valve to be fully open.</p> <p>BG HV-8111 is required to be open to prevent Train B CCP damage during low flow conditions. BG HV-8111 is opened in Step C21 by placing BG HS-8111A in ISO/OPEN position.</p> <p>BN LCV-112E is required to be open to provide a suction source from the RWST to the Train B CCP. BN LCV-112E is open in Step C19 by placing BN HS-112E in ISO/OPEN position.</p> <p>DSGN01B needs to be energized for containment cooling. The coolers are started in Step D13.</p> <p>DSGL15B is the Train B electrical penetration room cooler and is started in Step D7.</p>				

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C12	<p>At NG02AHF2, Position NORMAL ISO/CLOSE For ESW B/Service Water Cross- Connect Valve To ISO/CLOSE</p> <ul style="list-style-type: none"> EF HS-26A - ISO/CLOSE 	S	<p>This valve isolates the service water system and prevents flow diversion from ESW to the service water piping. This valve needs to be closed to ensure adequate flow to the required ESW loads. Step C11 restores power to the MCC cubicle for this valve.</p> <p>DCP 12170 modified the control circuit for EF HV-26 to address NRC IN 92-18 concerns.</p>	See Section 6.5 for timing associated with EDG cooling.	The limiting time is based on the need to establish EDG cooling. While Step C8 ensures the EDG is running, Step C6 potentially causes an automatic start. See Section 6.5 for discussion on ESW and EDG cooling.	No	N/A
C13	<p>Isolate Control Power To NG04:</p> <p>a. Position NORMAL ISOLATE switch to ISOLATE</p> <ul style="list-style-type: none"> NG HIS-16 - ISOLATE <p>b. On NG04, ensure Load Center NG04 Main Breaker - CLOSED</p> <ul style="list-style-type: none"> NG0401 - CLOSED 	S	<p>This step is performed to ensure power is available to PFSSD components supplied by NG04. NG04 supplies power to a number of PFSSD components, but only a few are required to be energized for OFN RP-017. These include:</p> <ul style="list-style-type: none"> AL HV-5 AL HV-30 AL HV-33 AL HV-34 DSGF2B EM HV-8803B DSGL11B EF HV-52 EG HV-16 EG HV-54 DSGN01D DPJE01B <p>Placing NG HIS-16 in isolate position will isolate the</p>	Prior to the need for supported systems	The required time to complete this step is based on the time to place the supported systems in service. See Steps A4, A5, A15, C22, C28, D4 and D13.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>trip circuit and prevent a spurious breaker trip after the breaker has been closed. The hand switch needs to be operated first before manually closing the breaker to ensure a trip does not occur.</p> <p>AL HV-5 needs to be opened to supply auxiliary feedwater to steam generator D. The valve is opened in Step A5 by placing AL HS-5 in LOCAL and AL HK-5B in OPEN. Power needs to be restored before the valve will operate.</p> <p>AL HV-30 needs to be opened to supply suction to the Train B MDAFP when the CST reaches low level. This is not a time critical step since the CST has sufficient volume for PFSSD. See Step A15 discussion.</p> <p>AL HV-33 needs to be opened to supply suction to the TDAFP when the CST reaches low level. This is not a time critical step since the CST has sufficient volume for PFSSD. See Step A15 discussion.</p> <p>AL HV-34 needs to be opened to ensure a suction supply from the CST to the Train B MDAFP. The valve is opened in Step A4 by placing AL HIS-34B in OPEN position. Step C13 needs to be completed before the valve will open.</p> <p>DSGF2B is the Train B MDAFP room cooler. The room cooler provides a suitable ambient air temperature for the equipment in the room. The cooler starts automatically when the pump starts as</p>				

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>long as power is available to the cooler motor. Power is established in Step C13. See Section 6.5 for discussion about room cooling.</p> <p>EM HV-8803B is opened in Step D4. Step C13 needs to be performed prior to the need for charging.</p> <p>DSGL11B is the Train B CCW pump room cooler. The room cooler provides a suitable ambient air temperature for the equipment in the room. The cooler starts automatically when either Train B CCW pump starts as long as power is available to the cooler motor. The CCW pumps are started in Step C22.</p> <p>EF HV-52 is opened in Step D4 by placing EF HS-52 in ISO/OPEN position. EF HV-52 needs to be open prior to the need for CCW. The CCW system is needed for CCP oil cooling and provides cooling water to the seal water heat exchanger. The Train B CCP is started in Step C23.</p> <p>EG HV-16 and EG HV-54 are opened in Step D4 by placing EG HS-16A and EG HS-54 in ISO/OPEN position. EG HV-16 and EG HS-54 need to be open to ensure CCW to the seal water heat exchanger prior to starting the Train B CCP. The seal water heat exchanger provides cooling for CCP recirc flow and is needed to ensure operability of the CCP. The Train B CCP is started in Step C23.</p> <p>DSGN01D needs to be energized for containment cooling. The coolers are started in Step D13.</p>				

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			DPJE01B needs to be energized to ensure Train B fuel oil transfer pump operability. The transfer pump is started in Step C28.				
C14	<p>Start Motor Driven AFW Pump B.</p> <p>a. Verify SRO performing Attachment A has completed steps A4 through A5.</p> <p>b. Start Motor Driven AFW pump B</p> <ul style="list-style-type: none"> • NB0205 - CLOSED <p>c. Notify SRO that Motor Driven AFW Pump B is running</p>	D	<p>a. Step A4 is required to be completed to ensure an adequate suction source to the AFW pump prior to starting the pump. Step A5 is required to be performed to ensure AFW flow from Train B MDAFP to steam generator D. If Step A5 is not complete before performing this step, there is no adverse impact since water will recirculate back to the CST.</p> <p>b. The MDAFP B is started by pushing the manual close push button at NB0205. Although control power is isolated, the springs are charged and ready to operate.</p> <p>Step C2 isolates control power to the NB02 bus and prevents a fire in the control room from spuriously opening NB0205 after it has been closed.</p>	15	SA-08-006 shows that PFSSD is assured if AFW is established to steam generator D within 15 minutes. See Section 6.3 for discussion about AFW.	No	C2, A4
C14 RNO	<p>a. DO NOT CONTINUE until steps A4 through A5 are complete.</p> <p>b. Perform Attachment G to charge the closing springs and manually close NB0205</p>	D	<p>a. This RNO ensures the operator does not continue until AFW Pump B valve alignment is complete in Steps A4 and A5.</p> <p>b. If the breaker re-opens after it has been closed or the springs are not charged, manual charging will be required to get the breaker to close. Attachment G provides the method to manually charge the springs. See discussion regarding Attachment G basis at the end of this table.</p>	15	SA-08-006 shows that PFSSD is assured if AFW is established to steam generator D within 15 minutes. See Section 6.3 for discussion about AFW.	No	C2, A4

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C15	<p>Ensure Motor Driven AFW Pump A Is Stopped:</p> <p>a. Remove CLOSE control power fuse (UC)</p> <ul style="list-style-type: none"> • NB0105/FUSE - OFF <p>b. Stop Motor Driven AFW Pump A</p> <ul style="list-style-type: none"> • NB0105 - OPEN 	D	<p>The Train A MDAFP breaker is opened to stop the pump and prevent uncontrolled AFW flow to steam generators B and C which could result in overfilling the steam generators. Although A Train equipment is not credited, spurious actuation of A Train equipment needs to be mitigated if it could lead to unwanted consequences. In this case, overfilling of the steam generators is not desired and is, therefore, being prevented in OFN RP-017.</p>	15	<p>SA-08-006 shows that if the pump is stopped within 15 minutes and other actions in the procedure are taken, overfilling of steam generators B and C will not occur.</p>	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C16	<p>Ensure Containment Spray Pump A is stopped:</p> <p>a. Remove CLOSE control power fuse (UC)</p> <ul style="list-style-type: none"> • NB0102/FUSE - OFF <p>b. Stop Containment Spray Pump A</p> <ul style="list-style-type: none"> • NB0102 - OPEN 	M	<p>This step ensures the Train A containment spray pump is not running and depleting the RWST inventory. The Train B containment spray pump is isolated in Step C5.</p> <p>Pulling the fuse isolates control power from the circuit to prevent a control room fire from closing the breaker. This action was approved by the NRC based on its inclusion in SLNRC-84-0109 (See Phase E action 18 and Note 20 in SLNRC 84-0109)</p>	67	<p>It is assumed that the Train A containment spray pump is operating and valve ENHV0006 is open to cause containment spray. E-1F9910 (see Fire Area C-22) shows that with 1 containment spray pump operating and flowing water to the header, operators have 67 minutes to stop the pump before the RWST level falls below that required for safe shutdown.</p>	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C17	<p>East Of NG02A, Align ESW Pump Room Ventilation:</p> <p>a. Position NORMAL ISO/OPEN switch for ESW Pump Room Supply Damper to ISO/OPEN</p> <ul style="list-style-type: none"> • GD HS-11A - ISO/OPEN <p>b. Position NORMAL ISO/RUN switch for ESW Pump Room Supply Fan to ISO/RUN</p> <ul style="list-style-type: none"> • GD HS-11 - ISO/RUN 	S	<p>ESW pump room ventilation maintains the ESW pump room temperature within required limits. Based on the Wolf Creek TRM, Table TR 3.7.22-1 the maximum temperature in the Train B ESW pump room is 149 F before equipment is declared inoperable. Maximum allowable sustained temperature in the room is 119 F. Step C9 starts the ESW pump. Step C10 energizes the Train B ESW pump room MCC.</p> <p>GD HS-11A isolates power to the ESW pump room supply damper and fails it open, which is the desired position.</p> <p>GD HS-11 starts the supply fan, isolates the control room circuits and inserts a redundant fuse.</p>	Prior to room reaching undesirable temperature	The timing basis depends on the time for the room to heat up to a point where the ESW pump will not operate. See Section 6.5 for discussion about room cooling.	No	N/A
C18	<p>At NG02AHF3, position NORMAL ISO/OPEN Switch For ESW To UHS Isolation Valve To ISO/OPEN.</p> <ul style="list-style-type: none"> • EF HS-38A - ISO/OPEN 	S	<p>Return flow from the ESW system to the UHS is required for diesel generator cooling, class 1E electrical equipment room cooling, auxiliary feedwater pump room cooler, centrifugal charging pump room cooler, electrical penetration room cooler, containment air coolers, component cooling water heat exchanger and component cooling water pump room cooler. EF HS-38A isolates the control room, adds a redundant fuse in the circuit and fully opens valve EF HV-38. Valve EF HV-38 is maintained partially open (66%) during normal operation and fully opens on SIS or</p>	Prior to the need for full flow in the ESW system	The timing basis depends on the limiting time to establish full flow in the ESW system. The valve needs to be fully open prior to establishing CCW heat exchanger and containment air	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>LOSP. A fire in the control room could cause a short that bypasses the control room handswitch and signals the valve to close. However, based on drawing E-13EF06A and E-025-00007, Sheet 185, the valve will not fully close because limit switch contact ZS/16 prevents the valve from closing past the 66% setpoint.</p> <p>The ESW loads that are necessary shortly after the diesel generator is started in Step C8 are diesel generator cooling, class 1E electrical equipment room cooling, auxiliary feedwater pump room cooler and electrical penetration room cooler. Based on calculation EF-10, the flow rates for each of these components are: diesel generator cooling (1,200 gpm), class 1E electrical equipment room cooling (66 gpm), auxiliary feedwater pump room cooler (128 gpm) and electrical penetration room cooler (100 gpm). The total flow to these loads is 1,494 gpm. As stated above, valve EF HV-38 will be approximately 66% open which is more than adequate to flow 1,494 gpm through this 30 inch valve. Therefore, Step C17 does not have to be performed to establish ESW flow to these loads.</p> <p>Step C17 will need to be completed before the remaining loads are needed to ensure full flow in the ESW system is available.</p>		<p>cooler flow, since the total flow to these systems is 11,350 gpm per calculation EF-10.</p> <p>See Section 6.5 for discussion about CCW and containment cooling.</p>		

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C19	<p>At NG02AFF4, Position NORMAL ISO/CLOSE Switch For RWST To RHR Pump B ISO Valve To ISO/CLOSE.</p> <ul style="list-style-type: none"> BN HS-8812B - ISO/CLOSE 	R, M	This action prevents or mitigates a loss of RWST inventory to the containment sump. The hand switch isolates the control room, inserts a redundant fuse in the control circuit and closes the valve. Step C11 restores power to the MCC cubicle for this valve.	28	Calculation XX-E-013 shows there is 28 minutes available before the RWST drains to a level below that required for cold shutdown.	No	N/A
C20	<p>On NG02AHR3, Open RWST To CCP B Suction Valve:</p> <ul style="list-style-type: none"> BN HS-112E - ISO/OPEN 	R, M	This step aligns the RWST to the Train B CCP. DCP 12175 added a control room isolation switch and redundant fuse at NG02AHR3 for this valve. This ensures valve BN HV-112E will open (if closed) and remain open throughout the event when BN HS-112E is placed in the ISO/OPEN position and power is restored in Step C11.	Prior to the need for charging	See Sections 6.1 and 6.2 for discussion about charging.	No	N/A
C21	<p>At NG02AFR2, Close VCT OUTLET ISO Valve.</p> <ul style="list-style-type: none"> BG HS-112C - ISO/CLOSE 	R, M	This valve is isolated before starting the charging pump to prevent hydrogen gas intrusion into the pump. DCP 12131 added a redundant fuse in the control circuit to ensure control power is available when the hand switch is placed in ISO/CLOSE. This ensures the valve will close in response to hand switch actuation after NG02 is energized in Step C11.	Prior to the need for charging	See Sections 6.1 and 6.2 for discussion about charging.	No	N/A
C22	<p>At NG02AHR1, open BG HV-8111 Charging Pump Mini Flow Isolation Valve.</p> <ul style="list-style-type: none"> BG HS-8111A - ISO/OPEN 	M	This valve is required to be open to protect the Train B CCP from overheating during low flow conditions. DCP 12175 added a control room isolation switch and redundant fuse at NG02AHR1 for this valve. This ensures valve BG HV-8111 will open (if closed) and remain open throughout the event when BG HS-8111A is placed in the ISO/OPEN position and power is restored in Step C11.	Prior to the need for charging	See Sections 6.1 and 6.2 for discussion about charging.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C23	<p>On NB02, Start One CCW Pump.</p> <p>a. Ensure Turbine Building Att B, Step B10 is complete</p> <p>b. NB0206 - CLOSED</p>	S	<p>The CCW system is required to provide cooling to the Train B CCP oil cooler and the seal water heat exchanger. Both of these components support operation of the Train B CCP.</p> <p>Step B10 closes the CCW outlet valves from the thermal barrier. This protects the CCW piping against water hammer and prevents inventory loss through the RCP seals. See Step B10 basis.</p> <p>Step C2 isolates control power to NB02 and ensures NB0206 does not spuriously open after it has been closed.</p> <p>Step C13 establishes power to the CCW pump room cooler and Step C17 completes lineup of ESW. Therefore, room cooling will be available prior to starting the pump.</p>	Prior to the need for supported components	See Section 6.5 for discussion about CCW.	No	B10, C2
C23 RNO	<p>a. Perform the following:</p> <p>1) WHEN Att B, Step B10 is complete, THEN perform Step C22.b.</p> <p>2) Do not continue until Step C22.b is complete.</p> <p>b. Perform the following:</p>	S	<p>a. The RNO ensures the operator does not continue until the prerequisite steps are complete.</p> <p>b.1 The RNO has the operator start CCW pump D if the B pump did not start. This RNO is included as an enhancement since the control room fire will not prevent an operator from manually closing NB0206.</p> <p>b.2 This RNO provides instructions for manually charging the springs and closing the breaker if it failed to close or did not remain closed. See discussion regarding Attachment G basis at the end of this table.</p>	Prior to the need for supported components	See Section 6.5 for discussion about CCW.	No	B10, C2

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
	1) IF NB0206 can NOT be closed, THEN close NB0207 to start CCW pump D. 2) IF no CCW pump can be started, THEN perform Attachment G to charge the closing springs and manually close breakers as necessary to establish one CCW pump running.						

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C24	<p>Start CCP B:</p> <p>a. Check RCP seal injection isolated and CCW service loop aligned</p> <ul style="list-style-type: none"> • Ensure Att B, Step B11 RCP seal isolation is complete <p style="text-align: center;">AND</p> <ul style="list-style-type: none"> • Ensure Steps D4 through D8 CCW service loop alignment are complete <p>b. NB0201 - CLOSED</p>	M	<p>Seal cooling is no longer restored in OFN RP-017 due to the uncertainty in the time before seal failure can occur. Therefore, prior to starting the CCP, operators verify seal injection is isolated. Seal injection is isolated in Step B11.</p> <p>The CCP oil cooler and seal water heat exchanger require CCW. Therefore, the CCW system needs to be aligned prior to starting the CCP. Step C22 starts the CCW pumps. Steps D4 and D5 align the CCW service loop to ensure adequate CCW flow to the CCP components.</p> <p>Other required alignments are made by this operator prior to performing Step C23. These alignments are made in steps C11, C19, C20 and C21. After all alignments are made, the CCP breaker is closed to start the pump.</p>	28	SA-08-006 shows the CCP needs to be started within 28 minutes. See Sections 6.1 and 6.2 for discussion about charging.	No	B11, C19, C20, C21, C22, D4, D5

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C24 RNO	<p>a. Perform the following:</p> <p>1) WHEN RCP seal injection is isolated AND CCW alignment is complete, THEN perform Step C23.b.</p> <p>2) Do Not continue until Step C23.b is complete.</p> <p>b. Perform Attachment G to charge the closing springs and manually close NB0201</p>	M	<p>a. The RNO ensures the operator does not continue until the prerequisite steps are complete.</p> <p>b. The RNO provides instructions for manually charging the springs and closing the breaker, if it failed to close or did not remain closed. See discussion regarding Attachment G basis at the end of this table.</p>	28	SA-08-006 shows the CCP needs to be started within 28 minutes. See Sections 6.1 and 6.2 for discussion about charging.	No	N/A
C25	Inform SRO That CCW and CCP Pumps Have Been Started	N/A	This step ensures the SRO is informed that the pumps are operating.	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C26	<p>Right Of NG04D, Align Diesel Generator Building Ventilation:</p> <ul style="list-style-type: none"> • Position NORMAL ISO/RUN switch for DG Ventilation Supply Fan to ISO/RUN <ul style="list-style-type: none"> ○ GM HS-11B - ISO/RUN • Open feeder breaker to GM TZ-11A <ul style="list-style-type: none"> ○ NG04DEF111 - OFF 	S	<p>This step ensures adequate Train B diesel generator room ventilation. The diesel generator room exhaust damper is failed open in Step C2 to ensure adequate diesel engine combustion air. The supply fan and outside air intake damper are not required for combustion air but are required for room cooling.</p> <p>GM HS-11B is an ISO/RUN switch that operates the Train B diesel generator room supply fan CGM01B. The switch isolates the control room, adds a redundant fuse in the circuit and starts the fan. The fan is powered from NG04DBF6 which is energized in Step C13.</p> <p>Opening NG04DEF111 will cut power to GM TZ-11A and fail the damper open. This damper is on the outside air intake for the room supply fan.</p>	155	<p>Calculation change notice AN-02-010-000-02 documents an analysis of the diesel generator room temperatures without supply fan operation. The calculation was performed using 3 different outside air temperatures (97, 100 and 105 F) and assumed the starting room temperature equals the outside room temperature (very conservative). The calculation shows that even at a starting room temperature of 105 F, it takes 155 minutes to reach the diesel generator design temperature of 122 F.</p>	No	N/A

TABLE 7.1
 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C27	<p>Isolate Possible RCS Leakage Paths:</p> <p>a. On NK41, open breaker for RCS To Excess Letdown Heat Exchanger Valves:</p> <ul style="list-style-type: none"> • NK4119 - OFF <p>b. On NK44, open breaker for RCS To Excess Letdown Heat Exchanger Valves:</p> <ul style="list-style-type: none"> • NK4407 - OFF 	M	<p>NK4119 and NK4407 supply power to portions of RL001/RL002. Panel RL001/RL002 supplies power to a number of loads, including the excess letdown heat exchanger valves. Loss of power to these valves will fail them closed, preventing inventory loss through this path.</p> <p>Loss of power to the remaining loads supplied by these breakers in RL001/RL002 will have no adverse impact.</p>	37	<p>For the excess letdown flow path to open, it would take spurious operation of at least 3 valves. Flow would be limited to the volume that can flow through the 1" excess letdown pipe. The pressurizer level is typically held at 55 to 60%. After a trip, the volume will shrink due to RCS cooldown to 561F. Based on SA-08-006, initial shrinkage is typically to 30% NR. Per WCRE-03, 30% equates to 4,373 gallons. The volume of water below the lowest level transmitter is 637 gallons. Therefore, the inventory that can be lost before going off scale low is</p>	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
					3,736 gallons. Assuming a maximum of 100 gpm lost through the excess letdown flow path, there is at least 37 minutes available to mitigate a failed open excess letdown flow path.		
C28	<p>On NK44, Open Breaker For S/G Blowdown Isolation Valves:</p> <ul style="list-style-type: none"> NK4411 - OFF 	R, M, D	<p>NK4411 supplies power to Separation Group 4 125 vdc loads in RL023/RL024. These loads include blowdown valves BM HV-1 thru BM HV-4. Disconnecting power to these valves will fail them closed, which is the desired position.</p> <p>Loss of power to the remaining loads supplied by this breaker will have no adverse impact.</p> <p>Also see discussion in Section 7.3.1.a.</p>	60	SA-08-006 shows the blowdown valves can remain open for the modeled duration of 1 hour.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C29	<p>Start EDG Fuel Oil Xfer Pump:</p> <p>a. At NG04DDF3, place Emergency FO Transfer Pump Isolation Switch in Isolate.</p> <ul style="list-style-type: none"> • JE HS-21C - ISOLATE <p>b. At panel KJ-122, start Emergency Fuel Oil Transfer Pump.</p> <ul style="list-style-type: none"> • JE HS-21B - RUN 	S	<p>Change package 12176 added hand switch JE HS-21C to isolate the pump control circuit from the Control Room. In addition, operation of the switch will insert a new fuse in the circuit in case the main fuse opened as a result of the fire. This ensures the transfer pump will start when JE HS-21B is placed in the RUN position. NG04 is energized in Step C13.</p>	60	<p>The diesel engine can run for at least 60 minutes using the fuel in the day tank, given the reduced loading imposed on the engine during PFSSD. Therefore, this action should be completed within 60 minutes.</p>	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C30	<p>Check EDG B Room Temperature</p> <p>a. Check room temperature greater than 65°F</p> <p>b. Check room temperature less than 110°F</p>	S	<p>This step was added in OTSC 10-0093 as a result of condition report 31408. Step C25 has operators fully open the B EDG pump room supply damper and start the supply fan. There are no operator actions taken for the recirculation damper. This lineup may not be adequate during all times of the year. In the winter months, drawing in 100% outside air with a closed recirculation damper could cause the room temperature to drop below freezing. In the summer months, with the recirculation damper open, the room could heat up to an undesired temperature. The temperature range of 65 to 110 degrees F ensures the room temperature remains within the required range. These are interim actions until a permanent resolution is determined. Condition Report Action 30350-02-07 is tracking the resolution of this issue.</p>	Prior to room reaching undesirable temperature	The timing basis depends on the time for the room to heat up or cool down to a point where the B EDG and associated components will not operate. See discussion for Step C25 for further discussion.	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
C30 RNO	<p>a. Perform the following:</p> <p>1) Open breaker NG04DBF6 to stop B EDG Room Supply Fan</p> <p>2) <u>WHEN</u> temperature reaches 90°F, <u>THEN</u> close breaker NG04DBF6 to start B EDG Room Supply Fan</p> <p>b. Perform the following:</p> <p>1) <u>WHEN</u> temperature reaches 110°F, <u>THEN</u> open breaker 12 on NG04DEF1 to fail Recirc Damper closed.</p> <p>2) <u>WHEN</u> temperature reaches 65°F, <u>THEN</u> close breaker 12 on NG04DEF1 to energize Recirc Damper.</p>	S	<p>This RNO performs the necessary steps to ensure the Train B EDG room temperature remains within the required range. These steps are performed locally. Opening NG04DBF6 will de-energize the supply fan and allow the room to heat up if the temperature drops below 65°F. When the temperature reaches 90°F, the operator will re-start the fan.</p> <p>When the room temperature reaches 110°F, the operator will open breaker NG04DEF112 to fail the recirculation damper closed, allowing 100% outside air into the room to cool the room. When the temperature drops to 65°F, the operator will close breaker NG04DEF112 to re-energize the recirculation damper to allow it to open. If the recirc damper does not open due to the fire in the control room, then the operator can perform the RNO for Step C29.a to increase the room temperature.</p> <p>These are interim actions until a permanent resolution is determined. Condition Report Action 30350-02-07 is tracking the resolution of this issue.</p>	Prior to room reaching undesirable temperature	The timing basis depends on the time for the room to heat up or cool down to a point where the ESW pump and associated components will not operate. See Section 6.5 for discussion about room cooling.	N/A	N/A
C31	Contact SRO at ASP For Further Direction	N/A	N/A	N/A	N/A	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D1	<p>In Rod Drive M/G Room Isolate Normal Letdown PK5117, RC & SUPPORT SYS. CONTROL PNL. RL001 & RL002.</p> <ul style="list-style-type: none"> • PK5117 - OFF 	M	<p>The PFSSD strategy is to use BG LCV-459 and BG LCV-460 to isolate normal letdown. In order to isolate BG LCV-459 and BG LCV-460, PK5117 is placed in the OFF position to disrupt power to these valves and fail them closed. This will also disrupt power to auxiliary pressurizer spray valve BGHV8145 and fail the valve closed. This action will also disrupt power to a number of other separation group 5 125 vdc loads in RL001/RL002, but this will have no adverse impact on PFSSD.</p>	7	<p>SA-08-006 assumes the letdown isolation valves are closed within 7 minutes and the auxiliary spray valve is closed within 7 minutes.</p>	No	N/A
D2	<p>Proceed to Emergency Locker 2026' Level And Obtain A Copy Of This Procedure.</p>	N/A	<p>Procedure is required to complete remaining Attachment D steps.</p>	N/A	N/A	N/A	N/A
D3	<p>Perform The Following:</p> <p>a. Obtain the following from emergency locker:</p> <ul style="list-style-type: none"> • Radio • Flashlight • FR Jump Suit • Circular soft jawed pliers <p>b. Select Channel 1 on radio</p>	N/A	<p>A radio is required to ensure communication with the SRO at the ASP and other operators. Channel 1 is used by Operations for communication. A flashlight supplements fixed battery powered emergency lights. The FR jump suit is required to operate certain breakers. The soft-jawed pliers are required to disconnect the amphenol connectors for the main steam isolation valves.</p>	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D4	<p>On NG04C, Perform the Following:</p> <ul style="list-style-type: none"> At NG04CJF3, place EG HS-16A to ISO/OPEN At NG04CKF1, place EG HS-54 to ISO/OPEN At NG04CKF2, place EM HS-8803B to ISO/OPEN Turn off NG04CKF3, EMHV8801B BIT DISCHARGE ISOLATION VALVE Bkr At NG04CNF3, place EF HS-52 to ISO/OPEN Turn off NG04CHF2, EFHV60 ESW FROM CCW HX ISO VALVE breaker 	M, S	<p>EG HS-16A is placed in ISO/OPEN to open EG HV-16 and provide a return flow path from the service loop to the Train B CCW pump suction. The valve is required to be open to ensure CCW flow to the seal water heat exchanger, which is required to ensure Train B CCP operability. The valve will open when power is restored to NG04 in Step C13. Placing the switch in ISO/OPEN before power is restored will have no adverse impact.</p> <p>EG HS-54 is placed in ISO/OPEN to open EG HV-54 and provide a supply flow path from the Train B CCW pump to the service loop. The valve is required to be open to ensure CCW flow to the seal water heat exchanger, which is required to ensure Train B CCP operability. The valve will not actually open until power is restored to NG04 in Step C13. Placing the switch in ISO/OPEN before power is restored will have no adverse impact.</p> <p>EM HS-8803B is placed in ISO/OPEN to ensure Train B CCP flow to the RCS through the BIT. This is the only boration and inventory control flow path credited. The valve will not actually open until power is restored to NG04 in Step C13. Placing the switch in ISO/OPEN before power is restored will have no adverse impact.</p> <p>NG04CKF3 is placed in OFF to prevent spurious operation of EM HV-8801B. DCP 12130 modified the control circuit for EM HV-8801B to address NRC IN 92-18 concerns. Step B13 throttles EM HV-8801B.</p>	Prior to the need for charging and supported equipment	<p>See Sections 6.1 and 6.2 for timing basis for charging.</p> <p>See Section 6.5 for timing basis for CCW and ESW.</p>	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
			<p>EF HS-52 is placed in ISO/OPEN to ensure a flow path from Train B ESW to the Train B CCW heat exchanger. The Train B CCW heat exchanger is required for CCP B oil cooler and the seal water heat exchanger, which are both required for CCP operability. The valve will not actually open until power is restored to NG04 in Step C13. Placing the switch in ISO/OPEN before power is restored will have no adverse impact.</p> <p>NG04CHF2 is placed in off position to prevent spurious operation of EF HV-60. This step was added as an interim compensatory measure in response to CR 41746, which identified that a control room fire could cause the valve to open. If this occurs, a flow imbalance would occur in the B ESW system. DCP 13898 is being prepared to add an isolation/close switch and redundant fuse to address this concern permanently. The Evaluation of Proposed Change for DRR 11-1583 associated with OFN RP-017, Rev. 36 evaluates this change.</p>				
D5	<p>On NG01B, Isolate Power To EM HV-8801A, BIT Outlet Valve</p> <ul style="list-style-type: none"> NG01BER2 – OFF 	M	<p>Valve EM HV-8801A is closed in Step B13 to prevent overfilling the pressurizer. Step D5 needs to be completed prior to Step B13 to prevent the valve from re-opening. This step was added as a compensatory measure per CR 00045442, which identified the potential to overfill the pressurizer if this valve were to spuriously open as a result of a safety injection signal. Closing valve EM HV-8801A or ensuring it is closed will prevent the pressurizer from going water solid.</p>	N/A	<p>The timing basis to close EM HV-8801A is being determined by CR 045442-02-04.</p>	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D6	<p>Locally Ensure CCW Return From Nuclear Auxiliary Components to Train A CCW Is Closed:</p> <ul style="list-style-type: none"> Verify with SRO at ASP, that Step 5.c is complete. Ensure EG HV-15 is closed. 	S	<p>EG HV-15 is closed to ensure flow is not diverted to the Train A CCW surge tank. The CCW lineup in OFN RP-017 maintains water flow from CCW to the excess letdown heat exchanger. Therefore, Train B return flow could potentially flow into the Train A CCW piping if EG HV-15 is open.</p> <p>Step 5.c opens the MCC breaker for EG HV-15 and needs to be completed before Step D5.</p>	Prior to the need for supported equipment	See Section 6.5 for timing basis for CCW.	No	5.c
D6 RNO	a. DO NOT CONTINUE until Step 5.c is complete.	S	The RNO ensures the operator does not continue until the prerequisite step is complete.	Prior to the need for supported equipment	See Section 6.5 for timing basis for CCW.	No	5.c
D7	Locally Check EF HV-60, ESW TRN B FROM CCW HX B Closed	S	CR 41746 identified a concern where EF HV-60 could spuriously open in the event of a control room fire. This would cause a flow imbalance in the ESW system and possibly reduce cooling flow to other essential PFSSD components. This step was added as a compensatory measure to immediately address the concern in this CR. DCP 13898 is being prepared to add an isolation/close switch and redundant fuse to address this concern permanently. The Evaluation of Proposed Change for DRR 11-1583 associated with OFN RP-017, Rev. 36 evaluates this change.	Prior to the need for supported equipment	See Section 6.5 for timing basis for ESW.	No	D4
D7 RNO	Manually close EF HV-60	S	See Step D6 Basis	Prior to the need for supported equipment	See Section 6.5 for timing basis for ESW.	No	D4

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D8	<p>In South Electrical Penetration Room, Place Boron Inj Upstream Test Line NORM ISO/CLOSE Switch To ISO/CLOSE.</p> <ul style="list-style-type: none"> EM HS-8843 - ISO/CLOSED 	M	<p>This step ensures one of the two SIS test lines is isolated to prevent flow diversion through the test line. Step D15 isolates the second line. Both valves are normally closed and fail closed on loss of power. Switch EM HS-8843 will isolate power to the valve and fail it closed.</p> <p>The SIS test lines discharge into a common 3/4 inch line. Flow would then pass two normally closed 3/4 inch air operated valves before returning to the RWST or the RHUT. For the failure to occur, there would have to be 3 spurious actuations, which is extremely unlikely and is not postulated for a control room fire.</p>	71 hours	<p>With the SIS flow path open, it would take a considerable amount of time to reduce RWST volume to below that needed for safe shutdown. Per XX-E-013, 214,260 gallons can be lost from the RWST. Assuming 50 gpm lost through the 3/4" SIS test line, it would take 71 hours to reduce RWST volume to a level below that required for safe shutdown.</p>	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D9	<p>On NG02B, Start Electrical Penetration Room Cooler:</p> <p>a. At NG02BAF2, place Norm/Iso-Run switch to ISO-RUN</p> <ul style="list-style-type: none"> o GL HS-35 - ISO-RUN <p>b. At NG02BAF2, depress start pushbutton</p>	S	<p>Based on the Wolf Creek TRM, Table TR 3.7.22-1, the allowable temperature in the Train B electrical penetration room is 101 F. The maximum temperature is 131 F.</p> <p>Switch GL HS-35, when placed in ISO/RUN position, will isolate the control room circuit and insert a redundant fuse. However, the unit will not start until the start push button is depressed, which will energize the 42 coil, close the seal in contact and start the unit. Therefore, both GL HS-35 and the push button need to be actuated to start the cooler. Step C13 establishes power to the cooler.</p>	Prior to room reaching unacceptable temperature	The timing of this step is based on the time for the room to reach temperatures beyond operability limits of the equipment. See Section 6.5 for discussion on room cooling.	No	N/A
D10	<p>On NG02B, Isolate Power To EG HV-133, THERMAL BARRIER CCW RETURN HV-61 BYPASS ISO VLV.</p> <ul style="list-style-type: none"> • NG02BHF1 - OFF 	S	Step B10 verifies EG HV-133 is closed after this step is complete. This valve is closed for the same reason that EG HV-61 is closed. See the discussion for Step 5.c.	Prior to the need for supported systems	See Section 6.5 for discussion about CCW.	No	N/A
D11	Inform the Reactor Operator that CCW Alignment is Completed	S	<p>This step provides confirmation to the RO that Step D8 has been completed.</p> <p>Step C22.a requires the RO to confirm Step B10 is complete. Step B10 cannot be completed until Steps 5.c and D8 are complete. When Steps 5.c, D8 and B10 are complete, the RO can start the CCW pump in Step C22.b.</p>	28	See Step C22 for timing basis for CCW.	N/A	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D12	<p>On NG02BHF3, Open ESW TO CTMT Isolation Valve:</p> <ul style="list-style-type: none"> EF HS-34 - ISO/OPEN 	S	<p>DCP 11086 added a control room isolation switch and redundant fusing at MCC cubicle NG02BHF3 for valve EF HV-34. This ensures the valve will open (if closed) and remain open throughout the event when EF HS-34 is placed in the ISO/OPEN position and power is restored to NG02B. This valve is required to be open to ensure ESW flow to the Train B containment coolers.</p> <p>Step C11 establishes power to load center NG02, which supplies power to cubicle NG02BHF3. If Step D10 is performed prior to Step C11, there will be no adverse impact.</p>	60	See Section 6.5 for discussion about containment cooling.	No	N/A
D13	<p>On NG02BHR2, Open ESW FROM CTMT Isolation Valve:</p> <ul style="list-style-type: none"> EF HS-46 - ISO/OPEN 	S	<p>DCP 11086 added a control room isolation switch and redundant fusing at MCC cubicle NG02BHR2 for valve EF HV-46. This ensures the valve will open (if closed) and remain open throughout the event when EF HS-46 is placed in the ISO/OPEN position and power is restored to NG02B. This valve is required to be open to ensure ESW flow from the Train B containment coolers.</p> <p>Step C11 establishes power to load center NG02, which supplies power to cubicle NG02BHR2. If Step D11 is performed prior to Step C11, there will be no adverse impact.</p>	60	See Section 6.5 for discussion about containment cooling.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D14	<p>On NG02B, open ESW To/From CTMT Air Cooler Valves.</p> <p>a. At NG02BDR1 open EF HV-32 ESW B To CTMT Air Coolers</p> <ul style="list-style-type: none"> • EF HS-32 - ISO/OPEN <p>b. At NG02BDR2 open EF HV-50 ESW B From CTMT Air Coolers</p> <ul style="list-style-type: none"> • EF HS-50 - ISO/OPEN 	S	<p>DCP 12131 added control room isolation switches and redundant fuses at MCC cubicles NG02BDR1 (EF HV-32) and NG02BDR2 (EF HV-50) for these valves. This ensures valves EF HV-32 and EF HV-50 will open (if closed) and remain open throughout the event when EF HS-32 and EF HS-50 are placed in the ISO/OPEN position and power is restored to NG02B. These valves are required to be open to ensure ESW flow to/from the Train B containment coolers.</p> <p>Step C11 establishes power to load center NG02, which supplies power to cubicles NG02BDR1 and NG02BDR2. If Step D12 is performed prior to Step C11, there will be no adverse impact.</p>	60	See Section 6.5 for discussion about containment cooling.	No	N/A
D15	<p>Start Containment Cooler Fans B and D:</p> <p>a. At NG02TAF1, start CTMT Cooler Fan B</p> <ul style="list-style-type: none"> • GN HS-9A - ISO/RUN <p>b. At NG04TAF1, start CTMT Cooler Fan D</p> <ul style="list-style-type: none"> • GN HS-17A - ISO/RUN 	S	<p>DCP 12177 installed a redundant fuse in the control circuit for each fan so that, in the event of a fire in the control room, the fans will start when GN HS-9A and GN HS-17A are placed in ISO/RUN position and power is restored to NG02T and NG04T.</p> <p>Step C11 establishes power to load center NG02, which supplies power to NG02TAF1. If Step D13 is performed prior to Step C11, there will be no adverse impact.</p> <p>Step C13 establishes power to load center NG04, which supplies power to NG04TAF1. If Step D13 is performed prior to Step C13, there will be no adverse impact.</p>	N/A	See Section 6.5 for discussion about containment cooling.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D16	<p>In North Electrical Penetration Room, Place Boron Inj Downstream Test Line NORM ISO/CLOSE Switch to ISO/CLOSE.</p> <ul style="list-style-type: none"> EM HS-8882 - ISO/CLOSED 	M	<p>This step ensures one of the two SIS test lines is isolated to prevent flow diversion through the test line. Step D6 isolates the second line. Both valves are normally closed and fail closed on loss of power. Switch EM HS-8882 will isolate power to the valve and fail it closed.</p> <p>The SIS test lines discharge into a common 3/4 inch line. Flow would then pass two normally closed 3/4 inch air operated valves before returning to the RWST or the RHUT. For the failure to occur, there would have to be 3 spurious actuations, which is extremely unlikely and is not postulated for a control room fire.</p>	71 hours	See D6 discussion.	No	N/A
D17	<p>Ensure MSIVs Are Closed By Unplugging the Amphenal Connectors:</p> <ul style="list-style-type: none"> AB HV-11 - A Train TB14540 AB HV-14 - A Train TB14533 AB HV-17 - A Train TB14538 AB HV-20 - A Train TB14535 	R, M, D	<p>This step ensures the MSIVs are closed if they did not close in Step 3. The MSIVs were replaced per DCPs 09952 and 11608 with system medium actuated valves. Unplugging the Amphenal connectors will isolate power to one train of solenoids and fail the valves closed.</p>	60	SA-08-006 shows all four MSIVs can stay open for at least 1 hour as long as there are no other failures. The steam dumps are isolated in Step C2 and the steam generator ARVs will control temperature. See Section 6.1 for additional discussion regarding MSIVs.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D18	Notify SRO at the Aux Shutdown Panel, Status of MSIVs	N/A	This step ensures the SRO knows the Amphenal connectors have been pulled. The new MSIVs have no external position indication so the operator at the ASP will have to rely on available instrumentation to determine position.	60	See D15 discussion.	N/A	N/A
D19	Request SRO At ASP To Ensure S/G A And C ARVs - CLOSED <ul style="list-style-type: none"> • AB PV-1 - CLOSED • AB PV-3 - CLOSED 	R, M, D	AB PV-1 and AB PV-3 are closed by the SRO at the ASP. AB PV-2 and AB PV-4 are isolated from the control room and controlled from the ASP.	60	See Section 6.1 for discussion about steam generator ARVs.	No	N/A
D20	Isolate air and N2 to AB PV-3, SG C ATMOSPHERIC RELIEF VLV: <ul style="list-style-type: none"> a. KAV1445 - CLOSED b. KAV1366 - CLOSED c. Vent air from regulator d. Verify AB PV-3 closed 	R, M, D	This step isolates air and nitrogen and bleeds air from the regulator to prevent the valve from opening.	60	See Section 6.1 for discussion about steam generator ARVs.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D20 RNO	d. Close AB-V029, SG C ATMOSPHERIC RELIEF VLV ISO	R, M, D	If AB PV-3 cannot be closed, then manual valve AB-V029 can be closed to isolate steam generator C ARV.	60	See Section 6.1 for discussion about steam generator ARVs.	No	N/A
D21	<p>Isolate air and N2 to AB PV-1, SG A ATMOSPHERIC RELIEF VALVE</p> <p>a. KAV1435 - CLOSED</p> <p>b. KAV1364 - CLOSED</p> <p>c. Vent air from regulator</p> <p>d. Verify AB PV-1 closed</p>	R, M, D	This step isolates air and nitrogen and bleeds air from the regulator to prevent the valve from opening.	60	See Section 6.1 for discussion about steam generator ARVs.	No	N/A
D21 RNO	d. Close AB-V018, SG A ATMOSPHERIC RELIEF VLV ISO	R, M, D	If AB PV-1 cannot be closed, then manual valve AB-V018 can be closed to isolate steam generator A ARV.	60	See Section 6.1 for discussion about steam generator ARVs.	No	N/A

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
D22	<p>In SGK04B Room, Start Class 1E Electrical Equipment A/C Unit:</p> <ul style="list-style-type: none"> • Position SGK05B NORMAL ISO/RUN Switch To ISO/RUN <ul style="list-style-type: none"> ○ GK HS-103 - ISO/RUN 	S	This step ensures room cooling to the Class 1E switchgear rooms. The cooler needs to be started before the rooms reach a temperature beyond operating limits for the equipment. Based on the TRM, Table 3.7.22-1, the maximum allowable temperature in the rooms supplied by SGK05B is 101 F. In order for the unit to operate, there needs to be power to NG02A and ESW flow to the cooler. Power is restored in Step C11. ESW lineup is completed by step C12. Steps C11 and C12 should be completed well before Step D20.	60	Technical Requirement 3.7.23 states that with one Class 1E A/C Unit inoperable, establish compensatory measures within 2 hours. For the purposes of OFN RP-017, 1 hour will be used as the timing requirement to restore cooling. See Section 6.5 for additional discussion about room cooling.	No	C9, C12
D23	Proceed As Directed By SRO at ASP.	N/A	Attachment D is complete and the SRO will direct the operator at this point.	N/A	N/A	N/A	N/A
E1	<p>Proceed to NB02 Switchgear Room And Obtain The Following:</p> <ul style="list-style-type: none"> * Copy of this procedure * Flashlight 	N/A	Procedure is required to complete remaining Attachment E steps.	N/A	N/A	N/A	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
E2	Place BN HV-8812A, RWST TO RHR PUMP A SUCTION ISOLATION VALVE Breaker To Off • NG01ACR2 - OFF	M	This Step ensures BN HV-8812A is de-energized and will not spuriously operate after it has been manually closed in the next step.	28	Calculation XX-E-013 shows there is 28 minutes available before the RWST drains to a level below that required for cold shutdown.	No	N/A
E3	In RHR Pump Room A, Close RWST To RHR Pump A Isolation Valve. • BN HV-8812A - CLOSED	M	Valve BN HV-8812A is normally open and is manually closed in OFN RP-017 to prevent the RWST from draining to the containment sump in the event EJ HV-8811A spuriously opens. Valve BN HV-8812A is a Train A valve so power may not be available, which is why manual operation is required. Step E2 isolates power to the control circuit to prevent spurious operation after the valve is closed. DCP 12173 modified the control circuit to ensure a control room fire will not damage the valve and prevent manual closure.	28	Based on XX-E-013, operators have 28 minutes to close the valve and prevent the RWST from draining to the containment sump.	No	E2

TABLE 7.1
DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017

STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
E4	<p>Ascend Ladders To 2000 Elevation Aux Feedwater Pump Room Area And Close The Following Valves:</p> <ul style="list-style-type: none"> ○ TD AFWP DISCHARGE TO SG A HV-8 INLET ISO. <ul style="list-style-type: none"> ○ AL-V056 – CLOSED ○ TD AFWP DISCHARGE TO SG D HV-6 INLET ISO. <ul style="list-style-type: none"> ○ AL-V061 – CLOSED ○ MD AFWP DISCHARGE TO SG A HV-7 INLET ISO. <ul style="list-style-type: none"> ○ AL-V032 – CLOSED ○ TD AFWP DISCHARGE TO SG C HV-12 INLET ISO. <ul style="list-style-type: none"> ○ AL-V071 – CLOSED 	D	This step isolates possible AFW flow diversion paths to prevent overfilling the steam generators.	35	Calculation SA-08-006 shows that the steam generators could overfill if the valves are not closed within 35 minutes.	No	N/A

TABLE 7.1 DETAILED EVALUATION OF EACH ACTION STEP IN OFN RP-017							
STEP	DESCRIPTION	PFSSD Function (Note 1)	BASIS	Req'd Time To Complete (min)	TIMING BASIS	CR Fire Impact? (Note 2)	Prereq Steps
E5	Notify HP that a non-RCA area was entered into from the RCA.	N/A	This step notifies HP that the operator entered the auxiliary feedwater area from the RCA and the area may be contaminated.	N/A	N/A	N/A	N/A
E6	Proceed To ASP And Inform The SRO That BN HV-8812A and the Aux Feedwater Valves Are Closed.	N/A	Attachment E is complete and the SRO will direct the operator at this point.	N/A	N/A	N/A	N/A
Att F	Actions to Protect Train A Equipment	N/A	This attachment was added based on Reference 3.1.a. See discussion under Reference 3.1.a and Step A16.	N/A	N/A	N/A	N/A
Att G	Manual Charging of Siemens Circuit Breakers	N/A	This attachment is included to provide instructions to operators on how to manually charge the Siemens circuit breakers. This attachment is used for some RNO actions throughout the procedure. The springs are charged for one cycle of operation so entering the attachment will not normally be necessary.	N/A	N/A	N/A	N/A

Table Notes:

1. PFSSD Functions are as follows: R - Reactivity Control; M - Reactor Coolant Makeup and Inventory Control; D - Decay Heat Removal; P - Process Monitoring; S - Support; N/A - Not Applicable
2. The column labeled "CR Fire Impact?" identifies if a fire in the control could potentially cause the component to mis-position after the step has been completed. Yes means the component can mis-position and No means the component cannot mis-position. N/A means the question is not applicable to the step.

Appendix 1

OFN RP-017 Credited Component Evaluation

Table A1 documents whether the components credited for hot standby following a control room fire are properly protected against hot shorts, open circuits or shorts to ground that could occur due to a fire in the control room. Also, the evaluation documents whether adequate isolation capability is provided to ensure the credited components remain functional and unaffected by the fire after control room isolation is completed.

This evaluation was performed to satisfy an NRC commitment made in Licensee Event Report 2010-003-00. This evaluation was originally performed as a corrective action for CR 00023410-02-01 and is being added to E-1F9915 per CR 00044460-02-01 to ensure the information is maintained in a controlled document. The evaluation has been updated since the original evaluation in CR 00023410-02-01 to reflect the current configuration in OFN RP-017.

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
ABHS0079 and ABHS0080	<p>The main steam isolation valves (MSIVs) are closed in OFN RP-017 to prevent rapid cooldown and return to criticality. Operators, upon exiting the control room, actuate All Close hand switches ABHS0079 and ABHS0080 to close the MSIVs. The Wolf Creek fire protection licensing basis does not allow us to credit that this actually works. Therefore, later steps have operators remove power from the MSIV solenoids to fail them closed. The circuit is shown on drawings E-13AB26, E-13AB27, E-13AB28 and E-13AB29.</p> <p>Power is removed from the A Train solenoids by placing NK5119 in the OFF position. This isolates separation group 1 power from MSFIS cabinet SA075A and fails the MSIVs closed. This also fails the main feedwater isolation valves closed, which is the desired PFSSD position.</p> <p>Power is also removed from the A Train solenoids by removing the Amphenol connectors at the associated terminal box. Loss of power to either train of solenoids will fail the MSIVs closed. A Train was chosen for convenience. Based on review of the drawings, a fire in the control room will not cause the MSIVs to re-open after the Amphenol connectors are dis-connected.</p> <p>Based on the above discussion, the MSIVs are protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
ABHV0005	<p>Valve ABHV0005 controls steam to the turbine driven auxiliary feedwater pump (TDAFP) from Steam Generator B and opens upon loss of 125 VDC power to the solenoid valve. Redundant control power originates from NK4201 through relay panel RP334 (Dwg E-13RP14) which does not run in the control room. Placing ABHIS0005B in the open position drops power to the solenoid and opens the valve. Upon arrival at the ASP, Operators place hand switch RPHIS0001 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP3 (Dwgs E-13RP11 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. Hand switch ABHIS0005B is placed in the open position at the ASP to open the valve and allow a steam supply to the TDAFP. The control circuit is isolated from the control room when RPHIS0001 is placed in the isolate position. Drawing E-13AB01A shows the control circuit. Based on a review of this drawing, the lockout relay contacts will isolate all portions of the circuit that run to the control room. A fire in the control room will not adversely impact valve ABHV0005 after the isolation switch is operated.</p> <p>Based on the above discussion, hand switch RPHIS0001 will isolate the control room and insert redundant fuses into the circuit so that hand switch ABHIS0005B will function. Therefore, ABHV0005 is protected.</p>
ABHV0006	<p>Valve ABHV0006 controls steam to the turbine driven auxiliary feedwater pump (TDAFP) from Steam Generator C and opens upon loss of 125 VDC power to the solenoid valve. Hand switch ABHIS0006B is placed in the closed position at the ASP to close the valve and prevent steaming steam generator C, which is not being provided with feedwater flow in procedure OFN RP-017. Upon arrival at the ASP, Operators place hand switch RPHIS0001 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP2 (Dwgs E-13RP11 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. Drawing E-13AB01 shows the control circuit. The valve opens upon loss of 125 VDC power to the solenoid valve and closes when the solenoid valve is energized. Redundant control power originates from NK4201 through relay panel RP334 (Dwg E-13RP14), which does not run in the control room. Placing RPHIS0001 in the ISOLATE position maintains power to the ABHV0006 control circuit and allows operators to maintain the valve in the closed position from the ASP. A fire in the control room will not affect operation of the valve after RPHIS0001 is placed in the isolate position. In the unlikely event valve ABHV0006 opens, PFSSD is assured because steam flow to the TDAFP remains available.</p> <p>Based on the above discussion, hand switch RPHIS0001 will isolate the control room and insert redundant fuses into the circuit so that hand switch ABHIS0006B will function. Therefore, valve ABHV0006 is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
ABHV0012, ABHV0015, ABHV0018 and ABHV0021	<p>MSIV Bypass valves ABHV0012, ABHV0015, ABHV0018 and ABHV0021 are failed closed in OFN RP-017 by removing 125 VDC control power from the control circuit. Control power is removed by pulling fuse #46 in panel RP209. This de-energizes auxiliary relay 94XAB05 and subsequently de-energizes solenoid valves associated with the MSIV bypass valves and causes them to close. The valve circuit is shown on drawing E-13AB23A. Panel RP209 wiring for fuse block 46 is shown on drawing E-093-00048. Based on drawing E-093-00048 fuse block 46 does supply power to auxiliary relay 94XAB05. Therefore, removal of fuse block 46 will cause the MSIV bypass valves to close. The MSIV bypass valves are not considered high/low pressure interfaces so consideration of multiple proper polarity hot shorts is not required. The negative side of the circuit shown on drawing E-13AB23A does not run in the control room. Therefore, after the fuse is pulled there is no possibility that the bypass valves can spuriously open as a result of a fire in the control room.</p> <p>Based on the above discussion, the MSIV bypass valves are adequately protected in the event of a control room fire.</p>
ABPV0001 and ABPV0003	<p>Steam generator ARVs ABPV0001 and ABPV0003 are closed in OFN RP-017 by isolating air and nitrogen to the valves and venting air from the regulators. The ARVs are not isolated from the control room. The Train A ASP has hand switches (ABHS0001 and ABHS0003) that transfer control of ABPV0001 and ABPV0003 to the ASP but the circuits run in the control room. Drawings J-110-00216 and J-110-00220 show the loop diagram for these circuits.</p> <p>For PFSSD, only two steam generators are needed to maintain hot standby. The control room fire strategy uses steam generator B and D ARVs (ABPV0002 and ABPV0004) for temperature control and closes steam generators A and C ARVs (ABPV0001 and ABPV0003) to prevent uncontrolled cooldown.</p> <p>Loss of air and nitrogen to the ARVs will fail the valves closed. A fire in the control room will not cause the valves to open in the absence of air and nitrogen. Therefore, ARVs ABPV0001 and ABPV0003 are protected.</p>
ABPV0002 and ABPV0004	<p>Steam generator ARVs ABPV0002 and ABPV0004 are controlled in OFN RP-017 at the ASP to control RCS temperature. Hand switches ABHS0002 and ABHS0004 at the ASP are placed in the LOCAL position to transfer control from the control room to the controller at the Train B ASP. The LOOP diagrams for ABPV0002 are shown on drawings J-110-00218, J-110-00219 and J-110-00933. The LOOP diagrams for ABPV0004 are shown on drawings J-110-00222, J-110-00223 and J-110-00934.</p> <p>Based on a review of these drawings and discussion with the Instrumentation and Control group, ABHS0002 and ABHS0004 will transfer control to the ASP and the control room circuit is isolated after these switches are placed in local position. Therefore, ABPV0002 and ABPV0004 are protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
AELI0502A	<p>This level indicator is used to verify steam generator B level. Drawings E-13AE08 and M-761-02303 show the circuit arrangement. Level transmitter AELT0502 sends a signal to SB148A in the Train B ESF switchgear room. From SB148A the signal is split and sent to the main control room indicator AELI0502 and ASP indicator AELI0502A. A fire in the control room that affects AELI0502 and associated cable will not affect AELI0502A because the signal converter will isolate any effects from a short occurring in the control room. Therefore, AELI0502A is protected.</p>
AELI0504A	<p>This level indicator is used to verify steam generator D level. Drawings E-13AE08 and M-761-02310 show the circuit arrangement. Level transmitter AELT0504 sends a signal to SB148B in the Train B ESF switchgear room. From SB148B the signal is split and sent to the main control room indicator AELI0504 and ASP indicator AELI0504A. A fire in the control room that affects AELI0504 and associated cable will not affect AELI0504A because the signal converter will isolate any effects from a short occurring in the control room. Therefore, AELI0504A is protected.</p>
ALHV0005	<p>Valve ALHV0005 is controlled at the ASP by placing hand switch ALHS0005 in the local position and controlling the valve using ALHK0005B. The AL HV-5 circuit is shown on drawings J-110-00349, J-110-00871 and J-110-00939. Technical data sheets for the Foxboro 200 system are provided in vendor manual J-110-00388. These drawings and data sheets were reviewed to determine the circuit configuration and operation of the local hand switch and local valve controller.</p> <p>When the local hand switch (ALHS0005) is placed in the LOCAL position, relay coils on a relay logic card are energized and the contacts change state. The change of state selects the output from the controller at the ASP and de-selects the control room controller. A fire in the control room could affect the control room controller but any spurious signal would not affect the valve controller. This is because spurious signals or hot shorts originating in the control room are isolated in RP147B by either contact output isolators or isolated current to voltage converters. Based on vendor manual J-110-00388, these devices will prevent spurious signals or hot shorts originating in the control room from affecting the ability to control ALHV0005 from the ASP.</p> <p>The physical makeup of the relay contacts allows only one possible state for each set of contacts. Therefore, the contact pair cannot be both open or both closed. One contact will be open and the other will be closed. Since the test procedure provides positive confirmation that the controller at the ASP does work, this provides reasonable assurance that the controller in the control room is completely isolated from the circuit when the local hand switch is placed in the LOCAL position. Based on the above discussion, there is reasonable assurance that AL HV-5 is isolated from the control room by demonstration that the controller at the ASP operates the valve. Therefore, ALHV0005 is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
ALHV0010	<p>Valve ALHV0010 is controlled at the ASP by placing hand switch ALHS0010 in the local position and controlling the valve using ALHK0010B. The AL HV-10 circuit is shown on drawings J-110-00354, J-110-00940 and J-110-00941. Technical data sheets for the Foxboro 200 system are provided in vendor manual J-110-00388. These drawings and data sheets were reviewed to determine the circuit configuration and operation of the local hand switch and local valve controller.</p> <p>When the local hand switch (ALHS0010) is placed in the LOCAL position, relay coils on a relay logic card are energized and the contacts change state. The change of state selects the output from the controller at the ASP and de-selects the control room controller. A fire in the control room could affect the control room controller but any spurious signal would not affect the valve controller. This is because spurious signals or hot shorts originating in the control room are isolated in RP147B by either contact output isolators or isolated current to voltage converters. Based on vendor manual J-110-00388, these devices will prevent spurious signals or hot shorts originating in the control room from affecting the ability to control ALHV0010 from the ASP.</p> <p>The physical makeup of the relay contacts allows only one possible state for each set of contacts. Therefore, the contact pair cannot be both open or both closed. One contact will be open and the other will be closed. Test procedure STS RP-004 provides positive confirmation that the controller at the ASP does work, so this provides reasonable assurance that the controller in the control room is completely isolated from the circuit when the local hand switch is placed in the LOCAL position.</p> <p>Based on the above discussion, there is reasonable assurance that ALHV0010 is isolated from the control room. Therefore, ALHV0010 is protected.</p>
ALHV0030	<p>Valve ALHV0030 is opened when necessary using ALHIS0030B to supply the Train B MDAFP with ESW. Upon arrival at the ASP, Operators place hand switch RPHIS0002 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP5 (Dwgs E-13RP12 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. Drawing E-13AL04B shows the control circuit for this valve. Based on a review of this drawing, the lockout relay contacts will isolate all portions of the circuit that run to the control room. A fire in the control room will not adversely impact valve ALHV0030 after the isolation switch is operated.</p> <p>Based on the above discussion, hand switch RPHIS0002 will isolate the control room and insert redundant fuses into the circuit so that hand switch ALHIS0030B will function. Therefore, valve ALHV0030 is protected.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
ALHV0033	<p>OFN RP-017 places ALHIS0033B in the close position to ensure valve ALHV0033 is closed. Step A15 opens the valve when it is necessary to swap to ESW to supply the TDAFW pump. Upon arrival at the ASP, Operators place hand switch RPHIS0002 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP6 (Dwgs E-13RP12 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. The control circuit is shown on drawing E-13AL04B. Based on a review of this drawing, the lockout relay contacts will isolate all portions of the circuit that run to the control room. A fire in the control room will not adversely impact valve ALHV0033 after the isolation switch is operated.</p> <p>Based on the above discussion, hand switch RPHIS0002 will isolate the control room and insert redundant fuses into the circuit so that hand switch ALHIS0033B will function. Therefore, ALHV0033 is protected.</p>
ALHV0034	<p>OFN RP-017 places ALHIS0034B in the open position to open valve ALHV0034. The ALHV0034 circuit is isolated from the control room when RPHIS0002 is placed in the isolate position. Upon arrival at the ASP, Operators place hand switch RPHIS0002 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP5 (Dwgs E-13RP12 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. The control circuit is shown on drawing E-13AL02B. Based on a review of this drawing, the lockout relay contacts will isolate all portions of the circuit that run to the control room. A fire in the control room will not adversely impact valve ALHV0034 after the isolation switch is operated. The valve may not readily open when ALHIS0034B is placed in the open position because power is not restored to the MCC until Step C13. This is acceptable because AFW is not needed until 15 minutes into the event. Step C13 is completed prior to 15 minutes.</p> <p>Based on the above discussion, hand switch RPHIS0002 will isolate the control room and insert redundant fuses into the circuit so that hand switch ALHIS0034B will function. Therefore, ALHV0034 is protected.</p>
ALHV0036	<p>Valve ALHV0036 is manually operated in OFN RP-017 because this valve is powered from Train A MCC cubicle NG03CEF4. Power is disconnected from the valve by opening Train A MCC cubicle breaker NG03CEF4. Train A components are not protected against faults occurring as a result of a control room fire. The control circuit for valve ALHV0036 is shown on drawing E-13AL02C. Change package 12170 modified the control circuit to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures a control room fire will not damage the valve and prevent it from being opened manually. Therefore, ALHV0036 is protected.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
APLI0004B	Condensate Storage Tank (CST) Level Indicator APLI0004B is used by operators in OFN RP-017 to verify level in the CST. When level drops to 14%, the procedure directs operators to swap to the ESW source. OFN RP-017 also directs operators to use the local indicator. Level indicator APLI0004B circuit is shown on drawing J-110-00098. Based on a review of this drawing, the level indicator is not isolated from the effects of a control room fire and could provide erroneous readings. The Note above the Step in OFN RP-017 where APLI0004B is used states that level indicator APLI0004B could be affected by the fire. Therefore, Operators will be aware that they should not rely on this level indicator. Isolation of this level indicator is not required because level in the CST is not a concern initially since sufficient volume exists to supply the steam generators for at least 4 hours. At that time, sufficient personnel will be available to locally monitor CST level. Therefore, the configuration is acceptable.
BBLI0460B	This level indicator is used to verify pressurizer level. Drawings E-13BB16 and M-761-02304 show the circuit arrangement. Level transmitter BBLT0460 sends a signal to SB148A in the Train B ESF switchgear room. From SB148A the signal is split and sent to the main control room indicator BBLI0460A and ASP indicator BBLI0460B. A fire in the control room that affects BBLI0460A and associated cable will not affect BBLI0460B because the signal converter will isolate any effects from a short occurring in the control room. Therefore, BBLI0460B is protected.
BBPI0406X	This pressure indicator is used to verify RCS pressure is being maintained between 2000 and 2300 psig. The circuit arrangement is shown on drawings E-13BB16 and M-761-02311. Pressure transmitter BBPT0406 sends a signal to SB148B in the Train B ESF switchgear room. From SB148B the signal is split and sent to the main control room indicator BBPI0406 and ASP indicator BBPI0406X. A fire in the control room that affects BBPI0406 and associated cable will not affect BBPI0406X because the signal converter will isolate any effects from a short occurring in the control room. Therefore, BBPI0406X is protected.
BBTI0423X	This temperature indicator is used to verify RCS Loop 2 cold leg temperature. Drawings E-13BB15 and M-761-02301 show the circuit arrangement. Loop 2 cold leg temperature element BBTE0423B sends a signal to Cabinet 2A which is SB148A located in the Train B ESF switchgear room (Fire Area C-10). From SB148A the signal is split and sent to the main control room indicator BBTI0423B and ASP indicator BBTI0423X. A fire in the control room that affects BBTI0423B and associated cable will not affect BBTI0423X because the signal converter will isolate any effects from a short occurring in the control room. Therefore, BBTI0423X is protected.
BG8402B	Valve BG8402B is a manual valve. A control room fire will not affect operation of the valve. Therefore, BG8402B is protected.

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
BGHV8111	<p>Valve BGHV8111 is opened in OFN RP-017 to ensure adequate minimum flow through the Train B charging pump. This prevents heatup and damage to the pump. Hand switch BGHS8111A, located at MCC cubicle NG02AHR1, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13BG11C. The circuit was modified in DCP 12175 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02AHR1. A previous step restores power to the MCC so that when the switch is actuated, the valve will open.</p> <p>Based on the above discussion, valve BGHV8111 is protected.</p>
BGLCV0112C	<p>Valve BGLCV0112C is closed in OFN RP-017 to isolate the VCT from the charging header. Hand switch BGHS0112C is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and close the valve. The circuit is shown on drawing E-13BG12A. The circuit was modified in DCP 12131 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will close when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and close the valve. Power to the valve is from MCC cubicle NG02AFR2. A previous step restores power to the MCC so that when the switch is actuated, the valve will close.</p> <p>Based on the above discussion, valve BGLCV0112C is protected.</p>
BGV0017	Valve BGV0017 is a manual valve. A control room fire will not affect operation of the valve. Therefore, BGV0017 is protected.
BGV0101	Valve BGV0101 is a manual valve. A control room fire will not affect operation of the valve. Therefore, BGV0101 is protected.
BGV0105	Valve BGV0105 is a manual valve. A control room fire will not affect operation of the valve. Therefore, BGV0105 is protected.
BNHV8812A	<p>Valve BNHV8812A is manually closed in OFN RP-017 to prevent draindown of the RWST to the containment sump. This valve is powered from Train A MCC cubicle NG01ACR2. The operator removes power from the valve by opening NG01ACR2 before manually closing the valve. The control circuit is shown on drawing E-13BN03. The circuit is not isolated from the control room. Removal of power will prevent spurious operation of the valve in the event of a control room fire. DCP 12173 modified the control circuit to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve can be manually closed when needed. Therefore, valve BNHV8812A is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
BNHV8812B	<p>Valve BNHV8812B is closed in OFN RP-017 to prevent flow diversion from the RWST to the containment sump. Hand switch BNHS8812B is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and close the valve. The circuit is shown on drawing E-13BN03A. The circuit was modified in DCP 12173 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will close when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and close the valve. Power to the valve is from MCC cubicle NG02AFF4. A previous step restores power to the MCC so that when the switch is actuated, the valve will close.</p> <p>Based on the above discussion, valve BNHV8812B is protected.</p>
BNLCV0112E	<p>Valve BNLCV0112E is opened in OFN RP-017 to establish a suction source from the RWST to the Train B CCP. Hand switch BNHS0112E, located at MCC cubicle NG02AHR3, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13BN01A. The circuit was modified in DCP 12175 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02AHR3. A previous step restores power to the MCC so that when the switch is actuated, the valve will open.</p> <p>Based on the above discussion, valve BNLCV0112E is protected.</p>
EFHV0026	<p>Valve EFHV0026 is closed in OFN RP-017 to prevent flow diversion from ESW to the service water piping. Hand switch EFHS0026A is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and close the valve. The circuit is shown on drawing E-13EF02A. The circuit was modified in DCP 12170 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will close when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and close the valve. Power to the valve is from MCC cubicle NG02AHF2. A previous step restores power to the MCC so that when the switch is actuated, the valve will close.</p> <p>Based on the above discussion, valve EFHV0026 is protected.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EFHV0032	<p>Valve EFHV0032 is opened in OFN RP-017 to establish Train B ESW flow to the Train B containment coolers. Hand switch EFHS0032, located at MCC cubicle NG02BDR1, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF07A. The circuit was modified in DCP 12131 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02BDR1. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EFHV0032 is protected.</p>
EFHV0034	<p>Valve EFHV0034 is opened in OFN RP-017 to establish Train B ESW flow to the Train B containment coolers. Hand switch EFHS0034, located at MCC cubicle NG02BHF3, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF09A. The circuit was modified in DCP 11086 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02BHF3. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EFHV0034 is protected.</p>
EFHV0038	<p>Valve EFHV0038 is opened in OFN RP-017 to establish Train B ESW flow to the UHS. Hand switch EFHS0038A, located at MCC cubicle NG02AHF3, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF06A. The circuit was modified in DCP 12170 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02AHF3. A previous step restores power to the MCC so that when the switch is actuated, the valve will open.</p> <p>Based on the above discussion, valve EFHV0038 is protected.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EFHV0046	<p>Valve EFHV0046 is opened in OFN RP-017 to establish Train B ESW flow to the Train B containment coolers. Hand switch EFHS0046, located at MCC cubicle NG02BHR2, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF09A. The circuit was modified in DCP 11086 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02BHR2. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EFHV0046 is protected.</p>
EFHV0050	<p>Valve EFHV0050 is opened in OFN RP-017 to establish Train B ESW flow to the Train B containment coolers. Hand switch EFHS0050, located at MCC cubicle NG02BDR2, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF08A. The circuit was modified in DCP 12131 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG02BDR2. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EFHV0050 is protected.</p>
EFHV0052	<p>Valve EFHV0052 is opened in OFN RP-017 to establish Train B ESW flow to the Train B CCW heat exchanger. Hand switch EFHS0052, located at MCC cubicle NG04CNF3, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EF05A. The circuit was modified in DCP 12172 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG04CNF3. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EFHV0052 is protected.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EFHV0060 / NG04CHF2	<p>Valve EFHV0060 is de-energized and closed in OFN RP-017 to prevent a flow imbalance in the essential service water (ESW) system. The valve is normally closed with manual bypass valve EFV0090 throttled to maintain proper flow for normal and emergency conditions. Condition report 00041746 identified that valve EFHV0060 is not operated in procedure OFN RP-017 and that if the valve spuriously opens as a result of the fire, a flow imbalance would occur and ESW flow to credited components may not be adequate. Therefore, a compensatory measure was added to OFN RP-017 to open breaker NG04CHF2 and close EFHV0060. Valve EFHV0060 has not been modified to address NRC IN 92-18. Change package 13898 is being prepared to modify the valve.</p> <p>A fire in the control room could cause valve EFHV0060 to open and be damaged in the open position. The condition is being addressed by change package 13898.</p>
EGHV0015	<p>Valve EGHV0015 is manually closed in OFN RP-017 to prevent flow diversion from Train B CCW to Train A CCW. Breaker NG03CHF3 is opened in an earlier step to remove power from the circuit. The circuit is shown on drawing E-13EG05C. The circuit was modified in DCP 12170 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve can be manually closed when necessary.</p> <p>A fire in the control room could damage the control circuit for the valve but the damage will not cause the valve to spuriously operate after the breaker is opened. Therefore, valve EGHV0015 is protected.</p>
EGHV0016	<p>Valve EGHV0016 is opened in OFN RP-017 to establish Train B CCW flow from the service loop. Hand switch EGHS0016A, located at MCC cubicle NG04CJF3, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EG05A. The circuit was modified in DCP 12172 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG04CJF3. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EGHV0016 is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EGHV0054	<p>Valve EGHV0054 is opened in OFN RP-017 to establish Train B CCW flow to the service loop. Hand switch EGHS0054, located at MCC cubicle NG04CKF1, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EG05D. The circuit was modified in DCP 12172 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG04CKF1. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored.</p> <p>Based on the above discussion, valve EGHV0054 is protected.</p>
EGHV0061	<p>Valve EGHV0061 is manually closed in OFN RP-017 because this valve is powered from Train A MCC cubicle NG03CKF3. Train A components are not protected against faults occurring as a result of a control room fire. An operator removes 480 VAC power from the valve by opening NG03CKF3 before another operator manually closes the valve in another step. The control circuit is shown on drawing E-13EG09A. The circuit is not isolated from the control room, nor is it required to be isolated. Removal of power will prevent spurious operation of the valve in the event of a control room fire. A 120 VAC hot short on the control room portion of the circuit will not cause the valve to spuriously operate because 480 VAC power has been removed from the valves power circuit. DCP 12130 modified the control circuit to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures this does not occur so the valve can be manually operated when needed. Therefore, valve EGHV0061 is protected.</p>
EGHV0133	<p>Valve EGHV0133 is manually closed in OFN RP-017. This valve is powered from Train B MCC cubicle NG02BHF1. An operator removes 480 VAC power from the valve by opening NG02BHF1 before another operator manually closes the valve in another step. The control circuit is shown on drawing E-13EG18A. The circuit is not isolated from the control room, nor is it required to be isolated. Removal of power will prevent spurious operation of the valve in the event of a control room fire. A 120 VAC hot short on the control room portion of the circuit will not cause the valve to spuriously operate because 480 VAC power has been removed from the valves' power circuit. DCP 12130 modified the control circuit to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures this does not occur so the valve can be manually operated when needed. Therefore, valve EGHV0133 is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EMHV8801A / NG01BER2	Valve EMHV8801A is closed in OFN RP-017 to prevent overfill of the pressurizer. This valve is powered from Train A MCC cubicle NG01BER2. An operator removes 480 VAC power from the valve by opening NG01BER2 before another operator manually closes the valve in another step. The control circuit is shown on drawing E-13EM02. The circuit is not isolated from the control room, nor is it required to be isolated. Removal of power will prevent spurious operation of the valve in the event of a control room fire. A 120 VAC hot short on the control room portion of the circuit will not cause the valve to spuriously operate because 480 VAC power has been removed from the valves' power circuit. Change package 13898 will be modifying the valve control circuit to address NRC IN 92-18 to ensure the valve can be manually closed. The pressurizer overfill concern was identified in CR 00045442.
EMHV8801B / NG04CKF3	Valve EMHV8801B is throttled in OFN RP-017 to control charging injection flow. This valve is powered from Train B MCC cubicle NG04CKF3. An operator removes 480 VAC power from the valve by opening NG04CKF3 before another operator manually throttles the valve in another step. The control circuit is shown on drawing E-13EM02A. The circuit is not isolated from the control room, nor is it required to be isolated. Removal of power will prevent spurious operation of the valve in the event of a control room fire. A 120 VAC hot short on the control room portion of the circuit will not cause the valve to spuriously operate because 480 VAC power has been removed from the valves' power circuit. DCP 12130 modified the control circuit to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve can be manually throttled when needed. Therefore, valve EMHV8801B is protected.
EMHV8803B	Valve EMHV8803B is opened in OFN RP-017 to establish Train B CCP flow to the boron injection tank (BIT). Hand switch EMHS8803B, located at MCC cubicle NG04CKF2, is used to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and open the valve. The circuit is shown on drawing E-13EM02B. The circuit was modified in DCP 12175 to address NRC IN 92-18 concerns. The concern in NRC IN 92-18 was that a hot short on the motor operator valve circuit could bypass the valves torque and limit devices and drive the valve to damage in the undesired position. The modification ensures the valve will open when the hand switch is actuated. Based on a review of the drawing, the hand switch will isolate all portions of the control room and open the valve. Power to the valve is from MCC cubicle NG04CKF2. If the hand switch is actuated before power is restored to the MCC, there will be no adverse impact. The valve will move to the open position when power is restored. Based on the above discussion, valve EMHV8803B is protected.

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
EMHV8843	<p>Valve EMHV8843 is closed in OFN RP-017 to prevent flow diversion from charging through the SIS test line which discharges to the RWST or the RHUT. Hand switch EMHS8843 is used to close the valve but does not completely isolate the control room. The circuit is shown on drawing E-13EM04A.</p> <p>The valve is a solenoid operated valve that requires 125 VDC to open. Actuation of hand switch EMHS8843 to the ISO/CLOSE position will open contacts on the positive side of the circuit and de-energize the solenoid. The negative side of the circuit is not isolated. Based on a review of the drawing, a positive hot short in the control room affecting this circuit will not cause the valve to open because the isolation contacts on the hand switch will be open, preventing the re-energization of the solenoid.</p> <p>Based on the above discussion, valve EMHV8843 is protected.</p>
EMHV8882	<p>Valve EMHV8882 is closed in OFN RP-017 to prevent flow diversion from charging through the SIS test line which discharges to the RWST or the RHUT. Hand switch EMHS8882 is used to close the valve but does not completely isolate the control room. The circuit is shown on drawing E-13EM05A.</p> <p>The valve is a solenoid operated valve that requires 125 VDC to open. Actuation of hand switch EMHS8882 to the ISO/CLOSE position will open a contact on the positive side of the circuit and de-energize the solenoid. The negative side of the circuit is not isolated. Based on a review of the drawing, a positive hot short in the control room affecting this circuit will not cause the valve to open because the isolation contacts on the hand switch will be open, preventing the re-energization of the solenoid.</p> <p>Based on the above discussion, valve EMHV8882 is protected.</p>
FCHV0312	<p>Valve FCHV0312 is opened using FCHIS0312B at the ASP. This allows steam to flow to the turbine driven auxiliary feedwater pump. Upon arrival at the ASP, Operators place hand switch RPHIS0001 in the ISOLATE position per OFN RP-017. This energizes lockout relay 86XRP1 (Dwgs E-13RP11 and E-13RP15), isolates the control room portions of the circuit and inserts redundant fuses to ensure the remaining portions of the circuit are energized. The control circuit for FCHV0312 is shown on drawing E-13FC23. Based on a review of this drawing, the lockout relay contacts will isolate all portions of the circuit that run to the control room. A fire in the control room will not adversely impact valve FCHV0312 after the isolation switch is operated.</p> <p>Based on the above discussion, hand switch RPHIS0001 will isolate the control room and insert redundant fuses into the circuit so that hand switch FCHIS0312B will function. Therefore, valve FCHV0312 is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
FCHV0313	<p>Hand switch FCHS0313 is placed in LOCAL position at the ASP to transfer control of FCHV0313 to the ASP and controlling the valve using FCHIK0313B. Drawings J-110-00642, J-110-00647 and J-110-00942 show the loop diagram for valve FCFV0313. Technical data sheets for the Foxboro 200 system are provided in vendor manual J-110-00388. These drawings and data sheets were reviewed to determine the circuit configuration and operation of the local hand switch and local valve controller.</p> <p>When the local hand switch (FCHS0313) is placed in the LOCAL position, relay coils on a relay logic card are energized and the contacts change state. The change of state selects the output from the controller at the ASP and de-selects the control room controller. A fire in the control room could affect the control room controller but any spurious signal would not affect the valve controller. This is because spurious signals or hot shorts originating in the control room are isolated in RP147B by either isolated voltage to current converters, contact output isolators or isolated current to voltage converters. Based on vendor manual J-110-00388, these devices will prevent spurious signals or hot shorts originating in the control room from affecting the ability to control FCHV0313 from the ASP.</p> <p>Based on the above discussion, there is reasonable assurance that the control room is isolated when FCHS0313 is placed in LOCAL position. Therefore, valve FCHV0313 is protected.</p>
GDHS0011	<p>Hand switch GDHS0011 isolates the Train B ESW pump room supply fan from the control room, inserts a redundant fuse on the secondary side of the control power transformer, and starts the fan. The circuit is shown on drawing E-K3GD01A. Based on a review of the schematic, the hand switch will isolate all portions of the control room and start the fan. Therefore, the fan will operate during the event.</p> <p>Exhaust damper GDTZ0011C opens when supply fan CGD01B starts. The exhaust damper circuit is shown on drawing E-K3GD03. When hand switch GDHS0011 is placed in the ISO/RUN position, auxiliary relay 3XGD2 is energized, which closes a contact and energizes the contactor relay 42 and starts the fan. Relay 42, when energized, opens a contact in the exhaust damper circuit, which de-energizes the exhaust damper and fails it in the full open position. None of the circuits associated with the exhaust damper are run in the control room. Therefore, the control room fire will not affect the exhaust damper.</p> <p>Hand switch GDHS0011A isolates the Train B ESW pump room outside air supply damper (GDTZ0011A) from the control room and opens the damper. The circuit is shown on drawings E-K3GD04A and J-110-00569.</p> <p>Based on drawing J-110-00569, the outside air supply damper closes on increasing current from a 4 – 20 mA Foxboro control circuit. Loss of signal current would fail the damper open. When hand switch GDHS0011A is placed in the ISO/OPEN position, the signal current is isolated and the damper fully opens due to the decrease in current to 0 mA. The hand switch is located in room 3302 (Train B ESF switchgear room). Therefore, a fire in the control room cannot bypass the switch and cause the damper to close.</p>

Table A1	
OFN RP-017 Credited Component Evaluation	
Component	Evaluation
	<p>The recirculation damper (GDTZ0011B) for the Train B ESW pump room is not included in the PFSSD design. A control room fire could cause the damper to fail in the full open, full closed or partially open position due to a smart hot short on the positive polarity of the 4 – 20 mA circuit (Dwg. J-110-00569). A restriction plate installed in the recirculation duct will limit airflow in the recirculation line to about 57% per Calculation GD-331.</p> <p>During normal operation, the outside air intake damper and recirculation damper operate as necessary to maintain the ESW pump room within design limits. In the winter months, most of the air flow is recirculated with minimal outside air makeup. In the summer months, most of the air flow is exhausted with minimal or no recirculation. For PFSSD following a control room fire regardless of time of year, the supply fan is started, the outside air intake damper and exhaust damper are fully opened and the recirculation damper is not controlled and could fail open, closed or somewhere in between. Consideration was not given for ensuring the room temperature is maintained within design limits. CR 00031408 has been written to address this issue.</p> <p>Based on the above discussion, the Train B ESW pump room supply fan, exhaust damper and outside air supply damper are protected. However, the OFN RP-017 configuration may not be acceptable for all times during the year.</p>
GKHS0103	<p>Class 1E electrical equipment A/C unit SGK05B is started in OFN RP-017 to provide cooling to the Train B Class 1E electrical equipment rooms. Hand switch GKHS0103 is placed in the ISO/RUN position to isolate the control room, insert a redundant fuse on the secondary side of the control power transformer, and start the unit. The circuit is shown on drawings E-13GK13A, M-622.1A-00002 and M-622.1A-00003.</p> <p>Based on a review of these drawings, hand switch GKHS0103 will isolate all portions of the control room and start the unit. After the switch is placed in the ISO/RUN position, a fire in the control room will not affect the unit. Therefore, SGK05B is protected.</p>
GLHS0035	<p>Train B electrical penetration room cooler SGL15B is started in OFN RP-017 to ensure adequate cooling to the equipment in the room. The circuit is shown on drawing E-13GL12A. Hand switch GLHS0035 is placed in the ISO/RUN position to isolate the control room and insert a redundant fuse in the control circuit. Then the operator depresses the start pushbutton on the MCC cubicle to start the unit. The unit is powered from MCC cubicle NG02BAF2.</p> <p>Based on a review of the drawing, hand switch GLHS0035 will isolate all portions of the control room. The pushbutton will energize the 42 relay, close the seal-in contact and start the unit. Therefore, SGL15B is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
GMHS0011B	<p>Train B diesel generator room supply fan CGM01B is started in OFN RP-017 using hand switch GMHS0011B. The hand switch isolates the control room, inserts a redundant fuse on the secondary side of the control power transformer, and starts the fan. The circuit is shown on drawing E-13GM01A. Based on a review of the drawing, the hand switch will isolate all portions of the control room and start the fan. Power to the fan is from MCC cubicle NG04DBF6. A previous step restores power to the MCC so that when the switch is actuated, the fan will start.</p> <p>Exhaust damper GMHZ0019 fails open when NK4413 is opened in an earlier step in OFN RP-017. The control circuit for GMHZ0019 is shown on drawing E-13GM04A. Hand switch GMHS0019B is no longer used in OFN RP-017 since disconnecting control power will open the damper. Therefore, exhaust damper GMHZ0019 is protected.</p> <p>Train B diesel generator room supply damper actuator GMTZ0011A is opened in OFN RP-017 to ensure a sufficient supply of outside air to the supply fan. The damper fails open on loss of power. OFN RP-017 has an operator remove power from the damper actuator by opening breaker NG04DEF111. The circuit is shown on drawing E-13GM02. After power is removed, a fire in the control room cannot cause the damper to close.</p> <p>The recirculation damper (GMTZ0011B) for the Train B diesel generator room is not included in the PFSSD design. A control room fire could cause the damper to fail in the full open, full closed or partially open position due to a smart hot short on the positive polarity of the 4 – 20 mA circuit (Dwg. J-110-00565). A restriction plate installed in the recirculation duct will limit airflow in the recirculation line to about 69% per Calculation GM-336.</p> <p>During normal operation, the outside air intake damper and recirculation damper operate as necessary to maintain the Train B EDG room within design limits. In the winter months, most of the air flow is recirculated with minimal outside air makeup. In the summer months, most of the air flow is exhausted with minimal or no recirculation. For PFSSD following a control room fire regardless of time of year, the supply fan is started, the outside air intake damper and exhaust damper are fully opened and the recirculation damper is not controlled and could fail open, closed or somewhere inbetween. Consideration was not given for ensuring the room temperature is maintained within design limits. CR 00031408 has been written to address this issue.</p> <p>Based on the above discussion, the Train B diesel generator building supply fan, supply damper and exhaust damper are protected. Therefore, there will be sufficient combustion air for the diesel engine. However, this configuration may not be adequate for maintaining room temperature at all times during the year.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
GNHS0009A	<p>Containment cooler SGN01B is started in OFN RP-017 to maintain the containment temperature within acceptable limits. Hand switch GNHS0009A is placed in ISO/RUN position to start the cooler from MCC NG02TAF1. The circuit is shown on drawing E-13GN02A. Based on a review of the drawing, the hand switch will isolate all portions of the control room, insert a redundant fuse on the secondary side of the control power transformer, and start the cooler. Therefore, a fire in the control room will not affect the cooler after the hand switch is placed in the ISO/RUN position.</p> <p>Based on the above discussion, containment cooler SGN01B is protected.</p>
GNHS0017A	<p>Containment cooler SGN01D is started in OFN RP-017 to maintain the containment temperature within acceptable limits. Hand switch GNHS0017A is placed in ISO/RUN position to start the cooler from MCC NG04TAF1. The circuit is shown on drawing E-13GN02A. Based on a review of the drawing, the hand switch will isolate all portions of the control room, insert a redundant fuse on the secondary side of the control power transformer, and start the cooler. Therefore, a fire in the control room will not affect the cooler after the hand switch is placed in the ISO/RUN position.</p> <p>Based on the above discussion, containment cooler SGN01D is protected.</p>
JEHS0021C	<p>Pump PJE01B is the Train B emergency diesel generator fuel oil transfer pump. The pump is started in OFN RP-017 by first placing hand switch JEHS0021C in the ISOLATE position then placing hand switch JEHS0021B in the RUN position. The circuit is shown on drawing E-13JE01A.</p> <p>Based on a review of the drawing, hand switch JEHS0021C will isolate all portions of the control room from the circuit and insert a redundant fuse in the secondary side of the control power transformer. Hand switch JEHS0021B will start the pump and maintain it running until the hand switch is placed in the STOP position.</p> <p>Based on the above discussion, pump PJE01B is protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
KJHS0101D	<p>Procedure OFN RP-017 has operators remove the break glass from switch KJHS0101D to actuate the switch. This step energizes relays ESA and ESB on the Train B diesel generator engine control circuit (Dwg E-13KJ03A). Multiple hot shorts could cause the control power fuses that provide power to both ESA and ESB relays to open, causing a loss of power to the relays. However, the Wolf Creek licensing basis for control room fires assumes only a single spurious signal occurs as a result of the fire. Therefore, it can be assumed that one of the two relays will energize.</p> <p>With at least one relay (ESA or ESB) energized, the unit parallel relay (UPR) will be de-energized (Dwg E-13NE13). Therefore, the diesel generator will not be in droop mode and will function properly as PFSSD loads are added.</p> <p>Also, with one relay (ESA or ESB) energized, relay 90 VEP will be energized which will switch the electronic voltage adjuster to a pre-determined setpoint and the voltage adjuster will ignore signals from the control room auto/manual raise/lower switches. This ensures a fire in the control room will not affect the output voltage of the EDG during the event.</p> <p>Based on the above discussion, actuation of KJHS0101D will achieve the desired outcome.</p>
KJHS0109	<p>Hand switch KJHS0109 is placed in the LOC/MAN position to isolate portions of the Train B diesel generator start/stop circuit from the control room. The switch also transfers control of the Train B diesel generator to the local panel in the diesel generator room.</p> <p>Based on drawing E-13KJ03A, KJHS0109 will isolate the control room stop portion of the circuit. This will ensure a fire in the control room will not inadvertently cause the diesel engine to shut down.</p>
KJHS0110	<p>Hand switch KJHS0110 is placed in the ISO position to isolate the Train B diesel generator control circuit from the control room and insert redundant fuses in a portion of the circuit.</p> <p>DCP 12097 added KJHS0110 and redundant fuses to ensure power is available to the field flashing circuit. However, CR 30350 identified an issue where certain fuses located in NE106 could blow, preventing field flashing. Steps were added to address this concern in the interim until a permanent modification is implemented.</p> <p>Based on a review of drawing E-13KJ03A, KJHS0110 will isolate the control room so that the speed relays will be energized when the diesel engine reaches a designated speed. However, as stated above, a portion of the field flashing circuit could be affected such that the field may not flash. This would prevent the generator from generating voltage. CR 30350 is tracking this issue.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NB0102	<p>Breaker NB0102 is opened to prevent operation of the Train A containment spray pump. The close control power fuse is first removed to ensure the breaker does not close as a result of the control room fire. The circuit is shown on drawing E-13EN01.</p> <p>The fuses that are removed are the two 15 amp fuses that protect the close circuit. The remainder of the circuit stays energized. A hot short from a fire in the control room could re-energize the positive polarity of the close circuit. However, the negative polarity will remain de-energized because the negative side of the close circuit does not run to the control room. Therefore, a fire in the control room will not cause a hot short that closes the breaker.</p> <p>Based on the above discussion, breaker NB0102 is protected.</p>
NB0201 through NB0207, NB0209 and NB0212	<p>OFN RP-017 opens breakers NB0201 through NB0207, NB0209 and NB0212 to shed most of the major loads from NB02. NB0209 and NB0212 are opened to fail off-site power to NB02 and cause an automatic start of the Train B emergency diesel generator. Some of the loads are added by OFN RP-017 after the Train B emergency diesel generator is started. Control power to the breakers is de-energized in a previous step. The breakers are opened by pushing the manual trip push button on the breakers. The breakers are closed when needed by pushing the manual close push button. The charging springs allow 1 cycle of operation without control power. The discussion for NK4401 / NB02 shows that the breakers are protected from the effects of a control room fire and will not spuriously operate after control power is removed. Therefore, the breakers are protected.</p>
NB0208, NB0210, NB0213 and NB0216	<p>These breakers are closed to energize various load centers and motor control centers. The discussion for NK4401 / NB02 shows that the breakers are protected from the effects of a control room fire and will not spuriously operate after control power is removed. Therefore, the breakers will remain closed for the duration of the event.</p>
NB0211	<p>NB0211 is closed to energize the NB02 bus from the Train B diesel generator. A previous step removes control power from the breaker, so spurious opening of the breaker caused by the control room fire will not occur. The control circuit for NB0211 is shown on drawing E-13NE11. The discussion for NK4401 / NB02 shows that the breaker is protected from the effects of a control room fire and will not spuriously operate after control power is removed. Therefore, NB0211 is protected.</p>
NB0215	<p>NB0215 is closed to energize the Train B ESW pump. A previous step removed control power from the breaker, so spurious opening of the breaker caused by the control room fire will not occur. The control circuit for NB0215 is shown on drawing E-K3EF01A. The discussion for NK4401 / NB02 shows that the breaker is protected from the effects of a control room fire and will not spuriously operate after control power is removed. Therefore, NB0215 will remain closed for the duration of the event.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NGHIS0015 / NG0201	<p>Breaker NG0201 is verified to be closed (or manually closed if not) in OFN RP-017 to ensure power is available to required loads fed from bus NG02. All PFSSD loads that are powered from NG02 are shown on drawing E-1F9424B. Not all of these loads are required after a control room fire. The control circuit for NG0201 is shown on drawing E-13NG11B. Prior to closing (or verifying closed) NG0201, hand switch NGHIS0015 is placed in the ISOLATE position to isolate the trip portion of the NG0201 control circuit from the control room. Based on a review of drawing E-13NG11B, placing NGHIS0015 in the ISOLATE position will isolate the trip circuit and prevent NG0201 from tripping. If the breaker has tripped prior to placing NGHIS0015 in the ISOLATE position, and the close control power fuse has blown as a result of the fire, the breaker can be re-closed because the close springs will be charged. Therefore, the configuration is acceptable.</p>
NGHIS0016 / NG0401	<p>Breaker NG0401 is verified to be closed (or manually closed if not) in OFN RP-017 to ensure power is available to required loads fed from bus NG04. All PFSSD loads that are powered from NG02 are shown on drawing E-1F9424D. Not all of these loads are required after a control room fire. The control circuit for NG0401 is shown on drawing E-13NG11A. Prior to closing (or verifying closed) NG0201, hand switch NGHIS0016 is placed in the ISOLATE position to isolate the trip portion of the NG0201 control circuit from the control room. Based on a review of drawing E-13NG11A, placing NGHIS0016 in the ISOLATE position will isolate the trip circuit and prevent NG0401 from tripping. If the breaker has tripped prior to placing NGHIS0016 in the ISOLATE position, and the close control power fuse has blown as a result of the fire, the breaker can be re-closed because the close springs will be charged. Therefore, the configuration is acceptable.</p>
NK4119 and NK4407	<p>The excess letdown isolation valves are failed closed in OFN RP-017 by placing 125 VDC disconnect switches NK4119 and NK4407 in the OFF position. This de-energizes power to the valves and fails them closed. The circuit is shown on drawing E-13BG48. The power distribution arrangement is shown on drawing E-13RL02. The excess letdown valves are considered high/low pressure interfaces so consideration of multiple spurious actuations is required.</p> <p>Based on a review of drawing E-13BG48, loss of power to the circuit will fail the valves closed. In order for both series valves to re-open, it would take four independent proper polarity hot shorts. Opening NK4119 and NK4407 will de-energize any potential separation group 4, 125 VDC sources in RL001/RL002. Switch PK5117 is opened in an earlier step, which removes 125 VDC from the separation group 5 source to RL001/RL002. Switch PK5211, which provides separation group 6 125 VDC power to RL001/RL002, is not opened in OFN RP-017. However, separation group 6 cables cannot come in contact with separation group 4 cables because of the physical separation requirements of IEEE 384, which are discussed in drawing E-11013 (5.8.1.B). Therefore, the excess letdown isolation valves will not spuriously open after power has been removed using NK4119 and NK4407.</p> <p>Based on the above discussion, the excess letdown isolation valves are protected.</p>

Table A1
OFN RP-017 Credited Component Evaluation

Component	Evaluation																																				
NK4401	<p>Disconnect switch NK4401 is placed in the OFF position to de-energize breaker control power for bus NB02. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, NK4401 is protected. Removing breaker control power from the NB02 bus in this manner prevents spurious operation of equipment supplied by NB02. The schematic diagram for each NB02 breaker is identified in the following table.</p> <table border="1" data-bbox="800 538 1350 1078"> <thead> <tr> <th>Breaker</th> <th>Schematic</th> </tr> </thead> <tbody> <tr><td>NB0201</td><td>E-13BG01A</td></tr> <tr><td>NB0202</td><td>E-13EM01</td></tr> <tr><td>NB0203</td><td>E-13EN01</td></tr> <tr><td>NB0204</td><td>E-13EJ01</td></tr> <tr><td>NB0205</td><td>E-13AL01B</td></tr> <tr><td>NB0206</td><td>E-13EG01C</td></tr> <tr><td>NB0207</td><td>E-13EG01D</td></tr> <tr><td>NB0208</td><td>E-13PG12A</td></tr> <tr><td>NB0209</td><td>E-13NB14</td></tr> <tr><td>NB0210</td><td>E-13NG10A</td></tr> <tr><td>NB0211</td><td>E-13NE11</td></tr> <tr><td>NB0212</td><td>E-13NB15</td></tr> <tr><td>NB0213</td><td>E-13NG10A</td></tr> <tr><td>NB0214</td><td>Spare</td></tr> <tr><td>NB0215</td><td>E-K3EF01A</td></tr> <tr><td>NB0216</td><td>E-K3NG10A</td></tr> <tr><td>NB0217</td><td>Spare</td></tr> </tbody> </table> <p>A review of each schematic diagram shows that a single hot short from an energized source conductor in the control room will not cause the control circuit on any of the equipment to become re-energized after control power has been removed. Two simultaneous hot shorts would be needed to re-energize the control circuit. Two or more proper polarity hot shorts are not assumed except for high/low pressure interface components. The equipment fed from NB02 is not considered high/low pressure interface so the potential to re-energize the control circuit is not credible. Therefore, the NB02 bus is protected.</p>	Breaker	Schematic	NB0201	E-13BG01A	NB0202	E-13EM01	NB0203	E-13EN01	NB0204	E-13EJ01	NB0205	E-13AL01B	NB0206	E-13EG01C	NB0207	E-13EG01D	NB0208	E-13PG12A	NB0209	E-13NB14	NB0210	E-13NG10A	NB0211	E-13NE11	NB0212	E-13NB15	NB0213	E-13NG10A	NB0214	Spare	NB0215	E-K3EF01A	NB0216	E-K3NG10A	NB0217	Spare
Breaker	Schematic																																				
NB0201	E-13BG01A																																				
NB0202	E-13EM01																																				
NB0203	E-13EN01																																				
NB0204	E-13EJ01																																				
NB0205	E-13AL01B																																				
NB0206	E-13EG01C																																				
NB0207	E-13EG01D																																				
NB0208	E-13PG12A																																				
NB0209	E-13NB14																																				
NB0210	E-13NG10A																																				
NB0211	E-13NE11																																				
NB0212	E-13NB15																																				
NB0213	E-13NG10A																																				
NB0214	Spare																																				
NB0215	E-K3EF01A																																				
NB0216	E-K3NG10A																																				
NB0217	Spare																																				

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NK4411	<p>The steam generator blowdown valves are failed closed in OFN RP-017 by placing 125 VDC disconnect switch NK4411 in the OFF position. The blowdown valves are not high/low pressure interfaces so consideration of multiple spurious actuations is not required. Switch NK4411 will not spuriously actuate in the event of a control room fire. Therefore, switch NK4411 is protected. The circuit for the blowdown valves is shown on drawings E-13BM06A through E-13BM06D. The power distribution is shown on drawing E-13RL07.</p> <p>When NK4411 is placed in the OFF position, the blowdown valves will fail closed. It would take multiple proper polarity hot shorts to re-energize the valves, which is not postulated in the case of non-high/low pressure interfaces. Therefore, opening NK4411 will effectively close the blowdown valves and maintain them closed for the duration of the event.</p> <p>Based on the above discussion, the steam generator blowdown valves are protected.</p>
NK4413	<p>Disconnect switch NK4413 is placed in the OFF position to remove 125 VDC control power from certain components fed from control room panel RL019 and RL020. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, NK4413 is protected. The power distribution circuit for NK4413 is shown on drawing E-13RL05. The PFSSD equipment supplied by NK4413 includes GMHZ0019, EGHV0070A, EGHV0070B and EGTV0030. Loss of 125 VDC control power to these components will fail the components in their desired position. None of these components are high/low pressure interfaces so multiple proper polarity hot shorts do not need to be considered. The control circuit for these components is shown on drawings E-13GM04A, E-13EG08 and E-13EG16. Based on a review of these drawings it would take two proper polarity hot shorts to re-energize the control circuit for these components to fail them in an undesired position after switch NK4413 is placed in the OFF position. A single hot short will not cause the control circuit to re-energize. Therefore, these components are protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NK4414 and NK5109	<p>The reactor head vent valves are failed closed in OFN RP-017 by placing 125 VDC disconnect switches NK4414 and NK5109 in the OFF position. This de-energizes power to the head vent valves and closes the valves. The circuit is shown on drawing E-13BB30. The power distribution arrangement is shown on drawing E-13RL06. The head vent valves are considered high/low pressure interfaces so consideration of multiple spurious actuations is required.</p> <p>Based on a review of drawing E-13BB30, loss of power to the circuit will fail the valves closed. In order for both series valves to re-open, it would take four independent proper polarity hot shorts. Opening NK4414 and NK5109 as well as NK5108 and NK4419 in earlier steps will de-energize any potential 125 VDC sources in RL021/RL022 and make this failure mode non-credible. Switch PK6117, which provides separation group 5 125 VDC power to RL021/RL022 and switch PK5205, which provides separation group 6 125 VDC power to RL021/RL022, is not opened in OFN RP-017. However, separation group 5 and 6 cables cannot come in contact with separation group 1 and 4 cables because of the physical separation requirements of IEEE 384, which are discussed in drawing E-11013 (5.8.1.B). Therefore, the reactor head vent valves will not spuriously open after power has been removed using NK4414 and NK5109.</p> <p>Based on the above discussion, the reactor head vent valves are protected.</p>
NK4416	<p>Disconnect switch NK4416 is placed in the OFF position to remove 125 VDC control power from SB032D. This action is taken to fail the steam dumps and cooldown valves closed. The steam dumps are not high/low pressure interfaces so multiple proper polarity hot shorts do not need to be considered. The control circuits for the steam dumps and cooldown valves are shown on schematic diagrams E-13AB08, E-13AB09, E-13AB11A, E-13AB11B, E-13AB11C, E-13AB12 and E-13AB31. Based on a review of these drawings it would take two proper polarity hot shorts to re-energize the control circuit for the steam dumps and cooldown valves to fail them in an undesired position after switch NK4416 is placed in the OFF position. A single hot short will not cause the control circuit to re-energize. Therefore, the steam dumps and cooldown valves are protected.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NK4421	<p>Disconnect switch NK4421 is placed in the OFF position to de-energize pressurizer PORV BBPCV0456A and fail it closed. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, NK4421 is protected. De-energizing the PORV circuit in this manner prevents spurious opening of the PORV. The PORV circuit is shown on drawing E-13BB40. Based on a review of this drawing, a single hot short from an energized source conductor in the control room will not cause the PORV to open. It would take multiple simultaneous negative and positive hot shorts to re-energize the PORV circuit. Two or more proper polarity hot shorts are not assumed except for high/low pressure interface components. The following paragraph discusses the combination of circuit failures necessary to cause the PORVs to open.</p> <p>Based on a review of drawing E-13BB40, in order for the PORV to open, the hot shorts would have to occur in control room panel RL021. A minimum of three 'smart' hot shorts would have to occur to open a PORV. These hot shorts include one external positive hot short, one external negative hot short and a conductor-to-conductor hot short. The external 125 VDC power source would have to be from the same separation group because IEEE-384 and E-11013 (5.8.1) do not allow cables of different separation groups to touch. Setroute was reviewed for all the separation group 4 cables with a 125 VDC potential (designated by a letter K after the system designation in the cable scheme) running to panel RL021. Based on this review the only other 125 VDC source that could energize the PORV is NK4414, which is a Separation Group 4 power supply. This switch is opened in Step C2 of OFN RP-017.</p> <p>Based on the above discussion, pressurizer PORV BBPCV0456A will not spuriously open after switches NK4421 and NK4414 are opened.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
NK5108	<p>Disconnect switch NK5108 is placed in the OFF position to de-energize pressurizer PORV BBPCV0455A and fail it closed. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, NK5108 is protected. De-energizing the PORV circuit in this manner prevents spurious opening of the PORV. The PORV circuit is shown on drawing E-13BB40. Based on a review of this drawing, a single hot short from an energized source conductor in the control room will not cause the PORV to open. It would take multiple simultaneous negative and positive hot shorts to re-energize the PORV circuit. Two or more proper polarity hot shorts are not assumed except for high/low pressure interface components. The pressurizer PORVs are not considered high/low pressure interfaces per License Amendment 193. The following paragraph discusses the combination of circuit failures necessary to cause the PORVs to open.</p> <p>Based on a review of drawing E-13BB40, in order for the PORV to open, the hot shorts would have to occur in control room panel RL021. A minimum of three 'smart' hot shorts would have to occur to open a PORV. These hot shorts include one external positive hot short, one external negative hot short and a conductor-to-conductor hot short. The external 125 VDC power source would have to be from the same separation group because IEEE-384 and E-11013 (5.8.1) do not allow cables of different separation groups to touch. Setroute was reviewed for all the separation group 1 cables with a 125 VDC potential (designated by a letter K after the system designation in the cable scheme) running to panel RL021. Based on this review the only other 125 VDC source that could energize the PORV is NK5109, which is a Separation Group 1 power supply. This switch is opened in Step C2 of OFN RP-017.</p> <p>Based on the above discussion, pressurizer PORV BBPCV0455A will not spuriously open after switches NK4421 and NK4414 are opened.</p>
NK5119	<p>Disconnect switch NK5119 supplies power to main steam and feedwater isolation cabinet SA075A. Opening this disconnect switch removes power from the Train A solenoids on the Main Steam Isolation Valves and Main Feedwater Isolation Valves. This will fail the valves in the closed position, which is the desired position for PFSSD.</p>
PA0107, PA0108, PA0204 and PA0205	<p>These breakers are manually tripped to stop the RCPs. The control circuit is not isolated from the control room, nor is it required to be isolated. Per OFN RP-017, operators first trip the breaker, remove control power, then verify that the breaker is still tripped. Control power is removed by opening disconnect switches PK4103 and PK6204. Removal of control power ensures control room fire damage will not inadvertently re-start the pump. Verification ensures the pump did not re-start prior to control power being removed. The circuit for all four RCPs is shown on drawing E-13BB01. The procedure adequately addresses tripping the RCP breakers and includes necessary steps to ensure the pumps do not re-start. Therefore, the configuration is acceptable.</p>

Table A1 OFN RP-017 Credited Component Evaluation	
Component	Evaluation
PK4103	<p>Disconnect switch PK4103 is placed in the OFF position to remove control power from PA01. For a control room fire, this is required to remove control power from breakers PA0107 and PA0108 for RCPs PBB01A and PBB01B, respectively, to ensure the RCPs do not re-start after they have been stopped. Other breakers on PA01 are not required for PFSSD following a control room fire. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, PK4103 is protected.</p> <p>The control circuit for PA0107 and PA0108 is shown on drawing E-13BB01. Based on a review of this drawing it would take two proper polarity hot shorts to re-energize the control circuit for these breakers to start the pumps after switch PK4103 is placed in the OFF position. A single hot short will not cause the control circuit to re-energize. The RCPs are not considered high low pressure interfaces so consideration of two proper polarity hot shorts is not required. Therefore, there is reasonable assurance that the RCPs will not spuriously start after they have been stopped.</p> <p>Based on the above discussion, removal of control power from PA01 in this manner will prevent spurious operation of RCPs PBB01A and PBB01B. Therefore, the configuration is acceptable.</p>
PK5117	<p>Disconnect switch PK5117 is opened in OFN RP-017 to fail normal letdown valves BGLCV0459 and BGLCV0460 closed and fail auxiliary pressurizer spray valve BGHV8145 closed. The letdown valve circuit is shown on drawing E-13BG10. The auxiliary spray circuit is shown on drawing E-13BG19. The power distribution arrangement for PK5117 is shown on drawing E-13RL02. The letdown isolation valves are considered high/low pressure interfaces so consideration of multiple spurious actuations is required. The spray valve is not considered a high/low pressure interface so multiple proper polarity hot shorts do not need to be considered.</p> <p>Letdown Valves</p> <p>Based on a review of drawing E-13BG10, loss of power to the circuit will fail the letdown valves closed. In order for both series valves to re-open, it would take four independent proper polarity hot shorts. Opening PK5117 as well as NK4119 and NK4407 in another step will de-energize these potential 125 VDC sources in RL001/RL002. The separation group 6 source of 125 VDC power remains available from switch PK5211. Based on E-11013 (5.8.3) separation groups 5 and 6 cables could be bundled together within the control room cabinets. Therefore, a source of 125 VDC power is available in RL001/RL002 to re-energize and open the valves.</p> <p>When PK5117 is opened, the two series letdown isolation valves (BGLCV0459 and BGLCV0460) fail closed and all three parallel letdown orifice isolation valves (BGHV8149A, BGHV8149B and BGHV8149C) fail closed. To re-establish a letdown flow path, three valves would need to re-open (both letdown isolation valves and one letdown orifice isolation valve). This would require six independent proper polarity hot shorts (3 negative and 3 positive) which is not credible.</p>

Table A1
OFN RP-017 Credited Component Evaluation

Component	Evaluation
	<p>Based on the above discussion, there is reasonable assurance that the letdown isolation valves will not re-open after PK5117 is placed in the OFF position.</p> <p>Auxiliary Pressurizer Spray Valve</p> <p>Based on a review of drawing E-13BG19, loss of power to the circuit will fail the spray valve closed. In order for the valve to re-open, it would two independent proper polarity hot shorts which is not postulated for non-high/low pressure interfaces.</p> <p>Based on the above discussion, there is reasonable assurance that the auxiliary pressurizer spray valve will not re-open after PK5117 is placed in the OFF position.</p>
PK6204	<p>Disconnect switch PK6204 is placed in the OFF position to remove control power from PA02. For a control room fire, this is required to remove control power from breakers PA0204 and PA0205 for RCPs PBB01D and PBB01C, respectively, to ensure the RCPs do not re-start after they have been stopped. Other breakers on PA02 are not required for PFSSD following a control room fire. There are no control room circuits that would prevent operation or cause spurious operation of this switch. Therefore, PK6204 is protected.</p> <p>The control circuit for PA0204 and PA0205 is shown on drawing E-13BB01. Based on a review of this drawing it would take two proper polarity hot shorts to re-energize the control circuit for these breakers to start the pumps after switch PK6204 is placed in the OFF position. A single hot short will not cause the control circuit to re-energize. The RCPs are not considered high low pressure interfaces so consideration of two proper polarity hot shorts is not required. Therefore, there is reasonable assurance that the RCPs will not spuriously start after they have been stopped.</p> <p>Based on the above discussion, removal of control power from PA02 in this manner will prevent spurious operation of RCPs PBB01C and PBB01D. Therefore, the configuration is acceptable.</p>

Appendix 2

Control Room Fire Consequence Evaluation for Motor Operated Valves

Table A2 documents an evaluation of the impact on post-fire safe shutdown if a fire occurs in the control room and affects motor operated valve circuits. The evaluation was originally performed per a corrective action for CR 041746-02-02. The evaluation has been added to E-1F9915 to ensure the information is maintained in a controlled document.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BGHIS8109	RL001	M-12BG03 (E-6)	BGHV8109	Normal Charging Pmp Recirc	Valve could open or remain closed.	The NCP is not used for PFSSD. If loss of flow occurs in the charging header and this valve fails closed, the NCP could be damaged. This will have no adverse impact on PFSSD since the Train B CCP is available in the event of a control room fire.
BGHIS0112C	RL001	M-12BG03 (E-7)	BGLCV0112C	VCT Outlet Valve	Valve can fail closed or remain open.	Valve is closed in OFN RP-017 by placing BGHS0112C in the ISO/CLOSE position. If the valve fails closed before lining up the RWST, the operating charging pump will lose suction and will be damaged. If RCP seal cooling flowpath remains available, then the pumps would have 12 gpm on the suction side, which is not sufficient to protect the running pump. If the seal flowpath is affected, which is possible for a fire in this cabinet, there will be no flow in the system. Since the NCP is the normally operating pump and is not credited for PFSSD, damage to it will not adversely affect PFSSD. If the valve remains open there is a possibility of H2 intrusion into the charging pump suction as discussed for other components throughout this table. A SIS would provide a permissive for the valve to close but the valve would not close until the RWST to charging valve is open. Therefore, a SIS would not cause a loss of suction to the pump.
BGHIS0112B	RL001	M-12BG03 (F-7)	BGLCV0112B	VCT Outlet Valve	Valve could close or remain open.	See discussion for BGHIS0112C.
BGHIS8112	RL001	M-12BG01 (E-3)	BGHV8112	Seal Water Ret Cont Iso Valve	Valve could close or remain open.	See discussion for BGHIS8100.
BGHIS8100	RL001	M-12BG01 (E-2)	BGHV8100	Seal Water Ret Cont Iso Valve	Valve could close or remain open.	If the valve closes, seal leakoff flow would be directed to the reactor coolant drain tank rather than the seal water heat exchanger. There is no adverse impact on PFSSD if this occurs. RCP seal damage will not occur because OFN RP-017 stops the RCPs and isolates seal injection.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BGHIS8104	RL001	M-12BG05 (B-4)	BGHV8104	Immediate Borate to CCP Suction	Valve could open or remain closed.	The valve can fail in any position with no impact on PFSSD. If the valve fails open with the boric acid transfer pumps running, boron will be added to the RCS, causing a reduction in reactivity. If the valve fails closed, it is in the correct PFSSD position.
BGHIS8110	RL001	M-12BG03 (E-3)	BGHV8110	CCP A Recirc	Valve could close or remain open.	If the A CCP is running at the time of the fire and this valve closes with little or no flow in the system, the pump could be damaged. The NCP is normally operating, so this is not a concern under normal operating conditions. The B CCP is credited for a control room fire so damage to the A CCP due to a control room fire will not adversely impact PFSSD.
BNHIS0112D	RL001	M-12BN01 (B-5)	BNLCV0112D	RWST to CCP	Valve could open or remain closed.	If the valve opens, there is no adverse impact on PFSSD since it would provide a suction source to the charging pump header. If the valve remains closed, CCP suction would be available from the VCT unless the VCT outlet valves close. OFN RP-017 lines up the RWST up to the charging header by opening BNLCV0112E before starting the B CCP. Therefore, failure of this valve to open will not affect PFSSD in the event of a control room fire.
BNHIS0112E	RL001	M-12BN01 (F-3)	BNLCV0112E	RWST to CCP	Valve could open or remain closed.	If the valve opens, there is no adverse impact on PFSSD since it would provide a suction source to the charging pump header. If the valve remains closed, CCP suction would be available from the VCT unless the VCT outlet valves close. OFN RP-017 lines up the RWST up to the charging header before starting the B CCP. The valve is opened by placing BNHS0112E in the ISO/OPEN position.
BGHIS8111	RL001	M-12BG03 (E-4)	BGHV8111	CCP B Recirc	Valve could close, causing a loss of CCP B mini flow.	If the B CCP is running at the time of the fire and this valve closes with little or no flow in the system, the pump could be damaged. The NCP is normally operating, so this is not a concern under normal operating conditions. Procedure OFN RP-017 opens this valve by placing BGHS8111A in the ISO/OPEN position.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BGHIS8106	RL001	M-12BG03 (E-3)	BGHV8106	CCP to Regen Hx Iso	Valve could open or close	If this valve closes, it is in the desired PFSSD position. If it remains open, charging flow would continue until manual valve BG8402B is closed.
BGHIS8105	RL001	M-12BG03 (E-3)	BGHV8105	CCP to Regen Hx Iso	Valve could open or close	If this valve closes, it is in the desired PFSSD position. If it remains open, charging flow would continue until manual valve BG8402B is closed.
BGHS8110	RL001	M-12BG03 (E-3)	BGHV8110	CCP A Recirc Iso Reset	Could cause a spurious reset or prevent a reset.	Switch is used to reset a safety injection signal. Based on a review of drawing E-13BG11B, fire damage to the switch will not cause the valve to open or close. Furthermore, the valve is not credited for PFSSD following a control room fire so the position of the valve will not affect PFSSD.
BGHS8111	RL001	M-12BG03 (E-5)	BGHV8111	CCP B Recirc Iso Reset	Could cause a spurious reset or prevent a reset.	Switch is used to reset a safety injection signal. Based on a review of drawing E-13BG11C, fire damage to the switch will not cause the valve to open or close. Therefore, there is no adverse impact on PFSSD. Procedure OFN RP-017 opens this valve by placing BGHS8111A in the ISO/OPEN position. Damage to the switch and associated cables will not prevent BGHS8111A from performing this function.
BGHIS8357A	RL001	M-12BG03 (C-4)	BGHV8357A	CCP A to RCP Seals	Valve could open or remain closed.	None. Seal injection is isolated by closing BGV0101 and BGV0105 in procedure OFN RP-017. With the valve open or closed, there is no adverse impact on PFSSD.
BGHIS8357B	RL001	M-12BG03 (B-4)	BGHV8357B	CCP B to RCP Seals	Valve could open or remain closed.	None. Seal injection is isolated by closing BGV0101 and BGV0105 in procedure OFN RP-017. With the valve open or closed, there is no adverse impact on PFSSD.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BBHIS8157A	RL001	M-12BB02 (E-1)	BBHV8157A	Excess Letdown to PRT	Could allow excess letdown flow to the PRT if 2 other valves to the excess letdown heat exchanger also open.	Could potentially lose ~50 gpm to the PRT if one excess letdown heat exchanger inlet flowpath (2 valves) also open. The excess letdown heat exchanger inlet valves are also controlled from RL001, so this condition could occur but it would require multiple spurious operations. Wolf Creek is not required to consider multiple spurious operations in the event of a control room fire. Furthermore, excess letdown is isolated in OFN RP-017 by opening breakers NK4119 and NK4407 to fail the excess letdown valves closed. Based on E-1F9915, operators have 37 minutes to mitigate a failed open excess letdown flowpath assuming 100 gpm loss. OFN RP-017A opens BBHV8157A to re-establish a letdown flowpath for cold shutdown. Valve BBHV8157A has been modified to address IN 92-18 concerns and is therefore available.
BBHIS8157B	RL001	M-12BB02 (D-1)	BBHV8157B	Excess Letdown to PRT	Could allow excess letdown flow to the PRT if 2 other valves to the excess letdown heat exchanger also open.	Could potentially lose ~50 gpm to the PRT if one excess letdown heat exchanger inlet flowpath (2 valves) also opens. The excess letdown heat exchanger inlet valves are also controlled from RL001, so this condition could occur but it would require multiple spurious operations. Wolf Creek is not required to consider multiple spurious operations in the event of a control room fire. Furthermore, excess letdown is isolated in OFN RP-017 by opening breakers NK4119 and NK4407 to fail the excess letdown valves closed. Based on E-1F9915, operators have 37 minutes to mitigate a failed open excess letdown flowpath assuming 100 gpm loss. OFN RP-017A opens BBHV8157B to re-establish a letdown flowpath for cold shutdown. Valve BBHV8157B has been modified to address IN 92-18 concerns and is therefore available.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
AEHIS0016	RL005	M-12AE01 (E-5)	AEHV0016	SG Feed Pump A FW Disch Valve	Could cause the valve to close or remain open.	The main feedwater pumps are not used for PFSSD. If the valve closes, PFSSD is achieved using auxiliary feedwater. If the valve stays open, backflow through the pump is prevented by check valve AEV0023. Steam generator overfill is prevented by opening switch NK5119 to fail close the MFIVs. Therefore, damage to this switch will not adversely impact PFSSD.
AEHIS0015	RL005	M-12AE01 (C-5)	AEHV0015	SG Feed Pump B FW Disch Valve	Could cause the valve to close or remain open.	The main feedwater pumps are not used for PFSSD. If the valve closes, PFSSD is achieved using auxiliary feedwater. If the valve stays open, backflow through the pump is prevented by check valve AEV0022. Steam generator overfill is prevented by opening switch NK5119 to fail close the MFIVs. Therefore, damage to this switch will not adversely impact PFSSD.
ALHIS0036A	RL005	M-12AL01 (B-4)	ALHV0036	CST to TDAFP Suction	Valve could spuriously close.	This valve is required to be open in OFN RP-017 to provide a suction source from the CST to the TDAFP. The valve is verified open in Step B7 and opened if it is not. This is a Train A valve so it is not isolated from the control room. Rather, the power is de-energized in Step 5.c to prevent spurious operation. If the valve spuriously closes before opening the breaker, an operator can locally open the valve. The valve was modified in DCP 12170 to address IN 92-18. Therefore, damage to this switch will not adversely impact PFSSD.
ALHIS0032A	RL005	M-12AL01 (D-3)	ALHV0032	ESW A to TDAFP Suction	Valve could spuriously open or remain closed.	This valve is normally closed and is not used in OFN RP-017. Train A ESW is not used in OFN RP-017. The valve can fail in any position with no adverse impact on PFSSD.
ALHIS0035A	RL005	M-12AL01 (D-3)	ALHV0035	CST to MDAFP A	Valve could spuriously close.	Valve is normally open to provide a suction source from the CST to the Train A MDAFP. The Train A MDAFP is not used in OFN RP-017 and therefore this valve can fail closed with no adverse impact on PFSSD.

**Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves**

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
ALHIS0031A	RL005	M-12AL01 (E-3)	ALHV0031	ESW to MDAFP A	Valve could spuriously open or remain closed.	Valve is normally closed and opens on LSP signal to provide a suction source from Train A ESW to the Train A MDAFP. The Train A MDAFP is not used in OFN RP-017. This valve can fail in any position with no adverse impact on PFSSD.
ALHIS0033A	RL005	M-12AL01 (C-3)	ALHV0033	ESW to TDAFP	Valve could spuriously open or remain closed.	This valve is opened in OFN RP-017 when aligning the alternate AFW source. The valve is isolated from the control room using RP HIS-2 in Step A-1. If the valve fails open it is possible that ESW would enter the TDAFP suction, which would allow raw water to enter the steam generators. This will not adversely affect PFSSD. If the valve fails closed, it can be lined up to the TDAFP after it is isolated in Step A1. The valve was modified to address IN 92-18 in DCP 12170. In either case, there is no adverse impact on PFSSD.
ALHIS0034A	RL005	M-12AL01 (H-4)	ALHV0034	CST to MDAFP B	Valve could spuriously close.	Valve is required to be open to provide the primary source of AFW from the CST to the Train B MDAFP. The valve is isolated from the control room in Step A1 using RP HIS-2 and opened using AL HIS-34B at the ASP. The valve was modified in DCP 12170 to address IN 92-18. Therefore, spurious operation of the valve will not adversely impact PFSSD.
ALHIS0030A	RL005	M-12AL01 (G-3)	ALHV0030	ESW to MDAFP B	Valve could spuriously open or remain closed.	This valve is opened in OFN RP-017 when aligning the alternate AFW source. The valve is isolated from the control room using RP HIS-2 in Step A-1. If the valve fails open it is possible that ESW would enter the MDAFP B suction, which would allow raw water to enter the steam generators. This will not adversely affect PFSSD. If the valve fails closed, it can be lined up to the B MDAFP after it is isolated in Step A1. In either case, there is no adverse impact on PFSSD. The valve was modified in DCP 12170 to address IN 92-18.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
FCHIS0312A	RL005	M-12FC02 (G-3)	FCHV0312	TDAFP Trip and Throttle Valve	Could prevent operation of the valve.	This valve is required in OFN RP-017 to provide steam to the TDAFP. The valve is isolated from the control room in Step A1 and opened in Step A13. If the valve goes full open, steam would flow only if either valve ABHV0005 or ABHV0006 and valve FCFV0313 also open. Valve FCFV0313 is normally open with the controller in manual and set to 3850 RPM. Therefore, with the proper valve lineup there could be steam release through the TDAFP. Excessive steam flow would likely result in FCHV0312 tripping on high speed.
ALHK0007A	RL006	M-12AL01 (F-8)	ALHV0007	SG A MD Aux FW B Control Valve	Could prevent flow control from MDAFP B to SG A.	Damage to this switch could cause a loss of auxiliary feedwater flow control from the Train B MDAFP to SG A. The Train B MDAFP is used in OFN RP-017 to supply SG D only. SG A is not credited in OFN RP-017 since the dump valve is on Train A. If this valve were to open while running the Train B MDAFP, auxiliary feedwater would flow to SG A but with possibly no steam dump capability the SG would overflow. Manual valve ALV0032 is closed in OFN RP-017 to prevent overfilling SG A.
ALHK0009A	RL006	M-12AL01 (E-8)	ALHV0009	SG B MD Aux FW A Control Valve	Could prevent flow control from MDAFP A to SG B.	Damage to this switch could cause a loss of auxiliary feedwater flow control from the Train A MDAFP to SG B. The Train A MDAFP is not used in OFN RP-017. The pump is secured in OFN RP-017 to prevent overfilling SGs B and C.
ALHK0011A	RL006	M-12AL01 (C-8)	ALHV0011	SG C MD Aux FW A Control Valve	Could prevent flow control from MDAFP A to SG C.	Damage to this switch could cause a loss of auxiliary feedwater flow control from the Train A MDAFP to SG C. The Train A MDAFP is not used in OFN RP-017. The pump is secured in OFN RP-017 to prevent overfilling SGs B and C.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
ALHK0005A	RL006	M-12AL01 (H-8)	ALHV0005	SG D MD Aux FW B Control Valve	Could prevent flow control from MDAFP B to SG D.	Damage to this switch could cause a loss of auxiliary feedwater flow control from the Train B MDAFP to SG D. This valve is credited in OFN RP-017 to ensure a flow path from MDAFP B to SG D. The valve is controlled in Step A5. Prior to Step A5 the valve could either fail open, fail closed or fail somewhere in-between. There is no adverse impact on PFSSD prior to controlling the valve. The design of the valve would not allow it to be damaged per IN 92-18 so the valve was not modified to address this concern. This is because the valve is a positionable MOV using hand controller ALHK0005A. Fire damage to the controller or circuits will not bypass the limit switches at the valve. Also, the thermal overloads for the valve are not bypassed, so they would open to protect the valve. Therefore, the valve cannot be damaged in a manner described in IN 92-18.
OHS-WL025A	RL013	M-0024, Sh. 2 (H-6)	OWL0014	Low Level Iso Vlv Ctrl Sw	Could prevent operation of the valve.	The makeup water system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
OHS-WL026A	RL013	M-0024, Sh. 2 (H-5)	OWL0015	Dewater Iso Vlv Ctrl Sw	Could prevent operation of the valve.	The makeup water system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
OHS-WL028A	RL013	M-0024, Sh. 2 (H-3)	OWL0017	Dewater Disch Vlv Ctrl Sw	Could prevent operation of the valve.	The makeup water system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
OHS-WL027A	RL013	M-0024, Sh. 2 (D-6)	OWL0016	Blowdown Iso Vlv Ctrl Sw	Could prevent operation of the valve.	The makeup water system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
OHS-WL029AA, OHS-WL029AB	RL013	M-0024, Sh. 2 (F-3)	OWL0018	Blowdown Disch Vlv Ctrl Sw	Could prevent operation of the valve.	The makeup water system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BNHIS0003	RL017	M-12BN01 (C-3)	BNHV0003	RWST to Containment Spray Pump B	Could close or remain open.	If the valve remains in its normally open position with no other spurious actuations, there would be no adverse impact on PFSSD. However, if the CS B pump starts and the containment spray isolation valve opens then Train B containment spray would occur and RWST inventory will be depleted until containment spray is stopped. The flow in the containment spray system with one pump operating is approximately 3,000 gpm. Based on calculation XX-E-013, Appendix 1, a maximum of 214,260 gallons of water can be lost from the RWST to maintain sufficient volume to achieve cold shutdown. Therefore, operators have approximately 71 minutes to stop the containment spray pump. The Train B pump is stopped in OFN RP-017 prior to 71 minutes. Therefore, the pump will be stopped within the required time period to prevent unacceptable RWST draindown.
ENHIS0007	RL017	M-12EN01 (B-7)	ENHV0007	Containment Recirc Sump to Containment Spray Pump B	Could spuriously open.	This valve is not credited for PFSSD. If it spuriously opens or remains closed there is no adverse impact on PFSSD. Check valve ENV0008 will prevent the RWST from draining to the containment sump if the valve opens.
ENHIS0016	RL017	M-12EN01 (D-4)	ENHV0016	Spray Additive Tank Isolation Valve	Could open or remain closed.	This valve is not credited for PFSSD. If it spuriously opens or remains closed there is no adverse impact on PFSSD.
ENHIS0012	RL017	M-12EN01 (C-4)	ENHV0012	Containment Spray Isolation Valve	Could spuriously open.	If this valve opens with no other spurious actuations, there would be no adverse impact on PFSSD. However, if the CS B pump starts then containment spray would occur, taking suction from the RWST. 71 minutes are available to mitigate this condition before the RWST reaches a level below that required for cold shutdown. Operators stop the CS B pump in OFN RP-017 prior to 71 minutes. Therefore, the pump would be stopped within the required time period to prevent unacceptable RWST draindown.
BNHIS8806B	RL017	M-12BN01 (E-3)	BNHV8806B	RWST to SI Pumps Suction	Could close or remain open.	If this valve remains in its normally open position, then there would be no adverse impact on PFSSD. If a spurious SIS occurs, there is no adverse impact because the SI pumps will not inject if RCS pressure is above 1565 psi. The SI pumps are not credited for PFSSD so if the valve closes, there would be no adverse impact.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EMHIS8923B	RL017	M-12EM01 (D-7)	EMHV8923B	SI Pump B Suction Isolation Valve	Could close or remain open.	If this valve remains in its normally open position, then there would be no adverse impact on PFSSD. If a spurious SIS occurs, there is no adverse impact because the SI pumps will not inject if RCS pressure is above 1565 psi. If the valve spuriously closes, there is no adverse impact since the Train B SI pump is not credited for PFSSD.
EMHIS8924	RL017	M-12EM01 (G-8)	EMHV8924	CVCS to SI pump Suction	Could close or remain open.	This normally open valve, along with normally closed parallel valves EMHV8807A and EMHV8807B provide an alternate SI pump suction path from the CVCS suction header. The SI system is not used for PFSSD. This valve can fail in any position with no adverse impact on PFSSD.
EMHIS8807B	RL017	M-12EM01 (F-7)	EMHV8807B	CVCS to SI pump Suction	Could open or remain closed.	If this normally closed valve opens with the SI pumps off, there is no adverse impact on PFSSD. If the pumps start there will be no flow in the system and RWST inventory will be maintained.
BNHIS8813	RL017	M-12BN01 (C-7)	BNHV8813	SI Return to RWST	Could close or remain open.	This normally open valve provides a return flowpath from the SI pumps to the RWST. If the valve closes with SI pumps running, damage could occur to the pumps if there is no flow in the system. The SI pumps are not credited for PFSSD so there would be no adverse impact.
BNHIS8813A	RL017	M-12BN01 (C-7)	BNHV8813	Valve BNHV8813 Power Lockout	Could close or remain open.	This switch is a power lockout for valve BNHV8813 and is normally in the ISO position, which maintains the valve in the open position. There is no adverse impact on PFSSD if this switch is affected.
EJHIS8804B	RL017	M-12EJ01 (B-4)	EJHV8804B	RHR HX B to SI Pump B	Could open or remain closed.	The valve is required to remain closed for PFSSD when operating Train B RHR for cold shutdown. If the valve opens prior to reaching RHR entry conditions there would be no adverse impact on PFSSD. Valve was modified to address IN 92-18 and is closed in OFN RP-017A to support cold shutdown.
EMHIS8814B	RL017	M-12EM01 (B-5)	EMHV8814B	SI Pump B Return to RWST	Could close or remain open.	This normally open valve provides a return flowpath from the Train B SI pump to the RWST. If the valve closes with Train B SI pump running, damage could occur to the pump if there is no flow in the system. The Train B SI pump is not credited for PFSSD so there would be no adverse impact.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EMHIS8821B	RL017	M-12EM01 (D-4)	EMHV8821B	SI Pump B to RCS Cold Leg Injection	Could close or remain open.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8802B	RL017	M-12EM01 (D-4)	EMHV8802B	SI Pump B Discharge Valve	Could open or remain closed.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8802BA	RL017	M-12EM01 (D-4)	EMHV8802B	Valve EMHV8802B Power Lockout	Could open or remain closed.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8835	RL017	M-12EM01 (C-4)	EMHV8835	SI Cold Leg Injection Valve	Could close or remain open.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8835A	RL017	M-12EM01 (C-4)	EMHV8835	Valve EMHV8835 Power Lockout	Could close or remain open.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8821A	RL017	M-12EM01 (E-4)	EMHV8821A	SI Pump A to RCS Cold Leg Injection	Could close or remain open.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8802A	RL017	M-12EM01 (F-4)	EMHV8802A	SI Pump A Discharge Valve	Could open or remain closed.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8802AA	RL017	M-12EM01 (F-4)	EMHV8802A	Valve EMHV8802A Power Lockout	Could open or remain closed.	The position of this valve (open or closed) has no adverse impact on PFSSD. If the SI pumps are running, injection will not occur until the RCS pressure drops below 1565 psig.
EMHIS8923A	RL017	M-12EM01 (F-7)	EMHV8923A	SI Pump A Suction Isolation Valve	Could close or remain open.	If this valve remains in its normally open position with no other spurious actuations, then there would be no adverse impact on PFSSD. If the valve spuriously closes, there is no adverse impact since the Train A SI pump is not credited for PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EMHIS8814A	RL017	M-12EM01 (B-6)	EMHV8814A	SI Pump A Return to RWST	Could close or remain open.	This normally open valve provides a return flowpath from the Train A SI pump to the RWST. If the valve closes with Train A SI pump running, damage could occur to the pump if there is no flow in the system. The Train A SI pump is not credited for PFSSD so there would be no adverse impact.
ENHIS0006	RL017	M-12EN01 (H-4)	ENHV0006	Train A Containment Spray Isolation Valve	Could spuriously open.	If this valve opens with no other spurious actuations, there would be no adverse impact on PFSSD. However, if the A CS pump starts then containment spray would occur, taking suction from the RWST. 71 minutes are available to mitigate this condition before the RWST reaches a level below that required for cold shutdown. The CS A pump is stopped in OFN RP-017 prior to 71 minutes. Therefore, the pump will be stopped within the required 71 minutes.
BNHIS0004	RL017	M-12BN01 (B-3)	BNHV0004	RWST to Containment Spray Pump A	Could close or remain open.	If the valve remains in its normally open position with no other spurious actuations, there would be no adverse impact on PFSSD. However, if the A CS pump starts and the containment spray isolation valve opens, Train A containment spray would occur and RWST inventory will be depleted until containment spray is stopped. The flow in the containment spray system with one pump operating is approximately 3,000 gpm. Based on calculation XX-E-013, Appendix 1, a maximum of 214,260 gallons of water can be lost from the RWST to maintain sufficient volume to achieve cold shutdown. Therefore, operators have approximately 71 minutes to stop the containment spray pump. The A CS pump is stopped in OFN RP-017 prior to 71 minutes. Therefore, RWST inventory will be maintained.
ENHIS0015	RL017	M-12EN01 (D-6)	ENHV0015	Spray Additive Tank Isolation Valve	Could open or remain closed.	This valve is not credited for PFSSD. If it spuriously opens or remains closed there is no adverse impact on PFSSD.
ENHIS0001	RL017	M-12EN01 (G-7)	ENHV0001	Containment Recirc Sump to Containment Spray Pump A	Could spuriously open.	This valve is not credited for PFSSD. If it spuriously opens or remains closed there is no adverse impact on PFSSD. Check valve ENV0002 will prevent the RWST from draining to the containment sump if the valve opens.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BBHIS8702A	RL017	M-12BB01 (F-4)	BBPV8702A	RCS Hot Leg to RHR Pump A	None	This valve is normally deenergized and is maintained closed. Damage to the hand switch will have no adverse impact on PFSSD since the valve cannot move from the closed position. Prior to lining up RHR for shutdown cooling, the valve is lined up in OFN RP-017A.
EJHIS8701A	RL017	M-12EJ01 (G-8)	EJHV8701A	RCS Hot Leg to RHR Pump A	None	This valve is normally deenergized and is maintained closed. Damage to the hand switch will have no adverse impact on PFSSD since the valve cannot move from the closed position. Prior to lining up RHR for shutdown cooling, the valve is lined up in OFN RP-017A.
BNHIS8812A	RL017	M-12BN01 (B-3)	BNHV8812A	RWST to RHR Pump A Suction	Valve could close or remain open.	If the valve closes there is no adverse impact on PFSSD. If the valve remains open and valve EJHV8811A opens, then the RWST would drain to the containment sump. OFN RP-017 closes BNHV8812A to prevent draindown via this path. BNHV8812A has been modified to address IN 92-18 per DCP 12173. Calculation XX-E-013, Appendix 1 has determined there is 28 minutes to mitigate RWST draindown to the sump if one RWST to sump flowpath fails open. This condition will be mitigated before the RWST drops below minimum level needed for cold shutdown.
EJHIS8811A	RL017	M-12EJ01 (F-7)	EJHV8811A	Ctmt Recirc Sump to RHR A Suction	Valve could spuriously open.	Damage to this switch could cause the valve to open. In addition, valve BNHV8812A may not automatically close as designed, causing the RWST to drain to the sump. This condition is mitigated in OFN RP-017 by manually closing BNHV8812A within the required time period of 28 minutes. The valve was modified to address NRC IN 92-18.
EJHIS0610	RL017	M-12EJ01 (H-6)	EJFCV0610	RHR Pump A Miniflow Valve	Valve could close.	Damage to this switch has no adverse impact on PFSSD since the Train A RHR system is not credited for a control room fire. The position of this valve (open or closed) will have no adverse impact on hot standby.
EJHIS8804A	RL017	M-12EJ01 (H-4)	EJHV8804A	RHR A to CVCS Iso Valve	Valve could open or remain closed.	Valve is required to remain closed when operating Train A RHR to prevent flow diversion to the charging header. The position of this valve (open or closed) will have no adverse impact on hot standby. The Train A RHR system is not credited for a control room fire so spurious operation of this valve will have no adverse impact on PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EJHIS8716A	RL017	M-12EJ01 (E-3)	EJHV8716A	RHR Pump A Hot Leg Recirc	Valve could close or remain open.	Damage to this switch could cause the valve to close or prevent it from closing. The Train A RHR system is not credited for PFSSD following a control room fire so damage to this switch will have no adverse impact on the ability to achieve cold shutdown. The position of this valve (open or closed) will have no adverse impact on hot standby. OFN RP-017A closes EJHV8840 to prevent hot leg recirculation when lining up RHR for cold shutdown.
EJHIS8809A	RL017	M-12EJ01 (G-3)	EJHV8809A	RHR A to Cold Leg Injection Loops 1 and 2.	Valve could close or remain open.	The Train A RHR system is not credited for a fire in the control room. The position of this valve (open or closed) will have no adverse impact on safe shutdown.
EJHIS8809AA	RL017	M-12EJ01 (G-3)	EJHV8809A	Valve EJHV8809A power lockout.	Valve could close or remain open.	The Train A RHR system is not credited for a fire in the control room. The position of this valve (open or closed) will have no adverse impact on safe shutdown.
EMHIS8807A	RL017	M-12EM01 (G-7)	EMHV8807A	CVCS to SI pump Suction	Valve could open or remain closed.	If this normally closed valve opens with no other spurious actuations, there is no adverse impact on PFSSD. If the pumps start there will be no flow in the system and RWST inventory will be maintained.
EJHIS8809B	RL017	M-12EJ01 (C-3)	EJHV8809B	RHR B to Cold Leg Inj Loops 3 and 4	Valve could close or remain open.	This valve is credited for a fire in the control room when lining up Train B RHR in OFN RP-017A for cold shutdown. Spurious operation of the valve during hot standby will not impact PFSSD. The valve was modified to address IN 92-18.
EJHIS8809BA	RL017	M-12EJ01 (C-3)	EJHV8809B	RHR B to Cold Leg Inj Loops 3 and 4	Valve could close or remain open.	This valve is credited for a fire in the control room when lining up Train B RHR in OFN RP-017A for cold shutdown. Spurious operation of the valve during hot standby will not impact PFSSD. The valve was modified to address IN 92-18.
EJHIS8840	RL017	M-12EJ01 (E-3)	EJHV8840	RHR Hot Leg Recirc Valve	Valve could open or remain closed.	This valve is closed in OFN RP-017A to prevent hot leg recirculation. The position of this valve (open or closed) will have no adverse impact on hot standby.
EJHIS8840A	RL017	M-12EJ01 (E-3)	EJHV8840	RHR Hot Leg Recirc Valve	Valve could open or remain closed.	This valve is closed in OFN RP-014 to prevent hot leg recirculation. The position of this valve (open or closed) will have no adverse impact on hot standby. The valve was modified to address IN 92-18.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EJHIS8716B	RL017	M-12EJ01 (C-3)	EJHV8716B	RHR Pump B Hot Leg Recirc	Valve could close or remain open.	Damage to this switch could cause the valve to close or prevent it from closing. The position of this valve (open or closed) will have no adverse impact on hot standby. OFN RP-017A closes EJHV8840 to prevent hot leg recirculation when lining up RHR for cold shutdown.
EJHIS0611	RL017	M-12EJ01 (B-6)	EJFCV0611	RHR B Miniflow Valve	Valve could close.	If the valve closes there will be no adverse impact unless the Train B RHR pump starts in which case the pump would have no recirc flow. The pump is stopped (or prevented from starting) in OFN RP-017. Valve EJFCV0611 is lined up in OFN RP-017A when placing RHR in service. The valve was modified to address IN 92-18.
EJHIS8701B	RL017	M-12EJ01 (C-8)	EJHV8701B	RCS Hot Leg to RHR Pump B	None	This valve is normally deenergized and is maintained closed. Damage to the hand switch will have no adverse impact on PFSSD since the valve cannot move from the closed position. Prior to lining up RHR for shutdown cooling, the valve is lined up in OFN RP-017A.
BBHIS8702B	RL017	M-12BB01 (H-5)	BBPV8702B	RCS Hot Leg to RHR Pump B	None	This valve is normally deenergized and is maintained closed. Damage to the hand switch will have no adverse impact on PFSSD since the valve cannot move from the closed position. Prior to lining up RHR for shutdown cooling, the valve is lined up in OFN RP-017A.
BNHIS8812B	RL017	M-12BN01 (D-3)	BNHV8812B	RWST to RHR B Suction	Valve could close or remain open.	If the valve closes there is no adverse impact on PFSSD. If the valve remains open and valve EJHV8811B opens, then the RWST would drain to the containment sump. OFN RP-017 closes BNHV8812B using BNHS8812B. Calculation XX-E-013, Appendix 1 has determined there is 28 minutes to mitigate RWST draindown to the sump if one RWST to sump flowpath fails open. This condition will be mitigated before the RWST drops below minimum level needed for cold shutdown.
EJHIS8811B	RL017	M-12EJ01 (D-7)	EJHV8811B	Ctmt Recirc Sump to RHR B Suction	Valve could spuriously open.	Damage to this switch could cause the valve to open. In addition, valve BNHV8812B may not automatically close as designed, causing the RWST to drain to the sump. This condition is mitigated in OFN RP-017 using switch BNHS8812B.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BNHIS8806A	RL017	M-12BN01 (B-5)	BNHV8806A	RWST to SI Pumps Suction	Could close or remain open.	If this valve remains in its normally open position with no other spurious actuations, then there would be no adverse impact on PFSSD. The SI pumps are not credited for PFSSD so if the valve closes, there would also be no adverse impact.
EGHIS0101	RL017	M-12EG02 (G-4)	EGHV0101	CCW to RHR HX A	Valve could open or close	If the valve opens, there is no adverse impact. If the valve closes, CCW flow to the Train A RHR heat exchanger would be prevented. The Train A RHR system is not credited for safe shutdown following a fire in the control room. The valve can fail in any position with no adverse impact on PFSSD.
EGHIS0102	RL017	M-12EG02 (C-4)	EGHV0102	CCW to RHR HX B	Valve could open or close	If the valve opens, there is no adverse impact. If the valve closes, CCW flow to the Train B RHR heat exchanger would be prevented. The Train B RHR system is credited for safe shutdown following a fire in the control room. The system is lined up in OFN RP-017A. The valve has been modified to address NRC IN 92-18.
BNHIS8812AA	RL017	M-12BN01 (B-3)	BNHV8812A	RWST to RHR Pump A Suction	Valve could close or remain open.	See discussion for BNHIS8812A.
BNHIS8812BA	RL017	M-12BN01 (D-3)	BNHV8812B	RWST to RHR B Suction	Valve could close or remain open.	See discussion for BNHIS8812B.
EMHIS8803B	RL018	M-12EM02 (B-7)	EMHV8803B	CCP B to BIT	Valve could remain closed or open.	Valve is required to be open in OFN RP-017. The valve is manually opened in OFN RP-017 Step B12. If the valve spurious opens, it is in the desired position and PFSSD is unaffected. The valve has been modified to address NRC IN 92-18.
EMHIS8803A	RL018	M-12EM02 (C-7)	EMHV8803A	CCP A to BIT	Valve could remain closed or open.	Valve is not used in OFN RP-017. If it spurious opens or fails in the closed position there is no impact on PFSSD.
EPHIS8808B	RL018	M-12EP01 (F-5)	EPHV8808B	Accum Tank B Outlet Iso Valve	Could cause the valve to close or remain open.	The position of this valve (open or closed) has no impact on PFSSD. The valve is used to control lineup of the accumulator to the RCS. The accumulator tanks are not used for PFSSD and therefore spurious operation of the valve will not adversely impact PFSSD. During shutdown, the accumulators are prevented from injecting in OFN RP-017A by isolating the outlet valves.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EPHIS8808A	RL018	M-12EP01 (G-5)	EPHV8808A	Accum Tank A Outlet Iso Valve	Could cause the valve to close or remain open.	The position of this valve (open or closed) has no impact on PFSSD. The valve is used to control lineup of the accumulator to the RCS. The accumulator tanks are not used for PFSSD and therefore spurious operation of the valve will not adversely impact PFSSD. During shutdown, the accumulators are prevented from injecting in OFN RP-017A by isolating the outlet valves.
EPHIS8808C	RL018	M-12EP01 (D-5)	EPHV8808C	Accum Tank C Outlet Iso Valve	Could cause the valve to close or remain open.	The position of this valve (open or closed) has no impact on PFSSD. The valve is used to control lineup of the accumulator to the RCS. The accumulator tanks are not used for PFSSD and therefore spurious operation of the valve will not adversely impact PFSSD. During shutdown, the accumulators are prevented from injecting in OFN RP-017A by isolating the outlet valves.
EPHIS8808D	RL018	M-12EP01 (B-5)	EPHV8808D	Accum Tank D Outlet Iso Valve	Could cause the valve to close or remain open.	The position of this valve (open or closed) has no impact on PFSSD. The valve is used to control lineup of the accumulator to the RCS. The accumulator tanks are not used for PFSSD and therefore spurious operation of the valve will not adversely impact PFSSD. During shutdown, the accumulators are prevented from injecting in OFN RP-017A by isolating the outlet valves.
EMHIS8801B	RL018	M-12EM02 (D-4)	EMHV8801B	BIT Discharge Iso Valve	Could cause the valve to open or remain closed	This valve is required to be open in OFN RP-017 to provide a charging path to the RCS. Step B18 opens the valve locally manually. If the valve opens as a result of the fire, it is in the desired PFSSD position. The valve has been modified to address NRC IN 92-18.
EMHIS8801A	RL018	M-12EM02 (E-4)	EMHV8801A	BIT Discharge Iso Valve	Could cause the valve to open or remain closed	This valve is not used in OFN RP-017. If the valve opens as a result of the fire, then a flow path from charging to the RCS will be established as required. If the valve fails to open, valve EMHV8801B is opened in Step B18. Therefore, spurious operation of the valve will not affect PFSSD.
KCHIS0253B	RL018	M-12KC02 (B-6)	KCHV0253	Fire Protection Header Outer Cmt Iso Valve	Could prevent operation of the valve	A fire in the control room does not require operation of the containment fire suppression system. Damage to this switch has no adverse impact on PFSSD.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EGHIS0014	RL019	M-12EG01 (C-7)	EGHV0014	ESW to CCW Train B Makeup	Could cause the valve to open.	Valve is normally closed. If the valve opens, valve EGHV0012 will prevent ESW water from entering the CCW system. If both valves open, the CCW surge tank would fill solid, however this would not impact the ability of the CCW system to perform its intended function. If necessary, manual valve EGV0185 could be closed to isolate the makeup.
EGHIS0012	RL019	M-12EG01 (C-8)	EGHV0012	ESW to CCW Train B Makeup	Could cause the valve to open.	Valve is normally closed. If the valve opens, valve EGHV0014 will prevent ESW water from entering the CCW system. If both valves open, the CCW surge tank would fill solid, however this would not impact the ability of the CCW system to perform its intended function. If necessary, manual valve EGV0185 could be closed to isolate the makeup.
EGHS0016	RL019	M-12EG01 (C-7)	EGHV0016, EGHV0054	CCW Train B to/from Service Loop	Could cause the valves to close or open.	Valves are closed when operating the Train A CCW system and opened when operating the Train B CCW system. If the valves spuriously open, they are in the desired PFSSD position for OFN RP-017. If the valves are closed, OFN RP-017 opens them using switches EGHS0016A and EGHS0054. The valves were modified to address IN 92-18.
EGHIS0071	RL019	M-12EG03 (H-6)	EGHV0071	CCW to RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for OFN RP-017. This valve, or bypass valve EGHV0126, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, it will be manually open in OFN RP-017A. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017. Valve was modified to address IN 92-18.
EGHIS0058	RL019	M-12EG03 (H-6)	EGHV0058	CCW to RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for OFN RP-017. This valve, or bypass valve EGHV0127, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, it will be manually open in OFN RP-017A. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017. Valve was modified to address IN 92-18.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EGHIS0062	RL019	M-12EG03 (A-5)	EGHV0062	CCW Return from RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for OFN RP-017. This valve is not required for cold shutdown. If the valve fails closed, it is in the desired PFSSD position. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017.
EGHIS0060	RL019	M-12EG03 (A-5)	EGHV0060	CCW Return from RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for OFN RP-017. This valve, or bypass valve EGHV0130, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, it will be manually open in OFN RP-017A. If the valve fails open, there is no adverse impact if CCW continues to flow through the RCP bearing coolers, motor air coolers, excess letdown heat exchanger and RCDT heat exchanger. Valve was modified to address IN 92-18.
EGHIS0061	RL019	M-12EG03 (B-5)	EGHV0061	CCW Return from RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and is required to be closed in OFN RP-017 to prevent a postulated steam bubble from forming in the CCW piping, potentially causing a water hammer. The valve is manually closed in OFN RP-017. Valve was modified to address IN 92-18.
EGHIS0059	RL019	M-12EG03 (B-5)	EGHV0059	CCW Return from RCS Iso Valve	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for OFN RP-017. This valve, or bypass valve EGHV0131, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, it will be manually open in OFN RP-017A. If the valve fails open, there is no adverse impact if CCW continues to flow through the RCP bearing coolers, motor air coolers, excess letdown heat exchanger and RCDT heat exchanger. Valve was modified to address IN 92-18.
EFHIS0042	RL019	M-12EF02 (D-2)	EFHV0042	ESW B to Service Water	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for PFSSD. If the valve closes, ESW return to the UHS is controlled by EFHV0038 in OFN RP-017. If this valve and EFHV0040 remains open, there is no adverse impact because proper ESW flow is ensured. Therefore, spurious operation of this valve will not affect PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EFHIS0038	RL019	M-12EF02 (D-2)	EFHV0038	ESW B to UHS	Could cause the valve to close or remain open.	Valve is normally throttled and is required to be fully open in OFN RP-017. If the valve fails open, it is in the desired PFSSD position. If it fails closed, it will be opened in OFN RP-017 using the isolation handswitch at the MCC. Valve has been modified to address IN 92-18.
EFHIS0041	RL019	M-12EF02 (E-2)	EFHV0041	ESW A to Service Water	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for PFSSD. Train A ESW is not credited for PFSSD in OFN RP-017. Therefore, spurious operation of this valve will not adversely impact PFSSD.
EFHIS0060	RL019	M-12EF02 (D-3)	EFHV0060	ESW B Return from CCW Hx B	Could cause the valve to open or remain closed.	This valve is normally closed with manual valve EFV0090 throttled to provide the proper flow for SIS or LOSP. If the valve opens, flow balance in the ESW system will be affected. If the valve closes, ESW flow through the CCW heat exchanger is ensured via normally throttled manual valve EFV0090. DCP 13898 is being prepared to modify the valve to address IN 92-18.
EFHIS0046	RL019	M-12EF02 (C-6)	EFHV0046	ESW B from Ctmt Air Coolers	Could cause the valve to close or remain open.	Valve is required to be open in OFN RP-017 to ensure proper operation of the containment air coolers. The valve is opened in OFN RP-017 when lining up the containment coolers. Valve has been modified to address IN 92-18.
EFHIS0050	RL019	M-12EF02 (C-6)	EFHV0050	ESW B from Ctmt Air Coolers	Could cause the valve to close or remain open.	Valve is required to be open in OFN RP-017 to ensure proper operation of the containment air coolers. The valve is opened in OFN RP-017 when lining up the containment coolers. Valve has been modified to address IN 92-18.
EFHIS0024	RL019	M-12EF01 (E-6)	EFHV0024	ESW B from Service Water Cross Connect	Could cause the valve to close or remain open.	This flowpath is required to be isolated in OFN RP-017 to prevent flow diversion from ESW to the service water system. Valve EFHV0026, which is installed in series with this valve, is isolated in OFN RP-017. If EFHV0024 closes, then it is in the desired PFSSD position. If EFHV0024 remains open, valve EFHV0026 is closed to isolate this flowpath.
EFHIS0052	RL019	M-12EF02 (D-5)	EFHV0052	ESW B to CCW Hx B	Could cause the valve to close or remain open.	Valve is normally open and is required to be open for OFN RP-017. If the valve spuriously closes, it is opened in OFN RP-017 using EFHS0052. Valve has been modified to address IN 92-18.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EFHIS0032	RL019	M-12EF02 (C-8)	EFHV0032	ESW B to Ctrmt Air Coolers	Could cause the valve to close or remain open.	Valve is required to be open in OFN RP-017 to ensure proper operation of the containment air coolers. The valve is opened in OFN RP-017 using EFHS0032. Valve has been modified to address IN 92-18.
EFHIS0034	RL019	M-12EF02 (C-7)	EFHV0034	ESW B to Ctrmt Air Coolers	Could cause the valve to close or remain open.	Valve is required to be open in OFN RP-017 to ensure proper operation of the containment air coolers. The valve is opened in OFN RP-017 using EFHS0034. Valve has been modified to address IN 92-18.
EFHIS0023	RL019	M-12EF01 (F-6)	EFHV0023	ESW A from Service Water Cross Connect	Could cause the valve to close or remain open.	Train A ESW is not used in OFN RP-017. Spurious operation of this valve will not adversely impact PFSSD.
EFHIS0051	RL019	M-12EF02 (H-5)	EFHV0051	ESW A to CCW Hx A	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EFHIS0031	RL019	M-12EF02 (G-8)	EFHV0031	ESW A to Containment Air Coolers	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EFHIS0033	RL019	M-12EF02 (G-7)	EFHV0033	ESW A to Containment Air Coolers	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EFHIS0025	RL019	M-12EF01 (F-7)	EFHV0025	ESW A from Service Water Cross Connect	Could cause the valve to close or remain open.	Train A ESW is not used in OFN RP-017. Spurious operation of this valve will not adversely impact PFSSD.
EFHIS0040	RL019	M-12EF02 (D-2)	EFHV0040	ESW B to Service Water	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for PFSSD. If the valve closes, ESW return to the UHS is controlled by EFHV0038 in OFN RP-017. If this valve and EFHV0042 remains open, there is no adverse impact because proper ESW flow is ensured. Therefore, spurious operation of this valve will not affect PFSSD.
EFHIS0059	RL019	M-12EF02 (H-3)	EFHV0059	ESW A Return from CCW Hx B	Could cause the valve to close or remain open.	Train A ESW is not used in OFN RP-017. Spurious operation of this valve will not adversely impact PFSSD.
EFHIS0045	RL019	M-12EF02 (G-6)	EFHV0045	ESW A from Containment Air Coolers	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EFHIS0026	RL019	M-12EF01 (E-7)	EFHV0026	ESW B from Service Water Cross Connect	Could cause the valve to close or remain open.	This flowpath is required to be isolated in OFN RP-017 to prevent flow diversion from ESW to the service water system. The valve is isolated in OFN RP-017 using EFHS0026A. If it spuriously closes, it is in the desired PFSSD position. Valve has been modified to address IN 92-18.
EFHIS0049	RL019	M-12EF02 (G-6)	EFHV0049	ESW A from Containment Air Coolers	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EFHIS0037	RL019	M-12EF02 (G-3)	EFHV0037	ESW A to UHS	Could cause the valve to close or remain open.	Train A ESW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EFHIS0039	RL019	M-12EF02 (F-2)	EFHV0039	ESW A to Service Water	Could cause the valve to close or remain open.	Valve is normally open and can be in any position for PFSSD. Train A ESW is not credited for PFSSD in OFN RP-017. Therefore, spurious operation of this valve will not adversely impact PFSSD.
EGHS0015	RL019	M-12EG01 (D-6)	EGHV0015, EGHV0053	CCW Train A to/from Service Loop	Could cause the valves to close or remain open.	These valves are open when operating the Train A CCW system. Valve EGHV0015 is manually closed in OFN RP-017 to prevent flow diversion from Train B CCW to Train A CCW system. Valve EGHV0015 has been modified to address IN 92-18. Valve EGHV0053 is not used in OFN RP-017 because check valve EGV0036 will prevent flow from the train B CCW system to the train A CCW system.
EGHIS0011	RL019	M-12EG01 (F-8)	EGHV0011	ESW to CCW Pump A	Could cause the valve to open or remain closed.	Train A CCW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EGHIS0013	RL019	M-12EG01 (F-7)	EGHV0013	ESW to CCW Pump A	Could cause the valve to open or remain closed.	Train A CCW is not credited in OFN RP-017. Spurious operation will not adversely impact PFSSD.
EGHIS0131	RL020	M-12EG03 (C-5)	EGHV0131	CCW Return Cmt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally closed and can be in any position for OFN RP-017. This valve, or valve EGHV0059, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, valve EGHV0059 is manually opened in OFN RP-017A. If the valve fails open, there is no adverse impact, as CCW would continue to flow through the RCP bearing coolers, motor air coolers, excess letdown heat exchanger and RCDT heat exchanger.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EGHIS0127	RL020	M-12EG03 (G-4)	EGHV0127	CCW Supply Cmtt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally closed and can be in any position for OFN RP-017. This valve, or valve EGHV0058, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, valve EGHV0058 will be manually open in OFN RP-017A. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017.
EGHIS0131A	RL020	M-12EG03 (C-5)	EGHV0131	CCW Return Cmtt Iso Valve	Could prevent operation of the power lockout feature but will not cause the valve to open.	Valve is normally closed with this hand switch in the ISO position, preventing accidental opening of the valve. Damage to this switch alone will not cause the valve to open. PFSSD is assured if this switch is damaged.
EGHIS0133	RL020	M-12EG03 (D-5)	EGHV0133	CCW Return Cmtt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally open and is required to be closed in OFN RP-017 to prevent a postulated steam bubble from forming in the CCW piping, potentially causing a water hammer. The valve is manually closed in OFN RP-017. Valve has been modified to address IN 92-18.
EGHIS0133A	RL020	M-12EG03 (D-5)	EGHV0133	CCW Return Cmtt Iso Valve	Could prevent operation of the power lockout feature but will not cause the valve to open.	Valve is normally closed with this hand switch in the ISO position, preventing accidental opening of the valve. Damage to this switch alone will not cause the valve to open. PFSSD is assured if this switch is damaged. Valve has been modified to address IN 92-18.
GSHIS0021	RL020	M-12GS01 (G-4)	GSHV0021	Hyd Purge Outer Cmtt Iso Vlv	Valve could open or remain closed.	If the valve opens, there is no adverse impact on PFSSD. Valve GSHV0020 will remain closed or, if GSHV0020 also opens, the Aux Building ESF filters will prevent release of radioactivity. In either case, PFSSD is assured.
EGHIS0130	RL020	M-12EG03 (B-5)	EGHV0130	CCW Return Cmtt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally closed and can be in any position for OFN RP-017. This valve, or valve EGHV0060, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, valve EGHV0060 is manually opened in OFN RP-017A. If the valve fails open, there is no adverse impact as CCW continues to flow through the RCP bearing coolers, motor air coolers, excess letdown heat exchanger and RCDT heat exchanger.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EGHIS0126	RL020	M-12EG03 (G-5)	EGHV0126	CCW Supply Ctmt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally closed and can be in any position for OFN RP-017. This valve, or valve EGHV0071, needs to be open for cold shutdown when using the excess letdown heat exchanger. If the valve fails closed, valve EGHV0071 will be manually open in OFN RP-017A. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017.
EGHIS0130A	RL020	M-12EG03 (B-5)	EGHV0130	CCW Return Ctmt Iso Valve	Could prevent operation of the power lockout feature but will not cause the valve to open.	Valve is normally closed with this hand switch in the ISO position, preventing accidental opening of the valve. Damage to this switch alone will not cause the valve to open. PFSSD is assured if this switch is damaged.
EGHIS0132	RL020	M-12EG03 (B-4)	EGHV0132	CCW Return Ctmt Iso Valve	Could cause the valve to open or remain closed.	Valve is normally closed and can be in any position for OFN RP-017. This valve is not required for cold shutdown. If the valve fails closed, it is in the desired PFSSD position. If the valve fails open, the CCW system is protected from a steam bubble by closing EGHV0061 and EGHV0133 in OFN RP-017.
EGHIS0132A	RL020	M-12EG03 (B-4)	EGHV0132	CCW Return Ctmt Iso Valve	Could prevent operation of the power lockout feature but will not cause the valve to open.	Valve is normally closed with this hand switch in the ISO position, preventing accidental opening of the valve. Damage to this switch alone will not cause the valve to open. PFSSD is assured if this switch is damaged.
GSHIS0020	RL020	M-12GS01 (G-5)	GSHV0020	Hyd Purge Inner Ctmt Iso Vlv	Valve could open or remain closed.	If the valve opens, there is no adverse impact on PFSSD. Valve GSHV0021 will remain closed or, if GSHV0021 also opens, the Aux Building ESF filters will prevent release of radioactivity. In either case, PFSSD is assured.
EGHIS0072	RL020	M-12EG02 (H-2)	EGHV0072	CCW Iso to PASS	Could prevent operation of the valve.	The Post-Accident Sampling System is not used for PFSSD. If the valve opens, CCW will flow to the PASS coolers only if three other valves also open. If this occurs, there is no adverse impact on PFSSD since the CCW system is sized to supply this load concurrent with all PFSSD loads.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EGHIS0074	RL020	M-12EG02 (H-1)	EGHV0074	CCW Iso to PASS	Could prevent operation of the valve.	The Post-Accident Sampling System is not used for PFSSD. If the valve opens, CCW will flow to the PASS coolers only if three other valves also open. If this occurs, there is no adverse impact on PFSSD since the CCW system is sized to supply this load concurrent with all PFSSD loads.
EGHIS0127A	RL020	M-12EG03 (G-4)	EGHV0127	CCW Supply Ctmt Iso Valve	Could prevent operation of the power lockout feature but will not cause the valve to open.	Valve is normally closed with this hand switch in the ISO position, preventing accidental opening of the valve. Damage to this switch alone will not cause the valve to open. PFSSD is assured if this switch is damaged.
EGHIS0073	RL020	M-12EG02 (H-2)	EGHV0073	CCW Iso to PASS	Could prevent operation of the valve.	The Post-Accident Sampling System is not used for PFSSD. If the valve opens, CCW will flow to the PASS coolers only if three other valves also open. If this occurs, there is no adverse impact on PFSSD since the CCW system is sized to supply this load concurrent with all PFSSD loads.
EGHIS0075	RL020	M-12EG02 (H-1)	EGHV0075	CCW Iso to PASS	Could prevent operation of the valve.	The Post-Accident Sampling System is not used for PFSSD. If the valve opens, CCW will flow to the PASS coolers only if three other valves also open. If this occurs, there is no adverse impact on PFSSD since the CCW system is sized to supply this load concurrent with all PFSSD loads.
BBHIS8037A	RL021	M-12BB02 (D-3)	BBHV8037A	PRT Drain to Ctmt Norm Sump	Could cause the valve to spuriously open.	Spurious opening of the valve will not cause a loss of inventory in the RCS. The valve is used to drain the contents of the PRT to the sump.
BBHIS8037B	RL021	M-12BB02 (D-3)	BBHV8037B	PRT Drain to Ctmt Norm Sump	Could cause the valve to spuriously open.	Spurious opening of the valve will not cause a loss of inventory in the RCS. The valve is used to drain the contents of the PRT to the sump.
BBHS8000A	RL021	M-12BB02 (E-7)	BBHV8000A	Cold O/P Arm Sw	Could prevent closing the valve.	The pressurizer PORVs are closed in OFN RP-017 by disconnecting power to the circuit. This will fail the valves closed. Therefore, failure of this valve to close will have no adverse impact on PFSSD.
BBHS8000B	RL021	M-12BB02 (F-8)	BBHV8000B	Cold O/P Arm Sw	Could prevent closing the valve.	The pressurizer PORVs are closed in OFN RP-017 by disconnecting power to the circuit. This will fail the valves closed. Therefore, failure of this valve to close will have no adverse impact on PFSSD.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BBHIS0013	RL021	M-12BB03 (C-3)	BBHV0013	CCW from RCP A	Could cause spurious operation of the valve.	RCP thermal barrier cooling is not credited in OFN RP-017. The CCW service loop is isolated in OFN RP-017 so there will be no flow to the thermal barrier. Spurious operation of this valve will have no adverse impact.
BBHIS0014	RL021	M-12BB03 (C-3)	BBHV0014	CCW from RCP B	Could cause spurious operation of the valve.	RCP thermal barrier cooling is not credited in OFN RP-017. The CCW service loop is isolated in OFN RP-017 so there will be no flow to the thermal barrier. Spurious operation of this valve will have no adverse impact.
BBHIS0015	RL021	M-12BB03 (C-3)	BBHV0015	CCW from RCP C	Could cause spurious operation of the valve.	RCP thermal barrier cooling is not credited in OFN RP-017. The CCW service loop is isolated in OFN RP-017 so there will be no flow to the thermal barrier. Spurious operation of this valve will have no adverse impact.
BBHIS0016	RL021	M-12BB03 (C-3)	BBHV0016	CCW from RCP D	Could cause spurious operation of the valve.	RCP thermal barrier cooling is not credited in OFN RP-017. The CCW service loop is isolated in OFN RP-017 so there will be no flow to the thermal barrier. Spurious operation of this valve will have no adverse impact.
BBHIS8351A	RL021	M-12BB03 (D-5)	BBHV8351A	Seal Wtr Supply to RCP A	Could cause the valve to close.	Seal injection is not required for OFN RP-017. Seal injection is isolated in OFN RP-017 using valves BGV0101 and BGV0105. Spurious closure of this valve will have no adverse impact on PFSSD.
BBHIS8351B	RL021	M-12BB03 (D-5)	BBHV8351B	Seal Wtr Supply to RCP B	Could cause the valve to close.	Seal injection is not required for OFN RP-017. Seal injection is isolated in OFN RP-017 using valves BGV0101 and BGV0105. Spurious closure of this valve will have no adverse impact on PFSSD.
BBHIS8351C	RL021	M-12BB03 (D-5)	BBHV8351C	Seal Wtr Supply to RCP C	Could cause the valve to close.	Seal injection is not required for OFN RP-017. Seal injection is isolated in OFN RP-017 using valves BGV0101 and BGV0105. Spurious closure of this valve will have no adverse impact on PFSSD.
BBHIS8351D	RL021	M-12BB03 (D-5)	BBHV8351D	Seal Wtr Supply to RCP D	Could cause the valve to close.	Seal injection is not required for OFN RP-017. Seal injection is isolated in OFN RP-017 using valves BGV0101 and BGV0105. Spurious closure of this valve will have no adverse impact on PFSSD.
BBHIS8000A	RL021	M-12BB02 (E-7)	BBHV8000A	Cold O/P Arm Sw	Could prevent closing the valve.	The pressurizer PORVs are closed in OFN RP-017 by disconnecting power to the circuit. This will fail the valves closed. Therefore, failure of this valve to close will have no adverse impact on PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
BBHIS8000B	RL021	M-12BB02 (F-7)	BBHV8000B	Cold O/P Arm Sw	Could prevent closing the valve.	The pressurizer PORVs are closed in OFN RP-017 by disconnecting power to the circuit. This will fail the valves closed. Therefore, failure of this valve to close will have no adverse impact on PFSSD.
ECHIS0011	RL021	M-12EC01 (H-5)	ECHV0011	Fuel Pool Hx CCW Disch Iso A	Could cause spurious operation of the valve.	Valve controls CCW flow to the Fuel Pool Hx. The fuel pool cooling system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
ECHIS0012	RL021	M-12EC01 (E-5)	ECHV0012	Fuel Pool Hx CCW Disch Iso B	Could cause spurious operation of the valve.	Valve controls CCW flow to the Fuel Pool Hx. The fuel pool cooling system is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
LFHIS0105	RL023	M-12LF03 (C-5)	LFHV0105	Control/Aux Bldg Sump Iso Vlv	Could cause the valve to close or open.	The auxiliary building drainage system is not relied on for PFSSD. Spurious operation of this valve will not adversely impact PFSSD.
LFHIS0106	RL023	M-12LF03 (C-4)	LFHV0106	Control/Aux Bldg Sump Iso Vlv	Could cause the valve to close or open.	The auxiliary building drainage system is not relied on for PFSSD. Spurious operation of this valve will not adversely impact PFSSD.
AFHIS0113	RL023	M-12AF02 (C-7)	AFLV0113C	Feed Wtr Htr 4A Iso Vlv	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0106	RL023	M-12AF02 (E-7)	AFLV0106C	Feed Wtr Htr 3A Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHIS0144	RL023	M-12AF02 (C-5)	AFLV0144C	Feed Wtr Htr 4B Iso Vlv	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0136	RL023	M-12AF02 (E-5)	AFLV0136C	Feed Wtr Htr 3B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHIS0173	RL023	M-12AF02 (C-3)	AFLV0173C	Feed Wtr Htr 4C Iso Vlv	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0165	RL023	M-12AF02 (E-3)	AFLV0165C	Feed Wtr Htr 3C Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
AFHS0007	RL023	M-12AF01 (G-8)	AFLV0007C AFLV0007D AFLV0007E	Feed Wtr Htr 7A Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0012	RL023	M-12AF01 (E-7)	AFLV0012C	Feed Wtr Htr 6A Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0012	RL023	M-12AF01 (E-7)	AFLV0012D	MSR C Scavenging Steam to HP Htr 6A	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0012	RL023	M-12AF01 (E-7)	AFLV0012E	MSR A Scavenging Steam to HP Htr 6A	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHIS0024	RL023	M-12AF01 (D-7)	AFLV0024C	Feed Wtr Htr 5A Iso Vlv	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0058	RL023	M-12AF01 (F-2)	AFLV0058C	Feed Wtr Htr 7B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0058	RL023	M-12AF01 (F-2)	AFLV0058D	Feed Wtr Htr 7B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0058	RL023	M-12AF01 (F-2)	AFLV0058E	Feed Wtr Htr 7B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0044	RL023	M-12AF01 (E-3)	AFLV0044C	Feed Wtr Htr 6B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0044	RL023	M-12AF01 (E-3)	AFLV0044D	Feed Wtr Htr 6B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHS0044	RL023	M-12AF01 (E-3)	AFLV0044E	Feed Wtr Htr 6B Drain Iso Vlvs	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
AFHIS0064	RL023	M-12AF01 (D-3)	AFLV0064B	Feed Wtr Htr 5B Iso Vlv	Could cause the valve to close or open.	The feed water heaters are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
AFHIS0210	RL023	M-12AF01 (C-3)	AFHV0210	Htr Drn Tk Start Up Drn to Cond	Could cause the valve to close or open.	The heater drain tank is not required for PFSSD. Spurious operation will not impact safe shutdown.
ADHIS0008	RL023	M-12AD02 (C-3)	ADHV0008	Cond Pump A Disch Iso	Could prevent operation of the valve.	The condensate pumps are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
ADHIS0017	RL023	M-12AD02 (C-5)	ADHV0017	Cond Pump B Disch Iso	Could prevent operation of the valve.	The condensate pumps are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
ADHIS0024	RL023	M-12AD02 (C-7)	ADHV0024	Cond Pump C Disch Iso	Could prevent operation of the valve.	The condensate pumps are not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
ADHIS0028	RL023	M-12AD02 (C-2)	ADHV0028	Cond Demin Bypass	Could prevent operation of the valve.	The valve is not required for PFSSD. Spurious operation of the valve will not adversely impact safe shutdown.
LFHIS0095	RL023	M-12LF09 (F-2)	LFFV0095	Cont Sump Iso Vlv	Could cause the valve to close or open.	The reactor building drainage system is not relied on for PFSSD. Spurious operation of this valve will not adversely impact PFSSD.
FCHIS0004	RL023	M-12FC03 (H-3)	FCHV0004	SGFP Turb A Above Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0104	RL023	M-12FC04 (H-3)	FCHV0104	SGFP Turb B Above Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0007	RL023	M-12FC03 (H-3)	FCHV0007	SGFP Turb A Below Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0107	RL023	M-12FC04 (H-3)	FCHV0107	SGFP Turb B Below Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0012	RL023	M-12FC03 (F-3)	FCHV0012	SGFP Turb A Above Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0112	RL023	M-12FC04 (F-3)	FCHV0112	SGFP Turb B Above Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
FCHIS0013	RL023	M-12FC03 (F-3)	FCHV0013	SGFP Turb A Below Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0113	RL023	M-12FC04 (F-3)	FCHV0113	SGFP Turb B Below Seat Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0071	RL023	M-12FC03 (A-4)	FCHV0071	SGFP Turb A Startup Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
FCHIS0171	RL023	M-12FC04 (A-4)	FCHV0171	SGFP Turb B Startup Drain	Could cause the valve to close or open.	The SGFP is not required for PFSSD. Damage to the switch will have no adverse impact on PFSSD.
ADHIS0113	RL023	M-12AD01 (F-4)	ADHV0113A, ADHV0113B, ADHV0113C, ADHV0113D	Vacuum Breaker Valves	Could cause the valve to close or open.	The condenser vacuum breaker valves are not required for PFSSD. Spurious operation will not adversely impact PFSSD.
KAHIS0030	RL024	M-12KA01 (C-1)	KAHV0030	Inst Air Supply to H2 Ctrl System	Could cause the valve to close or remain open.	The H2 control system is not credited for PFSSD. Damage to this switch will not adversely impact safe shutdown.
ACHIS0251	RL024	M-12AC02 (G-6)	ACHV0251, ACHV0252, ACHV0261, ACHV0263	2nd Stage Reheater Steam Drains	Could cause the valves to close or open.	The moisture separator reheater is not required for PFSSD. Spurious operation of the valves will have no adverse impact on safe shutdown.
ACHIS0189	RL024	M-12AC02 (G-7)	ACHV0189A, ACHV0189B, ACHV0189C, ACHV0189D	1st Stage Reheater Steam Supply	Could cause the valve to close or open.	The moisture separator reheater is not required for PFSSD. Spurious operation of the valve will have no adverse impact on safe shutdown.
ABHIS0032	RL024	M-12AB03 (H-5)	ABHV0031, ABHV0032	2nd Stage Reheater Steam Supply	Could cause the valve to close or open.	Valve is required to be closed if the MSIVs cannot be closed to prevent uncontrolled steam release. OFN RP-017 closes the MSIVs so spurious operation of this valve will not adversely impact PFSSD.

Table A2
Control Room Fire Consequence Evaluation for Motor Operated Valves

Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
ACHIS0131	RL024	M-12AC02 (F-2)	ACHV0118, ACHV0120, ACHV0121, ACHV0122, ACHV0123, ACHV0124, ACHV0125, ACHV0126, ACHV0144, ACHV0145, ACHV0152, ACHV0153, ACHV0255	Cold Reheat Line Drains	Could cause the valves to close or open.	The MSR drains are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ACHIS0253	RL024	M-12AC02 (F-6)	ACHV0253, ACHV0254, ACHV0262, ACHV0264	1st Stage Reheater Steam Drains	Could cause the valves to close or open.	The MSR drains are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ADHS0055	RL024	M-12AD02 (G-6)	ADHV0055, ADHV0066	LP Htr 1A to 4A Isol Valves	Could cause the valves to close or open.	The low pressure heaters are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ADHS0043	RL024	M-12AD02 (G-4)	ADHV0043, ADHV0054	LP Htr 1B to 4B Isol Valves	Could cause the valves to close or open.	The low pressure heaters are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ADHS0030	RL024	M-12AD02 (G-2)	ADHV0030, ADHV0041	LP Htr 1C to 4C Isol Valves	Could cause the valves to close or open.	The low pressure heaters are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ADHS0042	RL024	M-12AD02 (G-3)	ADHV0042	LP Htr Bypass Valves	Could cause the valve to close or open.	The low pressure heaters are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
AEHIS0017	RL024	M-12AE01 (E-5)	AEHV0017, AEHV0034	HP Htr 5B, 6B and 7B Isol Vlvs	Could cause the valves to close or open.	The heaters are not required for PFSSD. Spurious operation of the valves will have no adverse impact on safe shutdown.
AEHIS0018	RL024	M-12AE01 (E-4)	AEHV0018, AEHV0033	HP Htr 5A, 6A and 7A Isol Vlvs	Could cause the valves to close or open.	The heaters are not required for PFSSD. Spurious operation of the valves will have no adverse impact on safe shutdown.
AEHIS0038	RL024	M-12AE01 (G-4)	AEHV0038	HP Htrs Bypass Valves	Could cause the valve to close or open.	The heaters are not required for PFSSD. Spurious operation of the valves will have no adverse impact on safe shutdown.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
EAHIS0005	RL024	M-12EA02 (G-3)	EAHV0005	Serv Wtr Return to CW System	Could cause the valve to close or open.	The service water system is not credited for PFSSD. The ESW system is the credited service water supply. Spurious operation of this valve will not adversely impact safe shutdown.
EAHIS0006	RL024	M-12EA02 (H-3)	EAHV0006	Serv Wtr Return to CW System	Could cause the valve to close or open.	The service water system is not credited for PFSSD. The ESW system is the credited service water supply. Spurious operation of this valve will not adversely impact safe shutdown.
ACHIS0119	RL024	M-12AC02 (F-2)	ACHV0119, ACHV0127, ACHV0129, ACHV0148, ACHV0149, ACHV0150, ACHV0151, ACHV0225	MSR Shell Drain Jog Control	Could cause the valves to close or open.	The MSR drains are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ACHIS0072	RL024	M-12AC01 (C-6)	ACHV0071, ACHV0072	Startup Drain Valve	Could cause the valves to close or open.	The startup drains are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ACHS0181A	RL024	M-12AC02 (H-7)	ACPV0181A, ACPV0181B, ACPV0181C, ACPV0181D	Reheater Steam High Load Valves	Could cause the valves to close or open.	The MSR's are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ACHIS0134	RL024	M-12AC01 (H-7)	ACHV0130, ACHV0134, ACHV0135, ACHV0136, ACHV0137, ACHV0256, ACHV0260, ACHV0261, ACHV0263	Main Stop and Control Vlv Startup Drains	Could cause the valves to close or open.	The drains are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.
ACHS0181B	RL024	M-12AC02 (H-7)	ACPV0181A	Main Steam Supply to 2nd Stage Reheater	Could cause the valve to close or open.	The MSR's are not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.

Table A2 Control Room Fire Consequence Evaluation for Motor Operated Valves						
Control Room Instrument	Instrument Location	P&ID Drawing	Associated MOV(s)	Description	Consequence if Damaged	Impact on PFSSD in the Event of a Control Room Fire
CAHIS0001	RL026	M-12CA01 (G-8)	CAHV0001	Main Steam Seal Feed Valve	Valve could fail open or closed.	The main steam seal system is not required for PFSSD. Steam flow is isolated when the MSIVs are closed. Therefore, spurious operation of this valve will not adversely impact safe shutdown.
CAHIS0002	RL026	M-12CA01 (G-8)	CAHV0002	Main Steam Seal Feed Valve	Valve could fail open or closed.	The main steam seal system is not required for PFSSD. Steam flow is isolated when the MSIVs are closed. Therefore, spurious operation of this valve will not adversely impact safe shutdown.
CAHIS0004	RL026	M-12CA01 (H-8)	CAHV0004	Aux Steam Seal Feed Valve	Valve could fail open or closed.	The auxiliary steam seal system is not required for PFSSD. Steam flow is isolated when the MSIVs are closed. Therefore, spurious operation of this valve will not adversely impact safe shutdown.
CAHIS0003	RL026	M-12CA01 (G-7)	CAHV0003	Steam Seal Man Unloading Vlv	Valve could fail open or closed.	The steam seal system is not required for PFSSD. Steam flow is isolated when the MSIVs are closed. Therefore, spurious operation of this valve will not adversely impact safe shutdown.
ABHIS0046	RL026	M-12AB03 (B-8)	ABHV0046	Main Stm Hdr to Stm Seal System	Valve could fail open or closed.	The main steam seal system is not required for PFSSD. Steam flow is isolated when the MSIVs are closed. Therefore, spurious operation of this valve will not adversely impact safe shutdown.
FBHS0082	RL027	M-12FB01 (F-7)	FBHV0080, FBHV0081, FBPV0017A, FBPV0017B	Htr's 6A and 6B Mn Stm Alignment	Could prevent operation of the valves.	The auxiliary steam system is not required for PFSSD. Damage to the switch will not adversely impact safe shutdown.
BMHS0100	RL027	M-12BM01 (G-2)	BMHV0100, BMHV0101	Htr's 5A and 5B Bldwn Stm Alignment	Could cause the valves to open or close.	Valves are not used for PFSSD. Damage to the switch will have no adverse impact on PFSSD. Steam generator blowdown is isolated in OFN RP-017 by opening breaker NK4411.
AEHS0103	RL027	M-12AE01 (G-2)	AEHV0102, AEHV0103	FWP PAE02 Inlet and Outlet Iso Valves	Could prevent operation of the valves.	The motor driven feedwater pump is not required for PFSSD. Damage to the switch will have no adverse impact on safe shutdown.