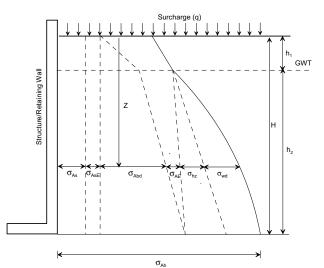
## Comanche Peak Nuclear Power Plant, Units 3 & 4 COL Application Part 2, FSAR



$$k_{A} = \tan^{2}(45 - \frac{\phi'}{2}) \approx 0.307$$
  

$$\Delta K_{AE}^{'} = K_{AE}^{'} - k_{A} \approx 0.133$$
  

$$\sigma_{As} = k_{A}q \approx 0.307q$$
  

$$\sigma_{AsE} = \Delta K_{AE}^{'}q \approx 0.133q$$
  

$$\sigma_{Abd} = k_{A}\gamma_{t}Z \approx 38.41Z$$
  

$$\sigma_{Abd} \approx 38.41h_{1} + 19.23(Z - h_{1})$$
  

$$\sigma_{AE} = \Delta K_{AE}^{'}\gamma_{e}(H - Z) \approx 8.33(H - Z)$$
  

$$\sigma_{hz} = \gamma_{w}(Z - h_{1}) \approx 62.4(Z - h_{1})$$
  

$$\sigma_{wd} = \frac{7}{8}k_{h}\gamma_{w}\sqrt{h_{2}(Z - h_{1})} \approx 5.46\sqrt{h_{2}(Z - h_{1})}$$
  

$$\sigma_{Ah} = \sigma_{As} + \sigma_{AsE} + \sigma_{Abd} + \sigma_{AE} + \sigma_{hz} + \sigma_{wd}$$

Static active earth pressure coefficient

Seismic active earth pressure coefficient (submerged case)

Static lateral pressure due to surcharge

Seismic lateral pressure due to surcharge

Static lateral pressure due to backfill above GWT (Z<h1)

Static lateral pressure due to backfill below GWT (Z>h1)

Seismic lateral pressure due to backfill

Hydrostatic lateral pressure due to GWT (Z>h1)

Hydrodynamic lateral pressure due to GWT (Z>h<sub>1</sub>)

Static plus seismic active horizontal pressure

- Units: lbs/ft<sup>2</sup> for pressure and ft for dimensions.
  - Assumed compacted backfill properties:
  - Total unit weight:  $\gamma_t = 125 \text{ lbs/ft}^3$

Notes:

- Internal effective friction angle:  $\phi' = 32^{\circ}$
- Effective cohesion intercept: C' = 0
- Hydrodynamic component does not apply to low permeability soils (k<10<sup>-3</sup> cm/sec).
- Compaction earth pressure is not included based on the assumption that light compaction equipment is used for compaction of soil adjacent to below-grade walls.

Figure 2.5.4-242 Active Earth Pressure