UNITED STATES
NUCLEAR REGULATORY COMMISSION
ADVISORY COMMITTEE ON REACTOR SAFEGUARDS
WASHINGTON, DC 20555 - 0001

June 15, 2012

MEMORANDUM TO: ACRS Members

FROM: Girija Shukla, Senior Staff Engineer ***/RA/***
Technical Safety Branch, ACRS

SUBJECT: CERTIFICATION OF THE MINUTES OF THE ACRS SUBCOMMITTEE ON THE UNITED STATES – ADVANCED PRESSURIZED WATER REACTOR, MARCH 22-23, 2012

The minutes for the subject meeting were certified on June 6, 2012. Along with the transcripts and presentation materials, this is the official record of the proceedings of that meeting. A copy of the certified minutes is attached.

Attachment: As stated

cc w/o Attachment: E. Hackett
C. Santos

cc w/ Attachment: ACRS Members

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June 15, 2012

MEMORANDUM TO: Girija Shukla, Senior Staff Engineer
Technical Safety Branch, ACRS

FROM: John Stetkar, Chairman
United Stated – Advanced Pressurized Water Reactor

SUBJECT: MINUTES OF THE MEETING OF THE ACRS SUBCOMMITTEE ON THE UNITED STATES – ADVANCED PRESSURIZED WATER REACTOR ON MARCH 22-23, 2012, IN ROCKVILLE, MD

I hereby certify, to the best of my knowledge and belief, that the minutes of the subject meeting are an accurate record of the proceedings for that meeting.

/RA/ **06/6/2012**
J. Stetkar Date
Chairman
ACRS Subcommittee on the
United States – Advanced Pressurized Water Reactor

ADVISORY COMMITTEE ON REACTOR SAFEGUARDS
MINUTES OF THE ACRS US-APWR SUBCOMMITTEE MEETING
MARCH 22-23, 2012

The ACRS United States – Advanced Pressurized Water Reactor (US-APWR) Subcommittee held a meeting on March 22-23, 2012 in Room T-2B1, 11545 Rockville Pike, Rockville, Maryland. On March 22, 2012, the meeting convened at 8:30 a.m. and adjourned at 4:56 p.m. On March 23, 2012, the meeting convened at 8:30 a.m. and adjourned at 10:31 a.m.

The entire meeting was open to the public.

No written comments or requests for time to make oral statements were received from members of the public related to this meeting.

ATTENDEES

ACRS Members/ Staff:

John Stetkar, Member
Said Abdel-Khalik, Member
Dennis Bley, Member
Charles Brown, Member
William Shack, Member
Ilka T. Berrios, Staff
Girija Shukla, Staff

NRC Staff:

Hossein Hamzehee, NRO
David Terao, NRO
Eileen McKenna, NRO
Larry Wheeler, NRO
Paul Kallan, NRO
Angelo Stubbs, NRO
Gordon Curran, NRO
Christopher Van Wert, NRO
David A. Nold, NRO
Raul Hernandez, NRO
William Ward, NRO
Ngola Otto, NRO
Eugene O. Eagle Jr., NRO
Robert Fitzpatrick, NRO
Ann Hodgdon, OGC

Other Attendees:

Ryan Sprengel, MNES
Hiroshi Hamamoto, MNES
James Curry, MNES
Jason Richard, MNES
Kevin Lynn, MNES
Masashi Ito, MNES
Masatoshi Nagai, MNES
C. Keith Pulson, MNES
Shinji Kawanago, MNES
Joseph Tapia, MNES
Shinji Kinchi, MNES
Ron Reynolds, MNES
Hideki Tanaka, MNES
Jim Rogers, MNES
Hiroki Nishic, MHI
Motohisa Kitamori, MHI

Marc Hotchkiss, MHI
Naoki Kawata, MHI
Yoshiyaki Tanigawa, MHI
Junya Hattori, MHI
Ketta Otan, MHI
Tom Fitzpatrick, Holtec
Chuck Bullard, Holtec
Todd Evans, Luminant

SUMMARY

The purpose of the meeting was to review Chapter 9, "Auxiliary Systems" of the Safety Evaluation Report (SER) with Open Items associated with the US-APWR design certification application. The meeting transcripts are attached and contain an accurate description of each matter discussed during the meeting. The presentation slides and handouts used during the meeting are attached to these transcripts.

The following table lists the significant issues that were discussed during the meeting with the corresponding pages in the transcript.

SIGNIFICANT ISSUES	
Issue	Reference Pages in Transcript
MHI provided a summary of the new and spent fuel storage facilities.	13-16
Members Shack and Brown, and Chairman Stetkar raised questions regarding the use of unanodized Metamic as a neutron absorber material in the spent fuel pool water with 4,000 ppm boric acid concentration.	16-20
Based on the US-APWR DCD Figure 9.1.4-2, Chairman Stetkar raised a concern regarding the failures that may occur while the weir gates are removed that could conceivably drain the spent fuel pool level down to the height of that weir wall. He asked for any information about the time until boiling would occur if it was drained to that level, and the time until fuel uncovery would start if drained to that level?	21-26
Based on the US-APWR DCD Figure 9.1.4-2, Chairman Stetkar asked if there are any drain lines from the transfer canal, cask pit and fuel inspection pit. If there are drain lines, how big they are?	27-28
MHI provided a summary of the spent fuel pit (SFP) cooling and purification system.	30-33
Chairman Stetkar raised the following question: If you're aligned in a refueling water storage pit cleanup mode so that you have one or both of the demineralizers aligned to the refueling water storage pit, and there is a break in the nonseismically-qualified section of the system, how do you isolate that break and prevent the refueling water storage pit from draining down into the fuel building?	33-36
Member Brown raised questions regarding the fuel pool instrumentation such as the level and temperature sensors.	36-40

MHI provided a summary of the light and heavy load handling systems.	43-48
Chairman Stetkar raised a question regarding the configuration of the spent fuel cask crane.	47-48
Member Bley raised a concern regarding the boron level in the spent fuel pit that's required to prevent criticality. MHI replied that soluble boron is needed only to prevent criticality for a misplaced fuel assembly outside the storage racks. Subcriticality is maintained under normal conditions, even if the pool is filled with pure water.	48-52
MHI provided a summary of the essential service water system.	53-56
MHI provided a summary of the component cooling water system.	56-73
Chairman Stetkar raised questions regarding the valves that connect the two trains in the component cooling water system. In Revision 3, the valves received automatic isolation signals, now they are manual. How does the operator determine train separation is required and what conditions require the operators to close those valves? Any guidance?	57-61, 205-219
Chairman Stetkar raised a concern regarding the possible overheating of reactor coolant pump motors after the loss of the component cooling water system. He also raised a concern regarding the vibration problems on the reactor coolant pumps after heating up the bearing oil system	63-71
MHI provided a summary of the potable and sanitary water system.	73-74
MHI provided a summary of the ultimate heat sink (UHS).	74-77
MHI provided a summary of the condensate storage facilities.	77-80
Chairman Stetkar raised a concern regarding the radioactive water leakages from the primary makeup water tank piping. MHI stated that the pipe between the primary water tank building and the auxiliary building is double-walled, with drainage to a radioactive waste sump.	78-80
MHI provided a summary of the chilled water system.	80-93
Chairman Stetkar and member Abdel-Khalik raised questions regarding the heat load of the emergency feedwater pumps and the heatup calculations for the turbine-driven pump rooms.	82-92
MHI provided a summary of the non-essential chilled water system.	93-95
Chairman Stetkar asked for clarification regarding the connection between the non-essential chilled water system and the component cooling water system.	95-104

MHI provided a summary of the turbine component cooling water system.	105-106
MHI clarified a committee's question regarding the unanodized Metamic, the borated water and the potential pH associated with it.	109-112
MHI provided a summary of the process auxiliaries.	112-114
MHI provided a summary of the sampling systems.	114-115
Chairman Stetkar asked for more information regarding two normally closed manual valves that are located at the outlet of the ESF room floor drains.	115-122
MHI provided a summary of the chemical and volume control system.	122-123
MHI provided a summary of the ventilation systems.	123-143
Chairman Stetkar asked if there are any safety-related components in the turbine building.	133
Chairman Stetkar asked for more information regarding the function and the classification of the containment fan coolers.	137-143
MHI provided a summary of the fire protection program.	143-158
Chairman Stetkar asked for additional information regarding the fire protection program: the configuration of the four safety divisions as they flow to the control room, and the barriers or separations that may have. MHI stated that the walls between the four electrical division cable rooms extend the full height to the Main Control Room floor. The divisional cables are distributed to the control panels in the sub-floor area below the Main Control Room raised floor.	147-153
MHI provided a summary of other auxiliary systems such as communications systems, lighting systems, gas turbine generator (GTG) systems (fuel oil storage and transfer, starting system, lubrication system)	159-167
Member Brown raised a concern regarding the communication system being compromised.	159-163
Member Brown asked additional questions regarding the water level and the temperature gauges in the spent fuel (differences between the original design and the changes made as a result of an RAI).	168-177
NRC staff's presentation	178-250
Chairman Stetkar identified an inconsistency between the SER and the DCD Section 9.1.3 regarding spent fuel pit cooling capabilities and temperatures under degraded cooling conditions.	180-186
Chairman Stetkar raised a concern about the time and capability to clean up the spent fuel pit and the RWSP (SER Section 9.1.3.4).	192-194

Chairman Stetkar raised a concern regarding the basis for a statement in the SER Section 9.1.4.4 (the staff determined that any cavity leakage will be less than the available makeup capability).	194-195
Chairman Stetkar raised a question regarding the heavy load handling system; if there are any structures, systems, and components (SSCs) important to safety that could be damaged by drops from the Turbine Buildng crane?	196-199
Chairman Stetkar raised a concern regarding the difference of the required capacity of the UHS. A UHS should be sufficient for 30 days of cooling without makeup, but a minimum of 36 days is required for a cooling pond.	219-223
Member Bley asked how the new orders that were issued as a result of Fukushima will apply to the new plants.	225-226
The staff discussed the locations of the tanks such as the condensate and demineralized water storage tanks to avoid any flooding if there is a failure. This will probably be a COL item.	230-238
Chairman Stetkar raised a concern regarding why the essential chilled water system does not need technical specifications.	239-242
The staff discussed the Main Control Room ventilation systems.	243-246
Chairman Stetkar raised a concern regarding whether the 60 minutes is an appropriate time for startup of the alternate AC source based on heatup of the Main Control Room environment. The staff indicated that a steady-state temperature of approximately 121 °F is reached long after 60 minutes. There is substantial margin to that temperature at 60 minutes.	246-247
The staff discussed potential effects on Main Control Room instrumentation and controls on a worse case essential chilled water system leak within a Main Control Room HVAC system air handling unit	248-250
MHI provided responses to Chairman Stetkar's comment about the weir wall and drainage of spent fuel pit level to the weir wall height that is shown in DCD Figure 9.1.4-2. MHI did not have the information about heatup and boiloff times with level at the weir wall height.	259-267
MHI provided a partial response to Chairman Stetkar's concerns about potential draining of the spent fuel pit. There are no drain lines from the fuel transfer tube or the bottoms of the refueling canal, cask loading pit, and fuel inspection pit.	268-272
MHI provided a partial response to Chairman Stetkar's comment about alignment of the spent fuel pit demineralizers for RWSP cleanup.	289-292
MHI provided response to Chairman Stetkar's question in 9.1.4 about seismic restraints on the cask crane. The crane has seismic restraints.	292-293
MHI provided response to Chairman Stetkar's question in 9.2.2, with regard to the 10 minutes for restoring cooling to the RCP pumps. The time is based on the pump manufacturer's recommendations for bearing cooling.	293-295
MHI provided response to Chairman Stetkar's question also in 9.2.2 about component cooling water.	296
MHI provided response to Chairman Stetkar's question in 9.2.6 about the dike around the demineralized water storage tank. The tank does not have a dike.	296

MHI provided response to Chairman Stetkar's question in 9.2.7, about why the motor-driven EFW pump heat load was higher than the turbine-driven pump heat load.	297
MHI provided response to Chairman Stetkar's question about turbine-driven EFW pump and whether steam leakage was considered. Steam leakage was not considered in the room heatup calculation.	298
MHI provided response to Chairman Stetkar's question in 9.2.7 about double-lock closed isolation valves on the line from the CCW to the fan coolers.	299
MHI provided response to Chairman Stetkar's question in 9.3.3 about the normally closed floor drains in the ESF rooms.	299-301
MHI provided response to Chairman Stetkar's question in 9.5.1 about the separation of all four cable trains below the control room.	301-304
Member Shack presented his conclusions regarding acceptable performance of unanodized Metamic in a highly borated water environment.	306-308
The staff provided response to Chairman Stetkar's question in 9.2.5 with regards to the 30-day and 36-day ultimate heat sink inventory requirements.	308-313
The staff discussed the crossties between the CCWS loops in 9.2.2. The staff will ask MHI about potentially optimistic analysis assumptions regarding the timing of offsite power failure and a single active failure during LOCA heat load conditions.	314-317
The staff discussed about the 24-hour duration for operator action.	317-318
The staff provided response to Chairman Stetkar's question in 9.1.3.1 with regards to the inconsistency in the SFP temperature with regards to the DCD and the SER.	319-321
The staff provided response to Chairman Stetkar's comment on Section 9.1.4 about drain down of the refueling cavity.	323-327
The staff provided response to Chairman Stetkar's question about the chilled water system and why it is not in the tech specs.	327-335
The staff discussed about a set of equipment, structures that are important to safety, and that safety-related is a subset of that larger set.	335-339

DOCUMENTS PROVIDED TO THE SUBCOMMITTEE

The following documents were provided to the members prior to the meeting:

- Memorandum to Edwin M. Hackett, U.S. Nuclear Regulatory Commission, United States - Advanced Pressurized Water Reactor Design Certification Application - Safety Evaluation with Open Items for Chapter 9, "Auxiliary Systems," 02/22/2012 (ML120390205)

- MUAP-DC009, Revision 3, Design Control Document for the US-APWR, Chapter 9, "Auxiliary Systems," Mitsubishi Heavy Industries, 03/31/2011 (ML110980217)

- MUAP-07032-NP, Revision 1, “Criticality Analysis for US-APWR New and Spent Fuel Storage Racks,” Mitsubishi Heavy Industries, December 2009 (ML093510508)

- MUAP-07033-NP, Revision 0, “Mechanical Analysis for US-APWR New and Spent Fuel Racks,” Mitsubishi Heavy Industries, March 2009 (ML090970187)

- MUAP-09014-NP, Revision 0, “Thermal-Hydraulic Analysis for US-APWR Spent Fuel Racks,” Mitsubishi Heavy Industries, June 2009 (ML091620275)

- MUAP-10020-NP, Revision 1, “US-APWR Safety-Related Air Conditioning, Heating, Cooling, and Ventilation Systems Calculations,” Mitsubishi Heavy Industries, March 2011 (ML111010226)

- “Markup for US-APWR DCD Revision 4 Section 9.2,” Mitsubishi Heavy Industries, 10/14/2011 (ML112940586)

Official Transcript of Proceedings

NUCLEAR REGULATORY COMMISSION

Title: Advisory Committee on Reactor Safeguards
US-APWR Subcommittee

Docket Number: (n/a)

Location: Rockville, Maryland

Date: March 22-23 2012

Work Order No.: NRC-1512 Pages 1-340

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UNITED STATES OF AMERICA

NUCLEAR REGULATORY COMMISSION

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ADVISORY COMMITTEE ON REACTOR SAFEGUARDS

(ACRS)

+ + + + +

US-APWR SUBCOMMITTEE

+ + + + +

THURSDAY

MARCH 22, 2012

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ROCKVILLE, MARYLAND

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The Subcommittee met at the Nuclear Regulatory Commission, Two White Flint North, Room T2B1, 11545 Rockville Pike, at 8:30 a.m., John Stetkar, Chairman, presiding.

SUBCOMMITTEE MEMBERS PRESENT:

JOHN W. STETKAR

SAID ABDEL-KHALIK

DENNIS C. BLEY

CHARLES H. BROWN, JR.

WILLIAM J. SHACK

NRC STAFF PRESENT:

ILKA BERRIOS, Designated Federal Official

HOSSEIN HAMZEHEE

PAUL KALLAN

LARRY WHEELER

RAUL HERNANDEZ

GORDON CURRAN

EILEEN McKENNA

ANGELO STUBBS

DAVID NOLD

ALSO PRESENT:

RYAN SPRENGEL

JAMES CURRY

YOSHIYUKI TANIGAWA

BRET BRICKNER

CHARLES BULLARD

NAOKI KAWATA

SHINJI KAWANAGO

HIROKI NISHIO

MOTOHISA KITAMORI

JUNYA HATTORI

KEVIN LYNN

MARC HOTCHKISS

HIROSHI HAMAMOTO

RONALD REYNOLDS

HIDEKI TANAKA

MASASHI ITO

T-A-B-L-E O-F C-O-N-T-E-N-T-S

P-R-O-C-E-E-D-I-N-G-S

8:32 a.m.

CHAIR STETKAR: The meeting will now come to order. This is a meeting of United States Advanced Pressurized Water Reactor Subcommittee. I'm John Stetkar, Chairman of the Subcommittee meeting.

ACRS members in attendance are Dennis Bley, Said Abdel-Khalik, Bill Shack, and Charles Brown.

Ilka Berrios of the ACRS staff is the designated federal official.

The Subcommittee will review Chapter 9, Auxiliary Systems of the Safety Evaluation Report with Open Items associated with the US-APWR design certification application. We'll hear presentations from Mitsubishi Heavy Industries and the NRC staff.

We have received no written comments or request for time to make oral statements from members of the public regarding today's meeting.

The Subcommittee will gather information, analyze relevant issues and facts and formulate proposed positions and actions as appropriate for deliberation by the full Committee.

The rules for participation in today's meeting have been announced as part of the notice of this meeting previously published in the Federal

Register. Parts of this meeting may need to be closed to the public to protect information proprietary to Mitsubishi Heavy Industries or other parties.

I'm asking the NRC staff and the Applicant to identify the need for closing the meeting before we enter into such discussions, and to verify that only people with a required clearance and need to know are present.

A transcript of the meeting is being kept and will be made available as stated in the Federal Register notice. Therefore, we request that participants in this meeting use the microphones located throughout the meeting room when addressing the Subcommittee. The participants should first identify themselves and speak with sufficient clarity and volume so that they may be readily heard.

First, regarding -- before we start, we scheduled this meeting for two days because there's a lot of material to cover. I wanted to make sure that you had enough opportunity for discussions and questions and understanding. I don't think we'll finish today. I don't think that we will require all day tomorrow.

I want to emphasize I don't want to keep -- make sure there's enough time so don't rush to try to finish today. If you need tomorrow morning, that's fine.

I doubt that we'll run all day tomorrow if we're kind of thinking of things so it's a little bit difficult to schedule the timing with this volume of material because you really don't know how much discussion will be necessary. I didn't want to artificially compress that discussion just by scheduling it for one day. Keep that in mind and I think everything will go okay.

We'll now proceed with the meeting. I call upon Hossein Hamzehee.

MR. HAMZEHEE: Thank you, sir. Thank you again. I think, as you said, we are ready for two days, although our preference is to finish everything today but the staff at MHI are available in case there is a need for the second day.

With that I am going to turn it to Paul. He's the Chapter PM.

MR. KALLAN: Hi. Good morning. My name is Paul Kallan. I'm the Senior Project Manager and also the Chapter PM for the US-APWR Chapter 9. I would like to thank the Subcommittee for having us here today. I would like to also thank MHI MNES for being here and also for making their presentations.

I would also like to thank staff for being here today.

This is the US-APWR DCD certification which was submitted to Mitsubishi Heavy Industries on December 31, 2007. We are currently on Revision 3 which was submitted March 31, 2011. We have taken eight chapter to the ACRS which is 2, 16, 8, 13, 11, 12, 5, and 10 previously to the ACRS. It has gone through the Subcommittee and full Committee. Although there's two COLAs associated with this chapter, today we are only going to present the DCD.

CHAIR STETKAR: Just for the record, parts of the review of this are based on Interim Revision 4 of the DCD. Is that correct?

MR. KALLAN: Correct.

CHAIR STETKAR: Okay. Thanks.

MEMBER BROWN: Do we have that yet?

MS. BERRIOS: In the CD that I sent you.

MEMBER BROWN: I didn't get it.

MEMBER BLEY: It was surreptitious.

CHAIR STETKAR: It was a stealth transmittal.

MEMBER BROWN: I only have Rev. 3. That's why I asked. My Chapter 7 stuff is only Rev. 3 so --

CHAIR STETKAR: That's okay. This was

just -- the staff will explain it, I'm sure, when we come up. I just wanted to get on the record what it is we're reviewing here.

With that, I'll turn it over to MHI.

MR. SPRENGEL: This is Ryan Sprengel with MNES, DC licensing manager. Thank you all, Subcommittee members. I think we've had many good interactions in the past and look forward to hopefully a lot of interactions this year. I think we've got a lot of chapters getting ready to come through you guys so we'll look for continued good interactions.

For today we are looking at Chapter 9, as was mentioned. I want to touch on that real quick. We are on DCD Chapter 3 -- Rev. 3, but we did do a markup. We had a lot of changes through our interactions with the staff and to facilitate looking at all these changes we submitted a compilation and it just showed a markup. It's what would become Rev. 4 but we have not submitted Rev. 4.

CHAIR STETKAR: You haven't, but just for clarity what we'll hear today from the SER and what we'll hear from you today is the status of the design as of that markup Interim Rev. 4. Is that correct?

MR. SPRENGEL: That is correct.

CHAIR STETKAR: The only reason I want to make that clear is because in at least the Component Cooling Water System there were substantive changes.

MR. SPRENGEL: Absolutely.

CHAIR STETKAR: We're going to be talking the Interim Rev. 4 version of that.

MR. SPRENGEL: That is correct.

MEMBER BLEY: I wonder if it's possible when you make your presentations to highlight the things that have changed across that revision.

MR. SPRENGEL: I think that will be a focus.

MEMBER BLEY: It might preclude some questions.

MR. SPRENGEL: Yes. Agreed.

CHAIR STETKAR: If they don't, I'll try because I compared the two.

MEMBER BLEY: Thank you.

MR. SPRENGEL: Okay. As you can see, we brought many people to support many experts and we are prepared for today and tomorrow so whatever you guys need we are ready to support. Hopefully we don't go into Saturday.

CHAIR STETKAR: We won't do that. I have a flight Saturday morning.

MR. SPRENGEL: As we've done in the past, if there is anything that we are not able to get back to you on today or tomorrow, we'll follow up in the future with written responses.

For now I will go and turn it over to Jim Curry.

MR. CURRY: Good morning. My name is Jim Curry and we are representing Mitsubishi Energy Systems and Mitsubishi Heavy Industries, the team here today, to discuss Chapter 9, Auxiliary Water Systems. As Mr. Prengel said, we appreciate the opportunity to meet with the Subcommittee.

The MHI team today includes system experts, contractors, licensing personnel, and members of the MNES and MHI management team. Each Chapter 9 section, 9.1 through 9.5, will be represented by a subset of this MHI team and the subset will be primarily at this table or at the end of the table over to my right.

There are also additional key folks who are present in the audience and we can access documentation on our servers as necessary to get the best information for the Committee.

Today we plan to focus on Chapter 9 subsections that we believe would be of most interest to the Committee. As you have heard, Chapter 9 covers a spectrum of systems. Some systems are safety related and many are not. We'll probably focus on those that have safety-related implications and spend less time on other subsections. However, the team here today includes members that can speak to any subsection.

The presentation materials that we are going to go through have the same general format which includes introductory slides with an acronym list and the names of the folks at this table and the table to my right, some summary information including simplified system schematics, and a table of SER open items and confirmation items.

We can give you the current status as we see it if you need for those open items. We also have some additional backup information slides which we may use if needed. If it's acceptable to the Committee, we plan to proceed in numerical order starting with Section 9.1, Fuel Storage and Handling.

CHAIR STETKAR: That would be wonderful.

MR. CURRY: Good news. Off to a good start. Okay. 9.1, as you know, is Fuel Storage and Handling so I would like to introduce Naoki Kawata who is here. Mr. Kawata is the deputy manager, MHI Water Reactor Systems Engineering Section. He will be supporting this presentation. I would also like to introduce Mr. Yoshiyuki Tanigawa. Mr. Tanigawa is an engineer, MHI Plant Layout Engineering Section.

Then the next three folks are with Holtec International who are the designers of our fuel racks and they are here to support us; Mr. Thomas Fitzpatrick, Mr. Charles Bullard. Mr. Fitzpatrick is the project manager. Mr. Bullard is the manager of the structural group so he'll be here to answer rack structural questions. Mr. Bret Brickner who is the criticality expert on the team.

The acronym list, as we talked about. We'll be going through each of these subsections of 9.1 in order as indicated. Let's start with the criticality safety of the new and spent fuel pool storage. You may find it helpful to take a look at the second slide in this, which is labeled Slide No. 5, the second technical slide.

In summary, the new and spent fuel storage facilities are located in the fuel handling area of the reactor building. The US-APWR has the containment vessel, pre-stressed concrete containment vessel surrounded by a reactor building. We call this the fuel storage area.

CHAIR STETKAR: Jim, just be sure you

don't get too far away from the microphones. We need it for the transcript. A lot of times it's easier if you use your mouse to point to things.

MR. CURRY: Thank you.

CHAIR STETKAR: The microphones are pretty sensitive but if you stray too far away, we have problems.

MR. CURRY: Thank you, Mr. Chairman. That's helpful.

Okay. So, in any event, the new and spent fuel storage facilities again, as I said, are located in the fuel-handling area of the reactor building. The reactor building is seismic Category I. New fuel is stored in low density racks. Spent fuel is stored in moderate density racks. The new fuel is stored dry. Spent fuel is stored in borated water.

In the new fuel storage pit, as we call it, we have the capability for 180 fuel assemblies. That corresponds to approximately one refueling batch, normal refueling plus an additional 50 locations.

In the spent fuel area, spent fuel pit -- sorry. The spent fuel pit area we have the capacity for 900 fuel assemblies which is about the amount of spent fuel from 10 years of operation assuming a two-year fuel cycle plus a full-core off-load.

CHAIR STETKAR: Jim.

MR. CURRY: Yes, sir.

CHAIR STETKAR: For configuration of things, in the DCD that explains what you just said pretty clearly, but it also mentions that there's a rack with a capacity for 12 damaged fuel assemblies. Where is that located?

MR. CURRY: The damaged fuel rack. Mr. Tanigawa.

MR. TANIGAWA: Damaged fuel racks is located in this area.

CHAIR STETKAR: Oh, okay. Okay. Because the drawing showed the configuration of the spent fuel racks, the 900. I didn't know whether that consumed the entire volume for all practical purposes of the spent fuel pit. It's over in one end of the spent fuel pit. Thanks.

MR. CURRY: The cooling and water quality of the spent fuel pit is maintained by the spent fuel pool cooling -- spent fuel pit cooling and purification system which we'll be discussing as part of Subsection 9.1.3.

The new and spent fuel storage, as I mentioned, these are in Category I structures designed to withstand the design basis external event conditions there defined in Chapter 2 of the DCD. Spent fuel and new fuel racks are designed to maintain subcriticality requirements consistent with 10 CFR 50.68 and we'll talk about that in a second. Equipment could potentially damage fuel if it were to fail is designed as seismic Category I. So sorry, seismic Category II.

MEMBER BROWN: You're talking about the cranes?

MR. CURRY: Yes, sir. Yes, sir.

The next couple of slides will kind of summarize the criticality analysis and will also summarize the structural requirements for the racks.

As I mentioned, criticality requirements are specified in 10 CFR 50.68 so we meet those requirements for the new fuel racks. New fuel racks are stored -- new fuel is stored dry. Spent fuel storage rack we do use soluble boron. Once again, we comply with these requirements which are 10 CFR 50.68.

Kind of some key points of the analysis conditions. The maximum enrichment 5 percent specified in the regulation. The appropriate assembly tolerances were considered in a criticality evaluation. Credit is taken for a neutron absorption in the racks. I think metamic is fundamentally what's used here. And, of course, dimensions are appropriately considered.

New fuel storage is constructed of stainless steel with the assumption of concrete reflectors in the calculations. Spent fuel storage rack stainless steel metamic.

MR. BRICKNER: There's no metamic in the refuel.

MR. CURRY: Spent fuel?

MR. BRICKNER: Spent fuel.

MR. CURRY: Yes. Spent fuel, right, is metamic, and the assumption of an infinite rack array in the lateral direction.

MEMBER SHACK: With the metamic, that's a naked aluminum, right?

MR. BRICKNER: It's a powder metallurgy.

MEMBER SHACK: It's a powder metallurgy but, I mean, it's boron carbide and aluminum matrix.

MR. BRICKNER: Yes.

MEMBER SHACK: So it's essentially exposed to the environment as unclad aluminum. There's no stainless steel clad on this stuff.

MR. BRICKNER: There is a sheathing. It's encapsulated in a sheathing but it's not sealed.

MEMBER BROWN: What do you mean byu

sheathing?

MR. BRICKNER: There's a stainless steel covering. The metamic is not mechanically fastened to the rack structure.

MEMBER SHACK: But it's exposed to the coolant.

MR. BRICKNER: It is. Correct.

MEMBER SHACK: And the pH of this stuff is? The pH limits in the pool is?

CHAIR STETKAR: It's 4,000 ppm boric acid.

MEMBER SHACK: Whatever that is.

MR. BRICKNER: I can't answer the pH levels in the pool.

MR. CURRY: If you give us a second, we'll look that up for you and get back to you.

MEMBER SHACK: Fine. It just seems like you're in a corrosive region for aluminum.

MR. BULLARD: There is a topical report that's been submitted to the NRC specifically on the use of metamic and spent fuel rack applications that I would point you to. It has been used and is installed in many spent fuel pools.

CHAIR STETKAR: At this types of pH levels, though? A lot of spent fuel pools don't quite have this boron concentration.

MR. BULLARD: That I don't know. I cannot confirm your answer.

MEMBER BROWN: Does the sheathing really encapsulate the metamic or is it -- you said it's not bonded.

MR. BULLARD: It's not sealed so the sheathing covers the metamic and then the sheathing itself is stainless steel like the rack so wall material. That sheathing is fillet-welded and spot-welded along its perimeter. There's a flange.

MEMBER BROWN: But water can get between it and the --

MR. BULLARD: But there are openings at the corners where there is access where the coolant can get beneath the sheathing. Metamic is also used in dry storage cask applications as well.

MR. CURRY: So we'll take as an action the pH requirements for the pool and see if we can get back to you on that.

CHAIR STETKAR: Do you happen -- the topical report had the same type of configuration open where the metamic is exposed to the coolant. It wasn't a sealed --

MR. BULLARD: Seam rack construction.

CHAIR STETKAR: Seam rack construction.

MEMBER SHACK: Now, do you sometimes anodize this or is this always used in an untreated condition? Here it says it will not be anodized so it sort of sounds as though that maybe sometimes you do.

MR. BULLARD: I would have to confirm that. I think the condition that is used here --

MEMBER SHACK: Is the standard condition?

MR. BULLARD: -- is the standard condition. I'm not aware of any applications where it's anodized.

MR. CURRY: All right. I would propose we move onto the structural requirements. The design and stress analysis of all the racks is consistent with Reg Guide 1.29 for seismic design. The load combinations, as indicated, are consistent with SRP Section 3.8.4.

The racks are free-standing. They can withstand a maximum uplift force based on the lifting capacity of the suspension hoist and the refuel machine which I think is 4,400 pounds. Of course, we can maintain a subcritical array in the event of any fuel handling accident. That's kind of a summary of the structural piece. Does anyone have any questions on the structural design?

CHAIR STETKAR: No, I think I'll wait until we bring up slides -- a few slides ahead before I ask a couple of questions. Continue.

MR. CURRY: Okay. We have some confirmatory items and one open item, I think, which we're working on with the staff. We recently received an RAI response March 5th so we'll be replying to that within 60 days. I think that's fundamentally what we had to say about new and spent fuel storage.

CHAIR STETKAR: Let me ask one -- I was trying to think about the most appropriate place to ask it and I can't decide so I'll ask it now. You might want to, just for reference, bring up your slide No. -- okay. I've lost track here. No. 15, I think, unless you have a better one. There's a figure in the CDC that is Figure 9.1.4-2 that a bit better illustrates the question I was going to ask, but this one might do.

The question is, and it's difficult to look at this elevation view and the plan view at the same time. There are -- in this elevation view there are weir walls. There are gates that separate the spent fuel pit from the transfer canal and irrigates that separate the cask pit and the fuel inspection pit from the transfer canal.

Those weir walls, the gates, as best as I can tell the bottom of the slot of the gate, in other words if you remove the gate, the bottom of that slot appears to be about, and I didn't have all of the dimensions available, but about two-and-a-half feet roughly above the top of the active fuel. It might be a little bit more, might be a little bit less. I was curious whether you know what that elevation difference is.

MR. CURRY: Let me confirm, but in all cases we really have, I think, 11.1 feet above the top of the fuel but let me confirm with Mr. Tanigawa.

CHAIR STETKAR: In other words, the reason I brought up this elevation if, for example, the top of the gray area was the bottom of that gate as if this is shown with the gates removed, the water level at that elevation, I think, is about 2.5 feet above the top of active fuel.

I don't know exactly where the top of active fuel is so it might be 2.75 feet or something like that. The key is it's not 12 feet. I just wanted to confirm that elevation because if I'm wrong, then some of the questions, follow-on questions, that I was going to ask are less significant.

MEMBER BROWN: The SER says 10 feet.

MR. CURRY: I think that's the minimum requirement.

MEMBER SHACK: That's the number I sort of had in my head.

CHAIR STETKAR: That's fine. That's minimum required water level for shielding and cooling.

MEMBER SHACK: Since there was a gate failure, the SFP will maintain 10 feet.

CHAIR STETKAR: I want to ask what the elevation of the bottom of the slot is.

MR. CURRY: Okay, Mr. Chairman. We have that slide of figure 9.1.4-2. Look on that figure. Unfortunately, we don't have it up on the screen here for everyone to see.

CHAIR STETKAR: The elevation of what it says weir is 47 feet 10 inches. The bottom of the spent fuel pool is 30 feet one inch. The height of a fuel assembly, if you look at the assembly that's in the grappling hook there, is about 15 feet roughly. If I add 15 feet to 30 feet, I come up to 45 feet which gives me about 2.5 feet. That's sort of what I was estimating but I didn't know if I was misinterpreting something on this drawing.

MR. CURRY: Your real concern is if we

had a failure of that gate, we'd only have two feet above.

CHAIR STETKAR: Not a failure. My concern is if I have the dimension -- I want to make sure I have the dimensions correct first. Let me -- perhaps you can study the drawings and get back to keep the discussion going. Here's the genesis of my question.

I understand basic refueling operations. I understand fuel movements. I understand minimum pool water levels. I understand anti-siphon devices. I kind of understand all of those things. I also know that there can be failures that may occur. I'm not saying anything about the probability of those failures.

There can be failures that may occur while the weir gates are removed that could conceivably drain the spent fuel pool level down to the height of that weir wall, whatever that is. The questions that I had, if those -- have you looked at -- do you have any information about the time until boiling would occur if you were drained to that level and the time until fuel uncovery would start if drained to that level?

Because you've uncovered the cooling

water -- you know, the cooling system suction lines are much higher than that. Basically once you drain down to that level the only cooling you have available is through some alternate makeup supply and times to boil-off.

If you have information about starting from that level, the time to reach boiling and the time to uncover -- to start uncovery of the fuel, or more accurately the time to start damaging the fuel because just fuel uncovery in this configuration won't necessarily start damage. I'm interested in those times. It's a way to sense under kind of the most extreme conditions what kind of time margins we have available.

MR. CURRY: We do have information on the time to boil which given loss of all spent fuel pool cooling.

CHAIR STETKAR: But starting at the initial --

MR. CURRY: Right. But I don't have it starting at the level that you're talking about. I think what we need to do is follow up on your suggestion and let us take a look at this figure and make sure we can give you a good answer on the potential water level given the failure -- you're postulating a failure of this.

CHAIR STETKAR: It would require some drain-down condition. As I said, at the moment I don't want to enter into probabilities of these things happening. I'm just trying to get a sense of what the margins might be and what sort of times are available. Don't necessarily read anything more into this than simply trying to understand what those times and margins are.

MR. CURRY: From this particularly configuration that you're referring to?

CHAIR STETKAR: Level at the weir.

MR. CURRY: Right.

CHAIR STETKAR: Whatever the water volume is.

MR. CURRY: Okay.

CHAIR STETKAR: And as kind of a related question to that, we may get into a little bit more of the systems in the coming slides here but this is useful. Do you know whether the fuel transfer tube has a drain line from it? I couldn't find any detailed information.

I'll tell you, my experience is some of them do and some of them don't. It's kind of a design-specific issue. That's why I ask. Is there a drain line connection to the bottom of the transfer tube or is this simply a tube?

MR. CURRY: One moment. No, the fuel transfer canister. That's really your question.

CHAIR STETKAR: Well, the fuel transfer -- again, if you've got that 9.1.4-2 slide, I'm talking about the tube itself that goes through the wall between the transfer canal and the refueling cavity, the tube that the little car goes through.

As I said, some plant designs I've seen have a drain line in that transfer tube connection and many plants don't. It doesn't how on this 9.1.4-2 but that's not the purpose of this figure. The purpose of this figure is just to show the general configuration. I was curious about is there a drain line. I don't need the answer right now. If you don't have it, just take it.

The other questions that I had about possibly drain lines is are there drain lines from the three volumes that you show on the right-hand side of this figure, in particular a drain line from the transfer canal, a drain line from the cask -- the pit, and a drain line from the fuel inspection pit. I'm assuming that there are because you need to drain those somehow usually.

MR. CURRY: Okay. We'd like to confirm that answer.

CHAIR STETKAR: As long as -- when you go back I'm interested in are there drain lines, yes or no, and, if there are drain lines, how large are they in terms of just size.

MR. CURRY: Yes, sir. We'll look at it in more detail.

CHAIR STETKAR: That's fine. The purpose of these meetings is to raise questions, as many as we can get answered during the meeting. That's good for everyone. If we can't get them answered, you know, they're take-aways.

Thank you. Oh, one other question. Some of these questions are basic configuration questions that I had. This drawing -- just a simple question. I think I know the answer to this. I just want to confirm it. On Figure 9.1.3-1 of the DCD, it's the drawing -- it's essentially the DCD drawing of what you have on the screen here.

The containment spray RHR cooling line suction elevations on that drawing are shown lower than the spent fuel pit cooling suction lines at a lower elevation. I didn't know whether that's actually the case or whether it's just the way to show both suction lines on the same drawing if they are at the same elevation.

My question is are the containment spray RHR suction lines located at the same elevation as the spent fuel pit suction lines? I found a lot of information in the DCD about the elevation of the spent fuel pit suction lines. It may just be an artifact of the way that drawing was put together to show the two of them.

MR. CURRY: Mr. Kawata.

MR. KAWATA: Yes. This is Naoki Kawata. Section related to containment spray RHR pump is same as spent fuel pit suction lines.

CHAIR STETKAR: Thank you. That helps. Thank you. With that I think now I'm pretty happy. You can start talking about the cooling system.

MR. CURRY: Okay. Thank you. All right. I think we understand we need to do a little research and we'll get back to you on those issues that you cited.

I think now we want to go to 9.1.3 and perhaps -- just to confirm with the Committee, our Holtec folks, structural criticality, we are going to replace them at this table at the moment, if the Committee has no objection, and talk from a system level perspective. Mr. Kawata will join us at this table.

Okay. As we mentioned before, Mr. Kawata is the deputy manager, MHI Water Reactor Systems Engineering Section. Let us talk about the SFPCS, Spent Fuel Pit Cooling and Purification System. We've already taken a peek at the slide that we'll be referring to.

Two redundant cooling and purification trains. Fundamentally the system has a safety-related function and a non-safety-related function. Safety-related function is the cooling function. The non-safety-related function is the purification and cleanup function.

Each train includes a pump, heat exchanger, a plate-type heat exchanger, a filter, and a demineralizer. They can be powered from our Class 1E sources. Obviously the SFPCS removes heat generated by spent fuel assemblies and it purifies water for several sources including the RWSP and refueling water storage auxiliary tanks.

Again, we need to follow up on your question from earlier but the piping and dates are arranged so that a failure will not result in a level less than 11.1 feet above the top of the assembly. We do have a seismic makeup source from the RWSP and the emergency feed-water pits.

The emergency feed-water pit could be a gravity-feed source. The design capability of the system is that the trains in conjunction with two trains of the RHR we can maintain spent fuel pool temperature below 120 degrees even with a full core off-load.

CHAIR STETKAR: The seismic we qualified, the makeup is from the fuel and water storage pit. Right?

MR. CURRY: That is a seismically qualified source.

CHAIR STETKAR: And that's the only one. Right?

MR. CURRY: No. The emergency feedwater it is also a seismic one.

CHAIR STETKAR: The pit is qualified, the piping isn't. In an earthquake the pit may remain full of water. The pipe in between may be broken so it's hard to figure out how to get water from point A to point B.

MR. CURRY: Right.

CHAIR STETKAR: It's my understanding that the connecting pipe from the EFP, the emergency feedwater pit, to this connection that's shown up here is not seismically qualified. Is that correct?

MR. KAWATA: Yes, that is correct because SRP is second water source, the makeup water source. It is not seismic.

CHAIR STETKAR: I just want to make sure that I understood that -- I understand that the line that you show coming from the RWSP recirculation pump is fully qualified all the way, and that the other sources from -- although the EFW pit itself is a seismic structural -- structurally seismically qualified, the piping between those is not, as is not the demineralized water supply. I think there is an alternate even from the Fire Protection System you can pipe in somehow. You do have one seismically qualified from the RWSP.

MR. CURRY: Yes, sir.

CHAIR STETKAR: Fully qualified the whole length. Okay.

MR. CURRY: So you see the schematic here. I think one of the members mentioned earlier we were referring to Interim Rev. 4. What that really was is a response to RAIs so the schematic here shows the isolation of the non-safety portion which is indicated by the equipment classification from 3 to N.

This shows only a single valve but we replaced that in response to an RAI with double-valve isolation. On the supply side automatically closed valves, check valves.

CHAIR STETKAR: And they are automatically closed valves now?

MR. CURRY: Yes, sir.

CHAIR STETKAR: Yes, sir.

MR. CURRY: Low-low spent fuel pool level.

CHAIR STETKAR: Low-low spent fuel pool level. Okay. Is that true?

MR. CURRY: The spent fuel pit level, yes.

CHAIR STETKAR: Terminology. SFP is always spent fuel pool to me so you'll have to excuse me.

MR. CURRY: I understand.

CHAIR STETKAR: That's interesting because that still makes my question relevant. The spent fuel pit demineralizers, as is shown on this drawing, can be aligned for cleanup of the refueling water storage pit. The line is coming in at the top. You go through the demineralizer and go back out to the refueling water storage pit recirculation pump --

pumps, plural.

If you're aligned in a refueling water storage pit cleanup mode so that you have one or, in the principle, it could be both of the demineralizers aligned to the refueling water storage pit, and you have a break in this section of the system, the nonseismically-qualified section of the system, how do you isolate that break and prevent the refueling water storage pit from draining down into the fuel building?

MR. CURRY: One moment.

CHAIR STETKAR: When the valves are manual I was going to ask where the scuba tanks are but since they are automatic, I can ask other questions.

Jim, in the interest of time, I mean, you know, you guys can discuss this during the break or lunchtime.

MR. CURRY: Thank you, sir.

CHAIR STETKAR: We have, you know, at least all day today and probably until tomorrow to scheduled for the meeting. Even if you want to take some of these away and even discuss them this evening if we go into tomorrow, we can kind of cleanup loose ends that way.

MR. CURRY: Thank you, sir. We

appreciate it.

CHAIR STETKAR: I'm sure we'll have time. There is also the danger of trying to answer questions on the fly sometimes because you may not get the right information on the record. Since everything is on the record, it's good to have the information correct.

MR. CURRY: Yes, sir.

CHAIR STETKAR: As you're thinking about that in terms of to kind of follow along just so you have the entire notion of what the question was going to be, the question is how will it be isolated if you're taking credit for manual isolation somehow, it's important to understand where those valves are located.

For example, if you do get flooding in a compartment and the valves are under water, it's pretty difficult for somebody to operate those valves manually. Even if they're automatic isolation valves, if they are in the flooded compartment, they may not operate. I would like to know physically where those valves are.

If they are in the same compartment with the nonqualified piping that could be broken, they may be submerged in a flood which could make it fairly difficult to isolate under either condition.

I mean, whether it's spent fuel pit or the RWSP. Also to kind of follow that line, if you had some estimate from at least operating experience, is this configuration similar to plants that are currently operating in Japan in terms of the spent fuel pit cooling and cleanup and connection to an RWSP?

MR. KAWATA: It is similar.

CHAIR STETKAR: It is similar? Okay. If you had some information about how frequently the spent fuel pit demineralizers are aligned for cleaning the RWSP, I mean, is it something that's done two days every month or is it only done during preparations for refueling?

That type of information would also help in terms of understanding if you are vulnerable to a break in this location that could be connected to the RWSP what fraction of the year, at least from actual operating experience. That I'm sure you won't be able to have in terms of time for this meeting. Those were all sort of subsidiary questions to the first issue.

Thank you.

MR. CURRY: All right. Well, I think basically we've kind of summarized the system just to --

MEMBER BROWN: If you're done, I'm not quite finished yet, I guess. You did address instrumentation when you talked about this. Looking at the DCD and then the SER as well, I didn't find any real definition but it appeared that there was no definition of how many level and/or temperature sensors you have installed in the spent fuel pool.

The drawing you reflect, if you take the one out of the DCD, gave the impression that there were two level sensors but only one temperature sensor. There's only one little stalk in there. There's two things off of it but I don't know what -- I don't know the convention for that particular symbol as to how many they are.

The second question associated with that relative to temperature is if you've only got one and it's only in one place, how do you know that's representative of the overall bulk temperature in the spent fuel pool? I often try to look at the flow rates and I couldn't tell what the flow rates were. There were numbers like 200 or 300 GPM and then I saw the pumps were for 3,000 GPM or some large number like that.

I'm an electrical guy so I couldn't relate to what the actual requirements were.

Obviously if there's some flow, but I don't know what that is to maintain a reasonable uniform temperature throughout the spent fuel pool.

The question that falls from that is if you lose power and you don't have any flow, how do you know you don't have one part of the pool since the fuel is not all uniformly hot? Some of it is older than newer spent fuel. How do you know you're not hotter in some locations you could be damaging than you have in another?

MR. CURRY: Let's start with the instrumentation piece of that, the leveling temperature indication.

MR. KAWATA: No, we have two temperature gauge.

MEMBER BROWN: You have two temperatures and two levels. Is there an RAI? I don't have the number for that. I didn't find it. I presume you all could tell me what the RAI is looking at that where they changed their design for that. I don't want it right now. It's just a matter of --

MR. HAMZEHEE: When the staff gets here we'll try to get you the RAI number for that.

MEMBER BROWN: Then we can look at it and see what it is. Also, the location relative to the overall one end of the pool vice the other. Then maybe if somehow you can address if there was no power.

Has somebody done an analysis that natural circulation is going to maintain a temperature of uniformity or are you going to have a big disparity from one point to another? Again, if it's not quick, I don't want to drag us. This is just a question that does not have to be answered right now.

MR. CURRY: Okay. We can look that up then.

MEMBER BROWN: I don't want to drag the meeting out while everybody looks the thing up.

MR. CURRY: We'll see what we can do.

MEMBER BROWN: The second question -- another question associated with that. What are the types? Are they continuous measurements for temperature or are they just a high and a low single-point measurements to say, "Hey, look. I'm too high," and, therefore, I tell somebody I got an alarm, or do I have a continuous readout on it? The same thing goes for the level.

Are they continuous or just a pressure switch type of arrangement which just says it's too low because I don't have a certain pressure? That's the second part to go along with that. That can be answered, again, at the same time that you answer the other one. Thank you.

MR. KAWATA: I understand.

MR. CURRY: All right. We would -- if there are no other questions --

CHAIR STETKAR: Yeah, there are. You'll learn. Related to -- the reason I wanted you to keep the drawing up there is I had a couple of other questions about the system and go back to the makeup. There are statements in the DCD about the seismically qualified makeup from the refueling water storage pit recirculation pumps. That is the qualified makeup supply.

Are the -- I couldn't find much information about the RWSP recirculation pumps in the DCD. There is a drawing that shows the configuration of the piping and so forth and there's a discussion of the containment isolation valves for them and things like that.

In particular, I went through the electrical load list in Chapter 8 and I couldn't find the power supplies for those pumps. Are they powered from Class 1E electrical buses or are they non-Class 1E power supplies?

MR. KAWATA: Yes.

CHAIR STETKAR: They are? Do you know what buses they are supplied from? I couldn't find them.

MR. KAWATA: The table shows --

CHAIR STETKAR: If it's in the DCD, just point me to the place in the DCD. I probably missed it.

Just identify yourself for the record.

MR. KAWANAGO: Shinji Kawanago from MNES. Basically that's in the pump and the power supply from the Class 1E load center. It's a roll bore gauge. It's a full load center so you cannot find --

CHAIR STETKAR: Oh, it's from an MCC down below the load center? Okay. Because I looked at the load centers and I couldn't find them. Thank you. Thank you. That answers basically that question. In the interest of keeping us going, I have pages of things here but I'm a slow reader and I think I got most of the information I wanted. I'll stop holding you up.

MR. CURRY: No problem.

All right. We would propose moving to light load handling system.

CHAIR STETKAR: Oh, I did -- I'm sorry.

I'm trying to look ahead in your slides to see what the topics are and get my babbling into the process at the appropriate time. Since you're going to the light load handling system, I wanted to kind of get the questions that I had about not only the cooling system configuration but some of the cooling system success criteria. This is just a question. As I understand it, your refueling is that basically it's a two-year fuel cycle and you replace about half the core. Is that right?

MR. CURRY: About 130.

CHAIR STETKAR: One third?

MR. CURRY: 130.

CHAIR STETKAR: Oh, yeah, 130 elements. There are statements in the DCD about heat loads related to normal -- either a normal refueling or a full core off-load. I understand that the cooling system capacity is based on full 10-year complement of spent fuel in the pool with a full core off-load so I'm not questioning that.

I was just curious is it normal practice in similar plants in Japan when you do a refueling to full off-load the core? Many plants in the U.S. do that. They do a full core off-load. It's just a lot easier.

It gives you more flexibility during the outage because there's no full in the core and it's a lot easier to move the fuel back in. I was curious whether that's a similar practice in Japan when you do a refueling. Do you do a full core off-load and then reload the core, or do you only off-load the 130 elements and do a fuel shuffle?

MR. KAWATA: In Japan usually a full core off-load.

CHAIR STETKAR: Okay. So essentially in a normal refueling outage we'll have the full core in the spent fuel pool for some number of days during that outage so the full core off-load is actually the normal refueling outage. That's basically what I wanted to get on the record. Thank you.

MR. CURRY: I'm slower and slower to turn the slides.

CHAIR STETKAR: This is an ACRS Subcommittee. Often times we spend a lot of time with just blank screens in front of us.

MR. CURRY: 9.1.4 Light Load Handling System. Basically there are two cranes involved in this system, two hoists; the refueling machine and spent fuel handling machine. They are shown on these -- on your following schematic.

The only safety-related function is really the isolation of the fuel transfer tube for containment purposes. The permanent cavity seal is used to retain water in the refueling cavity during refueling. The system is designed to meet the referenced ANSI/ANS standard. As we talked about, subcriticality is maintained even if the pool was flooded with unborated water.

We would go to Heavy Load Handling System.

CHAIR STETKAR: Okay. I was reading my notes. Can you go back to Slide 20?

MR. CURRY: Slide 20?

CHAIR STETKAR: Yeah. Maybe you can help me out. The DCD discusses -- this is the rapid cavity seal. The DCD discusses a leakage detection system for the cavity seal but I got -- there was not a drawing or a very clear discussion of that leakage detection system.

In some places I got the impression that the leakage detection system was actually just monitoring of level in the refueling cavity. I don't know whether this drawing shows it or not. Is there a separate leakage detection system that collects leakage through the deal?

MR. CURRY: Directly under the seal?

CHAIR STETKAR: Yes, directly under the seal. If there is, where is it?

MR. CURRY: I think if we could blow up this slide --

CHAIR STETKAR: We can see it pretty well.

MR. CURRY: Mr. Tanigawa-san, just to confirm, leakage detection system underneath the permanent cavity seal. Correct? Yes, there is.

CHAIR STETKAR: There is? Okay. Is it just a set of channels? I don't care too much about the design but there is a separate under the seal some sort of collection system that you can monitor for level or flow?

MR. CURRY: Through the ceiling.

CHAIR STETKAR: Leakage through the ceiling. That's good. That's basically what I was trying to confirm. In some of the discussion I kind of got the incorrect impression that -- there was discussions about level in the spent fuel pit is monitored and alarmed in the control.

The refueling cavity is monitored and alarmed in the control room and the operators will have time to align makeup which is all true, but it's not the same as a leakage detection system. Thank you. Go to Heavy Load.

MR. CURRY: Okay. The Overhead Heavy Load Handling System. Fundamentally, again, two cranes, the Polar Crane and the Spent Fuel Cask Handling Crane fall under this scope. These cranes are non-safety related seismic II, single-failure-proof consistent with NUREG-0554 requirements. Of course, we have limitations on the crane movements.

CHAIR STETKAR: Can you go back to where you show the plan view of the fuel building. You have a couple of slides that show that. There. The cask -- the spent fuel cask, whatever it's called -- crane. I'll call it crane -- can operate over the right-hand side of this figure. There are some drawings in the DCD that are pretty good that show normal routes of that crane.

My question was can it physically move over the spent fuel pit? I understand that it's not normally required to do that but, for example, do the crane rails for that crane extend to the left of the center line of the transfer canal over the spent fuel pit? Is it physically possible to move that crane over -- be careful of the paper with the --

MR. TANIGAWA: I'm sorry.

CHAIR STETKAR: -- over the spent fuel pit or is it physically limited to only the right-hand side of this drawing?

MR. TANIGAWA: Spent fuel cannot extend over the spent fuel pit physically and operate.

CHAIR STETKAR: That's all that matters. Thank you.

I'll ask the staff about the other one. Okay. Thank you.

MR. CURRY: I think that is fundamentally what we had to say about the Overhead Heavy Load Handling System. We have one open item which we're working on with the staff.

CHAIR STETKAR: Let me -- you'll have to excuse me. I have paper all over the place and I'm trying to read my notes. The spent fuel cask handling crane there is a discussion in the DCD that specifically notes that the polar crane in the containment has seismic restraints that prevent the crane from coming off the rails.

In other words, there are seismic restraints that prevent the crane from tipping and sliding off the rails. There was no mention of a similar seismic restraint on the spent fuel cask crane. I was curious whether that crane has a similar restraint to prevent lateral motion of the crane or tipping and sliding off the rails.

I didn't have drawings of that crane so I didn't know how it's configured. I don't even know what the rails look like. Since it wasn't mentioned and it was mentioned for the polar crane, I was curious whether it exist.

MR. CURRY: Well, it is seismic II but let us look.

CHAIR STETKAR: Even though it's seismic II, it's kind of an additional confidence about lateral motion and things like that.

MR. CURRY: One moment.

CHAIR STETKAR: Okay.

MR. CURRY: We would like to take that as an item and --

CHAIR STETKAR: That's fine. Understand fully.

MR. CURRY: I think that's all we have, sir, on 9.1, in this case, the Overhead Load Handling System. That concludes our presentation on 9.1.j

CHAIR STETKAR: Do any of the members have any questions about -- any further questions about spent fuel pit? Heavy load, light load handling? I think we're scheduled to have a break at

10:00 but I don't want to -- you look concerned.

MEMBER BLEY: Well, I've been hanging on one thing since the beginning with the heavy boron concentration in the water. I know we don't have emergency procedures or SAMGs as yet but what I've been thinking about is -- I looked through the PRA and the PRA dismisses everything about the spent fuel pool for reasons stated.

If there should be something in an external event that manages to somehow drain the water lower than the design would let it drain, what capabilities for refilling it and maintaining boron exist? If you didn't maintain the boron, is there any analysis of what would happen anywhere in the DCD? I looked all over it and I couldn't find anything.

CHAIR STETKAR: We'll let them answer.

MEMBER BLEY: It looked like you were waving your arms.

CHAIR STETKAR: No, I thought I found something but I thought it's probably better for them to --

MR. KAWATA: We can provide additional boron water.

CHAIR STETKAR: Well, I think the question is, you know, back to the criticality stuff can you achieve criticality? What's the boron level in the spent fuel pit that's required to prevent criticality? Right, Dennis?

MEMBER BLEY: That's right. The kind of thing I'm worried about it's certainly beyond the design basis of that. We need to look harder and harder at those.

CHAIR STETKAR: If you couldn't get criticality with pure water in there with no boron, that --

MEMBER BLEY: My question would certainly go away.

MR. KAWATA: For normal fuel storage there is no boron present.

MEMBER BLEY: I'm sorry?

MR. KAWATA: For normal fuel storage there is no boron present.

MEMBER BLEY: Normally you would need no boron?

MR. KAWATA: That's right.

MEMBER BLEY: Why is it there?

MR. KAWATA: Can you explain why we don't need boron?

MR. CURRY: And we have Mr. Brickner.

MR. BRICKNER: This is Bret Brickner with

Holtec. We don't take credit for the soluble boron to maintain criticality under normal conditions. We do credit some partial soluble boron for the accident condition.

MEMBER BLEY: And that accident condition is?

MR. BRICKNER: Is a misplaced fuel assembly outside the storage rack.

MEMBER BLEY: Ah, okay. So assuming that isn't the case, and even in a severe case dumping pure water in is fine?

MR. BRICKNER: That's correct.

MEMBER BLEY: That makes me happier. Thank you.

MR. BRICKNER: That's good.

CHAIR STETKAR: I thought I read that.

MEMBER BLEY: I was looking all over for it and I hadn't found it.

CHAIR STETKAR: Any other questions on fuel flow, fuel storage, anything?

Let's take a break because I don't want to interrupt -- we're going to start talking about cooling water systems and I don't want to stop us mid-stream in that. I think what we'll do is we'll take a break until 10:05.

(Whereupon, at 9:50 a.m. off the record until 10:07 a.m.)

CHAIR STETKAR: We're back in session.

MEMBER ABDEL-KHALIK: Mr. Chairman, before we move to the next section, just one question. What dictates the 4,000 bpm concentration of boron?

MR. CURRY: One moment. I think we want to know the basis for the 4,000 BPM boron in the spent fuel pit.

MR. NISHIO: The concentration of the SFP is the same as the RWSP.

MEMBER ABDEL-KHALIK: Right.

MR. NISHIO: It doesn't state it is a concentration of the RWSP from the safety analysis based on the MSLB.

MEMBER ABDEL-KHALIK: Steamline break?

MR. NISHIO: Steamline break. We will check on that. Based on the safety analysis we defined the most critical, the highest requirement of boron concentration of RWSP.

MEMBER ABDEL-KHALIK: So I guess we'll get that when we talk about Chapter 15?

CHAIR STETKAR: Chapter 15, I think, is coming up in June if I remember correctly, so we'll be sure to try to understand that when we hear that result.

MEMBER ABDEL-KHALIK: Thank you.

MR. CURRY: All right, 9.2. We have some additional folks that will be participating in this discussion. Marc Hotchkiss is representing MNES/MHI. His specialty is chilled water and ventilation systems. Junya Hattori-san. Mr. Hattori is the deputy manager, MHI Turbine Plant Engineering Section. Mr. Kawata-san you already met.

Motohisa Kitamori-san, please join us.

Mr. Kitamori is an engineer, Water Reactor Systems, Engineering Section. Keita Otani. Mr. Otani is an engineer in the Plant Layout Engineering Section, HVAC System and Fire Protection. We'll be calling on these gentlemen as we need for each of the systems covered here.

First few slides are acronyms. The water systems 9.2.1, 9.2.5, 9.2.7, 9.2.2. Essential Service Water System, 9.2.1; Component Cooling Water System 9.2.2; 9.2.5 Ultimate Heat Sink; and 9.2.7 Chilled Water System have safety-related implications. The other systems do not.

Essential Service Water System, as I mentioned, is a safety-related system. It transfer heat from the safety-related loads to the ultimate heat sink. It's obviously designed to mitigate the consequences of a design basis event and for safe shutdown, assuming a single failure and one train unavailable due to maintenance.

The Essential Service Water System is interlocked with the Component Cooling Water System on a train-by-train basis. The system consist of four 50-percent-capacity Essential Service Water pumps divided into four independent trains. In each line there are two 100-percent-capacity strainers.

The system consistent with Reg. Guide 1.189 provides backup to the fire service system. Again, you have a simplified schematic showing the design. Part of the design of the Essential Service Water System is plant specific. A good part of the design is a conceptual design.

As I indicated, there are four. You see the A, essential service water pump. There are four of those pumps. You also see the two 100-percent-capacity strainers in each line. The safety-related loads are the component cooling water heat exchanger, plate-type heat exchanger in the essential chiller unit. The heavy black line is standard plant design.

CHAIR STETKAR: Before you move from this slide, I found a statement in the DCD in Section

9.2.1.2.2.6. The statement says, "To avoid concerns with potential downstream pipe wall thinning, butterfly valves provided in the ESWS piping are not used for excessive throttling of the water flow.

The valves are sized such they are near the full open position during various modes of plant operation. Orifices having adequate differential pressures are installed downstream of the heat exchangers to prevent excess throttling of the butterfly flow control valves." What particular valves in this system are actually butterfly valves?

MR. CURRY: One moment.

CHAIR STETKAR: Only because I couldn't find something that I would normally consider a flow control valve. I saw a lot of locked-open manual valves and I got confused. I'm always interested in butterfly valves.

MEMBER BLEY: Just a quirk?

CHAIR STETKAR: Just a quirk.

MR. KAWATA: Okay. There are several.

CHAIR STETKAR: They may not show on this simply drawing but, if they do, I would appreciate it.

MR. KAWATA: For the standard design butterfly valves.

CHAIR STETKAR: They are all butterfly?

MR. KAWATA: Yes. The reason is the butterfly valve is for isolation valve for flow control.

CHAIR STETKAR: So if I look at -- let me make sure I understand. If I look at Figure 9.2.1-1 in the DCD, the actual flow diagram, and I look around the heat exchangers, there are valves that are shown around the heat exchangers as locked-open manual valves. Those are butterfly valves?

MR. KAWATA: Yes.

CHAIR STETKAR: Okay. Okay. I have to ask. Why do you use butterfly valves as isolation valves? Why not -- since they are locked open. Are they locked in a throttled position or are they locked fully open?

MR. KAWATA: Usually ESWS has piping over 24 inches. We use other types such as groves or gate. It would really be difficult to procure the bar.

CHAIR STETKAR: Okay. It's just because of the size of the piping it's a lot easier to find -- it's true it's a lot easier to find a large butterfly valve. Okay. Okay. Thank you. Thank you. I understand.

MR. CURRY: All right. Next system, Component Cooling Water System.

CHAIR STETKAR: One kind of strange question that I have. This is not particularly related -- well, I'll wait until we get to the ultimate heat sink. I'll wait until then. Sorry.

MR. CURRY: No problem, sir. Again, you may want to refer to the simplified P&ID.

The Component Cooling Water System is a closed, intermediate system between the essential service water system. It's cooled by the essential service water system. The system has a safety-related portion and also has non-safety-related portions of the system, non-essential loads. The non-essential portions are isolated automatically with redundant valving. I will point that out in a moment.

The Component Cooling Water System consist of 200 percent cooling subsystems. On this chart each of these two main sections is a subsystem served by one surge tank separated by a partition in the middle to divide the surge tank up.

Each subsystem consist of two 50-percent-capacity trains, each train containing a pump and a heat exchanger. Once again, the question came up about Interim with the Rev. 4. That was what we had submitted to the staff in terms of our DCD markups in response to RAI questions.

If we were to look at this drawing, you will see this double-valve isolation for the non-safety portions. That was a result, for example, of an RAI response and a change. That would be the summary. I don't know if there are any particular questions on that system.

CHAIR STETKAR: I have several questions so you'll just have to bear with me. Just keep the drawing up here so that we can use it as a reference. The valves -- the valves that connect the two trains to the common header so, Jim, on your -- those motor-operated valves there, the 20 valves and the seven valves, in Rev. 3 those valves received automatic isolation signals.

They do not receive -- you've added the isolation signal valves for the A2 and C2 headers that you pointed out, those air-operated valves, and you removed all of the isolation signals from those motor-operated valves that you're showing there. Is that correct?

MR. CURRY: That is correct.

CHAIR STETKAR: Okay. And it's noted in the DCD that says, "In the event of an accident the header tie-line valves, those motor-operated valves, are closed by operator action from the main control room to achieve independence between trains."

Essentially you're taking credit for a manual action to replace a previously automated isolation function. My question was I'm always concerned about placing more burden on operators based on design consideration. Why were the automatic isolation signals removed from those valves?

MR. CURRY: The basic reason is that it would isolate the thermal barriers. There is an SRP requirement which the staff pointed out in an RAI. We removed the automatic closure of the 20 and seven valves, the header tie-line valves that you're referring to that we would not automatically isolate the thermal barriers.

CHAIR STETKAR: That's basically in response to a question by the staff and we'll ask about that later. Given the fact that they are now manually operated from the main control room, and it says in the DCD that they are closed when an operator determines train separation is required, what conditions require the operators to close those valves?

I'm trying to understand now that the operators are faced with a requirement to close these valves under some conditions. I knew the conditions before because I knew what the isolation signals were. What conditions now would require the operators to close those valves? I mean, the word accident is used but I don't know what that means. Have you --

MR. CURRY: No particular accident requirement. It's just to achieve train separation and independence between trains.

CHAIR STETKAR: Does that mean if I'm an operator in the control room, every time I have an ECCS actuation, I must immediately go and close those valves to achieve train separation? I mean, is that something that's going to be in my emergency procedures because that's an accident?

MR. CURRY: There is some guidance. I mean, that will achieve train separation. There is some guidance on the timing in which that should be performed in order to achieve train separation.

CHAIR STETKAR: What's that guidance?

MR. CURRY: It's a SECY paper and I don't have --

CHAIR STETKAR: I don't care about SECY papers. I care about real plants and real designs.

MR. CURRY: But in order to achieve, you know, guidance, train separation even to account for a passive failure in a component, the SECY paper gives us some guidance, some timeline for the operator action.

CHAIR STETKAR: That's fine. What I'm hearing is the staff had better be prepared to answer my questions for this particular design what types of accidents and what types of guidance will be included in the emergency operating procedures for operator actions to close those valves. I hope the staff will be ready for that when we come to this system because I'm going to ask about that.

MR. HAMZEHEE: Yes, sir.

CHAIR STETKAR: And --

MEMBER ABDEL-KHALIK: What if these valves are automatically isolated or manually isolated? Wouldn't you have the same concern about the thermal barriers?

MR. CURRY: The -- right. The automatic isolation is just to separate the trains. We initially, I think, closed all those valves so that we wouldn't and so we would -- we were interrupting flow to the RCP thermal barrier.

MEMBER ABDEL-KHALIK: Okay.

CHAIR STETKAR: Let me make a quick note here. Now, if I now follow on this drawing header A1, there are -- the motor-operated valves that we just talked about, let's say on the supply line, there are motor-operated valves at the -- if I follow it down, two motor-operated valves at the outboard side of the containment penetration and then motor-operated valves in the return line. None of those valves have any automatic isolation signals. Is that correct?

MR. CURRY: That would be correct.

CHAIR STETKAR: There were formerly isolation signals for the containment isolation valves and they've been removed so the entire flow path now from train A and B through the A1 header back to the train A and B are all manually operated valves. Right?

MR. CURRY: That is correct. Let me confirm with Kawata-san but I believe the only automatic isolation we have in this system now is that one.

CHAIR STETKAR: That was my understanding trying to go through Interim Rev. 4. Now, I understand all of that piping is seismic Category I. Is that correct or not?

MR. CURRY: Well, not in the --

CHAIR STETKAR: No, no, no. In the A1 header.

MR. CURRY: Yes, sir.

CHAIR STETKAR: Okay. If I have a break in that header anywhere, though, without operator intervention I will disable both of the associated component cooling water trains. Right?

MR. CURRY: Just to be clear, a break in the safety-related portion?

CHAIR STETKAR: Yes. I mean, to emphasize it, you go down to the lower left-hand corner and break it where it says A1 header inside CV. In principle, anywhere in that common header I'll disable both of those component cooling water trains.

MR. CURRY: I should say we do have an RAI.

CHAIR STETKAR: I was going to ask. There is an RAI and an open item. Is the open item specifically addressing that issue because it wasn't clear. I was kind of bouncing back and forth from the SER. So it does address -- so there is --

MR. CURRY: That's the subject of that RAI.

CHAIR STETKAR: Right. That's the subject of this one.

MR. CURRY: 878-6200.

CHAIR STETKAR: Good. I just wanted to make sure that we're talking -- that I understood the subject of that RAI. The problem is we don't get all the RAIs, and I emphasize to the staff that we don't want them because if we ask for all of them, we'll get them and we already have 2,000 pages of things to read through. Good, thanks. We'll hear about that resolution once the open item is closed.

Let's see. I'm trying to see -- I'm looking at the DCD figures and trying to relate the valves to this drawing up here. If you -- there's discussions in the DCD about alignment of alternate cooling. For example, let's just take the A and B side of the drawing here.

If we're in a configuration with, let's say, B component cooling water pump out of service for maintenance so that A component cooling water pump is supplying all of the loads on the left-hand side here.

For some reason A component cooling water pump then fails, there are cross-tied possibilities you've outlined in that green dotted line that allow me to connect from the C&D loop so that I can maintain cooling for the A and B reactor coolant pumps.

I understand that. Those are also manually operated valves so the operators would need to open the two supply valves. Right? And open the two return valves and then close the return valve, the one in the upper left-hand corner of the green box, so that the water goes back to the C/D side and not to the A. You don't pump C/D water over to the A/B surge tanks. There's basically five valves that the operator has to reconfigure to establish that alternate cooling alignment.

In the DCD it talks about the fact that there's a 10-minute available time window to perform those actions after the loss of component cooling water based on overheating of the reactor coolant pump motors.

Is that the most limiting time limit? Because when you disable that cooling, you disable cooling to the motor coolers, the thermal barrier, which is not a big deal because you still have charging flow to the seals. And you disable cooling to the upper and lower bearing oil coolers for the motor upper bearing and the bottom bearing, the radial bearing between the motor and the pump.

Is the motor heating the most limiting time or -- that heats up first? You get into problems with the motor before you get into problems with the bearings? You have analyses that show that is actually your time window is 10 minutes?

MR. CURRY: One moment. Let me check on

the analysis. You are correct that in the DCD we talk about 10 minutes. Let us check on what the basis for the 10 minutes is.

CHAIR STETKAR: If you're going to do that, check also if there's an analysis to show what is the time. I'm interested in realistic times. I'm not interested in licensing type 10 minutes. I'm trying to understand what the real requirements on the operators might be. One question is what is the time to heat up the motor to unacceptable conditions, whatever those are.

The other question is what is the time to heat up the bearing oil system so that the bearing lubrication is affected and you might start to have vibration problems on the reactor coolant pumps? The concern here is if you start to have mechanical vibrations on the pumps, you can mechanically damage the pump seals, or you might be able to mechanically damage the pump seals depending on their clearances and exactly how they're designed.

Of course, if you have mechanical damage to the pump seals, we now have a LOCA condition. I'm interested in terms of the analyses to justify the time window for protection of the reactor coolant pump which is this motor protection issue. Actually, more importantly, what is the time window for protection of the pump seals, mechanical damage to the pump seals which is a bearing lubrication issue more than the motor itself.

MR. CURRY: There are a couple of issues. Seal cooling, as you pointed out, would continue to be provided by CVCS so we wouldn't operate indefinitely in this configuration because you've lost two trains so we would be in an LCO.

CHAIR STETKAR: But the LCO is like 72 hours or something like that. I suspect that the bearings might be into trouble before then. I think it's 72 hours. I'm not sure. I may be shooting from the hip but those are typical times for most of the tech specs, I think, on this plant. One train indefinitely and two trains for 72 hours.

MR. CURRY: Let us check. We will check. In any event, we wouldn't operate indefinitely. We still have seal injection in this --

CHAIR STETKAR: You do but the seal injection doesn't necessarily help you if you're getting mechanical vibrations on the shaft. That is the concern there. There are no automatic trips of the reactor coolant pumps. Is that correct? I think we asked that question once before. I seem to recall that there are not but I might not be remembering this correctly because we look at too many designs.

MR. CURRY: One moment.

MR. KAWATA: We have only one automatic trip from ECCS actuation.

CHAIR STETKAR: Oh, yeah. That's right. I remember that logic.

MR. KAWATA: We do not like to trip RCP because we make some --

CHAIR STETKAR: Right. Yeah. I remember that part of the logic. There is an ECCS. I can't remember the coincidence logic. I was thinking more in terms of normal -- I know there's over-current and under-voltage and the basic electrical trips but there are no protection trips for the reactor coolant pumps on high lube oil temperature or bearing vibration or motor high temperature or any of those types of trips that I remember. Anyway, if you've got -- the concerns are what are the real available time windows for those operator actions to open those cross ties.

MR. CURRY: Right. Just to rephrase your question, really it's the justification for the 10 minutes and the basis that we're not going to damage a pump if we are able to get cooling back over.

CHAIR STETKAR: That's right.

MR. CURRY: Okay.

CHAIR STETKAR: But, I mean, there are two. One is the 10 minutes, regardless of the basis, is based on motor cooling which is a motor protection issue. If I start to overheat the motor, I may not necessarily get mechanical damage, you know, to the mechanical vibration.

The 10 minute for motor protection, if it's 10 minutes, is protection of the pump itself so that the pump can stay running. The time window that we don't have any information about for overheating of the bearings is also a pump protection issue but, more specifically, it's a LOCA prevention issue. I don't know what that time is. It's probably longer than 10 minutes. If it's 11 minutes, it would be interesting.

Oh, and this is just confirmation. I think this answer is simple. The signals for I'll call them new, the air-operated isolation valves for the non-safety header, A2, C2, those, I saw a couple of different markups of Interim Rev. 4.

It's my understanding that those levels, those valves, are closed by low-low level in the respective surge tank, a containment spray or P signal, or an ECCS actuation S signal. Is that S signal interlocked with loss of off-site power or is it simply the S signal?

MR. KAWATA: S means simply ECCS actuation.

CHAIR STETKAR: Okay. Because I saw an interim markup. There used to be coincidence logic with an S and under-voltage and this is strictly ECCS. Okay. Good. I was hoping that was true so thank you.

Okay. This one is going to be difficult with this drawing but this is all we have. There is a fairly long discussion in the SER and the DCD regarding water hammer. Let me read something just to get it in context. In the SER -- I wasn't going to ask the staff about it, I will later, but I wanted to make sure I understood from the plant perspective what the concern and what the operation was.

In the SER, and I'll quote from the -- it's SER Section 9.2.2.4 under GDC-4 if you want to go find that section of the SER. It's quite a long quote but I need to kind of paraphrase everything.

It says, "Related to possible pressure transients on the plate type heat exchangers over-pressurizations, the typical operating practice when starting and stopping the CCW pumps is as follow: pump discharge valves, NCS, VLV-018A, B, C, D, are first closed.

The discharge valves are manually controlled by plant personnel at the valve location. Because of their large size, 24 inches, the rate of closure of a manual discharge valve is not so fast as to cause sudden increase i pressure or pressure differentials in the pump discharge piping. Thus, the potential for water hammer is minimized."

Then there's discussions about, you know, the fact the check valves close slowly as flow decreases. The valves in question are not shown on this drawing but, for the benefit of people who don't have the PNIDs pulled up in front of them, they are on the discharge side of the heat exchanger.

There is really no discharge valve for the pump. On this drawing they are between the heat exchanger outlet and the connection that goes either to the safety-related loads or the motor-operated valves for the cross ties.

Jim, if you could just put -- I know you're looking for the reference section. At this point put your -- just move up to the discharge side of the heat exchanger right there. That's where that valve is. Now, does this mean that every time I shut down a component cooling water pump, an operator has to physically go and slowly manually close that 24-

inch valve?

MR. CURRY: First thing, Nishio-san or Kawata-san can be very helpful with regard to Japanese experience, but there is no requirement to do that. I think we are talking about Japanese experience.

Mr. Nishio.

MR. NISHIO: On the Japanese plant, normally such a high -- when operator actuate or start high temperature pump, operator will open -- first he will close the valve and then start up the pump and gradually open the valve. This is not a requirement, just a practice of the Japanese plant.

CHAIR STETKAR: This is on pump start-up. When they start the pump manually, they first go close that valve and then start the pump and open it up kind of like you do on the service water pump.

MEMBER BLEY: So you don't over-current.

CHAIR STETKAR: Yeah, I understand that. But if these pumps are started automatically by a safety signal, those valves are open.

MR. NISHIO: This is not a requirement, just a practice.

CHAIR STETKAR: Okay. So the discussion -- I got confused because I thought that you were closing those valves to somehow throttle flow as you shut the pump down. Follow me? I was getting confused there. But that's the normal practice that they will be instructed when they start the pump manually to close the valve and then open it manually.

All right. The answer to that is yes. Thank you. I think -- let me read the questions that I have here for myself to make sure that -- the way it was written, I had somehow convinced myself that it was a pump shutdown evolution and that bothered me a little bit because it's kind of hard to close those valves under -- it's not good for the valves.

It's not good for the operators. I'll ask that staff that, too. Some of these things are more staff-oriented and I just have to show that I have it. I think I'm done with component cooling water. Thank you.

Anybody else, by the way? I don't necessarily want to dominate here. Please speak up.

Thanks.

MR. CURRY: Okay. The next section is non-safety-related system, the Potable and Sanitary Water. We hadn't planned to say much on this one but Mr. Kitamori is here if we have any detailed questions. This is a non-safety-related system. I think the key points are that the system uses check valves to prevent any radioactive contamination from interfacing with the system or any back-flow and then it has no connection to systems containing radioactive material.

CHAIR STETKAR: The DCD does mention that the source of the potable water is wells. Does that mean that any COL applicant who is going to implement the design will need to take an exception if they hook up to a normal city water system or some other supply?

MR. KITAMORI: Yes, for COL applicant we decide exception.

CHAIR STETKAR: Okay. I just wanted to make sure that was the case. A lot of plants don't have wells for these things. Most of them don't.

MR. CURRY: Okay. We will move on to 9.2.5 if there are no additional questions on 9.2.4. Ultimate heat sink is conceptual design information, although we have interface requirements. The ultimate heat sink is typical in that it dissipates heat from the ESWS.

We comply with the requirements of Reg. Guide 1.27 with regards to capacity. Seismic Category I structure and designed to withstand conditions defined in Chapter 2.

The ultimate heat sink consist of four

50-percent capacity mechanical draft cooling towers. Again, this is conceptual design information but this is what we have in the DCD. So four 50-percent capacity mechanical draft cooling towers, one associated with each ESWS train and three one-third capacity basins.

MEMBER BROWN: You said three 30-percent basins?

MR. CURRY: Thirty-three and a third. I could have said 30.

MEMBER BROWN: That's fine. You didn't.

CHAIR STETKAR: Jim, I came across -- it's in the DCD and it's in the SER. You missed it in other designs but there are statements that say essentially that the capacity of the ultimate heat sink should be sufficient for 30 days of cooling without makeup. This says, "Or a minimum of 36 days for cooling pond."

Why are there different requirements if I have something that I'll call an ultimate heat sink which might look like what's inside the dotted lines on this drawing? That has to have a 30-day capacity. Or if I have something that's called a cool pond that might look different but other people would call an ultimate heat sink, that has to be 36 days.

MR. CURRY: Mr. Chairman, that's from the Reg. Guide maybe. I'm not sure if anyone --

CHAIR STETKAR: I'll ask the staff then. That's fine. I was just curious whether you had any insights because it is stated in the DCD so, therefore, if I build my plant with a cooling bond, I have to make sure whatever I call a cooling -- I want to make sure we're not getting into semantics and that there's an actual technical basis for this because I've seen many people designate concrete ponds as an ultimate heat sink. It doesn't necessarily have to have cooling towers and look like what's in this dotted box here. I'll ask the staff about that. Thank you.

MEMBER BROWN: One -- just to pick on your diagram, you said three basins. Yet, your diagram say there's an A ultimate heat sink basin and little diagram on the left says to/from B, C and D which implies there are four heat sink basins. Which is it?

CHAIR STETKAR: I was a bit surprised you said three also because I thought I'd seen four. The conceptual drawing figure 9.2.5-1 in the DCD seems to show four.

MR. CURRY: Four 33 and a third percent

capacity basins. Right?

CHAIR STETKAR: I don't know what the capacities are. I'm just looking at a drawing.

MR. CURRY: Four 33 and a third. Thank you, sir.

CHAIR STETKAR: Ah, okay.

MR. CURRY: Right.

CHAIR STETKAR: Each has enough water in it for a third of the design basis. Ah, okay. Physically there are four separated basins. Okay. Thank you. One for Brown.

Anybody have anything more on the ultimate heat sink? Again, this is all going to be COL so we'll visit this in detail depending on whatever specific design the COL applicant proposes.

MR. CURRY: All right. Condensate Storage Facilities, also a non-safety-related system. Mr. Hattori-san is here to help us with that. Really three -- all non-safety related but three subsections; demin water, condensate storage and transfer, and primary makeup water system.

I think it's outlined here starting from the raw water supply. The demin water treatment plant is a COL item. Then the demin water storage tank provides makeup to the condensate storage tank, the two primary water tanks as well. Then off to turbine island users or nuclear island users.

CHAIR STETKAR: All four of those tanks, the two primary water makeup tanks, the CST and the demineralized water storage tank, are all outside in the yard. Is that correct?

MR. KITAMORI: Primary makeup tank is inside of the tank house.

CHAIR STETKAR: Tank house?

MR. KITAMORI: Yes. In that tank house we have the primary makeup water tank and RWST.

CHAIR STETKAR: Ah, okay. That primary water tank house is a separate building from obviously the reactor building and the auxiliary building?

MR. KITAMORI: Located outside of the reactor building.

CHAIR STETKAR: Okay. I guess -- uh, okay. I had a question here but I need to kind of rethink how to ask it. There is a statement that says the piping to and from -- this is in the DCD section on the condensate storage facilities. It's 9.2.6.2.6.

The statement says, "The piping to and from the primary makeup water tank is a single wall stainless piping designed to run above ground and penetrates the building wall directly into the tank.

This piping is mostly inside the auxiliary building in pipe chases. For piping between buildings, penetration sleeves are provided to collect and direct any leakages back into the building for further processing."

Since we are now talking about piping that goes between two different buildings, are the buildings next to one another or is there open space? I didn't look at the footprint of the plant layout to see where these buildings are, quite honestly, because I didn't have time.

MR. HATTORI: Hattori speaking. The condensate storage tank and the turbine building are separated.

CHAIR STETKAR: Yes. I'm talking in particular about the primary makeup water tanks. Where I'm going to is collection of radioactive leakages and how they are taken care of. There is quite a bit of discussion about condensate storage tank and demineralized water storage tank. Those are not likely to contain any radioactive fluids.

The primary makeup water tank may. It receives return flow from boric acid evaporators, at least, and other potentially radioactive users. We don't necessarily know that the primary makeup water tank is by definition clean water the same way as the demineralized water tank or the condensate storage tank.

So because this is non-safety related equipment with regard to collection and control of potentially radioactive fluid releases to the outside environment is why I'm asking about these piping sections because that's where this whole discussion evolved from the SER.

What I would like to understand is how that piping from -- between the primary water makeup building and whatever other buildings those pipes go into whether that's double-wall piping, whether it's single-wall piping, and what provisions there are for collection of potential leakage from that piping.

There are some discussions about -- it says there are sleeves from buildings that collect water and put it back into places where it goes into a radioactive sump. I'm not sure how that works in this particular configuration.

MR. NISHIO: Hiroki Nishio. Sometimes in the primary makeup water is located next to that auxiliary building.

CHAIR STETKAR: Oh, okay.

MR. NISHIO: The sleeve is a double pipe.

CHAIR STETKAR: Thank you. Good enough. Thanks.

MR. CURRY: So if there are no questions, may I proceed to 9.2.7?

CHAIR STETKAR: Any other questions?

MR. CURRY: 9.2.7. Chilled Water System. Mr. Hotchkiss is also our system expert on that. Basically the definition includes essential chilled water and non-essential chilled water. You see the loads that the chilled water system and we'll talk about non-essential chilled water systems shortly.

You see the chilled water system loads listed up there and also in the following slide, if you wish to look at it. The system, again, is for 50-percent capacity chiller units in four trains. I think those are the key points of that system.

CHAIR STETKAR: Couple questions on essential chilled water. This is beyond design basis accident but it's addressed in the DCD so it's fair game. In Interim Rev. 4, Section 9.2.7.2.1 it says that during loss of off-site power each of the essential chilled water systems is powered from respective safety emergency power source.

The essential filler units stop for one hour after a station blackout occurs until the alternate ac gas turbine generator restores power. We've reviewed Chapter 8 so we are familiar with the alternate ac gas turbines and how they're configured.

My question was I understand the licensing connotation of the one hour to restore power from the alternate ac gas turbine. Fortunately the ACRS doesn't necessarily have to think in those licensing terms. We like to understand how the plants work.

The question I had, the essential chilled water system cools several loads and I have questions about a couple loads later. One of the loads it cools are the air-handling units for the turbine-driven emergency feedwater pumps rooms. Those are trains A and D of the emergency feedwater system.

I was curious, and I would like to know, if I stop ventilation cooling for those rooms for one hour, what would be the temperature in that room at the end of that one-hour period? That's a room heat-up calc. The second part of that question is what is the most limiting qualification temperature for any of the components in that room?

In particular I'd be concerned about possible electronic governors for the turbine or any instrumentation. Or if you have any digital processing local units in there for instrumentation for control signals, what are their design qualification temperatures? The question is, you know, do we exceed those temperatures under this nominal one-hour period?

MR. CURRY: I think we got a similar question from the Chapter 8 Subcommittee.

CHAIR STETKAR: Yeah. Unfortunately I didn't have time to go back and see that. It sounded familiar but I thought I'd ask it again here. If you did go back and look it up, I don't recall getting an answer on that. I'm not sure.

MR. CURRY: Well, actually, I think it's going to be the subject of an audit but we do have a room heat-up calculation.

CHAIR STETKAR: Okay.

MR. CURRY: And I believe, Kevin Lynn, you may be able to help us out but I think it's going to be the subject of an audit with the staff. Do you have a scheduled date on that?

MR. LYNN: Yes, this is Kevin Lynn, MNES. There is going to be an audit under Chapter 8 for an RAI that is related to the turbine-driven EFW pump and room heat-up calculation. MHI is currently preparing the calculation results and we've gotten some feedback from the staff on what specific items they want to see.

We are revising the calculation to make sure we address each of those items with the date of being able to complete that by the end of March and then the audit would most likely be sometime in April but it's not officially scheduled at this time.

CHAIR STETKAR: Okay. That's good. As long as I know the staff is tracking it. I apologize, I didn't have time. I thought it sounded familiar with we look at so many different plants and I tend to ask similar questions for each plant and I get lost. I apologize for the repetition.

MR. CURRY: No apology necessary.

CHAIR STETKAR: There is a table in the DCD and it's Table 9.2.7-2 that lists -- what it does is it lists the flow rates and heat loads under normal and abnormal operation for the essential chill water system. I think I understand most of this but I had a question that the -- this is probably just because I'm not familiar enough with the plant.

The heat load for the A and D (dog) emergency feedwater pump area air-handling units, those are the turbine-driven emergency feedwater pump rooms, are 62,000 BTUs per hour. I understand there is heat load during normal operation because you have a steamline in that room, but the same heat load applies under abnormal operation when we actually have steam flowing through the turbine and we're heating up all of the turbine components and things.

Is that correct? Am I misunderstanding the sources of that heat load? The question is why are they the same during normal and abnormal operation? I understand why there's normally a heat load there of some amount.

MR. CURRY: And just to confirm, we're talking about 60, right?

CHAIR STETKAR: Mine says 62 because I'm looking at Interim Rev. 4 of the DCD.

MR. CURRY: Okay. Fine.

CHAIR STETKAR: I was politely instructed to look at that and not at Rev. 3. In Rev. 4 the 60 is crossed out and a new value of 62 is inserted.

MR. CURRY: Thank you, sir. We're on the same page.

CHAIR STETKAR: But it is 62 under both normal and abnormal. My basic question is why are they the same. Why isn't -- I don't know what basis went into determining that 62,000 BTUs per hour.

MR. KITAMORI: This is Kitamori speaking.

Heat load in the worst-case condition so actually during normal operation if different heat load abnormal condition. But to determine chill water unit capacity, we considered the worst condition achievable.

CHAIR STETKAR: So are you saying -- so I understand, does that mean that the 62,000 is the actual heat load when the turbine-driven pump is operating under whatever assumptions you made about, you know, conductive heat removal or whatever, so that during normal operation the real heat load would be less than 62?

MR. KITAMORI: Yes.

CHAIR STETKAR: Okay. Thanks. I understand that.

MEMBER ABDEL-KHALIK: Is that right? So if you have the chilled water system operating versus the case of a station blackout, you expect the heat load in the room to be smaller?

MR. HOTCHKISS: This is Marc Hotchkiss. I think what we're saying is we just assumed that this accident heat load for normal and accident conditions decides the chiller. In effect, under a normal condition, the heat load may be smaller. It probably would be smaller if we were not operating the emergency feedwater pump.

MEMBER ABDEL-KHALIK: Right.

MR. HOTCHKISS: But assume that under normal conditions decides the chiller so there's excess capacity essentially.

MEMBER ABDEL-KHALIK: No, but the question is if the pumps are operating and the chiller is operating, what is the heat load? That is the maximum heat load.

MR. HOTCHKISS: The pump -- the steam-driven emergency feedwater pump is the source of the heat load.

MEMBER ABDEL-KHALIK: Correct. But if the chiller is operating, that means the temperature in the room is at its lowest value which means heat losses from the system are at their highest value so that gives you the highest heat load on which you base the sizing of the system. The question is is that the same heat load you're assuming during the station blackout when the chiller is not operating?

MR. HOTCHKISS: The chiller operates on a station blackout after one hour after ac gas turbine generator starts.

MEMBER ABDEL-KHALIK: No, during that room heat-up period.

MR. HOTCHKISS: Well, there is no heat removal taking place during that one hour because the chiller's not operating if I'm understanding your question. After an hour we load the chiller back onto the electrical bus, start the chiller again and start cooling the room back down to an equilibrium value. These are equilibrium head load values accident conditions.

MEMBER ABDEL-KHALIK: Maybe I should ask the question, the 62,000 BTU per hour heat load calculation, what room temperature is assumed in that calculation?

MR. HOTCHKISS: It assumes to be the normal temperature range which for that room is 50 to 105 degrees. We would take the worst-case temperature condition to maximize the heat load and make sure --

MEMBER ABDEL-KHALIK: Which is the lowest temperature?

MR. HOTCHKISS: Yes.

MEMBER ABDEL-KHALIK: All right.

CHAIR STETKAR: One other question I had on that same table, if you have it in front of you. The motor-driven emergency feedwater pump areas, which are B and C, do not show the heat load during normal operation which I understand because they are motor-driven pumps.

During abnormal operation those areas showed heat load of 110,000 BTUs per hour which is not quite but almost twice the heat load in the turbine-driven emergency feedwater pump room. I was curious why the emergency feedwater pump rooms have a much higher heat load than the turbine-driven emergency feedwater pump rooms.

I've been around motors and turbines and it strikes me that rooms that have turbines in them are usually a lot warmer, unless the motor-winding resistance of these motors is really high. You may want to go back and check that if you don't have a quick answer. My problem is I have no absolute feel for any of these heat loads so the only thing I can do is look at relative values.

MR. CURRY: We'll take that as an item.

CHAIR STETKAR: I mean, I don't understand the reasons for that relative difference.

MEMBER ABDEL-KHALIK: Does the turbine-driven emergency feedwater pump room have a door?

MR. NISHIO: Yes, of course.

MEMBER ABDEL-KHALIK: It does have a door? Does the heat load calculation assume the door is open or closed?

MR. NISHIO: Closed.

MEMBER ABDEL-KHALIK: Assumes the door closed and you still get 62,000 BTUs per hour. Okay.

CHAIR STETKAR: I guess what we're asking is what justification there are for both of those values, both the 62 and -- I understand why the same value is being used in the turbine driven during normal operations. I'm happy with the fact that those two numbers are the same but I guess we would like justification for the basis for the 62 and the 110 so we understand why the difference and understand --

MR. CURRY: You're surprised the electrical --

CHAIR STETKAR: I'm surprised the electric is much higher than the turbine which brings into question what assumptions were made regarding the analyses for both of those rooms. The question is is the electric somehow really conservatively estimated by a different set of assumptions or in principle could the turbine driven heat load be optimistically estimated through a different set of assumptions because it just doesn't feel right.

MR. CURRY: We'll have to look at the calculations.

MEMBER ABDEL-KHALIK: I'm actually

surprised by the 62,000 BTUs per hour number.

MR. CURRY: You think it's high?

MEMBER ABDEL-KHALIK: It's low.

MR. CURRY: It's low. Okay. We'll look at the calculation and get back to the Committee.

CHAIR STETKAR: Thank you. And I have to ask a question that is probably a very stupid question and it will show you that I perhaps didn't spend as much time with the normal ventilation systems as I should have. There are several areas that are supplied by the essential trobe water system that do, indeed, have heat loads under normal plant operation; component cooling water area, the essential chilled water area, charging pumps, spent fuel pit.

Are those normally supplied by different ventilation systems and that's why there's no normal heat load shown in those areas? As I said, I have to apologize because I just didn't have a chance to do that kind of cross correlation. Do you follow my question? Those areas have normally operating equipment.

At any given time two of the component cooling water pumps will be running. I don't know whether they're -- it's either A or B and either C or D will be running. At any given time two of those rooms actually during normal operation will have a heat load. Yet, during normal operation there is no heat load shown on the essential chilled water system for those rooms, or any of the other; the charging pump rooms, spent fuel pit cooling pump rooms, annulus penetration, the penetration areas. The pipes don't know.

MR. HOTCHKISS: Mr. Chairman, this is Marc Hotchkiss. You are correct. They are supplied by normal auxiliary ventilation system normally.

CHAIR STETKAR: Thank you.

MR. HOTCHKISS: And then switch over to the emergency.

CHAIR STETKAR: Okay. Thanks. I apologize. I just didn't have a chance to cross-correlate that. Thank you.

MEMBER ABDEL-KHALIK: Experience in Japanese plants, do you ever have leaks in the turbine-driven aux feedwater pump rooms? Steam leaks?

MR. CURRY: So your question is Japanese experience.

MEMBER ABDEL-KHALIK: Right. During testing.

MR. CURRY: During testing.

MEMBER ABDEL-KHALIK: Right.

MR. CURRY: Turbine-driven feedwater pump.

MR. NISHIO: I have to -- we have to -- we did not hear of this. Some turbine-driven pump leak but we did not hear such a big steam leak.

MEMBER ABDEL-KHALIK: I'm wondering how much margin there is in that 62,000 BTU per hour calculated heat load.

MR. CURRY: I think if we look at the calculation and get you some more detail, it may answer a lot of questions. We'll be looking at that heat load calculation.

MEMBER ABDEL-KHALIK: Thank you.

MR. CURRY: Mr. Chairman, I was thinking of going to the non-essential chilled water system.

CHAIR STETKAR: That is an excellent thought.

MR. CURRY: All right, non-safety system with the exception of the containment isolation function. I think, once again, you have kind of a detailed or simplified schematic of the loads.

I think maybe the point of interest to the Committee might be the last bullet here for severe accidents we have the capability to connect the non-essential system to this component cooling water system to provide alternate cooling to the charging pumps and component cooling water system can also supply cooling water to the fan coolers.

CHAIR STETKAR: Jim, I want to ask about that connection. I have a couple of questions about it. First, in general, you don't have -- you do. If you pull up -- that doesn't help. One of the loads off the non-essential chilled water system are the -- I'm looking for what it's called here.

The main steam and feedwater piping area air handling units, do those -- I think I know the answer but I want to make sure I understand the plant layout. Are the areas that are cooled by those air handling units, do those areas contain the main steam isolation valves, main feedwater isolation valves, main steam depressurization valves, and main steam relief valves? Is that the section of the piping area?

MR. CURRY: Yes, that's correct.

CHAIR STETKAR: Okay. So if I lose ventilation in there, do you have any idea how those pieces of equipment respond? The main steam isolation valves and the feedwater isolation valves, if I remember right, are -- I don't remember if they are pneumatically or hydraulically operated valves but the point is they are not motor-operated valves.

The main steam depressurizations valves are motor-operated valves. The main steam relief valves are air-operated valves that fail in a closed position. I was curious about whether loss of ventilation for that area would have an affect on operation of any or all of those valves? In particular, you know, would they fail in specific positions?

Would motor operators or other instrumentation be disabled that could affect any of the safety-related functions from any of those components? I think the main steam relief valves are not safety related but the main steam depressurization valves are, if I recall.

MR. KAWATA: These are qualified in the main steam line break condition.

CHAIR STETKAR: Okay. They are qualified under main steam line break. Okay. Correct answer. Thank you.

Now, on the -- you don't have a drawing for the non-essential chilled water system, do you? Yes, you do. I'm sorry. The connections -- it's doesn't show on this one. Down in the lower left-hand corner of this drawing shows the connections between non-essential chilled water and component cooling water, those two little arrows that come in and out.

Unfortunately, this drawing you need to look at the component cooling water PNID and this drawing at the same time to understand my question. The SER says that the connection between the component cooling water system, and this is -- it comes from component cooling water system Header C1 so it's off that Header C1.

The design of this, as I understand it, is you can either supply component cooling water to the containment fan coolers, or you can supply non-essential chilled water back over to the charging pumps. It's a bi-directional sort of flow possibility.

In the SER it says that connection, because this is non-safety related piping, is -- what it says is, "There are redundant normally closed motor-operated valves to isolate the systems." I could find only one normally closed motor-operated valve on each of the supply and the -- it's bad to call it supply and return but in each of the lines between component cooling water and non-essential chilled water.

In other words, there is only one

normally closed valve between Header C1 and what is shown as an in-going arrow here from CCW, and only one normally closed motor-operated valve on what is shown as outgoing. I wasn't sure whether I was missing something or whether I'm misinterpreting the connotation of redundant normally closed motor-operated valves. To me that normally means two valves in series.

MR. CURRY: Right. We don't think you're misinterpreting. Kawata-san -- I don't know, Mr. Chairman, if you have Figure 9.2.2-1.

CHAIR STETKAR: Oh, yes, I do. 9.2.2-1?

MR. CURRY: Yes, sir.

CHAIR STETKAR: I have it. Finding it is something else. I do and it's Sheet 5. I'm sorry, Sheet 6. Is it 6? Sheet 5 according to my notes.

MR. CURRY: And we're looking at the living --

CHAIR STETKAR: We're looking at Interim Rev. -- I'm looking at Interim Rev. 4, Sheet 5 with 9.2.2-1 down in the lower left-hand corner of that sheet.

MR. CURRY: We're looking at Sheet 6.

CHAIR STETKAR: Six?

MR. CURRY: The valves we're looking at

are MOV-322A, 321A.

CHAIR STETKAR: No, those are the wrong valves. You're looking at the wrong valves. That's from the fire protection system.

MR. CURRY: Okay. Well, I'm sorry. I apologize. You are looking at the connection, yes. Yes. You're looking at the connection. What connection are you looking at? I thought I understood the way this worked and now I don't understand the way it works because I didn't look at Sheet 6.

I thought that the only connection was on Sheet 5 down in the lower left-hand corner. In other words, I'm trying to understand where these two single arrows on this drawing connect in the real world.

I thought they connected on Sheet 5 in the lower left-hand corner and that the flow from non-essential chilled water to the charging pumps came through these valves back up through the header and over to the charging pumps and I didn't look at Sheet 6 which shows another connection that says non-essential chilled water. Now I'm even more confused because -- I'm just confused.

MR. CURRY: One moment. We're checking.

MEMBER BLEY: You need to pick one.

CHAIR STETKAR: That's why I said you

kind of need to look at both. I'm finding I needed to look at more drawings at the same time because I thought I knew how it worked and I was apparently wrong.

MR. WHEELER: This is Larry Wheeler from the staff. The Interim Rev., I think, has some Chapter 19 figures that might show that information on it a little clearer so that's something you can take a look at.

CHAIR STETKAR: I didn't even think of looking there. Thank you. Why would the PRA have anything useful in it? If anybody happens to know the number of that figure, it might help. There it is.

MR. CURRY: Do you have an electronic copy, Mr. Chairman, or just a paper copy?

CHAIR STETKAR: Of which? Yes. The answer is yes. I have electronic. If you can just point me to which drawing.

MR. CURRY: Right. Okay.

CHAIR STETKAR: If that Chapter -- I'm look at, I think, the -- there is a figure in Chapter 9 that is 19.1-2, Sheet 34. I'm not sure if that is the one I should be looking at. It's entitled Simplified System Diagram: Alternate Component Cooling by Non-Essential Chilled Water System which may or may not -- yeah.

I was going to say which may or may -- it's got a nice sounding title but I'm having difficulty understanding what it's trying to tell me. What I was going to suggest -- quickly I'm not learning anything from this that's going to help me. Let's leave this.

In the interest of time maybe you can help me understand. Even sketches on a piece of paper or some drawing that might show all of the valves. I admit I didn't look at Sheet 6, 9.2.2-1, but, quite honestly, that's only confusing me a little bit more because I thought I understood how it worked just looking on Sheet 5.

Just looking on Sheet 5 I could -- the concern I originally had is looking at Sheet 5 if I broke the piping on the drawing that you have here in front of me, I could only find one isolation valve to isolate the CCW header from that break.

MR. CURRY: You're talking about right where I'm pointing. You're talking about a break there.

CHAIR STETKAR: Exactly.

MR. CURRY: Okay.

CHAIR STETKAR: As I said, in the SER

it's characterized as that interface, whatever it is, is isolated by redundant normally closed MOV.

MR. HAMAMOTO: This is Hiroshi Hamamoto. The interconnection line between the CCW and non-essential chilled water system has two connections. One is cooling tower for non-essential. Two is charging pump. Connection is between cooling tower to charging pump. Charging pump, cooling line is safety.

9.2.2-1, Sheet 6 is between safety and non-safety. The valve is double isolation. The other, Chapter 5, is a connection between CCW to the containment cooling -- cooling pump. That is a connection between the non-safety. That line is containment non-safety line to non-safety containment cooling. Isolation valve is only one.

CHAIR STETKAR: Thank you. I'm starting to understand it. I see now if I look at DCD Figure 9.2.7-2, Sheet No. 3, and Figure 9.2.2-1, Sheet No. 6, I at least see where I misinterpreted how I can get non-essential chilled water to the charging pumps so that the line on Sheet 6 of 9.2.2-1 connected to lines that are shown on 9.2.7-2, Sheet 3, and those lines, indeed contain two normally closed motor-operated valves.

I've isolated the non-essential stuff on the -- I'm sorry, the non-safety things on Sheet 3 of the non-essential from the safety related that's shown on the component cooling water. I see where that is.

Now, what I -- because I was looking at drawings I didn't quite understand the second part because this -- is the piping that's shown on this drawing seismically qualified? If it is, where is it seismically qualified? Because the way to supply component cooling water now to the fan coolers, that connection is shown on Sheet 5 of 9.2.2-1.

MR. HAMAMOTO: Sheet 5?

CHAIR STETKAR: Sheet 5.

MR. HAMAMOTO: Cooling containment.

CHAIR STETKAR: That only has one.

MR. HAMAMOTO: Yes. This chilled water system is non-essential. Non-essential means non-safety-related. Also this is connection to non-safety related CCW line so that we don't need double isolation.

CHAIR STETKAR: Okay. The reason -- this may be something I need to ask the staff for clarification, but in the SER there are a couple of statements regarding connections and there is a reason I'm confused. One says the non-ECWS includes a connection to the CCWS to allow chilled water use as alternate cooling for the charging pumps in the event of the failure of CCWS during severe accident conditions.

As indicated in Section 9.2.2 of the DCD, at the boundary of the non-ECWS and CCWS there are redundant normally closed motor-operated valves to isolate the system and those I now understand where they are. I got that.

It's also noted, though, that in addition the CCWS can be used as an alternative supply of cooling water to the containment fan coolers of the non-ECWS in the event of a severe accident. In order to provide isolation between the seismic Category I CCWS and the non-seismic non-ECWS two locked closed valves are provided as indicated in Section 9.2.2.2 of the DCD. Therefore, CCW system integrity and operability is assured by these isolation valves.

Now, given the fact that I'm slowly starting to understand these interconnections, my question now is the two locked closed valves that are mentioned in the SER, are those the two normally closed motor-operated valves that appear on Figure 9.2.2-1, Sheet 5, of the DCD in the lower left-hand corner?

MR. CURRY: Mr. Chairman, can you just

give us the SER page reference?

CHAIR STETKAR: Yes, I can. Page reference, unfortunately, if you look for SER Section 9.2.7.4.1 under GDC2.

MEMBER SHACK: Bill. 118.

CHAIR STETKAR: I was going to say Bill can find the page number quicker than I can.

MR. CURRY: Okay. Maybe we should look at these diagrams but that's the statement that we're trying to --

CHAIR STETKAR: I was trying to resolve these two statements. The first one I now understand because I was misunderstanding where that connection was from non-ECWS to the charging pumps in particular. I was getting flow in a different direction. That one I'm happy with. I understand that. The one that I am concerned -- questioning now is the second one that cites two locked closed valves.

MR. CURRY: From CCWS to the fan coolers.

CHAIR STETKAR: In particular, this supply that's shown on this drawing here from CCWS to the fan cooler which I now understand is a different connection. I'm trying to understand the subtleties of what two locked closed valves mean in the connotation of a break somewhere in this piping system.

MR. CURRY: Okay. So, just to repeat, we are looking for the two locked closed valves in CCWS to the fan coolers.

CHAIR STETKAR: Yes.

MR. CURRY: And we have an SER reference.

CHAIR STETKAR: There is an SER reference.

MR. CURRY: Thanks.

CHAIR STETKAR: Yes. That's all I have on non-ECWS. Thanks for your patience. That's one of the reasons why -- the fortunate thing is we do have enough time. As I said, sometimes it takes a while to get the questions sorted out. It's useful to have time so you can look up references. Thank you.

MR. CURRY: Absolutely. All right. I think we're on 9.2.8, Turbine Component Cooling Water System. It's a non-safety system and simply provides cooling water to various turbine loads. You see the three heat exchangers there at 50 percent capacity, as are the pumps.

That system is serviced by the non-essential service water system. The non-essential service water system provides cooling water to the turbine cooling water system. It's a once-through system discharging -- taking in-take water and discharging to the circ water system connections.

Just to avoid any confusion for those of you who have this piece on your slide, that is some kind of a ghost. I don't know why that's there but it shouldn't be there.

CHAIR STETKAR: It's just other pumps.

MR. CURRY: I thought we got rid of those.

So that concludes what we had planned to say on 9.2.

CHAIR STETKAR: We are exhausted so we're going to take a break for lunch now. We're doing pretty well on time so I'm going to be really generous. We'll reconvene at 1:00. We are recessed for lunch.

(Whereupon, at 11:49 a.m. off the record for lunch to reconvene at 1:02 p.m.)

A-F-T-E-R-N-O-O-N S-E-S-S-I-O-N

1:02 p.m.

CHAIR STETKAR: We're back in session.

MR. CURRY: Mr. Chairman, I think we left off of 9.2. We plan to start with 9.3.

CHAIR STETKAR: Yes.

MR. CURRY: Our Holtec consultants, Mr. Bullard, Mr. Brickner and Mr. Fitzpatrick will have to leave soon, but we do have an answer to the questions you asked this morning about Metamic.

CHAIR STETKAR: Good. Jim, thanks. You reminded me of something. We will plan to adjourn today at around 5:00. I mean, it depends on when we come to a stopping point. We will plan to come back tomorrow. I don't think necessarily we can cover all of the material today, and coming back tomorrow will also give you folks an opportunity, perhaps, to also do some more research tonight if that's necessary to answer some of the other questions.

So, for just administrative purposes, plan that we'll end around 5:00. It might be a little more, it might be a little later. We probably will not go to 5:30 today, and we should plan to come back tomorrow morning. But that doesn't change what you're going to say now.

MR. CURRY: No, and that's helpful in planning.

CHAIR STETKAR: But it's just for everyone's planning.

MR. CURRY: That's helpful. It also will be helpful if we can at least get through the presentation so we know what the Committee's questions are.

CHAIR STETKAR: Absolutely. We'll certainly shoot to do that. I don't know whether we'll finish, you know all of the staff's presentations by the end of this afternoon.

MR. CURRY: Okay.

CHAIR STETKAR: But certainly we'll get through yours.

MR. CURRY: That would be great.

MR. HAMZEHEE: We don't plan to talk too much.

CHAIR STETKAR: You don't plan to talk too much.

MR. HAMZEHEE: No.

CHAIR STETKAR: Okay.

MEMBER SHACK: The best laid plans of mice and men.

CHAIR STETKAR: Then make sure you have sharp pencils so you take notes.

MR. CURRY: Okay. So, where we left off this morning with the criticality, there was a Committee question regarding the anodized Metamic and the borated water and the potential pH associated with it. And so I think Mr. Bullard and Mr. Brickner have some information for us.

MR. BULLARD: Yes. Thanks, Jim.

I did want to confirm, I spoke with colleagues at our office. The Metamic material as fabricated and as installed in the racks is in the unanodized condition. And that is typical of Holtec-designed spent fuel racks installed at many nuclear power plants. So while it is not analyzed, it is not a first of a kind installation or application of that material.

And we will provide to MHI the ADAMS accession number so that you can review the topical report to find out more information about the material.

I think Bret is going to add more information with regard to the pH.

MR. BRICKNER: There was a question related to the soluble boron concentration and the pH, and while we don't report pH inside the boron concentration is very similar which we did in the testing, about 2500 ppm. And I've been told that the pH is about five for that testing. And I was told the pH was 4.9, is that correct?

MR. NISHIO: Around five.

MR. BRICKNER: About five? So it's a very comparable pH.

And I'm looking at our report that Chuck just mentioned. The testing was actually done with deionized water also, and the results showed that the deionized water was a harsher environment than the soluble boron in the testing

MEMBER SHACK: I'd like to see the accession number. But, yes, I'll have to look at that. I'm a little surprised at those results, but there's aluminum and there's aluminum, of course.

MR. BRICKNER: Yes.

MEMBER SHACK: I'm not exactly sure just precisely what alloy you're probably using, although there is a type earlier, it is some alloy. But, okay.

But there is a report, and so you're in that range for the report?

MR. BULLARD: Yes. I can show you through the Holtec number, but that's probably not as much use--

MEMBER SHACK: It's not. Oh, well give me the Holtec number, I can probably -- even that will be good enough.

CHAIR STETKAR: Well, we should probably get the topical report with the staff's --

MEMBER SHACK: Well, I'll get out it of ADAMS, but I'll look for it under the Holtec number. If they have it.

The only concern I have is --

MR. BULLARD: Would you liked the Holtec

number?

MEMBER SHACK: -- if that's a proprietary thing versus a topical report that might not be proprietary. I mean it's good for you, but --

MR. BRICKNER: There is some proprietary information, but I do believe that there is -- I'm, almost certain there's a nonproprietary version that's in ADAMS.

CHAIR STETKAR: It's just we have to be a little careful of what we discuss in open session in case this, you know this gets into information that's a proprietary session, that's the only concern I had.

MR. BULLARD: We can certainly share with you the Holtec report number at this time. It's Holtec Report No. HI-2022871. And there is an SE --

MEMBER SHACK: There's even an SE on it?

MR. BRICKNER: -- for that report. Yes.

MR. CURRY: So when these gentlemen leave, and this will be the last chance to ask any questions on criticality.

CHAIR STETKAR: Well, fellas, we have anymore?

I think you can leave. We know where to find you. Okay.

MR. BRICKNER: Thank you.

CHAIR STETKAR: Thank you very much. That was helpful.

MR. BULLARD: Thank you very much.

MR. CURRY: Okay. Next, I think we're going to Process Auxiliaries, which fundamentally is a nonsafety-related system with the exception of isolation functions. Mr. Kitamori-san is our expert here. And you know Mr. Kawata.

I said Mr. Kitamori-san. It should be Mr. Kitamori. Sorry.

All right. As usual, we have the names of the folks at this table, the acronym list for you, the process auxiliaries and our definition consists of the compressed air and gas systems, the sampling systems, the floor drain system and the CVC, that's the chemical and volume control system. The only safety-related function relates to isolation of these systems, containment isolation of these systems.

The compressed air and gas system is further divided up into three subsystems:

Instrument air;

Station service air, and;

Compressed gas.

And just flipping back, you have a simplified schematic also in your package there.

Instrument air consists of two 100 percent trains with a compressor, an air receiver, and an air dryer in each train.

Safety related AOVs fail in a safe position on loss of instrument air, and that of course is why it's not a safety-related function.

Station service air system consists of three 50 percent trains with compressors. As shown, we really have only two compressors but, you know two receives, three compressor packages I guess is the right way to say it.

The station service we can provide instrument air if additional air is needed.

Compress gas station. Gas, high pressure nitrogen gas which is used for the SIS accumulators and then the rest of the pressure gas systems are low pressure systems, nitrogen and hydrogen primarily.

Well, that summarizes that system.

The air compressors, I think I recall are all oil-free air compressors, is that correct? Do they use oil lubricants?

MR. HAMAMOTO: This is Hiroshi Hamamoto.

Compressor is oil-free.

CHAIR STETKAR: They are oil free? Thank you.

MR. CURRY: Thank you, Hamamoto-san.

All right, moving on to 9.3.2 the sampling systems. Again, no safety-related function. You see a list of sampling systems there, and there's a range of them. And their function is pretty much as expected: RCS sampling, containment atmosphere sampling, et cetera.

Equipment and floor drain systems. Again, no safety function except isolation valves. The equipment and floor drain system we have radioactive sumps on, radioactive sumps. The following subsystems as indicated:

Radioactive;

Non-radioactive;

Chemical and detergent,and;

Oily;

Liquid waste;

Radioactive liquid waste goes to the liquid waste management system.

CHAIR STETKAR: This drawing shows in the center of the drawing or left center of the drawing as we're looking at it the two normally closed manual valves that show there at the outlet of the ESF room floor drains. Could you tell us a little bit more about those valves and why they're normally closed? I mean, I think I understand but it was a bit difficult for me to follow the whole rationale through everything I read about them.

MR. KITAMORI: I am Motohisa Kitamori.

This manual valve is normally closed. And this manual valve is classified as safety-related to prevent from flooding.

So we have some -- drain -- this drain has piping, so we open this valve.

CHAIR STETKAR: So, the reason that they're normally closed, as I understand it, is to prevent flooding of the room through reverse flow in the drain line, is that right?

MR. KITAMORI: That is correct.

CHAIR STETKAR: Do these rooms have -- well, we'll have time to prejudice things. It's not clear to me how that valve normally being closed is necessarily good to prevent flooding in that room. Because if the water comes into the room from any other source other than backflow through the drain, it would seem to me that having that valve closed isn't necessarily a good thing for that room.

So, I'm curious. The ACRS does not design systems; it's not our job. We ask questions. I'm curious what decisions were made and whether you looked at all possible sources of flooding in those rooms to justify the decision to have those valves normally closed, which would require an operator if you had water entering the room from another source, like a broken pipe; why that would require an operator then to go try to drain that room or perhaps the broken pipe -- and I don't know which pipes run through those rooms. I mean, obviously if it's only the pipes related to the equipment in the room, I don't care if I fail it because its flooded or fail it because its -- but I also don't know exactly what's in those rooms either. I only know that it's called an essential service or essential equipment room. So I don't know what's in those rooms. I don't know what other pipes run through those rooms. I don't know if there are other drain lines that run through the rooms. I don't know if there's fire protection water that's runs. I don't know what's in there.

So, if you could kind of explain what sort of process you went through to conclude that the likelihood of reverse flooding through the drain system outweighed the likelihood of inlet -- you know, other sources of flooding in the room, I think that would be useful.

MR. CURRY: One moment.

MR. NISHIO: This is Hiroki Nishio.

So, in the room there is a second or a return from safety-related group only. And so in the US-APWR we divided into two areas, divided two portions, two safety-related pumps, two areas, safety-related. And so we did it to prevent the potential clogging effect to the -- for example, east side flooding does not effect go to the west side. East side to west side. To prevent that, we close that drain pipe.

To create this we can take a credit that one side flooding does not effect to the next side.

CHAIR STETKAR: I think I understand that.

MR. NISHIO: Yes.

CHAIR STETKAR: And as I said, as the ACRS we don't design systems. There is another design that I can think of that would accomplish the same function and leave a manual valve normally open. I'll just leave it at that.

And I'm interested in the rationale that said this is the best way to achieve that type of protection that you're talking about, either back flow through the drains or cross-tie or cross-flow from the different divisions through the drain system.

MR. CURRY: And I think we understand your question, which is well gee if you leave the valves open, then you have m,any sources of flooding in one drain, a drain valve that's open would drain the room.

CHAIR STETKAR: It would.

MR. CURRY: And not cause such a problem.

So, I don't know if we -- maybe we need to check on the flooding analysis. So we made a decision to close the valves --

CHAIR STETKAR: Yes.

MR. CURRY: -- which prevents, as Mr. Nishio said, losing both sides of the system but the question is what was more important.

CHAIR STETKAR: That's right: What was more important? Because in order to get cross -- I had no idea about the elevations of the rooms. I mean, as shown on this simplified schematic here, those rooms drain into lines that eventually go through a sump. And I'm not sure how gravity works, because I don't know how the different configurations are. But, you know are you protecting against essentially a plausible but quite unlikely condition and making yourself vulnerable to a more likely condition?

MR. CURRY: Do we have flooding sources

for each area, or maybe we need to do some research to see if potential flooding sources --

CHAIR STETKAR: Yes, I don't know what -- you know, I don't know whether your PRA has done that type of internal flooding analysis. I don't, Dennis, you looked a little.

MEMBER BLEY: There's some flooding, but I don't remember details.

CHAIR STETKAR: Okay. I mean, you'd need to look at, as I said, not only the safety-related piping in that room but are there any fire protection lines that happen to transit through the rooms or other drain lines, or -- you know -- I don't know what level of detail you have it at.

I was just curious. That one level I think I understand the kind of reaction to or licensing question, but sometimes those reactions may not necessarily be the best solution.

MR. CURRY: And the question is the basis for the valves being closed or open and what is more important?

CHAIR STETKAR: Right.

MR. CURRY: The back floor versus individual room flooding. So we can discuss that.

MR. KAWANAGO: This is Shinji Kawanago.

Yes, and we understand the question and what is the point. But what we want to emphasize again, and basically on a design-basis we need to think about, And it's internal flooding. And for example, the fire and it's a piping break, and the drain would come. And even if there is -- and -- even if we don't need to assume some piping tank break or potential -- and a tank went out, however we need to think about the fire piping break or as a source of the internal flooding.

CHAIR STETKAR: Right.

MR. KAWANAGO: And also, and this really we needed to have the -- and the division on the east side and the west side so that -- and in your point of those is our protection that internal flooding to effect the other division, and nobody's ready to quote this one. So, of course -- and usually there is no -- actually the -- the water. However, and to keep the safety --

CHAIR STETKAR: You know, I understand, and I'll stop trying to be cagey. Why didn't you put two series check valves in there that would allow water to flow this way and not water flow that, and keep the valves open? I mean, that would accomplish--

MEMBER BLEY: The same thing.

CHAIR STETKAR: -- that would allow water to flow this direction and not allow water to flow that direction and it would seem to accomplish both functions?

MR. KAWANAGO: Okay.

And as I said, we don't design things here, but I'll toss that as sort of my first thought of why didn't you do that? Somebody made the decision to do this and there must be some basis for that. One series check valve would probably be good enough, but for double isolation you might need two.

MR. KAWANAGO: We understand your point. And maybe that is one -- a resolution of the -- you know--

CHAIR STETKAR: But honestly, I mean you know that -- I have to be careful here because it is not our function to suggest designs. That's not our purpose. Our purpose is, however, to understand the technical rationale behind a specific design decision and make sure that from kind of an integrated safety perspective we have assurance that people have thought of all these different possibilities. How you solve it is your side.

MR. KAWANAGO: And to show the safety-related evaluation and whether or not we don't use a check valve. So this is a safety-related function, so we need to check the integrity of the value. So the-- we use to check valve, we can't check the integrated fuel degrade --

CHAIR STETKAR: And as I said, it's not our job to kind of design the system. It's just -- anyway, we'll leave it, but I'm still kind of interested to see if you looked, you know all sources of flooding and basis for that.

MR. CURRY: I understand.

And finally the last part of 9.3 is the CVCS. A typical chemical and volume control system maintaining coolant inventory:

Seal-water flow, we talked about it earlier as a function;

Capability of makeup for small leaks.

Controlling chemistry;

Safety-related functions are really maintaining the containment boundaries.

A simplified schematic showing the 200 percent charging pumps and the letdown line.

CHAIR STETKAR: Interpret silence and move on as quickly as you can. I don't have any questions on this one.

MR. CURRY: Thank you, sir.

All right. That concludes what we have to say about 9.3.

And I think we are ready to move to 9.4. So thank you.

So we are going to change the team a little bit. Mr. Hotchkiss is going to come up and Junya Hattori-san will be back and Keita Otani.

Mr. Hattori, Mr. Hotchkiss and Mr. Otani.

MR. HOTCHKISS: Okay. Good afternoon.

As Jim indicated, my name is Marc Hotchkiss. We're going to be talking about section 9.4 of the DCD, the ventilation systems. Okay. Okay.

This section is a similar format to the other ones you've seen today with we do introduce the technical experts: Otani-san, Hattori-san. And then we have a list of acronyms to refer to if necessary.

DCD Section 9.4 ventilation systems includes this list of systems and there's an indication of safety-related functions for each of these.

The main control room heating, ventilating and air conditioning system has safety-related functions, as you'd expect.

There is a section 9.4.2 for spent fuel pool area ventilation system, however the US-APWR does not have a separate defined spent fuel pool area ventilation system. That spent fuel pool area ventilation is accomplished by the aux building ventilation system, which is 9.4.3.

And we also discuss turbine building ventilation system, 9.4.4. Engineered safety feature ventilation system, 9.4.5 and containment ventilation systems 9.4.6.

So, we'll begin with the Main Control Room HVAC.

The Main Control Room HVAC system designed for US-APWRs is typical of U.S. plants, actually, very much as we'll see when we get to the flow diagram.

The functions of the system are to control the environment within the control room envelop, of which the Main Control Room is a part. And it is a safety-related system and functions to exclude entry of airborne radioactivity into the control room envelope from the outside air intake. And removed any radioactivity within the CRE environment.

How the system supports and maintains habitability and functioning of instrumentation during normal conditions and design basis accidents.

And this is a simplified diagram,

representation. I guess just one other system description type point. There are three modes of operation for the system. There's a normal mode, which essentially takes outside air as makeup air, circulates it through air handling units, conditions the air and exhausts through the kitchen/toilet exhaust fan. That's normal conditions.

There's a pressurization mode which is essentially the emergency condition which also uses outside air to pressurize the control room envelop, but filters that air through the emergency filtration units. I think I can get a mouse up here, which is this section, 200 percent trains emergency filtration units. And also recirculates a portion of the control room envelop air through those units during pressurization mode.

And the third mode of operation is isolation mode, and that occurs in the event of smoke detection or gas detection outside of the control room. And that isolates the outside air intake and recirculates the control room environment atmosphere through the air handling units for the conditioning of the air.

That's the description of the system.

CHAIR STETKAR: Marc, you characterized

on the exhaust fan, you show smoke purge-- I'm sorry. Smoke purge. Is that initiated automatically, do you know?

MR. HOTCHKISS: Smoke purge?

CHAIR STETKAR: Yes.

MR. HOTCHKISS: No.

CHAIR STETKAR: It's manual?

MR. HOTCHKISS: On a smoke signal it's shutdown as it was running, which it normally wouldn't be.

CHAIR STETKAR: Okay. Okay.

MR. HOTCHKISS: But once the condition is cleared, then it's manually maturated to clear smoke.

CHAIR STETKAR: Okay. Thank you.

MR. HOTCHKISS: And the exhaust fans are here not labeled, I guess on this drawing.

CHAIR STETKAR: They're different diagrams.

MR. HOTCHKISS: Any other questions on this system. Okay.

CHAIR STETKAR: Speaking about the ventilations, there are a lot of them, but they're pretty simple.

MR. HOTCHKISS: Yes. And they're very similar to what you're used to.

CHAIR STETKAR: Yes. Yes.

MR. HOTCHKISS: Okay. The next slide or two are related to open items that we are working with the staff on to close. They're documents in the SER.

Okay. The next system is auxiliary building ventilation system consisting of a number of subsystems:

The aux building HVAC system;

The non-Class 1E electrical room HVAC system;

The main steam/feedwater piping area HVAC system, which we discussed a little earlier, and;

The tech support center, TSC HVAC system.

The aux building and ventilation system is a nonsafety-related system, again very similar or the HVAC subsystem is nonsafety-related, very similar to US-PWR clients. The only safety-related function for this system is there are some isolation valves that close to allow safety-related ventilation systems to assume the ventilation functions during an accident. And there's also an isolation in front of the main vent stack during an accident condition.

The aux building HVAC system functions to maintain a proper operating environment within the auxiliary building, the reactor building, the power source building and the access control building during normal plant operation.

The system also functions to keep dose levels due to airborne radioactive material in normally occupied spaces below allowable values during normal conditions. And it does so by maintaining a slightly negative pressure within the controlled areas relative to the outside atmosphere. And that's accomplished by a greater exhaust flow than a supply flow.

And the system maintains air flow from areas of low radio activity to areas of potentially higher radioactivity by exhausting from the higher radiative, potentially higher radioactive areas.

And the next slide is a little busy, but it's a schematic representation of the system. On the left side are the supply fans, two 50 percent fans normally operating. And the center portion is just a representation of the spaces that are ventilated with supply on the left center and exhaust on the right side. And then the three exhaust fans,two of which are normally operating are shown on the right hand side of the drawing.

CHAIR STETKAR: Something I hadn't really thought about, so I have to be careful here, the center part of this drawing, for example the lines that feed the Safeguards component areas are shown with isolation dampers or valves that I think you said goes closed on an accident sequence, ECCS or whatever.

MR. HOTCHKISS: ECCS, yes.

CHAIR STETKAR: There are lines at the top that go to, for example, the CCW up pump areas and emergency feedwater pump areas and the essential chiller areas that don't have similar isolation valves. And yet I know, for example, there's essential chilled water cooling goes to air handling units in those areas. Can you tell us a little bit about the difference? I mean, I kind of asked the question earlier, but I -- I wasn't putting some of the pieces together correctly about, you know what provides normal ventilation and is there a transfer from what's called normal auxiliary building ventilation to safety-related room cooling? In particular, I understand the ones down below that are isolated. I'm more curious about the ones up above that don't show similar isolation valves for the component cooling and EFW and the chillers themselves.

MR. HOTCHKISS: Understand. Can I confer just briefly?

Okay. I think we're clear on this.

What's indicated with the dampers --

CHAIR STETKAR: Yes.

MR. HOTCHKISS: -- those are actuated on a high radiation signal in order to line up the containment low volume purge exhaust filtration units--

CHAIR STETKAR: Okay.

MR. HOTCHKISS: -- if there's high radiation in those spaces.

CHAIR STETKAR: Okay.

MR. HOTCHKISS: In the other ares, an excellent condition to safety-related air handling units start and provide cooling to the area, but auxiliary building ventilation is maintained. Only on a high radiation would we isolate the are.

CHAIR STETKAR: Okay. Okay. Than you.

And so to make sure I understand, are any of the dampers that are shown on this drawing I assume would show up on the figure in the DCD, are any of these dampers automatically closed by an ACCS signal?

MR. HOTCHKISS: No.

CHAIR STETKAR: No?

MR. HOTCHKISS: They would be closed on--

CHAIR STETKAR: Only high radiation? Thank you.

MR. HOTCHKISS: And there's a remote manual right there.

CHAIR STETKAR: Okay. That explains the differentiation about which areas show. Thank you.

MR. HOTCHKISS: Anything else on auxiliary building HVAC system?

Okay. The next systems to discuss, there's three on this slide on the aux building ventilation of the non-Class 1E electrical room HVAC system, it's nonsafety-related and it cools the non-Class 1E electrical room. It maintains ME conditions acceptable for electrical equipment and component operation, and it has the additional function of maintaining the hydrogen concentration in the room below one percent in the battery rooms, actually.

And the next bullet in the slide, the TSC, the Tech Support Center HVAC system, is also nonsafety -related. And that functions to limit the airborne radioactive material in the TSC envelope environment and remove radioactive material from the environment's refiltration.

And maintains proper environmental conditions for habitability and equipment operation within TSC.

The third system on this slide is the

main steam/feedwater piping area HVAC. It's also nonsafety-related and maintains proper environment for the components within the main steam/feedwater piping area.

And that's it for the auxiliary building ventilation system. An any question or we can move to turbine building ventilation.

The turbine building area ventilation system is nonsafety-related. Basically the turbine building is not expected to have any airborne radioactive material in the ambient or in the environment. And there are no safety-related components in the turbine building.

The system functions to maintain a suitable environment for operation of equipment within the turbine building.

CHAIR STETKAR: I've read a couple, and I don't remember whether I asked this before and it's not a ventilation system question. But the statement has been made a couple of times that there are no safety-related components in the turbine building. And "no," is a very big word.

Are there other safety-related instruments or signals that communicate from, for example, turbine trip to reactor protection system;

are those located in the turbine building?

MR. HOTCHKISS: There is equipment providing that function within the turbine building. We actually have an open item that's on this next slide related to that question.

CHAIR STETKAR: Okay.

MR. HOTCHKISS: And we're working with the staff now to resolve that.

CHAIR STETKAR: Okay. Okay. I just wanted to make sure I understood that. Thanks.

MR. HOTCHKISS: Okay. The next ventilation system is the engineered safety features ventilation system. It also consists of a number of subsystems:

The annulus emergency exhaust system;

The Class 1E electrical room HVAC system;

Safeguards component area HVAC system;

Emergency feedwater pump area HVAC system, and;

Safety-related component area HVAC system.

And we'll go through each one of these. A couple of these we talked about back when we were talking water.

Again, the annulus emergency exhaust

system is safety-related, it's an ESF ventilation system. And it functions to remove and retain through filtration fission products that may enter the air from the penetration areas and Safeguards components areas following an accident.

I'll just skip to the next slide just briefly while we're talking about annulus emergency exhaust, just to show the simplified run.

The system consists of potentially along the left side of the drawing two exhaust filtration units, each with a high efficiency filter and a high efficiency particulate air filter, a HEPA filter. And those components automatically start to filter the exhaust air from, as I mentioned, the penetration areas and the Safeguard component areas following an accident. Exhaust to the bench stack.

Okay. So back in the previous slide, we got a couple of the systems listed. The Class 1E electrical room HVAC systems functions to maintain proper operating environment for Class 1E to electric equipment in the rooms. And also maintains a hydrogen concentration below one percent by volume in the Class 1E battery rooms.

And the other three subsystems we discussed on the previous slide have the same function, and they're also safety-related, but they function to just provide the proper cooling and environment for operation of the equipment within the rooms.

We do have some simplified drawings of the Class 1E electric room HVAC system. I guess that's the only one we have.

Any questions on ESF ventilation?

Okay. The last ventilation system to present is the containment ventilation system. And that system consists of four subsystems:

The containment fan cooler system, we touched on that back when we discussed chilled water earlier this morning;

The control rod mechanism cooling system;

Reactor cavity cooling system, and;

The containment purge system.

We've got a brief description of each of those systems.

The containment fan cooler system functions to maintain a proper environment within containment during normal plant operation in the LOOP condition.

The CRDM cooling system removes heat from the CRDMs.

The reactor cavity cooling system functions to remove heat from the reactor vessel, the reactor vessel support structure and the primary shield wall. And it also functions to cool the supports for the primary shield in the reactor vessel to prevent concrete dehydration.

The containment purge system has two subsystems to it as well. The low volume purge and the high volume purge.

The low volume purge system functions to minimize the spread of radioactive contamination from areas serviced by the aux building HVAC system, which was what we just talked about on that figure of aux building ventilation. And essentially on a high radiation signal we can line up the affected area to this containment low volume purge system, which includes a HEPA filter and charcoal filter.

The system also provides relief from pressure buildup within containment cause by instrument air leakage and containment temperature fluctuations.

The high volume purge system is used to maintain low concentrations of radioactive airborne material in containment atmosphere to allow access during maintenance and inspection activities.

The next slide is a simplified floor diagram of all of those containment ventilation systems. On the left side is what we just discussed, the low volume purge and high volume purge on the upper part of the left are the air handling units which provide cooling or heating for the air in containment. And the lower portion of that slide on the left is the air cleanup portion, which includes high efficiency filters, HEPA and charcoal filtration for the low volume purge. And then a high efficiency filter and a HEPA for the high volume purge.

And to the right are the other three systems we discussed: The fan coolers, the CRDM cooling and the cavity cooling.

CHAIR STETKAR: I don't understand the function and the classification of the containment fan coolers in this part, and maybe you can help me.

The fan coolers are not safety-related?

MR. HOTCHKISS: That's correct.

CHAIR STETKAR: And you mentioned it, their function as stated is to provide normal environmental temperatures inside the containment, which everybody does that. But one of their functions is to maintain, and it's cited specifically, to maintain temperatures during a loss of offsite power, and it can be powered from the alternate ac gas turbines. So, they're kind of more than just normal nonsafety things, but they're not safety-related. Plus you've plumbed up some safety-related component cooling water supply to them, but not for a safety-related function.

So, I'm trying to understand -- I guess, you know they're not safety-related so that means we haven't seen the safety, you know Chapter 15 or Chapter 6 analyses yet. It hasn't come before us yet. So, apparently, the safety analyses do not include credit for them.

MR. HOTCHKISS: Correct.

CHAIR STETKAR: But do the analyses of loss of offsite power event include credit for that who have maintained environmental conditions inside the containment?

MR. HOTCHKISS: Now the loss of offsite power event that is not the loss of all ac event --

CHAIR STETKAR: That's right.

MR. HOTCHKISS: -- is the loss of offsite where we were loading 1E buses onto the GTGs.

CHAIR STETKAR: Right.

MR. HOTCHKISS: And in that event you still would need to shutdown the plant, cool down the containment, not a natural circulation, most likely so there's still going to be some containment atmosphere cooling required. So that's why these have a function of loss of offsite power containment cooling.

The other two -- well, the other events you were talking about you referred to as we have a cross connect to provide cooling to this from CCW is a severe accident mitigation alternative. And for the purpose of, you know in a severe accident, preventing -- or some sort of cooling if we don't have the normal design-basis containment protection system of containment spread. That's the safety-related containment protection , over pressure protection system is containment spread.

CHAIR STETKAR: What happens if I have a loss of offsite power and I do not have the fan coolers?

MR. HOTCHKISS: There is still a considerable amount of heat being generated from the equipment within containment, so the temperature would increase.

CHAIR STETKAR: Okay. Would I -- as I said, we haven't seen the accident analyses and I guess this is more appropriate for that discussion. But I'm just curious. On this plant they're somewhere between something that sounds like the purely nonsafety-related and something that sounds like it's safety-related.

So, I guess we'll just table that discussion for until we get the accident analyses--

MR. HOTCHKISS: The safety-related --

CHAIR STETKAR: -- for loss of offsite power.

MR. HOTCHKISS: The safety-related containment protection function is accomplished by containment spread.

CHAIR STETKAR: I understand. And if it were not for the point that you made and the point that's int he DCD that says "The containment fan cooler system is designed to satisfy the following design-basis:

Maintain containment air temperature below 120 degrees Fahrenheit during normal operations and below 150 degrees during LOOP condition." If it was not for that last phrase about some requirement for LOOP, I'd better understand.

MEMBER BLEY: Well, apparently they don't need for it that purpose, so you know classify it.

CHAIR STETKAR: Bit it's specifically designed for that purpose, so I --

MR. HOTCHKISS: But if -- okay.

CHAIR STETKAR: You're following --

MR. HOTCHKISS: Yes.

CHAIR STETKAR: LOOP is a design-basis event.

MEMBER BLEY: Actually, I think we'll see it better looking in the PRA. I don't think we're going to see it in Chapter 15, because if you just lose the sprays over it, it's great.

CHAIR STETKAR: Yes, but you don't want to lose the sprays on a loss of offsite power, do you? Good God, I hope not.

MEMBER BLEY: That's right.

CHAIR STETKAR: Yes.

MR. HOTCHKISS: Really the question is you're kind of poking at is are they risk significant.

CHAIR STETKAR: And I didn't want to raise that question. I originally thought about asking that question, but that's not appropriate for this group.

MEMBER BLEY: I think that's what it's complete.

CHAIR STETKAR: And I wouldn't necessarily have asked it in this forum, except for the fact that the LOOP design function is explicitly identified in the DCD.

MR. KAWANAGO: This is Shinji Kawanago from MNES.

And this is just in our information for the design -- to get it to the rest of offsite power. And as you stated, basically it is not a safety-related requirement. However, and when actually we have the loss of offsite power and you -- and after -- and after -- after the finish and it resolves loss of offsite power, immediately linked to restart the power plant immediately so that -- and if we don't have this cooling function of the reactor vessel, cooling, CRD cooling found, and temperature will increase, I mean with over and around 150 and we needed to shape -- of the CRDM and the coil and allowing the reactor --so again, it is not safety-related --

CHAIR STETKAR: It's not safety -- it's more, if you will, investment protection type?

MR. KAWANAGO: Sure, sure, sure.

CHAIR STETKAR: Okay. Okay. That helps. That helps. Thank you. Thank you.

MR. HOTCHKISS: Okay. So that was it for containment ventilation, unless there's other questions. Actually, that concluded 9.4.

MR. CURRY: All right. Mr. Chairman,

we're going to change to 9.5 and change the team up here. So we know Mr. Otani. And we're really starting with 9.5.1, so Mr. Ron Reynolds will be the leading presenter for this. And then for 9.5.2 our technical expert will be Mr. Tanaka for 9.5.2 to 9.5.8.

MR. REYNOLDS: Are we ready? Okay. Good afternoon. I'm Ron Reynolds. I have Otani-san as a technical expert with Chapter 9.5.1.

We have, again, a list of acronyms that we an go through. I think they're fairly straightforward.

And, of course, I'll be talking on this 9.5.1.5 protection program, and we'll start with that first section.

Again, as you are all aware, that the US-APWR is a four-train, 50 percent-train system. And during the construction of the US-APWR, for me I guess I could say but I had 25 years of experience, over 25 years in the nuclear industry and worked on construction of some, and worked on NUREG-0800 type plants, and worked on the pre-1979 plants. And this is a dream come true if you look at the US-APWR how it's compartmentalized. So, it's a good backbone for a fire protection program to start.

And with that- of course, the

requirements of 10 CFR 50.48, Appendix A; the NUREG-0800, Reg. Guide 1.189; all the NFPA codes including NFPA 804 we're using those requirements and that guidance you'll probably see are very similar to most other fire protection programs in that respect.

And so the primary objective of the fire protection:

To minimize the potential for fires and explosions to occur;

Rapidly detect, control and extinguish any of those fires that do occur, and;

Assure that any fire that is not properly extinguished by the fire suppression system will not prevent safe-shutdown of the plant and will minimize the potential for radiological release to the environment.

Pretty straightforward for all fire protection programs.

The fire protection program describes:

The defense-in-depth approach. We have the detection, suppression, separation, administrative controls; all of that adds up to the defense-in-depth approach in fire protection.

The program has got:

Describes overall fire protection program for the facility;

The positions and responsibilities for the program the fire brigade, their training, the requirements, the protocol, the fire protection engineers requirements and so forth;

Interface with control room and security as well.

The program describes automatic detection and the manual and automatic suppression systems. And as I did mentioned earlier, the administrative controls are also a big part of the fire protection program, Hot works permits, transit combustible permits, and even general housekeeping is a big part of it just to maintain control of combustibles, any transient combustibles into the plant.

Many of these programmatic issues do rely, or are the responsibility, I should say, of the COL Applicant to maintain and establish those programmatic controls.

Fire protection design features for the US-APWR:

Prevent fire initiation by controlling, separating and limiting the quantities of combustibles and sources of ignition. Again, that's the same thing as saying we have fire barriers, we're going to have administrative controls to ensure that we could reduce the sources of ignition and try to contain a fire if it does occur.

And again, that goes onto the next bullet. Isolate combustible materials and limit the spread of fire by subdividing the plant structures into fire areas. No further separated into fire zones.

Separate redundant safe-shutdown components and associated electrical divisions by 3-hour fire rated barriers. That's to preserve the capability to achieve and maintain safe shutdown of the plant following a fire. First we need two trains for safe shutdown of the plant. And you could assume one train is a maintenance, we could have a fire in one train.

Preserve the capability to achieve and maintain safe shutdown of the plant using the controls external to the Main Control Room. Should a fire require the occupants of the main control to leave, we have the remove shutdown room that's completely electrically separated, it's quite a distance away. I think it's three levels from the main control isolated with its own ventilation and isolation.

Separate redundant trains of safety-related equipment used to mitigate the consequences of a design-basis accident.

CHAIR STETKAR: Ron, before you slip through this, a couple of questions. And I don't now if you're the right person to as, but I'll ask it to get on the table.

MR. REYNOLDS: Yes.

CHAIR STETKAR: How are the cables from the four safety divisions configured as they flow to the control room? What sort of barriers or separation do you have?

I mean, I haven't studied the physical layout of the plant. I'm close enough to understand whether you have, you know the traditional large cable spreading room, which I assume you may not. And if you do, what sort of barriers do you have there to prevent multi-division fire impacts?

MR. REYNOLDS: I understand.

First of all, of course you know that we have the four-trains; they're all separated by fire barriers. And even within each train, there's additional separation of fire barriers. So, it's not just one fire area per train.

And, of course, all of those cables are separated. There's no interaction to the train.

Now, the question is: How do they all

come together to the control room?

CHAIR STETKAR: Right.

MR. REYNOLDS: And that's --

CHAIR STETKAR: I've actually worked on four-train plants.

MR. REYNOLDS: And fire is an issue because eventually they have to come to one point.

CHAIR STETKAR: Right.

MR. REYNOLDS: We do have four electrical rooms that are separated for Train A, B, C and D that have fire barrier separation. And these cables will be coming up through that floor -- or through the ceiling of that room into the floor of the --

CHAIR STETKAR: So under the control room there are actually four individual rooms?

MR. REYNOLDS: There's four electrical -- electrical rooms. Yes, I don't know what the relation is, I guess they're directly under where the electrical rooms are located. They're under the control room

CHAIR STETKAR: I'm just curious, because I have yet to see a four-train plant that doesn't somehow have a place where these things come together.

MR. REYNOLDS: Well, and even with this plant as they come through, there's a portion that will have -- at this point in the design there is a portion, I understand, that will have some close proximity and would possibly need fire wrapping on a cable or a conduit containing cable.

MEMBER BLEY: This is after they come out of this electrical rooms?

MR. REYNOLDS: Yes.

MEMBER BLEY: Somewhere like under the floor?

MR. REYNOLDS: Yes. I'm probably not able to describe exactly the routing of these cables clearly. I apologize for that.

CHAIR STETKAR: Maybe tomorrow. And the problem is if we start showing building layouts, occasionally you get into safe security related issues. But there's some configuration that you could show us, it might help, you know both a planned view and an elevation view. In principle we have those someplace, because as I said I didn't have enough time myself to do some homework and I was just curious because, you know you make a point about separation by barriers.

MR. REYNOLDS: Yes.

CHAIR STETKAR: And typically, as I said, I have yet to see a four-train plant that doesn't face the problem of multi-divisions in a single space.

MR. REYNOLDS: It is one of the more difficult hurdles to overcome. And --

CHAIR STETKAR: And the only reason I ask that is if, indeed, you do have that space what in your design -- you know, how are you protecting things within your design? You mentioned five wraps, for example.

MR. REYNOLDS: Right. That would be the protection of choice would be to put a qualified fire wrap on. And my understanding is that it's a very short segment of electrical conduit that would need to have potential for that to have a fire wrap. I mean, so we would pt either a three-hour fire wrap on or a one-hour automatic suppression detection. We would meet the requirements, that would be for certain. Okay.

CHAIR STETKAR: And here I have to admit I gave up. I didn't read the complete Fire Hazards Analysis.

In some designs that I've seen, I'm talking about the fourth checkmark here about abandoning the Main Control Room and going to remote shutdown.

In some designs that I've seen the plant design facilitates a fire in the control room that requires the operators to relocate to the Remote Shutdown Room, and does that quite well.

I've seen some plants where a fire in the Remote Shutdown Room because of the way the circuits are configured, not only disables the Remote Shutdown Room but also disables the Main Control Room. And design-basis is not that people live in the Remote Shutdown Room and relocate to the Main Control Room. So, I was curious whether you know, and this is kind of an electrical question but it comes upon the purview of the Fire Hazards Analysis, whether or not you've looked at fire in the Remote Shutdown Room because it's another place where several things together, that may affect not only the Remote Shutdown Room, obviously, but because of the way the circuits are configured, disable controls in the Main Control Room.

MR. REYNOLDS: Well as I mentioned before, and I could give the answer to the best that I know because it is more into the electrical I&C area, but it is electrically separated, the Remote Shutdown Room from the, Main Control Room. And in order to isolate the Main Control Room and then initiate actions from the Remote Shutdown Room, there's a series of actions that need to take place. Of course, there's a permissive switch. And I'm being able to tell you this in a general sense that allows you to disconnect the Main Control Room and the connect to the Remote Shutdown Room. Then there is another switch that severs the Main Control Room from that and allows that complete electrical separation.

CHAIR STETKAR: And that at a high level is kind of what I was looking for in the sense that if that's true, you have to actively, let's say, activate--

MR. REYNOLDS: That's correct.

CHAIR STETKAR: -- the Remote Shutdown Room, that's fine. There's some plants that have a Remote Shutdown Room essentially continuous but online.

MR. REYNOLDS: Right.

CHAIR STETKAR: The control signals kind of go through there and out to the equipment, or an active pat of the system. And if this design doesn't do that, that kind of answers my question.

MR. REYNOLDS: That's right.

CHAIR STETKAR: Thanks. Thank you.

MR. REYNOLDS: Sure.

CHAIR STETKAR: I'm still curious to see

how that room under -- that one is still open. I'm still curious to see how the room is configured and where the cables comes together.

MR. REYNOLDS: Okay. To go on to the next slide, clarification design features. That is to prevent fire initiation, detect and locate fires and provide operator indication of the location of the fire.

Okay. The detection system is going to also provide local, audible and visual alarms for occupants of the building. We'll follow NFPA requirements.

Provide the capability to extinguish fires in any plant area, to protect site personnel, limit fire damage, and enhance safe-shutdown capabilities.

Supply fire suppression water at a sufficient flow rate and pressure in accordance with NFPA codes. And that's basically looking at our largest sprinkler demand plus our 500 gallons for water hose allowance for a duration of two hours. We'll follow that with NFPA codes for the fire pumps, tanks if they're used and the fire main.

Maintain a 100 percent design capacity for the fire pumps, assuming the failure of one of the pumps or loss of offsite power. US-APWR uses two pumps and so one is electric and one is diesel driven.

The fire protection system is nonsafety-related, of course with the exception of the piping between and including the containment isolation valves. However, there are seismic design requirements that are applied to portions of the fire protection system; that's basically the standpipe systems that are in areas containing equipment required for safe shutdown following the SSE.

Okay. The Fire Hazards Analysis. The purpose of the Fire Hazards Analysis or FHA is to:

Evaluate the potential in-situ and transient fire and explosion hazards;

Also to define the fire barrier locations;

Identify detection and suppression coverage throughout the plant;

Confirm that the effects of a fire in any location in the plant do not adversely impact the ability to shutdown the plant ore release radioactivity to the environment;

Select appropriate measures for fire prevention, fire detection, fire suppression, and containment within each of the areas that contain system structures and components important to safety.

The FHA is performed for areas of the plant containing safety-related components and for other areas. It's also for the turbine building, other areas that may not contain safety-related equipment, but for the generation of electricity.

The FHA is performed on a fire area by fire area basis in fire zones. Again, it's fire areas that are bounded by fire barriers: Floor, ceiling, walls and within those fire areas we're separating again up to five zones. It gives a better feel for the fire protection engineer in the ongoing years even, to see where the concentration even within a fire area, where these combustibles are concentrated. So that's helpful.

The approach provides confidence that the plant safety is achieved and the intended fire protection program requirements are satisfied.

MEMBER SHACK: That is curious. Whenever you do reference 1.189 in that fire thing, it's always Rev 1. There's is a current version is Rev. 2.

MR. REYNOLDS: Well, it's kind of the code, its the regulation of when we were in --

MEMBER SHACK: Okay. When you submitted this.

MR. REYNOLDS: When we submitted Rev. 1 was the -- same with many of the fire -- NFPA codes that we used for the standard plant design. Of course, as the applicant --

MEMBER SHACK: Even though you haven't received your certification yet, it goes on to when you submitted it? Oh, okay.

MR. REYNOLDS: That concludes my presentation of 9.5.1. I know we have one open question that we have to look at when we get a chance, if you want to do that.

MR. CURRY: No. If staff brings it up, we'll --

MR. REYNOLDS: Okay. Okay. That's it. Any other questions?

I thank you very much.

CHAIR STETKAR: Yes. I was just looking through. As I said, I didn't have a chance to read all of the Fire Hazards Analysis. It's a number of pages. And I'm looking at the drawings.

I see on the planned view drawings, the four electrical rooms, I know where the control room is. But there's slices between. You know, there are slices at certain elevation and I suspect that there's something in between there that I'm not seeing, just because of the way the slices were taken. So, I'm still curious about that.

MR. REYNOLDS: Okay.

CHAIR STETKAR: That's a good point, though. I will ask the staff about that.

MEMBER SHACK: Well, the staff is referencing Rev. 3, which is a really interesting one. Okay.

CHAIR STETKAR: 1189?

MEMBER SHACK: Oh, okay. One and three but not 2.

CHAIR STETKAR: Well, but the transition to two was a change -- you know, things like multiple spurious operations and how you have to consider those.

MEMBER SHACK: Right. Again, the DCD references the NEI document and Rev. 2 has a rather substantial --

CHAIR STETKAR: It does reference --

MEMBER SHACK: Yes.

CHAIR STETKAR: -- because we're on -- not on hotwire.

MEMBER SHACK: Yes, it referenced. Again, that's really left to the COL Applicant to do. But it references that document as the basis for the

COL Applicant's analysis.

CHAIR STETKAR: And that does treat the multiple --

MEMBER SHACK: Rev. 2 has some reservations about the NEI document --

CHAIR STETKAR: Rev. 2 of the Reg. Guide--

MEMBER SHACK: Right. Right.

CHAIR STETKAR: But it doesn't reservations in the --

MEMBER SHACK: And I don't know when the COLA submitted its application, so --

CHAIR STETKAR: Well, we'll sort that out.

MR. CURRY: All right. To finish up with 9.5; 9.5.2 to 9.5.8 I'd like to introduce Mr. Hideki Tanaka who is our technical expert in this area -- in these areas. So, back on the original slide, I'm not going to try to go back to that, but it indicated that 9.5.1, 9.5.2, 9.5.3 they're not safety-related functions. The support system for the gas turbine generators do have safety-related functions.

So where Mr. Reynolds left off, we'll pick up, I think, on 9.5.2 Communications Systems. There are a variety of communications capabilities outlined in the DCD and fundamental ideas that there'll at least be two methods of communicating with outside agencies and internal to the plant provided by all of these different mechanisms which I'm sure the Committee is familiar with.

So, I will move on to lighting systems.

Yes, sir?

MEMBER BROWN: This is the first time I've ever asked this question in the light of this particular discussion, because I didn't think of it; the communications issue. You list a whole list of them here, and this is not unusual for the other tank designs. But in terms of the connection of offsite communication system is it possible for somebody offsite to commandeer a communication system, hack it, and make onsite announcements the way your all system is configured?

MR. CURRY: I don't know.

MEMBER BROWN: Well, I mean if you look at it from a telephone system that goes to a telephone. I'm talking about the public address type system or the offsite communication, or plant radio systems that could be compromised. It's not hard to hack into radio systems so if could have some guy out there giving counter- information that was done -- I just threw that out. It just occurred to me.

MR. CURRY: Let me --

MEMBER BROWN: I'm not asking you. That's totally off-the-wall.

MR. CURRY: Yes, that was a sabotage-type question which I'm not sure that --

CHAIR STETKAR: It is. It is.

MEMBER BROWN: It's different from cyber because it's not on the computer, necessarily.

MR. CURRY: True.

MEMBER BROWN: Unless you've got Verizon, which you don't know what's going to happen. Oh, I'm not supposed to say that.

MR. CURRY: It's okay. They're find your phone number.

MEMBER BROWN: Anyway, it'd be interesting to have some idea of the independence of the ability to communicate public address system-wise from offsite, insite and/or the radio system. The telephone system is kind of commercial, I imagine.

CHAIR STETKAR: We just may need to be a little bit careful because we're getting into that gray area --

MEMBER BROWN: I understand that.

CHAIR STETKAR: -- if you know security-related stuff. But we can --

MEMBER BROWN: I'm just putting it on the table for discussion at the appropriate time.

MR. CURRY:

MR. KLINE: Thank you. We'll note that comment.

MEMBER BROWN: I knew that would be appreciated.

MR. CURRY: All right. Lighting systems. Lighting nonsafety-related system. We've got normal lighting, emergency lighting, emergency lights divided up into those three subsets, including the third bullet titled "Normal/emergency lighting. But that's intended to be all lighting except the Main Control Room and the shutdown area.

So, as you would expect, normal lighting is non-Class 1E, emergency lighting --

MEMBER BROWN: Let me backtrack.

MR. CURRY: Sure.

MEMBER BROWN: Because when you get to do Chapter 7 this next question will come up, and you might as well be aware that I will be asking the question then. This is on your Slide 8 where you talk about communications between the MCR and the Technical Support Center and the Offsite Emergency Operations

Facility. When you were describing the overall architecture, and you may not be doing it but somebody will be, of the I&C system, how that communicates between what I call plant MCR/TSC complex and what I call the business or corporate entity that's at the site also will be of interest. That's talking about the firewalls and things.

MR. CURRY: That's right.

MEMBER BROWN: And I know that goes into a little bit a cyber, but there's still some questions that can be asked in that vein without venturing into the whole cyber security plan. So, I'm just giving you a heads up or I've giving Mitsubishi a heads up --

MR. CURRY: Somebody.

MEMBER BROWN: -- that questions will be forthcoming.

MR. CURRY: Right. And again, the relationship and the independence of the onsite communication system from offsite sources?

MEMBER BROWN: Yes, right. I mean data moving from the site systems to other. And I'm not going to go any farther until we see the architecture layout.

MR. CURRY: Yes.

MEMBER BROWN: I mean I took a look at it real quick and it wasn't real crisp as to all that. Just one of your diagrams kind of very high level.

MR. CURRY: Okay. I think we understand the issue.

MEMBER BROWN: Thank you.

MR. CURRY: Yes. All right. Lighting, again, just to -- and we were on the quick summary of the lighting and the emergency lighting. And I think I was down to the last bullet, the normal/emergency lighting is backed up by the alternate ac power source.

If we talk about the gas turbine gas-generator support system, fuel oil storage and transfer, I should have mentioned I think -- well, we'll get to that. 9.5.5 is not applicable because the GTGs are approved, so we won't be discussing 9.5.5.

The 9.5.4, you know basically is a summary of the fuel oil storage and transfer system. And as you see, typical components. Here's your simplified drawing that follows. We have a fuel oil storage tank, seven day tank with a day tank for 1.5 hours. Redundant fuel oil transfer pumps supplying each GTG set.

MEMBER BLEY: Because they're powered off of their own GTG, the transfer pumps?

MR. CURRY: The transfer pumps? Tanaka-san.

MR. TANAKA: The transfer pumps is separated from own trained.

MEMBER BLEY: Untrained? So that -- okay.

MR. TANAKA: Yes, sir.

MEMBER BLEY: So if the generator is working, you got power for the pump?

MR. CURRY: Starting system, starting air system criterion is less than 100 seconds.

CHAIR STETKAR: Jim, I'm sorry.

MR. CURRY: Sure.

CHAIR STETKAR: Could you go back to the drawing there? Are the fuel oil storage tank rooms, they're below grade, right? Are they sealed against flooding?

MR. TANAKA: Yes. Underground.

CHAIR STETKAR: They're underground now. Are they completely sealed against flooding?

MR. TANAKA: Yes.

CHAIR STETKAR: The answer is yes? Okay. Thank you. Concern being, obviously, that they're electrically driven pumps that have to work to support the combustion gas turbine. So if the room is full of water, it's not so good, unless they're really good pumps.

MEMBER SHACK: Hermetically sealed generators.

CHAIR STETKAR: Well, no. I mean the generators can be above flood level. If you fill up the generator rooms until the day tank is dry, and then it starts to really --

MR. CURRY: Okay. Starting air, the capacity -- and I should mention this all is related to the Class 1E GTGs, and there are four of them.

Starting air capacity, three consecutive GTG starts. Each system consists of air compressors and the associated drain chambers and receivers and staging. And there's a little schematic.

MEMBER SHACK: Is there some reason you chose not to meet the SRP requirements for five starts?

MR. CURRY: We think we do. And we have some explanation for that.

I will point out we have four, four gas turbines as opposed to diesel, so fundamentally that's where the answer lies.

MEMBER SHACK: Okay.

MR. CURRY: Okay?

CHAIR STETKAR: I think we did have some discussion with that back in Chapter 8. I don't remember the answer, but I know there was some discussion. The staff asked it. There was some discussion about, you know, why 3 is good enough.

MEMBER SHACK: Okay. So we've been there.

CHAIR STETKAR: So I think we've been there.

MR. CURRY: All right. Lubrication. Lubrication system is explanatory. Probably the interesting bullet might be the last one: We do not need a keep-warm system because the lube oil is qualified under cold conditions.

CHAIR STETKAR: How cold is cold? How cold? What temperature?

MR. TANAKA: Minus 20C.

MR. CURRY: Fahrenheit?

MR. TANAKA: Huh?

CHAIR STETKAR: Minus 20C is about what? Minus 15 Fahrenheit?

MEMBER BLEY: That's about minus 5.

CHAIR STETKAR: Maybe minutes 5. Yes, about minus 4 or 5.

MR. TANAKA: But actually lubrication system is contained in the -- is kept by the --

CHAIR STETKAR: Okay. Right, right, right.

MEMBER SHACK: Minus four.

MEMBER BLEY: Minus four. I'm sorry.

CHAIR STETKAR: Okay. I'm sorry. It's all installed in the gas turbine generator room, right? Thank you.

MR. CURRY: And there's your simplified schematic.

Air supply. Typical air supply system. Conventional air and exhaust system, screens, louvers, ventilation fans, duct work connections.

And that is the end of our presentation for 9.5.

CHAIR STETKAR: Excellent. Do any of the members have any other questions, comments for MHI? We're waiting.

MEMBER BROWN: Can we go all the way back to the beginning?

CHAIR STETKAR: Yes. You have even less of a life than I do. This is great.

MEMBER BROWN: While I was multi-tasking while I didn't know what you all were talking about, or even less than what you all were talking about --

CHAIR STETKAR: Let's go back to the beginning.

MEMBER BROWN: The water level gauges and the temperature gauges, I should put under either RAI--

CHAIR STETKAR: Spent fuel --

MEMBER BROWN: Spent fuel all the way back -- way back to the beginning. This is all the way back to the beginning of time. And I just wondered, there seemed to be some inconsistencies or differences between the original design and the change you made as a result of the RAI. And then as a result of those changes, then you changed the DCD Tier 1 and Tier 2 sections appropriately, and there's some inconsistencies there. So, I thought I'd ask a couple of questions.

Number 1, before there were two level gauges, I'll talk about level first, and they annunciated a high-low and low-low water level from the MCR locally. That's what you all said in your answer. That's not explicitly stated in the DCD, but that is what you all said in your answer.

The new thing, instead of two level gauges, you say you're going to have two level switches to provide a low-low setpoint which will annunciate to the MCR locally. So I presume the gauges that monitor level have disappeared and now you just have a low-low level alone, which also not only annunciate, it also interlocks with the SFP pumps, the spent fuel pumps to trip them off or to prevent their starting if the water level is down there?

Okay. Just a difference. No gauges, and you put a local, which sounds like a local nonsafety-related, continuous monitoring gauge. And I presume that's in the spent fuel pool area. And it measures the rounds of levels, but it didn't appear to be that you had any MCR, Main Control Room indication on that. It wasn't clear.

MR. CURRY: So just to repeat, we have an action item from this morning to clarify the level and the temperature indication. And you're pointing out that there's maybe an inconsistency in our --

MEMBER BROWN: Yes, and I'm going to mention a few other ones --

MR. CURRY: Okay.

MEMBER BROWN: -- just to -- and if we're going to clarify it at some point, I thought we might--

MEMBER SHACK: Clarify it all?

MEMBER BROWN: Pardon?

MEMBER SHACK: Yes, clarify it all instead of doing it twice. Okay. So that's just on the level gauges. And I know I went faster than you could write, so don't worry; I wrote this all down.

MR. CURRY: Okay. Appreciate that.

Yes. I was just going to ask you for the references on the two items.

MEMBER BROWN: The RAI is 756-5763 Revision 3, dated August 10th. And that's your alls response to the -- your alls response is August 10th.

MR. CURRY: Of 2011?

MEMBER BROWN: Yes, 2011.

MR. CURRY: Okay.

MEMBER BROWN: And it has all the other detail as well as the original RAI in it, plus the Tier markups for the Tier 1 and Tier 2 pages.

MR. CURRY: Okay.

MEMBER BROWN: Okay? So that's on the level.

The second thing was on the temperature gauges you went from one temperature gauge to two temperature gauges Class 1E. Okay. My question on that was related to: Where are they?

MR. CURRY: Right.

MEMBER BROWN: Are they distributed within the pool somehow such that you can -- I mean, if they're both stuck in the same, it's kind of useless.

MR. CURRY: That's right. And we discussed and are pulling some detail on this.

MEMBER BROWN: Yes, that was the part of that question.

MR. CURRY: Right.

MEMBER BROWN: The level gauges where water goes up and down, so I wasn't -- maybe I should be worried about that, but I wasn't.

CHAIR STETKAR: Well, the only question that comes up is if they only alarm at low-low level, you know what is low-low level?

MEMBER BROWN: The cavitation point.

CHAIR STETKAR: Yes, that's pretty high level --

MEMBER BROWN: The cavitation.

CHAIR STETKAR: -- pretty high level in the pool. It's not a continuous --

MEMBER BROWN: I don't know where the pumps take suction, so --

CHAIR STETKAR: Pretty high up.

MEMBER BROWN: Well, that's the other

point I hadn't gotten to yet. They do have a -- there is a topical report for the thermal hydraulic analysis that says without -- boil in about 2½ hours.

MR. CURRY: Okay.

MEMBER BROWN: So, that's a number.

CHAIR STETKAR: That's for the Design-Basis heat load ten years worth of spent fuel --

MEMBER BROWN: Whatever it is, yes.

CHAIR STETKAR: -- and full core offload. But, yes, I remember that number.

MEMBER BROWN: But they also apparently trips -- the ECCS system trips the SFPs off, the load sequencer does, and it does not restart them. They have to be restarted manually. I have no idea what we do in other plants, but I don't know if that's consistent or not. The loss of offsite power trips then on under voltage, that's kind of obvious. But then the low-low setpoint locks out. And I guess my concern, because it's interlocked. Now, I'm to come with an interlock, per se, because you obviously don't want to burn up the pumps if you can help it before you have water back in there that you can do something with, but if you have an interlock failure of -- you ought to be able to override some types of interlocks. And whether that's done manually or how that's accomplished, but you ought not be permanently locked out.

CHAIR STETKAR: Charlie, you're reading or you have something that I don't think I've seen.

MEMBER BROWN: Well, this is the RAI.

CHAIR STETKAR: Yes. You used the term "locks out." Is that --

MEMBER BROWN: Used the term interlock.

CHAIR STETKAR: An interlock? Okay.

MEMBER BROWN: Okay. And when I read an interlock, to me that's an interlock for the pumps. It turns it off. If you're running the pumps and the level goes down, it interlocks them in, turns them off and they use the term "interlock" in here. So I presume an interlock means it's interlocked, you can't start them if the load is below that. And they don't talk about an override.

CHAIR STETKAR: Well, yes.

MEMBER BROWN: What if the interlock fails, you get water pump back in and now you want to run it but you can't start them? That's the point.

MR. CURRY: Right.

MEMBER BROWN: In one of your paragraphs, someone tends to look at one of your answers, it was on the discussion of the operational -- during the loss of offsite power the pumps trip off. Then you go through a scenario of 2½ hours and what it needs to do to restart them. And you talk about when the level is -- of the low level alarm setpoint, not a low level. And it looks like low-low and high have all been water level -- it looks like they've disappeared. They were in some of your previous discussions, but not in the revised one.

So I'm just saying you ought to go -- somewhere along the line you and the staff ought to come to congruence as to consistency as to consistency. And I don't know if this has been resolved yet or it's still an open.

CHAIR STETKAR: We'll ask the staff when they come in.

MEMBER BROWN: Yes. Because it's just a matter of getting consistency. I mean, I kind of piddled around with this and since I was interested in it while we were talking.

CHAIR STETKAR: Yes. So, Jim, kind of what I've taken away, there's kind of an open issue and we'd kind of at a high level we'd like to understand details. But if I can characterize it at a high level, we'd like to understand how the level instrumentation, you know the current concept of the design, how it's designed, what signals does it provide, does it provide continuous displays, where are those displays and how do the trip and interlock signals for the spent fuel pit cooling pumps interact with those levels? In other words, does the low-low level signal -- or whatever it is, trip and lock out the pump, do the operators have to reset that signal, does it reset automatically at some other level, what is it? So basically, the kind of design of those of those level signals and what they do.

And, you know less complex, but for the temperature signals at what places in the spent fuel pit are those temperature measurements taken?

MR. CURRY: Yes.

CHAIR STETKAR: Are they somewhat representative?

MEMBER BROWN: There was one other. Again, this might just be editorial. When you talked about a revision piece in Tier 2 DCD describing the temperature instruments, you talk about two temperature instruments are installed. If it's high, they would annunciate it to MCR and locally. Then you use singular temperature transmitter is provided to monitor the temperature. Does that different? Are the other ones just alarm units only? For some reason you got one that's monitoring over the range? I just couldn't -- it's just inconsistency in terminology. That's why we really would like to know what are the ranges. Are they all continuous, whether they display, et cetera? And it's a little bit cryptic as you try to dig through the tables and stuff; that's all.

MR. CURRY: Yes. Thank you. I appreciate that.

And just to clarify, the inconsistency in terminology within the RAI response or are you comparing to some other --

MEMBER BROWN: I'm comparing here. What you all -- you're very clear. Okay. Your answer went through a discussion of what you had and what you were going to change to in the discussion. Then you provided an impact on DCD write-up which showed what changes you were going to do to the DCD to incorporate your discussion part of the write-up of what you're going to do. So, there's some inconsistencies between them, and it looks like you went from level gauges to just level switches. And there's only one local continuous monitor, and that's in the spent fuel pool within the reactor building.

CHAIR STETKAR: I mean, some of it if we had a better understanding of what the current design really looks like, some of that might --

MEMBER BROWN: And my personal interest is that we get something laid down fairly concretely so that two different people looking at the designs can interpret it such that you don't end up with what we really thought we were getting in the end. So, you don't have to say what they are, but what are they supposed to do and how many of them, and where are they. Okay. And where they indicate and annunciate, et cetera.

So, that was overall -- thanks for bearing --

CHAIR STETKAR: You want to go to like page 2 now?

MEMBER BROWN: No, that's it.

CHAIR STETKAR: Any other comments, questions by any of the Members? If not, I like to thank MHI, MNES and Holtec in their absence for what I think a really, really good discussion. Good presentation. We'll probably have more discussion late, you know tomorrow if we get some of the questions answered in kind of a real time.

But I'd like to thank you very much. I thought it was a well structured presentation, and I think we had a good discussion.

And we will recess until 3:05, and then hear from the staff.

(Whereupon, at 2:49 p.m. off the record until 3:08 p.m.)

CHAIR STETKAR: We are back in session. It's time to hear from the staff.

Paul?

MR. KALLAN: Okay. Thank you.

My name is Paul Kallan, again.

CHAIR STETKAR: I'm sorry. Do we have your handouts? Thank you.

MR. KALLAN: All right. Now this is the presentation to the Subcommittee on Chapter 9 for the Safety Evaluation with open items.

Just quickly, the staff team it's the staff that will be presenting today is Larry Wheeler, and he's a reactor systems engineer. He'll be going over 9.2.1 and 9.2.2.

Angelo Stubbs, he's a senior reactor systems engineer and he'll be going over DCD Section 9.2.6.

And David Nold, he's a reactor systems engineer and he'll be going over Sections 9.4.1 and 9.4.5.

The Lead Project Manager is Jeff Clocco, and he's not here today. And I'm just basically running the show.

Slide 3 and 4 is just the staff team. There's a large number of staff that worked on this document. And so I just listed them all in there.

Slide 5 is a table that basically what I did is I put the SRP, the section, the number of questions and the open items that related. And I think I'm not going to go over each section, but I just wanted to make sure that we listed all the sections with the open items and the questions, the amount of questions we get for each section.

There was approximately on Slide 10, we had 603 questions and 20 open items. We decided that staff wanted to only talk about certain significant open items which we're going to be presenting today that were of interest to the ACRS. And we're not going to go over all 20 of them.

And with that, I'm going to go to Slide 11 and turn it over to Larry Wheeler.

CHAIR STETKAR: Actually, Larry, no you're not. Because you're not going to skip over the fuel pool stuff, but we -- at least I have some questions about it. So, I hope you have somebody here to answer them.

In SER Section 9.1.3.4 under GDC 61 there's a statement that says DCD Tier 2 Section 9.1.3.1 Design Basis states that the spent fuel pool pit -- I'm sorry, cooling system is designed to maintain the water temperature below 48.9 degrees C, 120 degrees F with a newly operated half core and a fully loaded spent fuel pool with a single active failure preventing the use of one cooling train. With the additional capacity the residual heat removal system an entirely newly off loaded core can be handled without the water temperature rising above 60 degrees C, 140 degrees F. This also accounts for the possibility of a single active failure, therefore the spent fuel pool cooling system design meets the recommendations of SRP Section 9.1.3(iii)(1)(D).

And I'm not going to do the quote from the DCD because that's even longer. But if I read the DCD and read your statement, they're not consistent. And the reasons that they're not consistent are that the DCD seems to say that with a fully loaded spent fuel pit and the head load from a newly off loaded partial core, it can maintain -- the spent fuel pit cooling system can maintain spent fuel pit temperature at 140 degrees with a single active failure. You say a 120.

And I'm not sure about the other conditions with full core.

So, I'm curious about whether the conclusions of your analysis about what a single active failure is and what the temperature would be, because the statements in the DCD and the statements in the SER don't seem to be consistent. Now I'm not concerns about boiling here, but I'm concerned about is there a consistent understanding of the conditions. And quite honestly, I had to craft myself a little table that said if I have a half core or a full core and how many trains of spent fuel pit cooling system do I have running, what is the resulting temperature. And from the DCD I get one train of spent fuel pit cooling, what half core gives me 140. You say 120. And then I'm not sure under the full core conditions what a single failure means because I'm not quite sure how many trains are RHR and core spray are accounted for.

So, I'm not sure if you have anybody here to address that part of the --

MR. HERNANDEZ: I'm really here from the spent fuel pool.

CHAIR STETKAR: Give your name first.

MR. HERNANDEZ: Yes. My name is Raul

Hernandez.

You gave a lot of quotes there, so I'm going to ask you in a break give me the exact system failures, the exact areas of your scenario, so I can look it up and give you a straight answer.

CHAIR STETKAR: Yes. Let me give it to you on kind of the record here. It's Section 9.1.3.4 of the SER. Because my recollection is that that's a long section. It's under GDC-61. And the corresponding section of the DCD is .1.3.1.

MR. HERNANDEZ: Okay.

CHAIR STETKAR: And so you may want to go look at those.

MR. HERNANDEZ: Basically right here we're talking about the normal offload scenario, that one is the partial offload --

CHAIR STETKAR: Okay.

MR. HERNANDEZ: Maybe you weren't here when we discussed the full core of load we consider like the abnormal emergency scenario.

CHAIR STETKAR: That may be the way you think about it, but this morning I asked MHI the question about what is the practice in Japan, and currently the practice of many plants in the United States is for every refueling outage they offload the whole core. So therefore, the normal condition is a full core sitting in the spent fuel pit for some period of time.

MR. HERNANDEZ: And many designs are like that, but the way it was presented on the DCD the normal offload is like partial, the way that it was presented in the DCD.

CHAIR STETKAR: Okay. I guess we need to get clarification of that because I don't think it makes any difference -- I don't know. I mean, in terms of decisions about adequacy of cooling systems, except for the fact that it's fairly clear that if you have a full core offload, you need to supplement the cooling with at least one train of contain the spray RHR.

MR. HERNANDEZ: Yes.

CHAIR STETKAR: So that enters the mix. Apparently the normal spent fuel pit cooling system, even with both trains, I don't know what the temperature is with the full core offload. And if, indeed, the normal practice will be to offload the full core during every refueling outage, those then become the normal success criteria for the compliment of cooling systems. Follow me? I mean if that's the way the plant will do business is to offload the full core, that in my mind is the normal way to offload.

Okay.

MEMBER BROWN: Which part of the DCD did you read?

CHAIR STETKAR: 8.1.3.1.

MEMBER BROWN: Well, I looked at 9.1.3.3.1 and it looked like that was maybe even inconsistent within the DCD. But --

CHAIR STETKAR: I didn't try to look for consistency within the DCD.

MEMBER BROWN: Yes. It says in case of a single SFPS cooling system failure, one SFPS pump and one heat exchanger in service will maintain a temperature below 140 with a half core offload. That's with one spent fuel --

CHAIR STETKAR: And that's what I got. Sorry.

MEMBER BROWN: Then it goes on with a full core offload you have to have one train plus two RHRs or two trains and one RHR --

CHAIR STETKAR: Right.

MEMBER BROWN: -- at 140.

CHAIR STETKAR: Right.

MEMBER BROWN: So the numbers stayed the same, whereas if you look the SER they had a number like 124 or --

CHAIR STETKAR: Right. The DCD, as far as I could tell, hung together consistently. It was the SER's quoted configuration and temperatures didn't seem to --

MEMBER BROWN: For the half core looked to be --

CHAIR STETKAR: For the half core seemed to be low and --

MEMBER BROWN: But they didn't use just the -- they said "a newly" -- that's where the SER was fuzzy. So it says "Designed to maintain water temperature below 120 with a newly offloaded half core and a fully loaded SRP with the single failure." And the DCD didn't talk about a fully loaded SRP. It just talked about a --

CHAIR STETKAR: Well, all the conditions are done with a fully loaded --

MEMBER BROWN: Okay. It just stated --

CHAIR STETKAR: That's ten years of spent fuel, basically plus whether you have the half core

MEMBER BROWN: That's fine. That just quoted the standard assumption then.

CHAIR STETKAR: Anyway, if you could go back at that. The key is a single failure of what and what temperatures apply under what core loading, you know fuel pit loading conditions.

As I said, it's not a concern in terms of fundamental safety. It's a concern of making sure that the staff and the applicant are both understanding all of these combinatorics accurately.

MR. HERNANDEZ: Yes. It's not a limiting condition, but it's a consistency issue, I understand.

CHAIR STETKAR: Right. Right. Okay.

Let's see. Do I have any more on -- yes, I do.

MR. KALLAN: Do you have any other questions?

CHAIR STETKAR: Yes, I do and I'm not sure -- you know, this is curiosity. There was a confirmatory item. Charlie brought it up earlier and I was going to wait to ask you.

We know that the spent fuel pit cooling pumps are not automatically reloaded onto the Class 1E buses. They must be loaded manually. And apparently under the design loading conditions, apparently there's a time window of about 2.7 hours to restore spent fuel pit cooling before you start to boil starting from the minimum level conditions.

And there's a confirmatory item, 8.1.3-8 that apparently addresses sort of design related things.

I don't see any COL information items, and I don't know how those things work about specific procedural guidance so that the operators know that they need to do this. And the reason this is curiosity is I don't know what level of -- I know the plant has to develop emergency operating procedures. I'm presuming that they would capture this, but sometimes presuming is dangerous.

MR. HERNANDEZ: This item came about of having a lost of offsite power coincident with a LOCA. That was the condition that initiated this scenario. You have a LOCA and a loss of offsite power at the same time. That's more than the sequencing for the ECCS kicks in and the spent fuel pumps were not in that sequence. That was exactly the thing.

I'll ask the applicant on a RAI to clarify why the pumps were not loaded --

CHAIR STETKAR: Yes.

MR. HERNANDEZ: -- in the sequence and they credit the -- it's not a timing issue. There is plenty of time; that's where you see the two hours for maximum heat load. And then we asked them if that's the approach that we're going to take, that they get plenty of time, how are they monitoring the conditions? And that's where they upgraded the temperature and that would indicate a --

CHAIR STETKAR: Safety redundancy.

MR. HERNANDEZ: -- a safety redundant level.

In the RAI response they mentioned that the operator in the control room checks the level on the spent fuel pool before initiating the pumps again. If makeup is needed, they can initiate that from the spent fuel pool.

The description of the procedure is, it wasn't lengthy or complicated, it was simply a couple of actions. But I understand why you're asking that.

CHAIR STETKAR: Yes, and a couple of questions since you've obviously looked at this in more detail than I have. Is it only under the, let's call it a LOCA plus loss of offsite power condition where the spent fuel pit pumps are not reloaded? In other words, suppose I just have a loss of offsite power? Are the spent fuel pit pumps reloaded onto the gas turbines for only a loss of offsite power?

MR. HERNANDEZ: It's my understanding that they are, yes.

MEMBER BROWN: And again, that's not clear from reading the --

CHAIR STETKAR: Can I get somebody from MHI to confirm that?

MR. HERNANDEZ: They are powered from a Class 1E power, so it's just in the scenario that it wasn't that they specified that they had this loaded sequence in the spent fuel pool --

CHAIR STETKAR: Okay. They had a couple of loaded sequences.

MEMBER BROWN: Okay. You're in loss of offsite power, the SFP pump will trip under the LOCAs and then will not be automatically reactuated by the sequencer?

CHAIR STETKAR: That would be pretty clear. Thank you. So therefore, I don't care about the coincident LOCA. I care about anytime I lose offsite power, I lose --

MEMBER BROWN: But there's that point: There was an inconsistency between the DCD --

CHAIR STETKAR: Yes.

MEMBER BROWN: -- within the DCD and they clarify that and they came back and said "Oh, no. This is the way it is. And so they rewrote it and that was the proposed change to 9.1.3.3.1

CHAIR STETKAR: Okay.

MEMBER BROWN: And also the ECCS also

trips them off in the load sequence.

CHAIR STETKAR: Yes, I mean that makes sense.

MEMBER BROWN: The header for loss of offsite power didn't make a lot of sense.

CHAIR STETKAR: So now I understand, you know when they don't work and I understand that we have safety-related instruments. My question is I don't know because I haven't been through enough of these at what level -- what trips the staff concerns about COL information items? In other words, there are no EOPs for this plant. The EOPs are the responsibility of the COL Applicant.

One can take the approach of presuming that people write the EOPs perfectly or one can flag things that ought to be considered by the COL Applicant. And I don't know what the staff does in those issues.

In other words, simply have safety-related instrumentation, simply having the ability to close a switch, everybody always likes to take credit for the operators always doing a perfect thing at the perfect time because they have perfect information and perfect knowledge. We know better now. They don't, unless they have training procedures to tell them that they ought to be concerned about these functions.

So I think what I'm asking from the staff is ought there be a COL information item to flag the fact that instructions for restoration of spent fuel pit cooling should be integrated into their emergency operating procedures, or is that simply a presumption?

MEMBER BROWN: Well, with the change in the level indication there's only one level indication. The others ones are switches now as opposed to gauges. So I don't know how the Main Control Room operators is going to know unless there's somebody out in the reactor building, if that's where it is. That's why we've asked for the clarification.

So all we've got is the annunciator having told him there's him there's a low-low level alarm. It's not on, so you can manually restart the pump if he knows to do it.

CHAIR STETKAR: If he know to do it?

Okay. Well, I'm not hearing anything back, so I'll just -- and I'm not necessarily proposing that -- you know, we don't propose anything. I'm just sort of raising the generic question that as you go through these reviews and you identify in this case a function that relies completely on operator action, is it the presumption that the procedures will know that and take care of that simply because people say "Well, it's really easy to do" and they'll have a lot of indications available, and there's a couple of hours available to do it? And that's kind of a generic question to the staff.

MR. HERNANDEZ: I don't have an answer for you right now.

CHAIR STETKAR: I think the point has been made.

This is kind of a minor thing, but again it's a question about kind of consistency. This talks about there is some concerns about the time and capability to clean up the spent fuel pit and the RWSP. And apparently this comes back to, I guess there's some 72 hour time limit required by ANSI/ANS 57.2 Sections 6.3.2.10. Something I'm intimately familiar with, I guess.

So there is analyses done here that says that the purification stream is designed for -- I'm not going to quote the thing, but 265 gallons a minute. And if you take the total volume of the refueling water storage pit plus the volume of the spent fuel pit, it says you can pump that water, circulate the entire volume once in 64 hours. And then the SER goes on to say that since there are two independent streams, the entire system could be processed in about 32 hours. And all of that is true except for the fact that there is a pinch point in the system where there is a single pipe where you come back from the two purification streams, go through a single pipe and then go back to the two refueling water storage pit recirculation pump.

So, the question is is that pipe big enough to actually pass twice the flow rate? If it isn't, you know your assertions about 32 hours about 32 hours don't quite hold because they're not two completely independent parallel trains. They are on both ends of this single pipe systems.

So, I'm wondering if you thought about it? It doesn't make any difference, because even with a single train, you get under the 72 hour magic number, which apparently is important.

MR. HERNANDEZ: That is --

CHAIR STETKAR: But if that 32 hours is something that you used in your decision as confidence of additional margin, that may be an artificial level of confidence depending on the limitation flow through that common line

MR. HERNANDEZ: I cannot answer that

question. That is reviewed by the Chemical Engineering Branch, is a different reviewer who looks at that aspect, at the purification portion of the system.

CHAIR STETKAR: Okay. Take that away. I'm just searching for things where the SER may -- and I want to make sure that the SER doesn't impart an artificial sense of confidence or margin where that margin may not be available. Okay.

IF you're looking at it, the reference section of the SER is 9.1.3.4 under the chemistry stuff. It's GDC 14 and 16. Okay.

Bear with e here. I've got too many pieces of paper.

This again, there's statements, they sound like petty things, but again these are public documents that indeed express our level of understanding and review. And in SER Section 9.1.4.4, which is light load handling system, but it's in particular reactor cavity sealed, and I don't know who was responsible for that Apparently there's shuffling going on. And while the shuffling goes on -- this statement says "The staff evaluated the RAI response and determined that the refueling cavity and connected openings are designed with features that preclude the rapid draindown of the reactor cavity. The staff also determined that any refueling cavity leakage will be less than the available makeup capability."

Now, the staff has made this determination. I didn't find that statement anywhere in the DCD, I looked for it; that's why I didn't ask MHI.

I'd like to understand how you determined that any, meaning any possible refueling cavity leakage will be less than the available makeup capability. I'd like to see the supporting analysis for that.

You probably don't have it available, so if you can find it, we'd like to see it.

MR. KALLAN: No.

CHAIR STETKAR: Well, it says "The staff determined that any refueling cavity leakage," so you must have looked at all the leakage pathways, the possibility that they can be opened and compared them to the makeup capability, and there must be some justification for that. I'd like to see it, or perhaps that statement is a bit overstating the real world. Okay.

Let' see -- now, heavy load handling system? Suddenly there's a sigh of relief and the pitter-patter of feet running out the back.

And I had a question. The basic question I had is that I think you had some question RAIs about the scope of the heavy load handling cranes that were evaluated. Initially, I think they talked about the Polar Crane and the Cask Transfer Crane. And there might have been one more, I've forgotten. And they, indeed, you know added a number of local cranes' place, whatever you want to call them, to that list and addressed those.

The DCD tables specifically, and it's Table 9.1.5-3 in the DCD addresses cranes in place installed over safe shutdown equipment. And one of my questions is in the SER, and this is the SER Section 9.1.5.4, there's constantly in my mind this question about what our SSCs important to safety versus safe shutdown equipment. In particular, I'll ask you I'm assuming that there's a very large overhead crane in the turbine building, and are there any SSCs important to safety, not safe shutdown, not safety-related, but SSCs important to safety in the turbine building that could be damaged by drops from that crane?

MR. CURRAN: This is Gordon Curran from Balance of Plant.

I think that was an open item that they had earlier where they were discussing where you asked if there was any safety-related equipment in the turbine building, if that's what you're asking.

CHAIR STETKAR: No. I'm getting a little broader than that because it's this notion of -- I did ask that question, and I believe -- and I heard that there is an open item on that. In some sense, I'm asking about what is the -- you're going to quote directly from the SER. In its response, dated May 25, 2009, MHI referenced UAP-HF-09260. "The Applicant acknowledged the need for more detail on the cranes and hoists installed where load drops could result in damage to SSCs important to safety. Included in the DCD is Table 9.1.5-3 Cranes and Hoists Installed over Safety Shutdown Equipment identifying cranes and hoists including their respective seismic category and single failure proof status."

My question is, is important to safety in the staff's mind equivalent to safety-related and equivalent to safe shutdown?

MR. CURRAN: Safe shutdown equipment?

CHAIR STETKAR: Right.

MR. CURRAN: Yes. I was writing as if there was no components that would be effected by a drop -- excuse me. No safe shutdown equipment that would be effected by the drop in the turbine building.

CHAIR STETKAR: Okay. Okay. I understand that now. That's a bit different, though, then there have been numbers of discussions about the issue of SSCs important versus -- and for example some safety-related equipment may not be considered safe shutdown equipment. So we're really talking about kind of three categories of equipment here.

Safe shutdown is typically something that in a deterministic analysis somebody identifies as this is my minimum compliment of equipment that's required to achieve safe shutdown.

Safety-related has to with the -- you know, it's actually a broader set of equipment that's required to satisfy the Design-Basis Accident Analysis.

And then I see this in several staff reviews, is this issue of SSCs important to safety. And the only reason I bring it up, it's not a semantics issue; is that as part of the Design Certification there will be developed a Design Reliability Assurance Program. And that Design Reliability Assurance Program will have a population of SSCs in it. And those SSC are sometimes they're called risk-significant, sometimes they're called important to safety, but it's more than the safety-related equipment. It's a set of nonsafety-related equipment that's for a variety of quantitative and qualitative issues that's determined to be important enough to safety that it requires additional assurance of its reliability, typically through the Maintenance Rule PRogrma. And I want to be sure if, for example, that there's something in the turbine building that makes it onto that D-RAP list, do we then need to worry about dropping really heavy loads onto it?

And I don't know. As I said, I'm not familiar enough with how the whole review process goes. But that's sort of the genesis of my question.

And I understand now a little bit about what you were doing a little bit better. And I don't know what the D-RAP list is yet, because I don't think we've seen it and it may not exist yet.

So leave that as kind of a question. I'm not sure how you approach that yet, because it's one of these sort of integration issues that we don't necessarily identify equipment that requires additional scrutiny for its reliability, but then ignore the fact that it might be damaged by other things.

Okay. Let's talk about Essential Service Water.

MR. WHEELER: Okay. 9.2.1.

Good afternoon. My name is Larry Wheeler with the Balance of Fleet Branch. Let's talk about 9.2.1, Essential Service Water.

MHI previously described the ESW system. That design included the conceptual design of the four-trains of ESW, blowdown, strainer backwash connected to a common safety-related header. One isolation valve, the AOV-577 provided the safety-related to nonsafety-related boundary to the circulating water blowdown main header.

During the review of the Comanche Peak COL application it was discovered that neither of the COL Applicant nor the DCD Applicant had adequately described the power supplies, the I&C logic, the failures and effects analysis for this boundary. So we kind of got on the phone, we talked about it and decided that an RAI would go to MHI and DCD, and they would evaluate the AOV-577 and give us additional information.

CHAIR STETKAR: So essentially the DCD owns that valve now, is that the way to understand it or am I -- it's not quite that simple?

MR. WHEELER: I would say that the COL Applicants determine whether that conceptual design information applies to them.

CHAIR STETKAR: Okay.

MR. WHEELER: And then they get design description.

CHAIR STETKAR: Okay. Okay.

MR. WHEELER: That's why I was hoping that Comanche would pick this up. But during the phone call --

CHAIR STETKAR: Yes, it's right at -- yes. I read that.

MR. WHEELER: Because that AOV is described in the DCD under the thermal effects analysis, it kind of drowns out the DCD.

CHAIR STETKAR: Yes. Okay. Okay.

MR. WHEELER: But then North Anna has decided not to use that valve, so that's another story.

CHAIR STETKAR: Okay. But essentially if I understand it, you're saying that the functional requirements for that valve if it exists, are specified in the DCD?

MR. WHEELER: That's correct. It should--

CHAIR STETKAR: Whether or not somebody actually uses the valve or has that configuration as part of the COL --

MR. WHEELER: Because the DCD --

CHAIR STETKAR: -- but if they do have something that looks like that, they need to meet those functional requirements?

MR. WHEELER: The conceptual design I believe.

CHAIR STETKAR: Yes, conceptual design. Okay.

MR. WHEELER: That's all I have on 9.2.1. I'm going to go on to 9.2.2. What I'd like to do, Mr. Chairman is talk about 9.2.1 and 9.2.2, then talk about some of the questions you had from the staff from this morning. And then I can turn that on to Angelo.

CHAIR STETKAR: Okay. I know you'd like to do that. You're probably not going to be able to do that.

MR. WHEELER: Okay.

CHAIR STETKAR: The reason I wanted to flip ahead is I didn't know if you had a slide on of the ultimate heat sink, and you don't.

MR. WHEELER: I do not.

CHAIR STETKAR: So I'll bring it up under the Essential Service Water System.

I asked it this morning, and if you're going to address it later as pat of the plan, this notion of why 30 hours for an ultimate heat sink and 36 hours for a cooling pond.

MR. WHEELER: You mean 30 days or --

CHAIR STETKAR: I'm sorry. Days -- days. I can't read my own writing. Were you going to address that later?

MR. WHEELER: Yes.

CHAIR STETKAR: Okay. Good. I'll wait then and you can continue with your plan.

MR. WHEELER: Okay. Moving on to 9.2.2 Component Cooling. Of course, MHI previous described the CCWS system. That design includes a 3100 gallon surge tank between the CCWS trains. The CCWS train or pumps take a section from that common surge tank, and there's no safety-related make-up to that surge tank. In addition, there is no automatic valves that separate the trains out during an accident.

There are plant conditions in which bulk CCWS pumps coming off the common surge tank may be operated at the same time, unless for example during a plant startup and cool down.

The CCWS system is considered a moderate-energy system. A pipe break in the moderate-energy system has potential to draw in the common CCWS surge tank. Details of the postulated pipe break and the common CCWS header has not been adequately addressed by MHI, thus this is an open item.

We did receive the RAI response at the beginning of this month. The staff is still looking at the evaluation of that RAI response. It looks favorable that we'll be able to close this item out.

A little bit of the details of the RAI response is if the stress level for a safety-related Class 3 component, if the stress levels are low enough below a threshold, you don't need to postulate a pipe leak. And that's still being reviewed by the staff.

CHAIR STETKAR: Okay. They're going to take the approach that you don't have to postulate it?

MR. WHEELER: You don't have to postulate it if the stretch levels are below a certain value.

CHAIR STETKAR: Well, that make sense, but I'll have to see.

MR. WHEELER: Yes. Of course, that's different than high energy line break.

CHAIR STETKAR: I'm sure. That's right.

MR. WHEELER: So that closes the 9.2.1 and 9.2.2 discussions. So what I'd like to do is kind of get over some of the items from this morning. And one of the items to the staff that I had heard was the DCD roughly versus this interim Rev. 4. What happened was the staff had asked MHI for an interim Rev. 4 to simplify the staff's the SER on the safety-related systems. And this kind of follows suits with what we did on EPR.

CHAIR STETKAR: Yes.

MR. WHEELER: For some of these four safety-related systems, the staff generated over 150 RAIs. So for the staff to go through and talk about 150 RAIs through the SER would be very confusing.

When I started off doing the EPR 9.2.2 review, the SER turned out to e 120 pages. And by going on this type of concept, being able to shrink that SER down to less than 20 pages. So that's a little explanation of why the interim Rev. was so important to the staff. It shortened our review and OGC's review and, obviously, your review.

MEMBER BLEY: Yes. I would say we appreciate it too, but there were some other design similar so that every time you'd raise a question, it had already been solved. So thank you.

MR. WHEELER: Yes. The other question that I picked up from this morning is related to this cross-typing of CCWS trains that these NOV 7 series and 20 series valves. Originally I think in Rev. 2 that these valves got local signals to close and you'd have separation A and Train B, C and C and D.

Because the concerns with the loss of flow to the thermal barrier, this was MHI's design approach to ensure flow to the thermal barrier, but it causes other issues. And at the end, the train separation.

So for this issue there is a COL information item, 13.5.6. And there's operator action that's required by the COL to address isolating the trains within 24 hours. And in my SER there's a kind of a discussion about where the 24 hour came from the discussion was related to a SECY paper.

The other question that you had was --

CHAIR STETKAR: Can I stop you --

MR. WHEELER: Sure.

CHAIR STETKAR: -- because I want to follow-up on that a little bit. First of all when I asked the applicant this morning about the change to the design, they essentially said "Well, it was initiated because the Standard Review Plan says that you shall not have any automatic isolation for the CCWS flow to the reactor coolant pump thermal barriers. Is that true? I mean is that explicit that the--

MR. WHEELER: That is very clear in 9.2.2 SRP.

CHAIR STETKAR: Mm, okay. Even if I had the smartest, best designed automatic isolation signal, I have to rely on operator actions?

MR. WHEELER: The concern is, for example, the APR design CCDS is nonsafety, so you totally are relying on CCWS for seal coolant.

In this case CCDS and component cooling are both safety-related, so they're complimenting each other.

CHAIR STETKAR: So for a better design, I still because of a regulatory Standard Review Plan but the onus on the operators to save the day?

MR. HAMAMOTO: Hossein Hamzehee --

MR. WHEELER: I don't understand saving the day for --

CHAIR STETKAR: You know, I'm going to get to why they have to close these valves. I just sort of am curious about why the NRC -- it's interpreted that the NRC says certain functions shall be performed by the operators even, you know regardless of the design, regardless of how the signals might be designed and automated; that this is something that the operators, yet another thing that we need to burden the operators with.

MR. HAMAMOTO: Let me just clarify this to give you a detailed technical justification. Maybe later on we can do that because within this SRP as Larry said, but again this SRP also says this is the guidance preference. However, the applicant can propose other designs, but then they have to justify why they believe it's better and safer. And then the staff will review and either approve or disapprove.

CHAIR STETKAR: And I'm glad you put that on the record. Thank you.

MR. WHEELER: The Rev. 2 design for this system, had those valves gone closed and there was an operator action within an hour to re-establish CCWS flow to the thermal barriers, but that resulted in a whole bunch of other questions about water hammer. So this design was their fix for what the SRP says. Of course the SRP is guidance.

CHAIR STETKAR: Right. I thought about the Rev. 3 design and there was some fairly clever things that they put in the Rev. 3 design for isolating those lines. I didn't think much about water hammer.

MR. WHEELER: Yes.

CHAIR STETKAR: And a bit of my concern is that people get focused on specific issues. It's like the reverse flow through the drain line; that you try to make things perfect for one issue and, perhaps, not so good for more likely things.

MR. WHEELER: Okay.

CHAIR STETKAR: So protection against water hammer is certainly something that we need to think about. Burden on operators in also something that we need to think about. And I recognize that there was a need for --

MR. WHEELER Okay.

CHAIR STETKAR: -- the operators to restore cooling, you know if it was isolated automatically. So there may not be a design that completely removes the operators, you know the perfect design, if you will. But I'm trying to understand this notion of on the one hand the applicant perhaps taking an expedient approach because it's consistent with the SRP --

MR. WHEELER: Yes.

CHAIR STETKAR: -- for a particular issue that may be focused on water hammer, and yet introducing perhaps some additional burden on the operators which may not necessarily be in the best interest of overall, you know plant response.

But at least you've answered the first part of my question about the SRP. So I understand that a little bit better.

Now, I read the story, I didn't read the SECY papers; I didn't have enough time. But explain to me what the magic 24 hours is.

Now the current design says that they need to manually close those isolation or cross-tie valves, whatever you want to call them, the 7 and the 20 valves. In the DCD it's left nebulous under accident conditions. You know, basically determined by the operators.

MR. WHEELER: Right.

CHAIR STETKAR: In the SER there is this notion of they have to be closed within 24 hours based on a SECY paper.

MR. WHEELER: Right.

CHAIR STETKAR: What's the basis for that 24 hours?

MR. WHEELER: That was the proposal from MHI to use the 24 hour and use up. The SECY paper and the staff looked at that as being reasonable. The separation that I see, I only see two conditions in which we're really going to need to define the separation.

And the first one is when you have maintenance. If you have a Train A that's out and you want to keep B running, you obviously would isolate the A and the B side.

Two is if you have an accident signal and one pump is running and the other one's in standby, and the second pump actually comes on during the safety injection signals, and now you got two pumps running. And then, for example, A or B trips. So now you have one pump trying to supply the B loads, the common header loads and then it's also trying to support flow to the alpha ECCS loads.

And we asked MHI to evaluate whether there would be a degraded condition for the heat load and the pump's flow. And they came back and said that there was adequate margin in the heat exchanger, that's a plate-type heat exchanger. They had about a 20 percent margin in the heat exchanger. And that there was adequate flow in the pump; and I think it's somewhere in the five to seven percent range.

So right off the bat they said even if this scenario happened which both pumps were running and then one trips, you're supplying flow to the opposite header, do we have margin?

CHAIR STETKAR: Well --

MR. WHEELER: So then we looked at that and said "Well, okay. That's good that we have this margin, but let's put some type of time table of when it'll be a good idea to actually make that separation to get away from using that margin in --"

CHAIR STETKAR: Before we talk about the good idea and the time, I want to make sure that I understand the design and what you said earlier. And let me say it back so that I can actually see if I understand it.

Are you saying that they've done an analysis that shows if I have one pump running, let's call it the A pump --

MR. WHEELER: Yes. Right.

CHAIR STETKAR: -- supply flow now in parallel to all of the Train A loads --

MR. WHEELER: Right.

CHAIR STETKAR: -- all of the Train B loads.

MR. WHEELER: Right. Yes.

CHAIR STETKAR: -- now safety loads and the common header, the A1 common header --

MR. WHEELER: Yes.

CHAIR STETKAR: -- with the A2 common

header isolated --

MR. WHEELER: Right.

CHAIR STETKAR: -- that I'm okay?

MR. WHEELER: You're okay. That's in the SER.

CHAIR STETKAR: Fine. I thought I understand that, but good.

MR. WHEELER: Yes. But keep in mind the biggest flow on the opposite header would be to the RHR heater exchanger.

CHAIR STETKAR: Yes.

MR. WHEELER: And that valve hasn't opened.

CHAIR STETKAR: I'm sorry, it has if I've had a LOCA, hasn't it?

MR. WHEELER: But that system is just isolated.

CHAIR STETKAR: It has?

MR. WHEELER: Let me backup. I'm trying to remember in the RAI response, MHI took credit for that valve not being opened.

CHAIR STETKAR: Ah, well that's special.

MR. WHEELER: And maybe they looked at it at a range of failures that maybe is not complete.

CHAIR STETKAR: I mean, that's right. In

the initial scenario -- what got me thinking, and the reason I wanted to say it back is your scenario said well suppose I have a condition where both pumps come on--

MR. WHEELER: Yes.

CHAIR STETKAR: You know A and B on, and let's call that call that a LOCA.

MR. WHEELER: Okay.

CHAIR STETKAR: Or a steam line break, or you know some ECCS actuation thing. Let's call it a LOCA where you actually need heat removal. And then pump B trips.

MR. WHEELER: Right.

CHAIR STETKAR: You know, well the outlet -- I haven't looked at all of the logic diagrams and things. Will the outlet valve from the Train B heat exchanger then go closed or will it stay open? You know, can you get into a configuration where have an ECCS actuation signal --

MR. WHEELER: Yes.

CHAIR STETKAR: -- such that Pump A, let's call it, are supplying flow to all three of those lines --

MR. WHEELER: Right.

CHAIR STETKAR: -- you know with heat

being removed from both the A and B heat exchangers --

MR. WHEELER: Yes.

CHAIR STETKAR: -- or not only, you know just the component cooling, from all of the Train A and B ECCS loads, the pump coolers and all of that other stuff out there.

MR. WHEELER: Right. I think there's check valves that are going to prevent flow from the B side to go back through the alpha heat exchanger, so you're not going to get flow to that heat exchanger. Was that your question?

CHAIR STETKAR: No. If I just take a single pump --

MR. WHEELER: Yes.

CHAIR STETKAR: -- and connect it to --

MR. WHEELER: Yes, I got the flow diagram right in front of me.

CHAIR STETKAR: Yes. Okay. Well, let me find my flow diagram so that I can -- I've lost it.

Can I come to an alignment if I'm looking at Sheet 1 where the A component cooling water pump is supplying flow through the A -- what's called on the drawing the A supplied header --

MR. WHEELER: Yes.

CHAIR STETKAR: -- the A1 supply header -

-

MR. WHEELER: Yes.

CHAIR STETKAR: -- and the B supply header--

MR. WHEELER: Yes.

CHAIR STETKAR: -- where the heat loads on the A supply header and the B supply header are all running? In other words, the pumps that are cooled, the chillers that are cooled and the -- I'm sorry, not the chillers because this is CCWS. And the heat exchanger, you know like the RHR heat exchangers. Because all of those kind of come back together into the common return header at the -- you know, we're not going to worry about reverse flow in LOOPs.

MR. WHEELER: Yes.

CHAIR STETKAR: I'm assuming there are check valves out there anyway someplace, but that you now have one pump's worth of flow going through the three parallel sets of heat loads.

MR. WHEELER: Yes.

CHAIR STETKAR: And is that the analysis that they did?

MR. WHEELER: We'd have to go back and look at the RAI response. But I'm fairly certain that that's is correct.

CHAIR STETKAR: Okay. If that is, then that's a big confidence builder because if indeed the system doesn't get into trouble in terms of temperatures or, you know flow characteristics of the pump, or anything under those conditions, then it's not clear to me that the operators ever have to close the cross-tie valves. If indeed the RAI response doesn't address those conditions, if they made some assumptions about flow through the -- you know Train B let's call it in this case being isolated, and you know and particularly through the RHR heat exchanger because that will be the largest load, then that determines conditions under which perhaps the operators may need to close those cross-tie valves if that becomes unacceptable. And that might be less than 24 hours. But I don't know what the unacceptable conditions would become.

MR. WHEELER: Yes. I thought I did a fairly good job in the SER explaining the margins that were available during this scenario which one pump had tripped off and the other pump was supplying all the loads. And I'm trying to find that in the SER right now.

CHAIR STETKAR: Yes. And I did read the SER. I tried to understand it. And it wasn't, I guess--

MR. WHEELER: There's 1.32 E to the sixth BTU per hour added load to the heat exchanger during this duration in which one pump had tripped off and the other pump was supplying all the loads. And that's pretty insignificant against the heat exchangers that are designed for 190 E to the sixth.

CHAIR STETKAR: With that sort of flow rate, though, on the CCW side -- okay.

Well maybe -- we're going to get back together again tomorrow. Maybe you can --

MR. WHEELER: Okay. Yes.

CHAIR STETKAR: -- point me to the places. It may be there and I'm not -- you know, I'm being dense. I've been dense in the past. Ad it will continue in the future.

MR. WHEELER: Well, I'll go back over the RAI response.

CHAIR STETKAR: Now, Larry, the 24 hours from what you were saying earlier, is that -- I think you characterized it as something like well it would be a good idea at some time to separate these things.

MR. WHEELER: Yes.

CHAIR STETKAR: Is that basically what that SECY paper says? I mean, what's the basis for that 24 hours? If indeed this configuration gives you stable heat removal with no challenge to either heat removal or equipment survivability, why would the operators need to close those valves at all?

MR. WHEELER: In the SER we talked about the SECY-77-439 and it references this as that 24 hours or greater for long term cooling. So I can go back and then for tomorrow's discussion --

CHAIR STETKAR: Because I didn't go back--

MR. WHEELER: -- we can pull that document together and --

CHAIR STETKAR: Unfortunately, I didn't have time to go back and look that up. And I'm curious about it because it says SECY-77, which is a while ago.

Thanks. I'd appreciate it.

MR. WHEELER: Okay. I can do that.

The other question we had for these was 30 days versus 36 days --

CHAIR STETKAR: Yes.

MR. WHEELER: -- and the ultimate heat sink. And in the DCD it is not very clear what it means, but 30 days supply versus 36 day supply. And in the Reg. Guide, I believe, it essentially is talking about the analysis for meteorological conditions for 36 days for a cooling ponds. And that's because it takes if you're using cooling pond, an additional five days for that heat load to actually get to the cooling pond to its maximum temperature. So that's a difference between doing a meteorological review for 30 days versus the 36 days. And that's why I said the DCD is kind of unclear for the 36 day heat pump.

CHAIR STETKAR: Well, yes. And for example--

MR. WHEELER: And it says you have a 30 days supply.

CHAIR STETKAR: Right. And I understand the 30 days. That's --

MR. WHEELER: And then it starts talking about doing an analysis of 36 days meteorological data for the cooling pond design.

I'll this with you.

CHAIR STETKAR: What's the date on the Reg. Guide?

MR. WHEELER: '76.

CHAIR STETKAR: Yes. The only reason it honestly doesn't effect the subject of this meeting --

MR. WHEELER: Of the DCD, right.

CHAIR STETKAR: -- it doesn't effect the DCD at all. I'm just curious about the fact that if I'm now in the COL world, given these words in the DCD--

MR. WHEELER: Yes.

CHAIR STETKAR: -- given the words in the SER for the DCD --

MR. WHEELER: Yes.

CHAIR STETKAR: -- if I want to use a mechanical draft, cooling towers with things that look like large swimming pools --

MR. WHEELER: Yes.

CHAIR STETKAR: -- and call that my ultimate heat sink, I need to have 30 days worth of water in there accounting for what meteorological conditions.

If I instead want to dig a big hole out there in the south 40 and line it with some really good clay --

MR. WHEELER: Yes.

CHAIR STETKAR: -- and fill it full of water and have pumps take suction from it and allow for just normal evaporative cooling --

MR. WHEELER: Yes.

CHAIR STETKAR: -- the implications are I need to account for 36th days worth of inventory.

MR. WHEELER: Right.

CHAIR STETKAR: Even though I might call that other thing out there my ultimate heat sink.

MR. WHEELER: That's right.

CHAIR STETKAR: but I might call the Mississippi River my ultimate heat sink. So --

MR. WHEELER: For example, the EPR only has 72 hours of ultimate heat sink on site.

CHAIR STETKAR: Yes.

MR. WHEELER: They have safety-related pumps that bring in water from the Chesapeake Bay. So that's their approach to Reg. Guide 1.27. So --

CHAIR STETKAR: Calvert Cliffs' version of the EPR, not the EPR?

MR. WHEELER: That's right.

CHAIR STETKAR: But if I wanted to dig a pond, I'll call the site South Texas for example --

MR. WHEELER: Yes.

CHAIR STETKAR: -- where they built dug a big pond, that pond would need to supply 36 days worth of water according to that Reg. Guide?

MR. WHEELER: No. It says you need to do an analysis for 36 days of meteorological.

CHAIR STETKAR: Okay. Okay. Okay.

That's a Reg. Guide, now I know you said you'd leave it with me, but --

MR. WHEELER: 1.27.

CHAIR STETKAR: 1.27.

MR. WHEELER: Yes. And it's going through revision right now.

CHAIR STETKAR: That number sounds familiar.

You remember everything, Bill. Have we seen that?

MEMBER SHACK: 1.27, no.

CHAIR STETKAR: Okay.

MEMBER SHACK: That's a number that would stick in your head. I mean that's getting back there.

CHAIR STETKAR: Okay. All right. There is some explanation. And you said it is being revised now?

MR. WHEELER: Yes, it is.

CHAIR STETKAR: Okay.

MR. WHEELER: I'm not quite sure what we're doing with the 36 day thing, but now we'll have to look at in detail.

CHAIR STETKAR: Apparently, a timely question.

Component Cooling Water, since the slide is still up there, the SER discusses gas accumulation in the component cooling water system. And it seems to focus primarily on the surge tank. There's a discussion about the fact that there's a nitrogen cover gas on it, but because the piping arrangement, the elevation and things like that, that it's unlikely that that nitrogen would become entrained and cause any gas accumulation in the system.

Did you look at other possible ways that gas, not nitrogen, air could become entrained in the system in local high spots in the systems? For example, after maintenance if high points in the system were not vented. In other words, did you go through the system to assure yourself that it contains high point vents in local places where you might have essentially LOOPs created where you could accumulate gas? Not necessarily from nitrogen, but in leakage --

MR. WHEELER: Yes.

CHAIR STETKAR: -- maintenance, you know things like that?

MR. WHEELER: That wasn't the extent of my review. That would apply to any system across the board that if you don't have high point vents, then you can't hydrostatically test the system adequately. So you really can't meet ASME code. So kind of goes without saying that you're going to have to have high point vents in any ASME section 3 piping system.

CHAIR STETKAR: The only reason I raised it is I did see words like "high point vents" in other systems. I didn't see it in this.

MR. WHEELER: Yes. I kind of think it goes without saying that the systems have to have high point vents in their pockets.

One of the other comments you made was about a half hour ago about the spent fuel pool loss of cooling and the temperature alarms. And I think it kind of goes without saying that the COL is going to develop alarm responses for all those alarms that are going to deal with details, actions to the control room operators know what to do. So in the case of a high temperature alarm on the spent fuel pool, he's going to hit the alarm, he's going to get out the instruction and it's going to say, you know, verify pumps are running. If not, start a pump. I think that kind of goes without saying that the COLs have to develop alarm instructions for any alarm that comes into the control room

MEMBER BLEY: Could you clarify something for me?

MR. WHEELER: Yes.

MEMBER BLEY: At what point in time will the new orders that were issued as a result of Fukushima apply to these new plants?

MR. WHEELER: Well, I --

MS. McKENNA: This is Eileen McKenna.

We are still evaluating how we're going to apply the positions taken for Fukushima to new reactors. We think in general we have time to try to deal with these in a measured way an we are considering whether we ask questions. And we -- get new licenses get issued, have orders. But we're obviously in a position to have discussions.

MEMBER BLEY: I'm sure you are.

MS. McKENNA: We're not prepared today to say how we're going to approach it for this particular applicant.

MEMBER BLEY: Okay. So we don't know yet whether it will be before duel load or --

MS. McKENNA: Well, certainly I think before that. I think the question is at what point in the licensing process will these things be --

MEMBER BLEY: Yes, but there's a number of them that already have their --

MS. McKENNA: Yes. And in the case of Vogtle, I think the plan was to send -- and I think also a 50.54(f) letter on certain position. And we're also considering for all the other applicants --

MEMBER BLEY: Okay. So that might be before the COL?

MS. McKENNA: It could well be, yes.

MEMBER BLEY: Okay.

MR. WHEELER: So do you have any other questions?

CHAIR STETKAR: Let me just check my notes here. No.

MR. KALLAN: Okay. Thank you, Larry.

I turn it over to Angelo Stubbs.

MR. STUBBS: Okay. Good afternoon.

My name is Angelo Stubbs. I'm with the Balance of Plant Branch and I performed the review for FSAR Section 9.2.6 Condensate Storage Facilities.

I guess this morning the Applicant gave you a quick overview of that system. They also had a slide in there about the open item, but they didn't present it, unfortunately. But just some of the features. "Key," may not be really the word, but some of the ones that I wanted to bring up for saying this is as they told you this morning, the Condensate Storage Facility has three systems. It has a big bin water system, the condensate storage and transfer system and the primary makeup water system.

It basically supplies and receives condensate from the -- to and from the condensate hotwell as required. The system is a nonsafety-related system and has no safety-related functions. And a lot of the Condensate Storage systems, the condensate storage tank is used as a primary water source for aux feedwater and emergency feedwater. But for this design there is dedicated emergency feedwater pits that contains, I think, it's combined of 400,000 gallons of water that's used to support the operation of the emergency feedwater system. And also that supports the Station Blackout, which is the other thing that we looked at the condensate storage tank for.

According to the table they have in Chapter 9, the tank is about 750,000 gallons. It's a non-seismic tank. It has a dyke which they say it can contain the whole contents of the tank, but the dyke is a nonseismic dyke, so that -- and they say that's used to mitigate the environmental effects of system leakage or storage tank failure.

For our evaluation, I evaluate this as our SRP 9.2.6, and this is for general condensate storage facilities. And in some cases they have safety-related functions and some cases there's condensate storage facilities with no safety-related functions.

In the application in Chapter 1 Table 1.9.2 they indicated that the SRP 9.2.6 is not applicable for this plant, which is different for me because all the licensing plants I've seen and all the new reactors I've seen to some extent you use 9.2.6 and there is some GDCs that apply, and often they'll point out what doesn't apply and then just how to meet what does apply.

While we're reviewing this the heat transfer functions were not required, the GDC 44, 45, 46 is a plant that is a one-unit plant. So the GDC doesn't apply. But based on our review, I felt that GDC 2 and GDC 60 applied, also they needed to meet the requirement of the 10 CFR 20.1406.

So, after looking at what was presented in their design, those were the things that I felt needed to be meant.

In a slide I just took something out of the SRP, it doesn't show everything, but one of the things it indicates in the SRP is that outside designs should be compliant with GDC 60 and Reg. Guide 1.143. So their denial that GDC 60 applies, that was to point that out.

And also, in that same one it says that for nonsafety-related storage facilities there's a need for a seismic category 1 dyke or retention basin review. So I reviewed that.

The GDC 2 comes in, and in this case if there was an earthquake, you wouldn't be able to take credit for the tank not filling or the dyke containing the contents of the tank.

So we issued an RAI, and this is what the open item is, and we request that they provide justification for use of a nonseismic dyke in conjunction with the nonseismic tank. And we asked them how they would comply with GDC 2 and 60 if you had such a failure and what would happen with the resulting flooding that could occur if you had a seismic event that resulted in that failure.

MEMBER BLEY: And have they responded to that yet?

MR. STUBBS: They did respond to it. And their initial response to it in an RAI letter that they gave us on December 15th, 2011. And in that response they basically came to the conclusion that GDC 2 and GDC 60 were not applicable.

But what they said was "The condensate

storage tank is classified as nonsafety-related as the system does not perform any safety-related function. Hence, GDC 2 is not applicable. The CST, its dyke and pump house are strategically located away from the other structures, systems and components, particularly the safety-related SSCs, the flat site grading and the nuclear island area, and the yard drainage from the area minimizes any adverse impacts of any safety-related SSCs due to the failure of the tank and/or the dyke. Hence the CST and the CST dykes are designed as nonseismic."

So they credited that it was out in the yard away from other safety-related SSCs, and they talked about the site drainage. And in their slides this morning they have other things about entrance is being located one foot above, but -- and greater slope and drainage. And they have a conclusion that therefore the failure of the tank and dyke does not impact safety-related SSCs.

So, we did talk to them and try to explain what our concerns was. And I think they're going to be providing us a revised or a supplement to that RAI response. But at that time they still -- they seemed to be willing to address GDC 60, but they still was taking the stance that the way they read GDC 2 it doesn't apply. But I think they recognize the fact that the flooding issue needs to be addressed.

I looked at the site arrangement, and the reason I was focusing on the condensate storage tank is it seems to be located over in the yard just outside of the turbine building, not too far from the turbine building. And also in their response they talk about slope and drainage systems should be provided as site-specific plant design.

One of the things is this doesn't seem -- this feels like they're making conclusions there, but it seems like this is a site-specific issue. Well, a COL would need to be -- there would need to be a COL item.

MEMBER BLEY: And this is ground water. I mean --

CHAIR STETKAR: Well, and if it is though, if I'm the COL, I think I'd need to know that I need to consider this. Right? So at a minimum, there would to be an explicit COL information item that, you know MR. STUBBS: I think that there needs to be a COL --

CHAIR STETKAR: I mean, that's -- I mean we don't do that kind of thing.

MR. STUBBS: No, you know that's

something that I think needs to be done.

But looking at the plan, though, and looking at it the concern I had was with the power source building and the power source volts, both. And when I looked at the two COLs, one looked like everything looked okay and everything drained away. The other looked like it sort of drained back, it drains downhill which would pass by those building. And so it seems like that the statement seems fine, but it just has to be verified. If it's not verified, there needs to be a flooding evaluation that we can look at and that we can confirm the conclusion that's being drawn. And so far I've asked about that, I haven't seen that, and I have seen the COL item. So we still have work to do on that and it's one of those things that it's just like the turbine building when you have a break in the circ water line, there's a lot of water there. And in the case for one of the COLs where there's a dual site, you basically have two of these things side-by-side. SO you really have lots of water.

But when I look at what they have here, there's some recognition that there's a problem that has to be addressed, but to this point I don't see that it's fully addressed because the site grading is something is something that's going to be different from plant-to-plant. I think the COL has to be involved. Because either that or, you know they set up where they can't do it, then they're going to have to make a decision on their design whether to depart and make a dyke or something seismic. But that's the open issue. It was something that I, you know when I first read through it it looked okay, but then as I -- you know, as I went back to the site plan and started looking at thing, it seemed like we may have a problem there.

The other tanks, the demin storage tank was located sufficiently away in the general plan.

CHAIR STETKAR: That's what I was going to ask. You know, we're just about to muddy the waters, if you will, and ask about the demin storage tank because I meant to ask MHI this morning there's no mention of a dyke around that tank.

MR. STUBBS: No, I think --

CHAIR STETKAR: And it's equally nonseismic. It's 500,000 gallons --

MR. STUBBS: Right.

CHAIR STETKAR: -- instead of 750,000 gallons.

MR. STUBBS: Right.

CHAIR STETKAR: But it's still a considerable amount of water.

MR. STUBBS: It is. It is. And when I looked at the general layout, from what I looked at the location of it, it looked like it was a little bit down from the --

CHAIR STETKAR: With things like the locations of tanks, is that an R-COLs? I mean, could the R-COLA decide that they want to move it up there in the corner someplace --

MR. STUBBS: Well, here's the thing --

CHAIR STETKAR: -- if they'd like to do that?

MR. STUBBS: The other thing with both is tanks as part if the flood analysis of 3.4.1.2, the external outdoor tanks and piping should be evaluated. And they do talk about in 3.4.1 -- in 3.4.1.2 I think they actually put an example and they have the primary makeup storage tank, refueling water storage tank, demin water storage tanks,fire water storage tank -- they don't mention the condensate water tank at all, but they do talk about it as part of the flooding analysis and the flood evaluation they should be addressed. So, that's why I didn't bring it up there.

And maybe the condensate storage tank

should also be addressed as part of it also.

CHAIR STETKAR: But recognize that if we get the right kind of seismic event we're talking about not only the 750,000 gallons in the condensate--

MR. STUBBS: In the -- right.

MR. STUBBS: We're talking about the condensate storage tank and the demin storage tank.

MR. STUBBS: Right.

CHAIR STETKAR: Both of them, because they're equally nonseismic.

MR. STUBBS: Right.

CHAIR STETKAR: We're talking about the primary water makeup tanks --

MR. STUBBS: Right.

CHAIR STETKAR: -- which are in a building, but I don't know -- what, that is another 280,000 gallons of water.

MR. STUBBS: Yes. They're over by the refueling water storage tank at the end of the auxiliary building. So these in terms of location, they're sort of at the opposite ends of the plant -- the makeup water and the refueling water storage tank.

But you're right: If you have nonseismic tanks, all of them would be assumed to have failed.

CHAIR STETKAR: I mean, you know they're

not necessarily exactly equal, but --

MR. STUBBS: Right, right. But that would also be part of -- you know in the flooding analysis you would be looking at the failure on your nonseismic tanks and looking --

CHAIR STETKAR: Do they do that with all of them or do they do one-by-one and say "Okay, this one's got two gallons in it so that's not a problem, this one has eight gallons in it and that one's not a problem?

MR. STUBBS: Well, obviously the inventory isn't large enough, they probably don't look at it. But thinks that have large inventories, they should look at. And that's still part of our flood evaluation that we're trying to get to the point we've requested to have the calculations available for it to do a audit of. But whatever they can't do as part of the standard design, they need to make sure that the COL do. And because these locations may vary based on COL it seems like that may be something that the COL will end doing. It would be, you know put into as a bigger COL item in Chapter 3 to either verify that the slopping takes it away or do an analysis to show that the flooding don't affect safety-related SSCs or buildings.

CHAIR STETKAR: Okay.

MR. STUBBS: And that's really all I had. If you have questions, I'll be glad to answer them.

CHAIR STETKAR: I don't. Anyone else?

MR. KALLAN: Thank you, Angelo.

I guess I'll turn it over to David Nold.

CHAIR STETKAR: I'm sorry, Angelo. Does the demin tank had a dyke around, do you know?

MR. STUBBS: The only thing, in their DCD they're saying their dykes are at a primary water storage tank --

CHAIR STETKAR: I read that, yes. Let me ask MHI just to --

MR. STUBBS: There was no mention of a dyke around the demin.

CHAIR STETKAR: Can someone from MHI clarify? Is there a dyke -- I don't care of it's seismic or nonseismic. I'm just trying to find out at the moment whether there's a dyke around the demineralized water storage tank.

MR. MASASHI: I am Masashi Ito, MNES.

The primary makeup of the tank.

CHAIR STETKAR: Demineralized water tank. I know there's a DWST.

MR. MASASHI: Excuse me.

CHAIR STETKAR: If you don't have it, we're coming back tomorrow morning. If you don't have a quick answer, you know it's something we can find out tomorrow. Let's leave it at that. The staff doesn't have too much left, but I want to make sure that if we do have questions, we do need to finish by about 5:00. So we'll just leave it on the to do list for tomorrow morning.

MR. KALLAN: Okay. I'll turn it over to Dick.

MR. NOLD: Good afternoon. My name is David Nolan. I'm with the Containment and Ventilation Branch.

When the SER is submitted --

CHAIR STETKAR: I'm sorry, Dave.

MR. NOLD: Yes, sir.

CHAIR STETKAR: I'm trying to keep ahead. You guys are not talking about all of the stuff --

MR. NOLD: Right.

CHAIR STETKAR: -- in this chapter. And there was one issue that kind of bothers me, and it's on the essential chilled water system. So I don't know who the appropriate person to drive into this is, but --

MR. KALLAN: Yes. We have him --

CHAIR STETKAR: Ah. Hopefully, at least I can frame the question a little --

MR. KALLAN: -- for you.

CHAIR STETKAR: -- bit better on this one than I did earlier.

In the SER in Section 9.2.7.4.2, which is the tech specs regarding the chilled water system, there's the following statement: The US-APWR does not include any technical specifications for the ECWS or the non-ECWS. This is consistent with SRP Section 15 NUREG-1431 Standard Technical Specification for Westinghouse Plants and is acceptable to the staff."

I'm really curious why you don't need technical specifications for the essentially chilled water system, which is a safety-related system that supplies support to maintain acceptable environmental conditions for the operation of safety-related mechanical, electrical, instrumentation control and Main Control Room habitability systems, and the US-APWR technical specifications bases in Section B.3.7.8 for the essential service water system and B.3.7.9 for the ultimate heat sink specifically note that ESWS needs to supply cooling to the ECWS chillers. So, if I need supply cooling to the ECWR chillers, and that's in the tech specs and ECWS provides cooling to safety-related systems that are in the tech specs, I really don't understand why ECWS isn't in the tech specs simply because somebody who had never looked at at chilled water system wrote generic tech specs for a Westinghouse plant. So if you could explain to me why that's acceptable to the NRC staff, I'd be really interested in that explanation?

MR. CURRAN: What you read right there is from the SER?

CHAIR STETKAR: What I read from the SER is the quote "That the US-APWR does not include any tech specs for the ECWS or non-ECWS. This is consistent with SRP Section 16, NUREG-1431, Standard Technical Specifications for Westinghouse plants is acceptable to the staff." That's a direct quote from the SER.

MR. CURRAN: I don't --

CHAIR STETKAR: And no further justification.

MR. CURRAN: I don't have a good answer for you right now.

CHAIR STETKAR: Okay. I'd suggest you go back and look at that and think about it, because --

MR. CURRAN: That's in a different branch, and I will get back to you on that.

CHAIR STETKAR: Okay. Okay. I don't normally read those tech specs' actions, but I was skimming through it and wait a minute, no tech specs. And, indeed, there are no tech specs because I went to Chapter 16 and there aren't any tech specs. But if you do a word search on "chilled," you'll find out indeed there's a requirement -- you know, the tech spec bases for ESWS, surface water. Note that one of its functions is to cool those chillers.

Check with the tech spec folks, please.

MR. CURRAN: Okay.

CHAIR STETKAR: And now we can talk about Main Control Room spec.

MR. NOLD: Good afternoon. My name is david Nold, I'm from the Containment and Ventilation Branch.

When the SER was compiled last Fall, it was submitted with 13 open items. And probably most of the 20 listed, I have 13. Since last Fall the good news is that seven of those have either been moved to confirmatory items or closed. So we're down to the significant six, I guess is the best way to put it.

We're going to talk about three of those open items in two slides today. And let me start from there.

The staff's concern is captured in this slide as the ability of the US-APWR plant to maintain design temperatures within areas housing safety-related systems and components following the onset of Station Blackout. The staff seeks assurance that an alternate AC power source will be available within 60 minutes from the onset of Station Blackout.

This slide actually represents two open items or RAIs against DCD sections 9.4.1 and 9.4.5.

Section 9.4.1 pertains to the Main Control Room HVAC system which maintains design temperature limits within the Main Control Room envelop.

Section 9.4.5 pertains to subsystems of the engineered safety feature of ventilation system, maintains design temperature limits within areas housing safety-related equipment in the reactor building and the power source building.

The governing regulations are 10 CFR 50.63 Loss of All Alternating Power which reads in part: "The alternating AC power sources as defined by 50.2 will constitute acceptable capability to withstand Station Blackout provided in analysis performed which demonstrates that the plant has this capability from the onset of Station Blackout until the alternate Ac sources and required shutdown equipment are started and lined up to operate."

GDC 4 reads, in part, "Structures and systems more important to safety shall be designed to accommodate the effects of and to be compatible with the environmental conditions associated with the normal operation, maintenance, testing, including loss of cooling accidents."

Then we roll up into regulation. Essentially Reg. Guide 1.155 Station Blackout, by arriving in that Section C.3.3.5 provides specific guidance with respect to alternate AC power sources. Criteria 3 of Reg. Guide 1.155 "The time required for making this equipment available shall not be more than one hour as demonstrated by tests."

Criteria 5 reads: "The alternating AC power system which should be inspected, maintained and tested periodically to demonstrate operability and reliability. The reliability alternate AC power system should be or exceed 95 percent as determined in accordance with NSAC 108 or equivalent methodology."

Currently the DCD Chapter 14 test entitled "Alternate AC Power Sources for Station Blackout Pre-Operational Tests" contains pre-requisite No. 5 which reads: "A report exists that demonstrates the reliability of the actual AC power sources and meets or exceeds 95 percent as determined with NSAC 108 by equivalent methodology to meet Criterion 5 as Section C.3.3.5 of Reg. Guide 1.155 based on historical data of a similar type of the alternate AC power sources."

To make its regulatory finding, the staff seeks further clarification and enhancement of this pre-operational test to ensure it satisfies the intent of 10 CFR 50.63 and Reg. Guide 1.155.

I open the floor to questions on that slide.

CHAIR STETKAR: Yes. And I understand what you've just said. As part of this, are you also asking about whether the 60 minutes is an appropriate time for startup of the alternate AC source based on heatup of the Main Control Room environment? In other words, are there analyses to show that the maximum temperature in the Main Control Room does not exceed habitability -- suppose, for example, it got up to 190 degrees within 20 minutes? One would say that perhaps I should start the alternate AC gas turbines in something less than 20 minutes. Are you also questioning that 60 minute time with respect to heatup of the Main Control Room or are you just questioning whether or not the pre-operational tests and --

MR. NOLD: There was one RAI initiated that asks for calculations of that.

CHAIR STETKAR: Okay.

MR. NOLD: And they provided not a formal calculation, but a calculation that made sense in my mind. So there was no audit of their calculation, to answer your question. It seemed reasonable what they were telling me, is the best way to put it.

CHAIR STETKAR: And it substantially longer than 60 minutes until they --

MR. NOLD: The maximum temperature they calculated, I think was like one degree less than the limit of 122, I think it was. That's the maximum you'll ever get, and it will take forever to get there, several hours to get there.

CHAIR STETKAR: Oh, that's not the temperature at 60 minutes? That's the steady state--

MR. NOLD: Yes. That's the temperature after that.

CHAIR STETKAR: Okay. Thanks.

MR. NOLD: Yes. Right.

CHAIR STETKAR: And it takes much longer than 60 minutes to get there?

MR. NOLD: Yes, that was in our

conclusion. Right.

CHAIR STETKAR: Okay. Thanks. That shows margin on the 60 minutes.

MR. NOLD: Any other questions?

CHAIR STETKAR: No. Any other questions on this one?

MR. KALLAN: We'll go to the next one.

MR. NOLD: Okay. This slide here, it captures the staff's concern pertaining to the potential effects on Main Control Room instrumentation and controls on a worse case essential chilled water system leak within a Main Control Room HVAC system air handling unit.

Again, GDC 4 reads in part, and I'm going to read a little bit further this time with it: "Structures and systems, components important to safety shall be designed to accommodate the effects of and to be compatible with the environmental conditions associated with manual operation, maintenance testing, possibly accidents including loss of coolant accidents. These structures, systems and components shall be appropriately protected against dynamic effects, including the effects of missiles and discharging fluids that may result in equipment failures and for events and conditions outside the nuclear unit."

Could you put in a figure of reactor control room --

CHAIR STETKAR: Oh, yes. That helps.

MR. NOLD: Off in the right-hand corner there are four air handling units. Below is the actual control room envelope itself.

As this figure shows, there are four 50 percent capacity air handling units in the Main Control Room HVAC system. These air handling units are part of the control envelope and located directly above the Main Control Room at the next higher plant elevation.

The essential chilled water system design filter to the four handling units equals 45 gallons per minute. In the available worse case chilled water leak, the supply and return HVAC trunk lines are connected to the air handling units with the Main Control Room below could provide a path for an internal flood of the Main Control Room. The potential exists for multiple divisions of safety-related equipment being in the path of such failure.

The equipment drain line from each air handling unit is nonsafety-related. Nonetheless, the equipment drain line from the air handling unit to the sump below should be adequately sized to assure that it can dissipate by gravity the worst case leak of 45 gallons per minute. It cannot be cited as based on a noncondensate role of a air handling unit which would be significantly less.

The relevant performance of the Main Control Room HVAC system and the essential chilled water system will satisfy GDC 2 requirements. In particular, these components are to be installed as seismic Category 1 safety-related equipment Class 3.

To make its regulatory finding, the staff seeks further standing of the air handling unit design to ensure it satisfies the requirements of GDC 2 or GDC 4.

Any questions?

CHAIR STETKAR: I don't have any. This is an interesting one. I read something in the last six months or so. It's just relevant in terms of water that there actually was a flooding induced fire at a nuclear power plant where water from a leak found its way through things and down into some switchgear and caused some arcing. And it wasn't a bad fire or anything, but it's the first flooding induced fire I've ever heard of.

MR. NOLD: Yes.

CHAIR STETKAR: And there had been events -- I've forgotten the plan, that were leaks into I&C cabinets and things like that and caused those fires. So this is a good one.

Any other member comments, questions? If not, I thank you very, very much for your presentation. I think we had some good discussions.

There are --

MR. HAMAMOTO: John, a quick -- you had a couple of questions that I didn't provide the responses. Do you want to go over now

CHAIR STETKAR: Tomorrow. Tomorrow morning. Because we have several. I think MHI will come back with their responses. You folks can come back. Staff can come back with responses.

Obviously, we're going to finish I think well probably before noontime tomorrow morning. I don't want to change the start time. We start at 8:30 only because there's a notice of the times that we have to start and we kind of have to adhere to that a bit. So we'll start at 8:30 tomorrow morning. I expect to finish, you know mid-morning or so depending on much of the discussions are.

And, again, I thank everybody: MHI and the staff. And we'll reconvene tomorrow morning.

And we are adjourned for today.

(Whereupon, at 4:56 p.m. the ACRS Subcommittee was adjourned to reconvene March 23, 2012 at 8:30 a.m.)

UNITED STATES OF AMERICA

NUCLEAR REGULATORY COMMISSION

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ADVISORY COMMITTEE ON REACTOR SAFEGUARDS

(ACRS)

+ + + + +

US-APWR SUBCOMMITTEE

+ + + + +

FRIDAY

MARCH 23, 2012

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ROCKVILLE, MARYLAND

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The Subcommittee met at the Nuclear Regulatory Commission, Two White Flint North, Room T2B1, 11545 Rockville Pike, at 8:30 a.m., John

Stetkar, Chairman, presiding.

SUBCOMMITTEE MEMBERS PRESENT:

JOHN W. STETKAR, Chairman

CHARLES H. BROWN, JR., Member

WILLIAM J. SHACK, Member

NRC STAFF PRESENT:

ILKA BERRIOS, Designated Federal Official

PAUL KALLAN

NRC STAFF PRESENT: (cont'd)

HOSSEIN HAMZEHEE

LARRY WHEELER

RAUL HERNANDEZ

EILEEN McKENNA

ALSO PRESENT:

RYAN SPRENGEL

JAMES CURRY

NAOKI KAWATA

SHINJI KAWANAGO

RON REYNOLDS

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P-R-O-C-E-E-D-I-N-G-S

(8:35 a.m.)

CHAIRMAN STETKAR: The meeting will now come to order.

Today is the second day of a meeting of the United States Advanced Pressurized Water Reactor Subcommittee.

I'm John Stetkar, Chairman of the Subcommittee meeting.

ACRS members in attendance are Charles Brown and Bill Shack. Ilka Berrios of the ACRS staff is the designated federal official.

The Subcommittee will review Chapter 9, Auxiliary Systems, of the Safety Evaluation Report with open items associated with US-APWR design certification application.

Yesterday we heard presentations from Mitsubishi Heavy Industries and the NRC staff. Today we are going to discuss questions that were raised yesterday during our meeting.

We have received no written comments or requests for time to make oral presentations from members of the public regarding today's meeting. The Subcommittee will gather information, analyze relevant issues and facts, and formulate proposed positions and actions, as appropriate, for deliberation by the full Committee.

The rules for participation in today's meeting have been announced as part of the notice of this meeting previously published in the Federal Register. Parts of this meeting may need to be closed to the public to protect information proprietary to Mitsubishi Heavy Industries or other parties.

I am asking the NRC staff and the applicant to identify the need for closing the meeting before we enter into such discussions, and to verify that only people with the required clearance and need to know are present.

A transcript of the meeting is being kept and will be made available as stated in the Federal Register notice. Therefore, we request that participants in this meeting use the microphones located throughout the meeting room when addressing the Subcommittee. The participants should first identify themselves and speak with sufficient clarity and volume so that they may be readily heard.

We will now proceed with the meeting, and I will call upon I don't know who. Do you want to say anything?

MR. KALLAN: Well, this is Paul Kallan. I am the Senior Project Manager, and it is good to have us back here again today. Staff is going to answer the questions that you -- followup questions and also MHI's, too. So --

CHAIRMAN STETKAR: Good. Thanks, Paul.

With that, I will turn it over to MHI and --

MEMBER BROWN: Do we have to give him CPR or resuscitate him over there?

CHAIRMAN STETKAR: No, but I heard the --

(Laughter.)

-- click into place.

Before we start, we will take as long as we need this morning to address whatever answers that both MHI and the staff have.

If we -- you know, I don't think anybody will complain if we finish early, but whatever discussion it takes to make sure that we have understanding of whatever you have been able to address in the last, you know, 15 or 18 hours, or however long it has been, we would appreciate that. I think that the process works a lot better if we can get things resolved in this context.

So with that, I will turn it over to MHI.

MR. SPRENGEL: Well, good morning. This is Ryan Sprengel. I'm an ASDC licensing manager.

I would like to, again, thank the members and the NRC staff for continuing to support this meeting. We did work into either the wee hours of the night or the earlier hours of the morning, depending on how you look at it.

So this is a fortunate case where we do have, you know, this extra day that we can go ahead and address these instead of putting them off to an official transmittal later. We can go ahead and get these responses now and get them on the record.

So hopefully it provides some good clarification and responses to some of the comments we heard yesterday. And I think we have some good discussion material to present, and I will turn it over to Jim Curry.

MR. CURRY: Thank you, Mr. Sprengel. Okay. Good morning, Mr. Chairman. Again, my name is Jim Curry. And we have some folks here at the table which we will reintroduced, and some folks at the side table, and, as yesterday, some additional expertise in the audience. So our plan is to get you the best information that we can.

Okay. So at the table you recall Mr. Kawata, Mr. Tanigawa, and Mr. Otani. Okay. And then, we have Mr. Nishio, you know Mr. Sprengel and Mr. Kawanago over there at the side.

So what I propose is we will just go down our list of what we perceive to be the Committee's questions and give you some feedback.

CHAIRMAN STETKAR: Good.

MR. CURRY: And, again, in order of the presentation yesterday, I think, Mr. Chairman, you asked a question with regard to DCD Figure 9.1.4-2.

CHAIRMAN STETKAR: Yes.

MR. CURRY: And if I recall, your comment was about the weir wall and failure of the weir wall that is shown in that figure, and, really, what would the water level be and time to boiling if we did reduce the water level based on that weir wall failure.

I would point you to RAI 132-1538.

CHAIRMAN STETKAR: 132-1538?

MR. CURRY: Yes, sir. Question 9.1.2-7.

CHAIRMAN STETKAR: I can't write that fast. 9.1.2 --

MR. CURRY: Dash 7.

CHAIRMAN STETKAR: -- dash 7.

MR. CURRY: Right. So we provided the information that I am just going to summarize for you in that RAI response. Big picture is that if we fail that weir wall, the water level is reduced to about six feet below the starting point, the existing water level.

So that gives us quite a bit of room, still. And it's because that water isn't lost, it just flows into the refueling canals.

CHAIRMAN STETKAR: Okay. I think you misunderstood my question. My question was simply, suppose that the level is at the height of the weir wall. I'll worry about how it got there. Suppose that it is a level at the height of the weir wall. How long does it take to reach boiling? And how long does it take to reach fuel damage? I'll worry about how it got there.

MR. CURRY: Okay. And --

CHAIRMAN STETKAR: Because I will guarantee that there -- in a probabilistic sense there are draindown scenarios that can drain the water to that level, that involve flow paths that do not just involve failure of the weir wall and filling the adjacent -- immediately adjacent volume. I guarantee you that there are drain-down paths.

MR. CURRY: Okay.

CHAIRMAN STETKAR: I haven't personally identified all of them. That was my follow-on question to try to get a handle on where they might be. But I will guarantee you that there are drain-down paths.

MR. CURRY: Well, with that --

CHAIRMAN STETKAR: They may require human errors during refueling operations when the weir -- when weir gates are removed. But I guarantee you that there are drain-down paths somewhere. I have never seen a plant where I haven't been able to find at least one.

MR. CURRY: Okay.

CHAIRMAN STETKAR: So the question was not presuming some combination of failures. The question was simply suppose that the level is at the height of the weir wall. I wanted to confirm what that level really is. And given that, what is the time to heat up to boiling and the time to heat up -- let's call it fuel damage rather than fuel uncovery.

MR. CURRY: We appreciate that. Let me just kind of mention -- I mentioned the failure of one weir wall. Our analysis included complete connection of all cavities with all --

CHAIRMAN STETKAR: Okay.

MR. CURRY: -- weir walls out.

CHAIRMAN STETKAR: Okay.

MR. CURRY: So --

CHAIRMAN STETKAR: So you at least filled the other cavities.

MR. CURRY: Yes, sir.

CHAIRMAN STETKAR: Not just the --

MR. CURRY: Now, that's a different number.

CHAIRMAN STETKAR: Sure.

MR. CURRY: That still gives us about 12 feet above the fuel --

CHAIRMAN STETKAR: Yes. I understand that, because of --

MR. CURRY: Okay.

CHAIRMAN STETKAR: -- volumes of those cavities, yes.

MR. CURRY: Okay. So having said that, so that we have connected everything and we have done that analysis, your thought is that you would still like to know, well, let's just say we are at a level --

CHAIRMAN STETKAR: That's right.

MR. CURRY: Okay. Let me --

CHAIRMAN STETKAR: It can't get any -- see, the point is that it can't be any worse than that. And as long as there are drainage pathways that can get you to that water level, I am trying to understand what the bounds are in terms of your relative times. I know what the heatup time is given minimum water level.

You've done a heat-up calculation now at that -- or perhaps it is in this RAI response -- at that -- what is called an intermediate level given just transference of the upper part of the volume into the adjacent -- you know, what do you want to call them -- cavities or adjacent volumes.

MR. CURRY: Right. If you connected all of those volumes, we know what the level would be.

CHAIRMAN STETKAR: Yeah, yeah. And I'm

asking for the most -- the limiting, if the -- if you were draining to the bottom of the weir wall.

The reason I ask this is that we are not talking about PRA here. This is not a risk-informed licensing application, so I don't want to bring in the notion of PRA. However, people have performed PRAs of shutdown modes that indeed have examined configurations where the core is off-loaded into the spent fuel pool the same way that you do it.

You have a fuel transfer tube, you are connected to the reactor cavity, which is flooded up -- I mean, it is a standard plant design -- and have identified, based on plant-specific configurations and operational evolutions, errors or equipment failures that can open up drain paths.

Now, some of those drain paths may be from the primary system, but if the transfer gate is open you are now in an interconnected volume. So essentially you can drain the fuel pool into the containment through the transfer canal.

Now, you have a time available for that, so, like I said, I don't want to get into the probabilistics of all of this stuff, but indeed you can drain down to those weir wall elevations. In some cases, it requires drainage into the containment.

In some cases it requires drainage -- that's why I asked you about the drain lines from the transfer canal -- the transfer tube itself, or drain lines from the interconnected volumes, the fuel transfer -- the refueling canal and the other -- the cask volume, things like that.

They may be very rare events. And as I said, I am not getting into PRA space here. On the other hand, understanding what the margins may be under those conditions gives you a sense of timing and design margin for those types of events. That's the reason I asked the question.

You know, I don't want to prejudice studies. I have seen studies where indeed the bottom of the weir wall was below the top of the active fuel, which obviously is not here --

MR. CURRY: Not the case here.

CHAIRMAN STETKAR: -- because people had never thought of that.

MR. CURRY: Right. Well, I think as long as the Committee understands what we have done --

CHAIRMAN STETKAR: Yes.

MR. CURRY: -- and that is what we want to be sure. Let me just give a nod to the folks in the audience, you know, or my colleagues here. I do not believe that we have a heat-up calculation for the water at that level, at the weir wall level. So we are not prepared to give that to you --

CHAIRMAN STETKAR: Okay. Thanks.

MR. CURRY: -- today.

CHAIRMAN STETKAR: Thanks. As I said, I have to apologize, we don't get all of the RAIs, mostly because we ask for specific ones as they come up either in discussions like this or if they clearly, during our reviews of the major -- of the SER identify specific issues. The problem is if we ask for all of them, we would get all of them, and we'd now have 10,000 pages to read.

Does the response to this RAI question include the heat-up time, or does it only include the equilibrium water level?

MR. CURRY: I think it includes only the equilibrium water. The heat-up time is in another calculation.

CHAIRMAN STETKAR: Okay.

MR. CURRY: And of course, once again, we'll point out we haven't lost the water.

CHAIRMAN STETKAR: No, that's right. That's right.

MR. CURRY: In these situations, you

still have a heat sink.

CHAIRMAN STETKAR: Yes. And if you only do -- well, I guess if you are only doing a heat-up to boiling calculation, it doesn't make any difference.

MR. CURRY: Right.

CHAIRMAN STETKAR: Heat-up to fuel damage, once you get down below the weir wall, it --

MR. CURRY: Right.

CHAIRMAN STETKAR: -- then becomes different.

MR. CURRY: Right.

CHAIRMAN STETKAR: Okay.

MR. CURRY: But the scenario that you are talking about, I do not think we are prepared to talk about that scenario today.

CHAIRMAN STETKAR: Okay.

MR. CURRY: Agreed?

MR. KAWATA: Yes.

CHAIRMAN STETKAR: And for the benefit of the record and the benefit of the staff, I am not necessarily talking about something that is in the licensing basis for the plant either, because, as I said, we have identified these things during probabilistic risk assessment.

So I don't want to -- you know, I don't

necessarily want the staff to raise this as a particular concern and go on a witch hunt for draining pathways. I'm just trying to understand the plant design for our Committee's benefit.

MR. CURRY: Well, and we appreciate that, because clearly -- clearly, it is not a design basis.

CHAIRMAN STETKAR: Exactly.

MR. CURRY: We probably think it is not a credible event. But that would be our view.

CHAIRMAN STETKAR: The word "credible" is something we try not to use in the Subcommittee, so --

MR. CURRY: Mr. Kawanago?

MR. KAWANAGO: We understand your comment. Could you give me a little bit of time?

CHAIRMAN STETKAR: Sure.

MR. KAWANAGO: It is a long meeting.

CHAIRMAN STETKAR: So, you know, the good and bad things about the Subcommittee presentations especially is that in many cases we are trying to understand perhaps some details or interconnectivity in the plant design that you may not necessarily enter into in the licensing process, the design -- you know, the compartmentalized licensing process.

And some of these things kind of help us to understand that a little bit, and that is the genesis of some of these questions. We recognize that, you know, this has visibility, and things like that. And, again, I encourage the staff to take the context of our Subcommittee meetings into consideration.

So in this particular instance, I would hope that it is -- it doesn't generate RAIs and other areas of concern, because I don't see anything in the design that makes this plant any more or less vulnerable to these types of drain-down scenarios than any other currently operating plant or any other new reactor that we have seen.

So it is not -- you know, it is not a design-specific vulnerability. It is not anything. It is just simply a question.

MR. KAWANAGO: We tried to understand your question. This is Shinji Kawanago from MNES. We tried to confirm again what it is you are exactly asking on that question point. And because we would like to explain what is actually the drain line of this spent fuel pit. And the spent fuel is the data you also asked about and drain line in the spent fuel pit. And the spent fuel pit or this cask pit, basically we don't have any drain line.

CHAIRMAN STETKAR: There are no drain

lines in the cavity? The cask --

MR. KAWANAGO: No. No.

CHAIRMAN STETKAR: How do you drain those?

MR. KAWANAGO: It is a pump out.

CHAIRMAN STETKAR: Oh, you pump it out. You put a submersible --

MR. KAWANAGO: Yeah.

CHAIRMAN STETKAR: Oh, okay. Good.

MR. KAWANAGO: That is the basic system.

CHAIRMAN STETKAR: You are better than some people.

(Laughter.)

MR. KAWANAGO: And what we needed to assume -- and how do you say it is not the PRAs --

CHAIRMAN STETKAR: Right.

MR. KAWANAGO: -- and the discussion. However, I mean, we need to assume the gate failure and the water go to the -- a canal or cask pit. Basically, I don't want to say the PRA scope, but in a single failure, the water will go to the canal. And if we assume the additional gate failure and the water going to the -- in a cask pit, okay, that is basically worst case.

So, again, there is no drain piping, so

now if they are willing to assume some failure -- operational, misoperational, or something like that -- the water will go to the canal or cask pit. Okay? So, but still keep the total volume of the water, inventory still keep.

So of course when we calculate the boiling time, and then it is reduced from the 2.5 hours to the two hours or -- we have those -- such calculations. And, basically, we still keep the boiling time with -- it's approximate two hours. That is our calculation we have.

CHAIRMAN STETKAR: And I understand that, and I was not trying to -- I'm glad to hear you don't have drain lines from those other volumes. That is a good thing. I will still stand by my initial statement that I guarantee you I can find a drain path.

And to give you a hint of what I'm thinking about is if you look at Figure 9.1.4-2, the elevation of the top of the reactor vessel -- I'm assuming this isometric is about right -- seems to be just about the same elevation as the bottom of the slots in the weir wall.

There was an event at a nuclear powerplant in the United States a number of years ago.

This is not the specific configuration for that event. But because of a valving error during maintenance, they managed to drain the refueling water storage tank into the containment through the residual heat removal system, because of a valving error during maintenance.

So that -- and the residual heat removal system, for example, will be connected to the loops in the reactor coolant system. It will be operating during refueling. The fuel transfer tube will be open. You now have a completely connected volume of water.

And there are drainage paths through maintenance errors or equipment failures that indeed could drain that volume down to the top of the reactor vessel through the loops into the containment at full connected volume. That is one way you can get down to the bottom of that weir wall.

Now, I'm not talking about time. I'm not talking about time available for, you know, operators to isolate things. But there is a drainage path. There are mitigation possibilities, but, as I said, I guarantee I can find you a drainage path that will get you to the bottom of the weir wall.

MR. CURRY: And I think we understand your concern. If you could just give us one moment to confer --

CHAIRMAN STETKAR: Sure.

MR. CURRY: -- we'll make sure we have a path forward here.

(Pause.)

MR. KAWANAGO: We understand.

CHAIRMAN STETKAR: You understand? Okay.

MR. KAWANAGO: We understand your point.

CHAIRMAN STETKAR: I was going to say, in the interest of -- the problem is we are on the public record here, and long silences --

MR. CURRY: Absolutely. We appreciate it, sir. We understand the question, and we --

CHAIRMAN STETKAR: Okay, good.

MR. CURRY: -- will take that as an action.

CHAIRMAN STETKAR: Again, I will say it again for the record, for the staff, I personally hope that there aren't any RAIs that come out of this, because it is simply us trying to understand a bit about margins.

MR. CURRY: And that is very helpful, and we appreciate you putting it in that context.

CHAIRMAN STETKAR: Yes.

MR. CURRY: Thank you.

CHAIRMAN STETKAR: And you did confirm there are no drain lines from the refueling canal, the cask pit, or the fuel inspection pit, or the transfer tube itself.

MR. CURRY: That is correct.

CHAIRMAN STETKAR: Good.

MR. CURRY: As Mr. Kawanago said.

CHAIRMAN STETKAR: Good. And as I said there, in that case, you are indeed -- this design is indeed less vulnerable to some of these drain-down events than some others that we have looked at.

MR. CURRY: Okay. Thanks.

CHAIRMAN STETKAR: So that is -- that's why we ask these questions. You know, this gives us confidence that you are even less vulnerable than other designs to these types of events.

MR. CURRY: We appreciate that insight. That is great.

All right. Let us -- so we have discussed basically two of your questions from yesterday, the weir wall and the drain lines.

I think the question that Mr. Brown had was about the instrumentation. So as long as we are talking about the spent fuel pool, location of instrumentation, so why don't we go to that discussion.

So Mr. Kawata put together this -- and his team put together this slide for us, which kind of summarizes a little bit of the history. So in DCD Rev 3, in terms of level indication, we had two non-safety indications, and they were continuous.

All right. And we had a low low level pump trip -- pump trip on low low level. In RAI 756-5753, that was changed to make two or to add two safety grade level switches for the pump stop. We now have -- correct?

MR. KAWATA: That's right.

MR. CURRY: Okay.

CHAIRMAN STETKAR: And those -- Jim, just before -- and do those same safety grade level switches also initiate isolation of the non-safety --

MR. CURRY: Well, I think you are anticipating that --

CHAIRMAN STETKAR: I'm sorry. Never mind. Never mind. I'm in the wrong system. I'll be quiet. Go on. I'm sorry.

MR. CURRY: Not a problem, because you are probably anticipating maybe the third line.

CHAIRMAN STETKAR: Yeah.

MR. CURRY: We do have an open item.

CHAIRMAN STETKAR: Okay.

MR. CURRY: And which adds isolation of non-seismic --

CHAIRMAN STETKAR: Okay. That's -- I'm sorry, and I was getting ahead of you.

MR. CURRY: Right. So that is where we are in terms of the level indication.

Now, the locations -- I think there was a question on locations. So near --

MEMBER BROWN: Physical locations?

MR. CURRY: Physical locations --

CHAIRMAN STETKAR: And temperature?

MR. CURRY: That's true. I mean, do we have a temperature? Yeah.

MEMBER BROWN: I'm not finished with the level one yet.

MR. CURRY: Okay. Let's finish with the level.

MEMBER BROWN: Where the continuous type -- where is that read out?

MR. CURRY: Control room.

MR. KAWATA: Yes, both control room and the LOCA.

MEMBER BROWN: Okay. The reason I ask that is that in the RAI where it talks about in your all's discussion the DCD change, in your all's answer you talked about if you had to recover, it would be done with confirmation of SSP, SFP temperature, and the water level locally.

So there was an inconsistency between your answer in the 5753 -- that's why I was asking for, you know, just a little tabular readout of wherever these go, and then make sure it's reflected. When I looked at the table that you all modified, I did not see the continuous one even listed. It was just the two low level switches that was in -- let me find the right table number.

MR. KAWATA: Table 3D --

MEMBER BROWN: 3D-3. Two, excuse me. There is only two level gauges listed there. And based on the designation, those appear to be the two switches.

MR. KAWATA: We only show the safety-related, Table 3D-3. The continuous -- whatever it is, non-safety data. So we don't show that non-safety data needs to be mentioned in 3D.

CHAIRMAN STETKAR: I can kind of see the evolution of this thing. The questions were raised about need for safety-related instrumentation, so it has evolved from two non-safety, and now the RAI responses are focused on what they are making safety, and now the follow-on things are what functions are going to be performed by the safety-related. And apparently the single remaining non-safety-related continuous readout channel has been --

MEMBER BROWN: Lost in the shuffle.

CHAIRMAN STETKAR: Yeah. It's still -- it's there, but it has been lost, you know, out of the context of the discussions regarding, in particular, safety-related instrumentation.

MEMBER BROWN: Well, I am just kind of curious. We don't have a safety-related, you know, gauge that you can read. It's a non-safety-related, with nothing but a low level switch. I mean, to me it went from two non-safety-related gauges to no safety-related gauges, no visibility of the level in the main control room other than with a non-safety-related gauge.

And they used to have multiple levels of -- well, actually they have a high and a low level, although the figure that was provided in there only showed a low.

MEMBER SHACK: That's non-safety.

MEMBER BROWN: What?

MEMBER SHACK: That's non-safety.

MEMBER BROWN: No, I'm -- yeah, on the continuous one. And on the safety ones it is only a low low amount. It's not a low as well. So there is only one level indicator. I mean, I'm assuming --

MR. CURRY: The redundant safety level switches, right?

MEMBER BROWN: Well, they each feed their trains --

MR. CURRY: Right.

MEMBER BROWN: -- for the interlock purposes. I mean, at least that's the words said, that they were interlocked with their -- with one -- each with one of the two trains, whichever way you define them.

MR. CURRY: So you are correct, that is where we are at this point. We are done at safety level switches, non-safety, continuous readout.

MEMBER BROWN: The annunciation -- you say a setpoint. How low on the non-safety gauge?

MR. KAWATA: Yes.

MEMBER BROWN: I presume that is an alarm setpoint?

MR. KAWATA: Yes. We have alarms.

MEMBER BROWN: Annunciating?

MR. KAWATA: In safety items.

MEMBER BROWN: Well, those annunciate also. I think you said that in the words. The safe ones do annunciate also in the main control room.

MR. KAWATA: That's right. We use a non-safety-related instrument for normal makeup of SFP, so setpoint of the load for the non-safety, the loads are about four inches for the normal water level. The setpoint is low low for safety-related. The setpoint is below -- about four feet from the normal water level.

The purpose of that low low setpoint is to maintain the water level above the suction level --

MEMBER BROWN: I understand that.

MR. KAWATA: -- over the suction rate for pump protection. So for safety-related, to have only one setpoint is adequate, because -- so only one setpoint to maintain the pump integrity.

MEMBER BROWN: So I presume it is higher than the low low, the setpoint would be higher?

MR. CURRY: One moment.

CHAIRMAN STETKAR: I think that's what he said. He said the low level setpoint is four inches below the normal level, and the low low is four feet I think is what they said.

MEMBER BROWN: All right.

MR. CURRY: The low low is for the pump protection.

MEMBER BROWN: Yeah. No, I understand that point. I just -- I missed the specific level. I didn't catch that. Well, if that's what it is, I just --

CHAIRMAN STETKAR: I mean, in some sense, someone yesterday asked the question about, how does all of the current orders --

MEMBER BROWN: Well, that's ultimately where I was going with --

CHAIRMAN STETKAR: -- comply to a design certification. And the answer we got is the staff doesn't know yet.

MEMBER BROWN: Yeah. And --

CHAIRMAN STETKAR: So I'm hoping that by the time we see the final SER, with no open items, I'm hoping that the staff has the resolution of how the orders apply, either to the design certification or to the COL applicant, resolved by that time. Otherwise, I suspect we are going to have -- you know, the Committee may have questions about that.

MEMBER BROWN: Well, there are several of us that have brought up the issue of the instrumentation and the lack of, you know, continuous implementation and the circumstances under which the orders are being issued. And we -- so, yes, there's a couple of level gauges, that's fine if they're non-safety-related. But there are a couple of level gauges and then all of a sudden we don't have them anymore. So --

CHAIRMAN STETKAR: I mean, at least for me this clarifies --

MEMBER BROWN: Yes, I --

CHAIRMAN STETKAR: -- the current concept of the design. Now, how that may or may not change moving forward in light of the orders, in the context of the design certification, I don't think any of us know that.

MEMBER BROWN: No, I understand.

CHAIRMAN STETKAR: And the message is, this is still Phase 3 of the staff's review with open items, and we will see this again, you know, in Phase 4. And as I said, I hope that by the time we see Phase 4 the staff will have sorted out the applicability of the orders, you know, in particular to the two in progress. I mean, the same questions apply equally to USEPR.

MEMBER BROWN: Yes. I'm just respective of at least one other Committee member who, along with me, has raised this particular point, trying to make it clear that this -- there will probably be raised eyebrows at the -- during the full Committee.

I would argue that the full Committee may or may not agree with this, but, I mean, it will be brought up again in terms of the -- I don't want to say lack of, but the reduced amount of indication or the -- that may be available under some circumstances if you needed it. So it's -- and its ability to service people in the main control room.

Right now when I look at this, and I have finished reading the words, plus one other supplemental RAI that was given to me by the staff after our other conversation yesterday, there were -- there are still a few inconsistencies. I'm not going to sit here and grind through those.

This clarifies exactly what you are saying you are going to, and I would just encourage the staff and you all to make sure that the DCD changes are consistent. And I -- like you say, you only address safety-related stuff in the tables, but it would seem in the DCD, in the Tier 2 stuff, you ought to at least give an indication of where the non-safety unit reads out. Is it remote shutdown console as well as the main control room, etcetera? That just seemed to be lacking relative to where those are.

Same thing -- and I think both the temperatures, if you can flip over to the temperature, I think both of those are continuous, and they are both safety-related. And, again, where is that temperature indication clearly articulated as opposed to just locally?

A couple of your words in your discussions talked about recovering locally, which gave the implication that there was no remote indication. Whereas -- and that's why I'm saying on the other one, the level one, it just says, "I've got continuous," but where is it? That wasn't -- it wasn't crisply stated. In fact, it wasn't explicitly stated.

MR. CURRY: We appreciate that, and we understand your point about -- I think just to repeat back to you -- where is this instrument? Where can operators see and have this information?

MEMBER BROWN: And where the temperature was located in the pool itself. That was the other question.

MR. CURRY: Fairly high, two of them, safety-related at diagonal --

MEMBER BROWN: Diagonally across the

pool. You say "fairly high." What does that mean?

MR. CURRY: I don't know if we -- I don't know the exact elevation, but I --

MEMBER BROWN: It didn't seem to be specified. I couldn't find any --

MR. CURRY: Right. And I don't --

MEMBER BROWN: -- numbers.

MR. CURRY: I don't have that information here, but I guess I just wanted to get across the point that it is high in the pool and, you know, indicative of, you know, temperature in the pool area. But it is not high and low.

MEMBER BROWN: Still above the fuel level, top of the fuel --

MR. CURRY: Oh, yes, sir. Oh, yes, sir.

MEMBER BROWN: -- both of them above the top --

MR. CURRY: Oh, yes, sir. Absolutely.

MEMBER BROWN: So once the water level got below the fuel, or the top of the fuel, you would not have any indication of temperature, is that correct?

MR. CURRY: That is absolutely true.

CHAIRMAN STETKAR: Yes, you would probably be measuring air.

MEMBER BROWN: Pardon?

CHAIRMAN STETKAR: You would be measuring air at that point.

MEMBER BROWN: Well, no, you would be. If you don't have any sensors below that level, then you would be measuring air, which would be kind of useless.

CHAIRMAN STETKAR: Well, I suspect until that point it will be somewhere around 100 degrees C.

MEMBER BROWN: Well, once it starts boiling, it is what it is. It doesn't go any -- it doesn't change.

MEMBER SHACK: 100 degrees C is probably a pretty good guess, yes.

MEMBER BROWN: Okay.

CHAIRMAN STETKAR: Anyway, to kind of summarize this, I --

MEMBER BROWN: We are probably not finished with it, that is the --

CHAIRMAN STETKAR: I don't think we are finished, but I think that this information at least gives us enough to understand what the current snapshot of the design is.

MEMBER BROWN: Can we get a copy of these viewgraph pages?

CHAIRMAN STETKAR: We will get them. It's part of the public record now, so -- by the way, make sure -- you do realize that anything you show today is part of the public record. That's the caution that I read earlier regarding proprietary information. Keep that in mind as we get into some of these discussions, because everything that is shown here and anything that is said is part of the public record.

So if during these discussions -- and I would emphasize -- be sensitive if we delve into proprietary design information, let us know. We can close the meeting. We have the latitude to do that. It is simple to do. But I want to caution you about that, because we are getting into some details.

So far you have only mentioned things that are RAI responses, which are also, you know, on the docket. But if we get too far afield here, be sensitive to that.

MR. CURRY: Thank you, sir. We appreciate that.

CHAIRMAN STETKAR: And to just summarize, you know, it is all we can do at Phase -- we now have a snapshot of the current version of the design to support Phase 3 of our review. We will see the SER during Phase 4 with no open items, and I hope that by that time the whole integration or decisions regarding the integration of the orders with respect to this particular, either design certification or COLA, will have been ironed out.

And, you know, at that point in Phase 4 we can take that information, plus whatever the final resolution of the remaining RAIs and open items are, into consideration when we write our final letter, you know, on this chapter.

MEMBER BROWN: Could you flip back to the previous slide for just a minute? There is another RAI down there, 57.23, which I wanted to make a note of. That's the open one.

MR. CURRY: One moment. Is this the right -- yeah, okay.

MEMBER BROWN: I take it you all have either answered that and it hasn't been resolved with the staff, or what have you? It says open, so --

MR. CURRY: Yes. It is open. I'm not sure whether we've given a draft to the staff or whether we have formally submitted that, but yeah.

MEMBER BROWN: That's fine. That's good enough. Okay. I have it, so --

MR. CURRY: Okay. All right. Related to

the fuel pool, if you recall yesterday there was a question -- I think it was yours, Mr. Chairman -- about the RWSP line, the cleanup of the RWSP, and fundamentally how do we isolate that cleanup line, the purification loop around --

CHAIRMAN STETKAR: Yes.

MR. CURRY: -- the spent fuel pool cooling system. And on one of our slides we showed a connection to the RWSP and explained that we use the system for RWSP cleanup.

So we have confirmed there is no automatic isolation on that line. We would expect that line to be used only rarely during or after coming out of an outage. If there were leakage from that line, we would probably notice it first on some sump-level indication. We don't think the operation of the valves would be affected. I think you questioned whether they would be underwater if we had to close the valves.

CHAIRMAN STETKAR: Yeah. Either the inlet valves -- you replaced the -- you have automatic isolation valves.

MR. CURRY: You're talking about that connection to the RWSP.

CHAIRMAN STETKAR: The automatic

isolation valves -- and I've forgotten -- the problem is I only have a Rev 3 -- you had it yesterday on one of your slides I think.

MR. CURRY: Yes, if I could get the presentation up from yesterday. Thanks, Ilka.

CHAIRMAN STETKAR: And I've forgotten -- unfortunately, the only thing I have printed out is -- and I know -- is the Rev 3 -- it's Slide 15 of your SFPS -- SFPCS presentation. There you go.

Now, did I recall yesterday that in interim Rev 4 the -- did you say you changed the outlet valves? Right there. Those are now automatic isolation valves. That doesn't help the RWSP.

MR. CURRY: This one.

CHAIRMAN STETKAR: Yeah, yeah. And the inlet valves up at the top are still manual valves?

MR. CURRY: So sorry. So this is the path that we are talking about.

CHAIRMAN STETKAR: Yes.

MR. CURRY: Right? Okay.

CHAIRMAN STETKAR: Yes. Inlet there through the demineralizer back through the common cross-tie line back to the -- that path.

MR. CURRY: Right. Here is the automatic extension on --

CHAIRMAN STETKAR: Yes.

MR. CURRY: Okay. Right. And I think that was your question --

CHAIRMAN STETKAR: That's right.

MR. CURRY: -- from yesterday.

CHAIRMAN STETKAR: Yeah, yeah.

MR. CURRY: So as I mentioned, we researched that there is no automatic isolation. We would expect operator action, you know, to isolate that path. You asked how often it would be used. It would be rarely used.

CHAIRMAN STETKAR: And that is based on experience from similar --

MR. CURRY: Right. And the purpose.

CHAIRMAN STETKAR: That makes sense. I was just curious from -- some plants that have stand-alone refueling water storage tanks have a little continuously operating cleanup loop on them. I mean, I have seen many designs. This one is -- you know, because of your pit, you use this. I was just curious, based on the operating experience, how frequently people need to do cleanup on that. It's just a little different than a tank.

MR. CURRY: Okay.

CHAIRMAN STETKAR: And those valves that

show on this drawing around the demineralizers are all located in the demineralizer rooms, is that correct?

MR. CURRY: These valves?

CHAIRMAN STETKAR: Yes. I mean, that doesn't help the RWSP in particular here.

MR. CURRY: No, no.

CHAIRMAN STETKAR: But that was for other concerns about potential draining of the spent fuel pit.

MR. CURRY: Well, actually, we can talk about that one.

CHAIRMAN STETKAR: Okay.

MR. CURRY: Let's talk about that question next. We have that on our list. I think that question had to do with manual -- well, the question that we had on the list was the floor drain question from that area, and you had asked a question --

CHAIRMAN STETKAR: Oh, yes.

MR. CURRY: -- about closing the floor drains, why were the floor drains --

CHAIRMAN STETKAR: Not from this area. That was from the -- that was from the safety-related rooms.

MR. CURRY: Okay.

CHAIRMAN STETKAR: That was a different question regarding the --

MR. CURRY: Okay.

CHAIRMAN STETKAR: -- equipment and floor drain system --

MR. CURRY: Right.

CHAIRMAN STETKAR: -- in particular, that -- I don't recall having a question about floor drains from this --

MR. CURRY: Okay.

CHAIRMAN STETKAR: -- this room.

MR. CURRY: I think you're correct.

CHAIRMAN STETKAR: I was just curious about if someone -- if the operators had to go in and locally isolate this part of the system, either because of leakage --

MR. CURRY: These valves, okay.

CHAIRMAN STETKAR: -- those valves, you know, now the -- and even the other -- the valves that you have made automatic, the return valves to the spent fuel pool, are those valves physically located in the room with the demineralizers, or are they outside of that room? In other words, are they accessible, and could they be affected by flow?

MR. CURRY: One moment.

(Pause.)

Maybe, Mr. Chairman, we can check on that. I don't think we know the answer right now.

CHAIRMAN STETKAR: Okay.

MR. CURRY: Maybe we can put that to bed before we leave today.

CHAIRMAN STETKAR: Thanks.

MR. CURRY: All right. I think there was a question -- I think this kind of takes care of our questions on 9.1. that we had from the Committee. There was a question on -- or I should say 9.1.3 to be more exact. I think there was a question in 9.1.4 about the polar crane, seismic restraints on the polar crane.

CHAIRMAN STETKAR: Not the polar crane, the cask --

MR. CURRY: Well, the cask crane --

CHAIRMAN STETKAR: -- the cask crane. It does?

MR. CURRY: -- restraint. It does. Are you answering or --

CHAIRMAN STETKAR: No. You said polar crane. The question is: does the cask --

MR. CURRY: Have the same restraints.

CHAIRMAN STETKAR: -- have the same

restraints for, you know, tipping or preventing derailment basically.

MR. CURRY: Right. And the answer is yes.

CHAIRMAN STETKAR: It does. Good. Thank you.

MR. CURRY: All right. We had a question in 9.2.2, and that -- that really came up with regard to the 10 minutes for restoring cooling to the RCP pumps.

CHAIRMAN STETKAR: Yes.

MR. CURRY: And you questioned, well, what is the basis for the 10 minutes?

CHAIRMAN STETKAR: Yes.

MR. CURRY: And whether we would get into any trouble with vibration before that time. So the limiting reason for that cooling is bearing cooling.

CHAIRMAN STETKAR: That is bearing cooling.

MR. CURRY: Right. But heatup of the bearing versus the motor or things like that. So it's the bearing and it's a manufacturer's recommendation and the manufacturer tells us, you know, if you can get cooling back to the bearings within 10 minutes there is no significant vibration of the pump.

CHAIRMAN STETKAR: And just let me make sure, Jim, so that I understand it, because everything that I had read seemed to have -- seems to say motor cooling. But you're saying it is indeed bearing cooling. Because, you know, there are three coolers. There is the upper bearing lube oil cooler, the lower bearing lube oil cooler, and, you know, what is called the motor cooler, which I'm assuming is the motor winding cooler.

MR. CURRY: Right. And I think the question was, which one of these guys is limiting.

CHAIRMAN STETKAR: Yes.

MR. CURRY: And based on our research, the driver for the 10 minutes is the bearing.

CHAIRMAN STETKAR: Is the bearing, and that is -- actually, from my experience that is normal. That's why I was asking the question about why the motor was limiting. So it is the bearings, and it just --

MR. CURRY: Manufacturer's recommendation.

CHAIRMAN STETKAR: Manufacturer's recommendation. So you can -- you have assurance that if you can get it back in 10 minutes you are okay. You just don't necessarily know what the margin is to

-- you know, at 10 minutes and 30 seconds, do things get really bad, or is that just a manufacturer being very --

MR. CURRY: At this point, that was --

CHAIRMAN STETKAR: -- conservative.

MR. CURRY: -- that was what we used to set the 10 minutes.

CHAIRMAN STETKAR: Thanks. That at least helps, and to know that it's the bearing helps. I don't know what to do with it, but it helps. And I think you mentioned there is still an open RAI out through Chapter 8 or something like that about the basis for survivability of the pumps under loss of cooling. Is that right, Paul? Right, yeah.

MR. CURRY: All right. I think there was a question also in 9.2.2 about component cooling water, and do we have a problem. And, actually, I think this was a question to staff, so just very briefly, you know, we do not have a problem with pump runout if we open one train versus another train. You know, one pump of a CCW train provides cooling to both trains.

CHAIRMAN STETKAR: Right, right.

MR. CURRY: 9.2.6, there was a question about the dyke around the demineralized water storage tank. Answer is no.

CHAIRMAN STETKAR: Okay.

MR. CURRY: No dyke.

9.2.7, there was a question --

CHAIRMAN STETKAR: If you -- hold on just a second. I'm a slow writer, and I'm still back jotting down notes on the reactor coolant pumps.

(Pause.)

We eventually get the transcripts, but I hate going through those.

Let's see, no dyke.

Okay. I'm caught up, thanks.

MR. CURRY: Okay. The dyke question, 9.2.6, no dyke around the demineralized water storage tank.

CHAIRMAN STETKAR: Okay.

MR. CURRY: 9.2.7, Question G, the Committee was surprised that the electric pump, EFW pump heat load was higher than the turbine-driven pump heat load. The answer to that is the calculation for the electric pump was simply based on an efficiency-type calculation. So if the pump was 80 percent efficient, we assumed 20 percent went into the room and was a heat load to the room.

For the turbine-driven EFW pump, that is not the way the analysis took credit for installation of the pump and supporting exhaust piping. So that is why that heat load was not so significant.

CHAIRMAN STETKAR: Okay. So it is basically a different -- difference in the analysis.

MR. CURRY: Just in the analysis. All of the energy, all of the waste heat from the electric pump, was assumed to heat up the room.

CHAIRMAN STETKAR: Yes.

MR. CURRY: Not the case for the turbine-driven pump. You know, it is contained, goes back into the water, for example.

CHAIRMAN STETKAR: Okay. At least that is an explanation for the different -- I mean, you know, you are using it to size the ECWS capacity, and it is pretty conservative, you know, for the motor-driven. It explains the difference. Thanks.

MR. CURRY: 9.2.7 --

CHAIRMAN STETKAR: Hold on a second. As I said, I'm a really slow writer.

(Pause.)

MR. CURRY: And apparently, you know, the staff also asked the same question during an audit, so --

CHAIRMAN STETKAR: Oh, okay. We don't

get the RAIs. We don't even hear about the audits.

MR. CURRY: Okay.

CHAIRMAN STETKAR: Okay. Thanks, Jim. I'm caught up.

MR. CURRY: Related to that, there was a question about turbine-driven EFW pump and whether steam leakage was considered. And, you know, based on Japanese experience -- and also the question was Japanese experience, whether steam leaks were common, the answer to that is no. And steam leakage wasn't considered in the turbine-driven EFW pump room calculation, heatup calculation. The view is that such leakage would be minor and is encompassed by the margin.

CHAIRMAN STETKAR: Okay.

MR. CURRY: Also, in 9.2.7, there was a question about double-lock closed isolation valves on the line from the CCW to the fan coolers.

CHAIRMAN STETKAR: Yes.

MR. CURRY: And the short answer to that is there is only one locked closed valve on each line. It is not a double-lock closed valve, so it meets the requirement.

CHAIRMAN STETKAR: Yes. I was going to say those two single -- they are called lock closed, you know, motor-operated valves, which I'm assuming means that the motor is deenergized. Those are the two valves, one on the inlet and one on --

MR. CURRY: That's correct.

CHAIRMAN STETKAR: -- on the return.

MR. CURRY: Correct.

CHAIRMAN STETKAR: Okay. Okay. Thank you.

MR. CURRY: And then there is a question in 9.3.3, this is the one I misspoke on earlier about the floor drains in the ESF room. And you kind of questioned, well, why did we close -- why did we have normally closed valves versus open? And Mr. Nishio gave you the answer that --

CHAIRMAN STETKAR: I understand the concern about not coupling -- I think you characterize them as the east and the west sides, you know, through the common drain system. I understand that concern.

MR. CURRY: And I think you asked a question about balance. Well, gee, how did you -- did you overweight one issue or --

CHAIRMAN STETKAR: Right.

MR. CURRY: -- another? And we reviewed that. You questioned, well, could check valves have done the job? Again, it is a safety-related function.

The desire was to have valves that you could monitor. There is a sump in those rooms that has level indication. So if you had a leak -- that level indication that's in the control room, so if you had a leak, the operator could take action to open the drain valves if necessary.

So with the balance of the safety concern about keeping those -- the east and west sides separated, and the monitoring of potential leakage, which would allow for operator action to open the drain valves, the decision was to keep those valves normally closed.

CHAIRMAN STETKAR: And you said each room does have a sump with a level --

MR. CURRY: Yes.

CHAIRMAN STETKAR: -- level indication or a level alarm.

MR. CURRY: Yes, sir.

(Pause.)

CHAIRMAN STETKAR: Okay.

MR. CURRY: And then that brings us up to 9.5.1, the fire protection. You had a question about, really, the convergence of the four trains. And Mr. Ron Reynolds is back. He can explain that issue.

MR. REYNOLDS: Okay. Well, good morning.

Yes. We looked at the convergence of all four trains to the control room. That is the question. And the question is, do we have physical separation as all four trains enter into the control room?

And what we found is, yes, we do have that. As of yesterday, I thought we may have had a chance of some fire wrap being needed, which is certainly not an issue. But we had to go through the cable routing to determine that in fact we have the separation.

So I would ask the ACRS Committee to look at DCD Figures 9.A-3 and 9.A-5. Now, those figures are layouts --

CHAIRMAN STETKAR: Yes.

MR. REYNOLDS: -- and they are SRI.

CHAIRMAN STETKAR: Right.

MR. REYNOLDS: And so if we needed to go into more detail and description of how that happens, I would certainly be glad to give that. We probably need to do that --

CHAIRMAN STETKAR: We would have to close the meeting.

MR. REYNOLDS: That's correct, sir.

CHAIRMAN STETKAR: Let me ask, Ron, before we decide -- let me ask the other members. Do we want to look -- I see people searching on their computers, so they are probably looking at the figures. I looked at those figures yesterday. Are those figures -- you know, they're at specific elevations.

MR. REYNOLDS: Correct.

CHAIRMAN STETKAR: Is there any intermediate volume in an elevation between those two horizontal slices? In other words, the one thing -- I can't figure the figure number -- the one figure number shows distinct compartments with walls around them. The other figure shows simply the footprint of the main control room. Do the walls that are shown on the lower figure extend -- and tell me when I get into too sensitive things here -- extend all the way up to the main control room?

MR. REYNOLDS: Right. Simply -- I think your understanding is correct. It is an extension.

CHAIRMAN STETKAR: It does.

MR. REYNOLDS: As you look -- Figure 9.A-3 and 9.A-5, there is a 9.A-4 that has that intermediate level. And the rooms in discussion here are a continuation.

CHAIRMAN STETKAR: Are a continuation. Okay, great. Thank you. And 9.A-4 -- I probably missed 9.A-4.

MR. REYNOLDS: Well, that's not one that I was asking about. 9.A-4 is an intermediate interval.

CHAIRMAN STETKAR: Okay.

MR. REYNOLDS: But in most cases you will find just the footprint with an X through it, which represents that that wall would --

CHAIRMAN STETKAR: Oh, okay.

MR. REYNOLDS: -- or room would continue up to the next level.

CHAIRMAN STETKAR: Thank you. I'm not going to ask how you get -- so all of -- essentially they remain separated by division until they get to the main control room. And then, in the main control room --

MR. REYNOLDS: That's correct.

CHAIRMAN STETKAR: -- whether it's the sub-floor area in the main control room that you do all of the cross-talk there --

MR. REYNOLDS: That is correct.

CHAIRMAN STETKAR: Okay. Okay, good. I mean, that's good. Good. Thank you.

MR. REYNOLDS: You're welcome.

MR. CURRY: So, Mr. Chairman, that is the list of questions we have that we took yesterday. And so from our understanding at this point, we -- I have one action item that we talked about, which was the weir wall calculation.

CHAIRMAN STETKAR: Yes, the weir wall heatup.

MR. CURRY: So at this point that's where we think we are with regard to the Committee.

CHAIRMAN STETKAR: Well, you have a much better perspective than I do, because I have piles of notes and things here. What we will do is, after these meetings we always go back and go through the transcripts and go through our notes.

And if there are any remaining questions that we have, what we have typically done in the past is we will highlight them and make sure that they get to you probably through the staff. I think that is the way we have been doing it, right, Ilka? You know, in a sense of completeness.

I certainly appreciate you -- you obviously, as you said, either late night or early morning or really late night, I really appreciate all of the effort that you have put in. MHI has -- continues to be very, very responsive to these things. And we certainly -- we really appreciate this. It helps us. It keeps the process moving, and I certainly thank you very much.

Either of the other members have any further questions or points?

(No response.)

Well, thank you. I appreciate it. And thank you very much.

MR. CURRY: We thank the Committee. Thank you.

CHAIRMAN STETKAR: Did you want to say something?

MS. BERRIOS: If you want to take a break or you wanted to go straight with --

CHAIRMAN STETKAR: It depends on -- Paul, how long do you think you will need?

MR. KALLAN: Not long.

MR. HAMZEHEE: Ten to 15 minutes.

CHAIRMAN STETKAR: If it's 15 or 20 minutes, why don't we just go to completion. If it was going to be half an hour or 45 minutes, I would take a break. But let's --

MR. HAMZEHEE: It's about 10 to 15 minutes.

CHAIRMAN STETKAR: Fine. Let's just finish up with the staff and we can all happily depart.

(Pause.)

Let me just clarify things. Bill, to get it on the record -- I was kind of asking you offline, but you were talking loud enough that it was picked up. I had a question about -- you had a question yesterday about the possible anomaly of the performance of Metamic material.

MEMBER SHACK: In BWR and PWR environments.

CHAIRMAN STETKAR: You know, pure water versus high pH borated water. And you have looked at that and thought about it and it's okay.

MEMBER SHACK: Right. I mean, I have looked at the experience with it and it's good. I have looked at a number of reports telling me that it is -- it really -- you know, you do want to use -- or, you know, you may want to consider using the anodized version in the BWR. In a PWR, it's good.

Then, I was trying to figure out why that would be the case, because normally one things of aluminum oxide as being very stable at pH 7 and the solubility goes up as you go either acid or base. And we had the same anomaly actually in considering GSI-191 stuff at Argonne when we made aluminum precipitates and we suddenly found that it would dissolve in high purity water at pH 7 and it was quite stable in borated water at ph 5.

And that -- we finally concluded to ourselves that the problem was that you can't just look at solubility in terms of pH alone. There is an important factor of ionic strength, and in BWRs there isn't a floating -- there is not an ion to be found. I mean, the conductivity that they maintain is so low that it is incredible, and that is really what explains the difference in performance when you look at the nominal pHs and say, "It should be worse in PWRs, and it just isn't."

And as I say, that is consistent with our own lab experience with aluminum oxide for a completely different situation, but still looking at that solute stability and it just -- my chemists keep telling me I have to keep thinking about ionic strength, and I just sort of go first order to pH and get it wrong every time.

CHAIRMAN STETKAR: Thank you. So at least that -- I mean, that was kind of a lingering thing. You said you were going to go look at those reports. So that -- good. That's closed out.

Okay. Paul, it's yours.

MR. KALLAN: All right. So we have some followup answers to the questions that were -- that you asked yesterday. And we will start off with 9.2.5. I'll turn it over to Larry with regards to the ultimate heat status.

MR. WHEELER: Good morning, Mr. Chairman. I'm Larry Wheeler, Balance of Plant. And one of the items left over from yesterday was the design basis statement in 9.2.5.1, which talks about the reference to Reg Guide 1.27 and 36-day cooling related to a pond.

And I handed you a copy of Reg Guide 1.27. There is a discussion -- a long discussion related to meteorological conditions related to 30 days and 36 days using a pond. So I would recommend that I work with MHI and we kind of clean up the DCD, not that we are going to resolve it here, but maybe just refer that Reg Guide 1.27 applies and get rid of the cooling pond.

CHAIRMAN STETKAR: I think for expedience that might clarify any questions. Again, for the design certification, it is a moot point, because this is all COL.

MR. KALLAN: That's correct.

CHAIRMAN STETKAR: But for stability with the COL, especially -- I think you mentioned yesterday that Reg Guide 1.27 is in the process or review and revision and update. And I did read the Reg Guide last night. I am better educated than I was 24 hours ago. And sometimes better education leads to improved confusion. So we will just leave it that way.

At least you have answered my question. I was asking, you know, primarily what was -- was there regulatory, you know, guidance. And you pointed me in the right direction, so --

MR. KALLAN: Okay.

CHAIRMAN STETKAR: Thank you.

MR. KALLAN: Okay.

MEMBER BROWN: For somebody like me who is non-initiated into this nuance, this is an educational question, since we have a few minutes, if you don't mind. If I read your notes on 1.127 -- I'm trying to differentiate between cooling ponds and spray ponds. I mean, at 30 days -- if I look at 1.27 it kind of says 36 days -- 30-day supply of water.

MR. WHEELER: Right. That's my first -- 30 days.

MEMBER BROWN: But then it says 36 days for spray ponds.

MR. WHEELER: That's right.

MEMBER BROWN: I know if you're not spraying, I mean, what is -- is meteorological conditions, what --

MR. WHEELER: Well, I'll read to you from what the reg guide says. Not that that is going to help.

MEMBER BROWN: Probably going to have a brain freeze here.

MR. WHEELER: This is an example under the meteorological conditions paragraph. As an example, consider cooling ponds as a heat sink where the pond temperature may reach a maximum of five days following a shutdown. So what they are saying is for a pond, that maximum heat load to the pond is not going to get there for five days. So that is kind of my thought process of where the 36-day came from.

MEMBER BROWN: Okay. I remembered you talking about that yesterday, this five days. In other words, so initially you start off at some temperature for the pond. And if you -- and then you are using it under some conditions, that it takes five days to reach a maximum temperature that it is allowed to operate. Is that what you mean by "maximum temperature," or is that a stable equilibrium temperature? Or don't know?

MR. WHEELER: I can't --

MEMBER BROWN: Okay.

MR. WHEELER: I can't really comment on what is in the reg guide.

MEMBER BROWN: All right. We'll --

CHAIRMAN STETKAR: I think, you know --

MR. WHEELER: If we were designing spray ponds, I would probably, you know, learn a lot more information before walking in here, but --

CHAIRMAN STETKAR: I think the preface is -- the problem is, the discussion in the reg guide, in my interpretation of it -- and this is only my interpretation. I think any number of us in this room might have slightly different interpretations. It cites a couple of examples about how one might assign the most conservative meteorological conditions depending on a specific design of what you call the sink.

MEMBER BROWN: That's right. And that's the --

CHAIRMAN STETKAR: And they call it the --

MEMBER BROWN: -- external environment, like humidity, stuff like that?

CHAIRMAN STETKAR: That's right.

MEMBER BROWN: Okay.

CHAIRMAN STETKAR: That's meteorological, and they call it the sink. One example that they use is an actual draft cooling tower where you are obviously evaporating -- you know, you are designed to evaporate a volume. And they give an example about, you know, how one might divine the most limiting dry bulb temperature to use in your calculation to give you assurance that you have a 30-day cooling capability.

The other example they use -- and Larry cited it -- is a cooling pond. It doesn't say spray. It doesn't say cement pond. It doesn't say -- you know, it says pond, and it says, you know, in my interpretation you could use a five-day heatup time, plus an additional day for, you know, extreme meteorological conditions, and then 30 days.

But ultimately, the bottom line, the regulatory position consistently cites the fact that you need to demonstrate a 30-day cooling capability --

MR. WHEELER: Correct.

CHAIRMAN STETKAR: -- under limiting meteorological conditions.

MR. WHEELER: That's right.

CHAIRMAN STETKAR: And I think how you

develop those meteorological conditions for your site-specific configuration of whatever you call the sink, you know, probably a needs a bit better elaboration in an update to the reg guide.

MEMBER BROWN: Okay. I quit.

CHAIRMAN STETKAR: But I know where the 36 came from.

MR. WHEELER: I am on the committee to revise that reg guide, so I will take that note back and --

CHAIRMAN STETKAR: What is your schedule for it, just out of -- do you have one?

MR. WHEELER: It has been ongoing for two years. I don't know when we are supposed to present it.

CHAIRMAN STETKAR: Fine. We'll see it, you know, once --

MR. HAMZEHEE: John, if you are interested, we have a schedule for all the reg guide updates --

CHAIRMAN STETKAR: Yes.

MR. HAMZEHEE: -- SRPs. We can communicate that to you when you are available.

CHAIRMAN STETKAR: They always come to us before they are issued for comments, and then we make a decision whether we want to look at them at that time. They come back after public comments are resolved, and more frequently we look at them, you know, at that time. So we are plugged into that process.

MR. WHEELER: If we could move on, we will discuss 9.2.2. What I threw up here is just the Tier 1 figure. This shows the overall configuration of the Alpha and Bravo CCWS loops.

If you go to the next slide, I wanted to blow this section up, so we can talk about the cross-ties between in this case Alpha and Bravo.

The cross-tie discussion was an RAI 4365, Question 9.2.2-58. And in that response, which was related to the thermal barrier isolating and what to do with that scenario, this was MHI's response to allowing the Alpha/Bravo in this case to essentially not be isolated, to have the MOVs, the 7s, and the 20s open.

And in that response, they assumed on an ECCS signal the CCWS pump does not start. Therefore, the 145 valves do not open.

Now, by the way, the 145 valves, which you see on the discharge of the Alpha CS RHR heat exchangers, those are normally closed. And those 145s ought to open on an ECCS, plus a CCWS pump start. So an ECCS start by itself are not going to open.

CHAIRMAN STETKAR: It doesn't open those. You have to have the interlock with the pump start.

MR. WHEELER: You have to have the permissive from the pump being open, and the ECCS, and then that 145 valve goes open.

Now, 145 MOV takes about 120 seconds to open.

Now, a little bit more details about the flow paths, that if the Alpha train doesn't start, the B pump is now going to pick up the loads going to the opposite train. The flow through this ECW pump for this cooler is about 40 gpm. It's a small line about an inch and a half.

For the SI pump, it's 180 gallons per minute. It's about a three-inch diameter. And containment spray pump, that is 80 gpm, and that's a two-inch diameter pipe. So we are talking relatively small flows compared to the overall -- I think it's 12,000 gpm flow rate.

CHAIRMAN STETKAR: As long as the 145 valve is closed.

MR. WHEELER: That's my next --

CHAIRMAN STETKAR: Okay.

MR. WHEELER: -- my next point. The RAI response was limited to only looking at that scenario. It didn't really look at other events, and I kind of touched upon that yesterday, that if you actually get the ECCS or the station blackout, both Bravo trains come up, pump starts, the 145 goes open, 120 seconds later that valve is now full open, and 121 seconds into the event you lost your pump, your gas turbine, your electrical bus. Now you are going to get yourself into concern, because now you are picking up 4,400 gpm to that 14-inch line.

CHAIRMAN STETKAR: And the associated heat load, if we are talking about a LOCA.

MR. WHEELER: Exactly. So to back up, the RAI response was limited. The analysis needs to -- we need to look at that a little further to evaluate a maybe more limited scenario that now looks at that 145 valve being open. And the 24 hours to close that isolation between trains would not be acceptable.

CHAIRMAN STETKAR: Thank you. This, by the way, points out, you know, the design basis analysis. You have to assume a single failure. Assuming a single failure at time T-zero --

MR. WHEELER: That's right.

CHAIRMAN STETKAR: -- in this case is not necessarily the most conservative single failure. And that is -- thank you. This helps a lot.

MR. WHEELER: And I did point out yesterday, thinking that that 145 valve didn't open, and that is why it didn't open, because --

CHAIRMAN STETKAR: Because it was at T-zero.

MR. WHEELER: Right, yeah.

CHAIRMAN STETKAR: I mean, it was -- you know, the simultaneous, whatever, loss of offsite power with the limiting single failure presumed to be the GTG would get you that at T-zero.

MR. WHEELER: So the staff has an audit coming up with MHI next month, so I am sure we will have a little bit more discussion on this one.

CHAIRMAN STETKAR: Thank you.

MR. WHEELER: Moving on to the next slide, your references yesterday related to where the 24-hour duration for operator action, and I pulled the insert from the SECY-77-439.

CHAIRMAN STETKAR: Okay.

MR. WHEELER: And I bolded the section that MHI referenced in their RAI response saying that there is sort of a definition of establishing long-term cooling and that is the 24-hour period of time, and then they use that for kind of a signal for success for the operators to get them -- the valves closed, so that you can get off into long-term cooling.

And, once again, we will have to go back and revisit this now that there is kind of a more limited scenario that we need to evaluate.

CHAIRMAN STETKAR: But this is at least --and thanks for dredging this up. I didn't have the opportunity last night to find this one.

MR. WHEELER: And I have a copy of the SECY I can leave with you if --

CHAIRMAN STETKAR: Yes, I'd appreciate that, or, you know, give it to Ilka, so -- make sure that we get it distributed to everybody on the Subcommittee.

MR. WHEELER: Any other questions for ESW, component cooling, ultimate heat sink? Those are the ones that I --

CHAIRMAN STETKAR: Again, if you would bear with me for a couple of minutes, because I am a slow writer. I just want to make sure I make a couple of notes here.

(Pause.)

Okay. I apologize. I am a slow writer. But as I age, my retention is about 15 minutes. So if I don't make notes, I will forget it by the time I hit the door over there.

MR. KALLAN: Okay.

CHAIRMAN STETKAR: Thanks, Paul.

MR. KALLAN: There was a question on 9.1.3.1 with regards to the inconsistency in the temperature with regards to the DCD and the SER, and I wanted to turn it over to Raul Hernandez.

MR. HERNANDEZ: Yes. The description in that section of our FSAR is addressing the design criteria for the spent fuel pool cooling system, and it found, yes, there was an inconsistency.

The system is designed to maintain less than -- to maintain the water in the spent fuel pool less than 120 with both trains running. So I will need to correct this statement here that with a single active failure the temperature will not reach higher than 140.

CHAIRMAN STETKAR: With a half core.

MR. HERNANDEZ: Yes.

CHAIRMAN STETKAR: I'm sorry. Any single act of failure regardless -- half core, full core.

MR. HERNANDEZ: Well, you know, his first thing when he started looking at the half core, yes, the single act of failure applies to either one of them.

CHAIRMAN STETKAR: Right, right.

MR. HERNANDEZ: And it would be --

CHAIRMAN STETKAR: And the operative is 140 under that. Okay. Thanks. Thanks.

MR. HERNANDEZ: That statement was taken from the DCD.

CHAIRMAN STETKAR: I actually had to craft myself -- looking at all of the words in the DCD and the SER, I had to put together a little table with half core, full core, spent fuel, pit cooling trains, RHR, CS trains, and try to divine all of the things. That was the inconsistency, so --

MR. HERNANDEZ: Yeah. The inconsistency was the statement of the single act of failure.

CHAIRMAN STETKAR: Right.

MR. HERNANDEZ: The system is designed for 120, with both trains on it.

CHAIRMAN STETKAR: With both trains, 140 with a single act of failure.

MR. HERNANDEZ: Yes.

CHAIRMAN STETKAR: Yes. As I said, it wasn't -- I just wanted to make sure I understood that the table I put together was right, that I wasn't missing something. It is not a concern about the design of the system or, you know, any safety concern essentially. So thank you.

MR. HERNANDEZ: Yes. And in answering one of the other comments from the members about the heat load at that particular scenario, the DCD specifies that that is with a full pool and all of the locations are full. So it is a -- the limiting heat load at that moment.

There was also a comment on -- oh, let me wait until you finish.

(Pause.)

Another comment that you had on Section 9.1.3 was dealing with the particular RAI that I submitted about the shutdown of the spent fuel pool cooling pumps and the restart of the pumps. You were asking if -- why we didn't ask for a COL action for that particular procedure.

The determination when we need a COL action item basically comes down to staff -- to our consideration. You know, when we look at it, it is -- those actions are different from what we normally see, normal operations.

In this particular case, the actions

required are pretty straightforward -- you know, initiating a pump, checking levels. It is not asking for the operator to go outside of the containment -- outside of the control room to physically go to a specific location.

It is -- they are monitoring the temperature of the spent fuel pool, and when the temperature goes high they would have to take actions. And the actions are not something that they normally wouldn't do -- you know, check temperature, check level, and restart pumps. That's why I did not require a COL action item for this particular.

CHAIRMAN STETKAR: Okay. And that is -- looking for the thought process, and you have explained that. I mean, I think it is reasonable to presume that the COL applicant will look at the design of the plant and write, you know, procedural guidance consistent with that design. And you have pretty well explained sort of the thought process that the staff goes through about, you know, any need to specifically highlight things or not. So I think that makes sense.

MR. HERNANDEZ: When we talking about, you know, going outside of where the operators are normally located, or having to move to a specific location to take certain actions, that -- it is more demanding, and it's not going to be so straightforward, so simple as just when you are inside a control room and typical monitoring of the situations of the plant conditions.

CHAIRMAN STETKAR: All right.

MR. HERNANDEZ: Have any other questions on the spent fuel pool, spent fuel pool cooling?

CHAIRMAN STETKAR: I don't recall any. But as I said, I think that, yeah, we pulled together everything at the conclusion of the meeting. If there is anything that we missed in today's discussions, we will summarize it and make sure we get it to you.

MR. HERNANDEZ: You also had a comment on Section 9.1.4 where we are talking about draindown of the refueling cavity.

CHAIRMAN STETKAR: Yes.

MR. HERNANDEZ: There was a statement in the staff evaluation that their makeup capability is higher than the draindown. That statement came out of the responses to the staff's RAI. The staff sent two different RAIs dealing with draindown path from the refueling cavity. We specifically asked them to look into all of the connecting systems and look for possible draindown path.

The applicant went through in one of the responses and enumerated all of the different -- well, tabulated -- they put a table together with all of the different possible draindown paths and what would be the worst possible case. It was determined that the worst possible case was the drain for the reactor cavity area. And there makeup capability from the refueling water storage tank was higher than the maximum expected draindown path.

So I guess that we could rephrase the statement in the FSAR to point out exactly that we are referencing the expected draindown or the evaluated draindown, not --

CHAIRMAN STETKAR: I think that would help a lot, because the connotation of "any" is --

MR. HERNANDEZ: It was "any" from the evaluation.

CHAIRMAN STETKAR: -- is pretty large. By the way, do you have a reference for that particular RAI response?

MR. HERNANDEZ: Yes.

CHAIRMAN STETKAR: So that we can --

MR. HERNANDEZ: I have two RAIs. The original RAI was RAI 507-3393.

CHAIRMAN STETKAR: 507-3393.

MR. HERNANDEZ: Yes.

CHAIRMAN STETKAR: Okay.

MR. HERNANDEZ: Question 9.1.4-16.

CHAIRMAN STETKAR: 9.1.4-16. Okay.

MR. HERNANDEZ: And then subsequent RAI was RAI 633-4857.

CHAIRMAN STETKAR: 4857.

MR. HERNANDEZ: Question 9.1.4-21.

CHAIRMAN STETKAR: 9.1.4-21. Okay.

MR. HERNANDEZ: This is the response that has the table.

CHAIRMAN STETKAR: And the second one has the table?

MR. HERNANDEZ: Yes, the second one.

CHAIRMAN STETKAR: Okay. Could you make sure -- just get that to Ilka, so that we can take a look at it.

MR. HAMZEHEE: You should have it.

CHAIRMAN STETKAR: Okay. Yes, I'm --

MR. HERNANDEZ: This is with the RAIs dealing with refueling cavity seal, and we looked more than just the cavity seals and the other seals in that area. We also looked at other draindown paths.

The FSAR -- we will revise it to be -- specifically highlight that this is not a general statement for any leakages, just the ones that we evaluated.

CHAIRMAN STETKAR: That would help to clarify I think. And it's good -- and I think it's really good to have that background document. It essentially does what I was asking. You know, I was challenging this notion of, how can you say "any"? But it does say that, as a response to an RAI, there was a consistent evaluation done, which essentially is what I was driving at, you know, through the questions. So that's good.

Ryan?

MR. SPRENGEL: This is Ryan Sprengel. Just a clarification. We are talking about the SER.

MR. HERNANDEZ: Yes.

MR. SPRENGEL: Correct? Not the FSAR. Okay. Okay.

MR. HERNANDEZ: Well, yes.

MR. SPRENGEL: I just wanted to clarify.

CHAIRMAN STETKAR: Thanks for clarifying it.

MR. SPRENGEL: So the changes to the SER, without open items in the future, and then finally the FSER. That's my understanding.

CHAIRMAN STETKAR: Yes, thank you. Thanks for the clarification. That's important for the record.

Paul?

MR. KALLAN: There was a question on 9.1.5 with regards to heavy load crane. And it was Section 9.1.5.4 with regards to what are the SSC important to safety, and is it equivalent to safety, important to safety. And I don't think at this point -- I mean, we --

MS. McKENNA: This is Eileen McKenna. We are not prepared to respond to that at this time. I do actually have a followup, though, for the question about the chilled water system and why it is not in the tech specs.

I think the SER didn't really explain why it was not in the standard tech specs and just said that because it's not in the standard it's not in this application. But the basis is that the essential chilled water system is a support system to the rooms -- to the systems that are in rooms that it services. And the way it is handled through the tech specs is through the definition of operability for those systems.

In particular, if I may quote from the definition of "operability," a system, subsystem, train, component, or device shall be operable, or have operability, when it is capable of performing its specified safety functions and when all necessary attendant instrumentation controls, normal or emergency electric power, cooling and seal water, lubrication, and other auxiliary equipment that are required for the system, subsystem, train, component, or device to perform its functions are also capable of performing their required support functions.

So as a specific example, if the chillers are out of service in the space where, say, the turbine-driven emergency feedwater pump is located, it would be the responsibility of the operators to evaluate whether, given whatever that condition of the cooling for that space, whether that pump remains operable. And if they determine it is not operable, they would follow the limiting condition for operation and the actions associated with the pump.

CHAIRMAN STETKAR: Okay. I understand all of that, and I will ask you why, then, do we have technical specifications on ac electric power, dc electric power, gas turbine generators, diesel generators, essential service water systems, component cooling water systems? And I probably missed a few, which are all support systems which would in principle be covered under those statements that you just made.

Why do we have tech specs that are very explicit on all of those other things?

MS. McKENNA: The basis for when we have LCOs or criteria that are written into 50.36, and one of them that probably captures most of the things you are talking about is Criteria 3.

CHAIRMAN STETKAR: I mean -- I'm asking, if I go to tech specs today, the standard tech specs, there are LCOs for everything that I mentioned.

MS. McKENNA: Yes.

CHAIRMAN STETKAR: There is none for ECWS, simply because the people who drafted the generic tech specs thought about currently operating plants that don't have an essential chilled water system. Otherwise, they would have put one in there. That's the fact of the matter.

And if you draw the analogy that I don't need one for essential chilled water, then I don't need one for essential service water. I don't need one for component cooling water. I don't need one for ac power. I don't need one for dc power. Because it all relies on the fact that I need support for this pump that pumps water.

And the tech specs are not organized that way in the generic tech specs. They do have LCOs that call out surveillance requirements and allowed outage times for all of those other support systems that I listed.

The only exception in this particular design is essential chilled water, because I believe that the people who crafted the tech specs weren't familiar with designs that happened to have essential chilled water systems, which is not a traditional U.S. plant design feature. It is more traditional for other plants.

MS. McKENNA: True. But I think the point to be made is that something like a room ventilation, you may or may not need it for the equipment to be operable, whereas you clearly have to have electric power, and you clearly -- you know, so that there are situations where you could have the essential chilled water system degraded, you know, less than full complement, and the equipment that it services is still operable.

CHAIRMAN STETKAR: You know, I think it's a stretch because in specific -- in the US-APWR technical specifications, the bases for the ultimate heat sink and the essential service water system specifically referenced the fact that those are cooling supplies for the chillers. You know, I just don't --

MEMBER SHACK: Without offending your consistency and logic, is there a safety problem associated with this?

CHAIRMAN STETKAR: I think there might be. I think there might be in an operational sense, because the technical specifications are what the operators use day to day to give themselves assurance that they understand the plant configuration and any decreased margins.

And although it is nice to say that they should look at this pump and fully understand all of the subtleties of all of the support systems for this pump that might affect its operability, they have to do that.

But without the reminder in the technical specifications that, for example, train A of essential chilled water goes out and affects this pump and many other pumps, and room ventilation for electrical things, it is really, really difficult for operators to make those connections. Or it can be.

Having been in a plant trying to make several of those subtle connections where the tech specs weren't all that clear, it is not very easy to do. And I think without it having, you know, its specific identification in the tech specs, you are asking for people to perhaps, you know, overlook something.

So it's not just a consistency issue, because, I grant you, ultimately I need to understand that every support system for this particular pump is available. And indeed, in principle, I should look at essential chilled water as part of that support.

But it just -- I just don't understand that inconsistency, given the fact that every other support system -- I could make the same argument if they didn't put the dc power system in there. Right? Philosophical argument.

MEMBER SHACK: Well, except that Eileen sort of has an exception that, you know, might -- you know, really, we go through every system and find out whether it does it. But I think I would agree with her that it seems to cover a lot of them.

CHAIRMAN STETKAR: It covers philosophically.

MEMBER SHACK: Yes.

CHAIRMAN STETKAR: Philosophically, it covers everything.

MEMBER SHACK: No. The distinction between support systems that are in and support systems that are out.

CHAIRMAN STETKAR: We can talk about this later. I personally feel that -- again, this is a Subcommittee meeting. I don't speak for the Committee. I feel pretty strongly about this one, especially having been an operator. And I -- anyway, we will just leave it that way. And thanks for your clarification.

MS. McKENNA: We understand your concern.

CHAIRMAN STETKAR: I appreciate that.

MS. McKENNA: Consistent with our current guidance and interpretation of 50.36, they would not be required to be in the specs.

MR. HAMZEHEE: Directly.

MS. McKENNA: Directly. Correct, yes. Indirectly, the LCOs.

MR. HAMZEHEE: I think, John, there are some operating plants that do have safety chilled water, but not many. So --

CHAIRMAN STETKAR: Yeah. I don't actually know that --

MR. HAMZEHEE: There are a few.

CHAIRMAN STETKAR: Okay. I didn't know all of -- I know most of them don't. I'm much more familiar with newer plant designs that tend to have it because they need extra cooling.

Do you happen -- no, that's okay. It's not relevant to the -- I wasn't going to ask you for the plants. I was going to ask you whether you happen to know whether their tech specs include the chilled water systems.

MR. HAMZEHEE: That I can't recall.

CHAIRMAN STETKAR: And it's actually not germane necessarily to the current -- you know, the current issue. So it would be interesting, but not directly relevant.

MR. WHEELER: Excuse me, John. I was an STA at Perry and they had safety-related chillers. I'll go back and look at their FSAR and tech specs and see --

CHAIRMAN STETKAR: Did you have a safety-related chilled -- you had a safety-related chilled water system with chillers.

MR. WHEELER: Correct.

CHAIRMAN STETKAR: Okay, good. Good.

MR. WHEELER: I will take a look at Perry's tech specs.

CHAIRMAN STETKAR: Because I'm familiar with overseas plants that I have worked on, and they are -- that had chilled water systems, and there are

-- but they're foreign countries, so they're not relevant to this discussion.

But I understand -- you know, I understand the philosophy. I understand the rationale. And, thanks, that helped clarify that issue. I didn't say I agreed with it; I just understand it now.

(Laughter.)

Okay. Any other things, Paul?

MR. KALLAN: No. I think staff has answered all of your questions. And we have one takeaway -- the SSC important to safety.

CHAIRMAN STETKAR: Yes.

MR. KALLAN: That's it.

CHAIRMAN STETKAR: And that's something that I -- just to put that in perspective kind, I raised it yesterday for two reasons. One reason is that just recently -- and I can't recall the context, because we see so many things, but -- and when I say "recently" I mean in the last two or three months or so, because that is about all the memory that I have.

There was a discussion in some interaction that we had --

MEMBER SHACK: It was in the risk metric stuff.

CHAIRMAN STETKAR: Was it the risk metric stuff?

MEMBER SHACK:It was the risk metric stuff.

CHAIRMAN STETKAR: Well, was it? I don't think it was in that. There was a discussion about the sense that there is a set -- and this was raised by the staff, that there is a set of equipment, structures that are important to safety, and that safety-related is a subset of that larger set. I think it -- it fits into the 50.69, but I don't know whether it came up under the 50.69. But it --

MEMBER SHACK: It came up because there is a number of those risk-informed things that --

CHAIRMAN STETKAR: But, I mean, that is more clear. This was in a different context.

MR. HAMZEHEE: John, yesterday you were correct. I am almost positive the important to safety is part of the reliability assurance program. And they have to define all of the -- either the safety-related, non-safety-related.

MEMBER SHACK: If you look in the GDCs, which pre-date the reliability assurance program by decades, important to safety is there. Now, what did it mean -- you know, what did they have in mind at that time?

MR. HAMZEHEE: Right.

MEMBER SHACK: It is certainly different than the D-RAP.

MR. HAMZEHEE: Right, correct. And there was some loose definition and very -- not very well disciplined use of the terminology, because you have risk significant, safety significant, important to safety, has nothing to do with safety-related. Safety-related is --

MEMBER SHACK: That's true. That's well defined.

MR. HAMZEHEE: Yes. And I think John -- that's why he was trying to figure out --

CHAIRMAN STETKAR: A couple of things, and finish the -- one reason I raised it is that I was recalling -- and I don't remember the context -- an issue raised by the staff about the fact that there is important to safety, and that safety-related is a subset of that. So understanding what important to safety is has some relevance to issues raised by the staff.

Furthermore, in this particular -- the quote that I cited, there was an even further distinction because there was important to safety versus safe shutdown, which is even a further refinement of the notion of safety-related, because traditionally safe shutdown, for example, in fire analysis or flooding or those types of things is a -- or seismic is a specifically defined set of equipment that you rely on to achieve and maintain safe shutdown. So it is even more finely defined than even safety-related.

So you are now comparing some definition of important to safety versus protection of safe shutdown. And this was in the context of the heavy load drops.

And I agree, I think that -- I think at least for the new plants, in my mind, the better guidance for determining, in an active plant design -- if you want to call it that -- like US-APWR, the complement of equipment that is in the design reliability assurance program, there is at least guidance and some measure of consistency about determining what is in that set of equipment.

And I think it is reasonable to say that those determinations are consistent with the notion of important to safety, and that for the passive plants the analogy would be the RTNSS list.

So I think that in the new plant design

we are at least getting a bit of definition included, you know, around that box of what is important to safety. And that's good. The bad thing is that if, indeed, there are -- in this -- the genesis of this question, if there are indeed SSCs out in the turbine building that are -- that fit within that box, should they then be protected against heavy load drops? Which brings into question, you know, the turbine building crane and all that kind of thing.

MR. HAMZEHEE: I think we need to go back and make sure what we meant by important to safety. Are we talking about safety-related equipment or --

CHAIRMAN STETKAR: In the context of your SER.

MR. HAMZEHEE: Exactly.

CHAIRMAN STETKAR: Right, right.

MR. HAMZEHEE: So that is really the clarification the staff needs to do.

CHAIRMAN STETKAR: Right, right. Because I excerpted the words from your SER, because you were comparing important to safety versus safe shutdown.

Okay. So that's what we will -- to be discussed.

Do any of the members have any more questions? We usually go around the table.

MEMBER SHACK: It's a little short today.

CHAIRMAN STETKAR: It's a short table, but I'll do that. Charlie?

MEMBER BROWN: No, I'm done.

CHAIRMAN STETKAR: Bill?

MEMBER SHACK: No.

CHAIRMAN STETKAR: Okay. Are there any members of the public here who have any comments?

(No response.)

Didn't expect any. I don't think we have a bridge line, so I don't need to ask for that.

Again, I appreciate everybody's participation. Thank the staff for coming up with answers. And I appreciate everybody coming back today. I know it is a burden on some, but I think that it was useful to get resolution on a large number of these items.

Thank you, all, and with that we are adjourned.

(Whereupon, at 10:31 a.m., the proceedings in the foregoing matter were adjourned.)

Presentation to ACRS Subcommittee

Chapter 9: Auxiliary Systems

Section 9.1 Fuel Storage and Handling

March 22-23, 2012

Mitsubishi Heavy Industries, Ltd.

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Acronyms

ASME	:American Society of Mechanical Engineers
CMAA	:Crane Manufacturers Association of America
CVCS	:Chemical and Volume Control System
C/V	:Containment Vessel
EFWP	:Emergency Feedwater Pit
EPS	:Emergency Power Source
ESF	:Engineered Safety Feature
Hx	:Heat Exchanger
LLHS	:Light Load Handling System
MOV	:Motor-Operated Valve
OHLHS	: Overhead Heavy Load Handling System
PCS	:Permanent Cavity Seal
RAI	:Request for Additional Information
RHRS	:Residual Heat Removal System
RV	:Reactor Vessel
RWSAT	:Refueling Water Storage Auxiliary Tank
RWSP	:Refueling Water Storage Pit
R/B	:Reactor Building
SFP	:Spent Fuel Pit
SFPCS	:Spent Fuel Pit Cooling and Purification System
SSE	:Safe-Shutdown Earthquake

DCD Section 9.1 Fuel Storage and Handling

Section		Major Contents
9.1	Fuel Storage and Handling	9.1.1 Criticality Safety of New and Spent Fuel Storage
		9.1.2 New and Spent Fuel Storage
		9.1.3 Spent Fuel Pit Cooling and Purification System
		9.1.4 Light Load Handling System (Related to Refueling)
		9.1.5 Overhead Heavy Load Handling System

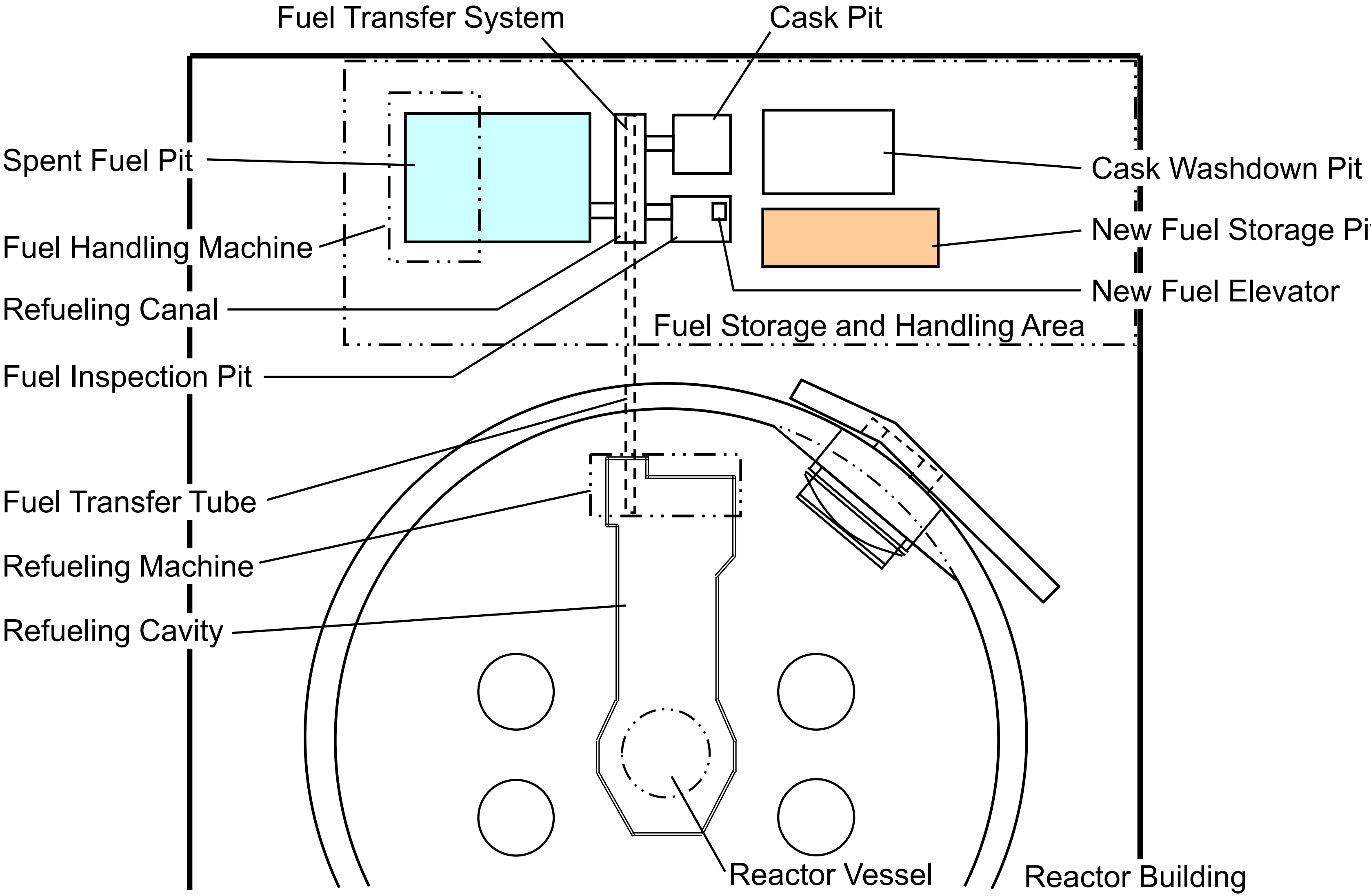
9.1.1 Criticality Safety of New and Spent Fuel Storage

- New and spent fuel storage facilities are located in the fuel handling area of the reactor building (R/B) which is designed to meet the seismic category I requirements of Regulatory Guide (RG) 1.29.

- New fuel is stored in low density racks installed in a dry new fuel storage pit.

- Spent fuel is stored in moderate density racks installed in a spent fuel pit (SFP) filled with borated water.

9.1.1 Criticality Safety of New and Spent Fuel Storage



Plan View of Light Load Handling System

- The robust concrete walls and ceiling surrounding the fuel storage and handling area is designed to withstand the loads and forces caused by earthquake, wind, tornadoes, floods, and internal and external missiles.
- New and spent fuel storage racks are designed to maintain the required degree of subcriticality, and are evaluated as seismic category I structures.
- Equipment potentially damaging the stored fuel is designed to be prevented from collapsing and falling down on the structures in the event of a safe-shutdown earthquake (SSE).

9.1.1 Criticality Safety of New and Spent Fuel Storage

- **Criticality is precluded by adequate design of fuel handing and storage facilities and by administrative control procedures. Criticality analyses are performed in accordance with the following acceptance criteria and relevant requirements.**
- **New Fuel Storage Rack**
  - ✓ 10 CFR 50.68 (b) item (2) and (3)

    K_{eff}* ≦ 0.95 for the flooded condition with unborated water

    K_{eff}* ≦ 0.98 for optimum moderation
- **Spent Fuel Storage Rack**
  - ✓ 10 CFR 50.68 (b) item (4)

    K_{eff}* ≦ 0.95 for the flooded condition with partial credit for soluble boron

    K_{eff}* < 1.0 with full density unborated water

* Maximum Keff value including all biases and uncertainties at a 95% probability and 95% confidence

➢ Analysis Conditions (1/2)

- ✓ Under the new fuel assumption, the fuel assembly is assumed to have a maximum enrichment of 5 wt% pursuant to 10 CFR 50.68 (b) item (7).
- ✓ Fuel assembly fabrication tolerances are considered.
- ✓ Credit is taken for the neutron absorption in the rack structural material and neutron poison, such as boron.
- ✓ The steel plate thickness and boron content are conservatively assumed to be minimum specification values.

US-APWR

➢ Analysis Conditions (2/2)

✓ New fuel storage rack

- The new fuel storage rack cell is constructed of stainless steel.
- A finite rack cell array and the surrounding concrete reflectors are used in the calculations.

✓ Spent fuel storage rack

- The spent fuel storage rack cell is constructed of stainless steel with boron.
- Metamic is selected as neutron absorber material.
- An infinite rack array in the lateral direction is assumed.

✓ Material composition, fabrication tolerances of the fuel and rack, and the fuel location within the rack cell uncertainties are considered.

➢ **No open or confirmatory items remain on this subsection.**

9.1.2 New and Spent Fuel Storage

US-APWR

- Structural Requirement -

- Structural design and stress analysis of the new and spent fuel storage racks are evaluated in accordance with the seismic category I requirements of Regulatory Guide 1.29.

- Loads and load combinations considered in the structural design and stress analysis are based on SRP Section 3.8.4, Appendix D.

- Racks can withstand a maximum uplift force based on the lifting capacity of the suspension hoist and the fuel handling machine.

- A subcritical array can be maintained in the event of a postulated drop of a fuel assembly and associated handling tool on a rack.

9.1.2 New and Spent Fuel Storage

➢ Major RAIs (Confirmatory Items)

RAI No.	Question 09.01.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
387-2931	22	**Preoperational test of the SFP:** Include in the DCD evaluation of the leak-tightness of the spent fuel pool liner as one of the objectives of preoperational test.	➢ MHI revised the DCD Chapter 14, Subsection 14.2.12.1.85 to add the test for leak-tightness of the SFP in objective, test method, and acceptance criteria of the preoperational test for the spent fuel pit cooling and purification system.

9.1.2 New and Spent Fuel Storage

➢ Major RAIs (Confirmatory Items)

RAI No.	Question 09.01.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
387-2931	23	**Blockage of the SFP leakage collection system:** Justify how the SFP leakage collection system meets the requirements of 10 CFR 20.1406 if the system is not periodically inspected to identify blockages. Clarify in the DCD that the SFP leakage collection system is sized to allow cleaning of blockages.	➢ MHI revised the DCD to clearly state that: • The inside of the SFP leakage collection pipes are inspected using a device such as fiberscope, and cleaned if necessary, approximately every refueling outage. • The SFP leakage collection pipes are sized to allow cleaning of blockages as specified in Regulatory Guide 4.21.

9.1.2 New and Spent Fuel Storage

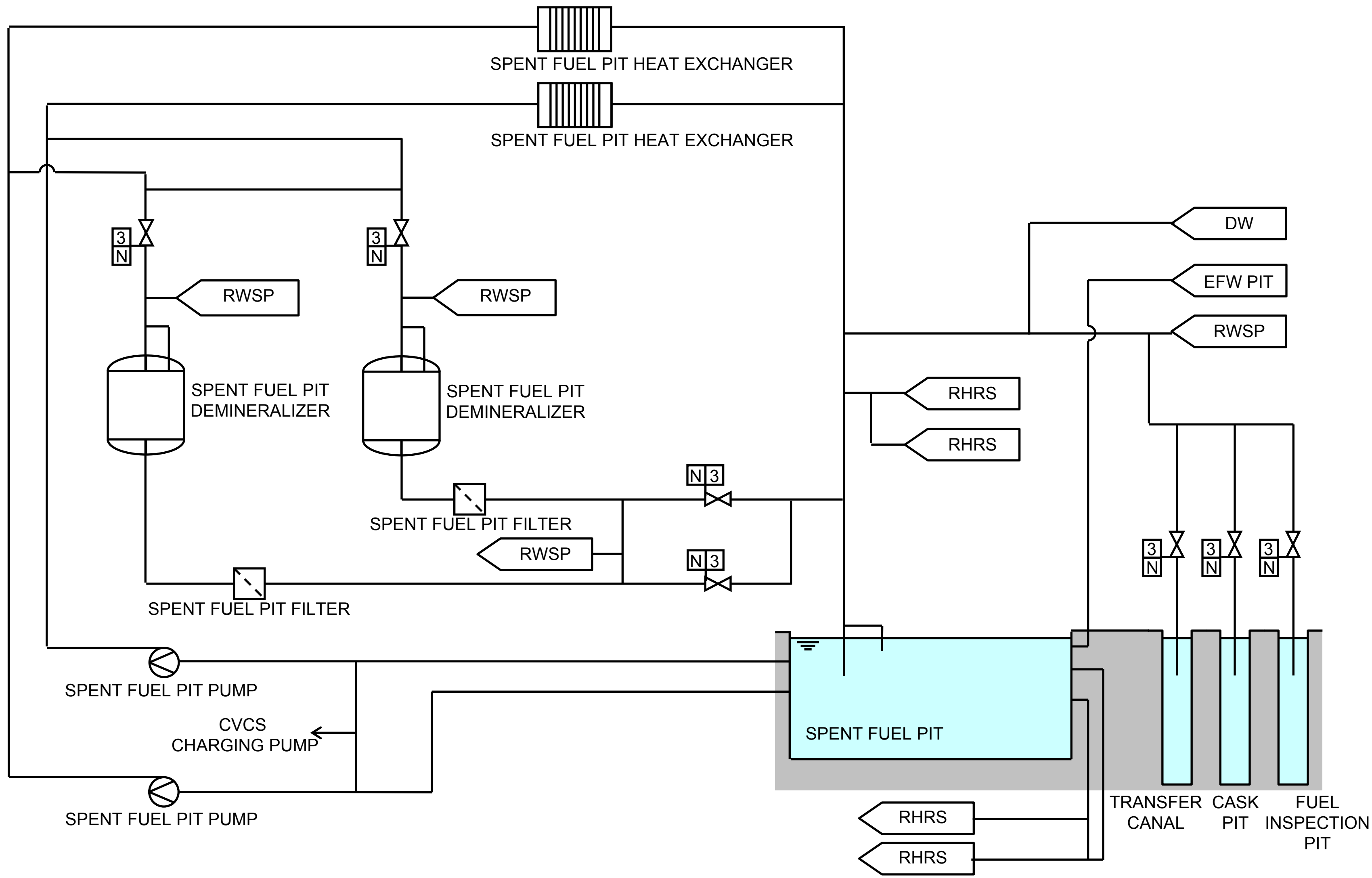
➢ Major RAIs (Issued/Open Action Applicant)

RAI No.	Question 09.01.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
906-6332	26	**Containment Racks:** Description and evaluation of fuel racks in the refueling cavity are missing throughout the DCD. Applicant should address SRP 9.1.2 and interfacing SRP sections. For example; •Structural design of the racks •Compatibility and chemical stability of the materials of the racks	[Preparation under way]

9.1.3 Spent Fuel Pit Cooling and Purification System (SFPCS)

- **The SFPCS is comprised of:**
  - ✓ **Two redundant cooling and purification trains.**
  - ✓ **Each train includes one pump, one heat exchanger (plate-type), one filter, and one demineralizer.**
  - ✓ **EPS can be aligned with SFP pumps as necessary.**
- **The SFPCS cools the SFP water by removing the decay heat generated by spent fuel assemblies in the SFP.**
- **The SFPCS purifies the borated water in SFP, RWSP, and RWSAT.**
- **The system piping is arranged such that the failure of any line cannot drain the SFP to a level less than 11.1 ft above the top of a stored assembly.**
- **The SFPCS is provided with Seismic Category I makeup water from the RWSP and the EFWP.**
- **The SFPCS trains, in conjunction with two trains of RHRS, maintain SFP temperature below 120°F during full core offload.**

9.1.3 Spent Fuel Pit Cooling and Purification System (SFPCS)



➢ Major RAI (Open Items)

RAI No.	Question 09.01.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
735-5723	7	**How presumed failures of non-safety-related portions of the SFPCS due to a seismic event or an internally generated missile event do not adversely affect the safety-related portion of the SFPCS.**	➢ The local manual isolation valve between the safety and non-safety portion (VLV-101A/B) of each train will be changed to double, automatic isolation MOVs which close on a low-low SFP water level signal. ➢ Each SFP pump also will be tripped on the low-low SFP water level signal.

9.1.4 Light Load Handling System (Related to Refueling)

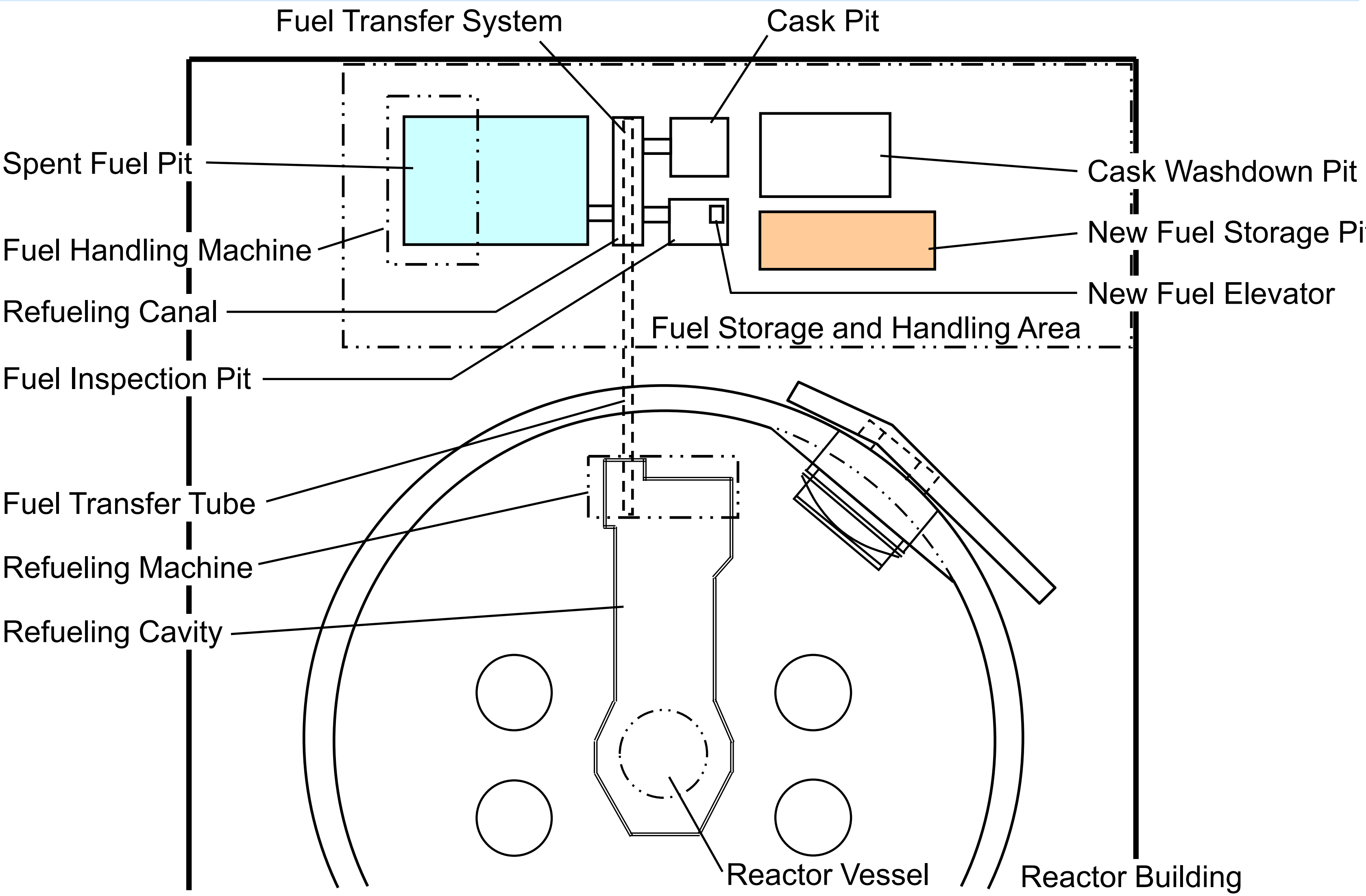
- **The Light Load Handling System (LLHS) consists of the equipment and structures involved in the handling of new, irradiated, and spent fuel.**

- **All of the LLHS is non-safety related, except**
  - Fuel transfer tube and blind flange
    → serves as part of the containment
  - Permanent cavity seal
    → retains water of refueling cavity during refueling to keep fuels in transit submerged

- **The LLHS is designed to meet the criteria specified in**
  - ✓ **ANSI/ANS57.1-1992, "Design Requirements For Light Water Reactor Fuel Handling Systems"**

- **Subcriticality is maintained by design with the equipment fully loaded with fuel and the pool flooded with unborated water.**

9.1.4 Light Load Handling System (Related to Refueling)



Plan View of Light Load Handling System

9.1.4 Light Load Handling System (Related to Refueling)

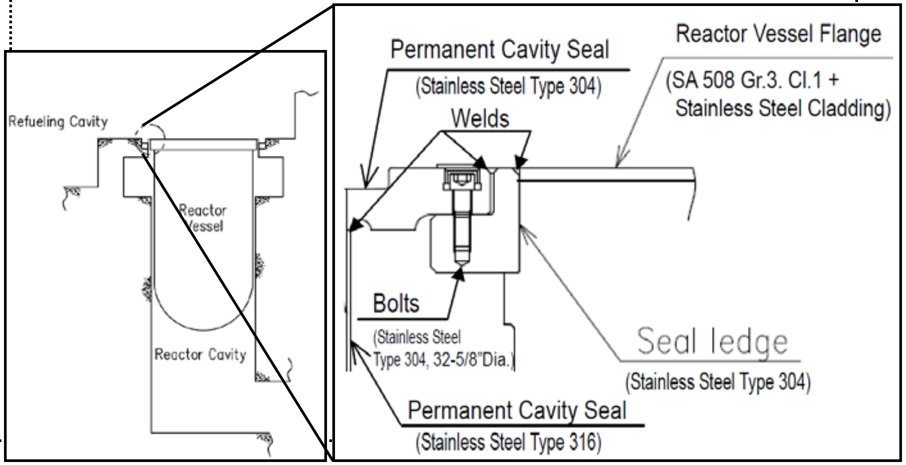
➢ Major RAIs (Confirmatory Items)

RAI No.	Question 09.01.04-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
555-4385	19	**Correction of wording:** Replace the word, "Decontamination pit“, with "Cask washdown pit“ in accordance with the name change stated in the Question 09.01.04-11.	➢ MHI will modify the inconsistent wordings used to stand for the cask washdown pit. (This is not technical issue.)

9.1.4 Light Load Handling System (Related to Refueling)

➢ Major RAIs (Open Items)

RAI No.	Question 09.01.04-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
887-6261	23	**Permanent Cavity Seal (PCS):** Will fabrication and installation of the PCS adversely affect the reactor vessel (RV)? - Provide details about; · Material · Connection between the PCS and the RV - Why ASME Section III, Class 3 will not be applied.	➢ The PCS is • made out of stainless steel (specific types of steel are provided in the response) • indirectly attached to the RV through the seal ledge with bolts and welds ➢ ASME Section III is not applicable, because the PCS is: • not a pressure-retaining component • outside jurisdictional boundary of the RV



9.1.5 Overhead Heavy Load Handling System

- The Overhead Heavy Load Handling System (OHLHS) consists of devices used for critical load handling evolutions.
- The OHLHS cranes are designed to meet the criteria specified in
  - ✓ CMAA-70, 2000, “Specifications for Top Running Bridge and Gantry Type Multiple Girder Electric Overhead Traveling Cranes”
  - ✓ ASME B30.2, 2005, “Overhead and Gantry Cranes”
- The Polar Crane and the Main Hoist on the Spent Fuel Cask Handling Crane are designed as non-safety related, seismic category II, single-failure-proof cranes, in accordance with NUREG-0554.
- Travel range of the spent fuel cask handling machine is limited to prevent load drop on the new and spent fuel storage pit by physical stops on the travel rails of the machine and the hoist carriage. (See Figure 9.1.5-1 in DCD)

9.1.5 Overhead Heavy Load Handling System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question 09.01.05-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
616-4865	19	**Auxiliary Hoist on the Polar Crane:** Administrative procedure to disallow carrying critical loads is the only measure credited to prevent unacceptable load drop accident, which does not conform to SRP 9.1.5.	➢ MHI revised the DCD to upgrade the Auxiliary Hoist on the Polar Crane to single failure-proof and committed to design the hoist in accordance with the requirement of ASME NOG-1 and NUREG-0554.

9.1.5 Overhead Heavy Load Handling System

➢ Major RAIs (Open Items)

RAI No.	Question 09.01.05-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
616-4865	18	**Equipment Hatch Hoist:** Justify how the SRP 9.1.5.III.4 guidance would be met for the Equipment Hatch Hoist, which is not single failure proof crane located over safe shut down equipment (SSE).	➢ MHI will delete the description about the Equipment Hatch Hoist from Subsection 9.1.5, because the hoist is dedicated to raising and lowering the equipment hatch, and therefore does not fit into the category of OHLHS, which is used for critical load handling evolutions.

Presentation to ACRS Subcommittee

Chapter 9: Auxiliary Systems

Section 9.2 Water Systems

March 22-23, 2012

Mitsubishi Heavy Industries, Ltd.

MHI Presenters

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Acronyms (1/2)

A/B	:Auxiliary Building
CDI	:Conceptual Design Information
CHP	:Charging Pump
CSF	:Condensate Storage Facilities
CCWS	:Component Cooling Water System
C/V	:Containment Vessel
CWS	:Circulating Water System
ECWS	:Essential Chilled Water System
ESW	:Essential Service Water
ESWS	:Essential Service Water System
Hx	:Heat Exchanger
HVAC	:Heating, Ventilation, and Air Conditioning
ITAAC	:Inspection, Test, Analysis, and Acceptance Criteria
LOCA	:Loss of Coolant Accident
LOOP	:Loss of Offsite Power
MCR	:Main Control Room
non-ECWS	:Non-Essential Chilled Water System
non-ESW	:Non-Essential Service Water
PSWS	:Potable and Sanitary Water System
R/B	:Reactor Building
RAI	:Request for Additional Information

Acronyms (2/2)

RWSP	:Refueling Water Storage Pit
SSCs	:Structures, Systems and Components
SSE	:Safe-Shutdown Earthquake
T/B	:Turbine Building
TCS	:Turbine Component Cooling Water System
UHS	:Ultimate Heat Sink

DCD Section 9.2 Water Systems

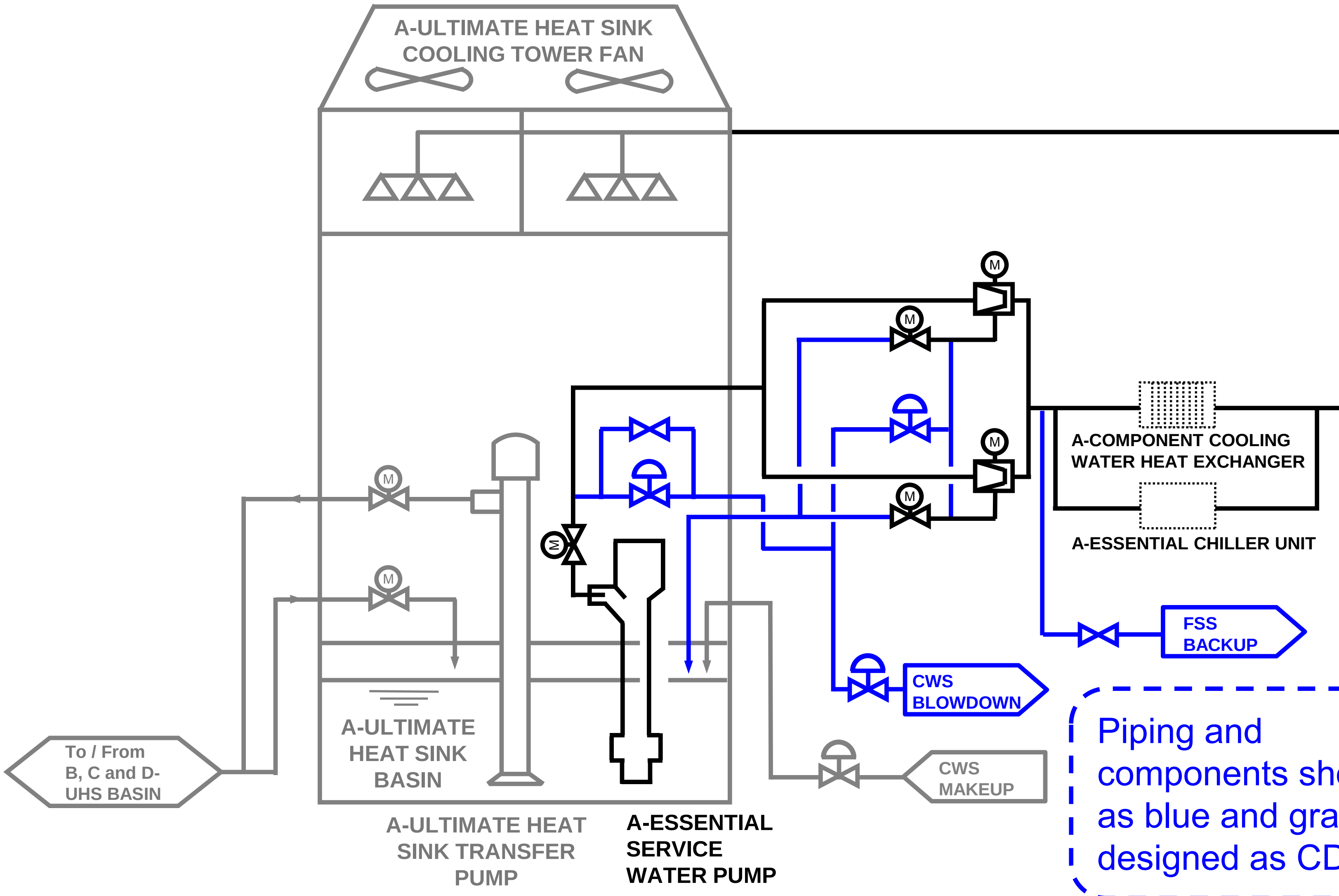
Section		Major Contents	Safety-Related Function
9.2	Water Systems	9.2.1 Essential Service Water System	Yes
		9.2.2 Component Cooling Water System	Yes
		9.2.4 Potable and Sanitary Water Systems	No
		9.2.5 Ultimate Heat Sink	Yes
		9.2.6 Condensate Storage Facilities (Demineralized Water, Condensate Storage, and Primary Makeup Water)	No
		9.2.7 Chilled Water System	Yes
		9.2.8 Turbine Component Cooling Water System	No
		9.2.9 Non-Essential Service Water System	No

9.2.1 Essential Service Water System (ESWS)

- The ESWS is a safety-related system, capable of transferring heat loads from safety-related SSCs to the UHS during normal operating and accident conditions.
- The ESWS, in conjunction with the plant UHS, is designed to remove heat from the plant auxiliaries required to mitigate the consequences of a design basis event and for safe shutdown, assuming a single failure and one train unavailable due to maintenance coincident with a LOOP.
- The ESWP is interlocked with CCW pump operation to support uninterrupted heat removal.

- The ESWS is consists of:
  - ✓ Four 50%-capacity ESW pumps into four independent trains.
  - ✓ Two 100%-capacity parallel strainers in each ESW pump discharge line.
  - ✓ Backup to FSS (CDI item)

9.2.1 Essential Service Water System (ESWS)



Piping and components shown as blue and gray are designed as CDI.

9.2.1 Essential Service Water System (ESWS)

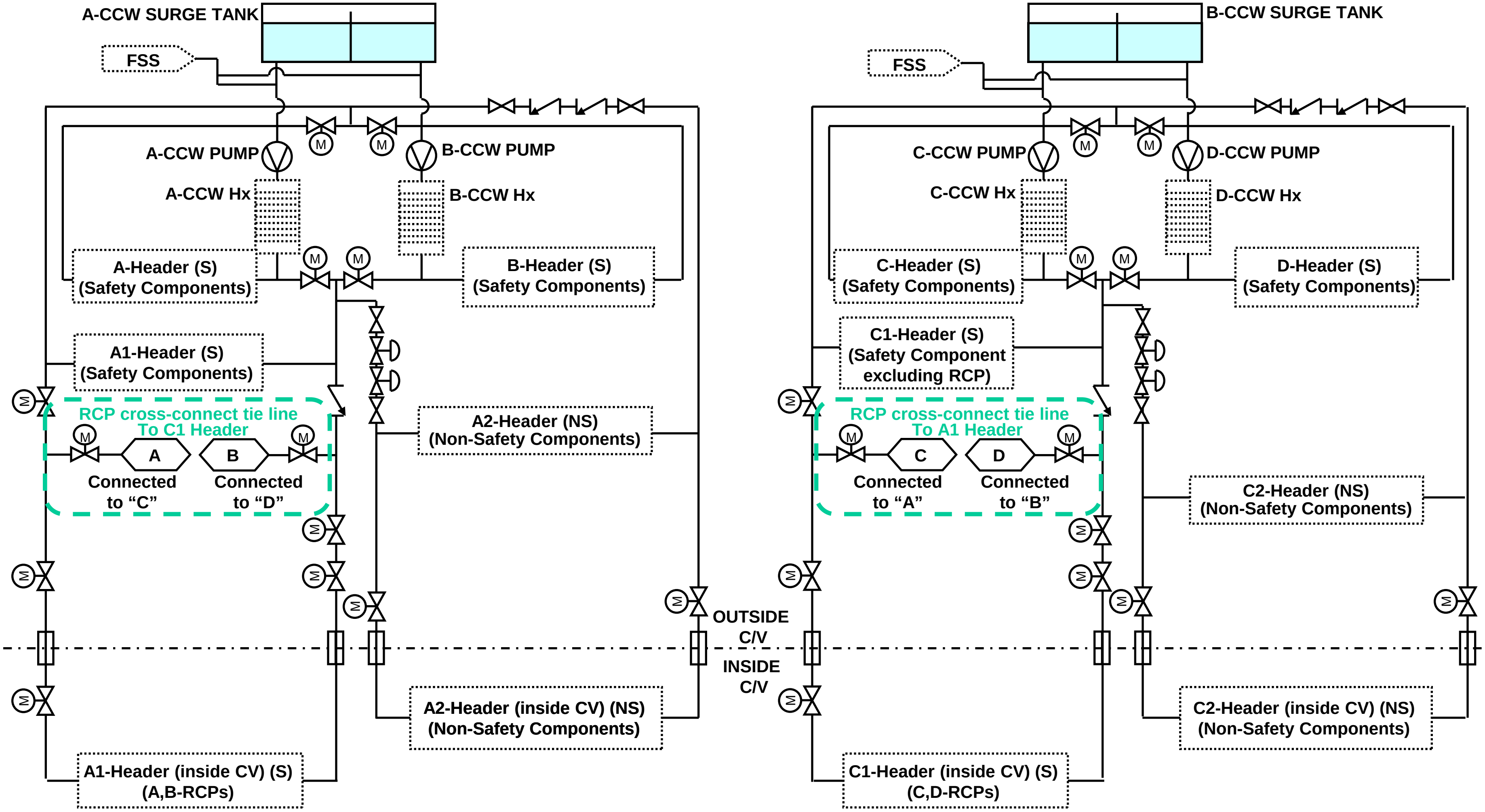
➢ SER Open and Confirmatory Items

RAI No.	Question 09.02.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
xxx-6344	-	Power supply to the boundary valve AOV-577 ➢ FMEA maybe needed for AOV-577 and VLV-544A/B/C/D ➢ All boundary valves should be listed in FMEA	➢ Draft RAI is currently under discussion.
-	-	Markup information in the Oct.14, 2011 letter	➢ All of the relevant RAI responses

9.2.2 Component Cooling Water System (CCWS)

- The CCWS is the closed, intermediate system between components cooled by CCW HX cooled by ESWS.
- The CCWS performs safety function of providing cooling water to components required for accident mitigation.
- Non-essential loads (non seismic/non safety) are isolated by automatic AOVs.
- The CCWS uses either offsite power supply or onsite Class 1E power supply.
- The CCWS has RCP cross-connect tie line between subsystems.
- Non-essential chilled water of fire protection water supply to CHP is available.
- The essential portion of CCWS is designed to Seismic Category I requirements to remain functional during and following an SSE.
- The CCWS is designed to withstand leakage in one train without loss of the system’s safety function.
- The ESWP is interlocked with CCW pump operation to support uninterrupted heat removal.
- The CCWS is consists of:
  - ✓ Two independent 100% cooling capacity subsystems.
  - ✓ Each subsystem is served by one CCW surge tank.
  - ✓ Each subsystem consists of two 50% capacity trains.
  - ✓ Each train contains one CCW pump and one CCW HX.

9.2.2 Component Cooling Water System (CCWS)



9.2.2 Component Cooling Water System (CCWS)

➤ SER Open and Confirmatory items

RAI No.	Question 09.02.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
878-6200	85	Design against postulated piping leakage in safety-related portion of CCWS	The safety-related portions of the CCWS meet the requirements of the BTP 3-4 B(iii)(1)(c) and therefore are exempted from postulating leakage cracks.
-	-	Markup information in the Oct.14, 2011 letter	All of the relevant RAI responses

9.2.4 Potable and Sanitary Water Systems (PSWS)

Potable and Sanitary Water Systems is designed as CDI with the following requirements

- **PSWS is Non-Safety Related**
- **PSWS is protected against radioactive contamination through distribution piping by installing a backflow prevention device**
- **PSWS has no interconnection to any systems having the potential for contaminating radioactive material**

9.2.4 Potable and Sanitary Water Systems (PSWS)

➢ **SER Open and Confirmatory items**

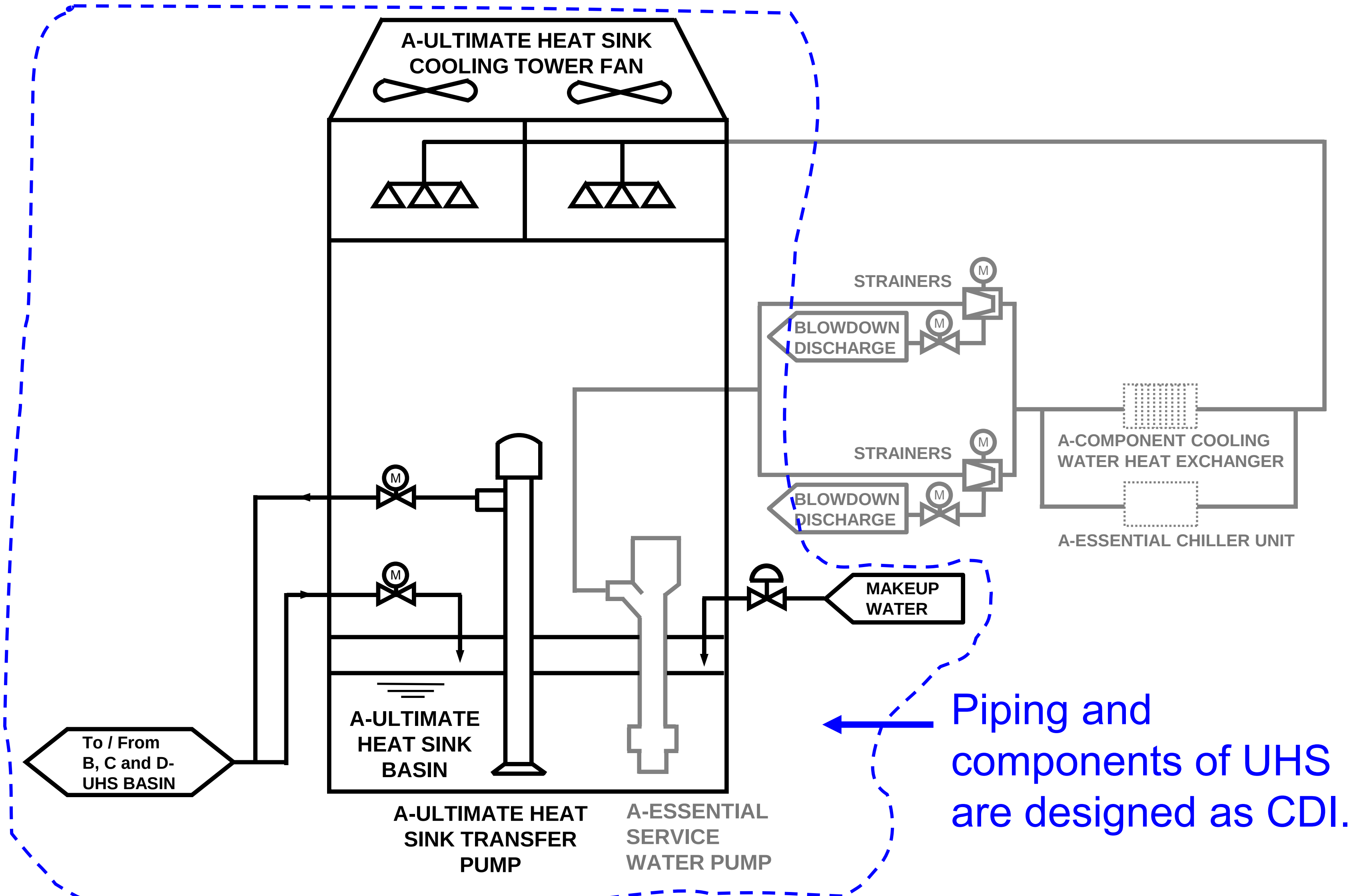
RAI No.	Question 09.02.04-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.2.5 Ultimate Heat Sink (UHS)

Ultimate Heat Sink is designed as CDI with the following requirement

- **The UHS dissipates the maximum heat loads from the ESWS under normal and accident conditions, including that of the LOCA or safe shutdown scenario with LOOP under the worst combination of adverse environmental conditions, including freezing.**
- **The UHS cools the unit for a minimum of 30 days (or minimum of 36 days for cooling pond) without makeup water regarding RG 1.27.**
- **The UHS Related Structures are Seismic Category I structures.**
- **The UHS withstands the effect of natural phenomena such as earthquakes, tornadoes, hurricanes, floods, tsunami and seiches without loss of capability to perform its safety functions.**

9.2.5 Ultimate Heat Sink (UHS)



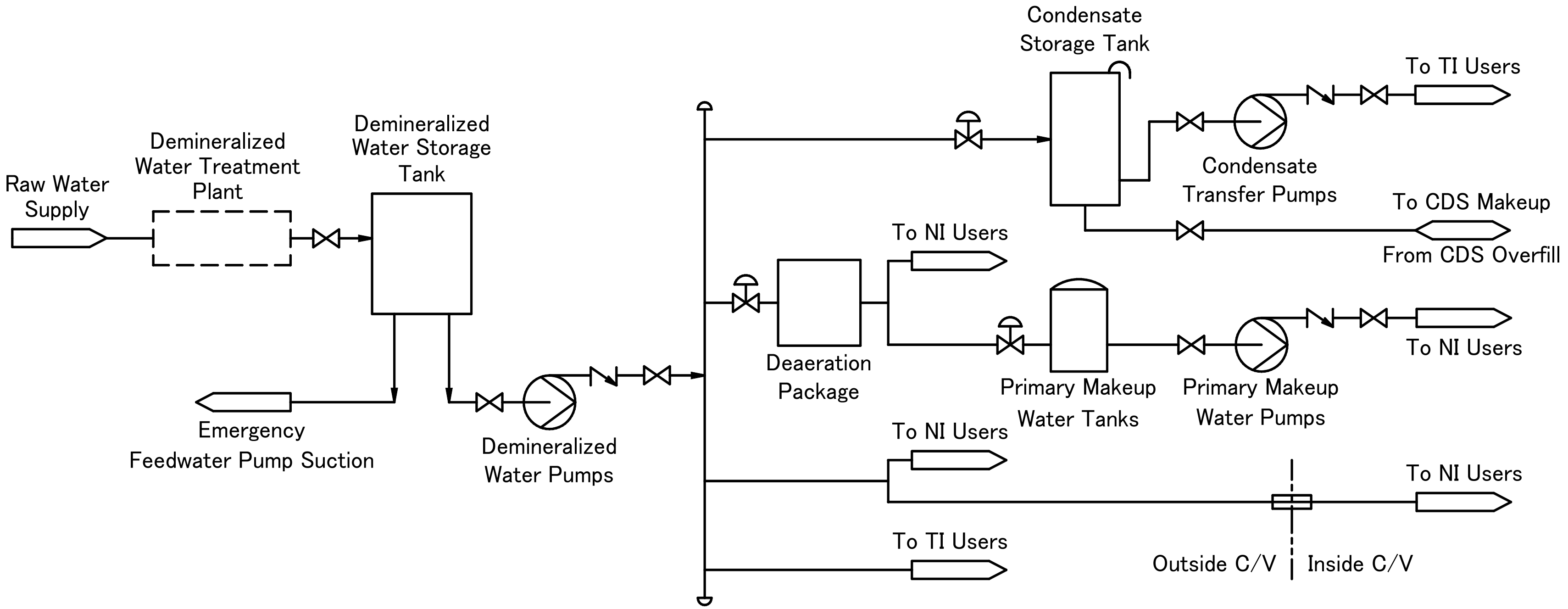
9.2.5 Ultimate Heat Sink (UHS)

- SER Open and Confirmatory items

RAI No.	Question 09.02.05-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.2.6 Condensate Storage Facilities (CSF)

- The CSF is a non safety-related system.
- The CSF provides treated water to primary and secondary systems.
- The CSF consists primarily of three systems:
  - Demineralized water system
  - Condensate storage and transfer system
  - Primary makeup water system



9.2.6 Condensate Storage Facilities (CSF)

US-APWR

➢ SER Open and Confirmatory Items

RAI No.	Question 09.02.06-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
863-6148	3	To explain the mitigation of the environmental effects that do not have impact on safety-related SSCs, even when CST and its dike fail.	➢ Entrance of the buildings are located 1 foot above ground level. ➢ CST, its dike and pumps are located away from the safety-related SSCs. ➢ Graded slope and drainage system should be provided as site-specific plant design. ➢ Therefore, failure of the tank and dike does not impact safety-related SSCs. ➢ DCD will be revised accordingly.

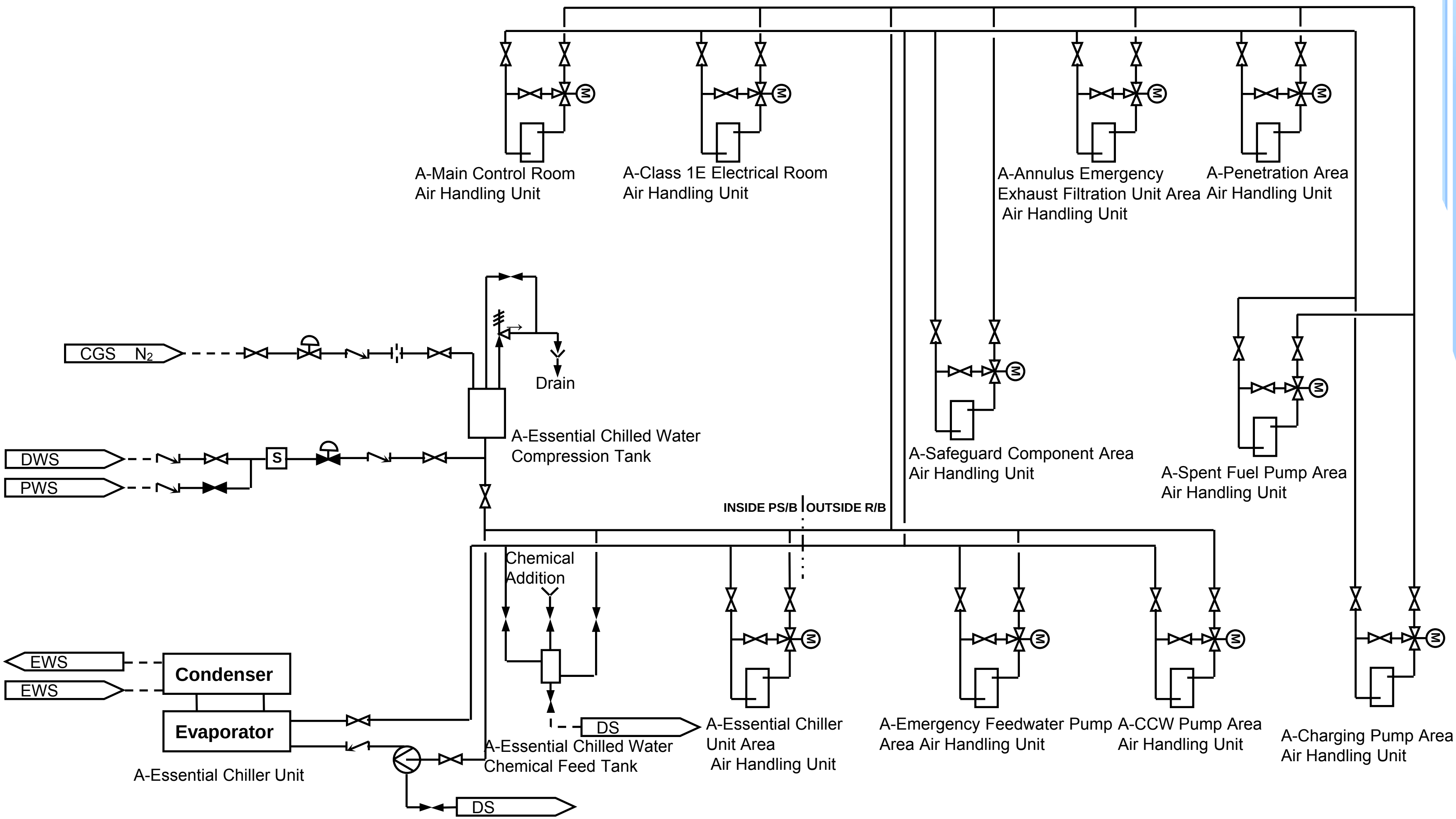
9.2.7 Chilled Water System

- **The chilled water system includes the Essential Chilled Water System (ECWS) and Non-Essential Chilled Water System (Non-ECWS).**
- **The ECWS is safety-related system and performs the following functions:**
  - ✓ **Provides, during normal and emergency operation, chilled water for the plant safety related air-cooling and ventilation systems.**
    - **- MCR HVAC System**
    - **- Class 1E electrical room HVAC system**
    - **- Safeguard component area HVAC system**
    - **- Emergency feedwater pump area HVAC system**
    - **- Safety related component area HVAC system**
- **The ECWS is consists of:**
  - ✓ **Four independent 50%-capacity chiller units into four independent trains.**
  - ✓ **Four independent 50%-capacity chilled water pumps into four independent trains.**
  - ✓ **Four independent 50%-capacity compression tanks into four independent trains.**

9.2.7 Chilled Water System

US-APWR

Essential Chilled Water System

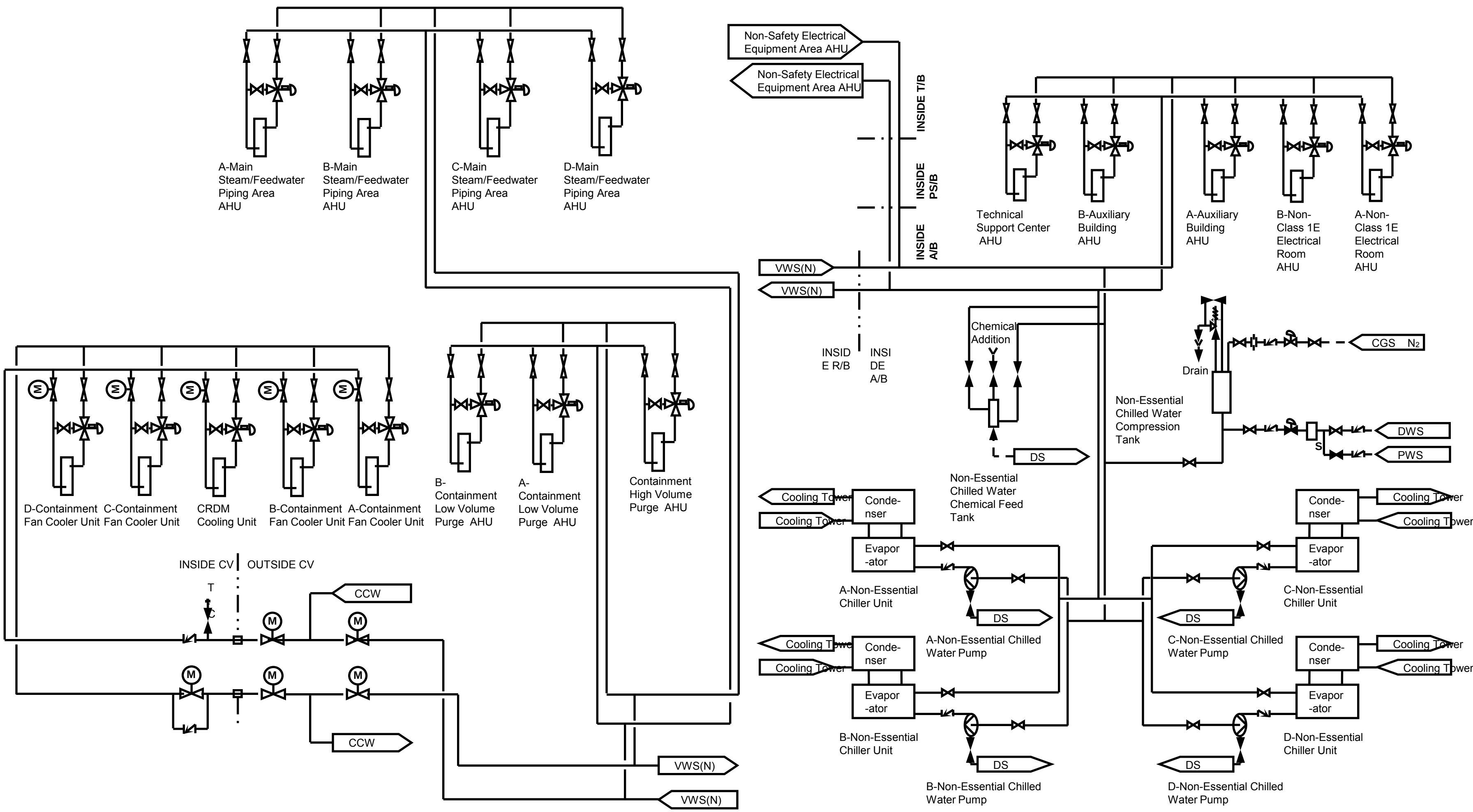


9.2.7 Chilled Water System

- The Non-ECWS is non-safety related system with the exception of piping and valves between and including containment isolation valves.
- The Non-ECWS performs the following function:
  - ✓ Provide chilled water for the HVAC systems serving the non-safety related areas during plant normal operation and LOOP.
  - ✓ Connect to the CCWS to provide alternate component cooling water to the charging pumps and to provide alternate cooling water to the containment fan cooler units from CCWS.

9.2.7 Chilled Water System

Non-Essential Chilled Water System



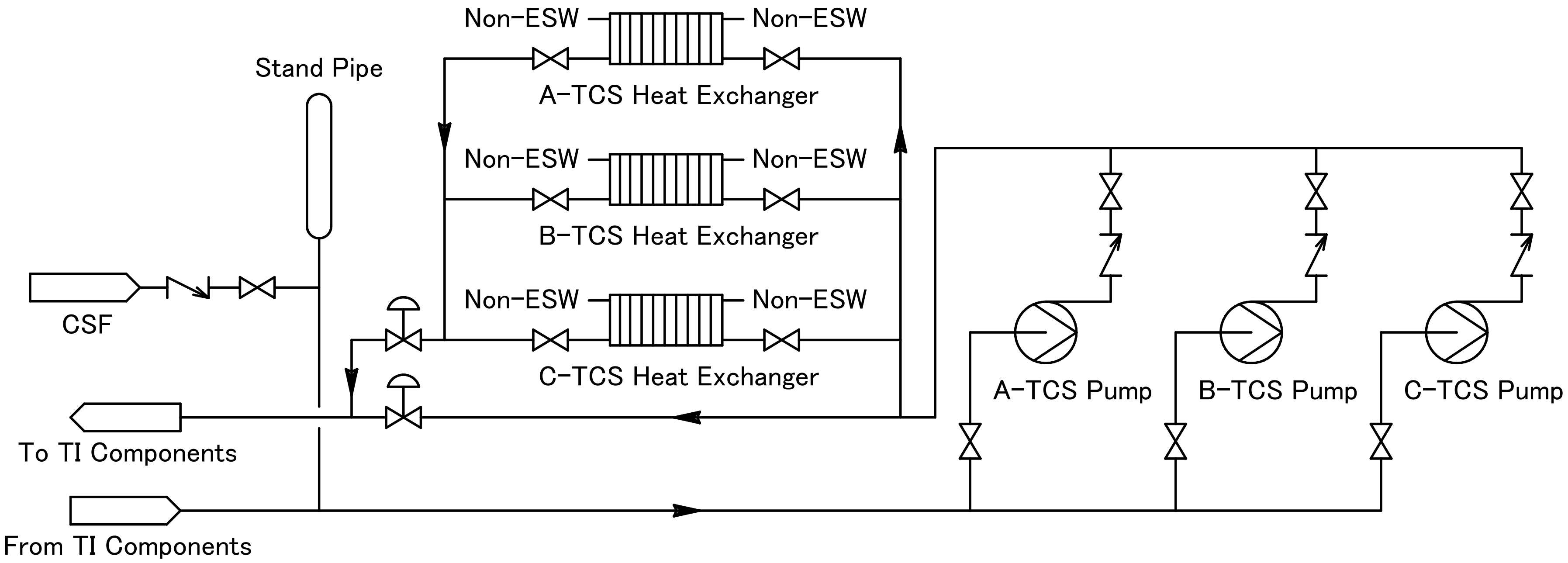
9.2.7 Chilled Water System

➢ SER Open and Confirmatory Items

RAI No.	Question 09.02.XX-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		There are no open and confirmatory items for 9.2.7.	

9.2.8 Turbine Component Cooling Water Systems (TCS)

- The TCS is a non safety-related system.
- The TCS provides demineralized cooling water for removal of heat from various T/B heat loads and rejection of heat to the non-essential service water system.



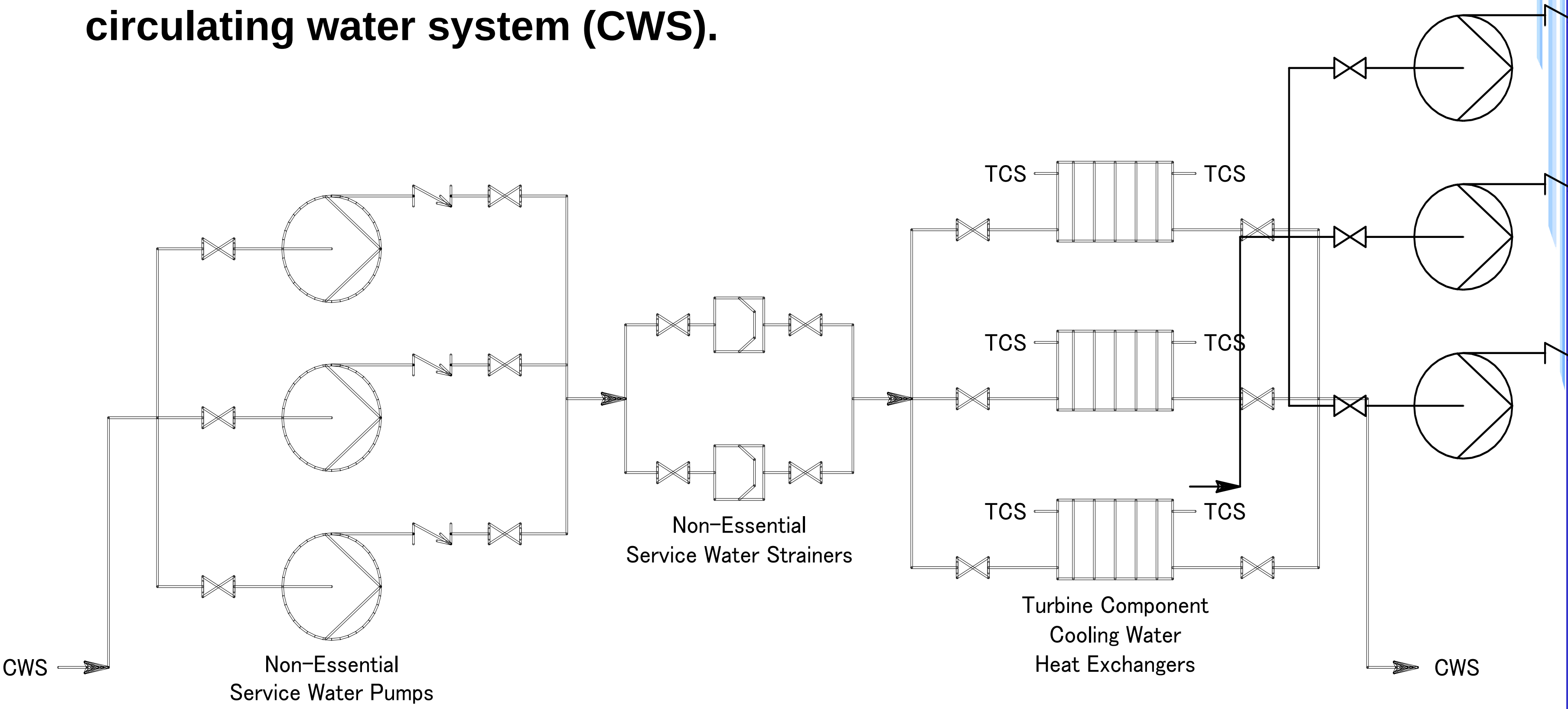
9.2.8 Turbine Component Cooling Water Systems (TCS)

➢ SER Open and Confirmatory items

RAI No.	Question 09.02.XX-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.2.9 Non-Essential Service Water System (non-ESW)

- The non-ESW is a non safety-related system.
- The non-ESW provides cooling water to remove heat from the TCS via the TCS heat exchanger and discharged to the heat sink via circulating water system (CWS).



9.2.9 Non-Essential Service Water System (non-ESW)

➢ SER Open and Confirmatory items

RAI No.	Question 09.02.XX-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

Presentation to ACRS Subcommittee

Chapter 9: Auxiliary Systems

Section 9.3 Process Auxiliaries

March 22-23, 2012

Mitsubishi Heavy Industries, Ltd.

MHI Presenters

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Acronyms (1/2)

AOV	: Air Operated Valve
A/B	: Auxiliary Building
BA	: Boric Acid
CAS	: Compressed Air System
CAGS	: Compressed Air and Gas Systems
CGS	: Compressed Gas System
CVCS	: Chemical and Volume Control System
C/V	: Containment Vessel
ECCS	: Emergency Core Cooling System
EFDS	: Equipment and Floor Drain Systems
ESF	: Engineered Safety Features
GWMS	: Gaseous Waste Management System
HUT	: Holdup Tank
HVAC	: Heating, Ventilation, and Air Conditioning
HEPA	: High-Efficiency Particulate Air
IAS	: Instrument Air System

Acronyms (2/2)

LWMS	: Liquid Waste Management System
PASS	: Post-Accident Sampling System
PGSS	: Primary Gaseous Sampling System
PLSS	: Primary Liquid Sampling System
PSS	: Process and Post-Accident Sampling Systems
PS/B	: Power Source Building
RAI	: Request for Additional Information
RCPB	: Reactor Coolant Pressure Boundary
RCS	: Reactor Coolant System
RCP	: Reactor Coolant Pump
SIS	: Safety Injection System
SSAS	: Station Service Air System
SSS	: Secondary Sampling System
SGBDSS	: Steam Generator Blowdown Sampling System
T/B	: Turbine Building
WWS	: Waste Water System

DCD Section 9.3 Process Auxiliaries

Section		Major Contents	Safety-Related function
9.3	Process Auxiliaries	9.3.1 Compressed Air and Gas Systems (CAGS)	Yes
		9.3.2 Process and Post-Accident Sampling System (PSS)	Yes
		9.3.3 Equipment and Floor Drain System (EFDS)	Yes
		9.3.4 Chemical and Volume Control System (CVCS)	Yes

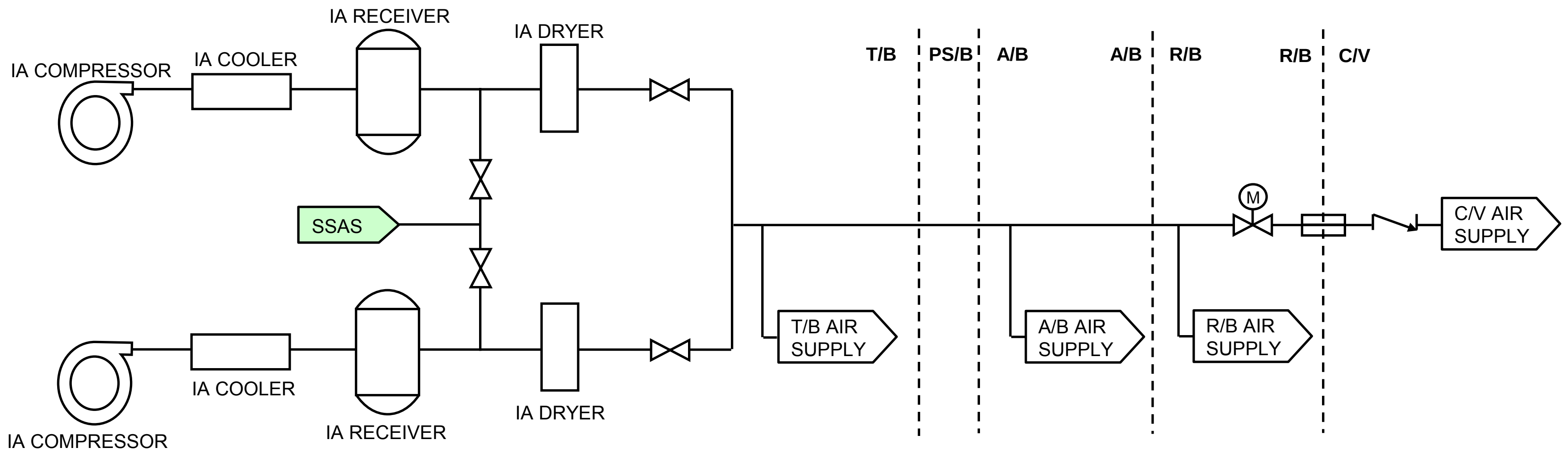
9.3.1 Compressed Air and Gas Systems (CAGS)

- **The CAGS has no safety-related function except for containment isolation.**
- **The CAGS consist of:**
  - ✓ Instrument Air System (IAS)
  - ✓ Station Service Air System (SSAS)
  - ✓ Compressed Gas System (CGS)

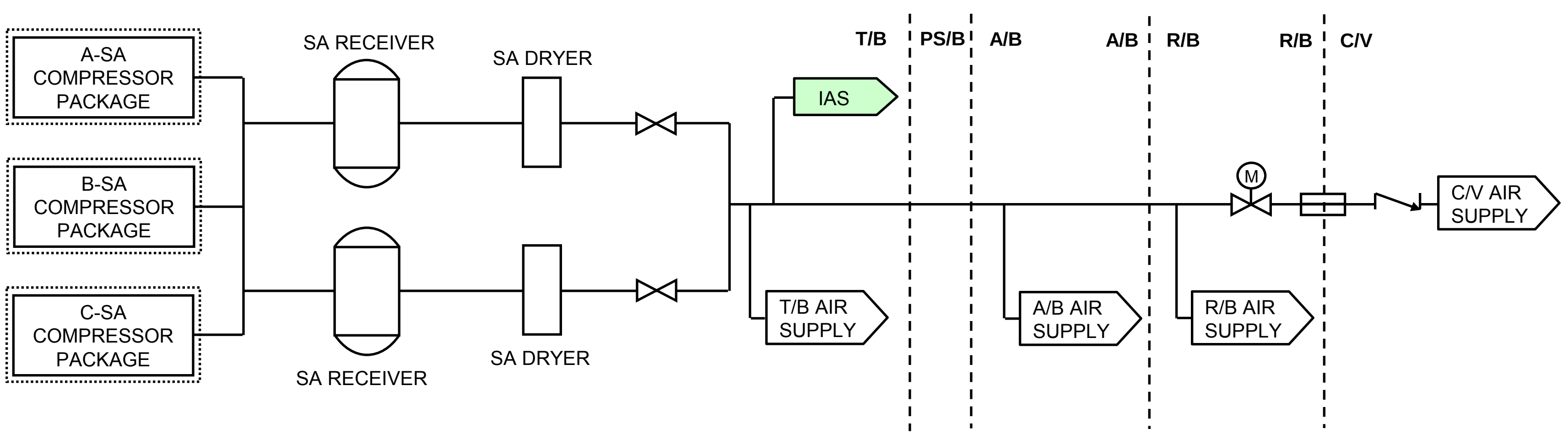
- **IAS**
  - ✓ The IAS consists of two 100% trains with a compressor, an air receiver, and an air dryer in each train.
  - ✓ The safety-related AOVs fail in safe position on loss of IA and do not need IAS to perform a safety function.
- **SSAS**
  - ✓ The SSAS consists of three 50% trains with compressors.
  - ✓ Three compressor trains share two receivers and two dryers.
  - ✓ The SSAS can supply IAS if additional air is needed.
- **CGS**
  - ✓ The CGS consists of high pressure nitrogen gas, low pressure nitrogen gas, and hydrogen gas distribution subsystems and provide pressure-regulated gases for purging, diluting, and inerting.
  - ✓ High pressure nitrogen gas is supplied to SIS Accumulators.

9.3.1 Compressed Air and Gas Systems (CAGS)

INSTRUMENT AIR SYSTEM



STATION SERVICE AIR SYSTEM



9.3.1 Compressed Air and Gas Systems (CAGS)

➢ SER Open and Confirmatory Items

RAI No.	Question 09.03.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.3.2 Process and Post-Accident Sampling Systems (PSS)

PSS have no safety-related function except for containment isolation. The PSS includes the following sub-systems:

- **The Primary Liquid Sampling System (PLSS)**
- **The Primary Gaseous Sampling System (PGSS)**
- **The Post-Accident Sampling System (PASS)**
- **The Secondary Sampling System (SSS)**
- **The SGBD Sampling System (SGBDSS)**
- **Manual local grab sample provision**

Each subsytem performs the following function:

- **PLSS collects liquid samples from RCS and auxiliary systems for analysis.**
- **PGSS collects gaseous samples from containment atmosphere.**
- **PASS collects highly radioactive samples of the reactor coolant, refueling water storage pit water and containment atmosphere for analysis following accident.**
- **SSS monitors water sample from the turbine cycle so as to control water chemistry.**
- **SGBDSS monitors secondary water in SGs to maintain acceptable water chemistry and detect primary to secondary SG tube leakage.**
- **Manual local grab sample allows collection of liquid samples from various sampling point for analysis.**

SER Open and Confirmatory Items

RAI No.	Question 09.03.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.3.3 Equipment and Floor Drain Systems (EFDS)

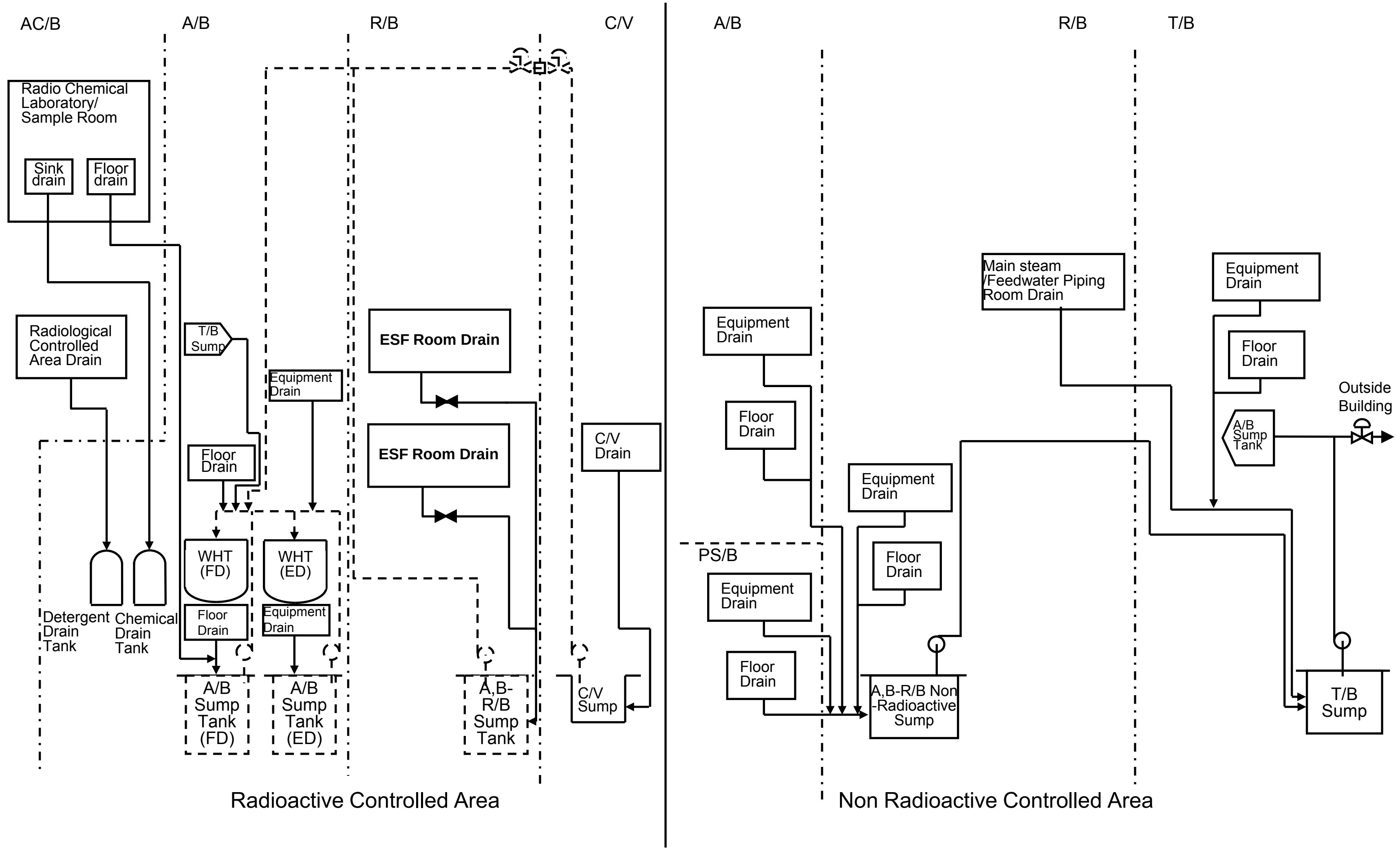
EFDS has no safety function except the isolation valves installed in the drainage piping from the ESF rooms. The EFDS includes the following sub-systems:

- **Radioactive liquid waste**
- **Non-radioactive liquid waste**
- **Chemical and detergent liquid waste**
- **Oily liquid waste**

EFDS performs the following functions:

- **EFDS collects liquid waste separately depending on the liquid waste property from equipment and floor drains by gravity during all modes of operation.**
- **Collected potential radioactive liquid waste in the EFDS is transferred to the LWMS for processing while collected non radioactive liquid waste is transferred to the T/B sump for processing.**

9.3.3 Equipment and Floor Drain Systems (EFDS)



Equipment and Floor Drain System Flow Diagram

9.3.3 Equipment and Floor Drain Systems (EFDS)

➢ SER Open and Confirmatory Items

RAI No.	Question 09.03.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.3.4 Chemical and Volume Control System (CVCS)

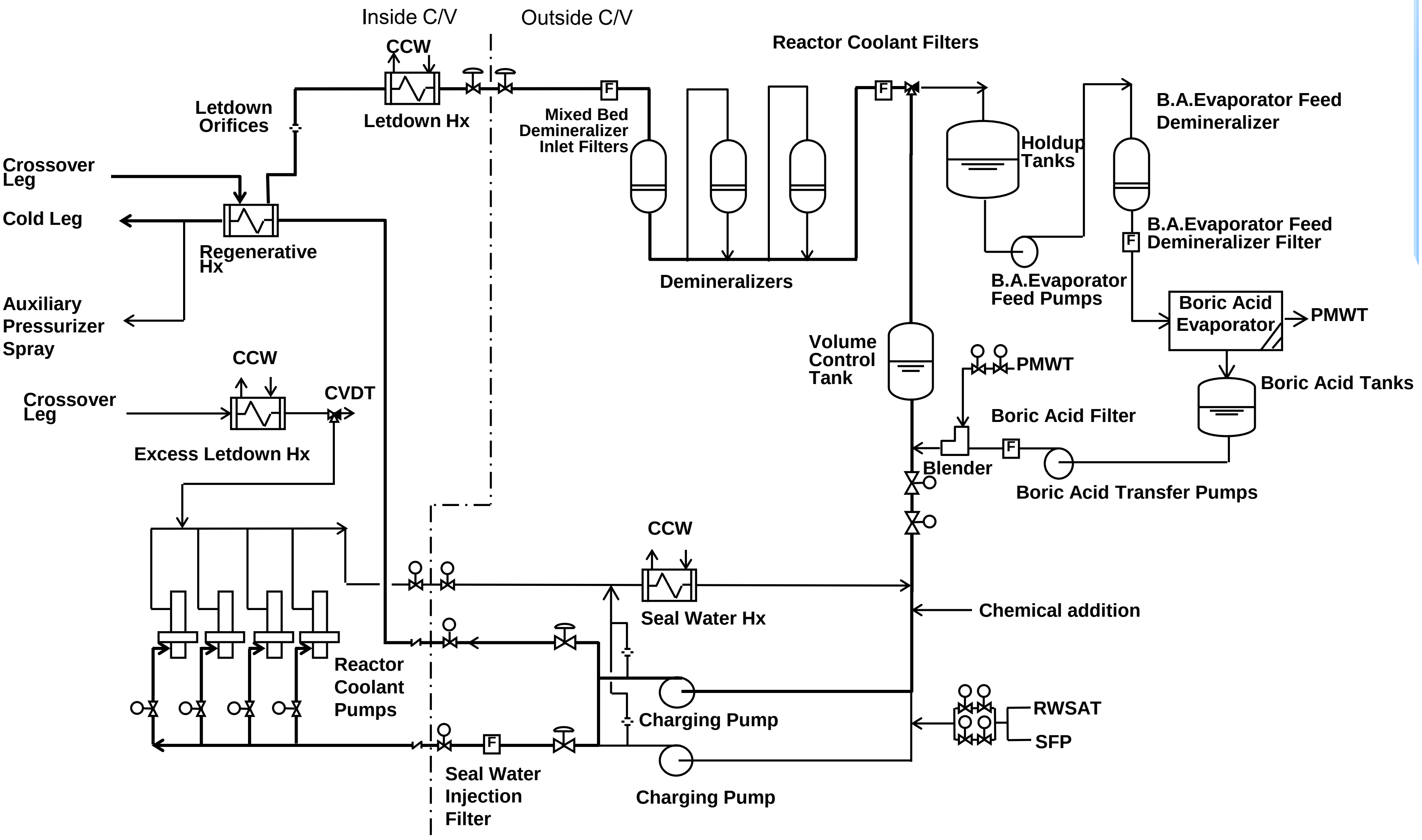
CVCS performs the following functions:

- **Maintain the coolant inventory in the RCS for all modes of operation**
- **Provide seal-water flow to the RCP**
- **Provide makeup capability for small RCS leaks**
- **Regulate the boron concentration in the reactor coolant**
- **Control the reactor coolant water chemistry**
- **Purify the reactor coolant by removal of the fission and activation products**

The CVCS performs or supports the following safety-related functions:

- **Provide reactor coolant pressure boundary (RCPB)**
- **Containment isolation for the CVCS lines penetrating the containment**
- **Provide capability to isolate the charging line upon ECCS actuation signal and high pressurizer water level signal**
- **Isolation of RCS boron dilution sources to preclude inadvertent reactivity additions**

9.3.4 Chemical and Volume Control System (CVCS)



9.3.4 Chemical and Volume Control System (CVCS)

➢ SER Open and Confirmatory Items

RAI No.	Question 09.03.04-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

Presentation to ACRS Subcommittee

Chapter 9: Auxiliary Systems

Section 9.4 Air Conditioning, Heating, Cooling, and Ventilation Systems

March 22-23, 2012

Mitsubishi Heavy Industries, Ltd.

MHI Presenters

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Acronyms (1/1)

A/B	: Auxiliary Building
AC/B	: Access Building
ASME	: American Society of Mechanical Engineers
CFR	: Code of Federal Regulations
CRE	: Control Room Envelope
COL	: Combined License
CRDM	: Control Rod Drive Mechanism
ESF	: Engineered Safety Features
GDC	: General Design Criteria
HEPA	: High-efficiency Particulate Air
HVAC	: Heating, Ventilation, and Air Conditioning
ITAAC	: Inspection, Test, Analysis, and Acceptance Criteria
LOCA	: Loss-of-coolant Accident
MCR	: Main Control Room
PS/B	: Power Source Building
R/B	: Reactor Building
RG	: Regulatory Guide
RIS	: Regulatory Issue Summary
SRP	: Standard Review Plan
SSC	: Structure, System, and Component
T/B	: Turbine Building
TSC	: Technical Support Center

DCD Section 9.4 Air Conditioning, Heating, Cooling, and Ventilation Systems

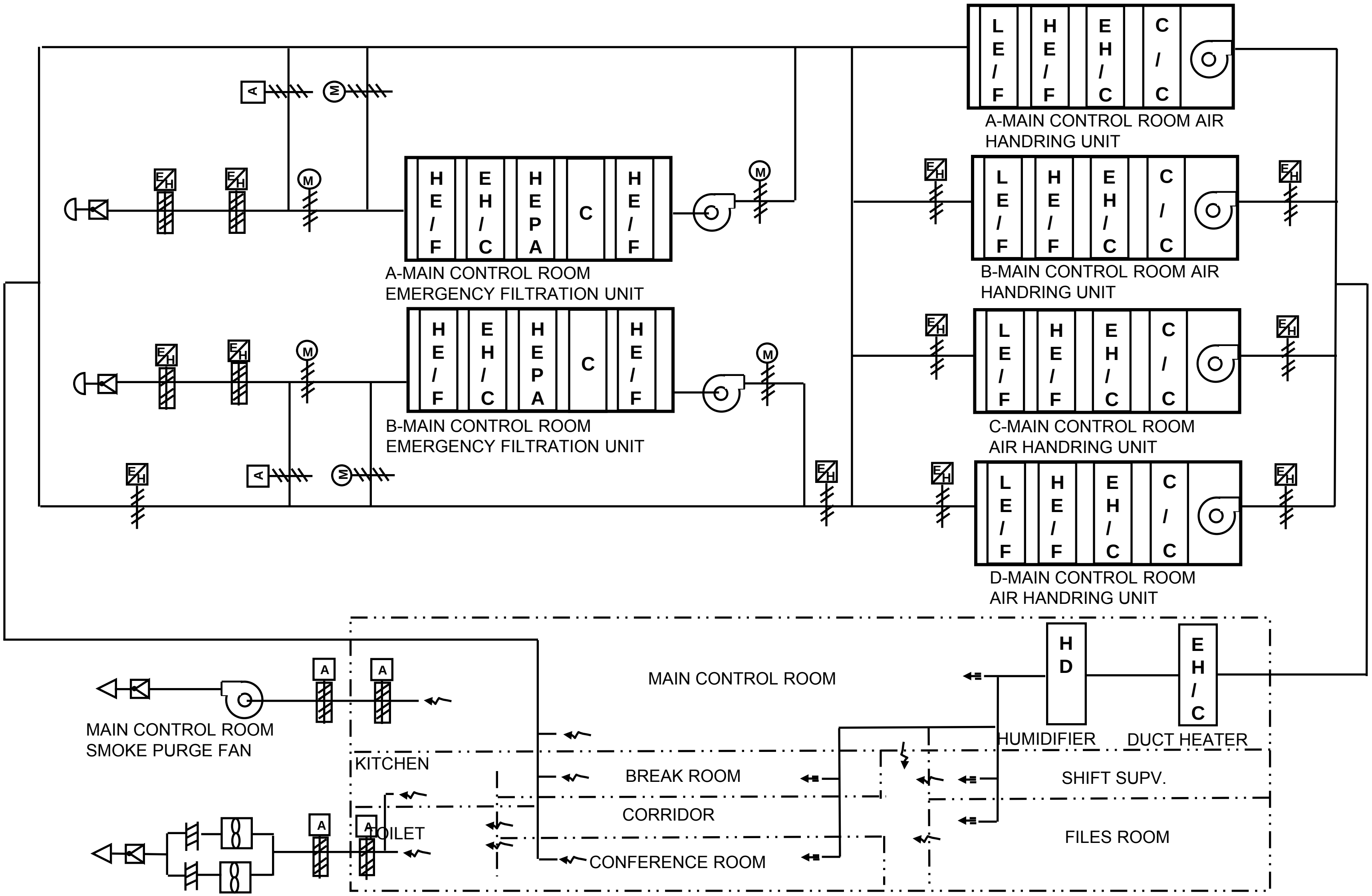
US-APWR

Section		Major Contents	Safety-Related function
9.4	Air Conditioning, Heating, Cooling, and Ventilation Systems	9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System	Yes
		9.4.2 Spent Fuel Pool Area Ventilation System	Not Applicable
		9.4.3 Auxiliary Building Ventilation System	Yes
		9.4.4 Turbine Building Area Ventilation System	No
		9.4.5 Engineered Safety Feature Ventilation System	Yes
		9.4.6 Containment Ventilation System	Yes

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

- **The MCR HVAC System provides and controls the proper environment in the MCR and other areas within the control room envelope (CRE).**
- **The MCR HVAC System is a safety-related system and performs the following functions:**
  - ✓ Excludes entry of airborne radioactivity into the CRE and removes radioactive material from the CRE environment.
  - ✓ Supports and maintains CRE habitability and permits personnel occupancy and proper functioning of instrumentation during normal conditions and design basis accidents.

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)



9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
883-6063	29	Open Item 09.04.01-29 - Provide the calculated values for maximum component temperatures in the adsorber section with normal ventilation unit flow and with filtration unit shutdown (post-LOCA condition) to conclude that design limiting temperature of 300F is not exceeded. - Provide the maximum expected post-accident radioactively-induced temperature of the charcoal filter beds.	➢ MHI is discussing draft response with NRC staff: ✓ The charcoal adsorber is designed in accordance with RG 1.52 and the actual loading is expected to be lower such that iodine desorption temperature would not be challenged. The high temperature alarm setpoint is established to prevent exceeding the temperature at which iodine desorption can occur. ✓ The high-high temperature alarm setpoint is established to prevent exceeding the temperature at which charcoal ignition can occur.

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

US-APWR

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
883-6063	29	Open Item 09.04.01-29 (continued) - Provide the maximum mass loading on the upstream HEPA filters of both the MCR emergency filter trains and the Annulus Emergency Exhaust System filter trains.	✓ The HEPA filter unit is designed in accordance with RG 1.52 and ASME AG-1. HEPA filter particulate loading is expected to be low relative to rated dust loading due to the installed upstream high efficiency pre-filter. The HEPA filters are installed to include margin over the design flowrate. MHI is in discussion with NRC staff regarding final resolution.

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
883-6063	30	Open Item 09.04.01-30 - Provide additional information related to the deletion of ITAAC Item 12 from Tier 1 Table 2.6.5-1 related to AAC GTG reliability.	MHI is in discussion with NRC staff regarding further substantiating the reason for this deletion.
883-6063	31	Open Item 09.04.01-31 Provide justification for non-safety related MCR HVAC humidifiers and controls. NRC staff requests a minimum credible humidity for the site conditions permitted in the DC with no humidity control to use for the qualification of control room electrical equipment or the change in the plant design to include safety-related humidifiers.	The response to this open item is under development.

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
883-6063	32	Open Item 09.04.01-32 Provide additional information regarding the design of the MCR air handling unit cooling coils and provisions to prevent coil leakage from entering the MCR through the supply duct.	➢ MHI provided: ✓ The safety-related, seismic category I MCR HVAC cooling coils are not subject to postulated failure consistent with the requirements of GDC 4. Therefore, special design features to protect against a cooling coil rupture or significant leak are not warranted. Normal AHU drains accommodate condensation and minor leakage. MHI is in discussion with NRC staff regarding final resolution.

9.4.1 Main Control Room Heating, Ventilation and Air Conditioning System (MCR HVAC System)

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.01-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
825-5999	09.04.05-21	Confirmatory Item 09.04.05-21 Provide a reference to the updated March, 2011 version of MUAP-10020 in the DCD.	➢ As described in the response to the RAI, MHI intends to revise the reference to MUAP-10020 in the next revision of the DCD to support closure of this confirmatory item.

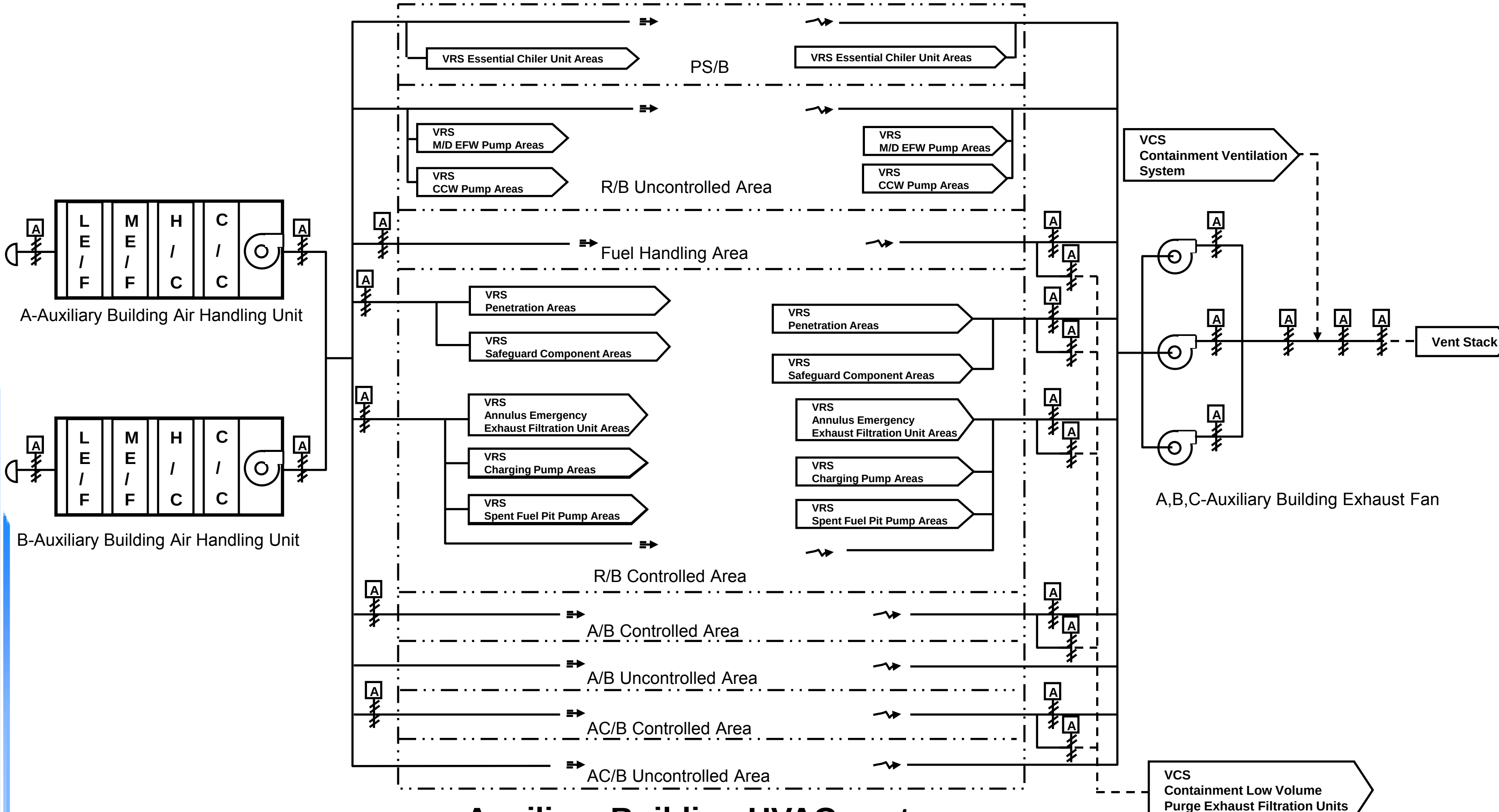
9.4.3 Auxiliary Building Ventilation System

The Auxiliary Building Ventilation System includes the following sub-systems:

- ✓ Auxiliary building HVAC system
- ✓ Non-Class 1E electrical room HVAC system
- ✓ Main steam/feedwater piping area HVAC system
- ✓ Technical support center (TSC) HVAC system

- ➢ **The auxiliary building HVAC system is a non-safety related system, with the exception of safety-related isolation dampers which isolate the penetration and the safeguard component areas, and the vent stack from the auxiliary building HVAC system.**
- ➢ **The auxiliary building HVAC system performs the following functions:**
  - ✓ Provide and maintain proper operating environment within the required temperature range for areas housing mechanical and electrical equipment within the A/B, R/B, PS/B and AC/B during normal plant operation.
  - ✓ Keep dose levels due to the airborne radioactivity in normally occupied areas below the allowable values.
  - ✓ Maintain a slightly negative pressure in the controlled areas relative to the outside atmosphere to minimize exfiltration from the radiological controlled areas.
  - ✓ Maintain airflow from areas of low radioactivity to areas of potentially higher radioactivity.

9.4.3 Auxiliary Building Ventilation System



Auxiliary Building HVAC system

9.4.3 Auxiliary Building Ventilation System

- **The Non-Class 1E electrical room HVAC system is non-safety related system and performs the following function:**
  - ✓ Provide and maintain the room ambient conditions within the required temperature range to support the continuous operation of the electrical equipment and components.
  - ✓ Maintain the hydrogen concentration below 1% by volume of battery room.
- **The TSC HVAC system is non-safety related system and performs the following functions:**
  - ✓ Exclude entry of airborne radioactivity into the TSC envelope and remove radioactive material from the TSC envelope environment.
  - ✓ Provide and maintain proper environmental conditions within the required temperature range to assure personnel comfort and to support the operation of the control and instrumentation equipment and components.
  - ✓ Support and maintain TSC habitability and permit personnel occupancy following plant emergency conditions.
- **The Main steam/feedwater piping area HVAC system is a non-safety related system.**
  - ✓ Provide and maintain proper environmental conditions within the required temperature range suitable to support the operation and assure the reliability of the electrical and mechanical components.

9.4.3 Auxiliary Building Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
831-6030	17	<u>Open Item 09.04.03-17</u> Provide additional justification for not including the ABVS function to provide dilution flow in support of the GWMS in Tier 1.	➢MHI provided: ✓The existing Tier 1 descriptions and ITAAC verify functional arrangement of ABVS to support the dilution flow function and are consistent with SRP 14.3 guidance and RIS 2008-05 guidance for Tier 1 content.

9.4.3 Auxiliary Building Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
831-6030	18	<u>Open Item 09.04.03-18</u> Clarify ITAAC Table 2.7.5.4-3 line item 10 to ensure ABVS exhaust flow greater than supply flow to maintain a negative pressure within the radiologically controlled areas.	➢MHI provided: ✓Revised wording for the ITAAC to clarify that the design commitment is to maintain exhaust airflow greater than supply airflow to control the release of potentially radioactive materials from radiologically controlled areas, and the acceptance criteria is that two of three exhaust fans will be operating and that exhaust flowrate will be greater than supply flowrate.

9.4.3 Auxiliary Building Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
831-6030	19	Open Item 09.04.03-19 Provide the description of the function of the ABVS exhaust flow damper to prevent backflow. Establish that the responsibility for ABVS flow balance testing and frequency is assigned to the COL applicant.	➢MHI provided: ✓The description of the function of the ABVS exhaust flow damper to prevent backflow will be included in the DCD. ✓A COL applicant item for ABVS flow balance testing and frequency will be included in the DCD.
831-6030	20	Open Item 09.04.03-20 Provide a description of the check valve in the sump line between the TB sump and the A/B that prevents backflow to the TB.	➢MHI provided: ✓The description of the check valve in the sump line between the TB sump and the A/B that prevents backflow to the TB will be included in the DCD and shown on the flow diagram.

9.4.3 Auxiliary Building Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
831-6030	21	<u>Open Item 09.04.03-21</u> Revise DCD Figure 9.4.3-1 (ABVS) to reflect the existence of backdraft dampers.	➢MHI provided: ✓DCD Subsection 9.4.3.2.1 system description will be revised to describe the backdraft dampers. The description is broadly applicable and inclusive of auxiliary building HVAC system branch ducts supplying or exhausting uncontrolled areas that may not be shown on the simplified flow diagram. Therefore, it is not practical or necessary to show the backdraft dampers on DCD Figure 9.4.3-1.

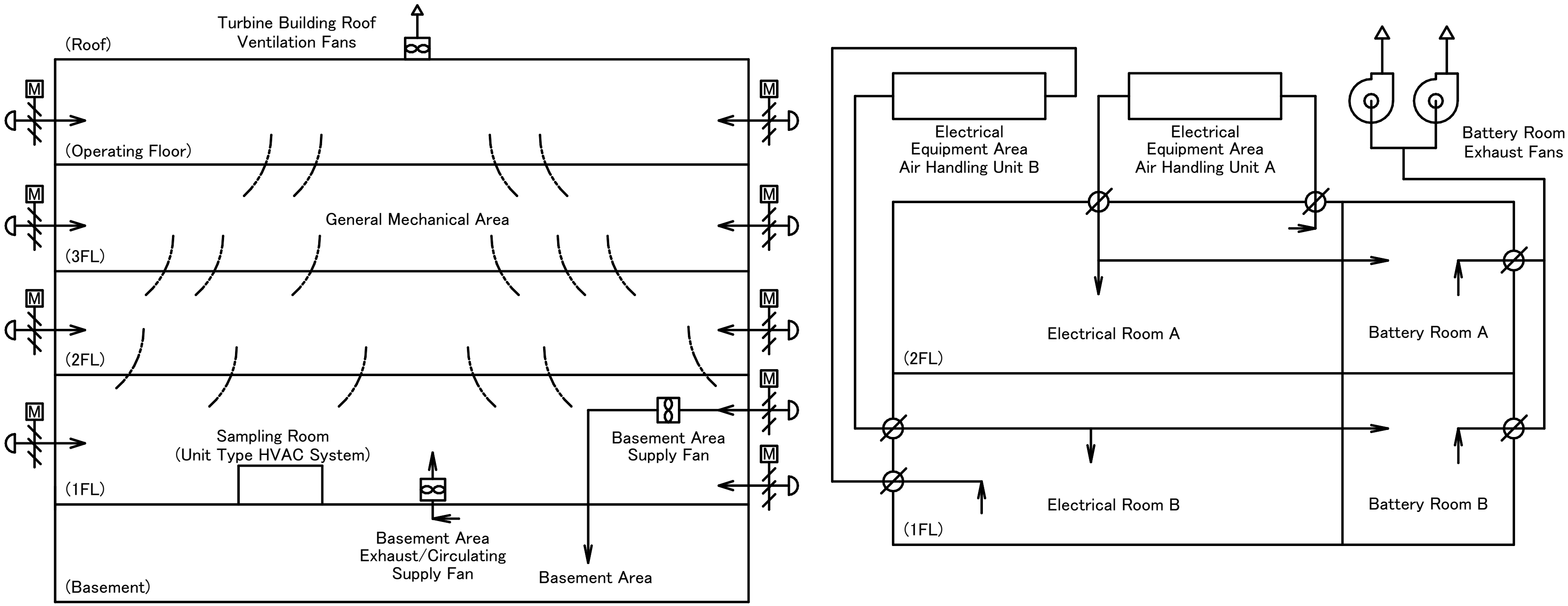
9.4.3 Auxiliary Building Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
355-2942	3	Confirmatory Item 09.04.03-3 Revise the DCD to reflect the existence of ABVS backdraft dampers.	➢MHI provided: ✓DCD Subsection 9.4.3.2.1 system description will be revised to describe the backdraft dampers to support closure of this item.

9.4.4 Turbine Building Area Ventilation System

- The Turbine Building Area Ventilation System (T/B HVAC) is a non safety related system.
- The T/B area is not expected to include airborn radioactive contamination. No safety related SSCs are in T/B.
- The T/B HVAC maintain a suitable environment for the operation of equipment in the turbine building.



9.4.4 Turbine Building Area Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.04-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
586-4690	6	To explain how GDC2 is not applicable, the DCD states that safety-related equipment is not located in the T/B. This commitment must be expanded to "Important to Safety" equipment. According to Appendix 3D of DCD Ch. 3, there are "Important to Safety" SSCs in T/B .	➢ Draft response currently under development.
713-5555 (follow-up)	7		
814-5943 (follow-up)	8		

9.4.5 Engineered Safety Feature (ESF) Ventilation System

- **The ESF Ventilation System is a safety related system and includes the following sub-systems:**
  - ✓ Annulus Emergency Exhaust System
  - ✓ Class 1E Electrical Room HVAC System
  - ✓ Safeguard Component Area HVAC System
  - ✓ Emergency Feedwater Pump Area HVAC System
  - ✓ Safety Related Component Area HVAC System

9.4.5 Engineered Safety Feature (ESF) Ventilation System

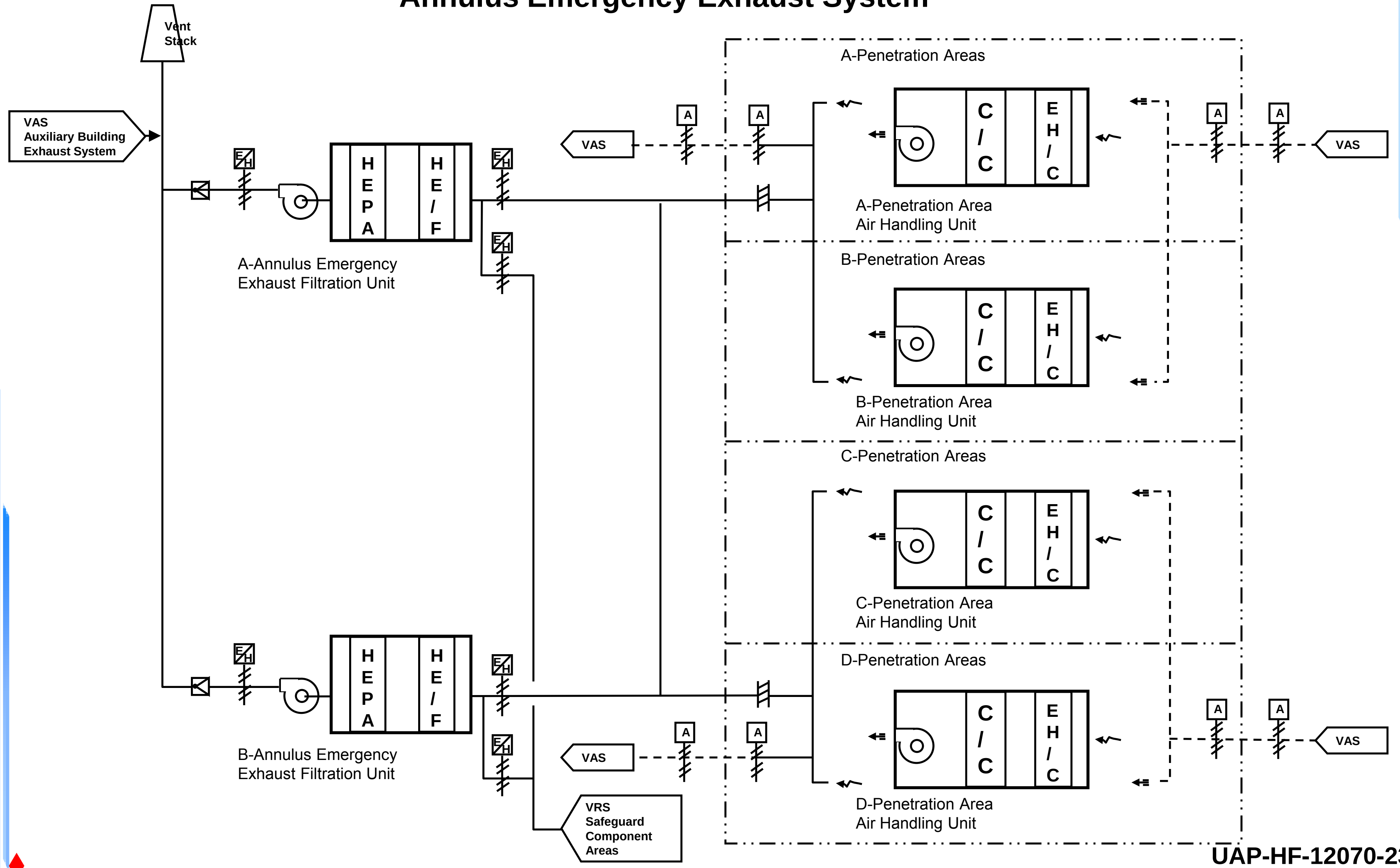
- **Annulus Emergency Exhaust System performs the following function:**
  - ✓ Remove and retain fission products by filtering the air that is exhausted from the penetration areas and safeguard component areas following an accident.

- **Class 1E Electrical Room HVAC System performs the following functions:**
  - ✓ Maintain proper operating environmental conditions within Class 1E electrical rooms.
  - ✓ Maintain the hydrogen concentration below 1% by volume in the Class 1E battery room.

- **Other subsystems of the ESF ventilation system provide the proper environmental conditions within plant areas that house engineered safety features equipment.**

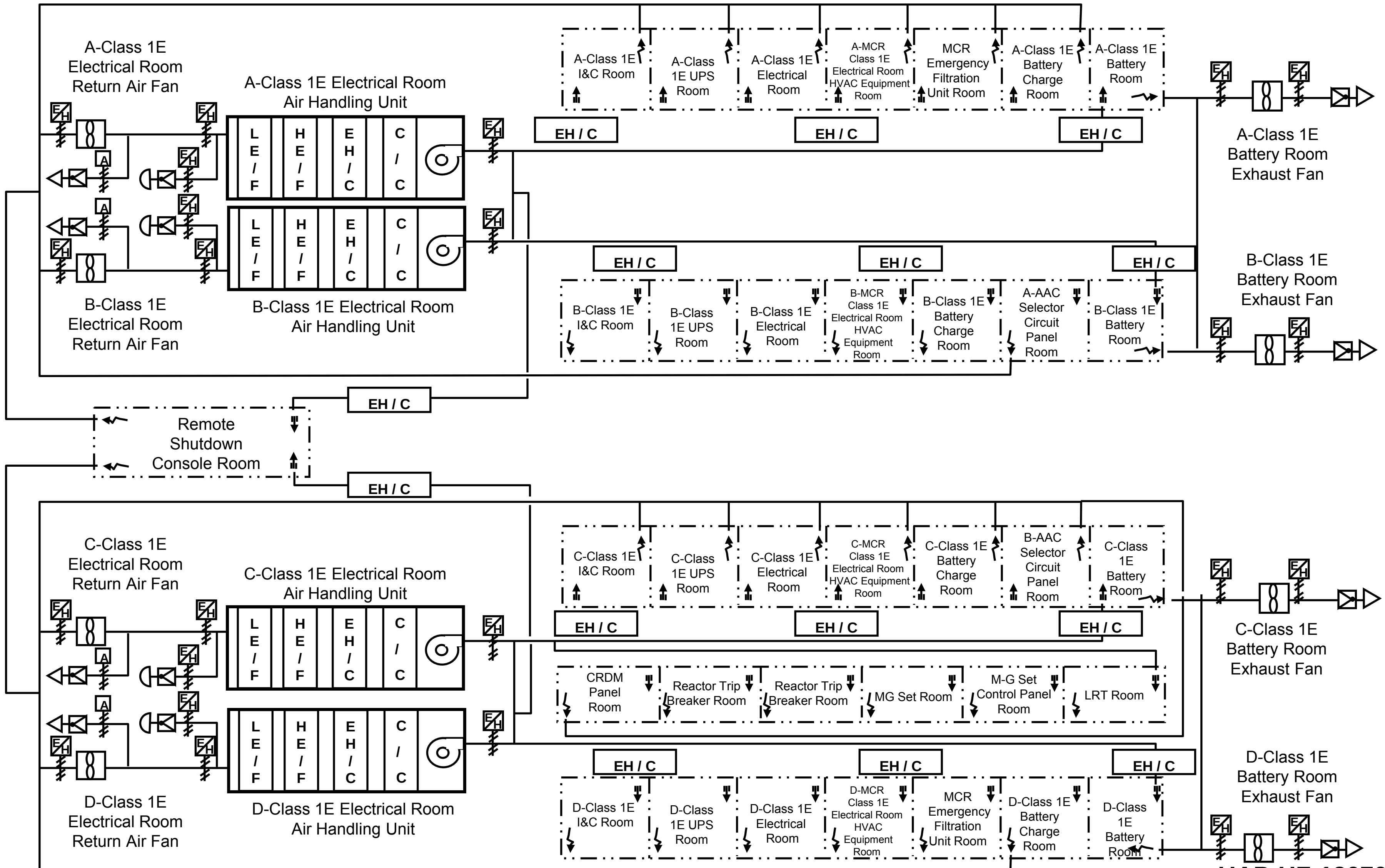
9.4.5 Engineered Safety Feature (ESF) Ventilation System

Annulus Emergency Exhaust System



9.4.5 Engineered Safety Feature (ESF) Ventilation System

Class 1E Electrical Room HVAC System



9.4.5 Engineered Safety Feature (ESF) Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.05-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
825-5999	20	<u>Open Item 09.04.05-20</u> Provide the revision to ITAAC Table 2.7.5.2-3 as committed in response to RAI 474-3811, Question 09.04.05-10.	➢MHI provided: ✓As part of the implementation of RIS 2008-05 guidance for Tier 1 ITAAC, MHI determined that portions of the committed changes to ITAAC Table 2.7.5.2-3 were not appropriate since those additions were not credited in accident analyses and were not key functions.

9.4.5 Engineered Safety Feature (ESF) Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.05-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
670-4773	18	Confirmatory Item 09.04.05-18 Provide a correction to the response to RAI 64-735, Question 9.4.5-18 related to battery hydrogen generation during discharge.	➢MHI will provide an amended response to RAI 64-735, Question 9.4.5-18 to support closure of this item.
825-5999	21	Confirmatory Item 09.04.05-21 Provide a reference to technical report MUAP-10020 (HVAC Calculations) in DCD Section 6.5.7.	➢As described in the response to the RAI, MHI intends to revise the reference to MUAP-10020 in the next revision of the DCD to support closure of this confirmatory item.

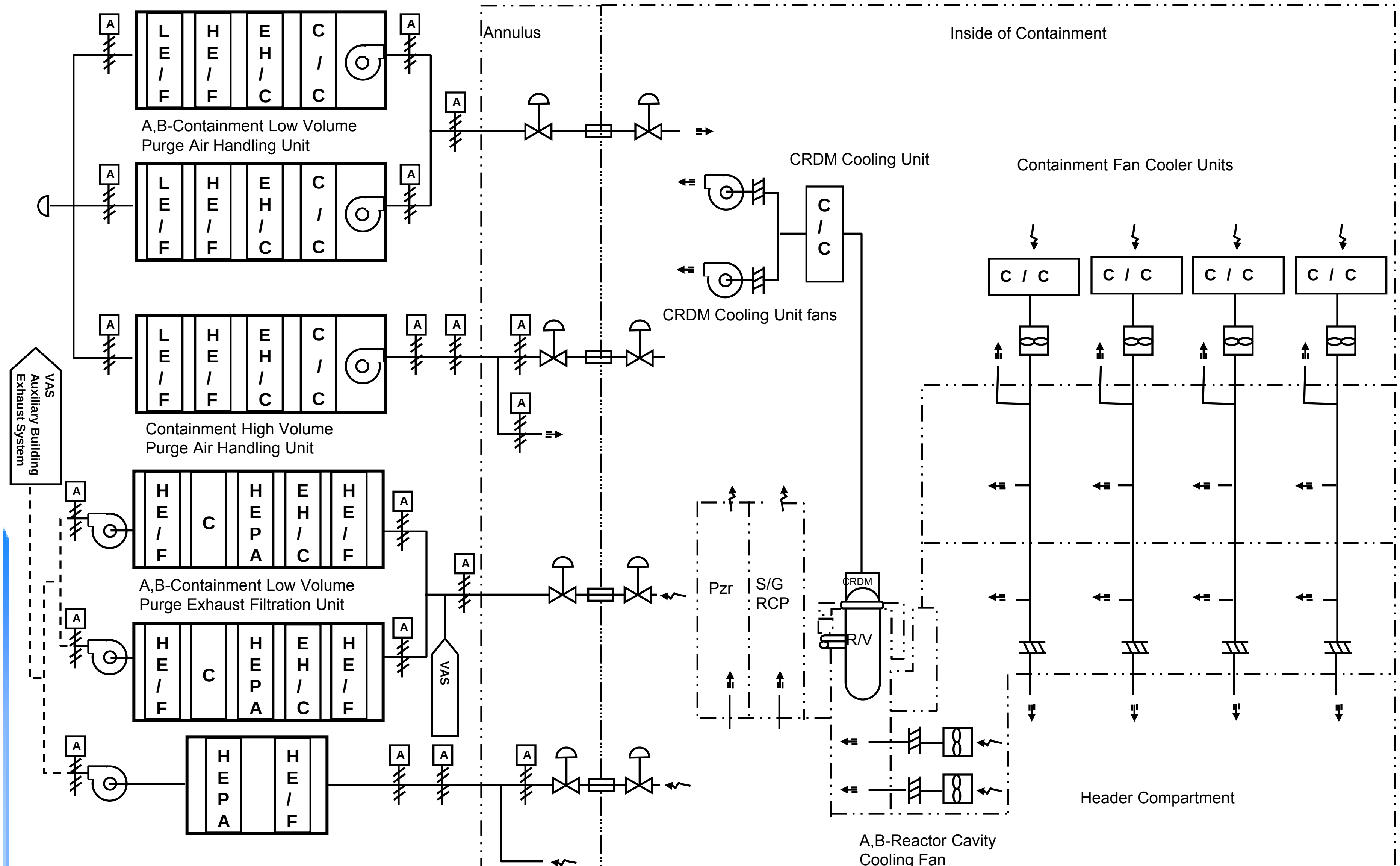
9.4.6 Containment Ventilation System

- **The Containment Ventilation System is a non-safety related system, with the exception of piping and valves between and including containment isolation valves, and includes the following sub-systems:**
  - ✓ Containment Fan Cooler System
  - ✓ Control Rod Drive Mechanism (CRDM) Cooling System
  - ✓ Reactor Cavity Cooling System
  - ✓ Containment Purge System
- **Containment Fan Cooler System performs the following function:**
  - ✓ Maintain proper environmental conditions in containment during normal plant operation and LOOP condition.
- **CRDM Cooling System performs the following function:**
  - ✓ Remove the heat dissipated by the CRDMs.
- **Reactor Cavity Cooling System performs the following functions:**
  - ✓ Remove the heat dissipated by the reactor vessel, the reactor vessel support structure, and the gamma radiation and fast neutron bombardment on the primary shield wall.
  - ✓ Provide adequate cooling for the primary shield and the reactor vessel support base plates to prevent concrete dehydration.

9.4.6 Containment Ventilation System

- **Containment Purge System includes the following sub-systems:**
  - ✓ Containment low volume purge system
  - ✓ Containment high volume purge system
- **Containment Low Volume Purge System performs the following functions:**
  - ✓ Minimize the potential spread of radioactive contamination from the areas serviced by the auxiliary building HVAC system.
  - ✓ Provide relief from pressure build-up within containment caused by instrument air leakage and containment temperature fluctuations.
- **Containment High Volume Purge System performs the following function:**
  - ✓ Maintain low concentrations of radioactivity in the containment atmosphere to allow access during maintenance and inspection activities

9.4.6 Containment Ventilation System



9.4.6 Containment Ventilation System

➢ Open Items and Confirmatory Items

RAI No.	Question 09.04.06-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
826-6014	06.05.01-22	Open Item 06.05.01-22: Provide ITAAC to demonstrate that as-built fire dampers fully close under system design flow rates.	➢MHI provided: ✓The fire dampers are designed and installed so that the air velocity in the ducts assists in closing and does not preclude proper damper closure per NFPA requirements. Therefore no testing for closure under design flow rates is required.
826-6014	06.05.01-21	Confirmatory Item 06.05.01-21: Amend DCD Subsection 14.2.12.1.66 to resolve inconsistencies as committed to in response to question 06.05.01-14.	➢MHI provided: ✓DCD Subsection 14.2.12.1.66 will be revised as committed in response to 06.05.01-14 to support closure of this item.

Presentation to ACRS Subcommittee

Chapter 9: Auxiliary Systems

Section 9.5 Other Auxiliary Systems

March 22-23, 2012

Mitsubishi Heavy Industries, Ltd.

MHI Presenters

James Curry, Ph.D., P.E., – Lead Presenter

Mitsubishi Nuclear Energy Systems, Inc.

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Acronyms (1/1)

EOF	:Offsite Emergency Operations Facility
FHA	:Fire Hazard Analysis
FOS	:Fuel Oil Storage and Transfer System
GTG	:Gas Turbine Generator
IESNA	:Illuminating Engineering Society of North America
LOOP	:Loss of Offsite Power
MCR	:Main Control Room
PABX	:Private Automatic Branch Telephone Exchange
PS/B	:Power Source Building
RSC	:Remote Shutdown Console
RG	:Regulatory Guide
SBO	:Station Blackout
SRP	:Standard Review Plan
SSC	:Structures, Systems, and Components
TSC	:Technical Support Center
UPS	:Uninterruptible Power Supply

DCD Section 9.5 Other Auxiliary Systems

Section		Major Contents	Safety-Related function
9.5	Other Auxiliary Systems	9.5.1 Fire Protection Program	No
		9.5.2 Communication Systems	No
		9.5.3 Lighting Systems	No
		9.5.4 Gas Turbine Generator Fuel Oil Storage and Transfer System	Yes
		9.5.5 Gas Turbine Generator Cooling Water System [Not Required]	Yes
		9.5.6 Gas Turbine Generator Starting System	Yes
		9.5.7 Gas Turbine Lubrication System	Yes
		9.5.8 GTG Combustion Air Intake, Turbine Exhaust, Room Air Supply, and Air Exhaust Systems	Yes

9.5.1 Fire Protection Program

- **Primary objectives of fire protection program:**
  - ✓ Minimize the potential for fires and explosions to occur.
  - ✓ Rapidly detect, control, and extinguish any fires that do occur.
  - ✓ Assure that any fire that is not promptly extinguished by the fire suppression system will not prevent safe-shutdown of the plant and will minimize the potential for radioactive releases to the environment.

- **Fire Protection Program describes:**
  - ✓ Defense-in-depth approach
  - ✓ Overall fire protection program for facility.
  - ✓ Positions and responsibilities for the program.
  - ✓ Manual and automatic detection and suppression systems
  - ✓ Administrative controls.
  - ✓ That the COL Applicant is responsible for providing site-specific information and a schedule for implementation.

9.5.1 Fire Protection Program

- **Fire protection design features include the following functions:**

  - ✓ Prevent fire initiation by controlling, separating, and limiting the quantities of combustibles and sources of ignition.
  - ✓ Isolate combustible materials and limit the spread of fire by subdividing plant structures into fire areas separated by fire barriers and further separate fire areas into fire zones.
  - ✓ Separate redundant safe-shutdown components and associated electrical divisions by 3-hour rated fire barriers to preserve the capability to achieve and maintain safe shutdown of the plant following a fire.
  - ✓ Preserve the capability to achieve and maintain safe shutdown of the plant using controls external to the main control room (MCR), should a fire require evacuation of the MCR or damage the MCR circuitry for safe-shutdown systems.
  - ✓ Separate redundant trains of safety-related equipment used to mitigate the consequences of a design basis accident.

9.5.1 Fire Protection Program

US-APWR

- **Fire protection systems are designed to:**
  - ✓ Detect and locate fires and provide operator indication of the location.
  - ✓ Provide the capability to extinguish fires in any plant area, to protect site personnel, limit fire damage, and enhance safe-shutdown capabilities.
  - ✓ Supply fire suppression water at a sufficient flow rate and pressure in accordance with NFPA codes.
  - ✓ Maintain 100% design capacity of fire pump, assuming failure of one fire pump or the loss of offsite power (LOOP). Design includes one electric and one diesel-driven fire pump.
  - ✓ The fire protection system is non-safety related with the exception of piping between and including containment isolation valves
  - ✓ Seismic design requirements are applied to portions of the system located in areas containing equipment required for safe-shutdown following a safe-shutdown earthquake (SSE).

9.5.1 Fire Protection Program

- **Fire Hazard Analysis (FHA) for US-APWR standard plant**
  - ✓ The purpose of the FHA is to:
    - Evaluate potential in-situ and transient fire and explosion hazards.
    - Define fire barrier locations
    - Identify detection and suppression coverage throughout the plant
    - Confirm that the effects of a fire in any location in the plant do not adversely impact the ability to safely shut down the reactor and that the release of radioactivity to the environment is controlled and minimized.
    - Select appropriate measures for fire prevention, fire detection, fire suppression, and fire containment for each fire area containing structures, systems, and components (SSCs) important to safety in accordance with NRC guidelines and regulations.
  - ✓ The FHA is performed for areas of the plant containing safety-related components and for areas containing systems important to the generation of electricity. The FHA is performed on a fire area by fire area basis with combustible loads identified by fire zone. This approach provides confidence that plant safety is achieved and the intent of fire protection program requirements are satisfied.

9.5.2 Communication Systems

- The Communication systems consist of:
  - ✓ Public address system/page
  - ✓ Telephone system
  - ✓ Sound powered telephone system
  - ✓ Plant radio system
  - ✓ Offsite communication system including emergency communication systems
- The means exists for communication between the MCR and TSC and from the MCR and TSC to Offsite Emergency Operations Facility (EOF), principal state and local emergency operations centers, and radiological field assessment teams.
- The means exist for communication from the MCR, TSC, and EOF to the NRC headquarters and regional emergency operations centers.

9.5.2 Communication Systems

➢ **Major RAIs (Confirmatory Items)**

RAI No.	Question 09.05.02-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
859-6105	11	Confirmatory Item 9.5.2-1: DCD Tier 2, Section 13.3 became specific on details concerning telecommunication in the Technical Support Center (TSC) by stating that, “Ample working areas for all personnel as described in section 9.5.2.” However, DCD Tier 2, Section 9.5.2, does not address “ample working areas.”	➢ MHI previously provided: ✓ The phrase was meant to say “Plant communications systems are described in Subsection 9.5.2” and states the correction would be made in the next DCD revision.

9.5.3 Lighting Systems

- **The lighting system consists of:**
  - ✓ Normal lighting: All indoor and outdoor areas
  - ✓ Emergency lighting
    - Class 1E emergency lighting: Safe shutdown operation area
    - Self-contained battery pack emergency lighting: Emergency operation area, safe ingress and egress route of personnel during emergencies
    - Normal/emergency lighting: All indoor plant area except the MCR and RSC room
- **The lighting system is supplied from:**
  - ✓ Normal lighting: Non-Class 1E power system
  - ✓ Emergency lighting
    - Class 1E emergency lighting: Class 1E power system
    - Self-contained battery pack emergency lighting: Class 1E power system or Non-Class 1E power system, as applicable
    - Normal/emergency lighting: Non-Class 1E power system, backed up by alternate ac power source

9.5.3 Lighting Systems

➢ Major RAIs (Open and Confirmatory Items)

RAI No.	Question 09.05.03-X	RAI Topic / NRC Concern	RAI Response / DCD Impact
		None	

9.5.4 GTG Fuel Oil Storage and Transfer System

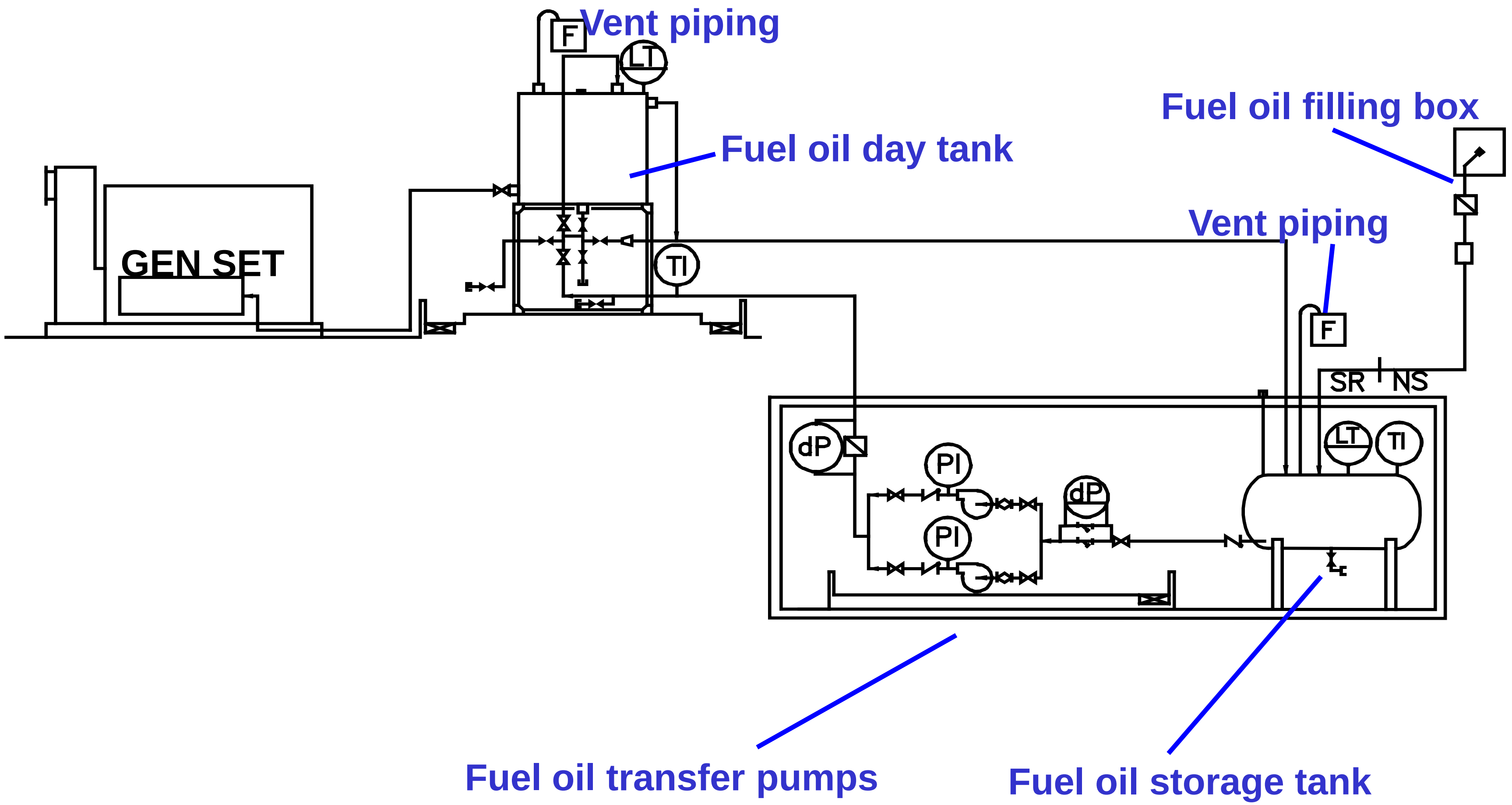
Design Features

- ✓ Each GTG FOS is composed of
  1) One fuel oil storage tank
  2) Two fuel oil transfer pumps
  3) One fuel oil day tank
  4) One fuel filling port
  5) Vent piping from both the fuel oil storage tank and the day tank
  6) Piping and Valves
  7) Instrumentation and Control

- ✓ Capacity
  - Fuel oil storage tank : 7 days
  - Fuel oil day tank : 1.5 hours

9.5.4 GTG Fuel Oil Storage and Transfer System

➢ System Configuration



9.5.4 GTG Fuel Oil Storage and Transfer System

US-APWR

➢ Major RAIs (Open Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
468-3360	9.5.4-49	To add standard for the design of gas turbines “ISO3977 part 3, 2004” **[Open Item 9.5.4-1]**	➢ This standard includes requirements which are applied to continuous operating type GTG and not appropriate for emergency/back-up type GTG. ➢ MHI will identify whether there are some deviations from this standard and make an exception for the emergency GTG support systems.

9.5.4 GTG Fuel Oil Storage and Transfer System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
754-5617	14.3.6-20	-Section2.6.4.1, Item 12.b Rev. 3 of Tier 1 of US-APWR DCD should similarly make it clear that each Class 1E EPS train is located in a separate room of the PS/B. **[Confirmatory Item 9.5.4-1]**	➢ MHI provided: Each redundant division of Class 1E EPSs is located in a separate room of the PS/B. The corresponding ITAAC Acceptance Criteria and Section 2.6.4.1 will be similarly revised.

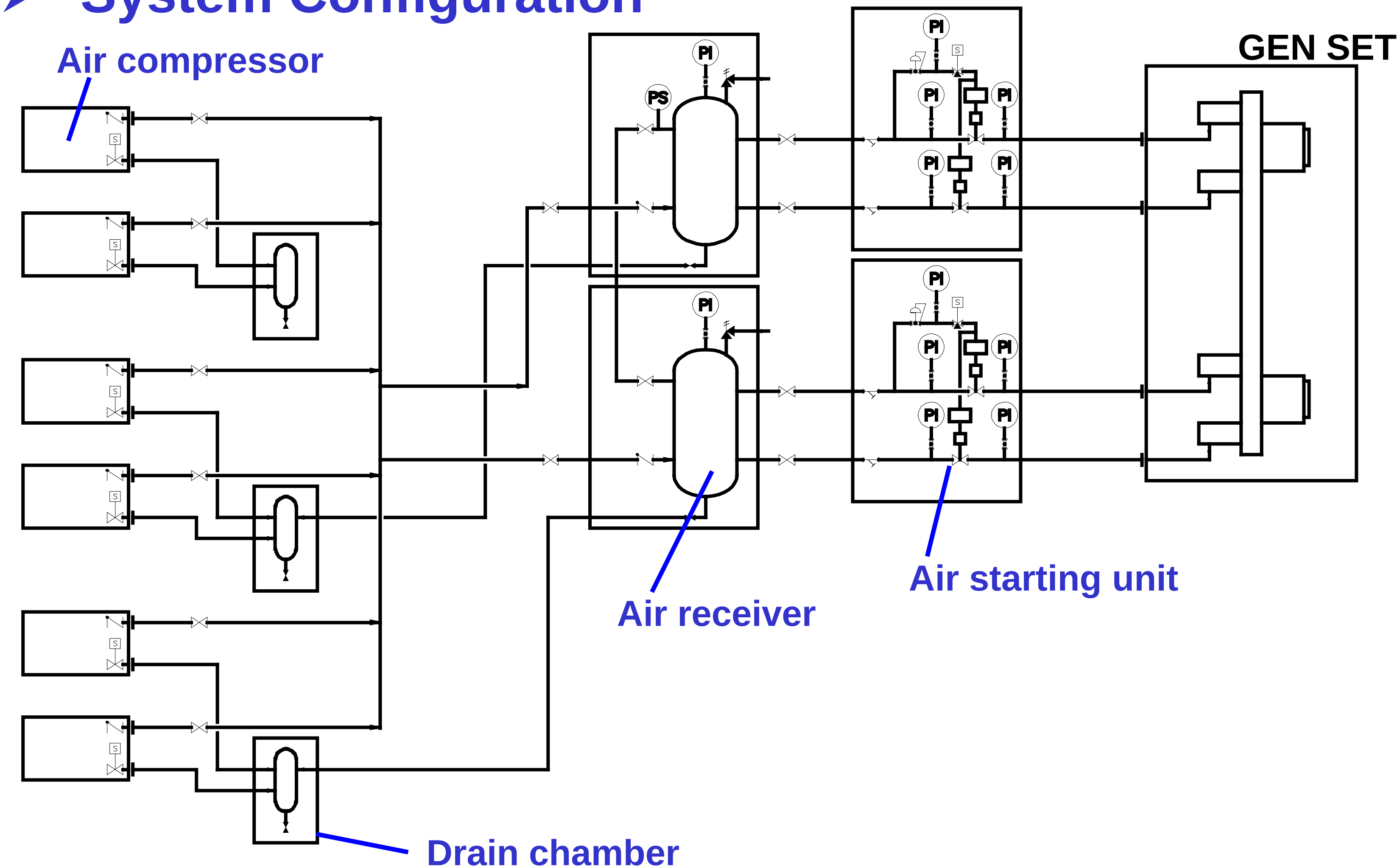
9.5.6 GTG Starting System

Design Features

- ✓ Starting time
  - Less than 100 seconds
- ✓ Starting system
  - Compressed air system
- ✓ Starting Air Capacity
  - Three consecutive GTG starts (without compressor assistance)
- ✓ Each GTG starting system is composed of
  1) Six air compressors with an air cooler
  2) Three drain chambers
  3) Two air receivers
  4) Two air starting units

9.5.6 GTG Starting System

➢ System Configuration



9.5.6 GTG Starting System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
319-2147	9.5.6-20	-The air starting system air receivers should be in accordance with ASME Section III, Class 3. -“Qualification and Test Plan of Class 1E Gas Turbine Generator System,” December 2007, states in accordance with ASME Section VIII. **[Confirmatory Item 9.5.6-1]**	➢ MHI provided: Air receivers are designed to not ASME Section VIII but ASME Section III, Class 3.
754-5617	14.3.6-28	-Rev. 3 of US-APWR DCD Tier1 Table 2.6.4-2, the starting air system are ASME Section III, Class3 from discharge of the air compressors through air starter at the GTG. - DCD Tier 2 Figure 9.5.6-1 (Rev 2) state non safety-related up to the inlet check valve of air receiver. **[Confirmatory Item 9.5.6-2]**	➢ MHI provided: Revising Tier 1, Table 2.6.4-2 to be consistent with Figure 9.5.6-1.

9.5.6 GTG Starting System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
319-2147	9.5.6-22	-"Qualification and Test Plan of Class 1E Gas Turbine Generator System," December 2007, indicates that pipes from air tanks to the generator set shall be zinc coated. -DCD Tier 2 Table 9.5.6-1 indicates that piping will be stainless steel and carbon steel. **[Confirmatory Item 9.5.6-3]**	➢ MHI provided: The zinc coated piping is not applied.
754-5617	14.3.6-24	-Rev. 3 of US-APWR DCD, Table 2.6.4-1, Item 19 addresses the functional arrangements of the fuel oil storage and transfer system and the ventilation/cooling air intake and exhaust system. -There is no similar item in Section 2.6.4.1 for the lube oil and starting air system. **[Confirmatory Item 9.5.6-4]**	➢ MHI provided: US-APWR DCD Rev. 3 Section 2.6.4.2 Design Description 19 and corresponding Table2.6.4-1 ITAAC #19 will be revised to verify GTG compressed air starting system configuration.

9.5.7 Gas Turbine Lubrication System

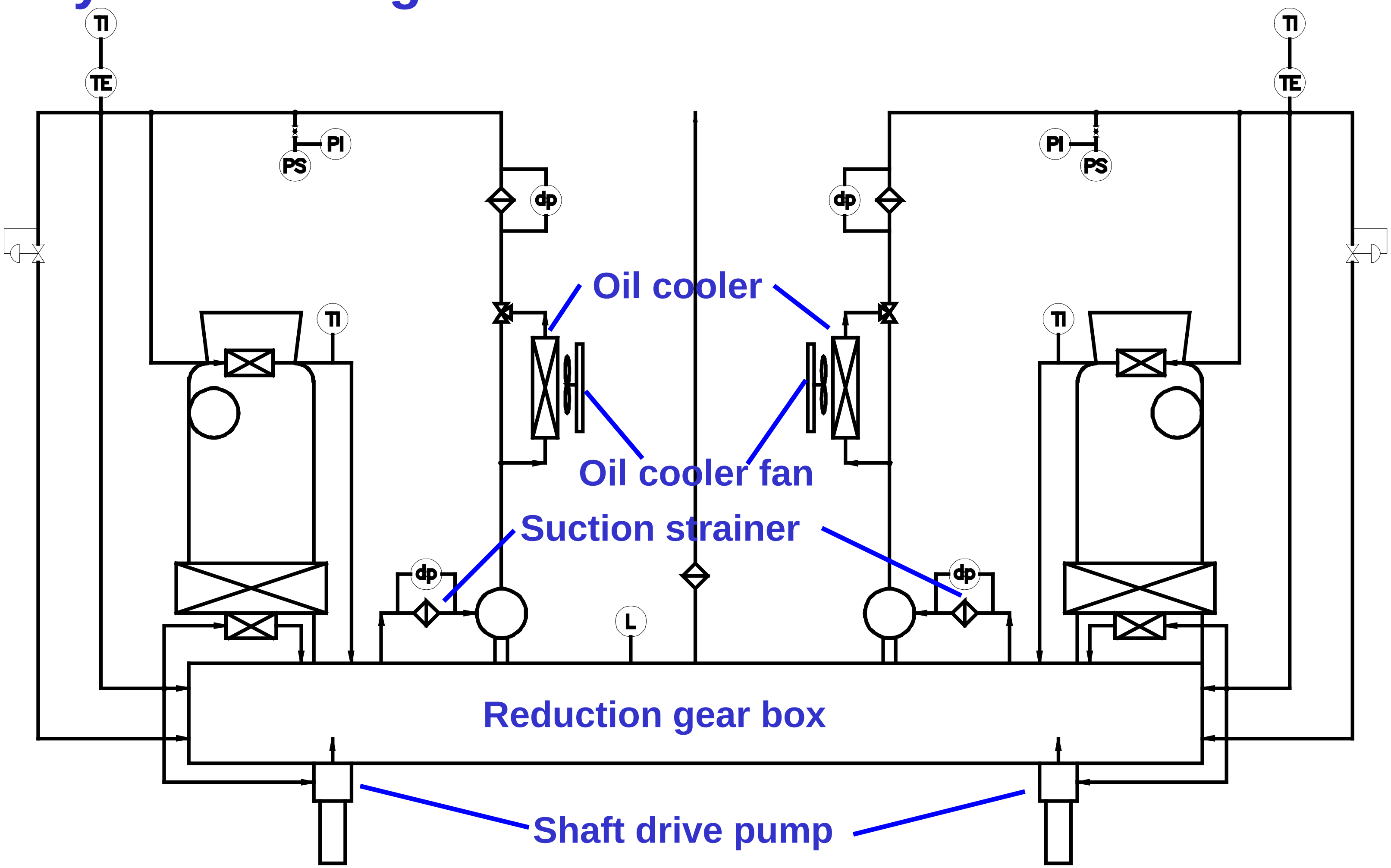
US-APWR

➢ Design Features

- ✓ The lubrication systems are composed of
  1) Two GT shaft drive pumps
  2) One reduction gear box (Oil Reservoir)
  3) Suction strainer at each oil pump suction line
  4) One full flow filter
  5) One lube oil cooler for each pump
  6) Oil cooler fan for each oil cooler
  7) Valves, piping and instrumentation
- ✓ All components of the system are contained in GTG enclosure.
- ✓ Keep-warm system is not installed, since lube oil performs under cold condition

9.5.7 Gas Turbine Lubrication System

➢ System Configuration



9.5.7 Gas Turbine Lubrication System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
754-5617	14.3.6-23	-Rev. 3 of US-APWR DCD, Table 2.6.4-1, Item 16 – The AC for the ITAAC should require that the as-built protection system are automatically bypassed when the Class 1E EPS is started by an ECCS actuation signal. **[Confirmatory Item 9.5.7-1]**	➢ MHI provided: US-APWR DCD Revision 3 Section 2.6.4.1 Design Description 16 and corresponding Table 2.6.4-1 ITAAC #16 will be revised to specify the automatic bypass feature.
754-5617	14.3.6-26	-Rev. 3 of US-APWR DCD, Table 2.6.4-1, Item 30 – This ITAAC should require that the oil capacity verified is based on the maximum expected oil consumption rate, e.g., just prior to a scheduled overhaul. **[Confirmatory Item 9.5.7-2]**	➢ MHI provided: US-APWR DCD Revision 3 Tier 1, Section 2.6.4.3 Design Description 30 and Table 2.6.4-1 ITAAC #30 will be revised to specify the lubricating oil consumption rate for calculating lubrication oil tank capacity (e.g., maximum expected oil consumption rate immediately prior to scheduled overhaul).

9.5.8 GTG Combustion Air Intake, Turbine Exhaust Room Air Supply, and Air Exhaust System

US-APWR

➢ Design Features

✓ Capable of supplying combustion air and providing for exhaust

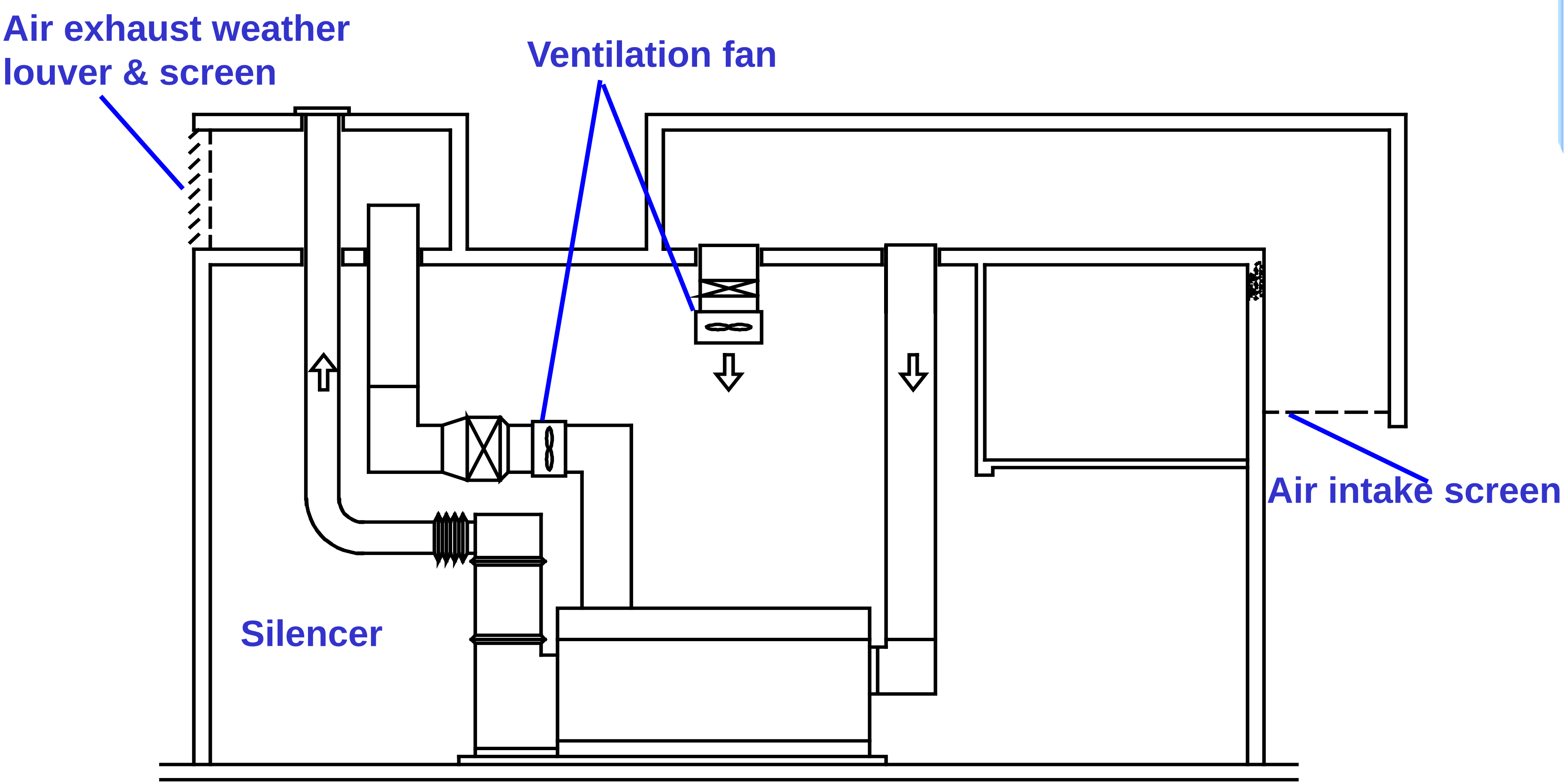
- Continuous operation of the GTGs at 110% rating output

✓ A combustion air intake and exhaust system consists of

1) Air intake screen
2) Air exhaust weather louver and screen
3) Silencer
4) Ventilation fan (room air supply and air exhaust)
5) Associated ductwork and flexible connections

9.5.8 GTG Combustion Air Intake, Turbine Exhaust Room Air Supply, and Air Exhaust System

➢ System Configuration



9.5.8 GTG Combustion Air Intake, Turbine Exhaust Room Air Supply, and Air Exhaust System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
704-5248	9.5.8-28	-The detail how the combustion air intake will be designed to prevent the ingestion of snow and rain. **[Confirmatory Item 9.5.8-1]**	➢ MHI provided: The intake structure extends beyond the edge and below the roof line of the PS/B. The air intake opening intake structure is in a horizontal position facing downward.
754-5617	14.3.6-22	-Rev. 3 of US-APWR DCD, Table 2.6.4-1, Item 11 – This ITAAC should verify a design that provides adequate separation of the intake and exhaust in accordance with the design description in Tier 2 Section 9.5.8.3 A which states that the exhaust is “located appropriately away” from the intake, “thereby minimizing the chances of the turbine exhaust being drawn into the intake.” **[Confirmatory Item 9.5.8-2]**	➢ MHI provided: US-APWR DCD Revision 3 Tier 1, Section 2.6.4.1 Design Description 11 and corresponding Table 2.6.4-1, ITAAC #11 will be revised to specify that the Class 1E EPS engine air intake is “appropriately separated from the engine exhaust to minimize recirculation of exhaust gases to the air intake.”

9.5.8 GTG Combustion Air Intake, Turbine Exhaust Room Air Supply, and Air Exhaust System

➢ Major RAIs (Confirmatory Items)

RAI No.	Question	RAI Topic / NRC Concern	RAI Response / DCD Impact
754-5617	14.3.6-25	-Rev. 3 of US-APWR DCD, Table 2.6.4-1, Item 25 – This item addresses the power supply for the fuel oil transfer pumps. -There are other support system components that are also powered by the respective Class 1E division power supply, such as the ventilation/cooling supply and exhaust fans. **[Confirmatory Item 9.5.8-3]**	➢ MHI provided: US-APWR DCD Revision 3 Tier 1, Section 2.6.4.2 Design Description 25 and Table 2.6.4-1 ITAAC #25 will be revised to verify Class 1E power for Class 1E EPS ventilatoin fans.

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United States Nuclear Regulatory Commission

Protecting People and the Environment

Presentation to the ACRS Subcommittee

Mitsubishi Heavy Industries (MHI)

US-APWR Design Certification Application Review

Safety Evaluation with Open Items: Chapter 9

AUXILIARY SYSTEMS

MARCH 22-23, 2012

Staff Review Team

- **Technical Staff Presenters**
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  - Angelo Stubbs – DCD Sections 9.2.6
  - David Nold – DCD Sections 9.4.1 and 9.4.5

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- **Eugene Eagle**
  Instrumentation and Controls Branch
- **Robert Fitzpatrick**
  Instrumentation and Controls Branch

Overview of Design Certification Application, Chapter 9

SRP Section/Application Section		No. of Questions	Number of OI
9.1.1	Criticality Safety of Fresh and Spent Fuel Storage and Handling	23	0
9.1.2	New and Spent Fuel Storage	25	0
9.1.3	Spent Fuel Pool Cooling and Cleanup System	9	1
9.1.4	Light Load Handling System	23	1
9.1.5	Overhead Heavy Load Handling Systems	19	1
9.2.1	Station Service Water System	59	1

Overview of Design Certification Application, Chapter 9

SRP Section/Application Section		No. of Questions	Number of OI
9.2.2	Reactor Auxiliary Cooling Water	85	1
9.2.4	Potable and Sanitary Water Systems	3	0
9.2.5	Ultimate Heat Sink	10	0
9.2.6	Condensate Storage Facilities	3	1
9.2.7	Chilled Water System (Reviewed under 9.2.2)	0	0
9.2.8	Turbine Component Cooling Water System (Reviewed under 9.2.2)	0	0

Overview of Design Certification Application, Chapter 9

SRP Section/Application Section		No. of Questions	Number of OI
9.2.9	Non-Essential Service Water System (Reviewed under 9.2.2)	0	0
9.3.1	Compressed Air System	5	0
9.3.2	Process and Post-accident Sampling Systems	16	0
9.3.3	Equipment and Floor Drainage System	19	0
9.3.4	Chemical and Volume Control System	25	0
9.4.1	Control Room Area Ventilation System	32	4

Overview of Design Certification Application, Chapter 9

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SRP Section/Application Section		No. of Questions	Number of OI
9.4.2	Spent Fuel Pool Area Ventilation System	7	0
9.4.3	Auxiliary and Radwaste Area Ventilation System	21	5
9.4.4	Turbine Area Ventilation System	8	1
9.4.5	Engineered Safety Feature Ventilation System	22	2
9.4.6	Containment Ventilation System	21	1
9.5.1	Fire Protection Program	19	0

Overview of Design Certification Application, Chapter 9

SRP Section/Application Section		No. of Questions	Number of OI
9.5.2	Communications Systems	12	0
9.5.3	Lighting Systems	9	0
9.5.4	Emergency Diesel Engine Fuel Oil Storage and Transfer System (Reviewed under 9.5.4)	51	1
9.5.5	Emergency Diesel Engine Cooling Water System	0	0
9.5.6	Emergency Diesel Engine Starting System	25	0
9.5.7	Emergency Diesel Engine Lubrication System	24	0

Overview of Design Certification Application, Chapter 9

SRP Section/Application Section		No. of Questions	Number of OI
9.5.8	Emergency Diesel Engine Combustion Air Intake and Exhaust System	28	0
Totals		603	20

Technical Topics

Section 9.2.1 - Essential Service Water System (ESWS)

- ESWS blowdown (4 trains) and strainer backwash discharge (4 trains) connect to a common header which discharges to circulating water blowdown (AOV-577)

- Safety related to nonsafety related interface

- ESW- AOV-577 automatically closes on UHS basin low level, ESWS pump stop, ECCS actuation, and LOOP

- **Open Item x (RAI 6344)** – Provide detailed information on the four different power supplies, I&C logic related to ESWS pump stop, and completed the Failure Modes and Effects Analysis (FMEA)

Technical Topics

Section 9.2.2 - Component Cooling Water System (CCWS)

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- 420 cubic feet CCWS surge tank is shared between two CCWS trains
- Total of two CCWS surge tanks per unit
- No automatic valve isolation is provided to separate the two CCWS trains
- CCWS surge tank has 7 days of water volume (no safety related makeup required)
- CCWS is a moderate-energy system (Table 3.6-1), operating < 200 F and < 275 psig.

- **Open Item x (RAI 878-6200, Question 09.02.02-85)** – Provide details on how the CCWS is designed against postulated piping leak paths since a leak in the common CCWS pump discharge header has a potential to drain the common CCWS surge tank, affects two CCWS trains
- Staff received MHI RAI response on March 5, 2012 – response is under staff's evaluation

Technical Topics

Section 9.2.6 - Condensate Storage Facilities

- **<u>Key Design Features</u>**
  - The CSF supplies/receives condensate as required by the condenser hotwell.
  - The CSF has no safety-related functions, EFWS draws water from EFW pits.
  - The CST is a 750,000 gallon non-seismic tank which uses a non-seismic dike to mitigate the environmental effects of system leakage or storage tank failure.
- **<u>CSF Safety Evaluation Review</u>**
  - Staff reviewed design against SRP 9.2.6, and found GDC 2 and GDC 60 to be applicable to US-APWR design. (DCD Table 1.9.2 shows SRP 9.2.6 as N/A)
  - SRP 9.2.6 Section III.3.E - (1) Outdoor storage tank designed in compliance with GDC 60 and Reg Guide 1.143. (2) For a non-safety-related storage facility, the need for a seismic Category 1 dike or retention basin is reviewed.
- **<u>Open Item 9.2.6-3 – (RAI 9.2.6.3)</u>**
  - Request that the applicant provide justification for use of a non-seismic dike. Specifically the applicant is asked to discuss how the CSF design complies with GDC 2, and 60, since failure of the tank and dike could result in the release of the condensate to the environment and potential flooding.

Technical Topics

Section 9.4.1 and 9.4.5 – Control Room Area Ventilation System and Engineered Safety Feature Ventilation System

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- **Regulation**: CFR 50.63 and GDC 4

- **Concern**: Staff seeks to maintain temperatures within design limits in areas served by the MCR HVAC system (Q 09.04.01-30) and by the ESF HVAC subsystems (Q 09.04.05-22) following SBO. Assurance is provided by establishing an AAC power source to these systems within 60 minutes of SBO onset.

- **Open Items:** DCD section 9.4.1; RAI 883-6063, Question 09.04.01-30 and DCD section 9.4.5; RAI 825-5999, Question 09.04.05-22. DCD Revision 3 test criteria of DCD section 14.2.12.1.46 “Alternate AC Power Sources for Station Black Out Preoperational Test” needs further clarification to ensure it meets the intent of RG 1.155.

Technical Topics

Section 9.4.1 – Control Room Area Ventilation System

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- **Regulation:** GDC 2 and GDC 4
- **Concern**: Staff could not conclude that a internal leak within the MCR AHUs, should it occur, would not present a threat to the instrumentation and controls located in the Main Control Room below via the common HVAC duct lines (i.e. supply and return). Non safety related equipment drains route normal condensate out of the AHUs.
- **Open Item:** DCD section 9.4.1, RAI 883-6063, Q 09.04.01-32. The essential chilled water system supplies cooling water to these AHUs and is a moderate energy system. The MCR AHUs are safety-related, equipment class 3, seismic category I components. Applicant in process of formulating a response.

Figure 9.4.1-1

(back-up slide)

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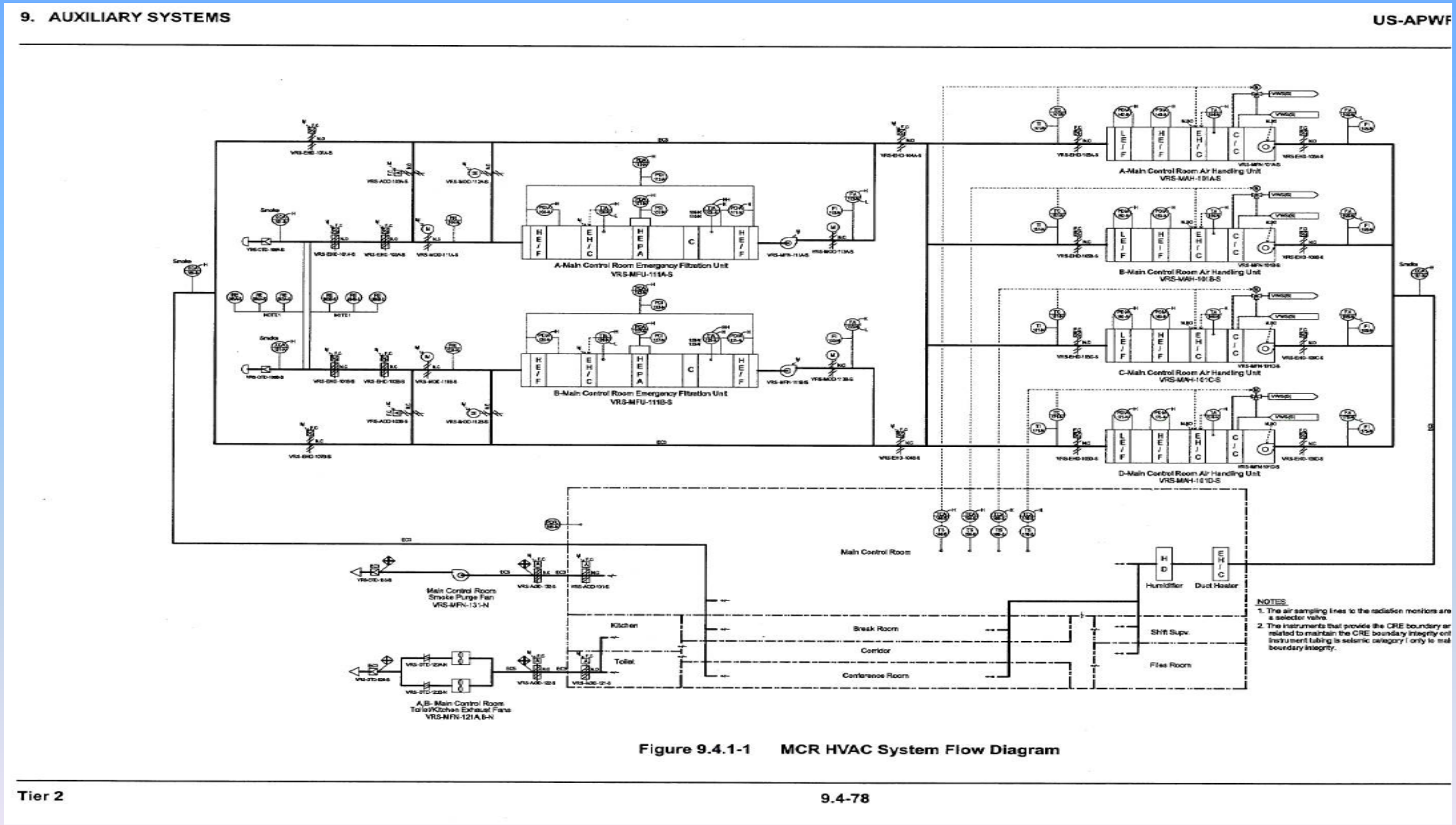


Figure 9.4.1-1 MCR HVAC System Flow Diagram

9.1.3 Spent Fuel Pit Cooling and Purification System (SFPCS)

➢ SFP water level

		Type	Set point	Interlock
DCD Rev.3	Non-safety x 2	Continuous	High	-
			Low	-
			Low-Low (*)	Pump stop
RAI 756-5753	Non-Safety x 1	Continuous	High	-
			Low	-
	Safety x 2	Level switch	Low-Low (*)	Pump stop
Open item RAI No. 735-5723	Non-Safety x 1	Continuous	High	-
			Low	-
	Safety x 2	Level switch	Low-Low (*)	Pump stop, non-seismic isolation

(*) Low-Low setpoint is above pump suction piping with adequate length to prevent vortex formation

- **SFP temperature**

		Type	Set point	Interlock
DCD Rev.3	Non-safety x 1	Continuous	High	-
RAI 756-5753	Safety x 2	Continuous	High	-

DCD Section 9.2.5.1 Design Bases

The UHS is designed with inventory sufficient to provide cooling for at least 30 days **(or at least 36 days for cooling pond in accordance with Regulatory Guide 1.27**) following an accident, with no makeup water.

RG 1.27 - 30 days supply
36 days period of time
(meteorological conditions) for spray
ponds

DCD_09.02.02-49
DCD_09.02.02-51

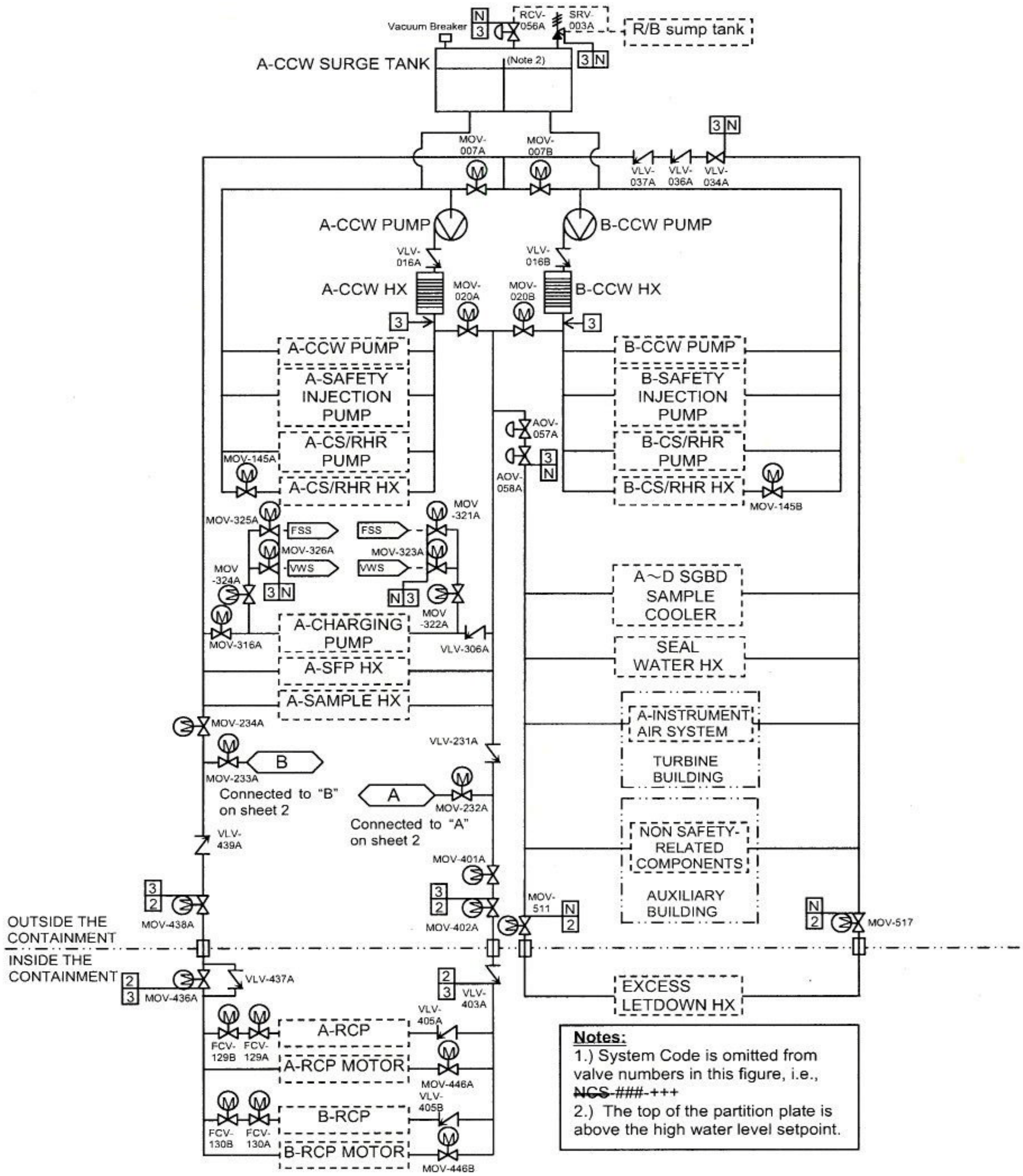
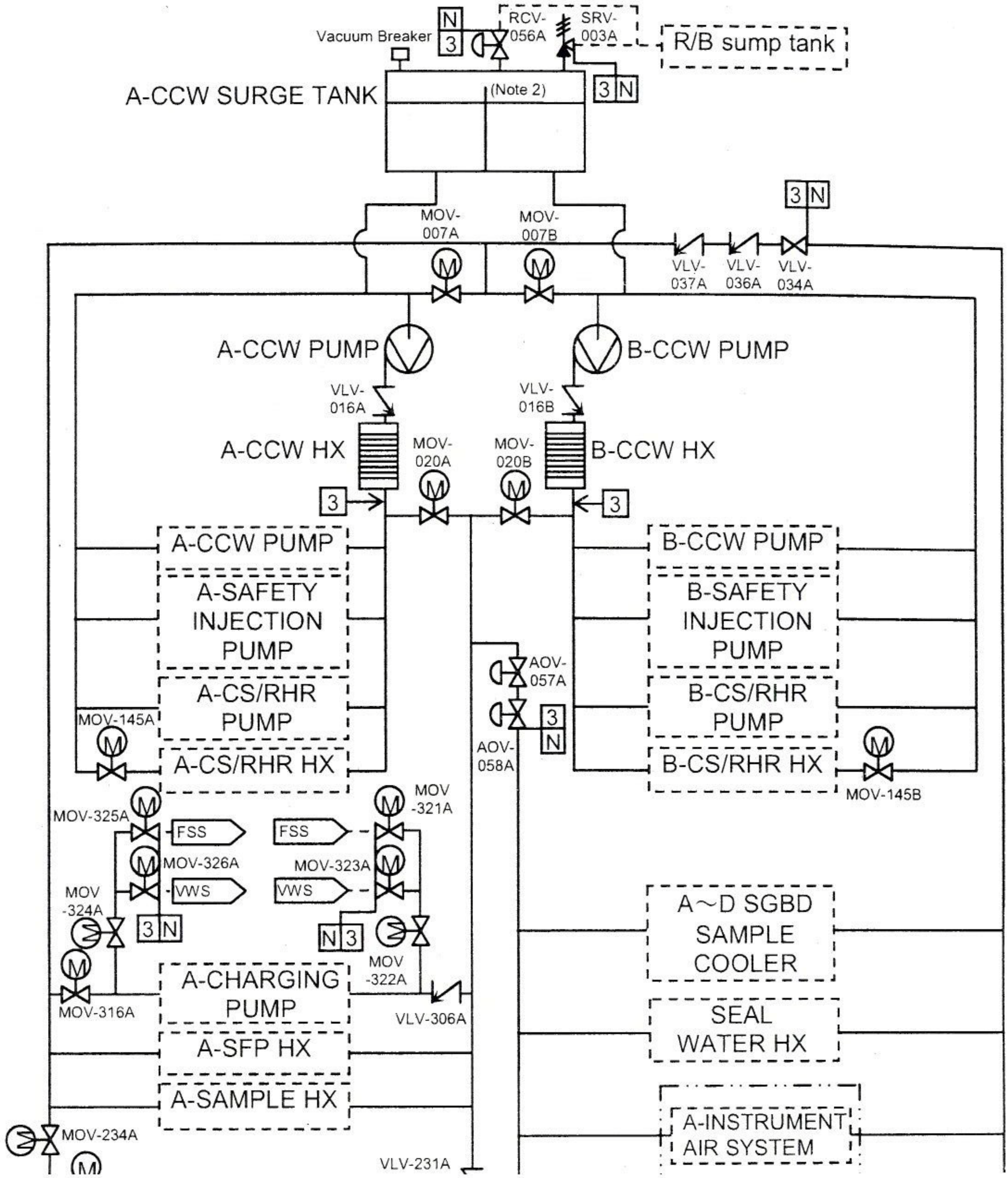


Figure 2.7.3.3-1 Component Cooling Water System (Sheet 1 of 2)



Vacuum Breaker
N
3
RCV-056A
SRV-003A
R/B sump tank
A-CCW SURGE TANK
(Note 2)
3 N
MOV-007A
MOV-007B
VLV-037A
VLV-036A
VLV-034A
A-CCW PUMP
B-CCW PUMP
VLV-016A
VLV-016B
A-CCW HX
B-CCW HX
MOV-020A
MOV-020B
3
A-CCW PUMP
B-CCW PUMP
A-SAFETY INJECTION PUMP
B-SAFETY INJECTION PUMP
AOV-057A
AOV-058A
A-CS/RHR PUMP
B-CS/RHR PUMP
MOV-145A
A-CS/RHR HX
B-CS/RHR HX
MOV-145B
MOV-325A
MOV-321A
FSS
MOV-326A
MOV-323A
VWS
MOV-324A
MOV-322A
A~D SGBD SAMPLE COOLER
MOV-316A
A-CHARGING PUMP
VLV-306A
SEAL WATER HX
A-SFP HX
A-SAMPLE HX
A-INSTRUMENT AIR SYSTEM
MOV-234A
VLV-231A

SECY-77-439

D. Passive Failure in a Fluid System
A passive failure in a fluid system means a breach in the fluid pressure boundary or a mechanical failure which adversely affects a flow path.

Examples include the failure of a simple check valve to move to its correct position when required, the leakage of fluid from failed components, such as pipes and valves--particularly through a failed seal at a valve or pump--or line blockage. Motor-operated valves which have the source of power locked out are allowed to be treated as passive components.

In the study of passive failures it is current practice to assume fluid leakage owing to gross failure of a pump or valve seal during the long term cooling mode following a LOCA (24 hours or greater after the event) but not pipe breaks.