REGULATORY INFORMATION DISTRIBUTION SYSTEM (RIDS) ACCESSION NBR:8812280112 DOC.DATE: 88/12/19 NOTARIZED: NO DOCKET # FACIL:50-263 Monticello Nuclear Generating Plant, Northern States 05000263 AUTHOR AFFILIATION AUTH.NAME MUSOLF, D. Northern States Power Co. RECIP.NAME RECIPIENT AFFILIATION Office of Nuclear Reactor Regulation, Director (Post 870411 SUBJECT: Forwards addl info re effect of DC power supply failure on I ECCS performance, per J Stefano 881128 request. DISTRIBUTION CODE: A001D COPIES RECEIVED:LTR / ENCL ( SIZE: D TITLE: OR Submittal: General Distribution S NOTES: COPIES COPIES RECIPIENT RECIPIENT LTTR ENCL ID CODE/NAME LTTR ENCL ID CODE/NAME Å PD3-1 LA 0 PD3-1 PD 2 2 1 1 STEFANO, J 1 D INTERNAL: ARM/DAF/LFMB 0 NRR/DEST/ADS 7E 1 1 1 D 1 1 NRR/DEST/CEB 8H 1 1 NRR/DEST/ESB 8D 1 1 1 1 NRR/DEST/RSB 8E NRR/DEST/MTB 9H S 1 1 NRR/DOEA/TSB 11 1 1 NRR/DEST/SICB 1 1 1 1 NUDOCS ABSTRACT NRR/PMAS/ILRB12 1 1 0 REG FILE 01 1 OGC/HDS1 1 1 RES/DSIR/EIB 1 1 1 1 NRC PDR EXTERNAL: LPDR

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10 CFR Part 50 Appendix K

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> MONTICELLO NUCLEAR GENERATING PLANT DOCKET NO. 50-263 LICENSE NO. DPR-22

Evaluation of Probability of DC Power Supply Failure Affecting ECCS Performance (TAC No. 71092)

- References: (1) Letter dated November 28, 1988 from John Stefano (NRC) to D M Musolf (NSP) concerning: "Effect of DC Power Supply Failure on Monticello ECCS Performance (TAC No. 71092)
  - (2) Letter dated October 4, 1988 from David Musolf (NSP) to the Director of NRR titled: "Effect of a DC Supply Failure on ECCS Performance"
  - (3) Letter dated October 20, 1988 from David Musolf (NSP) to the Director of NRR titled: "Additional Information concerning the Effect of a DC Supply Failure on ECCS Performance"

The purpose of this letter is to provide additional information related to the effect of a DC power supply failure on ECCS performance as requested in Reference (1). The attached report provides the analysis supporting our statement in References (2) and (3) that a coincident Loss of Coolant Accident, Loss of Offsite Power, and DC power supply failure is a low probability event. The report concludes that the total probability is approximately 7 x 10<sup>-11</sup> per year for this event.

The following related actions will also be completed:

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- 1) Submit proposed DC power supply design modification for NRC approval prior to February 15, 1989.
- 2) Install the NRC approved modification during the next refueling outage.



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**Northern States Power Company** 

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3) Perform a review of other passive electrical failures effect on LOCA analysis. This will be done as part of the Monticello Probabilistic Risk Assessment.

Please contact us if you have any questions related to this issue.

Danie Mus David Musolf

Manager Nuclear Support Services

c: Regional Administrator-II1, NRC NRR Project Manager, NRC Sr Resident Inspector, NRC G Charnoff

Attachment

Director of NRR December 19, 1988 Attachment

#### MONTICELLO NUCLEAR GENERATING PLANT

## A PROBABILITY ANALYSIS OF THE LOSS OF DC POWER SUPPLY FAILURE ON ECCS ANALYSIS

#### Large Break LOCA

Scenarios involving a loss of offsite power and additional failures are shown on Table 1 for the Large Break LOCA. Failures other than loss of 125 VDC are shown for comparison. Table 2 identifies the ECCS equipment available for each of the scenarios listed in Table 1.

Our current ECCS analysis assumed the worst single failure to be the failure of the selected injection valve to open with a loss of offsite power (Table 1 Case 3). Case Nos 9 and 12 would only have one core spray pump available. These two cases are further described below.

Case No 9 and 12 involve a large break LOCA with the loss of one division of 125 VDC bus, a loss of offsite power and Low Pressure Coolant Injection (LPCI) Loop Selection Logic selecting the loop without 125 VDC control power. In these cases, the plant would have only one low pressure pump injecting until manual action could be taken. The loss of a division's 125 VDC bus causes a loss of breaker control power to all equipment associated with that division including ability to automatically transfer the supply for that division's LPCI injection valves. If the LPCI Loop Selection logic selects the LPCI injection valve powered from the division without 125 VDC power, only one low pressure pump will be available for injection, i.e., the core spray pump powered from the division with 125 VDC power. Two RHR pumps would be available if the injection valve can be supplied with 480 V power. If the LPCI Loop Selects the LPCI injection valve powered from the division with 25 VDC power, two RHR pumps and one core spray pump will inject.

#### Probability of a Loss of Offsite Power

This analysis will consider a loss of offsite power anytime during the 24 hours following the LOCA to be of concern:

Probability of a Loss of Offsite Power per day	x	l day	=	Probability of a Loss of Offsite Power during the event
$(2.2 \times 10^{-4})$	x	1	_	$(2, 2 \times 10^{-4})$

#### Probability of a Loss of 125 VDC Power

This analysis will consider a loss of 125 VDC power anytime during the 24 hours following the LOCA to be of concern:

Probability				Probability
of a Loss of	х	l day	=	of a Loss of
125 VDC per				125 VDC Power
				during the event

 $(9 \times 10^{-4}) \times 1 \text{ day} = (9 \times 10^{-4})$ 

Case No. 9

ProbabilityProbabilityProbabilityProbabilityProbabilityof a Large xof a Loss of x of a Loss of xof Loss of xLPCI loop select-Break LOCAOffsite Power125 VDCDivision Iion logic selectper year125 VDCDivision IValve

 $(7 \times 10^{-4}) \times (2.2 \times 10^{-4}) \times (9 \times 10^{-4}) \times (0.5) \times (0.5) =$ 

 $3.5 \times 10^{-11}$  per year

Case No. 12

Probability Probability Probability Probability Probability of of a Large x of a Loss of x of a Loss of x of Loss of x LPCI loop select-Break LOCA Offsite Power 125 VDC Division II ion logic select per year 125 VDC Division II Valve  $(7 \times 10^{-4}) \times (2.2 \times 10^{-4}) \times (9 \times 10^{-4}) \times$ (0.5)x (0.5)  $3.5 \times 10^{-11}$  per year

If the break occurs in one of the recirculation loops, the LPCI loop selection logic will select the intact recirculation loop for the RHR pumps to inject into. If the break occurs outside the Recirculation System, the LPCI loop selection logic could select either loop. The factor of 0.5 accounts for the probability of the LPCI loop selection logic selecting the LPCI injection valve in the division with the loss of 125 VDC control power.

If the loss of one division's 125 VDC power occurs after the loss of offsite power, no problem will exist as the Diesel Generator supply breakers, powered from 125 VDC, will have closed and both divisions injection valves will have power. The above probability calculation does not specify the order of loss of one division's DC power and offsite power. The above calculation accounts for the possibility of loosing one division's 125 VDC power in a 24 hour period following the LOCA or having lost that division's 125 VDC power prior to the LOCA. The offsite power could have been lost anytime within the 24 hours following the LOCA. The probability calculation is conservative in this respect.

#### Core Spray Line Break

The core spray line inside the drywell is a special case as the break prevents one core spray pump from injecting into the vessel.

Scenarios of interest are shown on Table 3 for the Core Spray Line Break LOCA. Table 4 identifies the ECCS equipment available for each of the scenarios listed in Table 3. The core spray line break depressurizes the reactor in roughly 5 minutes. High Pressure Coolant Injection (HPCI) and Automatic Depressurization System (ADS) do play a role in this transient. ADS is available in all scenarios shown on Table 3, but is not listed as equipment available in Table 4 since it is available in all situations.

The availability of HPCI depends upon the availability of Division II 125 VDC.

Past LOCA sensitivities studies have shown that if 2 RHR pumps and one train of ADS are operable for a core spray line break, the peak clad temperature will not exceed 700°F. The case where one core spray pump, HPCI and one train of ADS are operable was not run by General Electric as it was considered to be bounded by the case with 2 RHR pumps and ADS available. The following cases are not bounded by past LOCA analysis: 22, 41 and 44. The probability of these cases occurring will be discussed below.

If the break occurs inside containment in core spray line of the opposite division as the loss of 125 VDC supply power, neither core spray pump would be available for low pressure injection. One core spray pump would pump to the break and the other's breaker would have no control power. If the LPCI Loop Selection logic selects the LPCI injection valve powered from the division without 125 VDC power, the RHR pumps would not be available until the swing bus could be manually transferred.

Probability of a Pipe Rupture per 10 foot section per hour	Number of Hours per year	-	Probability of a Pipe Rupture per 10 foot section per year
$(8.6 \times 10^{-10}) \times$	(6.57 x 10 <sup>3</sup> )	=	5.7 x $10^{-6}$

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Simultaneous Core Spray Line Break and Loss of Offsite Power: Probability of a Number of 10 foot Sections Probability of a Pipe Rupture per x of Core Spray Pipe between х Loss of Offsite 10 foot section The Reactor Vessel and Power the injection check valve per year in one division  $(5.7 \times 10^{-6})$ x  $(2.2 \times 10^{-4})$ х (2)  $2.5 \times 10^{-9} = P_{2}$ Case No. 22 Probability Probability of Probability of of a Loss of x Loss Division II x LPCI loop selection x  $P_a =$ 125 VDC 125 VDC logic selecting Division II valve  $(9 \times 10^{-4}) \times$ x (0.5) x  $(2.5 \times 10^{-9}) =$ (0.5) 5.6 x  $10^{-13}$  per year = P<sub>22</sub> Case No. 41 Probability Probability of Probability of x LPCI loop selection x  $P_a =$ of a Loss of x Loss Division I 125 VDC 125 VDC logic selecting Division I valve  $(9 \times 10^{-4}) \times 10^{-4}$ (0.5) x  $(2.5 \times 10^{-9})$ (0.5) х 5.6 x  $10^{-13}$  per year =  $P_{41}$ Case No. 44 Probability Probability of Probability of x Loss Division II x LPCI loop selection x  $P_a =$ of a Loss of 125 VDC 125 VDC logic selecting Division II valve  $(9 \times 10^{-4}) \times$ x (0.5) x  $(2.5 \times 10^{-9}) =$ (0.5) 5.6 x  $10^{-13}$  per year =  $P_{42}$ 

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Total Probability:

 $P_9 + P_{12} + P_{22} + P_{41} + P_{44} =$  Total Probability 3.5 x 10<sup>-11</sup> + 3.5 x 10<sup>-11</sup> + 5.6 x 10<sup>-13</sup> + 5.6 x 10<sup>-13</sup> + 5.6 x 10<sup>-13</sup> = 7.2 + 10<sup>-11</sup> per year  $\simeq$  7 x 10<sup>-11</sup> per year

This analysis was done using probabilities from the Monticello Individual Plant Evaluation (IPE) which is based on the Industry Degraded Core Rulemaking Group (IDCOR) IPE methodology. Plant specific data is used from the IPE when available. The Monticello IPE assumes one RHR pump or one core spray pump is sufficient to prevent core damage after a LOCA. This is based on General Electric Topical Report NEDO-24708.

The Monticello IPE concluded the overall core damage frequency to be 1.5E-5/year. Generally, sequences with a frequency less than 1E-7/year will not have a significant impact on the IPE results. Therefore, operation of Monticello for the next 9 months, when the plant will be modified to eliminate these scenarios, will not have a significant effect on safety.

However, in the unlikely event one of these scenarios did occur, plant procedures have been issued to restore power to the de-energized bus that supplies the LPCI injection valve. Operators have been trained in the use of these procedures.

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## LARGE BREAK LOCA RECIRCULATION SUCTION PIPE

## FAILURE COMBINATIONS CONSIDERED

Div CS <u>Pum</u>		Div II CS <u>Pump</u>		Div II <u>D/G</u>	Div I Inj <u>Valve</u>	Inj	Div I 125 <u>VDC</u>	Div II 125 <u>VDC</u>	LPCI LSL Div I <u>Valve</u>	LPCI LSL Div II <u>Valve</u>
1										
	NOT	E: THE	FOLLOWI	NG CASE	S ASSUM	E A LOSS	OF OFF:	SITE POWI	ER	
2										
3			Х							
4				Х						
5					Х				Х	
6					Х					Х
7						х			Х	
8						х				х
9							Х		Х	
10							Х			Х
11								х	Х	
12								Х		Х

NOTE: CS = Core Spray, LPCI = Low Pressure Coolant Injection LSL = Loop Selection Logic, D/G = Emergency Diesel Generator



## LARGE BREAK LOCA RECIRCULATION SUCTION PIPE EQUIPMENT AVAILABLE FOR SPECIFIC FAILURE COMBINATIONS

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Case <u>No</u>	Additional Failures	Low Pressure ECCS Equipment Available	
1	None	2 CS + 4 RHR	
2	Loss of Offsite Power	2 CS + 4 RHR	
3	Loss of Offsite Power and Loss of Div I D/G	1 CS + 2 RHR	
4	Loss of Offsite Power and Loss of Div II D/G	1 CS + 2 RHR	
	Loss of Offsite Power and Loss of Div I LPCI Injection valve and	nd:	
5	LPCI Loop selection logic selects Div I injection valve	2 CS	
6	LPCI Loop selection logic selects Div II injection valve	2 CS + 4 RHR	
	Loss of Offsite Power and Loss of Div II LPCI Injection valve an	and:	
7	LPCI Loop selection logic selects Div I injection valve	2 CS + 4 RHR	
8	LPCI Loop selection logic selects Div II injection valve	2 CS	
	Loss of Offsite Power and Loss of Div I 125 DC Power and:		
9	LPCI Loop selection logic selects Div I injection valve	1 CS	
10	LPCI Loop selection logic selects Div II injection valve	1 CS + 2 RHR	
	Loss of Offsite Power and Loss of Div II 125 DC Power and:		
11	LPCI Loop selection logic selects Div I injection valve	1 CS + 2 RHR	
12	LPCI Loop selection logic selects Div II injection valve	1 CS	

Note: CS = Core Spray Pump, RHR = Residual Heat Removal Pumps or LPCI pumps LPCI = Low Pressure Coolant Injection, D/G = Emergency Diesel Generator

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### CORE SPRAY LINE BREAK INSIDE THE DRYWELL

#### FAILURE COMBINATIONS CONSIDERED

								LPCI	LPCI
Div I	Div II			Div I	Div II	Div I	Div II	LSL	LSL
CS	CS	Div I	Div II	Inj	Inj	125	125	Div I	Div II
<u>Pump</u>	<u>Pump</u>	<u>D/G</u>	<u>D/G</u>	<u>Valve</u>	Valve	<u>VDC</u>	<u>VDC</u>	<u>Valve</u>	<u>Valve</u>

NOTE: THE FOLLOWING CASES ASSUME A DIVISION I CORE SPRAY LINE BREAK

1							
2	Х						
3		Х				х	
4		Х					Х
5			Х			х	
6			Х				Х
7				Х		х	
8				Х			Х
9					Х	х	
10					Х		Х

NOTE: THE FOLLOWING CASES ASSUME A DIVISION I CORE SPRAY LINE BREAK AND A LOSS OF OFFSITE POWER

11									
12	Х								
13		Х							
14			Х						
15				X				Х	
16				Х					х
17					Х			Х	
18					Х				х
19						Х		Х	
20						х			х
21							х	х	
22							Х		Х

NOTE: CS = Core Spray, LPCI = Low Pressure Coolant Injection LSL = Loop Selection Logic, D/G = Emergency Diesel Generator

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## CORE SPRAY LINE BREAK INSIDE THE DRYWELL

## FAILURE COMBINATIONS CONSIDERED

C	iv I S ump	Div II CS <u>Pump</u>	Div I <u>D/G</u>	Div II <u>D/G</u>	Div I Inj <u>Valve</u>	Div II Inj <u>Valve</u>	Div I 125 <u>VDC</u>	Div II 125 <u>VDC</u>	LPCI LSL Div I <u>Valve</u>	LPCI LSL Div II <u>Valve</u>
	NOTE	: THE F	OLLOWIN	G CASES	ASSUME	A DIVISI	ON II C	ORE SPRA	Y LINE	BREAK
23										
24	х									
25 26					X X				Х	v
27					Λ	х			x	х
28						Х				Х
29 30							X X		X	х
31							л	х	х	л
32								х		Х
	NOT			NG CASES OF OFFSI			ION II	CORE SPR	AY LINE	BREAK
33										
34 35	Х		v							
36			Х	x						
37					х				х	
38 39					Х					Х
39 40						X X			Х	x
41						**	х		х	л
42							Х			х
43 44								X X	х	x
					•			л		л
NOT	E: CS	= Core	Spray,	LPCI =	Low Pre	ssure Co	olant I	njection		

LSL = Loop Selection Logic, D/G = Emergency Diesel Generator

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## <u>CORE SPRAY LINE BREAK INSIDE THE DRYWELL</u> EQUIPMENT AVAILABLE FOR SPECIFIC FAILURE COMBINATIONS

Case <u>No</u>	Additional Failures <u>to a Division I Core Spray Line Break</u>	ECCS Equipment Available*
1	None	1 CS + 4 RHR + HPCI
2	Loss of Div II Core Spray Pump	4 RHR + HPCI
	Loss of Div I LPCI Injection valve and:	
3	LPCI Loop selection logic selects Div I injection valve	1 CS + HPCI
4	LPCI Loop selection logic selects Div II injection valve	1 CS + 4 RHR +HPCI
	Loss of Div II LPCI Injection valve and:	
5	LPCI Loop selection logic selects Div I injection valve	1 CS + 4 RHR + HPCI
6	LPCI Loop selection logic selects Div II injection valve	1 CS + HPCI
	Loss of Div I 125 DC Power and:	
7	LPCI Loop selection logic selects Div I injection valve	1 CS + 2 RHR + HPCI
8	LPCI Loop selection logic selects Div II injection valve	1 CS + 2 RHR + HPCI
	Loss of Div II 125 DC Power and	
9	LPCI Loop selection logic selects Div I injection valve	2 RHR
10	LPCI Loop selection logic selects Div II injection valve	2 RHR

\* ADS is not included since it will be available in all cases.

Note: CS = Core Spray Pump, RHR = Residual Heat Removal Pumps or LPCI pumps LPCI = Low Pressure Coolant Injection, D/G = Emergency Diesel Generator e 🔭

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## CORE SPRAY LINE BREAK INSIDE THE DRYWELL

Case <u>No</u>	Additional Failures <u>to a Division I Core Spray Line Break</u>	ECCS <u>Equipment Available</u>
11	Loss of Offsite Power	1 CS + 4 RHR + HPCI
12	Loss of Offsite Power and Loss of Div II Core Spray Pump	4 RHR + HPCI
.13	Loss of Offsite Power and Loss Div I D/G	1 CS + 2 RHR + HPCI
14	Loss of Offsite Power and Loss Div II D/G	2 RHR + HPCI
	Loss of Offsite Power and Loss of Div I LPCI Injection valve and:	
15 `	LPCI Loop selection logic selects Div I injection valve	1 CS + HPCI
16	LPCI Loop selection logic selects Div II injection valve	1 CS + 4 RHR + HPCI
	Loss of Offsite Power and Loss of Div II LPCI Injection valve and:	
17	LPCI Loop selection logic selects Div I injection valve	1 CS + 4 RHR + HPCI
18	LPCI Loop selection logic selects Div II injection valve	1 CS + HPCI
	Loss of Offsite Power and Loss of Div I 125 DC Power and:	
19	LPCI Loop selection logic selects Div I injection valve	1 CS + HPCI
20	LPCI Loop selection logic selects Div II injection valve	1 CS + 2 RHR + HPCI
	Loss of Offsite Power and Loss of Div II 125 DC Power and:	
21	LPCI Loop selection logic selects Div I injection valve	2 RHR
22	LPCI Loop selection logic selects Div II injection valve	None

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## Page 3

## CORE SPRAY LINE BREAK INSIDE THE DRYWELL

Case <u>No</u>	Additional Failures <u>to a Division II Core Spray Line Break</u>	ECCS <u>Equipment Available</u>
23	None	1 CS + 4 RHR + HPCI
24	Loss of Div I Core Spray Pump	4 RHR + HPCI
	Loss of Div I LPCI Injection valve and:	
25	LPCI Loop selection logic selects Div I injection valve	l CS + HPCI
26	LPCI Loop selection logic selects Div II injection valve	1 CS + 4 RHR +HPCI
	Loss of Div II LPCI Injection valve and:	
27	LPCI Loop selection logic selects Div I injection valve	l CS + 4 RHR + HPCI
28	LPCI Loop selection logic selects Div II injection valve	l CS + HPCI
	Loss of Div I 125 DC Power and:	
29	LPCI Loop selection logic selects Div I injection valve	2 RHR + HPCI
30	LPCI Loop selection logic selects Div II injection valve	2 RHR + HPCI
	Loss of Div II 125 DC Power and	
31	LPCI Loop selection logic selects Div I injection valve	1 CS + 2 RHR
32	LPCI Loop selection logic selects Div II injection valve	1 CS + 2 RHR

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## CORE SPRAY LINE BREAK INSIDE THE DRYWELL

Case <u>No</u>	Additional Failures <u>to a Division II Core Spray Line Break</u>	ECCS Equipment Available
33	Loss of Offsite Power	1 CS + 4 RHR + HPCI
34	Loss of Offsite Power and Loss of Div I Core Spray Pump	4 RHR + HPCI
35	Loss of Offsite Power and Loss Div I D/G	2 RHR + HPCI
36	Loss of Offsite Power and Loss Div II D/G	1 CS + 2 RHR + HPCI
	Loss of Offsite Power and Loss of Div I LPCI Injection valve and:	
37	LPCI Loop selection logic selects Div I injection valve	l CS + HPCI
38	LPCI Loop selection logic selects Div II injection valve	1 CS + 4 RHR + HPCI
	Loss of Offsite Power and Loss of Div II LPCI Injection valve and:	
39	LPCI Loop selection logic selects Div I injection valve	1 CS + 4 RHR + HPCI
40	LPCI Loop selection logic selects Div II injection valve	l CS + HPCI
	Loss of Offsite Power and Loss of Div I 125 DC Power and:	
41	LPCI Loop selection logic selects Div I injection valve	HPCI
42	LPCI Loop selection logic selects Div II injection valve	2 RHR + HPCI
	Loss of Offsite Power and Loss of Div II 125 DC Power and:	
43	LPCI Loop selection logic selects Div I injection valve	1 CS + 2 RHR
44	LPCI Loop selection logic selects Div II injection valve	1 CS