babcock & wilcox nuclear energy

B&W mPower™ Reactor Fuel System Mechanical Design Criteria MPWR-TECR-005012 Revision **000 9/23/2011**

(REDACTED VERSION)

B&W mPower™ Reactor Program Babcock & Wilcox Nuclear Energy, Inc. 109 Ramsey Place Lynchburg, VA 24501

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RECORD OF REVISION

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1. INTRODUCTION

The purpose of this technical report is to provide a description of the Babcock & Wilcox (B&W) mPower™ fuel system design, including key design parameters and illustrations, and to present a compilation of the fuel system design bases and criteria. A Fuel System Mechanical Design Topical report, based on the design bases and criteria contained herein, will be submitted to the NRC upon completion of the detailed analyses and testing.

Section 2 of this report describes the design of the B&W mPower fuel assembly and in-core control components. The information provided in this report represents the current design; it is expected that minor changes to the design will occur during the next two years through the fuel system development and licensing process.

Section 3 describes the fuel system mechanical design bases and criteria, with a general discussion of the approach to evaluating the design relative to the criteria.

2. **FUEL** SYSTEM **DESIGN** SUMMARY

The B&W mPower fuel assembly has been designed specifically for use with the core configuration of the B&W mPower reactor. The key fuel assembly parameters are listed in Table 2.0-1. Figure 2.0-1 shows a cross-section of the fuel assembly array, and Figure 2.0-2 provides a fuel assembly full-length view.

The 17x17 fuel assembly consists of **[**

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Affidavit 4(a)-(d)]

2.1 Fuel Rods

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2.2 Burnable Poison Rods

Supplementary reactivity control is provided by non-integral burnable poison rods (BPRs). [

] [CCI per Affidavit 4(a)-(d)]

2.3 Fuel Assembly Structure

The fuel assembly structural skeleton consists of the upper end fitting and the cage assembly. The fuel assembly cage, shown in Figure 2.3-1, includes the lower end fitting, the control rod guide tubes, and the spacer grids.

2.3.1 Lower End Fitting

A schematic view of the lower end fitting is provided in Figure 2.3.1-1.

] **[CCI** per Affidavit 4(a)-(d)]

2.3.2 Upper End Fitting

The upper end fitting is the uppermost structural component of the fuel assembly. [

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] [CCI per Affidavit 4(a)-(d)]

2.3.3 Control Rod Guide Tube Assembly

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2.3.4 Grid Assemblies

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2.4 In-core Control Components

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2.4.1 Control Rod Assemblies

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2.4.2 Neutron Source Rods

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Table 2.0-1 B&W mPower Fuel Assembly Design Summary

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Table 2.0-1 B&W mPower Fuel Assembly Design Summary (continued)

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Table 2.4.1-1 B&W mPower Control Rod Assembly Design Summary

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Table 2.4.2-1 B&W mPower Neutron Source Rod Design Summary

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Figure 2.0-1 Fuel Assembly Cross-Section

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Figure 2.0-2 Fuel Assembly Full-Length View

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Figure 2.1-1 Fuel Rod Schematic

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Figure 2.2-1 Burnable Poison Rod

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Figure 2.3.1-1 Lower End Fitting

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[CCI per Affidavit 4(a)-(d)]

Figure 2.3.1-2 Control Rod Guide Tube Assembly to LEF Joint

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[CCI per Affidavit 4(a)-(d)]

Figure 2.3.2-1 Upper End Fitting

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Figure 2.3.3-1 Control Rod Guide Tube Assembly

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Figure 2.3.3-2 Constraint Design for End Grids on Control Rod Guide Tubes

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Figure 2.3.3-3 Constraint Design for Mid Grids on Control Rod Guide Tubes

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Figure 2.3.4-1 End Grid

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Figure 2.3.4-2 Intermediate Spacer Grid

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Figure 2.4.1-2 Control Rod

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[CCI per Affidavit 4(a)-(d)]

Figure 2.4.1-3 Spider Assembly

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Figure 2.4.1-4 Type 2 Control Rod Assembly

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Figure 2.4.1-5 Hybrid Control Rod

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Figure 2.4.2-1 Primary Neutron Source Rod

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Figure 2.4.2-2 Secondary Neutron Source Rod

3. FUEL SYSTEM DESIGN BASES AND CRITERIA

3.1 Fuel System Desiqn Bases Summary

3.1.1 Design Requirements

Design requirements for the fuel system are described in the NRC Standard Review Plan (SRP) 4.2 (NUREG-0800) (Reference 4.1). These requirements are in compliance with General Design Criteria (GDC) 10, 27 and 35 of 10 CFR Part 50 Appendix A (Reference 4.2), 10 CFR Part 50.46 (Reference 4.3) and 10 CFR Part 100 (Reference 4.4). The requirements are also consistent with Section 4.2 of Regulatory Guide 1.70 (Reference 4.5) and with Section C.1.4.2 of Regulatory Guide 1.206 (Reference 4.6).

The design basis objectives of the fuel system are to ensure that:

- (a) the fuel system is not damaged as a result of normal operation or anticipated operational occurrences (AOOs);
- (b) fuel system damage is never so severe as to prevent control rod insertion when it is required:
- (c) the number of fuel rod failures is not underestimated for postulated accidents (PAs); and
- (d) core coolability is always maintained.

GDC 10 (Reactor design), within Appendix A to 10 CFR Part 50, addresses item (a) above: "The reactor core and associated coolant, control, and protection systems shall be designed with appropriate margins to ensure that specified acceptable fuel design limits are not exceeded during any condition of normal operation, including the effects of anticipated operational occurrences." Specifically, GDC 10 establishes Specified Acceptable Fuel Design Limits (SAFDLs) to ensure that the fuel system is not damaged.

With respect to the fuel system design, "not damaged" means that fuel rods do not fail, that the fuel system remains within operational tolerances, and that the functional capabilities are not reduced below those assumed in the safety analysis.

"Fuel rod failure" means that the fuel rod leaks and that the first fission product barrier (the cladding) has been breached. This criterion relates to 10 CFR Part 100, dose analysis.

"Coolability" means that the fuel assembly retains its rod-bundle geometry with adequate coolant flow passages (channels) to permit removal of residual heat even after a severe accident.

General requirements to maintain control rod insertability and core coolability appear repeatedly in GDC 27 (Combined reactivity control systems capability) and GDC 35 (Emergency core cooling). Specific coolability requirements for the loss-of-coolant accident (LOCA) are provided in 10 CFR Part 50.46.

To address these requirements, design criteria for the fuel system are categorized with respect to:

- (A) fuel system damage
- (B) fuel rod and burnable poison rod failure
- (C) fuel coolability

The complete set of design criteria required in SRP 4.2 (Reference 4.1) are listed in Table 3.1.1-1 to Table 3.1.1-3. Criteria related to fuel system damage and their applicability to fuel system components are summarized in Table 3.1.1-1. Criteria related to the failure of fuel rods and burnable poison rods are summarized in Table 3.1.1-2. Criteria related for fuel coolability and their applicability to fuel system components are summarized in Table 3.1.1 **-** 3.

Section 3.2 of this report presents a review of the B&W mPower fuel rod and fuel assembly design bases and criteria. It is noted that for some requirements related to postulated accidents, the Design Control Document (DCD) is referenced for the detailed discussion of the requirement.

3.1.2 Plant Conditions for Fuel System Design

Plant conditions for fuel assembly design are categorized according to expected frequency of occurrence and by type, as follows:

- (1) Normal operation (NO)
- (2) Anticipated Operational Occurrences (AOOs)
- (3) Postulated Accidents (PAs)

Normal operation typically includes the following events that are expected frequently or are performed regularly in the course of power operation, refueling, maintenance, and maneuvering of the plant (Reference 4.7):

Startup Shutdown (hot and cold) Refueling Hot standby Power operation Operational maneuvers Plant heatup and cooldown

Load change

Operation with permissible deviations

Anticipated operational occurrences, as defined in 10 CFR Part 50, Appendix A, are those conditions of operation that are expected to occur one or more times during the life of the nuclear plant. Postulated accidents are unanticipated occurrences. That is, they are postulated but are not expected to occur during the life of the nuclear power plant.

Analyses of AQOs and PAs are categorized according to type so that analysts can compare them on common bases, effect, and safety limits. Such comparisons can help to identify limiting event and cases for detailed examination, and eliminate non-limiting cases from further consideration.

AOOs and PAs are grouped into the following seven types (Reference 4.7):

- (1) Increase in heat removal by the secondary system
- (2) Decrease in heat removal by the secondary system
- (3) Decrease in reactor cooling system (RCS) flow rate
- (4) Reactivity and power distribution anomalies
- (5) Increase in reactor coolant inventory
- (6) Decrease in reactor coolant inventory
- (7) Radioactive release from a component or subsystem

The events for AOOs and PAs for the B&W mPower plant will be categorized in Chapter 15 (Transient and Accident Analysis) of the DCD to specify the limiting event for fuel system integrity.

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Table **3.1.1-1** Criteria for Fuel System Damage

[CCI per Affidavit 4(a)-(d)] **I**

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Table **3.1.1-2** Criteria for Fuel Rod and Burnable Poison Rod Failure

[CCI per Affidavit 4(a)-(d)]

Table **3.1.1-3** Criteria for Fuel Coolability

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3.2 Design Criteria and Methodology for Evaluating Fuel System Damage

Fuel system damage requirements apply to normal operation and AOOs. To meet the requirements of GDC 10 as it relates to SAFDLs for normal operation, including AQOs, fuel system damage criteria are specified for all known damage mechanisms.

Fuel damage criteria ensure that fuel system dimensions remain within operational tolerances and that functional capabilities are not reduced below those assumed in the safety analysis. When applicable, the fuel damage criteria consider high burnup effects based on irradiated material properties.

- 3.2.1 Cladding Stress
- (1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

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(3) Design Evaluation

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Rev. No. Document No. Title B&W mPower™ Reactor Fuel System Mechanical Design **MPWR-TECR-**000 005012 Criteria

- 3.2.2 Cladding Strain
- (1) Design Basis
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- (2) Design Criteria
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] [CCI per Affidavit 4(a)-(d)]

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- (3) Design Evaluation
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3.2.3 Stress and Loading Limit for Other than Cladding

3.2.3.1 Loads Applied by Core Restraint System

(1) Design Basis

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4(a)-(d)]

(2) Design Criteria

The design criteria associated with loads applied by the core restraint system are:

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(3) Design Evaluation

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3.2.3.2 Loads Applied in Fuel Handling and Shipping

- (1) Design Basis
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[CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

The design criteria associated with loads applied during shipping and handling are:

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] [CCI per

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(3) Design Evaluation

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3.2.4 Cladding Fatigue

(1) Design Basis

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(2) Design Criteria

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- (3) Design Evaluation
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3.2.5 Fretting Wear

(1) Design Basis

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(2) Design Criteria

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(3) Design Evaluation

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- (3) Design Evaluation
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] [CCI per Affidavit 4(a)-(d)]

3.2.7.3 Rod Bowing

- (1) Design Basis
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] [CCI per Affidavit 4(a)-(d)]

- (2) Design Criteria
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[CCI per Affidavit 4(a)-(d)]

- (3) Design Evaluation
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] [CCI per Affidavit 4(a)-(d)]

3.2.7.4 Dimensional Stability of Spacer Grids

(1) Design Basis

[To maintain sufficient restraint on the fuel rods and burnable poison rods during irradiation, and during loading and unloading operations for fuel assemblies, the spacer grids are designed to maintain dimensional stability during irradiation.] [CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

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(3) Design Evaluation

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] [CCI per Affidavit 4(a)-(d)]

3.2.8 Rod Internal Pressure

(1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

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(3) Design Evaluation

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] [CCI per

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3.2.9 Assembly Liftoff

(1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

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] [CCI per Affidavit

4(a)-(d)]

(3) Design Evaluation

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3.3 Design Criteria and Methodology for Evaluating Fuel Rod and BPR Failure

Fuel rod failure and burnable poison rod failure apply to normal operation, AOOs, and postulated accidents. Fuel rod and burnable poison rod failure is defined as the loss of rod hermeticity. **[**

] **[CCI**

] [CCI per Affidavit

The fuel rod and burnable poison rod failure criteria to be applied to the B&W mPower fuel system design are defined below.

4(a)-(d)]

3.3.1 Hydriding (1) Design Basis \overline{a}] [CCI per Affidavit 4(a)-(d)] (2) Design Criteria \mathbf{r} **]** [CCI per Affidavit 4(a)-(d)] (3) Design Evaluation **I]** [CCI per Affidavit 4(a)-(d)] 3.3.2 Cladding Collapse (1) Design Basis \mathbf{r} **]** [CCI per Affidavit 4(a)-(d)] (2) Design Criteria

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] [CCI per Affidavit 4(a)-(d)]

- (2) Design Criteria
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] [CCI per Affidavit 4(a)-(d)]

- (3) Design Evaluation
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Affidavit 4(a)-(d)] **]** [CCI per

3.3.5 Excessive Fuel Enthalpy

(1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

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(2) Design Criteria

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] [CCI per Affidavit 4(a)-(d)]

(3) Design Evaluation

The detailed evaluation of this criterion is discussed in Chapter 15 (Transient and Accident Analysis) of the DCD. **[**

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[CCI per Affidavit 4(a)-(d)]

3.3.6 Pellet-Cladding Interaction (PCI)

(1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

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] [CCI per Affidavit 4(a)-(d)]

(3) Design Evaluation

The methodology for the cladding strain evaluation is described in Section 3.2.2, and that for fuel pellet and burnable poison pellet centerline melting is described in Section 3.3.4.

3.3.7 Bursting

- (1) Design Basis
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] [CCI per Affidavit 4(a)-(d)]

- (2) Design Criteria
- **I**
- **I** [CCI per Affidavit 4(a)-(d)]
- (3) Design Evaluation
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] [CCI per Affidavit 4(a)-(d)]

The details of this evaluation are discussed in Chapter 15 (Transient and Accident Analysis) of the DCD.

- 3.3.8 Fuel Rod Mechanical Fracturing
- (1) Design Basis
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- (2) Design Criteria
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] **[CCI** per Affidavit

(3) Design Evaluation

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] [CCI per Affidavit 4(a)-(d)]

3.4 Design Criteria and Methodology for Evaluating Fuel Coolability

Coolability, or coolable geometry, implies that the fuel assembly retains its rod-bundle geometry with adequate coolant channels to permit removal of residual heat. Reduction of coolability can result from cladding embrittlement, violent expulsion of fuel, generalized cladding melting, gross structural deformation, and extreme coplanar fuel rod ballooning.

The fuel coolability criteria described below are applied to the analysis of postulated accidents. The details of the evaluations and analyses performed to assess these are presented in Chapter 15 (Transient and Accident Analysis) of the DCD.

- 3.4.1 Cladding Embrittlement
- (1) Design Basis

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] [CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

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[CCI per Affidavit 4(a)-(d)]

(3) Design Evaluation

The detailed evaluation of the design criteria for cladding embrittlement is discussed in Chapter 15 (Transient and Accident Analysis) of the DCD.

- 3.4.2 Violent Expulsion of Fuel
- (1) Design Basis
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] [CCI per Affidavit 4(a)-(d)]

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- (2) Design Criteria
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] **[CCI** per Affidavit 4(a)-(d)]

(3) Design Evaluation

The detailed evaluation is discussed in Chapter 15 (Transient and Accident Analysis) of the DCD.

3.4.3 Generalized Cladding Melting

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] [CCI per Affidavit 4(a)-(d)]

3.4.4 Fuel Rod Cladding Ballooning

(1) Design Basis

[The fuel assemblies are designed such that fuel rod and burnable poison rod cladding ballooning does not preclude core coolability under postulated accident conditions.] **[CCI** per Affidavit 4(a)-(d)]

(2) Design Criteria

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] [CCI per Affidavit 4(a)-(d)]

(3) Design Evaluation

In Chapter 15 (Transient and Accident Analysis) of the DCD, burst strain and flow blockage of Zircaloy-4 cladding are properly taken into account in the LOCA evaluation.

The possibility of DNB propagation is assessed in the non-LOCA evaluation.

- 3.4.5 Structural Deformation
- (1) Design Basis
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[CCI per Affidavit 4(a)-(d)]

(2) Design Criteria

Under combined SSE and LOCA event loads:

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(3) Design Evaluation

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4. References

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