

PMSTPCOL PEmails

From: STPCOL
Sent: Wednesday, September 28, 2011 4:50 PM
To: PMSTPCOL PEmails
Subject: FW: Transmittal of Letter U7-C-NINA-NRC-110116
Attachments: U7-C-NINA-NRC-110116.pdf

From: Tai, Tom
Sent: Tuesday, September 13, 2011 9:06 AM
To: Chakrabarti, Samir
Cc: Chakravorty, Manas; Thomas, Brian; STPCOL; Wunder, George
Subject: FW: Transmittal of Letter U7-C-NINA-NRC-110116

Samir,

Attached for your review are supplemental responses to RAI 03.08.04-30 (Supplement 6) and 03.08.04-34 (Supplement 1), including FSAR markup.

03.08.04-30 S6 addresses punch-list items 110 and 122, with markup to Table 3H.6-6 and Figures 3H.6-212, -213, and -248.

03.08.04-34 S1 addresses punch-list item 56. FSAR markup include:

Sections (3H.6.6.3.1 and 3H.7.5.3.1);
Tables (3H.6-7, 3H.6-8, 3H.6-9, and 3H.7-1), and
Figures (3H.6-51, 3H.6-54 to 3H.6-74 and -74A, 3H.6-75 to 3H.6-78 and -78A, 3H.6-116 and -116A, 3H.6-117 to 3H.6-120 and -120A, 3H.6-121 to 3H.6-122 and -122A, 3H.6-123 to 3H.6-126 and 126A, 3H.6-127 to 3H.6-134 and 134A, 3H.6-135 to 3H.6-136A, -136B, and -136C) in the FSAR are also revised.

Regards

Tom Tai
DNRL/NRO
(301) 415-8484
Tom.Tai@NRC.GOV

From: Elton, Loree [<mailto:leelton@STPEGS.COM>]
Sent: Tuesday, September 13, 2011 8:20 AM
To: Muniz, Adrian; Casto, Chuck; Wunder, George; Tonacci, Mark; Eudy, Michael; Anand, Raj; Foster, Rocky; Joseph, Stacy; Govan, Tekia; Tai, Tom
Subject: Transmittal of Letter U7-C-NINA-NRC-110116

Please find attached a courtesy copy of letter number U7-C-NINA-NRC-110116 which provides supplemental responses to NRC Request for Additional Information (RAI) Questions 03.08.04-30 and 03.08.04-34 related to the Combined License Application (COLA) Part 2, Tier 2, Section 3.8.

Note that the attachment has been compressed in .zip format in order to meet NRC incoming e-mail size limitations.

The official version of this correspondence will be placed in the mail. Please call John Price at 972-754-8221 if you have any questions concerning this letter.

Loree Elton
Licensing, STP 3 & 4
leelton@stpegs.com
361-972-4644

Hearing Identifier: SouthTexas34Public_EX
Email Number: 3082

Mail Envelope Properties (377CB97DD54F0F4FAAC7E9FD88BCA6D0805095FB12)

Subject: FW: Transmittal of Letter U7-C-NINA-NRC-110116
Sent Date: 9/28/2011 4:49:44 PM
Received Date: 9/28/2011 4:50:30 PM
From: STPCOL

Created By: STP.COL@nrc.gov

Recipients:
"PMSTPCOL PEmails" <PMSTPCOL.PEmails@nrc.gov>
Tracking Status: None

Post Office: HQCLSTR01.nrc.gov

Files	Size	Date & Time
MESSAGE	2068	9/28/2011 4:50:30 PM
U7-C-NINA-NRC-110116.pdf	6536563	

Options
Priority: Standard
Return Notification: No
Reply Requested: No
Sensitivity: Normal
Expiration Date:
Recipients Received:



Nuclear Innovation
North America LLC
4000 Avenue F, Suite A
Bay City, Texas 77414

September 12, 2011
U7-C-NINA-NRC-110116

U. S. Nuclear Regulatory Commission
Attention: Document Control Desk
One White Flint North
11555 Rockville Pike
Rockville MD 20852-2738

South Texas Project
Units 3 and 4
Docket Nos. 52-012 and 52-013
Supplemental Response to Request for Additional Information

Attached are Nuclear Innovation North America LLC (NINA) supplemental responses to NRC Request for Additional Information (RAI) Questions 03.08.04-30 and 03.08.04-34 related to the Combined License Application (COLA) Part 2, Tier 2, Section 3.8.

Where there are COLA markups, they will be made at the first routine COLA update following NRC acceptance of the RAI response.

There are no commitments in this letter.

If you have any questions regarding these responses, please contact me at (361) 972-7136 or Bill Mookhoek at (361) 972-7274.

I declare under penalty of perjury that the foregoing is true and correct.

Executed on 9/12/11

Scott Head
Manager, Regulatory Affairs
South Texas Project Units 3 & 4

jep

Attachments:

1. RAI 03.08.04-30, Supplement 6
2. RAI 03.08.04-34, Supplement 1

cc: w/o attachment except*
(paper copy)

(electronic copy)

Director, Office of New Reactors
U. S. Nuclear Regulatory Commission
One White Flint North
11555 Rockville Pike
Rockville, MD 20852-2738

*George F. Wunder
*Tom Tai
Charles Casto
U. S. Nuclear Regulatory Commission

Regional Administrator, Region IV
U. S. Nuclear Regulatory Commission
611 Ryan Plaza Drive, Suite 400
Arlington, Texas 76011-8064

Jamey Seely
Nuclear Innovation North America

Peter G. Nemeth
Crain, Caton and James, P.C.

Kathy C. Perkins, RN, MBA
Assistant Commissioner
Division for Regulatory Services
Texas Department of State Health Services
P. O. Box 149347
Austin, Texas 78714-9347

Richard Peña
Kevin Pollo
L. D. Blaylock
CPS Energy

Alice Hamilton Rogers, P.E.
Inspection Unit Manager
Texas Department of State Health Services
P. O. Box 149347
Austin, Texas 78714-9347

*Steven P. Frantz, Esquire
A. H. Gutterman, Esquire
Morgan, Lewis & Bockius LLP
1111 Pennsylvania Ave. NW
Washington D.C. 20004

*Tom Tai
Two White Flint North
11545 Rockville Pike
Rockville, MD 20852

RAI 03.08.04-30, Supplement 6**QUESTION:****Follow-up to Question 03.08.04-23**

In response to staff question requesting additional information (Letter U7-C-STP-NRC-100036, dated February 10, 2010) about how various steel and concrete elements of site-specific structures are designed, and the design results, the applicant provided some analysis and design information. The applicant also referred to the Supplement 2 response to Question 03.07.01-13 (Letter U7-C-STP-NRC-090230, dated 12/30/09) for pertinent design summary information. In order for the staff to conclude that the design of site-specific structures meet the requirements of GDC 2 by meeting the guidance provided in SRP 3.8.4 and 3.8.5, or otherwise, the applicant is requested to provide the following additional information:

1. The applicant states in the response that a three dimensional finite element analysis (FEA) is used for structural analysis and design of the UHS/RSW Pump House. FSAR Section 3H.6.6.1 states that analysis for the seismic loads was performed using equivalent static loads and the induced forces due to X, Y, and Z seismic excitations were combined using the SRSS method of combination. However, the applicant did not describe how the equivalent static loads due to seismic excitation were determined and applied to the static FEA model from the results of soil structure interaction (SSI) analysis used for determination of seismic response. Therefore, the applicant is requested to provide details of how seismic response analysis results from dynamic SSI analysis were transferred to the static FEA model, including how the effects of accidental torsion were included in the analysis and design of UHS/RSW Pump house. Please also update FSAR with the information, as appropriate.
2. The applicant stated in its response that the modulus of subgrade reaction for static loading was calculated as the average of the local values at nine locations under the foundation. The applicant is requested to provide these nine values, and explain why it is considered appropriate to use the average value. Please also explain how the foundation subgrade modulus was used for calculating nodal springs for the FEA model, and how the effect due to coupling of soil springs was considered in the analysis.
3. For seismic loading, the applicant has outlined a hand-calculated procedure that utilizes published formulas and charts to estimate the foundation spring constants. According to this procedure, the equivalent modulus and Poisson's ratio of a layered soil system are first estimated using the cumulative strain energy method. The resulting values are then used in the equations for computation of the spring constants for a rigid foundation of an arbitrary shape embedded in a uniform half-space. The shear moduli used for individual layers are strain compatible values, and include the mean, upper bound, and lower bound soil cases. The approximate procedure outlined above for developing the foundation spring constants does not take into account the pressure distribution under the base slab. Furthermore, this procedure does not account for the

frequency dependence of these springs. As such, the applicant is requested to provide a justification for not considering the effects of pressure distribution and system frequency in developing the foundation dynamic springs including describing the impact on the calculated results.

4. The applicant's response does not provide details as to how the soil springs calculated under static and seismic loadings are inputted to the 3-D static FEA model to calculate the design stresses. Therefore, the applicant is requested to describe in detail how the static and seismic soil springs are inputted into the FEA model, and how the results are obtained for stress evaluations. Specifically, the applicant is requested to explain if the two sets of springs were used in a single model, and how the two sets were combined to a single set of springs. Otherwise, if the two sets of springs were applied to separate FEA models, describe how the load combinations were performed. The applicant is also requested to provide sufficient detail to assist staff in understanding how static and seismic soil springs are used in the FEA model and results combined for stress evaluations.
5. In the FSAR mark-up of Sections 3H.6.6.3.1 and 3H.6.6.3.2 provided with the response, the applicant identifies the method used by the applicant for combining forces and moments. In this method, for each reinforcing zone, the maximum force or moment is coupled with the corresponding moment or force for design for the same load combination. It is not clear if this method of combining forces and moments for design will envelop the worst combination of forces and moments for all elements in a reinforcing zone. Therefore, the applicant is requested to describe the method of combining forces and moments used by the applicant with a typical example of a reinforcing zone, and demonstrate that this method of combination will yield the worst combination of forces and moments that should be considered for design.
6. The staff notes that in the FSAR mark-up of Section 3H.6.6.3.1 provided with the response, the reported values of soil springs for the RSW Pump House are significantly larger than those for the UHS basin. The applicant is requested to confirm these values, and explain the reason for the large difference.
7. The response did not include any information about the maximum static and dynamic bearing pressures under the foundations of UHS/RSW Pump House. The applicant is requested to provide the maximum static and dynamic bearing pressure under the foundations of UHS/RSW Pump House, compare these values with the maximum allowable static and dynamic bearing pressures, and include this information in the FSAR.
8. In its response to Question 03.07.01-19 (letter U7-C-STP-NRC-100129, dated June 7, 2010), the applicant provided analysis and design information for the seismic category I Diesel Generator Fuel Oil Storage Vault (DGFOSV) which was not previously included in the FSAR. The information included in the response does not describe how structural analysis and design of the structure was performed. Also, reference is made to FSAR

Section 3H.6.4 for design loads. FSAR Section 3H.6.4 has been updated several times in various responses, and it is not clear where this information can be found. Therefore, the applicant is requested to provide complete structural analysis and design information for the DGFOV to ensure it meets acceptance criteria 1 through 7 of SRP 3.8.4 and 3.8.5. The staff needs this information to conclude that the DGFOV is designed to withstand seismic loads and meet GDC 2. Include in the response an updated version of Appendix 3H where structural analysis and design information for all seismic category I structures can be found.

9. While reviewing this response, and other responses referenced in this response, the staff noted that the applicant has used different values of coefficient of friction for sliding stability evaluation; e.g., the value 0.3 was used for the RSW Pump House, 0.4 was used for UHS basin, 0.58 was used DGFOV, and for the Reactor Building (RB) and the Control Building (CB), it was stated to be more than 0.47. It is not clear if these values are the required coefficient of friction, or the minimum coefficient of friction available. The applicant is requested to clearly specify the minimum coefficient of friction at various locations of the site, if they are different, and explain how these values were determined. Please also clarify this information in the FSAR.
10. The staff noted references to Diesel Generator Fuel Oil Tunnel (DGFOT) in several RAI responses. Please confirm that DGFOT is not a seismic category I structure, and if it is seismic category I, include the analysis and design information to show how the design of the DGFOT meets the acceptance criteria 1 through 7 in the SRP 3.8.4 and 3.8.5 in the FSAR.

SUPPLEMENTAL RESPONSE:

The Supplement 5 response to this RAI was submitted with Nuclear Innovation North America (NINA) letter U7-C-NINA-NRC-110099, dated July 12, 2011. This supplement provides the response to the following action items discussed in the NRC audits performed during the weeks of May 23, 2011 and July 25, 2011.

Punch List Item 110

From the July 12, 2011 submittal in NINA letter 110099 (RAI 03.08.04-30):

- (a) Table 3H.6-6, "Results of RSW Piping Tunnel Design", discuss the small differences between Required vs. Provided Reinforcement (0.7 versus 0.79 or 0.97 versus 1.00) or non-existent (1.56 for both).*
- (b) Check see if Note 3 in Table 3H.6-6 is clear as written.*
- (c) Determine if there is a sketch defining the reinforcing zones in the RSWPT*
- (d) In Figure 3H.6-247, is the passive pressure shown applicable to the entire RSWPT design?*

Punch List Item 122

Provide SSI soil pressures for the RSW Tunnel

Response to Punch List Item 110:

Part a) In all cases the provided reinforcement equals or exceeds the required reinforcement. This meets the code requirements. Also, in determining the required reinforcement for RSW Piping Tunnel shown in Table 3H.6-6, in order to provide additional margin, the calculated moments and axial forces were divided by 0.9 (i.e. increased by $1/0.9 = 1.11$). Therefore, as a minimum a margin of 11% is available.

Part b) The notes of Table 3H.6-6 will be revised to further clarify this table (see Enclosure).

Part c) Figure 3H.6-248 (see Enclosure) provides the RSW Piping Tunnel layout and reinforcement zones.

Part d) The passive pressure shown in Figure 3H.6-247 is applicable to the entire RSW Piping Tunnel design (i.e. main tunnel segments, north portion, and access regions 1, 2, and 3)

Response to Punch List Item 122:

Figures 03.08.04-30 S6.1 and 03.08.04-30 S6.2 provide SSI and SSSI soil pressures on RSW Piping Tunnel east and west walls, respectively. Also shown in these figures are the seismic soil pressures used for the design of these walls. As shown in these figures, the seismic soil pressures used for design envelope all SSI and SSSI soil pressures except for a small portion along the wall height where SSI soil pressure from separated soil case is higher. The tunnel wall design was controlled by passive pressure. Based on the following this local exceedance is found acceptable.

Due to total out-of-plane load including SSI soil pressure from separated soil case:

Maximum calculated out-of-plane shear, $V1 = 28.07$ kips/ft

Maximum calculated out-of-plane moment, $M1 = 124.53$ kips-ft/ft

Due to controlling total out-of-plane load:

Calculated out-of-plane shear, $V2 = 36.52$ kips/ft

Calculated out-of-plane moment, $M2 = 226.78$ kips-ft/ft

As shown above, $V1 = 28.07$ kips/ft is less than $V2 = 36.52$ kips/ft and $M1 = 124.53$ kips-ft/ft is less than $M2 = 226.78$ kips-ft/ft. Thus, the design is conservative for separated soil case.

As a result of this response COLA Part 2, Tier 2, Appendix 3H will be revised as shown in the Enclosure.

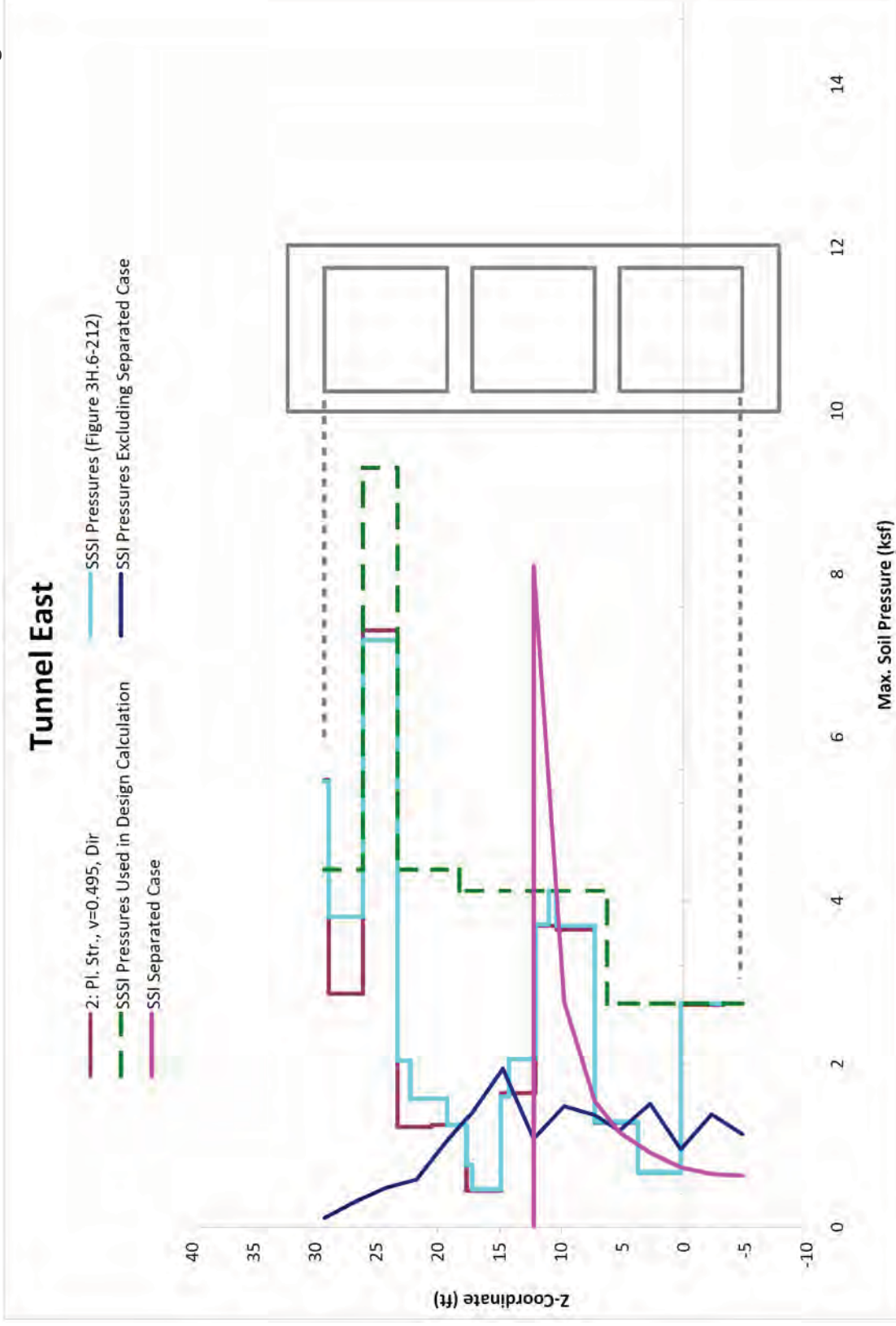


Figure 03.08.04-30 S6.1

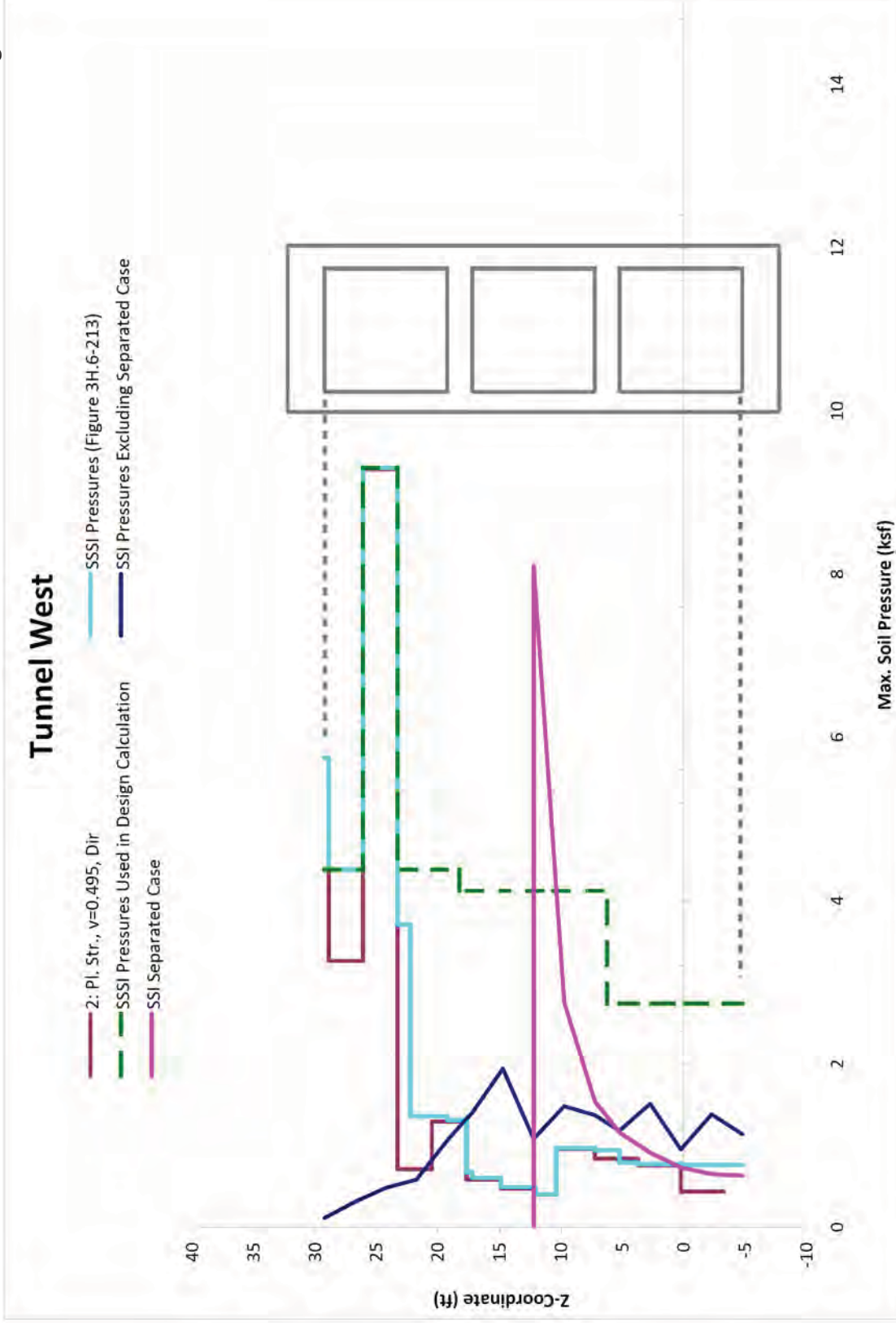


Figure 03.08.04-30 S6.2

Enclosure 1
COLA MARK-UPS

Table 3H.6-6: Results of RSW Piping Tunnel Design

Location Location ⁽⁴⁾	Item	Thickness (ft)	Governing Load Combination	Design Moment (kip-ft/ft)	Design Shear (kip/ft)	Area of Reinforcement (in ² /ft)		
						Moment Reinforcement ⁽¹⁾		Shear Reinforcement
						Required	Provided (both faces)	Required
Main Tunnel	Exterior Wall	3'-0"	D+Lo+F+H'+E'	226.78	36.52	1.56 (vertical)	1.56 (vertical)	None
	Roof Slab	3'-0"	1.4D+1.7L+1.4F+1.7H	55.90	11.29	0.7 (east-west)	0.79 (east-west)	None
	Interior Slab	2'-0"	D+Lo+F+H'+E' (2)	95.22	13.16	1.13 (east-west)	1.27 (east-west)	None
	Basemat	3'-0"	D+Lo+F+H'+E' (2)	123.94	19.10	0.97 (east-west)	1.00 (east-west)	None
	Exterior Wall	3'-0"	D+Lo+F+H'+E'	543.34	59.39	4.27 (east-west)	4.68 (east-west)	0.19
North End of Main Tunnel (near Control Building) (North End of Main Tunnel (West of Control Building)	Interior Wall	2'-0"	D+Lo+F+H'+E' (2)	152.15	19.96	1.69 (east-west)	2.25 (east-west)	None
	Roof Slab	3'-0"	1.4D+1.7L+1.4F+1.7H	86.64	15.29	0.70 (east-west)	0.79 (east-west)	None
	Interior Slab	2'-0"	D+Lo+F+H'+E' (2)	136.30	18.03	1.49 (east-west)	2.25 (east-west)	None
	Basemat	3'-0"	1.4D+1.7L+1.4F+1.7H	70.42	28.27	0.36 (north-south)	0.79 (north-south)	None
	Basemat	3'-0"	1.4D+1.7L+1.4F+1.7H	155.74	36.39	1.16 (east-west)	1.27 (east-west)	None
Main Tunnel (near Access- Region 1) Main Tunnel (in Access Region 1)	Basemat	3'-0"	1.4D+1.7L+1.4F+1.7H	46.60	20.54	0.70 (north-south)	0.79 (north-south)	None

Table 3H.6-6: Results of RSW Piping Tunnel Design (Continued)

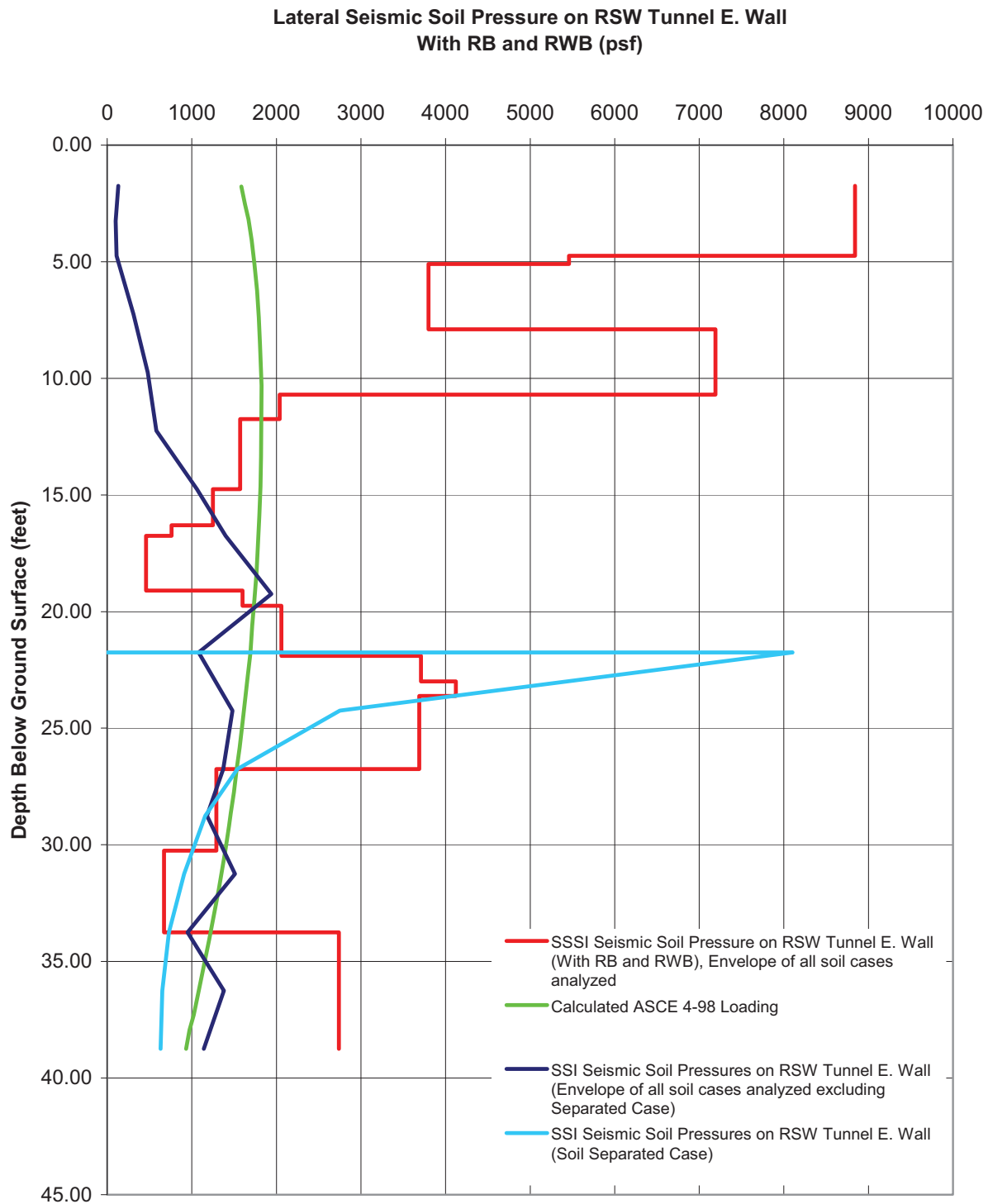
Location Location ⁽⁴⁾	Item	Thickness (ft)	Governing Load Combination	Design Moment (kip-ft/ft)	Design Shear (kip/ft)	Area of Reinforcement (in ² /ft)		
						Moment Reinforcement ⁽¹⁾		Shear Reinforcement
						Required	Provided (both faces)	Required
Main Tunnel (near Access Region 2) Main Tunnel (in Access Region 2)	Exterior Wall	3'-0"	D+Lo+F+H'+E'	321.96	29.22	2.21 (vertical)	2.25 (vertical)	None
				214.84	29.22	1.40 (horizontal)	1.56 (horizontal)	None
	Basemat	6'-0"	D+Lo+F+H'+E' ⁽²⁾	530.76	66.74	1.66 (east-west)	2.25 (east-west)	None
			1.4D+1.7L+1.4F+1.7H / D+Lo+F+H'+E' ⁽²⁾	500.50	66.74	1.78 (north-south)	2.25 (north-south)	None
Main Tunnel (near Access Region 3) Main Tunnel (in Access Region 3) North of Pump House	Exterior Wall	3'-0"	D+Lo+F+H'+E'	245.29	36.52	1.76 (vertical)	3.12 (vertical)	None
	Roof Slab	3'-0"	1.4D+1.7L+1.4F+1.7H	344.53	37.20	2.56 (north-south)	4.68 (north-south)	None
	Interior Slab	2'-0"	D+Lo+F+H'+E' ⁽²⁾	150.97	19.29	1.70 (north-south)	3.12 (north-south)	None
	Basemat	3'-0"	1.4D+1.7L+1.4F+1.7H	236.52	38.12	1.74 (north-south)	3.12 (north-south)	0.20

Table 3H.6-6: Results of RSW Piping Tunnel Design (Continued)

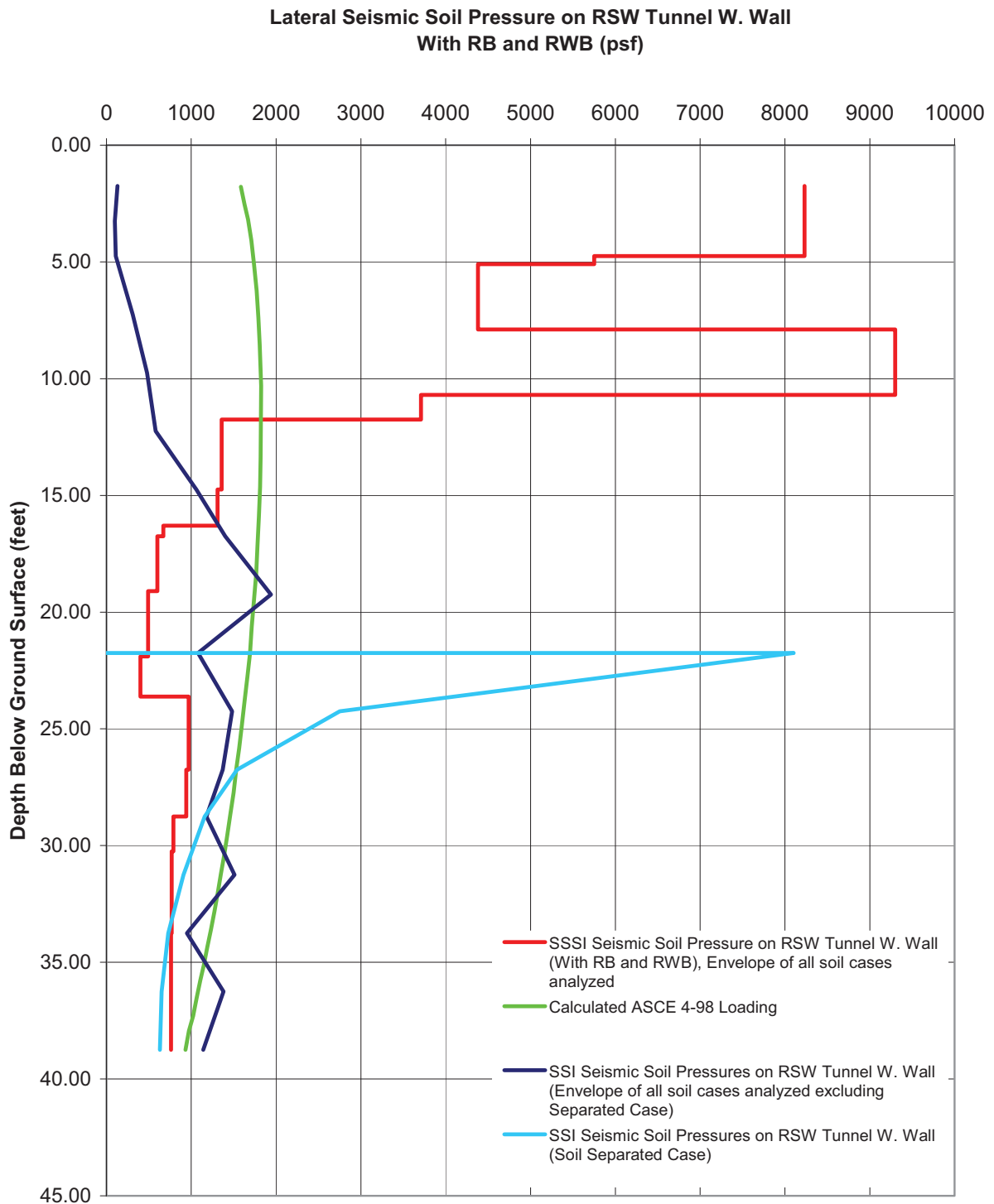
Notes:

- 1) Unless noted otherwise, the required reinforcement in the direction not reported in the table is controlled by the minimum required reinforcement. The minimum required reinforcement for 2'-0" thick and 3'-0" thick elements is 0.36 in²/ft and 0.54 in²/ft. For such cases the provided reinforcement is 0.79 in²/ft.
- 2) The loading also includes loads due to internal flooding.

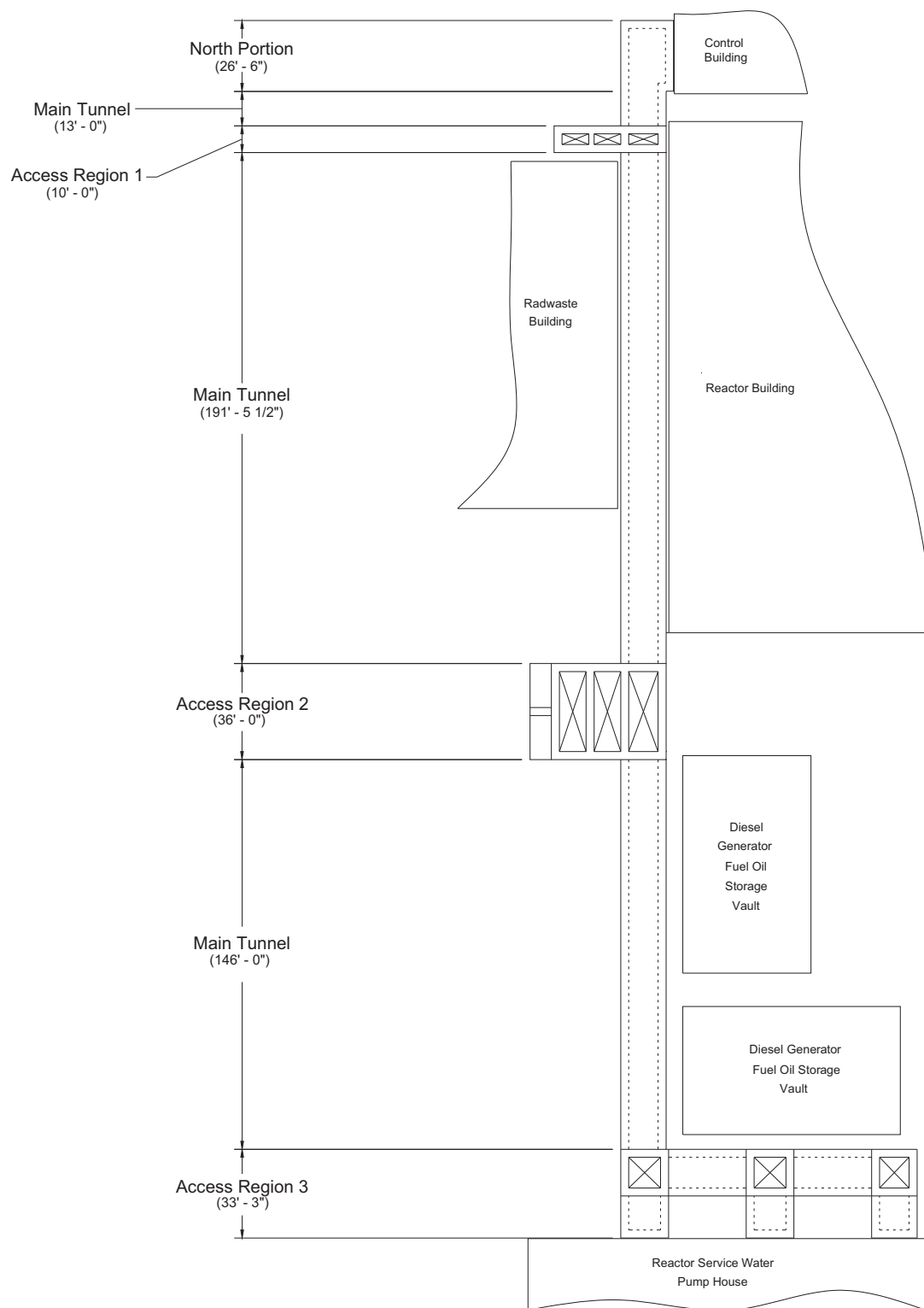
(3) The following additional reinforcement is required due to SSE Wave Propagation:	
For the Main Tunnel, #8 bars at 12" o.c. in the longitudinal direction of the Main Tunnel for 84'-0" (measured north from the centerline of the Main Tunnel and Access Region 3)	
For Access Region 3 from 0'-0" to 56'-0" (measured east from the centerline of the intersection of the Main Tunnel and Access Region 3)	
(i) Second layer of #11 bars at 12" o.c. in the transverse direction applied to both faces of the roof	
(ii) Second layer of #11 bars at 12" o.c. in the transverse direction applied to both faces of the interior slab	
(iii) Second layer of #11 bars at 12" o.c. in the transverse direction applied to both faces of the basement	
For Access Region 3 from 56'-0" to 103'-0" (measured east from the centerline of the intersection of the Main Tunnel and Access Region 3)	
(i) Second layer of #11 bars at 12" o.c. in the transverse direction applied to both faces of the roof	
(ii) Second layer of #11 bars at 12" o.c. in the transverse direction applied to both faces of the basement	
3) In addition to the reinforcement shown within this table, the following reinforcement is required due to SSE Wave Propagation:	
- For the Main Tunnel, 0.79 in ² /ft (applied to both faces of the walls and slabs) in the north-south direction of the Main Tunnel for 84'-0" (measured north from the centerline of the intersection of the Main Tunnel and Access Region 3)	
- For Access Region 3 from 0'-0" to 56'-0" (measured east from the centerline of the intersection of the Main Tunnel and Access Region 3), 1.56 in ² /ft (applied to both faces of the roof, interior slab, and basement) in the north-south direction	
- For Access Region 3 from 56'-0" to 103'-0" (measured east from the centerline of the intersection of the Main Tunnel and Access Region 3), 1.56 in ² /ft (applied to both faces of the roof and basement) in the north-south direction	
4) Refer to Figure 3H.6-248 for plan view of the RSW Tunnel	



**Figure 3H.6-212: Lateral Seismic Soil Pressure (psf) on RSW Piping Tunnel East Wall
(Main Cross Section of RSW Piping Tunnel)**



**Figure 3H.6-213: Lateral Seismic Soil Pressure (psf) on RSW Piping Tunnel West Wall
(Main Cross Section of RSW Piping Tunnel)**

**Figure 3H.6-248: RSW Tunnel Plan View**

RAI 03.08.04-34, Supplement 1**QUESTION:**

10 CFR 50, Appendix A, GDC 2, requires that structures important to safety shall be designed to withstand the effects of natural phenomena with appropriate combination of the effects of normal and accident conditions. To meet this requirement, all seismic category I structures must be designed for required strength at all locations in the structure. During the October 2010 Audit the applicant presented the procedures to verify the concrete sections of the UHS/PH structural members resulting from the code-required load combinations. The internal forces (i.e. shear, moment, axial force, torsion, etc.) used to determine the required strength of the structural members (i.e. walls, slabs, beam, columns, etc.) of the UHS/PH building are generated by the applicant with the help of SAP2000 models simulating the building's static and dynamic behavior. These element forces are subsequently processed by the applicant with a number of in-house developed programs for design of concrete sections. It was noted that concrete slabs and walls were designed for out-of-plane shear by averaging the element shear forces across cut lines that extended along the entire width of the walls and slabs. The staff considers that averaging of out of plane shear along the entire cut line of a slab or wall could lead to unconservative estimate of shear stress in slabs. The subject was discussed with the applicant during the audit. Although the applicant explained the procedure by referencing to ACI 349-97, Section 11.12, "Special provisions for slabs and footings," it did not provide the staff with a sufficient interpretation of the provision of the ACI code, which appears to be intended for shear strength of slabs and footings in the vicinity of columns, concentrated loads, or reactions, to close this issue. ACI 349-97, Section 13.3.1, states that a slab system may be designed by any procedure satisfying conditions of equilibrium and geometric compatibility, if shown that the design strength at every section is at least equal to the required strength. Averaging of out-of-plane shear across the entire width of a slab may not show that the design strength at every section is at least equal to the required strength. Therefore, in order for the staff to conclude that the site-specific structures are adequately designed for out-of plane shear, the staff requests STP to demonstrate that use of average shear force across the entire width of slab, instead of the shear force demand at every section obtained from analysis may be considered acceptable by any or more of the following:

- Obtain clarification from the ACI regarding validity of use of Section 11.12 of ACI 349-87 for the situations where the provisions of the code were used,
- Provide examples of any precedence where similar methodology was accepted by the staff,
- Provide detailed justification using industry accepted standards, technical references, experimental results, etc., to justify redistribution of the shear forces obtained from finite element analysis.

The applicant is also requested to update the FSAR as necessary.

SUPPLEMENTAL RESPONSE:

The original response to this RAI was submitted with Nuclear Innovation North America (NINA) letter U7-C-NINA-NRC-110050, dated April 5, 2011. This supplement provides the response to the following action item discussed in the NRC audits performed during the weeks of May 23, 2011 and July 25, 2011.

Beam shear discussion (Audit Action Item 3.8-21, Punch List Item 56):

Calculations will be revised and FSAR tables will be updated as a Confirmatory Action

COLA updates reflecting the results of the hydrodynamic mass effect on the columns will be included in this response (Punch List No. 17)

Finite element analysis was used for design of the following structures:

- Ultimate Heat Sink (UHS)/Reactor Service Water (RSW) Pump House
- Diesel Generator Fuel Oil Tunnels (DGFOT)
- Diesel Generator Fuel Oil Storage Vaults (DGFOSV)
- Radwaste Building (RWB)

As noted in the original response, unless noted otherwise, design of these structures for out-of-plane shear have been conservatively revised based on finite element analysis results for each element without averaging the shear over several elements. This supplemental response provides the summary of results for UHS/RSW Pump House and DGFOT. The summary of results for DGFOSV and RWB will be provided in RAI 03.08.04-34, Supplement 2 currently scheduled for submittal in October 2011.

UHS/RSW Pump House:

No averaging has been used for out-of-plane shear design except at four locations within the UHS basin basemat at the junction of basin buttresses with the basin basemat. At these four locations, the out-of-plane shear was averaged over a total length of twice the baseemat thickness (i.e. $2 \times 10 = 20$ ft, basemat thickness = 10 ft). This averaging of shear is justified for the following reasons:

- The local shear concentration is due to excessively refined mesh for a 10 ft thick mat. As can be seen from Figure 03.08.04-34 S1.1, the width of the basemat elements is only 5.88 ft.
- The basin buttresses are 6 ft thick walls. Considering a load distribution of 45° through the basemat thickness will yield an effective strip of 26 ft (i.e. $6 \text{ ft} + 2 \times 10 \text{ ft} = 26 \text{ ft}$) which exceeds the 20 ft used for shear averaging.

Tables 3H.6-7 through 3H.6-9 and Figures 3H.6-51 through 3H.6-74, 3H.6-74A, 3H.6-75 through 3H.6-78, 3H.6-78A, 3H.6-79 through 3H.6-116, 3H.6-116A, 3H.6-117 through 3H.6-120, 3H.6-120A, 3H.6-121 through 3H.6-122, 3H.6-122A, 3H.6-123 through 3H.6-126, 3H.6-126A, 3H.6-127 through 3H.6-134, 3H.6-134A, 3H.6-135, and 3H.6-136A through 3H.6-136C (see enclosure) have been revised to reflect the results of this analysis. In addition, these revised tables also reflect the results of the hydrodynamic mass effect on the UHS basin columns and beams considering the scaled column accelerations discussed in RAI 03.08.04-30, Supplement 4.

DGFOT:

No averaging has been used for out-of-plane shear design. Tables 3H.7-1 and Figures 3H.7-10A, 3H.7-14A, 3H.7-17, and 3H.7-19A (see Enclosure) have been revised to reflect the results of this analysis.

As a result of this response COLA Part 2, Tier 2, Appendix 3H will be revised as shown in the Enclosure.

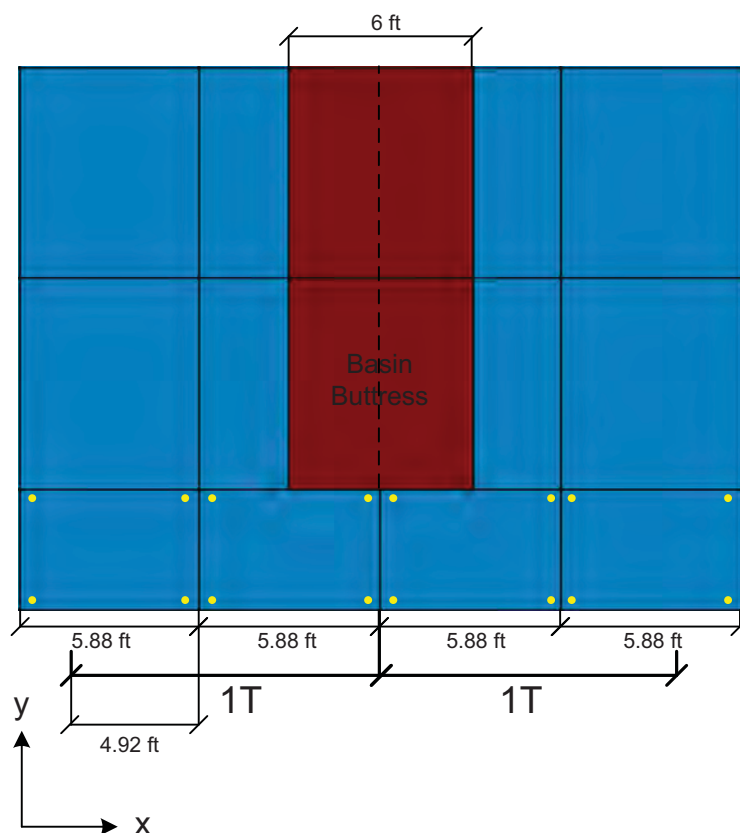


Figure 03.08.04-34 S1.1: Partial Plan View of UHS Basin Basemat Mesh
Out-of-plane Shear Averaged over 2T
T = Basemat Thickness, 10 ft

ENCLOSURE

COLA MARK-UPS

3H.6.6.3.1 UHS Basin/UHS Cooling Tower/RSW Pump House Concrete Wall and Slab Design

For each reinforcement zone, the following in-plane and transverse shears with the corresponding load combination are reported in Tables 3H.6-7 and 3H.6-8. The in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

The shell forces from every element for every load combination in the finite element model were evaluated to determine the required transverse reinforcement. The transverse shear and axial force reported in Tables 3H.6-7 and 3H.6-8 correspond to the maximum required transverse reinforcement for an element within that transverse reinforcement zone.

- The in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.
- The transverse shear is the maximum average transverse shear along a plane in that transverse reinforcement zone.

3H.7.5.3.1 Reinforced Concrete Elements

For each surface, the following in-plane and transverse shears with the corresponding load combination are reported in Table 3H.7-1 when the governing forces, moments and reinforcement is from the SAP2000 models. The in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

The shell forces from every element for every load combination in the finite element model were evaluated to determine the required transverse reinforcement. The transverse shear and axial force reported in Table 3H.7-1 correspond to the maximum required transverse reinforcement for an element within that transverse reinforcement zone.

- The in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

The transverse shear is the maximum average transverse shear along a plane in that transverse reinforcement zone.

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design

Location	Thickness (ft)	Face	Direction	Reference/Comment (1)	Drawing Number (2)	Reference/Comment (3)	Maximum Forces (3)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Results											
									Axial and Flexure Loads			In-Plane Shear Loads			Load Combination	Horizontal Section Corresponding Axial Force (kip/ft)	Vertical Section Corresponding Axial Force (kip/ft)	Transverse Shear Force (kip/ft)													
									Load Combination	Axial (k) (kip/ft)	Moment (k) (kip-ft)	Load Combination	In-plane (k) (kip-ft)																		
																					In-plane (k) (kip-ft)										
Pump House North Wall	9	North (outside)	Horizontal	3H-6-5	3H-6-5	3H-6-5	MTOM	2923	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	371	-413	D+L+F+H+T+E	32	7.8	-	-	-	-	-												
								MCOM	2914	D+L+F+H+T+E	-179	-25																			
								MMAT	2921	D+L+F+H+T+E	128	-548																			
								MMAC	2946	D+L+F+H+T+E	-56	-528																			
								MTOM	3425	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	149	-18																			
								MCOM	3482	D+L+F+H+T+E	-297	-415																			
								MMAT	4082	D+L+F+H+T+E	0	-734																			
								MMAC	5580	D+L+F+H+T+E	-131	-774																			
								MTOM	5586	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	186	-599																			
								MCOM	3590	D+L+F+H+T+E	-244	-580																			
								MMAT	5555	D+L+F+H+T+E	3	-490																			
								MMAC	5555	D+L+F+H+T+E	-63	-499																			
Pump House North Wall	9	Vertical	3H-6-5	3H-6-5	3H-6-5	3H-6-5	MTOM	8570	1.0D+1.2L+1.1SF+1.3H+1.2T+1.2W	271	-429	D+L+F+H+T+E	126	7.8	-	-	-	-	-												
								MCOM	3542	D+L+F+H+T+E	-281	-382																			
								MMAT	5541	D+L+F+H+T+E	3	-1188																			
								MMAC	4101	D+L+F+H+T+E	-149	-1229																			
								MTOM	2902	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	324	126																			
								MCOM	3481	D+L+F+H+T+E	-288	198																			
								MMAT	2914	D+L+F+H+T+E+W	86	348																			
								MMAC	3708	D+L+F+H+T+E	-159	360																			
								MTOM	5202	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	114	13																			
								MCOM	3477	D+L+F+H+T+E	-229	151																			
								MMAT	3707	D+L+F+H+T+E	9	324																			
								MMAC	3653	D+L+F+H+T+E	-70	441																			
Pump House East Wall	9	East (outside)	Horizontal	3H-6-6	3H-6-6	3H-6-6	MTOM	3642	D+L+F+H+T+E	207	95	D+L+F+H+T+E	126	4.68	-	-	-	-	-												
								MCOM	3642	D+L+F+H+T+E	-281	95																			
								MMAT	5435	D+L+F+H+T+E	6	468																			
								MMAC	3689	D+L+F+H+T+E	-147	481																			
								1-2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
								2-3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
								3-3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
								Pump House East Wall	9	East (outside)	Horizontal	3H-6-6	3H-6-6	3H-6-6	MTOM	3222	D+L+F+H+T+E	697	-170	D+L+F+H+T+E	155	12.48	-	-	-	-	-	(8)			
																MCOM	3222	D+L+F+H+T+E	-750	47											
																MMAT	3222	D+L+F+H+T+E	697	-495											
																MMAC	3222	D+L+F+H+T+E	-337	-498											
																MTOM	3979	1.0SD+1.3L+1.0SF+1.3H+1.2T+1.2W	248	-20											
MCOM	3979	D+L+F+H+T+E	-362	-31																											
MMAT	3121	D+L+F+H+T+E	61	-271																											
MMAC	3121	D+L+F+H+T+E	-51	-464																											
MTOM	8893	D+L+F+H+T+E	163	45																											
MCOM	8827	D+L+F+H+T+E	-446	-77																											
MMAT	8829	D+L+F+H+T+E	62	-428																											
MMAC	8823	D+L+F+H+T+E	-112	-596																											
Pump House East Wall	9	Vertical	3H-6-7	3H-6-7	3H-6-7	3H-6-7	MTOM	3221	D+L+F+H+T+E	484	-107	D+L+F+H+T+E	308	10.92	-	-	-	-	-	(8)											
								MCOM	8835	D+L+F+H+T+E	-484	-159																			
								MMAT	8813	D+L+F+H+T+E	120	-481																			
								MMAC	8814	D+L+F+H+T+E	-144	-295																			

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Reinforcement Number (1)	Maximum Forces (2)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
								Axial and Flexure Loads			In-Plane Shear Loads			Horizontal Section		Vertical Section			
								Load Combination	Axial (k) (kips-ft)	Flexure (k) (kips-ft)	Load Combination	In-plane (k) (kips-ft)		Transverse Shear Force (kips-ft)	Corresponding Axial Force (kips-ft)	Transverse Shear Force (kips-ft)	Corresponding Axial Force (kips-ft)		
Pump House East Wall (Cont'd)	3	East (outside)	Vertical	3H.6-7			MTOM	3228	215	-134	D+L+F+H+T+E	247	-	-	-	-	-		
							MCOM	8853	-521	-482	D+L+F+H+T+E								
							MMAT	8864	62	-531	D+L+F+H+T+E								
							MMAC	8864	-349	-462	D+L+F+H+T+E								
							MTOM	6039	76	-39	D+L+F+H+T+E								
							MCOM	6359	-506	-431	D+L+F+H+T+E	175	-	-	-	-	-		
							MMAT	3907	36	-299	D+L+F+H+T+E								
							MMAC	6491	-112	-344	D+L+F+H+T+E								
							MTOM	6998	199	-49	1399+38+109F+394+127+139W	115	-	-	-	-	-		
							MCOM	6528	-294	-42	D+L+F+H+T+E								
							MMAT	6968	109	-229	D+L+F+H+T+E								
							MMAC	6947	-450	-221	D+L+F+H+T+E								
							MTOM	6520	242	-411	140+135+139F+1394+139W	247	-	-	-	-	-		
							MCOM	6349	-440	-493	D+L+F+H+T+E								
							MMAT	6118	9	-536	D+L+F+H+T+E								
							MMAC	8869	-251	-484	D+L+F+H+T+E								
							MTOM	3222	606	40	D+L+F+H+T+E								
							MCOM	3222	-414	868	D+L+F+H+T+E	155	-	-	-	-	(8)		
							MMAT	3223	190	868	D+L+F+H+T+E								
							MMAC	3222	-414	868	D+L+F+H+T+E								
							MTOM	3988	262	129	D+L+F+H+T+E								
							MCOM	3988	-301	46	D+L+F+H+T+E	155	-	-	-	-	-		
							MMAT	3100	27	357	D+L+F+H+T+E								
							MMAC	3100	-42	357	D+L+F+H+T+E								
West (inside)	3H.6-8	Horizontal	MTOM	8894	108	179	D+L+F+H+T+E												
			MCOM	8829	-914	952	D+L+F+H+T+E	194	-	-	-	-	-	-					
			MMAT	8822	97	415	D+L+F+H+T+E												
			MMAC	8829	-493	582	D+L+F+H+T+E												
			MTOM	8827	62	65	140+140F+1394+139W												
			MCOM	8827	-446	204	D+L+F+H+T+E	283	-	-	-	-	-	-					
			MMAT	8851	6	817	D+L+F+H+T+E												
			MMAC	8881	-419	962	D+L+F+H+T+E												
			MTOM	3222	649	146	D+L+F+H+T+E												
			MCOM	8825	-484	1232	D+L+F+H+T+E	308	-	-	-	-	(8)						
			MMAT	8825	-	-	D+L+F+H+T+E												
			MMAC	8825	-493	1815	D+L+F+H+T+E												
3H.6-9	Vertical	MTOM	3226	199	51	D+L+F+H+T+E													
		MCOM	8853	-435	833	D+L+F+H+T+E	247	-	-	-	-	-	-						
		MMAT	8864	2	1179	D+L+F+H+T+E													
		MMAC	8853	-491	954	D+L+F+H+T+E													
		MTOM	3241	60	49	D+L+F+H+T+E													
		MCOM	8909	-397	62	D+L+F+H+T+E	234	-	-	-	-	-	-						
		MMAT	6397	1	999	D+L+F+H+T+E													
		MMAC	8889	-294	691	D+L+F+H+T+E													

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Drawing Number	Reinforcement Zone Number	Maximum Force(s)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
									Axial and Flexure Loads			In-Plane Shear Loads	Load Combination		Flexure (ft-kips)	Load (ft-kips)	Horizontal Section	Vertical Section		
									Load Combination	Flexure (ft-kips)	Load (ft-kips)									
Pump House East Wall (Cont'd)	9	West (inside)	Vertical	3H-6-69				MTCM 6444	46	202	D-L-F-H-T+E	175	D-L-F-H-T+E	-	-	-	-	-	-	-
								MCCM 6505	-320	20	D-L-F-H-T+E									
								MMAT 6466	1	533	D-L-F-H-T+E									
								MMAC 3937	-46	561	D-L-F-H-T+E									
								MTCM 6506	76	36	D-L-F-H-T+E									
								MCCM 6522	-244	217	D-L-F-H-T+E	120	D-L-F-H-T+E	-	-	-	-	-	-	
								MMAT 6603	4	368	D-L-F-H-T+E									
								MMAC 3106	-46	321	D-L-F-H-T+E									
								MTCM 6620	211	116	D-L-F-H-T+E	115	D-L-F-H-T+E	-	-	-	-	-	-	
								MCCM 6520	-300	164	D-L-F-H-T+E									
								MMAT 6520	2	222	D-L-F-H-T+E									
								MMAC 6520	-239	228	D-L-F-H-T+E									
Pump House South Wall	9	Transverse (Horizontal and Vertical)		3H-6-60				MTCM 5788	-249	-43	D-L-F-H-T+E	-	D-L-F-H-T+E	-	41	34	154	542	0.60	
								MCCM 5611	-1115	-117	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-130	-200	-304	-47	1.24	
								MMAT 5784	6	-439	D-L-F-H-T+E	-	D-L-F-H-T+E	-	49	23	76	476	0.44	
								MMAC 5794	-49	-439	D-L-F-H-T+E	-	D-L-F-H-T+E	-	32	32	37	436	0.31	
								MTCM 5784	149	-182	D-L-F-H-T+E	222	D-L-F-H-T+E	-	-	-	-	-	-	
								MCCM 5607	-787	-238	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
								MMAT 5793	0	-482	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
								MMAC 5793	-230	-483	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
								MTCM 5788	-243	-411	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
								MCCM 5609	-1036	-401	D-L-F-H-T+E	222	D-L-F-H-T+E	-	-	-	-	-	-	
								MMAT 5796	136	-1204	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
								MMAC 5796	-605	-1401	D-L-F-H-T+E	-	D-L-F-H-T+E	-	-	-	-	-	-	
Pump House West Wall	9	Horizontal	3H-6-63				MTCM 5783	97	205	D-L-F-H-T+E	235	D-L-F-H-T+E	-	-	-	-	-	-		
							MCCM 5608	-628	192	D-L-F-H-T+E										
							MMAT 5784	25	712	D-L-F-H-T+E										
							MMAC 5784	-163	785	1.6D+1.7L+1.7W+1.7W	-163	785								
							MTCM 5607	164	186	D-L-F-H-T+E										
							MCCM 5607	-222	17	D-L-F-H-T+E	222	D-L-F-H-T+E	-	-	-	-	-	-		
							MMAT 5774	0	578	D-L-F-H-T+E										
							MMAC 5757	-261	1168	1.6D+1.7L+1.7W+1.7W	-261	1168								
							MTCM 5783	97	205	D-L-F-H-T+E										
							MCCM 5608	-628	192	D-L-F-H-T+E										
							MMAT 5774	0	578	D-L-F-H-T+E										
							Pump House West Wall	9	West (outside)	Horizontal	3H-6-66			MTCM 5783	-	-	-	-	D-L-F-H-T+E	-
MCCM 5783	-	-	-	-	D-L-F-H-T+E	-								13	-145	126	46	0.20		
MMAT 6229	-252	-58	D-L-F-H-T+E	124	D-L-F-H-T+E	-								-	-	-	-	-		
MMAT 3008	59	-407	D-L-F-H-T+E																	
MMAC 6169	-122	-784	D-L-F-H-T+E																	

Table 3H.6.7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcing Number (1)	Zone Number (2)	Maximum Force (3)	Element	Longitudinal Reinforcement Design Loads				Transverse Shear Design Loads				Results			
								Axial and Flexure Loads		In-Plane Shear Loads		Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads		Transverse Shear Reinforcement Provided (in ² /ft)				
								Load Combination	Axial (k) (kips-ft)	Flexure (k) (kips-ft)	Load Combination		In-Plane Shear Load (kips-ft)						
														Transverse Shear Force (kip/ft)			Corresponding Axial Force (kip/ft)	Transverse Shear Force (kip/ft)	Corresponding Axial Force (kip/ft)
Pump House West Wall (Cont'd)	8	West (outside)	Vertical	3H.6.7	3H.6.6	2.4-L	MTCM	3291	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	974	-529	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	98	14.64	-	-	-		
							MCCM	3291	D+1.4F+H+T+E	-350	-356								
							MMAT	3291	D+1.4F+H+T+E	712	-243								
							MMAC	3291	D+1.4F+H+T+E	-19	-681								
							MTCM	3662	D+1.4F+H+T+E	84	-34								
							MCCM	3662	D+1.4F+H+T+E	-309	-49								
							MMAT	6125	D+1.4F+H+T+E	4	-200	D+1.4F+H+T+E	129	3.12	-	-	-	-	-
							MMAC	6146	D+1.4F+H+T+E	-158	-242								
							MTCM	3280	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	429	-56								
							MCCM	9136	D+1.4F+H+T+E	-255	-468	D+1.4F+H+T+E	129	6.24	-	-	-	-	-
							MMAT	9138	D+1.4F+H+T+E	7	-653								
							MMAC	9138	D+1.4F+H+T+E	-171	-600								
							MTCM	6125	1.4D+1.3L+1.05F+1.3M+1.27+1.3W	317	-384								
							MCCM	6167	D+1.4F+H+T+E	-233	-35								
							MMAT	9126	1.4D+1.3L+1.05F+1.3M+1.27+1.3W	69	-468	D+1.4F+H+T+E	75	7.8	-	-	-	-	-
							MMAC	9126	D+1.4F+H+T+E	-41	-341								
							MTCM	6151	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	84	-75								
							MCCM	9642	D+1.4F+H+T+E	-262	-8								
							MMAT	3673	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	19	-348	D+1.4F+H+T+E	132	3.12	-	-	-	-	-
							MMAC	6321	D+1.4F+H+T+E	-127	-468								
							MTCM	6131	D+1.4F+H+T+E	64	-691								
							MCCM	9377	D+1.4F+H+T+E	-315	-298								
							MMAT	6127	1.4D+1.3L+1.05F+1.3M+1.27+1.3W	26	-528	D+1.4F+H+T+E	132	4.68	-	-	-	-	-
							MMAC	6293	D+1.4F+H+T+E	-165	-696								
							MTCM	3283	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	222	-688								
							MCCM	9110	D+1.4F+H+T+E	-265	-315	D+1.4F+H+T+E	115	4.68	-	-	-	-	-
							MMAT	9105	D+1.4F+H+T+E	5	-684								
							MMAC	9105	D+1.4F+H+T+E	-52	-704								
							MTCM	3290	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	549	-273								
							MCCM	9134	D+1.4F+H+T+E	-760	-354	D+1.4F+H+T+E	144	9.36	-	-	-	-	-
							MMAT	9134	D+1.4F+H+T+E	256	-696								
							MMAC	9138	D+1.4F+H+T+E	-340	-1271								
							MTCM	3276	D+1.4F+H+T+E	485	-49								
							MCCM	9669	D+1.4F+H+T+E	-315	97								
							MMAT	3268	D+1.4F+H+T+E	2	-261	D+1.4F+H+T+E	124	6.24	-	-	-	-	-
							MMAC	9661	D+1.4F+H+T+E	-145	-292								
							MTCM	3291	D+1.4F+H+T+E	622	153								
							MCCM	3291	D+1.4F+H+T+E	-360	-217								
							MMAT	3291	D+1.4F+H+T+E	228	820	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	98	12.48	-	-	-	-	-
							MMAC	3291	D+1.4F+H+T+E	-126	620								
							MTCM	9667	1.05D+1.3L+1.05F+1.3M+1.27+1.3W	135	57								
							MCCM	9679	D+1.4F+H+T+E	-422	175	D+1.4F+H+T+E	129	3.12	-	-	-	-	-
							MMAT	9677	D+1.4F+H+T+E	0	-267								
							MMAC	9677	D+1.4F+H+T+E	-355	-288								

Table 3H.6.7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Zone Number ⁽¹⁾	Maximum Forces ⁽²⁾	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Results		
						Axial and Flexure Loads			In-Plane Shear Loads			Load Combination	Transverse Shear Force (kip/ft)	Horizontal Section Compressing Axial Force (kip/ft)	Vertical Section Compressing Axial Force (kip/ft)				
						Load Combination	Axial (k) (kip/ft)	Flexure (k) (kip/ft)	Load Combination	In-plane (k) (kip/ft)									
Pump House West Wall (Cov'd)	9	Horizontal	3H.6.8	4H-L	MTCM	3280	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	424	17										
						MCCM	9134	D+L+F+H+T+E	-607	222	D+L+F+H+T+E	129							
						MMAT	9134	D+L+F+H+T+E	21	369									
						MMAC	9134	D+L+F+H+T+E	-408	377									
						MTCM	6125	D+L+F+H+T+E	209	33									
						MCCM	6101	D+L+F+H+T+E	-199	12									
						MMAT	3029	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	7	122									
						MMAC	3029	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	-1	121									
						MTCM	6134	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	129	55									
						MCCM	8997	D+L+F+H+T+E	-244	68									
						MMAT	6285	D+L+F+H+T+E	0	462									
						MMAC	3073	D+L+F+H+T+E	-54	425									
Pump House West Wall (Cov'd)	9	Vertical	3H.6.9	MTCM	9116	D+L+F+H+T+E	129	87											
					MCCM	9102	D+L+F+H+T+E	-295	388										
					MMAT	9105	D+L+F+H+T+E	13	437										
					MMAC	9106	D+L+F+H+T+E	-218	739										
					MTCM	3201	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	664	95										
					MCCM	9134	D+L+F+H+T+E	-665	1406										
					MMAT	9134	D+L+F+H+T+E	4	1105										
					MMAC	9134	D+L+F+H+T+E	-665	1406										
						1.2	-	-	-	-	-	-	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	69		77	380	0.26	
						2.2	-	-	-	-	-	-	D+L+F+H+T+E	16		204	1	0.44	
						3.2	-	-	-	-	-	-	D+L+F+H+T+E	41		62	1213	0.80	
					Pump House Interior East Wall	4	Horizontal	3H.6.71	1H-L	MTCM	3248	D+L+F+H+T+E	381	484					
MCCM	3248	D+L+F+H+T+E	-477	-19															
MMAT	3248	D+L+F+H+T+E	194	-119															
MMAC	3248	D+L+F+H+T+E	-304	-119															
MTCM	3251	D+L+F+H+T+E	150	-23															
MCCM	8939	D+L+F+H+T+E	-645	-19															
MMAT	7016	D+L+F+H (Internal Floor)	5	-147															
MMAC	6984	D+L+F+H (Internal Floor)	-28	-265															
MTCM	3248	D+L+F+H+T+E	188	-7															
MCCM	3248	D+L+F+H+T+E	-487	-14															
MMAT	3248	D+L+F+H+T+E	98	-21															
Pump House Interior East Wall	4	Vertical	3H.6.72	2H-L							MTCM	6925	D+L+F+H+T+E	-191	-199				
					MCCM	6925	D+L+F+H+T+E	100	-10										
					MMAT	6925	D+L+F+H+T+E	100	-10										
					MMAC	6925	D+L+F+H+T+E	100	-10										
					MTCM	6925	D+L+F+H+T+E	100	-10										
					MCCM	6925	D+L+F+H+T+E	100	-10										
					MMAT	6925	D+L+F+H+T+E	100	-10										
					MMAC	6925	D+L+F+H+T+E	100	-10										
					MTCM	6925	D+L+F+H+T+E	100	-10										
					MCCM	6925	D+L+F+H+T+E	100	-10										
					MMAT	6925	D+L+F+H+T+E	100	-10										
					MMAC	6925	D+L+F+H+T+E	100	-10										
Pump House Interior East Wall	4	Horizontal	3H.6.73	2H-L	MTCM	8937	D+L+F+H+T+E	-665	152										
						MCCM	8937	D+L+F+H+T+E	-665	152									
						MMAT	7016	D+L+F+H (Internal Floor)	9	121									
						MMAC	6984	D+L+F+H (Internal Floor)	-21	197									
							1.2	-	-	-	-	-	-	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	69		77	380	0.26
							2.2	-	-	-	-	-	-	D+L+F+H+T+E	16		204	1	0.44
							3.2	-	-	-	-	-	-	D+L+F+H+T+E	41		62	1213	0.80
							1.2	-	-	-	-	-	-	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	69		77	380	0.26
							2.2	-	-	-	-	-	-	D+L+F+H+T+E	16		204	1	0.44
							3.2	-	-	-	-	-	-	D+L+F+H+T+E	41		62	1213	0.80
							1.2	-	-	-	-	-	-	1.05D+1.3L+1.0SF+1.3H+1.2T+1.3W	69		77	380	0.26
							2.2	-	-	-	-	-	-	D+L+F+H+T+E	16		204	1	0.44
	3.2	-	-	-	-	-	-	D+L+F+H+T+E	41		62	1213	0.80						

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reference Number (1)	Cracking Number (1)	Reinforcement Zone Number (1)	Maximum Force (2)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks				
									Axial and Flexure Loads			In-Plane Shear Loads			Subsidiary Section			Vertical Section						
									Load Combination	Flexure (ft-kips)	Axial (kips)	Load Combination	In-plane Shear (kips/ft)		Transverse Shear Force (kips)	Subsidiary Section Corresponding Axial Force (kips)	Transverse Shear Force (kips)	Vertical Section Corresponding Axial Force (kips)						
Pump House Internal East Wall (Cont'd)	4	West (bottom)	Vertical	3H.6-74		1 1/2-L		MTOM	3246	D-L-F-H-T-E	168	7												
								MCCM	3246	D-L-F-H-T-E	-497	5												
								MMAT	3245	D-L-F-H-T-E	74	16												
								MMAC	8937	D-L-F-H-T-E	-244	146												
								MTOM	3248	D-L-F-H-T-E	88	4												
								MCCM	8946	D-L-F-H-T-E	-382	16												
								MMAT	6998	D-L-F-H-T-E	15	54												
								MMAC	8853	D-L-F-H (Internal Flood)	-109	327												
									-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
								MTOM	3294	D-L-F-H-T-E	275	-46												
								MCCM	3294	D-L-F-H-T-E	-410	-57												
								MMAT	3171	D-L-F-H-T-E	12	-130												
Pump House Internal West Wall	4	East (top)	Horizontal	3H.6-75		2 1/4-L		MTOM	3299	D-L-F-H-T-E	99	-8												
								MCCM	9103	D-L-F-H-T-E	-552	-25												
								MMAT	6752	D-L-F-H (Internal Flood)	8	-127												
								MMAC	6750	D-L-F-H (Internal Flood)	-29	-201												
								MTOM	3294	D-L-F-H-T-E	139	-16												
								MCCM	9105	D-L-F-H-T-E	-465	-29												
								MMAT	3294	D-L-F-H-T-E	93	-21												
								MMAC	9101	D-L-F-H-T-E	-112	-181												
								MTOM	3296	D-L-F-H-T-E	70	-7												
								MCCM	9108	D-L-F-H-T-E	-380	-7												
								MMAT	6601	D-L-F-H-T-E	1	-57												
								Pump House Internal West Wall	4		Horizontal	3H.6-77				MMAC	6576	D-L-F-H (Internal Flood)	-103	-333				
MTOM	3294	D-L-F-H-T-E	275	42																				
MCCM	3294	D-L-F-H-T-E	-410	17																				
MMAT	3171	D-L-F-H-T-E	12	101																				
MMAC	3171	D-L-F-H-T-E	-732	-113																				
MTOM	3299	D-L-F-H-T-E	99	7																				
MCCM	9101	D-L-F-H-T-E	-575	104																				
MMAT	6752	D-L-F-H (Internal Flood)	1	137																				
MMAC	6750	D-L-F-H (Internal Flood)	-28	-203																				
MTOM	3294	D-L-F-H-T-E	139	6																				
MCCM	9105	D-L-F-H-T-E	-465	64																				
Pump House Internal West Wall	4	West (bottom)	Vertical	3H.6-78		1 1/2-L										MMAT	3294	D-L-F-H-T-E	24	23				
								MMAC	9101	D-L-F-H-T-E	-328	-201												
								MTOM	3296	D-L-F-H-T-E	70	6												
								MCCM	9108	D-L-F-H-T-E	-384	33												
								MMAT	6744	D-L-F-H-T-E	44	89												
								MMAC	6576	D-L-F-H (Internal Flood)	-228	-143												
									-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
								MTOM	3615/36A															
								MCCM	3615/36A															
									-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
								MTOM	3615/36A															
								MCCM	3615/36A															
MMAT	3615/36A																							

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement (Longitudinal and Vertical)	Reinforcement Zone Number (ft)	Maximum Forces (k)	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
							Element	Axial and Flexure Loads			In-Plane Shear Loads		Horizontal Section Transverse Shear Force (kip/ft)	Vertical Section Transverse Shear Force (kip/ft)	Corresponding Axial Force (kip/ft)			
								Load Combination	A _{sc} /ft ² (kip/ft)	Flexure (k) (kip-ft)	Load Combination					In-plane (k) (kip/ft)		
Pump House Baffles ¹⁰	6	Horizontal	3H-6-9	14-L	MCCM	13320	1.05D+1.3L+1.05F+1.3H+1.27+1.3W	225	9	D+L+F+H+T+E	218	4.68	-	-	-	-	-	
						MCCM	13401	D+L+F+H+T+E	-275	53								
						MMAT	13445	D+L+F+H+T+E	89	198								
						MMAC	13451	D+L+F+H+T+E	-50	142								
						MTDM	13320	D+L+F+H+T+E	188	-69								
						MCCM	13420	D+L+F+H+T+E	-261	-59	D+L+F+H+T+E	92	4.68	-	-	-	-	
		Vertical	3H-6-8	15-L	MMAT	13414	D+L+F+H+T+E	103	146									
						MMAC	13414	D+L+F+H+T+E	-48	143								
						MTDM	13410	D+L+F+H+T+E	471	72								
						MCCM	13437	1.4D+1.3L+1.05F+1.7H+1.7W	-521	288	D+L+F+H+T+E	92	7.8	-	-	-	-	
						MMAT	13457	D+L+F+H+T+E	7	475								
						MMAC	13437	D+L+F+H+T+E	-127	477								
UHS Basin North Wall	6	Horizontal	3H-6-2	24-L	MTDM	6177	D+L+F+H+T+E	1005	-346	D+L+F+H+T+E	42	12.48	-	-	-	-		
						MCCM	8673	D+L+F+H+T+E	-294	-499								
						MMAT	8691	D+L+F+H+T+E	57	-1311								
						MMAC	8691	D+L+F+H+T+E	-130	-1311								
						MTDM	6095	1.4D+1.3F+1.3H+1.4T0	648	-139	D+L+F+H+T+E	176	9.36	-	-	-	-	
						MCCM	2076	1.05D+1.3L+1.05F+1.3H+1.27+1.3W	-612	-182								
		Vertical	3H-6-1	15-L	MMAT	3359	D+L+F+H+T+E	39	-688	D+L+F+H+T+E	153	0.24	-	-	-	-		
						MMAC	3359	D+L+F+H+T+E	-180	-1058								
						MTDM	5796	1.4D+1.3F+1.3H+1.4T0	282	-335								
						MCCM	3900	D+L+F+H+T+E	-688	-86	D+L+F+H+T+E	139	4.68	-	-	-	-	
						MMAT	5975	1.4D+1.3L+1.05F+1.7H+1.7W	66	-533								
						MMAC	3574	1.4D+1.3F+1.3H+1.4T0	-46	-477								
UHS Basin North Wall	6	Horizontal	3H-6-2	15-L	MTDM	2977	D+L+F+H+T+E	248	-129	D+L+F+H+T+E	139	4.68	-	-	-	-		
						MCCM	6198	D+L+F+H+T+E	-334	-101								
						MMAT	6198	D+L+F+H+T+E	26	-664								
						MMAC	6198	D+L+F+H+T+E	-250	-694								
						MTDM	2980	D+L+F+H+T+E	259	-190								
						MCCM	6199	D+L+F+H+T+E	-320	-41	D+L+F+H+T+E	175	0.24	-	-	-	-	
		Vertical	3H-6-3	15-L	MMAT	6113	D+L+F+H+T+E	0	-713									
						MMAC	6113	D+L+F+H+T+E	-144	-213								
						MTDM	3004	D+L+F+H+T+E	313	-184	D+L+F+H+T+E	208	7.8	-	-	-	-	
						MCCM	6116	D+L+F+H+T+E	-332	-149								
						MMAT	6116	D+L+F+H+T+E	76	-736								
						MMAC	6116	D+L+F+H+T+E	-189	-236								
UHS Basin North Wall	6	Horizontal	3H-6-2	4-L	MTDM	3027	D+L+F+H+T+E	473	-699	D+L+F+H+T+E	249	12.48	-	-	-	-		
						MCCM	5988	D+L+F+H+T+E	-507	-205								
						MMAT	6124	D+L+F+H+T+E	133	-800								
						MMAC	6124	D+L+F+H+T+E	-46	-660								
						MTDM	6093	D+L+F+H+T+E	281	-59								
						MCCM	6093	D+L+F+H+T+E	-284	-41	1.05D+1.3L+1.05F+1.3H+1.27+1.3W	214	0.24	-	-	-	-	
		Vertical	3H-6-3	15-L	MMAT	4149	D+L+F+H+T+E	133	-372									
						MMAC	4149	D+L+F+H+T+E	-5	-303								

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Drinking Number (1)	Reinforcement Zone Number (2)	Maximum Force (3)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Results				
								Axial and Flexure Loads			In-Plane Shear Loads			Multiaxial Section		Virtual Section							
								Load Combination	Axial (ft) (kips/ft)	Flexure (ft) (kips/ft)	Load Combination	In-plane (ft) (kips/ft)		Transverse Shear Force (kips/ft)	Corresponding Axial Force (kips/ft)	Transverse Shear Force (kips/ft)	Corresponding Axial Force (kips/ft)						
UHS Bulkhead North Wall (Cont'd)	8	North (outside)	Vertical	3H-43			MTDM 6005	D-1-L-F-H-T-E	375	-744	D-1-L-F-H-T-E	222	9.36	-	-	-	-	-					
							MCCM 2409	D-1-L-F-H-T-E	-462	-352													
							MMAT 6005	D-1-L-F-H-T-E	375	-744													
							MMAC 6005	D-1-L-F-H-T-E	-188	-744													
							MTDM 2609	1-4D+13F+13M+14To	143	-152													
							MCCM 2400	D-1-L-F-H-T-E	-589	-197													
							MMAT 3024	D-1-L-F-H-T-E	3	-589													
							MMAC 3000	D-1-L-F-H-T-E	-272	-587													
							MTDM 2609	1-4D+13F+13M+14To	360	336													
							MCCM 3942	D-1-L-F-H-T-E	-265	368													
							MMAT 2950	1-4D+13L+13F+17M+17W	112	1113													
							MMAC 3936	D-1-L-F-H-T-E	-3	1062													
			Horizontal	3H-54			MTDM 6177	1-6D+13L+1-6D+13M+12T+13W	1029	209													
							MCCM 6973	D-1-L-F-H-T-E	-294	193													
							MMAT 7921	D-1-L-F-H-T-E	168	1219													
							MMAC 7921	D-1-L-F-H-T-E	-77	1219													
							MTDM 6095	1-4D+13L+13F+17M+17W	829	417													
							MCCM 3903	D-1-L-F-H-T-E	-344	210													
							MMAT 3002	1-4D+13F+13M+14To	224	900													
							MMAC 3002	1-4D+13L+13F+17M+17W	-4	896													
							MTDM 6807	1-4D+13F+13M+14To	179	227													
							MCCM 3900	D-1-L-F-H-T-E	-658	152													
							MMAT 6902	1-4D+13L+13F+17M+17W	58	943													
							MMAC 6902	1-4D+13F+13M+14To	-129	975													
		South (inside)		3H-55			MTDM 6005	1-4D+13F+13M+14To	664	777													
							MCCM 2010	1-6D+13L+1-6D+13M+12T+13W	-486	99													
							MMAT 3027	1-4D+13L+13F+17M+17W	127	1461													
							MMAC 3027	D-1-L-F-H-T-E	-24	1347													
							MTDM 6005	1-4D+13F+13M+14To	522	61													
							MCCM 3941	D-1-L-F-H-T-E	-384	263													
							MMAT 6941	1-4D+13L+13F+17M+17W	149	1296													
							MMAC 4195	D-1-L-F-H-T-E	-9	1193													
							MTDM 2077	D-1-L-F-H-T-E	248	53													
							MCCM 6946	D-1-L-F-H-T-E	-268	141													
							MMAT 6950	D-1-L-F-H-T-E	28	341													
							MMAC 6929	1-4D+13F+13M+14To	-87	398													
		Vertical	3H-56				MTDM 3001	D-1-L-F-H-T-E	309	36													
							MCCM 6916	D-1-L-F-H-T-E	-269	183													
							MMAT 6900	1-4D+13F+13M+14To	23	423													
							MMAC 6900	1-4D+13L+13F+17M+17W	-57	476													
							MTDM 3027	D-1-L-F-H-T-E	475	411													
							MCCM 6986	D-1-L-F-H-T-E	-507	713													
							MMAT 6986	D-1-L-F-H-T-E	39	713													
							MMAC 6986	D-1-L-F-H-T-E	-607	713													

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Drinking Water Supply	Reinforcement Zone Number (1)	Maximum Force (2)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks					
								Axial and Flexure Loads		In-Plane Shear Loads			Horizontal Section		Vertical Section								
								Load Combination	Flexure (ft-kip)	Axial (ft-kip)	Load Combination		In-plane Shear (ft-kip)	Transverse Shear Force (ft-kip)	Corresponding Axial Force (ft-kip)	Transverse Shear Force (ft-kip)			Corresponding Axial Force (ft-kip)				
UHS Basin North Wall (Cont'd)	6	South (inside)	Vertical	3H-6-8	4 1/4	MTDM	915E	D+L+T+H+T+E	242	338	9.36	-	-	-	-	-	-						
							916E	D+L+T+H+T+E	-352	451	-	D+L+T+H+T+E	-	-	-	-	-						
							917E	D+L+T+H+T+E	35	1265	-	-	-	-	-	-	-						
							918E	D+L+T+H+T+E	-12	1268	-	-	-	-	-	-	-						
							919E	D+L+T+H+T+E	281	138	-	-	-	-	-	-	-						
							920E	D+L+T+H+T+E	-294	114	-	-	-	-	-	-	-						
							921E	D+L+T+H+T+E	19	360	6.24	-	-	-	-	-	-						
							922E	D+L+T+H+T+E	-43	366	-	1.00D+1.3L+1.09F+1.3M+1.27+1.3W	-	-	-	-	-						
							923E	D+L+T+H+T+E	373	523	-	-	-	-	-	-	-						
							924E	D+L+T+H+T+E	-602	591	-	-	-	-	-	-	-						
							925E	D+L+T+H+T+E	39	793	-	-	-	-	-	-	-						
							926E	D+L+T+H+T+E	-696	793	-	-	-	-	-	-	-						
							927E	D+L+T+H+T+E	142	90	-	-	-	-	-	-	-						
							928E	D+L+T+H+T+E	-606	147	-	-	-	-	-	-	-						
							929E	D+L+T+H+T+E	19	450	6.24	-	-	-	-	-	-						
							930E	D+L+T+H+T+E	-277	945	-	-	-	-	-	-	-						
UHS Basin South Wall	6	South (outside)	Vertical	3H-6-8	4 1/4	MTDM	931E	D+L+T+H+T+E	-	-	-	-	-	-	-	-	-	-					
							932E	D+L+T+H+T+E	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
							933E	D+L+T+H+T+E	-329	-544	-	-	-	-	-	-	-	-	-	-	-	-	-
							934E	D+L+T+H+T+E	61	-1117	-	-	-	-	-	-	-	-	-	-	-	-	-
							935E	D+L+T+H+T+E	-428	-1117	-	-	-	-	-	-	-	-	-	-	-	-	-
							936E	D+L+T+H+T+E	275	-187	6.24	-	-	-	-	-	-	-	-	-	-	-	-
							937E	D+L+T+H+T+E	-362	-290	-	-	-	-	-	-	-	-	-	-	-	-	-
							938E	D+L+T+H+T+E	29	-444	-	-	-	-	-	-	-	-	-	-	-	-	-
							939E	D+L+T+H+T+E	-31	-444	-	-	-	-	-	-	-	-	-	-	-	-	-
							940E	D+L+T+H+T+E	369	-290	-	-	-	-	-	-	-	-	-	-	-	-	-
							941E	D+L+T+H+T+E	-237	-110	-	-	-	-	-	-	-	-	-	-	-	-	-
							942E	D+L+T+H+T+E	155	-606	7.8	-	-	-	-	-	-	-	-	-	-	-	-
							943E	D+L+T+H+T+E	-19	-500	-	-	-	-	-	-	-	-	-	-	-	-	-
							944E	D+L+T+H+T+E	169	-102	-	-	-	-	-	-	-	-	-	-	-	-	-
							945E	D+L+T+H+T+E	-364	-76	4.68	-	-	-	-	-	-	-	-	-	-	-	-
							946E	D+L+T+H+T+E	3	-506	-	-	-	-	-	-	-	-	-	-	-	-	-
947E	D+L+T+H+T+E	-176	-496	-	-	-	-	-	-	-	-	-	-	-	-	-							
948E	D+L+T+H+T+E	212	-91	-	-	-	-	-	-	-	-	-	-	-	-	-							
949E	D+L+T+H+T+E	-326	-14	6.24	-	-	-	-	-	-	-	-	-	-	-	-							
950E	D+L+T+H+T+E	49	-353	-	-	-	-	-	-	-	-	-	-	-	-	-							
951E	D+L+T+H+T+E	-154	-587	-	-	-	-	-	-	-	-	-	-	-	-	-							
952E	D+L+T+H+T+E	238	-111	-	-	-	-	-	-	-	-	-	-	-	-	-							
953E	D+L+T+H+T+E	-389	-69	4.68	-	-	-	-	-	-	-	-	-	-	-	-							
954E	D+L+T+H+T+E	29	-606	-	-	-	-	-	-	-	-	-	-	-	-	-							
955E	D+L+T+H+T+E	-211	-686	-	-	-	-	-	-	-	-	-	-	-	-	-							
956E	D+L+T+H+T+E	240	-164	-	-	-	-	-	-	-	-	-	-	-	-	-							
957E	D+L+T+H+T+E	-389	-85	-	-	-	-	-	-	-	-	-	-	-	-	-							
958E	D+L+T+H+T+E	26	-605	6.24	-	-	-	-	-	-	-	-	-	-	-	-							
959E	D+L+T+H+T+E	-246	-605	-	-	-	-	-	-	-	-	-	-	-	-	-							

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reference Number (1)	Reference Number (2)	Maximum Force(s)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
								Axial and Flexure Loads			In-Plane Shear Loads			Load Combination	Transverse Shear Force (kip/ft)	Subsidiary Section Corresponding Axial Force (kip/ft)	Vertical Section Corresponding Axial Force (kip/ft)		
								Load Combination	Axial (kip/ft)	Flexure (kip-ft)	In-Plane Shear Load (kip/ft)								
South (outside)	Vertical	3H-60	7 1/2			MTDM	2103	D+L+F+H+T+E	217	-103	D+L+F+H+T+E	4.68	-	-	-	-	-		
						MCDM	1973	D+L+F+H+T+E	-385	-38									
						MMAT	1972	D+L+F+H+T+E	7	-437									
						MMAC	1868	D+L+F+H+T+E	-175	-601									
						MTDM	1880	D+L+F+H+T+E	227	-308									
						MCDM	1880	D+L+F+H+T+E	-237	-125									
		6 1/2		MMAT	1880	1-Ø+7L+17F+13H+17W	165	-370	D+L+F+H+T+E	88		D+L+F+H+T+E	6.24	-	-	-	-	-	
				MMAC	1880	D+L+F+H+T+E	-42	-305											
				MTDM	2002	1-Ø+17F+13H+1-Ø	301	424											
				MCDM	3531	D+L+F+H+T+E	-249	438											
				MMAT	4318	D+L+F+H+T+E	158	1408	D+L+F+H+T+E	98		D+L+F+H+T+E	10.02	-	-	-	-		
				MMAC	4318	D+L+F+H+T+E	-79	1408											
North (inside)	Vertical	3H-60	2 1/4		MTDM	4473	D+L+F+H+T+E	607	384										
					MCDM	4362	D+L+F+H+T+E	-329	339	D+L+F+H+T+E	33		D+L+F+H+T+E	9.36	-	-	-	-	
					MMAT	4497	D+L+F+H+T+E	70	698										
					MMAC	4497	D+L+F+H+T+E	-90	698										
					MTDM	3815	D+L+F+H+T+E	275	280										
					MCDM	3507	D+L+F+H+T+E	-362	193	D+L+F+H+T+E	64		D+L+F+H+T+E	6.24	-	-	-	-	
		3H-60		MMAT	4436	1-Ø+7L+17F+13H+17W	98	713											
				MMAC	4436	1-Ø+7L+17F+13H+17W	-37	729											
				MTDM	2188	1-Ø+17F+13H+1-Ø	360	154											
				MCDM	2118	1-Ø+17F+13H+1-Ø	-191	671	D+L+F+H+T+E	76		D+L+F+H+T+E	9.36	-	-	-	-		
				MMAT	2140	1-Ø+17F+13H+1-Ø	286	848											
				MMAC	2002	1-Ø+17F+13H+1-Ø	-21	862											
North (inside)	Vertical	3H-60	7 1/4		MTDM	1795	1-Ø+17F+13H+1-Ø	232	89	D+L+F+H+T+E	98		D+L+F+H+T+E	6.24	-	-	-	-	
					MCDM	1006	10Ø+13L+10ØF+13H+12F+13W	-244	214										
					MMAT	1687	1-Ø+7L+17F+13H+17W	64	720	D+L+F+H+T+E			D+L+F+H+T+E	6.24	-	-	-	-	
					MMAC	1687	1-Ø+17F+13H+1-Ø	-43	726										
					MTDM	2204	1-Ø+17F+13H+1-Ø	366	588										
					MCDM	3836	10Ø+13L+10ØF+13H+12F+13W	-246	38	D+L+F+H+T+E	98		D+L+F+H+T+E	10.02	-	-	-	-	
		6 1/4		MMAT	4205	D+L+F+H+T+E	111	1548											
				MMAC	4205	D+L+F+H+T+E	-76	1548											
				MTDM	3500	10Ø+13L+10ØF+13H+12F+13W	197	42											
				MCDM	1014	D+L+F+H+T+E	-273	120	D+L+F+H+T+E	131		D+L+F+H+T+E	4.68	-	-	-	-		
				MMAT	4317	D+L+F+H+T+E	12	328											
				MMAC	1119	1-Ø+17F+13H+1-Ø	-137	461											
Vertical	3H-60	2 1/4		MTDM	3587	10Ø+13L+10ØF+13H+12F+13W	204	15											
				MCDM	1197	D+L+F+H+T+E	-290	142	D+L+F+H+T+E	169		D+L+F+H+T+E	6.24	-	-	-	-		
				MMAT	4375	D+L+F+H+T+E	24	255											
				MMAC	1197	1-Ø+7L+17F+13H+17W	-259	308	D+L+F+H+T+E			D+L+F+H+T+E	6.24	-	-	-	-		
				MTDM	2199	D+L+F+H+T+E	238	28											
				MCDM	1586	D+L+F+H+T+E	-324	170	D+L+F+H+T+E	149		D+L+F+H+T+E	4.68	-	-	-	-		
		3 1/4		MMAT	1980	D+L+F+H+T+E	6	344											
				MMAC	1291	1-Ø+17F+13H+1-Ø	-129	447											

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Number (ft)	Drawing Number (ft)	Reinforcement Zone Number (ft)	Maximum Forces (ft)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks		
									Axial and Flexure Loads		In-Plane Shear Loads			Load Combination	Corresponding Axial Force (kip/ft)	Transverse Shear Force (kip/ft)	Horizontal Section			Vertical Section	
									Load Combination	Flexure (ft-kip/ft)	Load Combination	In-plane (ft ² /ft)									
UHS Basin South Wall (Cont'd)	8	North (panels)	Vertical		4-V/L			2142	D+L+F+H+T+E	240	67	D+L+F+H+T+E	6.24	-	-	-	-	-	-		
									MCCM	1553	-323	193									
									MMAT	1553	5	263									
									MMAC	1553	-311	263									
									MTCA	2103	-217	32									
									MCCM	1700	-269	137									
									MMAT	4504	14	375									
									MMAC	3838	-75	402									
									MTCA	1880	-227	38									
									MCCM	1854	-388	568									
									MMAT	1868	27	937									
									MMAC	1791	-139	1307									
UHS Basin East Wall	8	East (panels)	Horizontal	3H-6-1	3H-6-1			6234	1.0D+1.3L+1.0SF+1.3H+1.2T+1.3W	410	-48	1.0D+1.3T+1.3H+1.4Tb	-	-	-	-	1.0D+1.3T+1.3H+1.4Tb	128	0.30		
									MCCM	5205	-311	-1019									
									MMAT	5241	64	-2078									
									MMAC	5241	-222	-2130									
									MTCA	2611	-216	-608									
									MCCM	3504	-348	-325									
									MMAT	3506	27	-688									
									MMAC	3506	-180	-1033									
									MTCA	2200	-306	-216									
									MCCM	2622	-230	-136									
									MMAT	1995	103	-688									
									MMAC	1998	-21	-579									
UHS Basin East Wall	8	East (panels)	Horizontal	3H-6-2	3H-6-2			2000	1.0D+1.3L+1.0SF+1.3H+1.2T+1.3W	-230	-136	D+L+F+H+T+E	7.8	-	-	-	-	-	-		
									MCCM	2649	-275	-248									
									MCCM	2620	-182	-111									
									MMAT	2649	162	-606									
									MMAC	2627	-101	-489									
									MTCA	2275	-266	-222									
									MCCM	2852	-460	-197									
									MMAT	4295	0	-683									
									MMAC	5234	-283	-1073									
									MTCA	4286	-419	107									
									MCCM	5235	-311	471									
									MMAT	5235	209	2186									
MMAC	5235	-67	2124																		
UHS Basin East Wall	8	West (panels)	Horizontal	3H-6-4	3H-6-4			2297	1.0D+1.3L+1.0SF+1.3H+1.2T+1.3W	386	546	D+L+F+H+T+E	10.62	-	-	-	-	-	-		
									MCCM	3893	-295	96									
									MMAT	3980	138	1469									
									MMAC	3890	-7	1413									
									MTCA	2528	-204	101									
									MCCM	3507	-348	-20									
									MMAT	2494	81	891									
									MMAC	5236	-69	796									

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Drinking Number (1)	Reference Number (1)	Zone Number (2)	Maximum Forces (3)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks									
									Axial and Flexure Loads			In-Plane Shear Loads			Horizontal Section		Vertical Section												
									Load Combination	Axial (k) (kips-ft)	Flexure (k) (kips-ft)	Load Combination	In-plane (k) (kips-ft)		Transverse Shear Force (kips-ft)	Corresponding Axial Force (kips-ft)	Transverse Shear Force (kips-ft)	Corresponding Axial Force (kips-ft)											
																					Load Combination								
UHS Bulk Head Wall (Cont'd)	6	West (outside)	Horizontal	3H.6-6				MTDM	2527	140D+1.9F+1.3W+1.4FD	346	247	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2414	D+L+F+H+T+E	-128	124																	
								MMAT	1980	140D+1.3L+1.9F+1.7W+1.1W	75	695																	
								MMAC	1980	140D+1.9F+1.3W+1.4FD	-65	800																	
								MTDM	2603	140D+1.9F+1.3W+1.4FD	239	164	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2979	105D+1.3L+1.09F+1.3W+1.2T+1.3W	-240	233																	
								MMAT	2462	140D+1.3L+1.9F+1.7W+1.1W	58	749																	
								MMAC	2462	140D+1.9F+1.3W+1.4FD	-84	707																	
								MTDM	2456	140D+1.9F+1.3W+1.4FD	341	334	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	3655	105D+1.3L+1.09F+1.3W+1.2T+1.3W	-265	74																	
								MMAT	2441	140D+1.3L+1.9F+1.7W+1.1W	176	1101																	
								MMAC	3935	D+L+F+H+T+E	-1	1070																	
								MTDM	2308	D+L+F+H+T+E	166	173	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2689	D+L+F+H+T+E	-338	277																	
								MMAT	5308	D+L+F+H+T+E	13	546																	
								MMAC	5308	D+L+F+H+T+E	-4	546																	
UHS Bulk Head Wall (Cont'd)	6	West (inside)	Vertical	3H.6-6				MTDM	2349	D+L+F+H+T+E	261	166	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2690	D+L+F+H+T+E	-375	254																	
								MMAT	4267	D+L+F+H+T+E	25	1067																	
								MMAC	4267	D+L+F+H+T+E	-168	1138																	
								MTDM	2373	D+L+F+H+T+E	266	136	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2707	D+L+F+H+T+E	-365	242																	
								MMAT	4265	D+L+F+H+T+E	20	795																	
								MMAC	4265	D+L+F+H+T+E	-160	795																	
								MTDM	2605	D+L+F+H+T+E	232	138	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	2832	D+L+F+H+T+E	-460	679																	
								MMAT	2655	D+L+F+H+T+E	9	1176																	
								MMAC	2655	140D+1.3L+1.9F+1.7W+1.1W	-165	1331																	
								Transverse and Vertical					1.7	-	-	-	-	-	-	-	-	-	-	-	-	-			
													2.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
													3.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
UHS Bulk Head Wall	6	West (outside)	Horizontal	3H.6-7				MTDM	5176	105D+1.3L+1.09F+1.3W+1.2T+1.3W	462	-124	D+L+F+H+T+E	-	-	-	-	-	-										
								MCDA	5171	D+L+F+H+T+E	-416	-657																	
								MMAT	5177	D+L+F+H+T+E	92	-2201																	
								MMAC	5177	D+L+F+H+T+E	-137	-2201																	
								MTDM	4614	140D+1.9F+1.3W+1.4FD	368	-286	D+L+F+H+T+E	-	-	-	-	-	-	-									
								MCDA	3477	105D+1.3L+1.09F+1.3W+1.2T+1.3W	-365	-143																	
								MMAT	3866	D+L+F+H+T+E	32	-864																	
								MMAC	3866	D+L+F+H+T+E	-275	-659																	
								MTDM	2222	140D+1.9F+1.3W+1.4FD	846	-326	D+L+F+H+T+E	-	-	-	-	-	-	-									
								MCDA	2220	D+L+F+H+T+E	-156	-185																	
								MMAT	2320	D+L+F+H+T+E	240	-577																	
								MMAC	2320	D+L+F+H+T+E	-113	-416																	
								MTDM	1986	140D+1.9F+1.3W+1.4FD	431	-482	D+L+F+H+T+E	-	-	-	-	-	-	-									
								MCDA	1953	D+L+F+H+T+E	-150	-299																	
								MMAT	1623	140D+1.3L+1.9F+1.7W+1.1W	109	-461																	
								MMAC	2197	D+L+F+H+T+E	-17	-434											-	-	-				

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Drawing Number	Reinforcement Zone Number	Maximum Force(s)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks	
									Axial and Flexure Loads			In-Plane Shear Loads		Transverse Shear Force		Vertical Section				
									Load Combination	Axial (k) (kips ft)	Flexure (k) (kips ft)	Load Combination		In-plane (k) (kips ft)	Transverse Shear Force (kips ft)	Corresponding Axial Force (kips ft)	Transverse Shear Force (kips ft)			Corresponding Axial Force (kips ft)
UHS Basin West Wall (Cont'd)		East (paving)	Horizontal	3H.6-7				MTDM 2315	1.4D + 1.5F + 1.3M + 1.6To	466	-360									
								MCDM 2314	D + L + F + H + T + E	271	-327	D + L + F + H + T + E	141							
								MMAT 2314	D + L + F + H + T + E	3	-514									
								MMAC 2314	D + L + F + H + T + E	-48	-614									
								MTDM 2302	1.4D + 1.5F + 1.3M + 1.6To	260	-296									
								MCDM 2405	1.0SD + 1.3L + 1.0SF + 1.3M + 1.2T + 1.3W	-214	-44	D + L + F + H + T + E	141							
								MMAT 1903	1.4D + 1.3L + 1.1SF + 1.7M + 1.7W	72	-514									
								MMAC 1903	1.4D + 1.5F + 1.3M + 1.6To	-48	-481									
								MTDM 2219	1.4D + 1.5F + 1.3M + 1.6To	917	-67									
								MCDM 2596	D + L + F + H + T + E	-172	-183	D + L + F + H + T + E	190							
								MMAT 2596	D + L + F + H + T + E	73	-904									
								MMAC 2596	D + L + F + H + T + E	-32	-904									
		West (columns)	Vertical	3H.6-8				MTDM 2604	D + L + F + H + T + E	298	-119									
								MCDM 2405	D + L + F + H + T + E	-278	-69	D + L + F + H + T + E	133							
								MMAT 2604	D + L + F + H + T + E	40	-704									
								MMAC 3800	D + L + F + H + T + E	-75	-725									
								MTDM 2239	D + L + F + H + T + E	284	-286	D + L + F + H + T + E	162							
								MCDM 2605	D + L + F + H + T + E	-379	-160									
								MMAT 2320	D + L + F + H + T + E	75	-791	D + L + F + H + T + E								
								MMAC 5170	D + L + F + H + T + E	-266	-1099									
								MTDM 2402	D + L + F + H + T + E	294	-203									
								MCDM 2607	D + L + F + H + T + E	-483	-63	D + L + F + H + T + E	191							
								MMAT 4253	D + L + F + H + T + E	4	-1011									
								MMAC 5176	D + L + F + H + T + E	-286	-1036									
		East (paving)	Horizontal	3H.6-9				MTDM 2406	D + L + F + H + T + E	166	-271									
								MCDM 2612	D + L + F + H + T + E	-379	-110	D + L + F + H + T + E	116							
								MMAT 5164	D + L + F + H + T + E	1	-446									
								MMAC 5176	D + L + F + H + T + E	-73	-279									
								MTDM 4262	1.0SD + 1.3L + 1.0SF + 1.3M + 1.2T + 1.3W	464	132	D + L + F + H + T + E								
								MCDM 5171	D + L + F + H + T + E	-416	1733									
								MMAT 5171	D + L + F + H + T + E	288	2357									
								MMAC 5171	D + L + F + H + T + E	-109	2283									
								MTDM 4515	1.4D + 1.3L + 1.1SF + 1.7M + 1.7W	228	128	D + L + F + H + T + E	37							
								MCDM 3807	1.0SD + 1.3L + 1.0SF + 1.3M + 1.2T + 1.3W	-363	60									
								MMAT 3842	D + L + F + H + T + E	168	1263	D + L + F + H + T + E	61							
								MMAC 3889	D + L + F + H + T + E	-73	1233									
		East (paving)	Horizontal	3H.6-9				MTDM 2220	1.4D + 1.5F + 1.3M + 1.6To	666	1136									
								MCDM 2314	D + L + F + H + T + E	-271	462	D + L + F + H + T + E	120							
								MMAT 2320	1.4D + 1.3L + 1.1SF + 1.7M + 1.7W	732	1266									
								MMAC 2226	D + L + F + H + T + E	-33	1169									
								MTDM 2226	1.4D + 1.5F + 1.3M + 1.6To	921	332									
								MCDM 2183	1.0SD + 1.3L + 1.0SF + 1.3M + 1.2T + 1.3W	-256	276	D + L + F + H + T + E	120							

[illegible]

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Reinforcement Number (1)	Maximum Force(s) (2)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks	
								Axial and Flexure Loads		In-Plane Shear Loads			Load Combination	Nonlinear Section Transverse Shear Force (kip-ft)	Corresponding Axial Force (kip-ft)	Vertical Section Transverse Shear Force (kip-ft)			Corresponding Axial Force (kip-ft)
								Load Combination	Axial (kip-ft)	Flexure (kip-ft)	Re-bar (2)								
UHS Basin North-South Between Curbs (3)	8	East and West	Vertical	3H-6-103	1-1/4	MCCM	742L	D-L-F-H-T+E	742	-114	D-L-F-H-T+E	227	9.36	-	-	-	-	-	
							721Z	D-L-F-H-T+E	-497	103	-	-	-	-	-	-	-	-	
							784S	D-L-F-H-T+E	124	-1010	-	-	-	-	-	-	-	-	
							784S	D-L-F-H-T+E	-122	-1010	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	991	397	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-492	412	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	964	595	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-411	595	-	-	-	-	-	-	-	-	
							742L	D-L-F-H-T+E	-	-	-	-	-	-	-	-	-	-	
							742L	D-L-F-H-T+E	-	-	-	-	-	-	-	-	-	-	
UHS Basin East-West Between Curbs (3)	8	North and South	Horizontal	3H-6-105	2-1/4	MCCM	767L	D-L-F-H-T+E	699	274	D-L-F-H-T+E	278	9.36	-	-	-	-		
							767L	D-L-F-H-T+E	-1110	-479	-	-	-	-	-	-	-	-	
							767L	D-L-F-H-T+E	246	607	-	-	-	-	-	-	-	-	
							767L	D-L-F-H-T+E	-627	607	-	-	-	-	-	-	-	-	
							767L	D-L-F-H-T+E	166	189	-	-	-	-	-	-	-	-	
							749L	D-L-F-H-T+E	-96	195	-	-	-	-	-	-	-	-	
							769L	D-L-F-H-T+E	116	-486	-	-	-	-	-	-	-	-	
							769L	D-L-F-H-T+E	-42	298	-	-	-	-	-	-	-	-	
							769L	D-L-F-H-T+E	417	-34	-	-	-	-	-	-	-	-	
							769L	D-L-F-H-T+E	-362	114	-	-	-	-	-	-	-	-	
Cooking Tower North and South Walls	2	North and South	Horizontal	3H-6-107	1-1/4	MCCM	114Z	D-L-F-H-T+E	220	-8	D-L-F-H-T+E	31	6.24	-	-	-	-		
							112Z	D-L-F-H-T+E	-171	-34	-	-	-	-	-	-	-	-	
							468	D-L-F-H-T+E	77	-169	-	-	-	-	-	-	-	-	
							468	D-L-F-H-T+E	-12	-169	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	360	-103	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-647	-107	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	99	-209	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-181	-209	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-	-	-	-	-	-	-	-	-	-	
							730Z	D-L-F-H-T+E	-	-	-	-	-	-	-	-	-	-	

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement (1)	Drawing Number (1)	Reinforcement (2)	Maximum Forces (3)	Element	Longitudinal Reinforcement Design Loads					Transverse Shear Design Loads					Transverse Shear Reinforcement Provided (in ² /ft)	Remarks	
									Axial and Flexure Loads				In-Plane Shear Loads		Longitudinal Reinforcement (in ² /ft)	Transverse Shear Design Loads					
									Load Combination	Axial (k) (kips-ft)	Moment (k) (kips-ft)	Fracture (k) (kips-ft)	Load Combination	In-plane (k) (kips-ft)		Transverse Shear Force (kips-ft)	Horizontal Section Corresponding Axial Force (kips-ft)	Vertical Section Corresponding Axial Force (kips-ft)			
																					Load Combination
Cooling Tower North and South Walls (Cont'd)	2	North (End of North Wall) and South (End of South Wall)	Vertical	3H-109		3H-109	MTOM	980	D+L+FF+H+T+E	292	-23	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MCOM	980	D+L+FF+H+T+E	-297	-32	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MMAT	980	D+L+FF+H+T+E	134	-45	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MMAC	980	D+L+FF+H+T+E	-242	-45	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MTOM	915	D+L+FF+H+T+E	82	-3	D+L+FF+H+T+E	89	1.96	-	-	-	-	-		
							MCOM	902	D+L+FF+H+T+E	-40	-4	D+L+FF+H+T+E	89	1.96	-	-	-	-	-		
							MMAT	444	D+L+FF+H+T+E	1	-21	D+L+FF+H+T+E	89	1.96	-	-	-	-	-		
							MMAC	396	D+L+FF+H+T+E	-16	-24	D+L+FF+H+T+E	89	1.96	-	-	-	-	-		
							MTOM	644	D+L+FF+H+T+E	167	-66	D+L+FF+H+T+E	89	4.68	-	-	-	-	-		
							MCOM	459	D+L+FF+H+T+E	-259	-57	D+L+FF+H+T+E	89	4.68	-	-	-	-	-		
							MMAT	691	D+L+FF+H+T+E	143	-117	D+L+FF+H+T+E	89	4.68	-	-	-	-	-		
							MMAC	452	D+L+FF+H+T+E	-66	-112	D+L+FF+H+T+E	89	4.68	-	-	-	-	-		
		MTOM	923	D+L+FF+H+T+E	292	-38	D+L+FF+H+T+E	92	0.24	-	-	-	-	-							
		MCOM	923	D+L+FF+H+T+E	-303	-12	D+L+FF+H+T+E	92	0.24	-	-	-	-	-							
		MMAT	1135	D+L+FF+H+T+E	266	-39	D+L+FF+H+T+E	92	0.24	-	-	-	-	-							
		MMAC	1135	D+L+FF+H+T+E	-48	-39	D+L+FF+H+T+E	92	0.24	-	-	-	-	-							
		MTOM	1147	D+L+FF+H+T+E	230	18	D+L+FF+H+T+E	31	4.68	-	-	-	-	-							
		MCOM	1127	D+L+FF+H+T+E	-171	62	D+L+FF+H+T+E	31	4.68	-	-	-	-	-							
		MMAT	697	D+L+FF+H+T+E	48	115	D+L+FF+H+T+E	31	4.68	-	-	-	-	-							
		MMAC	697	D+L+FF+H+T+E	-44	115	D+L+FF+H+T+E	31	4.68	-	-	-	-	-							
		MTOM	-	D+L+FF+H+T+E	360	-103	D+L+FF+H+T+E	28	7.49	-	-	-	-	-	(B)						
		MCOM	-	D+L+FF+H+T+E	-547	107	D+L+FF+H+T+E	28	7.49	-	-	-	-	-	-						
		MMAT	-	D+L+FF+H+T+E	99	-239	D+L+FF+H+T+E	28	7.49	-	-	-	-	-	-						
		MMAC	-	D+L+FF+H+T+E	-151	-239	D+L+FF+H+T+E	28	7.49	-	-	-	-	-	-						
	South (End of North Wall) and North (End of South Wall)	3H-110	Horizontal	3H-110		3H-110	MTOM	980	D+L+FF+H+T+E	292	24	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MCOM	980	D+L+FF+H+T+E	-297	44	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MMAT	1	D+L+FF+H+T+E	110	48	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MMAC	1	D+L+FF+H+T+E	-253	48	D+L+FF+H+T+E	87	0.24	-	-	-	-	-		
							MTOM	1164	D+L+FF+H+T+E	34	5	D+L+FF+H+T+E	59	1.96	-	-	-	-	-		
							MCOM	932	D+L+FF+H+T+E	-38	3	D+L+FF+H+T+E	59	1.96	-	-	-	-	-		
							MMAT	795	D+L+FF+H+T+E	1	22	D+L+FF+H+T+E	59	1.96	-	-	-	-	-		
							MMAC	693	D+L+FF+H+T+E	-19	24	D+L+FF+H+T+E	59	1.96	-	-	-	-	-		
							MTOM	392	1.05D+1.3W+1.3H+1.2T+1.3W	169	5	D+L+FF+H+T+E	59	4.68	-	-	-	-	-		
							MCOM	459	D+L+FF+H+T+E	-239	81	D+L+FF+H+T+E	59	4.68	-	-	-	-	-		
							MMAT	860	D+L+FF+H+T+E	168	131	D+L+FF+H+T+E	59	4.68	-	-	-	-	-		
							MMAC	860	D+L+FF+H+T+E	-186	136	D+L+FF+H+T+E	59	4.68	-	-	-	-	-		
	East (End of North Wall) and West (End of South Wall)	3H-111	Vertical	3H-111		3H-111	MTOM	923	D+L+FF+H+T+E	292	47	D+L+FF+H+T+E	92	0.24	-	-	-	-	-		
							MCOM	923	D+L+FF+H+T+E	-303	26	D+L+FF+H+T+E	92	0.24	-	-	-	-	-		
							MMAT	1135	D+L+FF+H+T+E	249	59	D+L+FF+H+T+E	92	0.24	-	-	-	-	-		
							MMAC	1135	D+L+FF+H+T+E	-124	59	D+L+FF+H+T+E	92	0.24	-	-	-	-	-		
							MTOM	-	-	-	-	-	-	-	-	-	-	-	-	-	
							MCOM	-	-	-	-	-	-	-	-	-	-	-	-	-	-
							MMAT	-	-	-	-	-	-	-	-	-	-	-	-	-	-
							MMAC	-	-	-	-	-	-	-	-	-	-	-	-	-	-
							MTOM	289	D+L+FF+H+T+E	41	-304	D+L+FF+H+T+E	-	-	-	-	-	-	-	-	-
							MCOM	294	D+L+FF+H+T+E	-60	-19	D+L+FF+H+T+E	-	-	-	-	-	-	-	-	-
							MMAT	273	D+L+FF+H+T+E	1	-395	D+L+FF+H+T+E	-	-	-	-	-	-	-	-	-
							MMAC	273	D+L+FF+H+T+E	-42	-395	D+L+FF+H+T+E	-	-	-	-	-	-	-	-	-

[illegible]

Table 3H.6-7: Results of UHS/RSW Pump House Concrete Wall Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Drawing Number (1)	Reinforcement Zone Number (2)	Maximum Force (3)	Axial and Flexure Loads				In-Plane Shear Loads		Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Results	
							Load Combination	Axial (k) (kips/ft)	Flexure (k) (kips-ft)	Load Combination	Shear (k) (kips/ft)	Horizontal Section		Vertical Section						
												Transverse Shear Force (kip/ft)		Corresponding Axial Force (kip/ft)	Transverse Shear Force (kip/ft)	Corresponding Axial Force (kip/ft)				
Cooling Tower West Wall (Cont'd)	9	East (front)	Horizontal	3H-6-119	14-L	MTM	185	D+L+F+H+T+E	42	228	31	D+L+F+H+T+E	-	-	-	-	-	-		
						MCCM	220	D+L+F+H+T+E	-62	269										
						MMAT	220	D+L+F+H+T+E	3	299										
						MMAC	220	D+L+F+H+T+E	-62	269										
						MTM	210	D+L+F+H+T+E	133	139										
						MCCM	29	D+L+F+H+T+E	-172	979	35	D+L+F+H+T+E	-	-	-	-	-	-		
	8	East (front)	Vertical	3H-6-120	24-L	MMAT	29	D+L+F+H+T+E	94	1484										
						MMAC	29	D+L+F+H+T+E	-16	1484										
						MTM	222	D+L+F+H+T+E	35	964										
						MCCM	55	D+L+F+H+T+E	-119	56	112	D+L+F+H+T+E	-	-	-	-	-	-		
						MMAT	214	D+L+F+H+T+E	3	248										
						MMAC	205	D+L+F+H+T+E	-37	260										
Cooling Tower Island Wall (Cont'd)	8	East (front)	Vertical	3H-6-120	24-L	MTM	205	D+L+F+H+T+E	125	544										
						MCCM	220	D+L+F+H+T+E	-295	421	112	D+L+F+H+T+E	-	-	-	-	-	-		
						MMAT	29	D+L+F+H+T+E	7	1187										
						MMAC	30	D+L+F+H+T+E	-166	1251										
	8	Transverse (Horizontal and Vertical)	3H-6-120A	24-T	-	-	-	-	-	-	-	-	-	177	-20	124	9	0.80		
					-	-	-	-	-	-	-	-	-	-	-	-	-	40	0.31	
					-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
					-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
					-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
					-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Cooling Tower Island Wall	2	East and West	Horizontal	3H-6-121	24-L	MTM	2427	D+L+F+H+T+E	83	-116	30	D+L+F+H+T+E	-	-	-	-	-	-		
						MCCM	1897	D+L+F+H+T+V+W	-117	-11										
						MMAT	2427	D+L+F+H+T+E	19	-136										
						MMAC	2427	D+L+F+H+T+E	-9	-139										
						MTM	2633	D+L+F+H+T+E	378	89										
						MCCM	2426	D+L+F+H+T+E	-232	-60	44	D+L+F+H+T+E	-	-	-	-	-	-	-	-
	2	East and West	Vertical	3H-6-122	24-L	MMAT	2426	D+L+F+H+T+E	61	-126										
						MMAC	2426	D+L+F+H+T+E	-4	-126										
						MTM	2426	D+L+F+H+T+E	31	23										
						MCCM	2426	D+L+F+H+T+E	-67	-30	44	D+L+F+H+T+E	-	-	-	-	-	-	-	-
						MMAT	2461	D+L+F+H+T+E	2	-64										
						MMAC	1958	D+L+F+H+T+E	-49	-66										
2	Vertical	3H-6-122	24-L	MTM	2597	1.05D+1.3L+1.3M+1.27+1.3W	211	2												
				MCCM	2633	D+L+F+H+T+E	-220	-54	44	D+L+F+H+T+E	-	-	-	-	-	-	-	-		
				MMAT	1520	D+L+F+H+T+E	31	-147												
				MMAC	1520	D+L+F+H+T+E	-63	-147												
				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
				3H-6-122A	24-T	-	-	-	-	-	-	-	-	-	-	15	128	11	270	0.80

Notes:

(1) The reinforcement layout drawings show the various zones used to define the minimum reinforcement that will be provided based on finite element analysis results. Actual provided reinforcement based on final rebar layout may exceed the reported provided reinforcement and the zones with higher reinforcement may be extended beyond their reported boundaries.

(2) Each reinforcement layout drawing is divided into reinforcement zones. The reinforcement zone naming convention is as follows: "H" = horizontal, "V" = vertical, "T" = transverse reinforcement.

(3) The maximum tension (MTCA) and compression (MCCM) axial forces are provided with the corresponding moment from the same load combination. The minimum moment that has a corresponding compression (MMAT) in the same load combination and the maximum moment that has a corresponding tension (MMAC) in the same load combination are also provided. For zones where axial tension or axial compression does not occur for any load combination, dashes are input into the corresponding cell.

(4) Negative axial load is compression and positive axial load is tension. Negative moment applies tension to the top face of the shell element and positive moment applies tension to the bottom face of the shell element.

(5) The reported in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

(6) NOT USED.

(7) The Pump House Operating Floor and Roof Deck includes the metal decking (2.5 inches).

(8) For certain areas of the structure, the standard element post-processing methods were too conservative. For such cases, detailed manual design was performed and the design forces determined by the detailed manual design are provided in the table.

(9) The transverse reinforcement for the UHS Beam and RSW Pump House Brackets is spaced with a maximum center-to-center spacing of 4".

Table 3H.6-8: Results of UHS/RSW Pump House Concrete Slab Design

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Drawing Number (1)	Reinforcement Zone Number (2)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks				
								Axial and Flexure Loads			In-Plane Shear Loads			Load Combination	Subtotal Section					Vertical Section			
								Load Combination	Area (ft ²) (kip/ft)	Flexure (ft) (kip/ft)	Shear (ft) (kip/ft)	Shear (ft) (kip/ft)			Shear (ft) (kip/ft)	Shear (ft) (kip/ft)	Shear (ft) (kip/ft)						
																				Transverse Shear Force (kip/ft)	Corresponding Axial Force (kip/ft)	Transverse Shear Force (kip/ft)	Corresponding Axial Force (kip/ft)
North-South	East/West			3H-6-123	1-1/4		MTCM	9644	1.05D+1.3L+1.05F+1.2W+1.27+1.3W	300	-17												
							MCN1	9637	D+1.5F+H+T+E	-66	-79												
							MAAT	13467	D+1.5F+H+T+E	7	-650												
							MMAC	13467	1.4D+1.3L+1.3F+1.3W+1.3W	-16	-1027												
							MTCM	13481	D+1.5F+H+T+E	227	-30												
							MCN1	13549	D+1.5F+H+T+E	-181	-175												
				2-1/4			MAAT	10584	1.4D+1.4F+1.3W+1.3W	1	-776												
							MMAC	10583	1.4D+1.3L+1.3F+1.3W+1.3W	-104	-1213												
							MTCM	13535	D+1.5F+H+T+E	303	-113												
							MCN1	13490	D+1.5F+H+T+E	-135	-39												
							MAAT	13467	D+1.5F+H+T+E	93	-1036												
							MMAC	13467	1.4D+1.3L+1.3F+1.3W+1.3W	-31	-1355												
North-South	North/South			3H-6-124	2-1/4		MTCM	9651	D+1.5F+H+T+E	40	-265												
							MCN1	9669	D+1.5F+H+T+E	-107	-208												
							MAAT	9614	D+1.5F+H+T+E	9	-493												
							MMAC	9614	1.4D+1.3L+1.3F+1.3W+1.3W	-23	-1101												
							MTCM	13560	1.05D+1.3L+1.05F+1.3W+1.27+1.3W	318	-152												
							MCN1	13470	D+1.5F+H+T+E	-155	-434												
				3-1/4			MAAT	13470	D+1.5F+H+T+E	16	-817												
							MMAC	13470	D+1.5F+H+T+E	-100	-1305												
							MTCM	13470	1.4D+1.3L+1.3F+1.3W+1.3W	-41	-1046												
							MTCM	9645	1.05D+1.3L+1.05F+1.3W+1.27+1.3W	373	142												
							MCN1	9637	D+1.5F+H+T+E	-79	23												
							MAAT	13470	1.4D+1.4F+1.3W+1.3W	15	1047												
Bottom	East/West			3H-6-125	2-1/4		MTCM	10485	D+1.5F+H+T+E	64	307												
							MCN1	10549	D+1.5F+H+T+E	-181	377												
							MAAT	10303	1.4D+1.4F+1.3W+1.3W	0	1068												
							MMAC	10303	D+1.5F+H+T+E	-100	1305												
							MTCM	10584	D+1.5F+H+T+E	74	519												
							MCN1	10517	D+1.5F+H+T+E	-199	2116												
				3-1/4			MAAT	10515	1.4D+1.4F+1.3W+1.3W	0	1389												
							MMAC	10517	1.4D+1.3L+1.3F+1.3W+1.3W	-164	2525												
							MTCM	10775	D+1.5F+H+T+E	61	494												
							MCN1	10689	D+1.5F+H+T+E	-154	123												
							MAAT	10303	1.4D+1.4F+1.3W+1.3W	1	1113												
							MMAC	10303	1.4D+1.3L+1.3F+1.3W+1.3W	-130	1627												
Bottom	East/West			3H-6-125	1-1/4		MTCM	13481	D+1.5F+H+T+E	227	268												
							MCN1	10685	D+1.5F+H+T+E	-113	87												
							MAAT	13466	D+1.5F+H+T+E	132	936												
							MMAC	13466	1.4D+1.4F+1.3W+1.3W	-8	1191												
							MTCM	13535	D+1.5F+H+T+E	303	209												
							MCN1	13490	D+1.5F+H+T+E	-136	135												
				2-1/4			MAAT	10549	D+1.5F+H+T+E	225	621												
							MMAC	13467	1.4D+1.4F+1.3W+1.3W	-44	665												
							MTCM	10517	D+1.5F+H+T+E	62	449												
							MCN1	9650	D+1.5F+H+T+E	-107	282												
							MAAT	10775	D+1.5F+H+T+E	1	915												
							MMAC	10791	1.4D+1.3L+1.3F+1.3W+1.3W	-143	1999												

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Drawing Number	Reinforcement Zone Number	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
								Axial and Rebar Loads		In-Plane Shear Loads			Horizontal Section		Vertical Section			
								Load Combination	Area (ft ²) (ft ² /ft)	Phase (ft) (ft ² /ft)	Load Combination		Transverse Shear Force (kips/ft)	Corresponding Axial Force (kips/ft)	Transverse Shear Force (kips/ft)	Corresponding Axial Force (kips/ft)		
Pump House Foundation Mat (C-1)	6	Bottom	North-South	3H-5-126	3H-5-126	3H-5-126	MTCM	13552	1.8D+1.3E+1.3W+1.3T+1.3T+1.3W	315	286	D+L+F+H+T+E	50	-	-	-	-	
							MCCM	13470	D+L+F+H+T+E	-155	965	D+L+F+H+T+E	50	-	-	-	-	
							MMAT	13470	D+L+F+H+T+E	9	862	D+L+F+H+T+E	50	-	-	-	-	
							MMAG	13470	1.4D+1.4F+1.3W+1.7W	465	1182	D+L+F+H+T+E	50	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-126	3H-5-126	3H-5-126	MTCM	13546	D+L+F+H+T+E	49	-16	D+L+F+H+T+E	98	-	-	-	-	
							MCCM	13105	D+L+F+H+T+E	-332	-1	D+L+F+H+T+E	98	-	-	-	-	
							MMAT	13434	1.4D+1.4F+1.3W+1.7W	4	-44	D+L+F+H+T+E	98	-	-	-	-	
							MMAG	13434	1.4D+1.3E+1.3F+1.3W+1.7W	-34	-49	D+L+F+H+T+E	98	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
Pump House Floor SL-15-2 nd	1.75	Bottom	North-South	3H-5-128	3H-5-128	3H-5-128	MTCM	13126	D+L+F+H+T+E	31	-3	D+L+F+H+T+E	87	-	-	-	-	
							MCCM	13080	D+L+F+H+T+E	-264	-4	D+L+F+H+T+E	87	-	-	-	-	
							MMAT	13289	1.4D+1.4F+1.3W+1.7W	0	-32	D+L+F+H+T+E	87	-	-	-	-	
							MMAG	13566	D+L+F+H+T+E	-126	-35	D+L+F+H+T+E	87	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-128	3H-5-128	3H-5-128	MTCM	13046	D+L+F+H+T+E	74	7	D+L+F+H+T+E	87	-	-	-	-	
							MCCM	13105	D+L+F+H+T+E	-332	0	D+L+F+H+T+E	87	-	-	-	-	
							MMAT	13507	1.4D+1.4F+1.3W+1.7W	1	18	D+L+F+H+T+E	87	-	-	-	-	
							MMAG	13570	1.4D+1.3E+1.3F+1.3W+1.7W	-42	19	D+L+F+H+T+E	87	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
UHS Blah Foundation Mat	10	Bottom	North-South	3H-5-130	3H-5-130	3H-5-130	MTCM	13126	D+L+F+H+T+E	31	6	D+L+F+H+T+E	87	-	-	-	-	
							MCCM	13080	D+L+F+H+T+E	-264	4	D+L+F+H+T+E	87	-	-	-	-	
							MMAT	13552	1.4D+1.3E+1.3F+1.3W+1.7W	-103	25	D+L+F+H+T+E	87	-	-	-	-	
							MMAG	13552	1.4D+1.3E+1.3F+1.3W+1.7W	-103	25	D+L+F+H+T+E	87	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-130	3H-5-130	3H-5-130	MTCM	13146	D+L+F+H+T+E	391	-366	D+L+F+H+T+E	187	-	-	-	-	
							MCCM	13149	D+L+F+H+T+E	-261	-241	D+L+F+H+T+E	187	-	-	-	-	
							MMAT	13149	1.4D+1.3E+1.3F+1.3W+1.7W	42	-1266	D+L+F+H+T+E	187	-	-	-	-	
							MMAG	13147	1.4D+1.3E+1.3F+1.3W+1.7W	-40	-1134	D+L+F+H+T+E	187	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
UHS Blah Foundation Mat	10	Bottom	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13197	1.4D+1.3F+1.3W+1.4Fw	606	-377	D+L+F+H+T+E	63	-	-	-	-	
							MCCM	13231	D+L+F+H+T+E	-751	-1499	D+L+F+H+T+E	63	-	-	-	-	
							MMAT	13251	D+L+F+H+T+E	402	-2487	D+L+F+H+T+E	63	-	-	-	-	
							MMAG	13251	1.4D+1.3E+1.3F+1.3W+1.7W	-30	-2443	D+L+F+H+T+E	63	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13199	1.4D+1.3F+1.3W+1.4Fw	602	-472	D+L+F+H+T+E	12	-	-	-	-	
							MCCM	13117	D+L+F+H+T+E	468	-542	D+L+F+H+T+E	12	-	-	-	-	
							MMAT	13119	1.4D+1.3E+1.3F+1.3W+1.7W	77	-3055	D+L+F+H+T+E	12	-	-	-	-	
							MMAG	13119	D+L+F+H+T+E	-17	-3014	D+L+F+H+T+E	12	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
UHS Blah Foundation Mat	10	Bottom	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13191	1.4D+1.3F+1.3W+1.4Fw	447	-1446	D+L+F+H+T+E	16	-	-	-	-	
							MCCM	13124	D+L+F+H+T+E	-239	-261	D+L+F+H+T+E	16	-	-	-	-	
							MMAT	13117	1.4D+1.3E+1.3F+1.3W+1.7W	96	-4406	D+L+F+H+T+E	16	-	-	-	-	
							MMAG	13117	D+L+F+H+T+E	44	-3565	D+L+F+H+T+E	16	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13485	1.4D+1.3F+1.3W+1.4Fw	200	-480	D+L+F+H+T+E	8	-	-	-	-	
							MCCM	13487	D+L+F+H+T+E	-112	-121	D+L+F+H+T+E	8	-	-	-	-	
							MMAT	13463	1.4D+1.3E+1.3F+1.3W+1.7W	171	-1140	D+L+F+H+T+E	8	-	-	-	-	
							MMAG	13553	D+L+F+H+T+E	-25	-4979	D+L+F+H+T+E	8	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
UHS Blah Foundation Mat	10	Bottom	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13558	1.4D+1.3F+1.3W+1.4Fw	602	-370	D+L+F+H+T+E	24	-	-	-	-	
							MCCM	13195	D+L+F+H+T+E	-319	-1322	D+L+F+H+T+E	24	-	-	-	-	
							MMAT	13198	D+L+F+H+T+E	410	-4993	D+L+F+H+T+E	24	-	-	-	-	
							MMAG	13198	D+L+F+H+T+E	-17	-4200	D+L+F+H+T+E	24	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	
		Top	North-South	3H-5-131	3H-5-131	3H-5-131	MTCM	13485	1.4D+1.3F+1.3W+1.4Fw	200	-480	D+L+F+H+T+E	8	-	-	-	-	
							MCCM	13487	D+L+F+H+T+E	-112	-121	D+L+F+H+T+E	8	-	-	-	-	
							MMAT	13463	1.4D+1.3E+1.3F+1.3W+1.7W	171	-1140	D+L+F+H+T+E	8	-	-	-	-	
							MMAG	13553	D+L+F+H+T+E	-25	-4979	D+L+F+H+T+E	8	-	-	-	-	
							-	-	-	-	-	-	-	-	-	-	-	

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Drilling Method (ft)	Reinforcement Zone Number (ft)	Maximum Forces (ft)	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks			
							Axial and Flexure Loads		In-Plane Shear Loads			Horizontal Section		Vertical Section						
							Load Combination	Asial (kips/ft)	Flexure (kips-ft/ft)	Load Combination		In-plane (kips/ft)	Transverse Shear Zone (kips/ft)	Horizontal Section (kips/ft)	Vertical Section (kips/ft)					
East/West	7-HL	MFCM	1011	1.4D + 1.7F + 1.3H + 1.4E _o	344	-1109														
			MCCM	1011	D + L + F + H + T + E	-146	-728													
			HMAT	1010	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	167	-2618													
			MMAC	1010	D + L + F + H + T + E	-9	-2432													
		MFCM	1016	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	534	-3021														
			MCCM	1016	D + L + F + H + T + E	-307	-1208													
			HMAT	1016	D + L + F + H + T + E	337	-4002													
			MMAC	1016	D + L + F + H + T + E	-19	-3665													
		MFCM	1019	1.4D + 1.7F + 1.3H + 1.4E _o	247	-502														
			MCCM	1017	D + L + F + H + T + E	-172	-508													
			HMAT	1017	D + L + F + H + T + E	90	-1407													
			MMAC	1017	D + L + F + H + T + E	-49	-1407													
	8-HL	MFCM	1017	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	538	-3374														
			MCCM	1017	D + L + F + H + T + E	-340	-1508													
			HMAT	1017	D + L + F + H + T + E	335	-4224													
			MMAC	1017	D + L + F + H + T + E	-10	-4724													
		MFCM	1018	1.4D + 1.7F + 1.3H + 1.4E _o	233	-745														
			MCCM	1018	D + L + F + H + T + E	-160	-693													
			HMAT	1018	D + L + F + H + T + E	191	-2779													
			MMAC	1018	D + L + F + H + T + E	-2	-2846													
		MFCM	1018	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	505	-3582														
			MCCM	1018	D + L + F + H + T + E	-310	-1663													
			HMAT	1018	D + L + F + H + T + E	326	-4418													
			MMAC	1018	D + L + F + H + T + E	-4	-4418													
9-HL	MFCM	1010	1.4D + 1.7F + 1.3H + 1.4E _o	160	-271															
		MCCM	1010	D + L + F + H + T + E	-118	-343														
		HMAT	1010	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	187	-1179														
		MMAC	1010	D + L + F + H + T + E	-6	-968														
	MFCM	1016	1.4D + 1.7F + 1.3H + 1.4E _o	262	-1079															
		MCCM	1016	D + L + F + H + T + E	-127	-643														
		HMAT	1016	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	269	-3584														
		MMAC	1016	D + L + F + H + T + E	-4	-2709														
	MFCM	1017	1.4D + 1.7F + 1.3H + 1.4E _o	174	-179															
		MCCM	1016	D + L + F + H + T + E	-114	-589														
		HMAT	1017	D + L + F + H + T + E	98	-1791														
		MMAC	1017	D + L + F + H + T + E	-5	-1791														
10-HL	MFCM	1019	1.4D + 1.7F + 1.3H + 1.4E _o	244	-638															
		MCCM	1019	D + L + F + H + T + E	-105	-1337														
		HMAT	1019	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	103	-2215														
		MMAC	1019	D + L + F + H + T + E	-5	-1943														
	MFCM	1017	1.4D + 1.7F + 1.3H + 1.4E _o	164	-705															
		MCCM	1025	D + L + F + H + T + E	-98	-41														
		HMAT	1017	1.4D + 1.7L + 1.7F + 1.3H + 1.7H	66	-1289														
		MMAC	1025	D + L + F + H + T + E	-34	-1422														
	MFCM	1025	1.4D + 1.7F + 1.3H + 1.4E _o	232	-751															
		MCCM	1025	D + L + F + H + T + E	-165	-758														
		HMAT	1022	D + L + F + H + T + E	196	-2060														
		MMAC	1022	D + L + F + H + T + E	-9	-2060														

(ft-ft Base Foundation Mat (Cont'd))

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Reinforcement Zone Number	Maximum Forces (k)	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks		
							Axial and Flexure Loads		In-Plane Shear Loads			Load Combination	Horizontal Section		Vertical Section				
							Load Combination	Asial (k) (kips/ft)	Phase (k) (kips/ft)	Load Combination			Transverse Shear Force (k/ft)	Transverse Shear Force (k/ft)	Transverse Shear Force (k/ft)			Transverse Shear Force (k/ft)	
East/West	3Hx5.126				7Hx5.1		MFCA	11635	1.4D + 1.3F + 1.3M + 1.4E ₁	930	-199	-	-	-	-	-	-		
							MCDA	10961	D + L + F + H + T + E	-474	-86	D + L + F + H + T + E	21	-	-	-	-		
							MAWT	15041	1.4D + 1.3F + 1.3M + 1.4E ₂	442	-566	-	-	-	-	-	-		
							MMAC	10041	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	-100	-1191	-	-	-	-	-	-		
							MFCA	4277	1.4D + 1.3F + 1.3M + 1.4E ₃	869	-105	-	-	-	-	-	-		
							MCDA	8338	D + L + F + H + T + E	-740	-47	D + L + F + H + T + E	39	-	-	-	-		
							MAWT	15148	D + L + F + H + T + E	125	-1398	-	-	-	-	-	-		
							MMAC	13148	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	448	-1640	-	-	-	-	-	-		
							MFCA	11956	1.4D + 1.4F + 1.3H + 1.3W	213	-40	-	-	-	-	-	-		
							MCDA	11840	D + L + F + H + T + E	-179	-650	D + L + F + H + T + E	51	-	-	-	-		
							MAWT	15194	D + L + F + H + T + E	94	-1201	-	-	-	-	-	-		
							MMAC	12194	D + L + F + H + T + E	-56	-1236	-	-	-	-	-	-		
North/South	3Hx5.132				7Hx5.1		MFCA	13046	D + L + F + H + T + E	250	-523	-	-	-	-	-	-		
							MCDA	13248	D + L + F + H + T + E	-539	-749	D + L + F + H + T + E	154	-	-	-	-	-	
							MAWT	13248	D + L + F + H + T + E	53	-1003	-	-	-	-	-	-		
							MMAC	12348	D + L + F + H + T + E	-150	-1003	-	-	-	-	-	-		
							MFCA	12085	1.4D + 1.4F + 1.3H + 1.3W	291	-341	-	-	-	-	-	-		
							MCDA	12117	D + L + F + H + T + E	-304	-760	D + L + F + H + T + E	154	-	-	-	-	-	
							MAWT	12097	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	95	-1600	-	-	-	-	-	-		
							MMAC	12117	1.4D + 1.3F + 1.3M + 1.4E ₁	-106	-1552	-	-	-	-	-	-		
							MFCA	12090	1.4D + 1.4F + 1.3H + 1.3W	552	-2097	D + L + F + H + T + E	117	-	-	-	-	-	
							MCDA	12090	D + L + F + H + T + E	-450	-459	D + L + F + H + T + E	117	-	-	-	-	-	
							MAWT	12090	D + L + F + H + T + E	252	-2652	-	-	-	-	-	-		
							MMAC	12090	D + L + F + H + T + E	-23	-2795	-	-	-	-	-	-		
East/West	3Hx5.132				7Hx5.1		MFCA	12106	1.4D + 1.4F + 1.3H + 1.3W	404	-2505	-	-	-	-	-	-		
							MCDA	12109	D + L + F + H + T + E	-475	-724	D + L + F + H + T + E	154	-	-	-	-	-	-
							MAWT	12109	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	395	-3394	-	-	-	-	-	-	-	
							MMAC	12109	D + L + F + H + T + E	-6	-3603	-	-	-	-	-	-	-	
							MFCA	13137	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	699	-4489	-	-	-	-	-	-	-	
							MCDA	13352	D + L + F + H + T + E	-522	-512	D + L + F + H + T + E	149	-	-	-	-	-	-
							MAWT	13137	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	696	-4489	-	-	-	-	-	-	-	
							MMAC	13137	D + L + F + H + T + E	-3	-3699	-	-	-	-	-	-	-	
							MFCA	11956	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	274	-1401	-	-	-	-	-	-	-	
							MCDA	11920	D + L + F + H + T + E	-158	-271	D + L + F + H + T + E	60	-	-	-	-	-	-
							MAWT	11945	D + L + F + H + T + E	99	-2775	-	-	-	-	-	-	-	
							MMAC	11467	D + L + F + H + T + E	-2	-3520	-	-	-	-	-	-	-	
North/South	3Hx5.132				7Hx5.1		MFCA	11776	1.4D + 1.3F + 1.3M + 1.4E ₁	257	-1507	-	-	-	-	-	-		
							MCDA	11652	D + L + F + H + T + E	-191	-231	D + L + F + H + T + E	61	-	-	-	-	-	-
							MAWT	11656	D + L + F + H + T + E	133	-3670	-	-	-	-	-	-	-	
							MMAC	11656	D + L + F + H + T + E	-44	-3336	-	-	-	-	-	-	-	
							MFCA	11756	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	324	-454	-	-	-	-	-	-	-	
							MCDA	11935	D + L + F + H + T + E	-211	-36	D + L + F + H + T + E	86	-	-	-	-	-	-
							MAWT	11779	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	274	-2527	-	-	-	-	-	-	-	
							MMAC	11779	D + L + F + H + T + E	-34	-1771	-	-	-	-	-	-	-	
							MFCA	11775	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	520	-2762	-	-	-	-	-	-	-	
							MCDA	11775	D + L + F + H + T + E	-262	-560	D + L + F + H + T + E	86	-	-	-	-	-	-
							MAWT	11790	1.4D + 1.3L + 1.3F + 1.3H + 1.1W	404	-2045	D + L + F + H + T + E		-	-	-	-	-	-
							MMAC	11776	D + L + F + H + T + E	-22	-1088	-	-	-	-	-	-	-	

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Driveway Number (ft)	Door Number (ft)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (psi ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (psi ft)	Remarks
								Axial and Flexure Loads		In-Plane Shear Loads			Multistage Section		Vertical Section			
								Load Combination	Phase (ft) (psi ft)	Load Combination	Phase (ft) (psi ft)		Transverse Shear Zone (psi ft)	Multistage Section (psi ft)	Transverse Shear Zone (psi ft)	Vertical Section (psi ft)		
13'-6" L	13'-6" L	13'-6" L	North-South	13'-6" L	13'-6" L	13'-6" L	13'-6" L	1.4D + 1.7L + 1.7W + 1.7E	251	-245	D + L + F + H + T + E	67	-	-	-	-	-	
								D + L + F + H + T + E	-202	-52	-	-	-	-	-	-	-	
								D + L + F + H + T + E	65	-63	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-41	-63	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	342	-182	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-173	-432	-	-	-	-	-	-	-	
								D + L + F + H + T + E	95	-2785	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-8	-2785	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	447	-474	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-231	-43	-	-	-	-	-	-	-	
								D + L + F + H + T + E	161	-2086	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-30	-2086	-	-	-	-	-	-	-	
15'-6" L	15'-6" L	15'-6" L	North-South	15'-6" L	15'-6" L	15'-6" L	15'-6" L	1.4D + 1.7L + 1.7W + 1.7E + 1.7W	687	-5307	D + L + F + H + T + E	117	-	-	-	-	-	
								D + L + F + H + T + E	-203	-371	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	675	-5331	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-4	-3627	-	-	-	-	-	-	-	
								D + L + F + H + T + E	300	-343	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-284	-43	-	-	-	-	-	-	-	
								D + L + F + H + T + E	78	-962	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-121	-1085	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	364	-1378	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-177	-328	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	227	-3419	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-4	-3071	-	-	-	-	-	-	-	
19'-6" L	19'-6" L	19'-6" L	North-South	19'-6" L	19'-6" L	19'-6" L	19'-6" L	1.4D + 1.7L + 1.7W + 1.7E + 1.7W	724	-5438	D + L + F + H + T + E	164	-	-	-	-	-	
								D + L + F + H + T + E	-207	-659	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	720	-5508	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-3	-4321	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	361	-488	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-176	-159	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	260	-1488	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-21	-1222	-	-	-	-	-	-	-	
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	308	-479	-	-	-	-	-	-	-	
								D + L + F + H + T + E	-124	-548	-	-	-	-	-	-	-	
								D + L + F + H + T + E	107	-2582	-	-	-	-	-	-	-	
								D + L + F + H + T + E	0	-2085	-	-	-	-	-	-	-	
21'-6" L	21'-6" L	21'-6" L	North-South	21'-6" L	21'-6" L	21'-6" L	21'-6" L	1.4D + 1.7L + 1.7W + 1.7E + 1.7W	524	-2690	D + L + F + H + T + E	96	-	-	-	-	-	
								D + L + F + H + T + E	-282	-1088	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	308	-2548	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	-16	-3017	-	-	-	-	-	-	-	-
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	192	-864	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	-91	-275	-	-	-	-	-	-	-	-
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	71	-1350	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	-3	-1034	-	-	-	-	-	-	-	-
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	171	-342	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	-168	-422	-	-	-	-	-	-	-	-
								1.4D + 1.7L + 1.7W + 1.7E + 1.7W	3	-1518	-	-	-	-	-	-	-	-
								D + L + F + H + T + E	-2	-1482	-	-	-	-	-	-	-	-

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thicknss (ft)	Face	Direction	Reinforcement Zone Number (ft)	Maximum Forces (ft)	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
						Axial and Flexure Loads		In-Plane Shear Loads			Transverse Shear Zone		Horizontal Section			
						Load Combination	Asial (d) (in ² /ft)	Phase (d) (in ² /ft)	Load Combination		Transverse Shear Zone (in ² /ft)	Horizontal Section (in ² /ft)	Transverse Shear Zone (in ² /ft)	Horizontal Section (in ² /ft)		
Top	North-South	3H.6.132		24-H		MT2M	5064	1.4D + 1.3F + 1.3W + 1.4E	956	-118						
						MC2M	5041	D + L + F + H + T + E	467	-76	D + L + F + H + T + E	29				
						HA0T	8318	1.4D + 1.3F + 1.3W + 1.4E	427	-1651						
						MA0C	6318	1.4D + 1.3F + 1.3W + 1.3W	-100	-1322						
						MT2M	13149	D + L + F + H + T + E	381	843						
						MC2M	13149	D + L + F + H + T + E	381	564						
						HA0T	13149	D + L + F + H + T + E	250	1101						
						MA0C	6344	1.4D + 1.3F + 1.3W + 1.3W	-10	959						
						MT2M	13205	1.4D + 1.3F + 1.3W + 1.4E	936	447						
						MC2M	13251	D + L + F + H + T + E	701	606						
24-H						HA0T	13150	1.4D + 1.3F + 1.3W + 1.3W	23	1666						
						MA0C	13150	1.4D + 1.3F + 1.3W + 1.4E	-14	1537						
						MT2M	12504	1.4D + 1.3F + 1.3W + 1.4E	956	74						
						MC2M	12117	D + L + F + H + T + E	458	600						
						HA0T	11081	D + L + F + H + T + E	13	2884						
						MA0C	11081	D + L + F + H + T + E	-48	2684						
						MT2M	11025	1.4D + 1.3F + 1.3W + 1.4E	201	661						
						MC2M	12130	D + L + F + H + T + E	237	109						
						HA0T	8449	1.4D + 1.3F + 1.3W + 1.3W	59	1417						
						MA0C	6549	1.4D + 1.3F + 1.3W + 1.4E	-70	1320						
Bottom						MT2M	12123	1.4D + 1.3F + 1.3W + 1.4E	229	665						
						MC2M	12124	D + L + F + H + T + E	420	1608						
						HA0T	11017	D + L + F + H + T + E	14	2684						
						MA0C	11017	D + L + F + H + T + E	-49	2484						
						MT2M	11664	1.4D + 1.3F + 1.3W + 1.3W	107	210						
						MC2M	11666	D + L + F + H + T + E	-113	509						
						HA0T	11664	D + L + F + H + T + E	26	1588						
						MA0C	11664	D + L + F + H + T + E	-29	1588						
						MT2M	11658	D + L + F + H + T + E	426	947						
						MC2M	11658	D + L + F + H + T + E	-310	2798						
24-H						HA0T	11658	D + L + F + H + T + E	223	3328						
						MA0C	11658	D + L + F + H + T + E	-102	3328						
						MT2M	11021	1.4D + 1.3F + 1.3W + 1.4E	327	278						
						MC2M	11511	D + L + F + H + T + E	148	1171						
						HA0T	11648	D + L + F + H + T + E	60	2487						
						MA0C	11648	D + L + F + H + T + E	-57	2387						
						MT2M	11764	D + L + F + H + T + E	346	1776						
						MC2M	11764	D + L + F + H + T + E	-307	2680						
						HA0T	11764	D + L + F + H + T + E	229	3272						
						MA0C	11764	D + L + F + H + T + E	-42	3072						
10-H						MT2M	11775	1.4D + 1.3F + 1.3W + 1.3W	210	1598						
						MC2M	11763	D + L + F + H + T + E	-170	1119						
						HA0T	11762	D + L + F + H + T + E	67	2273						
						MA0C	11762	D + L + F + H + T + E	-11	2273						
						MT2M	11693	1.4D + 1.3F + 1.3W + 1.4E	372	357						
						MC2M	11697	D + L + F + H + T + E	-172	156						
						HA0T	11143	D + L + F + H + T + E	30	2215						
						MA0C	11143	D + L + F + H + T + E	-44	2215						

Table 3H.6.8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Driveway Number (1)	Reinforcement Zone Number (2)	Maximum Forces (3)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks
									Axial and Flexure Loads		In-Plane Shear Loads			Horizontal Section		Vertical Section			
									Load Contribution	Area (in ² /ft)	Load Contribution	Area (in ² /ft)		Transverse Shear Zone (ft ² /ft)	Horizontal Section (ft ² /ft)	Transverse Shear Zone (ft ² /ft)	Vertical Section (ft ² /ft)		
									Load Contribution	Area (in ² /ft)	Load Contribution	Area (in ² /ft)		Transverse Shear Zone (ft ² /ft)	Horizontal Section (ft ² /ft)	Transverse Shear Zone (ft ² /ft)	Vertical Section (ft ² /ft)		
UHS Base/Foundation Mat (Cont'd)	10	Bottom			3H.6.8.3	13-HL	MCCM	1407	D+L+F+H+E	343	2206	-	-	-	-	-	-	-	-
							MCCM	1407	D+L+F+H+E	-340	3302	-	-	-	-	-	-	-	-
							MMAT	1407	D+L+F+H+E	238	3436	-	-	-	-	-	-	-	-
							MMAC	1407	D+L+F+H+E	-103	3436	-	-	-	-	-	-	-	-
							MCCM	10084	1.4D+1.3T+1.3H+1.4E	217	454	-	-	-	-	-	-	-	-
							MCCM	10104	D+L+F+H+E	-173	1025	-	-	-	-	-	-	-	-
							MMAT	10090	D+L+F+H+E	89	1891	-	-	-	-	-	-	-	-
							MMAC	10080	D+L+F+H+E	-34	1891	-	-	-	-	-	-	-	-
							MCCM	11545	D+L+F+H+E	333	1780	-	-	-	-	-	-	-	-
							MCCM	11565	D+L+F+H+E	-310	2419	-	-	-	-	-	-	-	-
							MMAT	11245	D+L+F+H+E	212	3412	-	-	-	-	-	-	-	-
							MMAC	11245	D+L+F+H+E	-114	3412	-	-	-	-	-	-	-	-
							MCCM	11651	1.4D+1.3L+1.3T+1.3H+1.3W	192	543	-	-	-	-	-	-	-	-
							MCCM	11548	D+L+F+H+E	-121	461	-	-	-	-	-	-	-	-
							MMAT	9042	1.4D+1.3L+1.3T+1.3H+1.3W	1	1384	-	-	-	-	-	-	-	-
							MMAC	8524	1.4D+1.4E+1.7H+1.7W	-12	1514	-	-	-	-	-	-	-	-
UHS Base/Foundation Mat (Cont'd)	10	Bottom			3H.6.8.4	14-HL	MCCM	18912	1.4D+1.3T+1.3H+1.4E	233	119	-	-	-	-	-	-	-	
							MCCM	11363	D+L+F+H+E	-165	115	-	-	-	-	-	-	-	-
							MMAT	8114	1.4D+1.4E+1.7H+1.7W	42	1791	-	-	-	-	-	-	-	-
							MMAC	8119	1.4D+1.3T+1.3H+1.4E	-33	1636	-	-	-	-	-	-	-	-
							MCCM	18916	1.4D+1.3T+1.3H+1.4E	933	496	-	-	-	-	-	-	-	-
							MCCM	11555	D+L+F+H+E	-484	223	-	-	-	-	-	-	-	-
							MMAT	4588	1.4D+1.4E+1.7H+1.7W	21	1827	-	-	-	-	-	-	-	-
							MMAC	6530	1.4D+1.3T+1.3H+1.4E	-20	1789	-	-	-	-	-	-	-	-
							MCCM	4878	1.4D+1.3T+1.3H+1.4E	904	132	-	-	-	-	-	-	-	-
							MCCM	8338	D+L+F+H+E	-740	134	-	-	-	-	-	-	-	-
							MMAT	4588	1.4D+1.4E+1.7H+1.7W	9	1862	-	-	-	-	-	-	-	-
							MMAC	4586	1.4D+1.3T+1.3H+1.4E	-23	1848	-	-	-	-	-	-	-	-
							MCCM	18906	1.4D+1.4E+1.7H+1.7W	219	187	-	-	-	-	-	-	-	-
							MCCM	11640	D+L+F+H+E	-162	222	-	-	-	-	-	-	-	-
							MMAT	14566	1.4D+1.4E+1.7H+1.7W	23	1784	-	-	-	-	-	-	-	-
							MMAC	14566	1.4D+1.3T+1.3H+1.4E	-96	1123	-	-	-	-	-	-	-	-
UHS Base/Foundation Mat (Cont'd)	10	Bottom			3H.6.8.5	15-HL	MCCM	18927	1.4D+1.4E+1.7H+1.7W	256	38	-	-	-	-	-	-	-	
							MCCM	12110	D+L+F+H+E	-354	1522	-	-	-	-	-	-	-	-
							MMAT	12111	D+L+F+H+E	26	1889	-	-	-	-	-	-	-	-
							MMAC	12111	D+L+F+H+E	-162	1782	-	-	-	-	-	-	-	-
							MCCM	13246	D+L+F+H+E	250	806	-	-	-	-	-	-	-	-
							MCCM	13246	D+L+F+H+E	-539	185	-	-	-	-	-	-	-	-
							MMAT	11519	D+L+F+H+E	101	2223	-	-	-	-	-	-	-	-
							MMAC	11519	D+L+F+H+E	-93	2223	-	-	-	-	-	-	-	-
							MCCM	11573	1.4D+1.3L+1.3T+1.3H+1.3W	202	415	-	-	-	-	-	-	-	-
							MCCM	11523	D+L+F+H+E	-95	537	-	-	-	-	-	-	-	-
							MMAT	13208	1.4D+1.4E+1.7H+1.7W	2	1491	-	-	-	-	-	-	-	-
							MMAC	13206	1.4D+1.4E+1.7H+1.7W	-9	1488	-	-	-	-	-	-	-	-
							MCCM	11681	1.4D+1.4E+1.7H+1.7W	304	751	-	-	-	-	-	-	-	-
							MCCM	11596	D+L+F+H+E	-389	1847	-	-	-	-	-	-	-	-
							MMAT	11698	D+L+F+H+E	68	3289	-	-	-	-	-	-	-	-
							MMAC	11698	D+L+F+H+E	-26	3289	-	-	-	-	-	-	-	-

Table 3H.6-8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

[illegible]

Table 3H.6-8: Results of UHS/RSW Pump House Concrete Slab Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout (ft)	Reinforcement Zone Number ⁽²⁾	Maximum Forces ⁽³⁾	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Provided (in ² /ft)	Transverse Shear Design Loads				Transverse Shear Reinforcement Provided (in ² /ft)	Remarks	
							Axial and Flexure Loads		In-Plane Shear Loads			Horizontal Section		Vertical Section				
							Load Combination	Axial (kip/ft)	Flexure (kip-ft)	Load Combination		In-plane (kip/ft)	Load Combination		Load Combination			
													Transverse Shear (kip/ft)	Transverse Shear (kip/ft)	Transverse Shear (kip/ft)			Transverse Shear (kip/ft)

Notes:

(1) The reinforcement layout drawings show the minimum reinforcement that will be provided based on finite element analysis results. Actual provided reinforcement based on final slab layout may exceed the reported provided reinforcement and the zones with higher reinforcement may be extended beyond their reported boundaries.

(2) Each reinforcement layout drawing is divided into reinforcement zones. The reinforcement zone naming convention is as follows: "T" = vertical, "L" = horizontal, "V" = vertical, "H" = horizontal, "VH" = transverse reinforcement.

(3) The maximum tension (MTCM) and compression (MCCM) axial forces are provided with the corresponding moment from the same load combination. The maximum moment that has a corresponding tension (MMT) or the same load combination and the maximum moment that has a corresponding compression (MMC) is the same load combination are also provided. For zones where either axial tension or axial compression does not occur for any load combination, dashes are listed in the corresponding cell.

(4) Negative axial load is compression and positive axial load is tension. Negative moment applies tension to the top face of the slab element and positive moment applies tension to the bottom face of the slab element.

(5) The reported in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

(6) NOT USED.

(7) The Pump House Operating Floor and Roof slab thickness includes the metal decking (2.5 inches).

(8) For certain areas of the structure, the standard element post-processing methods were too conservative. For such cases, detailed manual design was performed and the design forces determined by the detailed manual design are provided in the table.

(9) The transverse reinforcement for the UHS Slab and RSW Pump House Buttresses is spaced with a maximum center-to-center spacing of 4".

Table 3H.6-9: Results of UHS/RSW Pump House Beams and Columns Design

Location	Item	Critical Element Number	Load Combination	Maximum Forces	Design Loads				Reinforcement			Remarks		
					Axial (kips)	Moments (ft-kips)		Shear (kips)	Longitudinal	Transverse				
						M2	M3			Torsion	V2		V3	Provided (in)
UHS Basin	5' x 5' Columns	516	1.4D+1.7L+1.7F+1.7H+1.7W	Maximum axial compression with corresponding forces	-3587	-1473	904	-	-	-	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	Local Axis definition: 1 = vertical 2 = east-west 3 = north-south Transverse reinforcement includes one closed loop which accounts for two legs in each direction.
		487	D+LoF+H+To+E'	Maximum axial tension with corresponding forces	348	1148	465	-	-	-	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		510	D+LoF+H+To+E'	Maximum M2 moment with corresponding forces	-1096	-9127	1990	-	-	-	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		506	D+LoF+H+To+E'	Maximum M3 moment with corresponding forces	-630	834	7298	-	-	-	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		506	D+LoF+H+To+E'	Maximum V2	-	-	-	-	212	-	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		510	D+LoF+H+To+E'	Maximum V3	-	-	-	-	-	-278	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		505	D+LoF+H+To+E'	Maximum Torsion	-	-	-	-	-	452	148.5	7 #5 @ 4" O.C	7 #5 @ 4" O.C	
		518	1.4D+1.7L+1.7F+1.7H+1.7W	Maximum axial compression with corresponding forces	-4746	-2484	822	-	-	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
		497	D+LoF+H+To+E'	Maximum axial tension with corresponding forces	645	2639	2900	-	-	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
		496	D+LoF+H+To+E'	Maximum M2 moment with corresponding forces	-2509	-13456	-10148	-	-	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
5' x 12' Columns	5' x 12' Columns	518	D+LoF+H+To+E'	Maximum M3 moment with corresponding forces	-3435	3346	30990	-	-	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	Local Axis definition: 1 = vertical 2 = east-west 3 = north-south Transverse reinforcement includes one closed loop which accounts for two legs in each direction.
		518	D+LoF+H+To+E'	Maximum V2	-	-	-	-	453	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
		496	D+LoF+H+To+E'	Maximum V3	-	-	-	-	-	-398	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
		497	D+LoF+H+To+E'	Maximum Torsion	-	-	-	-	-980	-	175.5	13 #5 @ 4" O.C	7 #5 @ 4" O.C	
		16	D+LoF+H+To+E'	Maximum axial compression with corresponding forces	-3313	-2668	-3215	-	-	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
		16	D+LoF+H+To+E'	Maximum axial tension with corresponding forces	5158	1054	2155	-	-	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
		36	D+LoF+H+To+E'	Maximum M2 moment with corresponding forces	947	-6596	44	-	-	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
		16	D+LoF+H+To+E'	Maximum M3 moment with corresponding forces	-1848	2332	6466	-	-	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
		16	D+LoF+H+To+E'	Maximum V2	-	-	-	-	683	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
		36	D+LoF+H+To+E'	Maximum V3	-	-	-	-	-	798	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	
4' x 4'-0" Beams	4' x 4'-0" Beams	403	D+LoF+H+To+E'	Maximum Torsion	-	-	-	-	698	-	155.16	8 #5 @ 4" O.C	6 #5 @ 4" O.C	

Table 3H.7-1: Results of DGFOT Concrete Design

Location	Thickness (ft)	Face	Direction	Reinforcement Layout Drawing Number (ft)	Reinforcement Zone Number (2)	Maximum Forces (3)	Element	Longitudinal Reinforcement Design Loads					Longitudinal Reinforcement Provisions (ksi/ft)	Transverse Shear Design Forces				Remarks
								Axial and Flexure Loads			In-Plane Shear Loads			Load Combination	Horizontal Section	Vertical Section		
								Loads (1)	Flexure (4)	Phase (5)	In-plane (6)							
												Combination				(ft-kips/ft)	(ft-kips/ft)	
Tunnel Walls	2	Near Side	Horizontal	3H7-11	1-4L	Max. Tension w/ corresponding moment	D + L + H + E (WP)	130	-28	D + L + H + E (WP)	26	4.68	-					
						Max. Compression w/ corresponding moment	D + L + H + E (WP)	-46	-1									
						Max. Moment with axial tension	D + L + H + E (WP)	48	-32									
						Max. Moment with axial compression	D + L + H + E (WP)	-1	-28									
						Max. Tension w/ corresponding moment	D + L + H + E (WP)	89	-11	D + L + H + E (WP)	21	3.12	-					
						Max. Compression w/ corresponding moment	D + L + H + E (WP)	-77	-1									
						Max. Moment with axial tension	D + L + H + E (WP)	62	-17									
						Max. Moment with axial compression	D + L + H + E (WP)	-8	-16									
						Max. Tension w/ corresponding moment	D + L + H + E (WP)	108	-28	D + L + H + E (WP)	26	4.68	-					
						Max. Compression w/ corresponding moment	D + L + H + E (WP)	-123	-6									
						Max. Moment with axial tension	D + L + H + E (WP)	104	-28									
						Max. Moment with axial compression	D + L + H + E (WP)	-9	-28									
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + E (WP)	26	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + E (WP)	-129	25															
Max. Moment with axial tension	D + L + H + E (WP)	4	28															
Max. Moment with axial compression	D + L + H + E (WP)	-22	35															
Max. Tension w/ corresponding moment	D + L + H + E	35	-6	D + L + H + W	59	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-96	-16															
Max. Moment with axial tension	D + L + H + E (WP)	14	-46															
Max. Moment with axial compression	D + L + H + E (WP)	-10	-46															
Access Region Walls	2	Far Side	Vertical	3H7-14	1-4L	-	D + L + H + W	-	17	D + L + H + W	59	3.12	-					
						-												
						-												
						-												
						Max. Tension w/ corresponding moment	D + L + H + W	35	-6	D + L + H + E (WP)	34	3.12	-					
						Max. Compression w/ corresponding moment	D + L + H + W	-96	-16									
						Max. Moment with axial tension	D + L + H + E (WP)	14	-46									
						Max. Moment with axial compression	D + L + H + E (WP)	-10	-46									
						-				D + L + H + W	182	3.12	-					
						-												
						-												
						-												
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		
-																		
Max. Tension w/ corresponding moment	D + L + H + W	109	0	D + L + H + W	182	3.12	-											
Max. Compression w/ corresponding moment	D + L + H + W	-129	25															
Max. Moment with axial tension	D + L + H + W	4	28															
Max. Moment with axial compression	D + L + H + W	-22	35															
-				D + L + H + W	182	3.12	-											
-																		
-																		

Table 3H.7-1: Results of DGFOF Concrete Design (Continued)

Location	Thickness (ft)	Face	Direction	Reinforcement Layout	Reinforcing Number (ft)	Reinforcing Zone Number (ft)	Reinforcing Forces (ft)	Element	Longitudinal Reinforcement Design Loads				Longitudinal Reinforcement Ratio (ft ² /ft)	Transverse Shear Design Forces			Remarks															
									Axial and Flexure Loads		In-Plane Shear Loads			Horizontal Section	Vertical Section																	
									Loads (ft)	Flexure (ft-kips / ft)	Reinforcing (ft ² /ft)	Reinforcing (ft ² /ft)																				
Basement	2	Main Side	Horizontal	3H7-15	1-1/L	1-1/L	-	-	D + L + H + W	See Note (10)	D + L + H + E (WP)	27	3.12			-	-															
																		Max. Tension w/ corresponding moment	2504	D + L + H + E (WP)	96	8										
																							Max. Compression w/ corresponding moment	300	D + L + H + E (WP)	117	12					
																												Max. Moment with axial tension	2351	D + L + H + E (WP)	21	
																																Max. Moment with axial compression
																		Max. Tension w/ corresponding moment	2425	D + L + H + E (WP)	20	40										
																							Max. Compression w/ corresponding moment	301	D + L + H + E (WP)	23	6					
																												Max. Moment with axial tension	2433	D + L + H + E (WP)	16	-74
																		Max. Tension w/ corresponding moment	2315	D + L + H + W	13	2										
Max. Compression w/ corresponding moment	300	D + L + H + E (WP)	-36	79																												
					Max. Moment with axial tension	2436	D + L + H + E (WP)	1	56																							
										Max. Moment with axial compression	2406	D + L + H + E (WP)	-20	87																		
Roof of Tunnel	2	Far Side	Horizontal	3H7-17	1-1/L	1-1/L	-	-	-						-	-	-	-	12	12	1	0.44										
										Max. Tension w/ corresponding moment	174	D + L + H + W	124	-11																		
																							Max. Compression w/ corresponding moment	1703	D + L + H + E (WP)	-117	-4					
																												Max. Moment with axial tension	1696	D + L + H + W	53	-36
										Max. Tension w/ corresponding moment	1710	D + L + H + E (WP)	116	7																		
																							Max. Compression w/ corresponding moment	1703	D + L + H + E (WP)	-117	12					
																												Max. Moment with corresponding axial tension	1695	D + L + H + W	10	41
										Max. Tension w/ corresponding moment	1694	D + L + H + W	17	-20																		
Max. Compression w/ corresponding moment	1694	D + L + H + E (WP)	-29	-45																												
					Max. Moment with corresponding axial tension	1710	D + L + H + E (WP)	0	-46																							
															Max. Moment with corresponding axial compression	174	D + L + H + E (WP)	-14	-20													
Max. Tension w/ corresponding moment	1694	D + L + H + W	16	9																												
					Max. Compression w/ corresponding moment	1639	D + L + H + E (WP)	-23	6																							
										Max. Moment with corresponding axial tension	209	D + L + H + E (WP)	2	54																		
															Max. Moment with corresponding axial compression	209	D + L + H + E (WP)	-5	54													
Roof of Tunnel	2	Far Side	Vertical	3H7-18A	1-1/L	1-1/L	-	-	-	-	-	-	-	21						33	22	0.44										
															Max. Tension w/ corresponding moment	1694	D + L + H + W	16	9													
																							Max. Compression w/ corresponding moment	1639	D + L + H + E (WP)	-23	6					
																												Max. Moment with corresponding axial tension	209	D + L + H + E (WP)	2	54

Notes:

(1) The reinforcement layout drawings show the various zones used to define the minimum reinforcement that will be provided based on finite element analysis results. Actual provided reinforcement based on final value input and including development length may exceed the required provided reinforcement and the zones with higher reinforcement may be extended beyond their reported boundaries. The dimensions in the reinforcement drawings are based on the dimensions of the 2D SAP2000 shell elements, which are modeled at the midline of the walls and slabs.

(2) Each reinforcement layout drawing is divided into reinforcement zones. The reinforcement zone naming convention is as follows: "H" = horizontal, "V" = vertical, "L" = longitudinal reinforcement, "T" = transverse reinforcement. For slabs, vertical corresponds to Y-axis and horizontal corresponds to X-axis as shown on Figure 3H.7.1.

(3) The maximum tension and compression axial forces are provided with the corresponding moment from the same load combination. The maximum moment that has a corresponding tension in the same load combination and the maximum moment that has a corresponding compression in the same load combination are also provided.

(4) Negative axial load is compression and positive axial load is tension. Negative moment applies tension to the top face of the shell element and positive moment applies tension to the bottom face of the shell element. For walls or slabs where the same reinforcement is provided on both faces, the moment is shown as absolute values.

(5) The reported in-plane shear is the maximum average in-plane shear along a plane that crosses the longitudinal reinforcement zone.

(6) Not used.

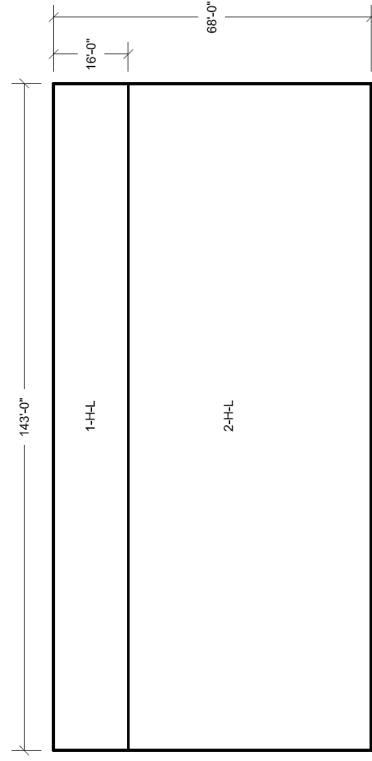
(7) In areas where horizontal and vertical transverse shear zones overlap, the total transverse shear reinforcement to be supplied in the overlapping area is the sum of the transverse reinforcement required from the horizontal and vertical zones.

(8) Openings in the Access Regions have not been included in the Reinforcement Layout Drawings.

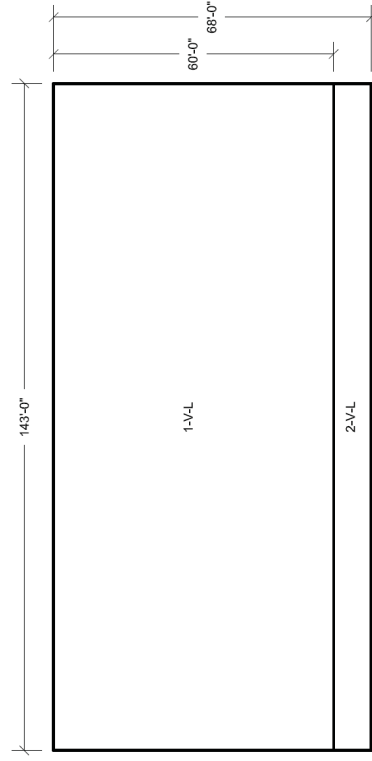
(9) The Access Region is governed by the tornado load combination. The outside layer of transverse reinforcement (all 4 near side vertical longitudinal reinforcement) is utilized to resist an axial force of 805 kip due to a concrete/tornado missile load as well as a tornado wind pressure of 264 psf. The remaining capacity of the near side vertical longitudinal reinforcement is provided with the far side vertical longitudinal reinforcement in conjunction with the far side vertical longitudinal reinforcement to resist a torsional moment of 1438 kip-ft due to an eccentric tornado missile load as well as a tornado wind pressure of 264 psf. The outside layer of transverse reinforcement is provided with the far side vertical longitudinal reinforcement in conjunction with the far side vertical longitudinal reinforcement to resist a torsional moment of 1438 kip-ft due to an eccentric tornado missile load as well as a tornado wind pressure of 264 psf.

(10) The basement near side horizontal reinforcement is governed by the tornado load combination. The outside layer of transverse reinforcement (all 4 near side vertical longitudinal reinforcement) is utilized to resist an axial force of 805 kip due to a concrete/tornado missile load as well as a tornado wind pressure of 264 psf. The remaining capacity of the near side vertical longitudinal reinforcement is provided with the far side vertical longitudinal reinforcement in conjunction with the far side vertical longitudinal reinforcement to resist a torsional moment of 1438 kip-ft due to an eccentric tornado missile load as well as a tornado wind pressure of 264 psf.

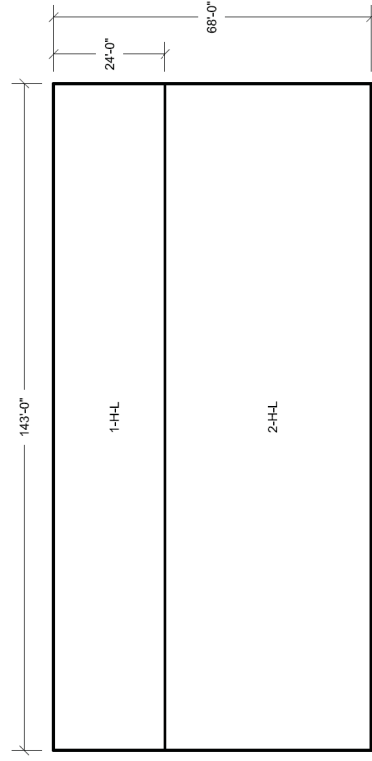
(11) The "E" (WP) designation in the load combination column indicates seismic SSE loading including wave propagation effects.



**FIGURE 3H.6.64-PUMP HOUSE NORTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE**



**FIGURE 3H.6.52- PUMP HOUSE NORTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE**



**FIGURE 3H.6.53- PUMP HOUSE NORTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE**

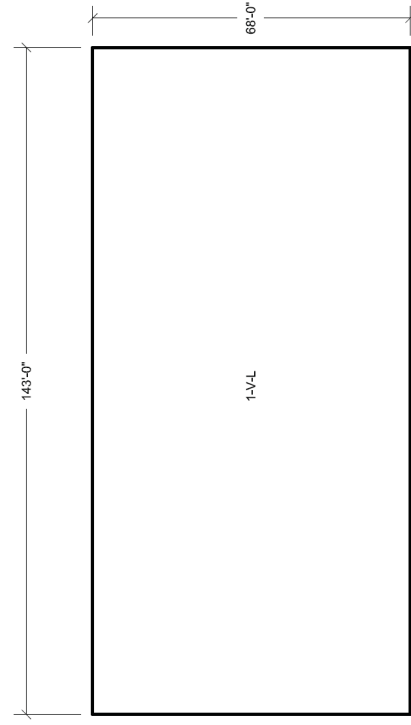


FIGURE 3H.6.54-PUMP HOUSE NORTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

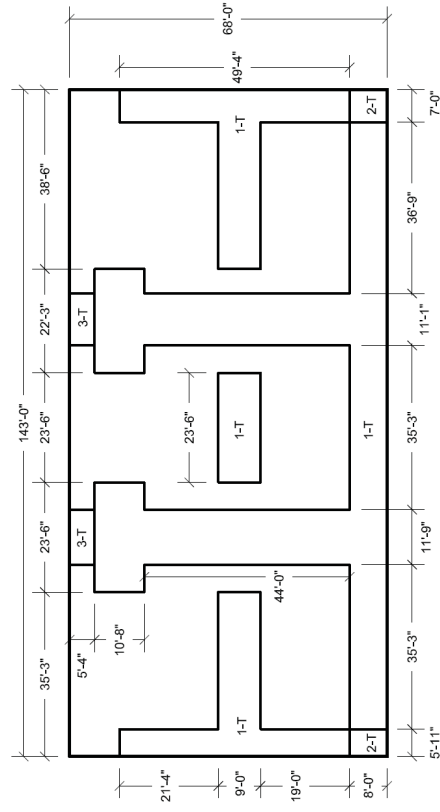
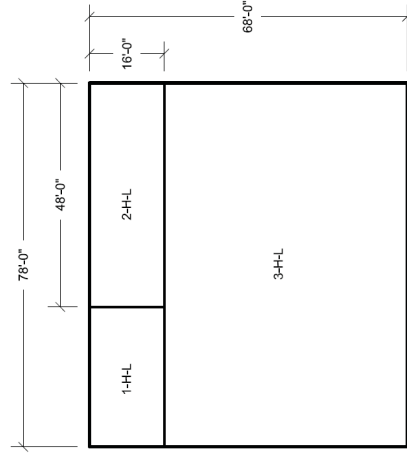


FIGURE 3H.6.55: PUMP HOUSE NORTH WALL LOOKING SOUTH
TRANSVERSE REINFORCEMENT ZONES



**FIGURE 3H.56: PUMP HOUSE EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE**

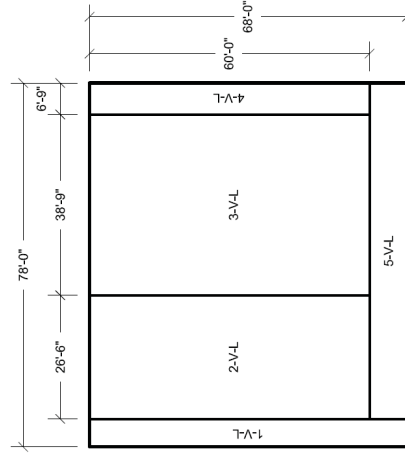


FIGURE 3H.67: PUMP HOUSE EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

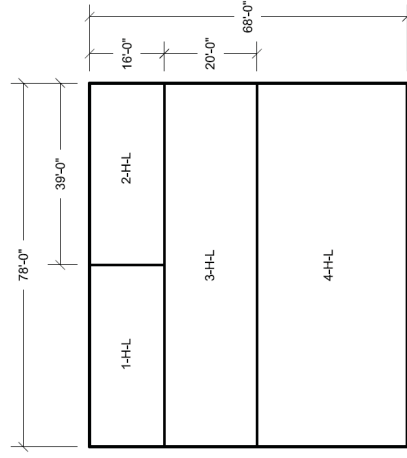


FIGURE 3H.6-58: PUMP HOUSE EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

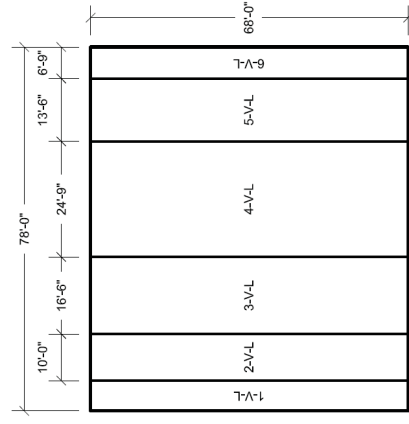
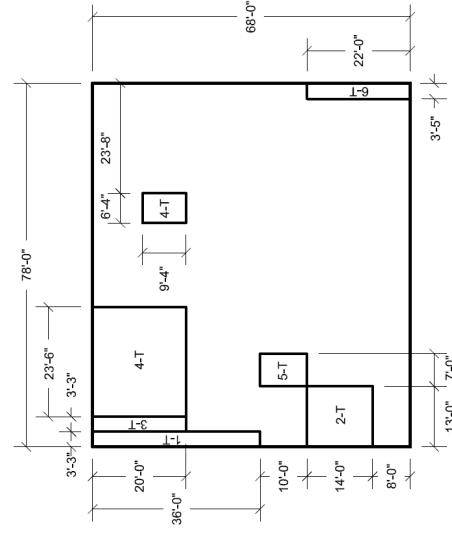


FIGURE 3H-6-59: PUMP HOUSE EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE



**FIGURE 3H.6-60: PUMP HOUSE EAST WALL LOOKING WEST
TRANSVERSE REINFORCEMENT ZONES**

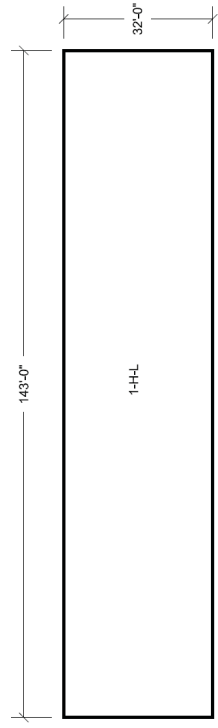


FIGURE 3H.6-61: PUMP HOUSE SOUTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

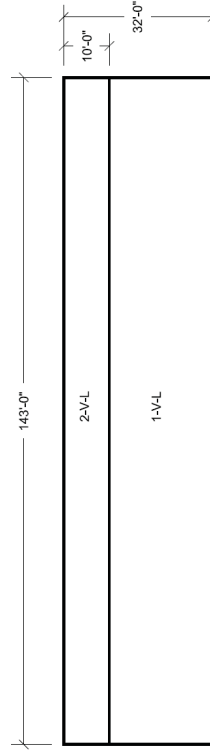


FIGURE 3H.6-62: PUMP HOUSE SOUTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

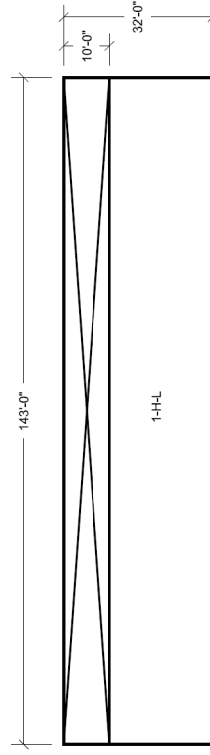


FIGURE 3H.6-43: PUMP HOUSE SOUTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

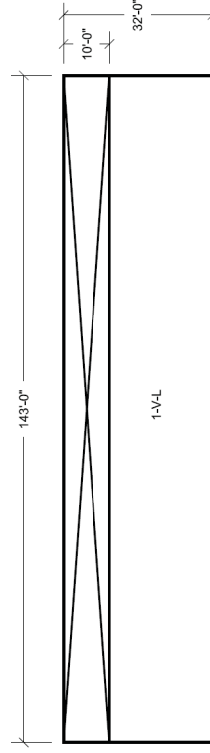


FIGURE 3H.6-64: PUMP HOUSE SOUTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

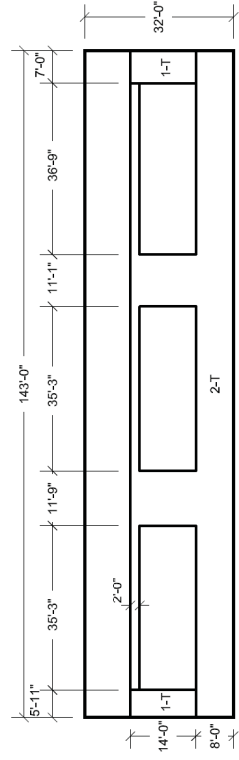


FIGURE 3H.6-65: PUMP HOUSE SOUTH WALL LOOKING SOUTH
TRANSVERSE REINFORCEMENT ZONES

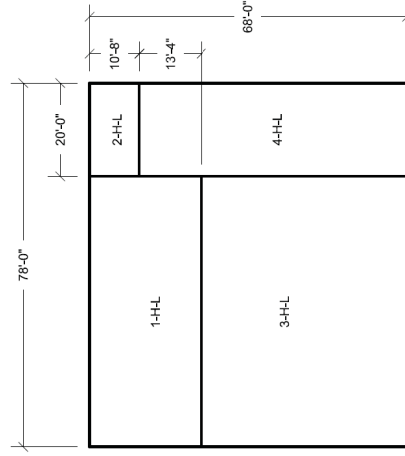


FIGURE 3H.6-56: PUMP HOUSE WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

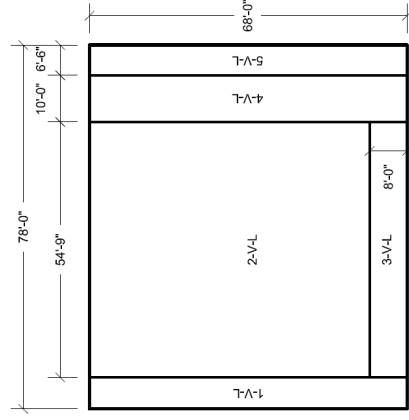


FIGURE 3H-6-57: PUMP HOUSE WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

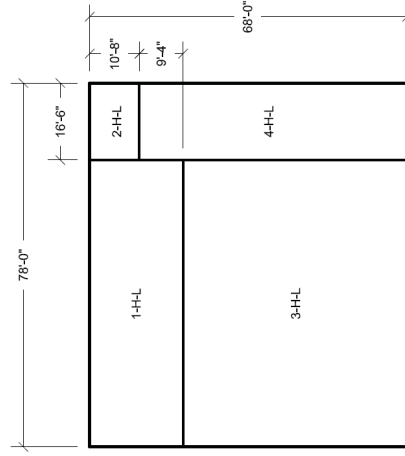


FIGURE 3H.6-68: PUMP HOUSE WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

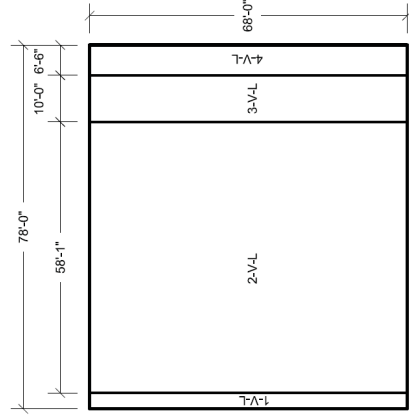


FIGURE 3H.6-58: PUMP HOUSE WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

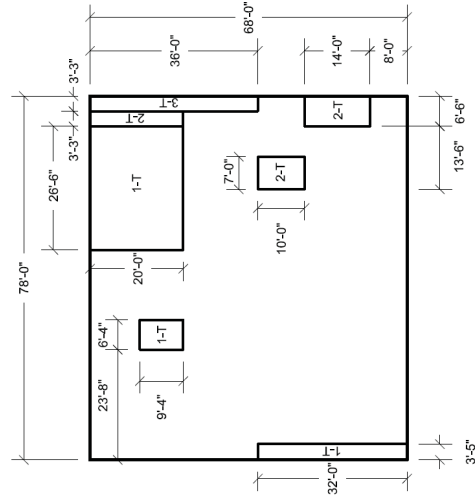


FIGURE 3H.6-70: PUMP HOUSE WEST WALL LOOKING EAST
TRANSVERSE REINFORCEMENT ZONES

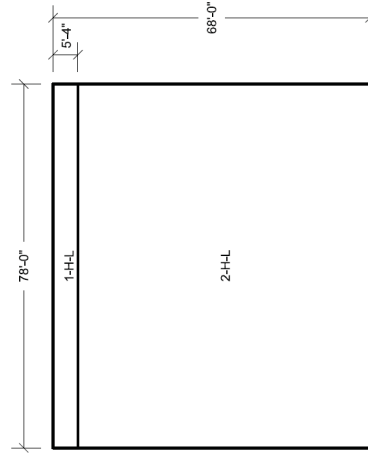


FIGURE 3H-6-71: PUMP HOUSE INTERNAL EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

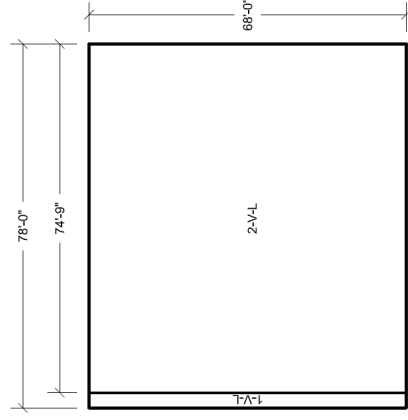


FIGURE 3H.6-72: PUMP HOUSE INTERNAL EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

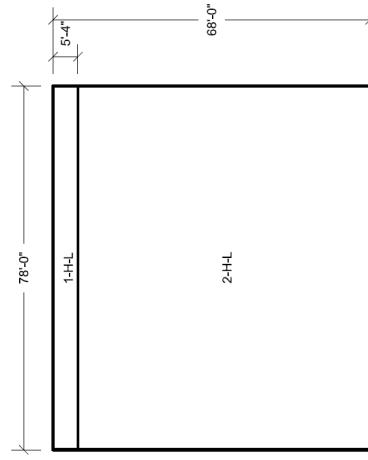


FIGURE 3H.6-73: PUMP HOUSE INTERNAL EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

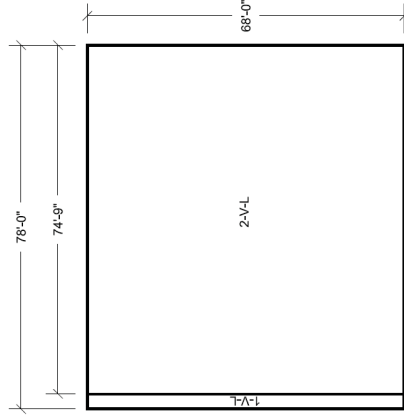


FIGURE 3H.6-74: PUMP HOUSE INTERNAL EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

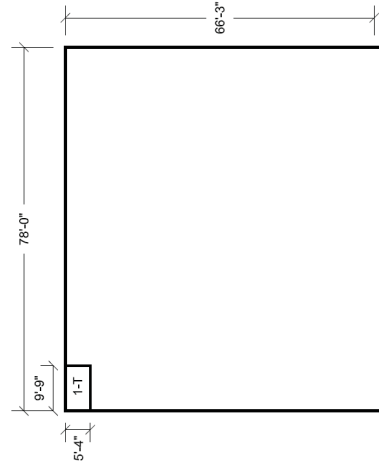


FIGURE 3H.6-74A: PUMP HOUSE INTERNAL EAST WALL LOOKING WEST
TRANSVERSE REINFORCEMENT ZONES

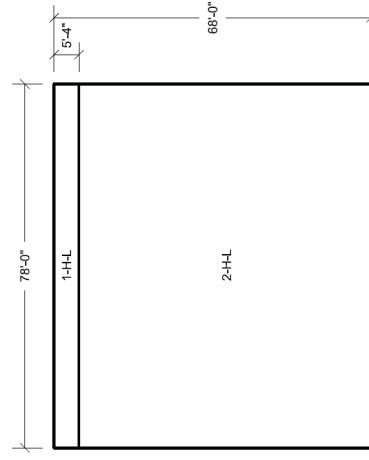


FIGURE 3H.6-75: PUMP HOUSE INTERNAL WEST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

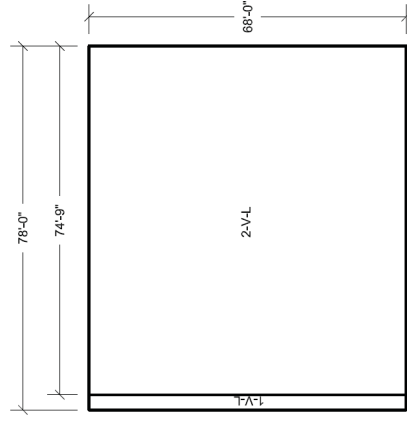


FIGURE 3H.6-76: PUMP HOUSE INTERNAL WEST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

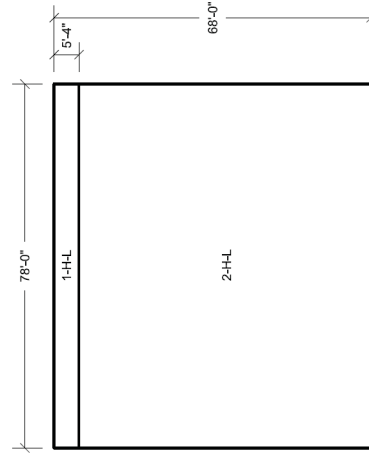


FIGURE 3H.6-77: PUMP HOUSE INTERNAL WEST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

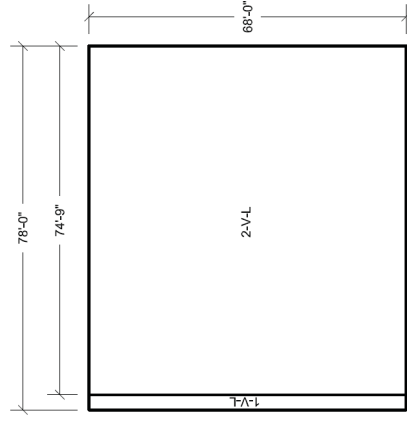


FIGURE 3H.6-78: PUMP HOUSE INTERNAL WEST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

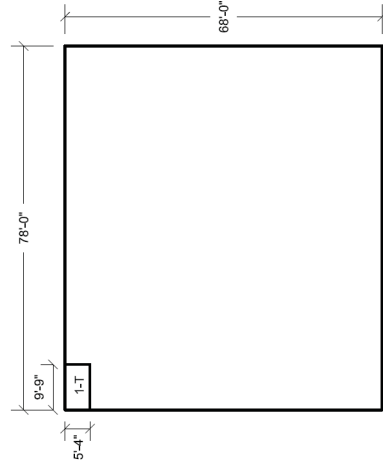


FIGURE 3H.6-78A: PUMP HOUSE INTERNAL WEST WALL LOOKING WEST
TRANSVERSE REINFORCEMENT ZONES

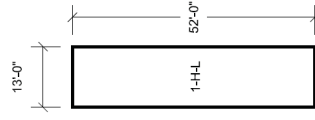


FIGURE 3H.6-79: PUMP HOUSE EAST BUTTRESS LOOKING NORTH & PUMP HOUSE WEST BUTTRESS LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
NEAR AND FAR SIDE FACES

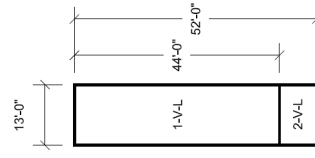


FIGURE 3H.6-80: PUMP HOUSE EAST BUTTRESS LOOKING NORTH & PUMP HOUSE WEST BUTTRESS LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
NEAR AND FAR SIDE FACES

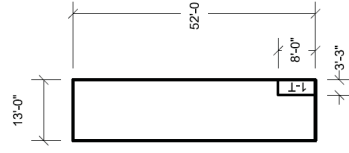


FIGURE 3H.6-81: PUMP HOUSE EAST BUTTRESS LOOKING NORTH & PUMP HOUSE WEST BUTTRESS LOOKING SOUTH
TRANSVERSE REINFORCEMENT ZONES

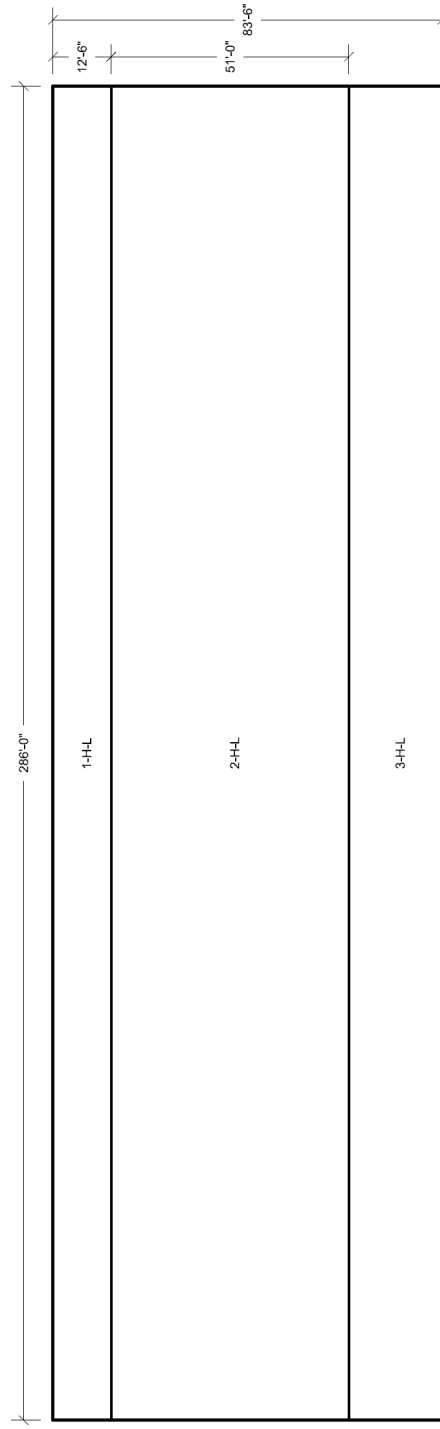


FIGURE 3H.6-82: UHS BASIN NORTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

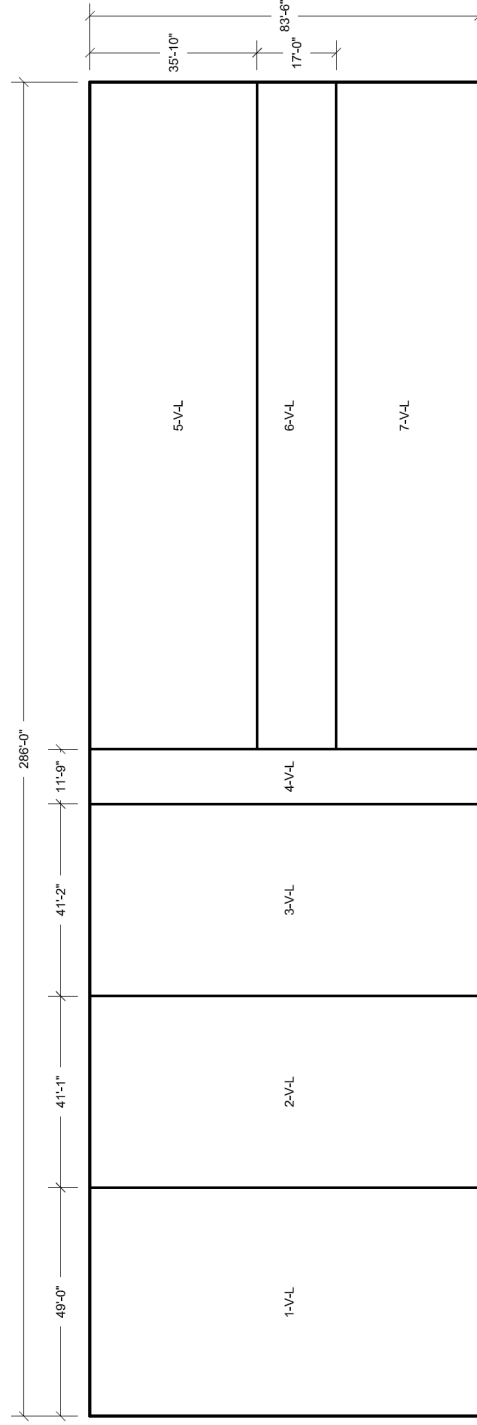


FIGURE 3H-6-83: UHS BASIN NORTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

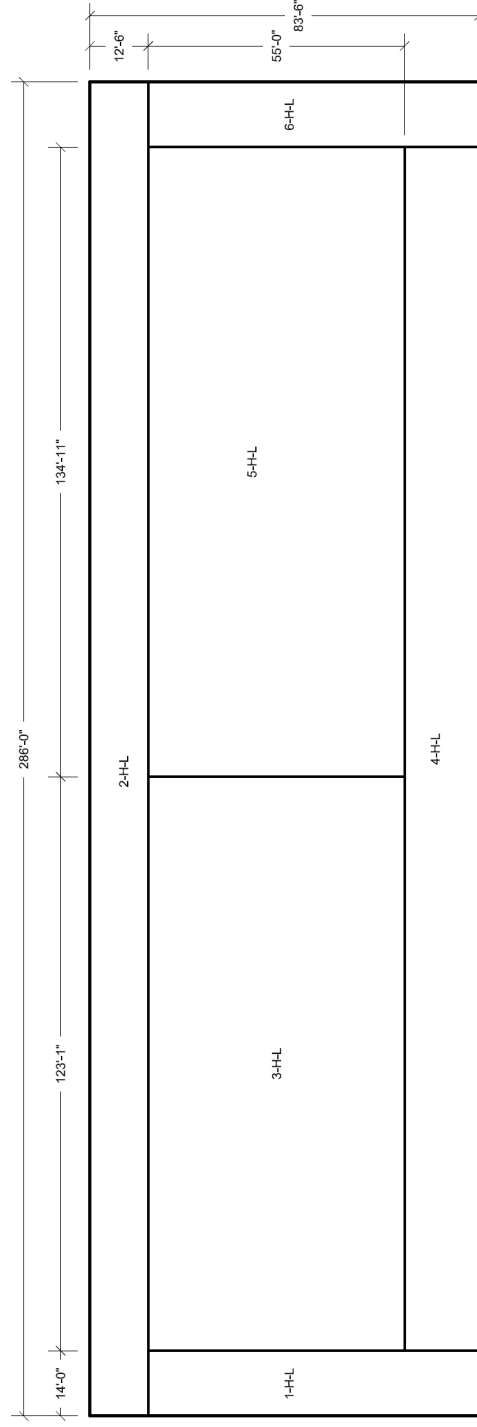


FIGURE 3H.6-84: UHS BASIN NORTH WALL LOOKING SOUTH
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

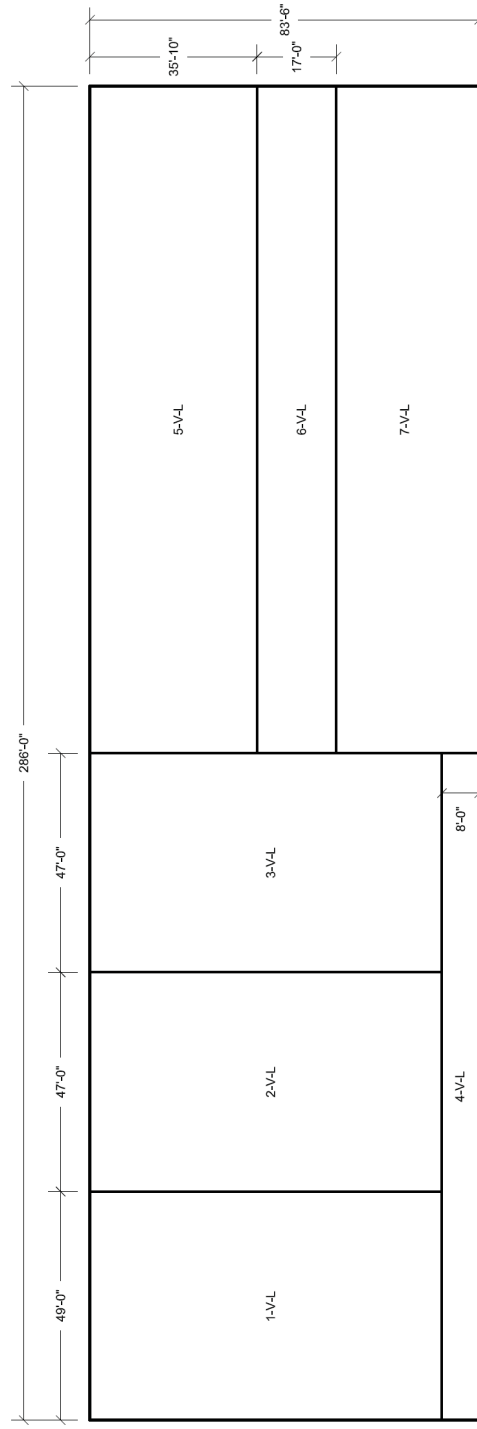
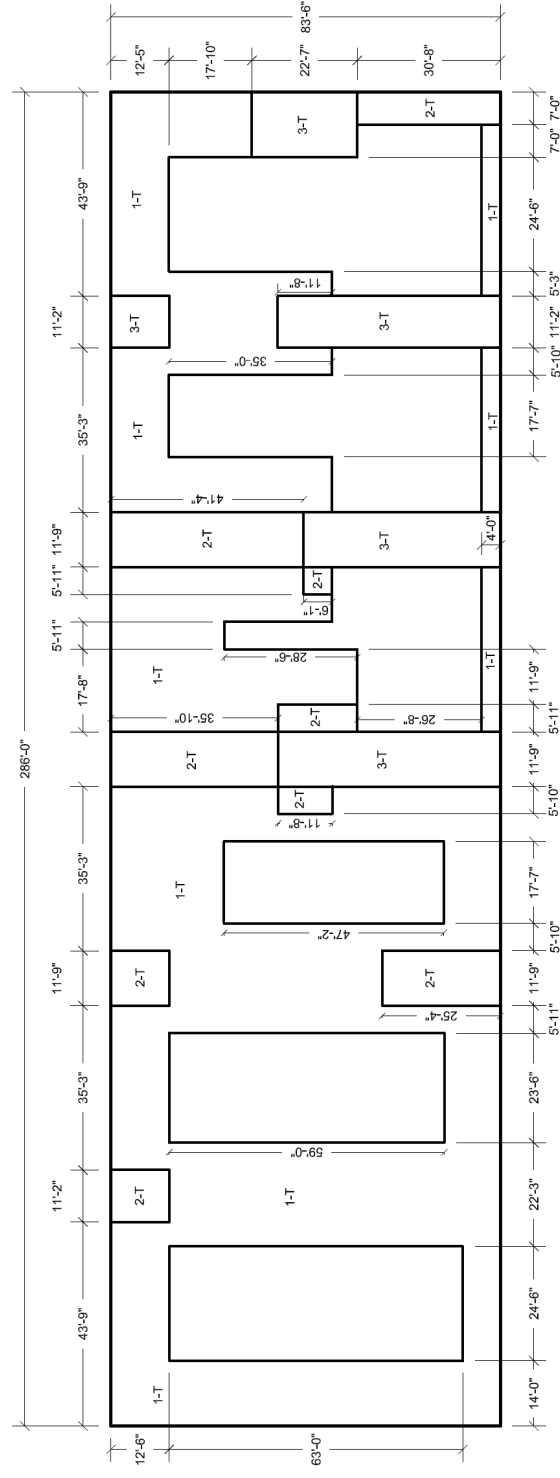


FIGURE 3H.6-85: UHS BASIN NORTH WALL LOOKING SOUTH
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE



**FIGURE 3H.6-86: UHS BASIN NORTH WALL LOOKING SOUTH
TRANSVERSE REINFORCEMENT ZONES**

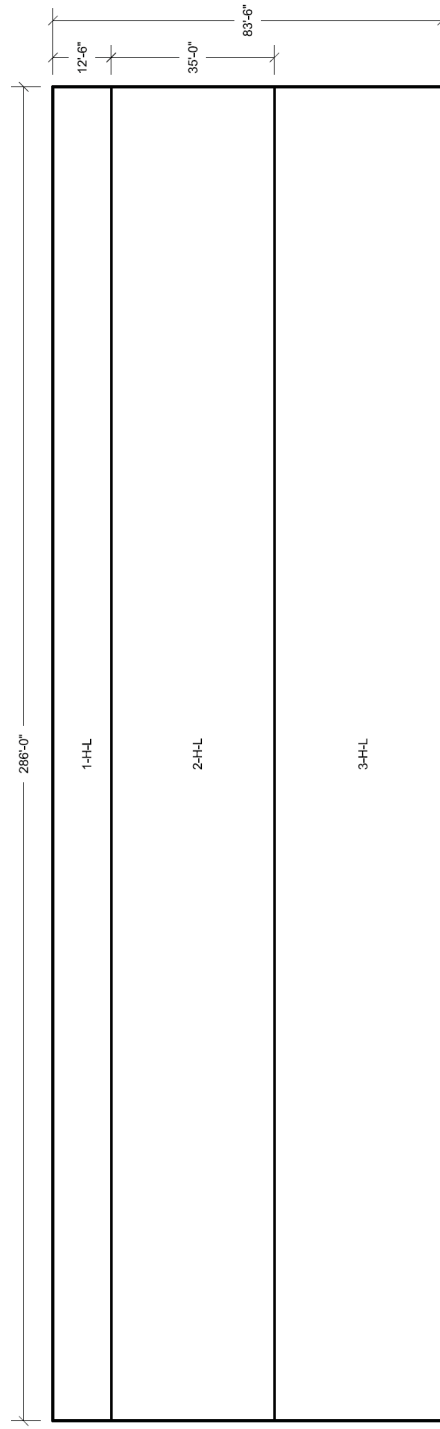


FIGURE 3H-6-87: UHS BASIN SOUTH WALL LOOKING NORTH
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

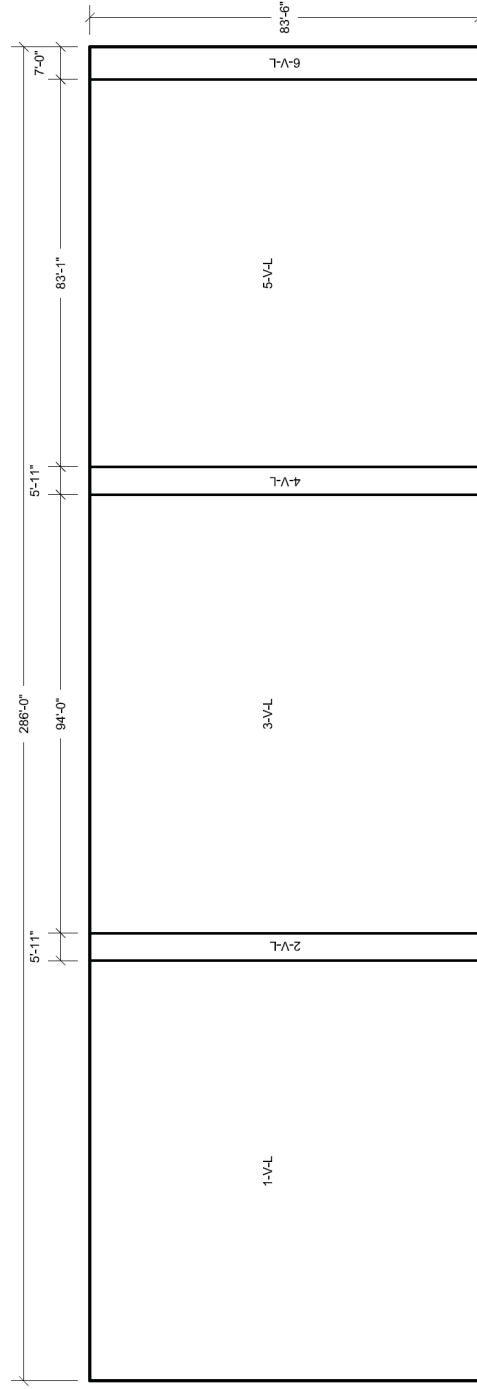


FIGURE 3H-6-88: UHS BASIN SOUTH WALL LOOKING NORTH
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

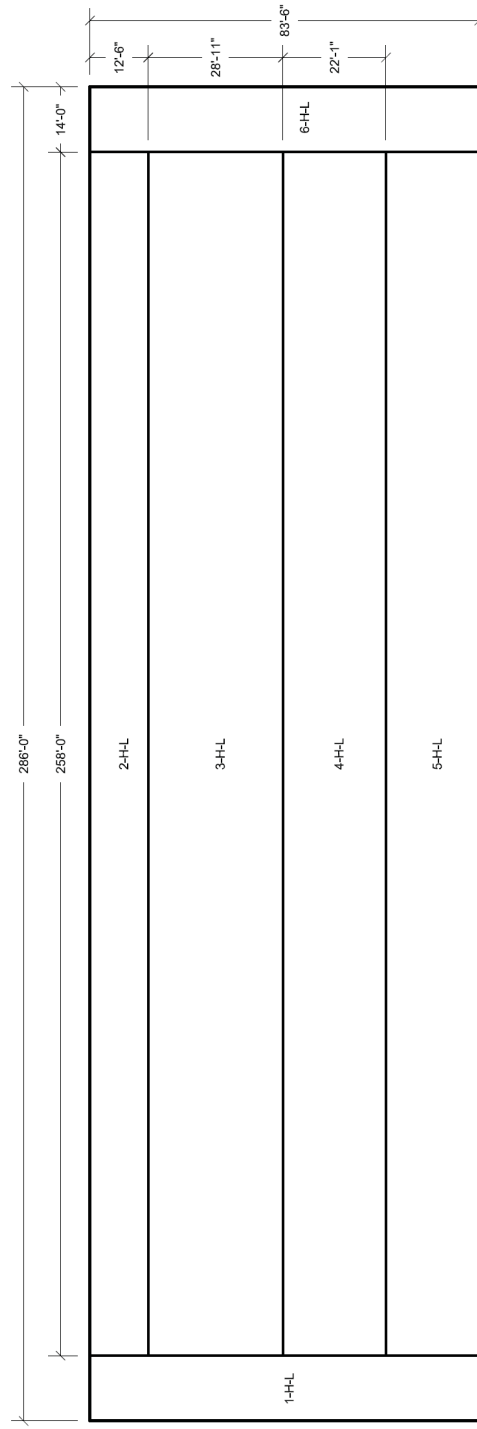


FIGURE 3H.6-88: UHS BASIN SOUTH WALL LOOKING NORTH
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

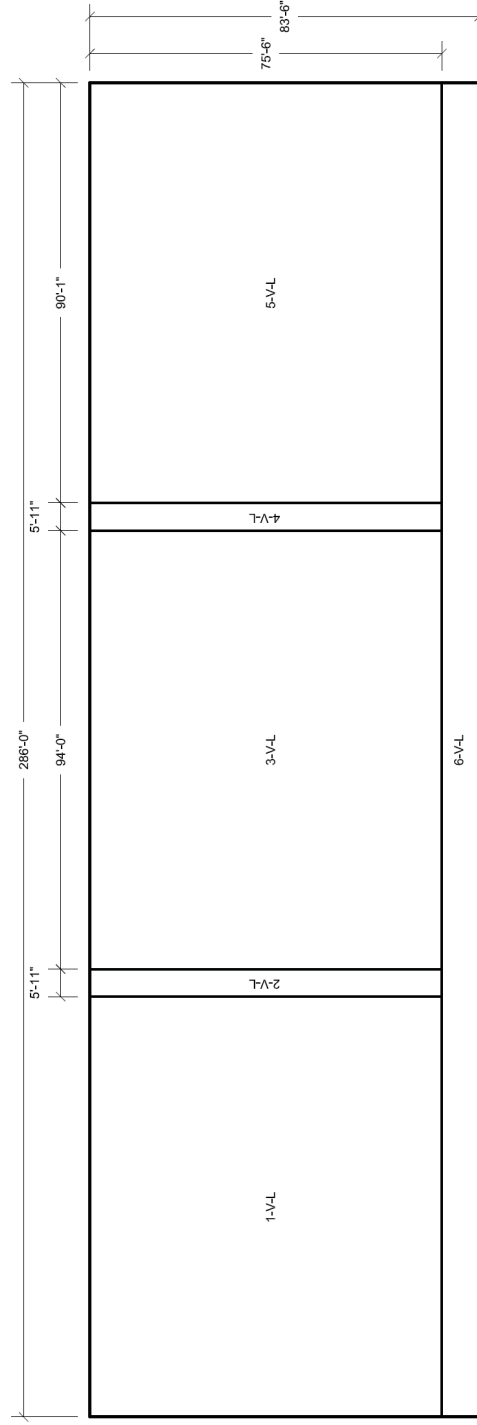
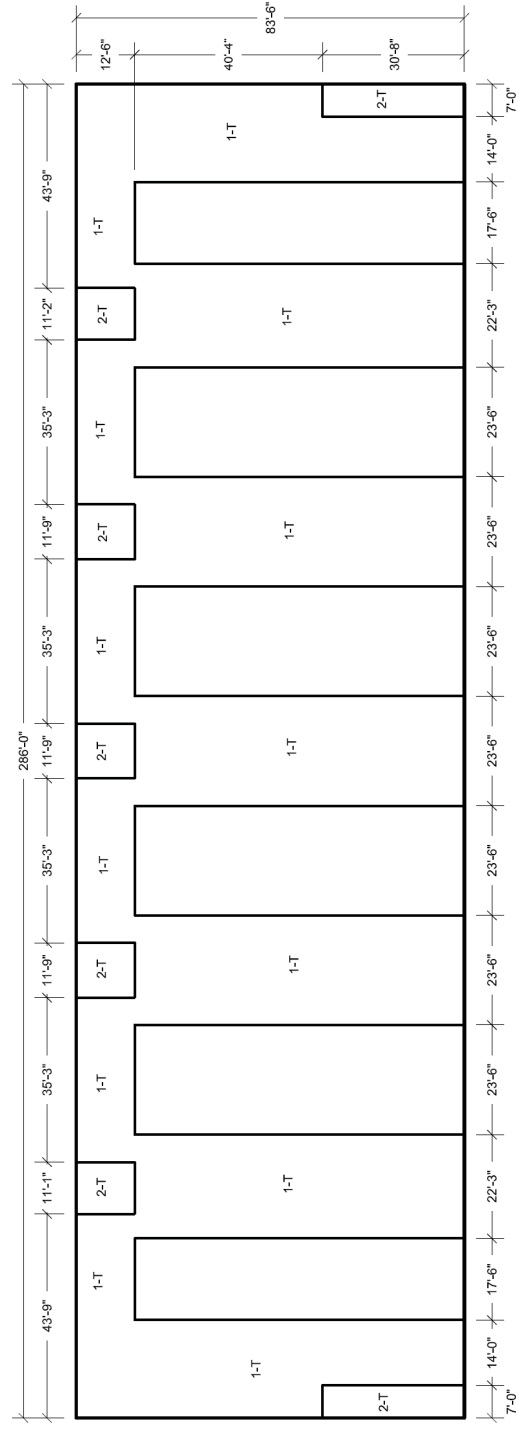


FIGURE 3H.6-90: UHS BASIN SOUTH WALL LOOKING NORTH
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE



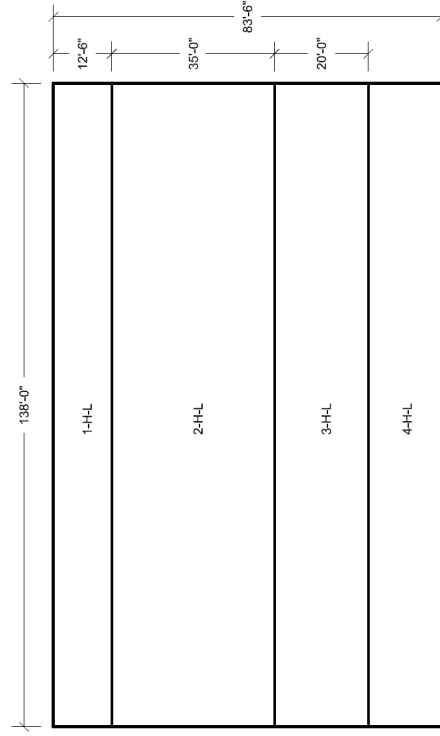


FIGURE 3H.6-92: UHS BASIN EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

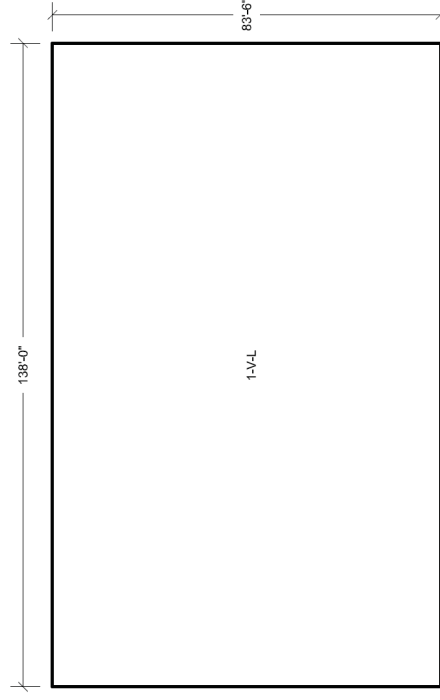


FIGURE 3H.6-93: LHS BASIN EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

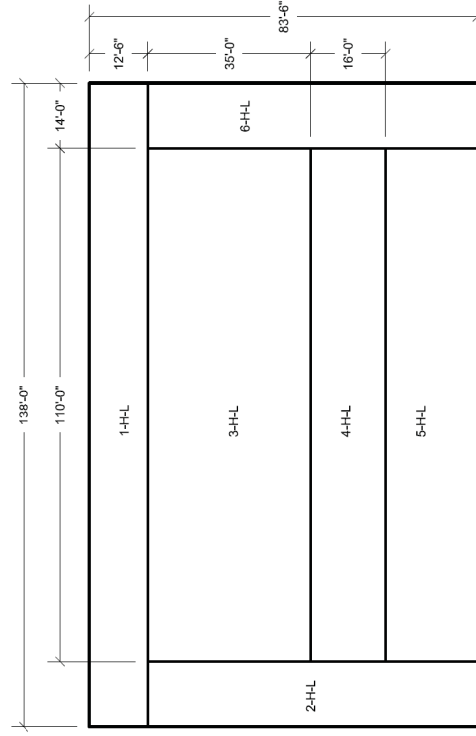


FIGURE 3H.6-94: UHS BASIN EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

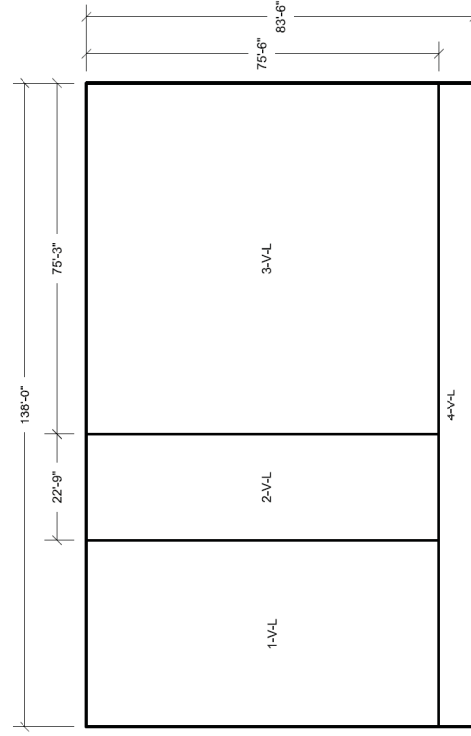


FIGURE 3H.6-95: LHS BASIN EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE



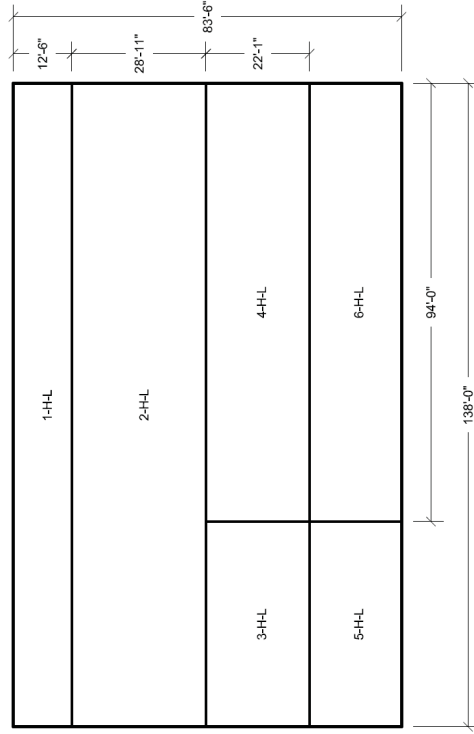


FIGURE 3H.6-97: UHS BASIN WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

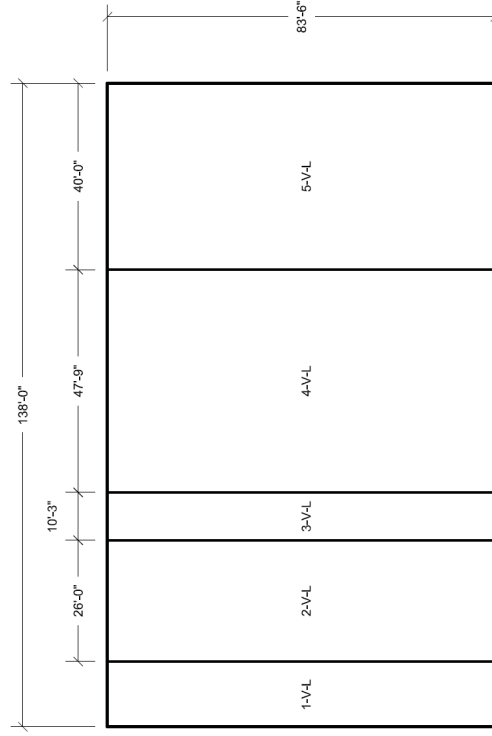


FIGURE 3H.6.98: LHS BASIN WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

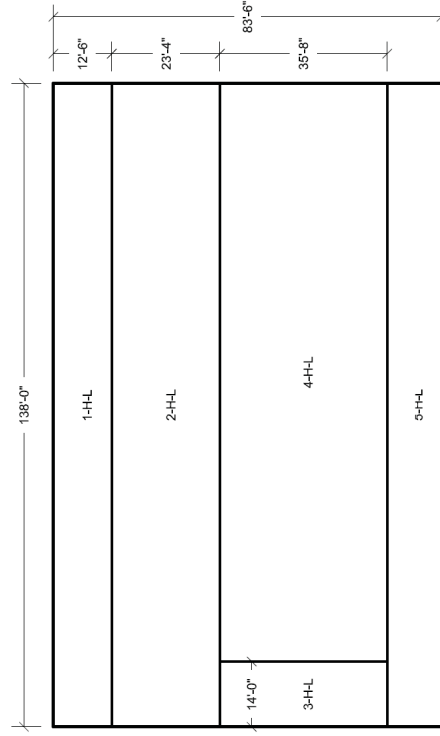


FIGURE 3H.6-98: UHS BASIN WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

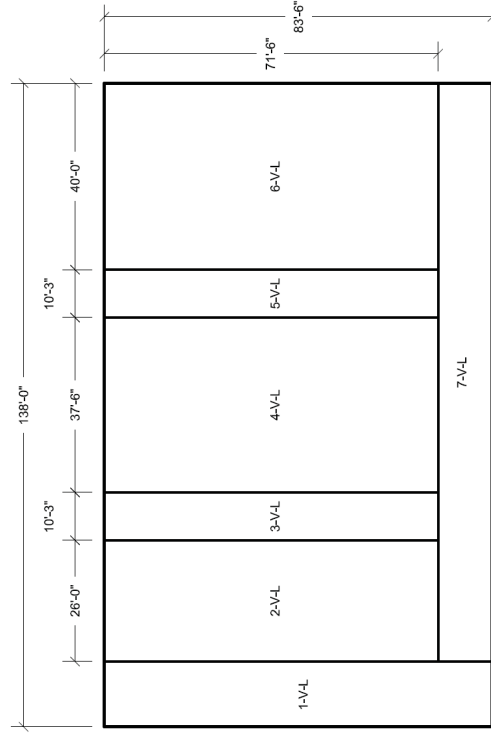


FIGURE 3H.6-100: UHS BASIN WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

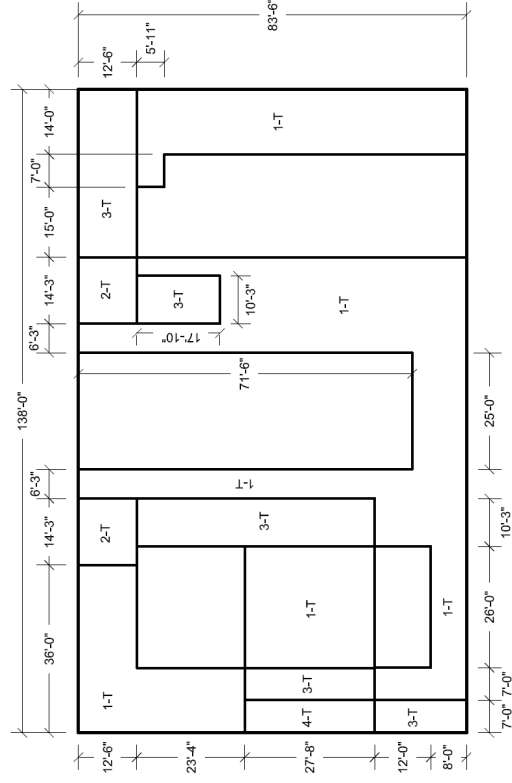


FIGURE 3H.6-101: UHS BASIN WEST WALL LOOKING EAST
TRANSVERSE REINFORCEMENT ZONES

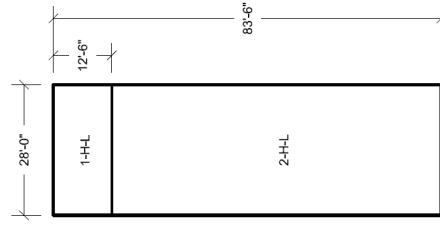


FIGURE 3H.6-102: UHS BASIN NORTH BUTTRESS LOOKING WEST & UHS BASIN SOUTH BUTTRESS LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
NEAR & FAR SIDE FACES

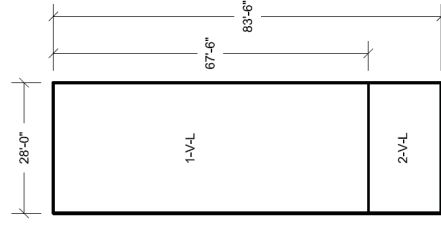


FIGURE 3H.6-103: UHS BASIN NORTH BUTTRESS LOOKING WEST & UHS BASIN SOUTH BUTTRESS LOOKING EAST
VERTICAL REINFORCEMENT ZONES
NEAR & FAR SIDE FACES

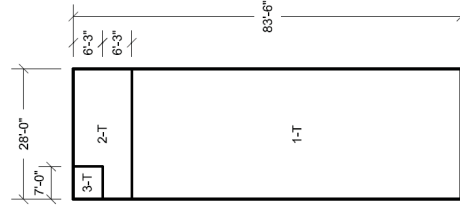


FIGURE 3H.6-104: UHS BASIN NORTH BUTTRESS LOOKING WEST & UHS BASIN SOUTH BUTTRESS LOOKING EAST
TRANSVERSE REINFORCEMENT ZONES

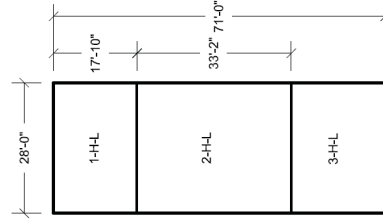


FIGURE 3H.6-105: UHS BASIN EAST BUTTRESS LOOKING NORTH & UHS BASIN WEST BUTTRESS LOOKING SOUTH.
HORIZONTAL REINFORCEMENT ZONES
NEAR AND FAR SIDE FACES

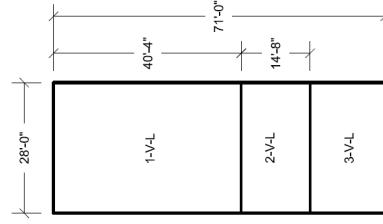


FIGURE 3H.6-106: UHS BASIN EAST BUTTRESS LOOKING NORTH & UHS BASIN WEST BUTTRESS LOOKING SOUTH.
VERTICAL REINFORCEMENT ZONES.
NEAR AND FAR SIDE FACES

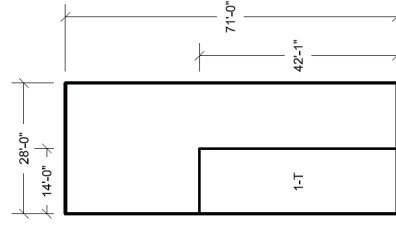


FIGURE 3H.6-107: UHS BASIN EAST BUTTRESS LOOKING NORTH & UHS BASIN WEST BUTTRESS LOOKING SOUTH. TRANSVERSE REINFORCEMENT ZONES

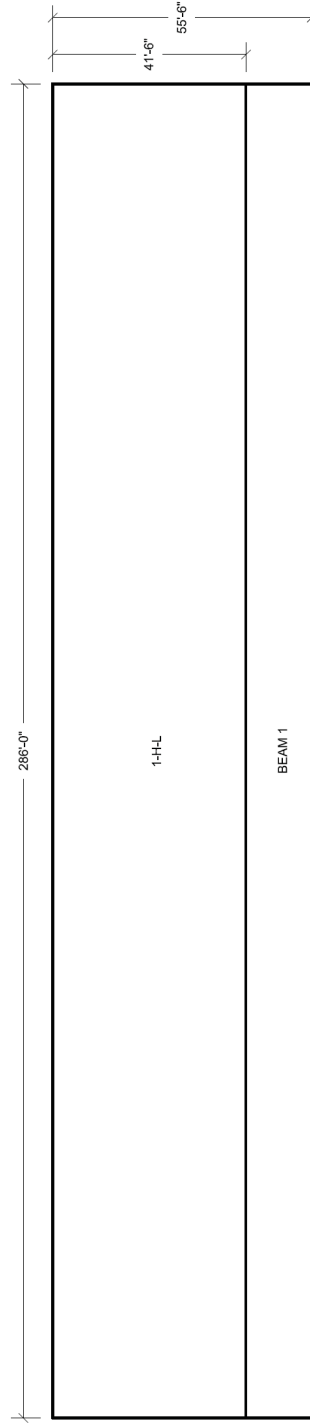


FIGURE 3H.6-108: COOLING TOWER NORTH (AND SOUTH) WALL LOOKING SOUTH (NORTH)
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

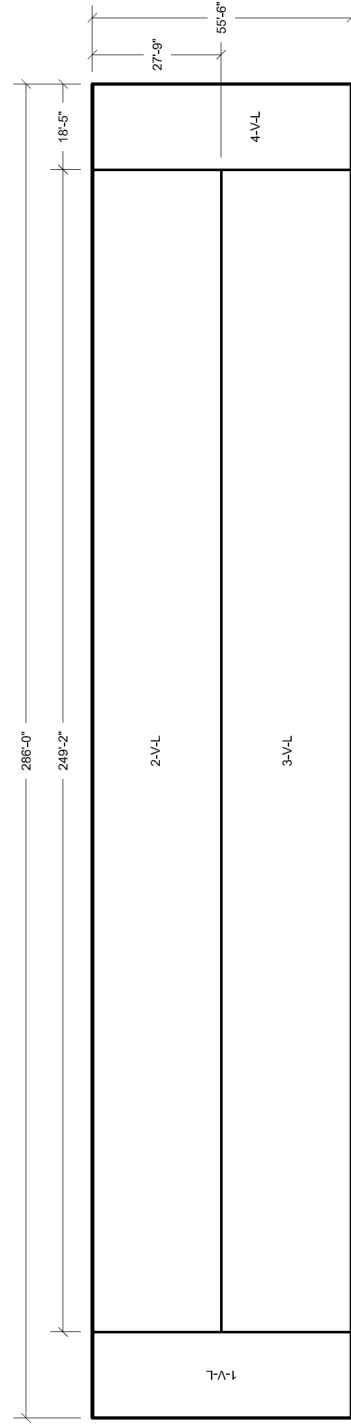


FIGURE 3H.6-108: COOLING TOWER NORTH (AND SOUTH) WALL LOOKING SOUTH (NORTH)
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

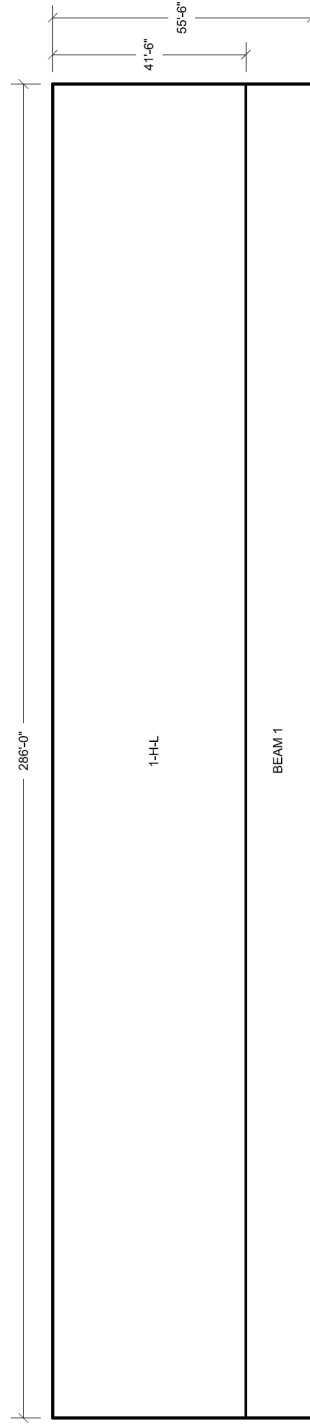


FIGURE 3H.6-110: COOLING TOWER NORTH (AND SOUTH) WALL LOOKING SOUTH (NORTH)
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

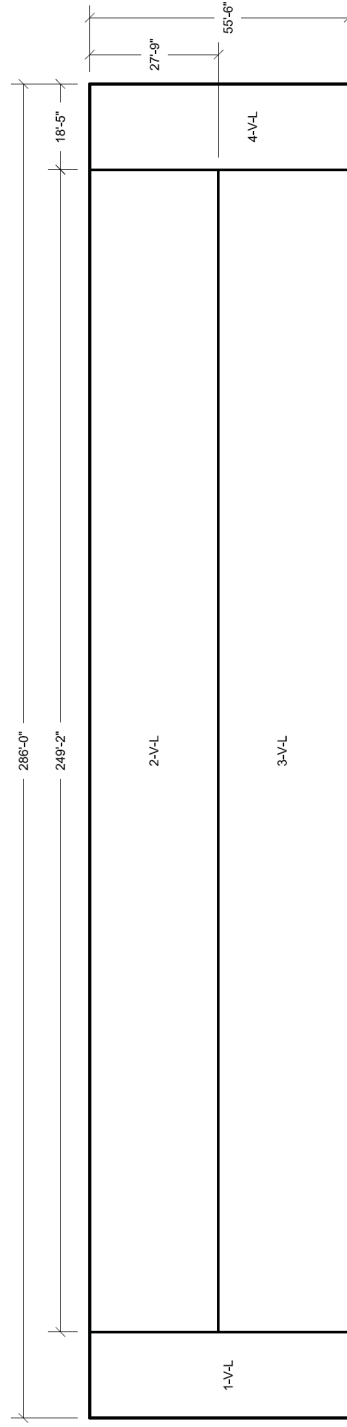


FIGURE 3H.6-111: COOLING TOWER NORTH (AND SOUTH) WALL LOOKING SOUTH (NORTH)
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

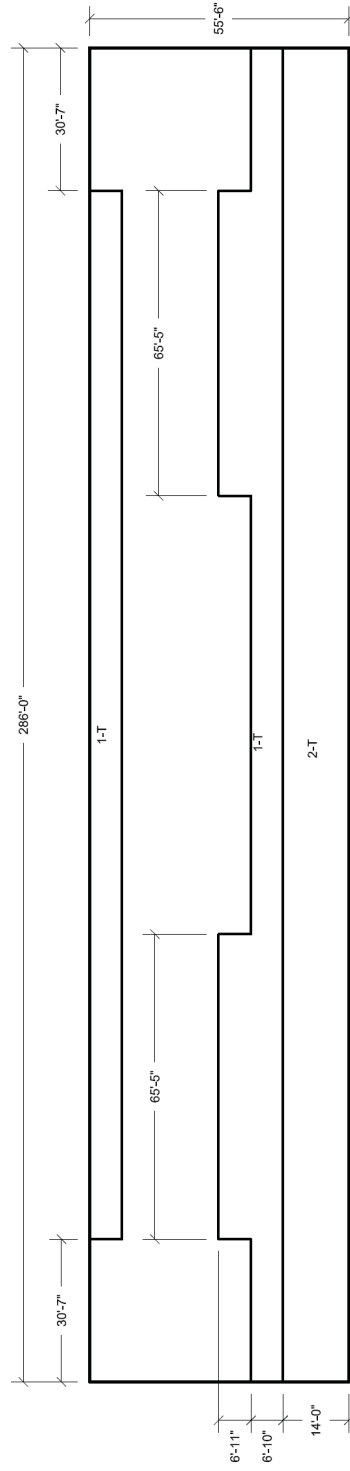


FIGURE 3H.6-112: COOLING TOWER NORTH (AND SOUTH) WALL LOOKING SOUTH (NORTH)
TRANSVERSE REINFORCEMENT ZONES

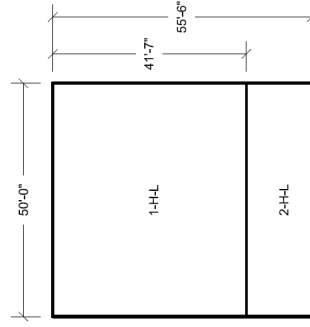


FIGURE 3H-6-113: COOLING TOWER EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

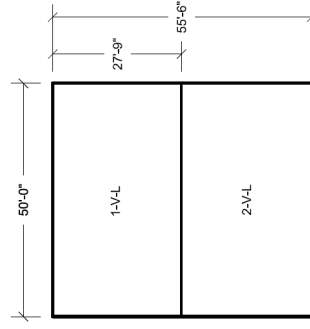


FIGURE 3H-6-114: COOLING TOWER EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

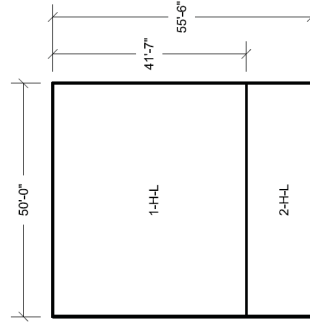


FIGURE 3H-6-11S: COOLING TOWER EAST WALL LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

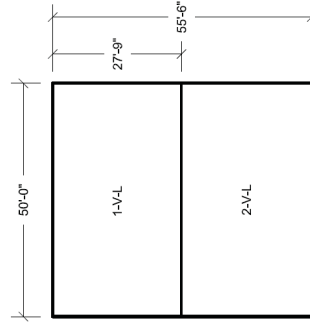
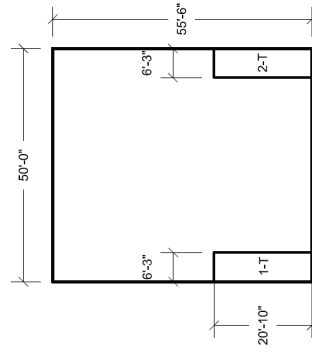


FIGURE 3H.6-118: COOLING TOWER EAST WALL LOOKING WEST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE



**FIGURE 3H.6-116A: COOLING TOWER EAST WALL LOOKING WEST
TRANSVERSE REINFORCEMENT ZONES**

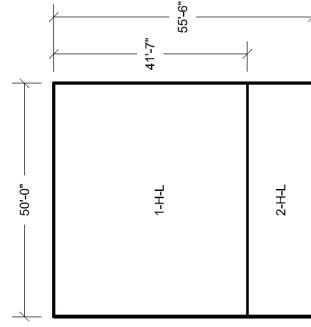


FIGURE 3H.6-117: COOLING TOWER WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
NEAR SIDE FACE

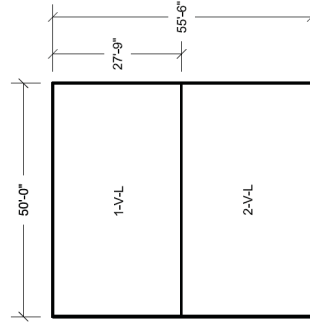


FIGURE 3H.6-118: COOLING TOWER WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
NEAR SIDE FACE

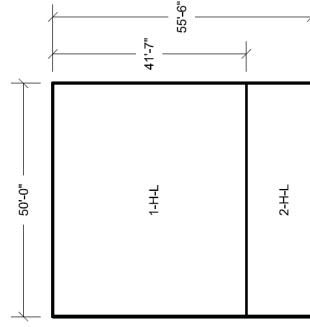


FIGURE 3H.6-118: COOLING TOWER WEST WALL LOOKING EAST
HORIZONTAL REINFORCEMENT ZONES
FAR SIDE FACE

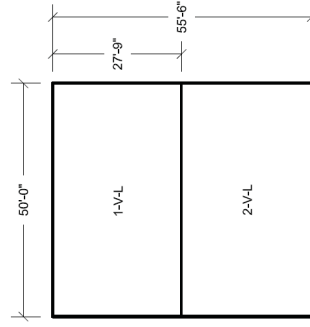


FIGURE 3H.6-128: COOLING TOWER WEST WALL LOOKING EAST
VERTICAL REINFORCEMENT ZONES
FAR SIDE FACE

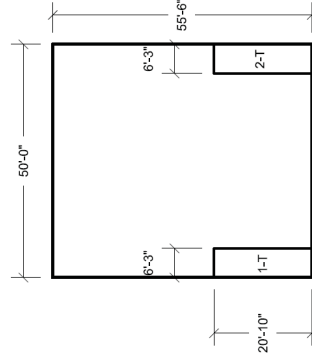


FIGURE 3H-6-120A: COOLING TOWER WEST WALL LOOKING EAST
TRANSVERSE REINFORCEMENT ZONES

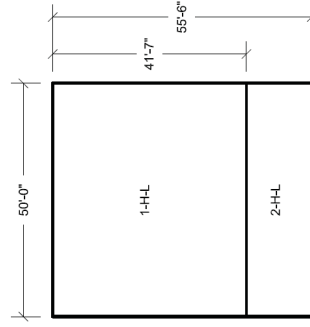


FIGURE 3H.6-12: COOLING TOWER INTERNAL WALLS LOOKING WEST
HORIZONTAL REINFORCEMENT ZONES
NEAR AND FAR SIDE FACES

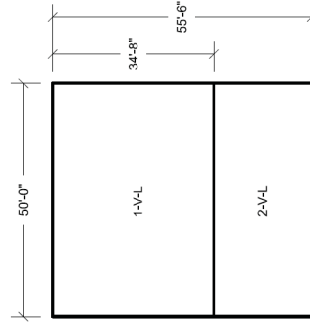


FIGURE 3H.6-122: COOLING TOWER INTERNAL WALLS LOOKING WEST
VERTICAL REINFORCEMENT ZONES
NEAR AND FAR SIDE FACES

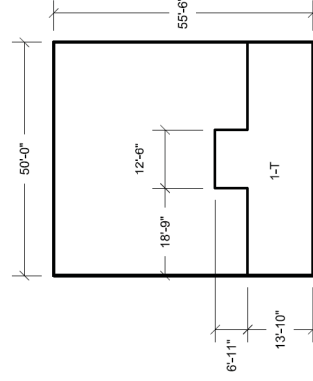


FIGURE 3H-6-122A: COOLING TOWER INTERNAL WALL LOOKING WEST
TRANSVERSE REINFORCEMENT ZONES

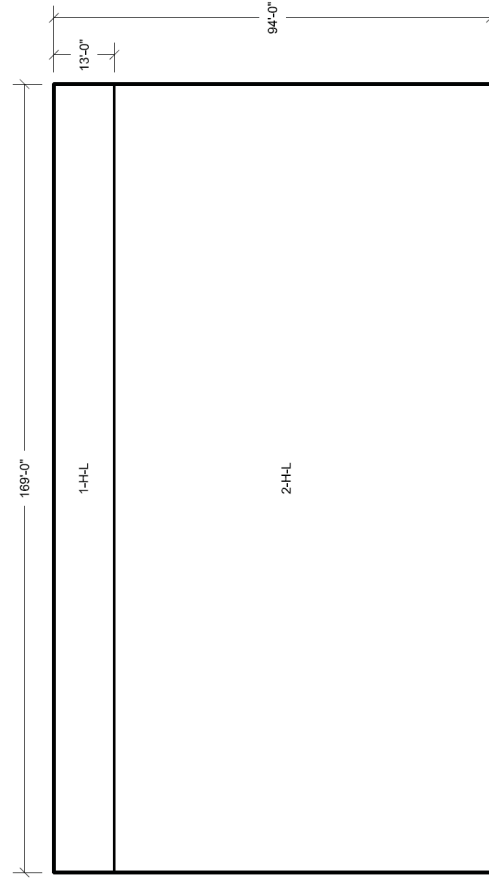


FIGURE 3H.6-123: PUMP HOUSE FOUNDATION MAT
EAST/WEST REINFORCEMENT ZONES
TOP FACE

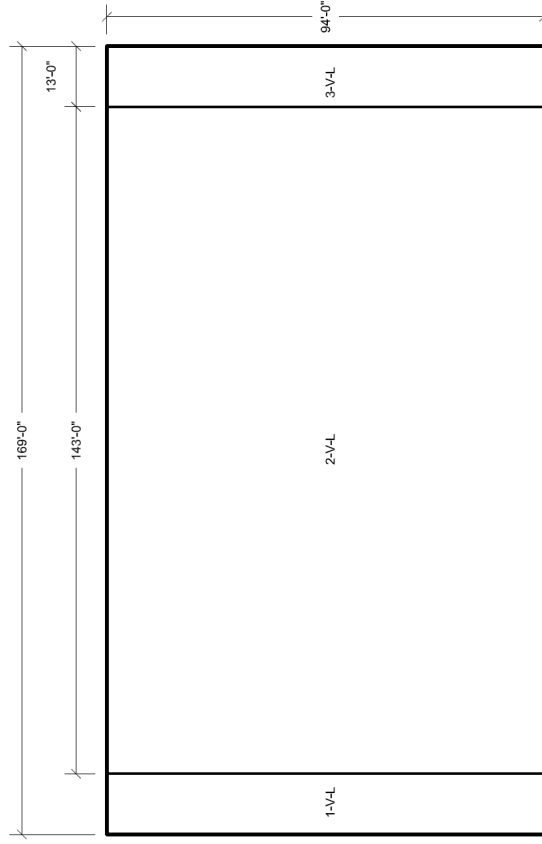


FIGURE 3H.6-124: PUMP HOUSE FOUNDATION MAT
NORTHSOUTH REINFORCEMENT ZONES
TOP FACE

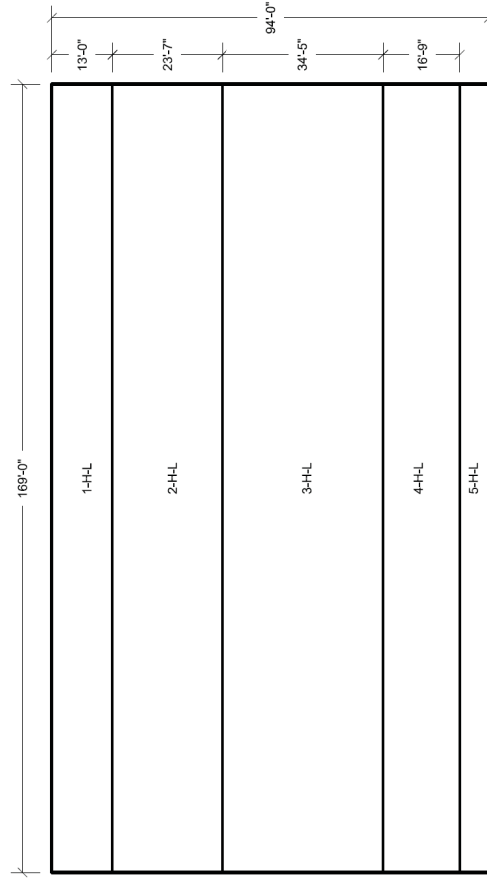


FIGURE 3H.6-12: PUMP HOUSE FOUNDATION MAT
EAST/WEST REINFORCEMENT ZONES
BOTTOM FACE

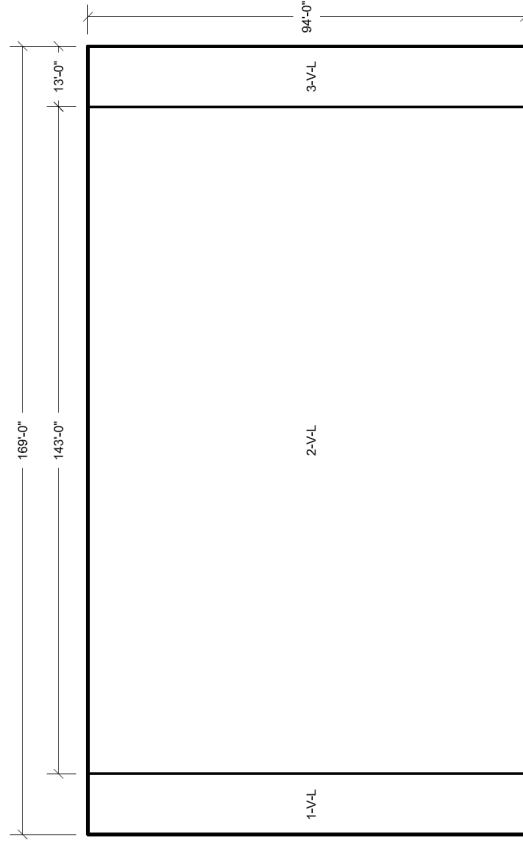


FIGURE 3H.6-126: PUMP HOUSE FOUNDATION MAT
NORTH SOUTH REINFORCEMENT ZONES
BOTTOM FACE



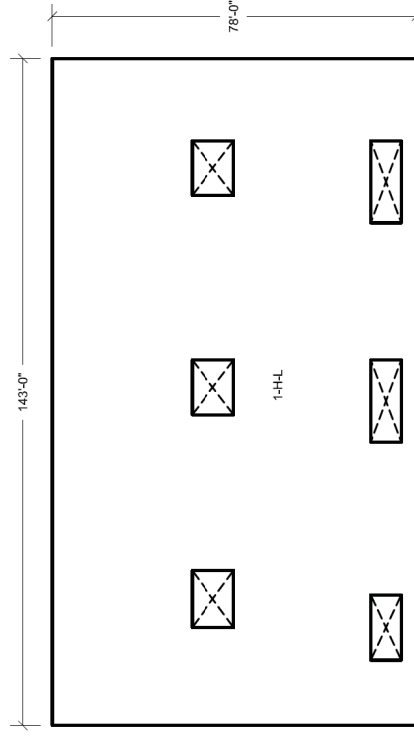


FIGURE 3H-6-127: PUMP HOUSE FLOOR EL. 15'-2"
EAST/WEST REINFORCEMENT ZONES
TOP FACE

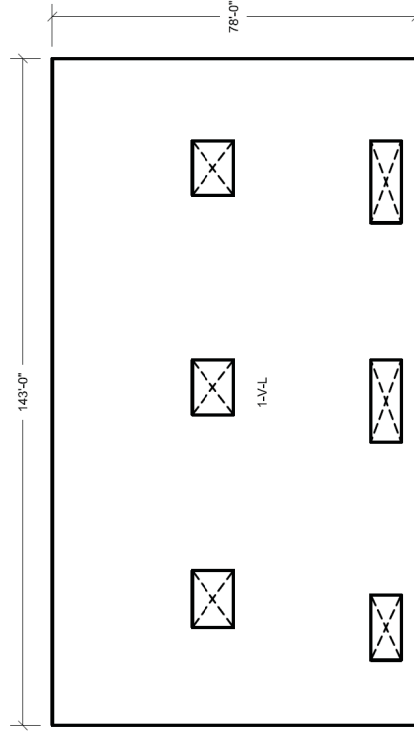


FIGURE 3H.6-128: PUMP HOUSE FLOOR EL. 15'-2"
NORTHSOUTH REINFORCEMENT ZONES
TOP FACE

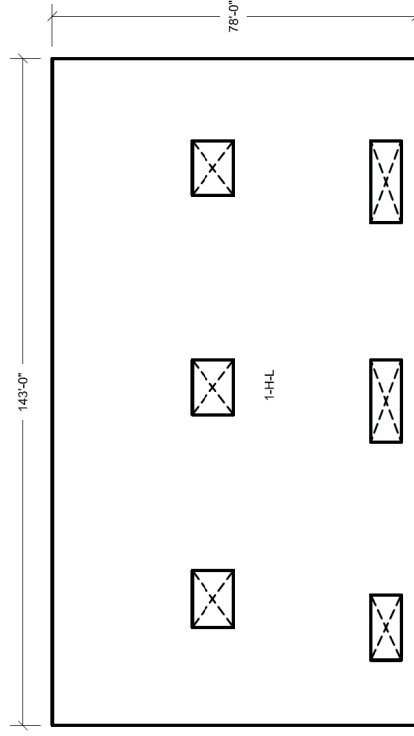


FIGURE 3H-6-128: PUMP HOUSE FLOOR EL. 15'-2"
EAST/WEST REINFORCEMENT ZONES
BOTTOM FACE

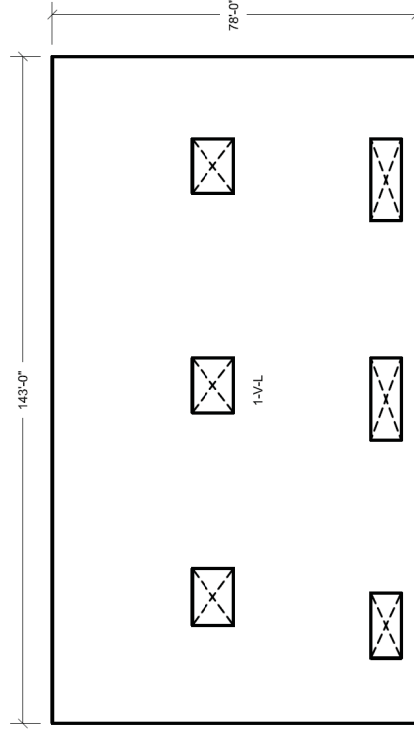


FIGURE 3H-6-130: PUMP HOUSE FLOOR EL. 15'-2"
NORTHSOUTH REINFORCEMENT ZONES
BOTTOM FACE

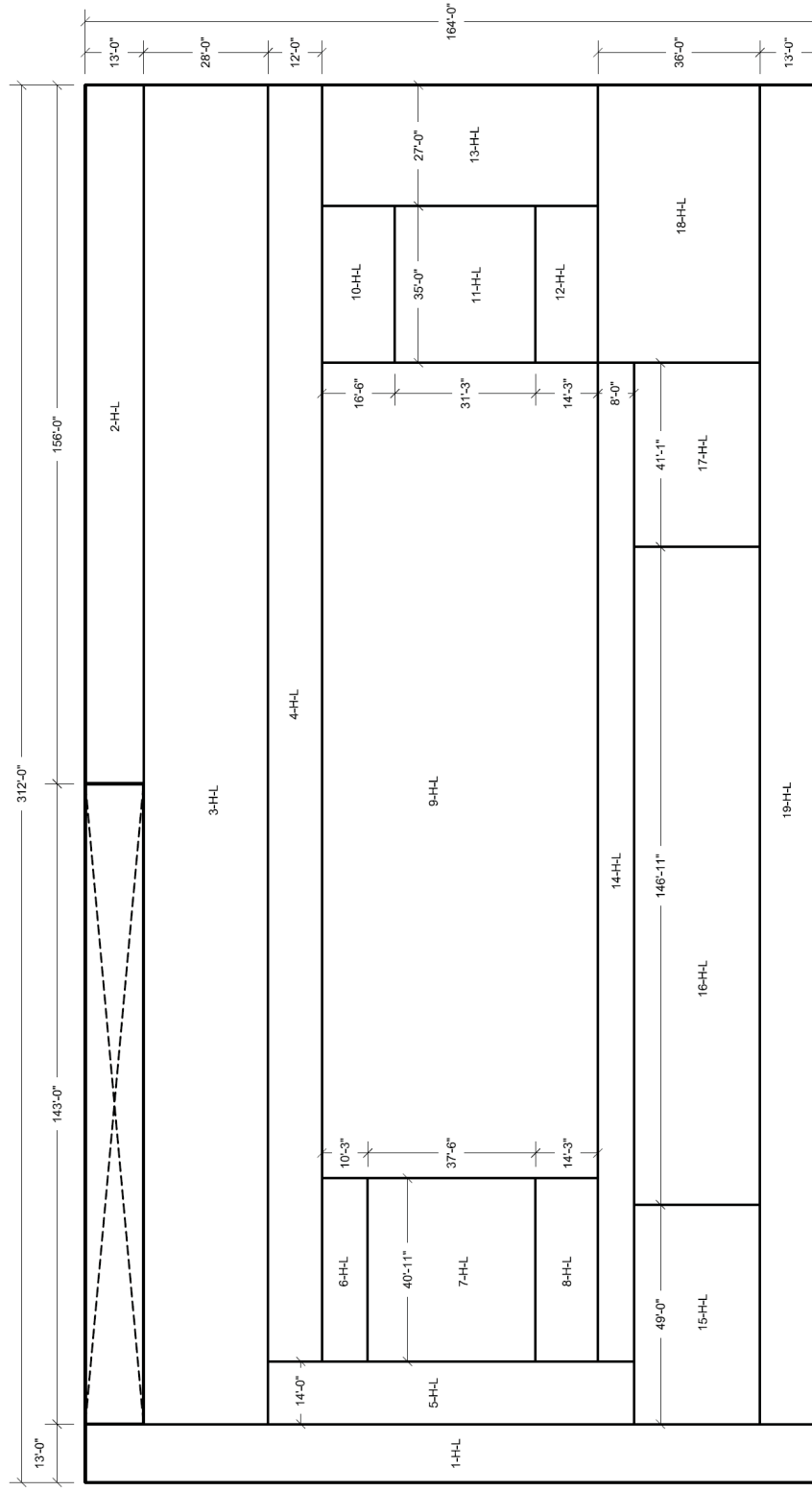


FIGURE 3H.6-131: UHS BASIN FOUNDATION MAT
EAST/WEST REINFORCEMENT ZONES
TOP FACE



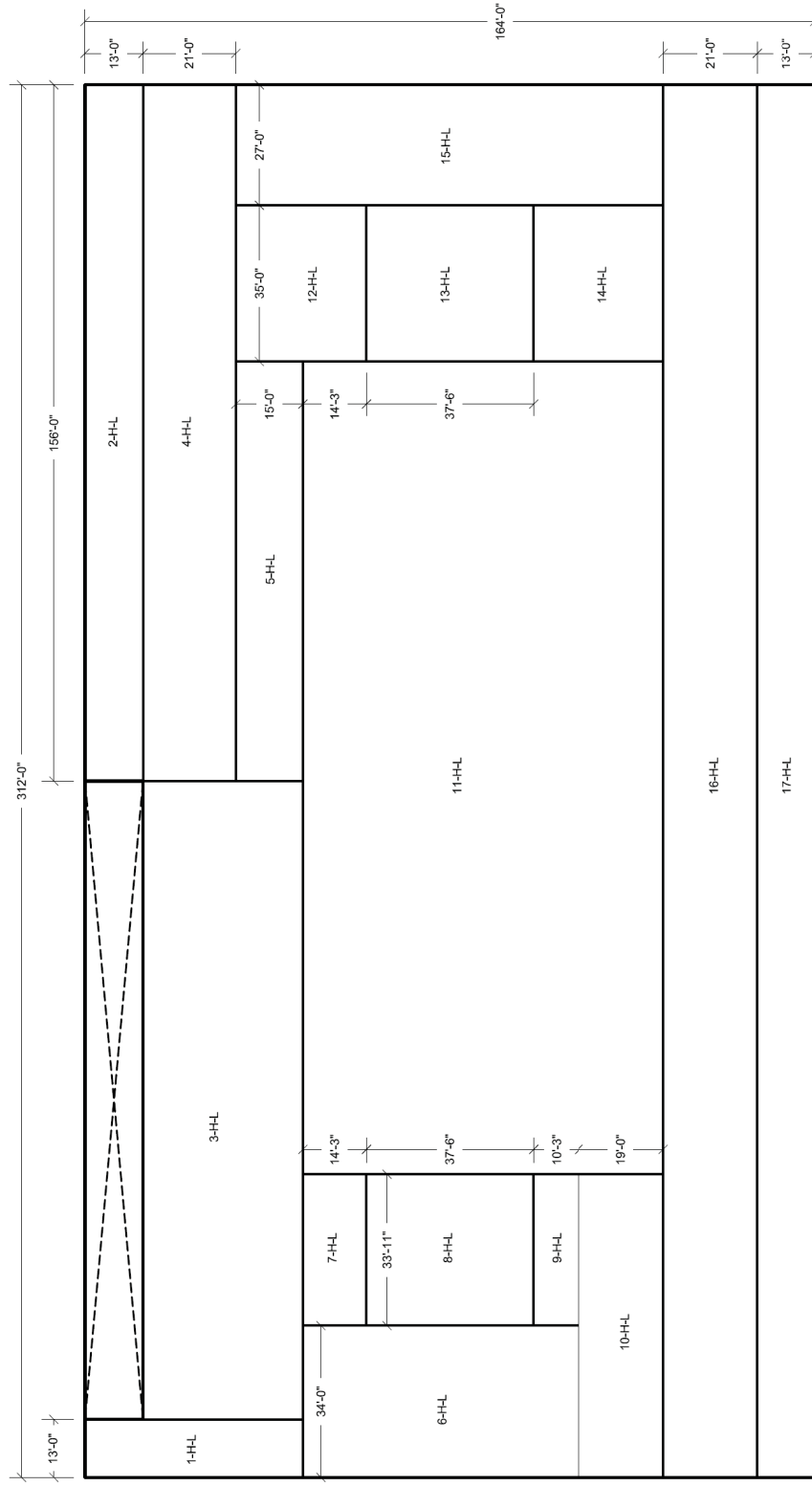


FIGURE 3H.6-133: UHS BASIN FOUNDATION MAT
EAST/WEST REINFORCEMENT ZONES
BOTTOM FACE

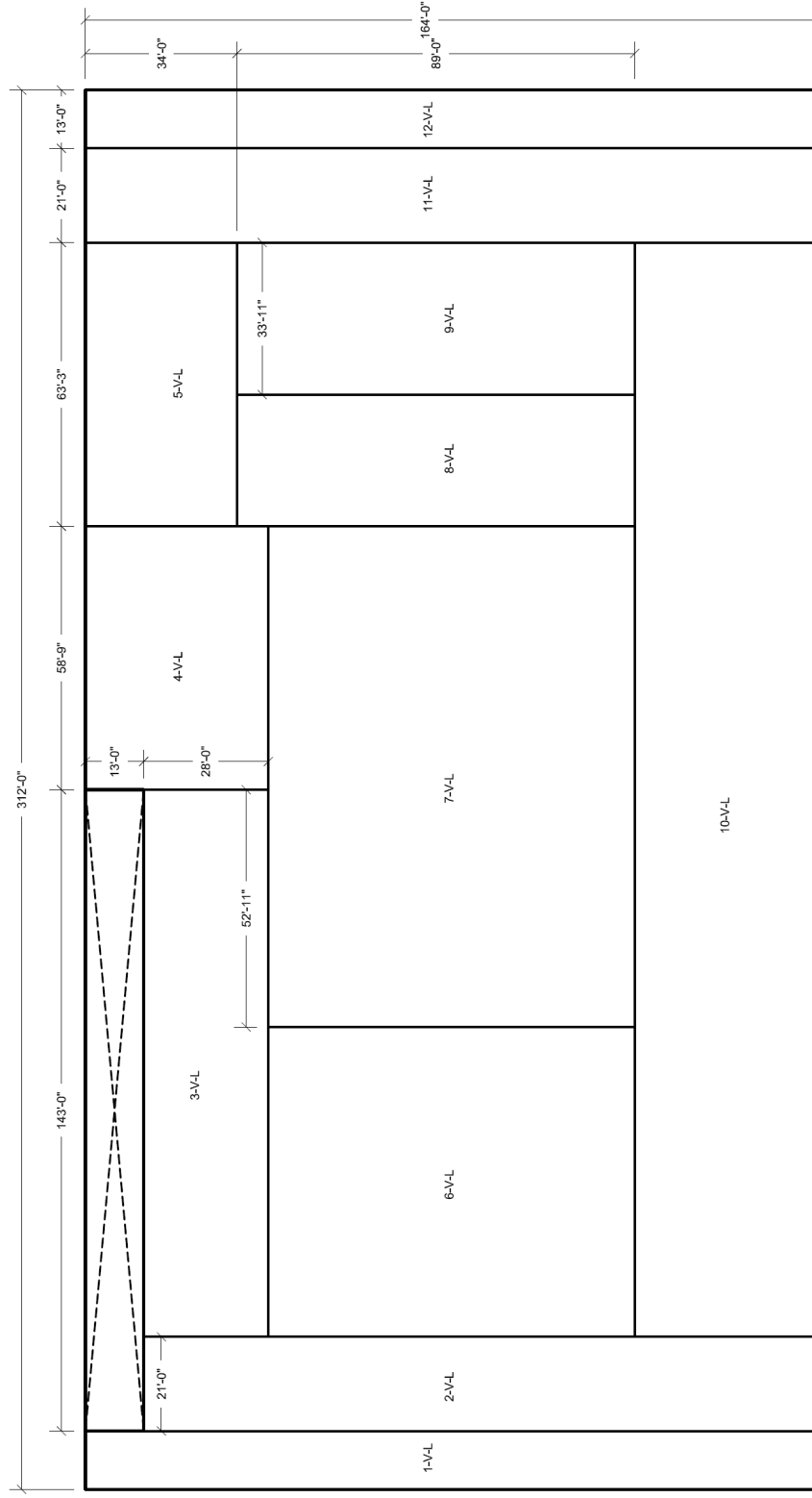


FIGURE 3H.6-134: UHS BASIN FOUNDATION MAT
NORTH/SOUTH REINFORCEMENT ZONES
BOTTOM FACE

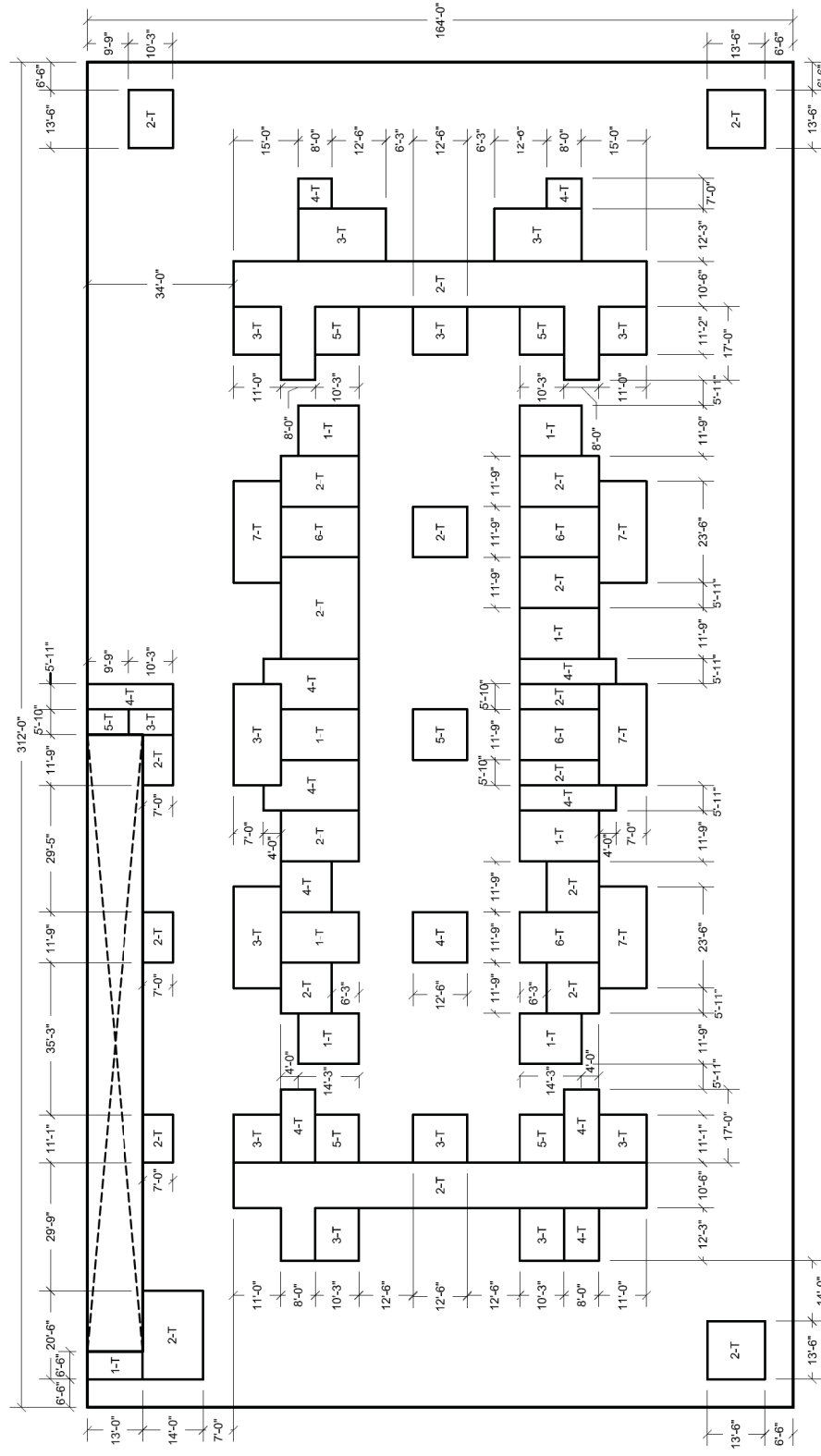


FIGURE 3H.6-134A: UHS BASIN FOUNDATION MAT
TRANSVERSE REINFORCEMENT ZONES

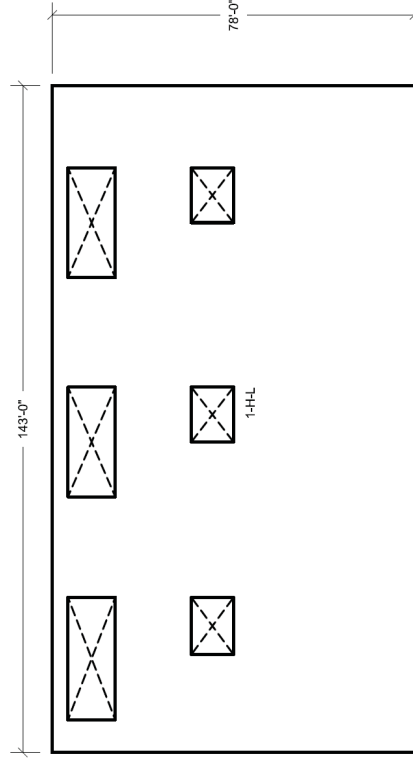


FIGURE 3H.6-135: PUMP HOUSE ROOF
EAST/WEST REINFORCEMENT ZONES
TOP FACE

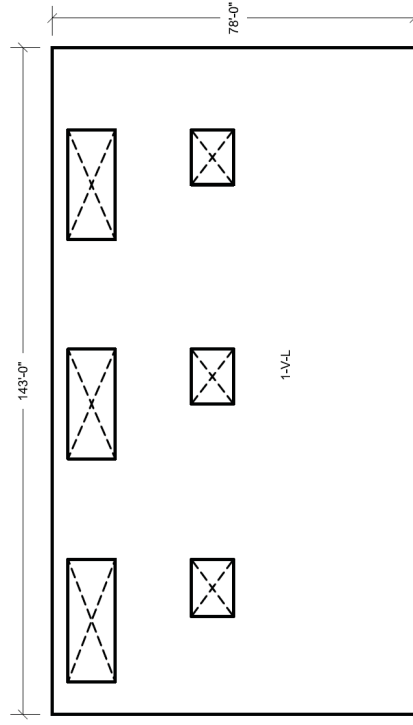


FIGURE 3H.6-138A: PUMP HOUSE ROOF
NORTH SOUTH REINFORCEMENT ZONES
TOP FACE

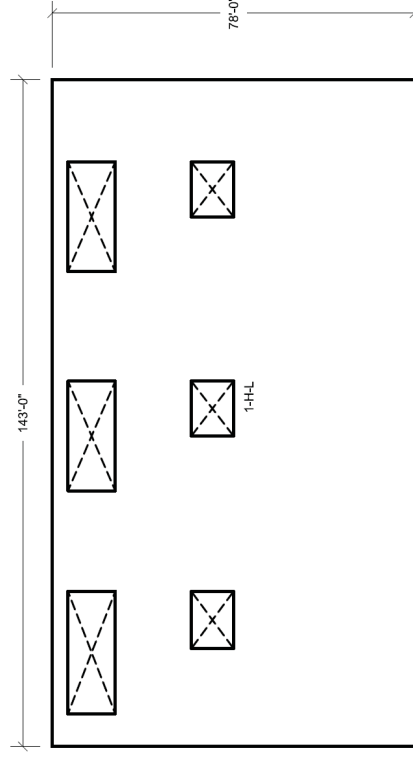


FIGURE 3H.6-138B: PUMP HOUSE ROOF
EAST/WEST REINFORCEMENT ZONES
BOTTOM FACE

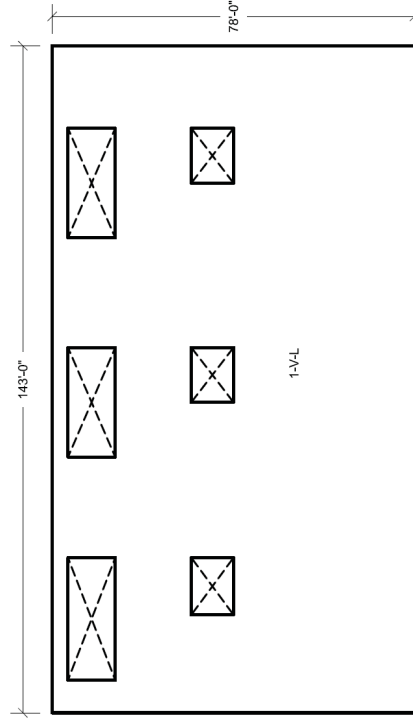


FIGURE 3H.6.1.86C: PUMP HOUSE ROOF
NORTH-SOUTH REINFORCEMENT ZONES
BOTTOM FACE



