

Davis-BesseNPEM Resource

From: CuadradoDeJesus, Samuel
Sent: Thursday, June 16, 2011 9:04 AM
To: 'dorts@firstenergycorp.com'
Cc: 'custer@firstenergycorp.com'; Medoff, James
Subject: RE: Today's Conference Call with Davis Besse

Steve

Below are the topics our staff will be discussing during the conference call today. Please forward it to your team.

- 1) Discuss absence of a TLAAs on their bases for non-Class 1, non-piping components.
- 2) Discuss extension of the scope of RAI 4.1-2 to both the time-dependent J-integral analysis in and the time-dependent fatigue crack growth analysis in Structural Integrity Associates (SIA) Topical Report No. SIR-99-040, Revision 1, "ASME Code Case N-481 of Davis Besse Reactor Coolant Pumps." (ADAMS Accession No. ML011200090). The scope of the RAI, as issued, only talked about the fatigue crack growth analysis in the Report, which forms the basis for applying VT-1 or EVT-1 visual examinations of the outside surfaces of the reactor coolant pump (RCP) casing welds in lieu of the UT examinations that would be required by the ASME Section XI Code of Record. There is a possibility, that 10 CFR 50.55a made them update to a more recent edition of the ASME Section XI Code that has incorporated the visual examinations requirements for the pump casings. If this is the case we need to know whether their CLB is still relying on the SIA report in support using the visual methods cited in the updated ASME Section XI Code of Record.
- 3) Discuss their UFSAR Appendix 5A design basis for RCP flywheel integrity – we agree that the RTndt analysis for the flywheels in that appendix does not need to include a time-dependent neutron fluence-based $\Delta RTndt$ adjustment in the manner that they are included in the RTndt analyses for the reactor vessel beltline components (i.e. beltline base metals and weld components). However, UFSAR Appendix 5A states that the SRP 5.4.1.1 acceptance basis is an 80°F difference basis between the RTndt value and the operating temperature (which according to the UFSAR Appendix, puts the minimum 120°F operating temperature for them). Contrary to this statement, we determined that the SRP 5.4.1.1 states (recommends) that the difference between the RTndt value and the operating temperature should be at least 100°F, which for full conformance with the SRP basis would dictate a minimum operating temperature of 140 °F for the RCP flywheels at Davis Besse. The UFSAR Section 5A also states that Section 3.1 of the UFSAR gives the 120 °F operating temperature basis for the flywheels, but we could not find any such basis in UFSAR Section 3.1. The other thing we need to inform them is that SRP 5.4.1.1 on flywheel integrity (which they use as the UFSAR Appendix 5A basis) states that the RTndt values for the RCP flywheel plate will be based on actual drop-weight testing results; however, they establish the RTndt value for the SA-533 flywheel plates materials using generic application of the RTndt values for their SA-533 plate materials for the RV beltline materials (pick 40°F as the highest value. We are aware that this is a current licensing basis issue – thus no RAI will be issued.
- 4) DCI/CVIB will discuss aging management of reactor vessel internal (RVI) components with them, with Seung Min's (DLR) participation on CASS AMRs for RVI components. Chris Sydnor is DCI/CVIB's lead review. Ganesh Cheruvenki may attend. The discrepancy between the Technical Specification 5.5.4 inspection requirements for their RVI vent valve discs and their plant-specific PWR Vessel Internals Program criteria are among one matter that needs to be discussed with them. The other is on the adequacy of the AMRs for the RVI components.

The call will be held at 1:00 PM EDT, 12 noon CDT and 10:00 PDT.
The phone number and pass code for the conference call are:

Phone Number: 877-917-9488
Participant passcode: 60937

Hearing Identifier: Davis_BesseLicenseRenewal_Saf_NonPublic
Email Number: 134

Mail Envelope Properties (Samuel.CuadradoDeJesus@nrc.gov20110616090300)

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From: CuadradoDeJesus, Samuel

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