



EPRI/NRC-RES FIRE PRA METHODOLOGY

Fire Fundamentals: Definitions

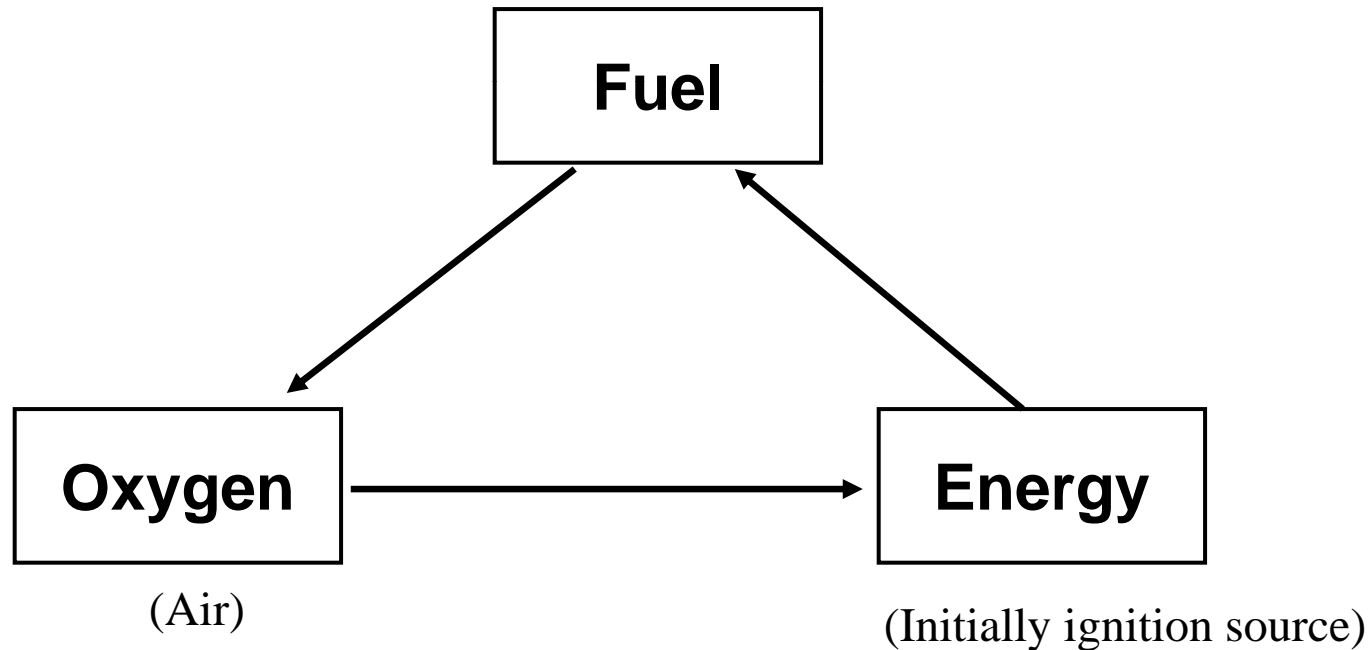
A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

What is a Fire?

- Fire is an exothermic chemical reaction involving a fuel and oxygen in the air
 - Requires presence of:
 - Material that can burn, the fuel
 - Oxygen (air)
 - Energy (initial ignition source)
 - Ignition source can be a spark, short in an electrical device, etc.

What is a Fire?

- Fire Triangle



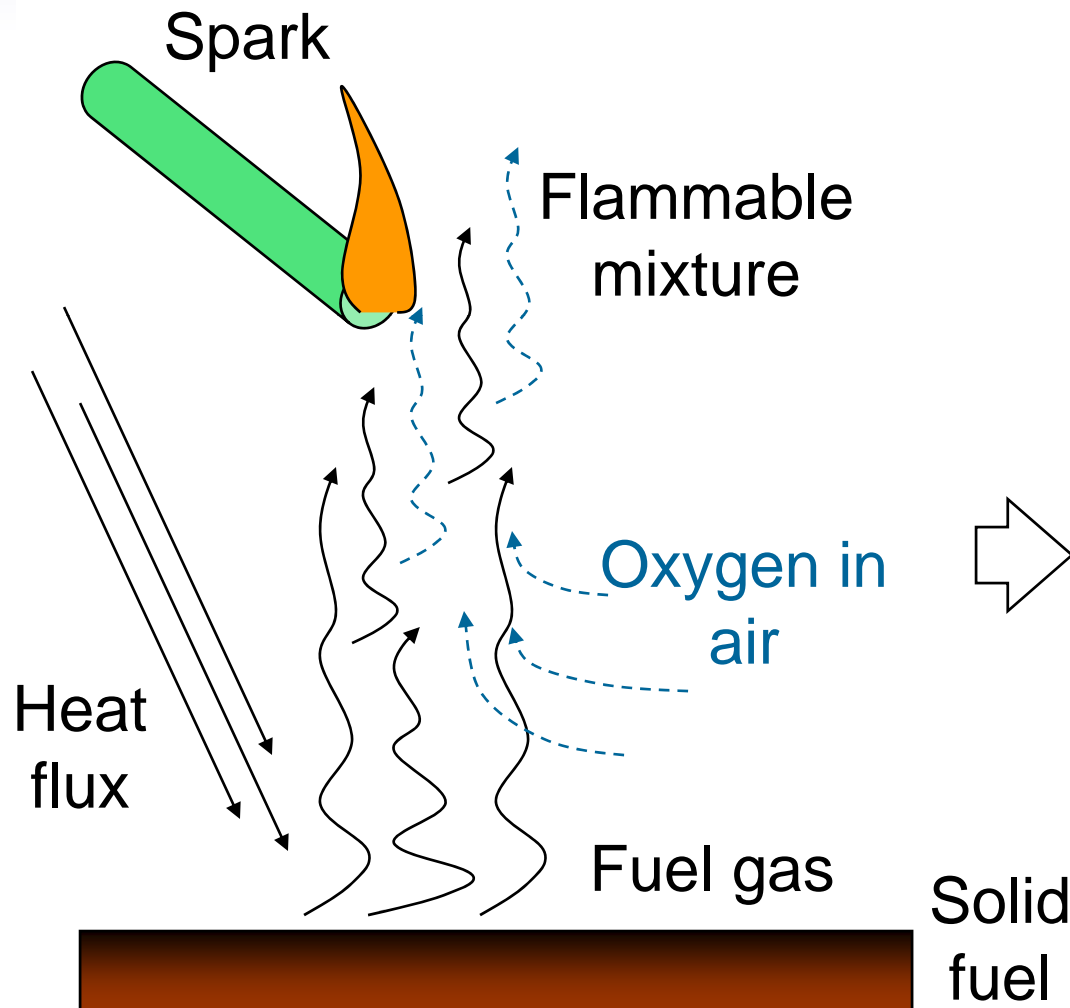
Materials that May Burn

- Materials that can burn are generally categorized by:
 - Ease of ignition (ignition temperature or flash point)
 - Flammable materials (e.g., gasoline)
 - Combustible materials (e.g., wood, high ignition temperature oils, and diesel fuel)
 - State
 - Solid (wood, electrical cable insulation)
 - Liquid (diesel fuel)
 - Gaseous (hydrogen)

Combustion Process

- Combustion process involves . . .
 - An ignition source comes into contact and heats up the material
 - Material vaporizes and mixes up with the oxygen in the air and ignites
 - Exothermic reaction generates additional energy that heats the material, that vaporizes more, that reacts with the air, etc.
 - Flame is the zone where chemical reaction is taking place

What is Fire?



Flame Characteristics

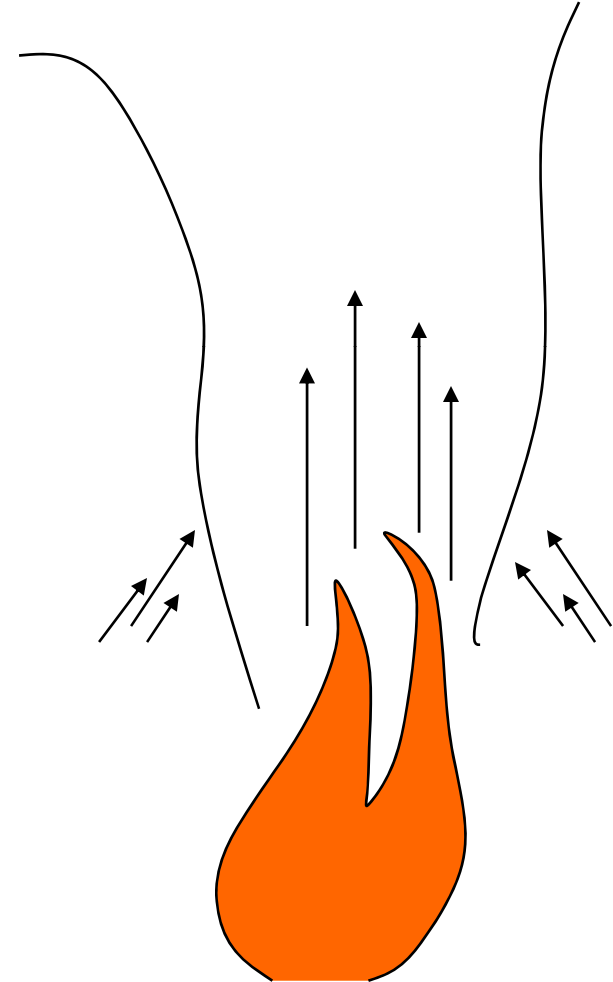
- Flame characteristics
 - Flame color depends on the material burning
 - Most flames are visible to the naked eye
 - Flame temperature can range from 1,500°F to 3,500°F – For example . . .
 - Laminar flames ~ 3,500 °F, e.g., a candle flame
 - Turbulent flames ~ 1,500 °F, e.g., a fire place

Effects of a Fire

- A fire generates heat, smoke and combustion products
 - Heat is the main adverse effect of concern in a nuclear power plant
 - Heat generated by the fire is transferred by radiation and convection
 - Products of combustion include soot and other species such as HCL, etc.
 - Smoke and soot can adversely affect equipment
 - Smoke can be a hindrance to plant operators

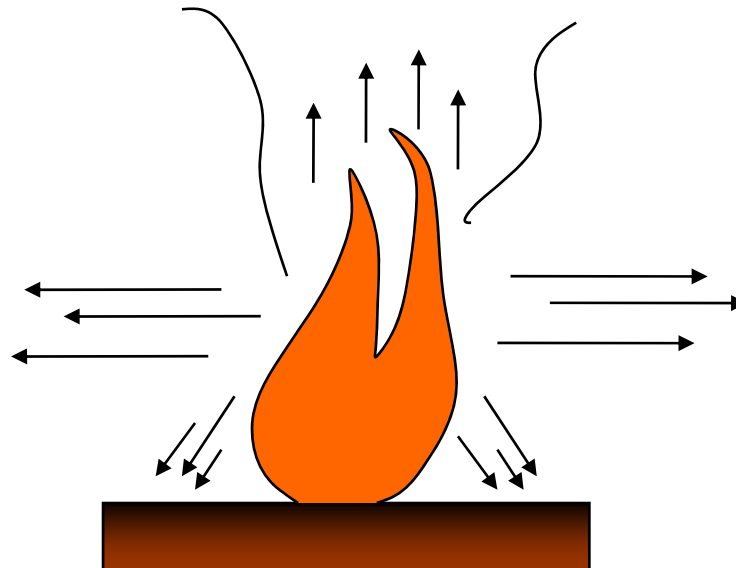
Fire Plume

- A fire plume . . .
 - Draws fresh air from the surroundings
 - A part of the air gets used in the flame
 - Air drawn above the flames gets heated up
 - The hot gases rise and envelope items above the fire with very hot gases
 - Hot gases transfer the larger portion of the energy generated by a fire by convection



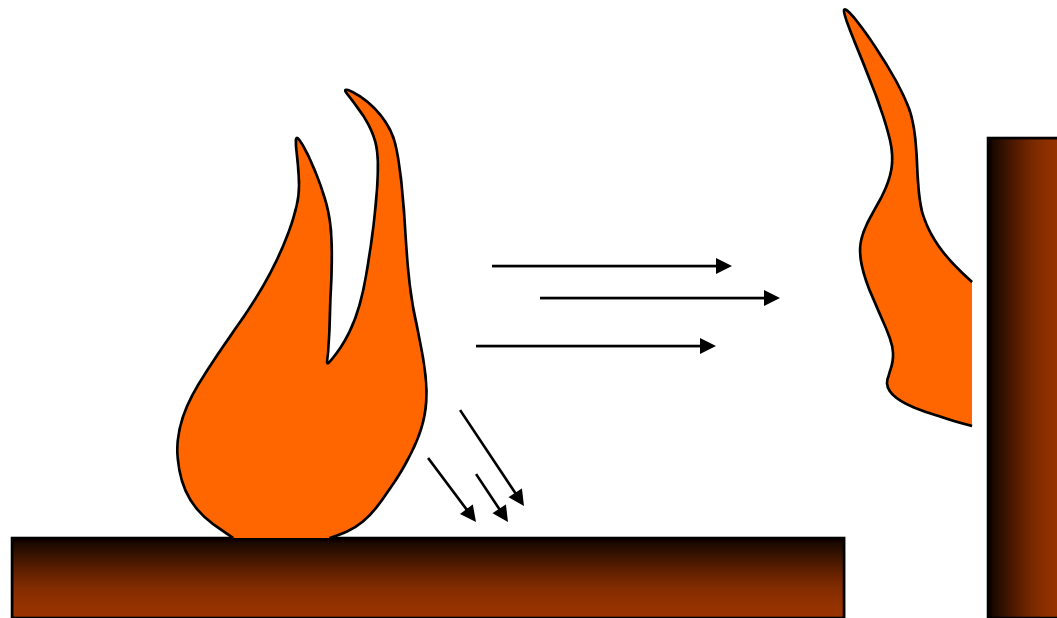
Radiative Heat of a Fire

- Radiative heat from a fire is emanated from the flame in all directions
 - A part of the radiative heat evaporates the fuel to continue the combustion process



Flame Spread and Fire Propagation

- Flame spread is a series of ignitions that can lead to fire propagation to adjacent or nearby items



Definitions

- Pyrolysis – Breakdown of the molecules of a solid material from exposure to heat into gaseous molecules that combust in the flame.
- Smoldering – A slow combustion process without visible flames that occurs in a porous solid fuel (e.g., burning of charcoal briquets or wood in a fire pit). Generally occurs because of limited oxygen access to the burning surfaces. It can generate large quantity of carbon monoxide which is lethal if inhaled.

Definitions

- Spontaneous Ignition – Ignition of a combustible or flammable material without an ignition source, which is generally caused by raising material temperature above its auto-ignition temperature.

vs. ...

- Piloted Ignition – Ignition of a combustible or flammable material in the presence of a pre-existing flame (the “pilot” flame)
- Piloted ignition generally occurs at a lower temperature than spontaneous ignition

Definitions

- Flame - A flame is the visible (light-emitting) part of a fire. It is caused by an exothermic reaction taking place in a thin zone where fuel vapors and oxygen in the air meet.
- Fire Plume - A fire plume is a buoyant column of hot air rising above the base of a fire
- Ceiling Jet – When the fire plume hits the ceiling, the flowing gasses turn 90° and form a relatively thin layer of flowing gas just below the ceiling – this is the “ceiling jet”

Definitions

- Hot Gas Layer – As the fire progresses, the heated air and combustion products tend to collect in a layer between the ceiling and somewhere above the floor – this is the HGL (sometimes called the smoke layer)

vs. ...

- Lower or Cold Gas Layer – The gasses that remain between the floor and the bottom of the HGL and that generally remain at near ambient temperatures
- The depth of the HGL (distance from the ceiling to the bottom of the HGL) will be determined largely by ventilation conditions (e.g., an open door, open window...)

Definitions

- Diffusion Flame – The flame of a burning material (liquid or solid) where the combustion process occurs at the interface where vaporized fuel comes into contact with the oxygen in the air (e.g., flame on top of a candle or the wood in a fireplace.)

VS. ...

- Pre-mixed Flame – The flame of burning gaseous material that is mixed with air upstream of the flame (e.g., the flame of a gas range or gas fired furnace)
- Most of the fires we are concerned with involve diffusion flames

Definitions

- Laminar Flame – A flame with laminar flow of gases (e.g. typical candle flame).

VS. ...

- Turbulent Flame – a flame with turbulent flow of gases (e.g., most flames bigger than a candle).
- Most flames greater than a few inches tall demonstrate turbulent (non-laminar) behavior because of increased gas velocities caused by increased heat.

Definitions

- Conduction – Heat transfer between two adjacent stationary media through the interface between them (e.g., putting your hand on a cold surface)
- Convection – Heat transfer between a moving fluid and a solid or liquid material (e.g., blowing over a hot food to cool it down)
- Radiation – Heat transfer through open space via electromagnetic energy between two materials of different temperatures that are within line of sight of each other (e.g., infra-red radiation from a very hot material).

Definitions

Some key fire characteristics...

- Mass Loss Rate (Burning Rate) – The rate of mass loss of a burning material in a fire. It is commonly expressed in terms of mass per unit area per unit time (e.g., 10 g per cm² per second).
- Heat Release Rate (HRR) – The energy release per unit time from a combustible material (kW)
- Heat Flux – Heat transferred expressed per unit time per unit area (kW/m²). Its is a good measure of fire hazard.

Definitions

- Heat Release Rate Profile – The heat release rate as a function of time.
 - Example . . .

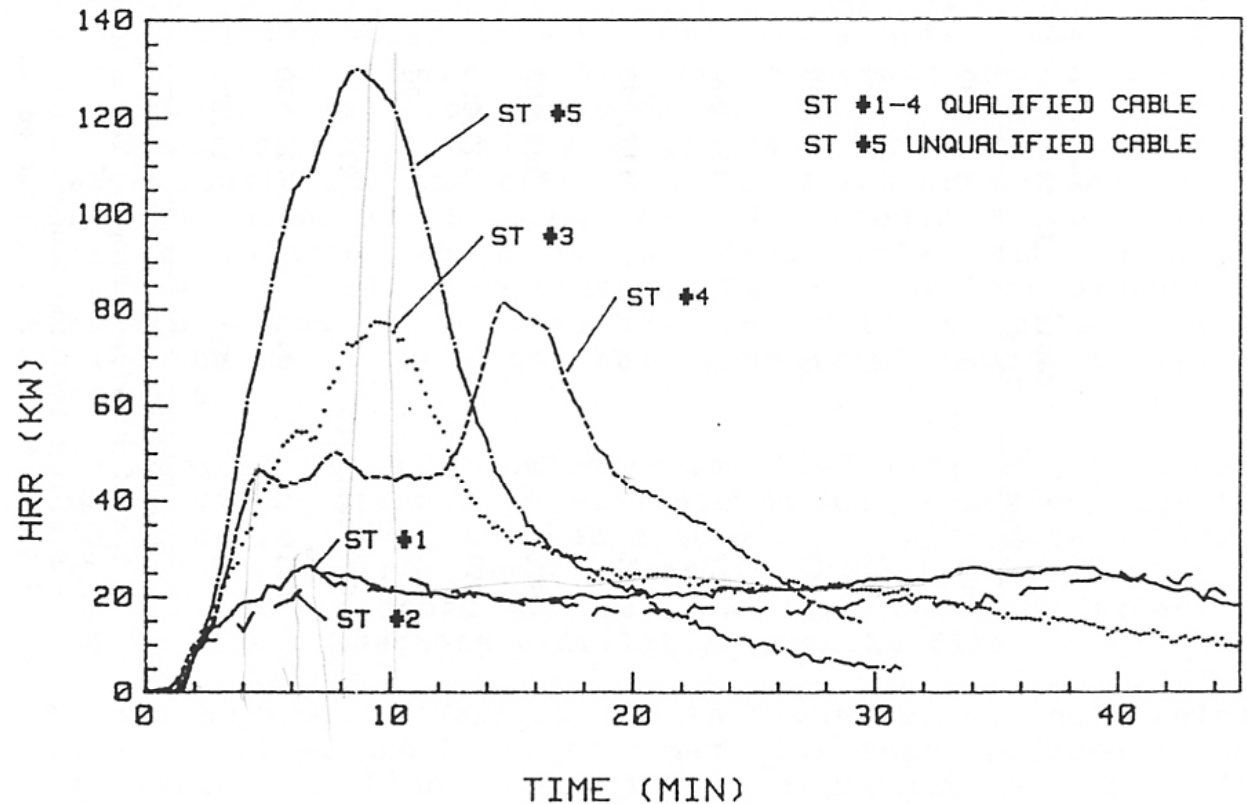


Figure 8. Heat Release Rate Plots for Scoping Tests #1 through 5

Definitions

- Fire in the Open – A fire occurring in a large or unconfined space such that there is no feedback between the fire and the ambient environment

VS. ...

- Compartment Fire (Enclosure Fire) – A fire occurring in an enclosed space such that the fire impact its surroundings creating a feedback effect; e.g.
 - The walls get hot and feed radiant energy back to the fire
 - A HGL forms and feeds radiant energy back to the fire
 - The HGL descends to the floor and reduces the oxygen available to the fire
- We tend to deal mainly with compartment fires.

Definitions

- Fuel Limited Fire – A fire where the heat generated by the fire is limited only by the surface burning rate of the material.

VS. ...

- Oxygen Limited Fire – A fire (typically inside a compartment or enclosure) where the heat release rate is limited by Oxygen availability
 - Not enough air for fire to grow beyond a certain point
- We tend to deal primarily with fuel limited fires, but cabinet fires, for example, may be oxygen limited

Definitions

- Upper and Lower Flammability Limits – Concentration of a flammable gas in air in a pre-mixed flame that can sustain combustion. If the mixture is close to lower flammability limit, it is too lean. If the mixture is close to the upper flammability limit, it is too fuel rich.
- Fire Modeling vs. Fire Analysis Tasks – Fire modeling is the analytical process of estimating the behavior of a fire event in terms of the heat flux impinging material near the fire and behavior of those materials as a result of that.

Definitions

- Zone-of-Influence (ZOI) – The area around a fire where radiative and convective heat transfer is sufficiently strong to damage equipment or cables and/or heatup other materials to the point of auto-ignition.



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Fires in the Open and Fully Ventilated Fires

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Recall: Fuel limited fires

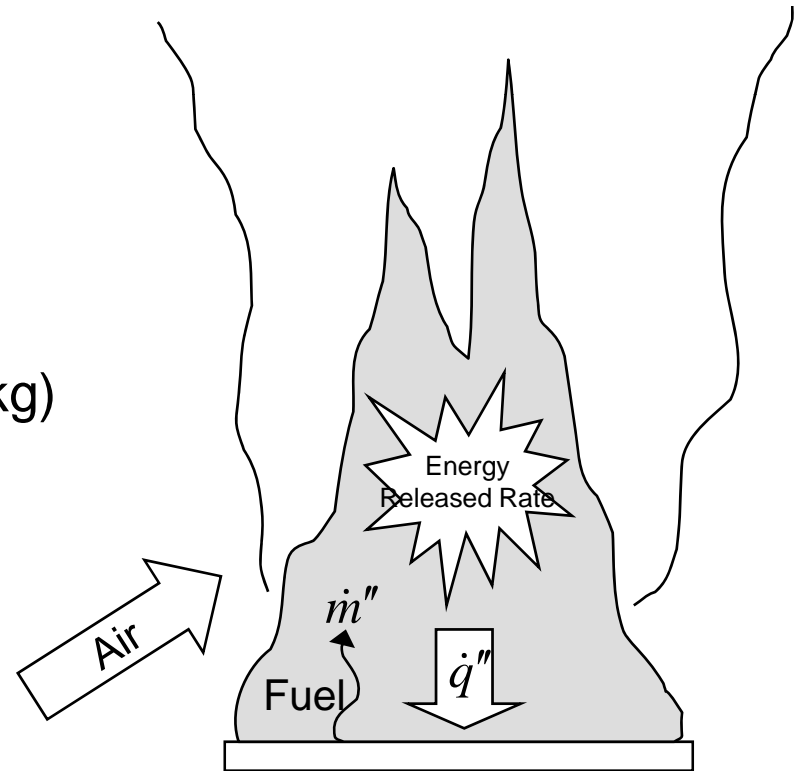
- A fire event where heat generated from the fire is limited by the surface burning rate of the material.
- Sufficient air is always available for the fire.
- Generates hot gases and radiative heat
- Generally applies to fires in the open or fires in large compartments
 - A nuclear power plant has lots of large compartments...

Heat Release Rate

- The heat release rate from a fire can be estimated using the following equation:

$$\dot{Q} = \dot{m}'' \cdot A \cdot \Delta H_c$$

- \dot{m}'' is the burning mass flux
- ΔH_c is the heat of combustion (kJ/kg)
- A is the burning area (m²)

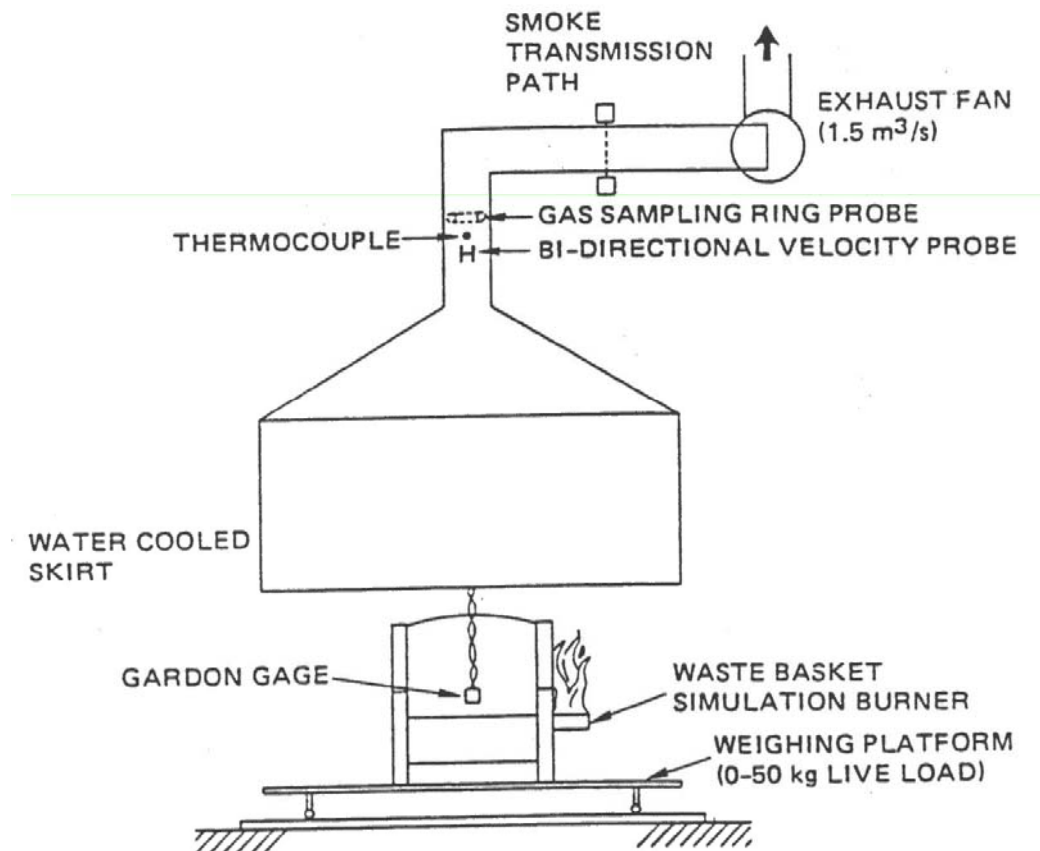


Heat Release Rate

- Can be estimated experimentally using oxygen consumption calorimeters

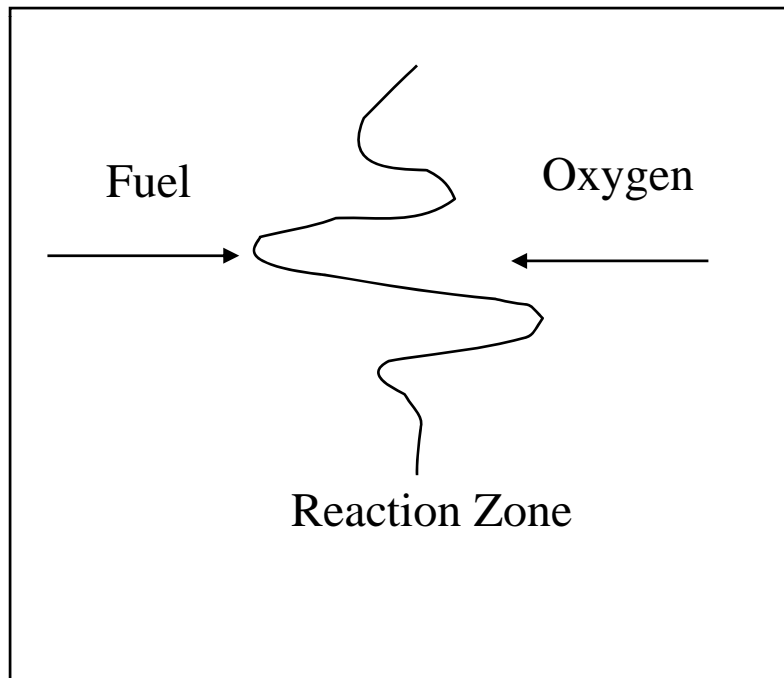
$$\dot{Q} = \dot{m}_{O_2} \cdot \Delta H_c (kJ / kg_{O_2})$$

$$\Delta H_c = 13.1 \text{ kJ/kg}_{O_2}$$



Flames

- Laminar
- Turbulent



Ignition of Gases

- With a spark or small flame (**pilot**) present, ignition is based on whether the gaseous fuel concentration is between the upper (rich) and lower (lean) flammability limits.
 - The fuel-air (oxidizer) mixture is said to be flammable if a flame will propagate in this mixture.
- For no pilot present, a gaseous fuel in air can also ignite if the mixture is at or above the **auto-ignition** temperature.
 - The auto-ignition temperature is usually measured for a stoichiometric mixture in which no fuel and oxygen remain after the reaction.

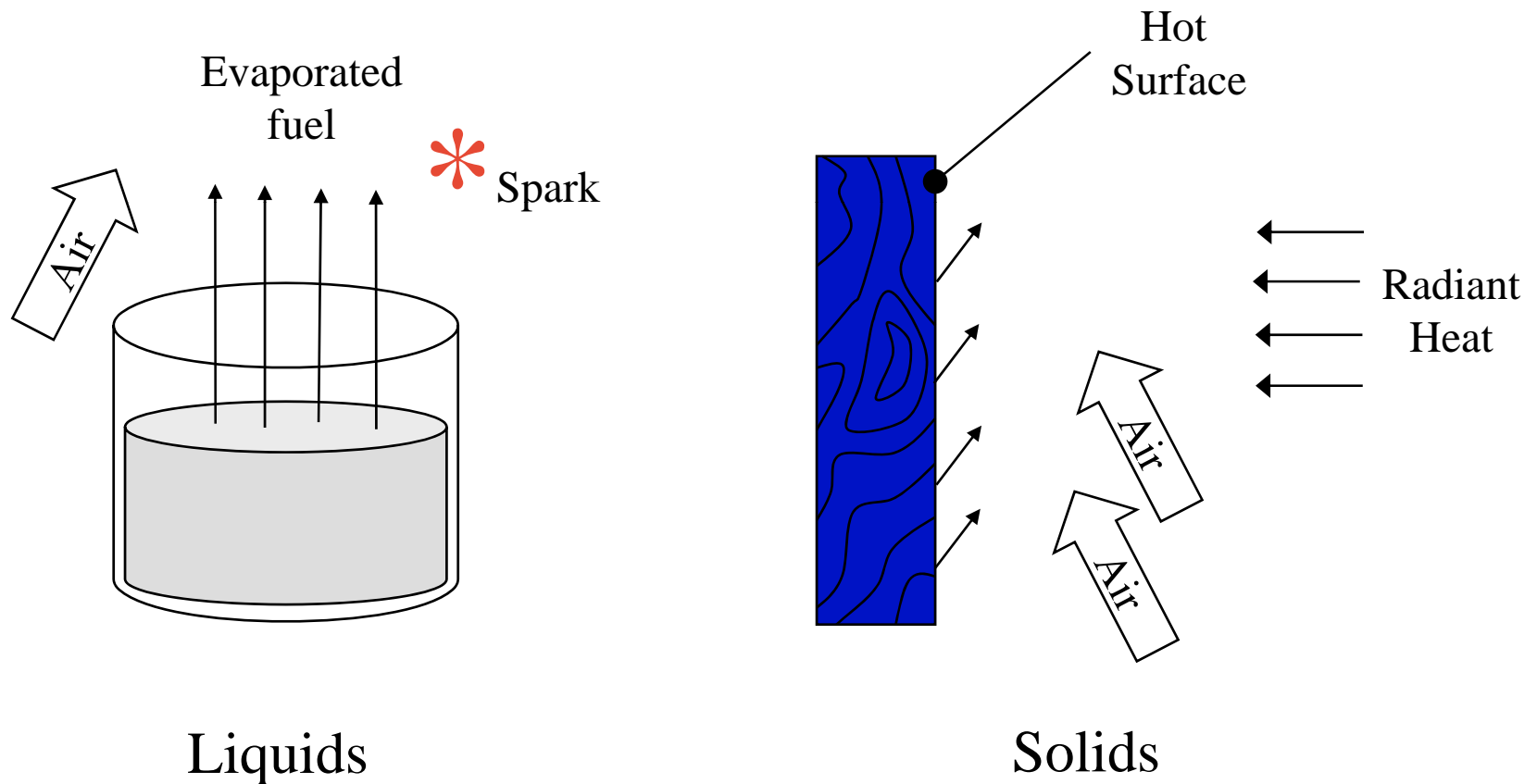
Ignition of Liquids

- For a liquid to ignite, it must first **evaporate** sufficiently to form a flammable mixture in the presence of a pilot.
 - This occurs at a liquid temperature called a **flash-point** temperature.
 - In general, this can be called the **piloted ignition temperature** and the term carries over to solids.
 - The flash-point is the temperature at which the amount of liquid evaporated from the surface achieves the lower flammable limit.
- If no pilot is present, the mixture must be heated to the auto-ignition temperature.
- Auto-ignition temperature of gases is above its boiling point.

Ignition of Solids

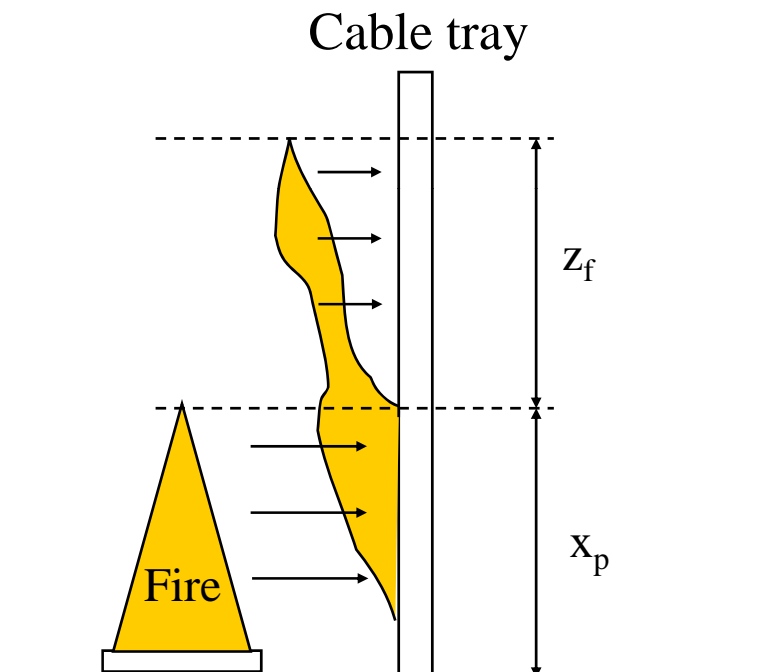
- Solids do not vaporize like liquids when heated. They form gaseous decomposition compounds leaving behind possible char in a process called **pyrolysis**.
- At some point, the gases ignite by piloted ignition or auto-ignition.
- Typically, piloted ignition temperatures for solids range from 250°C (~480°F) to 450°C(~840°F).
- Auto-ignition temperatures can exceed 500°C (~930°F).
 - For a given material, these temperatures are not constants and can change with the nature of heating.
 - For practical purposes, a (piloted) ignition temperature (T_{ig}) may be treated as a property of a combustible solid.
- We shall consider thin (less than ~1 mm) and thick solids to have different time responses to ignition when exposed to impinging heat flux

Ignition



Flame Spread

- Motion of vaporization front at the ignition temperature for solids and liquids



Typical Flame Spread Rates

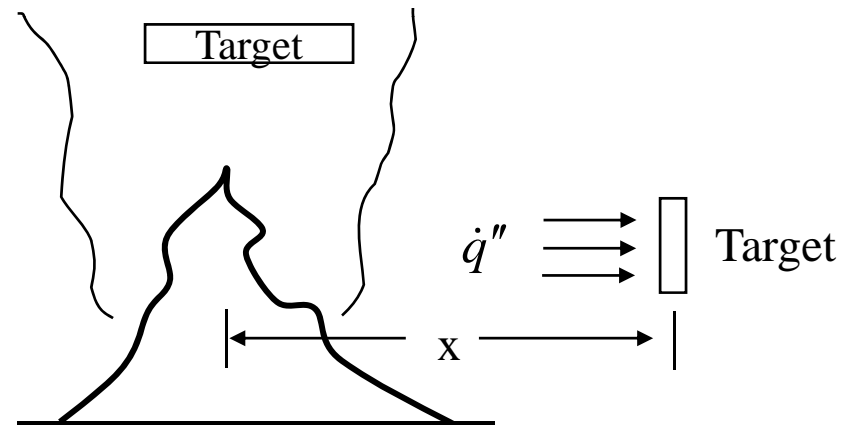
- It is very difficult to compute flame spread rate because formulas are not completely available, rates may not be steady, and fuel properties are not generally available. Nevertheless, we can estimate approximate magnitudes for spread rates based on the type of system. These estimates are listed below:

<u>Spread</u>	<u>Rate (cm/s)</u>
Smoldering solids	0.001 to 0.01
Lateral or downward spread on thick solids	0.1
Upward spread on thick solids	1.0 to 100. (0.022 to 2.2 mph)
Horizontal spread on liquids	1.0 to 100.
Premixed flames (gaseous)	10. to 100.(laminar) $\approx 10^5$ (detonations)

Zone of Influence

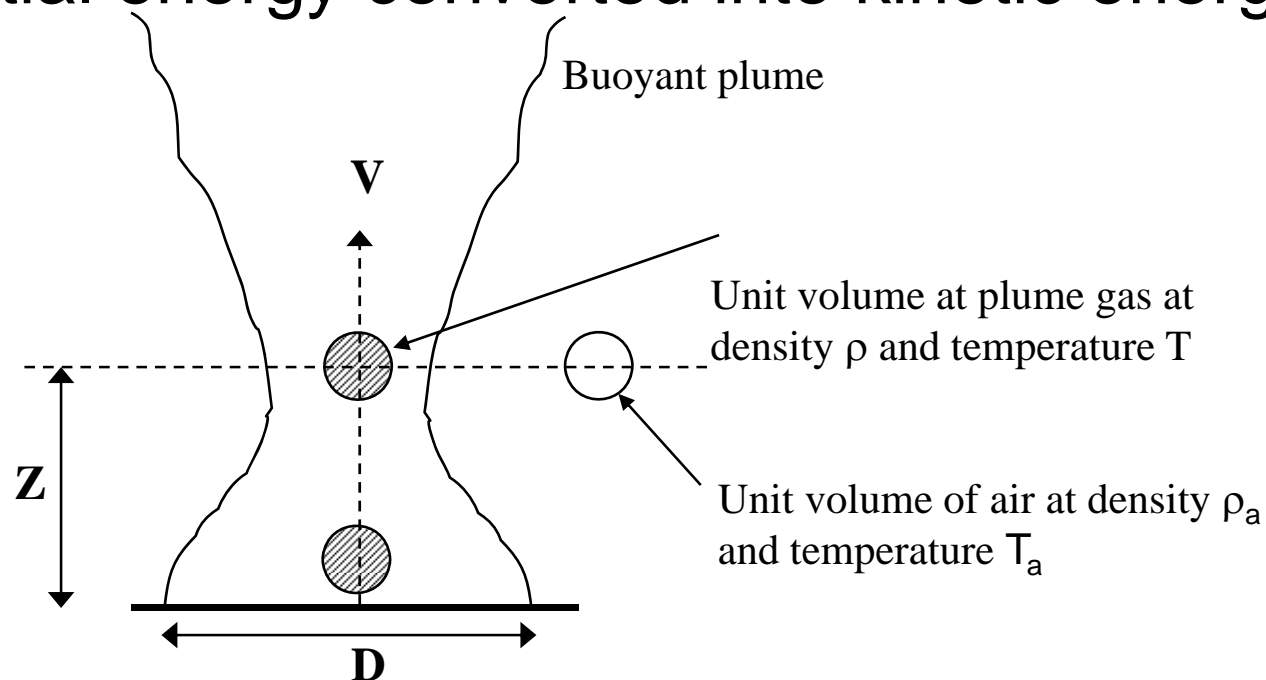
- Regions nearby the fire where damage is expected. For fires in the open:
 - Flame Radiation

- Convection inside the fire plume



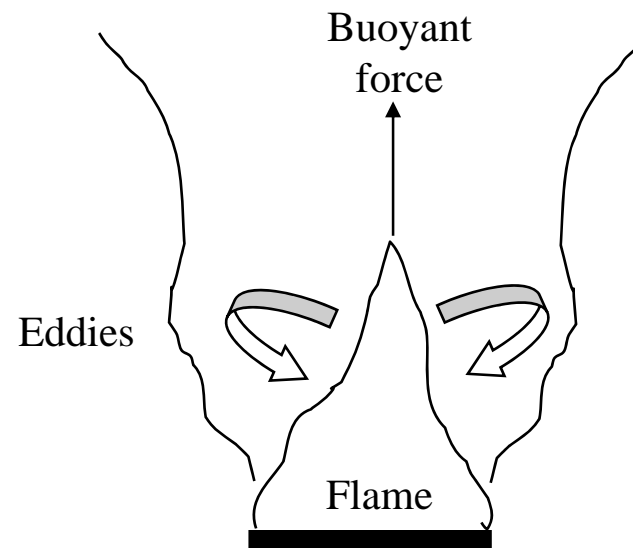
Buoyant Flow

- Temperature rise gives a decrease in density
- Potential energy converted into kinetic energy



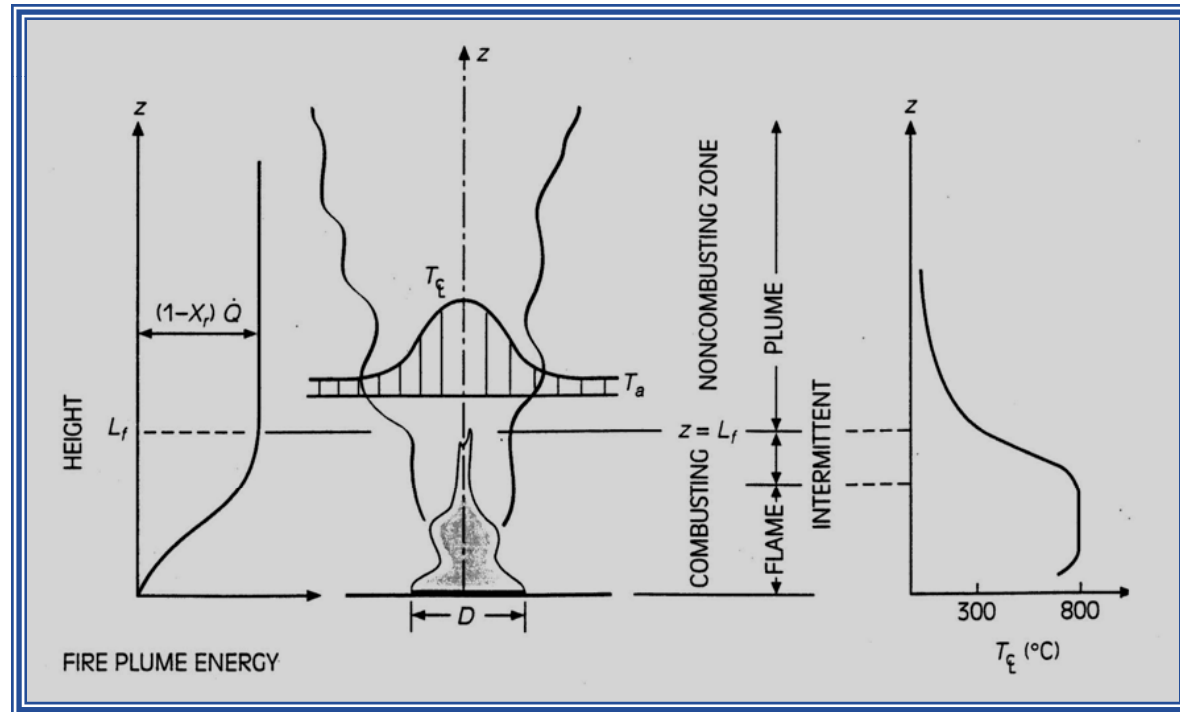
Turbulent Entrainment

- Entrainment is air drawn into the fire plume by upward movement of the buoyant plume
- Engulfment of air into the fire plume
- Eddies: fluctuating and rotating balls of fluid, large scale rolling-up fluid motion on the edge of the plume.

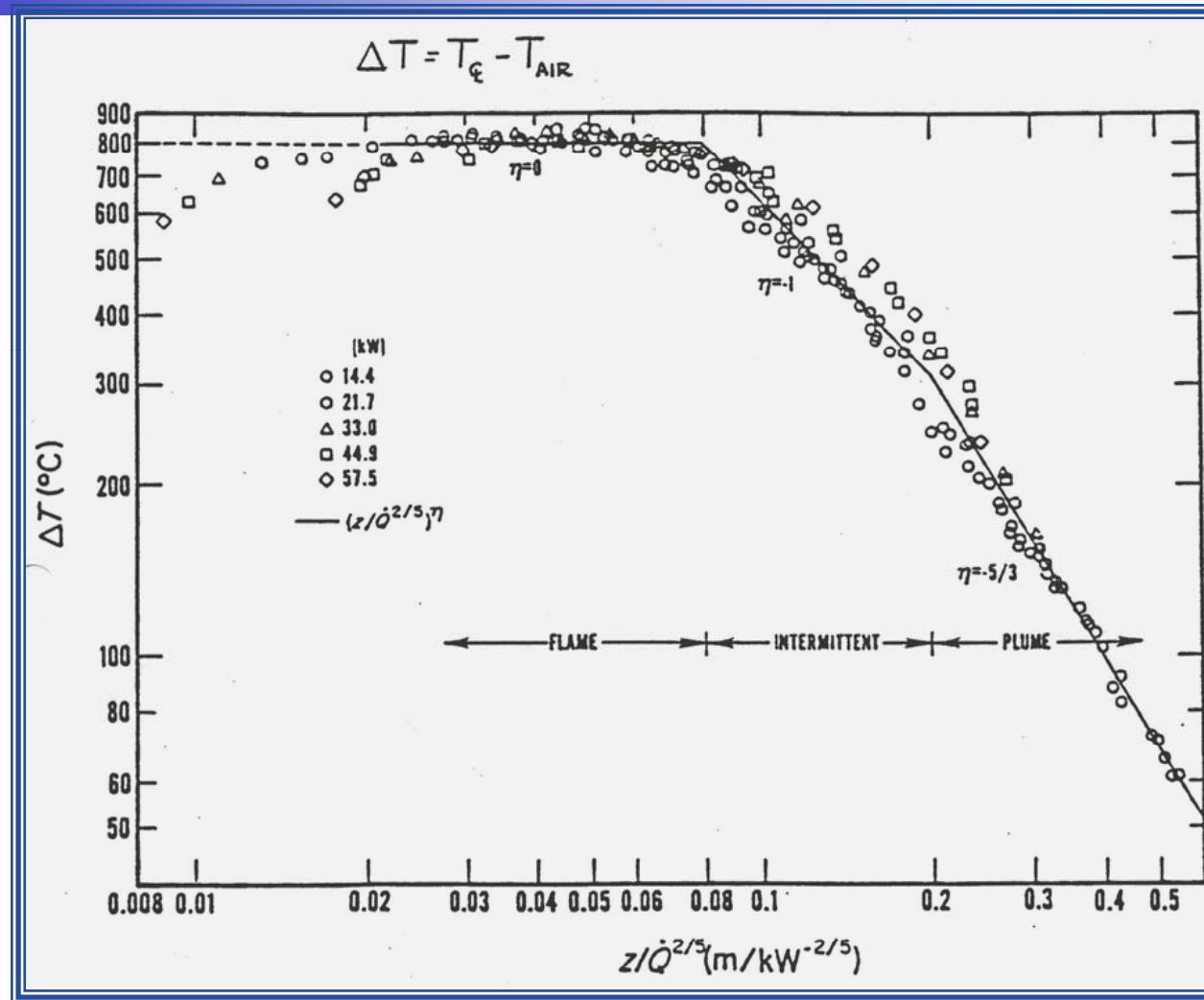


Turbulent Fire Plume

- Very low initial fuel velocity
- Entrainment and flame height controlled by buoyancy



Fire Plume Temperature Along the Centerline



Example Case - Zone-of-Influence Calculation Flame Height and Plume Temperature

$$L = 0.235 \dot{Q}_f^{2/5} - 1.02D$$

$$T_{pl} = T_{amb} + 25 \left(\frac{(k_f \dot{Q}_f (1 - \chi_r))^{2/5}}{((H_p - F_e) - z_o)} \right)^{5/3}$$

Heskestad's Flame Height Correlation

$$z_o = 0.083 \dot{Q}_f^{2/5} - 1.02D$$

Input

D - Fire diameter [m]	0.6
Q _f - HRR [kW]	250

Result

L - Flame height [m]	1.5
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Heskestad's Plume Temperature Correlation

Input

T _{amb} - Ambient temperature [C]	20
Q _f - HRR [kW]	250
F _e - Fire elevation [m]	0
H _p - Target Elevation [m]	3.7
z _o - Fire Diameter [m]	1

Result

T _{pl} - Plume Temp [C]	328
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Example Case - Zone-of-Influence Calculation Radiation Heat Flux

- Flame Radiation: Point Source Model

$$\dot{q}_{irr}'' = \frac{\dot{Q}_f \chi_r}{4\pi R^2}$$

Input Parameters:

- \dot{Q}_f : Fire heat release rate (kW)
- R : Distance from flames (m)
- χ_r : Radiation fraction of the heat release rate (FIVE recommends 0.4)
- D : Fire diameter (m)

Example Case - Zone-of-Influence Calculation Radiation Heat Flux

$$\dot{q}_{irr}'' = \frac{\dot{Q}_f \chi_r}{4\pi R^2}$$

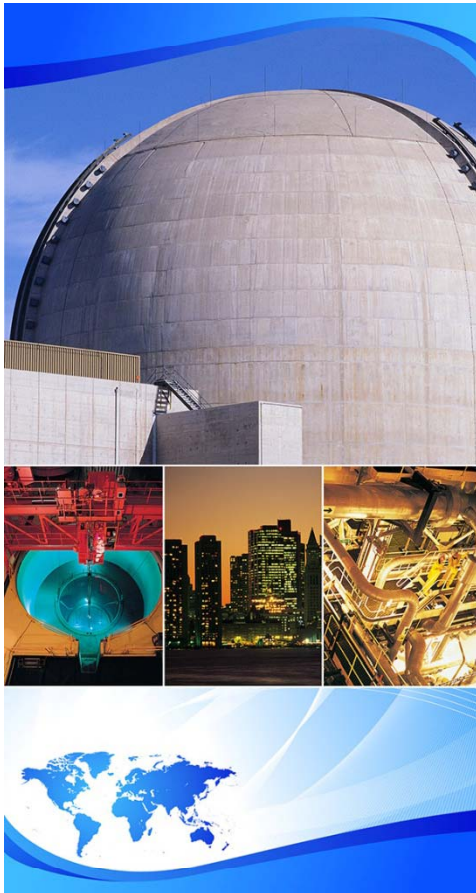
Point Source Flame Radiation Model

Inputs

Fire heat release rate [kW]	317
Radiation fraction	0.40
Distance from flames [m]	1.5

Results

Heat flux [kW/m ²]	4.5
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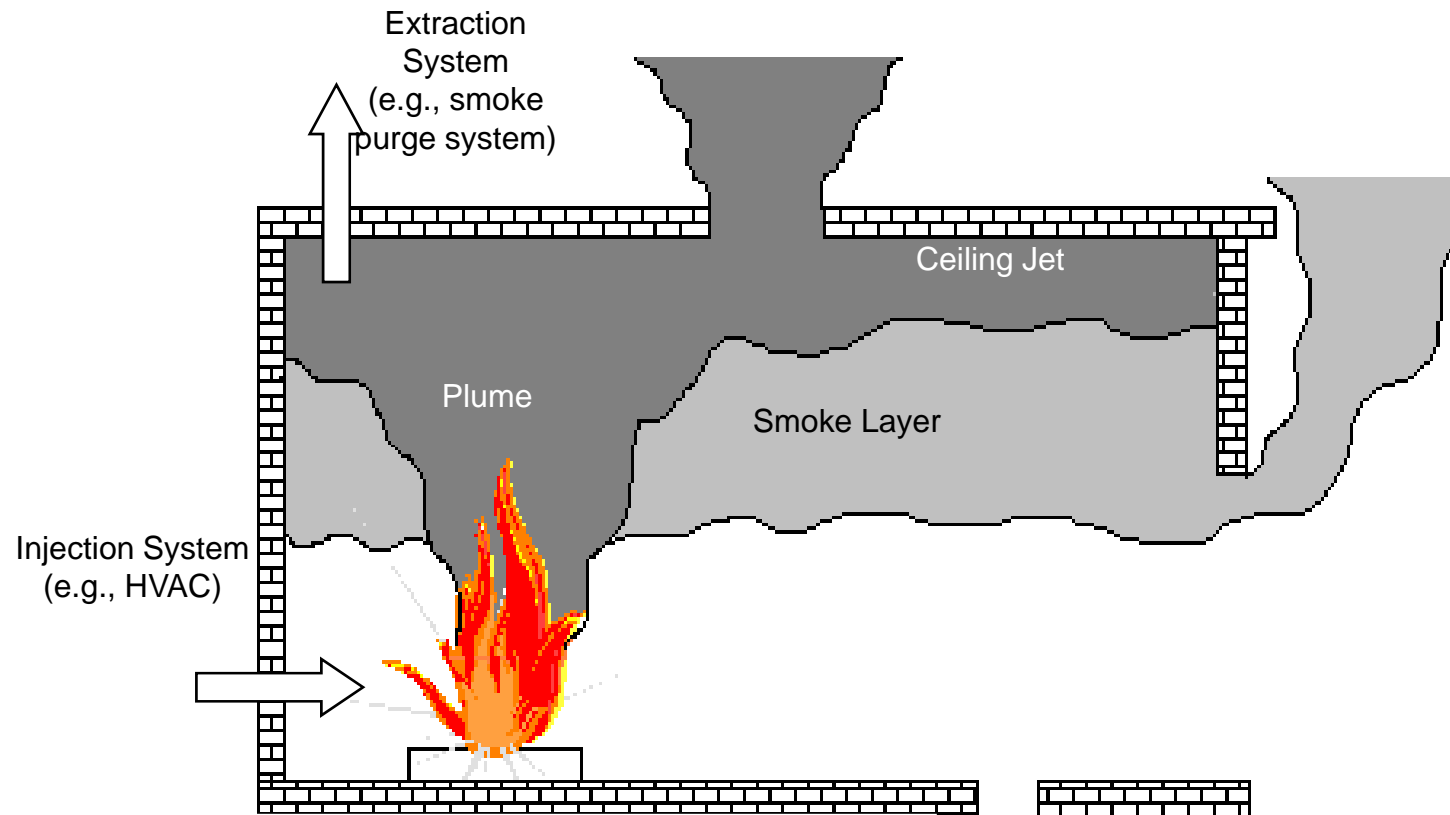
Compartment Fires

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Outline

- Compartment fire dynamics – qualitative description
- Pressure profiles and vent flows
- The hot gas layer
- Heat transfer
- Combustion products

Qualitative Description



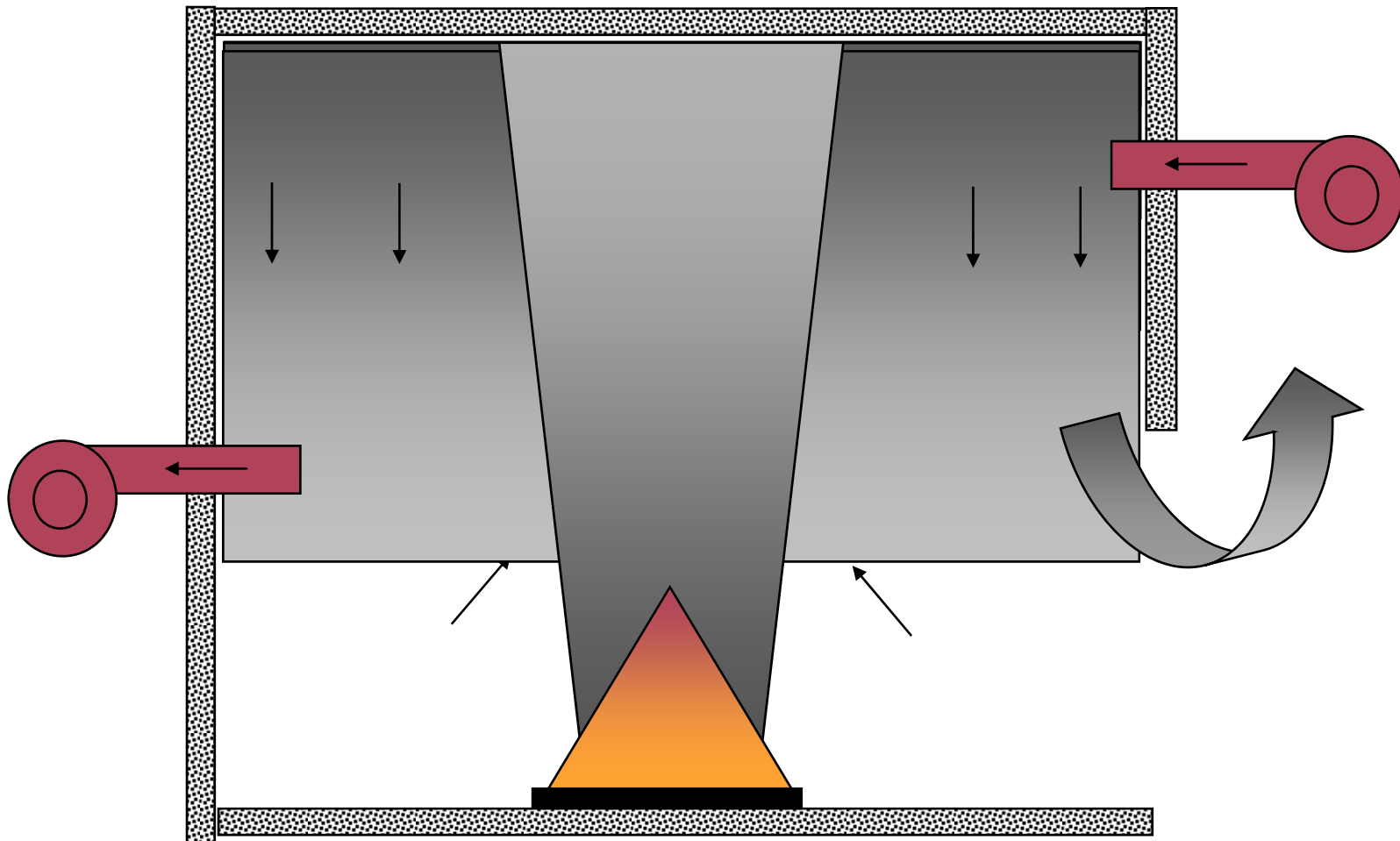
Phases in a Compartment Fire

- Ignition: Process that produces an exothermic reaction
 - Piloted or spontaneous
 - Accompanying process can be flaming or smoldering combustion
- Growth
 - Can occur at different rates depending on type of fuel, interactions with surroundings, and access to oxygen
- Hot gas layer buildup and room heatup
- Flashover: Rapid transition to a state of total surface involvement of combustible materials within an enclosure
 - Temperatures between 500°C (930°F) to 600°C (1,110°F), or
 - Heat fluxes between 15 kW/m² to 20 kW/m²

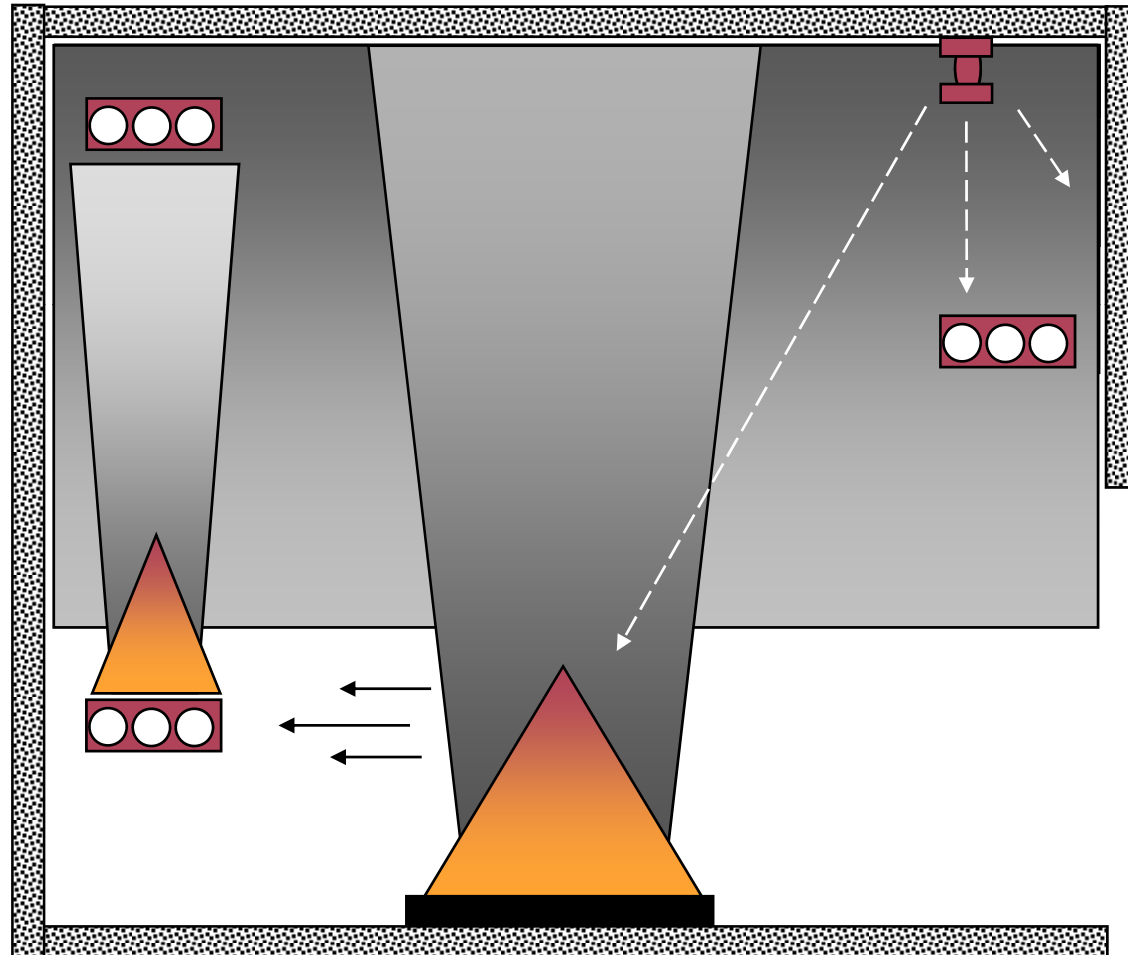
Phases in a Compartment Fire

- Fully developed fire: The energy released in the enclosure is at its greatest level and is very often limited by the available oxygen
 - Gas temperatures between 700°C (1,300°F) and 1200°C (2,200°F)
- Decay: Fuel becomes consumed
 - Hazard indicators (temperature and heat fluxes) start to decrease
- Other terminology may include
 - Pre-flashover fire
 - Focus on life safety and sensitive targets
 - In NPP, cables damage at 218°C (424°F) for thermoplastic cables and 330°C (626°F) for thermoset cables
 - Post-flashover fire:
 - Focus in structural stability and safety of firefighters

Compartment Fires



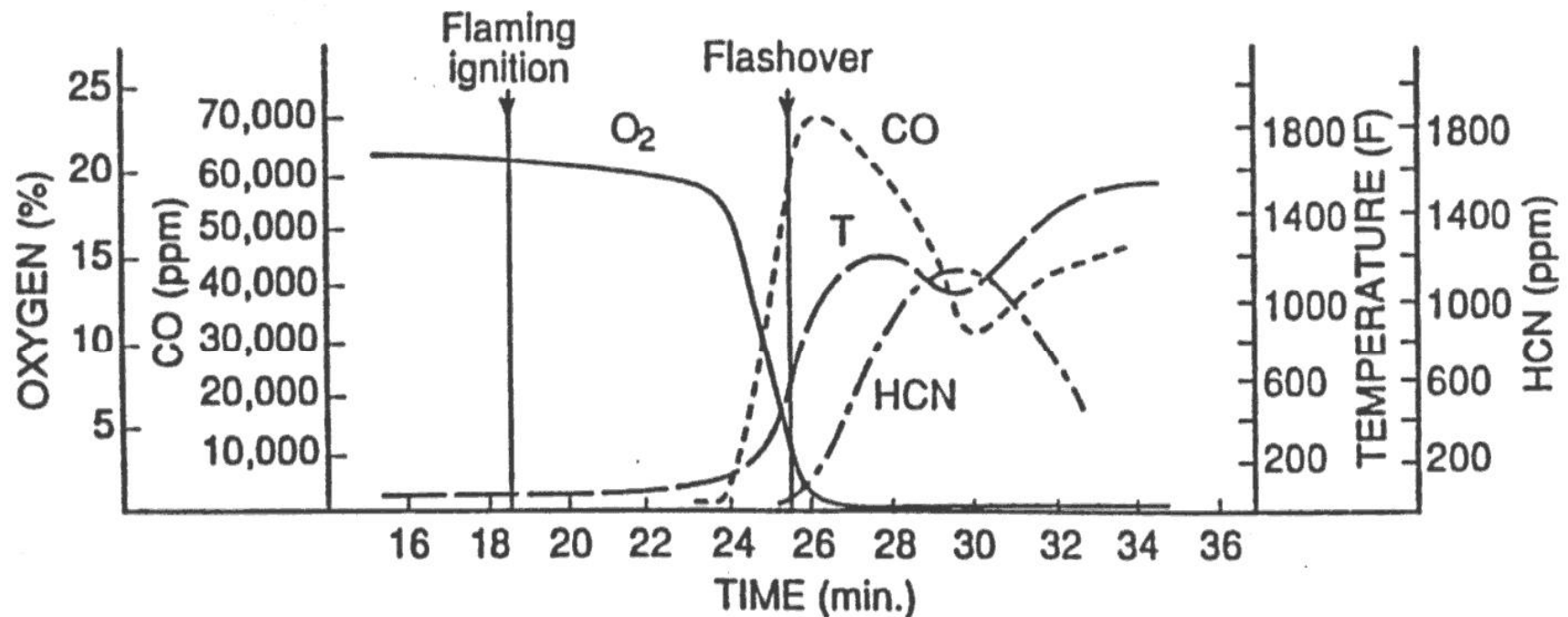
Compartment Fires



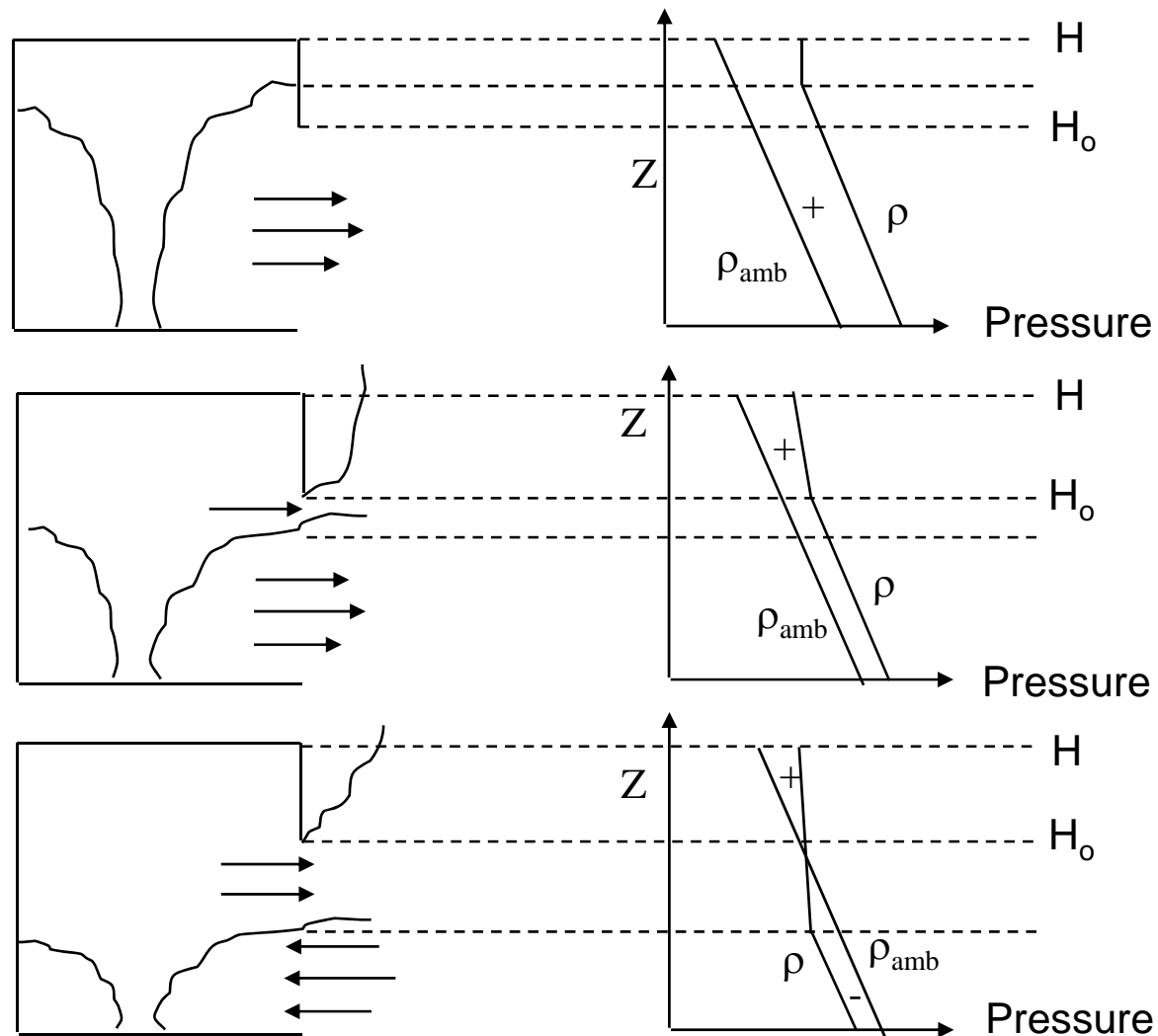
Sense of Scale

Room: 12 x 18 x 8 ft. high; open doorway

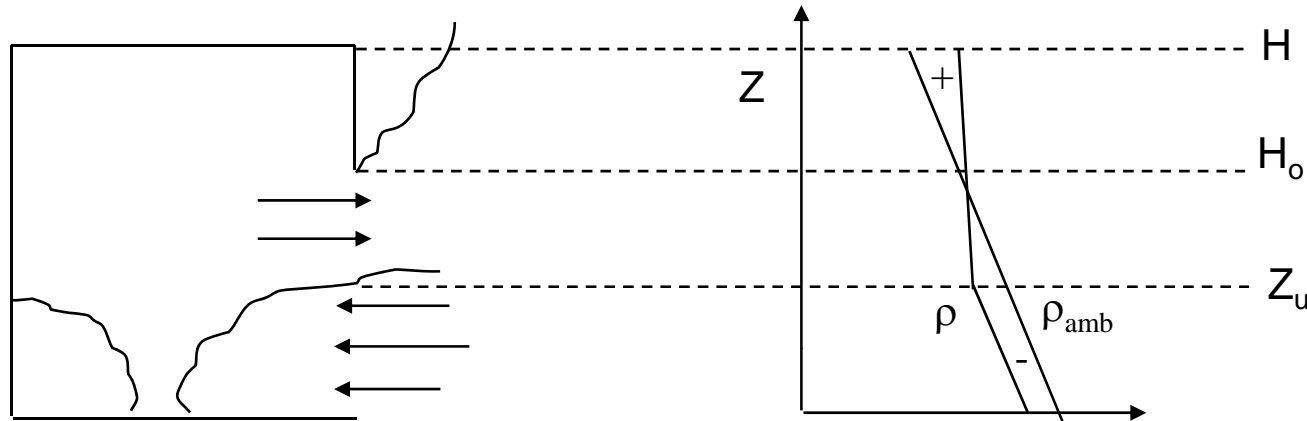
Data at 5.5 ft. height



Pressure Profiles & Vent Flows



Pressure Profiles & Vent Flows



$$P_i(h) = P_i(0) - \rho_o g Z_u - \rho_u g (h - Z_u)$$

← Inside Profile

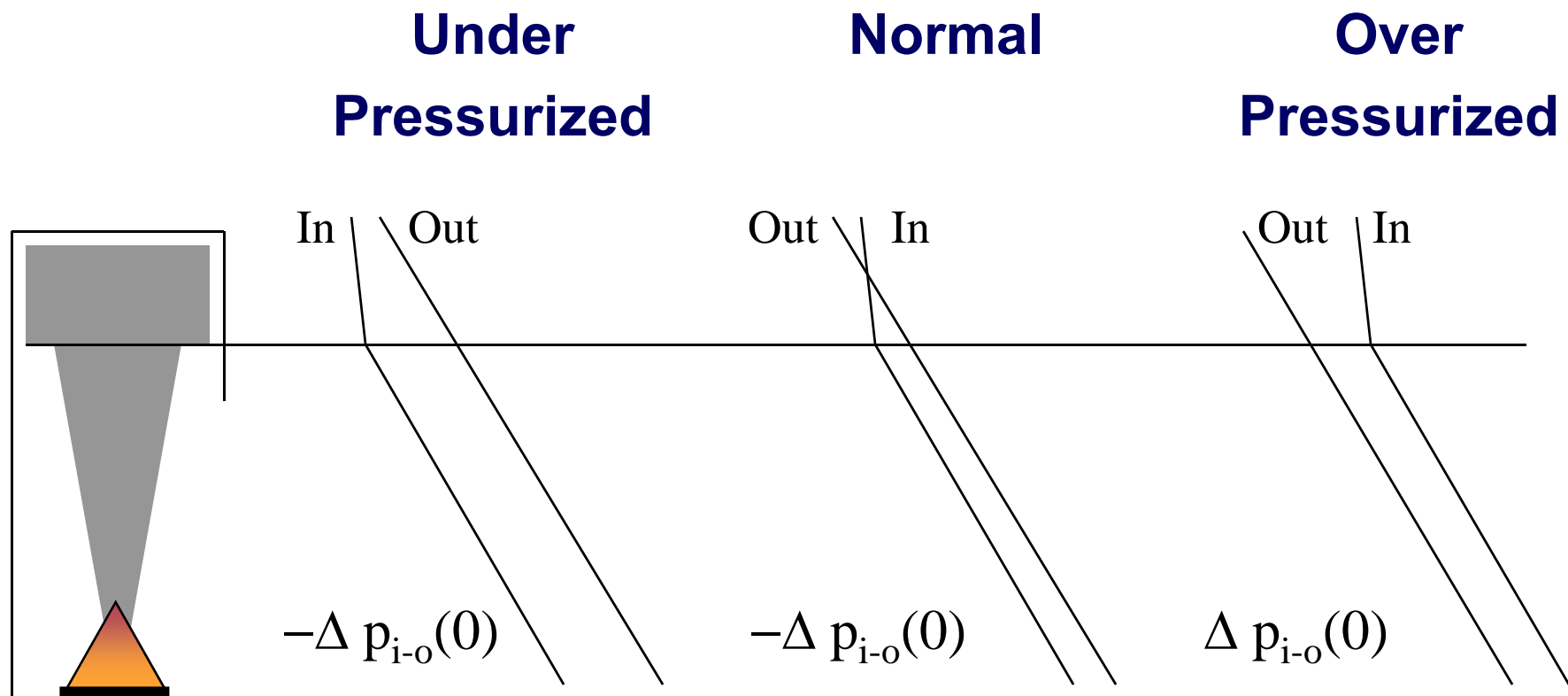
$$P_o(h) = P_o(0) - \rho_o g h$$

← Outside Profile

$$\Delta P_{i-o}(h) = \Delta P_i(0) + \rho_o g (h - Z_u) + \rho_u g (Z_u - h)$$

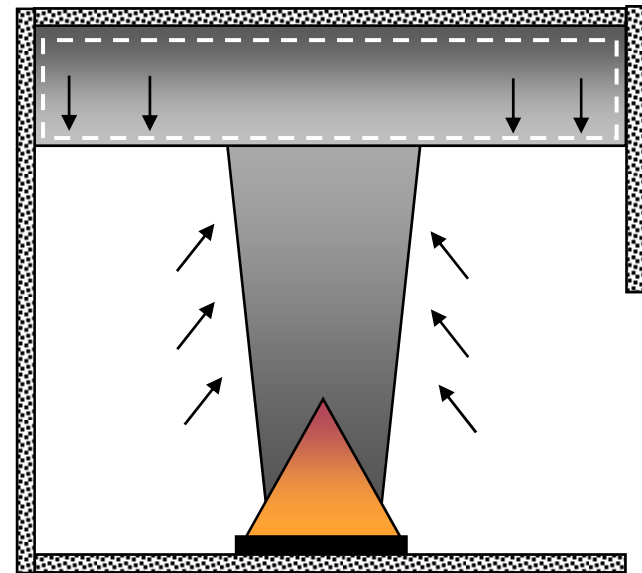
← ΔP Profile

Pressure Profiles & Vent Flows



Hot Gas or Smoke Layer

- Accumulation of hot gases in the upper part of the room
- Mass: entrainment (~90%) and combustion products (~10%)
- Volume: entrainment, combustion products, and expansion due to energy added
- Temperature rise: expansion generates a larger volume than corresponding mass resulting in lower gas densities.
- Conservation of mass and energy



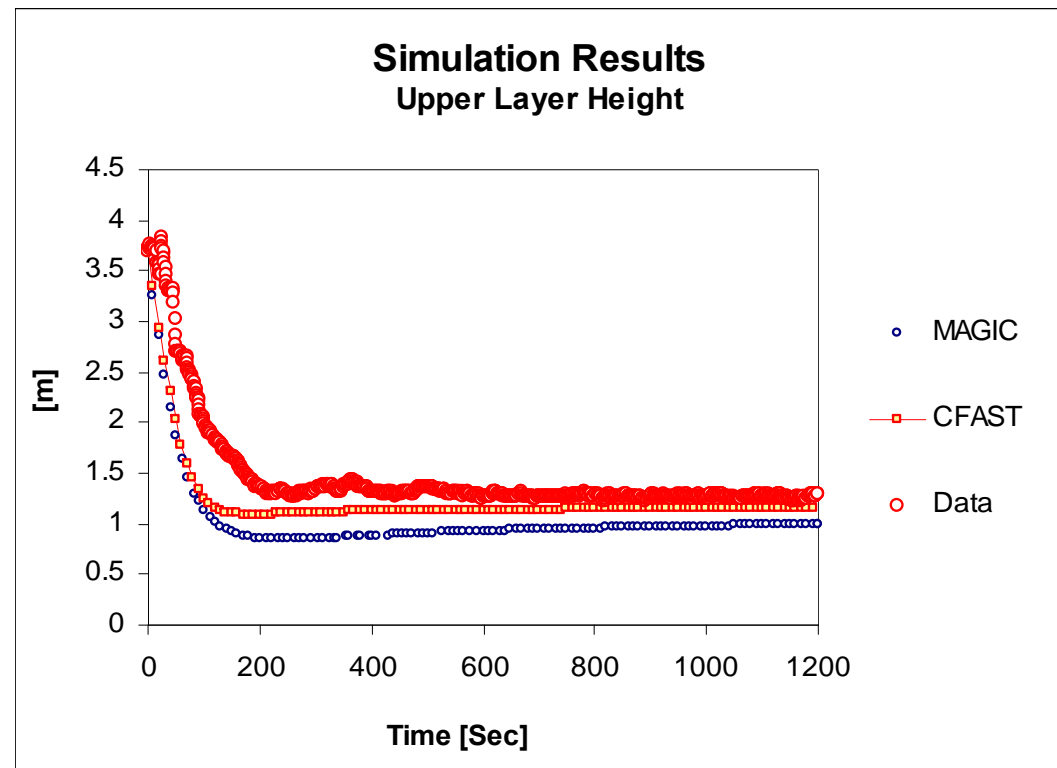
Hot Gas or Smoke Layer

Room size:

– 22 x 7 x 3.7 m

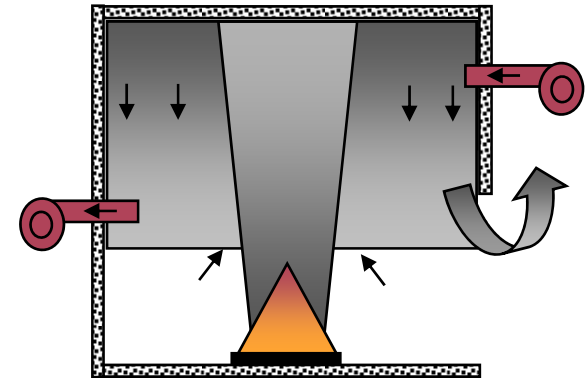
Fire: ~1 MW

Door: 2 x 2 m



Hot Gas or Smoke Layer

- Conservation of Mass
 - Rate of change of mass in the control volume
 - Accumulation
 - Mass flow through the control surface
 - Plume flow
 - Supply and exhaust systems
 - Flow through doors and windows

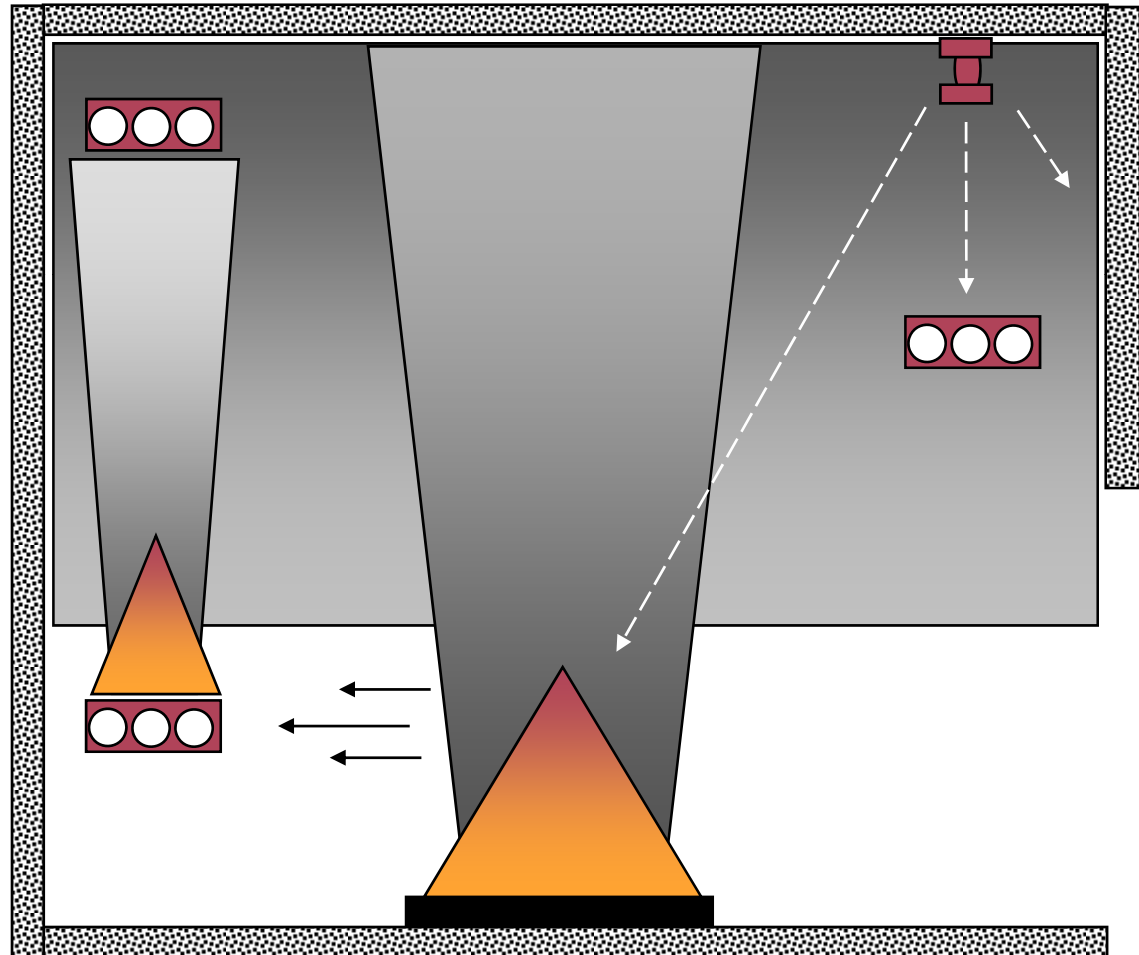


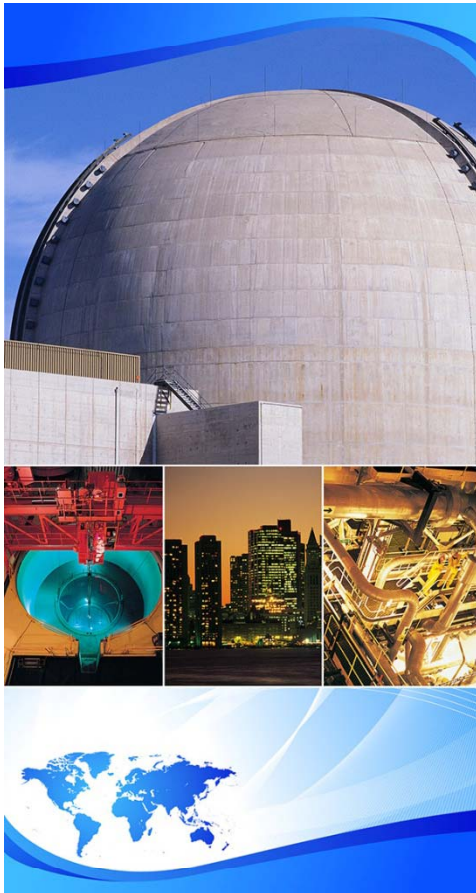
Heat Transfer

- To walls
 - Convection and radiation
 - Conduction losses
- To targets
 - Convection and radiation
- Heat losses
 - Conduction through walls
 - Convection and radiation through openings and vents

Heat Transfer

- Conduction
- Convection
- Radiation





EPRI/NRC-RES FIRE PRA METHODOLOGY

Detection and Suppression

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Objectives

- Fire PRA credits fire detection and suppression features when appropriate
- The objective of this presentation is to briefly describe typical detection and suppression features that are credited

Fire Detection

- Typical fire detection features credited in the Fire PRA
 - Prompt detection
 - Smoke detection
 - Heat detection
 - Incipient detection
 - Delayed detection

Prompt Detection

- Continuous fire watch
- Hotwork or other activity-specific fire watch
- Continuously manned rooms, e.g., the control room

Smoke Detection

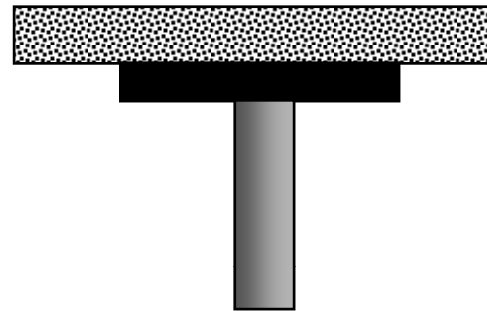
- Spot type smoke detectors
 - Ionization detection
 - Optical density detection
- Generally, smoke particles move into the chamber for the device to actuate
- Needs power (generally line and backup battery)



Heat Detection

- Heat detectors

- Detection devices
- Sprinkler heads
- Linear heat detectors

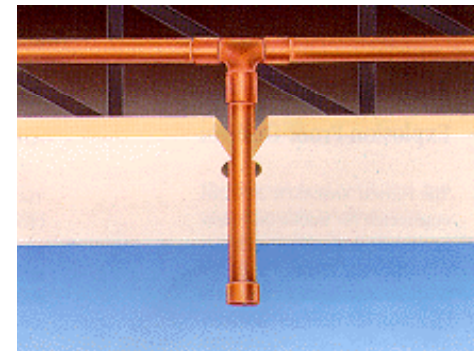


- Generally characterized by a response time index and an activation temperature

- Response Time Index (RTI): a parameter describing how fast the device responds to the surrounding gas temperature
- Activation Temperature: the temperature at which the detection device actuates

Incipient Detection

- Examples include air sampling systems
- Typically used where conventional fire detectors can't provide sufficiently rapid response.
- The objective is for plant personnel to prevent potential fire impacts



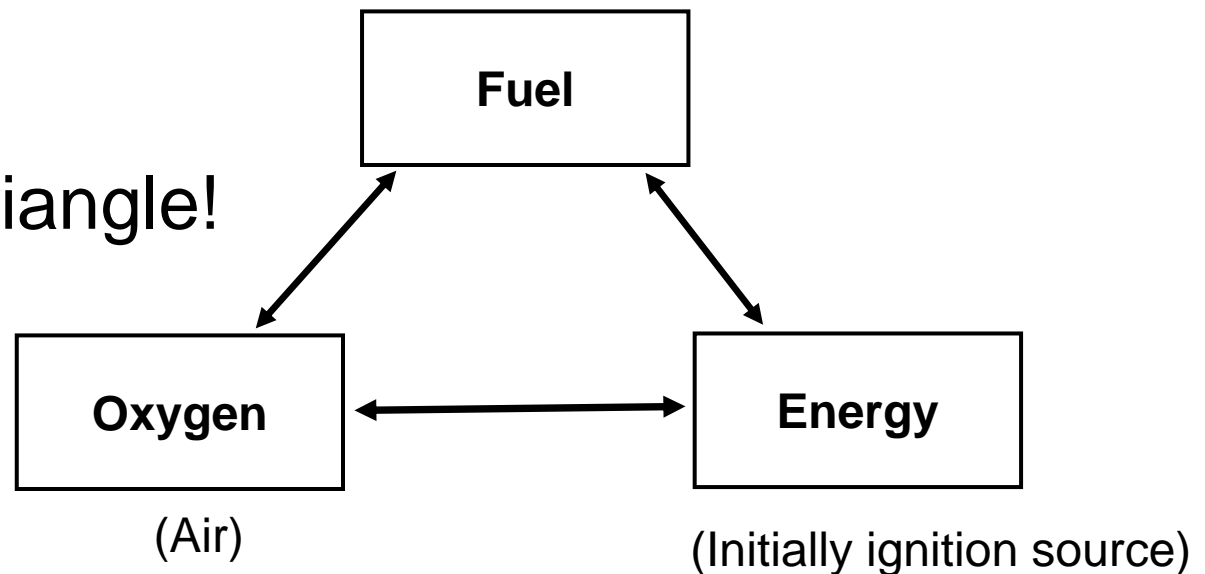
Delayed Detection

- Roving fire watch
- Plant personnel
- Control room indication
 - The control room receives a process alarm and dispatches an operator to inspect the situation.

Fire Suppression

- Fire can be suppressed by:
 - Cooling down the burning fuel and adjacent items – example: water spray
 - Removing oxygen – example: CO₂
 - Separating burning surface from impinging heat flux from the flame – example: Foam

Break the fire triangle!



Fire Suppression

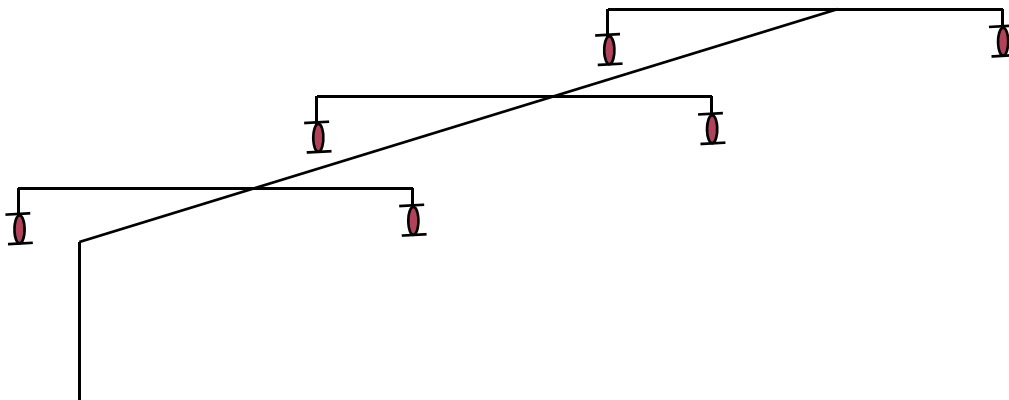
- Prompt suppression
- Automatic sprinklers
- Dry-Pipe/Pre-action sprinklers
- Deluge systems
- CO2: Automatic or Manual
- Halon: Automatic or Manual
- Fire brigade

Prompt Suppression

- Hotwork fire watch
- Some of the operators are generally trained in the use of portable extinguishers

Automatic Sprinklers

- Fusible links at the nozzles
- Water readily available
- Full room coverage, localized, in trays, etc.



Fire PRA Workshop, 2011
Fire Fundamentals – Detection and Suppression

Slide 12



A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Dry-Pipe/Pre-Action Sprinklers

- Sprinkler pipes are maintained dry (upstream shutoff valve keeps the water away from sprinkler heads)
- A smoke detection system opens the shutoff valve that fills the pipes (turns the system into a wet system)
- Sprinkler heads need to open from exposure to heat from the fire.

Deluge Sprinklers

- Pipes are maintained dry
- All sprinkler heads are open
- A smoke or heat detection system signals the main shutoff valve open
- All sprinklers discharge at the same time upon opening of the shutoff valve
- Generally used for protecting large liquid filled transformers and high fire hazard areas

Carbon Dioxide

- CO₂ gas is used to displace oxygen from the fire.
- Automatic CO₂- Suppression agent is generally released after heat or flame detection, and a life safety alarm and delay time
- Manual CO₂- Requires an operator or fire brigade personnel to activate the system after smoke detection
- Must maintain proper suppression agent concentration for a soak time
- Life safety considerations – will displace oxygen for humans as well as the fire

Halon

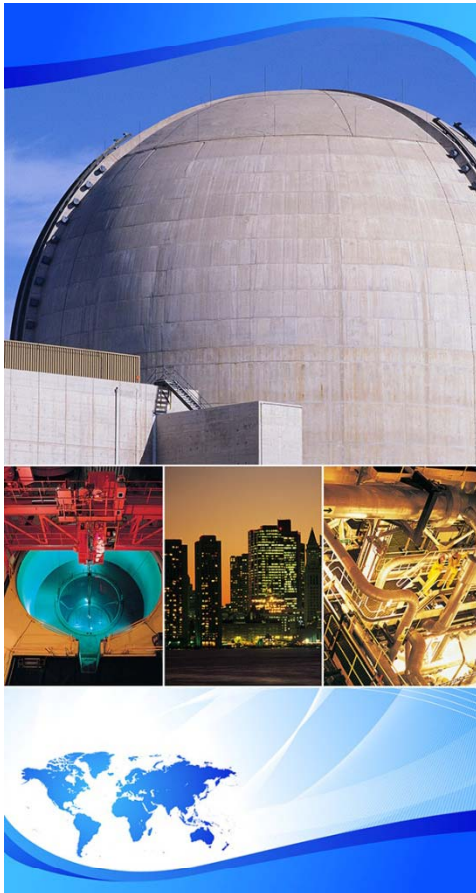
- Halon interferes with the chemical oxidation process
- Automatic Halon- Suppression agent is generally released after smoke or heat detection and a life safety alarm and delay time
- Manual Halon- Requires an operator or fire brigade personnel to activate the system after smoke detection
- Must maintain proper suppression agent concentration for a soak time
- No life safety issues – does not displace oxygen, safe for use in occupied space
- Not being manufactured any more and existing systems are being phased out because of environmental (ozone) considerations

Fire Brigade

- Credited in most fire scenarios
- Typically characterized by the response time and time to start suppression activities in each room
- Typically use portable extinguishers (gaseous) first, followed by water (fire hose) if needed
- Typically plants maintain a professional brigade or operators/plant personnel are trained in fire fighting techniques

Passive Fire Protection

- Passive fire protection refers to fixed features put in place for reducing or preventing fire propagation.
- Such features include coatings, cable tray barriers, fire stops, self-closing dampers, penetration seals, self-closing doors, and fire-rated walls.



EPRI/NRC-RES FIRE PRA METHODOLOGY

Analysis Tools

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Analysis Tools: Outline

- Fire Modeling in a Fire PRA
- How fire develops in a scenario
- What damage is generated
- When damage is generated
- Timing of detection and suppression activities

Five Steps of Fire Modeling

1. Define modeling objectives
2. Select and describe fire scenarios
3. Select the appropriate model(s)
4. Run/apply the model
5. Interpret modeling results

Fire Modeling

- **Fire modeling:** an approach for predicting various aspects of fire generated conditions
- **Compartment fire modeling:** modeling fires inside a compartment
- Requires an idealization and/or simplification of the physical processes involved in fire events
- Any departure of the fire system from this idealization can seriously affect the accuracy and validity of the approach

Capabilities

- Areas of application

- Thermal effects of plumes, ceiling jets and flame radiation
- Room heat up, and hot gas layer
- Elevated fires and oxygen depletion
- Multiple fires
- Multi-compartments: corridors and multi-levels
- Smoke generation and migration
- Partial barriers and shields
- Fire detection
- Special models or areas for future research
- Cable fires
- Fire growth inside the main control board
- Fire propagation between control panels
- High energy fires
- Fire suppression
- Hydrogen or liquid spray fires

Fire Models

- **Hand calculations:** Mathematical expressions that can be solved by hand with a relatively small computational effort
 - Quasi steady conditions
 - Usually semi-empirical correlations developed with data from experiments
- **Zone models:** Algorithms that solve conservation equations for energy and mass in usually two control volumes with uniform properties
- **Field models:** Algorithms that solve simplified versions of the Navier-Stokes equations. The room is divided into large number of cells and conservation equations are solved in each of them.
- **Special models:** There are fire scenarios critical to NPP applications that are beyond capability of existing computational fire models
 - Fire experiments,
 - Operating experience, actual fire events
 - Engineering judgment

Hand Calculations

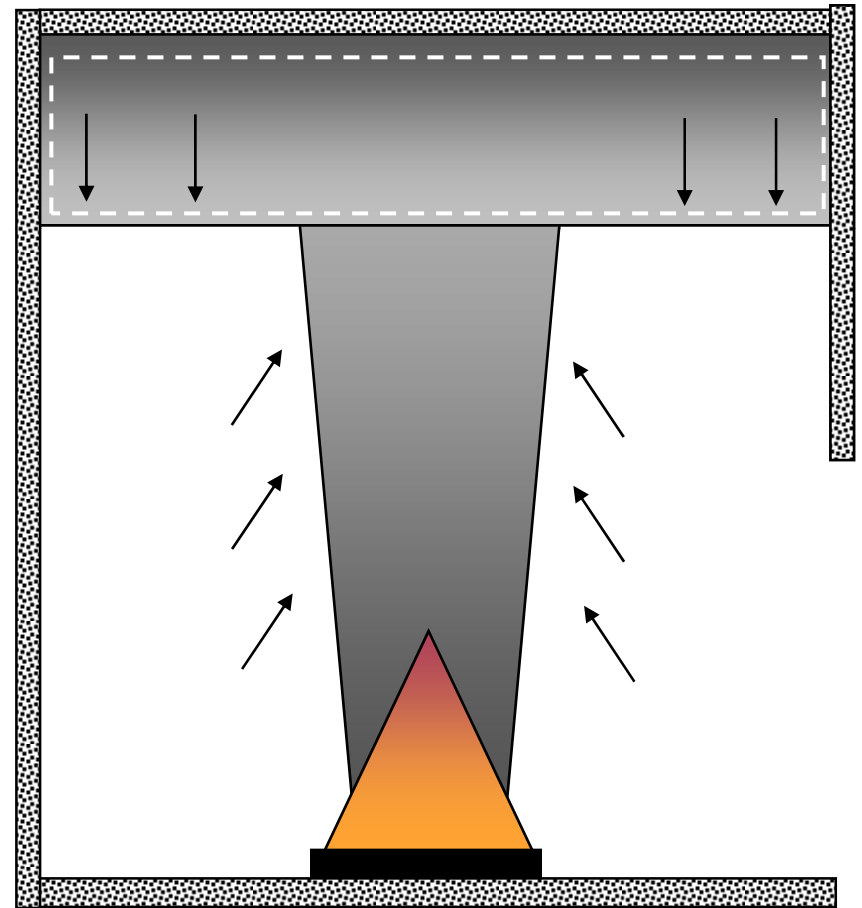
- Heat release rate, flame height and flame radiation
- Fire plume velocity, temperature heat flux, and entrainment
- Ceiling jet velocity, temperature, and heat flux
- Overall room temperature
- Target temperature, and time to target damage

Example of Hand Calcs: FDT's

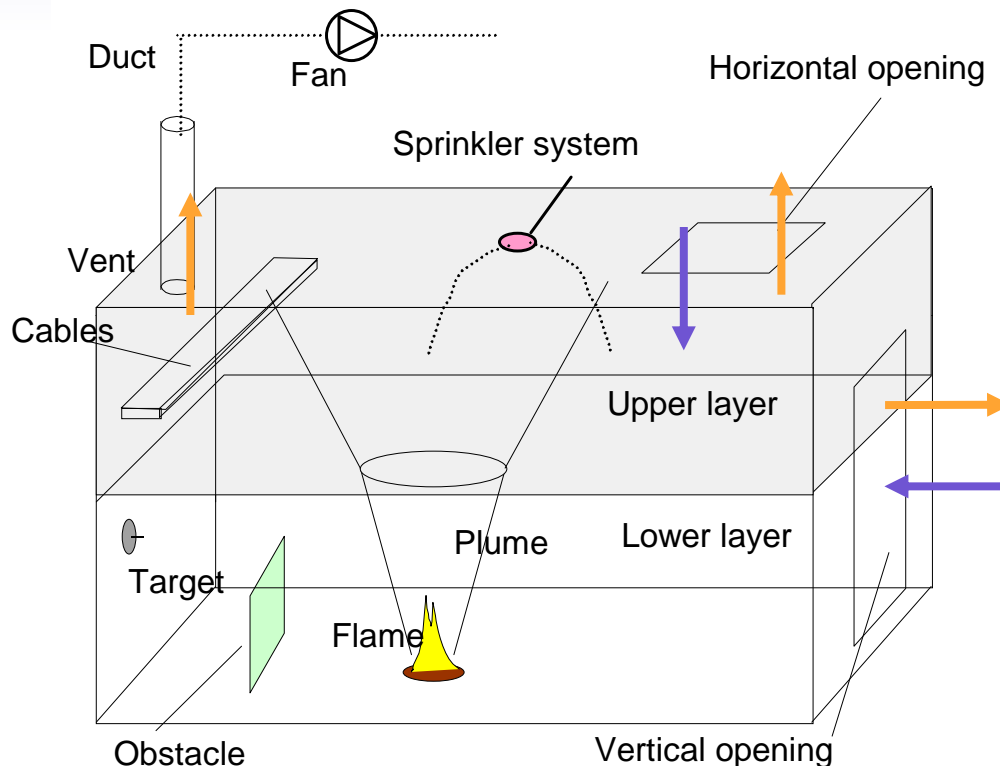
- **FDTs** are a series of Microsoft Excel® spreadsheets issued with **NUREG-1805, “Quantitative Fire Hazard Analysis Methods for the U.S. Nuclear Regulatory Commission Fire Protection Inspection Program.”**
- The primary goal of FDTs was to be a training tool to teach NRC Fire Protection Inspectors.
- The secondary goal of FDTs was to be used in plant inspections and support other programs that required Fire Dynamics knowledge such as, SDP and NFPA 805.

Zone Models

- Usually two zones
 - Upper hot gas layer
 - Lower layer with clear and colder air
- Mass and energy balance in the zones
 - Entrainment
 - Natural flows in and out
 - Forced flows in and out
- Fire is treated as a point of heat release



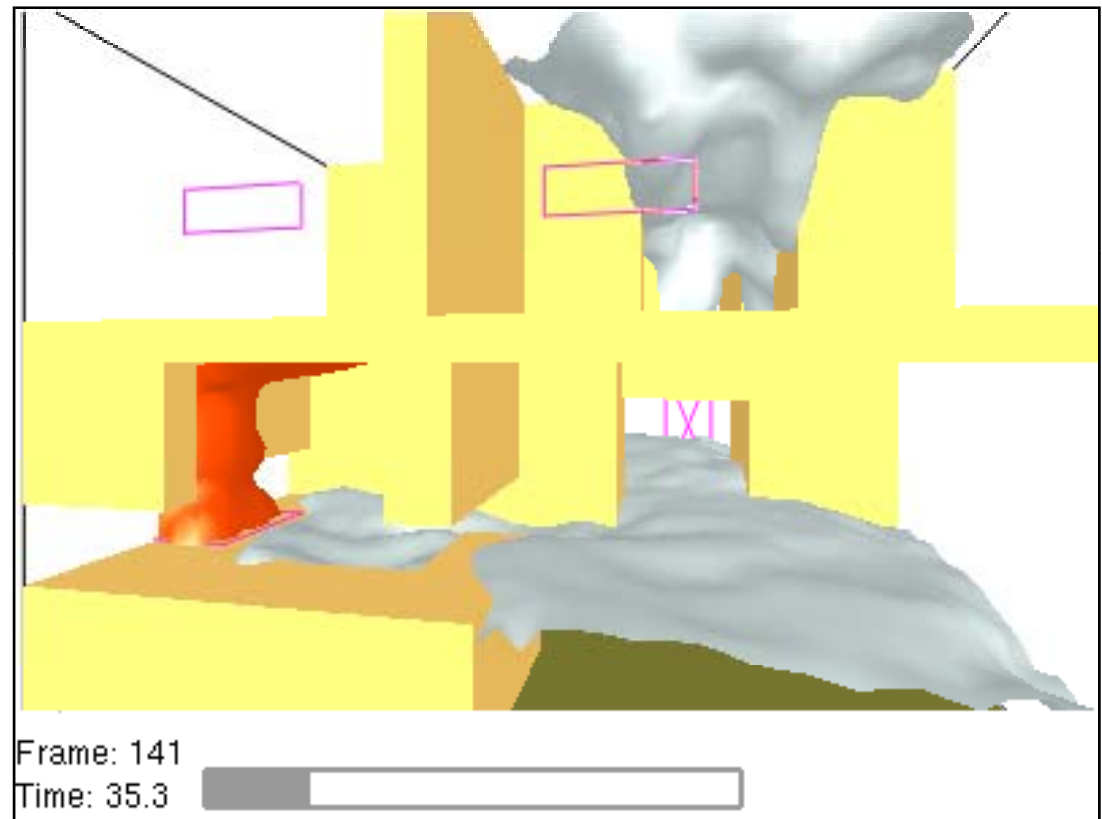
Example of a Zone Model: MAGIC



- Gaseous phase combustion, governed by pyrolysis rate and oxygen availability
- Heat transfer between flame, gases and smoke, walls and surrounding air, thermal conduction in multi-layer walls, obstacles to radiation
- Mass flow transfer: Fire-plumes, ceiling-jet, openings and vents
- Thermal behavior of targets and cables
- Secondary source ignition, unburned gas management
- Multi-compartment, multi-fire, etc.

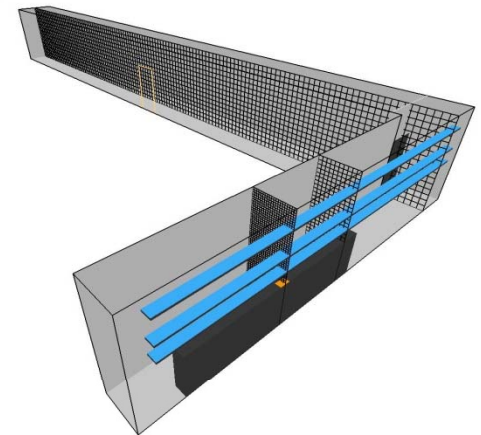
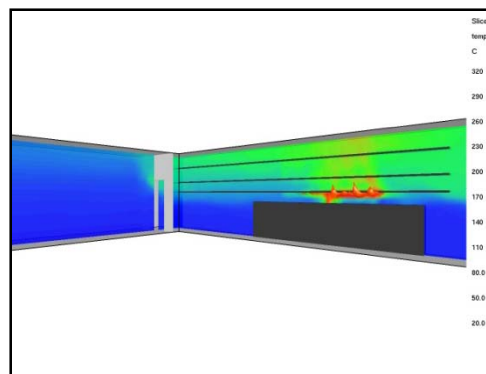
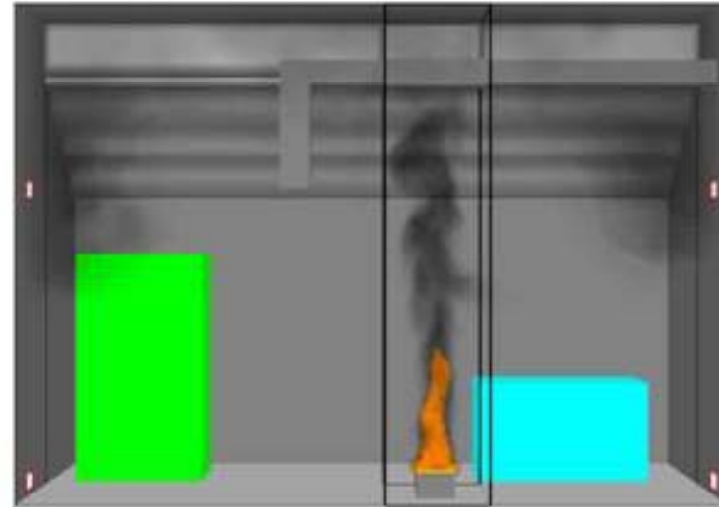
Field Models

- Solve a simplified form of the Navier Stokes equations for low velocity flows
- Calculation time in the order of hours, days or weeks
- May help in modeling complex geometries



Example of Field Model: FDS

- Fire Dynamics Simulator
- Developed and maintained by NIST



Special Models

- Cable fires
- High energy arcing faults and fires
- Fire growth inside the main control board
- Fire propagation between control panels
- *The method described here is documented in the, EPRI 1011989 & NUREG/CR-6850, “EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities.”*

Which Model to Choose

- Hand calculations available
 - Combustion - Heat release rates, flame heights
 - Fire generated conditions
 - Plume temperatures and velocities
 - Ceiling jet temperatures and velocities
 - Flow through vents
 - Enclosure temperature
 - Time and temperature to flashover
 - Target temperature and time to target damage
 - Heat transfer: irradiation from flames, plume and ceiling jet convective flux
- Analysts may need to go back and find additional parameters required

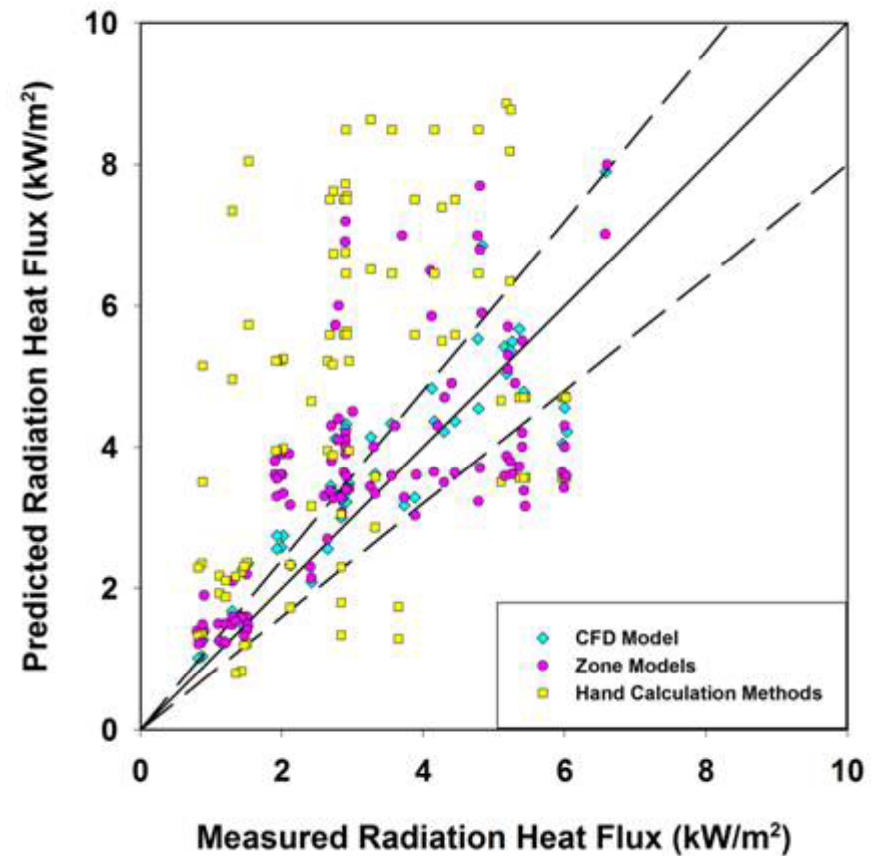
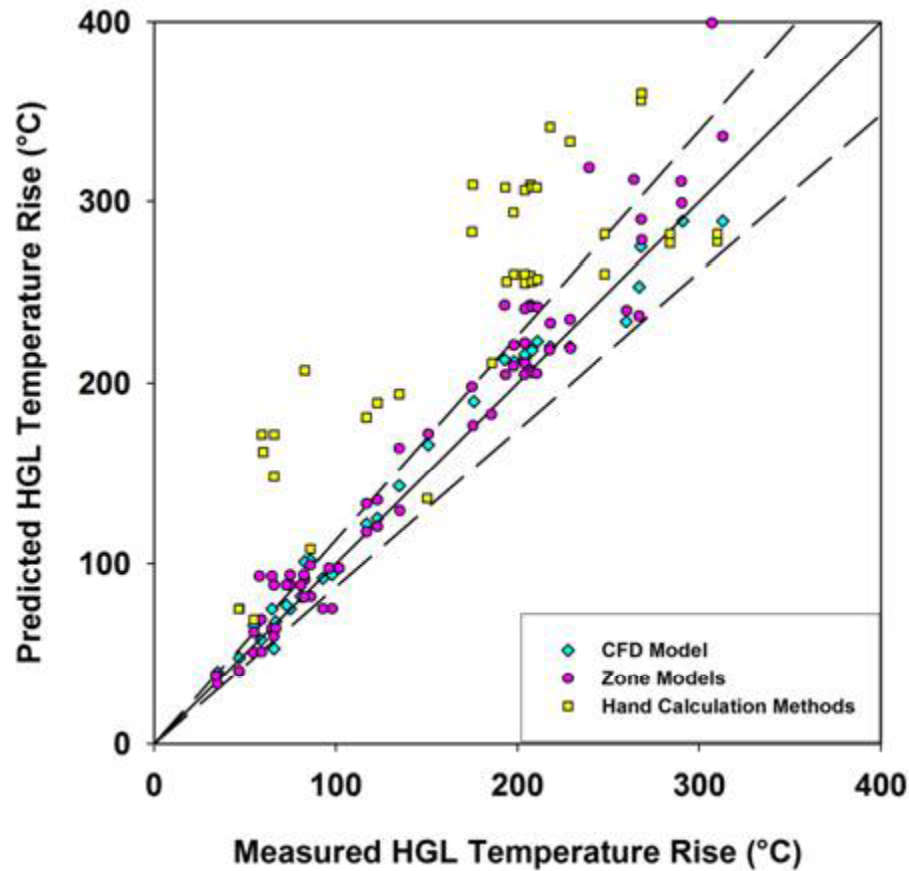
Verification and Validation

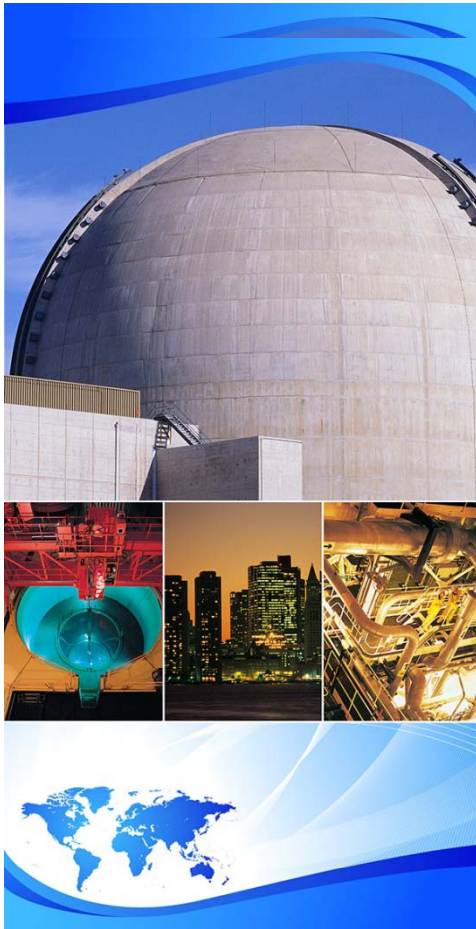
- **Verification:** the process of determining that the implementation of a calculation method accurately represents the developer's conceptual description of the calculation method and the solution to the calculation method. *Is the Math right?*
- **Validation:** the process of determining the degree to which a calculation method is an accurate representation of the real world from the perspective of the intended uses of the calculation method. *Is the Physics right?*
- See NUREG-1824

Verification and Validation

Parameter				Fire Model		
		FDT ^s	FIVE-Rev1	CFAST	MAGIC	FDS
Hot gas layer temperature ("upper layer temperature")	Room of Origin	YELLOW+	YELLOW+	GREEN	GREEN	GREEN
	Adjacent Room	N/A	N/A	YELLOW	YELLOW+	GREEN
Hot gas layer height ("layer interface height")		N/A	N/A	GREEN	GREEN	GREEN
Ceiling jet temperature ("target/gas temperature")		N/A	YELLOW+	YELLOW+	GREEN	GREEN
Plume temperature		YELLOW-	YELLOW+	N/A	GREEN	YELLOW
Flame height		GREEN	GREEN	GREEN	GREEN	YELLOW
Oxygen concentration		N/A	N/A	GREEN	YELLOW	GREEN
Smoke concentration		N/A	N/A	YELLOW	YELLOW	YELLOW
Room pressure		N/A	N/A	GREEN	GREEN	GREEN
Target temperature		N/A	N/A	YELLOW	YELLOW	YELLOW
Radiant heat flux		YELLOW	YELLOW	YELLOW	YELLOW	YELLOW
Total heat flux		N/A	N/A	YELLOW	YELLOW	YELLOW
Wall temperature		N/A	N/A	YELLOW	YELLOW	YELLOW
Total heat flux to walls		N/A	N/A	YELLOW	YELLOW	YELLOW

Verification and Validation





EPRI/NRC-RES FIRE PRA METHODOLOGY

Fire Scenarios

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

Fire Scenario

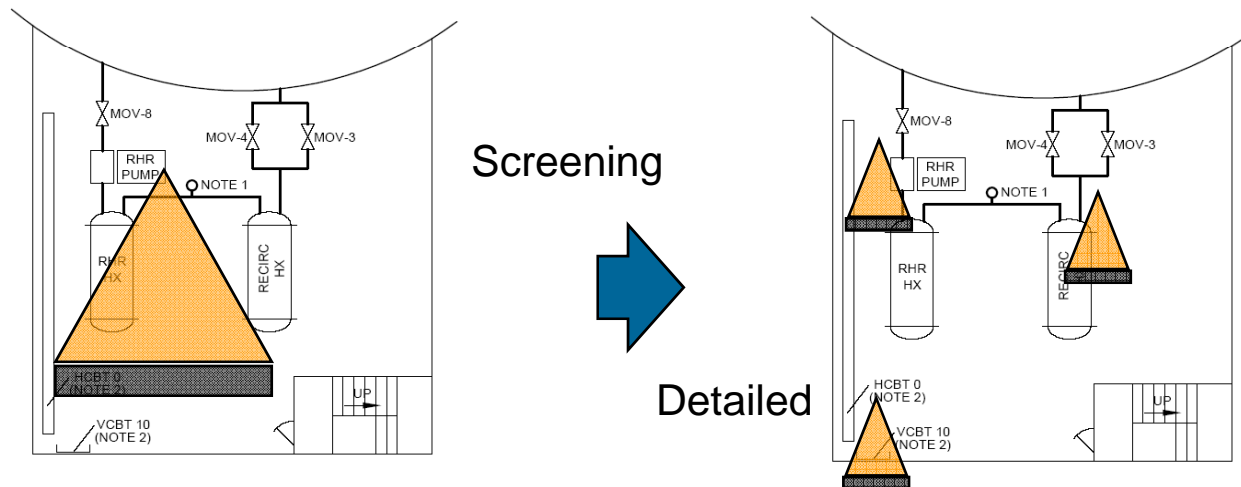
- A set of elements representing a fire event:
 - The ignition source, e.g., electrical cabinets, pumps
 - Intervening combustibles, e.g., cables
 - Targets, e.g., power, instrumentation or control cables
 - Fire protection features, e.g., automatic sprinklers
 - The compartment where the fire is located
 - A time line

Fire Scenario Time Line

1. Starts with a specific ignition source
2. Fire growth involving the affected fuel,
3. Heat transfer from the fire to other items within the zone of influence,
4. Damage of the affected items (e.g., cables and equipment items),
5. Propagation of the fire to other materials,
6. Detection of the fire (Note: this step could occur right after #2, or even #1 if there is very early warning smoke detection present)
7. Automatic initiation of suppression systems of the area,
8. Fire brigade response,
9. Successful fire extinguishment.

Fire Scenario - *Level of Detail*

- In practice, varying levels of detail are used to define the fire scenarios in a typical Fire PRA.
 - Level of detail may depend on initial stages of screening, anticipated risk significance of the scenario
- In principle, at any level of detail, a fire scenario represents a collection of more detailed scenarios.



Fire Scenario *Initial Screening Stage*

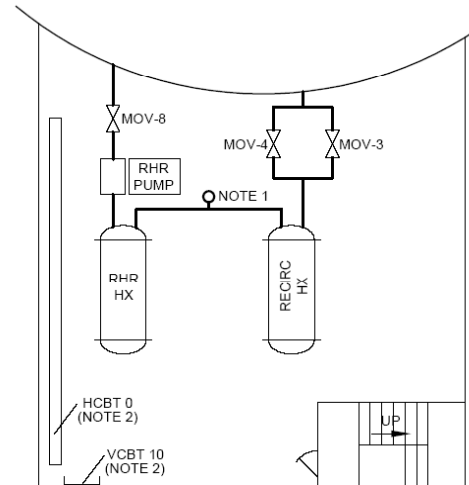
- In the initial stages of screening, fire scenarios are defined in terms of compartments and loss of all items within each compartment.
 - Assumes all items fail in the worst failure mode
 - Detection and suppression occur after the worst damage takes place
 - Fire does not propagate to adjacent compartments
- In multi-compartment fire propagation analysis, a similar definition is used in the initial screening steps for combinations of adjacent compartments.

Detailed Scenario Identification Process

- In the detailed analysis tasks, the analyst takes those fire scenarios that did not screen out in the initial stage and breaks them down into scenarios using greater level of detail.
 - Level of detail depends on the risk significance of the unscreened scenario
 - Details may be introduced in terms of . . .
 - Sub-groups of cables and equipment within the compartment
 - Specific ignition sources and fuels
 - Fire detection and suppression possibilities

Example – Screening Level

- At the screening level, a fire in this compartment fails all equipment and cables shown in this diagram.
- The fire is assumed to be confined to this room



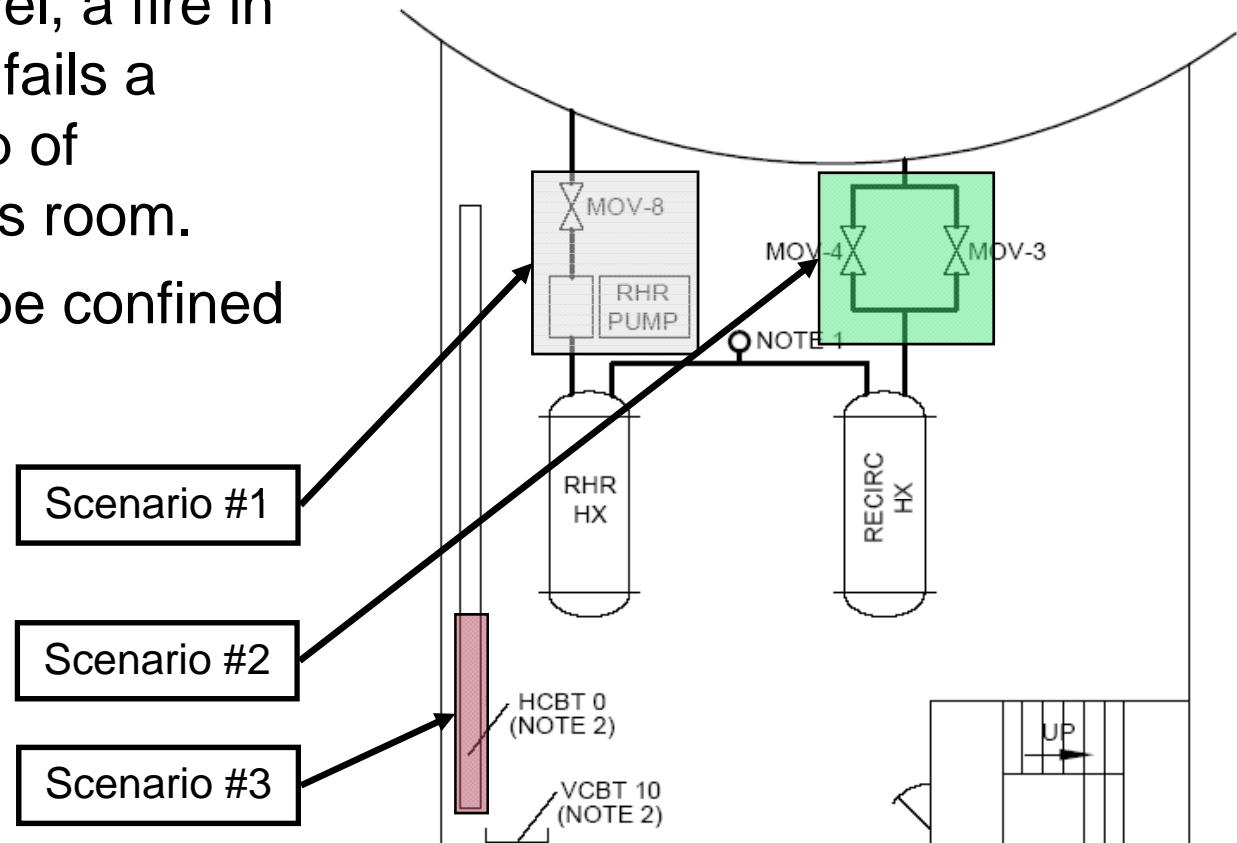
NOTES:

1. VERTICAL PIPE PENETRATION TO UPPER ELEVATION.
2. PENETRATION TO UPPER FLOOR IS SEALED.

HCBT: HORIZONTAL CABLE TRAY
VCBT: VERTICAL CABLE TRAY

Example – Detailed Analysis

- At the detailed level, a fire in this compartment fails a specific sub-group of components in this room.
- The fire may still be confined to this room



Select and Describe Fire Scenarios

- Selection of fire scenarios:
 - How many fire scenarios are enough to demonstrate the objective?
 - Which scenarios are the appropriate ones?
- Selecting scenarios is dependent on the objectives of the fire risk quantification
 - Fire conditions that are actually modeled
 - Represent a complete set of fire conditions relevant to the objectives
- Selection of scenarios is dependent on the hazard characteristics of the area
 - Combustibles, layouts, fire protection
- The fire scenario should challenge the conditions being considered
 - Can the fire cause damage? vs. Which fire can cause damage?

Select and Describe Fire Scenarios

1. Scenarios should have an ignition source and at least one target or other measurable objectives
2. Consider the range of possible intervening combustibles
3. Scenarios should capture targets as well as fire's ability to ignite or damage them
4. Include in the scenario any fire protection system (active or passive) that may influence the outcome of the event

Select and Describe Fire Scenarios

5. Sometimes, multiple ignition sources or targets can be combined into one scenario
6. Sketch the scenario on a compartment layout drawing and try to qualitatively describe the conditions that a fire might generate. After the analysis, compare this qualitative prediction with the modeling results.
7. Do not neglect the importance of details such as ceiling obstructions, soffits, open or close doors, etc.

Scenario Quantification

- Ignition frequency: fire frequency for the postulated ignition source
- Apportioning factor: probability that the ignition occurs in a specific ignition source or plant location
- Severity factor: probability that the fire is severe enough to generate the postulated damage
- Non suppression probability: probability of failing to suppress the fire
- Circuit failure probability: probability that the affected circuits will generate the postulated equipment impact
- Conditional core damage probability

$$CDF = \lambda \cdot W \cdot SF \cdot P_{ns} \cdot P_{cf} \cdot CCDP$$

Scenario Quantification

- A fire in a specific plant location
 - That is severe enough
 - That is unsuppressed
 - That generates the postulated circuit failure mode
 - That prevents safe shutdown

$$\lambda_{is} = \lambda_g \cdot W \cdot 1 \cdot 1 \cdot 1$$

$$\lambda_{is} = \lambda_g \cdot W_{is} \cdot SF \cdot 1 \cdot 1$$

$$\lambda_{is} = \lambda_g \cdot W_{is} \cdot SF \cdot P_{ns} \cdot 1$$

$$\lambda_{is} = \lambda_g \cdot W_{is} \cdot SF \cdot P_{ns} \cdot P_{cf}$$

$$\lambda_{CDF} = \lambda_{is} \cdot cc dp$$

Table E-1
List of Heat Release Rate Distributions

Case	Ignition Source	HRR kW (Btu/s)		Gamma Distribution		Reference
		75th	98th	α	β	
1	Vertical cabinets with qualified cable, fire limited to one cable bundle	69 (65)	211 (200)	0.84 (0.83)	59.3 (56.6)	Table G-1
2	Vertical cabinets with qualified cable, fire in more than one cable bundle	211 (200)	702 (665)	0.7 (0.7)	216 (204)	Table G-1
3	Vertical cabinets with unqualified cable, fire limited to one cable bundle	90 (85)	211 (200)	1.6 (1.6)	41.5 (39.5)	Table G-1
4	Vertical cabinets with unqualified cable, fire in more than one cable bundle closed doors	232 (220)	464 (440)	2.6 (2.6)	67.8 (64.3)	Table G-1
5	Vertical cabinets with unqualified cable, fire in more than one cable bundle open doors	232 (220)	1002 (950)	0.46 (0.45)	386 (366)	Table G-1
6	Pumps (electrical fires)	69 (65)	211 (200)	0.84 (0.83)	59.3 (56.6)	Table G-1
7	Motors	32 (30)	69 (65)	2.0 (2.0)	11.7 (11.1)	Table G-1
8	Transient Combustibles	142 (135)	317 (300)	1.8 (1.9)	57.4 (53.7)	Section G-4

Table E-2
Discretized Distribution for Case 1 Heat Release Rate (Vertical Cabinets with Qualified Cable, Fire Limited to One Cable Bundle)

Bin	Heat Release Rate – kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	26 (25)	11 (10.5)	0.446
2	26 (25)	53 (50)	38 (36)	0.219
3	53 (50)	79 (75)	64 (61)	0.129
4	79 (75)	106 (100)	92 (87)	0.078
5	106 (100)	132 (125)	118 (112)	0.048
6	132 (125)	158 (150)	145 (137)	0.030
7	158 (150)	185 (175)	171 (162)	0.019
8	185 (175)	211 (200)	197 (187)	0.012
9	211 (200)	237 (225)	224 (212)	0.007
10	237 (225)	264 (250)	250 (237)	0.005
11	264 (250)	290 (275)	276 (262)	0.003
12	290 (275)	317 (300)	303 (287)	0.002
13	317 (300)	343 (325)	329 (312)	0.001
14	343 (325)	369 (350)	356 (337)	0.001
15	369 (350)	Infinity	427 (405)	0.001

Table E-3
Discretized Distribution for Case 2 Heat Release Rate (Vertical Cabinets with
Qualified Cable, Fire in more than One Cable Bundle)

Bin	Heat Release Rate – kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	90 (85)	34 (32.7)	0.506
2	90 (85)	179 (170)	130 (123)	0.202
3	179 (170)	269 (255)	221 (209)	0.113
4	269 (255)	359 (340)	310 (294)	0.067
5	359 (340)	448 (425)	400 (379)	0.041
6	448 (425)	538 (510)	490 (464)	0.026
7	538 (510)	628 (595)	579 (549)	0.016
8	628 (595)	717 (680)	669 (634)	0.010
9	717 (680)	807 (765)	759 (719)	0.006
10	807 (765)	897 (850)	848 (804)	0.004
11	897 (850)	986 (935)	938 (889)	0.003
12	986 (935)	1076 (1020)	1028 (974)	0.002
13	1076 (1020)	1166 (1105)	1118 (1060)	0.001
14	1166 (1105)	1255 (1190)	1208 (1145)	0.001
15	1255 (1190)	Infinity	1462 (1386)	0.001

Table E-4
Discretized Distribution for Case 3 Heat Release Rate (Vertical Cabinets with
Unqualified Cable, Fire Limited to One Cable Bundle)

Bin	Heat Release Rate - kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	26 (25)	15 (14.2)	0.227
2	26 (25)	53 (50)	39 (37)	0.261
3	53 (50)	79 (75)	65 (62)	0.192
4	79 (75)	106 (100)	92 (87)	0.126
5	106 (100)	132 (125)	118 (112)	0.079
6	132 (125)	158 (150)	143 (136)	0.048
7	158 (150)	185 (175)	170 (161)	0.028
8	185 (175)	211 (200)	196 (186)	0.016
9	211 (200)	237 (225)	223 (211)	0.010
10	237 (225)	264 (250)	249 (236)	0.005
11	264 (250)	290 (275)	275 (261)	0.003
12	290 (275)	317 (300)	302 (286)	0.002
13	317 (300)	343 (325)	328 (311)	0.001
14	343 (325)	369 (350)	354 (336)	0.001
15	369 (350)	Infinity	414 (392)	0.001

Table E-5**Discretized Distribution for Case 4 Heat Release Rate (Vertical Cabinets with Unqualified Cable, Fire in more than One Cable Bundle Closed Doors)**

Bin	Heat Release Rate - kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	53 (50)	36 (34)	0.082
2	53 (50)	106 (100)	80 (76)	0.213
3	106 (100)	158 (150)	131 (124)	0.224
4	158 (150)	211 (200)	184 (174)	0.177
5	211 (200)	264 (250)	235 (223)	0.122
6	264 (250)	317 (300)	288 (273)	0.077
7	317 (300)	369 (350)	341 (323)	0.046
8	369 (350)	422 (400)	394 (373)	0.027
9	422 (400)	475 (450)	446 (423)	0.015
10	475 (450)	528 (500)	499 (473)	0.008
11	528 (500)	580 (550)	552 (523)	0.004
12	580 (550)	633 (600)	603 (572)	0.002
13	633 (600)	686 (650)	656 (622)	0.001
14	686 (650)	739 (700)	709 (672)	0.001
15	739 (700)	Infinity	816 (773)	0.001

Table E-6
Discretized Distribution for Case 5 Heat Release Rate (Vertical Cabinets with
Unqualified Cable, Fire in more than One Cable Bundle Open Doors)

Bin	Heat Release Rate - kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	137 (130)	42 (39.5)	0.638
2	137 (130)	274 (260)	197 (187)	0.155
3	274 (260)	411 (390)	337 (319)	0.081
4	411 (390)	549 (520)	475 (450)	0.047
5	549 (520)	686 (650)	612 (580)	0.029
6	686 (650)	823 (780)	749 (710)	0.018
7	823 (780)	960 (910)	886 (840)	0.011
8	960 (910)	1097 (1040)	1024 (971)	0.007
9	1097 (1040)	1234 (1170)	1162 (1101)	0.005
10	1234 (1170)	1372 (1300)	1299 (1231)	0.003
11	1372 (1300)	1509 (1430)	1436 (1361)	0.002
12	1509 (1430)	1646 (1560)	1573 (1491)	0.001
13	1646 (1560)	1783 (1690)	1710 (1621)	0.001
14	1783 (1690)	1920 (1820)	1847 (1751)	0.001
15	1920 (1820)	Infinity	2276 (2157)	0.001

Table E-7
Discretized Distribution for Case 6 Heat Release Rate (Pumps – Electrical Fires)

Bin	Heat Release Rate – kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	26 (25)	11 (10.5)	0.446
2	26 (25)	53 (50)	38 (36)	0.219
3	53 (50)	79 (75)	64 (61)	0.129
4	79 (75)	106 (100)	92 (87)	0.078
5	106 (100)	132 (125)	118 (112)	0.048
6	132 (125)	158 (150)	145 (137)	0.030
7	158 (150)	185 (175)	171 (162)	0.019
8	185 (175)	211 (200)	197 (187)	0.012
9	211 (200)	237 (225)	224 (212)	0.007
10	237 (225)	264 (250)	250 (237)	0.005
11	264 (250)	290 (275)	276 (262)	0.003
12	290 (275)	317 (300)	303 (287)	0.002
13	317 (300)	343 (325)	329 (312)	0.001
14	343 (325)	369 (350)	356 (337)	0.001
15	369 (350)	Infinity	427 (405)	0.001

Table E-8
Discretized Distribution for Case 7 Heat Release Rate (Motors)

Bin	Heat Release Rate – kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	7 (7)	5 (4.4)	0.132
2	7 (7)	15 (14)	12 (11)	0.227
3	15 (14)	22 (21)	18 (17)	0.205
4	22 (21)	30 (28)	25 (24)	0.153
5	30 (28)	37 (35)	33 (31)	0.105
6	37 (35)	44 (42)	40 (38)	0.069
7	44 (42)	52 (49)	47 (45)	0.043
8	52 (49)	59 (56)	55 (52)	0.027
9	59 (56)	66 (63)	62 (59)	0.016
10	66 (63)	74 (70)	70 (66)	0.010
11	74 (70)	81 (77)	77 (73)	0.006
12	81 (77)	89 (84)	84 (80)	0.003
13	89 (84)	96 (91)	92 (87)	0.002
14	96 (91)	103 (98)	99 (94)	0.001
15	103 (98)	Infinity	116 (110)	0.001

Table E-9
Discretized Distribution for Case 8 Heat Release Rate (Transients¹)

Bin	Heat Release Rate – kW (Btu/s)			Severity Factor (P _i)
	Lower	Upper	Point Value	
1	0 (0)	37 (35)	22 (21.2)	0.169
2	37 (35)	74 (70)	55 (52)	0.249
3	74 (70)	111 (105)	92 (87)	0.205
4	111 (105)	148 (140)	128 (121)	0.143
5	148 (140)	185 (175)	165 (156)	0.093
6	185 (175)	222 (210)	202 (191)	0.058
7	222 (210)	258 (245)	238 (226)	0.035
8	258 (245)	295 (280)	275 (261)	0.020
9	295 (280)	332 (315)	312 (296)	0.012
10	332 (315)	369 (350)	349 (331)	0.007
11	369 (350)	406 (385)	386 (366)	0.004
12	406 (385)	443 (420)	423 (401)	0.002
13	443 (420)	480 (455)	460 (436)	0.001
14	480 (455)	517 (490)	497 (471)	0.001
15	517 (490)	Infinity	578 (548)	0.001

Table H-1
Damage Criteria for Electrical Cables – Generic Screening Criteria for the
Assessment of the Ignition and Damage Potential of Electrical Cables [See Ref 8-1]

Cable Type	Radiant Heating Criteria	Temperature Criteria
Thermoplastic	6 kW/m ² (0.5 BTU/ft ² s)	205°C (400°F)
Thermoset	11 kW/m ² (1.0 BTU/ft ² s)	330°C (625°F)

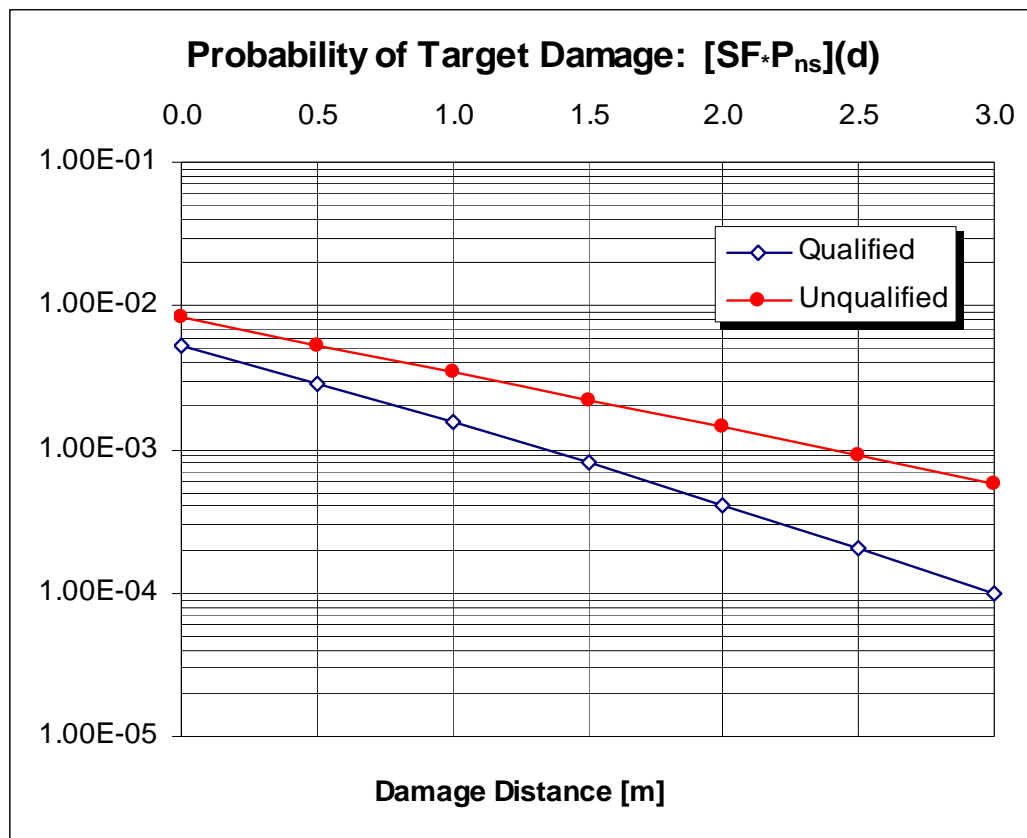


Figure L-1
Likelihood of Target Damage Calculated as the Severity Factor Times the
Probability
of Non-suppression for MCB Fires

Table P-2

Probability Distribution for Rate of Fires Suppressed per Unit Time, λ (Source: EPRI1019259, Supplement to NUREG/CR-6850)

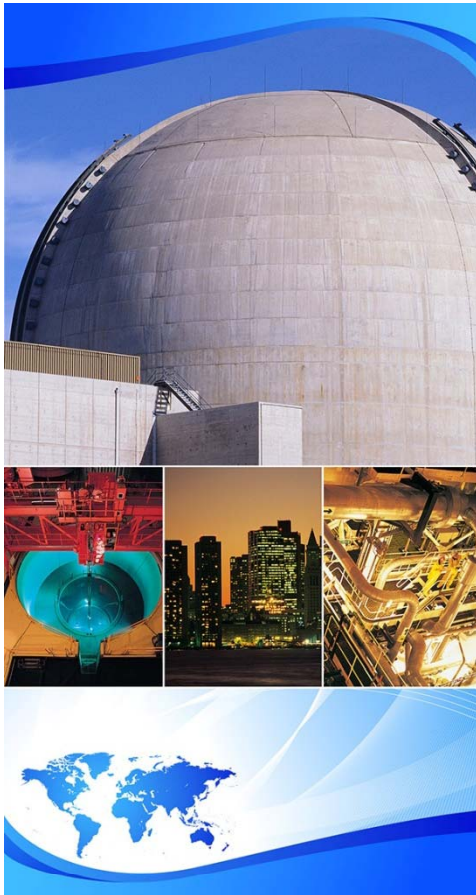
Suppression Curve	No. of original events/revised events	Original NUREG/CR-6850		Revised Analysis	
		Original Total Suppression Time	Original Mean Suppression Rate [/min]	Revised Total Duration	Revised Mean Suppression Rate [/min]
T/G fires	21/21	749	0.03	846	0.025
Control room	6/6	18	0.33	18	0.33
PWR containment	3/3	23	0.13	40	0.075
Outdoor transformers	14/14	373	0.04	390	0.036
Flammable gas	5/5	195	0.03	197	0.025
Oil fires	36/36	404	0.09	474	0.076
Cable fires	5/5	21	0.24	31	0.161
Electrical fires	114/113	942	0.12	1113	0.102
Welding fires	19/18	99	0.19	106	0.188
Transient fires	24/22	199	0.12	174	0.126
High-energy arcing faults	3/3	239	0.01	276	0.011
All fires	245 ²¹ /246	3113	0.08	3655	0.067

Table P-3

Numerical Results for Suppression Curves (Source: EPRI1019259, Supplement to NUREG/CR-6850)

Time (min)	T/G fires	High-energy arcing faults	Outdoor transformers	Flammable gas	Oil fires	Electrical fires	Transient fires	PWR containment	Welding	Control room	Cable fires	All fires
0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
5	0.883	0.947	0.836	0.881	0.684	0.602	0.531	0.687	0.392	0.189	0.446	0.714
10	0.780	0.897	0.698	0.776	0.468	0.362	0.282	0.472	0.153	0.036	0.199	0.510
15	0.689	0.850	0.584	0.683	0.320	0.218	0.150	0.325	0.060	0.007	0.089	0.364
20	0.609	0.805	0.488	0.602	0.219	0.131	0.080	0.223	0.024	0.001	0.040	0.260
25	0.538	0.762	0.408	0.530	0.150	0.079	0.042	0.153	0.009	*	0.018	0.186
30	0.475	0.722	0.341	0.467	0.102	0.048	0.023	0.105	0.004	*	0.008	0.133
35	0.419	0.684	0.285	0.411	0.070	0.029	0.012	0.072	0.001	*	0.004	0.095
40	0.370	0.647	0.238	0.362	0.048	0.017	0.006	0.050	*	*	0.002	0.068
45	0.327	0.613	0.199	0.319	0.033	0.010	0.003	0.034	*	*	*	0.048
50	0.289	0.581	0.166	0.281	0.022	0.006	0.002	0.024	*	*	*	0.035
55	0.255	0.550	0.139	0.248	0.015	0.004	*	0.016	*	*	*	0.025
60	0.226	0.521	0.116	0.218	0.010	0.002	*	0.011	*	*	*	0.018
65	0.199	0.493	0.097	0.192	0.007	0.001	*	0.008	*	*	*	0.013
70	0.176	0.467	0.081	0.169	0.005	*	*	0.005	*	*	*	0.009
75	0.155	0.443	0.068	0.149	0.003	*	*	0.004	*	*	*	0.006
80	0.137	0.419	0.057	0.131	0.002	*	*	0.002	*	*	*	0.005
85	0.121	0.397	0.047	0.116	0.002	*	*	0.002	*	*	*	0.003
90	0.107	0.376	0.040	0.102	0.001	*	*	0.001	*	*	*	0.002
95	0.095	0.356	0.033	0.090	*	*	*	*	*	*	*	0.002
100	0.084	0.337	0.028	0.079	*	*	*	*	*	*	*	0.001

* A value of 1E-3 should be used



EPRI/NRC-RES FIRE PRA METHODOLOGY

Introduction and Overview: the Scope and Structure of Fire Analysis Module

Francisco Joglar-Biloch - Science Applications International Corp.
Dave Stroup – U.S. NCR Office of Nuclear Regulatory Research

Joint RES/EPRI Fire PRA Training Workshop
San Diego, CA, August 2011 and
Jacksonville, FL, November 2011

A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

What we'll cover in the next four days

An overview...

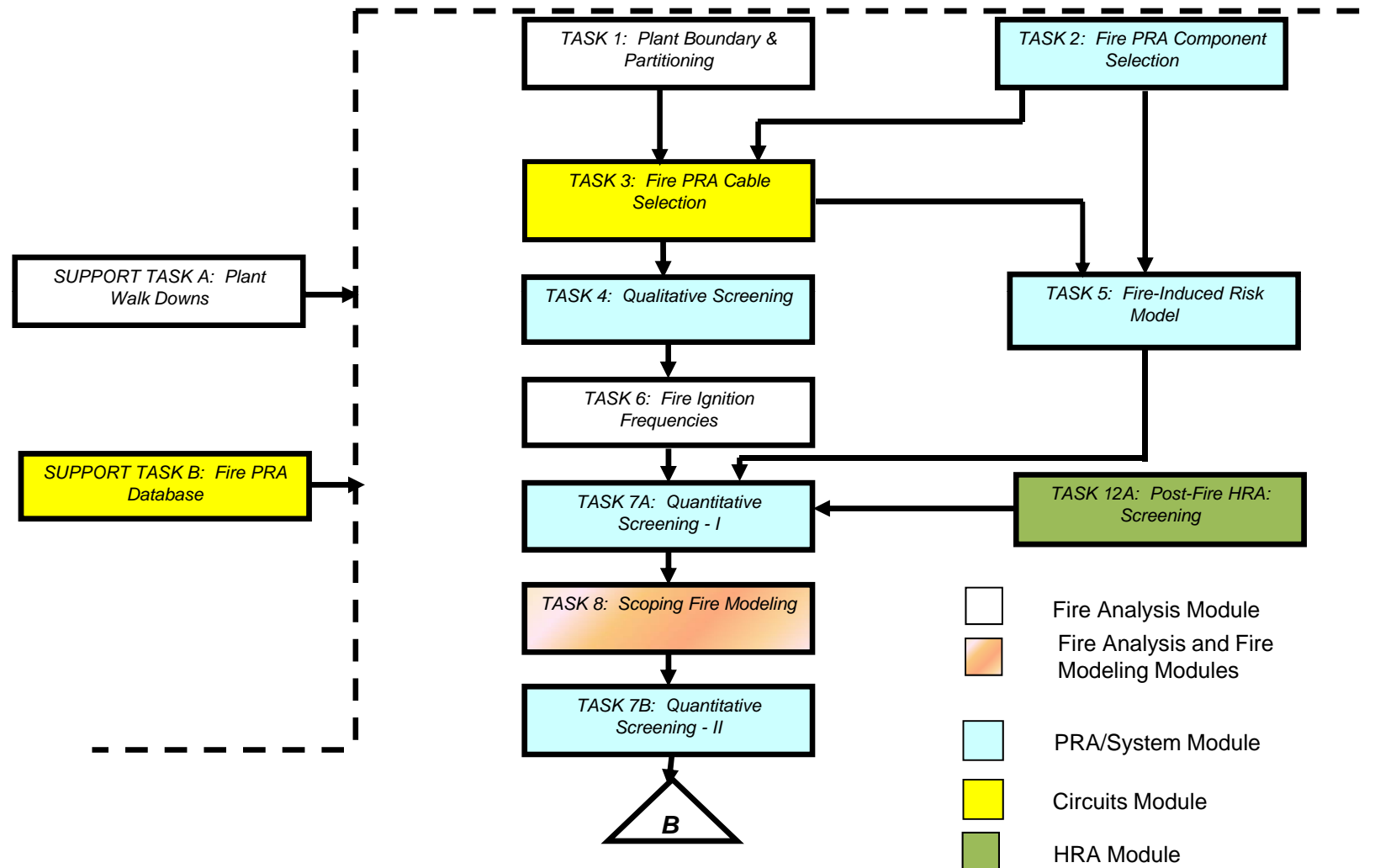
- The purpose of this presentation is to provide an Overview of the Module 3 – Fire Analysis
 - Scope of this module relative to the overall methodology
 - Which tasks fall under the scope of this module
 - General structure of the each technical task in the documentation
 - Quick introduction to each task covered by this module:
 - Objectives of each task
 - Task input/output
 - Task interfaces

Training Objectives

- Our intent:
 - To deliver practical implementation training
 - To illustrate and demonstrate key aspects of the procedures
- We expect and want significant participant interaction
 - Class size should allow for *questions and discussion*
 - We will take questions about the *methodology*
 - We *cannot* answer questions about a *specific application*
 - We will moderate discussions, and we will judge when the course must move on

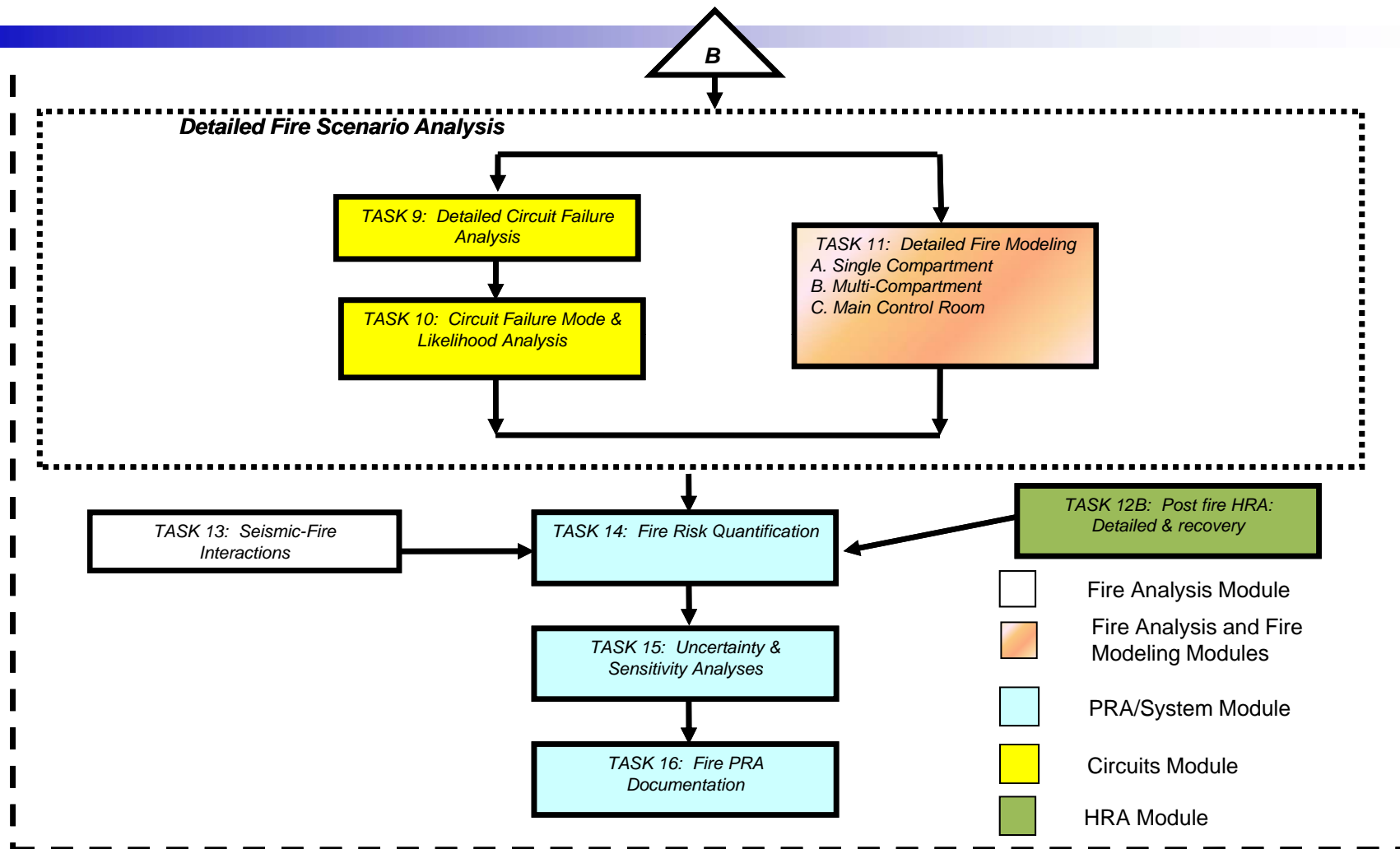
Recall the overall fire PRA structure

Module 3 covers tasks in white and white/orange



Recall the overall fire PRA structure (2)

Module 3 covers tasks in white and white/orange



Each technical task has a common structure as presented in the guidance document

1. Purpose
 2. Scope
 3. Background information: General approach and assumptions
 4. Interfaces: Input/output to other tasks, plant and other information needed, walk-downs
 5. Procedure: Step-by-step instructions for conduct of the technical task
 6. References
- Appendices: Technical bases, data, examples, special models or instructions, tools or databases

Scope of Module 3: Fire Analysis

- This module covers those parts of the method specifically related to the identification and analysis of fires, fire damage, and fire protection systems and features
- Tasks covered are:
 - Task 1: Plant Partitioning
 - Task 6: Fire Ignition Frequency
 - Task 8: Scoping Fire Modeling
 - Task 11: Detailed Fire Scenario Analysis
 - Task 13: Seismic/Fire Interactions (briefly)
 - Support Task A: Plant Walkdowns

Task 1: Plant Partitioning (1 of 3)

Module 3

- Objectives:
 - Define the global analysis boundary of the FPRA
 - Divide the areas within the global analysis boundary into fire compartments
- The fire compartments become the “basic units” of analysis
 - Generally we screen based on fire compartments
 - Risk results are often rolled up to a fire compartment level
- A note on terminology:
 - The PRA standard uses “physical analysis units” rather than “fire compartments”
 - Definitions are quite similar, overall role in analysis is identical
 - Don’t let the terminology difference trip you up – intent is the same

Task 1: Plant Partitioning (2 of 3)

Module 3

- The global analysis boundary is intended to be a liberal definition of the region potential interest
 - It will likely encompass areas of essentially no risk, but that is OK, screening steps will identify these
- The fire compartments are a matter of analysis convenience
 - Fire compartments may equal fire areas if you so choose
 - You can also subdivide fire areas into multiple compartments
 - The sum of the fire compartments must equal the global analysis boundary
 - No omissions, no overlap between compartments

Task 1: Plant Partitioning (3 of 3)

Module 3

- Ultimately, the FPRA is expected to provide some resolution to each defined fire compartment and to all locations within the global analysis boundary
- Module will cover:
 - Guidance and criteria for defining the global analysis boundary
 - Guidance and criteria for defining fire compartments
- Ultimately, there is not a lot of new guidance in this task
 - A lot like what was done in the IPEEE days

Task 6: Fire Ignition Frequency (1 of 3)

Module 3

- Objective: To define fire frequencies suitable to the analysis of fire scenarios at various stages of the FPRA
- Fire frequencies will be needed at various resolutions:
 - An entire fire area
 - A fire compartment (or physical analysis unit)
 - A group of fire ignition sources (e.g., a bank of electrical cabinets)
 - A single ignition source (e.g., one electrical panel)

Task 6: Fire Ignition Frequency (2 of 3)

Module 3

- Task begins with generic industry-average statistics on fire
 - EPRI fire event database
 - Events filtered for applicability and sorted into ignition source bins
 - Plant-wide fire frequency is provided for each bin
- The real “trick” is to convert the generic values into values specific to your plant and to a given fire scenario
 - Approach is based on ignition source counting and apportionment of the plant-wide frequency based on local population

Task 6: Fire Ignition Frequency (3 of 3)

Module 3

- Quite a bit is new relative to fire frequency:
 - The fire event data have been re-analyzed entirely to suit the new method
 - That means older IPEEE-vintage frequencies are obsolete
 - There has been a switch towards component-based fire frequencies and away from generic room-based fire frequencies
 - Some areas have received special treatment
 - e.g., main control room

Task 8: Scoping Fire Modeling (1 of 2)

Module 3

- Objective: To identify (and screen out) fire ignition sources that are non-threatening and need not be considered in detailed fire modeling
- Non-threatening means they cannot:
 - Spread fire to other combustibles, or
 - Damage any FPRA equipment item or cable

Task 8: Scoping Fire Modeling (2 of 2)

Module 3

- Scoping fire modeling introduces a number of key concepts associated with the treatment of fire sources and damage targets
 - The Fire Severity Profile approach
 - Damage criteria for cables and equipment
 - Assumptions associated with specific fire sources

Task 11: Detailed Fire Modeling (1 of 3) Module 3

- Objective: To identify and analyze specific fire scenarios
- Divided into three sub-tasks:
 - 11a: General fire compartments (as individual risk contributors)
 - 11b: Main Control Room analysis
 - 11c: Multi-Compartment fire scenarios

Task 11: Detailed Fire Modeling (2 of 3)

Module 3

- Task 11 involves many key elements
 - Selection of specific fire scenarios
 - Combinations of fire sources and damage targets
 - Analysis of fire growth/spread
 - Application of fire models
 - Analysis of fire damage
 - Time to failure
 - Analysis of fire detection and suppression

Task 11: Detailed Fire Modeling (3 of 3) Module 3

- Task 11 comes with a wide range of supporting appendices including:
 - Specific fire sources such as high energy arc faults, turbine generator fires, and hydrogen fires
 - Treatment of fire severity and severity factors
 - Treatment of manual fire suppression
 - Treatment for main control board fires
- Module will cover key appendices

Task 13: Seismic/Fire Interactions

Module 3

- Objective: A *qualitative* assessment of potential fire/seismic interactions
- Module will cover this task *briefly*
 - No significant changes from IPEEE guidance (e.g., the Fire PRA Implementation Guide)



Any questions before we move on?