REACTOR CONTAINMENT BUILDING INTEGRATED LEAKAGE RATE TEST

TYPES A, B, AND C PERIODIC TEST



IOWA ELECTRIC LIGHT AND POWER COMPANY DUANE ARNOLD ENERGY CENTER

DOCKET No. 50-331 OPERATING LICENSE No. DPR-49

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Prepared by

STONE & WEBSTER ENGINEERING CORPORATION BOSTON, MASSACHUSETTS

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REFERENCES

- 1. 10CFR Part 50, Appendix J, Primary Reactor Containment Leakage Testing for Water-Cooled Power Reactors, January 1, 1989.
- 2. STP No. 47A002, Primary Containment Leakage Rate Test, Duane Arnold Energy Center, Surveillance Test Procedure.
- 3. ANSI N45.4, American National Standard, Leakage-Rate Testing of Containment Structures for Nuclear Reactors, March 16, 1972.
- 4. ANSI/ANS-56.8, Containment System Leakage Testing Requirements, January 20, 1987.
- 5. Bechtel Corporation's Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants, BN-TOP-1, Revision 1, November 1, 1972.
- 6. STP No. 47A003, Containment Leak Tightness Test Type B Penetrations, Duane Arnold Energy Center, Surveillance Test Procedure.
- 7. STP No. 47A004, Airlock Local Leak Rate Test, Duane Arnold Energy Center, Surveillance Test Procedure.
- 8. STP No. 47A005, Containment Isolation Valve Leak Tightness Test Type C Penetrations, Duane Arnold Energy Center, Surveillance Test Procedure.

¹ This document used only as a guideline and any reference to said document in no way implies compliance.

SECTION 1

1.0 PURPOSE

The purpose of this report is to present a description and analysis of the August 1990 Periodic Type A Primary Containment Integrated Leakage Rate Test (ILRT) and a summary of the Periodic Types B and C Local Leakage Rate Tests (LLRT) conducted since December 1988 at the Duane Arnold Energy Center (DAEC). DAEC is operated by the Iowa Electric Light and Power Company (IE). Specific plant information and technical data is contained in Attachment 1A.

Stone & Webster Engineering Corporation (SWEC) provided engineering consultation services to Iowa Electric Light and Power Company during the performance of this test.

This report is submitted as required by 10CFR50, Appendix J, Paragraph V.B.

ATTACHMENT 1A

TEST DATA SUMMARY

A. Plant Information

Operator Iowa Electric Light and Power Company
Plant Duane Arnold Energy Center
Location Palo, Iowa
Containment Type Mark I, BWR/4
Docket Number 50-331
Operating License No. DPR-49
Date Test Completed August 30, 1990

B. Technical Data

Containment Net Free Air Volume as Tested	205,360 cu. ft.
Drywell Free Air Volume	109,400 cu. ft.
Torus Free Air Volume	95,960 cu. ft.
Design Pressure	56 psig
Calculated Peak Accident Pressure	43 psig
Containment Design Temperature	281 °F
Containment ILRT Average Temperature Limits	40-100 °F

SECTION 2

- 2.0 SUMMARY
- 2.1 TYPE A TEST
- 2.1.1 Test Summary

Pressurization for the ILRT began at approximately 0525 hours on August 29, 1990. Pressurization was initially at 6.3 psi/hour but was slowed to 3.6 psi/hour when the air drier appeared to overload. Extensive investigations of all penetration areas were conducted throughout the pressurization and the Type A test. One major leak was detected at a cracked nipple on the containment side of isolation valve CV4304. This leak was monitored during the pressurization and throughout the test.

Containment pressurization was secured at approximately 1525 hours on August 29, 1990. The pressurization piping system was isolated and vented. The leakage from CV4304 was measured locally and estimated to be in the range of 100,000 SCCM.

At 2000 hours on August 29, 1990, the thermal stabilization criteria of Reference 2 was satisfied. Pressure, temperature and dew point data were continuously recorded throughout the test period at 15 minute intervals.

The Type A test was successfully completed at 0400 hours on August 30, 1990 with a Total Time Upper Confidence Limit (UCL-TT) of 1.063981 percent/day and a Mass Point Upper Confidence Limit of 1.035137 percent/day. Both Total Time and Mass Point leakage rates were below the 0.75L_a acceptance criteria.

The Superimposed Verification Test was started at 0515 hours on August 30, 1990 and was successfully completed at 0915 hours on August 30, 1990. The results of the verification test satisfied the requirements of Reference 2 (See Appendix G, page 3).

After the completion of the verification test, the broken nipple on CV4304 was replaced and verified to be leak tight prior to the completion of depressurization.

Depressurization of the containment began at approximately 1000 on August 30, 1990 and was completed at 2000 on August 30, 1990.

2.2 LOCAL LEAKAGE RATE TESTS (Types B and C)

The Local Leakage Rate Tests (LLRT) of containment isolation valves and other containment penetrations were conducted as required by the methods described in the plant surveillance procedures, References 6, 7 and 8, for the Types B and C Tests.

Section 4 of this report summarizes the data for the LLRT conducted since the December 1988 Type A test in accordance with Appendix J, 10CFR50, Paragraph V.B. Also contained in Section 4 of this report is the 1990 LLRT Summary Analysis.

SECTION 3

3.0 TYPE A TEST

3.1 EDITED LOG OF EVENTS

This log was edited from information contained in the ILRT Coordinator's Official Type A Log of Events or from Reference 2.

August 28, 1990

- 2000 Drywell inspection successfully completed.
- 2030 Drywell cooling and fans secured.

August 29, 1990

- 0525 Pressurization started.
- 0545 CV4312 closed at 1 psi differential pressure.
- Jumper on CV4312 discovered not to be making contact. This was corrected and flow re-established with two compressors running.
- 0830 Energized dewpoint sensor power supply. Walk down for leakage detection initiated.
- Large leak detected on top of valve CV4304. Appears to be leaking at cracked nipple on containment side of the valve seat.
- Dewpoint rising rapidly. Drier appears to be overloaded. Drains opened and back pressure increased on the drier.
- One compressor tripped out. Will continue pressurization with one compressor to help control dewpoint.
- 1525 Pressurization secured with a peak pressure of 59.2574 psia.
- Reactor coolant temperature increasing steadily. Operations personnel were making efforts to control temperature with RHR.
- 1640 Leakage at CV4304 was measured and estimated to be about 100,000 SCCM or about 0.6 % per day.
- 1950 Thermal stabilization criteria was satisfied at the 1945 data set.
- 2000 Leakrate test started.

- Leak surveys have revealed only minor leakage. V43-161 which is the vent valve in the pressurization line up is leaking slightly. V24-51 and V22-65 are showing slight packing leaks.
- Additional small leaks found at packing of V43-199 and CV4310 in the drywell exhaust valve room.

August 30, 1990

- 0400 Short duration test criteria satisfied.
- 0414 Superimposed leakage established.
- 0515 Superimposed verification test started.
- 0915 Superimposed verification test successfully completed.
- 1000 Started depressurization of the containment.
- 2000 Containment depressurized.

3.2 GENERAL TEST DESCRIPTION

3.2.1 Prerequisites

In accordance with Reference 2, the following is a listing of the pertinent prerequisites and other procedural requirements completed and documented prior to containment pressurization:

- a. Site meteorological data recorded during the performance of the ILRT (Attachment 3.2A)
- b. All required test instrumentation installed and functionally verified within 6 months of the test.
- c. Primary containment ventilation system secured.
- d. Satisfactory inspection of the primary containment in accordance with Reference 2.
- e. Pressurization system lined-up and ready for operation.
- f. RCS temperature maintained stable prior to and during the performance of the ILRT.
- g. Data acquisition and analysis computer systems used for the test are operational.
- h. All required system valve lineups completed.
- i. Drywell-to-torus vacuum breakers are blocked open.
- j. Restricted plant access plan in effect.
- k. An Official Type A Log of Events established and maintained by the ILRT Coordinator.
- l. All pressurized components and systems either removed from the containment or vented.
- m. All required Types B and C leakage rate testing completed.
- n. Verification flowmeter installed.
- o. Instrument Selection Guide (ISG) calculated.

3.2.2 Equipment and Instrumentation

Pressurization of the primary containment was achieved by utilizing two diesel driven air compressors, an aftercooler, and a refrigerant air drier. The system included adequate instrumentation and valving to maintain proper monitoring and control of the compressed air quality throughout the pressurization sequence. The capacity of the temporary air compressors is approximately 1,800 standard cubic feet per minute (SCFM).

The various containment parameters required to calculate containment leakage during the test, were monitored using instrumentation which consisted of 15 resistance temperature detectors, 6 dewpoint temperature sensors, and 2 absolute pressure indicators. Pertinent data for the test instrumentation is listed in Attachment 3.2B, and the general locations of the test instrumentation for both the drywell and the suppression chamber are shown in Attachments 3.2C and 3.2D. Elevations and azimuths are approximate.

A rotometer was used to perform the superimposed leakage verification test.

Instrument Selection Guide (ISG)

Sensor Type	No. of Sensors	Sensitivity Error	System Error
Pressure	2	0.015 psi	0.00 psi
Temperature	15	2.00 °F	0.00 °F
Dewpoint Temp.	6	5.00 °F	0.00 °F

Test Duration (t) 8 hrs. Test Pressure 57.696 psia Test Temperature 80 °F = 540 °R Test Dewpoint Temp. 80 °F

$$ISG = \pm \frac{2400}{t} \sqrt{2 \times \left(\frac{EP}{P}\right)^2 + 2 \times \left(\frac{ET}{T}\right)^2 + 2 \times \left(\frac{EP_{\nu}}{P}\right)^2}$$

ISG \leq 0.25 L_a which equals 0.5% per day since L_a = 2.0% per day

a. EP = error associated with absolute pressure instruments

$$EP = \frac{0.015}{\sqrt{2}} = 0.010607$$

b. ET = error associated with temperature instruments

$$ET = \frac{2.0}{\sqrt{15}} = 0.516398$$

c. $EP_v = error$ associated with vapor pressure instruments

$$EP_{\rm v} = \frac{0.082896}{\sqrt{6}} = 0.033842$$

Using values established in a,b and c above, calculate ISG.

$$ISG = \pm \frac{2400}{8} \sqrt{2 \times \left(\frac{0.010607}{57.696}\right)^2 + 2 \times \left(\frac{0.0.516398}{540}\right)^2 + 2 \times \left(\frac{0.033842}{57.696}\right)^2}$$

ISG = ± 0.482309 which is less than 0.5%/day (25% of L_2)

3.2.3 Data Acquisitiou System

A programmable, multichannel data logger was used to scan the data from the 15 resistance temperature detectors and 6 dewpoint temperature sensor input signals. The 2 pressure readings were taken manually. Data was taken at 15 minute intervals throughout the test.

3.2.4 Data Resolution System

The recorded data was manually inputted to a dedicated computer system using Stone & Webster Engineering Corporation's (SWEC) ILRT analysis program for data reduction and leakage rate calculations. The computer program converted the Dewcel Element Temperatures to Dewpoint Temperatures using a polynomial curve fit derived from the Dewcel vendor's test data. The following calculations used the instantaneous values of the ILRT sensors to determine both the Mass Point and Total Time Analysis Method leakage rates.

Absolute Method of Mass Point Analysis

The Absolute Method of Mass Point Analysis consists of calculating the air mass within the containment structure, over the test period using pressure, temperature, and dewpoint temperature observations made during the ILRT. The air mass is computed using the ideal gas law as follows:

$$M = 144 \times V \frac{(P - P_{v})}{RT}$$
 (Eq. 1)

where:

M = air mass, lbm

P = total pressure, psia

 P_{v} = average vapor pressure, psia

 $R = 53.35 \text{ ft-lbf/lbm}^{\circ}R \text{ (for air)}$

T = average containment temperature, °R

V = containment free volume, ft³

The leakage rate is then determined by plotting the air mass as a function of time, using a least-squares fit to determine the slope, A = dM/dT. The leakage rate is expressed as a percentage of the air mass lost in 24 hours or symbolically:

Leakage Rate =
$$-2400 \left(\frac{A}{B} \right)$$
 (Eq. 2)

Where A is the slope of the least-squares curve and B is the y-intercept. The sign convention is such that the leakage out of the containment is positive, and the units are in percent/day.

A confidence interval is calculated using a Student's T distribution. The sum of the leakage rate and confidence interval is the Upper Confidence Limit - Mass Point (UCL-MP).

Absolute Method of Total Time Analysis

The Absolute Method of Total Time Analysis consists of calculating air lost from the containment, using pressure, temperature, and dewpoint temperature observations made during the ILRT.

The containment air mass is computed using Equation 1. The measured leakage rate at any time (t) is then determined by subtracting the mass at that time (Mt) from the initial mass (Mi) and dividing by the initial mass. The measured leakage rate is expressed as a percentage of containment mass lost in 24 hours or symbolically:

Measured Leakage rate =
$$2400 \frac{(M_i - M_t)}{M_i(\Delta t)}$$
 (Eq. 3)

The sign convention is such that leakage out of the containment is positive, and the units are in percent/day.

The calculated leakage rate is then determined by plotting the measured leakage rate as a function of time and then performing a least-squares curve fit of the measured leakage rate values as follows:

Calculated Leakage rate =
$$At+B$$
 (Eq. 4)

Where, A is the slope and B is the y-intercept of the least squares curve.

A confidence interval is calculated using the requirements of Bechtel Topical Report BN-TOP-1, Rev. 1.

The sum of the calculated leakage rate and the confidence interval is the Upper Confidence Limit - Total Time (UCL-TT).

SITE METEOROLOGY

<u>Date</u>	<u>Time</u>	Ambient Temp. (Deg F)	Dewpoint Temp. (Deg F)	Barometric Pressure (In. Hg)	General Weather Conditions
August 29, 1990	0600	67.0	62.0	30.0	clear
	0700	64.9	60.9	30.0	clear
	0800	66.7	62.8	30.0	clear
	0900	70.6	60.0	30.0	clear
	1000	75.9	60.2	30.0	clear
	1100	78.5	59.8	30.0	clear
	1200	79.8	58.6	30.0	clear
	1300	80.7	60.2	30.0	clear
	1400	81.1	60.8	30.0	clear
	1500	80.6	63.0	29.9	cloudy
	1600	79.3	64.1	29.9	rain
	1700	66.3	62.2	30.0	cloudy
	1800	69.2	63.5	30.0	cloudy
	1900	68.7	61.5	30.0	cloudy
	2000	67.6	62.9	30.0	cloudy
	2100	66.9	63.7	30.0	partly cloudy
	2200	66.3	63.1	30.0	cloudy
	2300	65.9	62.4	30.0	cloudy
,	2400	66.2	63.3	30.0	cloudy
August 30, 1990	0100	65.8	62.9	30.0	cloudy
,	0200	65.6	62.5	30.0	foggy
	0300	64.0	61.2	30.0	foggy
	0400	64.5	61.4	30.0	foggy
	0500	62.7	59.8	30.0	foggy
	0600	61.9	59.0	30.0	clear
	0700	61.5	58.5	30.1	clear
•	0800	63.3	59.5	30.1	sunny

ATTACHMENT 3.2B

INSTRUMENTATION LIST

The following instruments were calibrated and functionally verified within 6 months prior to the performance of this test and in accordance with 10CFR50, Appendix J.

Instrument	Weight Fraction	Computer Point	Zone	Azimuth	Elevation	Range	Accuracy
A.	Temperatu	ıre					
T1	0.1155	C0	6	270°	735	32-250°F	±0.5°F
T2	0.1155	C1	6	0°	735	32-250°F	±0.5°F
Т3	0.1155	C2	6	90°	735	32-250°F	±0.5°F
T4	0.1155	C3	6	180°	735	32-250°F	±0.5°F
T 5	0.047	C4	4	45°	749	32-250°F	±0.5°F
Т6	0.047	C5	4	225°	750	32-250°F	±0.5°F
T12	0.024	C11	5	Rx CL	750	32-250°F	±0.5°F
T 7	0.053	C6	3	90°	764	32-250°F	±0.5°F
T 8	0.053	C7	3	210°	763	32-250°F	±0.5°F
T14*	0.054	C13	3	315°	766	32-250°F	±0.5°F
T 9	0.046	C8	2	20°	786	32-250°F	±0.5°F
T10	0.046	C9	2	150°	786	32-250°F	±0.5°F
T13*	0.046	C12	2	290°	787	32-250°F	±0.5°F
T11	0.061	C10	1	345°	828	32-250°F	±0.5°F
T15*	0.061	C14	1	165°	828	32-250°F	±0.5°F
В.	Dewpoint Tem	perature					
M5	0.231	C24	С	270°	735	32-150°F**	±5.0°F
M6	0.231	C25	С	90°	735	32-150°F**	±5.0°F
M3	0.139	C22	В	225°	750	32-150°F**	±5.0°F
M4	0.139	C23	В	45°	749	32-150°F**	±5.0°F
M1	0.130	C20	Ā	340°	809	32-150°F**	±5.0°F
M2	0.130	C21	A	160°	809	32-150°F**	±5.0°F



INSTRUMENTATION LIST

Instrument	Weight Fraction	Computer Point	Zone	Azimuth	Elevation	Range	Acouracy
C. Pressure	•						
P1 P2	0.500000 0.500000	Local Local	Drywe Torus	11 - -	-	0-100psia 0-100psia	± 0.015%FS ± 0.015%FS
D. Superimp	osed Leakage	Verification	Test Flo	w Instrum	ent		
Rotometer	<u>-</u>	-	Local	_	_	5-19scfm	±1.0%F.S.

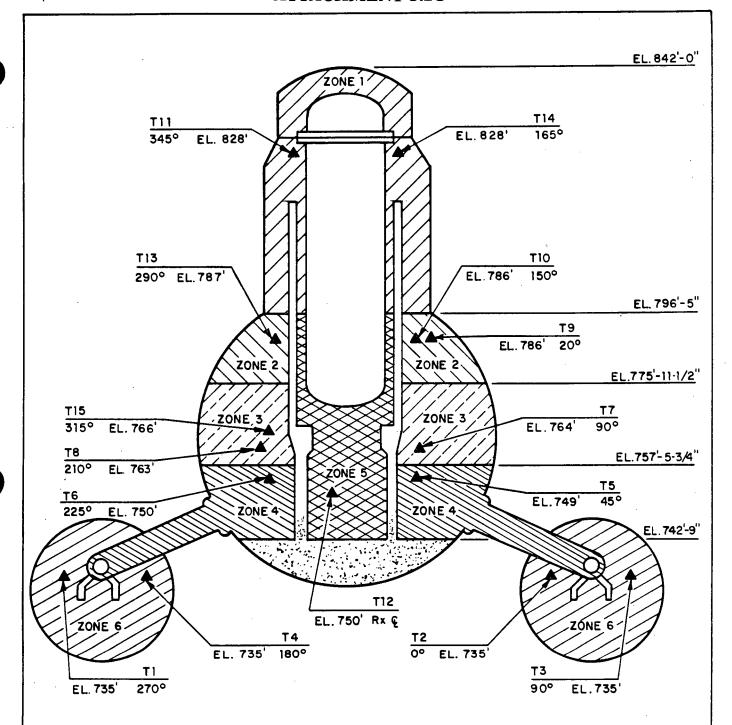
Notes:

- * Temporary RTD and/or Dewpoint Sensors.
- ** The Dewcel Element Temperatures (ET) were converted to Dewpoint Temperatures (DPT) by the following polynomial equation:

 $DPT = -1.5923290156E + 1 + 3.2150392932E - 1 \times ET + 2.7879779394E - 3 \times ET^{2} - 7.1099385788E - 6 \times ET^{3}$

This equation is valid over the range of 51.2 to 83.7 $^{\circ}F$ Dewpoint Temperature (ET of 121 to 169 $^{\circ}F$)

ATTACHMENT 3.2C



NOTES:

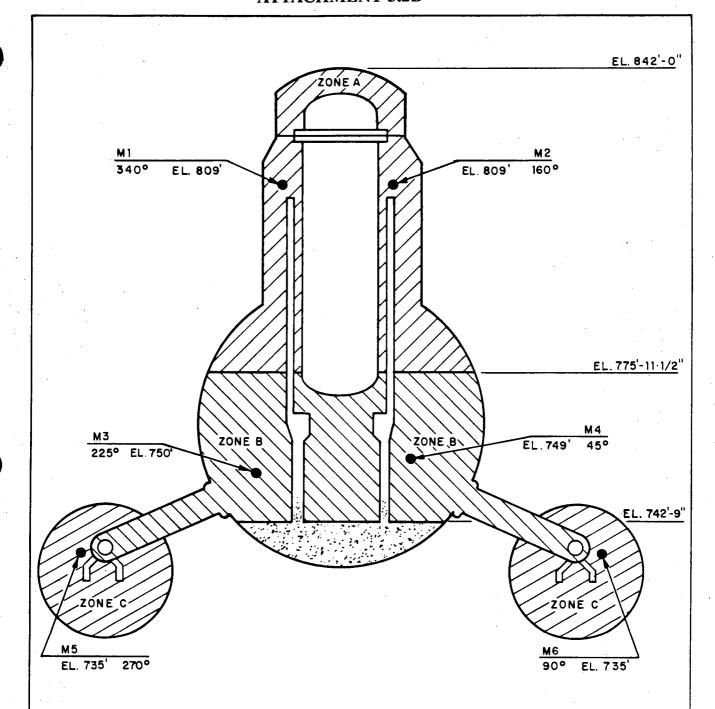
- ZONE BOUNDARIES ARE APPROXIMATE, REFERENCE DAEC DWG. No. M-156
- 2. RTD ELEVATIONS AND AZIMUTH POSITIONS ARE APPROXIMATE

ATTACHMENT 3.2C

ILRT TEMPERATURE DETECTOR

LOCATIONS

DUANE ARNOLD ENERGY CENTER



NOTES:

- 1. ZONE BOUNDARIES ARE APPROXIMATE, REFERENCE DAEC DWG. No. M-156
- 2. DEWPOINT TEMPERATURE SENSOR ELEVATIONS AND AZIMUTH POSITIONS ARE APPROXIMATE

ATTACHMENT 3.2D

ILRT DEWPOINT TEMPERATURE
SENSOR LOCATIONS

DUANE ARNOLD ENERGY CENTER

3.3 TEST RESULTS

3.3.1 Presentation of Test Results

The test data for the August 1990 ILRT is based on a 8 hour test period starting at 2000 hours on August 29, 1990. The final test results were determined using SWEC's ILRT computer program. The Measured Input Data, Reduced Input Variables, Mass Point Analysis Test Results, Total Time Analysis Test Results, and representative graphs are contained in Attachments 3.3A through 3.3K.

Both the Mass Point and Total Time Analysis Test Results for the ILRT satisfied the procedural acceptance criteria.

The Type A Test instrumentation was verified by the Superimposed Leakage Verification Test Method. The Measured Input Data, Reduced Input Variables, Mass Point Analysis Test Results, Total Time Analysis Test Results, and representative graphs are contained in Attachments 3.3L through 3.3S.

Both the Mass Point and Total Time Analysis Test Results for the Superimposed Leakage Verification Test satisfied the procedural acceptance criteria.

3.3.2 ILRT Results

The 57.696 psia ILRT was conducted in accordance with Reference 2. The results for the ILRT and for the Supplemental Test are shown below.

3.3.2.1 ILRT Results - Mass Point Analysis

	<u>Item</u>		(Percent/Day)
1.	L _{am} , Leakage Rate Calculated		1.028984
2.	UCL, Upper Confidence Level		0.006153
3.	UCL-MP, L _{am} Leakage Rate plus UCL (1&2)		1.035137
4.	Corrections for:		
	(See Sections 3.3.2.4)		
	i. Type B & C Penaltie	s 0.048644	
	ii. Water Levels	0.033722	
	iii. Total Corrections		0.082366
	(i. and ii.)		
5.	Total Reported Type A Leakag (Items 3&4 iii.)	e Rate	1.117503

Results were within the acceptable limits of 0.75 L_a or 1.5 percent/day.

3.3.2.2 ILRT Results - Total Time Analysis

	<u>Item</u>	(Percent/Day)
1.	L _{am} , Leakage Rate Calculated	1.033847
2.	UCL, Upper Confidence Level	0.030133
3.	UCL-TT, L _{am} Leakage Rate plus UCL (1&2)	1.063981
4.	Corrections for: (See Section 3.3.2.4)	
	i. Type B & C Penalties 0.0486ii. Water Levels 0.0337	
	iii. Total Corrections (i. and ii.)	0.082366
5.	Total Reported Type A Leakage Rate (Items 3&4 iii.)	1.146347

Results were within the acceptable limits of 0.75 L_a or 1.5 percent/day.

3.3.2.3 Supplemental Test Results

The Supplemental Verification Test was performed using the Superimposed Leakage Verification Test Method in accordance with Reference 2. The results for the Superimposed Leakage Verification Test are shown below.

1. The Superimposed Leakage Verification Test is acceptable provided L_c falls within the following range:

$$(L_{am} + L_o - 0.25 \times L_a) \leq L_c \leq (L_{am} + L_o + 0.25 \times L_a)$$
 (Eq. 5)

a. Mass Point

$$(1.028984 + 2.064705 - 0.5) \le 2.696423 \le (1.028984 + 2.064705 + 0.5)$$

 $(2.593689) \le 2.696423 \le (3.593689)$

b. Total Time

$$(1.033847 + 2.064705 - 0.5) \le 2.70051 \le (1.033847 + 2.064705 + 0.5)$$

 $(2.598552) \le 2.70051 \le (3.598552)$

The Superimposed Leakage Verification Test met the requirements set forth in Reference 2.

3.3.2.4 Leakage Penalties Added to Type A Leakage

Penetration leakage to be added since these penetrations were isolated or could not be vented and drained during the Type A test. The leakage assigned is the recorded value for minimum pathway analysis.

i.	Type B & C Pena	llties <u>Description</u>	Leakage <u>SCCM</u>
	, X-9A	Feedwater	2700.
	X-9B	Feedwater	950.
	X-10	RCIC Steam	450.
	X-11	HPCI Steam	450.
	X-16A	Core Spray	0.
	X-16B	Core Spray	215.
	X-21	Service Air	0.
	X-23A	RBCCW Inlet	950.
	X-23B	RBCCW Inlet	210.
	X-24A	RBCCW Outlet	220.
	X-24B	RBCCW Outlet	720.
	X-32D	N ₂ Comp Suction	275.
	X-32E	Recirc. Pump Seal	0.
	X-32F	Recirc. Pump Seal	0.
	X-36	CRD Return	34.
	X-40C	Jet Pump	0.
	X-40D	Jet Pump	0.
	X-41	Recirc. Loop Sample	159.
	X-229H	PASS	380.
	X-219	HPCI/RCIC Vac. Br.	0.

Total Type B & C Leakage 7713 SCCM Total Type B & C Leakage 0.048644 percent/day

ii.	Water Level Corrections	Description	<u>Gallons</u>
		Rx Vessel	0.0
		D.W. Equipment Sump	518.0
		D.W. Floor Sump	0.0
		Torus	0.0

Total Water Level Corrections 518.0 Gallons
Total Water Level Corrections 0.033722 percent/day

iii	Total Corrections	Description	Leakage <u>Percent/Day</u>	
	Total Type A Corrections (i. and ii.)	Penalties and Corrections	0.082366	

08/29/90	20:00								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.785	85.525	85.538	85.454	84.930					
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24				
95.703	96.328					170.880			
DC 21	RTD 0			PRESS B		170.000	133.030	130.400	107.700
164.880	83.785			58.8777					
104.000	03.703	03,330	30.7034	5,0.0777					
08/29/90	20:15								
, ,									
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5		RTD 6	RTD 7	RTD 13
83.731	85.470	85.484	85.400	84.942					89.925
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24		DC 22		DC 20
95.714	96.339					170.760	155.920	158.640	170.000
DC 21	RTD 0	RTD 2							
165.140	83.731	85.484	58.9754	58.8693					
08/29/90	20:30								
00/29/90	20.30								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.698	85.439	85.438	85.357				89.955	88.728	89.925
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24		DC 22	DC 23	DC 20
95.769	96.414	97.332 1	25.280	125.450	169.560	170.660			
DC 21	RTD 0	RTD 2							
165.110	83.698	85.438	58.9676	58.8616					
00.400.400	20.45								
08/29/90	20:45								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.651	85.391	85.402	85.332	84.992	84.131	84.308	89.942	88.746	89.943
RTD 8	RTD 9		RTD 10	RTD 14	DC 24	DC 25	DC 22	DC 23	DC 20
95.784	96.443				169.490	170.580	156.000	158.840	170.310
DC 21	RTD 0	RTD 2 I	PRESS A	PRESS B					
165.240	83.651	85.402	58.9604	58.8539					
00.400.400	01 00								
08/29/90	21:00								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.591	85.341	85.352	85.271		84.145			88.728	89.945
RTD 8	RTD 9		RTD 10		DC 24		DC 22	DC 23	DC 20
95.832	96.457	97.432 1	25.230	125.350	169.440	170.500			
DC 21	RTD 0			PRESS B				_	
165.370	83.591	85.352 5	8.9534	58.8466					

08/29/90	21:15								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	ም ፐስ 5	RTD 11	RTD 6	RTD 7	RTD 13
83.559	85.307	85.309	85.238	85.028					
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14					
95.887	96.511				DC 24				
						170.450	156.260	159.040	170.440
DC 21	RTD 0			PRESS B					
165.560	83.559	85.309	58.9465	58.8395					
08/29/90	21:30								
00,20,00	22.50								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.517	85.264	85.266	85.195	84.996	84.167			88.760	89.957
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24			DC 23	DC 20
95.909	96.565					170.420			
DC 21	RTD 0	RTD 2			107.510	170.420	130.230	137.100	170.730
165.500	83.517			58.8327					
200.000	03.31,	03.200	30.7377	30.0327					
08/29/90	21:45								
PTD O	DTD 1	D. Clark	Dan 3	DWD /	DMD C	DWD 11	D		
RTD 0	RTD 1	RTD 2	RTD 3						RTD 13
83.484	85.232	85.232	85.163	85.039	84.179		90.021	88.794	89.991
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24		DC 22	DC 23	DC 20
95.941	96.599				169.300	170.370	156.310	159.170	170.720
DC 21	RTD 0	RTD 2							
165.700	83.484	85.232	58.9330	58.8256					
08/29/90	22:00								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.457	85.203	85.205	85.134	85.065	84.161	84.437	90.037	88.819	90.016
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24	DC 25	DC 22	DC 23	DC 20
95.989	96,667					170.360			170 750
		RTD 2	PRESS A	PRESS B	107.100	170.300	130.320	137.340	170.750
165.830									
				55.5255					
08/29/90	22:15								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
83.423	85.171			85.099					90.016
RTD 8	RTD 9	RTD 12		RTD 14	DC 24		DC 22	DC 23	DC 20
96.043	96.710					170.310			
DC 21	RTD 0		PRESS A		109.130	1/0.310	130.400	173.300	1/0./90
165.780	83.423		58.9200						
100.700	JJ.42J	02.1/1	JU. JZUU	JO.OIZZ					

08/29/90	22:30								
RTD 0 83.399 RTD 8 96.084 DC 21 166.050	RTD 1 85.144 RTD 9 96.751 RTD 0 83.399	RTD 2	RTD 3 85.087 RTD 10 125.030 PRESS A 58.9136	85.094 RTD 14 125.210 PRESS B	169.030	84.476 DC 25	90.087 DC 22	88.837 DC 23	90.034
08/29/90		05,135	30.9130	J6.6037					
00/29/90	22.43								
RTD 0 83.370 RTD 8 96.131 DC 21 166.150	RTD 1 85.106 RTD 9 96.810 RTD 0 83.370	RTD 2	RTD 3 85.037 RTD 10 125.030 PRESS A 58.9074	85.130 RTD 14 125.190 PRESS B	84.258 DC 24 169.100	84.535	90.112 DC 22	88.862 DC 23	90.048 DC 20
08/29/90	23:00								
RTD 0 83.350 RTD 8 96.186 DC 21 166.000	RTD 1 85.083 RTD 9 96.841 RTD 0 83.350	RTD 2	RTD 3 85.005 RTD 10 125.030 PRESS A 58.9014	PRESS B	84.301 DC 24 168.990	84.503	90.112 DC 22	RTD 7 88.873 DC 23 159.650	RTD 13 90.059 DC 20 171.170
00 /00 /00	00.15								
08/29/90	23:15								
RTD 0 83.316 RTD 8 96.229 DC 21 166.270	RTD 1 85.063 RTD 9 96.896 RTD 0 83.316	RTD 2	84.994 RTD 10	PRESS B	RTD 5 84.335 DC 24 168.940	RTD 11 84.557 DC 25 170.040	RTD 6 90.157 DC 22 156.970	RTD 7 88.885 DC 23 159.700	RTD 13 90.082 DC 20 171.270
08/29/90	23:30								
RTD 0 83.296 RTD 8 96.260 DC 21 166.370	RTD 1 85.029 RTD 9 96.972 RTD 0 83.296	RTD 2	RTD 10	PRESS B	84.366 DC 24	84.589	DC 22	88.905 DC 23	RTD 13 90.102 DC 20 171.380

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08/29/90 23:45
   RTD 0
          RTD 1
                  RTD 2
                         RTD 3
                                RTD 4
                                        RTD 5 RTD 11
                                                       RTD 6
                                                               RTD 7
                                                                     RTD 13
  83.274 84.997 85.008 84.929 85.196 84.355 84.600 90.177
                                                              88.916
                                                                     90.102
         RTD 9 RTD 12 RTD 10 RTD 14 DC 24
   RTD 8
                                              DC 25
                                                       DC 22
                                                               DC 23
                                                                      DC 20
  96.326 97.015 97.988 124.960 125.100 167.920 169.620 159.340 159.900 171.410
   DC 21
         RTD 0
                 RTD 2 PRESS A PRESS B
 166.220 83.274 85.008 58.8836 58.7745
08/30/90 00:00
   RTD 0
         RTD 1
                RTD 2
                        RTD 3
                               RTD 4
                                       RTD 5 RTD 11
                                                       RTD 6
                                                              RTD 7
                                                                     RTD 13
  83.249 84.981 85.005 84.904 85.235 84.384 84.662 90.218
                                                             88,946
                                                                     90.143
   RTD 8
          RTD 9 RTD 12 RTD 10 RTD 14 DC 24
                                               DC 25
                                                      DC 22
                                                              DC 23
                                                                      DC 20
  96.376 97.042 98.050 124.980 125.080 166.660 168.790 162.120 159.880 171.610
          RTD 0
                RTD 2 PRESS A PRESS B
 166.400 83.249 85.005 58.8780 58.7685
08/30/90 00:15
   RTD 0
          RTD 1
                 RTD 2
                         RTD 3
                                RTD 4
                                        RTD 5 RTD 11
                                                       RTD 6
                                                              RTD 7
                                                                     RTD 13
  83.231 84.954 84.976 84.875 85.271 84.400
                                              84.655
                                                      90.211 88.971
                                                                     90.168
         RTD 9 RTD 12 RTD 10 RTD 14 DC 24
   RTD 8
                                               DC 25
                                                       DC 22
                                                              DC 23
  96.412 97.090 98.108 125.000 125.000 167.320 169.110 160.680 160.030 171.740
   DC 21
         RTD 0 RTD 2 PRESS A PRESS B
 166.640 83.231 84.976 58.8723 58.7626
08/30/90 00:30
   RTD 0
          RTD 1
                 RTD 2
                         RTD 3
                               RTD 4
                                        RTD 5 RTD 11
                                                       RTD 6
                                                              RTD 7
  83.209 84.943 84.953 84.886 85.305 84.421 84.698
                                                      90.254
                                                             88,994 90,180
         RTD 9 RTD 12 RTD 10 RTD 14
  RTD 8
                                      DC 24
                                              DC 25
                                                      DC 22
                                                              DC 23
                                                                     DC 20
  96.455 97.167 98.172 124.970 125.070 168.810 170.310 157.110 160.110 171.720
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 166.560 83.209 84.953 58.8670 58.7572
08/30/90 00:45
  RTD 0
         RTD 1
                RTD 2
                        RTD 3
                               RTD 4
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
 83.200 84.920 84.933 84.875 85.326
                                       84.443
                                              84,709
                                                      90.286 89.005
                                                                    90.202
         RTD 9 RTD 12 RTD 10 RTD 14
  RTD 8
                                      DC 24
                                               DC 25
                                                      DC 22
                                                              DC 23
 96.510 97.210 98.226 124.960 125.010 168.780 170.650 157.280 160.210 171.800
  DC 21
                RTD 2 PRESS A PRESS B
          RTD 0
166.950 83.200 84.933 58.8617 58.7514
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08/30/90	01:00								
RTD 0 83.178 RTD 8 96.576 DC 21 166.850	RTD 1 84.911 RTD 9 97.275 RTD 0 83.178	RTD 2	RTD 3 84.854 RTD 10 124.920 PRESS A 58.8561	PRESS B	84.475 DC 24 168.830	DC 25	RTD 6 90.297 DC 22 157.080	RTD 7 89.037 DC 23 160.240	RTD 13 90.234 DC 20 171.810
08/30/90	01:15								
RTD 0 83.174 RTD 8 96.625 DC 21 166.900	RTD 1 84.906 RTD 9 97.302 RTD 0 83.174	RTD 2	RTD 3 84.839 RTD 10 125.060 PRESS A 58.8509	RTD 14 124.940 PRESS B		DC 25	RTD 6 90.304 DC 22 157.540	RTD 7 89.064 DC 23 160.320	RTD 13 90.262 DC 20 172.000
08/30/90	01:30								
RTD 0 83.147 RTD 8 96.664 DC 21 167.110	RTD 1 84.877 RTD 9 97.350 RTD 0 83.147	RTD 2	RTD 3 84.821 RTD 10 124.980 PRESS A 58.8458	PRESS B			RTD 6 90.340 DC 22 157.400	RTD 7 89.080 DC 23 160.450	RTD 13 90.266 DC 20 172.130
08/30/90	01:45								
RTD 0 83.124 RTD 8 96.718 DC 21 167.190	RTD 1 84.857 RTD 9 97.395 RTD 0 83.124	RTD 2	PRESS A	PRESS B		RTD 11 84.784 DC 25 170.650	RTD 6 90.363 DC 22 157.480	RTD 7 89.103 DC 23 160.430	RTD 13 90.278 DC 20 172.230
08/30/90	02:00								
RTD 0 83.120 RTD 8 96.777 DC 21 167.220	RTD 1 84.841 RTD 9 97.454 RTD 0 83.120	98.495 RTD 2	84.796 RTD 10	85.430 RTD 14 124.860 PRESS B	84.590 DC 24	84.879 DC 25	RTD 6 90.402 DC 22 157.550	89.118 DC 23	RTD 13 90.316 DC 20 172.170

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08/30/90 02:15
                                      RTD 5 RTD 11 RTD 6
                                                           RTD 7 RTD 13
         RTD 1
                RTD 2
                       RTD 3 RTD 4
  RTD 0
 83.120 84.841 84.842 84.796 85.476 84.613 84.845 90.433 89.153 90.350
        RTD 9 RTD 12 RTD 10 RTD 14 DC 24 DC 25
                                                     DC 22 DC 23
  RTD 8
 96.823 97.553 98.570 124.970 124.940 168.610 170.500 157.510 160.620 172.390
                RTD 2 PRESS A PRESS B
  DC 21
        RTD 0
 167.110 83.120 84.842 58.8309 58.7192
08/30/90 02:30
                RTD 2
                       RTD 3
                              RTD 4
                                      RTD 5 RTD 11
                                                     RTD 6
                                                            RTD 7 RTD 13
  RTD 0
         RTD 1
  83.093 84.823 84.835 84.778 85.501 84.627 84.915 90.438 89.178 90.376
        RTD 9 RTD 12 RTD 10 RTD 14 DC 24
                                             DC 25 DC 22 DC 23
                                                                  DC 20
  RTD 8
  96.879 97.556 98.629 124.870 124.840 168.580 170.470 157.840 160.690 172.450
  DC 21
        RTD 0 RTD 2 PRESS A PRESS B
 167.280 83.093 84.835 58.8262 58.7142
08/30/90 02:45
                                       RTD 5 RTD 11
                                                     RTD 6
                                                            RTD 7 RTD 13
                RTD 2
                        RTD 3
                               RTD 4
  RTD 0
         RTD 1
  83.082 84.811 84.813 84.755 85.523 84.660 84.938 90.460 89.200 90.387
                                                           DC 23 DC 20
  RTD 8 RTD 9 RTD 12 RTD 10 RTD 14 DC 24 DC 25 DC 22
  96.925 97.644 98.672 124.860 124.860 168.590 170.480 157.690 160.770 172.450
   DC 21 RTD 0 RTD 2 PRESS A PRESS B
 167.480 83.082 84.813 58.8212 58.7091
08/30/90 03:00
                                      RTD 5 RTD 11
                                                     RTD 6
                                                            RTD 7 RTD 13
         RTD 1
                RTD 2
                       RTD 3
                               RTD 4
   RTD 0
  83.066 84.798 84.797 84.753 85.530 84.688 84.976 90.499 89.227 90.426
        RTD 9 RTD 12 RTD 10 RTD 14 DC 24 DC 25
                                                     DC 22
                                                             DC 23
  RTD 8
  96.975 97.671 98.733 124.740 124.900 168.500 170.440 157.980 160.810 172.530
   DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 167.540 83.066 84.797 58.8165 58.7041
08/30/90 03:15
         RTD 1
                RTD 2
                       RTD 3
                              RTD 4
                                       RTD 5 RTD 11
                                                     RTD 6
                                                             RTD 7 RTD 13
   RTD 0
  83.060 84.791 84.781 84.746 85.566 84.703 84.992 90.515 89.255 90.453
         RTD 9 RTD 12 RTD 10 RTD 14
                                      DC 24
                                             DC 25
                                                    DC 22
                                                             DC 23
   RTD 8
  97.022 97.752 98.780 124.770 124.890 168.490 170.440 157.860 160.880 172.650
                RTD 2 PRESS A PRESS B
   DC 21
         RTD O
 167.690 83.060 84.781 58.8119 58.6991
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08/30/90	03:30								
RTD 0 83.060 RTD 8 97.076 DC 21 167.870	RTD 1 84.779 RTD 9 97.795 RTD 0 83.060	RTD 2	PRESS A	RTD 4 85.587 RTD 14 124.720 PRESS B 58.6942		85.024	DC 22	RTD 7 89.287 DC 23 160.900	RTD 13 90.464 DC 20 172.840
08/30/90	03:45								
RTD 0 83.051 RTD 8 97.120 DC 21 167.830	RTD 1 84.768 RTD 9 97.850 RTD 0 83.051	RTD 2	PRESS A	RTD 4 85.621 RTD 14 124.760 PRESS B 58.6897	RTD 5 84.758 DC 24 168.400	RTD 11 85.024 DC 25 170.390	RTD 6 90.581 DC 22 158.410	RTD 7 89.298 DC 23 160.950	RTD 13 90.496 DC 20 172.790
08/30/90	04:00								
RTD 0 83.040 RTD 8 97.174 DC 21 167.770	RTD 1 84.757 RTD 9 97.893 RTD 0 83.040	RTD 2		PRESS B	RTD 5 84.789 DC 24 168.520	RTD 11 85.046 DC 25 170.400	RTD 6 90.590 DC 22 158.080	RTD 7 89.341 DC 23 161.070	RTD 13 90.519 DC 20 172.820

Time (hh:mm)	Press. (PSIA)	V.P. (PSI)	Temp. (R)	Dewpoint (F)	Mass (LbM)
20:00	58.931	0.5345	551.588	81.630	58683.09
20:15	58.922	0.5353	551.560	81.676	58676.99
20:30	58.915	0.5349	551.546	81.654	58671.04
20:45	58.907	0.5355	551.532	81.687	58664.52
21:00	58.900	0.5359	551.509	81.710	58659.37
21:15	58.893	0.5363	551.500	81.734	58652.84
21:30	58.886	0.5366	551.484	81.751	58647.40
21:45	58.879	0.5368	551.483	81.761	58640.41
22:00	58.873	0.5372	551.475	81.787	58634.07
22:15	58.866	0.5369	551.467	81.767	58628.75
22:30	58.860	0.5378	551.464	81.823	58621.65
22:45	58.853	0.5385	551.461	81.860	58614.88
23:00	58.847	0.5376	551.454	81.809	58610.42
23:15	58.841	0.5385	551.468	81.863	58601.74
23:30	58.835	0.5399	551.462	81.944	58594.87
23:45	58.829	0.5390	551.450	81.892	58591.16
00:00	58.823	0.5385	551.459	81.863	58584.89
00:15	58.817	0.5396	551.454	81.924	58578.46
00:30	58.812	0.5409	551.467	81.998	58570.39
00:45	58.807	0.5429	551.469	82.110	58562.69
01:00	58.801	0.5427	551.47 1	82.098	58557.01
01:15	58.796	0.5436	551.485	82.154	58549.05
01:30	58.790	0.5437	551.479	82.159	58544.54
01:45	58.785	0.5443	551.481	82.191	58538.49
02:00	58.780	0.5443	551.493	82.193	58531.98
02:15	58.775	0.5442	551.514	82.184	58524.89
02:30	58.770	0.5450	551.507	82.232	58519.94
02:45	58.765	0.5453	551.513	82.246	58513.92
03:00	58.760	0.5457	551.518	82.269	58508.16
03:15	58.755	0.5460	551.529	82.285	58501.83
03:30	58.751	0.5473	551.526	82.364	58496.01
03:45	58.746	0.5470	551.535	82.346	58490.69
04:00	58.741	0.5470	551.545	82.343	58484.92

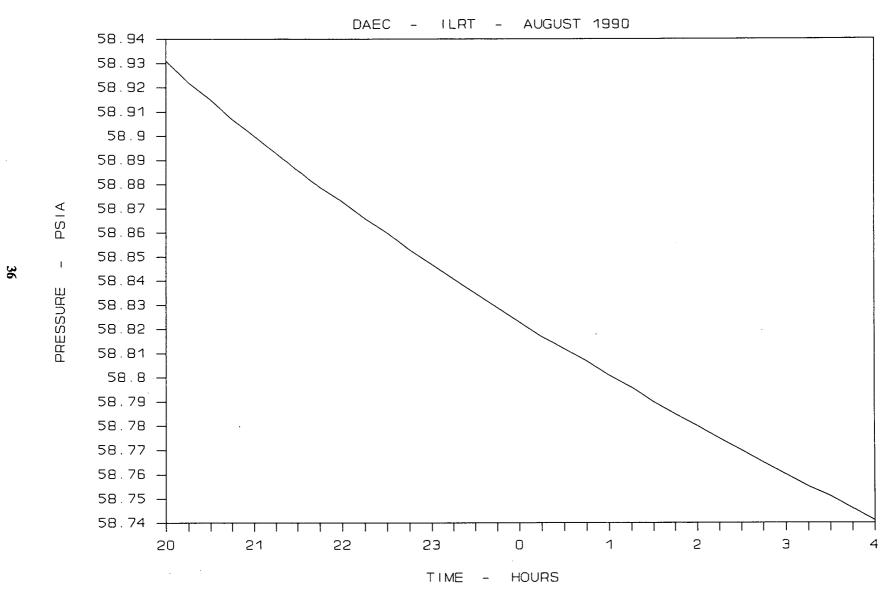
Duane Arnold Energy Center - 1990 ILRT FROM 20:00 HOURS ON 08/29/90 TO 04:00 HOURS ON 08/30/90 ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS

Time (hh:mm)	Mass (LbM)	Leakage (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
20:00	58683.09	0.000000	0.000000	0.000000
20:00	58676.99	0.000000	0.000000	0.000000
20:30	58671.04	0.985807	0.061065	1.046872
20:45	58664.52	1.009100	0.040669	1.049769
21:00	58659.37	0.980252	0.043488	1.023740
21:15	58652.84	0.984573	0.026319	1.010892
21:30	58647.40	0.976062	0.020187	0.996249
21:45	58640.41	0.986439	0.018605	1.005044
22:00	58634.07	0.994665	0.016686	1.011351
22:15	58628.75	0.992084	0.013356	1.005440
22:30	58621.65	0.998344	0.012628	1.010973
22:45	58614.88	1.006187	0.013242	1.019429
23:00	58610.42	1.001803	0.011985	1.013788
23:15	58601.74	1.010985	0.013896	1.024881
23:30	58594.87	1.019783	0.014966	1.034749
23:45	58591.16	1.016553	0.013424	1.029977
00:00	58584.89	1.014522	0.011962	1.026484
00:15	58578.46	1.013757	0.010613	1.024370
00:30	58570.39	1.018020	0.010383	1.028404
00:45	58562.69	1.024590	0.011403	1.035993
01:00	58557.01	1.028203	0.010900	1.039104
01:15	58549.05	1.034177	0.011536	1.045713
01:30	58544.54	1.035499	0.010589	1.046087
01:45	58538.49	1.036065	0.009701	1.045765
02:00	58531.98	1.036773	0.008934	1.045706
02:15	58524.89	1.038366	0.008381	1.046747
02:30	58519.94	1.037822	0.007765	1.045587
02:45	58513.92	1.036992	0.007245	1.044238
03:00	58508.16	1.035675	0.006860	1.042534
03:15	58501.83	1.034598	0.006481	1.041079
03:30	58496.01	1.033218	0.006205	1.039423
03:45	58490.69	1.031157	0.006152	1.037309
04:00	58484.92	1.028984	0.006153	1.035137

Duane Arnold Energy Center - 1990 ILRT FROM 20:00 HOURS ON 08/29/90 TO 04:00 HOURS ON 08/30/90 ABSOLUTE TEST METHOD, TOTAL TIME ANALYSIS TEST RESULTS

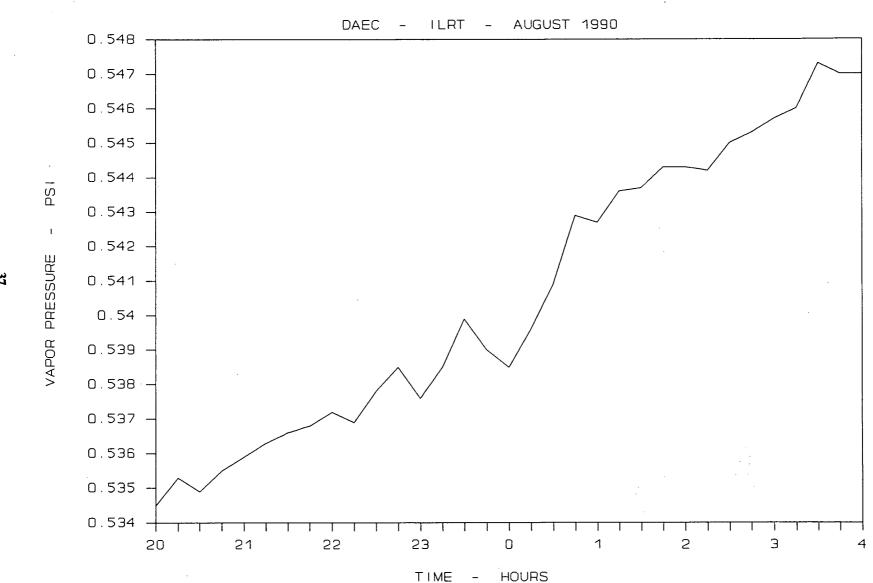
Time (hh:mm)	Mass (LbM)	Meas.Leak. (PCT./DAY)	Calc.Leak. (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
20:00	58683.09	0.000000	0.000000	0.000000	0.000000
20:15	58676.99	0.998169	0.000000	0.000000	0.000000
20:30	58671.04	0.985807	0.000000	0.000000	0.000000
20:45	58664.52	1.013063	1.006460	0.156687	1.163147
21:00	58659.37	0.970186	0.983302	0.102617	1.085919
21:15	58652.84	0.989788	0.984926	0.066917	1.051844
21:30	58647.40	0.973277	0.977282	0.051315	1.028597
21:45	58640.41	0.997548	0.984313	0.048832	1.033145
22:00	58634.07	1.002504	0.990847	0.045614	1.036461
22:15	58628.75	0.987843	0.989633	0.040394	1.030027
22:30	58621.65	1.005140	0.994781	0.038404	1.033185
22:45	58614.88	1.014529	1.001436	0.037757	1.039192
23:00	58610.42	0.990761	0.999287	0.035915	1.035202
23:15	58601.74	1.023764	1.006702	0.036770	1.043472
23:30	58594.87	1.030941	1.014218	0.037218	1.051436
23:45	58591.16	1.002632	1.013216	0.036163	1.049379
00:00	58584.89	1.004094	1.012698	0.034965	1.047663
00:15	58578.46	1.006923	1.012845	0.033650	1.046495
00:30	58570.39	1.024241	1.016472	0.032655	1.049127
00:45	58562.69	1.036682	1.021857	0.032731	1.054588
01:00	58557.01	1.031265	1.025306	0.031757	1.057062
01:15	58549.05	1.044221	1.030468	0.031688	1.062156
01:30	58544.54	1.030276	1.032437	0.030707	1.063144
01:45	58538.49	1.028539	1.033794	0.029920	1.063715
02:00	58531.98	1.030061	1.035160	0.029192	1.064351
02:15	58524.89	1.035189	1.037077	0.028422	1.065499
02:30	58519.94	1.026538	1.037453	0.028200	1.065653
02:45	58513.92	1.024977	1.037528	0.028148	1.065676
03:00	58508.16	1.022048	1.037166	0.028364	1.065530
03:15	58501.83	1.022491	1.036875	0.028476	1.065351
03:30	58496.01	1.020141	1.036291	0.028756	1.065047
03:45	58490.69	1.015314	1.035153	0.029426	1.064578
04:00	58484.92	1.013087	1.033847	0.030133	1.063981

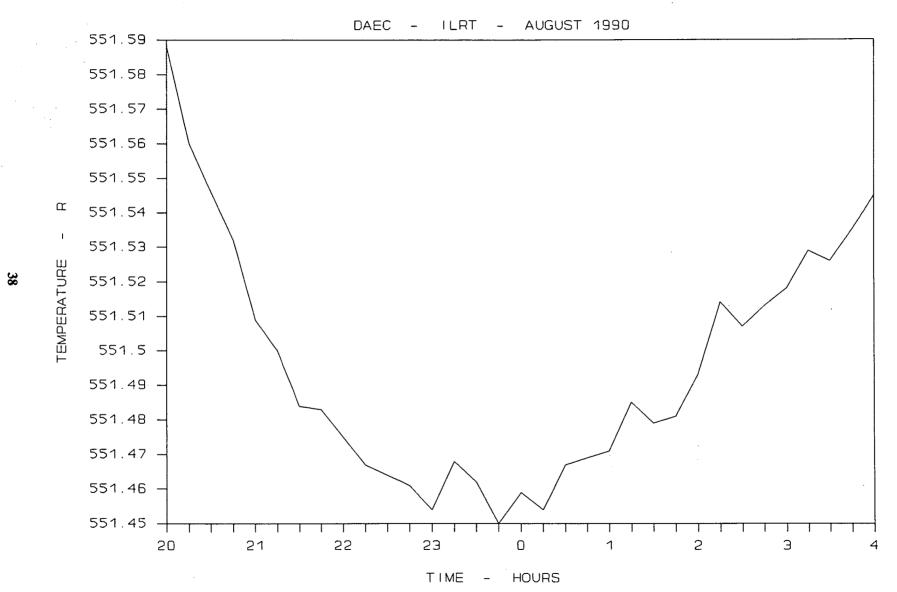
CONTAINMENT PRESSURE VS. TIME



ATTACHMENT 3.3E GRAPH 1

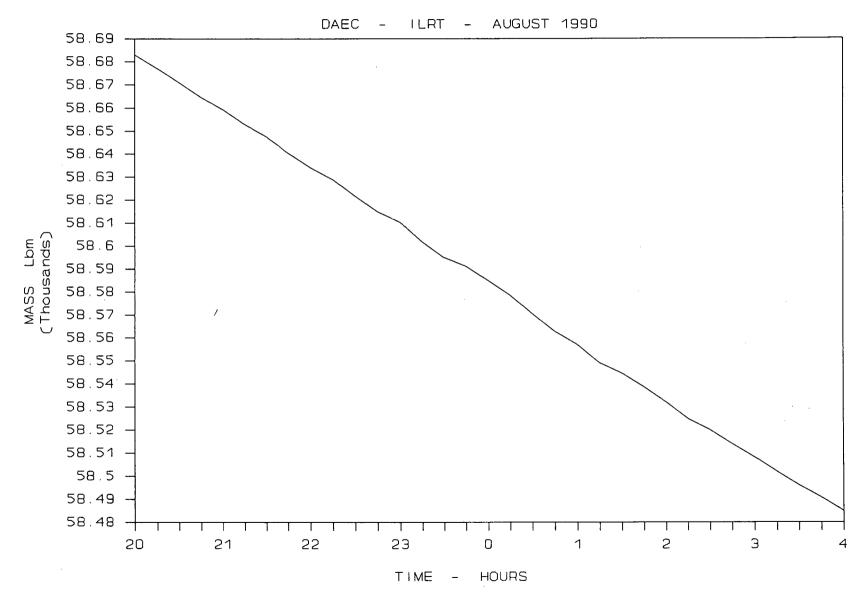






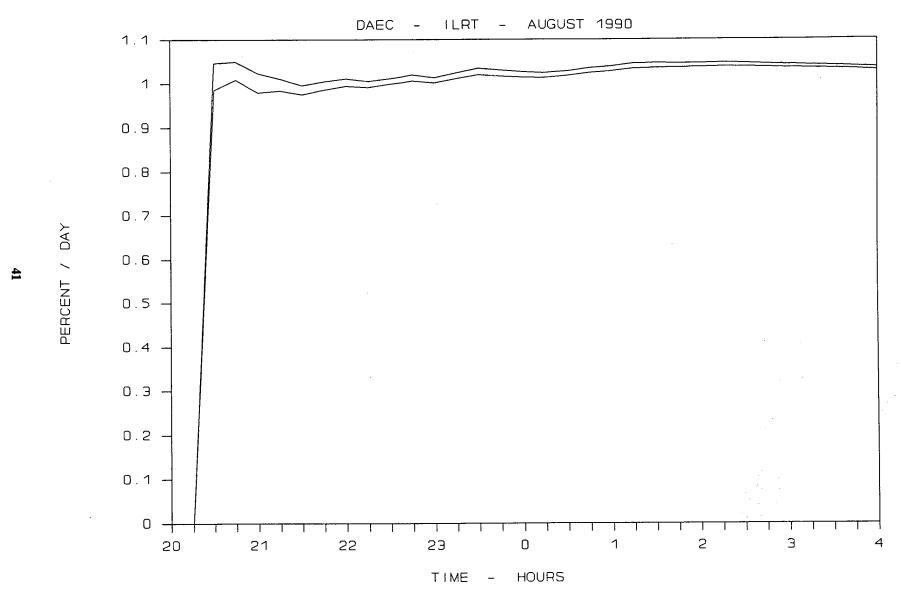
ATTACHMENT 3.3G GRAPH 3

CONTAINMENT MASS VS. TIME



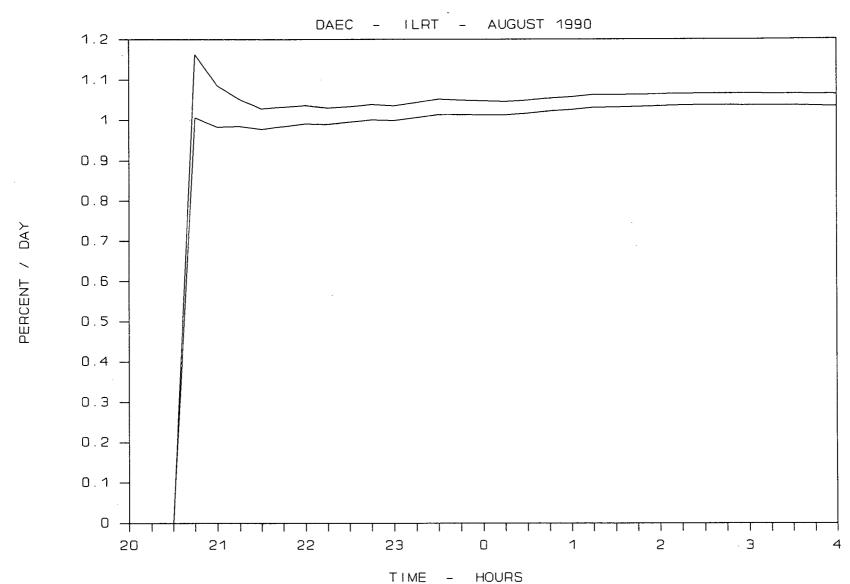
ATTACHMENT 3.3I

GRAPH 5



GRAPH 6





Dnane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 VERIFICATION TEST MEASURED INPUT DATA

```
08/30/90 05:15
                       RTD 3
                                      RTD 5 RTD 11
                                                     RTD 6
                                                             RTD 7 RTD 13
  RTD 0
         RTD 1
                RTD 2
                              RTD 4
 82.975 84.693 84.693 84.649 85.762 84.887 85.164
                                                     90.698 89.439 90.617
        RTD 9 RTD 12 RTD 10 RTD 14 DC 24
                                             DC 25 DC 22 DC 23 DC 20
  RTD 8
 97.412 98.141 99.215 124.400 124.590 168.380 170.220 158.390 161.330 173.300
                RTD 2 PRESS A PRESS B
  DC 21
         RTD 0
 168.080 82.975 84.693 58.7308 58.6159
08/30/90 05:30
                       RTD 3
                              RTD 4
                                      RTD 5 RTD 11
                                                      RTD 6
                                                             RTD 7 RTD 13
  RTD 0
        RTD 1
                RTD 2
  82.964 84.682 84.684 84.638 85.784 84.909 85.218 90.710 89.473 90.649
                                      DC 24
                                             DC 25 DC 22
                                                             DC 23
         RTD 9 RTD 12 RTD 10 RTD 14
  RTD 8
 97.466 98.218 99.290 124.280 124.580 168.360 170.190 158.510 161.390 173.390
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.320 82.964 84.684 58.7158 58.6006
08/30/90 05:45
                                       RTD 5 RTD 11
                                                      RTD 6
                                                             RTD 7 RTD 13
  RTD 0
         RTD 1
                 RTD 2
                       RTD 3
                               RTD 4
  82.953 84.660 84.672 84.627 85.816 84.941 85.230 90.744 89.484
         RTD 9 RTD 12 RTD 10 RTD 14
                                      DC 24
                                                     DC 22
                                                             DC 23
                                             DC 25
  RTD 8
  97.512 98.261 99.324 124.390 124.580 168.360 170.160 158.480 161.390 173.440
                RTD 2 PRESS A PRESS B
  DC 21
         RTD 0
 168.230 82.953 84.672 58.7005 58.5852
08/30/90 06:00
                                                      RTD 6
                                                             RTD 7 RTD 13
                RTD 2
                       RTD 3
                               RTD 4
                                       RTD 5 RTD 11
  RTD 0
         RTD 1
  82.944 84.660 84.672 84.616 85.839 84.963 85.273 90.787 89.527
                                                                   90.692
         RTD 9 RTD 12 RTD 10 RTD 14 DC 24
                                             DC 25
                                                      DC 22
                                                             DC 23
  RTD 8
  97.566 98.284 99.387 124.410 124.640 168.360 170.150 158.460 161.470 173.390
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.260 82.944 84.672 58.6857 58.5699
08/30/90 06:15
                                       RTD 5 RTD 11
                                                             RTD 7 RTD 13
         RTD 1
                RTD 2
                        RTD 3
                               RTD 4
                                                      RTD 6
  RTD 0
  82.944 84.650 84.650 84.616 85.848 84.984 85.273 90.775 89.527
                                                                   90.703
  RTD 8
         RTD 9 RTD 12 RTD 10 RTD 14
                                      DC 24
                                              DC 25
                                                      DC 22
                                                             DC 23
  97.609 98.347 99.441 124.410 124.610 168.370 170.140 158.500 161.490 173.580
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.330 82.944 84.650 58.6707 58.5547
```

Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 VERIFICATION TEST MEASURED INPUT DATA

```
08/30/90 06:30
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
                 RTD 2
                        RTD 3
                                RTD 4
  RTD 0
         RTD 1
 82.939 84.646 84.645 84.600 85.900 85.013 85.345 90.825 89.577
                                                                    90.742
                                      DC 24 DC 25 DC 22 DC 23
                                                                     DC 20
         RTD 9
                RTD 12 RTD 10 RTD 14
  RTD 8
                99.502 124.380 124.690 168.350 170.140 158.670 161.520 173.530
 97.659 98.399
                RTD 2 PRESS A PRESS B
  DC 21
         RTD 0
168.390 82.939 84.645 58.6560 58.5395
08/30/90 06:45
                               RTD 4
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
  RTD 0
         RTD 1
                 RTD 2
                        RTD 3
 82.921 84.628 84.629 84.595 85.903 85.029 85.350 90.884 89.570 90.758
                                                      DC 22
                                                              DC 23
                                      DC 24
                                              DC 25
         RTD 9 RTD 12 RTD 10 RTD 14
  RTD 8
 97.707 98.446 99.561 124.410 124.680 168.310 170.100 158.860 161.570 173.670
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.530 82.921 84.629 58.6410 58.5244
08/30/90 07:00
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
                 RTD 2
                        RTD 3
                               RTD 4
  RTD 0
         RTD 1
                                                     90.873 89.625
                                                                    90.781
  82.910 84.628 84.629 84.584 85.937 85.061 85.350
         RTD 9 RTD 12 RTD 10 RTD 14
                                                      DC 22
                                       DC 24
                                              DC 25
                                                             DC 23
  RTD 8
  97.761 98.501 99.604 124.470 124.720 168.280 170.080 158.870 161.710 173.600
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.590 82.910 84.629 58.6262 58.5093
08/30/90 07:15
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
                               RTD 4
  RTD 0
         RTD 1
                 RTD 2
                         RTD 3
  82.890 84.628 84.606 84.573 85.957 85.072 85.393 90.895 89.636 90.813
         RTD 9 RTD 12 RTD 10 RTD 14
                                      DC 24
                                               DC 25
                                                      DC 22
                                                              DC 23
  RTD 8
  97.804 98.564 99.650 124.410 124.610 168.260 170.110 158.890 161.720 173.570
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.630 82.890 84.606 58.6112 58.4941
08/30/90 07:30
                                                              RTD 7 RTD 13
   RTD 0
         RTD 1
                 RTD 2
                         RTD 3
                                RTD 4
                                        RTD 5 RTD 11
                                                      RTD 6
  82.899 84.605 84.606 84.562 85.991 85.115 85.393 90.938 89.668 90.836
         RTD 9 RTD 12 RTD 10 RTD 14
                                        DC 24
                                               DC 25
                                                      DC 22
                                                              DC 23
   RTD 8
  97.847 98.598 99.713 124.350 124.580 168.280 170.100 158.890 161.810 173.740
                RTD 2 PRESS A PRESS B
         RTD 0
   DC 21
        82.899 84.606 58.5961 58.4788
 168.660
```

Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 VERIFICATION TEST MEASURED INPUT DATA

```
08/30/90 07:45
                                                              RTD 7 RTD 13
  RTD 0
         RTD 1
                RTD 2
                        RTD 3
                               RTD 4
                                       RTD 5 RTD 11
                                                      RTD 6
                                                     90.959 89.691 90.856
 82.879 84.596 84.595 84.550 86.012 85.126 85.447
                                      DC 24 DC 25 DC 22 DC 23 DC 20
         RTD 9 RTD 12 RTD 10 RTD 14
  RTD 8
 97.890 98.652 99.778 124.450 124.650 168.250 170.020 158.860 161.770 173.810
         RTD 0
                RTD 2 PRESS A PRESS B
  DC 21
 168.780 82.879 84.595 58.5811 58.4634
08/30/90 08:00
                RTD 2
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
  RTD 0
         RTD 1
                       RTD 3
                               RTD 4
 82.857 84.596 84.584 84.541 86.023 85.147 85.479 90.993 89.711 90.879
         RTD 9 RTD 12 RTD 10 RTD 14 DC 24
                                               DC 25
                                                      DC 22
                                                             DC 23
  RTD 8
 97.924 98.718 99.821 124.480 124.590 168.270 169.970 159.110 161.840 173.920
                RTD 2 PRESS A PRESS B
  DC 21
         RTD 0
 168.840 82.857 84.584 58.5661 58.4480
08/30/90 08:15
                                                      RTD 6
                                                              RTD 7 RTD 13
  RTD 0
          RTD 1
                 RTD 2
                        RTD 3
                                RTD 4
                                       RTD 5 RTD 11
 82.846 84.573 84.563 84.530 86.046 85.169 85.470 90.993 89.723
                                                                    90.899
         RTD 9 RTD 12 RTD 10 RTD 14
                                       DC 24 DC 25
                                                     DC 22
                                                             DC 23
  RTD 8
         98.749 99.876 124.470 124.560 168.260 170.020 159.090 161.820 173.860
 97.979
  DC 21
         RTD 0
                RTD 2 PRESS A PRESS B
 168.840 82.846 84.563 58.5508 58.4325
08/30/90 08:30
  RTD 0
          RTD 1
                RTD 2
                         RTD 3
                                RTD 4
                                       RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
  82.843 84.569 84.548 84.525 86.062 85.197 85.465 91.011 89.761
                                                                    90.918
                                      DC 24
                                              DC 25
                                                      DC 22
                                                              DC 23
  RTD 8
          RTD 9 RTD 12 RTD 10 RTD 14
  98.029 98.788 99.937 124.470 124.690 168.220 170.020 159.090 161.870 174.040
          RTD 0
   DC 21
                RTD 2 PRESS A PRESS B
 169.020
        82.843 84.548 58.5358 58.4175
08/30/90 08:45
          RTD 1
                RTD 2
                        RTD 3
                                RTD 4
                                        RTD 5 RTD 11
                                                      RTD 6
                                                              RTD 7 RTD 13
   RTD 0
  82.832 84.546 84.536 84.503 86.084 85.208 85.519
                                                     91.020 89.772 90.929
          RTD 9 RTD 12 RTD 10 RTD 14
                                       DC 24
                                               DC 25
                                                      DC 22
                                                              DC 23
  RTD 8
  98.072 98.831 99.991 124.560 124.650 168.300 170.020 158.860 161.920 174.020
                RTD 2 PRESS A PRESS B
   DC 21
          RTD 0
 168.880 82.832 84.536 58.5210 58.4022
```

Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 VERIFICATION TEST MEASURED INPUT DATA

08/30/90	09:00								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
82.821	84.546	84.516	84.494	86.107	85.242	85.551	91.054	89.807	90.961
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24	DC 25	DC 22	DC 23	DC 20
98.115	98.896	100.060	124.500	124.680	168.180	169.980	159.160	161.970	174.180
DC 21	RTD 0	RTD 2	PRESS A	PRESS B					
168.050	82.821	84.516	58.5061	58.3869					
•				•					
08/30/90	09:15								
RTD 0	RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 11	RTD 6	RTD 7	RTD 13
82.810	84.537	84.516	84.494	86.139	85.262	85.583	91.074	89.816	90.984
RTD 8	RTD 9	RTD 12	RTD 10	RTD 14	DC 24	DC 25	DC 22	DC 23	DC 20
98.169	98.951	100.100	124.590	124.660	168.160	170.010	159.300	162.070	174.240
DC 21	RTD 0	RTD 2	PRESS A	PRESS B					
169.050	82.810	84.516	58.4912	58.3717					

Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 VERIFICATION TEST REDUCED INPUT VARIABLES

Time (hh:mm)	Press. (PSIA)	V.P. (PSI)	Temp. (R)	Dewpoint (F)	Mass (LbM)
					50/1/ 07
05:15	58.673	0.5482	551.555	82.415	58414.27
05:30	58.658	0.5489	551.560	82.452	58397.87
05:45	58.643	0.5487	551.572	82.441	58381.38
06:00	58.628	0.5488	551.589	82.443	58364.39
06:15	58.613	0.5492	551.592	82.471	58348.39
06:30	58.598	0.5495	551.611	82.487	58331.00
06:45	58,583	0.5501	551.617	82.521	58314.65
07:00	58.568	0.5502	551.634	82.527	58297.79
07:15	58.553	0.5503	551.631	82.532	58282.82
07:30	58.537	0.5508	551.638	82.559	58266.29
07:45	58.522	0.5507	551.655	82.552	58249.39
08:00	58.507	0.5514	551.661	82.591	58232.75
08:15	58.492	0.5513	551.661	82.589	58217.33
08:30	58.477	0.5519	551.678	82.618	58199.98
08:45	58.462	0.5515	551.683	82.599	58184.61
09:00	58.447	0.5507	551.694	82.550	58169.21
09:15	58.431	0.5527	551.708	82.664	58150.55

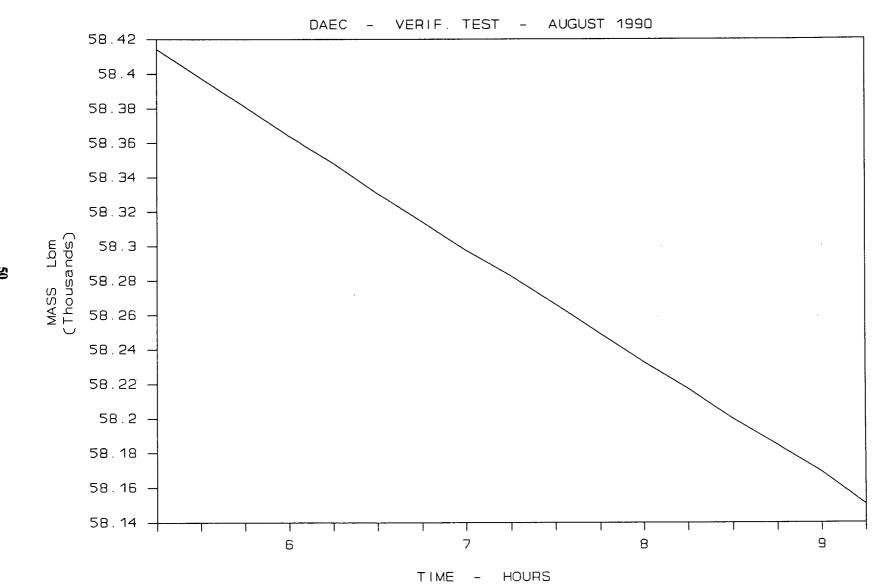
Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS VERIFICATION TEST

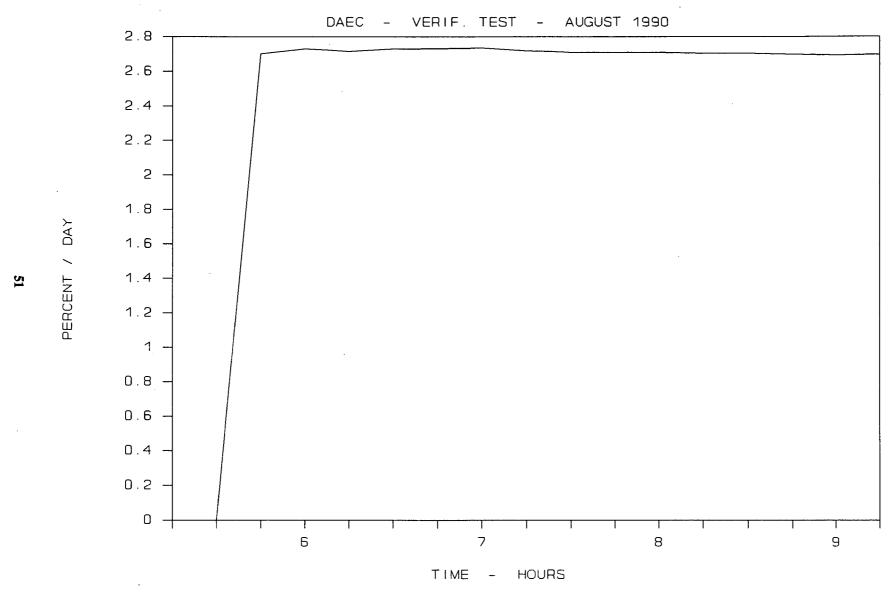
Time (hh:mm)	Mass (LbM)	Leakage (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
05:15	58414.27	0.00000	0.000000	0.000000
05:30	58397.87	0.000000	0.000000	0.000000
05:45	58381.38	2.702877	0.036900	2.739776
06:00	58364.39	2.730037	0.046493	2.776530
06:15	58348.39	2.715376	0.029306	2.744683
06:30	58331.00	2,731532	0.026409	2.757941
06:45	58314.65	2.732591	0.017693	2.750284
07:00	58297.79	2.736188	0.013343	2.749531
07:15	58282.82	2.719476	0.020884	2.740361
07:30	58266.29	2.710816	0.018814	2.729630
07:45	58249.39	2.709147	0.015246	2.724393
08:00	58232.75	2.709163	0.012543	2.721706
08:15	58217.33	2.703426	0.012074	2.715500
08:30	58199.98	2.704010	0.010279	2.714289
08:45	58184.61	2.699963	0.009768	2.709730
09:00	58169.21	2.693531	0.010727	2.704257
09:15	58150.55	2.696423	0.009861	2.706284

Duane Arnold Energy Center - 1990 ILRT FROM 05:15 HOURS TO 09:15 HOURS ON 08/30/90 ABSOLUTE TEST METHOD, TOTAL TIME ANALYSIS TEST RESULTS VERIFICATION TEST

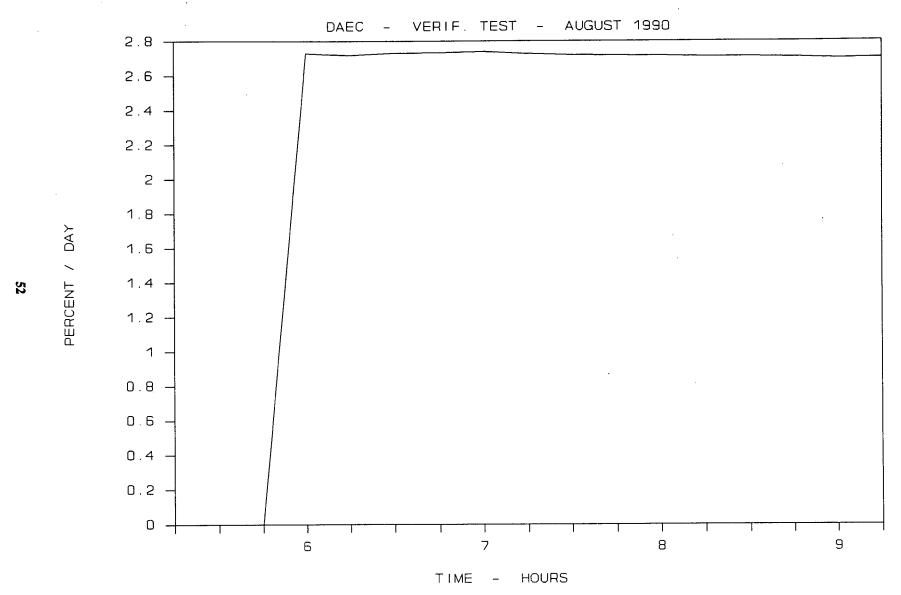
Time (hh:mm)	Mass (LbM)	Meas.Leak. (PCT./DAY)	Calc.Leak. (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
			0.00000	0.00000	0.00000
05:15	58414.27	0.000000	0.000000	0.000000	0.000000
05:30	58397.87	2.695407	0.000000	0.000000	0.000000
05:45	58381.38	2.702877	0.000000	0.000000	0.000000
06:00	58364.39	2.732231	2.728584	0.086548	2.815132
06:15	58348.39	2.706562	2.718692	0.084802	2.803494
06:30	58331.00	2.736818	2.732080	0.056009	2.788089
06:45	58314.65	2.728607	2.734380	0.044456	2.778836
07:00	58297.79	2.734591	2.738184	0.037002	2.775186
07:15	58282.82	2.700287	2.726010	0.050931	2.776941
07:30	58266.29	2.702107	2.718551	0.050022	2.768573
07:45	58249. 39	2.709701	2.715994	0.045735	2.761729
08:00	58232.75	2.711967	2.714875	0.042008	2.756883
08:15	58217.33	2.697190	2.709692	0.040707	2.750399
08:30	58199.98	2.708964	2.709030	0.038051	2.747081
08:45	58184.61	2.695944	2.705190	0.036611	2.741801
09:00	58169.21	2.684940	2.699541	0.036428	2.735969
09:15	58150.55	2.708796	2.700510	0.035173	2.735684







ATTACHMENT 3.3R GRAPH 9



SECTION 4

4.0 LOCAL LEAKAGE RATE TESTS (TYPES B AND C)

Section 4 summarizes the results of the Local Leakage Rate Test's (LLRT's) data which has been obtained from periodic testing performed since the December 1988 Periodic Type A test. Maintenance data is provided for surveillance testing performed in 1990. Each penetration's leakage rate can be obtained from site reference material.

Attachment 4B contains an analysis of the containment penetrations that were repaired during the 1990 Refueling Outage to assess the as found containment condition.

The acceptance criteria for Types B and C testing are in accordance with 10CFR50, Appendix J. The combined as left leakage rate for all penetrations and valves, subject to Types B and C tests in 1990, were well below the acceptance criteria of less than $0.60L_a$.

The data contained in this section are summarized below:

Attachment No.	Title
4A	1990 Local Leakage Rate Test Data
4B	1990 Local Leakage Rate Test Summary Analysis.

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
	Testable Gaskets (Type B)					
X-1	Drywell Personnel Airlock	В	Airlock	4046/03-14-89 5545/10-21-89 5114/11-14-89 5932/11-19-89 5696/11-22-89 5700/11-28-89	4046/03-14-89 5545/10-21-89 5114/11-14/89 5932/11-19-89 5696/11-22-89 5700/11-28-89	
X-1	Drywell Airlock Hatch	В	Gaskets	0/06-29-90	0/08-17-90	Replaced O-Rings.
X-2	Equipment Access Hatch	В	Gaskets	0/06-29-90	0/08-25-90	Replaced O-Rings.
X-4	Drywell Head Access Hatch	В	Gaskets	0/07-06-90	0/07-19-90	Replaced O-Rings.
X-6	CRD Removal Hatch	В.	Gaskets	0/06-28-90	0/08-27-90	Replaced O-Rings.
X-35A	TIP Drive	В	Gaskets	85/07-11-90	85/07-11-90	
X-35B	TIP Drive	В	Gaskets	85/07-11-90	85/07-11-90	
X-35C	TIP Drive	В	Gaskets	0/07-11-90	0/07-11-90	
X-35D	TIP Purge Line	В	Gaskets	70/07-11-90	70/07-11-90	
X-53	Spare	В	Gaskets	0/06-24-90	0/06-24-90	
	Drywell Head	В	Gaskets	4920/06-29-90	0/08-23-90	Gaskets replaced, O.C. review.
X-58A	Stabilizer Access Port	В	Gaskets	240/07-09-90	0/08-22-90	Replaced O-Rings.
X-58B	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-58C	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
X-58D	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
X-58E	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
X-58F	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
X-58G	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
X-58H	Stabilizer Access Port	В	Gaskets	0/07-09-90	0/08-22-90	Replaced O-Rings.
N-200A	Torus Access Hatch - South	В	Gaskets	0/06-24-90	0/09-01-90	Replaced O-Rings.
N-200B	Torus Access Hatch - North	В	Gaskets	0/06-24-90	0/08-18-90	Replaced O-Rings
	Electrical Canisters (Type B)					
X-100B	Neutron Monitoring	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-100C	Neutron Monitoring	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-100E	Neutron Monitoring	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-100F	Neutron Monitoring	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-100G	RPV Vibration Monitoring	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-101A	Recirc. Pump Power	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-101C	Recirc. Pump Power	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-103	Thermocouple	В	Electrical Pen.	0/06-27-90	0/06-27-90	

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-104A	CRD Rod Position Indication	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-104B	CRD Rod Position Indication	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-104C	CRD Rod Position Indication	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-104D	CRD Rod Position Indication	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-105B	Power & Control	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-105D	Power & Control	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-106A	Power & Control	В	Electrical Pen.	0/06-27-90	0/06-27-90	
X-106C	Power & Control	В	Electrical Pen.	0/06-27-90	0/06-27-90	
N-230B	Vacuum Breaker Cables	В	Electrical Pen.	0/06-27-90	0/06-27-90	
	Flange O-Rings (Type B)					
X-25	Drywell Purge Outlet	В	CV-4302	- 0/06-28-90	0/11-23-89 0/07-19-90	Replaced O-Rings. Replaced O-Rings.
X-26	Drywell Purge Outlet	В	CV-4307	0/06-28-90	0/08-14-90	Replaced O-Rings.
N-220	Torus Purge Supply	В	CV-4308	0/06-28-90	0/08-14-90	Replaced O-Rings.
N-205	Torus Purge Outlet	В	CV-4300	0/06-26-90	0/08-21-90	Replaced O-Rings.
N-213A	Torus Drain Line Flange - South	В	Flange	0/06-26-90	0/06-26-90	

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
N-213B	Torus Drain Line Flange - North	В	Flange	0/06-25-90	0/06-25-90	
N-231	RB/Torus Vacuum Breaker	В	CV-4304	0/06-26-90	0/08-14-90	Replaced O-Rings.
N-231	RB/Torus Vacuum Breaker	В	CV-4305	0/06-26-90	0/08-14-90	Replaced O-Rings.
·	Expansion Bellows (Type B)					
X-7A	Steam to Turbine	В	Bellows	0/07-06-90	0/07-06-90	
X-7B	Steam to Turbine	В	Bellows	0/07-06-90	0/07-06-90	
X-7C	Steam to Turbine	В	Bellows	0/07-06-90	0/07-06-90	
X-7D	Steam to Turbine	В	Bellows	0/07-06-90	0/07-06-90	
X-9A	RPV Feedwater	В	Bellows	0/07-09-90	0/07-09-90	
X-9B	RPV Feedwater	В	Bellows	0/07-09-90	0/07-09-90	
X-10	Steam to RCIC Turbine	В	Bellows	290/07-09-90	290/07-09-90	
X-11	Steam to HPCI Turbine	В	Bellows	0/07-09-90	0/07-09-90	
X-12	Shutdown Pump Supply RHF	R В	Bellows	0/06-27-90	0/06-27-90	
X-13A	RHR Pump Discharge	В	Bellows	0/06-27-90	0/06-27-90	
X-13B	RHR Pump Discharge	В	Bellows	0/06-27-90	0/06-27-90	
X-15	RWCU Supply	В	Bellows	0/07-10-90	0/07-10-90	
X-16A	Core Spray Pump Discharge	В	Bellows	0/07-09-90	0/07-09-90	

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As fouud leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-16B	Core Spray Pump Discharge	В	Bellows	0/07-09-90	0/07-09-90	
X-17	RPV Head Spray	В	Bellows	0/07-09-90	0/07-09-90	
N-201A	Vent Line	В	Bellows	0/06-28-90	0/06-28-90	
N-201B	Vent Line	В	Bellows	0/06-28-90	0/06-28-90	
N-201C	Vent Line	В	Bellows	0/06-28-90	0/06-28-90	
N-201D	Vent Line	В	Bellows	0/06-28-90	0/06-28-90	
N-201E	Vent Line	В	Bellows	0/06-27-88	0/06-27-88	
N-201F	Vent Line	В	Bellows	0/06-27-90	0/06-27-90	
N-201G	Vent Line	В	Bellows	0/06-27-90	0/06-27-90	
N-201H	Vent Line	В	Bellows	0/06-27-90	0/06-27-90	
N-213A	Torus Drain Line Bellows - Inboard (South)	В	Bellows	0/07-12-90	0/07-12-90	
N-213A	Torus Drain Line Bellows - Outboard (South)	В	Bellows	0/07-12-90	0/07-12-90	
N-213B	Torus Drain Line Bellows - Inboard (North)	В	Bellows	0/06-29-90	0/06-29-90	
N-213B	Torus Drain Line Bellows - Outboard (North)	В	Bellows	0/06-29-90	0/06-29-90	

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
	Valve Bonnets (Type B)					
X-39A	Drywell Spray	В	MO-2000	0/07-02-90	0/07-02-90	
X-39B	Drywell Spray	В	MO-1902	615/07-14-90	615/07-14-90	
N-211A	Torus Spray	В	MO-1933	615/07-14-90	615/07-14-90	
N-211B	Torus Spray	В	MO-2006	20/07-03-90	20/07-03-90	
X-26	Shaft Stem Seals (Type B)	В	CV-4307	7,300/07-02-90	0/08-16-90	Replaced O-Rings,
A-20	Drywell Purge Supply	Ь	CV-4307	7,300/07-02-90	0/06-10-90	repaired galled shaft and replaced shaft.
N-220	Torus Purge Supply	В	CV-4308	4,500/07-02-90	0/08-16-90	Replaced O-Rings

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
	Local Leakage Rate Tests	(Type C)				
X-7A	"A" Main Steam Line	С	CV-4412(IPC) CV-4413(OPC)	2,500/09-15-89 (Combined)	2,500/09-15-89 (Combined)	
X-7A	"A" Main Steam Line	С	CV-4412(IPC)	15,750/06-30-90	175/08-25-90	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.
			CV-4413(OPC)	(Combined)	(Combined)	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-7B	"B" Main Steam Line	С	CV-4415(IPC)	4,425/09-16-89 470/09-25-69Reworked valve disc seat and main seat.		
			CV-4416(OPC) CV-4416(OPC)	(Combined) >82,000/09-16-89	(Combined) 590/09-22-89	Replaced stem. Replaced disc & piston with oversized internals, replaced stem.
X-7B	"B" Main Steam Line	С	CV-4415(IPC)	2,375/06-30-90	275/08-25-90	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.
			CV-4416(OPC)	(Combined)	(Combined)	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-7C	"C" Main Steam Line	С	CV-4418(IPC)	2,000/09-16-89	2000/09-16-89	
			CV-4419(OPC)	12,000/09-16-89	1,600/09-22-89	Reworked disc & valve seat.
X-7C	"C" Main Steam Line	C	CV-4418(IPC)	1,450/06-29-90	320/08-25-90	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.
			CV-4419(OPC)	(Combined)	(Combined)	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-7D	"D" Main Steam Line	С	CV-4420(IPC)	2,975/09-16-89	2,975/09-16-89	
			CV-4421 (OPC)	1,725/09-16-89	1,725/09-16-89	
X-7D	"D" Main Steam Line	С	CV-4420(IPC)	2,225/06-29-90	380/08-25-90	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.
			CV-4421(OPC)	(Combined)	(Combined)	Internals replaced/oversized, machined seat ring, replaced operator assembly with a unit utilizing larger springs, guide tube and cylinder. All MSIVs were modified under DCP-1476.

Pen No.	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-8	Steam Drain	С	MO-4423(IPC)	0/07-01-90	0/08-25-90	Replaced body to bonnet gasket.
			MO-4424(OPC)	- 2,200/07-01-90	1,880/03-13-89 0/08-11-90	Repacked. Repacked with live load and short box conversion, Overhauled operator.
X-9A	Feedwater	С	V-14-3(IPC)	87,750/07-02-90	9,300/08-16-90	Removed soft seat under DCP-1504. Verified disc to seat ring fit-up. Repacked.
			MO-4441(OPC)	950/07-02-90	2,700/08-25-90	Repacked with live load and short box conversion, overhaul operator.
			MO-2312(OPC)	(Combined)	(Combined)	Replaced stem and disc, machined seat rings, overhaul operator.

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-9B	Feedwater	С	V-14-1(IPC)	7,150/07-06-90	8,050/08-10-90	Removed soft seat under DCP-1504, verified disc to ring fit-up, repacked.
			MO-4442(OPC) MO-2740(OPC) MO-2512(OPC)	950/07-07-90 (Combined) (Combined)	950/08-02-90 (Combined) (combined)	Overhaul operator. Replaced torque switch.
X-10	RCIC Condensate Return	С	CV-2410(IPC)	375/07-03-90	0/08-18-90	Replaced valve per DCP-1461.
			CV-2411(OPC)	425/07-03-90	0/08-18-90	Replaced valve per DCP-1461.
X-10	RCIC Steam	С	MO-2400(IPC) CV-2401(OPC)	500/06-30-90 1,100/06-30-90	500/08-25-90 450/08-25-90	Repacked with live load and short box configuration.
X-11	HPCI Condensate Return	С	CV-2211(IPC)	3,450/07-03-90	350/10-06-89 0/08-14-90	Packing tightened. Replaced valve per DCP-1461.
			CV-2212(OPC)	3,450/07-03-90	350/10-06-89 0/08-14-90	Packing tightened. Replaced valve per DCP-1461.

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-11	HPCI Steam	С	MO-2238(IPC)	- 700/06-30-90	300/03-13-89 1,300/08-25-90	Packing tightened. Installed spring Pack-Live load.
			MO-2239(OPC)	- 140/06-30-90	74/03-13-89 450/08-28-90	Repacked. Repacked stem, replaced packing follower with short box and live load configuration, overhauled operator.
X-15	Reactor Water Cleanup	С	MO-2700(IPC)	0/07-05-90	0/08-02-90	Overhauled operator.
			MO-2701 (OPC)	0/07-05-90	40/08-02-90	Repacked with short box and live load configuration.
X-16A	Core Spray	С	MO-2117(IPC) MO-2115(OPC)	150/07-02-90 21,000/07-02-90	150/07-02-90 0/07-10-90	Increase torque switch setting to 12,218 ft-lbs.
X-16B	Core Spray	С	MO-2137(IPC) MO-2135(OPC)	355/08-01-90 610/08-01-90	215/08-16-90 610/08-01-90	
X-19	Drywell Drain	С	CV-3704(IPC) CV-3705(OPC)	0/07-02-90 0/07-02-90	0/07-02-90 0/07-02-90	
X-20	Demineralized Water	С	V-09-111(IPC) V-09-65(OPC)	0/07-20-90 0/07-20-90	0/07-20-90 0/07-20-90	

Pen No.	System Name	Test Type	Equipment/ <u>Valves (Note 1)</u>	As fouud leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-21	Service Air	С	Blind Flange(IPC)	0/07-22-90	0/07-22-90	
			V-30-287(OPC)	(Combined)	(Combined)	
X-22,	N ₂ Compressor Discharge	С	V-43-214(IPC)	0/07-23-90	0/07-23-90	
N-229A	N-229A		CV-4371C(OPC)	210/07-23-90	210/07-23-90	
			CV-4371A(OPC)	440/07-23-90	440/07-23-90	
X-23A	Drywell Cooling Water Supply	y C	CV-5718A(IPC)	950/07-06-90	950/07-06-90	
, ,			V-57-77(OPC)	(Combined)	(Combined)	
X-23B	Drywell Cooling Water Supply	y C	CV-5718B(IPC)	89,250/07-20-90	210/08-11-90	Replaced stem, cleaned up seating surfaces.
			V-57-78(OPC)	(Combined)	(Combined)	Cleaned internals, repacked with short box configuration.
X-24A	Drywell Cooling Water Return	n C	CV-5704A(IPC) V-57-75(OPC)	220/07-18-90 (Combined)	220/07-19-90 (Combined)	
X-24B	Drywell Cooling Water Return	n C	CV-5704B(IPC) V-57-76(OPC)	720/07-20-90 (Combined)	720/07-20-90 (Combined)	
X-25	Drywell Purge Outlet	С	CV-4302(IPC)	26,200/11-21-89	13,000/11-23-89	Replaced 'T' seal
			CV-4303(OPC)	(Combined)	(Combined)	and O-Rings.
			CV-4303(OFC)	(Combined)	(Combined)	

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As fouud leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-25	Drywell Purge Outlet	С	CV-4302(IPC)	2,950/06-28-90	5,200/07-19-90	Replaced 'T' seal and flange O-Rings.
			CV-4303(OPC)	(Combined)	(Combined)	Replaced 'T' seal and flange O-Rings.
			CV-4310(OPC)	5,400/06-28-90	5,400/06-28-90	
X-26, N-220	Drywell Purge Supply	С	CV-4306(IPC)	540/07-02-90	1,900/08-20-90	Replaced 'T' seal and O-Rings, repaired galled shaft at O-Ring contact and replaced shaft O-Rings.
			CV-4307(OPC)	(Combined)	(Combined)	Replaced 'T' seal and flange O-Rings, also replaced shaft O-Rings.
			CV-4308(OPC)	(Combined)	(Combined)	Replaced 'T' seal and flange O-Rings, also replaced shaft O-Rings.
X-26, N-220	Drywell and Torus Makeup	С	CV-4311(IPC)	1,350/07-02-90	1,350/07-02-90	
N ZEO			CV-4312(OPC) CV-4313(OPC)	2,000/07-02-90 425/07-03-90	2,000/07-02-90 425/07-03-90	
X-32D	N ₂ Compressor Suction	С	CV-4378A(IPC) CV-4378B(OPC)	275/07-06-90 295/07-06-90	275/07-06-90 295/07-06-90	
X-32E	Recirc. Pump A Seal	С	V-17-96(IPC) CV-1804B(OPC)	0/07-07-90 0/07-07-90	0/07-07-90 0/07-07-90	
X-32F	Recirc. Pump B Seal	С	V-17-83(IPC) CV-1804A(OPC)	0/07-07-90 0/07-07-90	0/07-07-90 0/07-07-90	

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-35A	TIP Check	С	Check Valve(OPC)	650/07-20-90	650/07-20-90	·
X-35B	TIP Ball	С	Ball Valve(OPC)	0/07-20-90	0/07-24-90	
X-35C	TIP Ball	С	Ball Valve(OPC)	0/07-20-90	0/07-24-90	
X-35D	TIP Ball	С	Ball Valve(OPC)	0/07-20-90	0/07-24-90	
X-36	CRD Return	С	V-17-53(IPC) V-17-52(OPC)	69/08-02-90 34/08-02-90	69/08-02-90 34/08-02-90	See note 2. See note 2.
X-39A	CAD Supply	С	SV-4332A(IPC) SV-4332B(OPC)	40/07-16-90 60/07-16-90	40/07-16-90 60/07-16-90	
X-39B	CAD Supply	С	SV-4331A(IPC) SV-4331B(OPC)	0/07-16-90 -	0/07-16-90 0/11-09-89	Repaired main and pilot seats and cleaned parts.
				0/07/16/88	<105/05-17-89 0/07-16-90	Rebuilt valve.
X-40C	Jet Pump Coolant Sample	С	SV-4594B(IPC) SV-4595B(OPC)	0/07-11-90 10,500/07-11-90	0/07-11-90 0/08-25-90	Overhauled valve.
X-40D	Jet Pump Coolant Sample	С	SV-4594A(IPC) SV-4595A(OPC)	0/07-11-90 0/07-11-90	0/07-11-90 0/07-11-90	
X-41A	Recirc. Loop Sample	С	CV-4639(IPC) CV-4640(OPC)	159/07-06-90 - 500/07-06-90	159/07-06-90 238/12-06-89 500/07-0 6 -90	Repacked.
				300/07-00-30	300/07-00-30	

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-42	Standby Liquid Control	С	V-26-9(IPC) V-26-8(OPC)	520/08-01-90 15,100/08-01-90	520/08-01-90 800/08-08-90	Disassembled, cleaned internals, reassembled.
X-46F	CAM Return	С	SV-8105B(IPC) SV-8106B(OPC)	0/07-10-90 0/07-10-90	0/07-10-90 0/07-10-90	
X-48	Drywell Drain Discharge	С	CV-3728(IPC) CV-3729(OPC)	0/07-04-90 0/07-04-90	0/07-04-90 0/07-04-90	
X-50B	CAM Supply	С	SV-8101A(IPC) SV-8102A(OPC)	0/07-24-90 0/07-24-90	0/07-24-90 0/07-24-90	
X-50D	CAM Supply	С	SV-8105A(IPC) SV-8106A(OPC)	0/07-24-90 0/07-24-90	0/07-24-90 0/07-24-90	
X-50E	CAM Supply	С	SV-8103A(IPC) SV-8104A(OPC)	0/07-24-90 0/07-24-90	0/07-24-90 0/07-24-90	
X-54	CCW Return	С	MO-4841A(IPC)	35/07-10-90	170/08-04-90	Replaced torque switch.
X-55	CCW Supply	С	MO-4641B(OPC)	225/07-10-90	140/08-04-90	Replaced torque switch.
X-56C	CAM Supply	С	SV-8101B(IPC) SV-8102B(OPC)	0/06-30-90 0/06-30-90	0/08-26-90 0/08-26-90	See note 3. See note 3.
X-56D	CAM Supply	С	SV-8103B(IPC) SV-8104B(OPC)	0/06-30-90 0/06-30-90	0/08-26-90 0/08-26-90	See note 3. See note 3.

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
N-205	Torus Exhaust Outlet	С	CV-4300(IPC)	9,500/07-03-90	440/08-21-90	Replaced 'T' seal and flange O-Rings.
			CV-4301 (OPC)	(Combined)	(Combined)	Replaced 'T' seal and flange O-Rings.
			CV-4309(OPC)	14,000/07-03-90	14,000/07-03-90	
N-211A	CAD Supply	С	SV-4333A(IPC)	- 35/07-17-90	<125/04-25-89 0/07-17-90	Rebuilt valve. Rebuilt valve.
			SV-4333B(OPC)	0/07-17-90	0/07-17-90	
N-211B	CAD Supply	С	SV-4334A(IPC) SV-4334B(OPC)	1,500/07-17-90 1,500/07-17-90	1,500/07-17-90 1,500/07-17-90	
N-212	RCIC Turbine Exhaust	С	V-24-8(IPC) V-24-23(OPC)	141/07-03-90 (Combined)	141/07-03-90 (Combined)	See note 2.
N-212	RCIC Turbine Exhaust Vacuum Breaker	С	V-24-46(IPC)	50/07-03-90	2,475/08-11-90	Performed BS-3 inspection on internals.
			V-24-47(OPC)	815/07-03-90	2,750/08-13-90	Performed BS-3 inspection on internals.
N-214	HPCI Turbine Exhaust	С	V-22-17(IPC) V-22-16(OPC)	596/07-03-90 (Combined)	596/07-03-90 (Combined)	See note 2.
N-214	HPCI Turbine Exhaust Vacuum Breaker	С	V-22-63(IPC)	500/07-03-90	735/08-14-90	Performed BS-3 inspection on internals.
			V-22-64(OPC)	510/07-03-90	850/08-14-90	Performed BS-3 inspection on internals.

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
N-219	HPCI/RCIC Exhaust	С	MO-2290B(IPC)	1,150/07-04-90	380/08-11-90	Replaced torque switch.
			MO-2290A(OPC)	1,050/07-04-90	1,050/07-04-90	SWITCH.
N-222	HPCI Condensate Return	С	V-22-22(IPC)	0/07-06-90	84/08-12-90	See note 2. Performed BS-3 inspection on internals.
			V-22-21(OPC)	(Combined)	(combined)	Performed BS-3 inspection on internals.
N-229B	CAM Supply	С	SV-8107A(IPC) SV-8108A(OPC)	0/07-12-90 0/07-12-90	0/07-12-90 0/07-12-90	
N-229C	CAM Return	С	SV-8109A(IPC) SV-8110A(OPC)	0/07-12-90 0/07-12-90	0/07-12-90 0/07-12-90	
N-229F	CAM Return	С	SV-8109B(IPC) SV-8110B(OPC)	0/07-12-90 0/07-12-90	0/07-12-90 0/07-12-90	
N-229G	CAM Supply	С	SV-8107B(IPC) SV-8108B(OPC)	0/07-12-90	0/07-12-90	
N-229H	PASS Sample Return	С	SV-8772A(IPC) SV-8772B(OPC)	0/07-12-90 0/07-12-90 0/07-12-90	0/07-12-90 0/07-12-90 0/07-12-90	
N-231	Vacuum Breaker	С	CV-4304(IPC)	260/07-01-90	225/08-14-90	Replaced 'T' seal and flange O-Rings, replaced body drain nipple.
			V-43-169(OPC)	(Combined)	(combined)	inppie.

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
N-231	Vacuum Breaker	C	CV-4305(IPC)	450/07-01-90	235/08-20-90	Replaced 'T' seal flange O-Rings and 3-way valve.
			V-43-168(OPC)	(Combined)	(combined)	• .,

Notes:

- (IPC) Inside Reactor Containment
 (OPC) Outside Reactor Containment
- 2. These valves were tested with water as the test medium. The test results are in cc/min.
- 3. CAM supply piping was cut and valve locations moved per DCP-1492.

ATTACHMENT 4B 1990 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

The as found LLRT, the repair, and the as left LLRT for each boundary, or penetration, was reviewed. The net leakage contribution for each penetration was determined using the following criteria:

- 1. A leakage equivalent to the repair improvement achieved on each valve in the penetration is calculated.
- 2. The leakage equivalent is the difference between the as found and the as left leakage rates.
- 3. If a repair was not performed, a zero leakage equivalent is assessed to the valve.
- 4. The leakage equivalent assessed to a penetration may be reduced due to the safety-related service of the system associated with the penetration(s). Justification for this reduction will be provided with the analysis.
- 5. The net equivalent leakage for the penetration is the lowest of the inside or outside valve grouping (e.g., simulates minimum pathway leakage). The inside barrier may be inside the containment or the innermost barrier of the two barriers outse the containment. See Attachment 4A.
- 6. No repair improvement credit is taken if the as left leakage rate is higher than the as found leakage rate. Only those penetrations where repairs were performed are included in this attachment.
- 7. If the as left leakage rate of a repaired valve is lower than the as left leakage rate of a valve that didn't require a repair, then the penetration net equivalent leakage is the difference between the as left leakage rates, or the repair improvement of the reworked valve.
- 8. For series valves tested together (i.e. combination test), the penetration net equivalent leakage is half the difference between the as found and the as left leakage rates when both valves are repaired at the same time (prior to performing another test).
- 9. When the summation of the leakage equivalent and the leakage measured during a successful Type A test is greater than L_a, the penetration(s) with excessive leakage(s) shall be analyzed under a failure analysis program.
- 10 All leakage rate values are in SCCM.

Conclusions:

The resulting net equivalent leakage of 75,842 SCCM or 0.486569 percent/day indicates that the as found ILRT test results determined by analysis are below the plant's maximum allowable leakage rate of 2.0 percent/day.

ATTACHMENT 4B 1988 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

Pen <u>Num.</u>	<u>System</u>	<u>Inside</u>	<u>Outside</u>	<u>Net</u>	<u>Notes</u>
X-53	Drywell Head	-	4,920	4,920	
X-58A	Stabilizer Access Port	-	240	240	
X-26	Drywell Purge Supply	-	7,300	7,300	
N-220	Torus Purge Supply	-	4,500	4,500	
X-7A	Main Steam	7788	7788	7788	Comb. Test
X-7B	Main Steam	1050	1050	1050	
X-7C	Main Steam	565	565	565	
X-7D	Main Steam	923	923	923	Comb. Test
X- 8	Steam Drain	0	2,200	0	
X-9A	Feedwater	78,450	0	0	
X-9B	Feedwater	0	0	0	
X-10	RCIC Cond. Ret.	375	425	375	
X-10	RCIC Steam	0	650	0	
X-11	HPCI Cond. Return	3,450	3,450	3,450	
X-11	HPCI steam	0	0	0	
X-15	RWCU	0	0	0	
X-16A	Core Spray	0	21,000	0	
X-16B	Core Spray	140	0	0	
X-23B	Drywell Cooling Water Supply	44,520	44,520	44,520	Comb. Test
X-25	Drywell Purge Outlet	-	0	0	Comb. Test
X-26, N-220	Drywell & Torus Makeup	0	0	0	
X-40C	Jet Pump Coolant Sample	0	10,500	0	
X-42	Standby Liquid Control	0	14,300	0	
X-54	CCW Return	0	O	0	
X-55	CCW Supply	-	85	85	
X-56C	CAM Supply	0	0	0	
X-56D	CAM Supply	0	0	0	

ATTACHMENT 4B 1988 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

Pen Num.	System	<u>Inside</u>	<u>Outside</u>	<u>Net</u>	<u>Notes</u>	
N-205	Torus Exhaust Outlet	-	0	0	Comb. Test	
N-211A	CAM Supply	35	0	0		
N-212	RCIC Turb. Exhaust	0	0	0		
N-214	HPCI Vac. Br.	0	0	0		
N-219	HPCI Exhaust	770	0	0		
N-222	HPCI Condensate	0	0	0		
N-231	Vacuum Breaker	-	35	18	Comb. Test	
N-231	Vacuum Breaker	· -	215	108		