REACTOR CONTAINMENT EULDING. INTEGRATED LEAKAGE AND LEST

TYPES A, B, AND PERIODIC TEST

IOWA ELECTRIC LIGHT AND POWER COMPANY DUANE ARNOLD ENERGY CENTER

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REFERENCES

- 1. 10CFR Part 50, Appendix J, Primary Reactor Containment Leakage Testing for Water-Cooled Power Reactors, November 15, 1988.
- 2. STP No. 47A002, Primary Containment Leakage Rate Test, Duane Arnold Energy Center, Surveillance Test Procedure.
- 3. ANSI N45.4, American National Standard, Leakage-Rate Testing of Containment Structures for Nuclear Reactors, March 16, 1972.
- 4. ANSI/ANS-56.8, Containment System Leakage Testing Requirements, January 20, 1987.
- 5. Bechtel Corporation's Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants, BN-TOP-1, Revision 1, November 1, 1972.
- 6. STP No. 47A003, Containment Leak Tightness Test Type B Penetrations, Duane Arnold Energy Center, Surveillance Test Procedure.
- 7. STP No. 47A004, Airlock Local Leak Rate Test, Duane Arnold Energy Center, Surveillance Test Procedure.
- 8. STP No. 47A005, Containment Isolation Valve Leak Tightness Test Type C Penetrations, Duane Arnold Energy Center, Surveillance Test Procedure.

This document used only as a guideline and any reference to said document in no way implies compliance.

SECTION 1

PURPOSE

The purpose of this report is to present a description and analysis of the December 1988 Periodic Type A Primary Containment Integrated Leakage Rate Test (ILRT) and a summary of the Periodic Types B and C Local Leakage Rate Tests (LLRT) conducted since June 1987 at the Duane Arnold Energy Center (DAEC). DAEC is operated by the Iowa Electric Light and Power Company (IE). Specific plant information and technical data is contained in Attachment 1A.

This report is submitted as required by 10CFR50, Appendix J, Paragraph V.B.

ATTACHMENT 1A

TEST DATA SUMMARY

A. Plant Information

Operator Iowa Electric Light and Power Company
Plant Duane Arnold Energy Center
Location Palo, Iowa
Containment Type Mark I, BWR/4
Docket Number 50-331
Operating License No. DPR-49
Date Test Completed December 16, 1988

B. Technical Data

Containment Net Free Air Volume as Tested	205,360 cu. ft.
Drywell Free Air Volume	109,400 cu. ft.
Torus Free Air Volume	95,960 cu. ft.
Design Pressure	56 psig
Calculated Peak Accident Pressure	43 psig
Containment Design Temperature	281 °F
Containment ILRT Average Temperature Limits	40-100 °F

SECTION 2

SUMMARY

2.1 TYPE A TEST

2.1.1 Test Summary

Pressurization for the ILRT began at approximately 2025 hours on December 14, 1988. The air flow was adjusted for optimum compressor cycling and a pressurization rate of approximately 5.7 psi per hour was achieved. Extensive investigations of all penetration areas were conducted throughout the pressurization and the Type A test. Several minor leaks were detected and monitored but no significant leakage was found. At 0330 on December 15, 1988, the CRD pump stop check valves V-17-08 and V-17-10 were closed due to concerns with dropping Reactor Vessel water level.

Containment pressurization was secured at approximately 0403 hours on December 15, 1988. The pressurization piping system was isolated and vented.

At 0815 hours on December 15, 1988, the thermal stabilization criteria of Reference 2 was satisfied. Pressure, temperature and dew point data were continuously recorded throughout the pressurization at 20 minute intervals and throughout the remainder of the test period at 15 minute intervals.

The Type A test was successfully completed at 1615 hours on December 15, 1988 with a Total Time Upper Confidence Limit (UCL-TT) of 0.195644 percent/day and a Mass Point Upper Confidence Limit of 0.159811 percent/day. Both Total Time and Mass Point leakage rates were well below the 0.75L_a acceptance criteria.

The Superimposed Verification Test was started at 1800 hours on December 15, 1988 and was successfully completed at 2200 hours on December 15, 1988. The results of the verification test satisfied the requirements of Reference 2 (See Appendix G, page 3).

Shortly after the start of the superimposed verification test, the closure of the CRD pump stop check valves at 0330 on December 15, 1988 was re-evaluated. It was believed that the justification given for this action was subject to challenge. IE decided that an extra leakage rate test would be conducted after the completion of the superimposed leakage verification test to prove that closure of the CRD pump stop check valves did not adversely effect the test results. Conditions for the extra test included securing the superimposed flow and opening the CRD pump check valves. Criteria for the extra test were established prior to the completion of the superimposed leakage verification test. After the superimposed leakage verification test, the containment was allowed to stabilize for about one and a half hours. The extra test was started at 0030 on December 16, 1988 and successfully completed at 0230 on December 16, 1988. The calculated Total Time Leakage rate for the extra test was 0.126602 percent per day. This leakage rate was less than the leakage rate determined

from the Type A test, confirming that closure of the valves did not adversely impact the test.

Depressurization of the containment began at approximately 0430 on December 16, 1988 and was completed at 1100 on December 16, 1988.

2.2 LOCAL LEAKAGE RATE TESTS (Types B and C)

The Local Leakage Rate Tests (LLRT) of containment isolation valves and other containment penetrations were conducted as required by the methods described in the plant surveillance procedures, References 6, 7 and 8, for the Types B and C Tests.

Section 4 of this report summarizes the data for the LLRT conducted since the June 1987 Type A test in accordance with Appendix J, 10CFR50, Paragraph V.B. Also contained in Section 4 of this report is the 1988 LLRT Summary Analysis.

SECTION 3

TYPE A TEST

3.1 EDITED LOG OF EVENTS

This log was edited from information contained in the ILRT Coordinator's Official Type A Log of Events or from Reference 2.

December 14, 1988

- 0200 Drywell inspection successfully completed.
- O445 In situ instrumentation checks complete. Two RTDs and one dewcel were outside of acceptable range.
- 2025 Commenced pressurizing containment. Pressurization rate is approximately 5.7 psi/hour.
- 2330 Commenced plant walkdown.

December 15, 1988

- 0330 Reactor Vessel level was dropping. Closed valves V-17-08 and V-17-10.
- 0403 Pressurization secured.
- 0815 Temperature stabilization criteria satisfied. The 0815 data point is the first test data point.
- 1410 Leak survey revealed two valves V-30-289 and V-30-290 which were open but capped. The caps should have been removed. ILRT results will be adjusted for the penetration 21 Type C leakage rate.
- 1615 ILRT successfully completed.
- 1700 Started superimposed flow.
- 1800 Started superimposed test.
- 1900 Review of 0330 log entry on the closure of CRD pumps discharge stop check valve. The justification for closing these valves is subject to challenge.

- Near the completion of the superimposed test, it was decided to perform an extra test to determine the impact of closing the CRD pumps discharge isolation valves on the Type A leakage rate. The conditions for the extra test involved securing the superimposed leakage, opening the stop check valves, stabilizing for about an hour and then conducting a short leakage test. The criteria for the extra test was established and documented in the log.
- 2200 Superimposed verification test successfully completed.
- 2210 Secured verification flow.
- 2250 Opened valves V-17-08 and V-17-10.

December 16, 1988

- 0030 Declared start of the extra test to determine the leakage of V-17-08 and V-17-10.
- 0230 Completed the extra leakage rate test successfully.
- 0430 Initiated depressurization
- 1100 Depressurization completed.

3.2 GENERAL TEST DESCRIPTION

3.2.1 Prerequisites

In accordance with Reference 2, the following is a listing of the pertinent prerequisites and other procedural requirements completed and documented prior to containment pressurization:

- a. Site meteorological data recorded during the performance of the ILRT (Attachment 3.2A)
- b. All required test instrumentation installed and functionally verified within 6 months of the test.
- c. Primary containment ventilation system secured.
- d. Satisfactory inspection of the primary containment in accordance with Reference 2.
- e. Pressurization system lined-up and ready for operation.
- f. RCS temperature maintained stable prior to and during the performance of the ILRT.
- g. Data acquisition and analysis computer systems used for the test are operational.
- h. All required system valve lineups completed.
- i. Drywell-to-torus vacuum breakers are blocked open.
- j. Restricted plant access plan in effect.
- k. An Official Type A Log of Events established and maintained by the ILRT Coordinator.
- l. All pressurized components and systems either removed from the containment or vented.
- m. Temperature survey satisfactorily performed.
- n. All required Types B and C leakage rate testing completed or analyzed for impact on the test.
- o. Verification flowmeter installed.
- p. Instrument Selection Guide (ISG) calculated.

3.2.2 Equipment and Instrumentation

Pressurization of the primary containment was achieved by utilizing a permanent system consisting of two station air compressors with integral aftercoolers. The system included adequate instrumentation and valving to maintain proper monitoring and control of the compressed air quality throughout the pressurization sequence. The capacity of the station air compressors is approximately 2,200 standard cubic feet per minute (SCFM). Air not required to maintain the service air header pressure was supplied to the primary containment through temporary hoses that connected the service air system to the Containment Atmosphere Control System.

The various containment parameters required to calculate containment leakage during the test, were monitored using instrumentation which consisted of 13 resistance temperature detectors, 5 dewpoint temperature sensors, and 3 absolute pressure indicators. Pertinent data for the test instrumentation is listed in Attachment 3.2B, and the general locations of the test instrumentation for both the drywell and the suppression chamber are shown in Attachments 3.2C and 3.2D. Elevations and azimuths are approximate.

A rotometer was used to perform the superimposed leakage verification test.

Instrument Selection Guide (ISG)

Sensor Type	No. of Sensors	Sensitivity Error	System Error
Pressure	3	0.09 psi	0.00 psi
Temperature	13	1.00 °F	0.50 °F
Dewpoint Temp.	- Drywell 3	5.00 °F	0.50 °F
-	Torus 2	5.00 °F	0.50 °F

Test Duration 8 hrs.
Test Pressure 57.696 psia
Test Temperature 74 °F = 534 °R

Test Dewpoint Temp. 65 °F

ISG =
$$\pm \frac{2400}{t} \left[2 \left(\frac{EP}{P} \right)^2 + 2 \left(\frac{ET}{T} \right)^2 + 2 \left(\frac{EP}{P_v} \right)^2 \right]^{1/2}$$

ISG \leq 0.25 L_a which equals 0.5% per day since L_a = 2.0% per day

a. EP = error associated with absolute pressure instruments

$$EP = 0.09 / \sqrt{3}$$

$$EP = 0.051962$$

b. ET = error associated with temperature instruments

$$ET = 1.118034 / \sqrt{13}$$

$$ET = 0.310$$

c. $EP_v = error$ associated with vapor pressure instruments

$$EP_v = 0.053516 / \sqrt{5}$$

$$EP_{v} = 0.023937$$

Using values established in a,b and c above, calculate ISG.

ISG =
$$\pm \frac{2400}{24} \left[2 \left(\frac{0.051961}{57.696} \right)^2 + 2 \left(\frac{0.310}{534} \right)^2 + 2 \left(\frac{0.023937}{57.696} \right)^2 \right]^{1/2}$$

ISG = \pm 0.162532 which is less than 0.5%/day (25% of L_a)

3.2.3 Data Acquisition System

A programmable, multichannel data logger was used to scan the data from the 15 resistance temperature detectors and 6 dewpoint temperature sensor input signals. These signals were sent to microcomputers which also recorded the 3 pressure sensor readings. These microcomputers logged data every 15 seconds during the pressurization and throughout the test and provided printed output of the instantaneous data readings every 20 minutes during pressurization and every 15 minutes during the Leakage Rate, Verification and extra tests.

3.2.4 Data Resolution System

The recorded data was manually inputted to a dedicated computer system using Stone & Webster Engineering Corporation's (SWEC) ILRT analysis program for data reduction and leakage rate calculations. The computer program converted the Dewcel Element Temperatures to Dewpoint Temperatures using a polynomial curve fit derived from the Dewcel vendor's test data. The following calculations used the instantaneous values of the ILRT sensors to determine both the Mass Point and Total Time Analysis Method leakage rates.

Absolute Method of Mass Point Analysis

The Absolute Method of Mass Point Analysis consists of calculating the air mass within the containment structure, over the test period using pressure, temperature, and dewpoint temperature observations made during the ILRT. The air mass is computed using the ideal gas law as follows:

$$M = \frac{144V(P-P_{\nu})}{RT}$$
 (Eq. 1)

where:

M = air mass, lbm

P = total pressure, psia

P_v = average vapor pressure, psia R = 53.35 ft-lbf/lbin^oR (for air)

T = average containment temperature, °R

V = containment free volume, ft³

The leakage rate is then determined by plotting the air mass as a function of time, using a least-squares fit to determine the slope, A = dM/dT. The leakage rate is expressed as a percentage of the air mass lost in 24 hours or symbolically:

Leakage Rate =
$$-2400$$
 (A/B) (Eq. 2)

Where A is the slope of the least-squares curve and B is the y-intercept. The sign convention is such that the leakage out of the containment is positive, and the units are in percent/day.

A confidence interval is calculated using a Student's T distribution. The sum of the leakage rate and confidence interval is the Upper Confidence Limit - Mass Point (UCL-MP).

Absolute Method of Total Time Analysis

The Absolute Method of Total Time Analysis consists of calculating air lost from the containment, using pressure, temperature, and dewpoint temperature observations made during the ILRT.

The containment air mass is computed using Equation 1. The measured leakage rate at any time (t) is then determined by subtracting the mass at that time (Mt) from the initial mass (Mi) and dividing by the initial mass. The measured leakage rate is expressed as a percentage of containment mass lost in 24 hours or symbolically:

Measured Leakage Rate = 2400 (Mi-Mt) (Eq. 3)
$$Mi(\Delta t)$$

The sign convention is such that leakage out of the containment is positive, and the units are in percent/day.

The calculated leakage rate is then determined by plotting the measured leakage rate as a function of time and then performing a least-squares curve fit of the measured leakage rate values as follows:

Calculated Leakage Rate =
$$At + B$$
 (Eq. 4)

Where, A is the slope and B is the y-intercept of the least squares curve.

A confidence interval is calculated using the requirements of Bechtel Topical Report BN-TOP-1, Rev. 1.

The sum of the calculated leakage rate and the confidence interval is the Upper Confidence Limit - Total Time (UCL-TT).

SITE METEOROLOGY

Date	<u>Time</u>	Ambient Temperature (Deg F)	Dewpoint Temperature (Deg F)	Barometric Pressure (In. Hg)	General Weather Conditions
December 14, 1988	2115	26.8 24.4	19.6 17.4	30.2 30.2	Good Good
	2215 2315	22.5 20.8	14.9 9.5	30.3	Good Good
December 15, 1988	0015 0115 0215 0315 0415	18.5 16.7 15.4 14.4 13.3	6.9 7.2 4.8 3.8 3.4	30.3 30.4 30.4 30.5 30.5	Good Good Good Good
	0515 0615 0715 0815	13.5 13.5 11.6 10.2	3.1 2.7 0.8 -0.1	30.5 30.5 30.6 30.6	Good Good Good Good
	0915 1015				Note 1 Note 1
	1115 1215 1315	10.9 11.4 12.6	-4.8 -3.8 -6.0	30.6 30.6 30.6	Good Good
	1415 1515 1615	11.3 9.8	-5.5 -6.4	30.6 30.7	Note 2 Good Good
	1715 1815 1915	8.1 6.9 5.9	-5.7 -4.7 -5.4	30.7 30.7 30.7	- - -
	2015 2115 2215 2315	4.7 3.1 0.6 -0.5	-5.8 -5.8 -5.1 -5.9	30.6 30.6 30.6 30.6	
December 16, 1988	0015 0115 0215	-1.1 -1.5 -0.5	-5.9 -6.7 -5.7	30.6 30.5 30.5	
	0230	-0.5	-4.8	30.5	-

Notes:

- 1. Computer was down.
- 2. No data available.

ATTACHMENT 3.2B

INSTRUMENTATION LIST

The following instruments were calibrated and functionally verified within 6 months prior to the performance of this test and in accordance with 10CFR50, Appendix J.

Instrument	Weight Fraction	Computer Point	Zone	Azimuth	Elevation	Range	Accuracy
A. Temperat	ure					•	
Tl	0.154	CO	6	270°	735	32-250°F	±0.5°F
T2	0.154	C1	6	0°	735	32-250°F	±0.5°F
T3**	0.000	C2	6	90°	735	32-250°F	±0.5°F
T4	0.154	C3	6	180°	735	32-250°F	±0.5°F
T 5	0.047	C4	4	45°	749	32-150°F	±0.5°F
T6	0.047	C5	4	225°	750	32-150°F	±0.5°F
T 7	0.053	C6	3	90°	764	32-150°F	±0.5°F
T8	0.053	C7	3	210°	763	32-150°F	±0.5°F
T9**	0.000	C8	2	20°	786	32-150°F	±0.5°F
T10	0.092	C9	2	150°	786	32-150°F	±0.5°F
T11	0.061	C13	1	345°	828	32-150°F	±0.5°F
T12	0.024	C10	5	Rx CL	750	32-150°F	±0.5°F
T13*	0.046	C14	2	290°	787	32-150°F	±0.5°F
T14*	0.061	C12	1	165°	828	32-150°F	±0.5°F
T15*	0.054	C11	3	315°	766	32-150°F	±0.5°F
B. Dewpoint	Temperature						
M1**	0.000	C20	A	340°	809	32-150°F***	±5.0°F
M2	0.260	C21	A	160°	809	32-150°F***	±5.0°F
М3	0.139	C22	В	225°	750	32-150°F***	±5.0°F
M4	0.139	C23	В	45°	749	32-150°F***	±5.0°F
M5	0.231	C24	С	270°	735	32-150°F***	±5.0°F
M6*	0.231	C2 5	С	90°	735	32-150°F***	±5.0°F



INSTRUMENTATION LIST

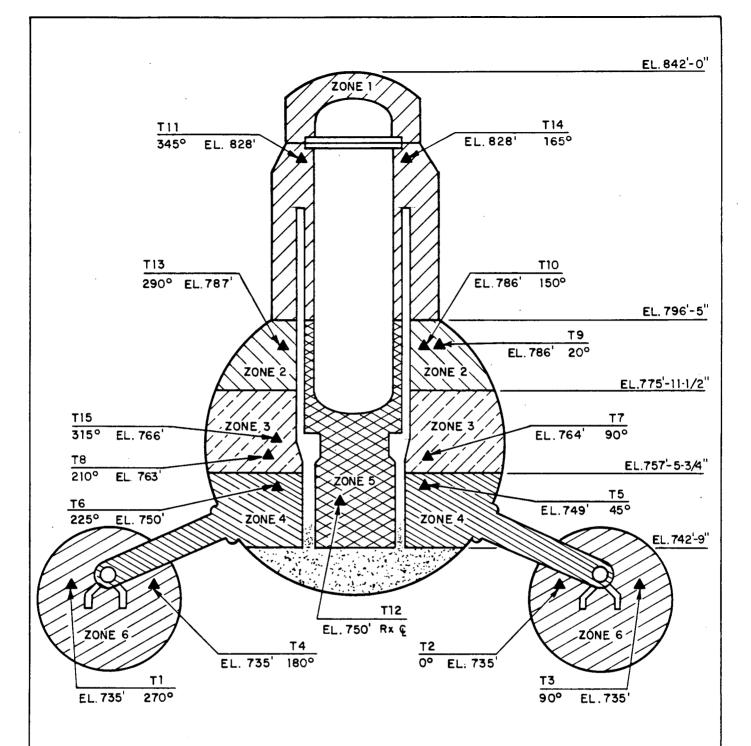
Instrument	Weight Fraction	Computer Point	Zone	Azimuth	Elevation	Range	Accuracy
C. Pressure	1						
P1	0.500000	Local	Drywel	1 -	_	0-100psia	± 0.02% FS
P2	0.500000	Local	Torus	_	_	0-100psia	± 0.02% FS
Р3	0.000000	Local	Drywel	1 -	-	0-100psia	± 0.02% FS
D. Superimposed Leakage Verification Test Flow Instrument							
Rotometer	: -	Local	-	-	_	5-19scfm	±1.0%F.S.

Notes:

- * Temporary RTD and/or Dewpoint Sensors.
- ** Instruments not used during the test because of in situ tests outside of acceptable range.
- *** The Dewcel Element Temperatures (ET) were converted to Dewpoint Temperatures (DPT) by the following polynomial equation:

 $DPT = -1.5923290156E + 1 + 3.2150392932E - 1 \times ET + 2.7879779394E - 3 \times ET^{2} - 7.1099385788E - 6 \times ET^{3}$

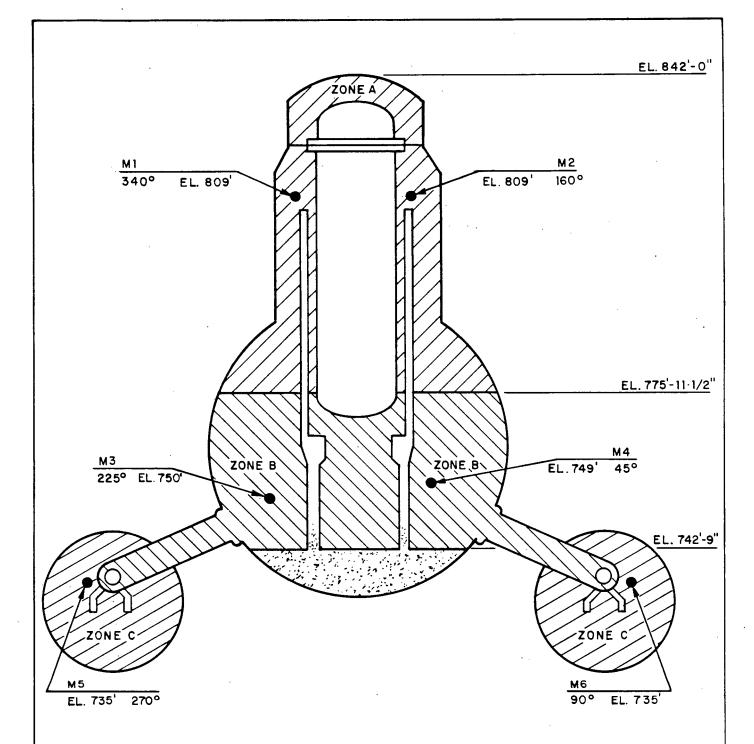
This equation is valid over the range of 51.2 to 83.7 °F Dewpoint Temperature (ET of 121 to 169 °F)



NOTES:

- ZONE BOUNDARIES ARE APPROXIMATE, REFERENCE DAEC DWG. No. M-156
- 2. RTD ELEVATIONS AND AZIMUTH POSITIONS ARE APPROXIMATE

ATTACHMENT 3.2C
ILRT TEMPERATURE DETECTOR
LOCATIONS
DUANE ARNOLD ENERGY CENTER



NOTES:

- 1. ZONE BOUNDARIES ARE APPROXIMATE, REFERENCE DAEC DWG. No. M-156
- 2. DEWPOINT TEMPERATURE SENSOR ELEVATIONS AND AZIMUTH POSITIONS ARE APPROXIMATE

ATTACHMENT 3.2D
ILRT DEWPOINT TEMPERATURE
SENSOR LOCATIONS
DUANE ARNOLD ENERGY CENTER

3.3 TEST RESULTS

3.3.1 Presentation of Test Results

The test data for the December 1988 ILRT is based on a 8 hour test period starting at 0815 hours on December 15, 1988. The final test results were determined using SWEC's ILRT computer program. The Measured Input Data, Reduced Input Variables, Mass Point Analysis Test Results, Total Time Analysis Test Results, and representative graphs are contained in Attachments 3.3A through 3.3K.

Both the Mass Point and Total Time Analysis Test Results for the ILRT satisfied the procedural acceptance criteria.

The Type A Test instrumentation was verified by the Superimposed Leakage Verification Test Method. The Measured Input Data, Reduced Input Variables, Mass Point Analysis Test Results, Total Time Analysis Test Results, and representative graphs are contained in Attachments 3.3L through 3.3S.

Both the Mass Point and Total Time Analysis Test Results for the Superimposed Leakage Verification Test satisfied the procedural acceptance criteria.

3.3.2 57.696 psia ILRT Results

The 57.696 psia ILRT was conducted in accordance with Reference 2. The results for the ILRT and for the Supplemental Test are shown below.

3.3.2.1 ILRT Results - Mass Point Analysis

	<u>Item</u>	(Percent/Day)
1.	L _{am} , Leakage Rate Calculated	0.155734
2.	UCL, Upper Confidence Level	0.004077
3.	UCL-MP, L _{am} Leakage Rate plus UCL (1&2)	0.159811
4.	Corrections for: (See Sections 3.3.2.4)	
	i. Type B & C Penalties 0.030150 ii. Water Levels 0.003108	
	iii. Total Corrections (i. and ii.)	0.033258
5.	Total Reported Type A Leakage Rate (Items 3&4 iii.)	0.193069

Results were within the acceptable limits of $0.75\ L_a$ or $1.5\ percent/day$.

3.3.2.2 ILRT Results - Total Time Analysis

	<u>Item</u>	(Percent/Day)
1.	L _{am} , Leakage Rate Calculated	0.151511
2.	UCL, Upper Confidence Level	0.044132
3.	UCL-TT, L _{am} Leakage Rate plus UCL (1&2)	0.195644
4.	Corrections for: (See Section 3.3.2.4)	
	i. Type B & C Penalties 0.030150 ii. Water Levels 0.003108	
	iii. Total Corrections (i. and ii.)	0.033258
5.	Total Reported Type A Leakage Rate (Items 3&4 iii.)	0.228902

Results were within the acceptable limits of 0.75 L_a or 1.5 percent/day.

3.3.2.3 Supplemental Test Results

The Supplemental Verification Test was performed using the Superimposed Leakage Verification Test Method in accordance with Reference 2. The results for the Superimposed Leakage Verification Test are shown below.

1. The Superimposed Leakage Verification Test is acceptable provided L_c falls within the following range:

$$(L_{am} + L_o - 0.25 L_a) \le L_c \le (L_{am} + L_o + 0.25 L_a)$$

Where:
$$L_{am}$$
 = Type A calculated leakage rate (computer)
 $(L_{am} - MP = 0.155734 \%/day)$
 $(L_{am} - TT = 0.151511 \%/day)$

$$L_o$$
 = Superimposed leakage rate (rotameter)
(L_o = 1.981938 %/day)

$$L_a$$
 = Maximum allowable leakage rate $(L_a = 2.0 \%/\text{day})$

$$L_c$$
 = Composite leakage rate (computer)
(L_c - MP = 1.854681 %/day)
(L_o - TT = 1.845804 %/day)

a. Mass Point

$$(0.155734 + 1.981938 - 0.500) \le 1.854681 \le (0.155734 + 1.981938 + 0.500)$$

 $(1.637672) \le 1.854681 \le (2.637672)$

b. Total Time

$$(0.151511 + 1.981938 - 0.500) \le 1.845804 \le (0.151511 + 1.981938 + 0.500)$$

 $(1.633449) \le 1.845804 \le (2.633449)$

The Superimposed Leakage Verification Test met the requirements set forth in Reference 2.

3.3.2.4 Leakage Penalties Added to Type A Leakage

Penetration leakage to be added since these penetrations were isolated or could not be vented and drained during the Type A test. The leakage assigned is the recorded value for minimum pathway analysis.

i.	Type B & C Pena	llties <u>Description</u>	Leakage <u>SCCM</u>
	X-23A	RBCCW Inlet	. 1400.
	X-23B	RBCCW Inlet	575.
	X-24B	RBCCW Outlet	1000.
	X-24A	RBCCW Outlet	110.
	X-9A	Feedwater	< 110.
	X-9B	Feedwater	< 150.
	X-10	RCIC Steam	0.
	X-11	HPCI Steam	0.
	X-16B	Core Spray	< 110.
	X-16A	Core Spray	250.
	X-32D	N ₂ Comp Suction	0.
	X-36	CRD Return	125.
	X-32E	Recirc. Pump Seal	0.
	X-32F	Recirc. Pump Seal	0.
	X-40C	Jet Pump	< 150.
	X-40D	Jet Pump	<90.
	X-41	Recirc. Loop Sample	<35.
	X-229H	PASS	<240.
	X-219	HPCI/RCIC Vac. Br.	410.
	X-21	Service Air	25.

Total Type B & C Leakage 4780 SCCM Total Type B & C Leakage 0.030150 percent/day

ii.	Water Level Corrections	Description	<u>Gallons</u>
		Rx Vessel	0.0
	•	D.W. Equipment Sump	4772.2
		D.W. Floor Sump	0.0
		Torus	0.0

Total Water Level Corrections 4772.2 Gallons
Total Water Level Corrections 0.003108 percent/day

üi	Total Corrections	<u>Description</u>	Leakage Percent/Day
	Total Type A Corrections (i. and ii.)	Penalties and Corrections	0.033258

12/15/88	08:15								
RTD 1 77.454 RTD 11 85.412 DC 6 155.45	RTD 2 77.400 RTD 12 95.773 RTD 1 77.45	76.627 RTD 13 136.590 RTD 3		RTD 15	85.564 DC 1 164.23 PRESS 3	RTD 7 92.826 DC 2 160.77	RTD 8 92.511 DC 3 159.52	103.680 DC 4	RTD 10 103.130 DC 5 154.07
12/15/88	08:30				,				
RTD 1 77.361 RTD 11 85.451 DC 6 155.30	RTD 1	RTD 3	PRESS 1	86.115 RTD 15		92.844 DC 2	DC 3		DC 5
12/15/88	08:45								
RTD 1 77.236 RTD 11 85.498 DC 6 155.18	RTD 1	RTD 3	PRESS 1		85.695 DC 1 163.82 PRESS 3	RTD 7 92.871 DC 2 160.92	DC 3	104.000	DC 5
12/15/88	09:00								
RTD 1 77.150 RTD 11 85.544 DC 6 155.06	RTD 1	RTD 3	PRESS 1	RTD 15		RTD 7 92.903 DC 2 161.14	DC 3	RTD 9 104.140 DC 4 157.82	DC 5
12/15/88	09:15								
RTD 1 77.062 RTD 11 85.598 DC 6 154.89	RTD 2 77.007 RTD 12 96.045 1 RTD 1 77.06	76.248 RTD 13 136.870 RTD 3	PRESS 1	86.283	PRESS 3	RTD 7 92.926 DC 2 161.24	92.663 DC 3	104.320	RTD 10 103.740 DC 5 153.60

12/15/88	09:30								·
RTD 1 76.976 RTD 11 85.641 DC 6 154.74	RTD 2 76.933 RTD 12 96.131 RTD 1 76.98	RTD 3	PRESS 1	RTD 5 86.337 RTD 15 106.910 PRESS 2 59.1317	DC 1 164.92 PRESS 3	RTD 7 92.969 DC 2 161.27	DC 3	104.440	DC 5
12/15/88	09:45								
RTD 1 76.899 RTD 11 85.716 DC 6 154.63	RTD 1		PRESS 1	RTD 5 86.412 RTD 15 107.030 PRESS 2 59.1305		RTD 7 93.066 DC 2 161.42	RTD 8 92.826 DC 3 160.30	RTD 9 104.590 DC 4 157.93	
12/15/88	10:00								
RTD 1 76.824 RTD 11 85.739 DC 6 154.52	RTD 2 76.781 RTD 12 96.252 RTD 1 76.82	RTD 3	PRESS 1	RTD 5 86.423 RTD 15 107.190 PRESS 2 59.1302	85.933 DC 1 164.77 PRESS 3	93.098 DC 2	DC 3	RTD 9 104.750 DC 4 158.05	DC 5
12/15/88	10:15								
RTD 1 76.758 RTD 11 85.825 DC 6 154.42	RTD 1	RTD 3	PRESS 1	RTD 5 86.500 RTD 15 107.350 PRESS 2 59.1293	85.988 DC 1 164.59 PRESS 3	RTD 7 93.132 DC 2 161.40	DC 3	RTD 9 104.890 DC 4 158.23	
12/15/88	10:30								
RTD 1 76.688 RTD 11 85.843 DC 6 154.36	RTD 12 96.399 RTD 1	75.862 RTD 13 137.170 RTD 3	76.275 RTD 14 141.750 PRESS 1		PRESS 3	93.191 DC 2		105.040 DC 4	104.450 DC. 5

12/15/88	10:45								
RTD 1 76.617 RTD 11 85.868 DC 6 154.24	RTD 2 76.595 RTD 12 96.481 RTD 1 76.62	RTD 3		86.598 RTD 15			RTD 8 92.969 DC 3 160.70	105.190 DC 4	DC 5
12/15/88	11:00								
RTD 1 76.568 RTD 11 85.972 DC 6 154.17	RTD 1	RTD 3	PRESS 1	RTD 5 86.648 RTD 15 107.780 PRESS 2 59.1297	DC 1 165.38 PRESS 3	RTD 7 93.279 DC 2 161.95	DC 3	RTD 9 105.330 DC 4 158.47	104.710 DC 5
12/15/88	11:15								
RTD 1 76.509 RTD 11 85.999 DC 6 154.09	RTD 2 76.475 RTD 12 96.633 RTD 1 76.51	137.360 RTD 3		86.695 RTD 15		RTD 7 93.316 DC 2 161.88		RTD 9 105.470 DC 4 158.60	RTD 10 104.880 DC 5 153.03
12/15/88	11:30								
RTD 1 76.454 RTD 11 86.076 DC 6 154.02	RTD 1	RTD 3	PRESS 1	RTD 5 86.727 RTD 15 108.080 PRESS 2 59.1312		93.404 DC 2	DC 3	RTD 9 105.590 DC 4 158.65	DC 5
12/15/88	11:45								
RTD 1 76.400 RTD 11 86.085 DC 6 153.95	RTD 2 76.366 RTD 12 96.773 RTD 1 76.40	75.595 RTD 13 137.430 RTD 3	76.027 RTD 14 142.060 PRESS 1	86.781	DC 1 165.63 PRESS 3	RTD 7 93.436 DC 2 162.30		105.730 DC 4	RTD 10 105.110 DC 5 152.99

12/15/88	12:00								
RTD 1 76.357 RTD 11 86.140 DC 6 153.85	RTD 1	RTD 3	PRESS 1		86.337 DC 1 165.89 PRESS 3	RTD 7 93.479 DC 2 162.71	RTD 8 93.207 DC 3 161.08	105.860 DC 4	
12/15/88	12:15								
RTD 1 76.302 RTD 11 86.194 DC 6 153.80	RTD 12 96.905 1 RTD 1	RTD 3	75.928 RTD 14 142.020 PRESS 1	PRESS 2	86.392 DC 1 165.88		93.284 DC 3	RTD 9 106.000 DC 4 158.80	DC 5
12/15/88	12:30								
RTD 1 76.250 RTD 11 86.228 DC 6 153.72	RTD 1	RTD 3	75.864 RTD 14 142.120 PRESS 1	RTD 15	86.426 DC 1 165.58 PRESS 3	RTD 7 93.579 DC 2 162.58	93.307 DC 3	106.130	DC 5
12/15/88	12:45								
RTD 1 76.225 RTD 11 86.260 DC 6 153.66	RTD 2 76.194 RTD 12 97.045 RTD 1 76.22	RTD 3	75.850 RTD 14 142.170 PRESS 1	RTD 15	86.478 DC 1 166.09 PRESS 3	DC 2	93.295 DC 3	106.260 DC 4	DC 5
12/15/88	13:00								
RTD 1 76.182 RTD 11 86.314 DC 6 153.64	RTD 1	75.409 RTD 13 137.760 RTD 3	75.806 RTD 14 142.060 PRESS 1	87.033	DC 1 166.22 PRESS 3	RTD 7 93.685 DC 2 162.98		106.380 DC 4	DC 5

RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.139 76.105 75.355 75.763 87.076 86.575 93.708 93.393 106.490 105.870 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1										
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RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.489 97.349 137.910 142.260 109.280 166.41 163.24 161.79 159.40 152.63 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3 153.41 76.08 75.30 59.1200 59.1392 59.2015 12/15/88 14:00 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.046 76.014 75.253 75.668 87.224 86.723 93.844 93.606 106.850 106.240 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.516 97.399 138.000 142.260 109.410 166.71 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3 153.47 76.05 75.25 59.1214 59.1404 59.2027 12/15/88 14:15 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.019 75.976 75.237 75.641 87.260 86.761 93.903 93.653 106.980 106.330 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.555 97.480 138.050 142.270 109.490 166.71 163.57 161.86 159.54 152.53 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3	76.085	76.051	75.300	75.707	87.194	86.684	93.837	9 3.5 45	106.740	106.110
DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3 153.41 76.08 75.30 59.1200 59.1392 59.2015 12/15/88 14:00 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.046 76.014 75.253 75.668 87.224 86.723 93.844 93.606 106.850 106.240 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.516 97.399 138.000 142.260 109.410 166.71 163.39 161.79 159.39 152.60 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3 153.47 76.05 75.25 59.1214 59.1404 59.2027 12/15/88 14:15 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.019 75.976 75.237 75.641 87.260 86.761 93.903 93.653 106.980 106.330 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.555 97.480 138.050 142.270 109.490 166.71 163.57 161.86 159.54 152.53 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3		RTD 12	RTD 13	RTD 14	RTD 15	DC 1	DC 2	DC 3	DC 4	DC 5
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153.41 76.08 75.30 59.1200 59.1392 59.2015 12/15/88 14:00 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.046 76.014 75.253 75.668 87.224 86.723 93.844 93.606 106.850 106.240 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.516 97.399 138.000 142.260 109.410 166.71 163.39 161.79 159.39 152.60 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3 153.47 76.05 75.25 59.1214 59.1404 59.2027 12/15/88 14:15 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.019 75.976 75.237 75.641 87.260 86.761 93.903 93.653 106.980 106.330 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.555 97.480 138.050 142.270 109.490 166.71 163.57 161.86 159.54 152.53 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3	DC 6	RTD 1	RTD 3	PRESS 1	PRESS 2	PRESS 3				
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12/15/88 14:15 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 RTD 8 RTD 9 RTD 10 76.019 75.976 75.237 75.641 87.260 86.761 93.903 93.653 106.980 106.330 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.555 97.480 138.050 142.270 109.490 166.71 163.57 161.86 159.54 152.53 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3										
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RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 86.555 97.480 138.050 142.270 109.490 166.71 163.57 161.86 159.54 152.53 DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3										
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DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3										
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12/15/88	14:30								
RTD 1 75.992 RTD 11 86.602 DC 6 153.31	RTD 1	RTD 3	PRESS 1	RTD 5 87.319 RTD 15 109.650 PRESS 2 59.1434	DC 1 166.77 PRESS 3	93.930 DC 2	D C 3		RTD 10 106.450 DC 5 152.52
12/15/88	14:45								
RTD 1 75.958 RTD 11 86.645 DC 6 153.23	RTD 1	RTD 3	PRESS 1	87.353 RTD 15	167.11 PRESS 3	93.973 DC 2	DC 3	RTD 9 107.220 DC 4 159.67	106.550 DC 5
12/15/88	15:00								
RTD 1 75.942 RTD 11 86.673 DC 6 153.23	RTD 1	RTD 3	PRESS 1	87.412 RTD 15	166.81 PRESS 3	94.023 DC 2	DC 3	107.370 DC 4	DC 5
12/15/88	15:15				,				
RTD 1 75.910 RTD 11 86.727 DC 6 153.27	RTD 1	RTD 3	PRESS 1	87.466 RTD 15	DC 1 167.33 PRESS 3	94.077 DC 2	93.837 DC 3	107.470 DC 4	DC 5
12/15/88	15:30								
RTD 1 75.894 RTD 11 86.800 DC 6 153.20	RTD 1	75.123 RTD 13 138.300 RTD 3	PRESS 1		DC 1 167.06 PRESS 3			107.600 DC 4	DC 5

12/15/88	15:45								
RTD 1 75.878 RTD 11 86.836 DC 6 153.13	97.882 1 RTD 1	75.117 RTD 13 L38.320 RTD 3	PRESS 1	87.543 RTD 15	167.31 PRESS 3	94.152 DC 2	DC 3	RTD 9 107.690 DC 4 159.99	DC 5
12/15/88	16:00								
RTD 1 75.849 RTD 11 86.886 DC 6 153.04	RTD 12 97.941 1 RTD 1	RTD 3	PRESS 1		DC 1 167.34 PRESS 3	RTD 7 94.211 DC 2 163.97	DC 3	RTD 9 107.810 DC 4 160.19	DC 5
12/15/88	16:15								
RTD 1 75.824 RTD 11 86.924 DC 6 153.07	RTD 12	RTD 3	PRESS 1		PRESS 3	RTD 7 94.241 DC 2 164.29	RTD 8 93.980 DC 3 162.54	DC 4	RTD 10 107.220 DC 5 152.31

Time (hh:mm)	Press. (PSIA)	V.P. (PSI)	Temp. (R)	Dewpoint (F)	Mass (LbM)
08:15	59.128	0.4440	551.124	75.987	59021.99
08:30	59.126	0.4442	551.120	75.997	59 0 20.41
08:45	59.125	0.4440	551.116	75.9 83	59019.48
09:00	59.123	0.4447	55 1.10 4	76.035	59018.79
09:15	59.122	0.4442	551.099	76.001	59018 .66
09:30	5 9.12 2	0.44 42	551 .0 9 9	76.00 2	59018.09
09:45	59.121	0.444 4	551.111	76.012	590 1 5. 7 7
10:0 0	59.120	0.4446	551.112	76.027	59015.13
10:15	59.120	0.44 42	551.126	76.000	59013.37
10:30	59.120	0.4449	551.118	76.048	59 013 .57
10:45	5 9.12 0	0.4450	551.141	76.053	5 901 0. 9 5
11: 0 0	59.120	0.4452	551.149	76.065	59010.11
11:15	59.120	0.4448	551. 16 0	76.038	590 0 9.62
11:30	59.121	0.4461	551.171	7 6.13 0	59007.96
11:45	59.121	0.4459	551.181	76.1 1 4	590 07. 3 0
12:00	59.123	0.4466	5 51.19 5	76.162	59006.35
12:15	59.12 3	0.4464	551.204	76.14 7	5 90 06. 3 2
12:30	5 9.12 4	0.4462	551.208	76.138	59006.88
12:45	59.125	0.4475	551.231	76.222	590 03 .87
13:00	59.126	0.4476	551.241	76.22 7	590 03.98
1 3:1 5	59.127	0.4475	5 51.269	76.224	59002.14
13:30	59.129	0.4474	551.288	76.218	590 01.6 4
13:45	59.130	0.4482	551.314	76.272	58999.01
14:00	59.131	0.4487	551.328	76. 3 02	589 98 .4 7
14:15	59.132	0.4 49 0	5 51.3 41	76.327	58998.19
14:30	59.134	0.4486	551.369	76.298	58997.16
14:45	5 9.13 5	0.4483	551.37 5	76.279	58998.24
15:00	59.137	0.4497	551.401	76.369	5 8995 .9 3
15:15	59.139	0.4500	551.418	76.389	58995.55
15:30	59.140	0.4507	551.4 49	76.440	58 992. 8 6
15:45	59.142	0.4504	551.469	76.419	58992.78
16:00	59.144	0.4503	551.489	76.410	58992. 2 1
16:15	59.145	0.4515	551.499	76.492	58991.78

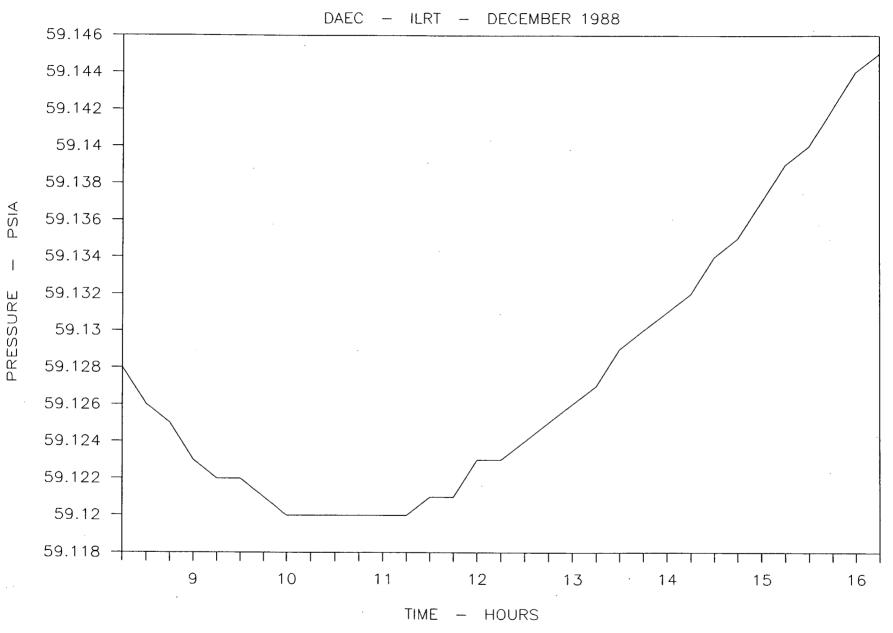
Duane Arnold Energy Center - 1988 ILRT FROM 08:15 HOURS TO 16:15 HOURS ON 12/15/88 ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS

Time (hh:mm)	Mass (LbM)	Leakage (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
08:15	59021.99	0.000000	0.000000	0.000000
08:30	59020.41	0.000000	0.000000	0.000000
08:45	59019.48	0.203669	0.263484	0.467153
09:00	59018.79	0.170824	0.068957	0.239781
09:15	59018.66	0.134604	0.058648	0.193251
09:30	59018.09	0.118087	0.040270	0.158357
09:45	59015.77	0.140057	0.037116	0.177173
10:00	59015.13	0.146242	0.027567	0.173809
10:15	590 13.3 7	0.158436	0.024726	0.183162
10:30	5 9013.57	0.154216	0.019883	0.174099
10:45	59 01 0.95	0.164240	0.019201	0.183442
11:00	59010.11	0.168959	0.016550	0.185510
11:15	5900 9.62	0.168878	0.013860	0.182738
11:30	59007.96	0.171739	0.012141	0.183880
11:45	590 07. 30	0.171963	0.010450	0.182413
12:00	59006.35	0.171746	0.009091	0.180838
12:15	59006.32	0.168326	0.008699	0.177025
12:30	59006.88	0.161383	0.010404	0.171787
12:45	59003.87	0.161584	0.009274	0.170859
13:00	59003.98	0.159174	0.008661	0.167835
13:15	5 9002.1 4	0.159214	0.007812	0.167025
13:30	59001.64	0.158312	0.007139	0.165451
13:45	58999.01	0.160558	0.006874	0.167432
14:00	58998 .47	0.161550	0.006363	0.167913
14:15	589 98.1 9	0.161262	0.005849	0.167111
14:30	58997.16	0.161088	0.005392	0.166480
14: 45	58998.24	0.158277	0.005703	0.163980
15:00	58995.93	0.157636	0.005325	0.162961
15:15	58995.55	0.156453	0.005086	0.161538
15:30	58992.86	0.157308	0.004814	0.162122
15: 45	58992.78	0.157133	0.004501	0.161634
16:00	58992.21	0.156623	0.004244	0.160867
16:15	58991.78	0.155734	0.004077	0.159811

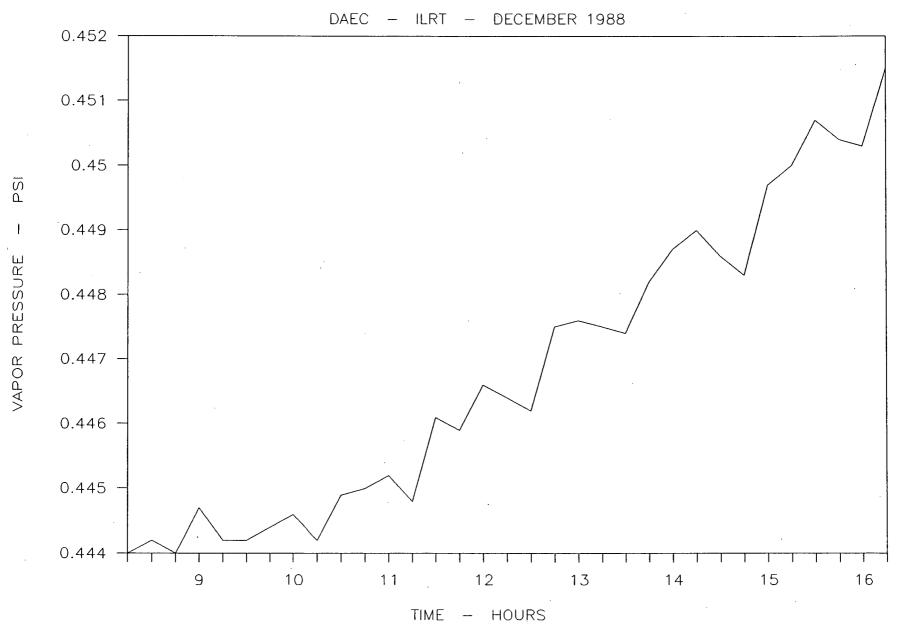
Duane Arnold Energy Center - 1988 ILRT FROM 08:15 HOURS TO 16:15 HOURS ON 12/15/88 ABSOLUTE TEST METHOD, TOTAL TIME ANALYSIS TEST RESULTS

Time (hh:mm)	Mass (LbM)	Meas.Leak. (PCT./DAY)	Calc.Leak. (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
08:15	59021.99	0.000000	0.000000	0.000000	0.000000
08:30	59020.41	0.257009	0.00000	0.000000	0.000000
08:45	59019.48	0.203669	0.000000	0.000000	0.000000
09:00	59018.79	0.173101	0.169305	0.090062	0.259367
09:15	59018.66	0.135467	0.133032	0.036593	0 .16 9626
09:30	59018.09	0.126659	0.113400	0.052275	0.165676
09:45	59015.77	0.168581	0.126643	0.109686	0.236328
10:00	59015.13	0.159418	0.130980	0.104520	0.235500
10:15	59013.37	0.175223	0.140885	0.104242	0.245128
10:30	59013.57	0.152114	0.139082	0.093758	0.232840
10:45	59010.95	0.179444	0.147579	0.092413	0.239992
11:00	59010.11	0.175546	0.152616	0.0 879 95	0.240611
11:15	5900 9.6 2	0.167581	0.154113	0.082535	0.236648
11:30	59007.96	0.175522	0.157528	0.078756	0.236283
11:45	59007.30	0.170577	0.158965	0 .0 7 4748	0.233712
12:00	59006.35	0.169563	0.159 9 06	0.071164	0.231070
12:15	59006.32	0.159269	0.158357	0.067714	0.226071
12:30	59006.88	0.144569	0.153978	0.065012	0.218989
12:45	59003.87	0.163701	0.154356	0.062 623	0.216979
13:00	59003.98	0.154166	0.152852	0.060223	0.213075
13:15	59002.14	0.161440	0.152985	0.058281	0.211266
13:30	59001.64	0.157595	0. 1524 49	0. 056 3 96	0.208845
13:45	58999.01	0.169887	0.154113	0.055303	0.209416
14:00	58998.47	0.166275	0.154975	0.053987	0.20 8 961
14:15	58998.19	0.161292	0.154958	0.052559	0.207517
14:30	58997.16	0.161540	0.155000	0.051249	0.206 25 0
14:45	5 8 9 98. 24	0.148563	0.153170	0.049 98 7	0.203157
15:00	58995.93	0.156990	0.152765	0.048807	0.201572
15:15	58995.55	0.153565	0.15 1 962	0.047672	0.199635
1 5:30	58992.86	0.163376	0.152553	0.046860	0.199414
15:45	58992.78	0.158355	0.152456	0.045928	0.198384
16:00	58992.21	0.156235	0.152122	0.045017	0.197138
16:15	58991.78	0.153525	0.151511	0.044132	0.195644

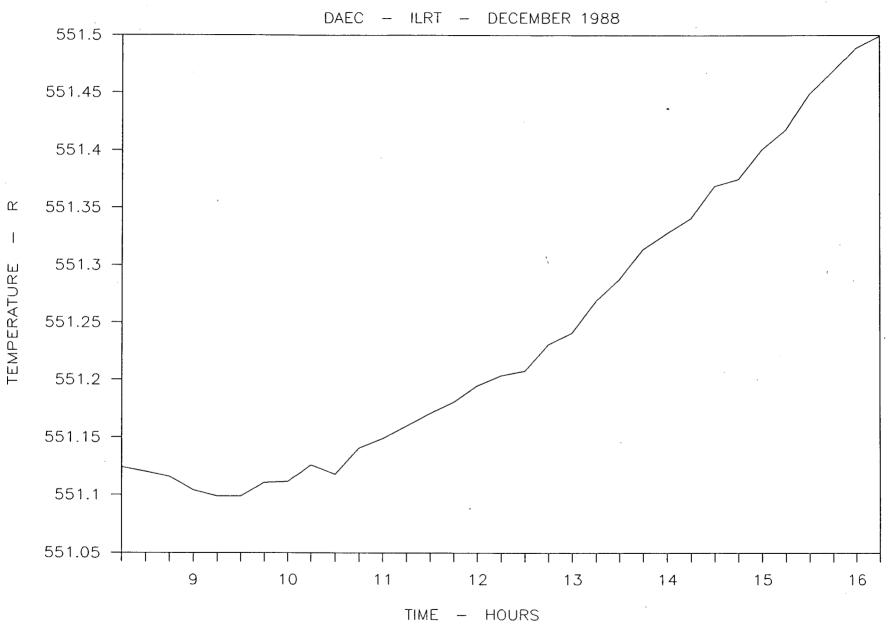
CONTAINMENT PRESSURE vs. TIME



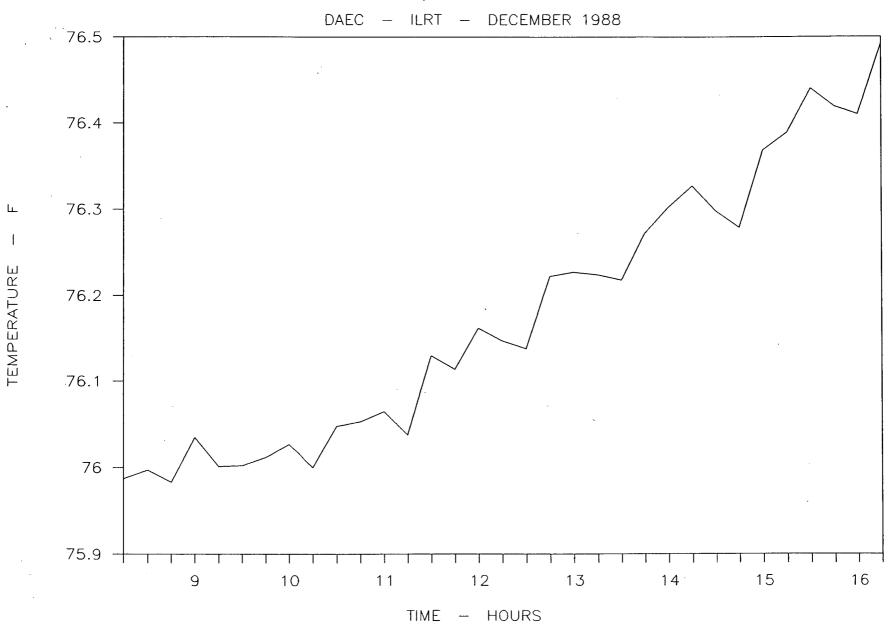
CONTAINMENT VAPOR PRESSURE vs. TIME



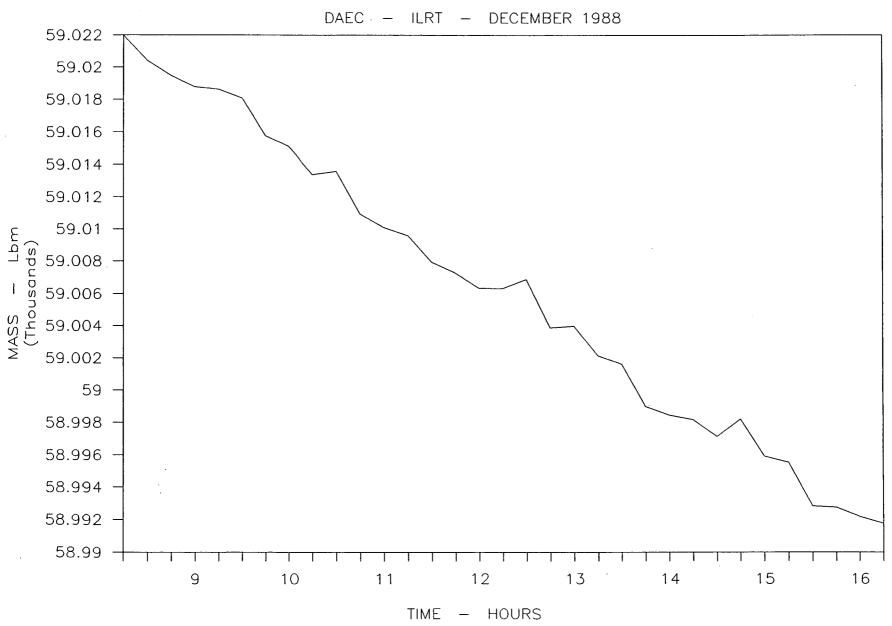
CONTAINMENT TEMPERATURE vs. TIME



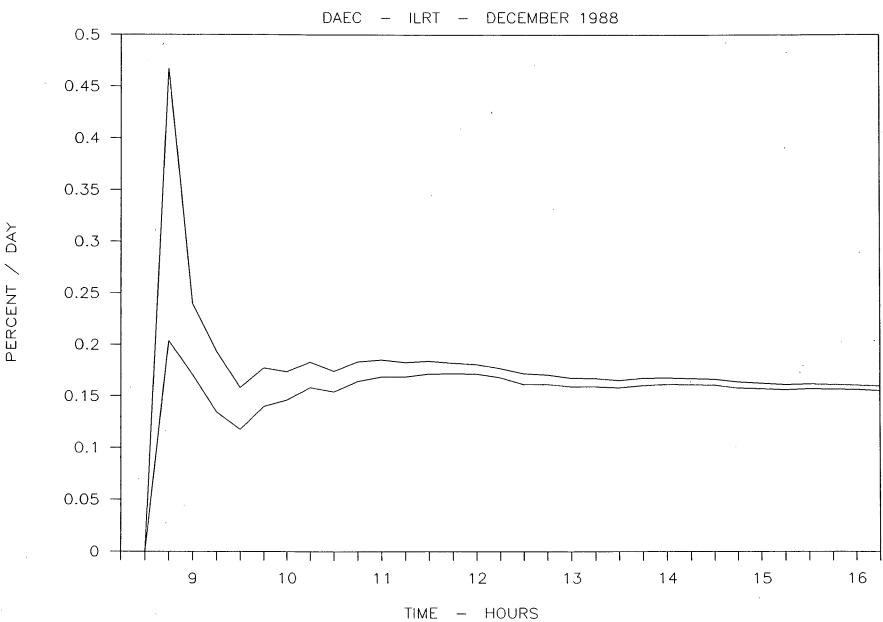
CONTAINMENT DEWPOINT TEMP. vs. TIME



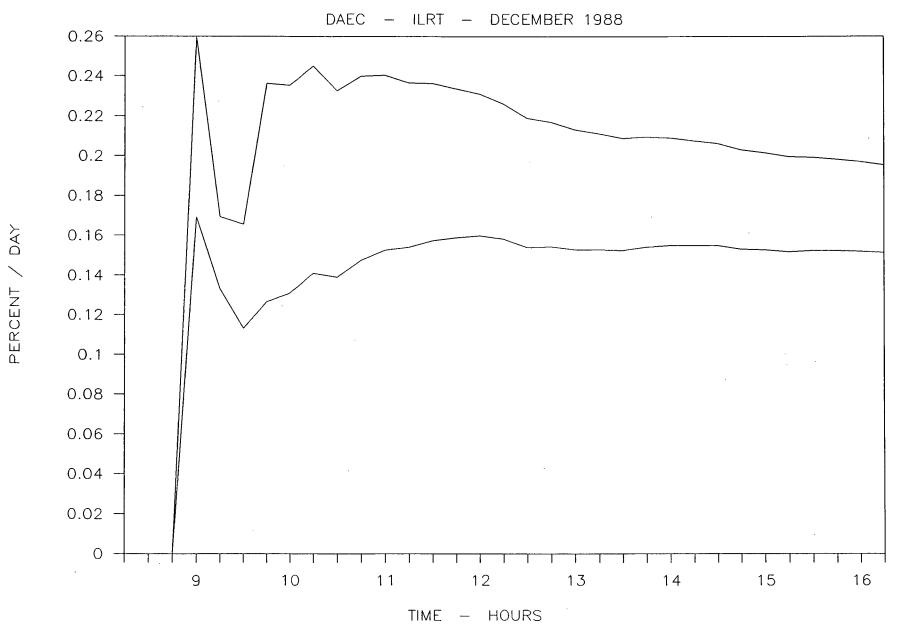
CONTAINMENT MASS vs. TIME



MASS POINT LEAKAGE & UCL



TOTAL TIME LEAKAGE & UCL



Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 VERIFICATION TEST MEASURED INPUT DATA

12/15/88	18:00								
RTD 1 75.665 RTD 11 87.201 DC 6 152.84	RTD 1	RTD 3	PRESS 1	87.940	PRESS 3	94.529 DC 2		RTD 9 108.670 DC 4 160.63	RTD 10 107.990 DC 5 152.18
12/15/88	18:15								
RTD 1 75.643 RTD 11 87.221 DC 6 152.79	RTD 2 75.599 RTD 12 98.508 RTD 1 75.64	RTD 3	PRESS 1	87.972 RTD 15		94.560 DC 2	DC 3	RTD 9 108.780 DC 4 160.63	DC 5
12/15/88	18:30								
RTD 1 75.618 RTD 11 87.283 DC 6 152.75	RTD 2 75.584 RTD 12 98.578 RTD 1 75.62	RTD 3	75.222 RTD 14 142.740 PRESS 1	88.022	PRESS 3	94.587 DC 2	94.327 DC 3	RTD 9 108.860 DC 4 160.68	RTD 10 108.180 DC 5 152.12
12/15/88	18:45								
RTD 1 75.627 RTD 11 87.337 DC 6 152.77	RTD 1	RTD 3	PRESS 1	RTD 5 88.065 RTD 15 111.580 PRESS 2 59.0962	PRESS 3	94.631 DC 2	94.361 DC 3	RTD 9 108.990 DC 4 160.77	108.310 DC 5
12/15/88	19:00								
RTD 1 75.595 RTD 11 87.357 DC 6 152.69	75.552 RTD 12 98.698 RTD 1	74.845 RTD 13 138.990 RTD 3	75.190 RTD 14 142.930 PRESS 1	RTD 5 88.096 RTD 15 111.670 PRESS 2 59.0875	87.564 DC 1 167.88 PRESS 3	RTD 7 94.653 DC 2 165.16	94.361 DC 3	109.090 DC 4	RTD 10 108.420 DC 5 152.09

Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 VERIFICATION TEST MEASURED INPUT DATA

12/15/88	19:15								
RTD 1 75.579 RTD 11 87.385 DC 6 152.68	RTD 1	RTD 3	PRESS 1	RTD 5 88.146 RTD 15 111.750 PRESS 2 59.0788	DC 1 168.36 PRESS 3	RTD 7 94.712 DC 2 165.35	RTD 8 94.420 DC 3 163.09		
12/15/88	19:30								
RTD 1 75.563 RTD 11 87.457 DC 6 152.68	RTD 1		PRESS 1	RTD 5 88.205 RTD 15 111.870 PRESS 2 59.0698	87.652 DC 1 168.85 PRESS 3	RTD 7 94.773 DC 2 165.11	RTD 8 94.490 DC 3 163.37	RTD 9 109.270 DC 4 161.06	RTD 10 108.590 DC 5 152.05
12/15/88	19:45								
RTD 1 75.545 RTD 11 87.471 DC 6 152.67	RTD 1	139.030 RTD 3	PRESS 1	88.232 RTD 15	DC 1 168.69 PRESS 3	94.767 DC 2		109.360 DC 4	RTD 10 108.710 DC 5 152.07
12/15/88	20:00								
RTD 1 75.541 RTD 11 87.532 DC 6 152.74	RTD 1	RTD 3	PRESS 1	88.271 RTD 15		94.805 DC 2	DC 3	RTD 9 109.480 DC 4 161.11	DC 5
12/15/88	20:15								
RTD 1 75.529 RTD 11 87.575 DC 6 152.62	RTD 1	74.790 RTD 13 139.200 RTD 3	75.124 RTD 14 143.000 PRESS 1	RTD 5 88.337 RTD 15 112.210 PRESS 2 59.0445	DC 1 168.88 PRESS 3	RTD 7 94.860 DC 2 165.38	94.544 DC 3	109.570 DC 4	RTD 10 108.880 DC 5 152.00

Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 VERIFICATION TEST MEASURED INPUT DATA

12/15/88	20:30							
RTD 1 75.509 RTD 11 87.598 DC 6 152.60	75.475 74 RTD 12 RT 99.068 139 RTD 1 F	RTD 3 RTD 4 1.770 75.112 TD 13 RTD 14 1.180 143.090 RTD 3 PRESS 1 74.77 59.0165	88.348 RTD 15 112.280 PRESS 2	87.827 DC 1 168.98 PRESS 3	RTD 7 94.903 DC 2 165.54	94.676 DC 3	RTD 9 109.670 DC 4 161.35	
12/15/88	20:45							
RTD 1 75.497 RTD 11 87.618 DC 6 152.63	75.454 74 RTD 12 RT 99.122 139 RTD 1 F	RTD 3 RTD 4 2.758 75.101 RTD 13 RTD 14 2.230 143.130 RTD 3 PRESS 1 74.76 59.0079	88.414 RTD 15 112.340 PRESS 2	87.858 DC 1 168.94 PRESS 3	RTD 7 94.968 DC 2 165.73	94.676 DC 3	RTD 9 109.760 DC 4 161.39	DC 5
12/15/88	21:00							
RTD 1 75.470 RTD 11 87.657 DC 6 152.56	75.436 74 RTD 12 RT 99.170 139 RTD 1 R	RTD 3 RTD 4 2.740 75.073 RTD 13 RTD 14 2.290 143.100 RTD 3 PRESS 1 74.74 58.9993	88.427 RTD 15 112.450 PRESS 2	DC 1 169.09 PRESS 3	94.973 DC 2	94.724 DC 3	109.860 DC 4	RTD 10 109.180 DC 5 151.98
12/15/88	21:15							
RTD 1 75.475 RTD 11 87.706 DC 6 152.48	75.432 74 RTD 12 RT 99.242 139 RTD 1 R	TD 3 RTD 4 .736 75.080 TD 13 RTD 14 .370 143.170 RTD 3 PRESS 1 74.74 58.9909	RTD 15 112.530 PRESS 2	87.945 DC 1 168.94 PRESS 3	95.023 DC 2	DC 3	RTD 9 109.960 DC 4 161.43	DC 5
12/15/88	21:30							
RTD 1 75.459 RTD 11 87.743 DC 6 152.52	75.405 74 RTD 12 RT 99.301 139 RTD 1 R		88.536 RTD 15 112.660 PRESS 2	87.983 DC 1 169.03 PRESS 3	RTD 7 95.059 DC 2 165.61	94.755 DC 3	RTD 9 110.060 DC 4 161.58	

Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 VERIFICATION TEST MEASURED INPUT DATA

RTD 1	RTD 2	RTD 3	RTD 4	RTD 5	RTD 6	RTD 7	RTD 8	RTD 9	RTD 10
75.443	75.409	74.715	75.045	88.586	88.022	95,100	94.860	110.150	109.480
RTD 11	RTD 12	RTD 13	RTD 14	RTD 15	DC 1	DC 2	DC 3	DC 4	DC 5
87.804	99.360	139.490	143.180	112.770	169.38	166.01	163.94	161.59	151.93

DC 6 RTD 1 RTD 3 PRESS 1 PRESS 2 PRESS 3

152.49 75.44 74.72 58.9734 58.9921 59.0553

12/15/88 22:00

12/15/88 21:45

RTD 8 RTD 9 RTD 10 RTD 1 RTD 2 RTD 3 RTD 4 RTD 5 RTD 6 RTD 7 88.053 95.154 94.848 110.240 109.570 75.443 75.400 74.715 75.036 88.597 RTD 11 RTD 12 RTD 13 RTD 14 RTD 15 DC 1 DC 2 DC 3 DC 4 DC 5 87.827 99.426 139.480 143.170 112.860 169.47 166.23 163.87 161.66 151.93 DC 6 RTD 3 PRESS 1 PRESS 2 PRESS 3 RTD 1 152.45 75.44 74.72 58.9648 58.9840 59.0467

Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 VERIFICATION TEST REDUCED INPUT VARIABLES

Time (hh:mm)	Press. (PSIA)	V.P. (PSI)	Temp. (R)	Dewpoint (F)	Mass (LbM)
18:00 18:15 18:30 18:45 19:00 19:15 19:30 19:45 20:00 20:15 20:30 20:45 21:00 21:15 21:30	59.113 59.104 59.095 59.087 59.078 59.070 59.060 59.052 59.043 59.035 59.026 59.017 59.009 59.000 58.991	0.4531 0.4540 0.4521 0.4535 0.4540 0.4545 0.4545 0.4553 0.4552 0.4555 0.4559 0.4566 0.4566	551.632 551.657 551.676 551.704 551.726 551.740 551.765 551.787 551.811 551.834 551.860 551.878 551.890 551.930 551.942	76.596 76.655 76.655 76.627 76.659 76.693 76.689 76.743 76.739 76.754 76.785 76.845 76.845 76.830 76.824 76.831	58943.33 58930.95 58921.84 58908.87 58897.35 58886.84 58875.06 58863.54 58852.25 58841.14 58828.88 58817.33 58807.68 58794.82 58784.64
21:45 22:00	58.983 58.974	0.4576	551.972 551.988	76.831 76.897 76.929	58771.80 58761.25

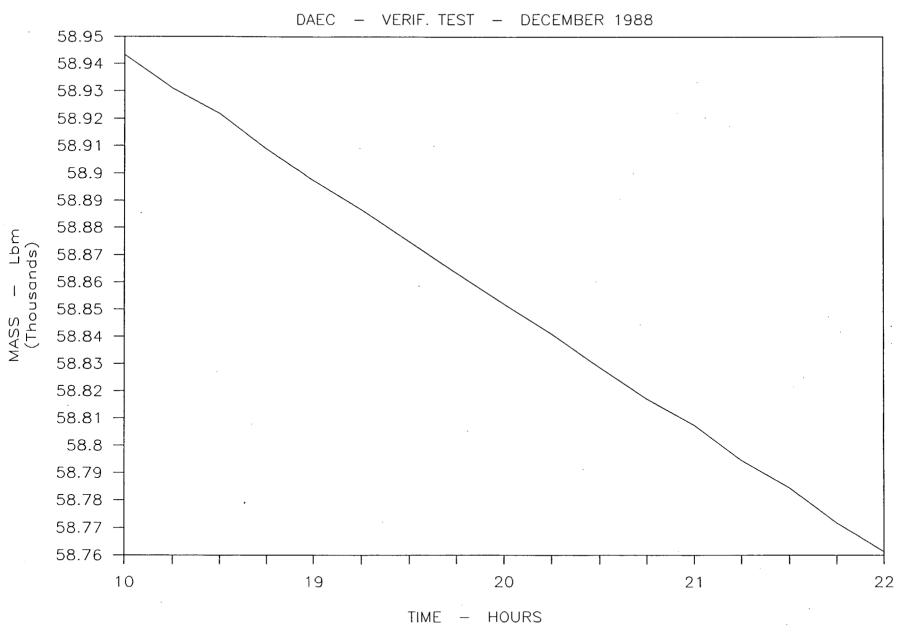
Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS VERIFICATION TEST

Time (hh:mm)	Mass (LbM)	Leakage (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
18:00 18:15	58943.33 58930.95	0.000000	0.000000	0.000000 0.000000
18:30	58921.84	1.749963	1.312447	3.062410
18:45	58908.87	1.832031	0.245316	2.077347
19:00	58897.35	1.857540	0.118531	1.976071
19:15	58886.84	1.843928	0.072227	1.916156
19:30	58875.06	1.847081	0.048413	1.895494
19:45	58863.54	1.850772	0.035044	1.885816
20:00	58852.25	1.851683	0.026485	1.878168
20:15	58841.14	1.849889	0.020827	1.870716
20:30	58828.88	1.855538	0.017799	1.873337
20:45	58817.33	1.859783	0.015302	1.875085
21:00	58807.68	1.852900	0.014670	1.867570
21:15	58794.82	1.855456	0.012742	1.868198
21:30	58784.64	1.852162	0.011471	1.863634
21:45	58771.80	1.855234	0.010455	1.865689
22:00	58761.25	1.854681	0.009194	1.863876

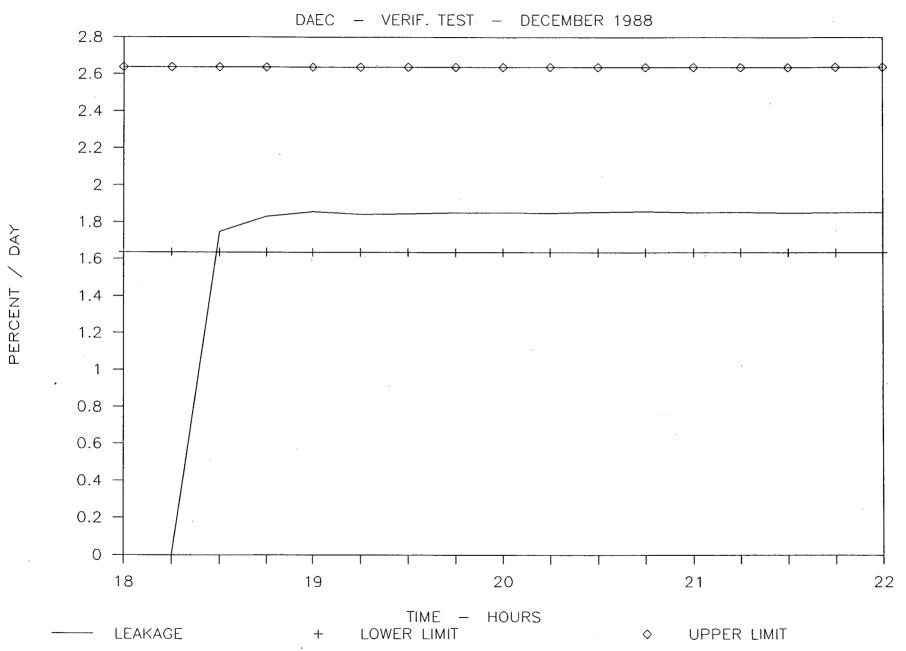
Duane Arnold Energy Center - 1988 ILRT FROM 18:00 HOURS TO 22:00 HOURS ON 12/15/88 ABSOLUTE TEST METHOD, TOTAL TIME ANALYSIS TEST RESULTS VERIFICATION TEST

Time (hh:mm)	Mass (LbM)	Meas.Leak. (PCT./DAY)	Calc.Leak. (PCT./DAY)	Confidence (PCT./DAY)	UCL (PCT./DAY)
18:00	58943.33	0.000000	0.000000	0.00000	0.000000
18:15	58930.95	2.015640	0.000000	0.000000	0.000000
18:30	58921.84	1.749947	0.000000	0.000000	0.000000
18:45	58908.87	1.870666	1.806264	1.528234	3.334497
19:00	58897.35	1.872378	1.830797	0.621687	2.452484
19:15	58886.84	1.840144	1.824043	0.395901	2.219943
19:30	58875.06	1.853243	1.828454	0.304112	2.132566
19:45	58863.54	1.856440	1.833187	0.252673	2.085860
20:00	58852.25	1.854208	1.835664	0.218655	2.054319
20:15	58841.14	1.849327	1.835773	0.194130	2.029904
20:30	58828.88	1.863971	1.841150	0.177205	2.018355
20:45	58817.33	1.865537	1.845660	0.163663	2.009323
21:00	58807.68	1.841158	1.841906	0.151640	1.993546
21:15	58794.82	1.860603	1.844518	0.142451	1.986969
21:30	58784.64	1.846068	1.842873	0.134132	1.977005
21:45	58771.80	1.862431	1.845607	0.127662	1.973268
22:00	58761.25	1.853492	1.845804	0.121594	1.967398

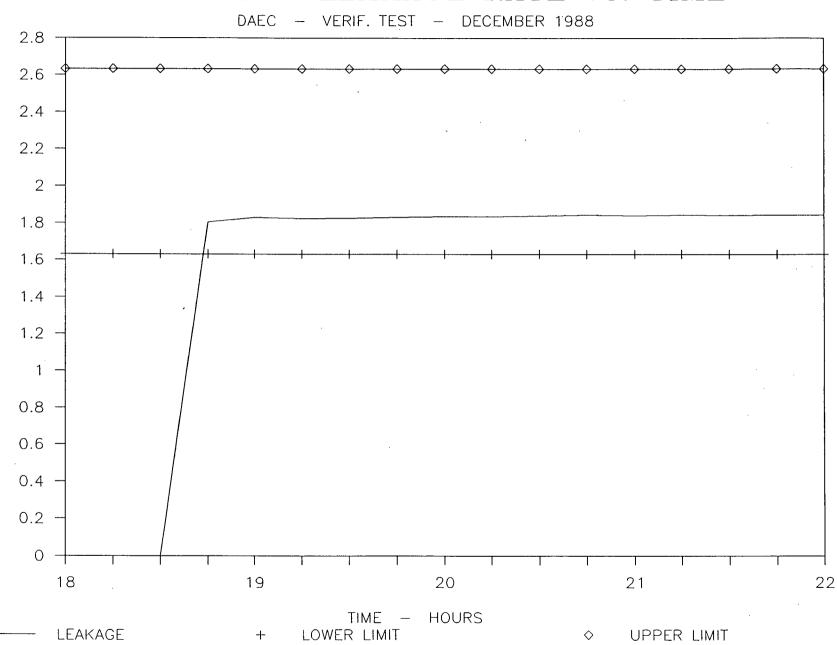
CONTAINMENT MASS vs. TIME



MASS POINT LEAKAGE RATE vs. TIME



TOTAL TIME LEAKAGE RATE vs. TIME



PERCENT / DAY

SECTION 4

LOCAL LEAKAGE RATE TESTS (TYPES B AND C)

Section 4 summarizes the results of the Local Leakage Rate Test's (LLRT's) data which has been obtained from periodic testing performed since the June 1987 Periodic Type A test. Maintenance data is provided for surveillance testing performed in 1988. Each penetration's leakage rate can be obtained from site reference material.

Attachment 4B contains an analysis of the containment penetrations that were repaired during the 1988 Refueling Outage to assess the as found containment condition.

The acceptance criteria for Types B and C testing are in accordance with 10CFR50, Appendix J. The combined as left leakage rate for all penetrations and valves, subject to Types B and C tests in 1988, were well below the acceptance criteria of less than $0.60L_a$.

The data contained in this section are summarized below:

Attachment No.	<u>Title</u>
4A	1988 Local Leakage Rate Test Data
4B	1988 Local Leakage Rate Test Summary Analysis.

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
	Testable Gaskets (Type B)					
X-1	Drywell Personnel Airlock	В	Airlock	6441/06-04-88 7572/08-26-88 4197/12-14-88 1235/12-23-88	6441/06-04-88 7572/08-26-88 4197/12-14-88 1235/12-23-88	
X-1	Drywell Airlock Hatch	В	Gaskets	<150/10-13-88	<150/10-13-88	
X-2	Equipment Access Hatch	В	Gaskets	0/10-01-88	380/12-12-88	Replaced O-Rings
X-4	Drywell Head Access Hatch	В	Gaskets	<25/10-13-88	<25/10-13-88	
X-6	CRD Removal Hatch	В	Gaskets	0/09-30-88	0/12-14-88	Replaced O-Rings
X-35A	TIP Drive	В	Gaskets	0/10-27-88	0/10-27-88	
X-35B	TIP Drive	В	Gaskets	0/10-27-88	0/10-27-88	
X-35C	TIP Drive	В	Gaskets	0/10-27-88	0/10-27-88	
X-35D	TIP Purge Line	В	Gaskets	0/10-27-88	0/10-27-88	
X-53	Spare	В	Gaskets	0/09-29-88	0/11-17-88	Replaced O-Rings
	Drywell Head	В	Gaskets	<18/09-30-88	0/12-02-88	Replaced O-Rings
X-58A	Stabilizer Access Port	В	Gaskets	240/10-17-88	240/10-17-88	
X-58 B	Stabilizer Access Port	В	Gaskets	<240/10-17-88	<240/10-17-88	
X-58C	Stabilizer Access Port	В	Gaskets	<240/10-17-88	<240/10-17-88	

Pen No.	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-58D	Stabilizer Access Port	В	Gaskets	2475/10-17-88	<200/11-12-88	Replaced O-Rings
X-58E	Stabilizer Access Port	В	Gaskets	<240/10-17-88	<240/10-17-88	
X-58F	Stabilizer Access Port	В	Gaskets	<240/10-17-88	<240/10-17-88	
X-58G	Stabilizer Access Port	В	Gaskets	<240/10-17-88	<240/10-17-88	
X-58H	Stabilizer Access Port	В	Gaskets	285/11-12-88	<200/10-17-88	Replaced O-Rings
N-200A	Torus Access Hatch - South	В	Gaskets	0/09-29-88	25/11-21-88	Replaced O-Rings
N-200B	Torus Access Hatch - North	В	Gaskets	0/09-29-88	0/12-17-88	Replaced O-Rings
	Electrical Canisters (Type B)					
X-100B	Neutron Monitoring	В	Electrical Pen.	0/10-14-88	0/10-14-88	
X-100C	Neutron Monitoring	В	Electrical Pen.	0/10-14-88	0/10-14-88	
X-100E	Neutron Monitoring	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-100F	Neutron Monitoring	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-100G	RPV Vibration Monitoring	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	•
X-101A	Recirc. Pump Power	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-101C	Recirc. Pump Power	В	Electrical Pen.	<80/10-14-88	<80/10-14-88	
X-103	Thermocouple	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-104A	CRD Rod Position Indication	В	Electrical Pen.	<150/10-13 -88	<150/10-13-88	

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-104B	CRD Rod Position Indication	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-104C	CRD Rod Position Indication	В	Electrical Pen.	0/10-14-88	0/10-14-88	
X-104D	CRD Rod Position Indication	В	Electrical Pen.	0/10-14-88	0/10-14-88	
X-105B	Power & Control	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-105D	Power & Control	В	Electrical Pen.	<80/10-14-88	<80/10-14-88	
X-106A	Power & Control	В	Electrical Pen.	<150/10-13-88	<150/10-13-88	
X-106C	Power & Control	В.	Electrical Pen.	<80/10-14-88	<80/10-14-88	
N-230B	Vacuum Breaker Cables	В	Electrical Pen.	<110/10-13-88	<110/10-13-88	
	Flange O-Rings (Type B)					
X-25	Drywell Purge Outlet	В	CV-4302	1150/09-30-88	1550/10-26-88	Replaced Test Fitting
X-26	Drywell Purge Outlet	В	CV-4307	0/10-08-88	0/10-08-88	
N-220	Torus Purge Supply	В	CV-4308	0/10-08-88	0/10-08-88	
N-205	Torus Purge Outlet	В	CV-4300	<110/10-11-88	<110/10-11-88	
N-213A	Torus Drain Line Flange - South	В	Flange	<240/10-14-88	<240/10-14-88	
N-213B	Torus Drain Line Flange - North	В	Flange	<110/10-13-88	<110/10-13-88	

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
N-231	RB/Torus Vacuum Breaker	В	CV-4304	<110/10-11-88	<110/10-11-88	
N-231	RB/Torus Vacuum Breaker	В	CV-4305	<110/10-11-88	<110/10-11-88	
	Expansion Bellows (Type B)					
X-7A	Steam to Turbine	В	Bellows	<110/10-08-88	<110/10-08-88	
X-7B	Steam to Turbine	В	Bellows	0/10-08-88	0/10-08-88	
X-7C	Steam to Turbine	В	Bellows	<150/10-08-88	<150/10-08-88	
X-7D	Steam to Turbine	В	Bellows	<110/10-08-88	<110/10-08-88	
X-9A	RPV Feedwater	В	Bellows	<110/10-08-88	<110/10-08-88	
X-9B	RPV Feedwater	В	Bellows	<150/10-08-88	<150/10-08-88	
X-10	Steam to RCIC Turbine	В	Bellows	0/10-08-88	0/10-08-88	
X-11	Steam to HPCI Turbine	В	Bellows	0/10-08-88	0/10-08-88	
X-12	Shutdown Pump Supply RHR	В	Bellows	<240/10-15-88	<240/10-15-88	
X-13A	RHR Pump Discharge	В	Bellows	<240/10-15-88	<240/10-15-88	
X-13B	RHR Pump Discharge	В	Bellows	<240/10-15-88	<240/10-15-88	
X-15	RWCU Supply	В	Bellows	<110/10-25-88	<110/10-25-88	
X-16A	Core Spray Pump Discharge	В	Bellows	<110/10-15-88	<110/10-15-88	
X-16B	Core Spray Pump Discharge	В	Bellows	0/10-13-88	0/10-13-88	

Pen <u>No.</u>	System Name	Test Type	Equipment/ <u>Valves (Note 1)</u>	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-17	RPV Head Spray	В.	Bellows	<100/10-17-88	<100/10-17-88	
N-201A	Vent Line	В	Bellows	<240/10-13-88	<240/10-13-88	
N-201B	Vent Line	В	Bellows	<250/10-13-88	<250/10-13-88	
N-201C	Vent Line	В	Bellows	<240/10-13-88	<240/10-13-88	
N-201D	Vent Line	В	Bellows	<250/10-13-88	<250/10-13-88	
N-201E	Vent Line	В	Bellows	<110/10-13-88	<110/10-13-88	
N-201F	Vent Line	В	Bellows	<110/10-13-88	<110/10-13-88	
N-201G	Vent Line	В	Bellows	<110/10-13-88	<110/10-13-88	
N-201H	Vent Line	В	Bellows	<110/10-13-88	<110/10-13-88	
N-213A	Torus Drain Line Bellows - Inboard (South)	В	Bellows	<240/10-14-88	<240/10-14-88	
N-213A	Torus Drain Line Bellows - Outboard (South)	В	Bellows	<240/10-14-88	<240/10-14-88	
N-213B	Torus Drain Line Bellows - Inboard (North)	В	Bellows	<110/10-14-88	<110/10-14-88	
N-213B	Torus Drain Line Bellows - Outboard (North)	В	Bellows	<110/10-13-88	<110/10-13-88	

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
	Valve Bonnets (Type B)					
X-39A	Drywell Spray	В	MO-2000	<110/09-30-88	<110/09-30-88	
X-39B	Drywell Spray	В	MO-1902	<200/09-30-88	<200/09-30-88	
N-211A	Torus Spray	В	MO-1933	<100/09-30-88	<100/09-30-88	
N-211B	Torus Spray	В	MO-2006	<110/09-30-88	<110/09-30-88	
	Shaft Stem Seals (Type B)					
X-26	Drywell Purge Supply	В	CV-4307	22,000/10-08-88	<150/10-29-88	Replaced O-Rings
N-220	Torus Purge Supply	В	CV-4308	2,680/10-08-88	0/10-29-88	Replaced O-Rings

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
	Local Leakage Rate Tests (Ty	pe C)				
X-7A	"A" Main Steam Line	С	CV-4412(IPC)	17,000/10-02-88	350/12-03-88	Internals oversized, replaced stem and reworked seats
			CV-4413(OPC)	351,160/10-01-88	(Combined)	Internals oversized, valve re-bored, reworked seats, spring guide replaced, three springs replaced, stem replaced
X-7B	"B" Main Steam Line	С	CV-4415(IPC)	6,300/10-02-88	750/12-10-88	Internals replaced, reworked seats, replaced stem and torqued packing
			CV-4416(OPC)	<80/10-01-88	(Combined)	
X-7C	"C" Main Steam Line	С	CV-4418(IPC)	700/10-02-88	1310/12-10-88	Dressed and repacked
			CV-4419(OPC)	6,200/10-01-88	890/12-14-88	Valve re-bored, internals oversized, stem replaced, reworked seats, pilot seat in disk remachined and stem disk machined

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-7D	"D" Main Steam Line	С	CV-4420(IPC)	19,000/10-02-88	<95/12-03-88	Internals replaced and machined, seats reworked and packing adjusted
			CV-4421 (OPC)	0/10-02-88	(Combined)	Piston and disk oversized
X-8	Steam Drain	С	MO-4423(IPC)	0/10-03-88	0/10-03-88	
			MO-4424(OPC)	14,000/10-03-88	<150/12-20-88	Wedge machined, seat narrowed, repacked valve, MOVATS tested
X-9A	Feedwater	С	V-14-3(IPC)	384,500/10-05-88	<110/12-09-88	Soft seat installed and stuffing box conversion per DCP-1422
			MO-4441(OPC)	2,000/10-05-88	925/12-20-88	Replaced packing and installed live loading
			MO-2312(OPC)	(Combined)	(Combined)	MOVATS testing, new motor installed; cleaned and machined valve, reset limit switch

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-9B	Feedwater	С	V-14-1(IPC)	371,845/10-20-88	<150/12-02-88	Soft seat installed and stuffing box conversion per DCP-1422
			MO-4442(OPC)	132,000/10-20-88	3000/12-13-88	Replaced packing and installed live loading, repaired position indicator
	,		MO-2740(OPC)	(Combined)	(Combined)	Repacked and installed live loading, VOTES testing
			MO-2512(OPC)	(Combined)	(combined)	VOTES testing, MOVATS testing, replaced motor and adjusted torque
						switch
X-10	RCIC Condensate Return	С	CV-2410(IPC) CV-2411(OPC)	0/10-11-88 0/10-11-88	0/10-11-88 0/11-26-88	Replaced packing
X-10	RCIC Steam	С	MO-2400(IPC) CV-2401(OPC)	0/10-03-88 1,500/10-03-88	0/10-03-88 2,950/12-12-88	MOVATS testing MOVATS & VOTES testing, torque switch adjusted, repacked valve and installed live loading.
X-11	HPCI Condensate Return	С	CV-2211(IPC) CV-2212(OPC)	1,400/10-11-88 265/10-11-88	445/12-07-88 500/12-07-88	Replaced valve Replaced valve

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-11	HPCI Steam	С	MO-2238(IPC)	0/10-04-88	0/12-14-88	Valve disassembled, wedge has cracks on stellite seat,
			CV-2239(OPC)	460/10-04-88	220/12-05-88	MOVATS testing MOVATS testing, grease in limit switch was changed and valve repacked
X-15	Reactor Water Cleanup	С	MO-2700(IPC)	1,500/08-26-88 1,050/10-21-88	1,500/08-26-88	Torque Switch
			MO-2701(OPC)	<250/10-21-88	1,050/10-21-88 <800/11-09-88	replaced VOTES tested, replaced the EQ qualified limit switches set, repacked valve
X-16A	Core Spray	С	MO-2117(IPC)	2,200/10-06-88	250/11-28-88	VOTES tested, flushed LS assembly
			MO-2115(OPC)	<110/10-06-88	1,000/11-28-88	Replaced motor, rebuilt operator VOTES tested replaced the EQ qualified limit switches set, repacked valve
X-16B	Core Spray	С	MO-2137(IPC)	<150/11-05-88	<110/12-06-88	Operator overhauled, torque switch balanced
			MO-2135(OPC)	185/11-05-88	185/11-05-88	Switch Dalanced

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-19	Drywell Drain	С	CV-3704(IPC)	19,000/10-12-88	1,575/12-09-88	Machined wedge, lapped valve seats, and repacked
			CV-3705(OPC)	550/10-12-88	550/10-12-88	and repaired
X-20	Demineralized Water	С	V-09-111(IPC)	<240/10-18-88	<240/10-18-88	
			V-09-65(OPC)	<240/10-18-88	<240/10-18-88	
X-21	Service Air	С	Blind Flange(IPC)	25/11-27-88	25/11-27-88	
			V-30-287(OPC)	(Combined)	(Combined)	
X-22,	N ₂ Compressor Discharge	С	V-43-214(IPC)	630/10-12-88	630/10-12-88	
N-229A			CV-4371C(OPC)	290/10-12-88	290/10-12-88	
			CV-4371A(OPC)	775/10-12-88	775/10-12-88	
X-23A	Drywell Cooling Water Supply	/ C	CV-5718A(IPC)	1,400/10-10-88	1,400/10-10-88	
			V-57-77(OPC)	(Combined)	(Combined)	
X-23B	Drywell Cooling Water Supply	, C	CV-5718B(IPC)	14,000/11-18-88	575/12-07-88	Cleaned valve seat and replaced packing
		•	V-57-78(OPC)	(Combined)	(Combined)	
X-24A	Drywell Cooling Water Return	C	CV-5704A(IPC) V-57-75(OPC)	<110/10-10-88 (Combined)	<110/10-10-88 (Combined)	
			¥-31-13(OFO)	(Compined)	(Combined)	
X-24B	Drywell Cooling Water Return	C	CV-5704B(IPC) V-57-76(OPC)	1,000/11-18-88 (Combined)	1,000/11-18-88 (Combined)	

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-25	Drywell Purge Outlet	С	CV-4302(IPC)	8,850/09-30-88	7,700/12-07-88	Replaced two test
			CV-4303(OPC)	(Combined)	(Combined)	connection fittings O-Rings on stem seal, pneumatic valve replaced
		,	CV-4310(OPC)	6,250/09-30-88	6,250/09-30-88	valve replaced
X-26, N-220	Drywell Purge Supply	С	CV-4306(IPC) CV-4307(OPC) CV-4308(OPC)	275/10-08-88 (Combined) (Combined)	275/10-08-88 (Combined) (Combined)	
X-26, N-220	Drywell and Torus Makeup	С	CV-4311(IPC)	5,950/10-05-88	250/11-25-88	Lapped seat and narrowed width of seat on downstream side, replaced springs
			CV-4312(OPC) CV-4313(OPC)	2,250/10-05-88 610/10-07-88	1,000/11-15-88 610/10-07-88	ropidoda opinigo
X-32D	N₂ Compressor Suction	С	CV-4378A(IPC) CV-4378B(OPC)	0/10-14-88 0/10-14-88	0/10-14-88 0/10-14-88	
X-32E	Recirc. Pump A Seal	С	V-17-96(IPC) CV-1804B(OPC)	<150/10-05-88 0/10-05-88	<150/10-05-88 0/10-05-88	
X-32F	Recirc. Pump B Seal	С	V-17-83(IPC) CV-1804A(OPC)	0/10-05-88 5,400/10-04-88	0/10-05-88 220/12-12-88	Replaced stem and seat, lapped seat and repacked valve
X-35 A	TIP Check	С	Check Valve(OPC)	720/1 0-27-88	720/10-27-88	

Pen <u>No.</u>	System Name	Test Type	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
X-35B	TIP Ball	C	Ball Valve(OPC)	0/10-27-88	0/10-28-88	
X-35C	TIP Ball	С	Ball Valve(OPC)	0/10-27-88	0/10-28-88	
X-35D	TIP Ball	С	Ball Valve(OPC)	0/10-27-88	0/10-28-88	
X-36	CRD Return	С	V-17-53(IPC) V-17-52(OPC)	125/10-25-88 <172/10-25-88	125/10-25-88 <172/10-25-88	See Note 2 See Note 2
X-39A	CAD Supply	С	SV-4332A(IPC) SV-4332B(OPC)	<110/10-12-88 <110/10-12-88	<110/10-12-88 <110/10-12-88	
X-39B	CAD Supply	С	SV-4331A(IPC) SV-4331B(OPC) (<110/10-11-88 (See Note 3)/03/16/88	<110/10-11-88 <130/03-16-88	Replaced retainer ring and O-Rings
				<110/10-11-88	<110/10-11-88	mig and ormigo
X-40C	Jet Pump Coolant Sample	С	SV-4594B(IPC) SV-4595B(OPC)	<150/10-10-88 <150/10-10-88	<150/10-10-88 <150/10-10-88	
X-40D	Jet Pump Coolant Sample	С	SV-4594A(IPC) SV-4595A(OPC)	<90/10-08-88 <90/10-08-88	<90/10-08-88 <90/10-08-88	
X-41A	Recirc. Loop Sample	С	CV-4639(IPC) CV-4640(OPC)	<35/10-14-88 <110/10-14-88	<35/10-14-88 <110/10-14-88	
X-42	Standby Liquid Control	С	V-26-9(IPC) V-26-8(OPC)	420/11-05-88 3,400/11-05-88	420/11-05-88 1,400/11-07-88	Valve was cleaned and lapped
X-46F	CAM Return	·C	SV-8105B(IPC) SV-8106B(OPC)	0/10-13-88 0/10-13-88	0/10-13-88 0/10-13-88	
X- 4 8	Drywell Drain Discharge	С	CV-3728(IPC) CV-3729(OPC)	<150/10-14-88 <150/10-14-88	<150/10-14-88 <150/10-14-88	

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
X-50B	CAM Supply	С	SV-8101A(IPC) SV-8102A(OPC)	<110/10-12-88 0/10-12-88	<110/10-12-88 0/10-12-88	
X-50D	CAM Supply	С	SV-8105A(IPC) SV-8106A(OPC)	<110/10-12-88 <110/10-12-88	<110/10-12-88 <110/10-12-88	
X-50E	CAM Supply	С	SV-8103A(IPC) SV-8104A(OPC)	<110/10-12-88 <110/10-12-88	<110/10-12-88 <110/10-12-88	
X-54	CCW Return	С	MO-4841A(IPC)	250/10-07-88	250/10-07-88	
X- 5 5	CCW Supply	С	MO-4841B(OPC)	0/10-08-88	0/10-08-88	
X-56C	CAM Supply	С	SV-8101B(IPC) SV-8102B(OPC)	<240/10-13-88 0/10-13-88	<240/10-13-88 0/10-13-88	
X-56D	CAM Supply	С	SV-8103B(IPC) SV-8104B(OPC)	<240/10-13-88 <240/10-13-88	<240/10-13-88 <240/10-13-88	
N-205	Torus Exhaust Outlet	С	CV-4300(IPC)	420/10-12-88	285/12-08-88	Cleaned Miller air plate and replaced
			CV-4301 (OPC)	(Combined)	(Combined)	sub plate seal
	·		CV-4309(OPC)	13,000/10-11-88	13,000/10-11-88	
N-211A	CAD Supply	С	SV-4333A(IPC) SV-4333B(OPC)	3,450/10-11-88 2,750/10-11-88	3,450/10-11-88 2,750/10-11-88	
N-211B	CAD Supply	С	SV-4334A(IPC) SV-4334B(OPC)	315/10-12-88 310/10-12-88	315/10-12-88 310/10-12-88	
N-212	RCIC Turbine Exhaust	С	V-24-8(IPC) V-24-23(OPC)	76/10-09-88 (Combined)	76/10-09-88 (Combined)	See Note 2

Pen <u>No.</u>	System Name	Test Type	Equipment/ <u>Valves (Note 1)</u>	As found leakage (SCCM) / date	As left leakage (SCCM) / date	<u>Remarks</u>
N-212	RCIC Turbine Exhaust Vacuum Breaker	С	V-24-46(IPC)	420/10-08-88	420/10-08-88	
	Vacuum Dreaker		V-24-47(OPC)	120/10-08-88	120/10-08-88	
N-214	HPCI Turbine Exhaust	С	V-22-17(IPC) V-22-16(OPC)	8,048/11-14-88 (Combined)	8,048/11-14-88 (Combined)	See Note 2
N-214	HPCI Turbine Exhaust Vacuum Breaker	С	V-22-63(IPC)	725/10-08-88	725/10-08-88	
	vacaum broaker		V-22-64(OPC)	520/10-08-88	520/10-08-88	
N-219	HPCI/RCIC Exhaust	С	MO-2290B(IPC) MO-2290A(OPC)	430/10-11-88 150/10-11-88	430/10-11-88 410/12-09-88	Replaced torque switch, cleaned valve and lapped wedge, MOVATS testing
N-222	HPCI Condensate Return	С	V-22-22(IPC) V-22-21(OPC)	0/10-10-88 (Combined)	0/10-10-88 (combined)	See Note 2
N-229B	CAM Supply	С	SV-8107A(IPC)	<240/10-12-88	<25/11-17-88	Replaced O-Rings and coil assembly
			SV-8108A(OPC)	<240/10-12-88	<25/11-17-88	Replaced O-Rings and coil assembly
N-229C	CAM Return	C	SV-8109A(IPC) SV-8110A(OPC)	260/10-12-88 260/10-12-88	76/11-17-88 80/11-1 7- 88	Rebuilt valve Rebuilt valve
N-229F	CAM Return	С	SV-8109B(IPC) SV-8110B(OPC)	<110/10-13-88 <110/10-13-88	32/11-17-88 28/11-17-88	Rebuilt valve Rebuilt valve
N-229G	CAM Supply	С	SV-8107B(IPC) SV-8108B(OPC)	<240/10-13-88 <240/10-13-88	0/11-17-88 0/11-17-88	Rebuilt valve Rebuilt valve

Pen <u>No.</u>	System Name	Test <u>Type</u>	Equipment/ Valves (Note 1)	As found leakage (SCCM) / date	As left leakage (SCCM) / date	Remarks
N-229H	PASS Sample Return	С	SV-8772A(IPC) SV-8772B(OPC)	<240/10-13-88 <240/10-13-88	<240/10-13-88 <240/10-13-88	
N-231	Vacuum Breaker	С	CV-4304(IPC)	650/10-11-88	<150/11-30-88	Adjusted regulators and replaced Miller 310 valve
			V-43-169(OPC)	(Combined)	(combined)	oro raivo
N-231	Vacuum Breaker	С	CV-4305(IPC) V-43-168(OPC)	180/10-12-88 (Combined)	180/10-12-88 (combined)	

Notes:

- 1. (IPC) Inside Reactor Containment (OPC) Outside Reactor Containment
- 2. These valves were tested with water as the test medium. The test results are in cc/min.
- 3. Unable to measure the leakage rate because the valve would not close.

ATTACHMENT 4B 1988 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

The as found LLRT, the repair, and the as left LLRT for each boundary, or penetration, was reviewed. The net leakage contribution for each penetration was determined using the following criteria:

- 1. A leakage equivalent to the repair improvement achieved on each valve in the penetration is calculated.
- 2. The leakage equivalent is the difference between the as found and the as left leakage rates.
- 3. If a repair was not performed, a zero leakage equivalent is assessed to the valve.
- 4. The leakage equivalent assessed to a penetration may be reduced due to the safety-related service of the system associated with the penetration(s). Justification for this reduction will be provided with the analysis.
- 5. The net equivalent leakage for the penetration is the lowest of the inside or outside valve grouping (e.g., simulates minimum pathway leakage). The inside barrier may be inside the containment or the innermost barrier of the two barriers outside the containment. See Attachment 4A.
- 6. No repair improvement credit is taken if the as left leakage rate is higher than the as found leakage rate. Only those penetrations where repairs were performed are included in this attachment.
- 7. If the as left leakage rate of a repaired valve is lower than the as left leakage rate of a valve that didn't require a repair, then the penetration net equivalent leakage is the difference between the as left leakage rates, or the repair improvement of the reworked valve.
- 8. For series valves tested together (i.e. combination test), the penetration net equivalent leakage is half the difference between the as found and the as left leakage rates when both valves are repaired at the same time (prior to performing another test).
- 9. When the summation of the leakage equivalent and the leakage measured during a successful Type A test is greater than L_a, the penetration(s) with excessive leakage(s) shall be analyzed under a failure analysis program.
- 10. All leakage rate values are in SCCM.

Conclusions:

The resulting net equivalent leakage of 178,171 SCCM or 1.123683 percent/day indicates that the as found ILRT test results determined by analysis are below the plant's maximum allowable leakage rate of 2.0 percent/day.

ATTACHMENT 4B 1988 LOCAL LEAKAGE RATE SUMMARY ANALYSIS

Dom	1900 EOOME EEMINIOE WITH DOWNMAN THE WIELDING				
Pen <u>Num.</u>	System	<u>Inside</u>	<u>Outside</u>	Net	<u>Notes</u>
X-53	Drywell Head	-	18	18	
X-58D	Stabilizer Access Port	-	2,275	2,275	
X-58H	Stabilizer Access Port	-	85	85	
X-26	Drywell Purge Supply	-	21,850	21,850	
N-220	Torus Purge Supply	-	2,680	2,680	
X-7A	Main Steam	16,825	350,985	16,825	
X-7B	Main Steam	5,550	0	0	
X-7C	Main Steam	0	5310	0	
X-7D	Main Steam	18,905	0	0	
X-8	Steam Drain	0	13,850	0	
X-9A	Feedwater	384,390	1075	1075	
X-9B	Feedwater	371,695	129,000	129,000	
X-11	HPCI Steam	0	240	0	
X-11	HPCI Cond. Return	955	0	0	
X-16A	Core Spray	1,950	0	0	
X-16B	Core Spray	40	0	40	
X-19	Drywell Drain	17,425	0	0	
X-23B	Drywell Cooling Water Supply	13,425	575	575	Comb. Test
X-25	Drywell Purge Outlet	-	1,150	1,150	Comb. Test
X-26, N-220	Drywell & Torus Makeup	5700	1,250	1,250	
X-32F	Recirc. Pump B Seal	0	5,180	0	
X-42	Standby Liquid Control	0	2,000	0	
N-205	Torus Exhaust Outlet	-	135	135	Comb. Test
N-229B	CAM Supply	215	215	215	
N-229C	CCAM Return	184	180	180	
N-229F	CAM Return	78	82	78	
N-229G	GCAM Supply	240	240	240	
N-231	Vacuum Breaker	-	500	500	Comb. Test