

TEST REPORT ON LOAD CYCLE TEST OF AXIAL TUBE

END CRACKS IN WELDED SLEEVE/TUBE SAMPLES

TR-MCC-185, REV. 00

CE TASK NO. 848841

ABB COMBUSTION ENGINEERING NUCLEAR POWER
MATERIALS TECHNOLOGY
WINDSOR, CONNECTICUT

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The information contained in this document has been reviewed and satisfies the applicable items contained in Checklist No. 4 of QAP 3.6.

Name C. Hoffmann

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TR-MCC-185, Rev. 00

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1.0 PURPOSE

The purpose of this program was to determine whether or not cracks located in the tube ends of steam generator tubes would propagate into weld joints after sleeves are installed. This determination was made through a test program that involved the cyclic testing of sleeved tube specimens containing tube end cracks.

2.0 CONCLUSIONS

On the basis of the tests performed, it is concluded that ABB can successfully weld a sleeve to a tube containing cracked ends. The process of machining away the tube end and welding a sleeve in the fillet weld region assures that the crack is no longer a potential primary to secondary leak path. Cyclic testing of these joints revealed that the crack did not propagate into the weld joint during loading. These test results are applicable to welded tube plug joints.

3.0 INTRODUCTION

During recent inspections of the steam generator tubes at the Kewaunee Nuclear Station, longitudinal cracks were found in the ends of some of the tubes. Questions were raised to ABB-CE concerning the potential of these cracks to propagate into weld joints that would be made during steam generator tube sleeving.

A request (Attachment 1) was made to Materials Technology by Steam Generator Services to perform tests to determine the potential for crack propagation. A test program was developed (Reference 6.1) and the tests and examinations performed.

4.0 DISCUSSION

4.1 Specimen Preparation

Tube specimens were prepared per Figure 1. Tube samples (.875" OD x .050" wall) were rolled into carbon steel blocks, then fillet welded in place. An EDM process was employed to make a notch in the tube to simulate an axial crack. The notch was approximately .0125" wide, 1 3/4" long and 100% throughwall on each sample.

After the tube ends were machined, sleeves were installed and welded in accordance with the Keweenaw site traveller, Reference 6.2. Upon completion of sleeve installation, baseline sleeve eddy current inspection and liquid penetrant examination were performed. Attachment 2 is the complete eddy current inspection report and Attachment 3 consists of all liquid penetrant test results.

Four samples were completed, three for cyclic testing and one for "baseline", to be used for comparison. The three samples for cyclic testing were K-6, K-7 and K-9, while the baseline specimen was K-4.

4.2 Cyclic Testing

4.2 Cyclic Testing

Three of the sleeved specimens, K-6, K-7 and K-9, were cyclic tested by Materials technology using a MTS test system. Each specimen was cycled between -200 lbs. and -2550 lbs. for 2000 cycles. The specimens were tested at a frequency of one cycle per second. This test sequence was intended to simulate the loading on the weld joint due to heatup and cooldown cycles, as well as transient conditions. This test sequence duplicates the original tests for the sleeve, as described in the sleeve licensing report, Reference 6.3. Upon completion of the cyclic testing, the samples were liquid penetrant tested.

4.3 Metallographic Examination

The four specimens were examined metallographically in order to determine crack location relative to the weld joint. Each of the specimens was mounted in a fixture and the weld joint was ground down incrementally in the transverse direction until the crack in the tube was visible.

5.0 TEST RESULTS

5.1 Eddy Current Tests

The eddy current test results are included as Attachment 2. These tests were performed for information purposes. Eddy current test data for notched samples, as well as data from the Kewaunee steam generators are included.

5.2 Liquid Penetrant Tests

The liquid penetrant test results are included as Attachment 3. The specimens passed the tests, both before and after cyclic testing. There were no indications of cracks or voids on the weld joint surfaces.

5.3 Cyclic Tests

The specimens did not fail the cyclic tests that were performed. No visible cracks or weld joint failures were visible. Each specimen was tested for the full 2000 cycle requirement.

5.4 Metallographic Examination

As described in Section 4.3, the specimens were incrementally ground in the transverse direction until the crack was revealed. Approximately .025" was removed on the first grind, and approximately .005" thereafter. After each grind, the specimen was placed on a polishing wheel in order to more clearly reveal the crack location by removing any "smeared" metal. In all cases, the first measurements were taken from the highest point of the weld bead. The amount of weld metal removed for each specimen is shown in the table below.

| <u>Specimen No.</u> | <u>Condition</u> | <u>Amount Weld Metal Removed</u> |
|---------------------|------------------|----------------------------------|
| K-4 | Baseline | .056" |
| K-6 | Cyclic Tested | .044" |
| K-7 | Cyclic Tested | .060" |
| K-9 | Cyclic Tested | .043" |

In all cases the crack appeared after the interface between sleeve and tube was revealed. This indicates that the crack was not present in the weld metal, but only in the unwelded tube material. The reason for the slight difference between the amount of metal removed is that there is a minimal variation in weld height around the length of the weld. This variation is due to heat buildup during the weld process.

5.5 Applicability to Plugging

It is the position of ABB that these sleeve tests are applicable to welded tube joints. The joint configuration is similar and the loading conditions are more conservative for the sleeve joint than for the plug joint.

6. REFERENCES

- 6.1 00000-MCC-114, Test Program for Weld Integrity Testing of a Steam Generator Sleeve Welded to an Axially Cracked Steam Generator Tube End.
- 6.2 ST No. 848842-001, Rev. 0, Installation of Welded Steam Generator Tube Sleeves Using Peripheral Tooling.
- 6.3 CEN-413-P, Keweenaw Steam Generator Tube Report Using Leak Tight Sleeves.

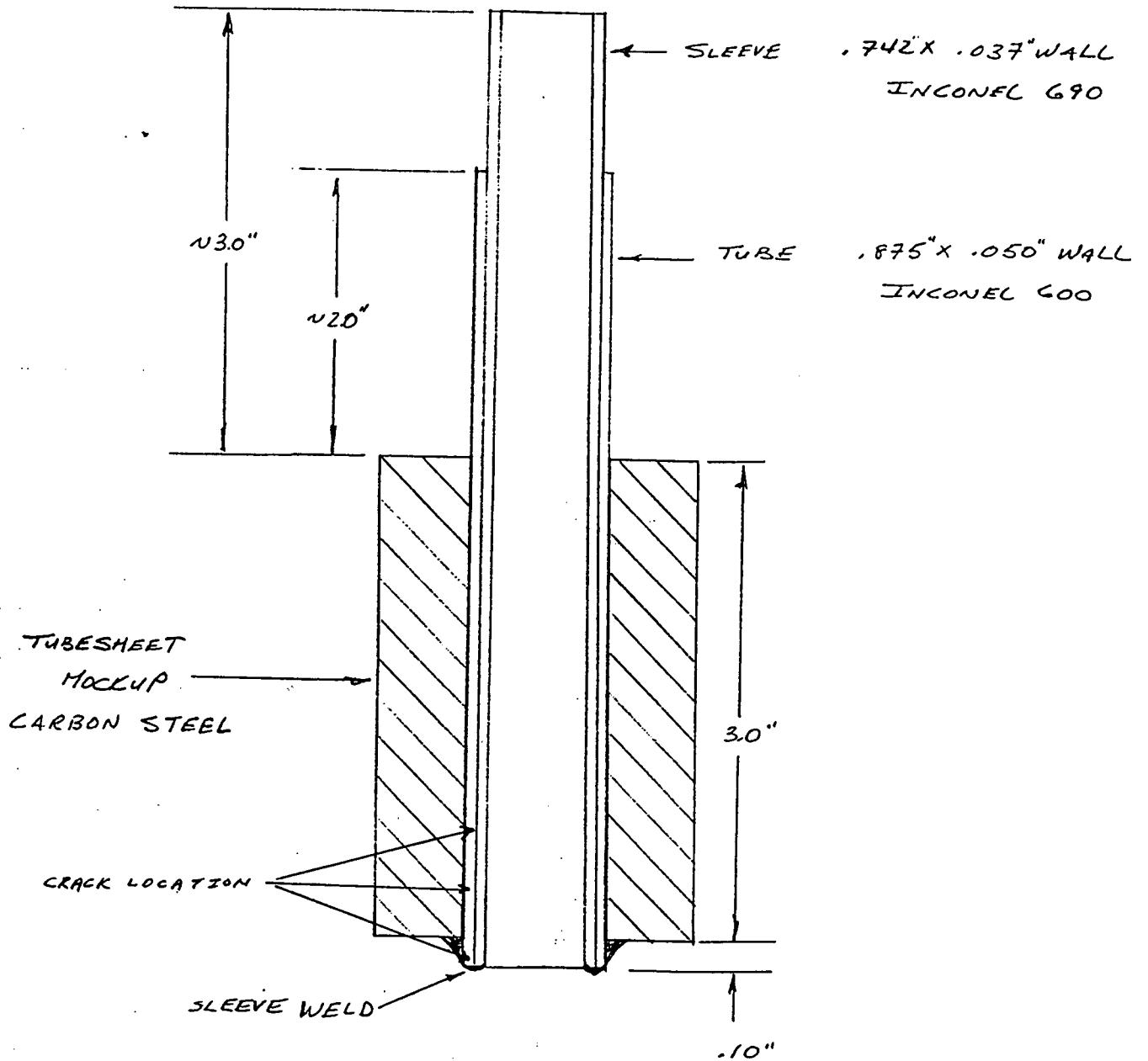


Figure 1. Axial Tube End Crack Sample

ATTACHMENT 1

TEST REQUEST



Inter-Office Correspondence

To: E.P. Kurdziel
9428-1206

Daniel Stepnick
D. G. Stepnick
9445-M088

cc: W. R. Gahwiller
G. H. Stevens

January 2, 1992

Subject: Transmittal of Test Request Involving Welded Sleeve Installation In Cracked Tube Ends

Reference: Kewaunee Steam Generator Tube Repair using Leak Tight Sleeves, Sleeve Qualification No. CEN-413-P

The purpose of this memo is to transmit the attached Test Request, T.R. NO. T-MCC-185, Supplement Number 00. This test request outlines the preparation and testing of samples which will be used to justify the structural integrity of installed welded tube sheet sleeves in steam generator tubes containing axial cracks near the tube ends.

The significant steps for sample preparation and testing follow:

1. Roll and fillet weld tube samples
2. Perform ECT baseline of tube samples
3. To simulate axial cracks, EDM notch tube samples
4. Repeat ECT program
5. Machine tube ends prior to sleeve installation
6. Install and weld sleeve samples
7. Perform load cycle test on sleeve/tube samples per the requirements of the referenced Sleeve Qualification Report. Load Range: -200 to -2550 pounds
Cycles: 2000
8. Perform dye penetrant testing and metallographic examination of samples.

SG92000.DS

ABB-CENP Mat./Chem. Tech. Test - Task Request

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| | | |
|-----------------|--|---|
| Test Task Name: | Load Cycle Test of Axial Tube End Crack welded Sleeve / Tube Samples | T. R. No. T-MCC-185 Suppl. No. 00 Account No. 848841 Time Charge No. 848841 |
|-----------------|--|---|

Requirements:

- Prepare test specimens by rolling ; welding 5/8 tubes into blocks. EDM notch that will be through-wall at tube end.
- Machine tube ends per Keweenaw Traveller, ST NO. 848842-001.
- Install sleeves per Keweenaw Traveller, ST NO. 848842-001.
- Perform baseline eddy current testing on sample
- Perform load cycle testing on samples in accordance with procedure No. 00000-MSD-072, Rev. 01.
 - Load Range - 200 to -2550 lbs.
 - 2000 cycles.
- Perform eddy current testing, dye penetrant testing and metallographic examination

| | | |
|-----------------------------|---|---|
| Quality Assurance: | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | |
| Quality Class: | <input checked="" type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 3 | |
| Safety Related: | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | PURPOSE (Testing - Only One Applies) |
| QAM 101 - QAP 3.6: | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | Develop Design Input: <input type="checkbox"/> Yes <input checked="" type="checkbox"/> (No) |
| Quality Plan No.: | | Verify Design: <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No |
| Other Quality Requirements: | | |

Requested By: D. Proctor CEP No. 9445-M088 Date: 12/13/91
 Task Approved By: CEP No. Date:

| For Dept 9428 Use Only | |
|--|------------------------|
| Estimated By: | Date: |
| Engineer Assigned: | Date: |
| Supv / Prod Mgr Assigned: | Date: |
| Work Authorized By: | Date: |
| Targeted Work Completion Date: | NPS / SDS Estimate No. |
| Distribution: | |
| Originals: | |
| Copy: | |
| Estimated Total Technology Services Activity Costs | |

ATTACHMENT 2

EDDY CURRENT TEST REPORT

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

SUMMARY

Field eddy current data for Kewaunee steam generator tubes was reviewed by ABB Combustion Engineering Outage Services, Windsor, CT. In addition, laboratory eddy current data was taken from expanded, welded and electric discharge machined notched samples. Comparison of the laboratory and field data was performed and is reported in tabular and graphic form. While the signals can be ranked from most flaw-like to least flaw-like, there is no strong evidence that the field eddy current signals are caused by a flaw discontinuity in the SG tube wall. Indications from ID initiated flaws are often similar to indications caused by probe lift off and tube geometry (dings, weld, ovalization). It is recommended that future tests during the refueling outage include the 3 coil MRPC at a slower test speed and that verification of these results be confirmed with visual or penetrant testing.

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

1.0 INTRODUCTION

Eddy Current testing was performed on steam generator (SG) tubes at the Kewaunee Nuclear Plant. This data was forwarded to ABB CE Outage Services for further evaluation.

2.0 SCOPE

Data from 16 SG tubes was provided. In addition, laboratory samples of SG tubes were tested and the data analyzed. The field and laboratory data were compared.

3.0 METHODS

3.1 Field Data Analysis. Field eddy current consisted of motorized rotating eddy current (MRPC) data and was analyzed by a certified data analyst using the Eddynet Analysis System. This is the standard, state of the art, eddy current analysis system in general usage for field examinations of nuclear plant eddy current data. High resolution graphic printouts of the field data and tabular summaries are provided as part of this report.

3.2 Tube Samples. The tube samples discussed here were described elsewhere in the main body of this report. Since there is a reasonable probability that the signals in the field data are caused by probe wobble or tube geometry irregularities, SG

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

tube samples with and without flaw indications and geometry variations were tested in the laboratory using probe pusher/pullers similar to those used for field examinations. The data was analyzed in the same manner as the field data. High resolution graphic printouts of the field data and tabular summaries are provided as part of this report.

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

4.0 RESULTS AND DISCUSSION

4.1 Field Data Analysis. The results of the field data analysis are tabulated in Table 1. All measurements were taken at 400 kHz; the 100% hole was set at 10 degrees; a three point curve was established with the 100%, 60% and 40% notches; the 60% notch was set at 5.0 volts vert. max.; and 1 inch was assumed between the calibration standard flaws for setting the axial scale of the terrain plots. Table 1 contains a reading for the signal and noise volts in the region of the signal as well as a calculation for the signal to noise ratio (S/N). The S/N ratio is very low for these signals and ranges from 0.04 to 0.3. Values for the estimated length (range of 0.29" to 1.68") of the signal indications as well as the angles (range of 4 to 50 degrees) of the signal indications are provided. For real ID flaws the phase angle is often similar to the phase angle for ID tube noise and probe wobble. In addition, for ID flaws, there is typically very little change in phase angle with depth (poor resolution). A column which estimates the degree to which the signal is flawlike (1 most, 2 more, 3 least or not) is also included in Table 1. Figure 1 shows a category 1 signal where the 400 kHz lissajous is flawlike with supporting evidence from all other frequencies. Figure 2 shows a category 2 signal where the 400 kHz lissajous is flawlike with little supporting evidence from the other

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

frequencies. Figure 3 show a 400 kHz signal which is not flawlike. The most flawlike signals have more vertical signal component. Tube R38C61 is the most probable flaw of all the samples due to the location and S/N ratio. The complete graphics will be found in Section 5.0.

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

TABLE 1
KEWAUNEE FIELD EDDY CURRENT DATA ANALYSIS
(April 1991 Data/December 1991 Analysis)

| <u>Row</u> | <u>Col</u> | Signal <u>Volts</u> | Noise <u>Volts</u> | <u>S/N</u> | Length (Inches) | Angle (Degs) | %TW | Est. <u>1/</u> |
|------------|------------------|------------------------|-----------------------|------------|--------------------|-----------------|-----|-------------------|
| 18 | 12 | 6.3 | 25.4 | 0.2 | 0.6 | 4 | 60 | 2-3 |
| 29 | 13 | 6.7 | 35.2 | 0.2 | 1.2 | 13 | 98 | 2 |
| 30 | 14 | 6.7 | 32.9 | 0.2 | 1.68 | 23 | 91 | 1 |
| 31 | 15 | 4.7 | 31.7 | 0.1 | 1.68 | 24 | 90 | 1 |
| 41 | 42 | 1.1 | 30.4 | 0.04 | 0.29 | 359 | 0 | 3 |
| 45 | 41 | 1.1 | 16.4 | 0.1 | 0.43 | 42 | 78 | 1 |
| 1 | 16 | 8.0 | 27.7 | 0.3 | 0.35 | 11 | 99 | 2 |
| 37 | 45 | 0 | 9.9 | 0 | - | - | - | 3 |
| 38 | 61 ^{2/} | 4.5 | 3.3 | 1.4 | 0.5 | 7 | 70 | 1 |
| 37 | 68 | 3.3 | 42.6 | 0.1 | 0.78 | 18 | 94 | 1 |
| 4 | 88 | 2.6 | 40.8 | 0.1 | 0.60 | 12 | 99 | 2 |
| 18 | 87 | 3.5 | 34.4 | 0.1 | 0.6 | 25 | 89 | 1 |
| 15 | 91 | 1.2 | 32.2 | 0.04 | 0.36 | 50 | 73 | 1 |
| 10 | 91 | 5.9 | 19.0 | 0.3 | 0.35 | 19 | 94 | 1 |
| 5 | 90 | 1.6 | 38.9 | 0.04 | 0.60 | 33 | 84 | 1 |
| 4 | 89 | 8.8 | 37.1 | 0.2 | 0.55 | 21 | 92 | 1 |

1/ Key: 1 Most Flawlike
2 More Flawlike
3 Least or Not Flawlike

2/ For tube R38C61 the signal indication starts at TEH +1.85".

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

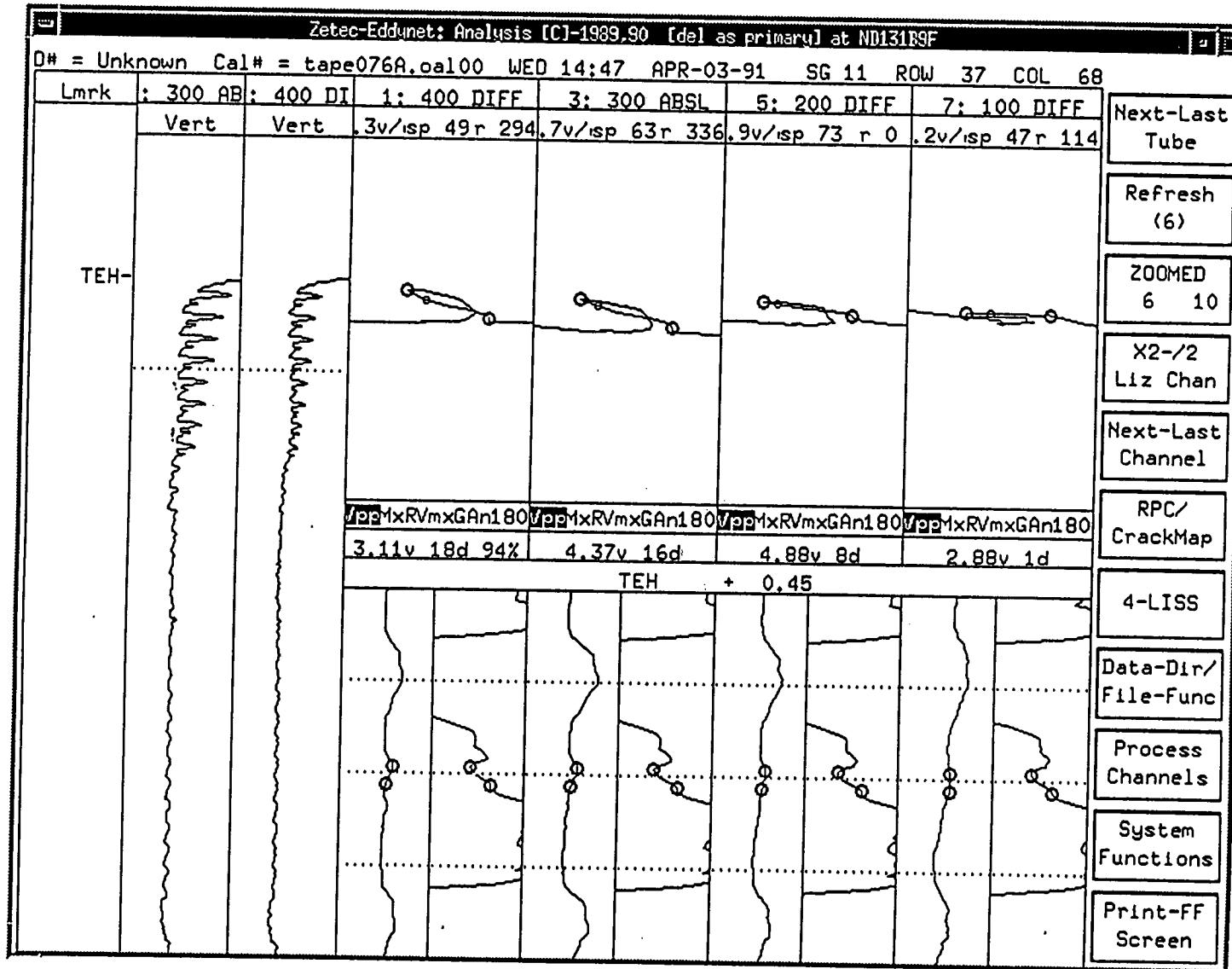


Figure 1--Kewaunee Eddy Current

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

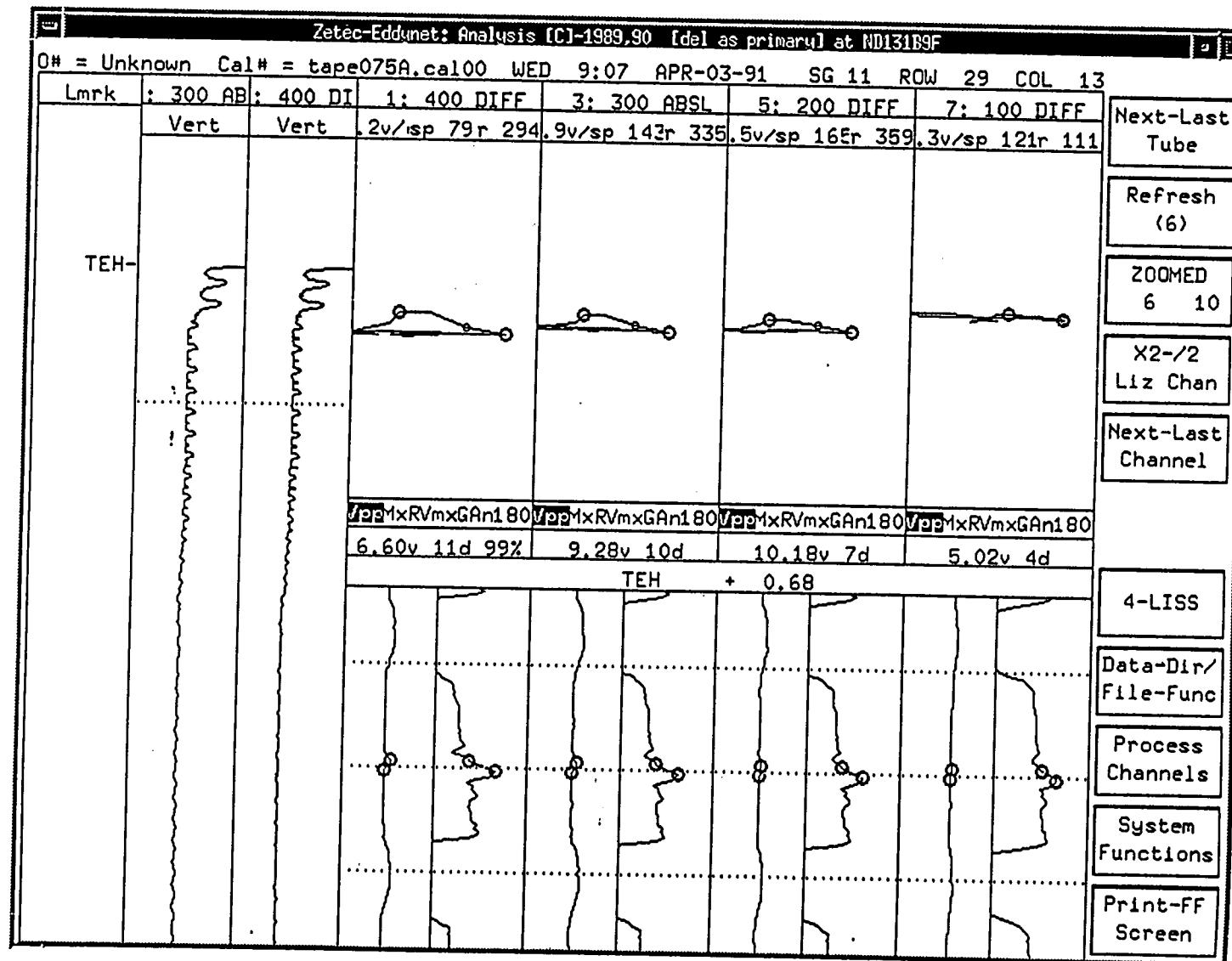


Figure 2--Kewaunee Eddy Current

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

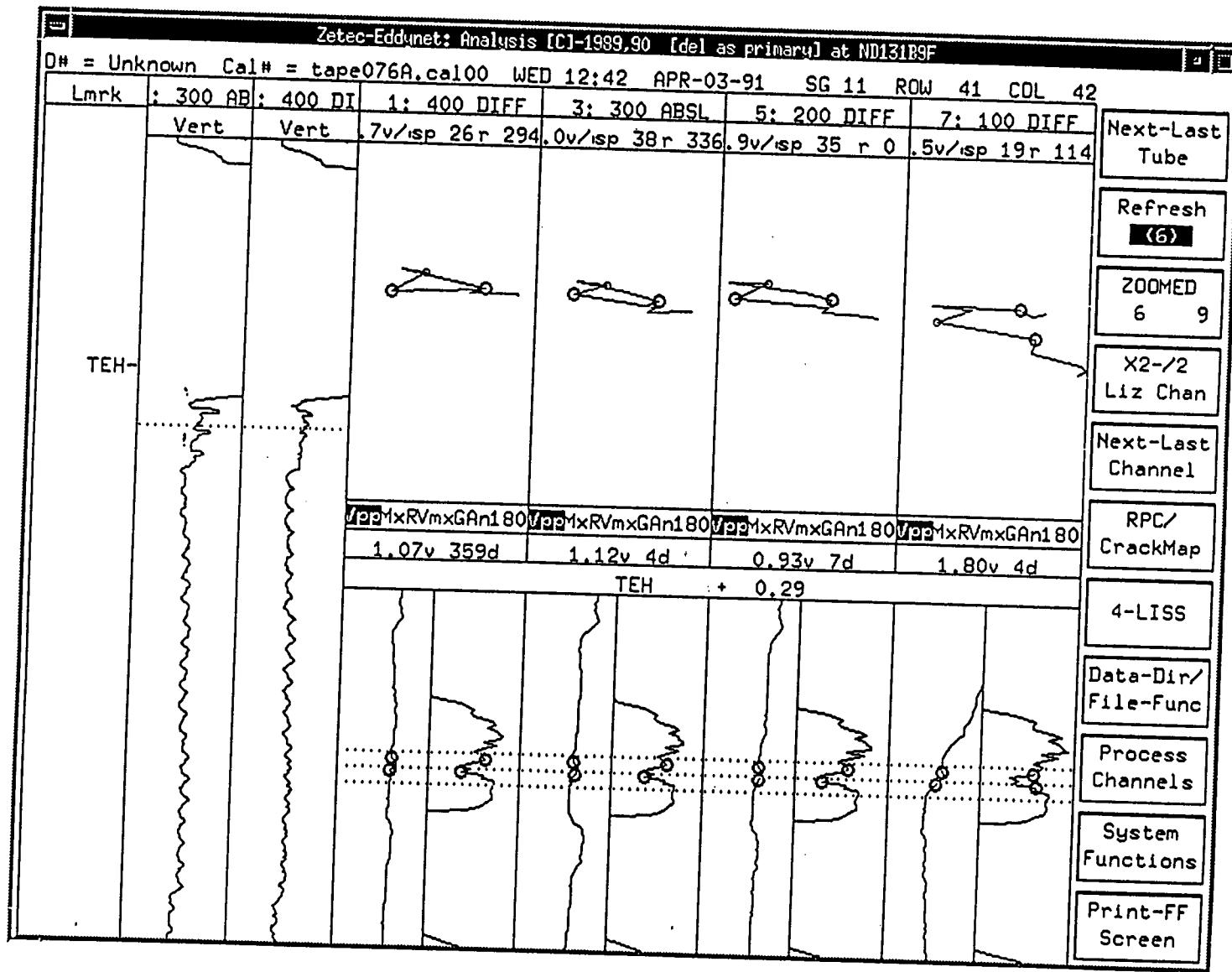


Figure 3--Kewaunee Eddy Current

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

4.1 Tube Samples. The results of the analysis of the eddy current data from the tube samples are tabulated in Table 2. The analysis setup was the same as for the field data. Some of the noise volts (range 3.0 to 73.8) are comparable to the volts from the noise in the field data, but the signal to noise ratios are higher ranging from 1.1 to 11.6. The signal voltages are a magnitude larger than those expected in the field due to the size of the EDM notches. Figure 4 shows a typical signal from a tube to tubesheet hand weld. The sample tubes had varying degrees of these indications. Figure 5 show a typical signal from an EDM notch in a tube/tubesheet sample. The notch starts at the tube end and stops at 1.5 inches from the tube end. Figure 6 show a liftoff signal in the tube/tubesheet sample caused by excessive penetration of tubesheet weld. Figure 7 show a liftoff signal caused by a .015" dimple dent in the tube. The complete graphics will be found in Section 6.0.

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

TABLE 2
KEWAUNEE LAB SAMPLES EDDY CURRENT DATA ANALYSIS
(December 1991 Data)

| <u>Sample Number</u> ^{1/} | Noise Signals ^{2/} | | | | EDM Signals ^{3/} | | | | <u>S/N</u> |
|------------------------------------|-----------------------------|-------------|------------|------------|---------------------------|-------------|------------|------------|------------|
| | <u>Volts</u> | <u>Degs</u> | <u>%TW</u> | <u>Loc</u> | <u>Volts</u> | <u>Degs</u> | <u>%TW</u> | <u>Loc</u> | |
| <u>Samples without notches:</u> | | | | | | | | | |
| 1 | 15.6 | 59 | 83 | .08 | n/a | | | | |
| 2 | 3.0 | 114 | 37 | .09 | n/a | | | | |
| 5 | 6.3 | 43 | 90 | .17 | n/a | | | | |
| | 3.9 | 30 | 94 | .10 | n/a | | | | |
| 8 | 73.8 | 63 | 81 | .21 | n/a | | | | |
| <u>Samples with notches:</u> | | | | | | | | | |
| 3 | 12.0 | 45 | 89 | .14 | 29.7 | 14 | 86 | .72 | 2.5 |
| 4 | 9.9 | 40 | 91 | .22 | 43.3 | 32 | 93 | .99 | 4.4 |
| | 3.9 | 87 | 66 | .20 | | | | | 11.1 |
| 6 | 25.2 | 35 | 92 | .10 | 27.0 | 21 | 97 | .66 | 1.1 |
| 7 | 4.4 | 69 | 78 | .13 | 51.2 | 32 | 93 | .79 | 11.6 |
| 9 | 7.5 | 46 | 88 | .19 | 29.2 | 24 | 96 | .65 | 3.9 |
| 10 | 15.6 | 80 | 71 | .15 | 52.5 | 30 | 44 | .44 | 3.4 |

1/ Samples described in main report.

2/ Lack of weld, lift off, probe wobble, etc.

3/ All 1½" long.

KEWAUKEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

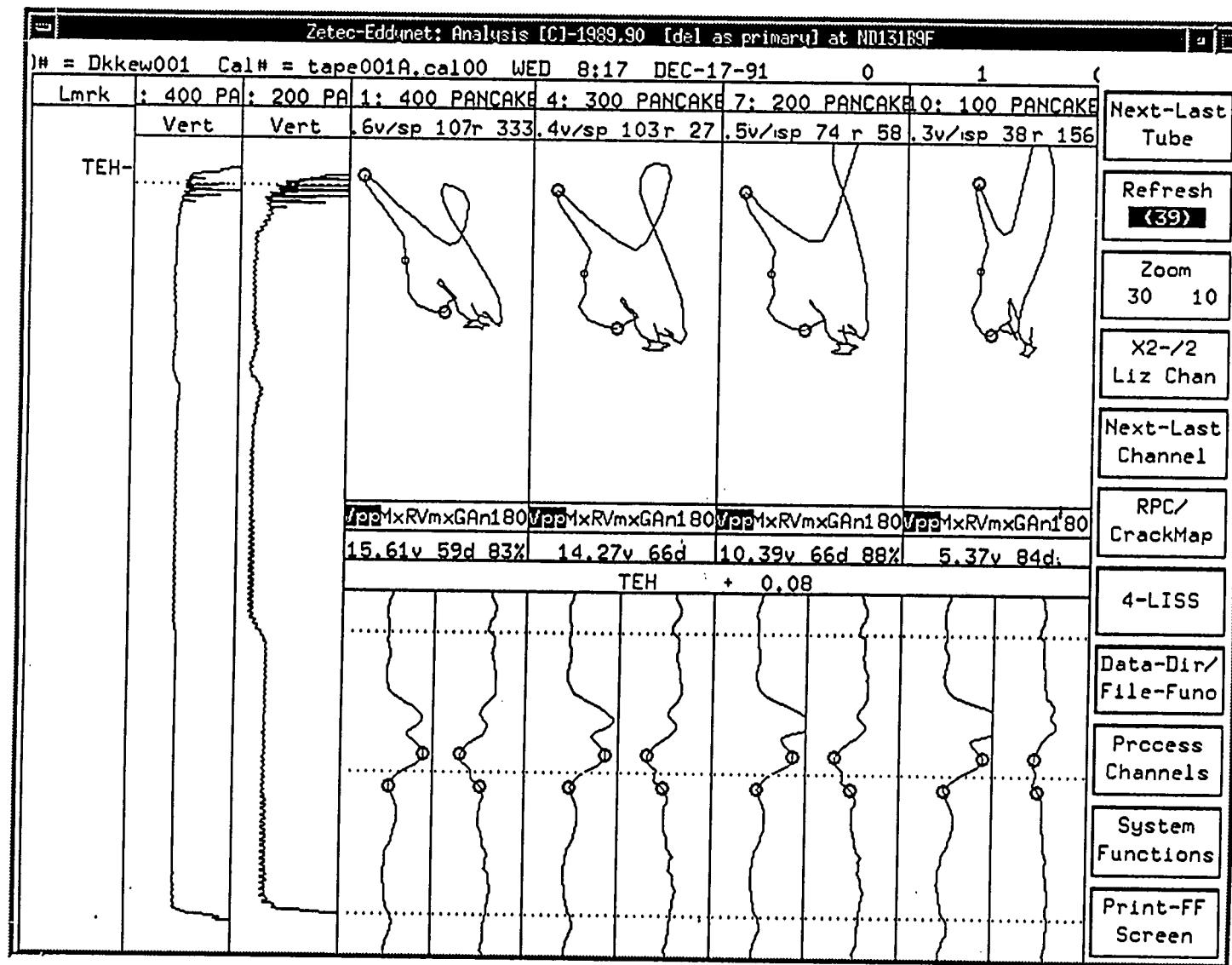


Figure 4--Kewaunee Eddy Current-Weld signal

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

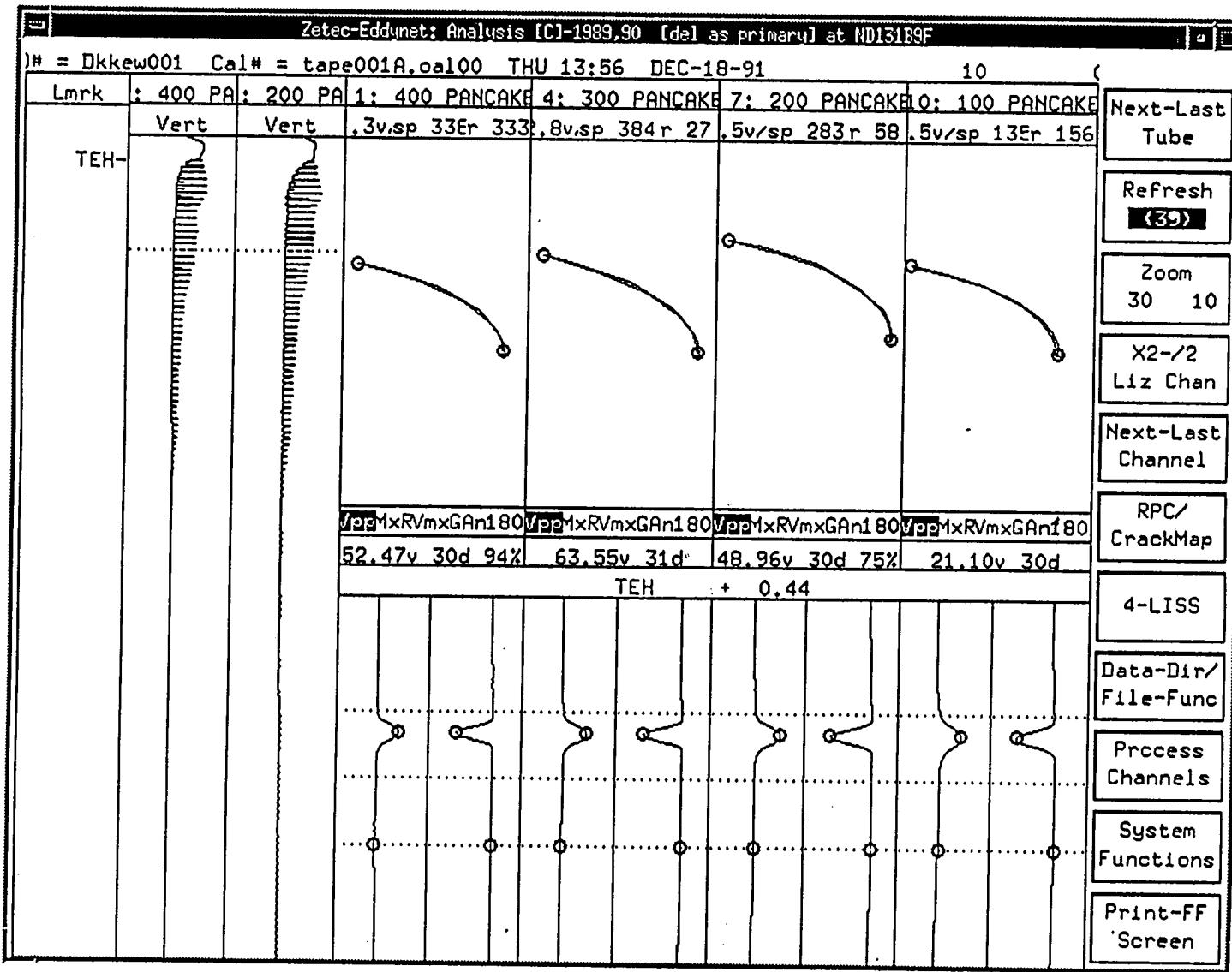


Figure 5--Kewaunee Eddy Current-EDM Notch Signal

KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

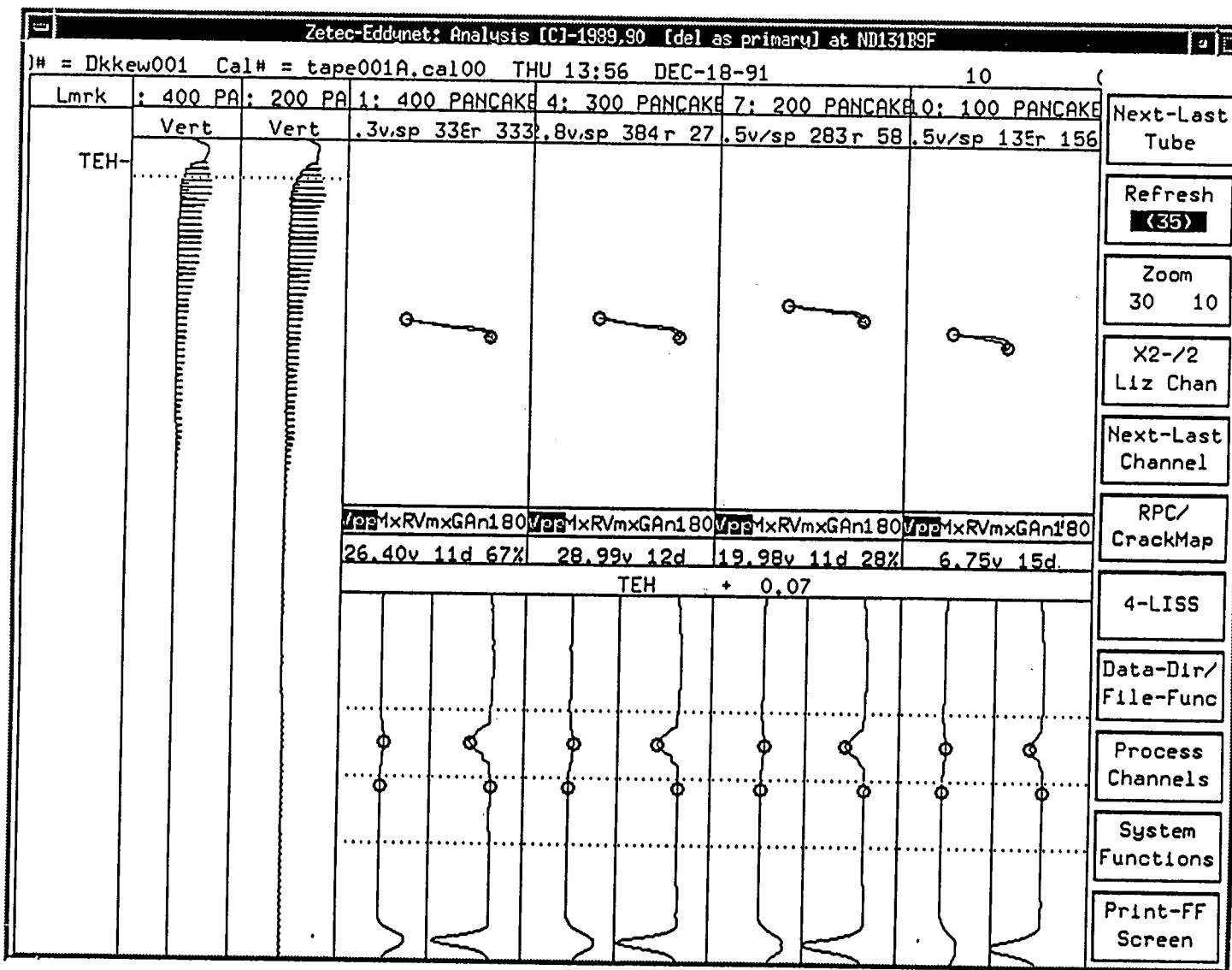


Figure 6--Kewaunee Eddy Current-Liftoff signal-Excessive Penetration

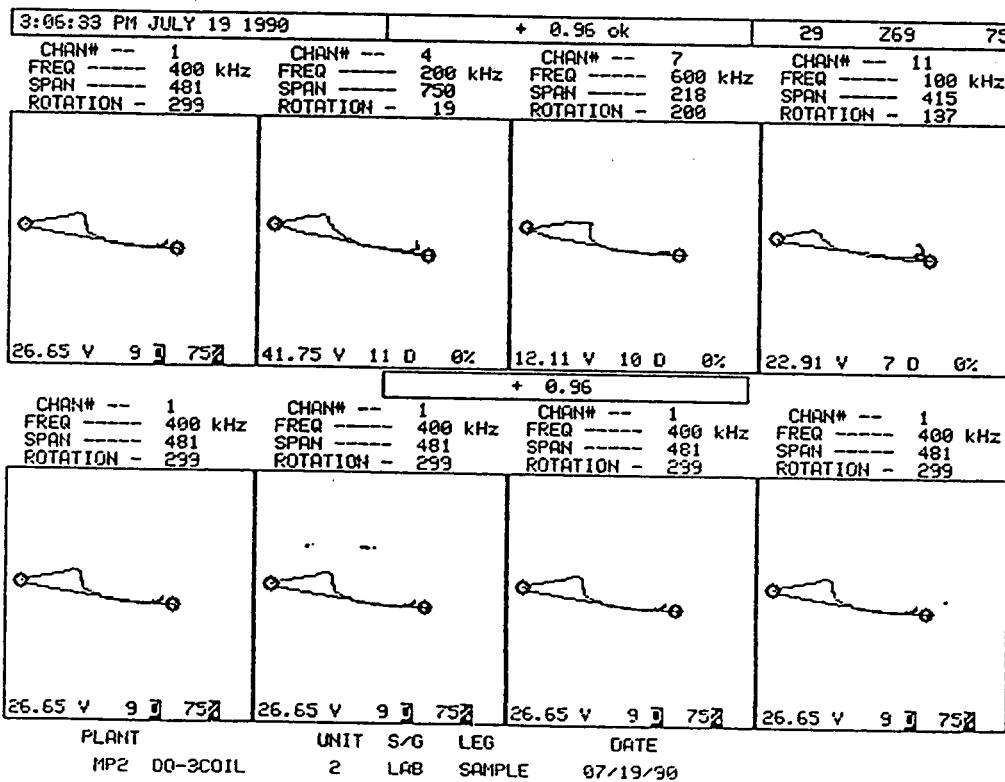
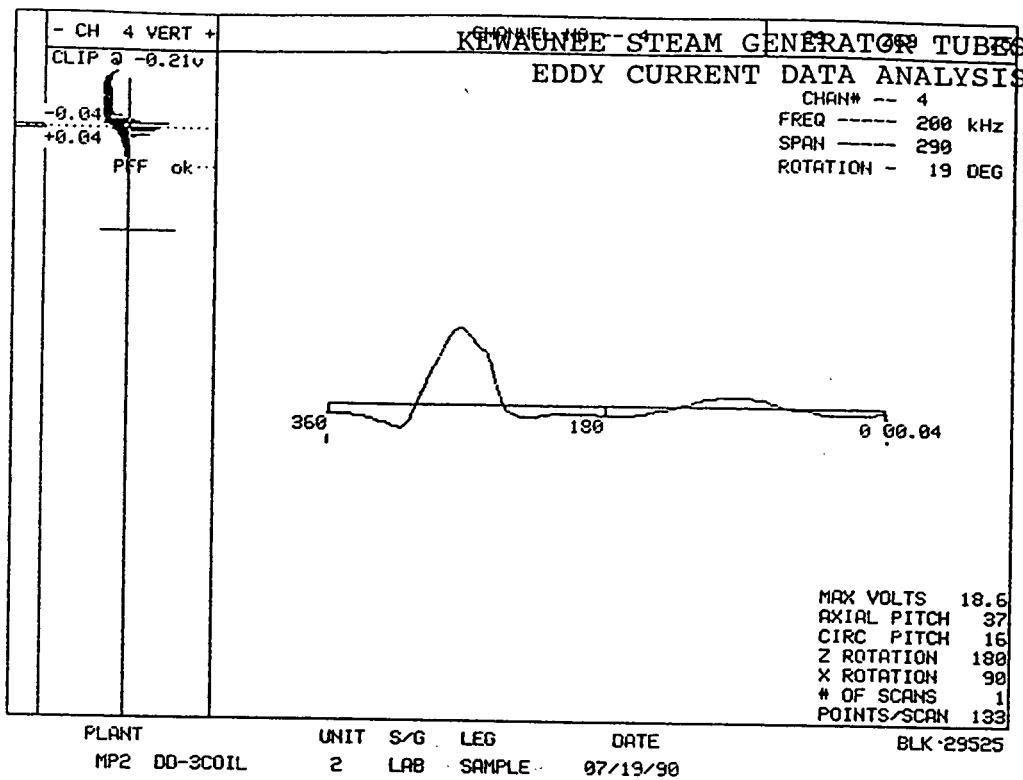


Figure 7A--Kewaunee Eddy Current-Liftoff Signal-Dent

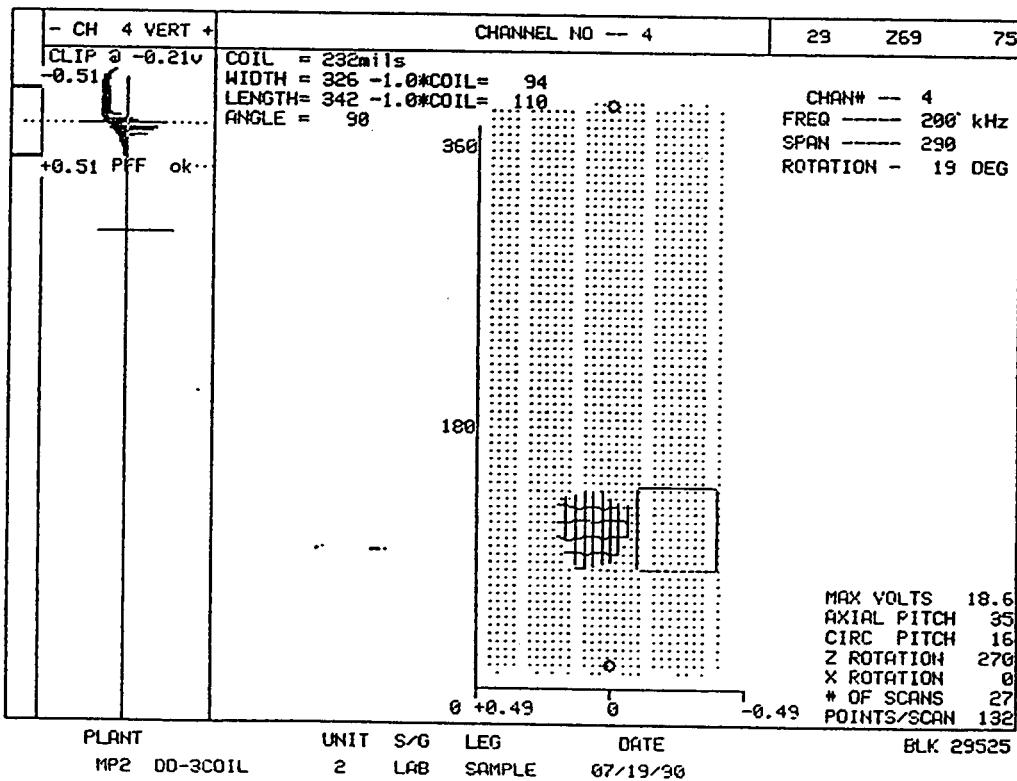
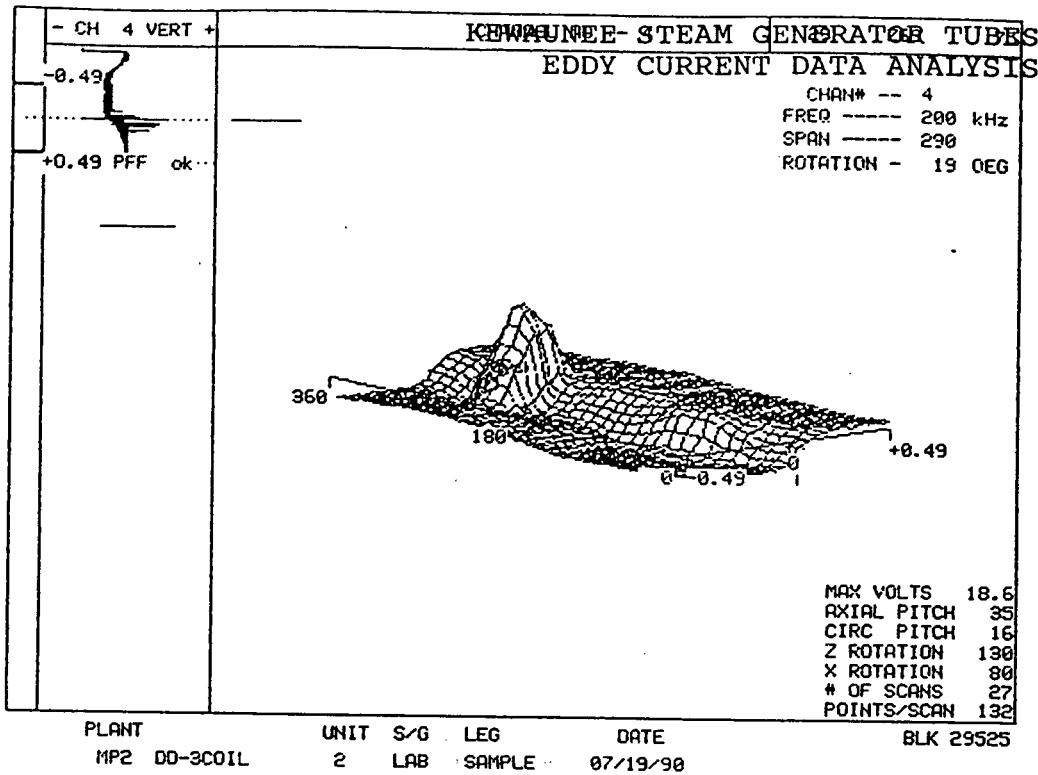
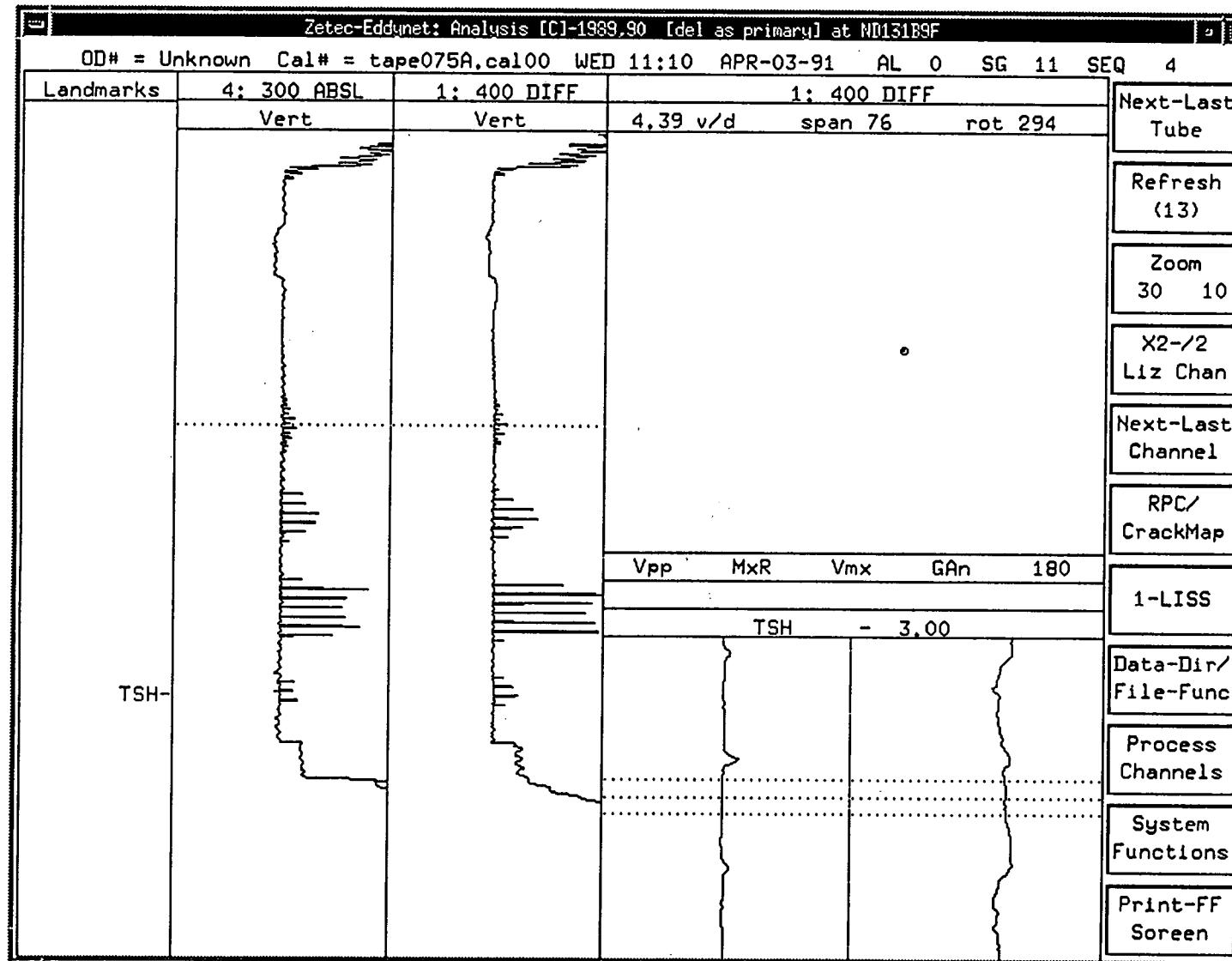
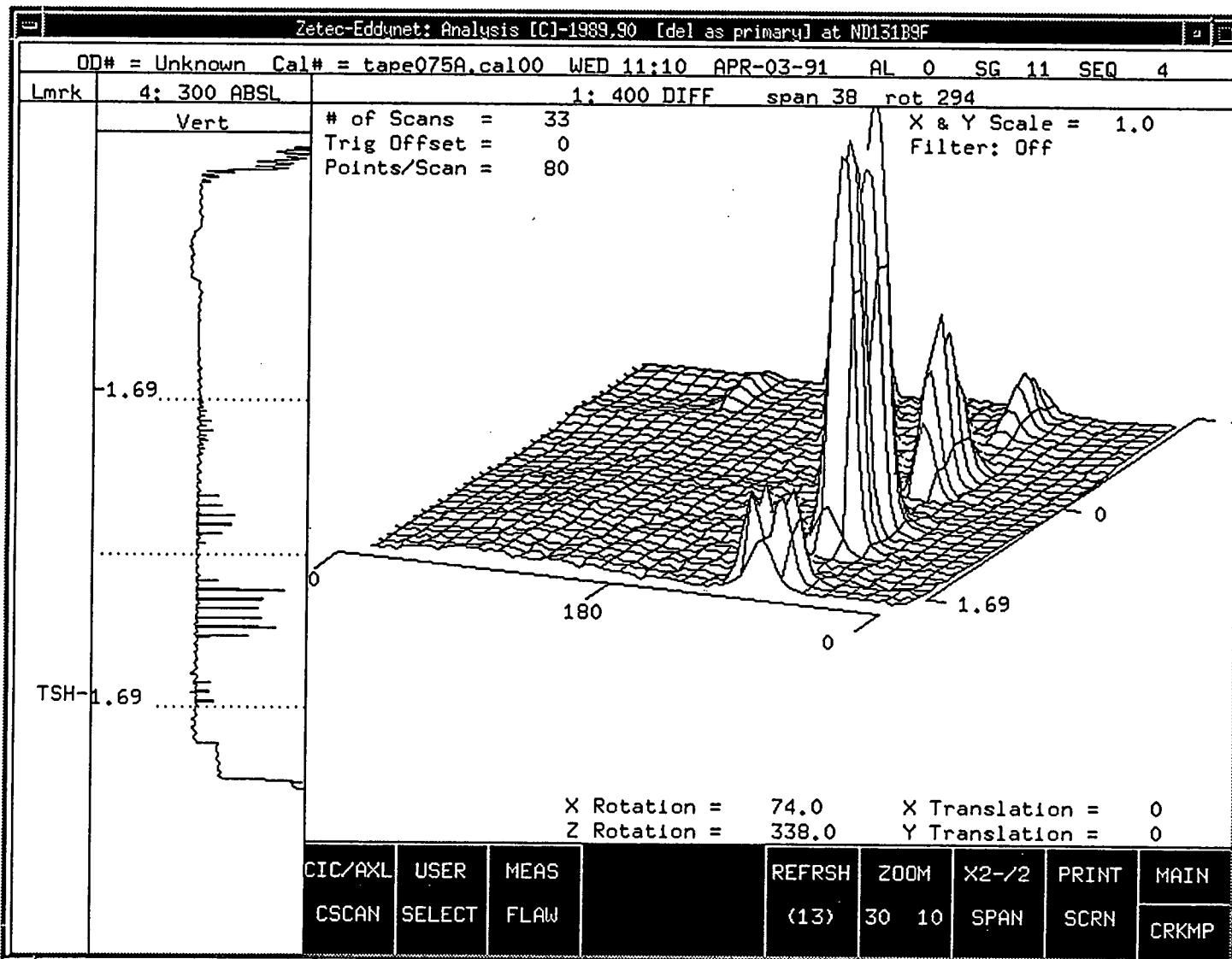


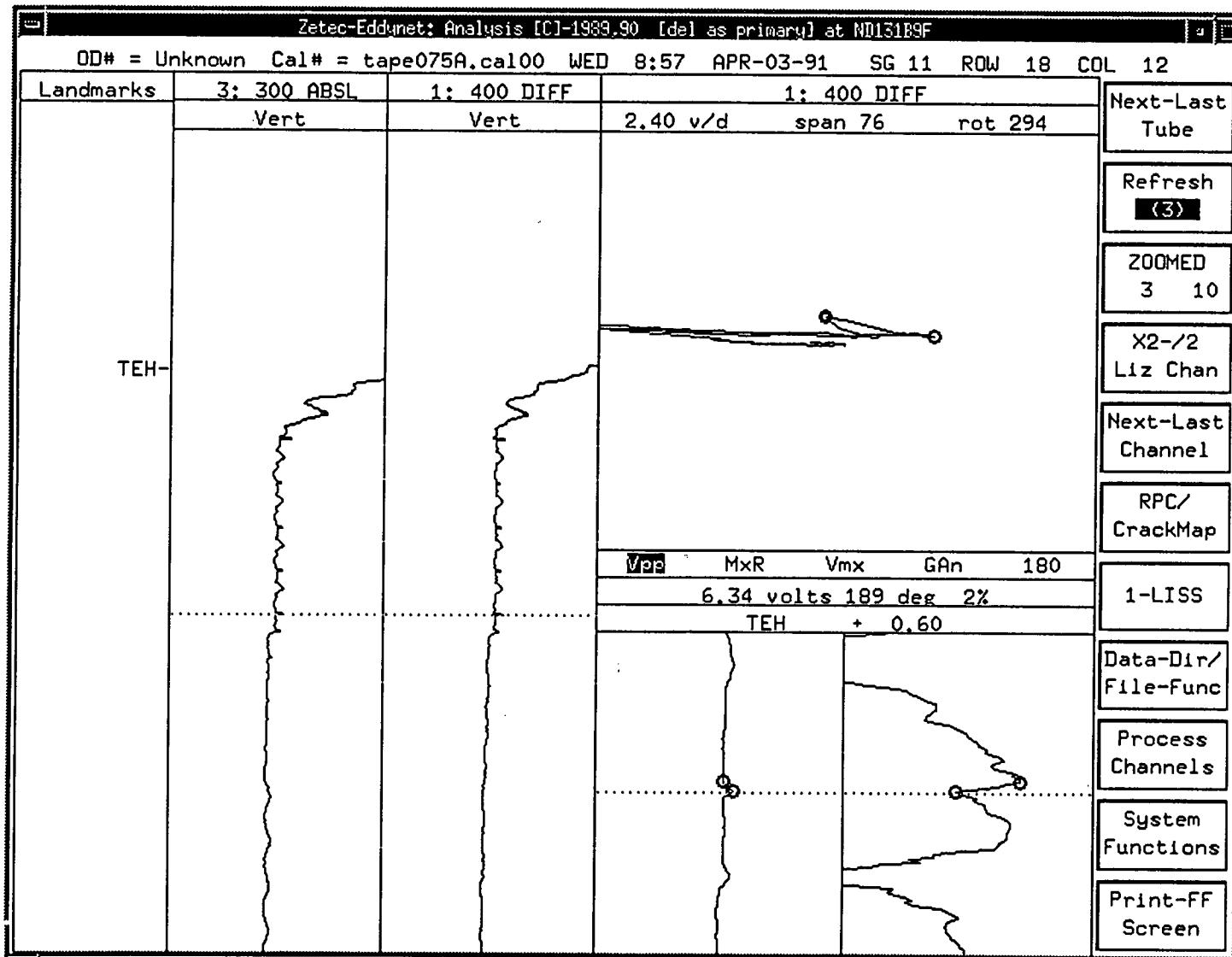
Figure 7B--Kewaunee Eddy Current-Liftoff Signal-Dent

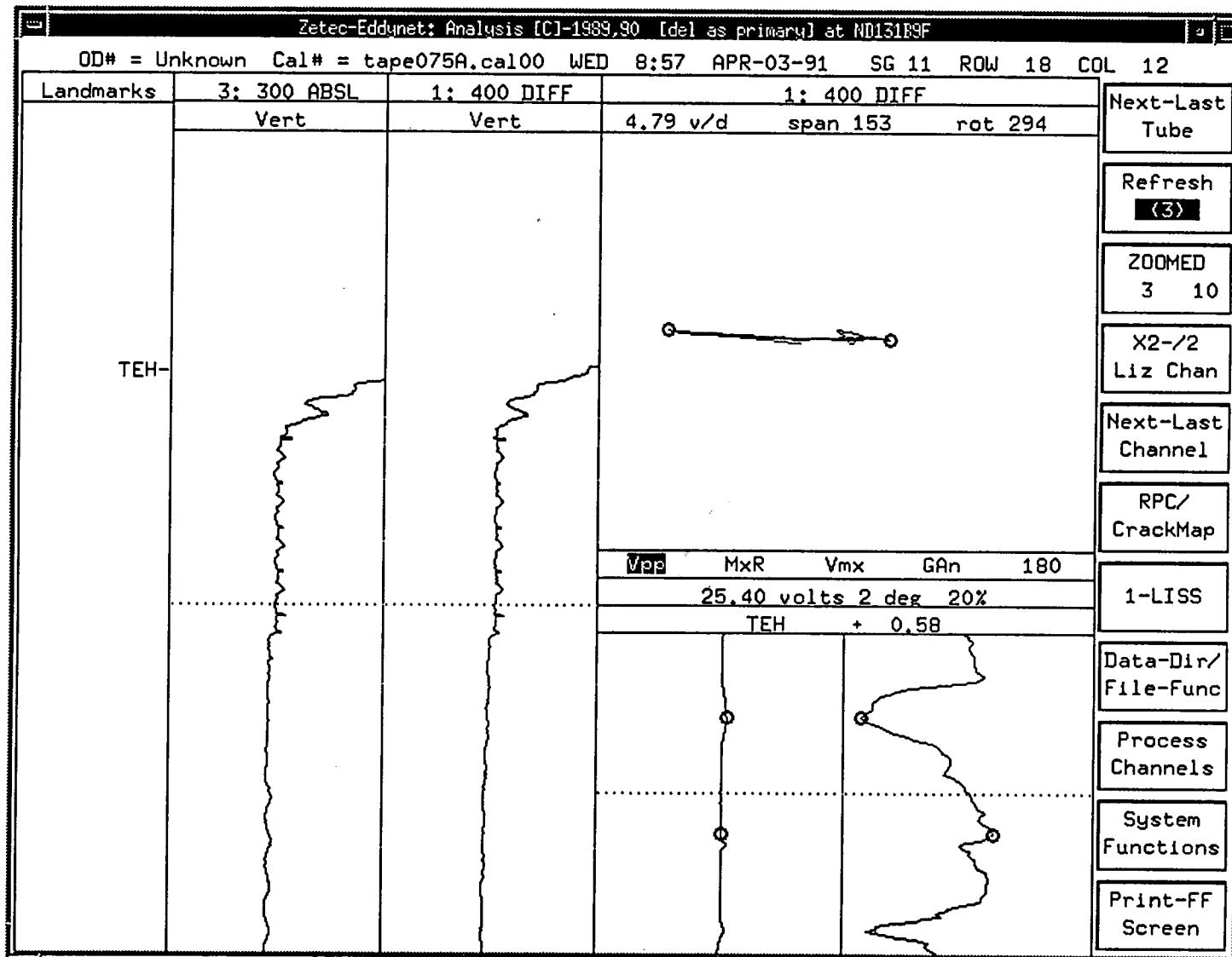
KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

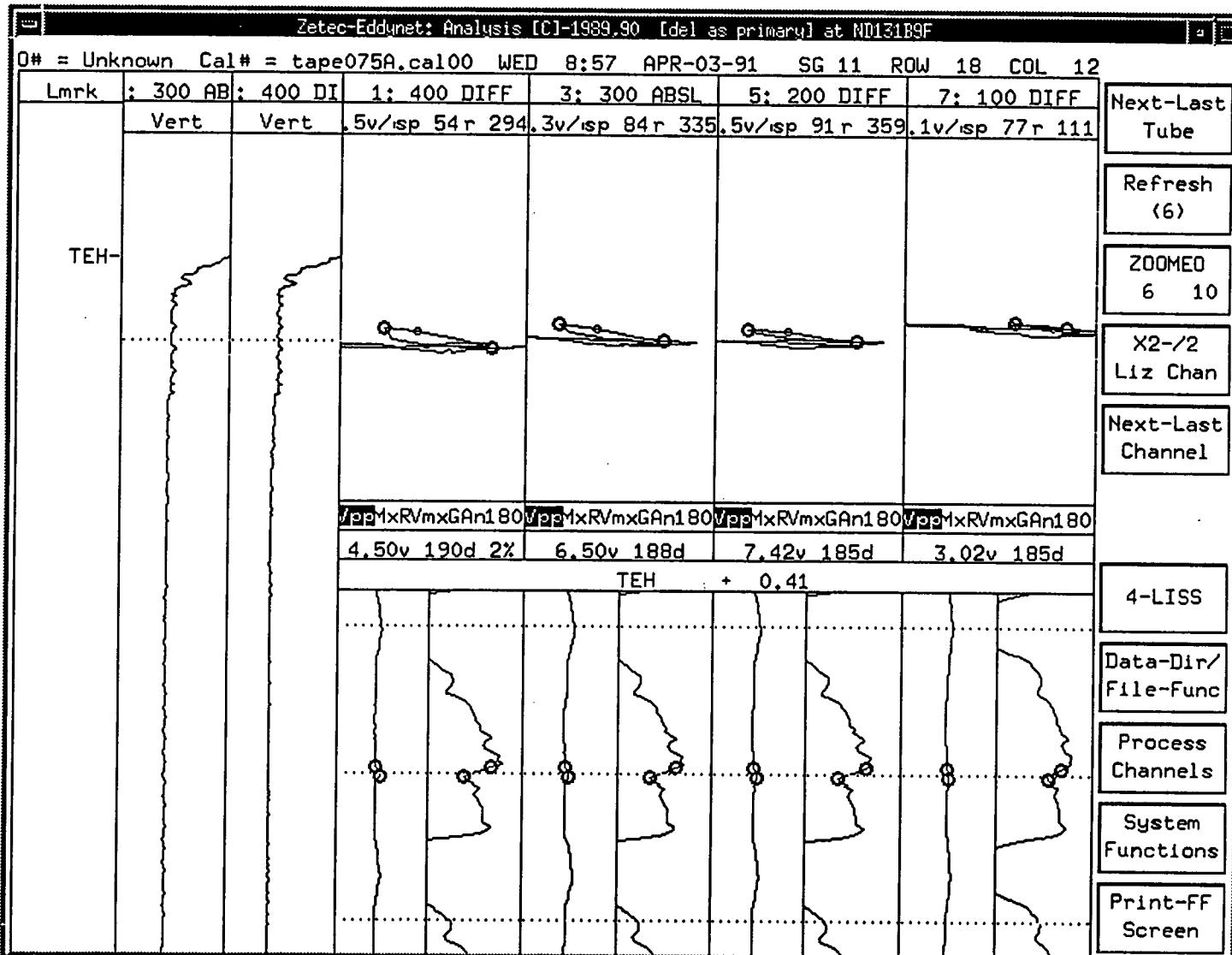
SECTION 5.0 - FIELD EDDY CURRENT GRAPHICS

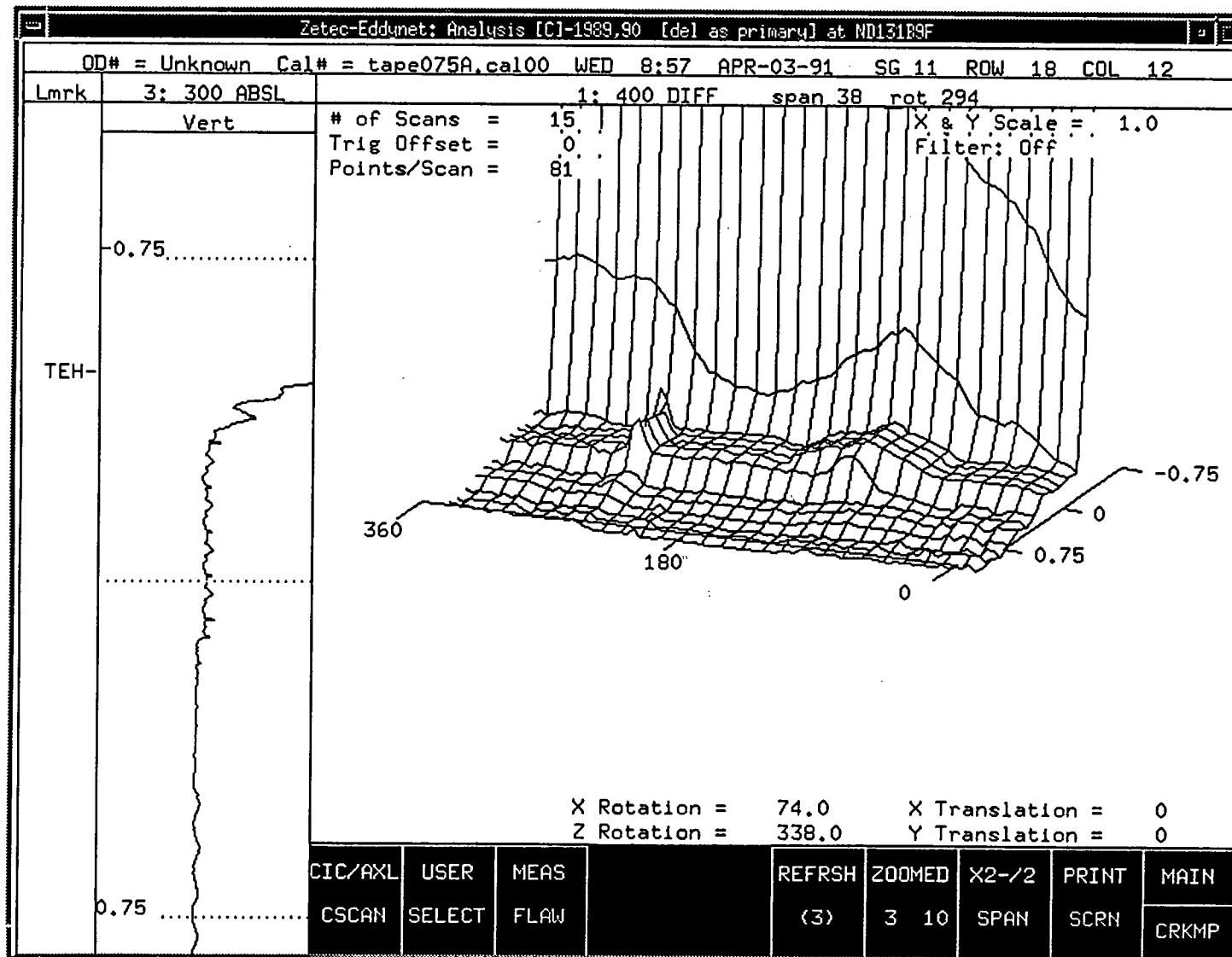


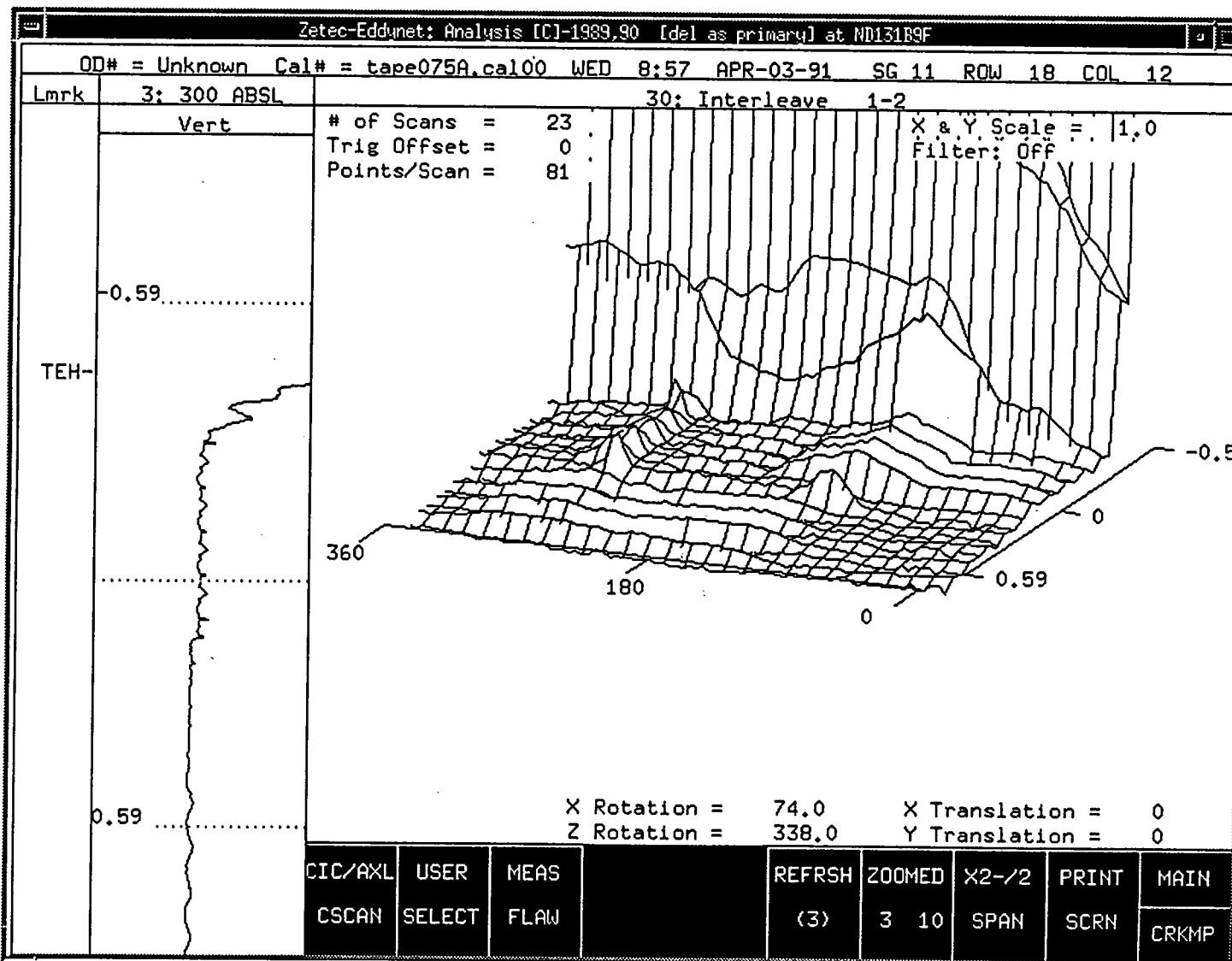


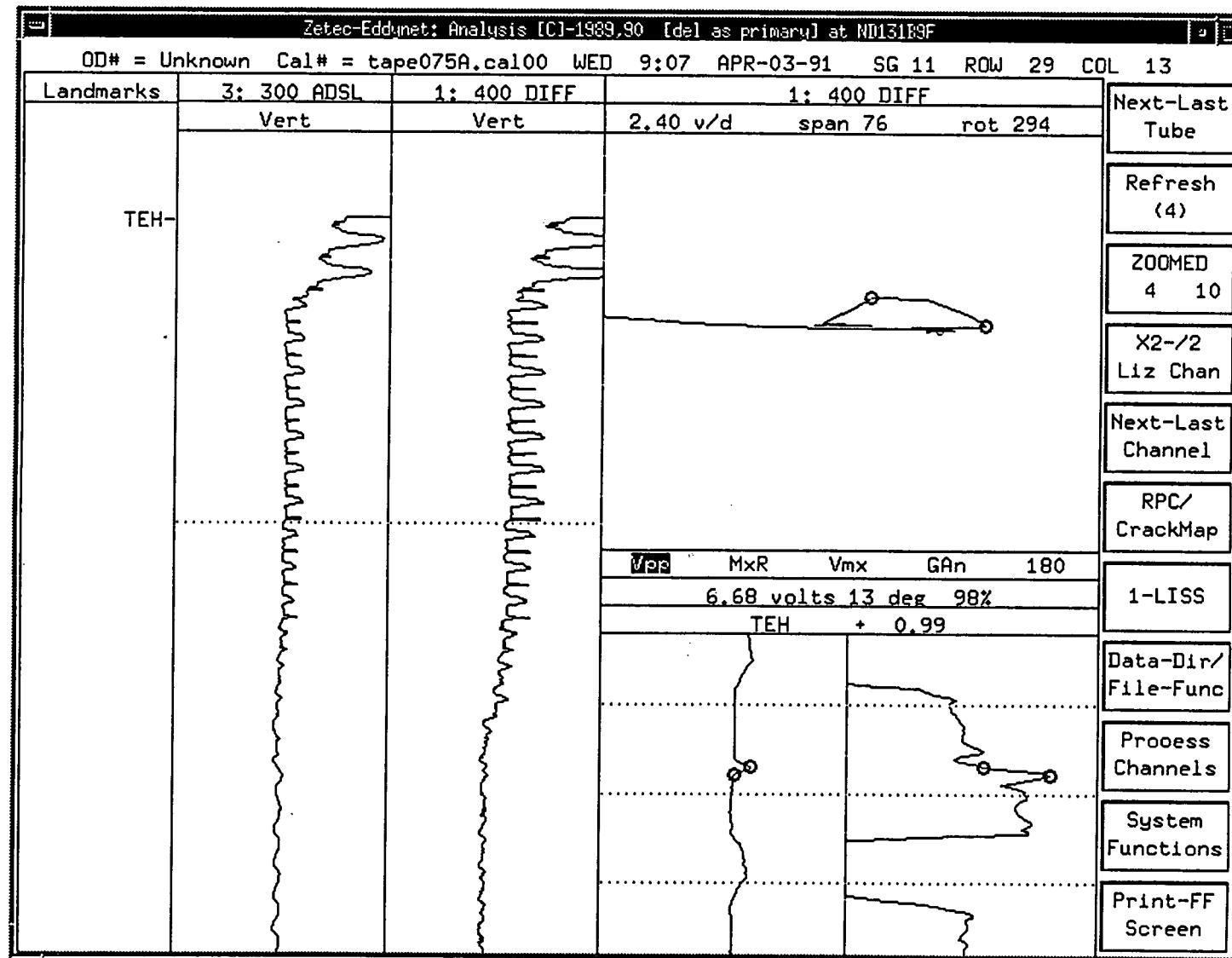


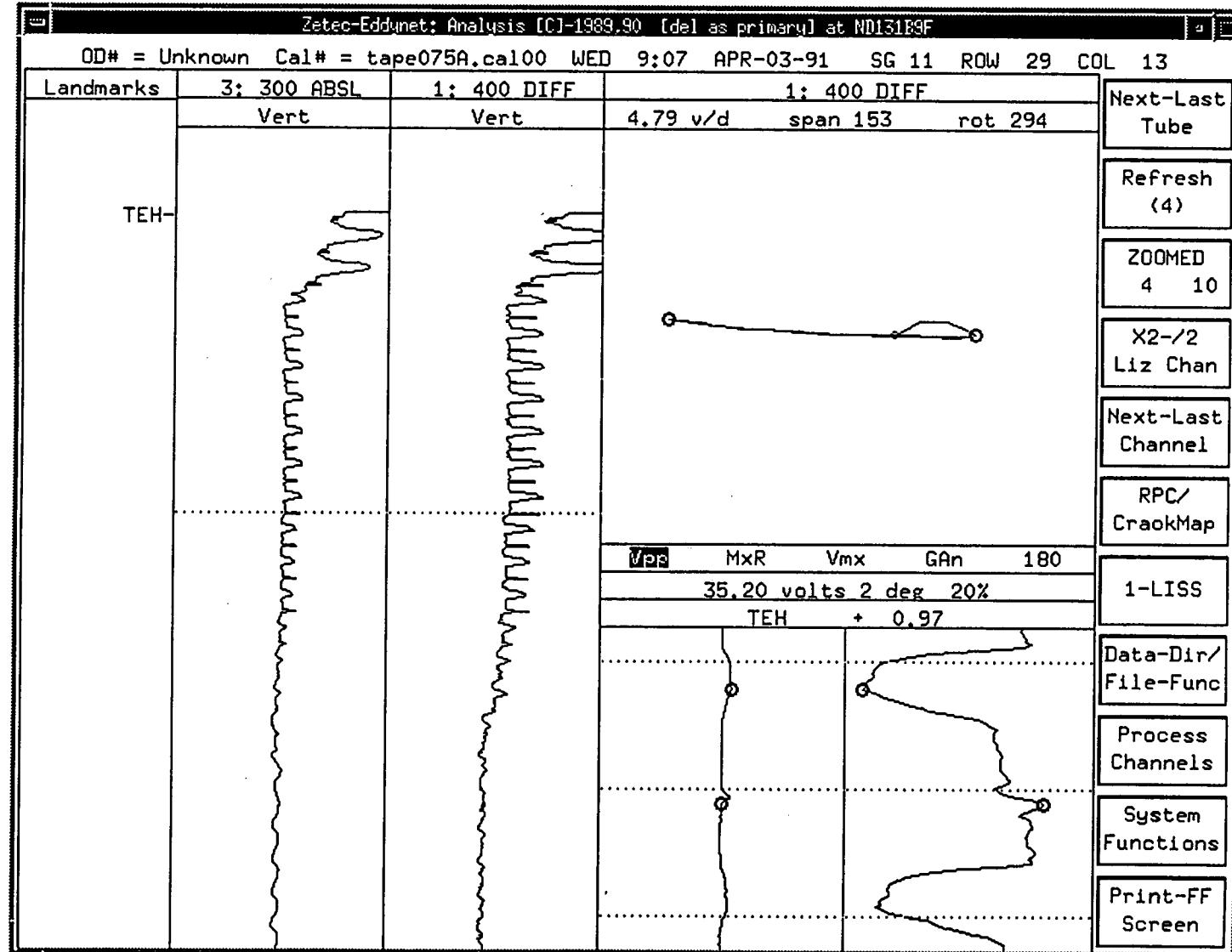


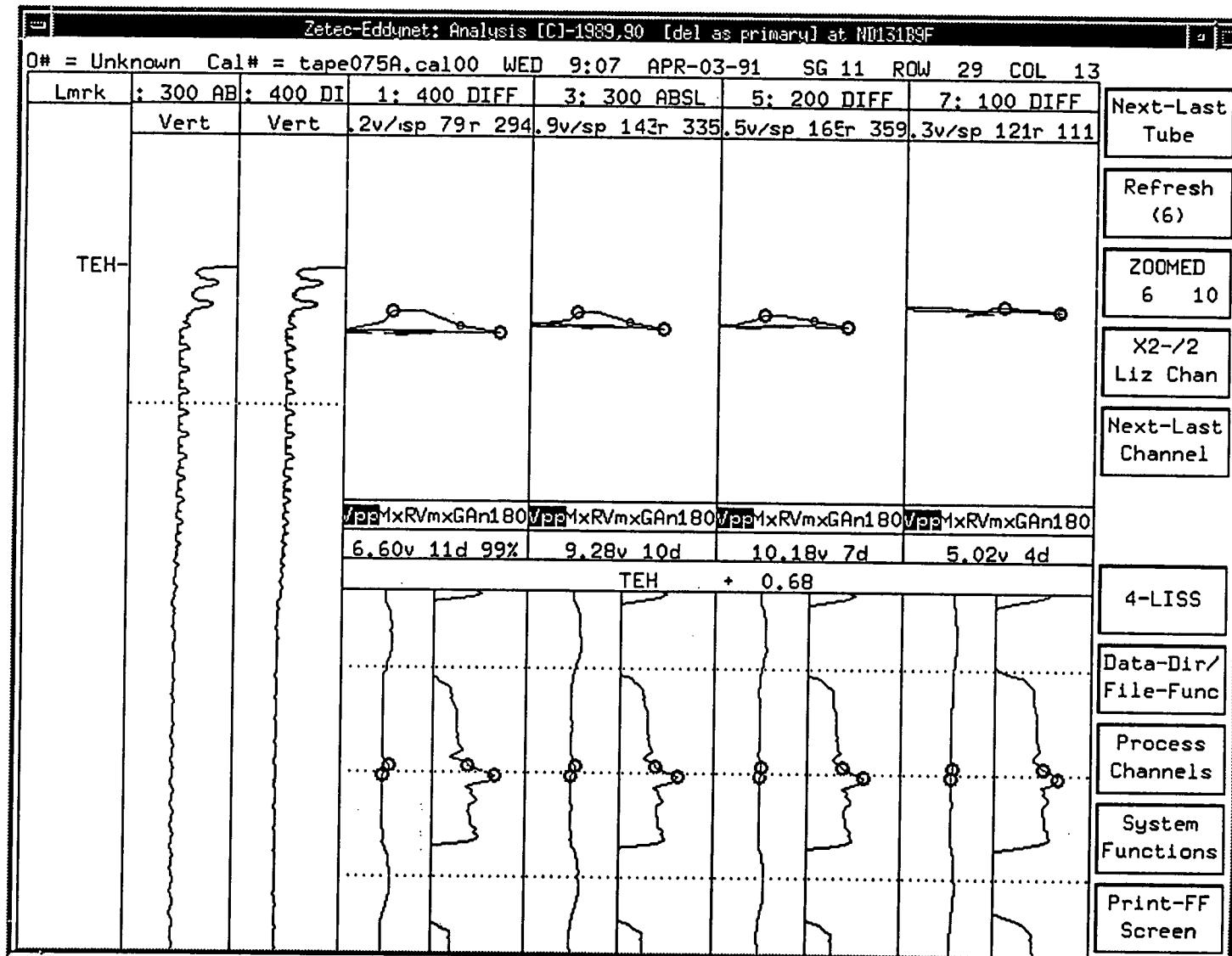


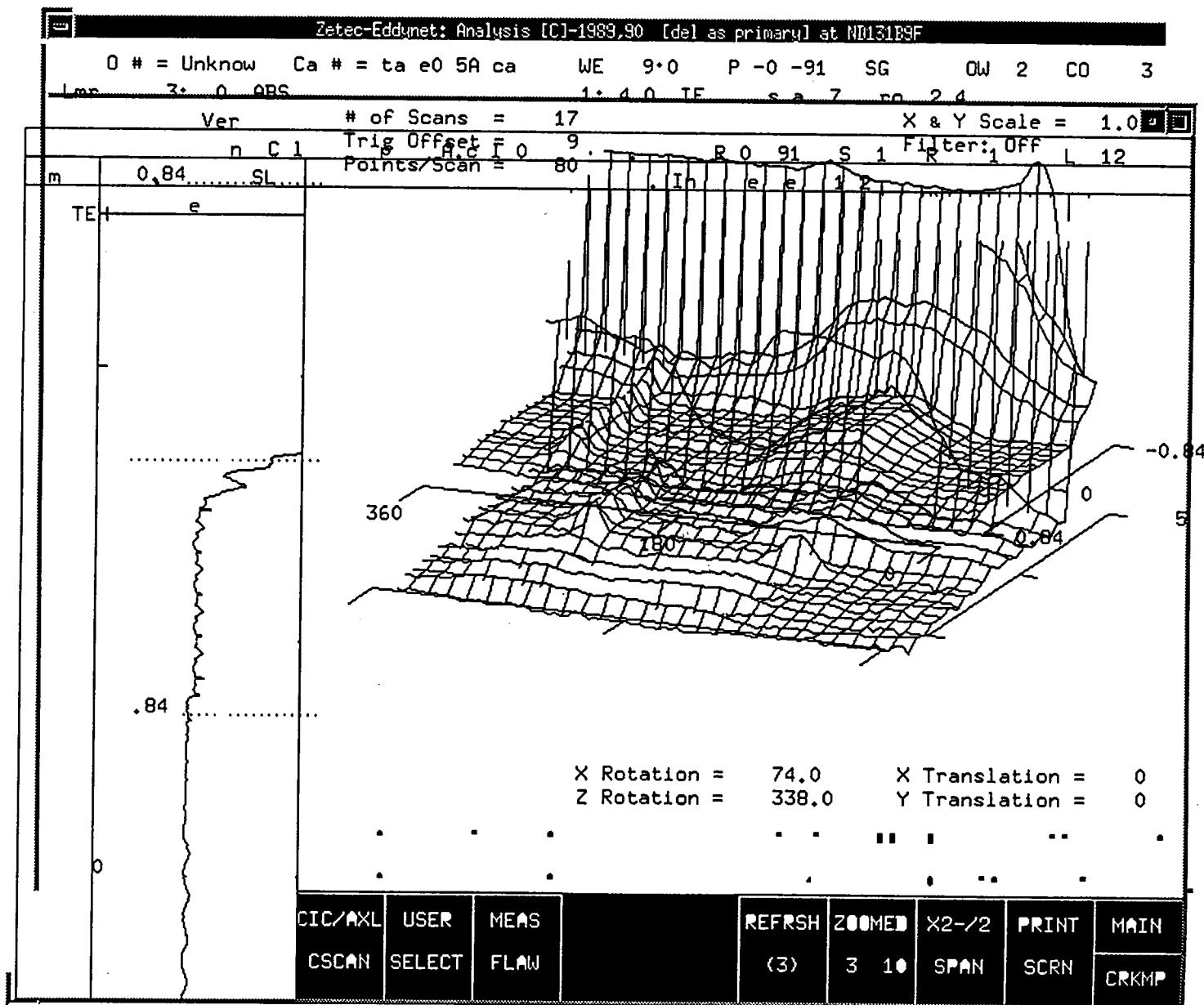


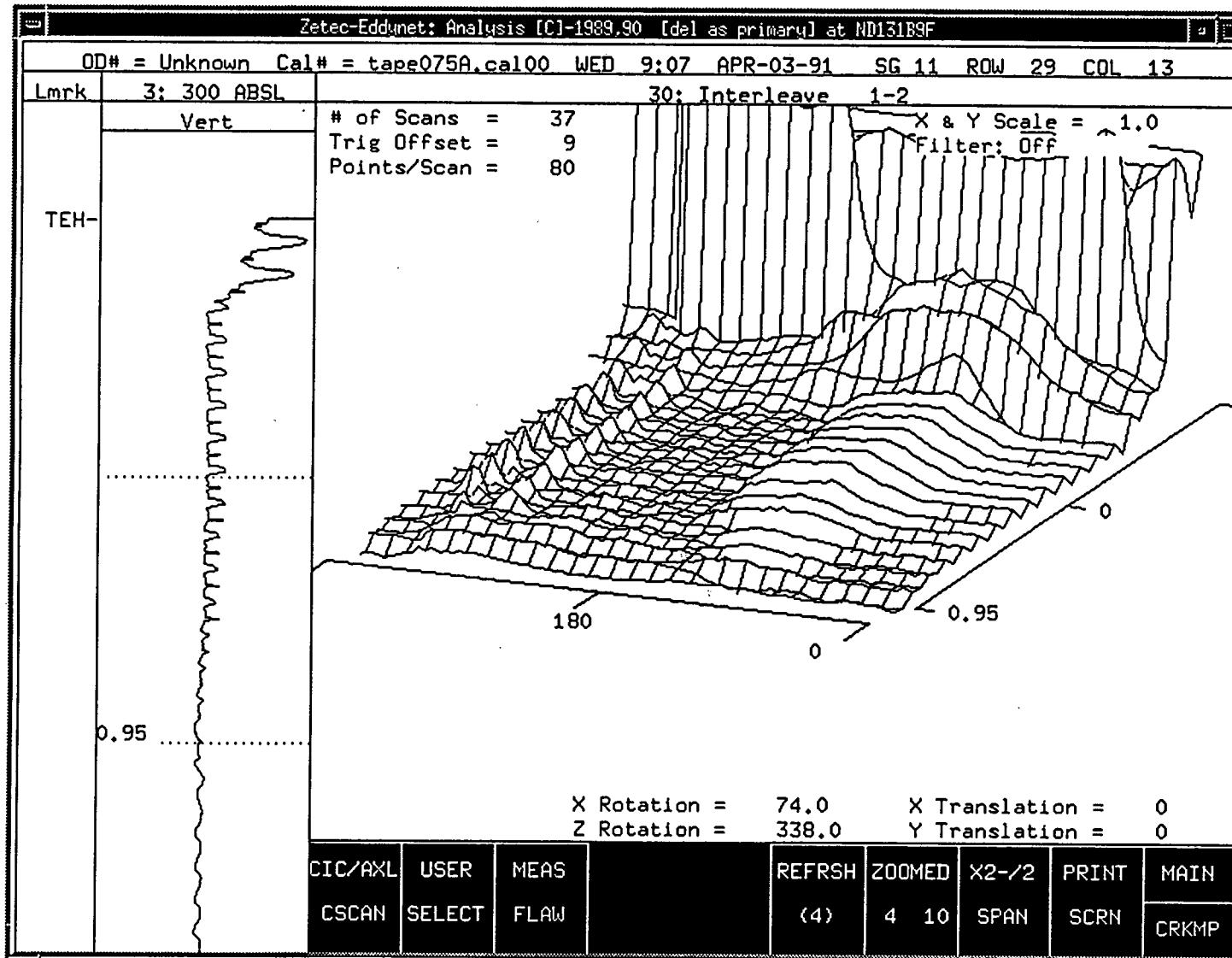


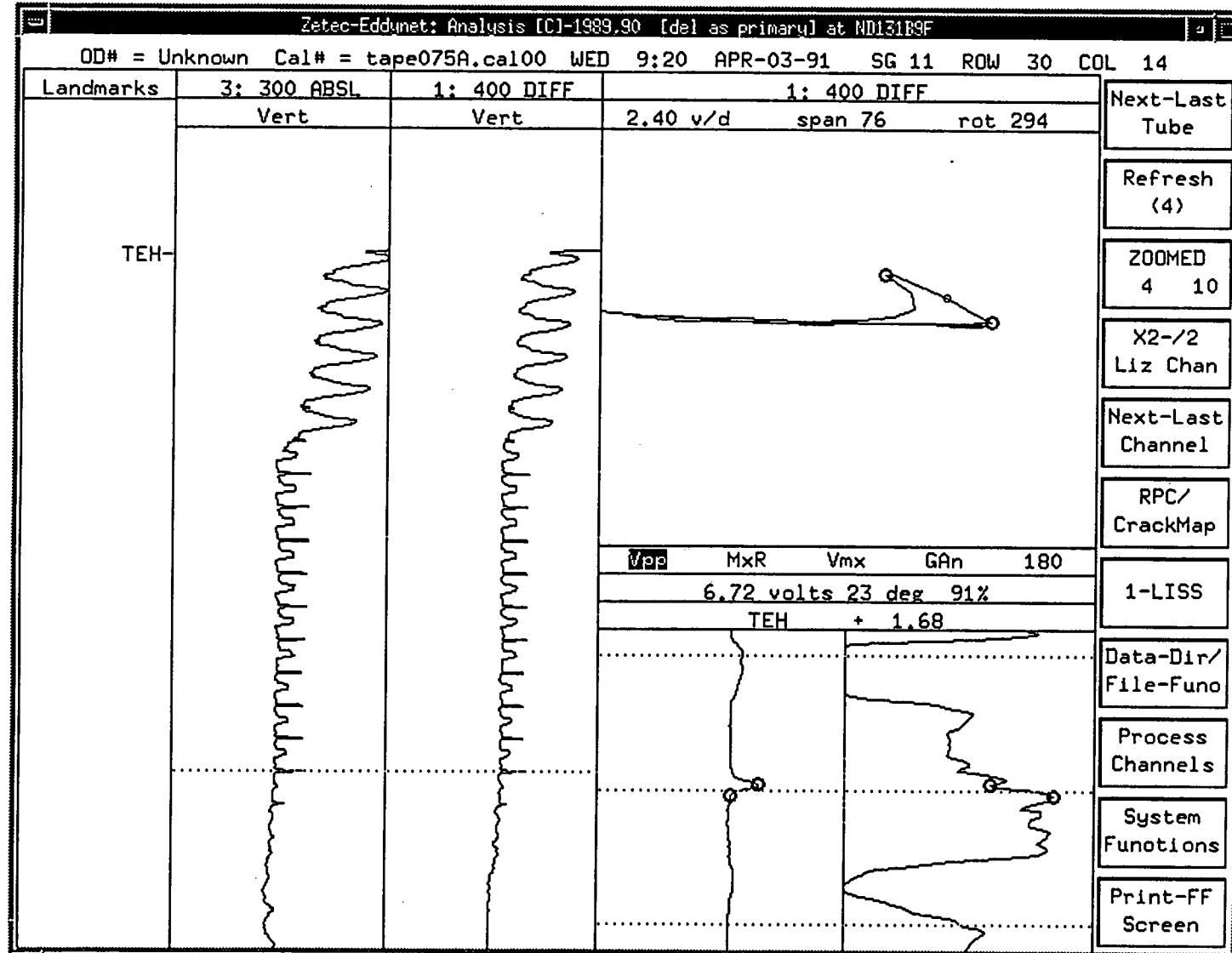


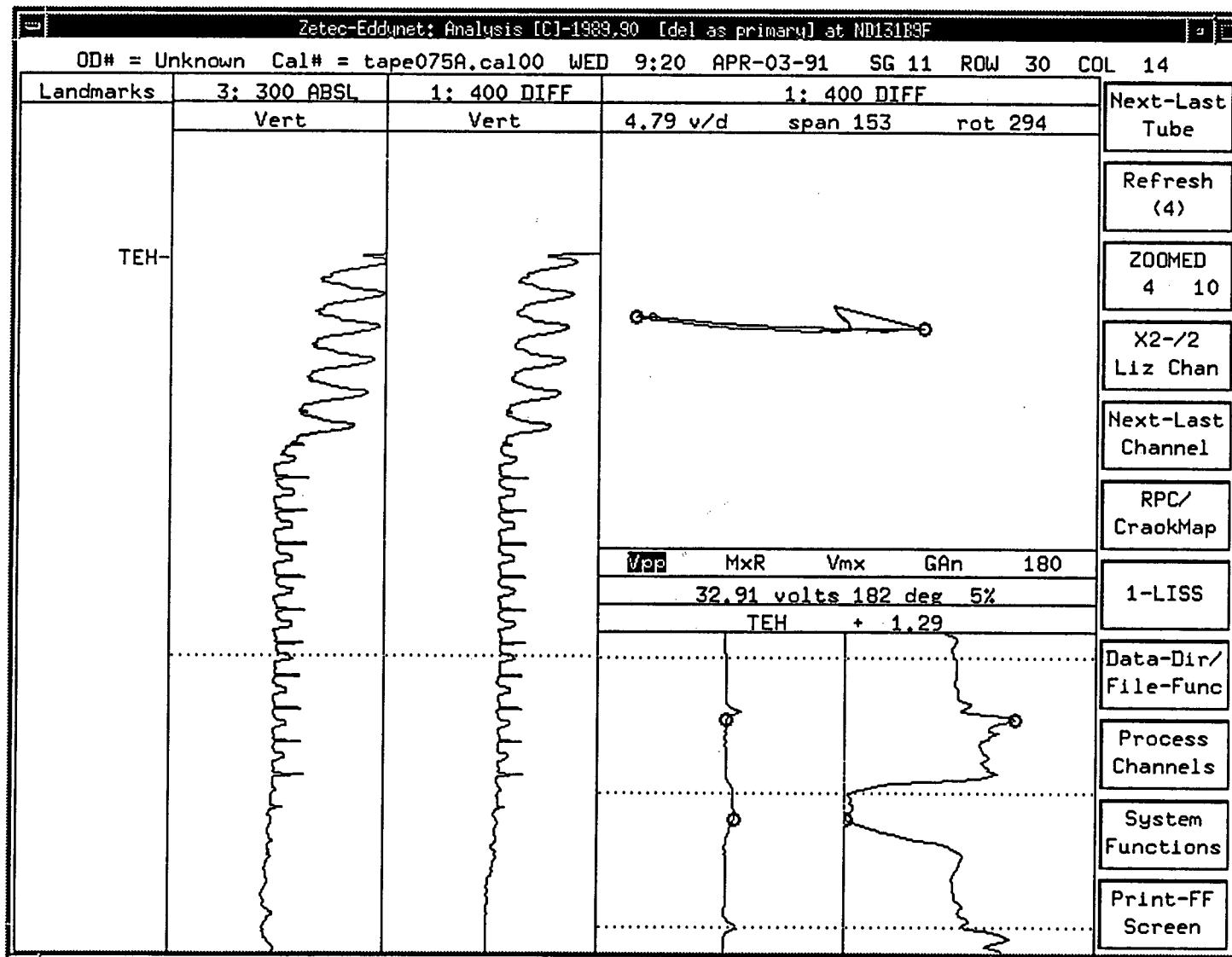


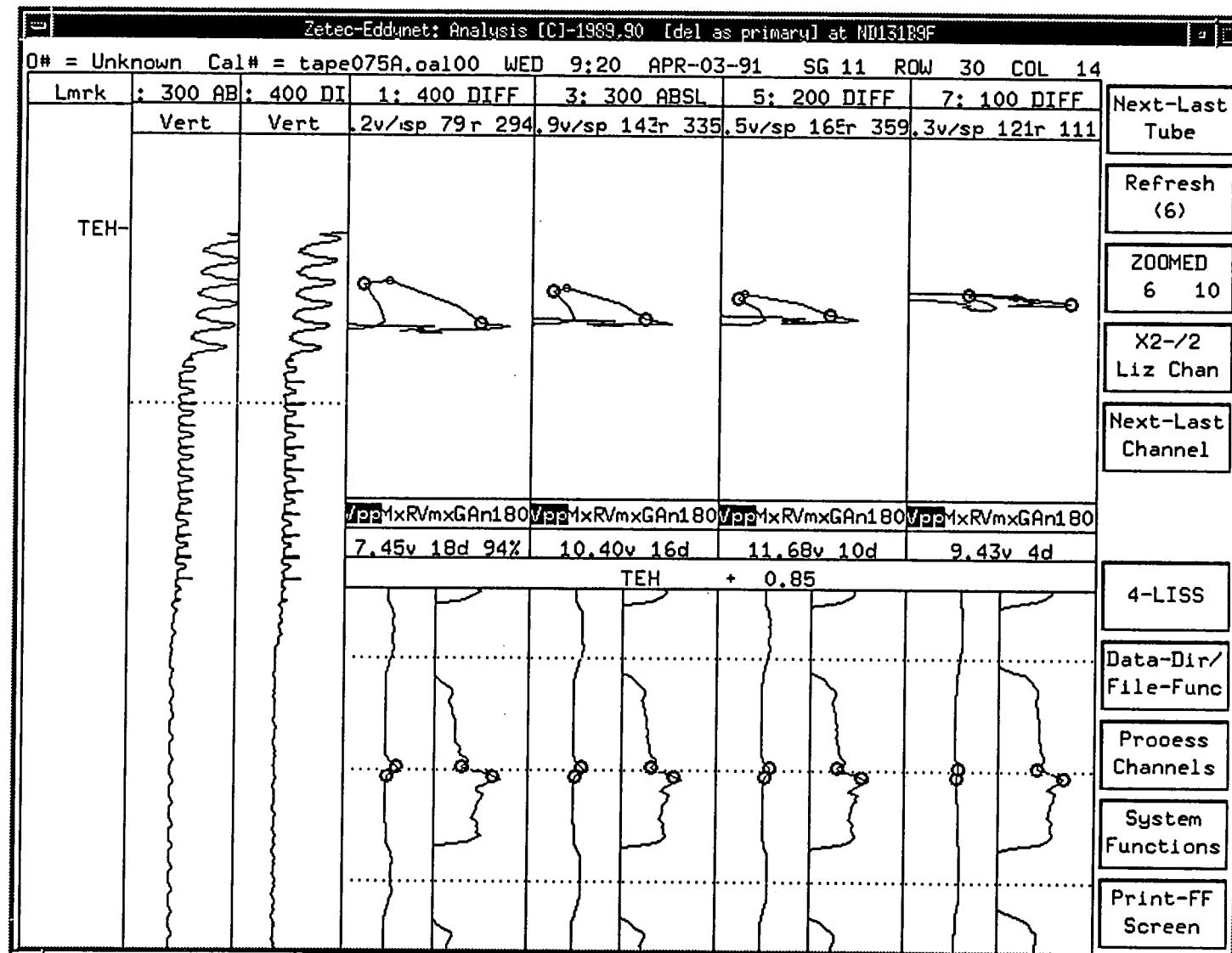


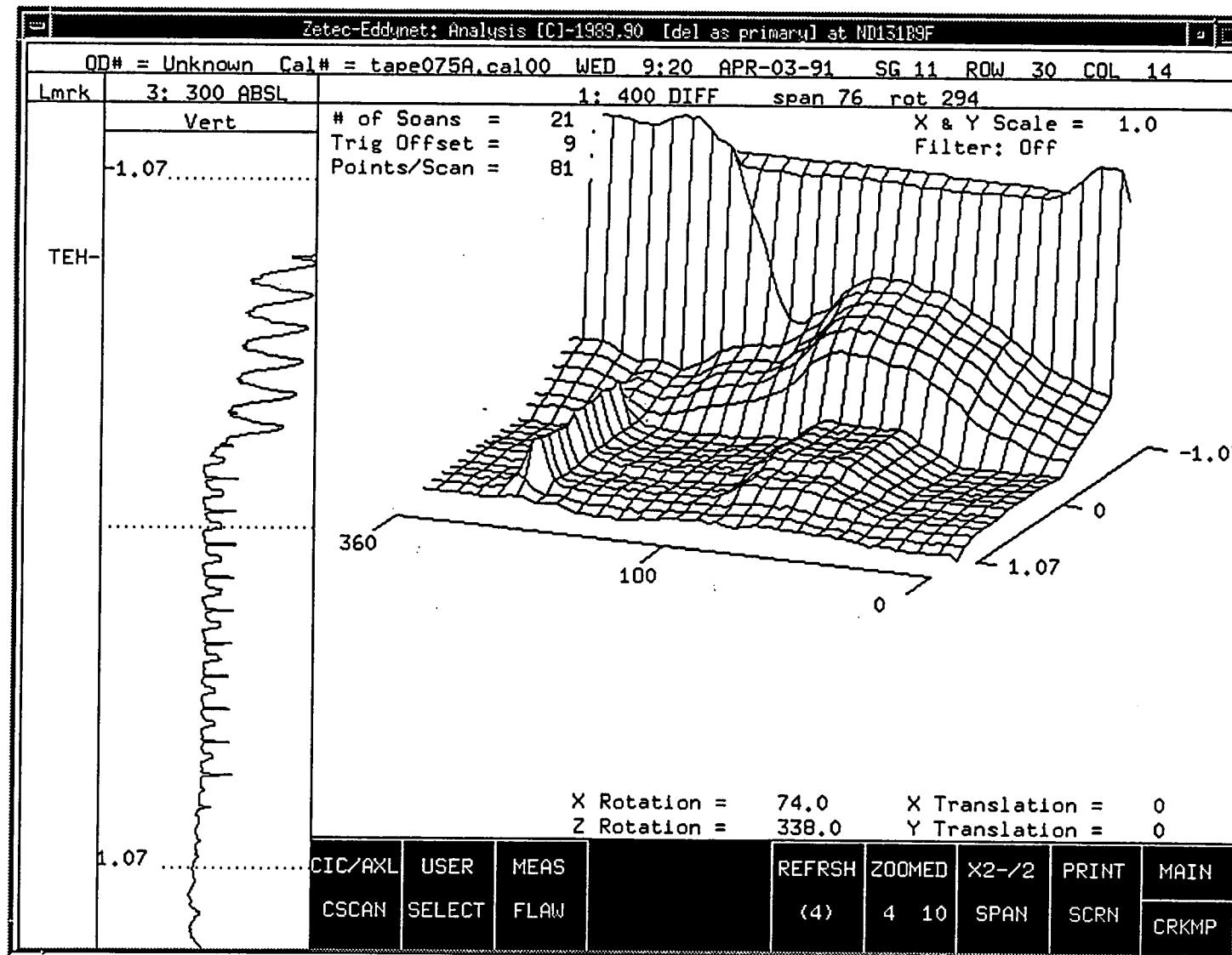


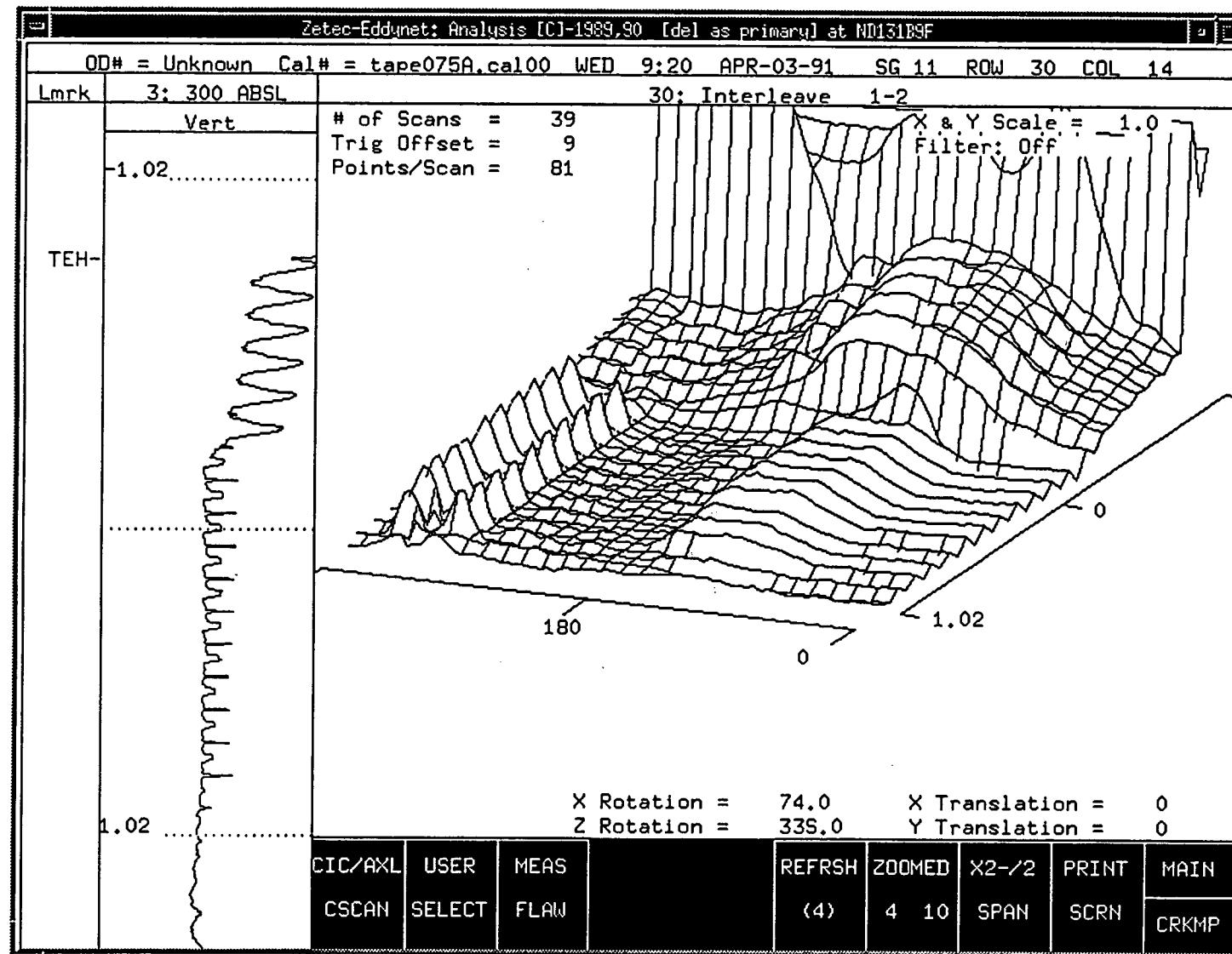


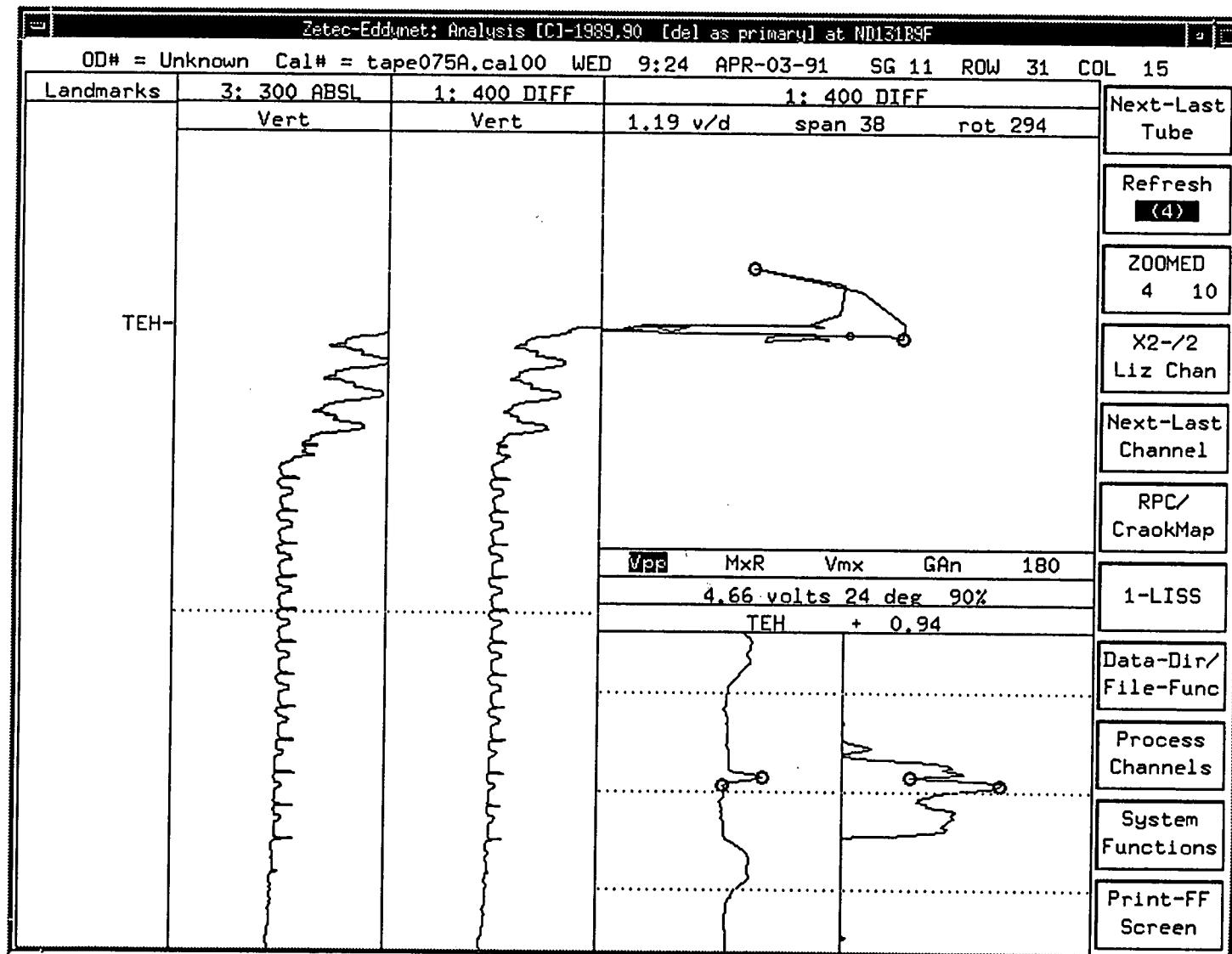


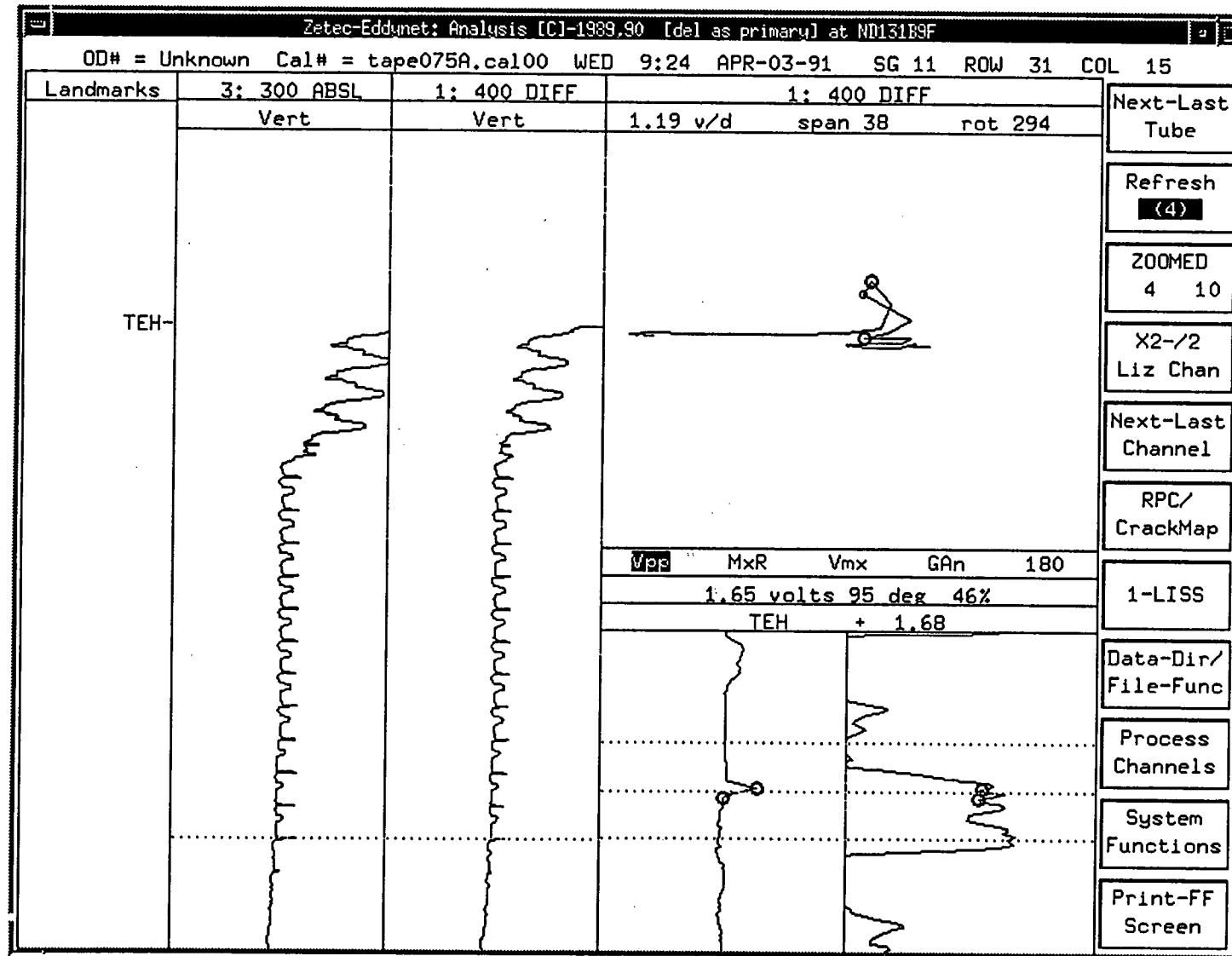


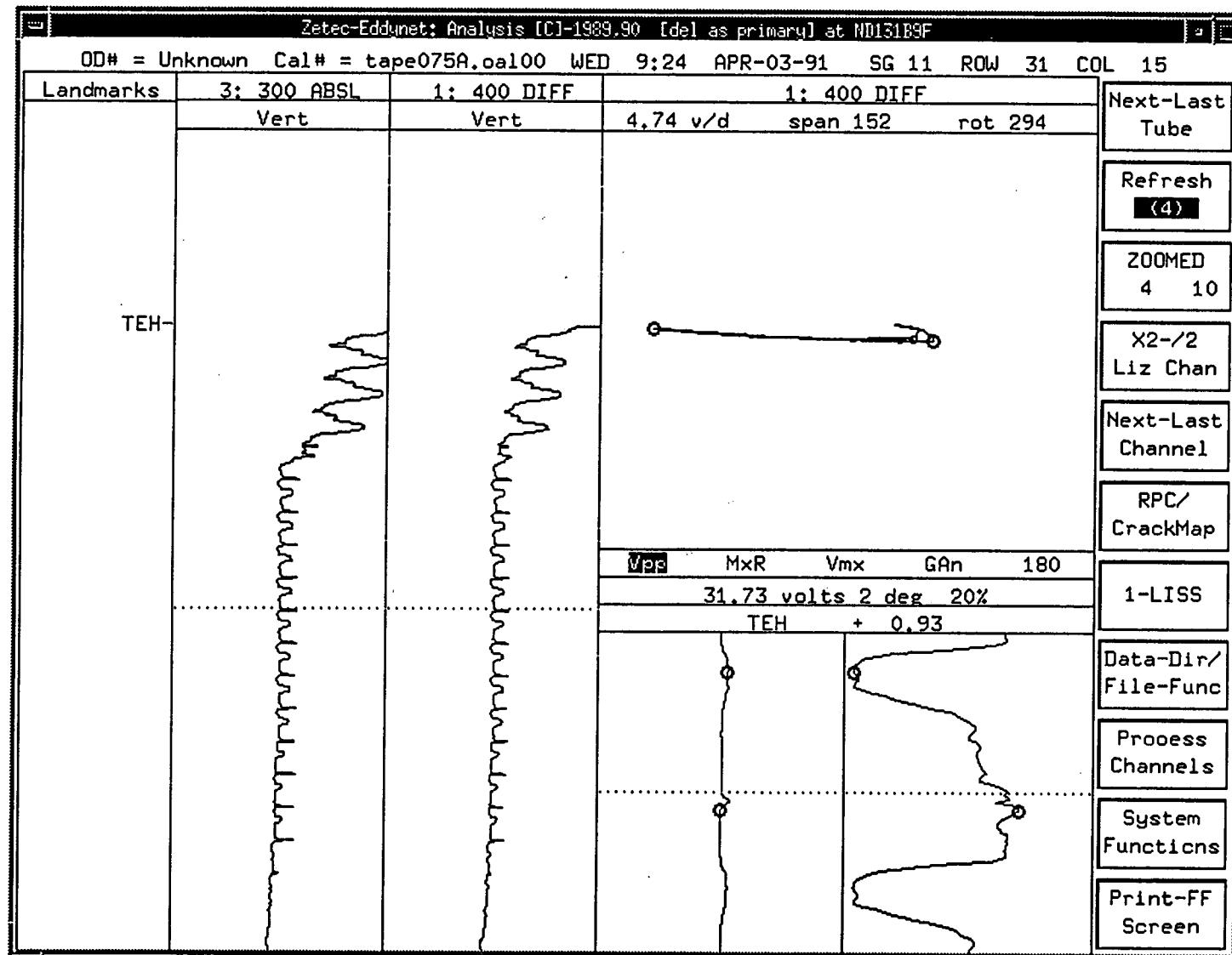


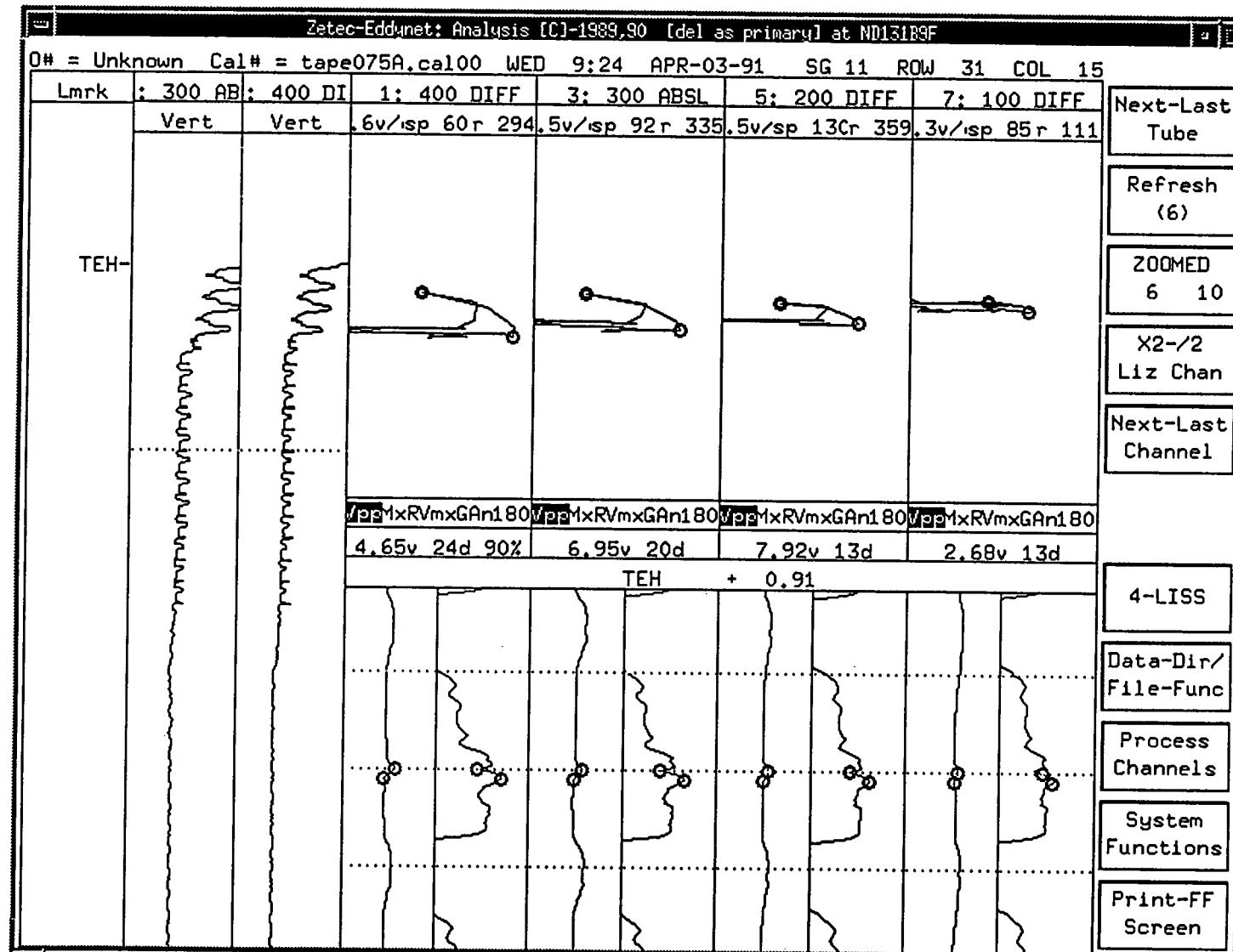


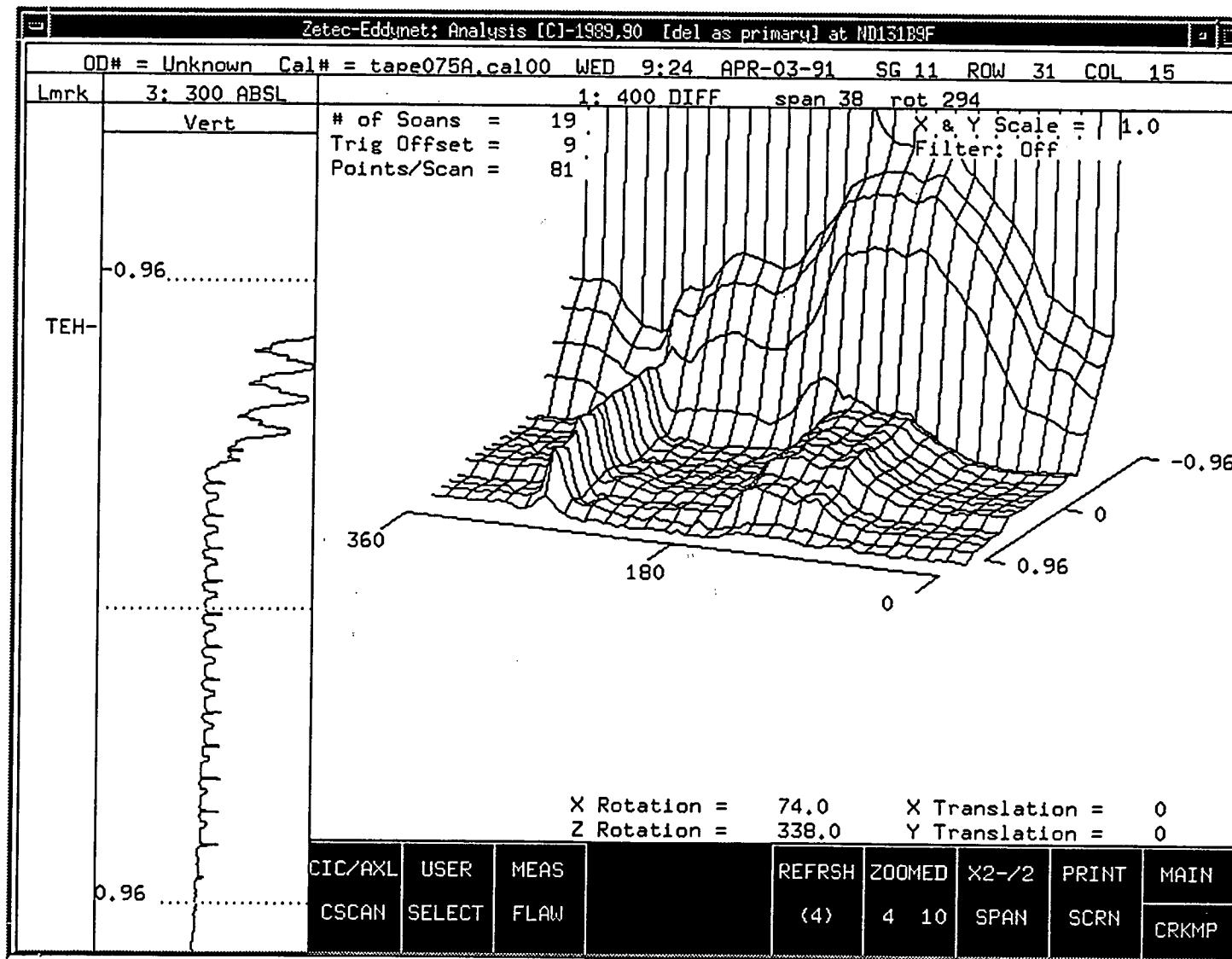


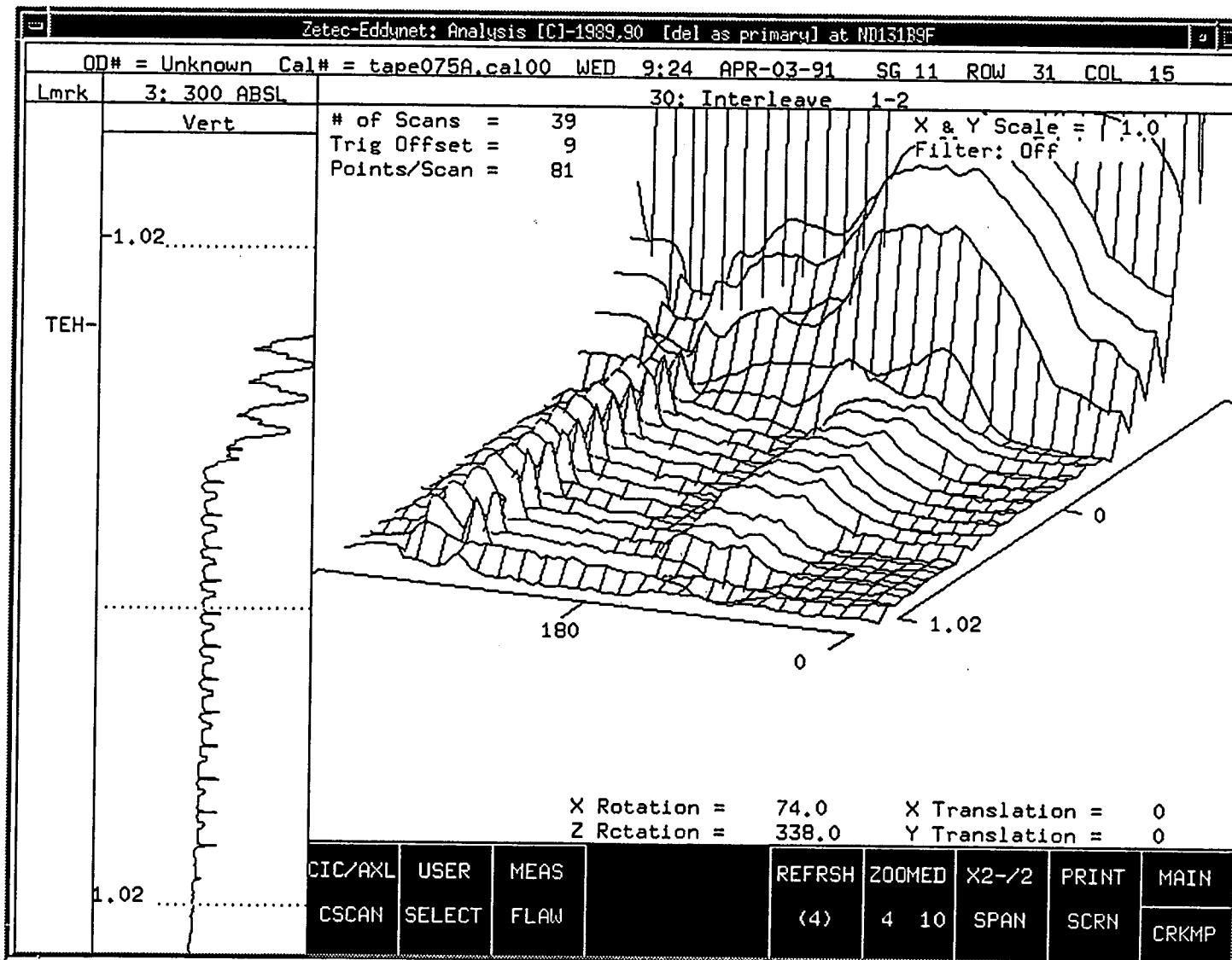


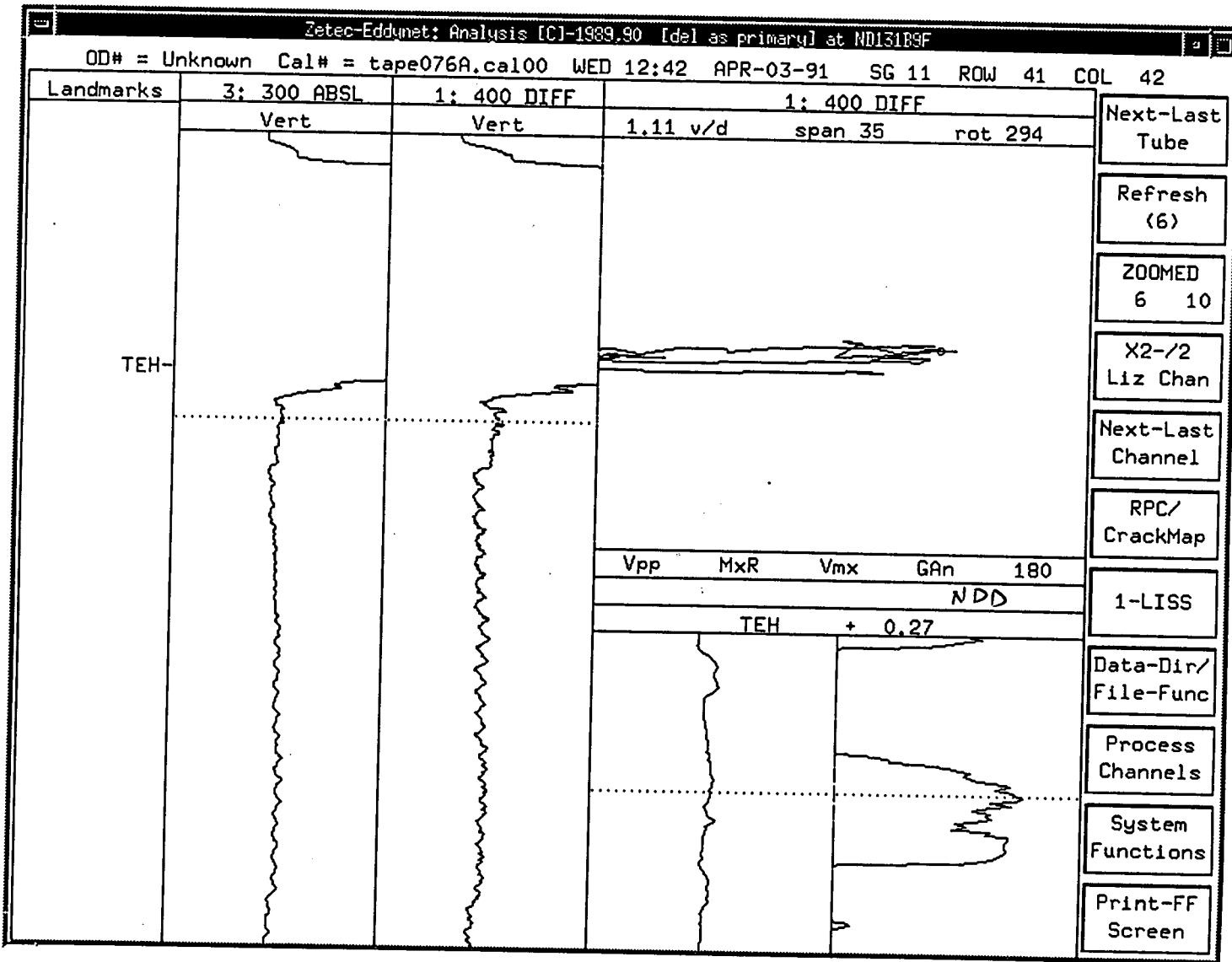


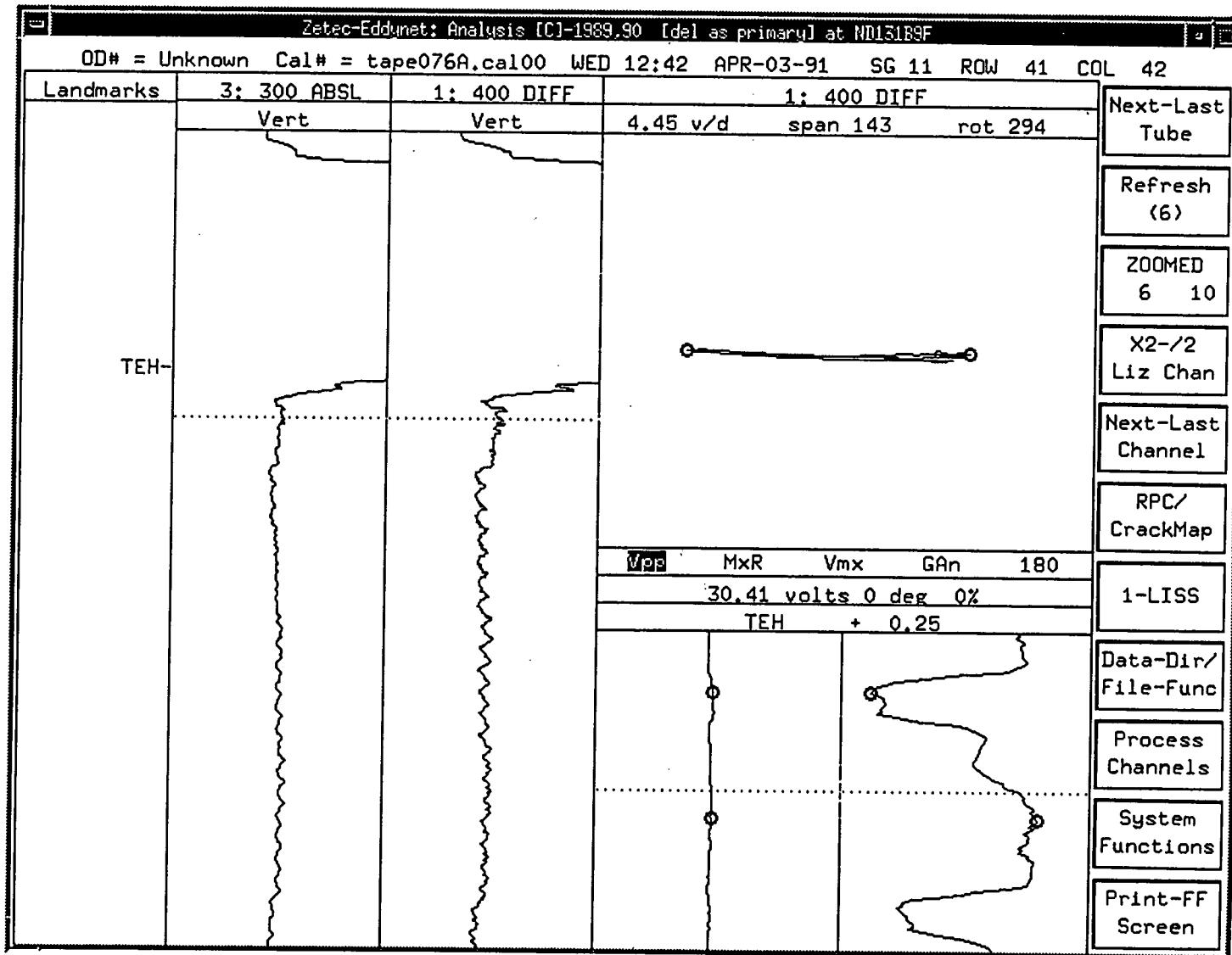


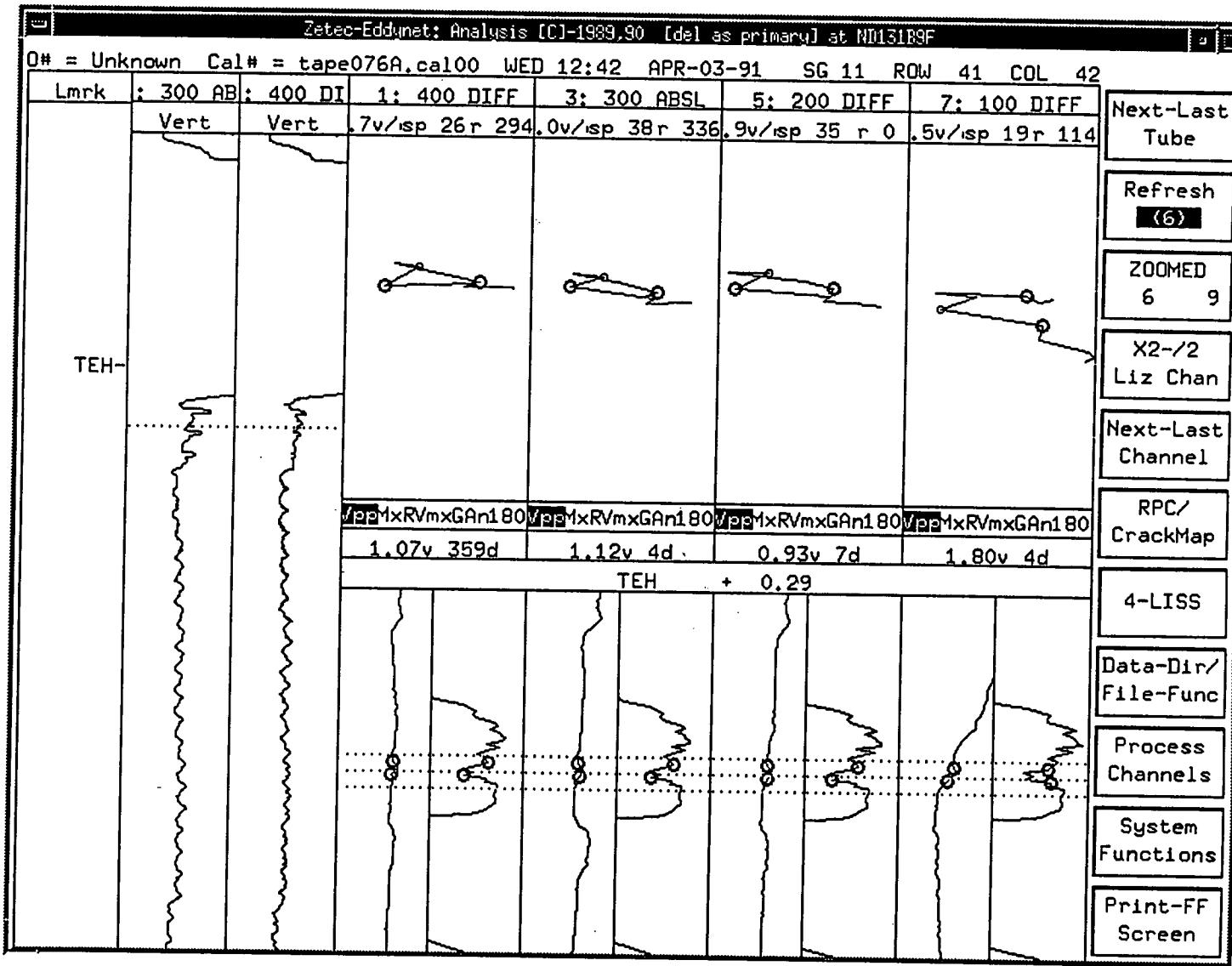


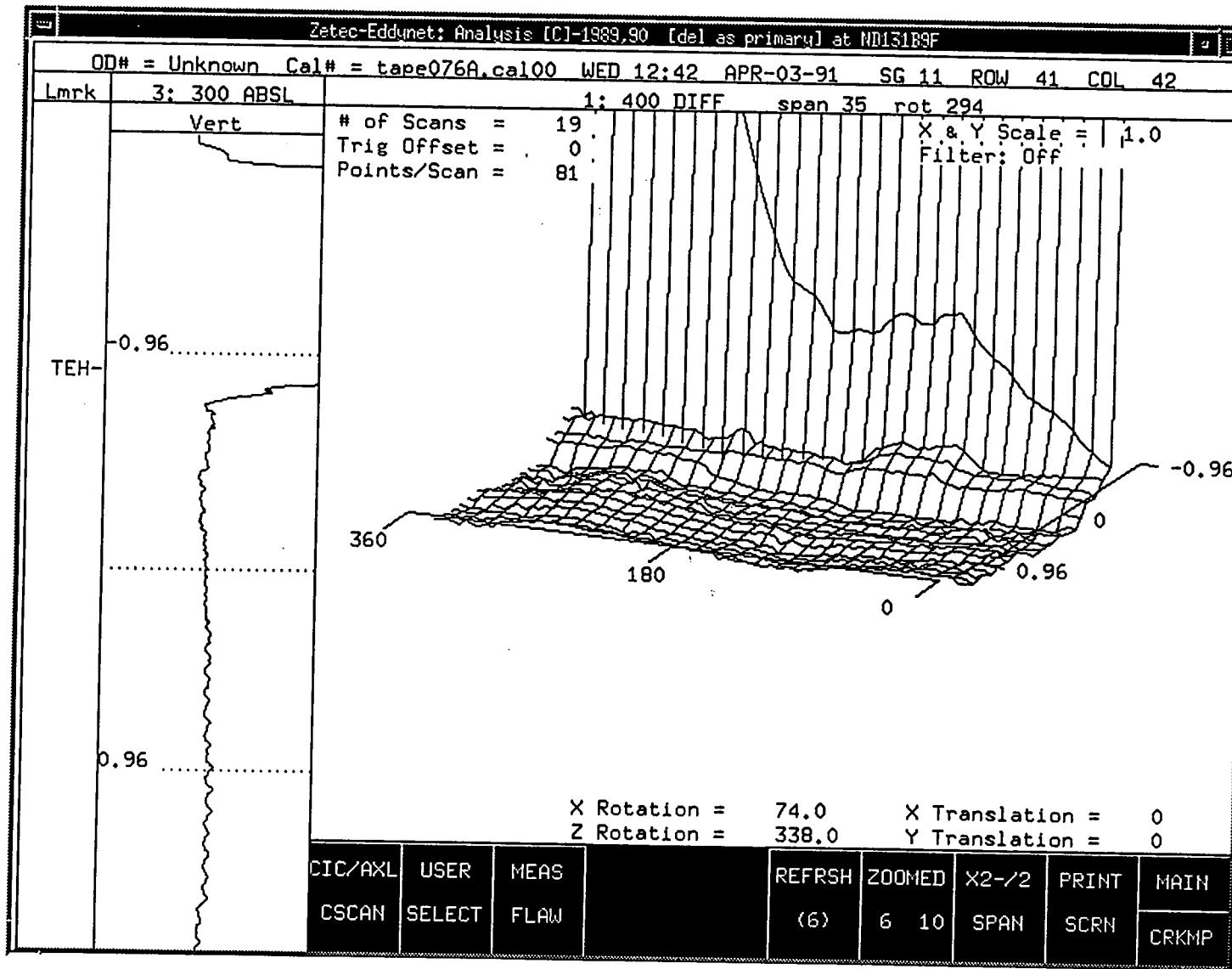


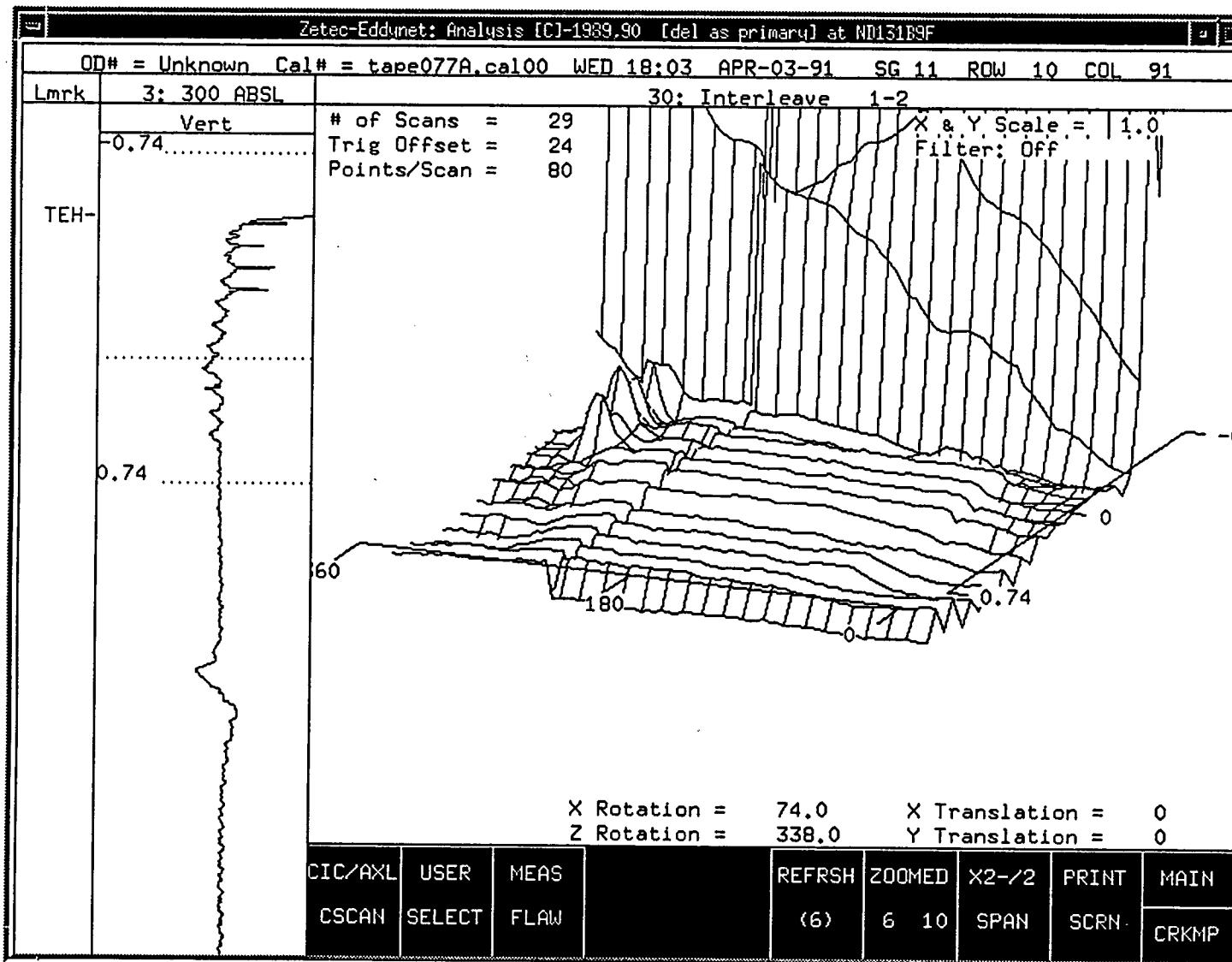


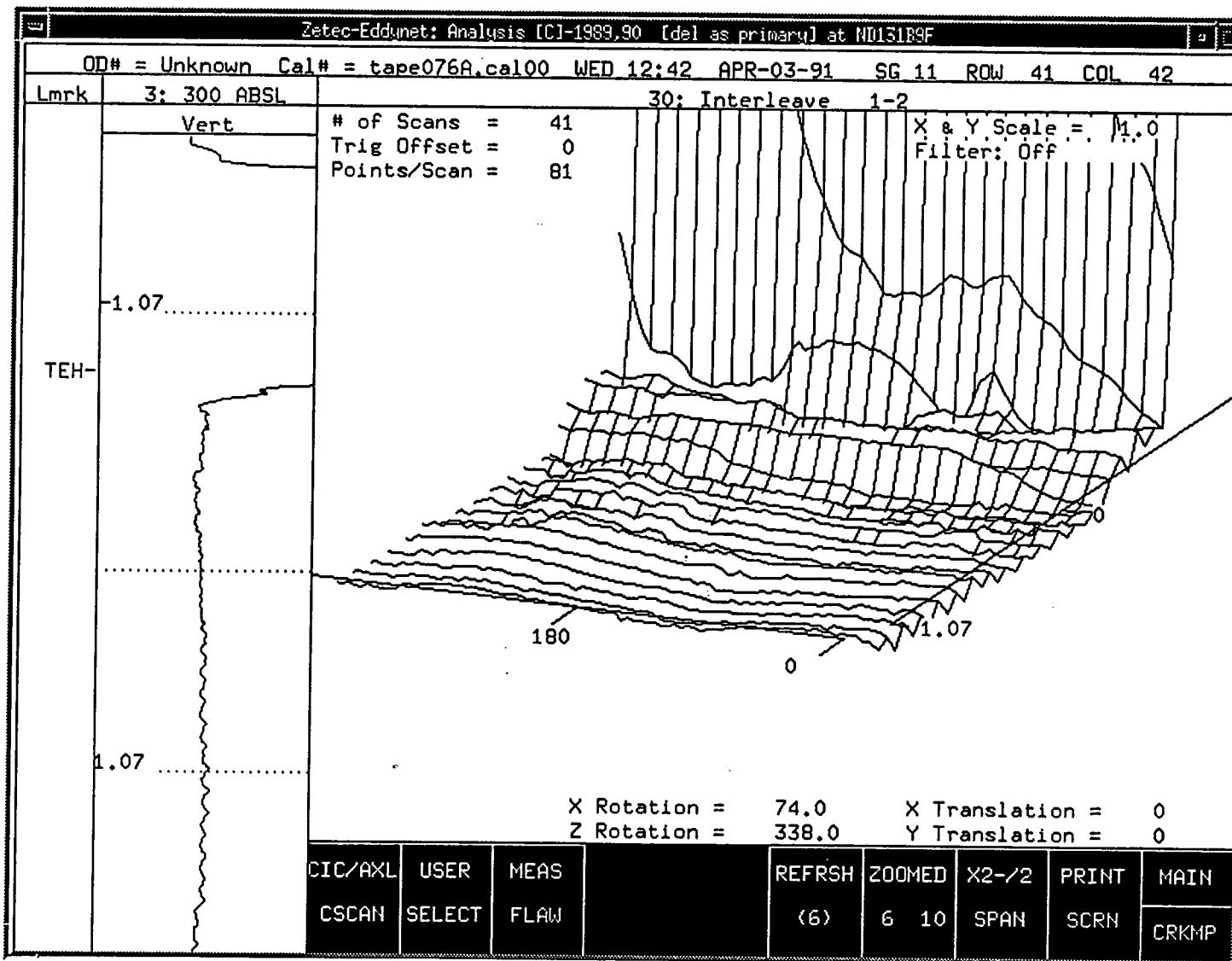


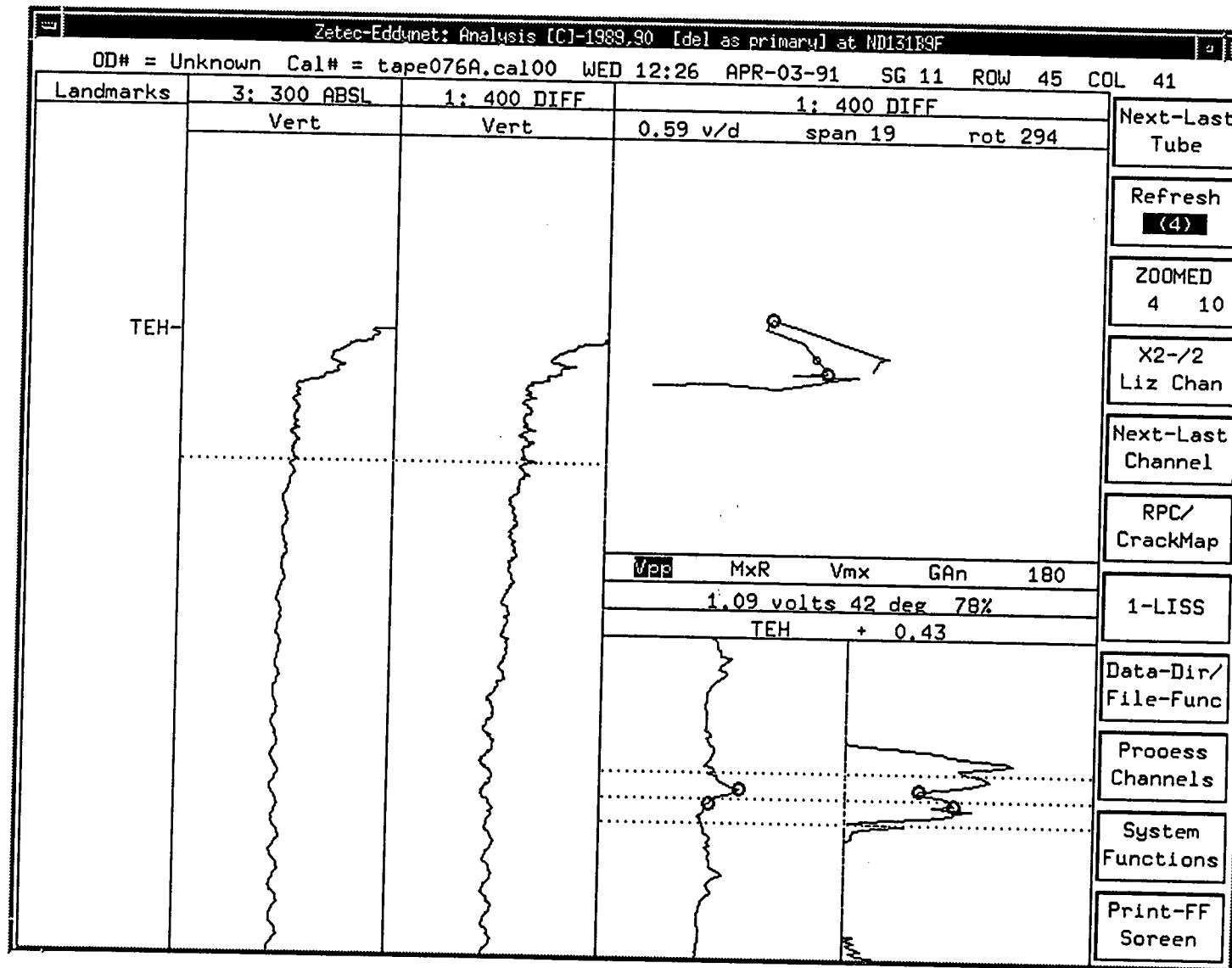


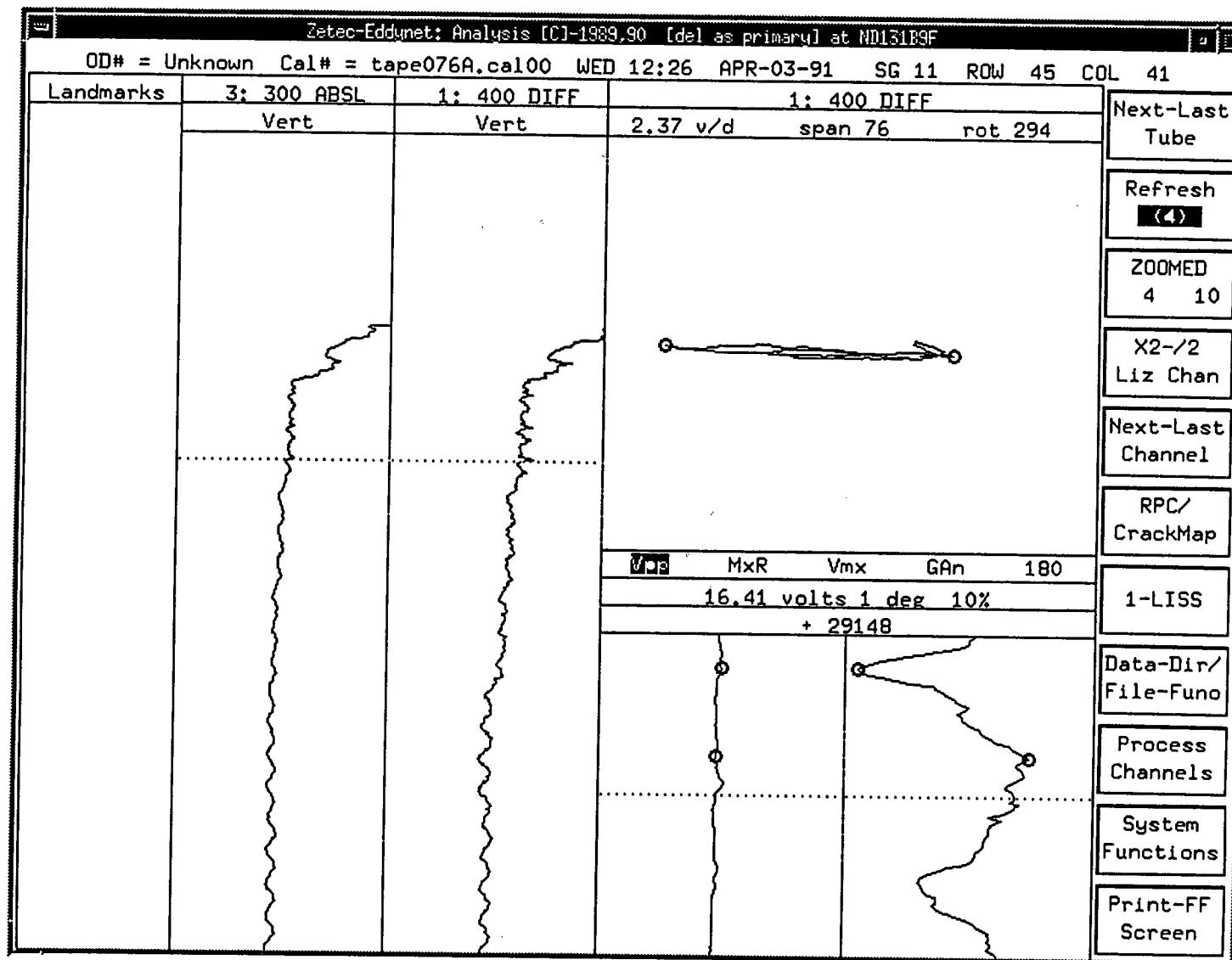


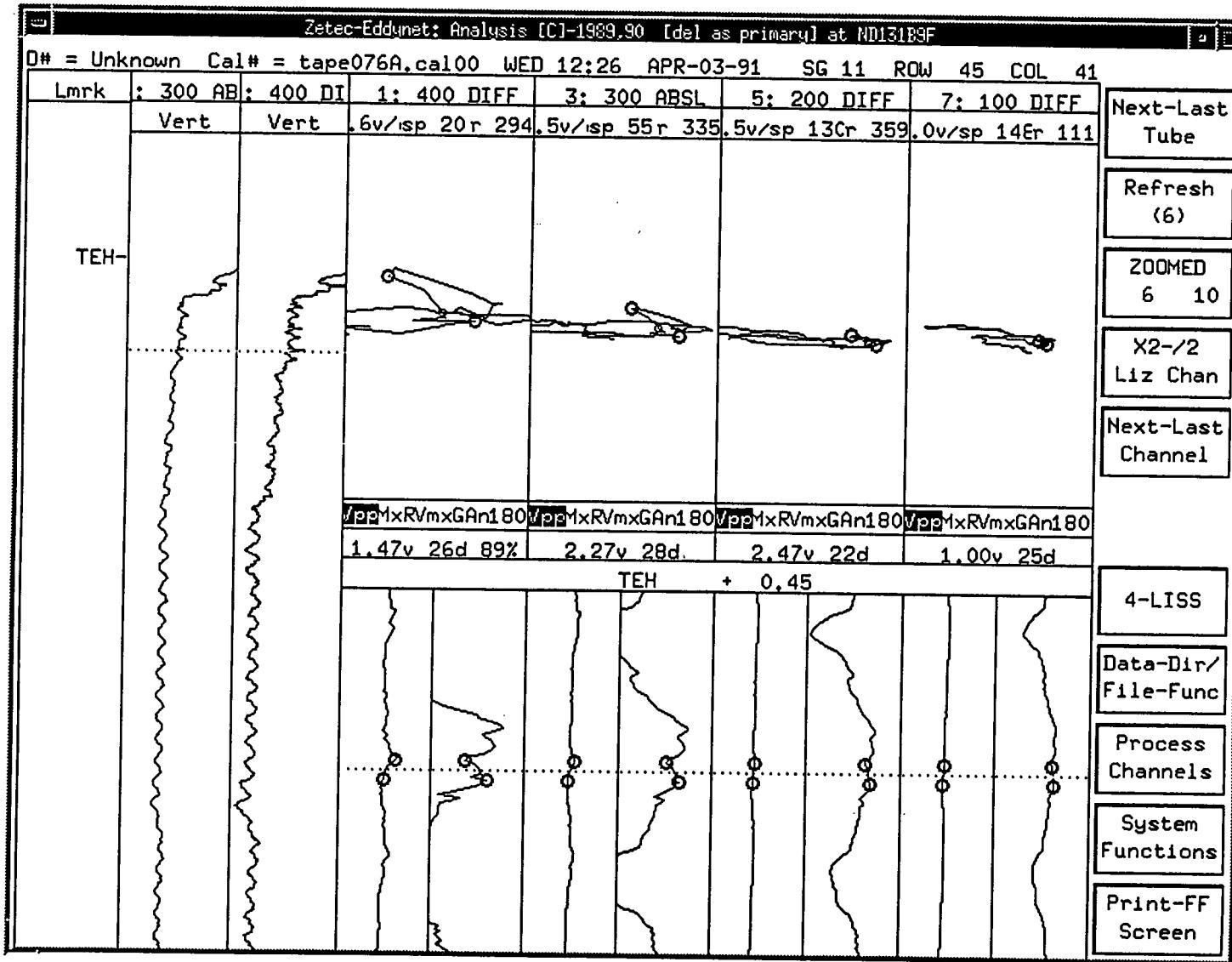


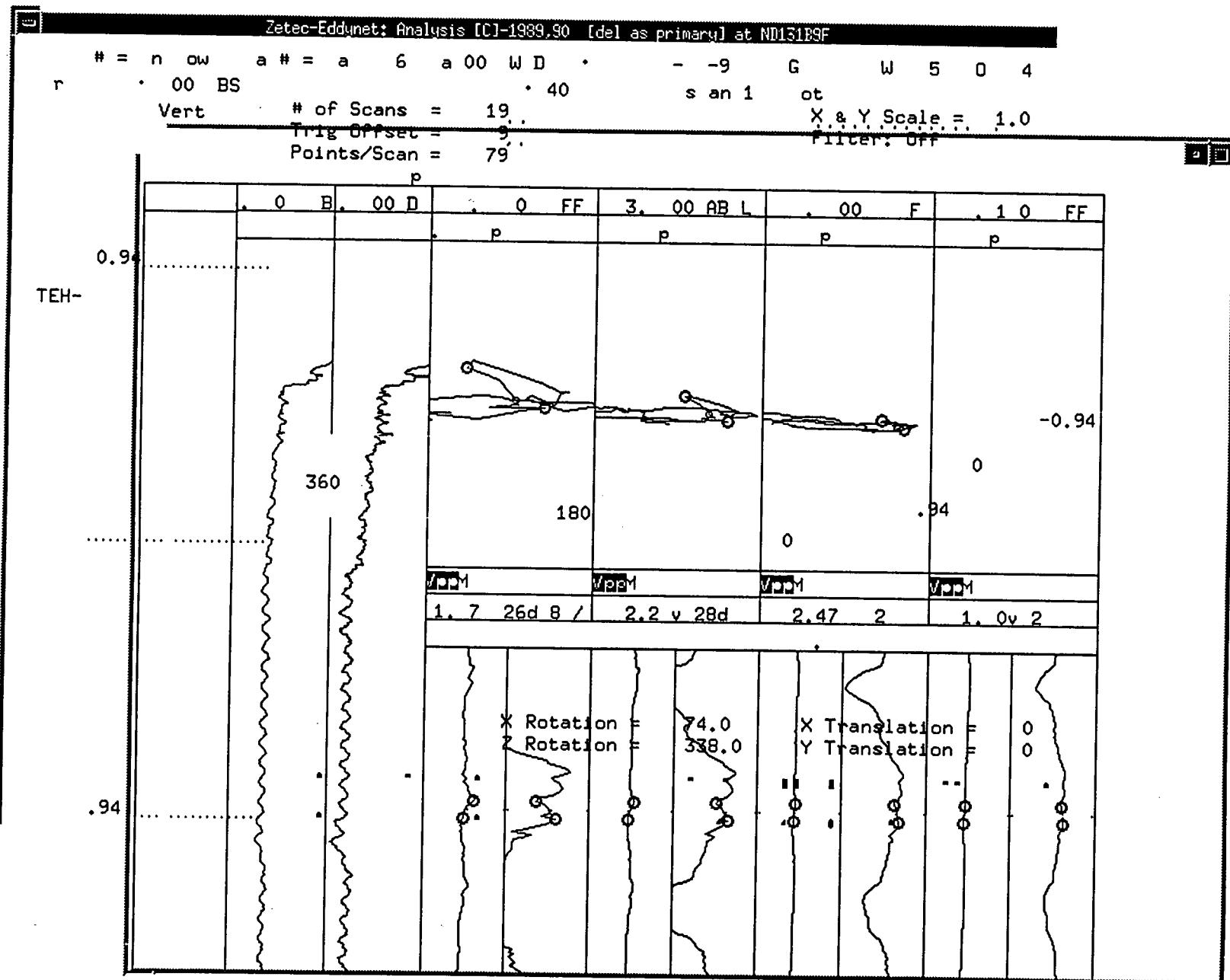


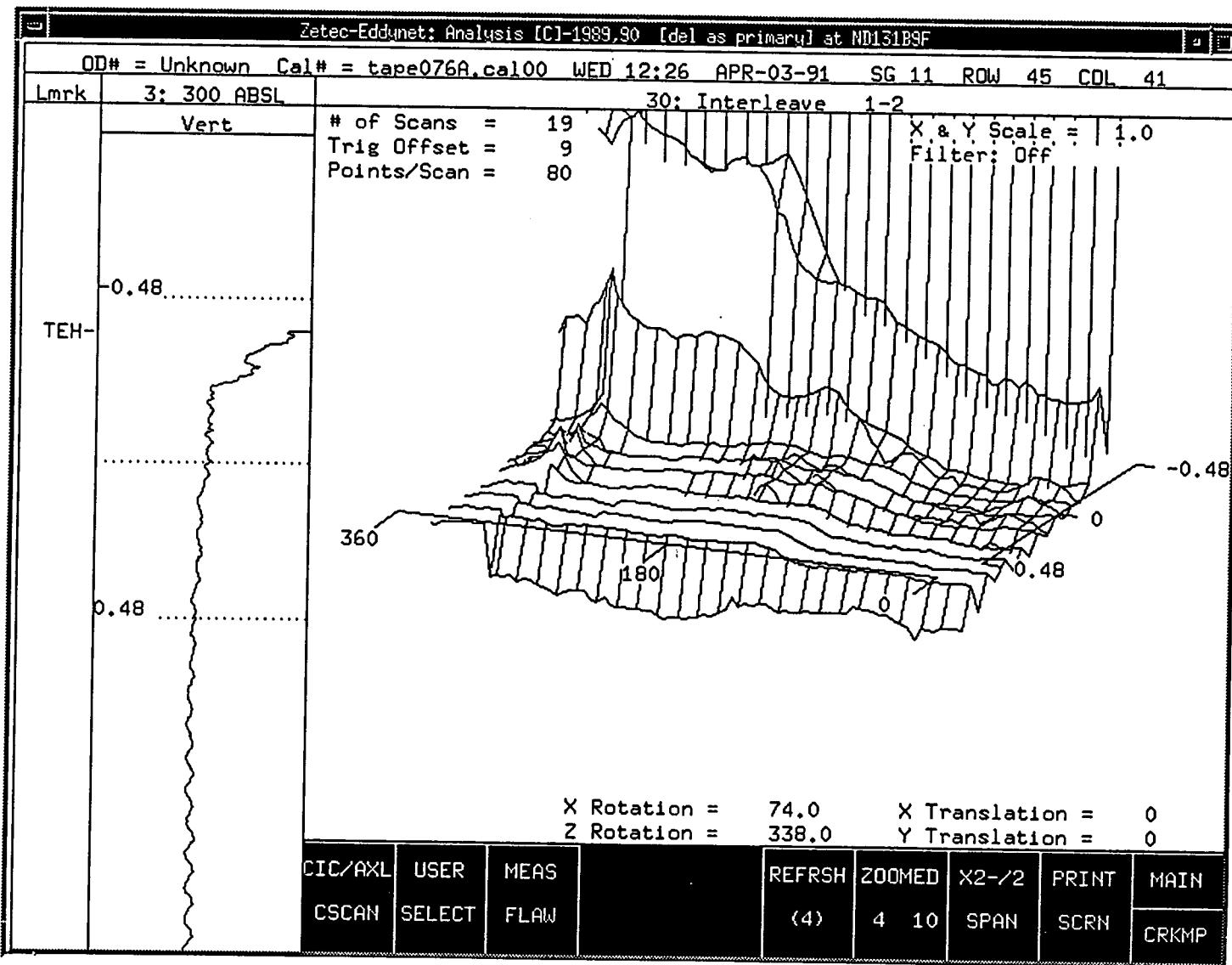


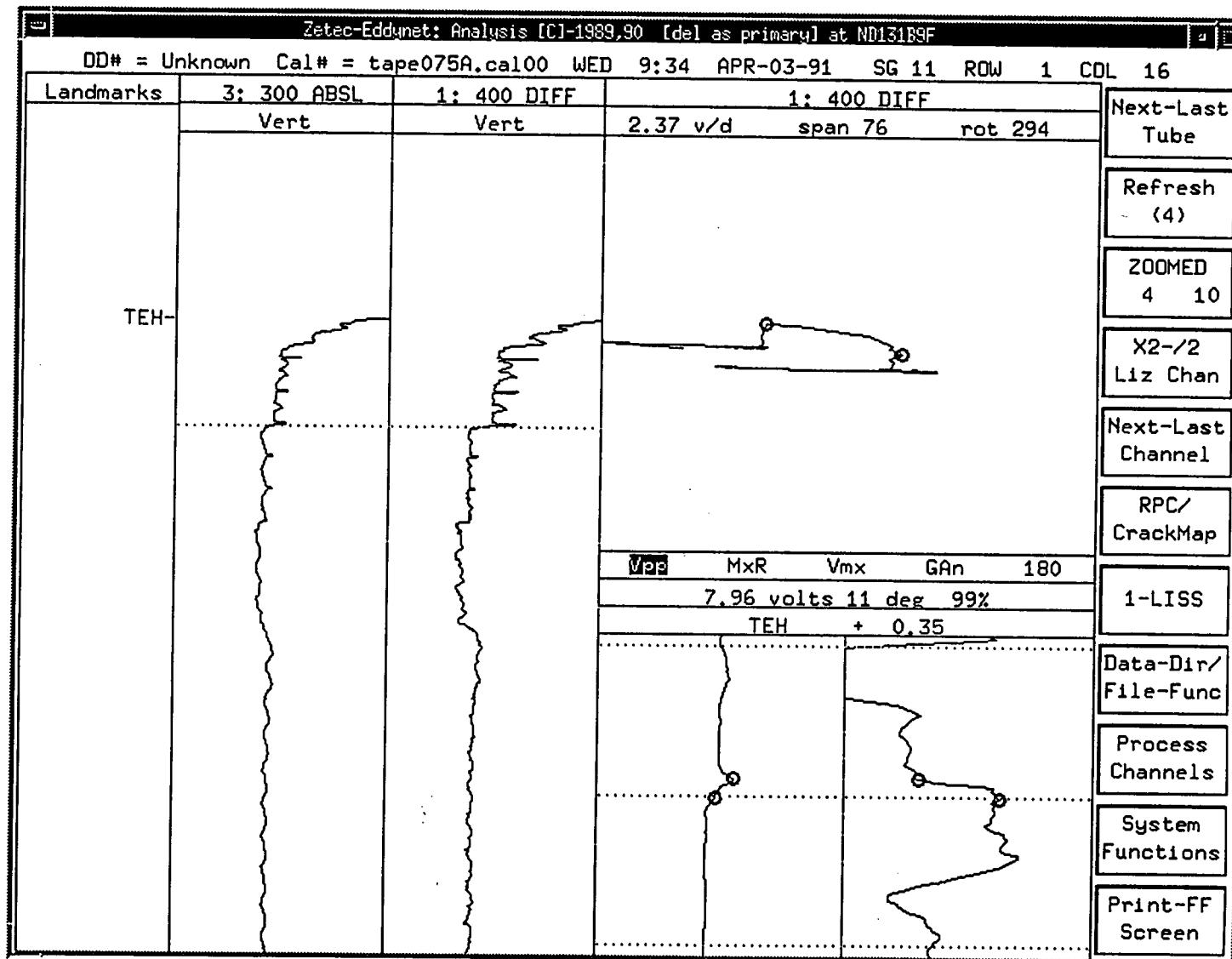


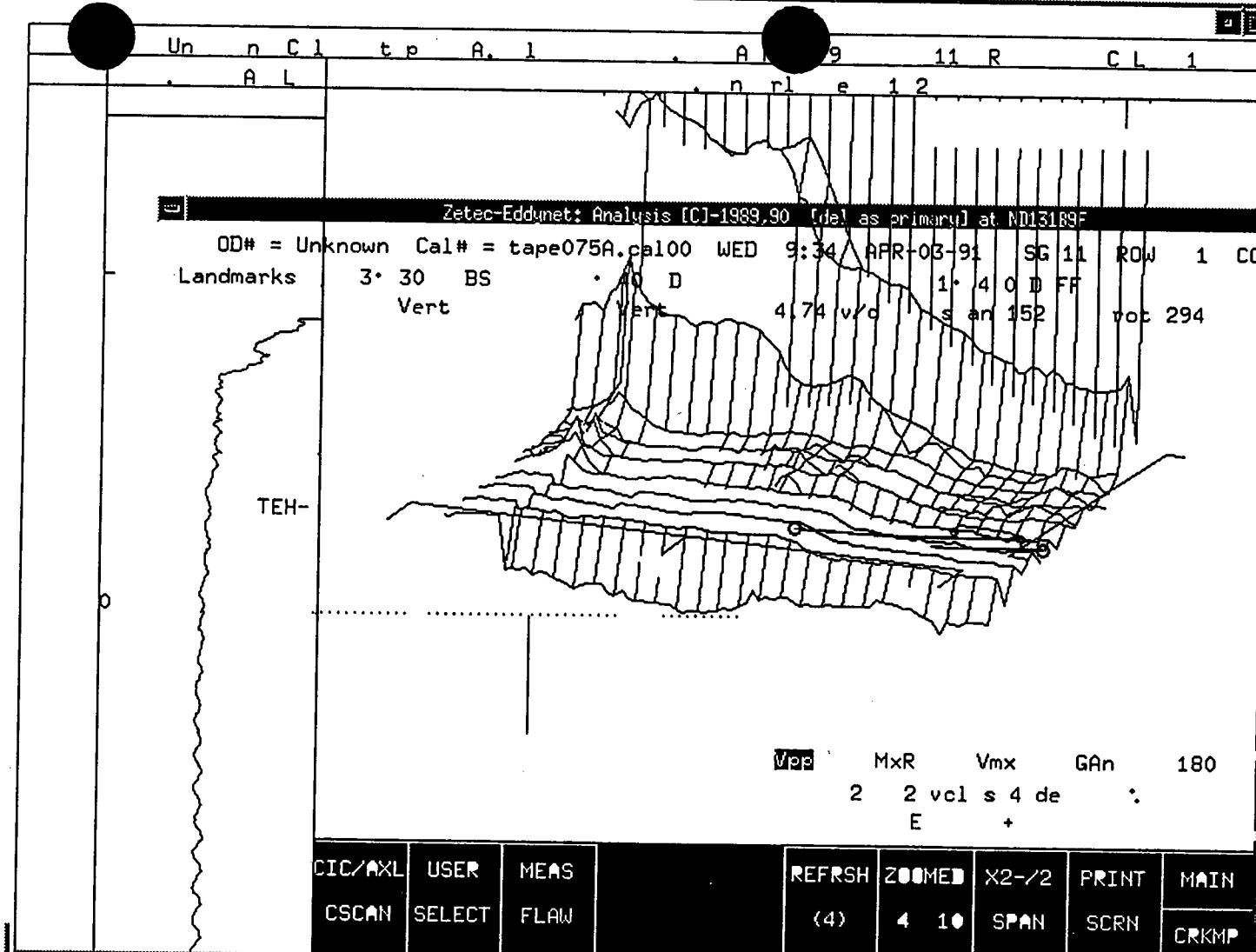












Next-Last
Tube

Refresh
(4)

ZOOMED
4 10

X2-/2
Liz Chan

Next-Last
Channel

RPC/
CrackMap

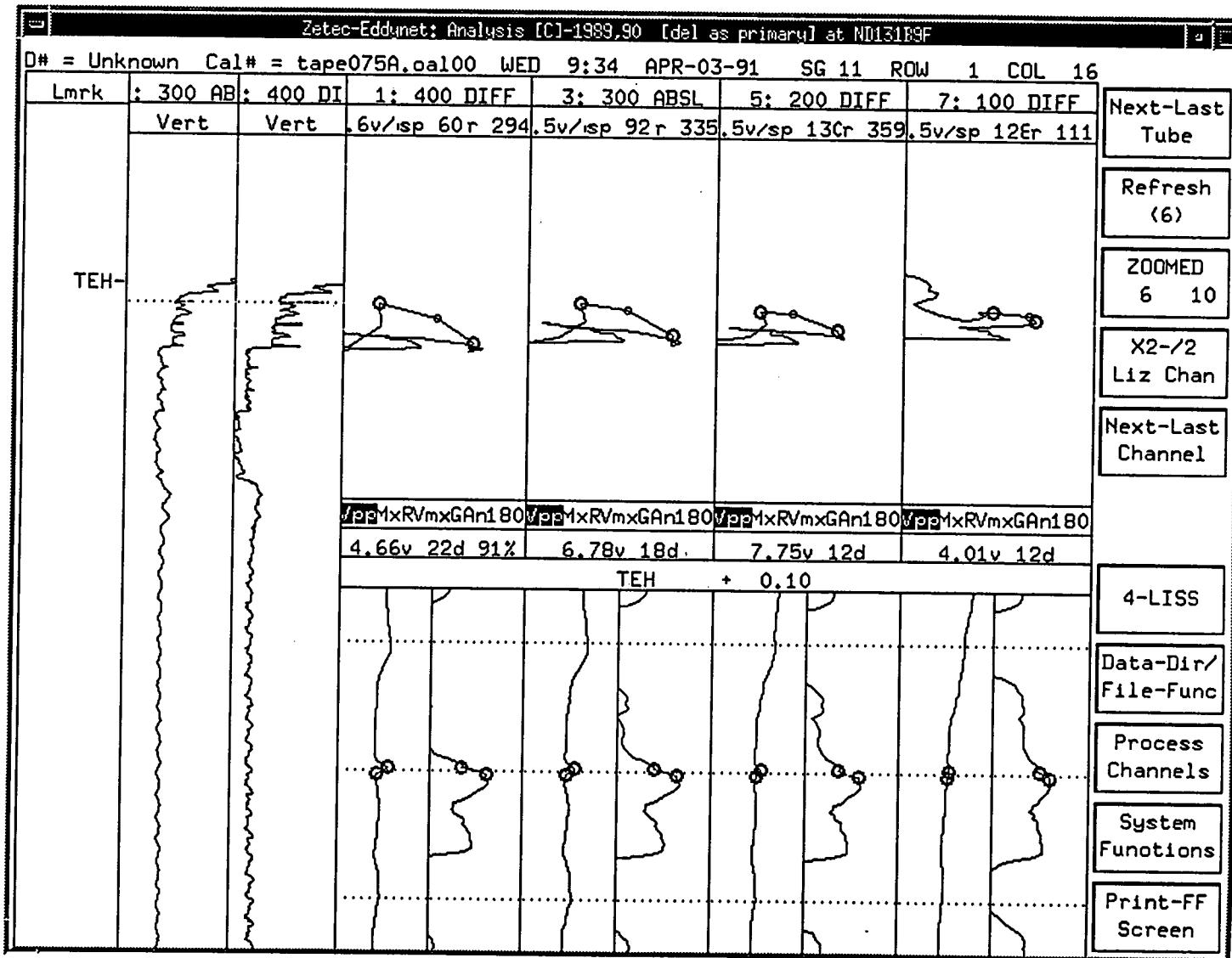
1-LISS

Data-Dir/
File-Func

Process
Channels

System
Functions

Print-FF
Screen



Next-Last
Tube

Refresh
(6)

ZOOMED
6 10

X2-/2
Liz Chan

Next-Last
Channel

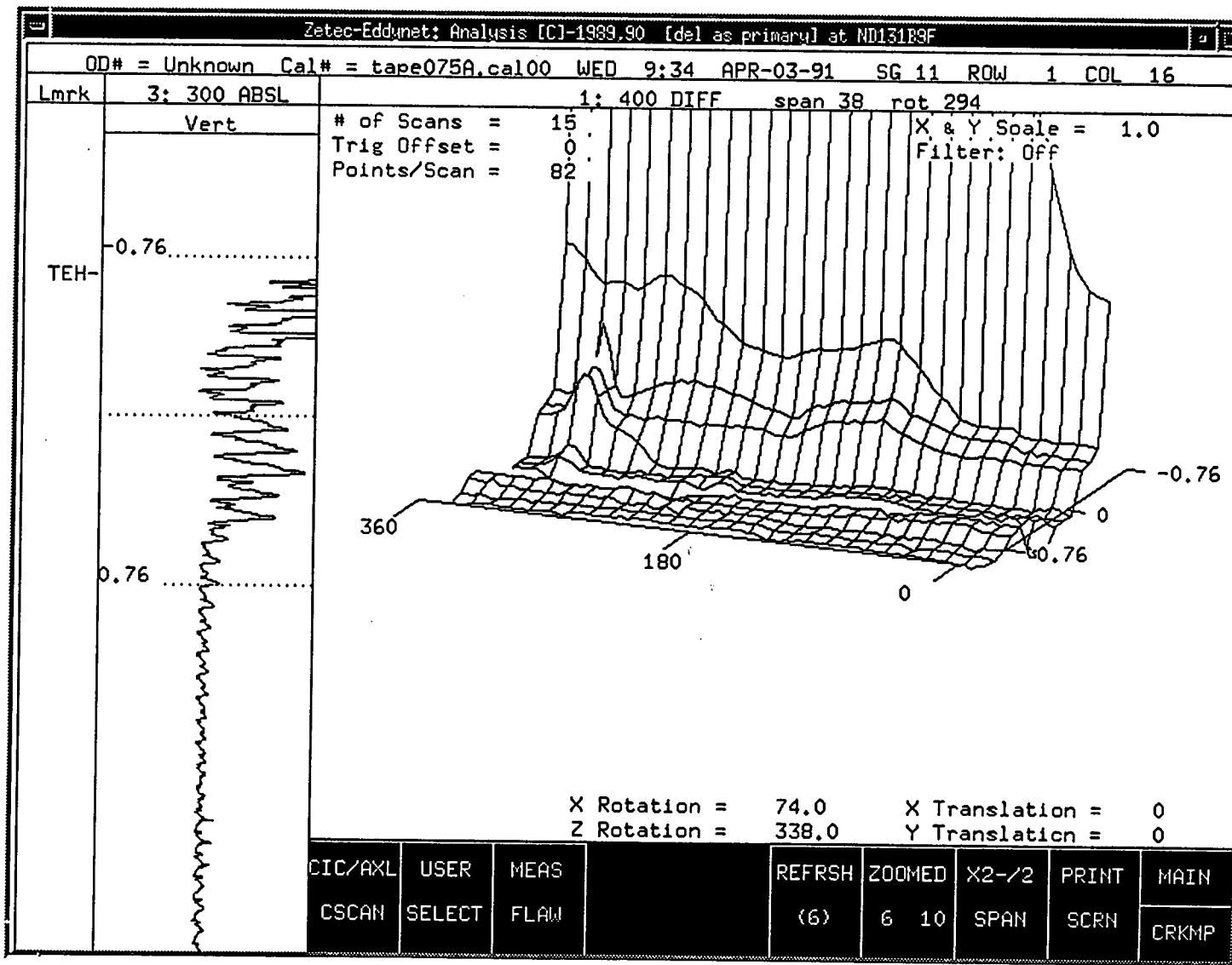
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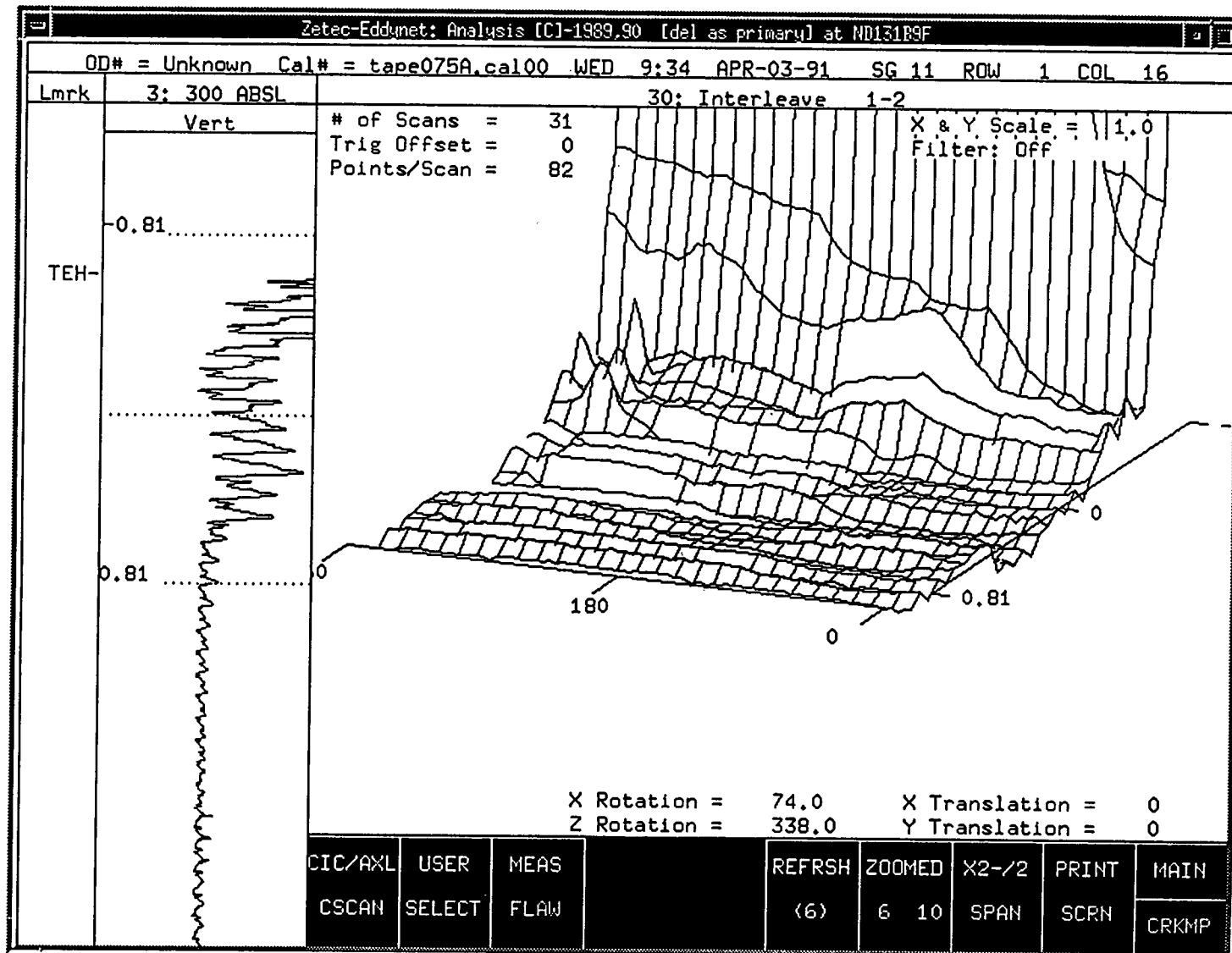
Data-Dir/
File-Func

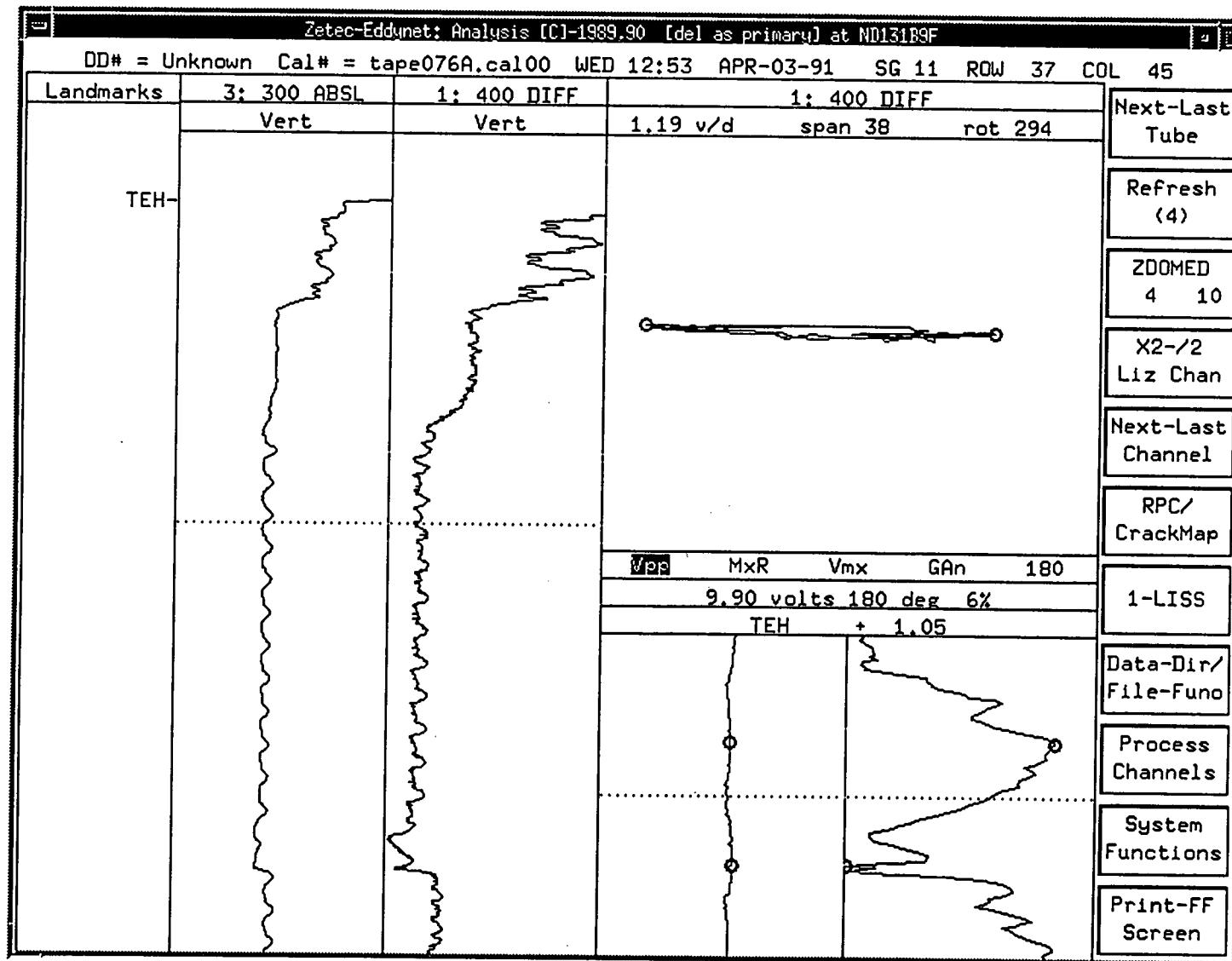
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Channels

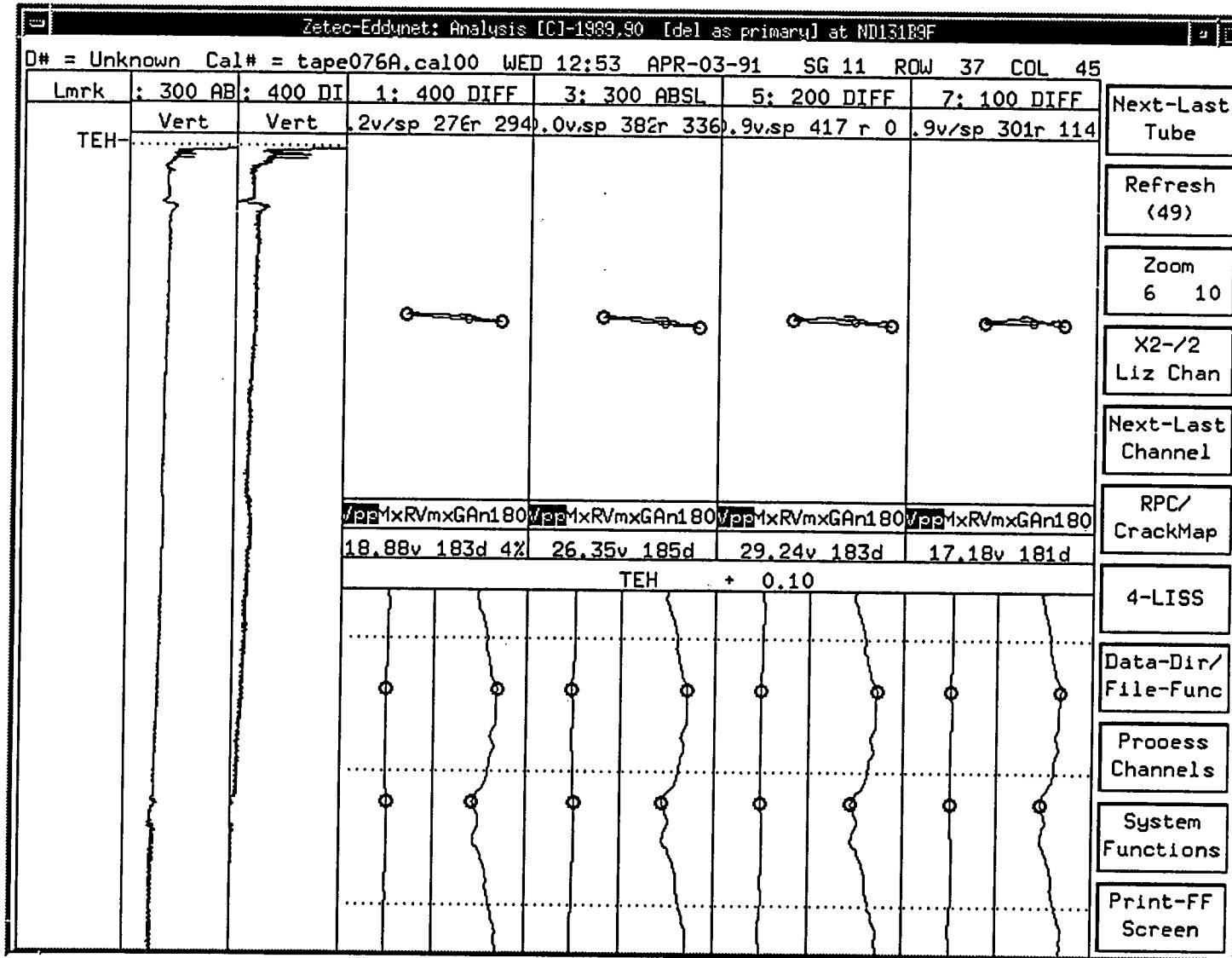
System
Functions

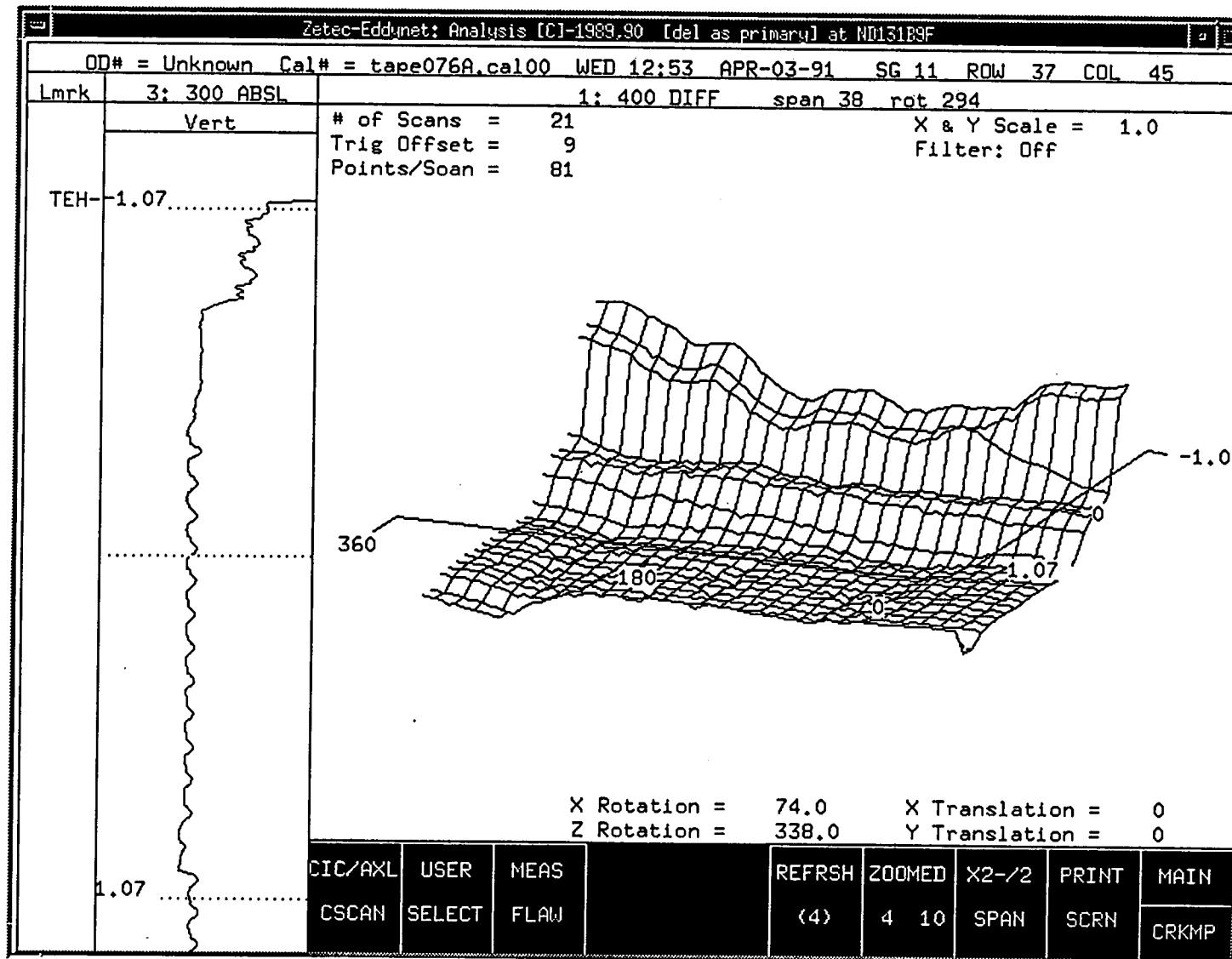
Print-FF
Screen

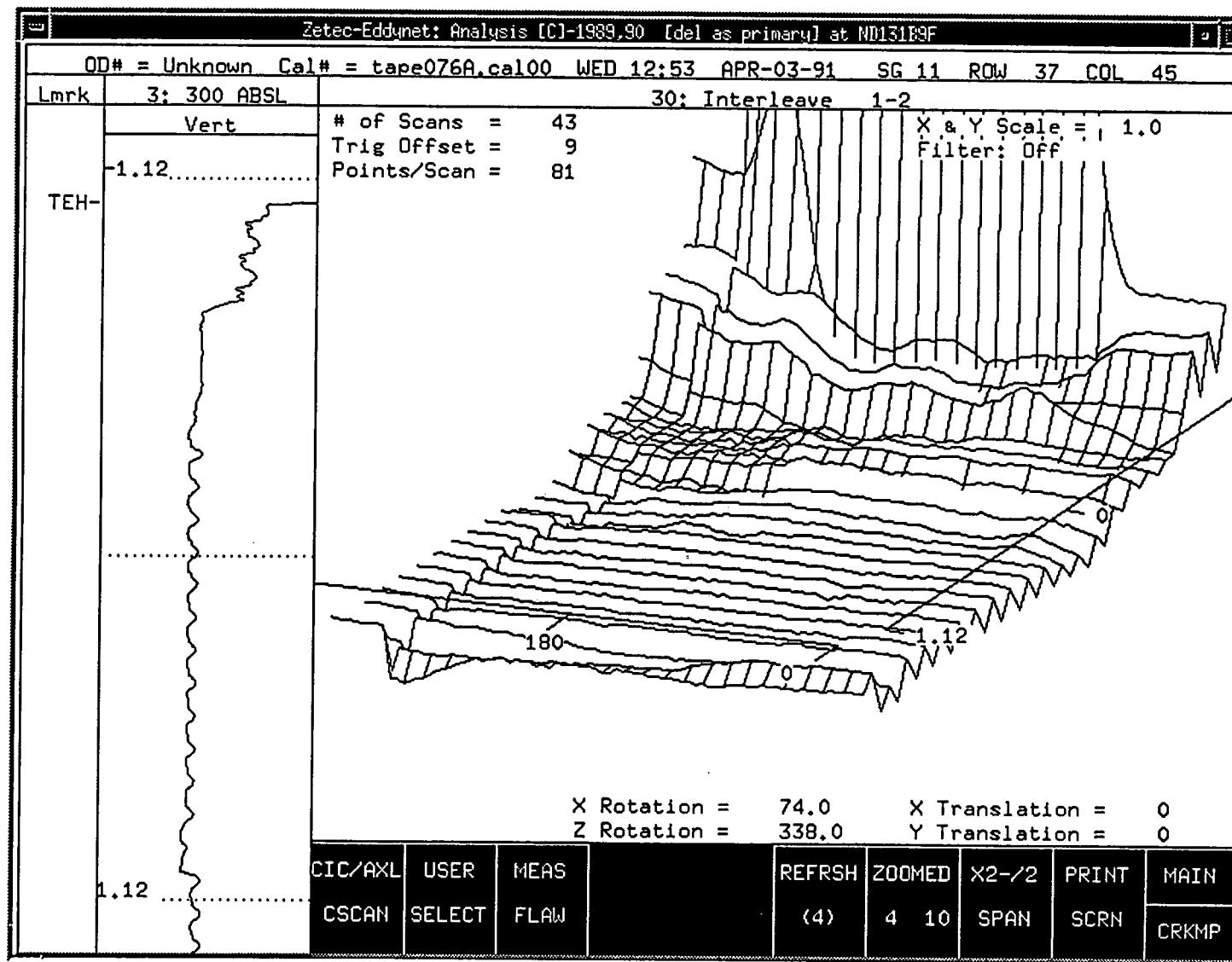


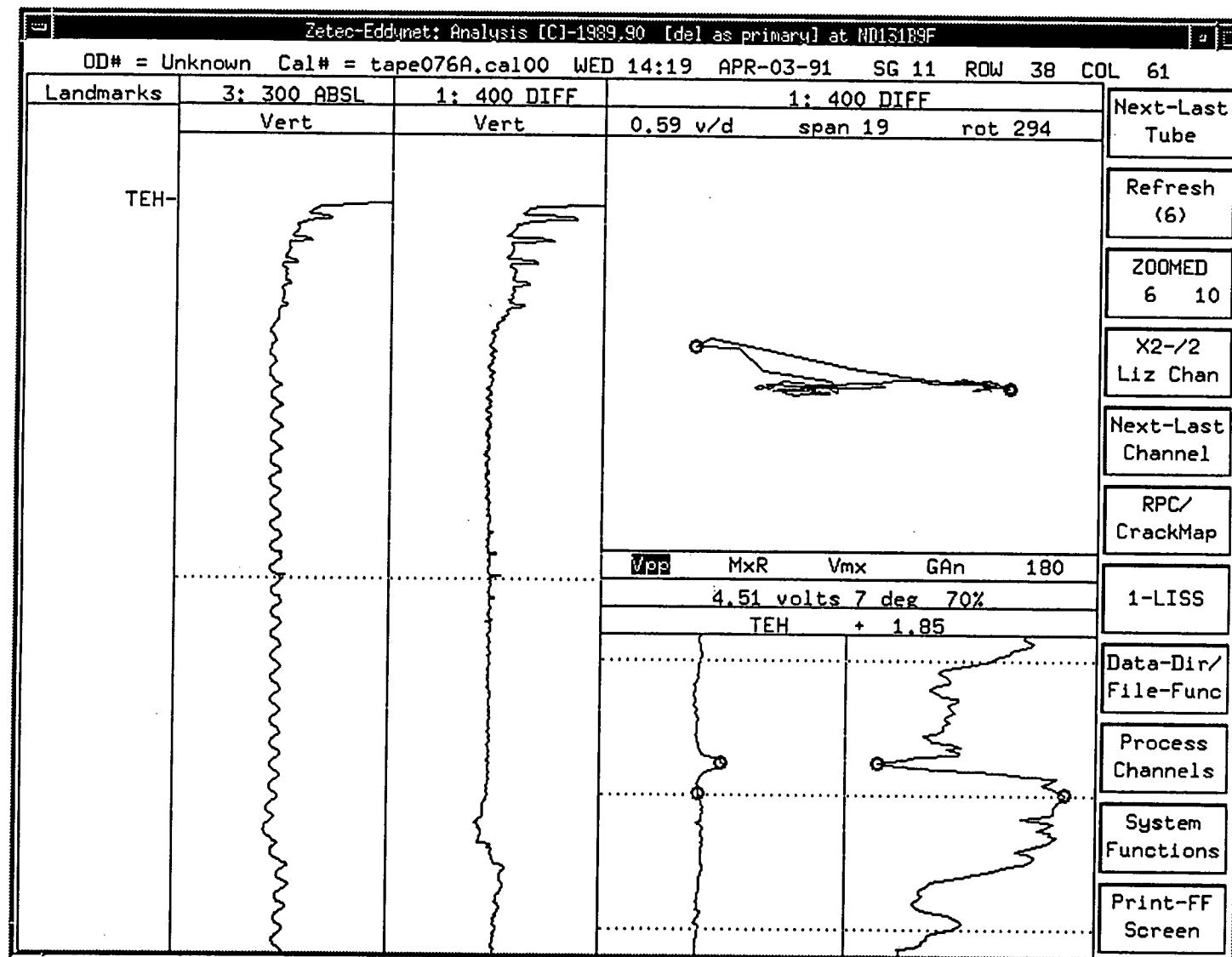


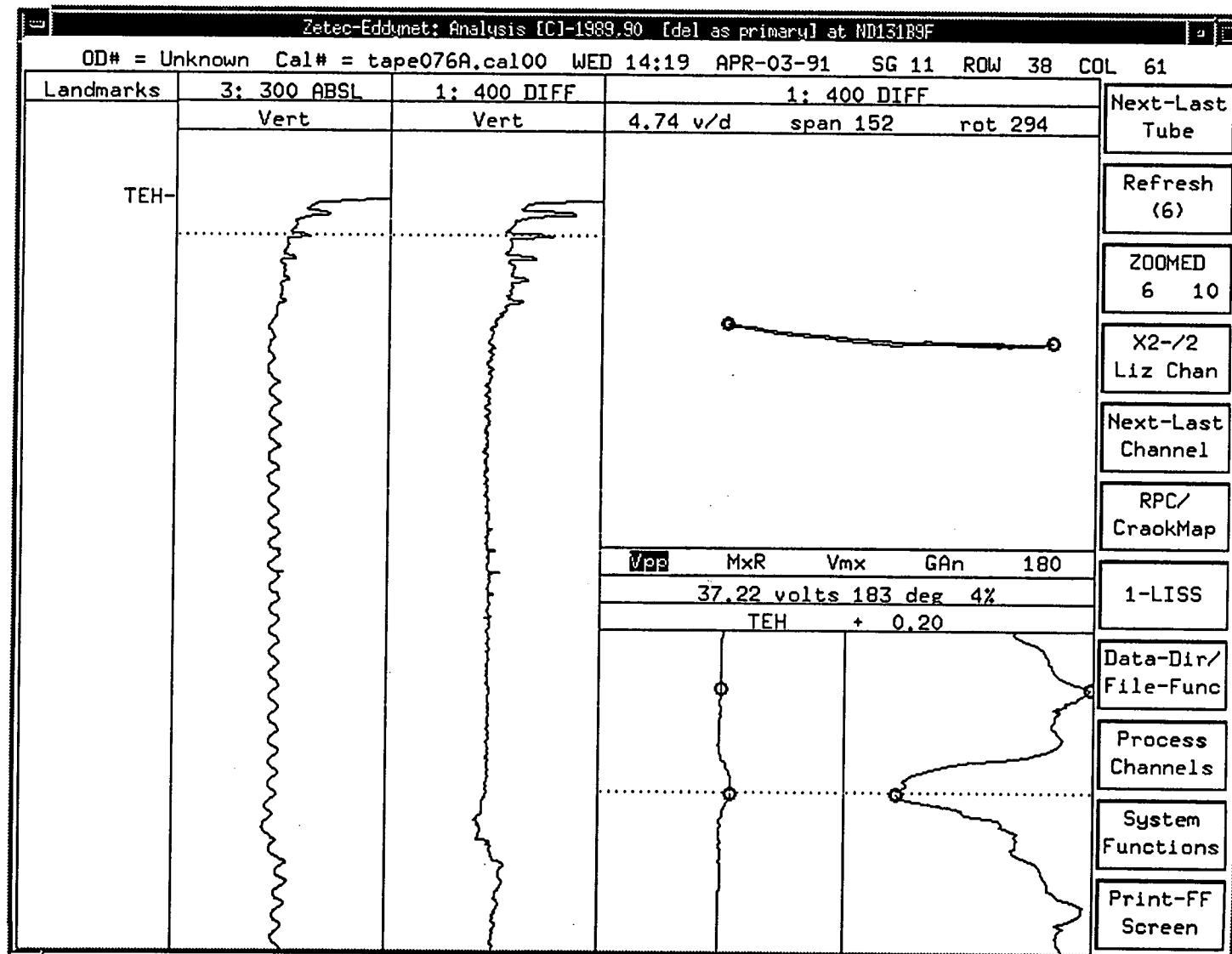


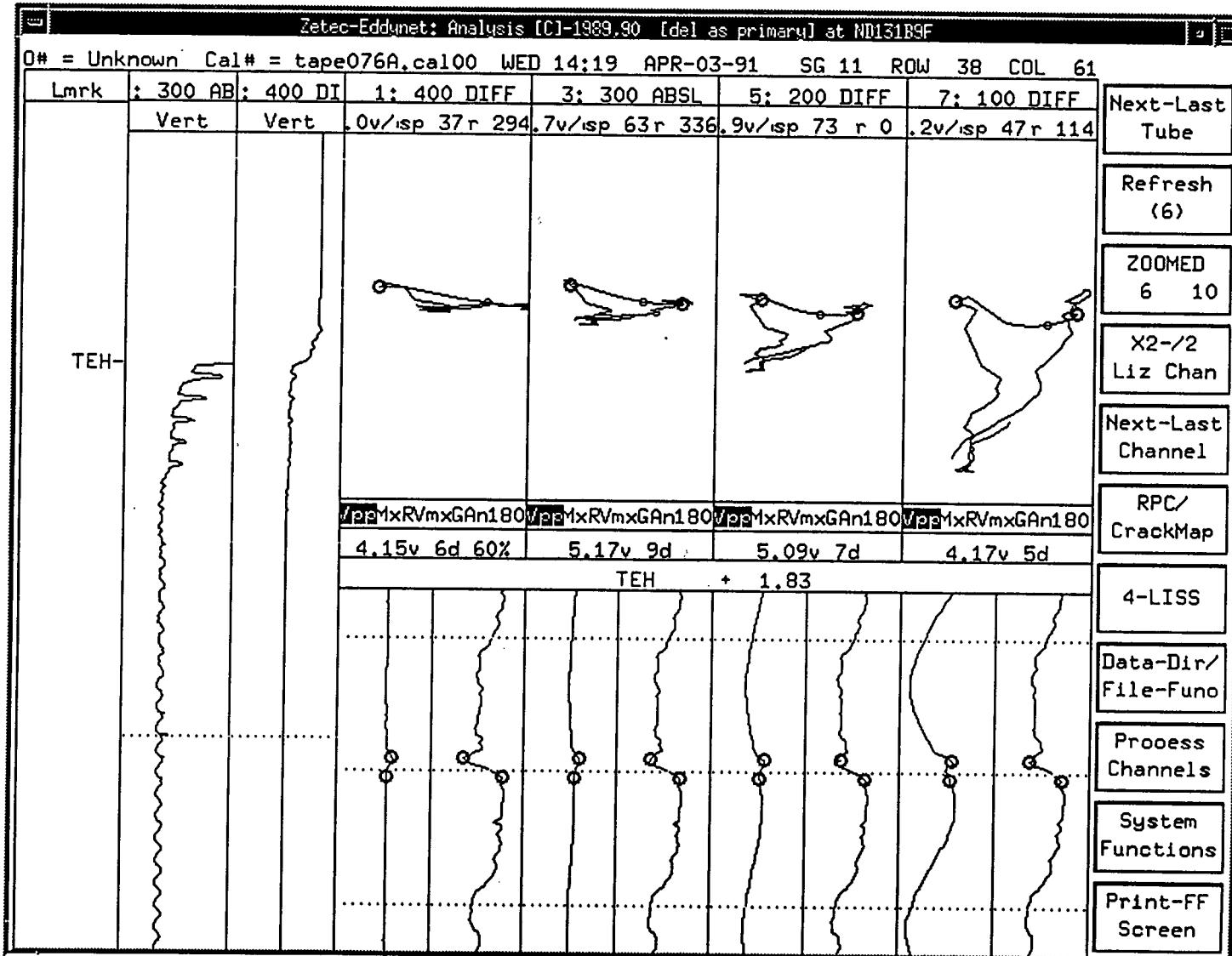


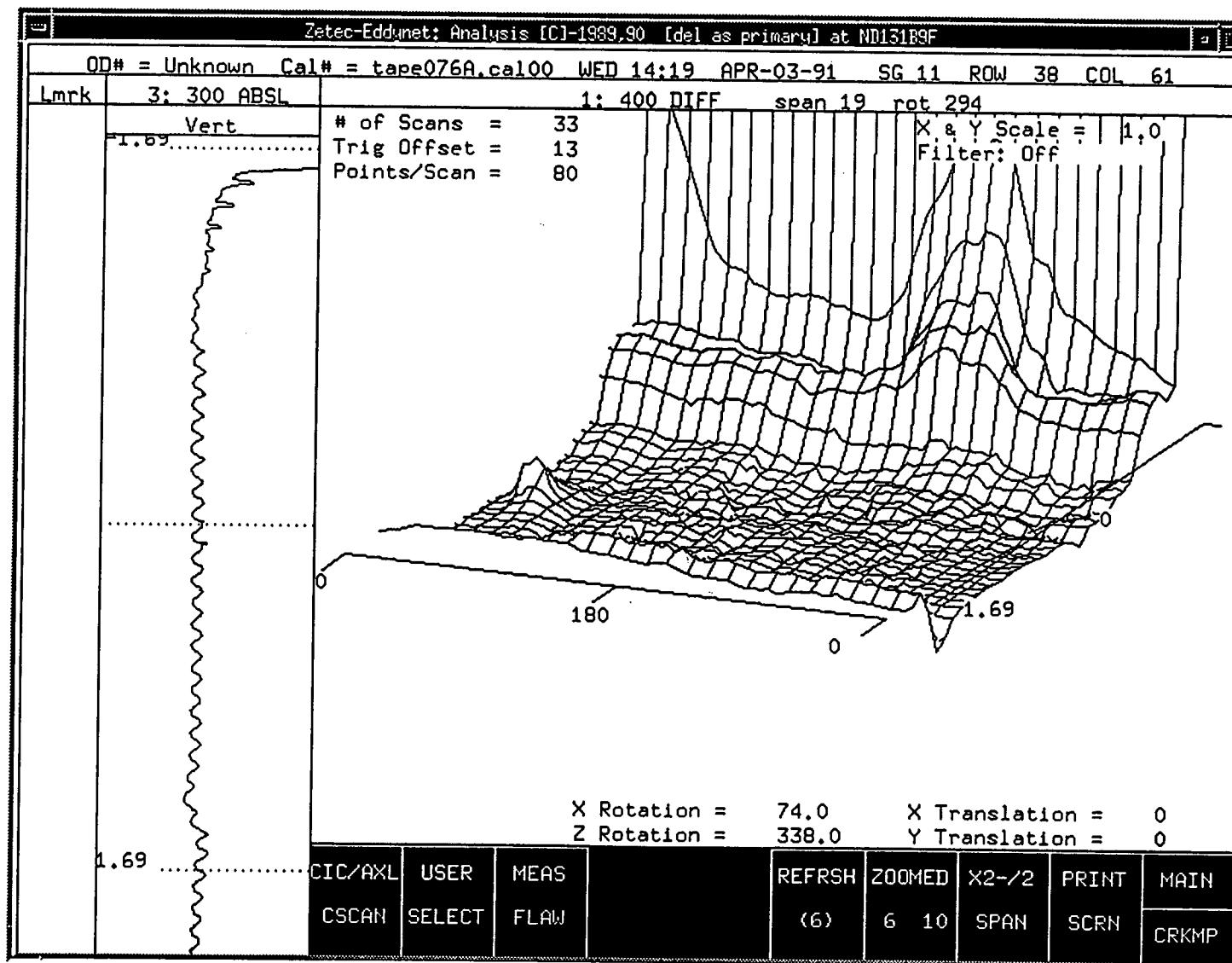


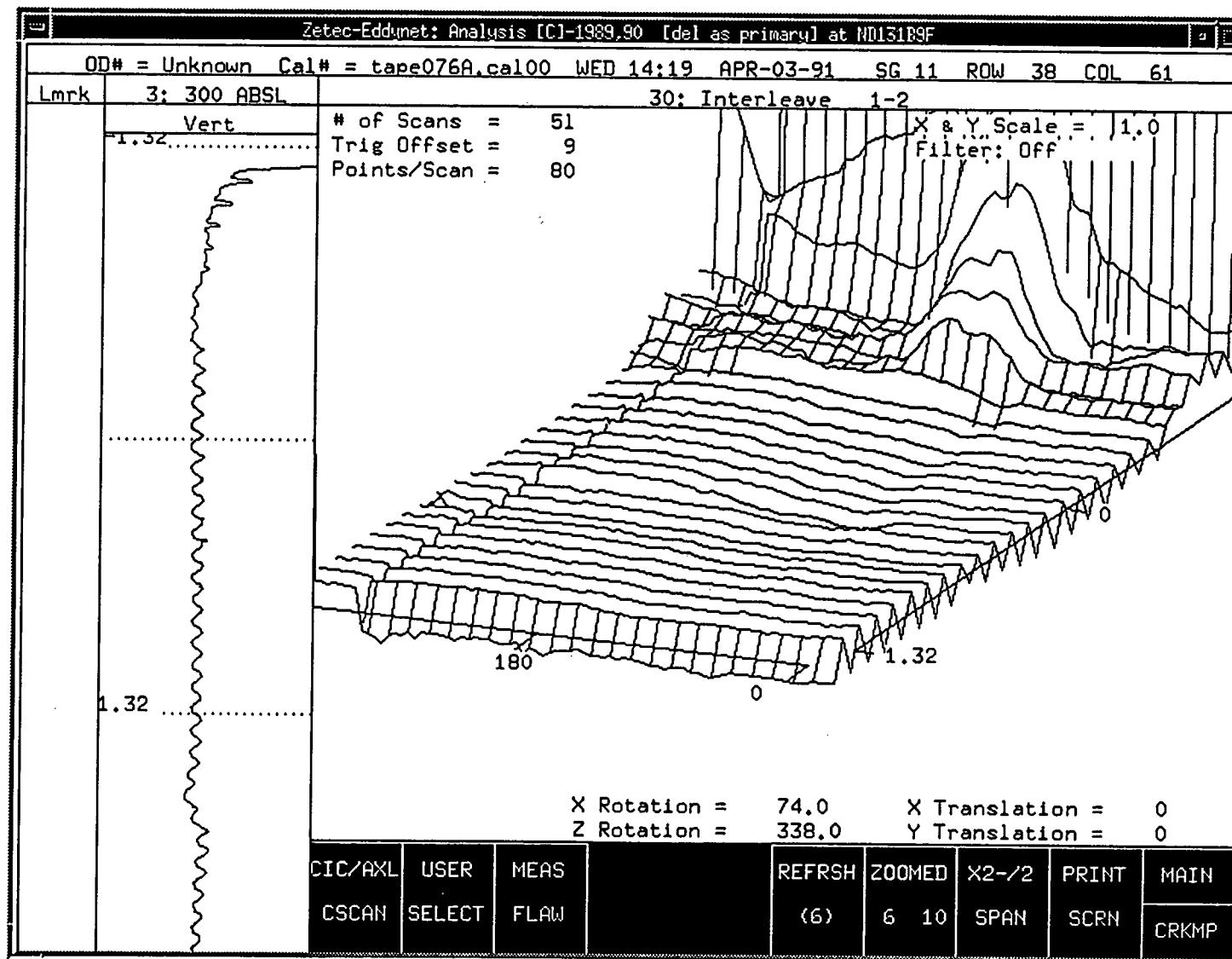


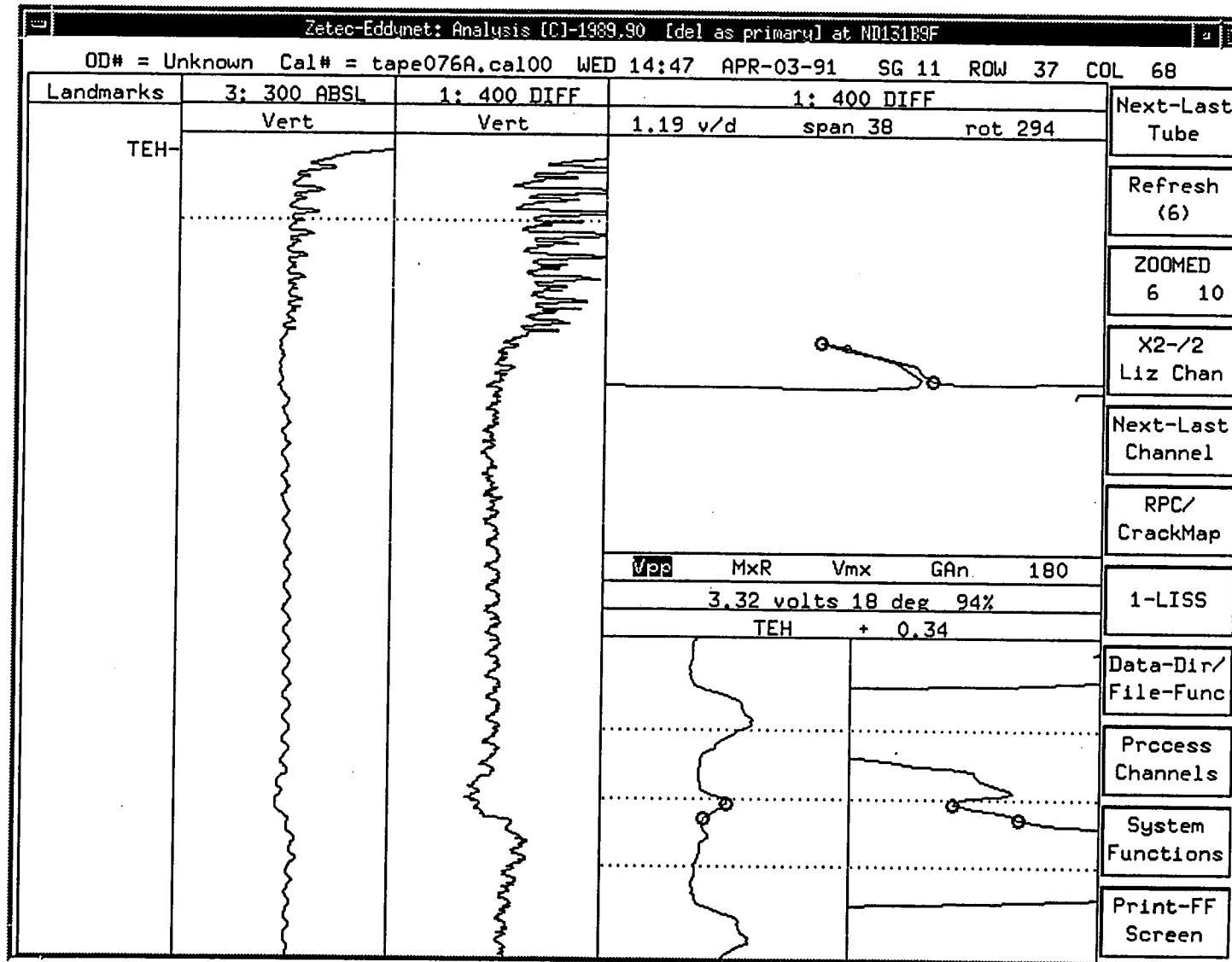


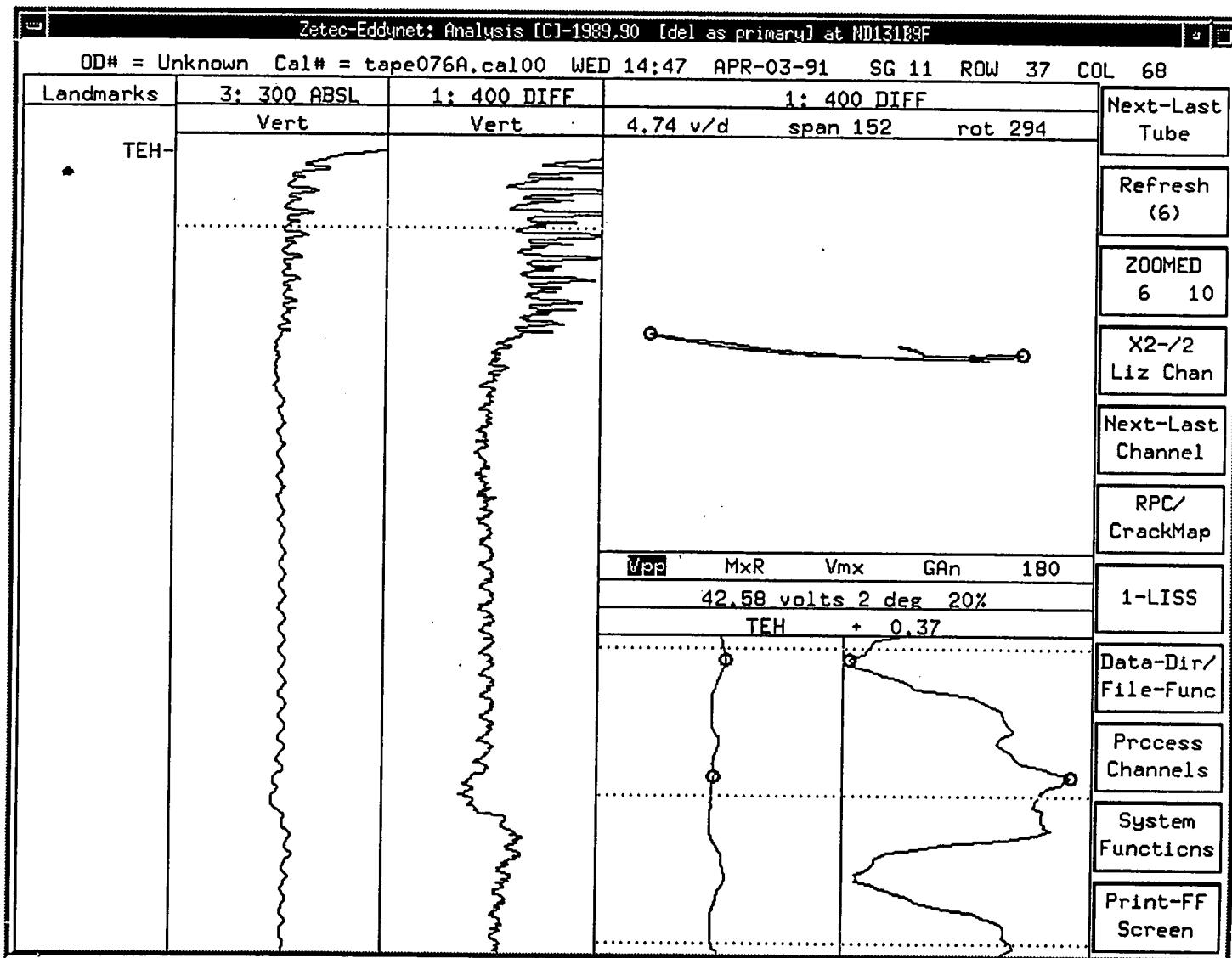


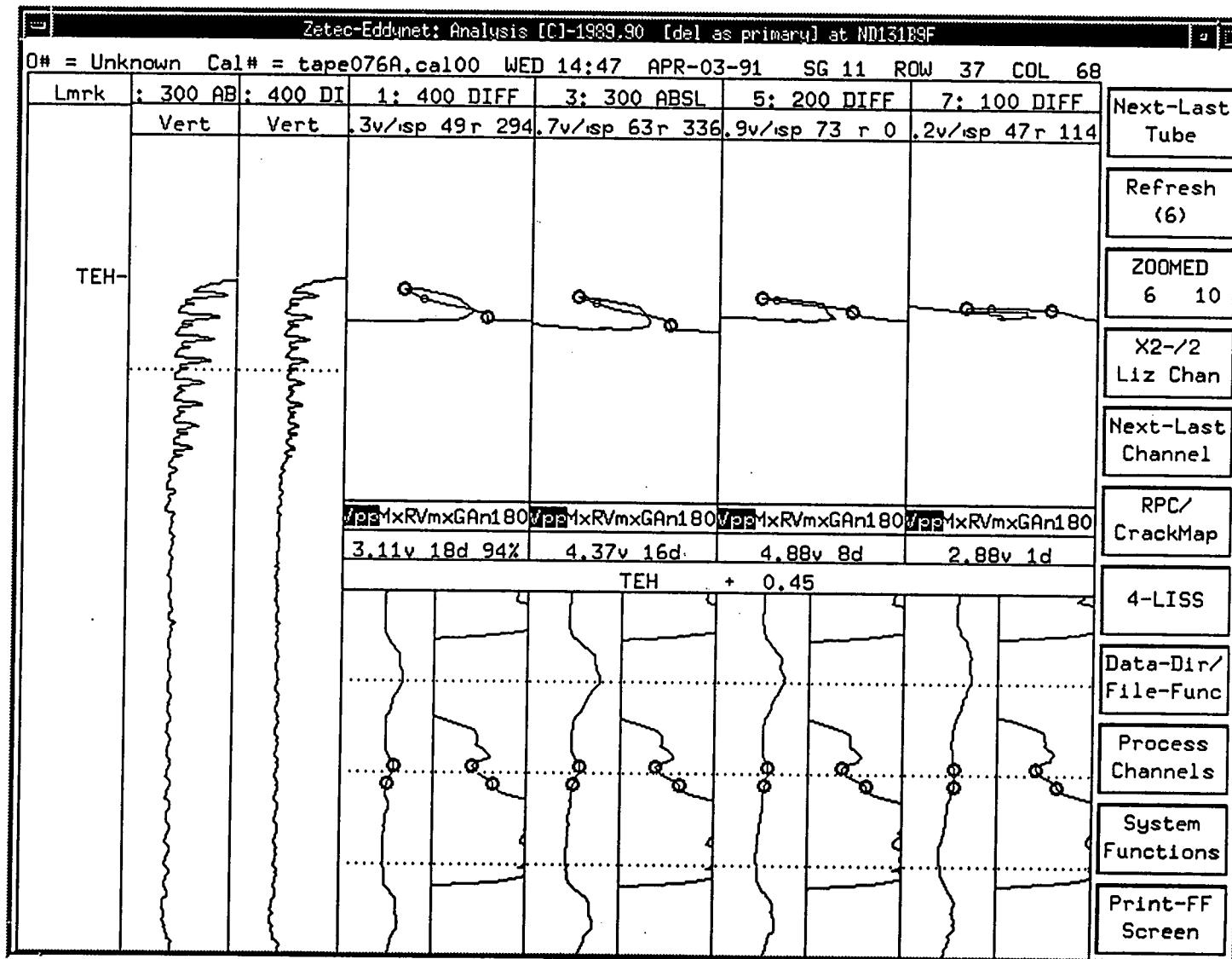


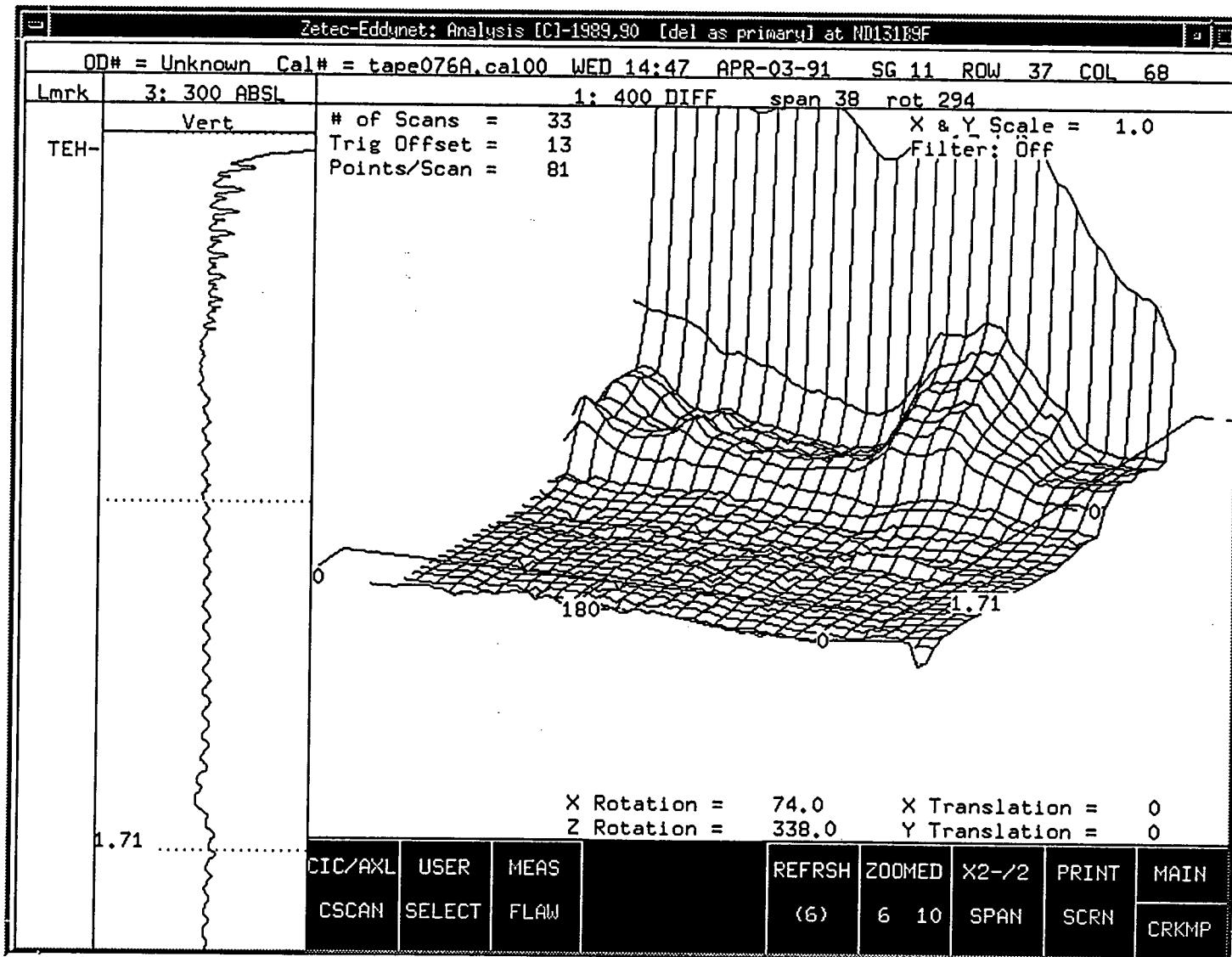


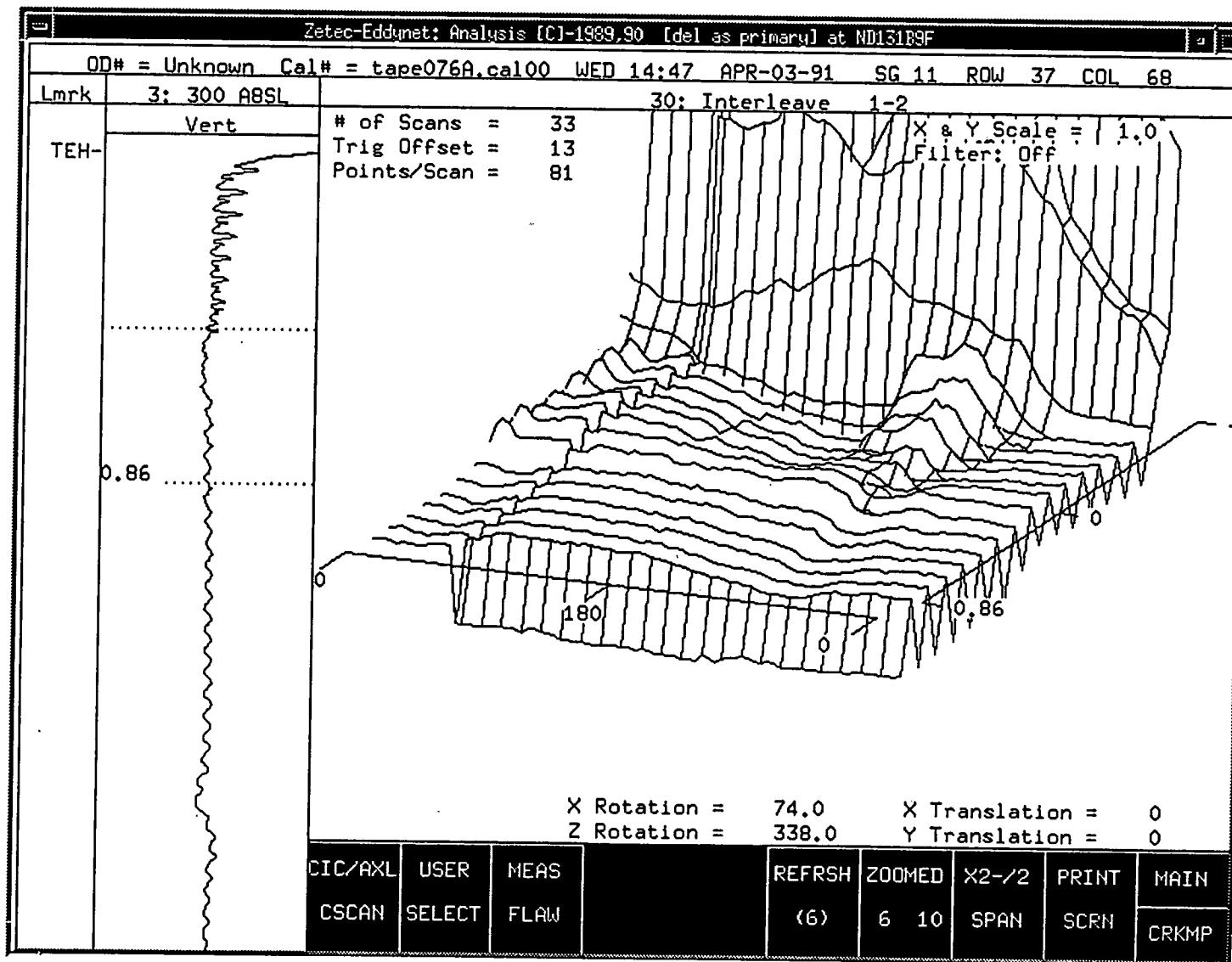


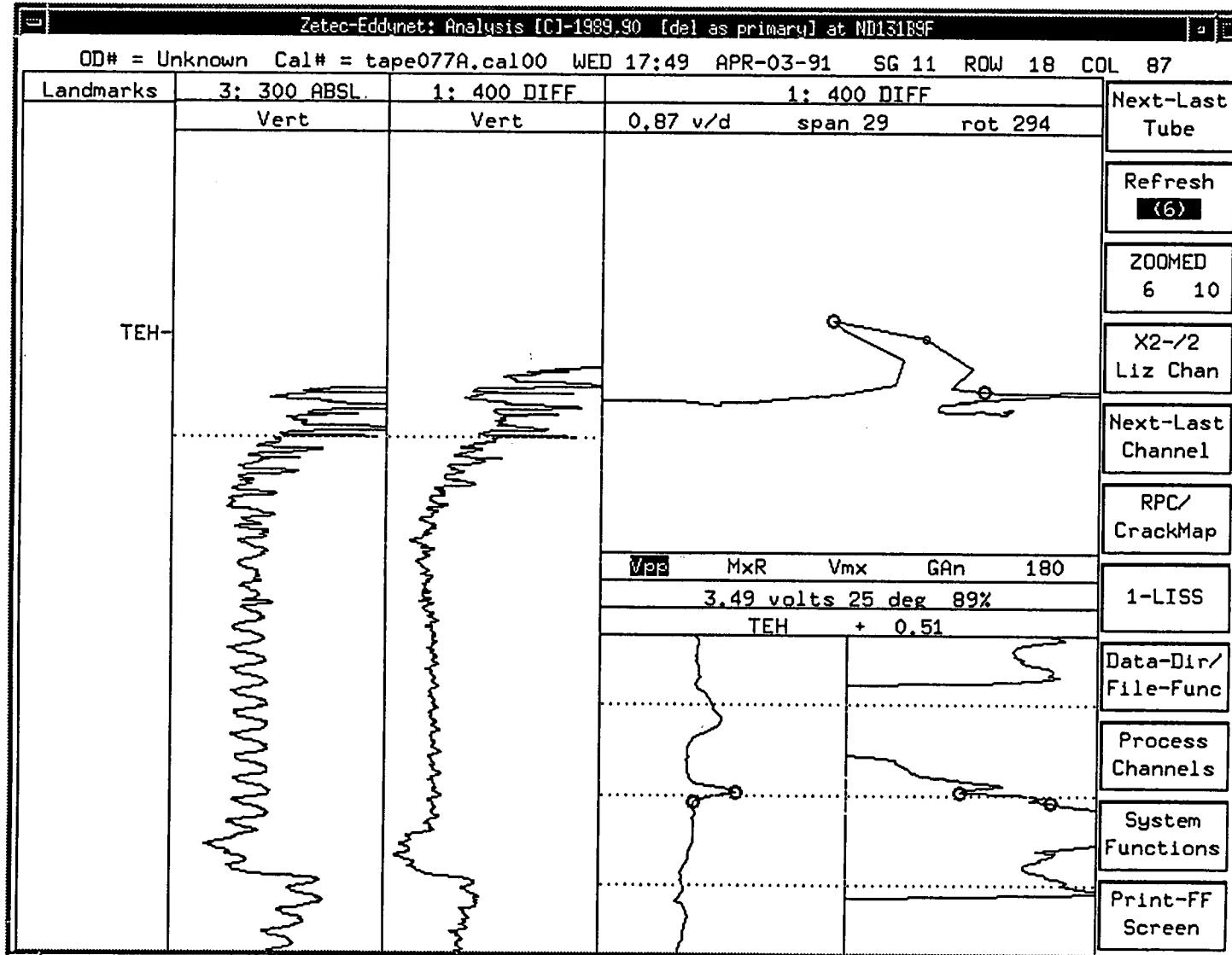


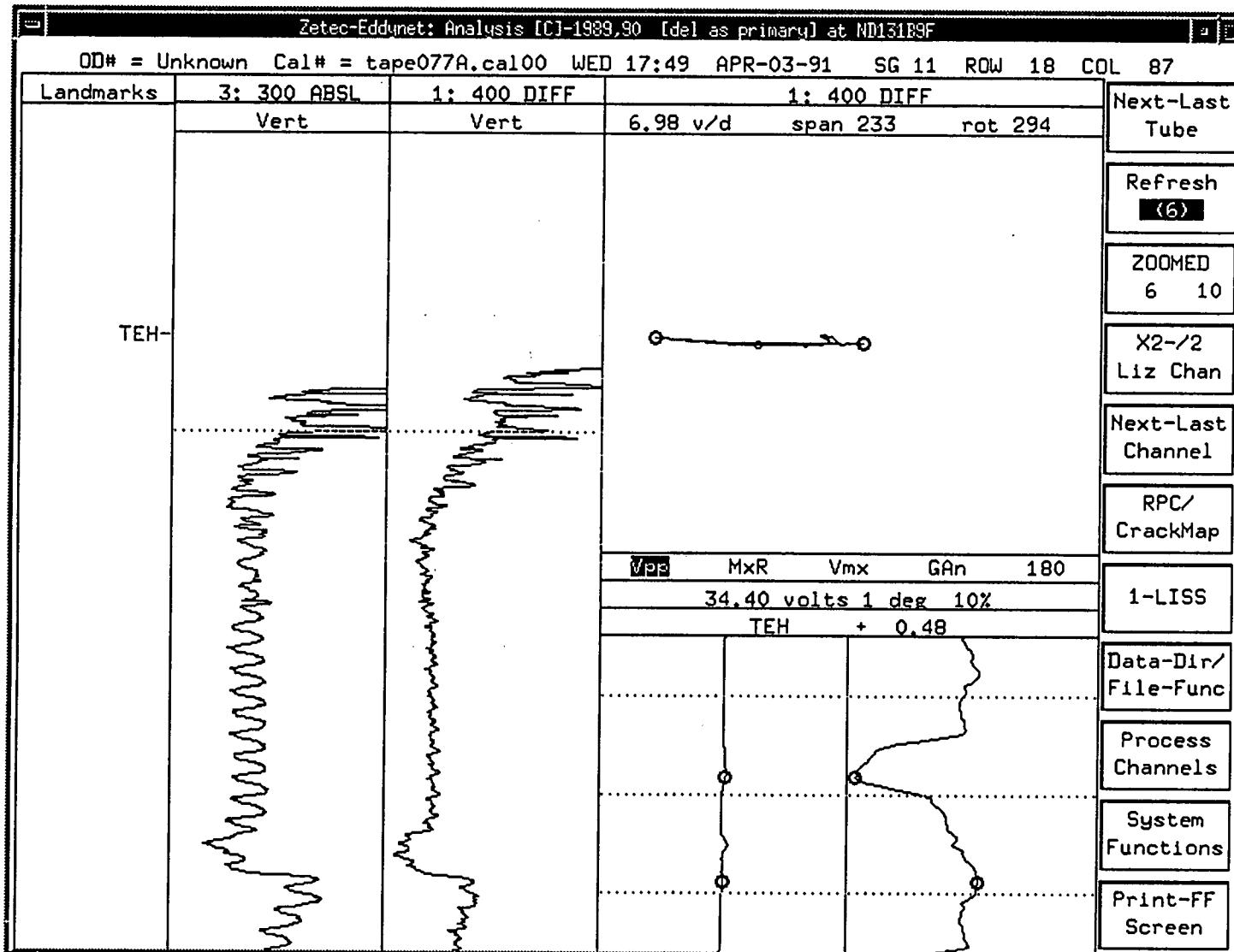


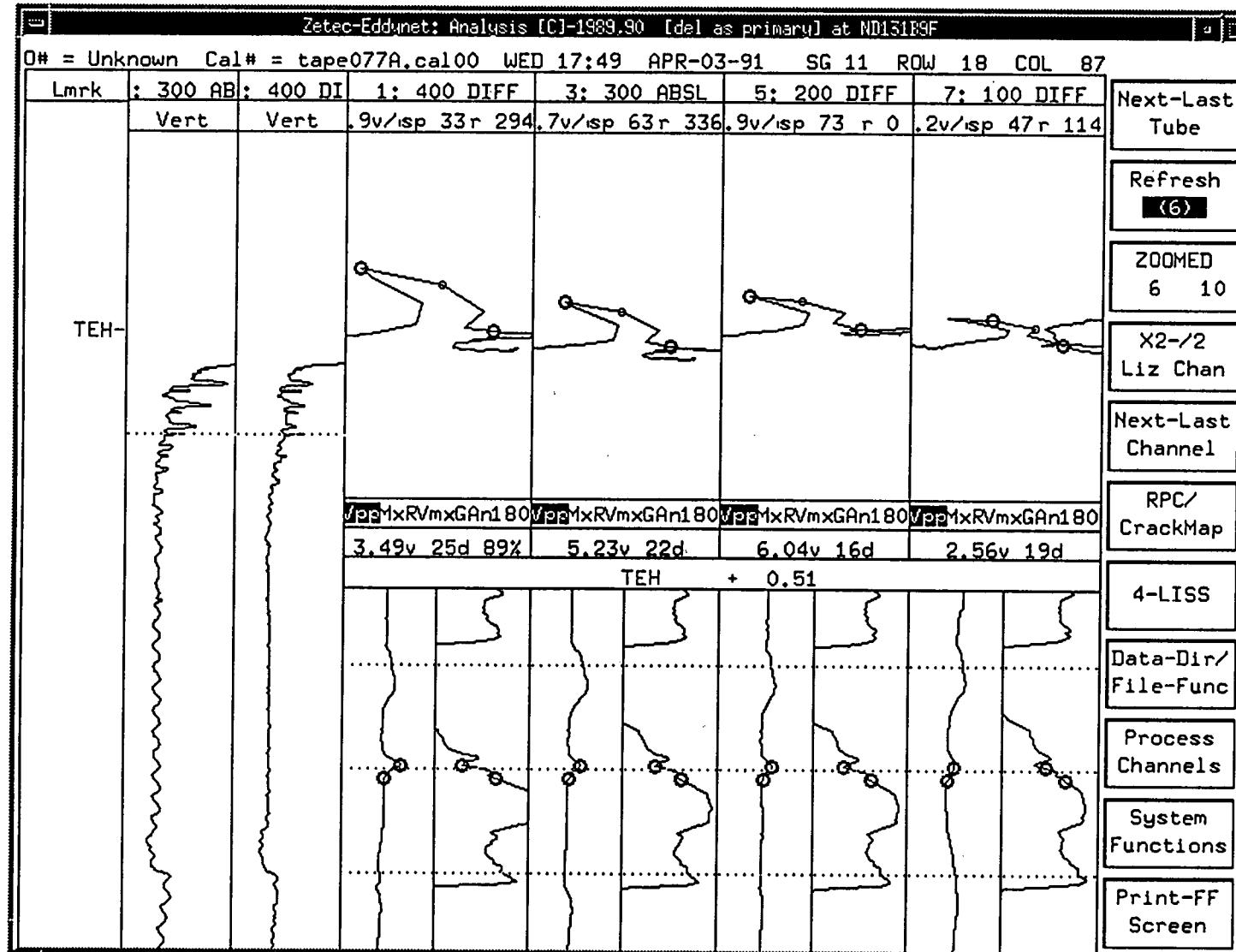


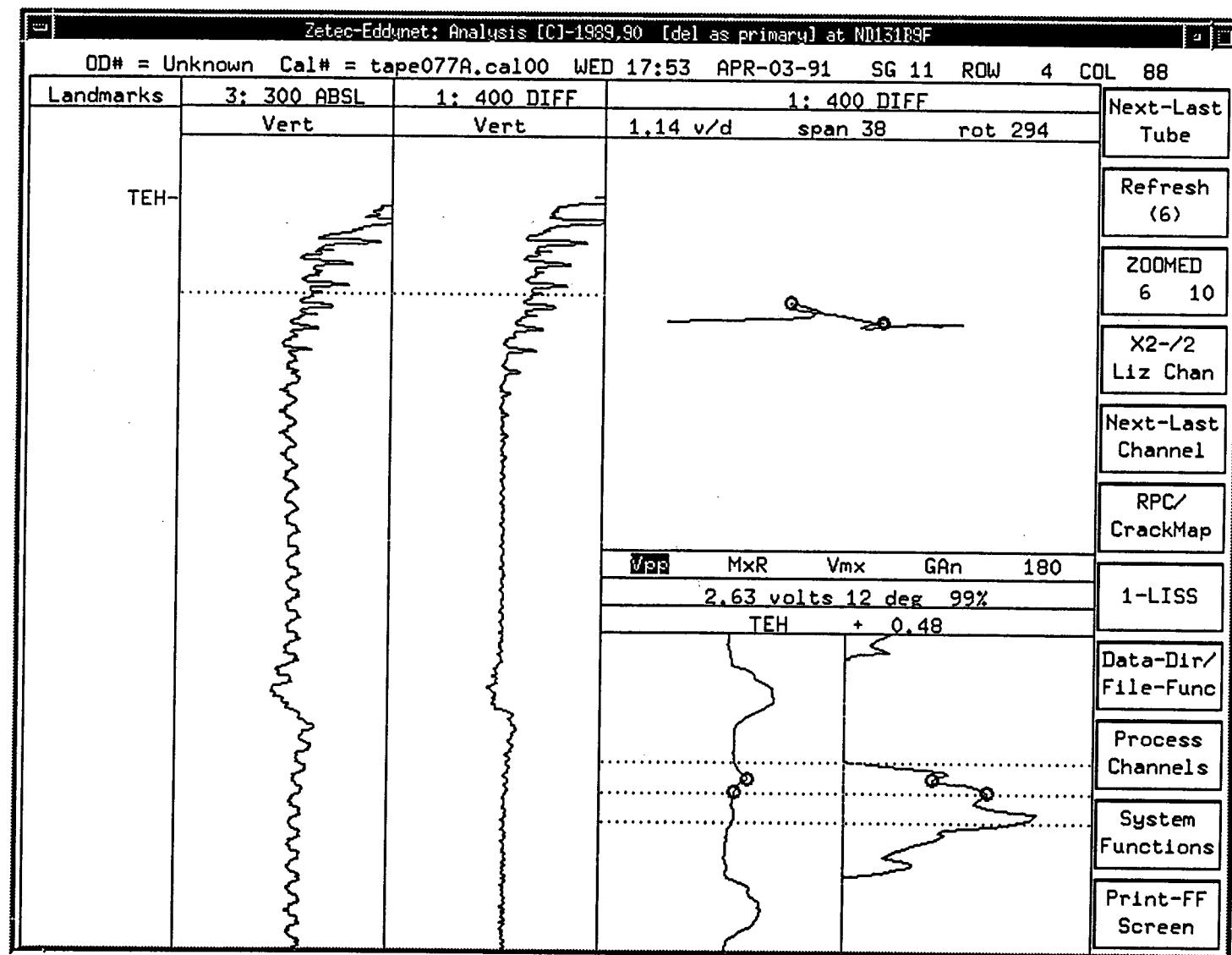


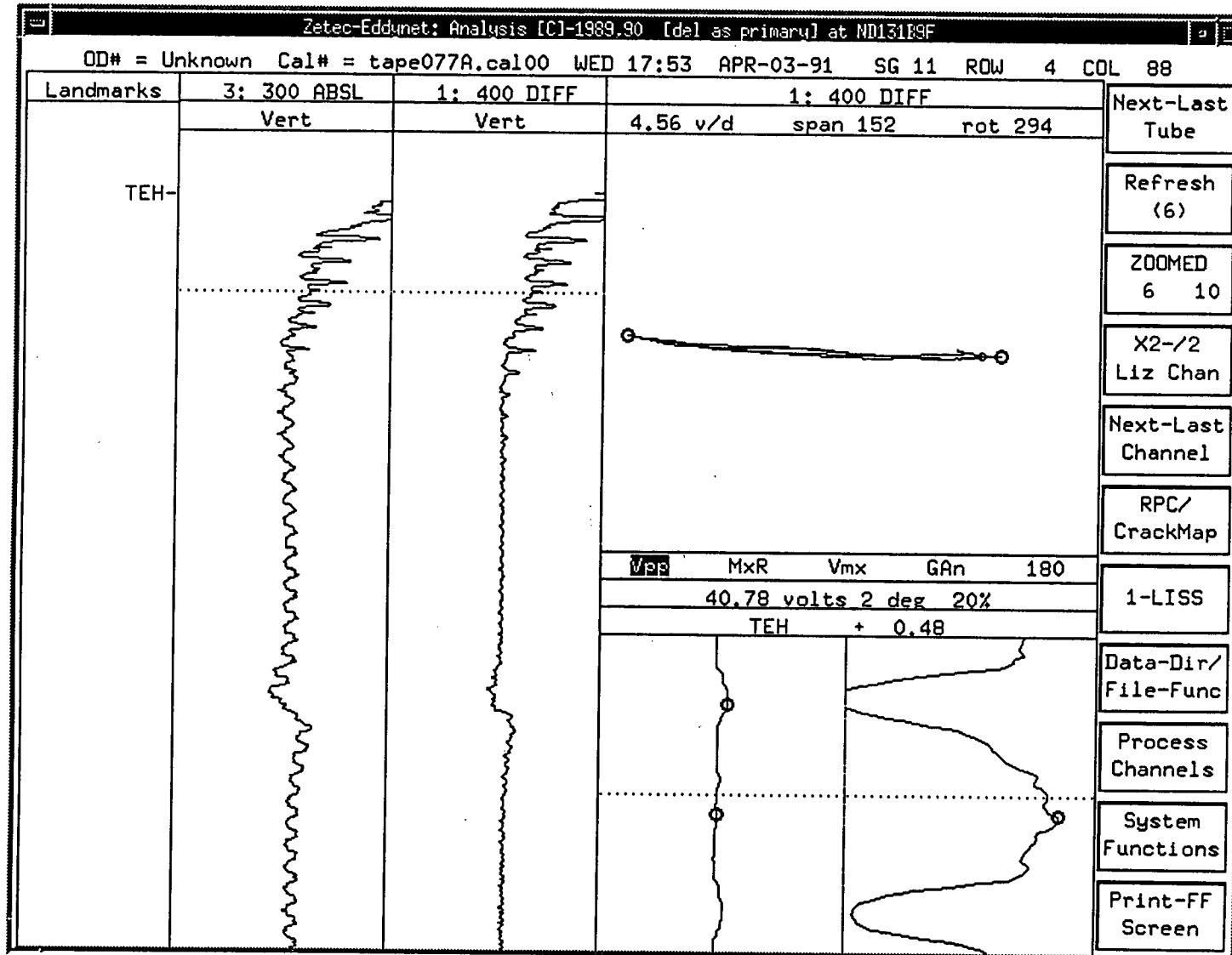


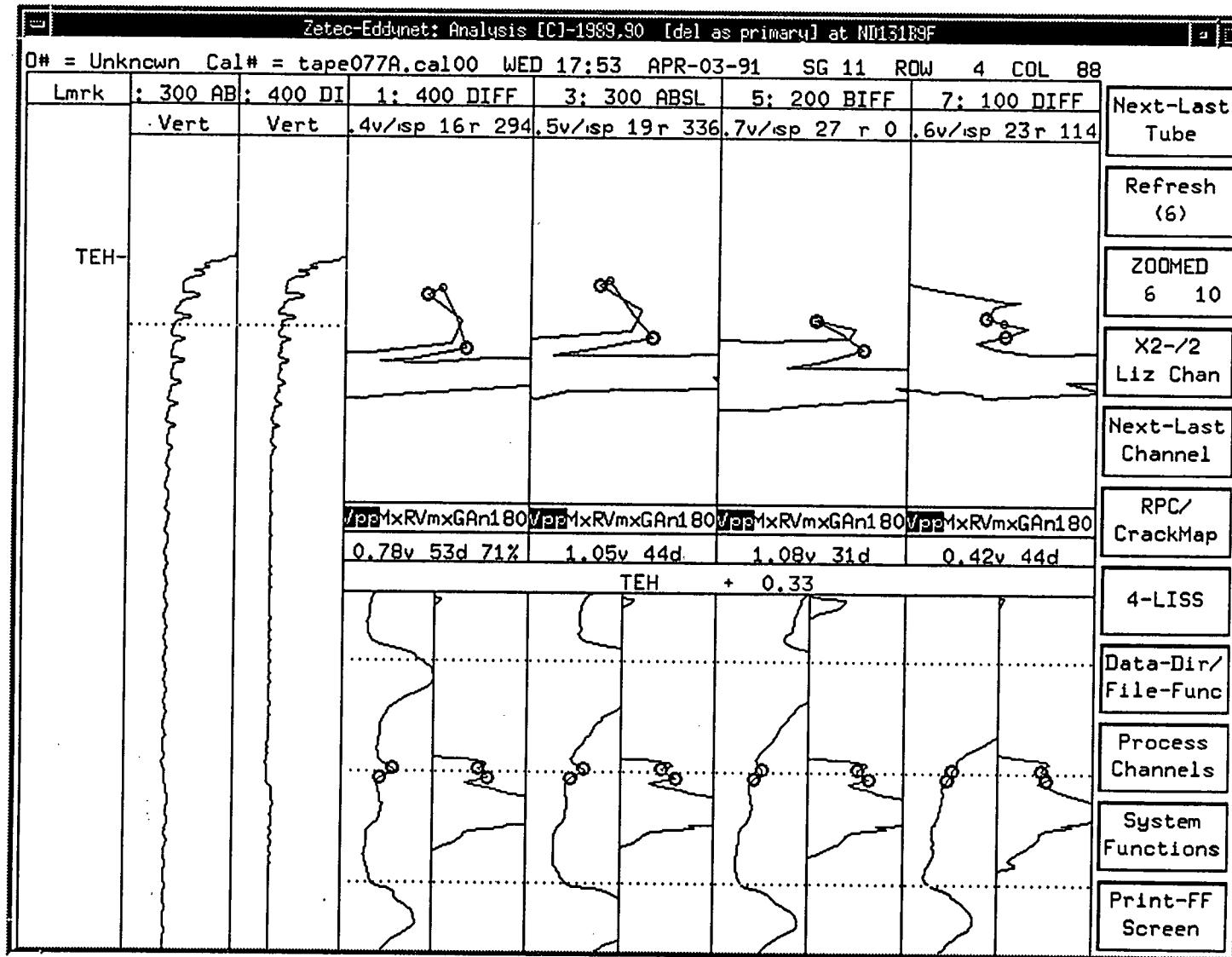


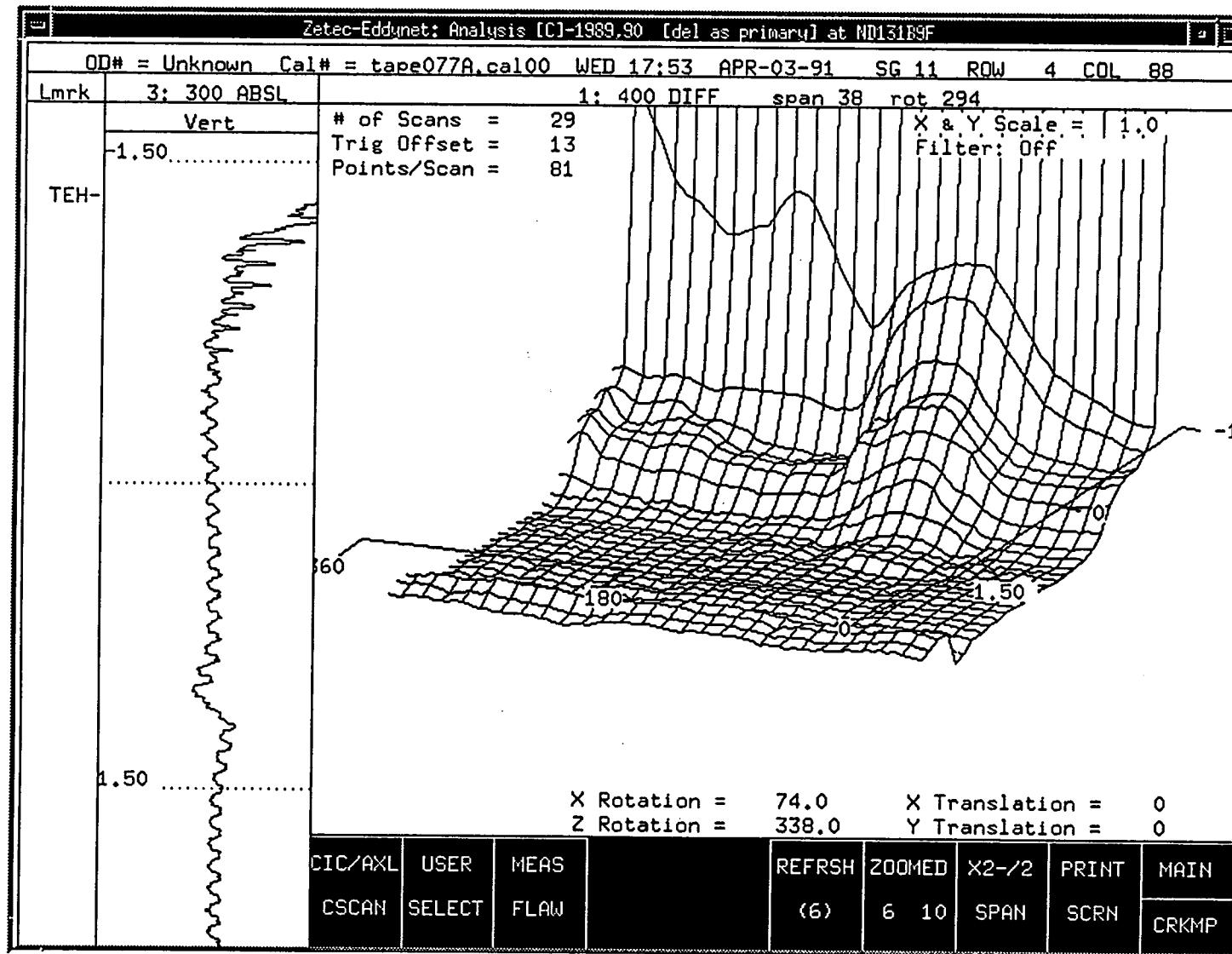


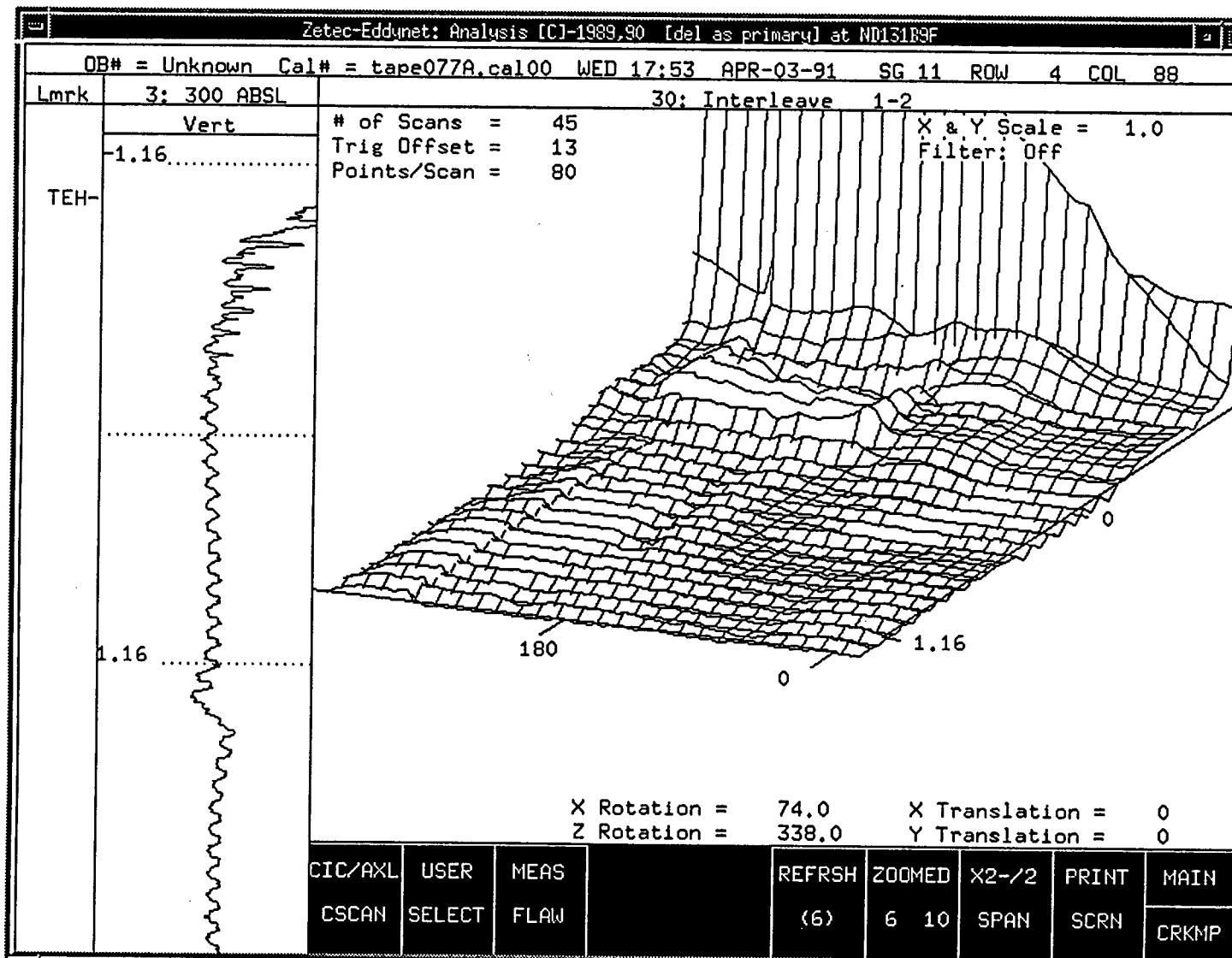


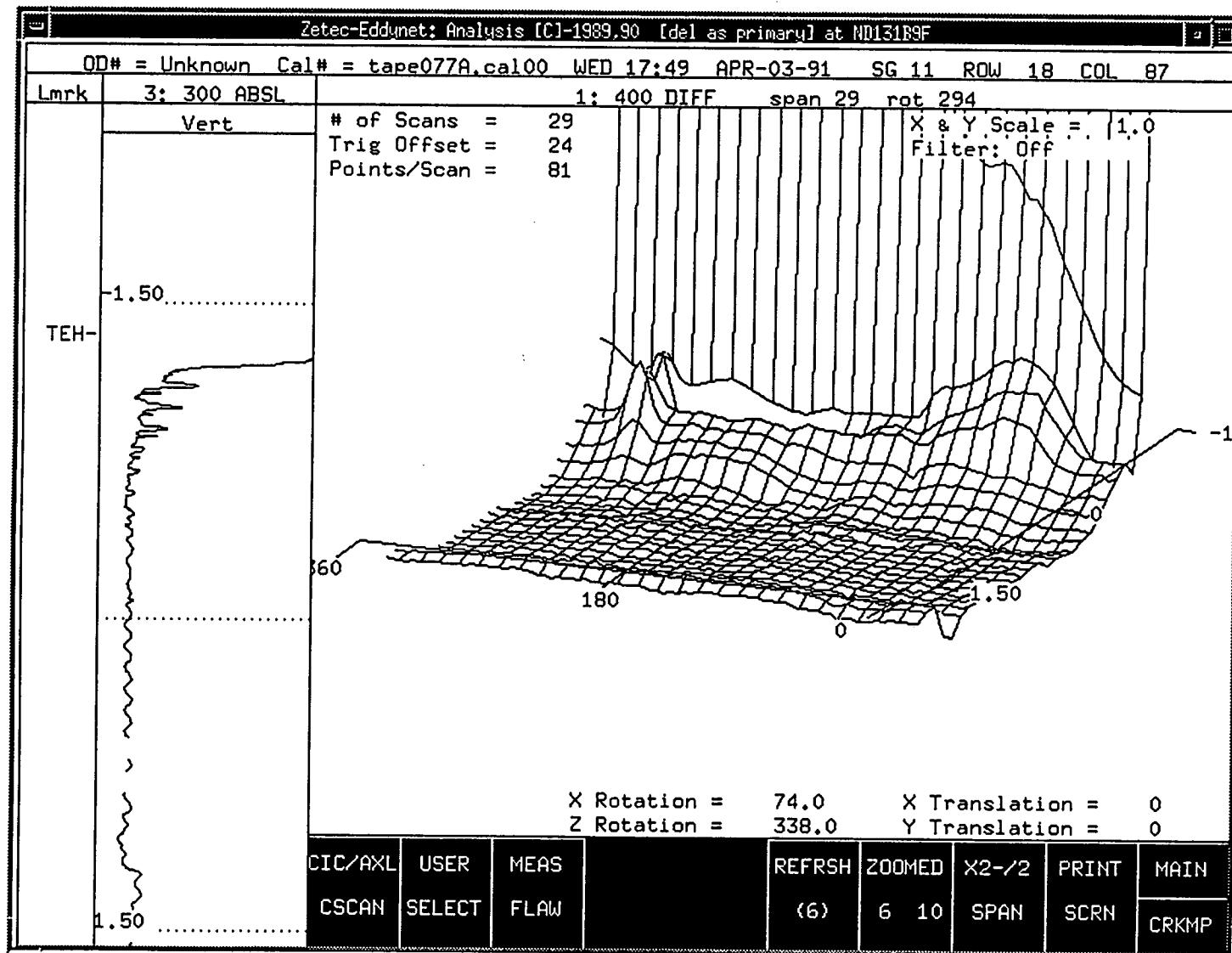


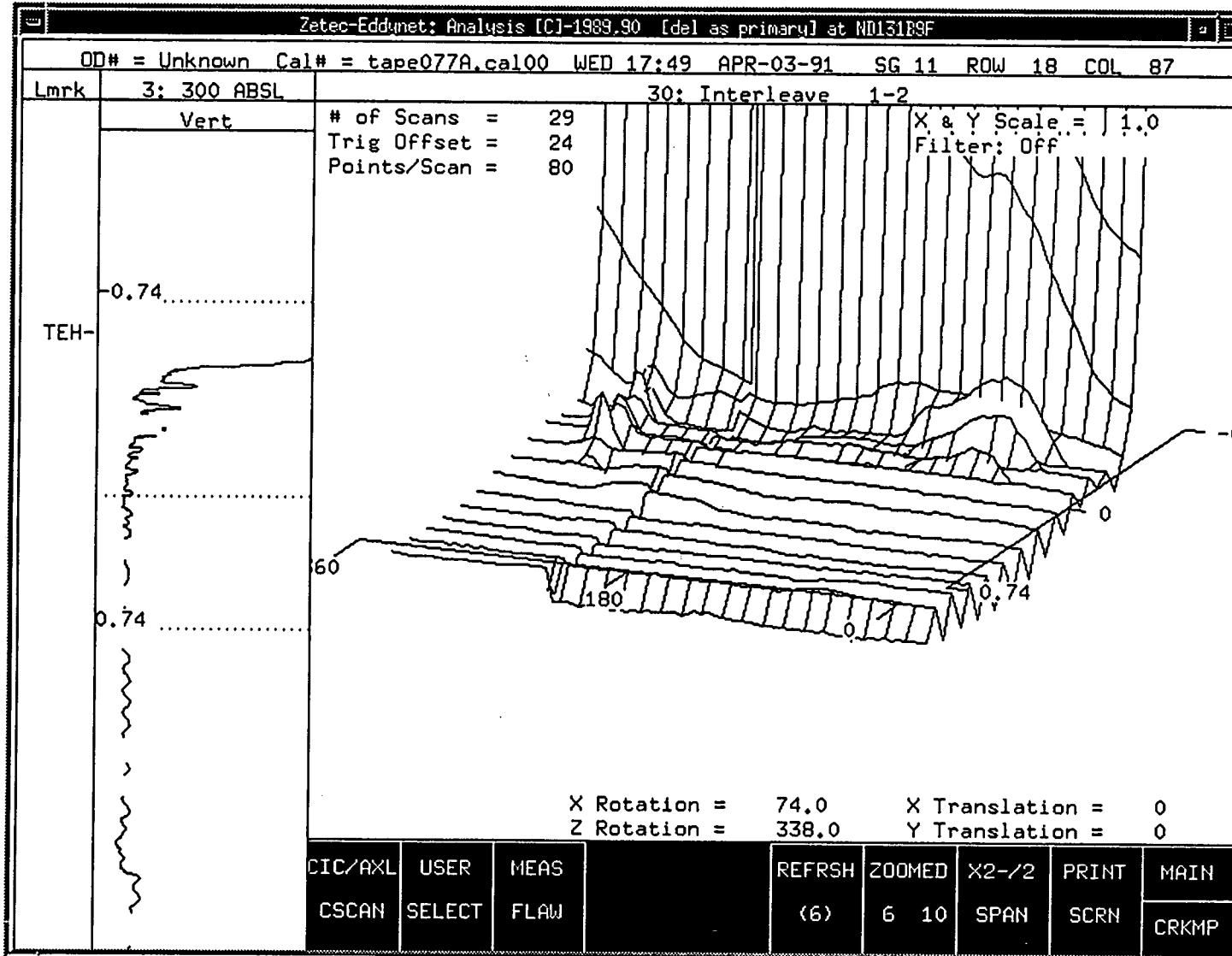


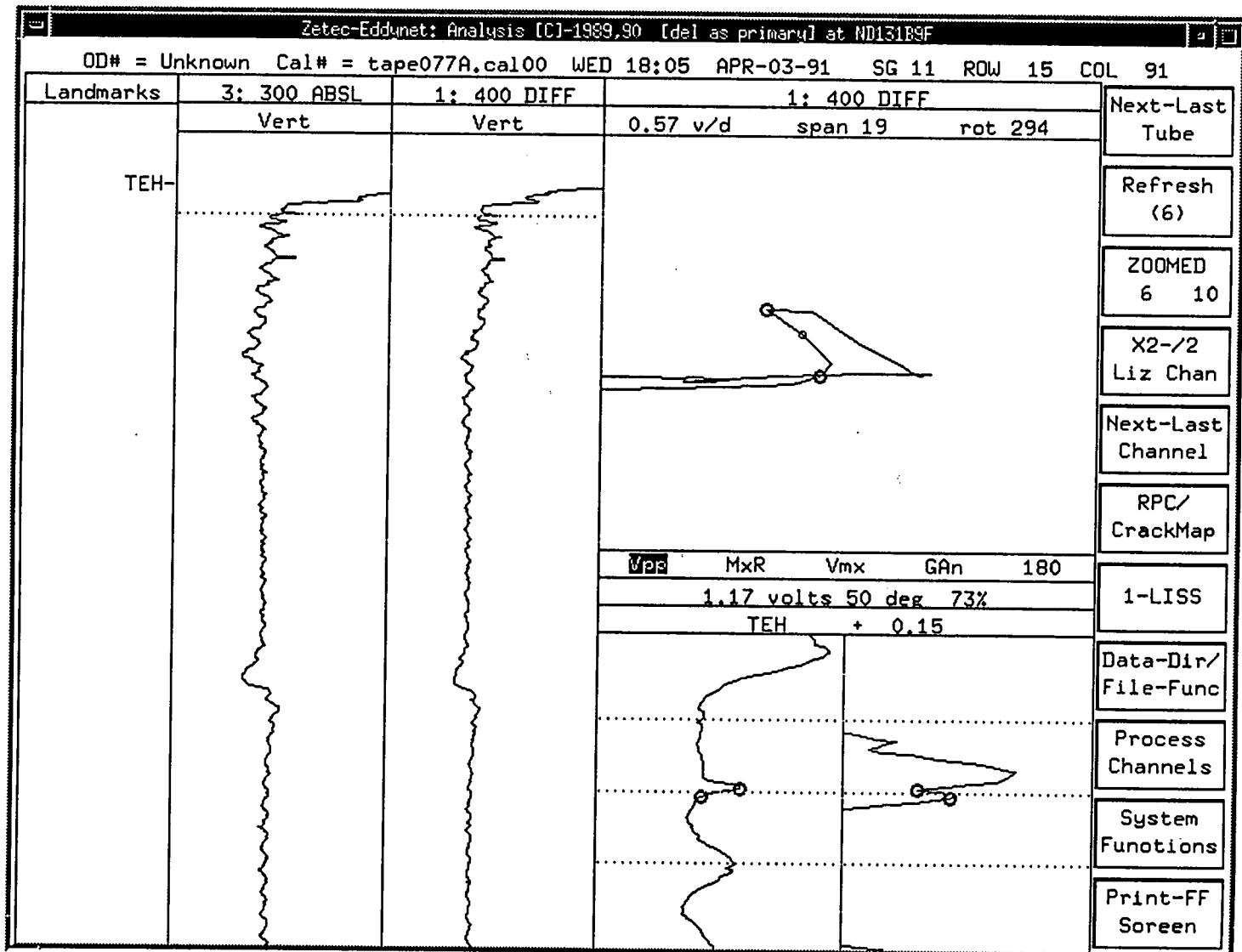


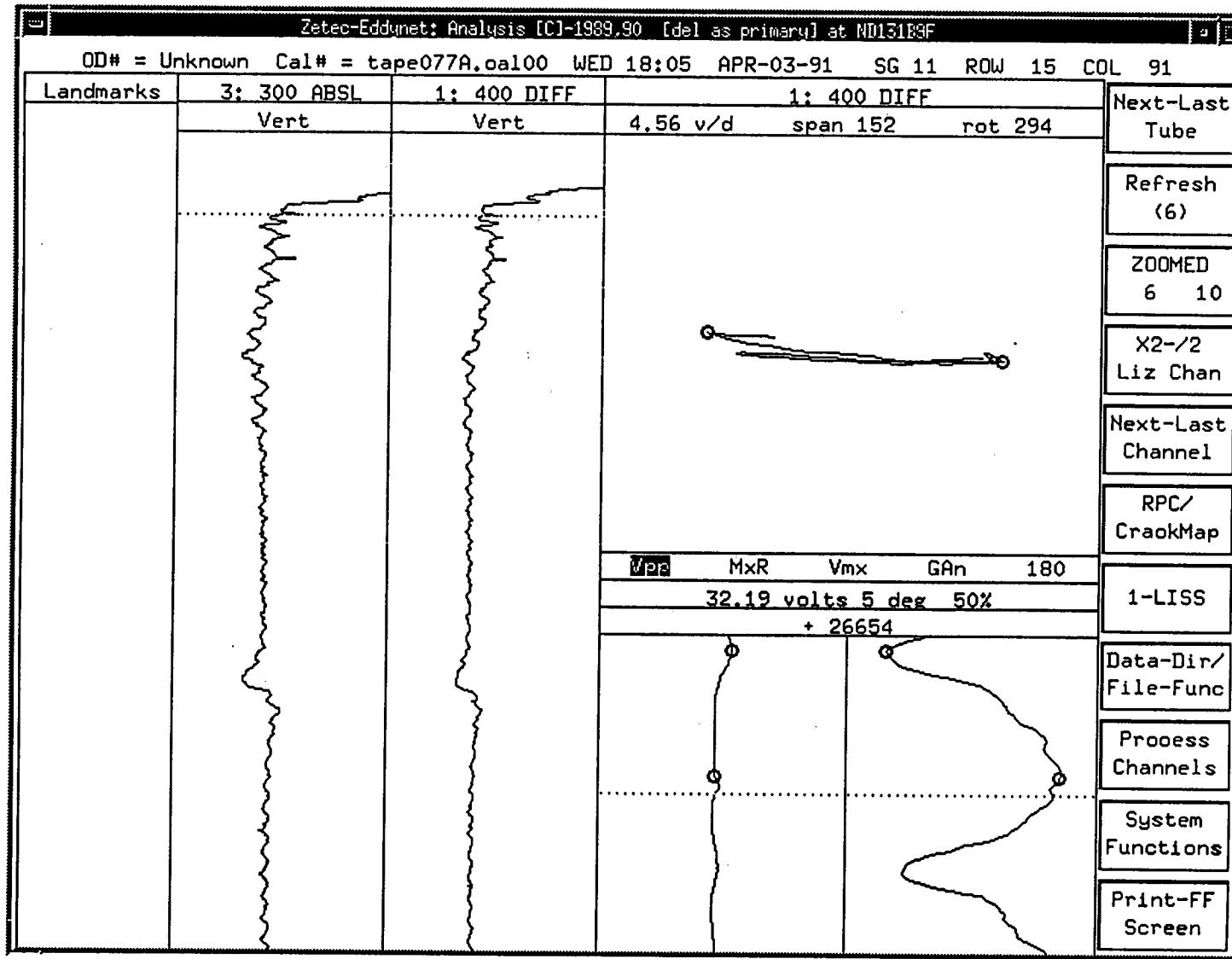


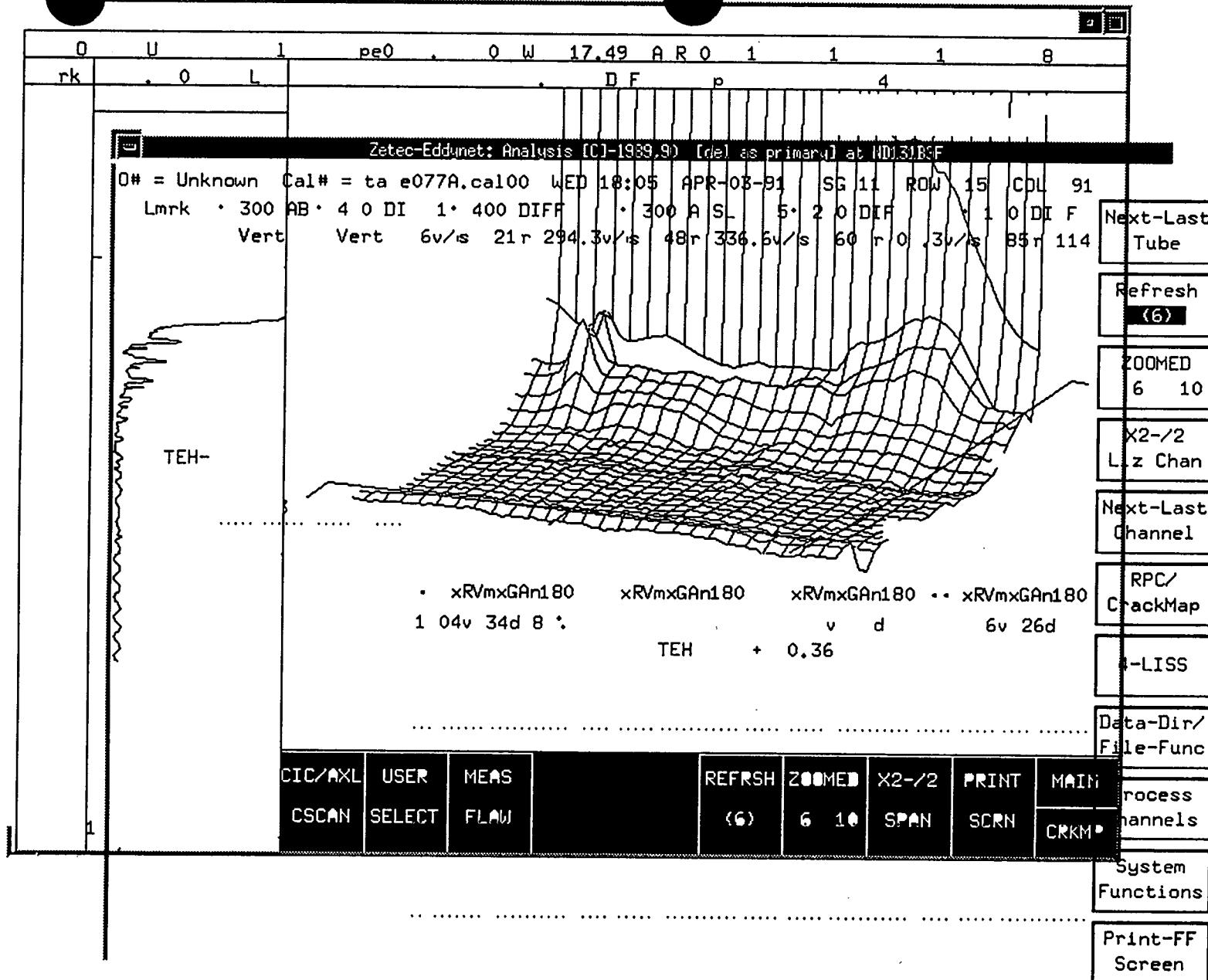


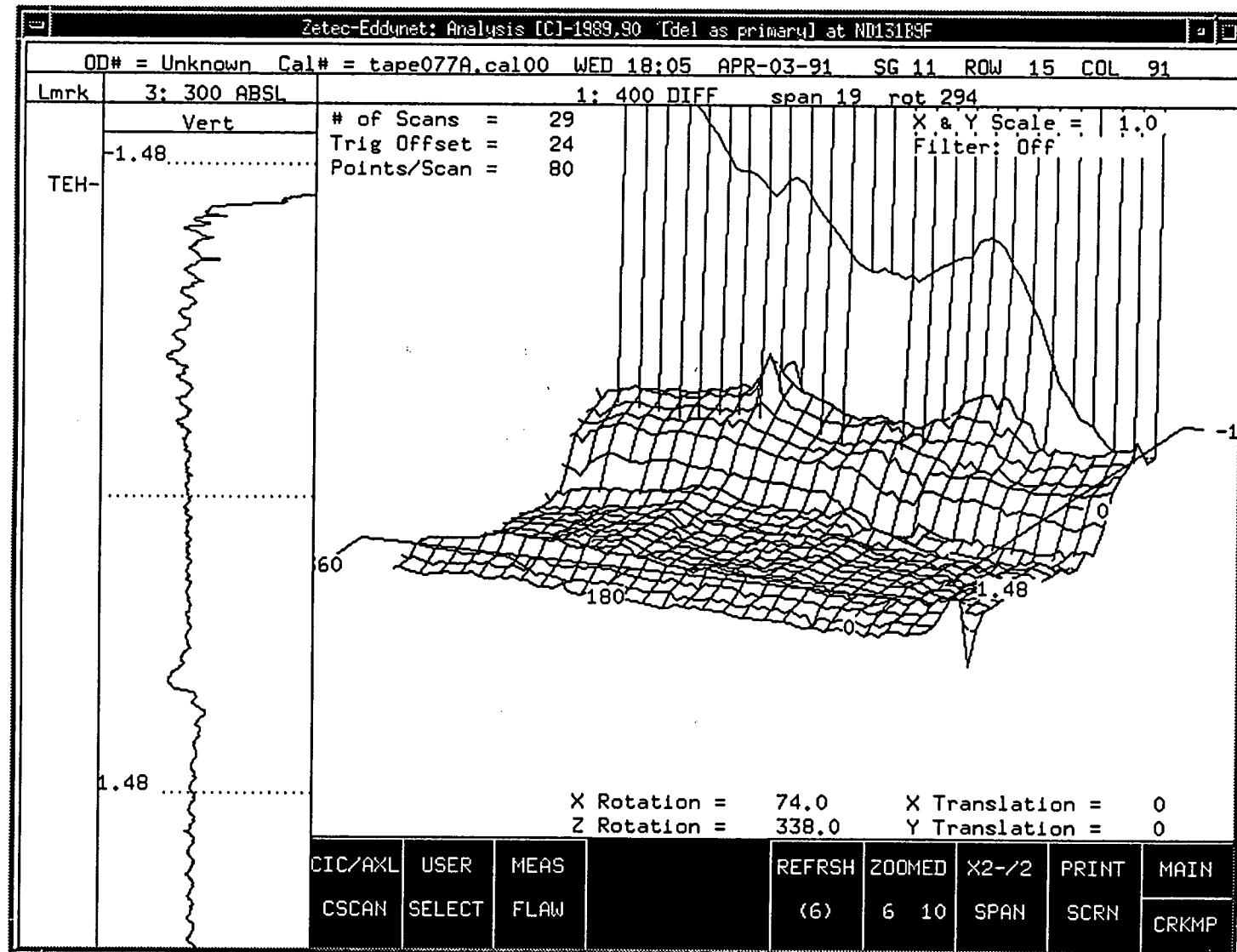


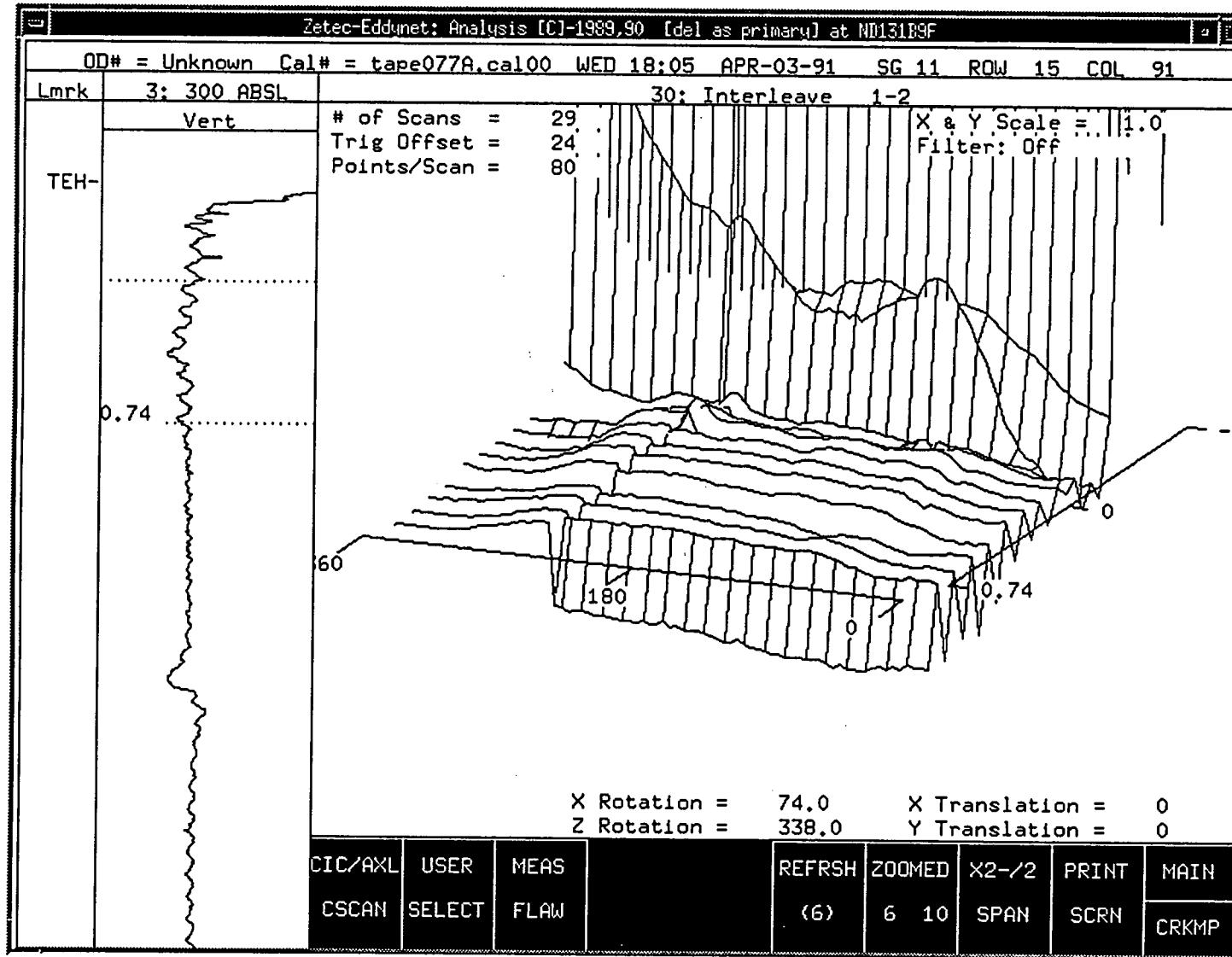


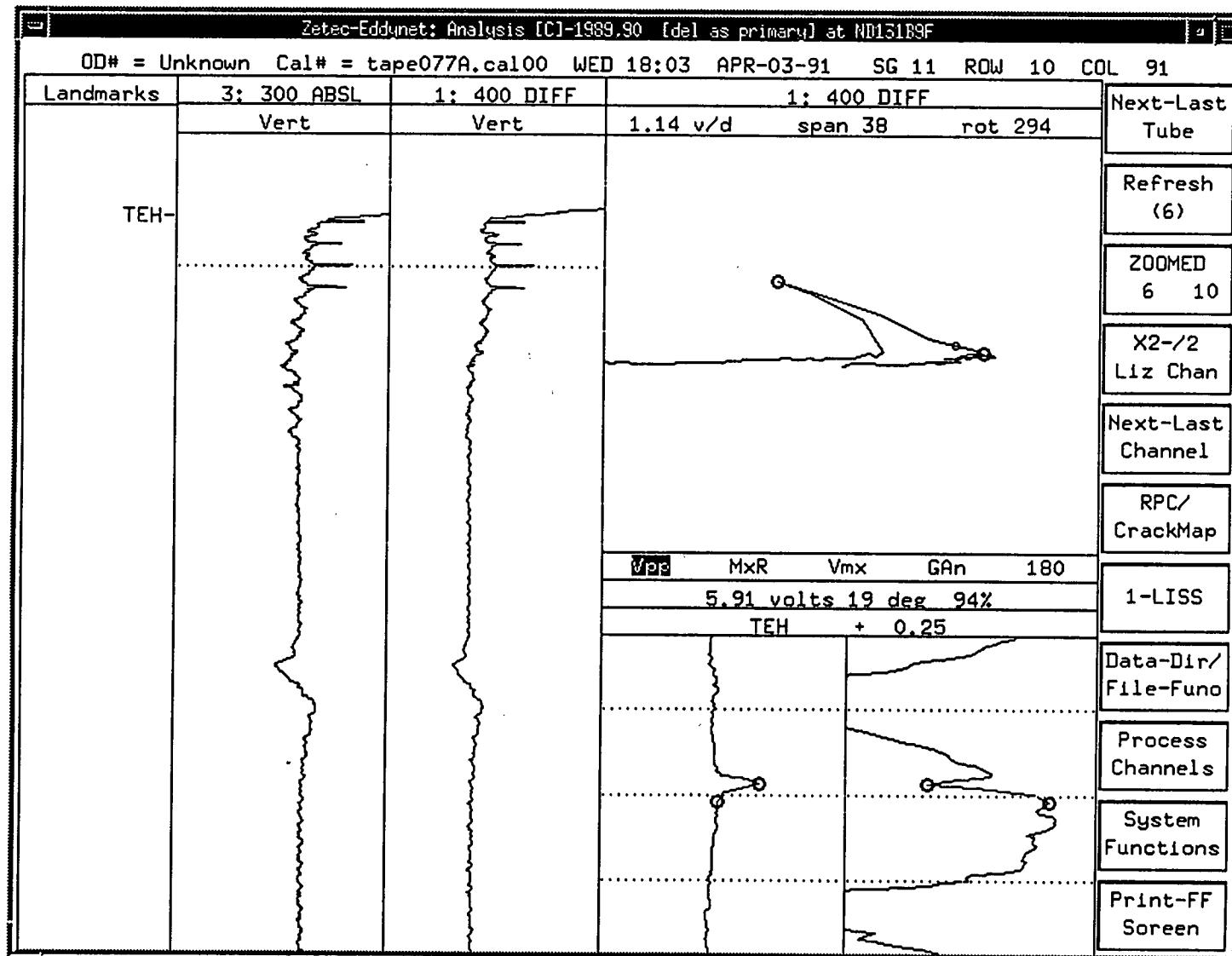


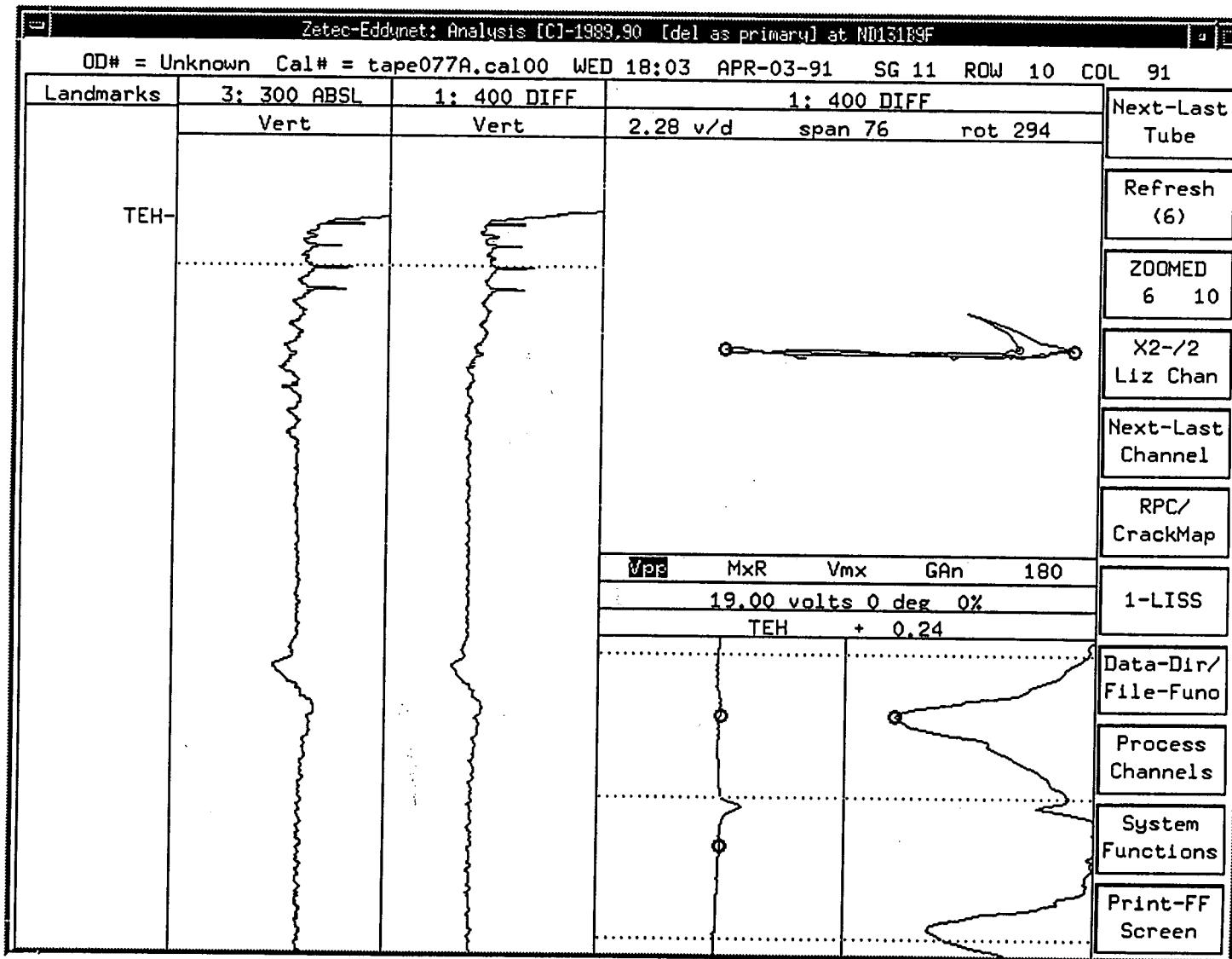


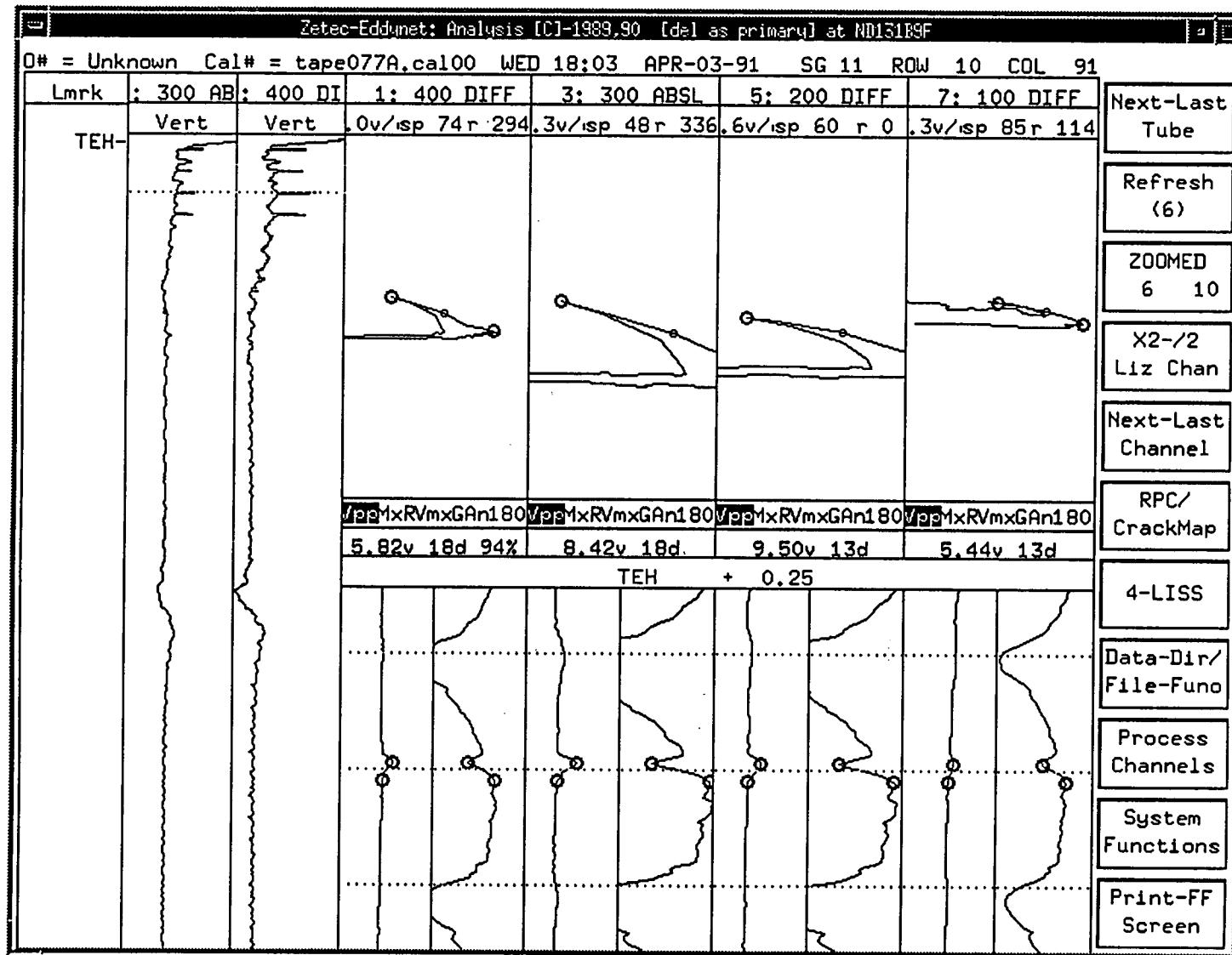


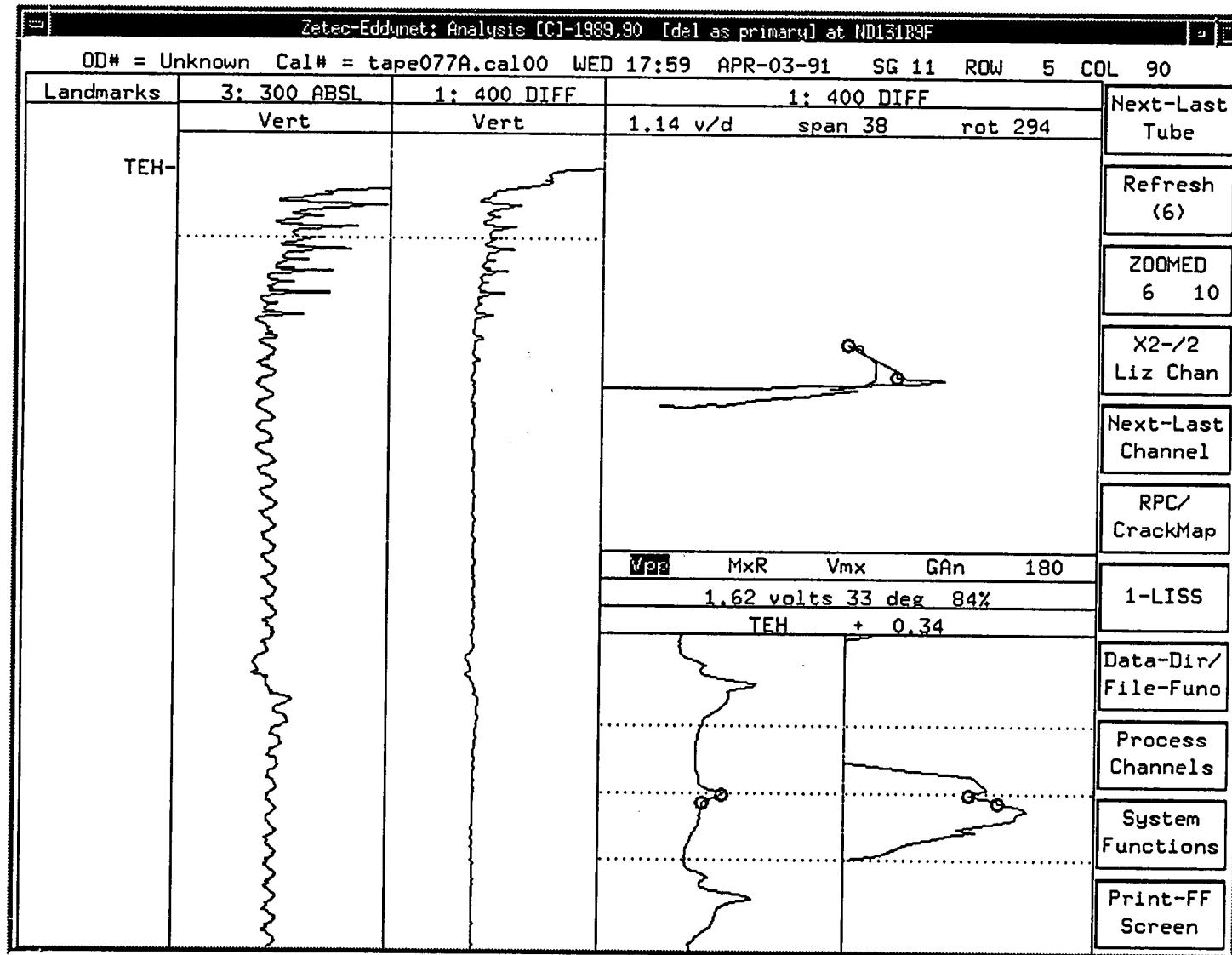


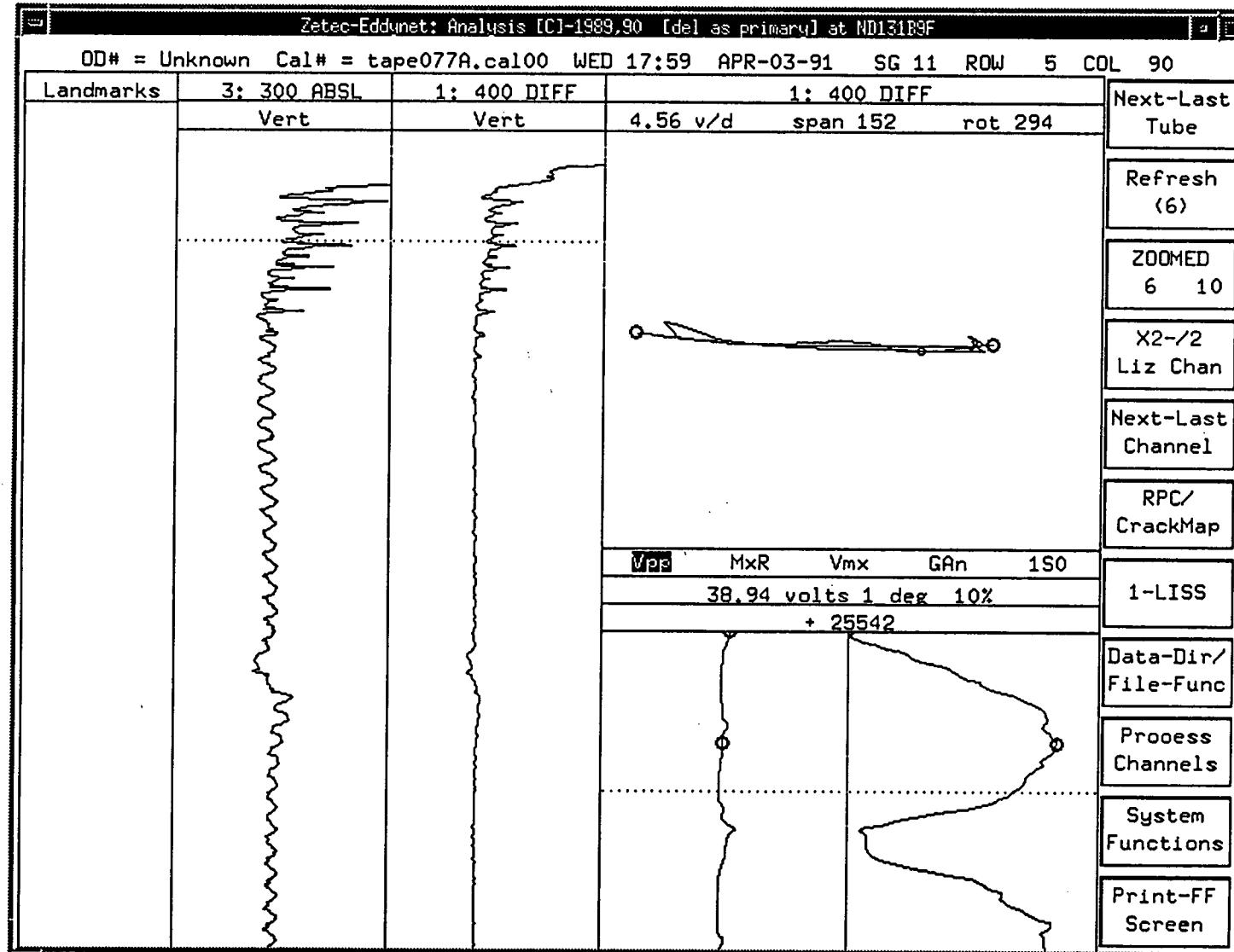


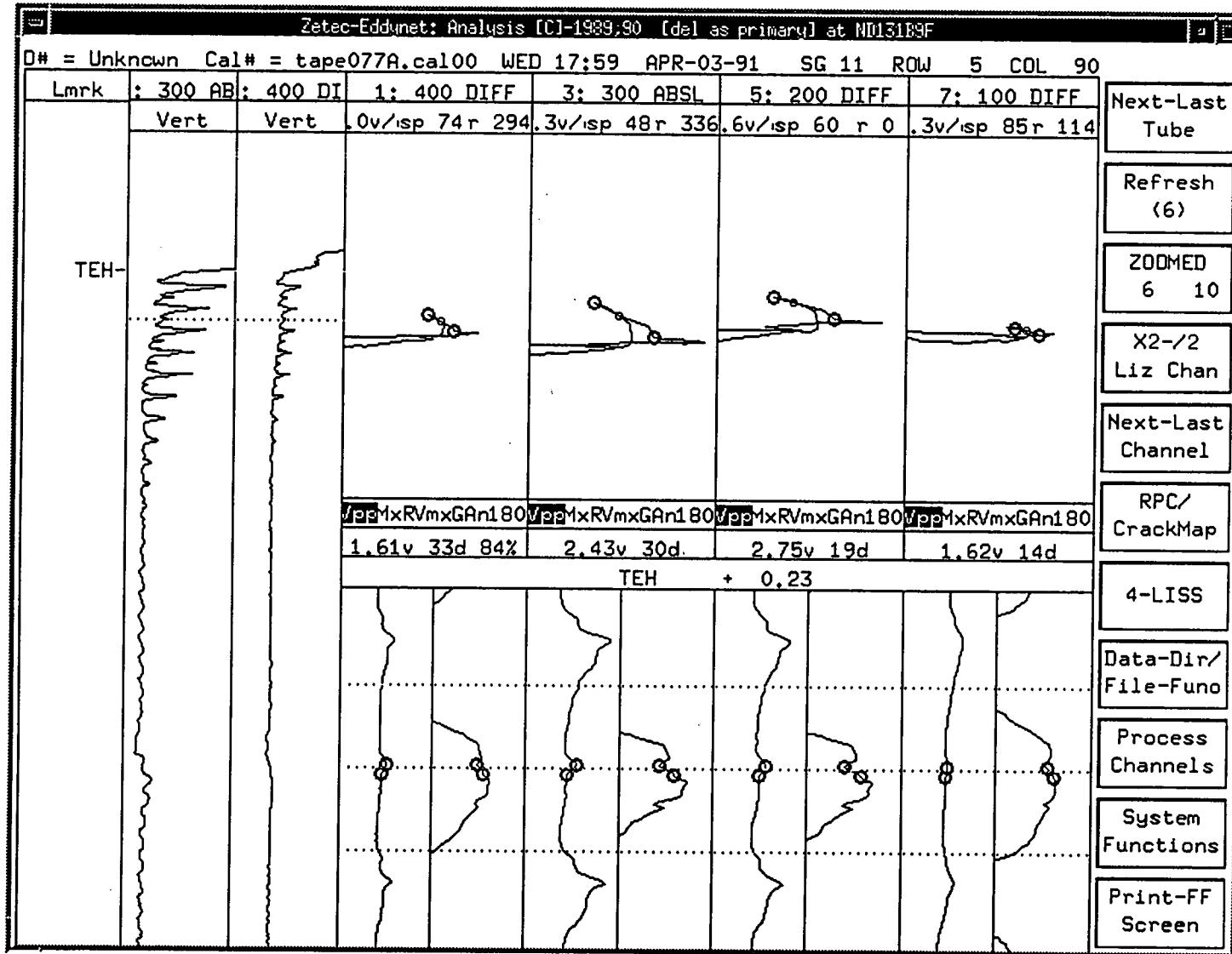


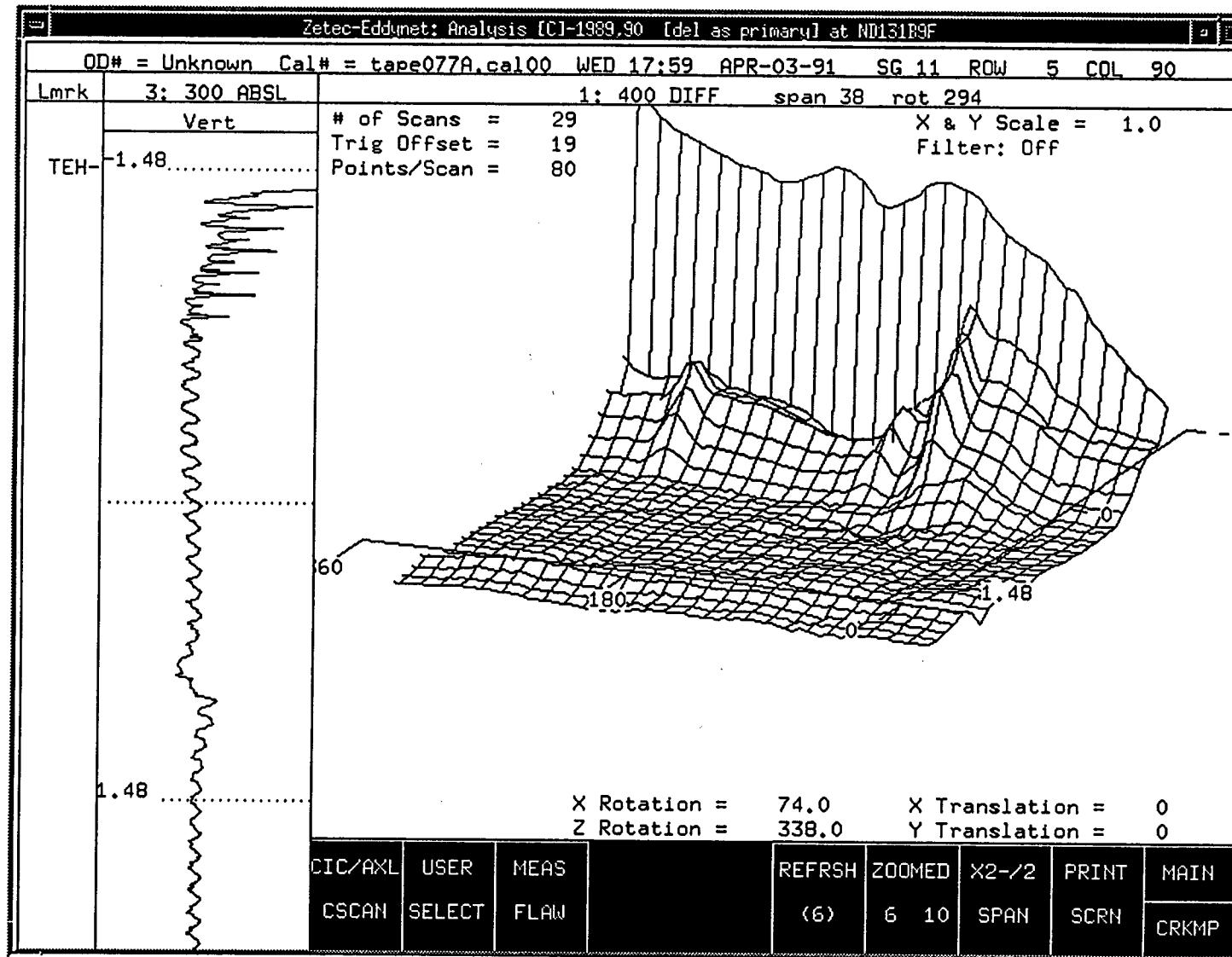


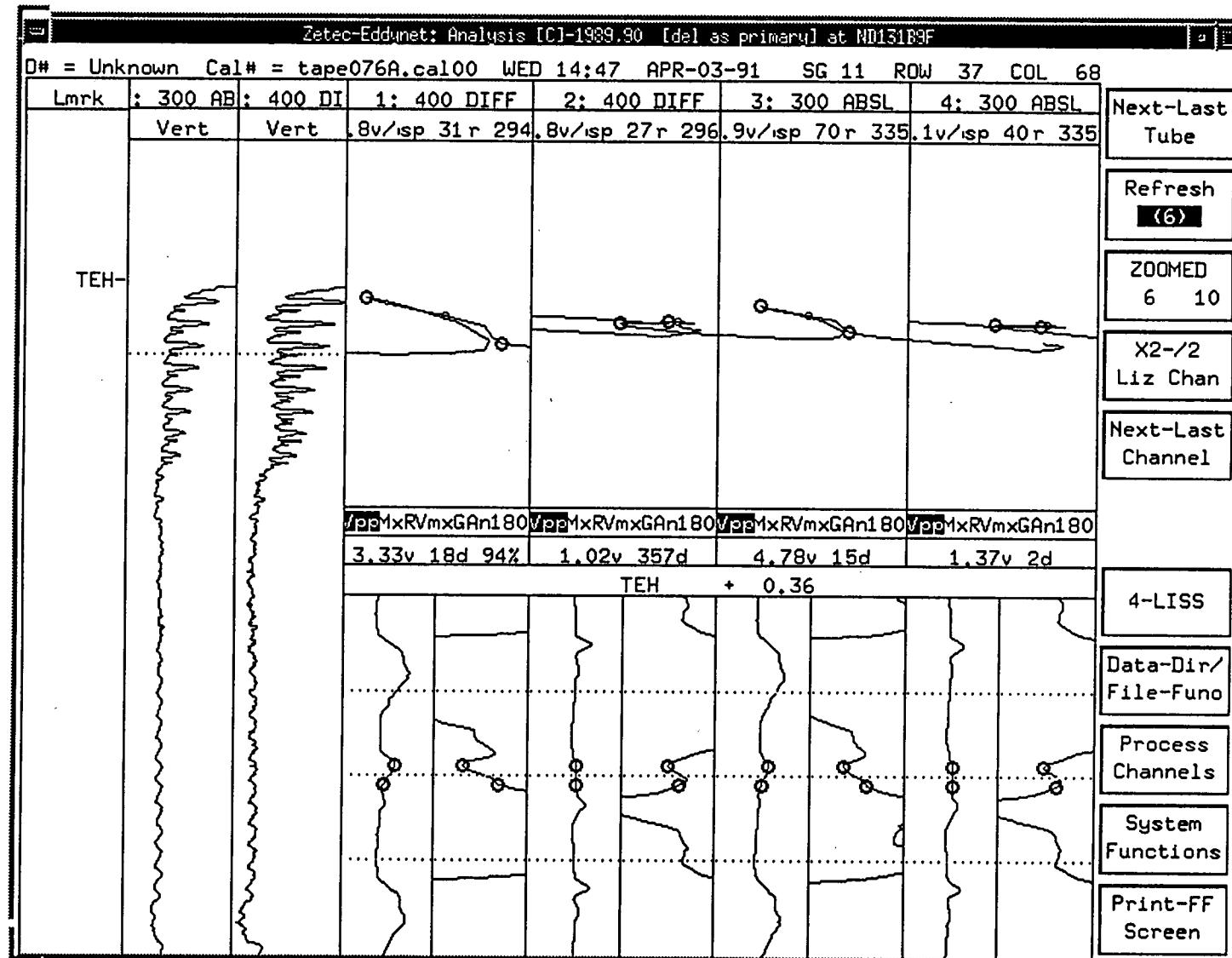


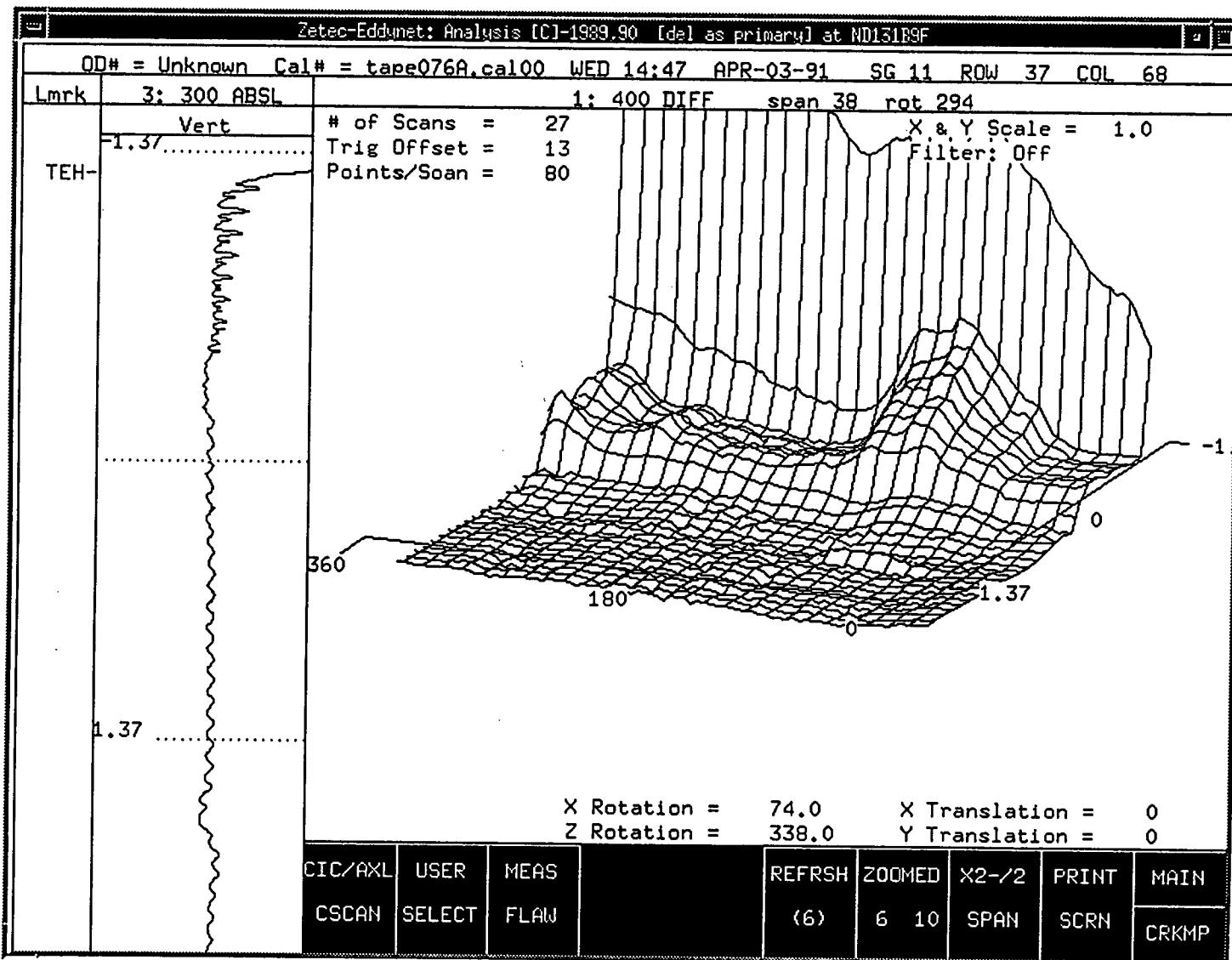


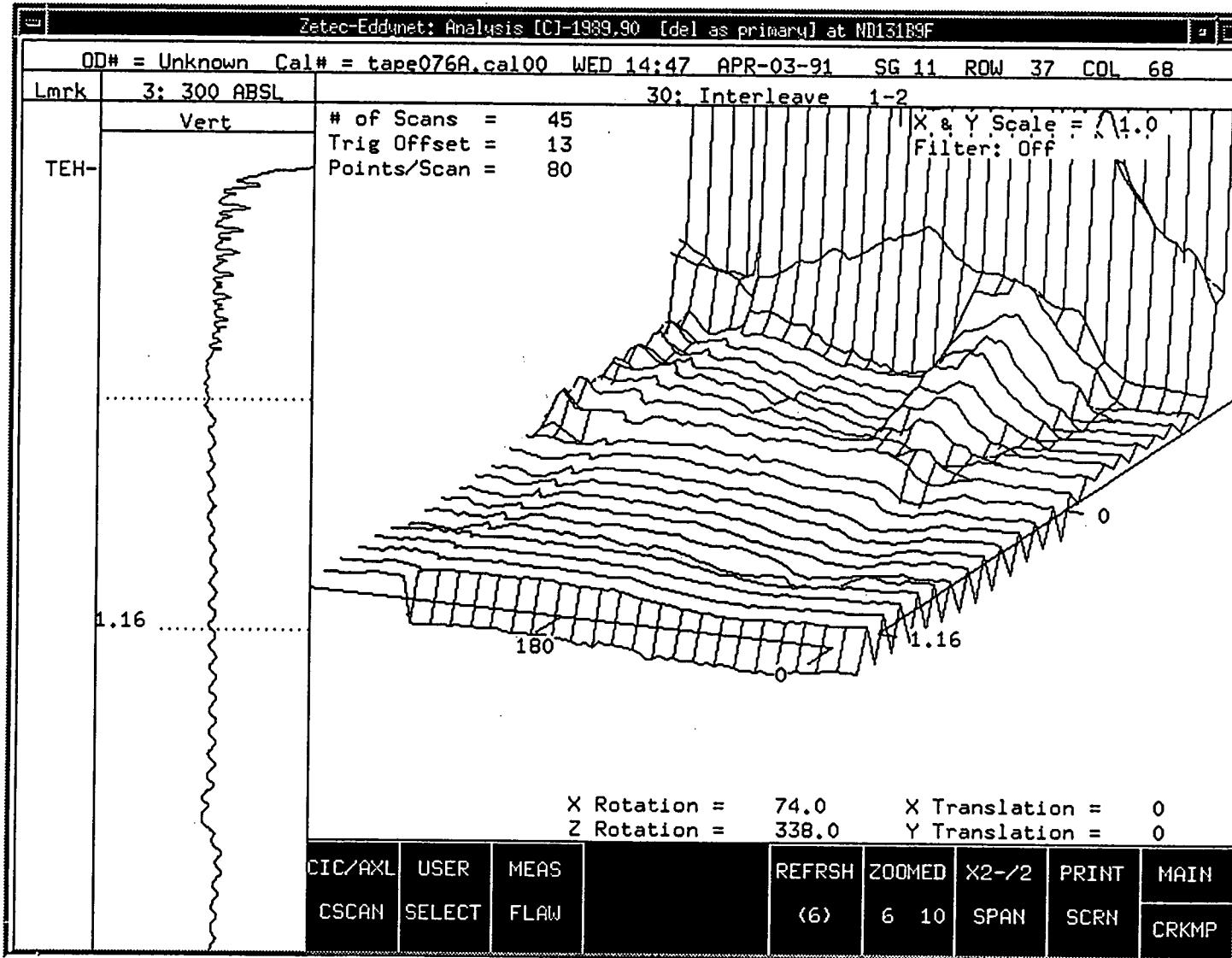


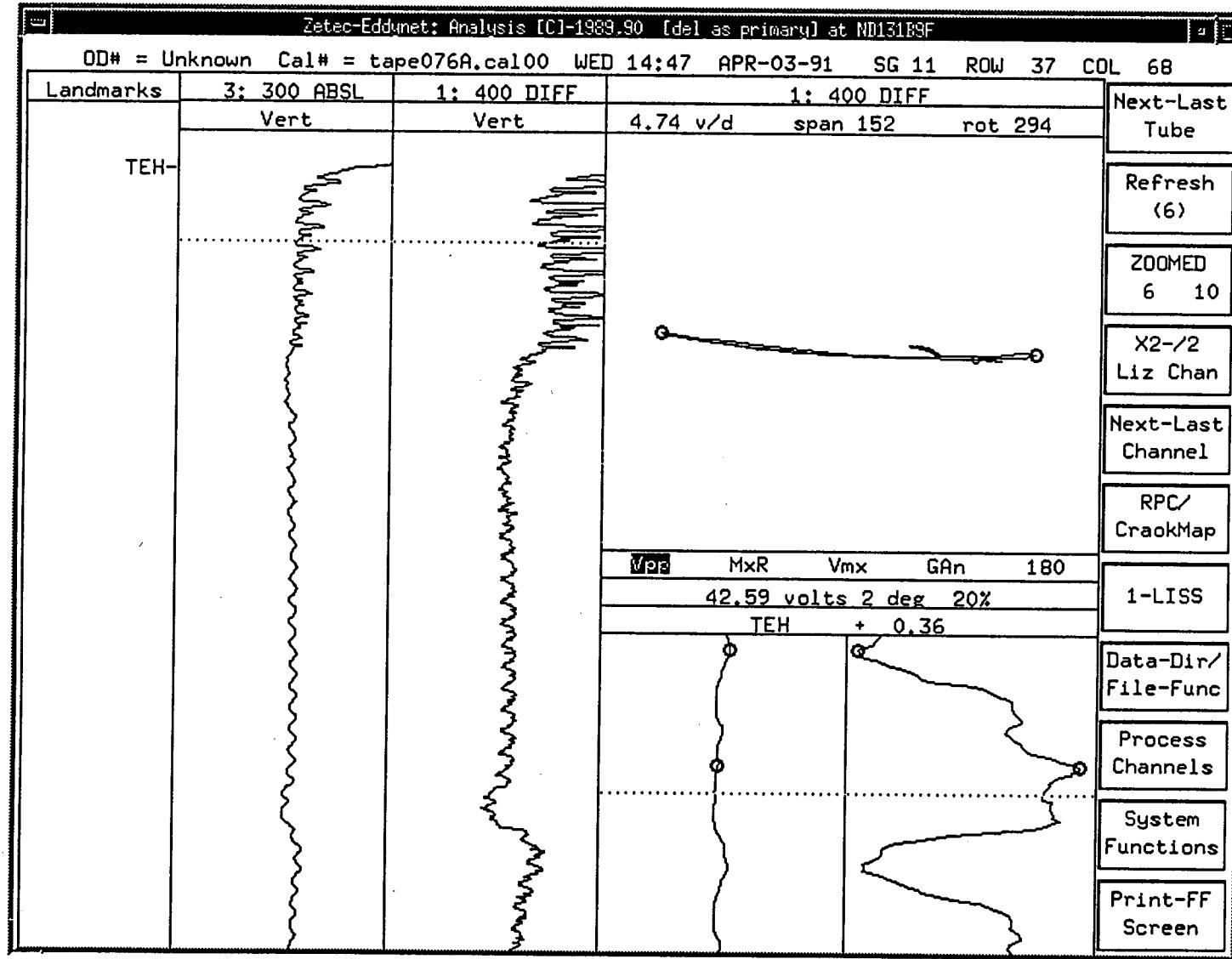


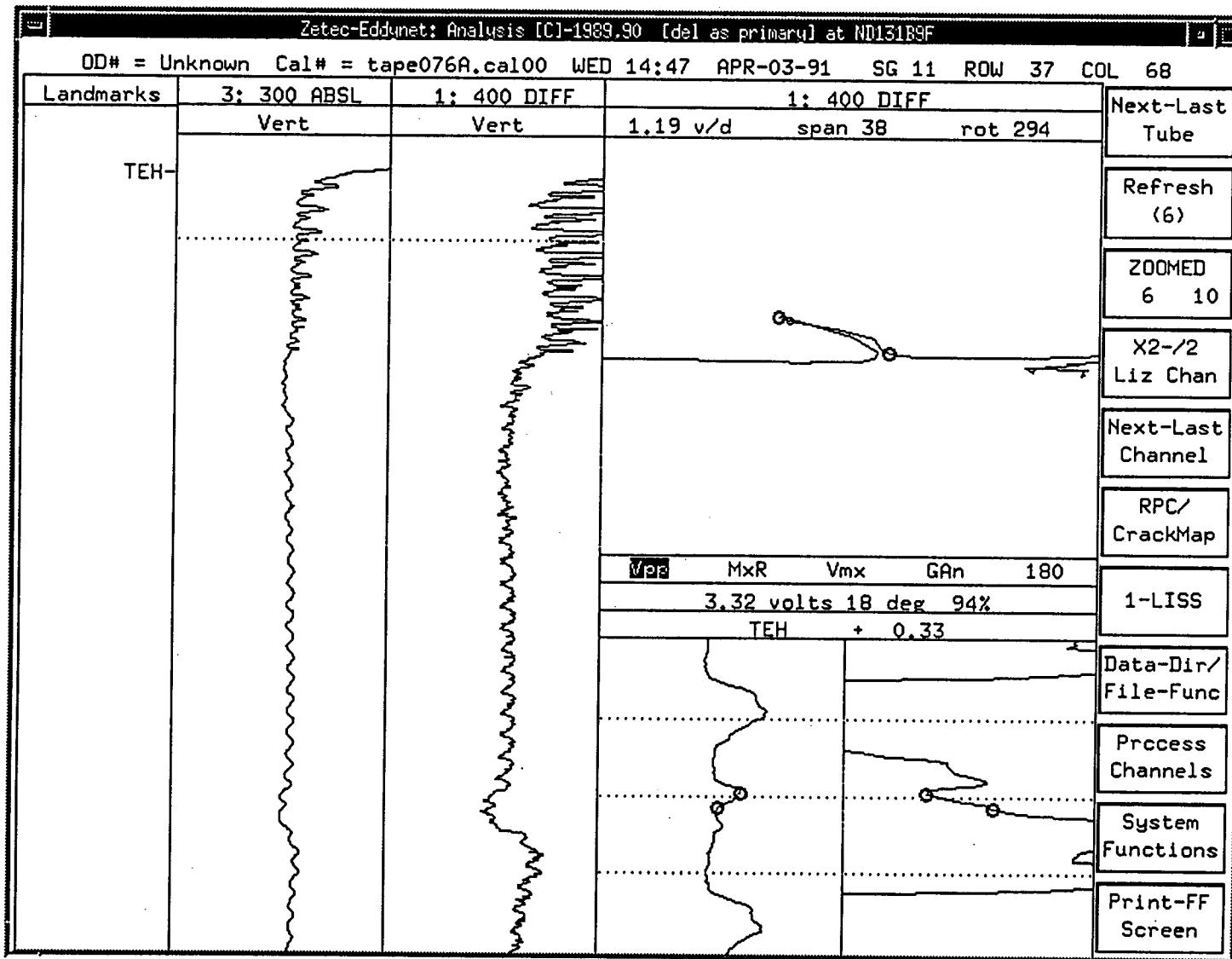


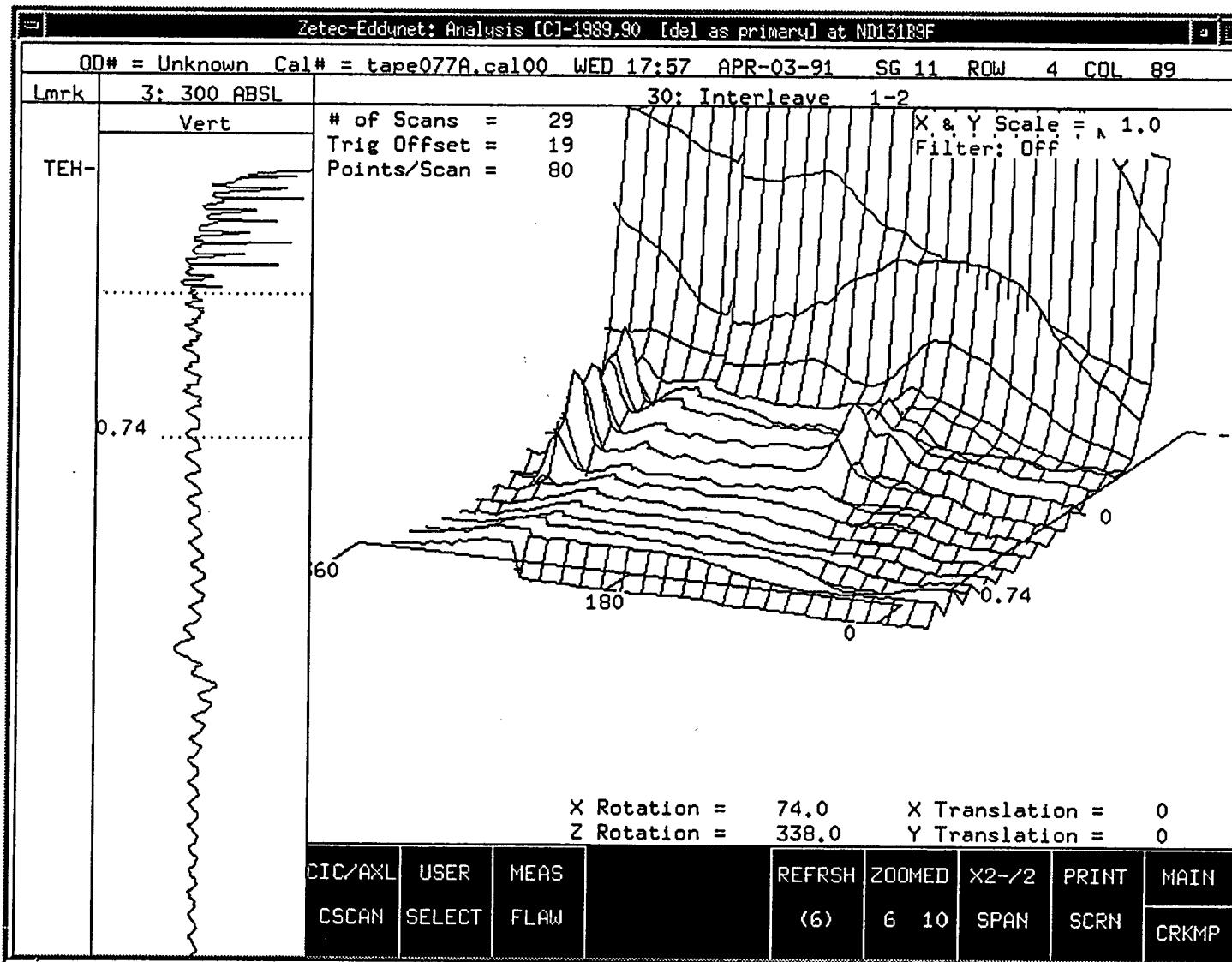


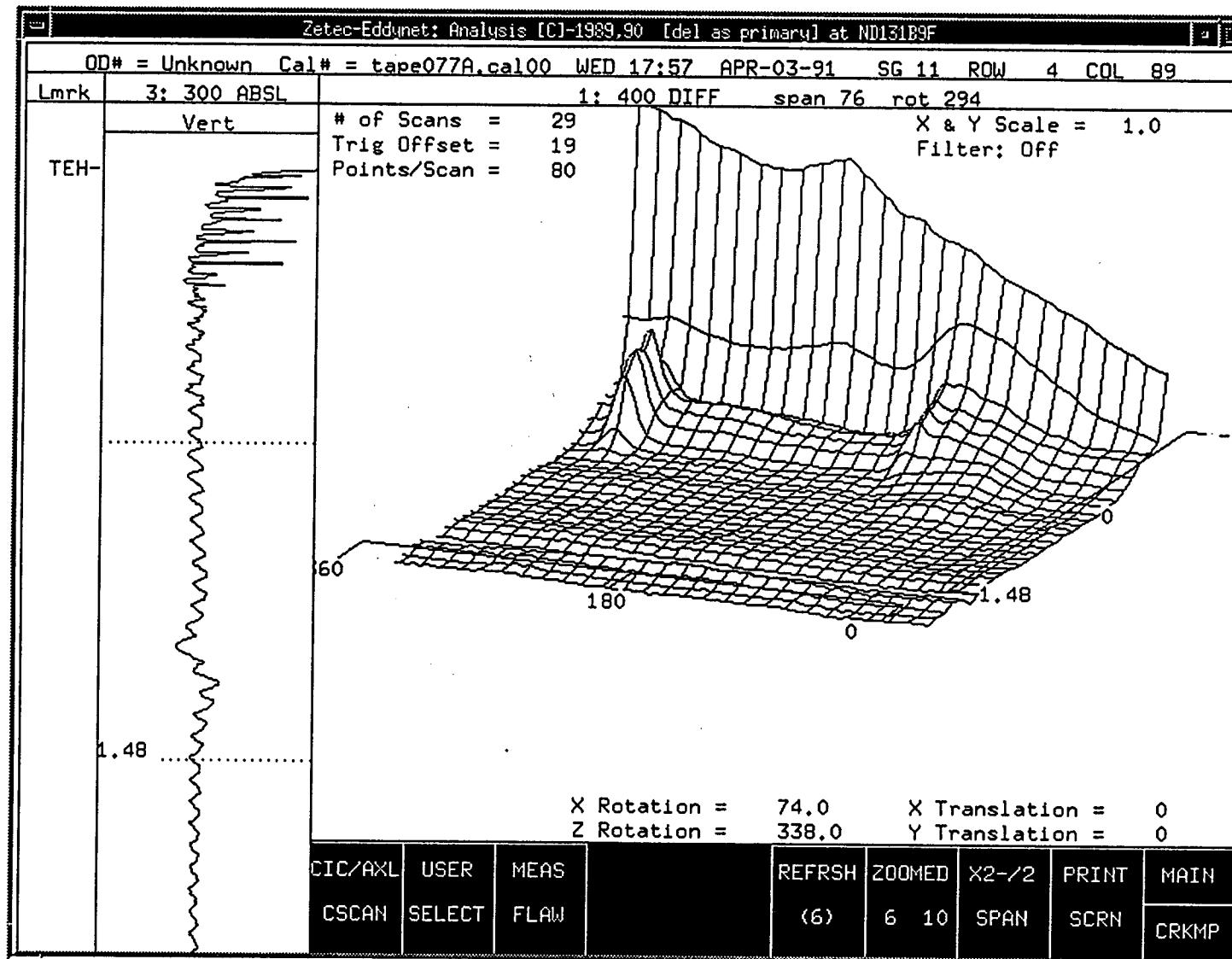


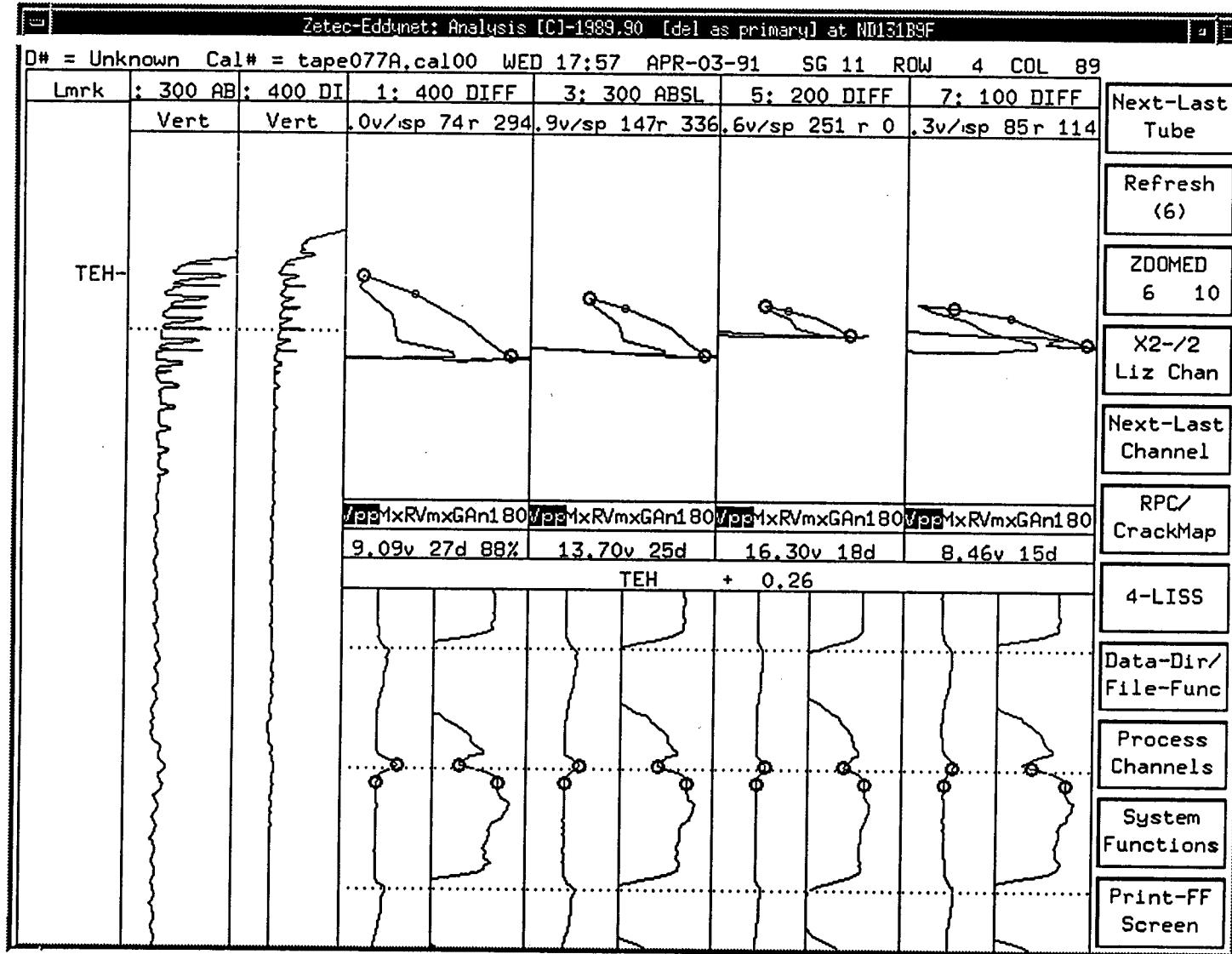


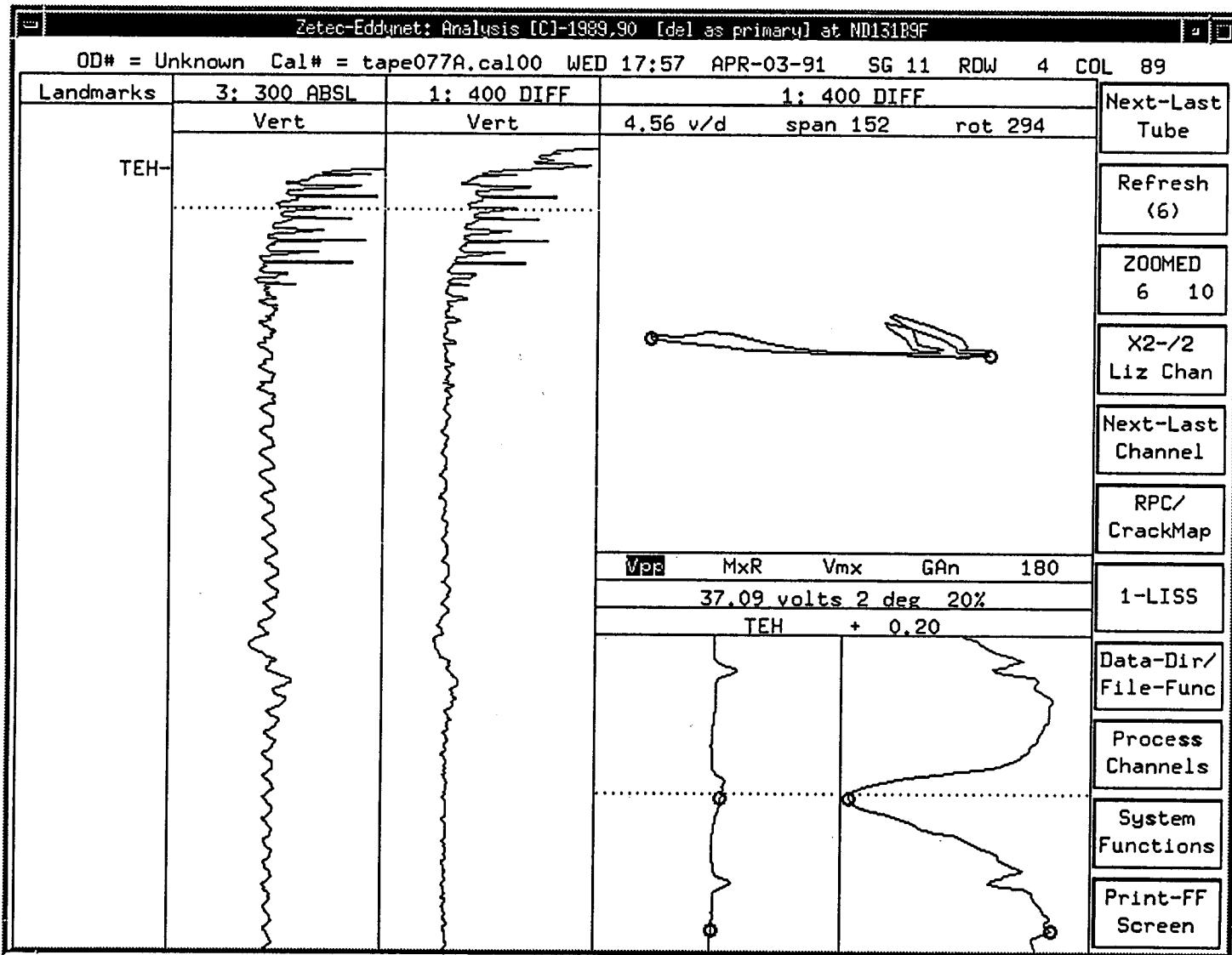


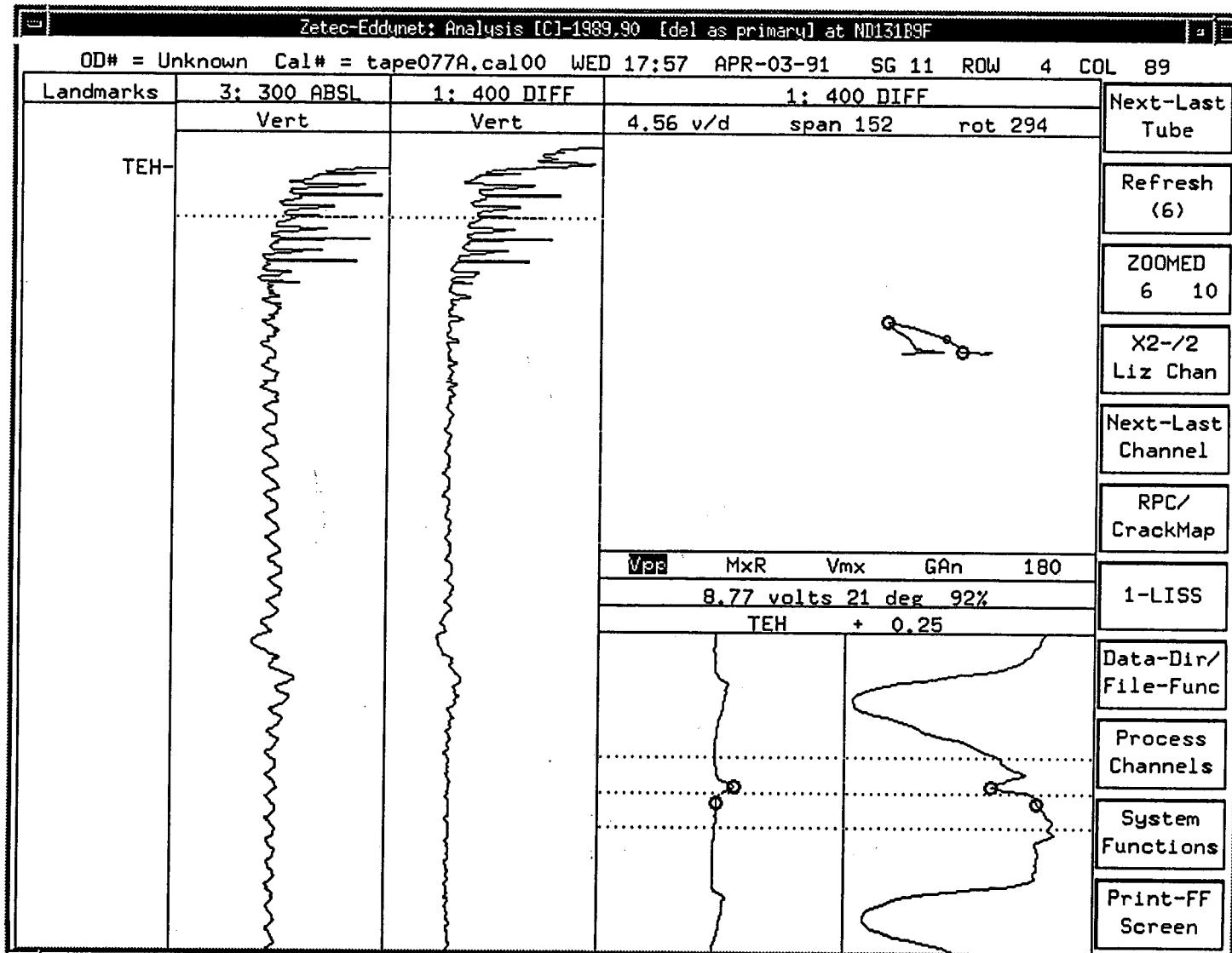


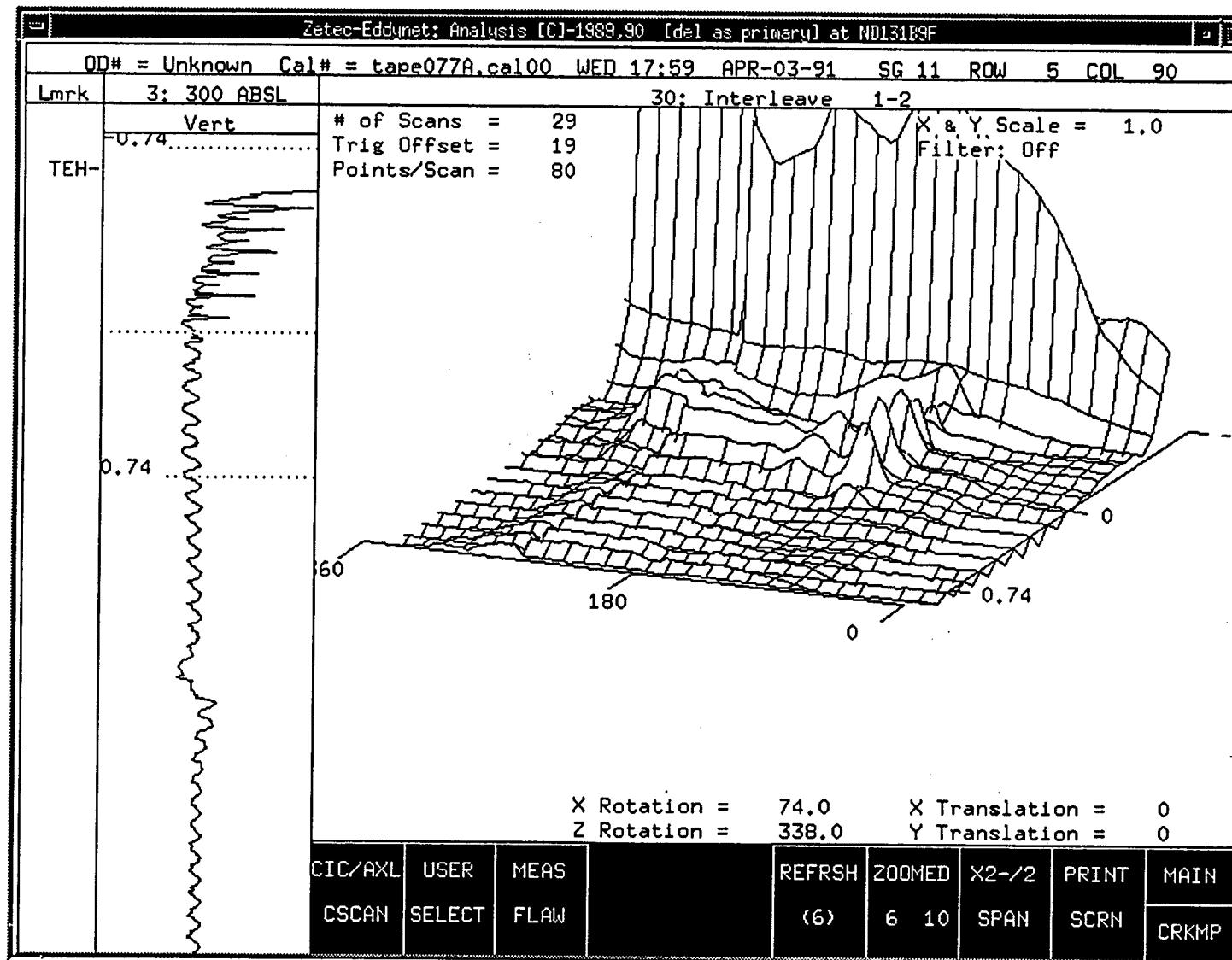






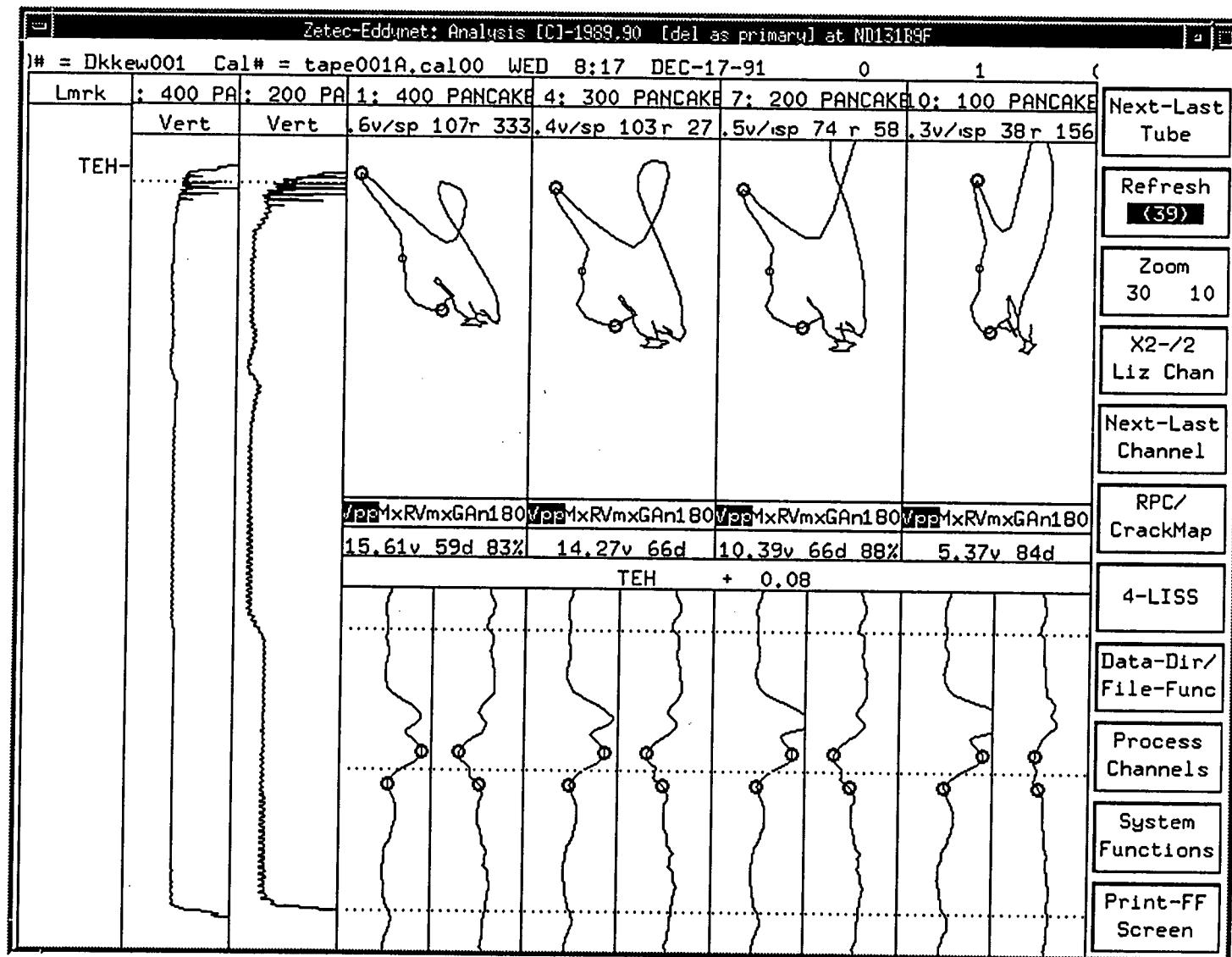


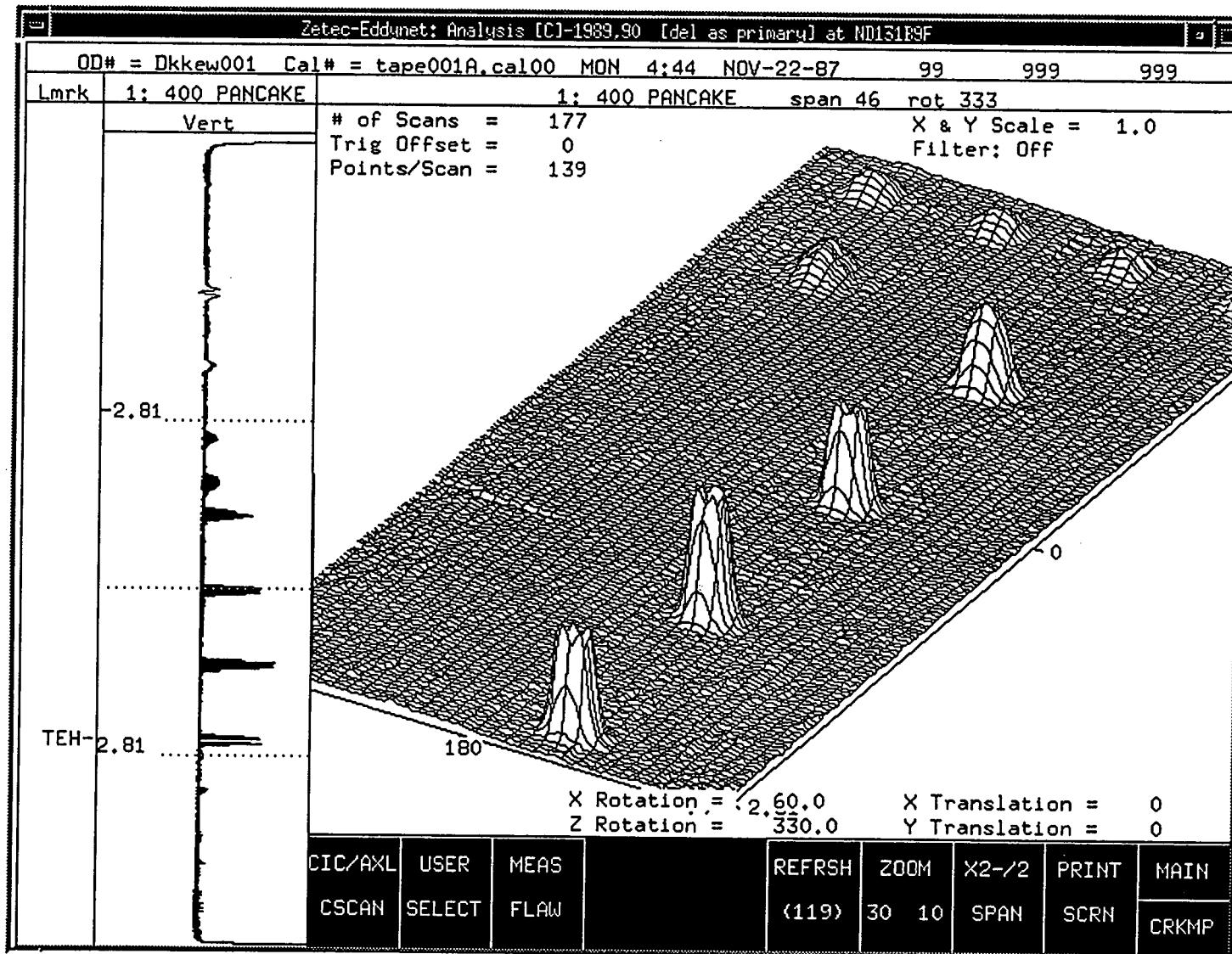


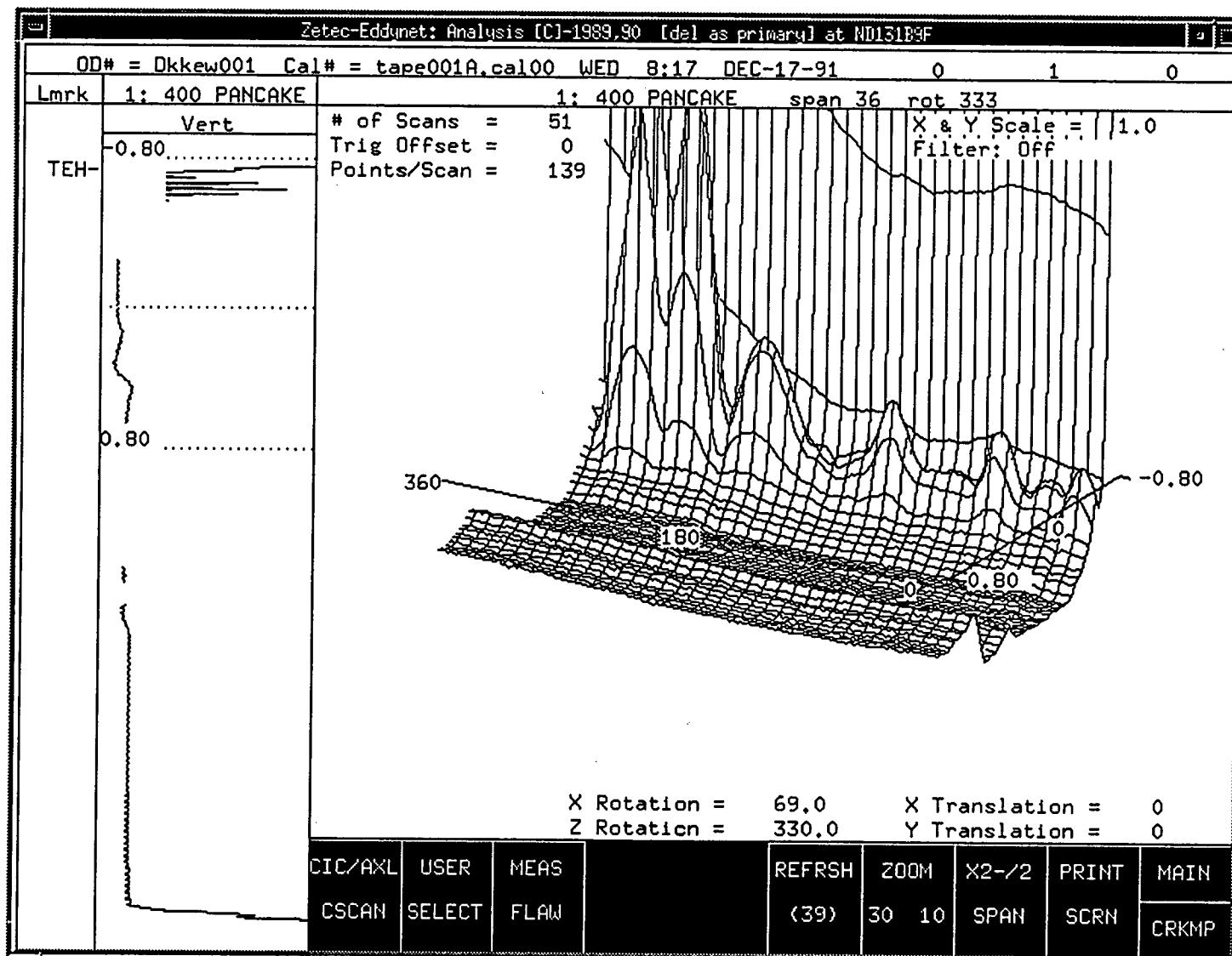


KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

SECTION 6.0A - LAB SAMPLE EDDY CURRENT GRAPHICS
EXPANDED WELDED SAMPLES

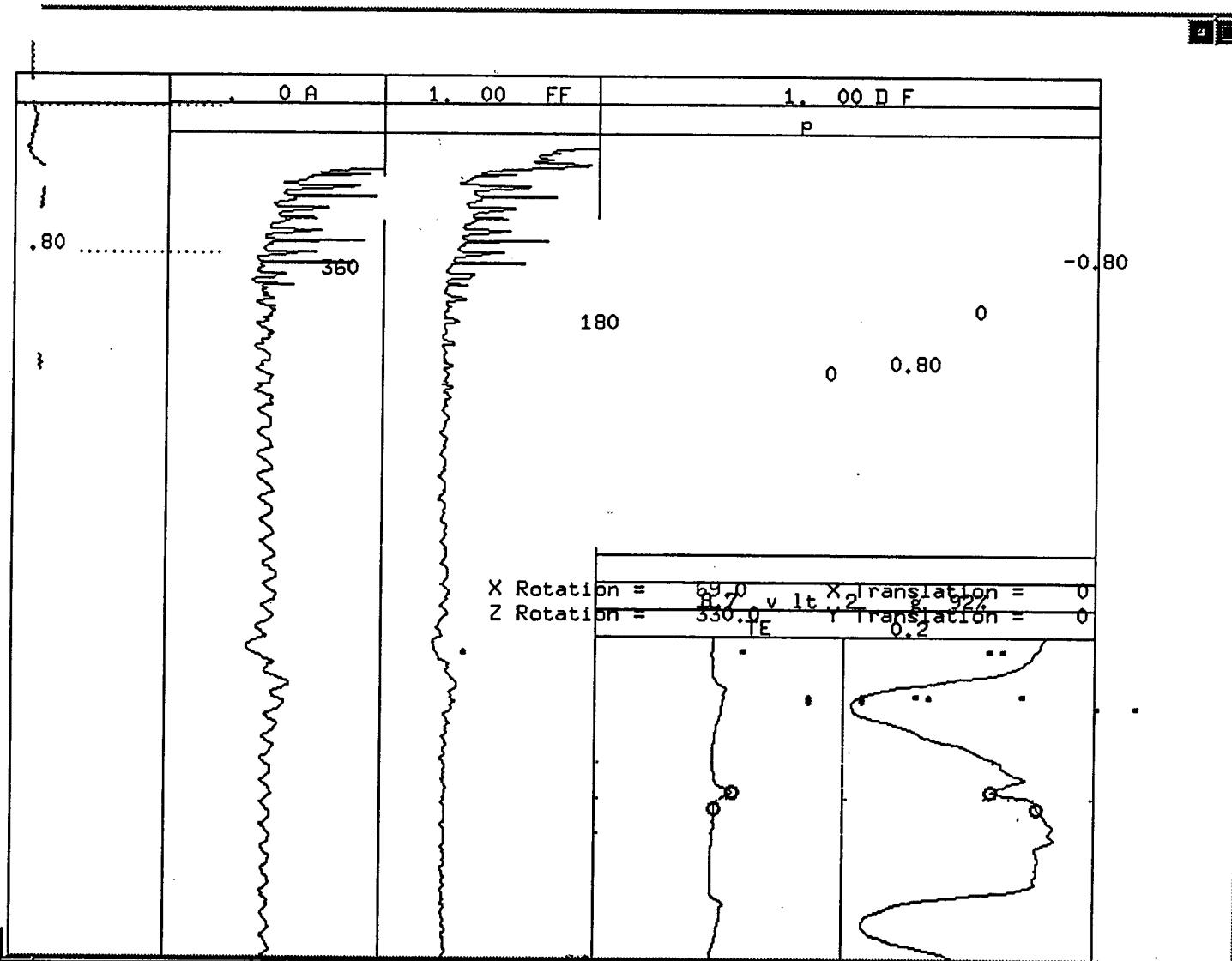


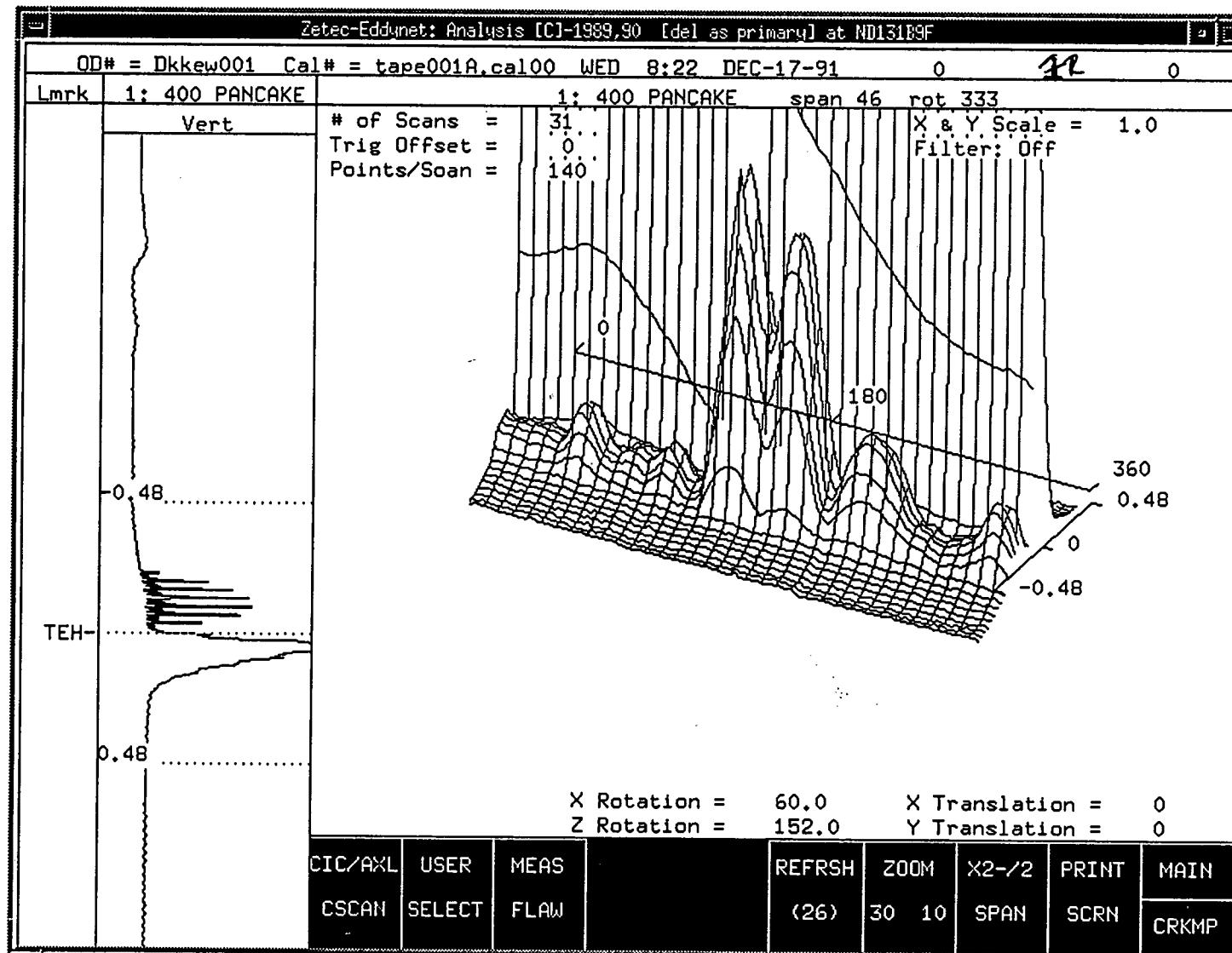


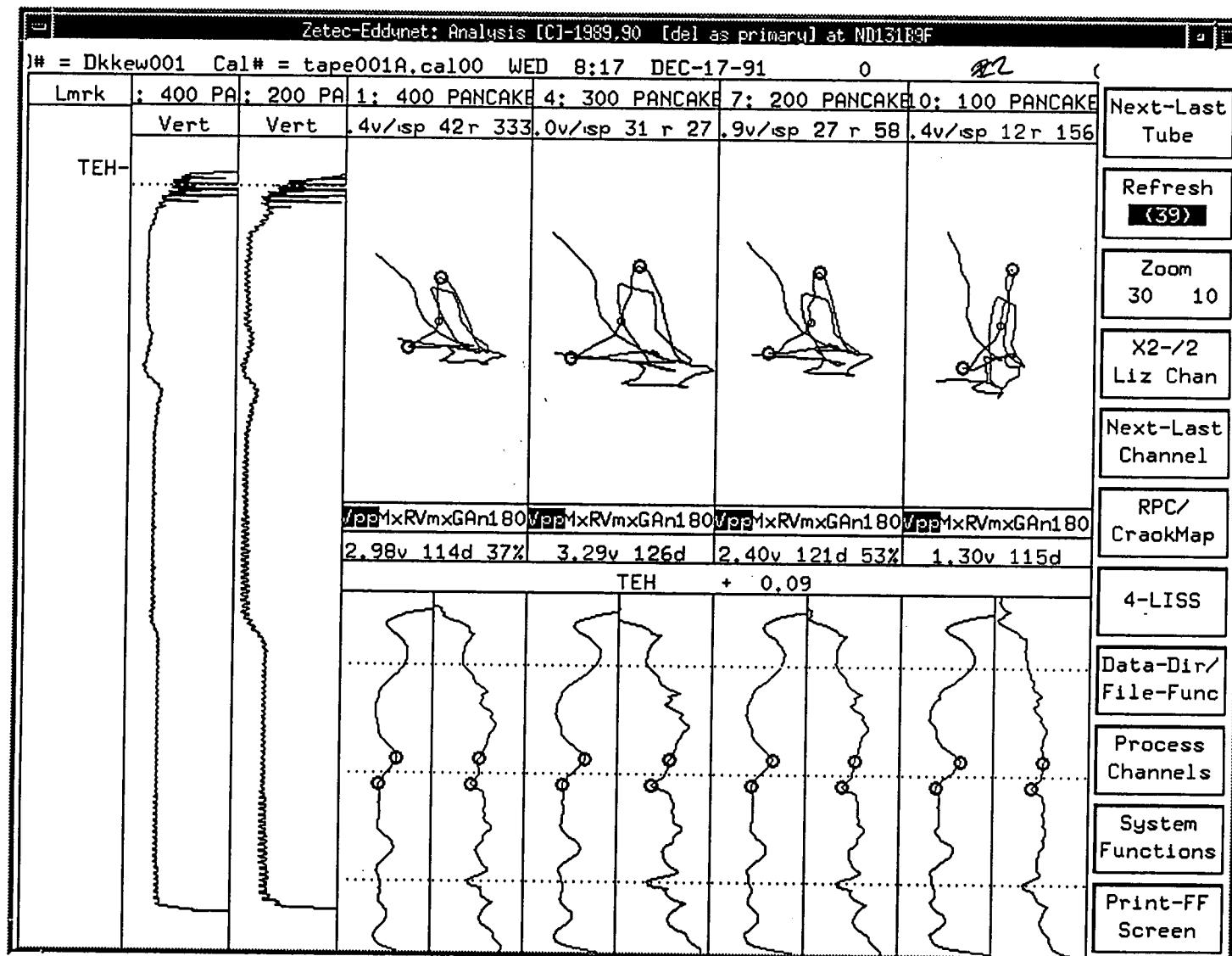


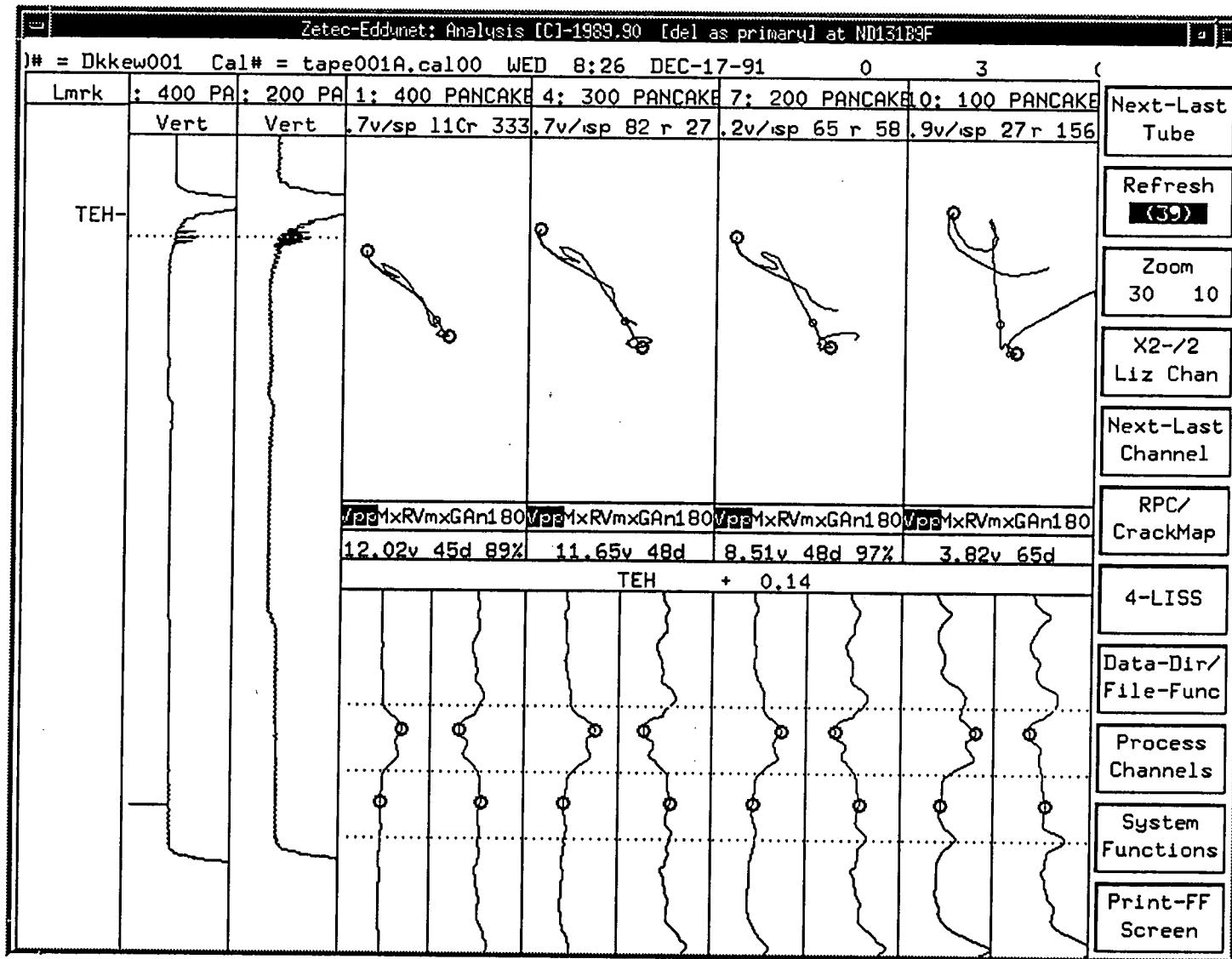
Zetec-EddyNet: Analysis [C]-1989,90 [del as primary] at ND131BSF

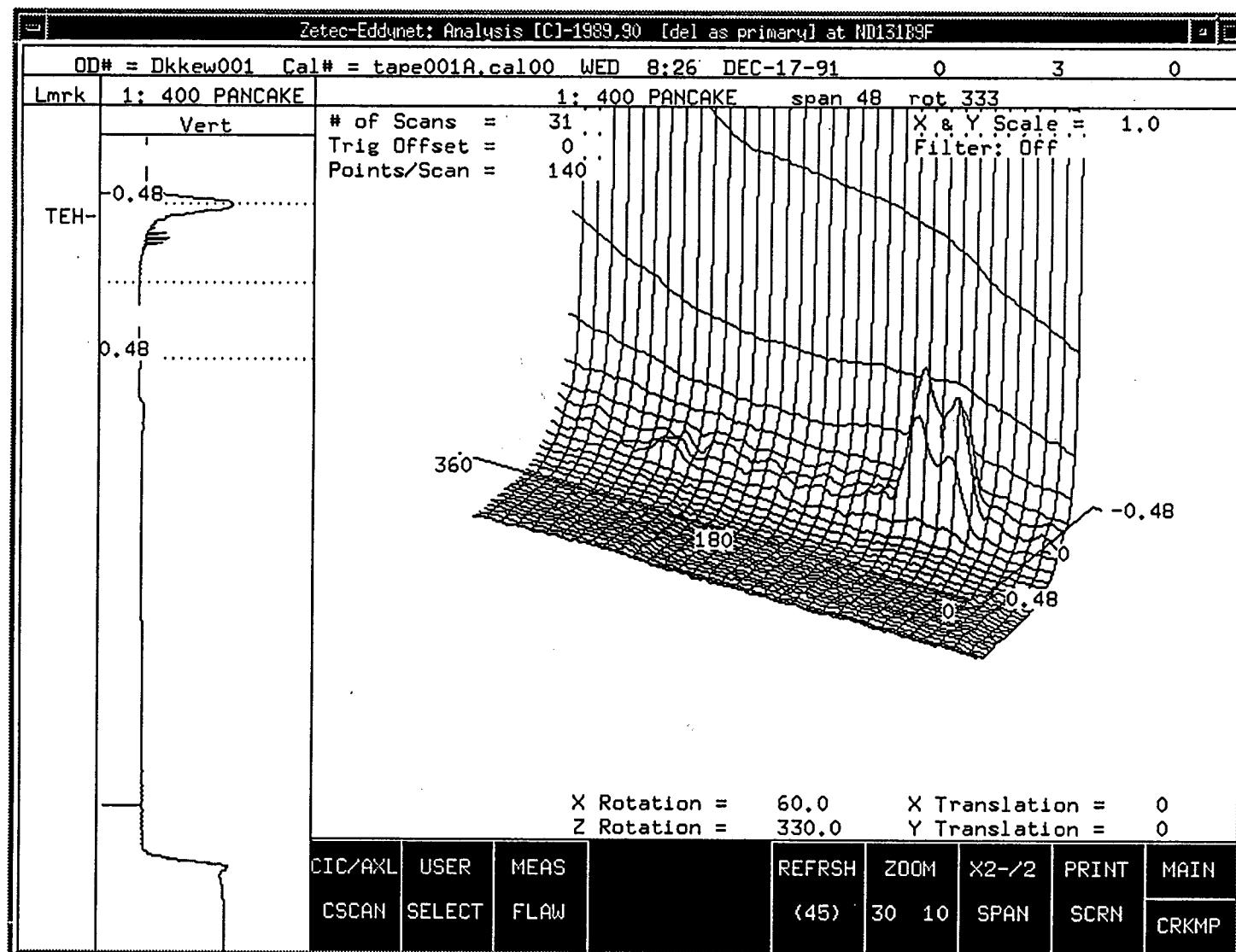
D# = k w0 1 Cal# = a 1A a100 WED 8· 7 DEC-1 - 1 0 1 0
mrk · 40 PANCAK · 40 PANCAKE s n 3 r 33
Vert # of Scans = 51 X & Y Scale = 1.0
Trig Offset = 0 Filter: Off
TEH- 0.80 Points/Scan = 139

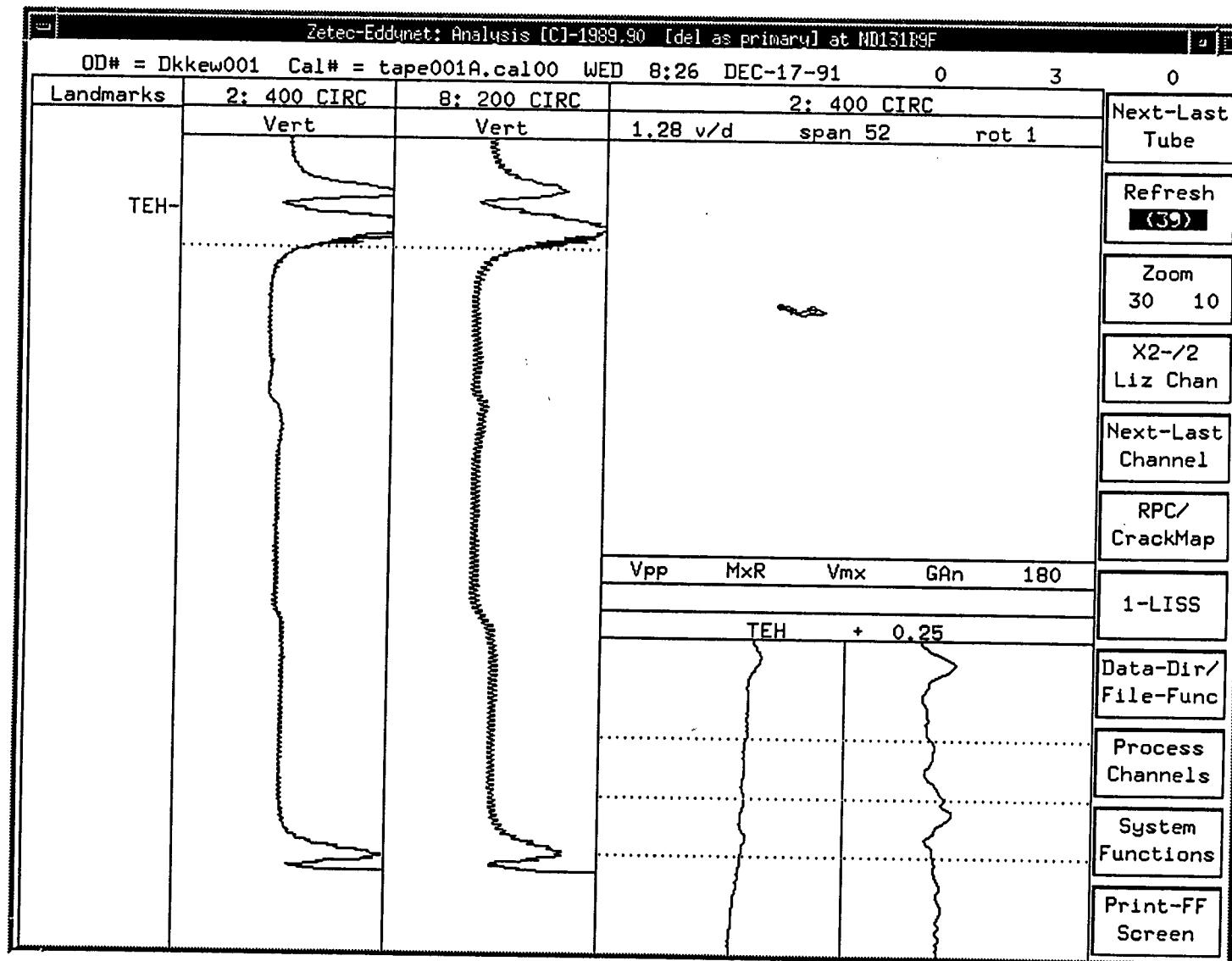


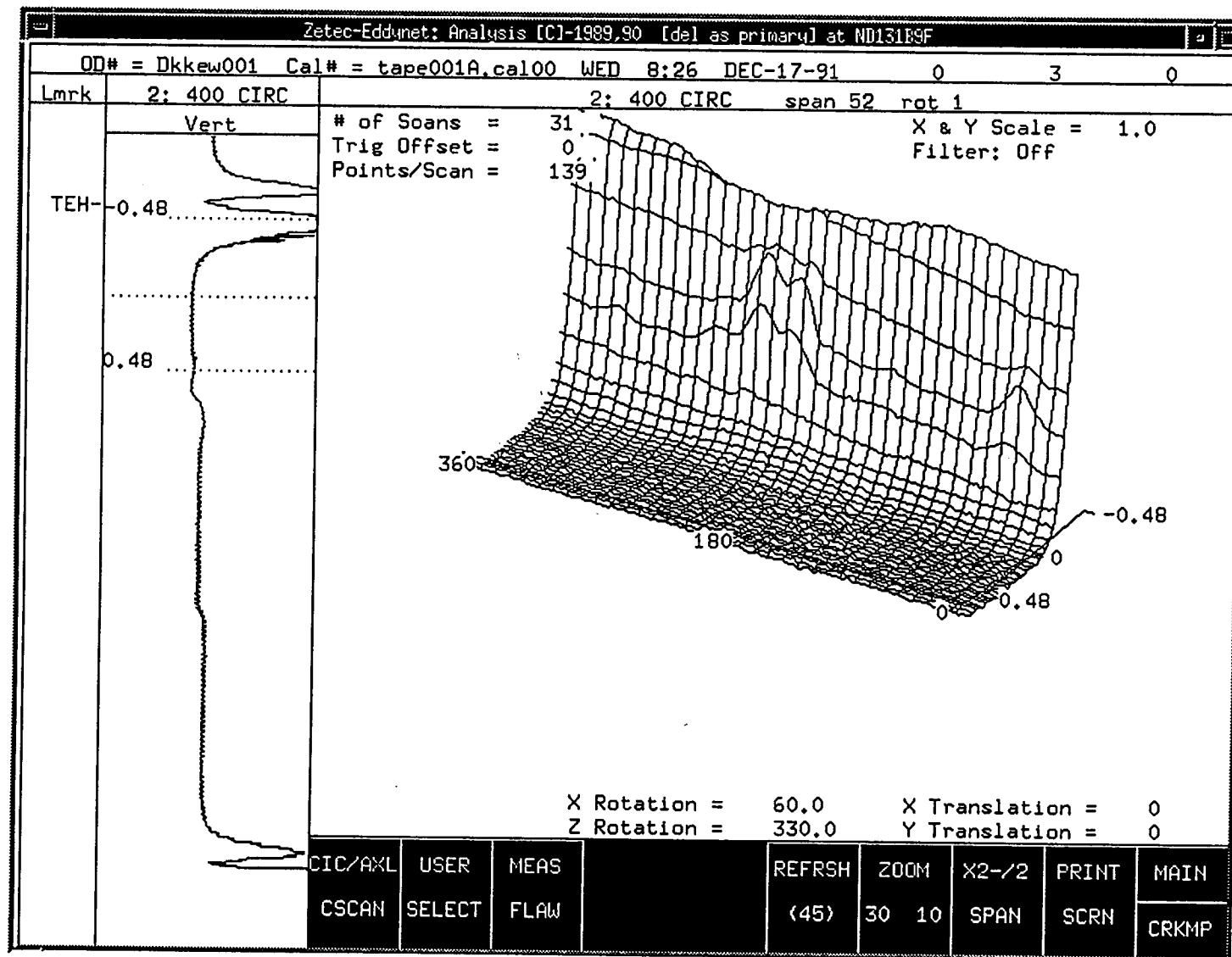


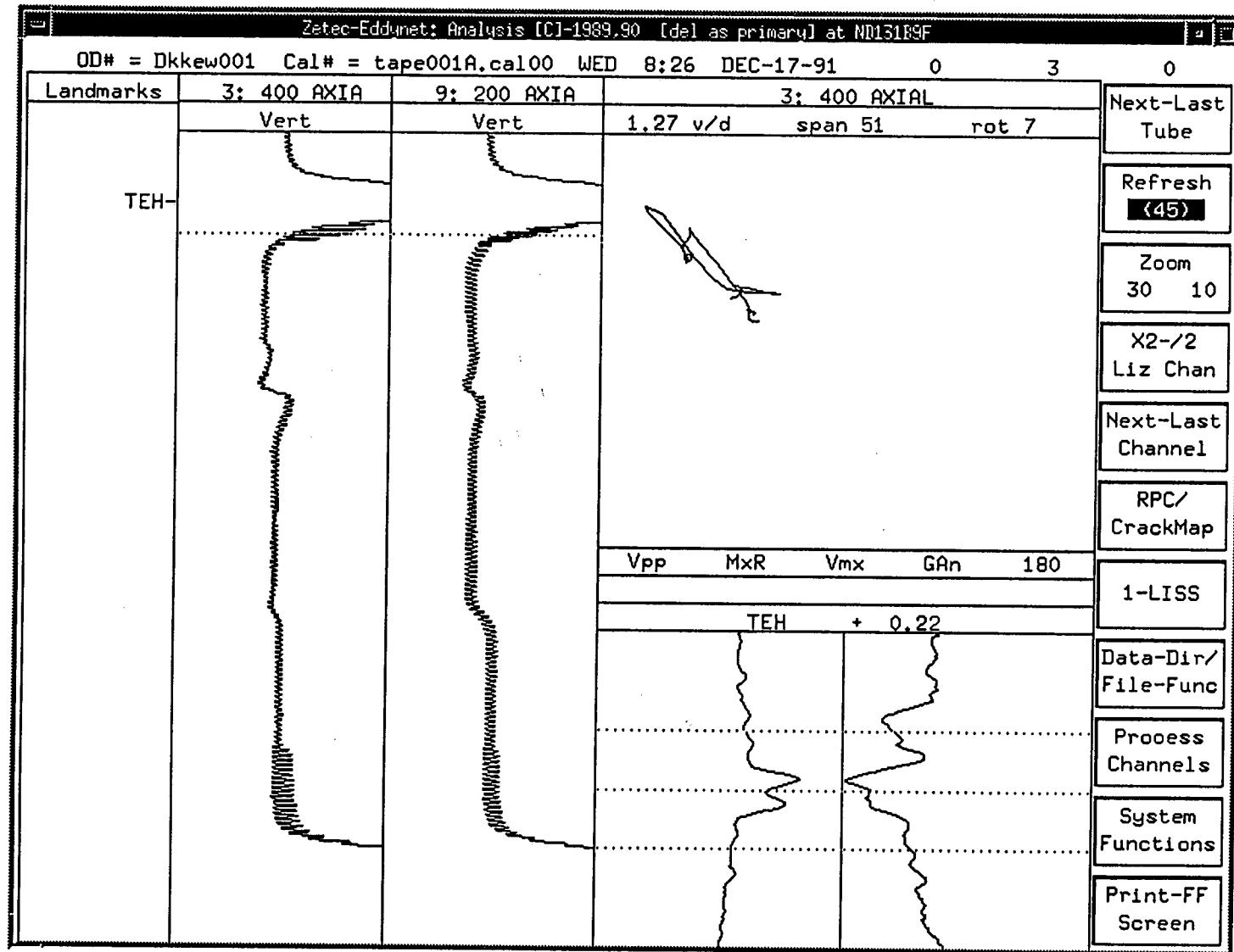


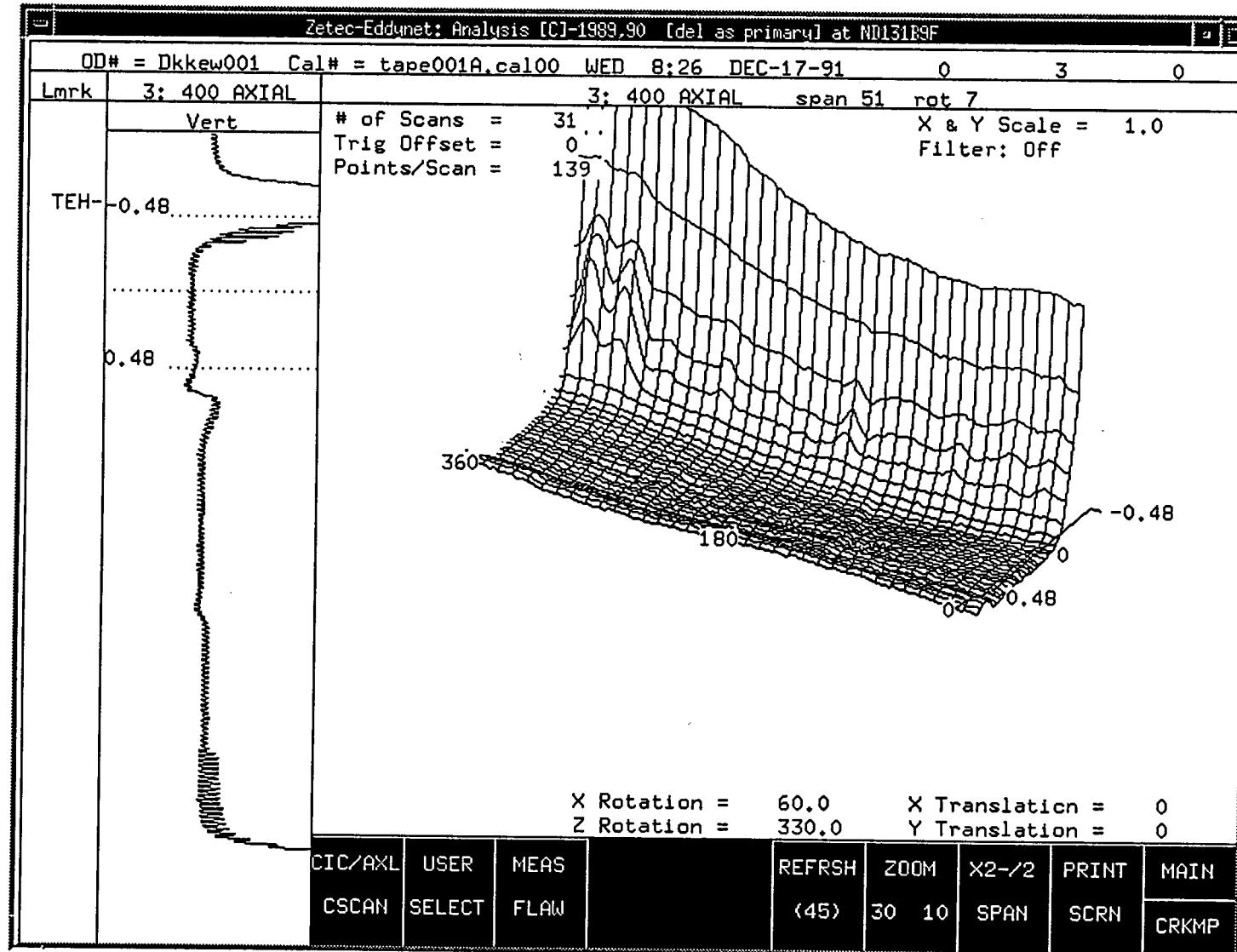


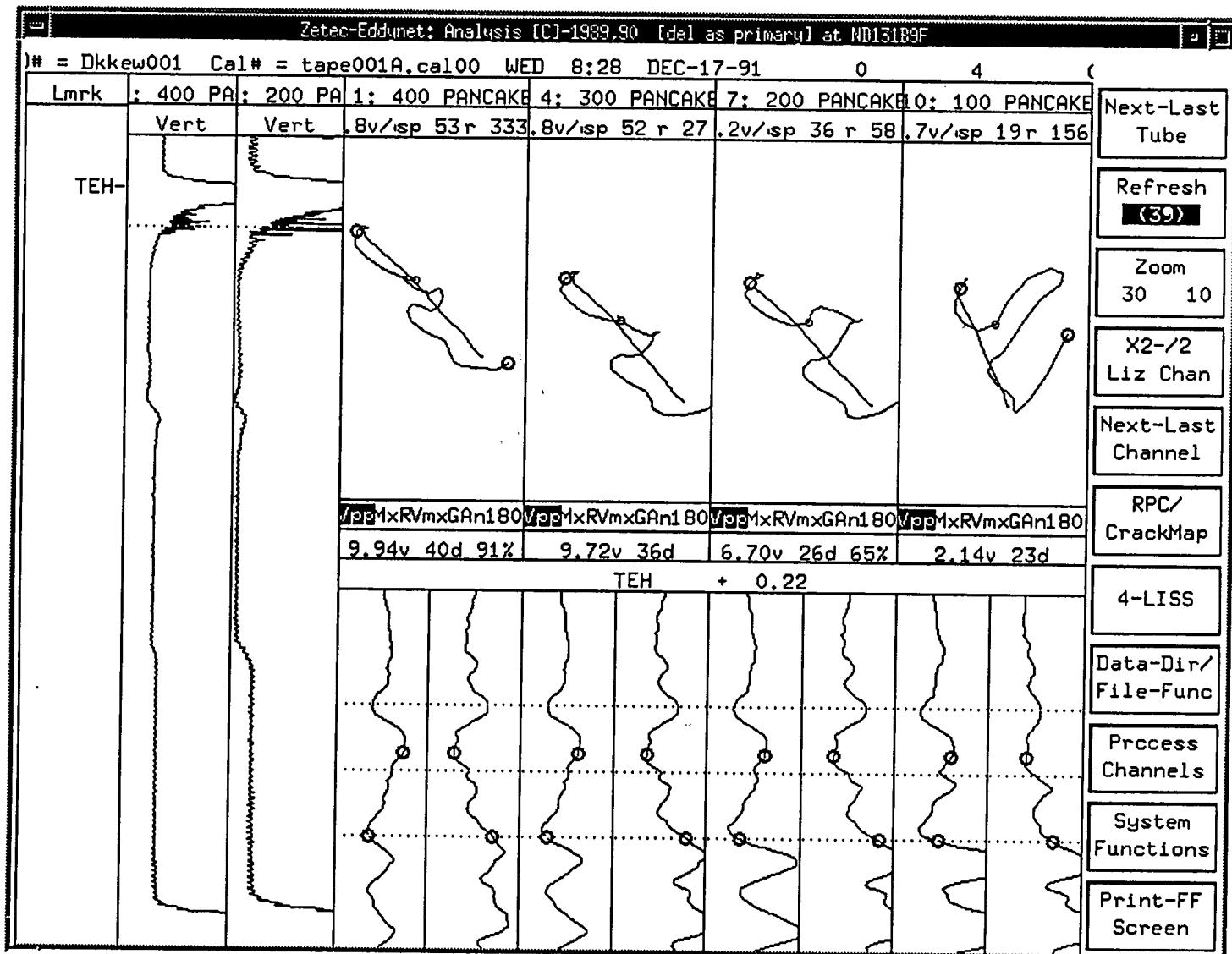


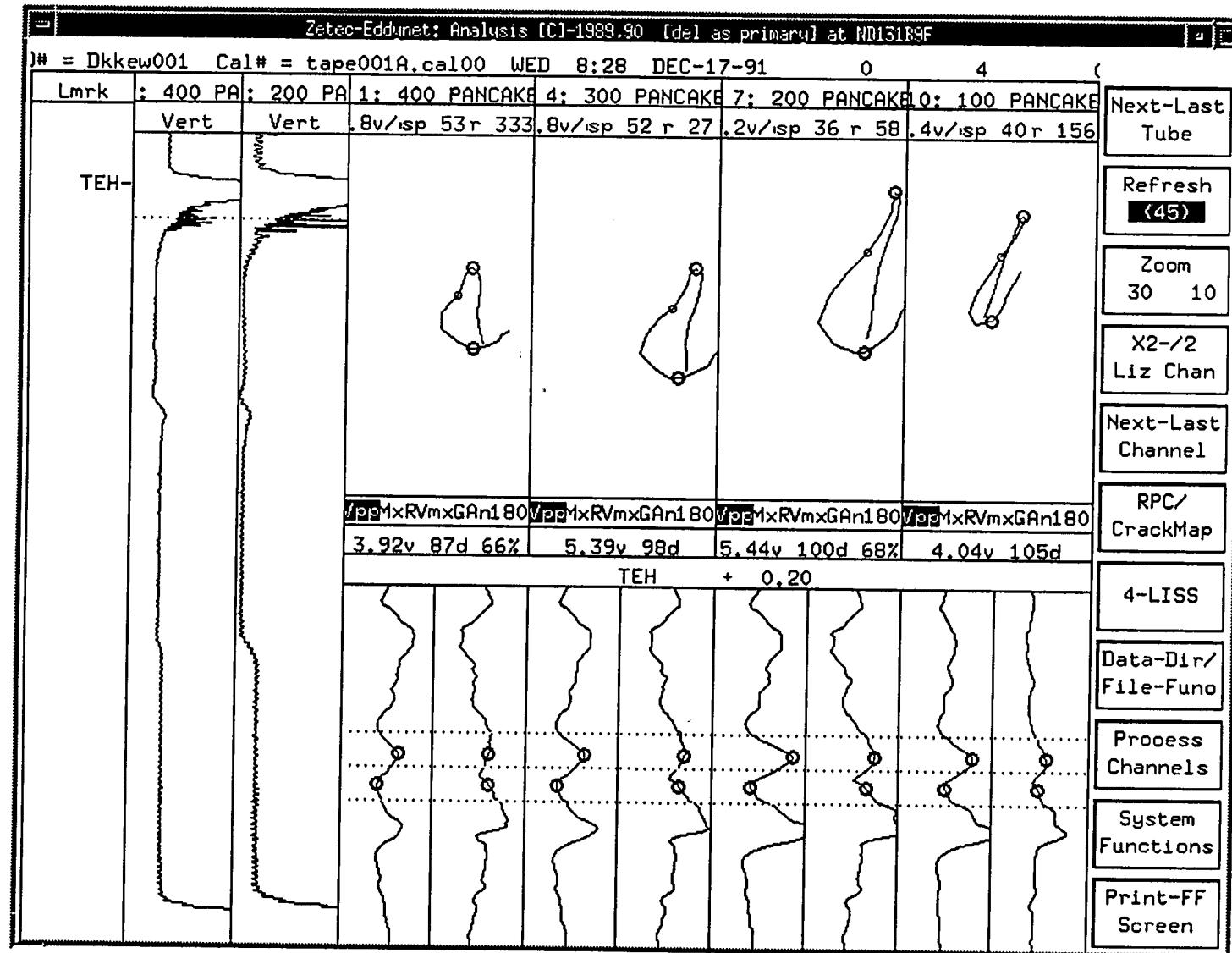


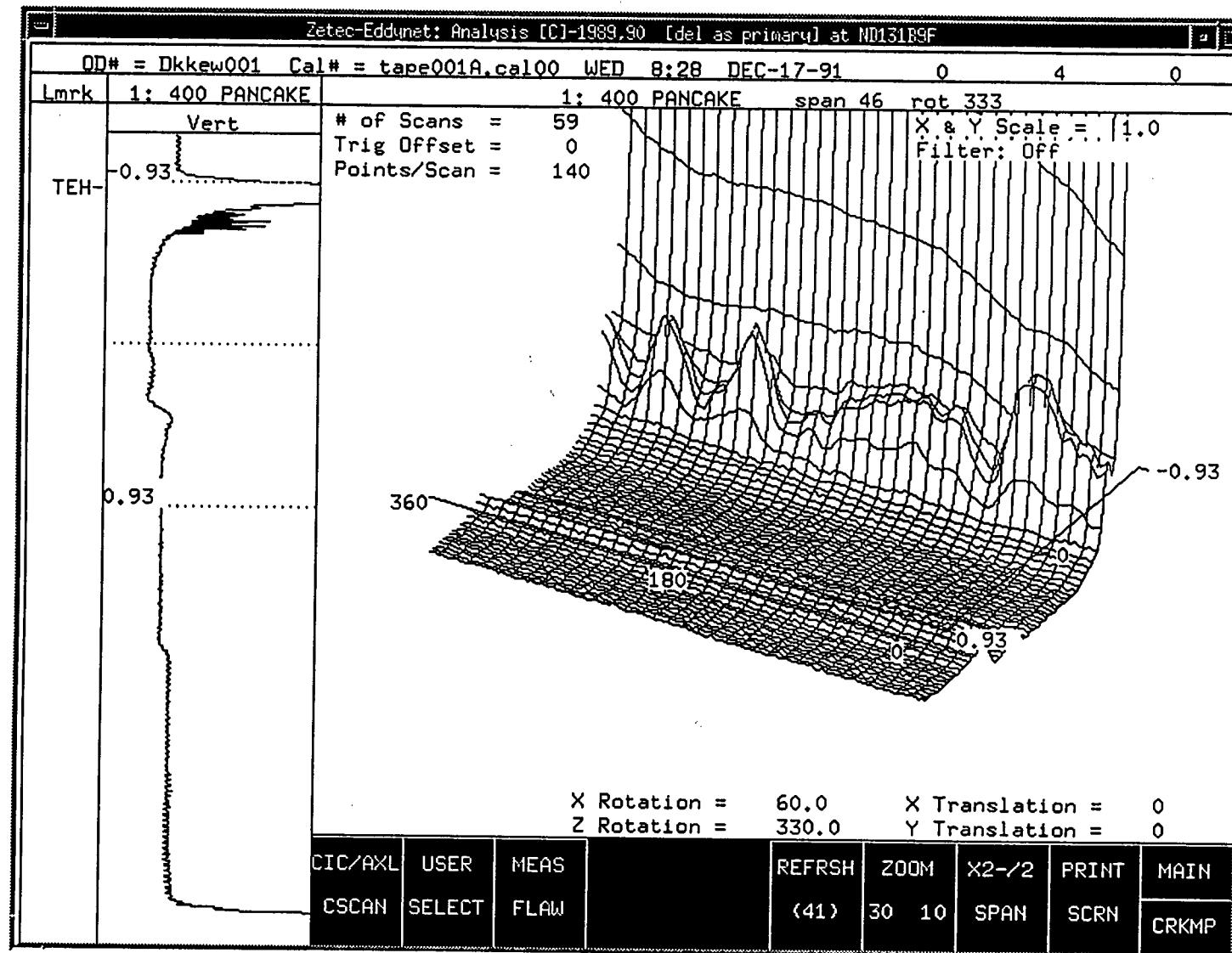


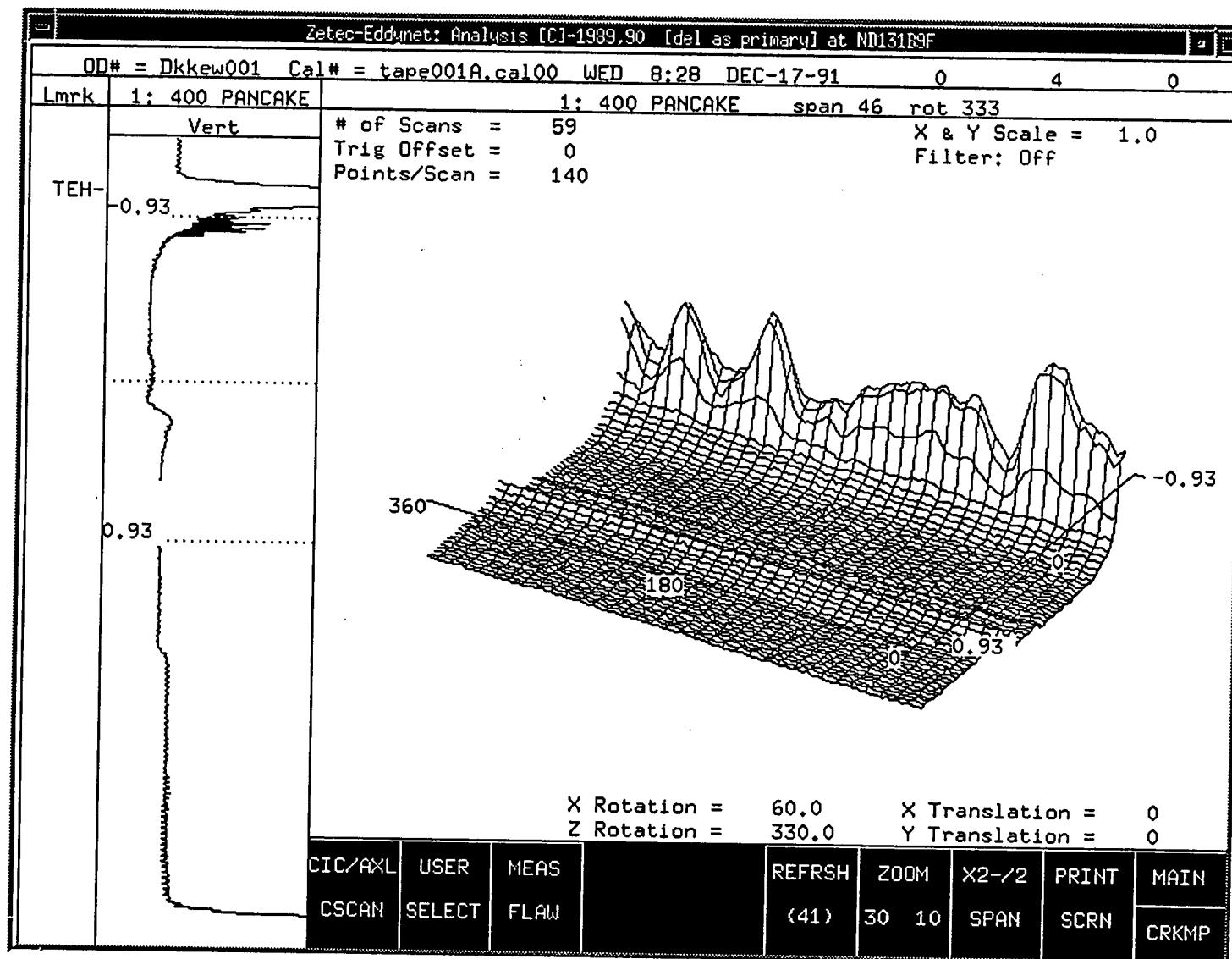


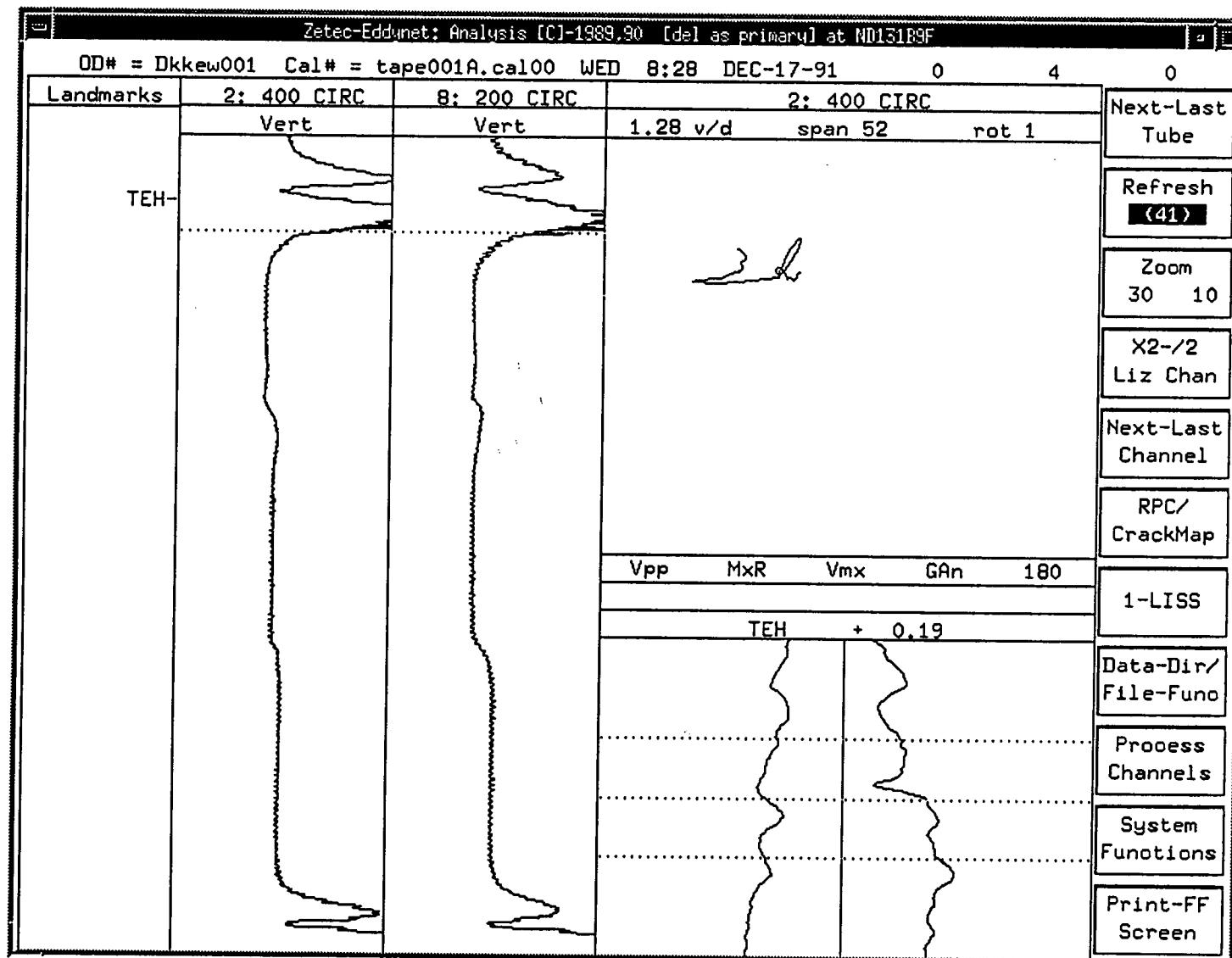


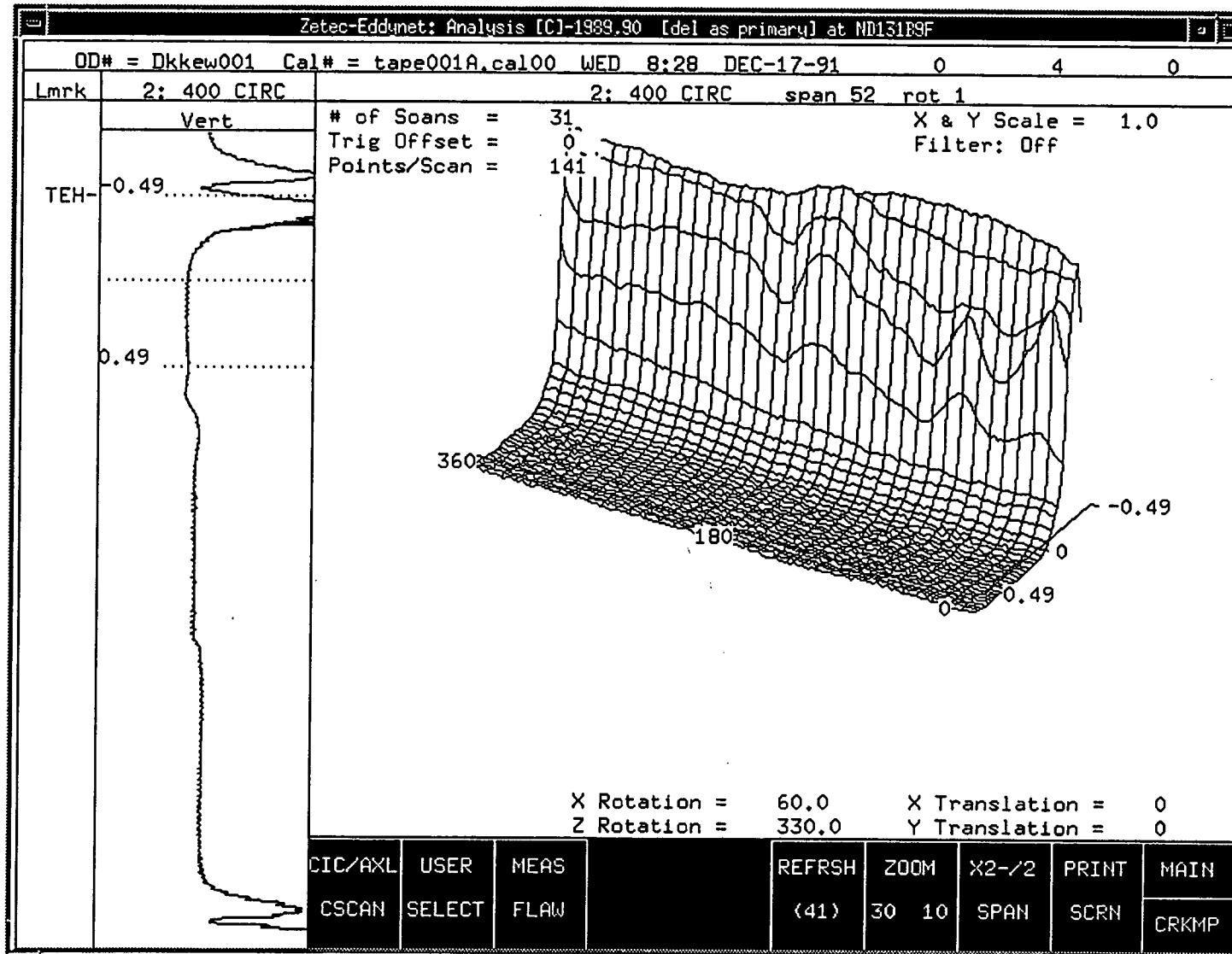


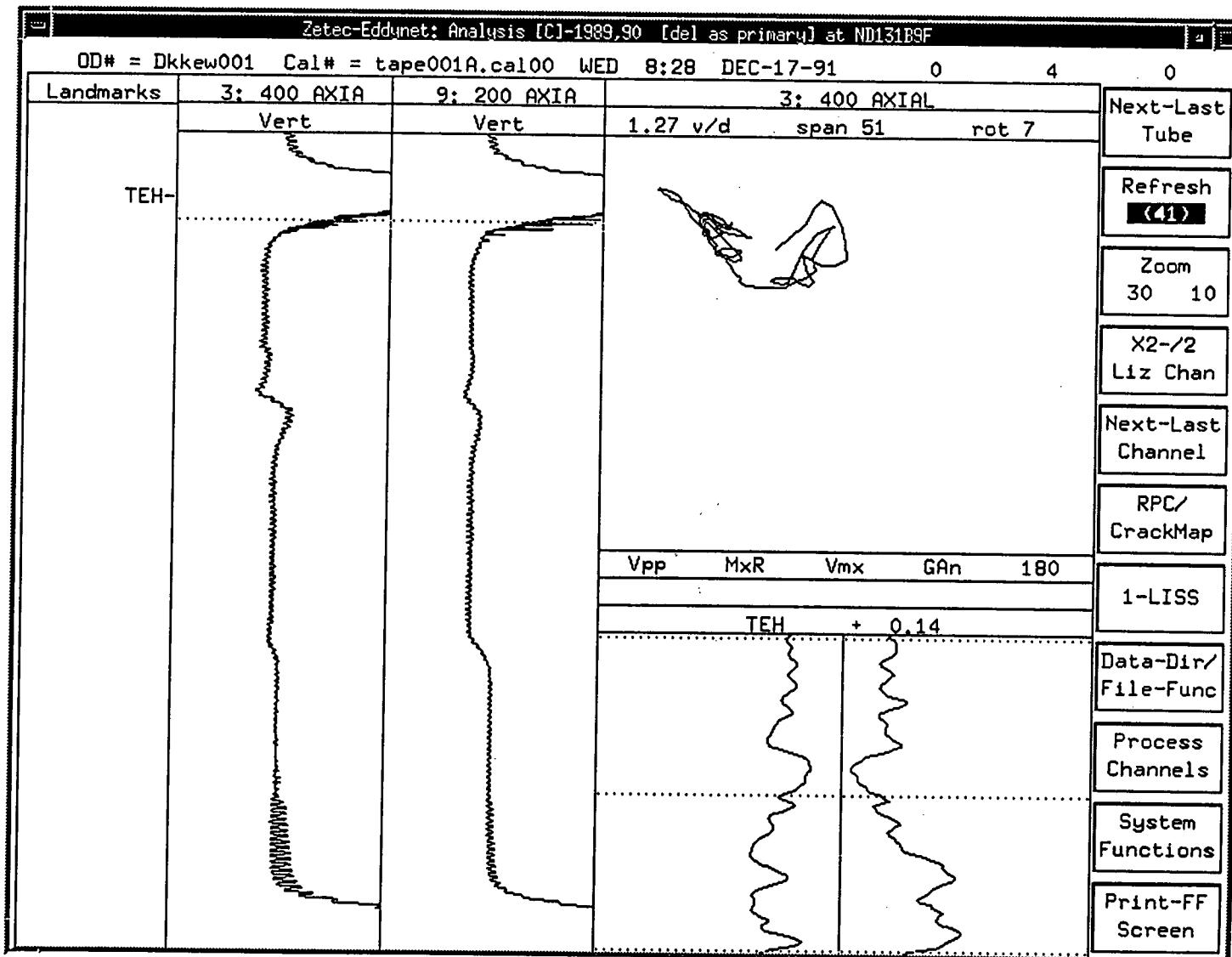


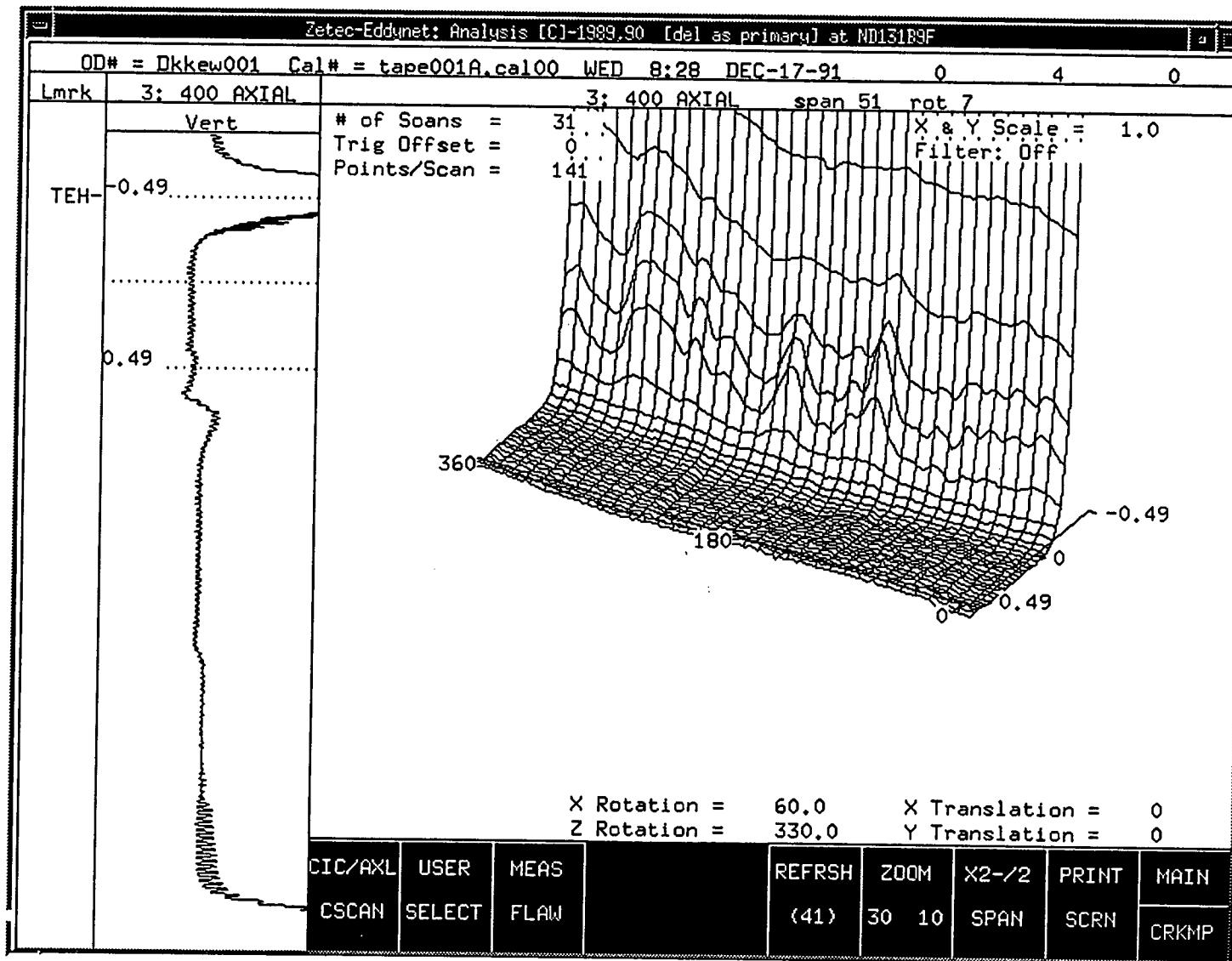


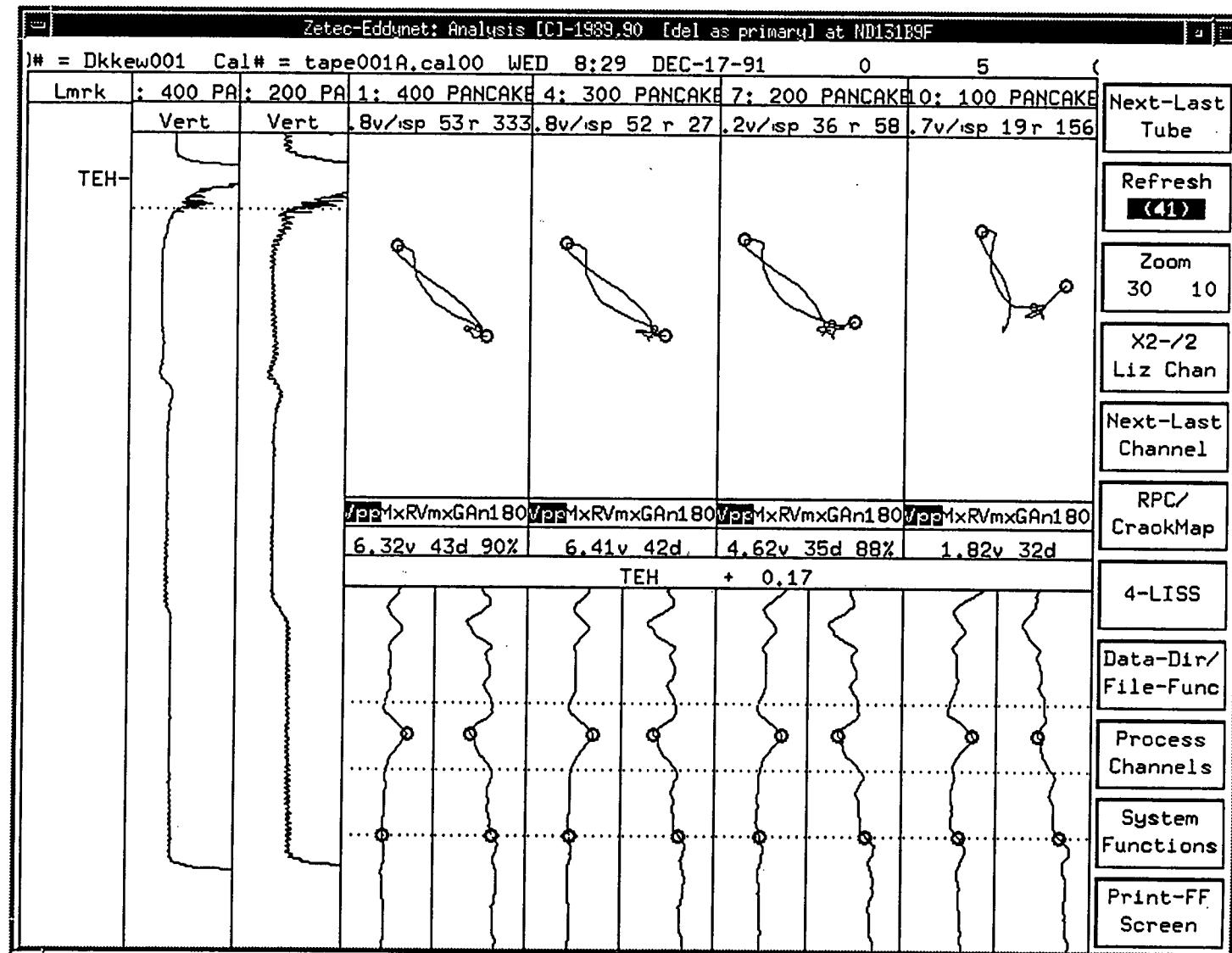


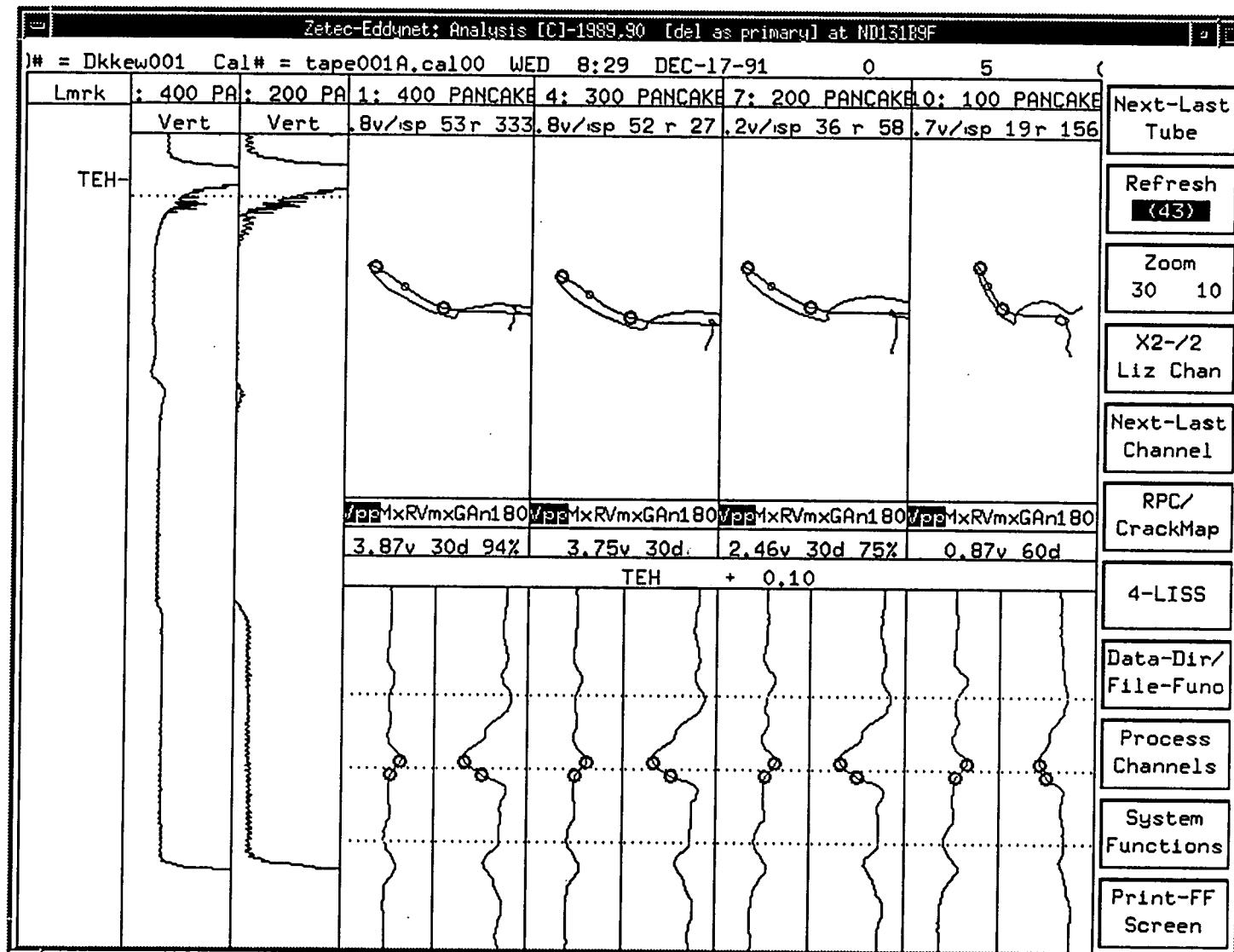


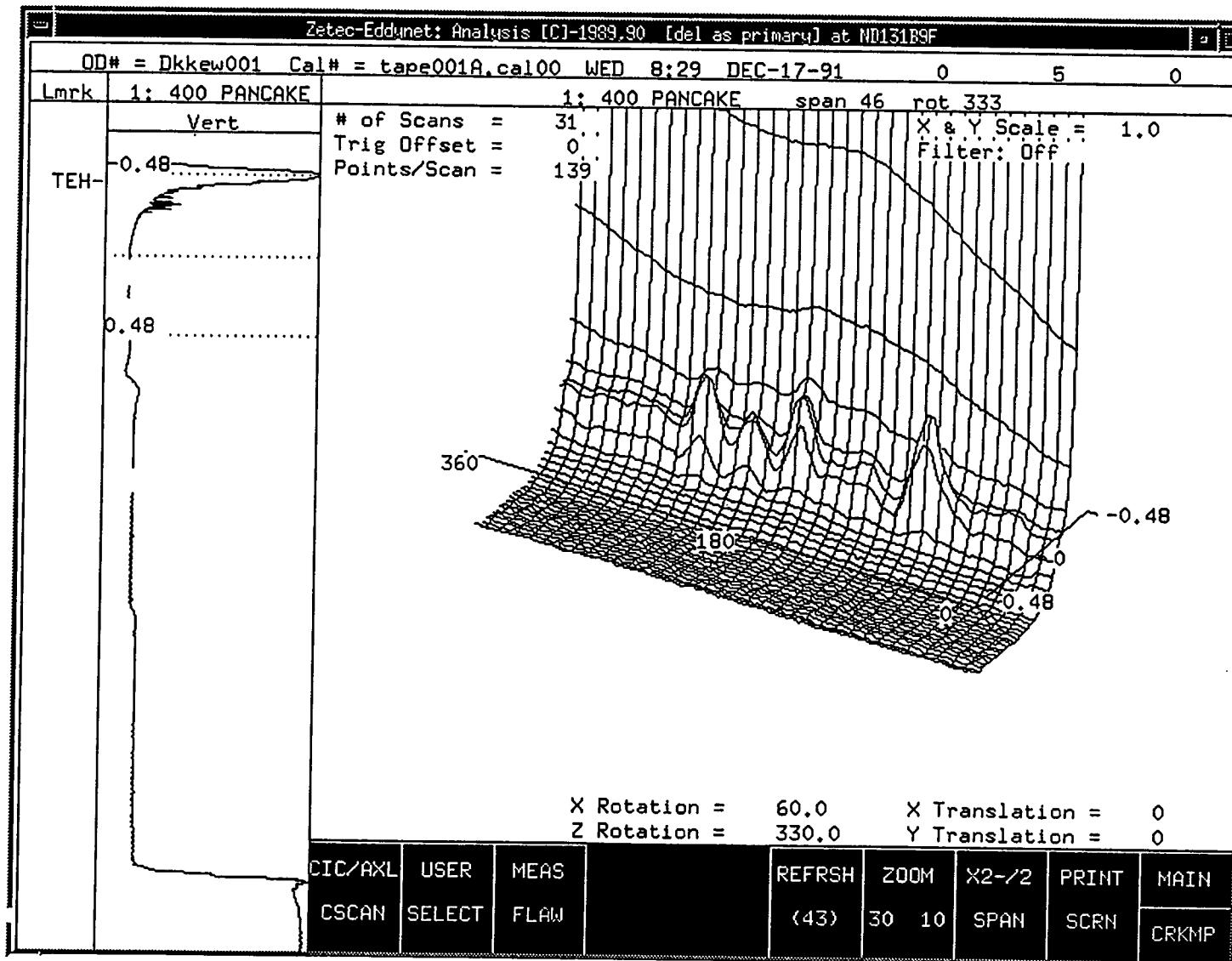


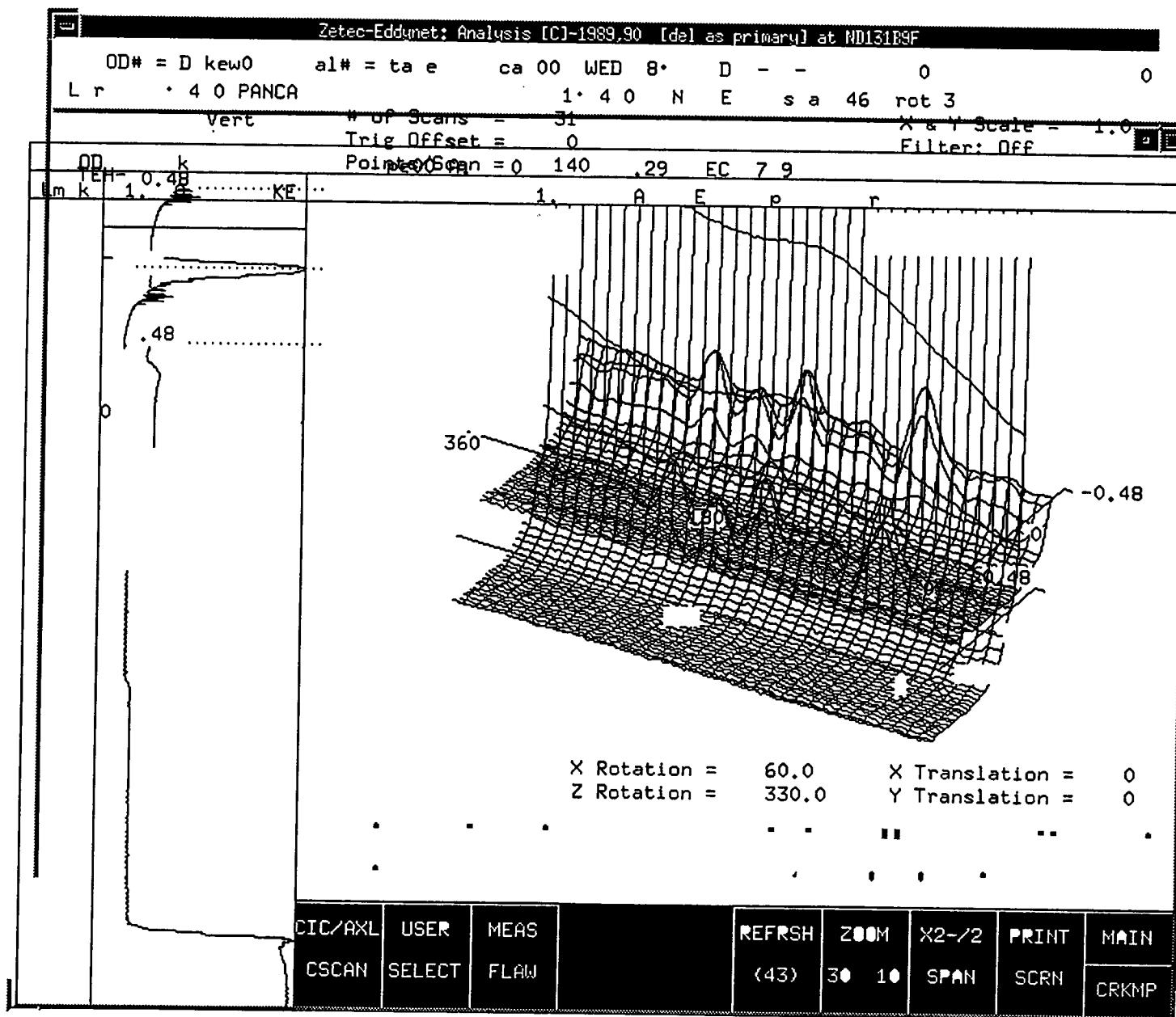


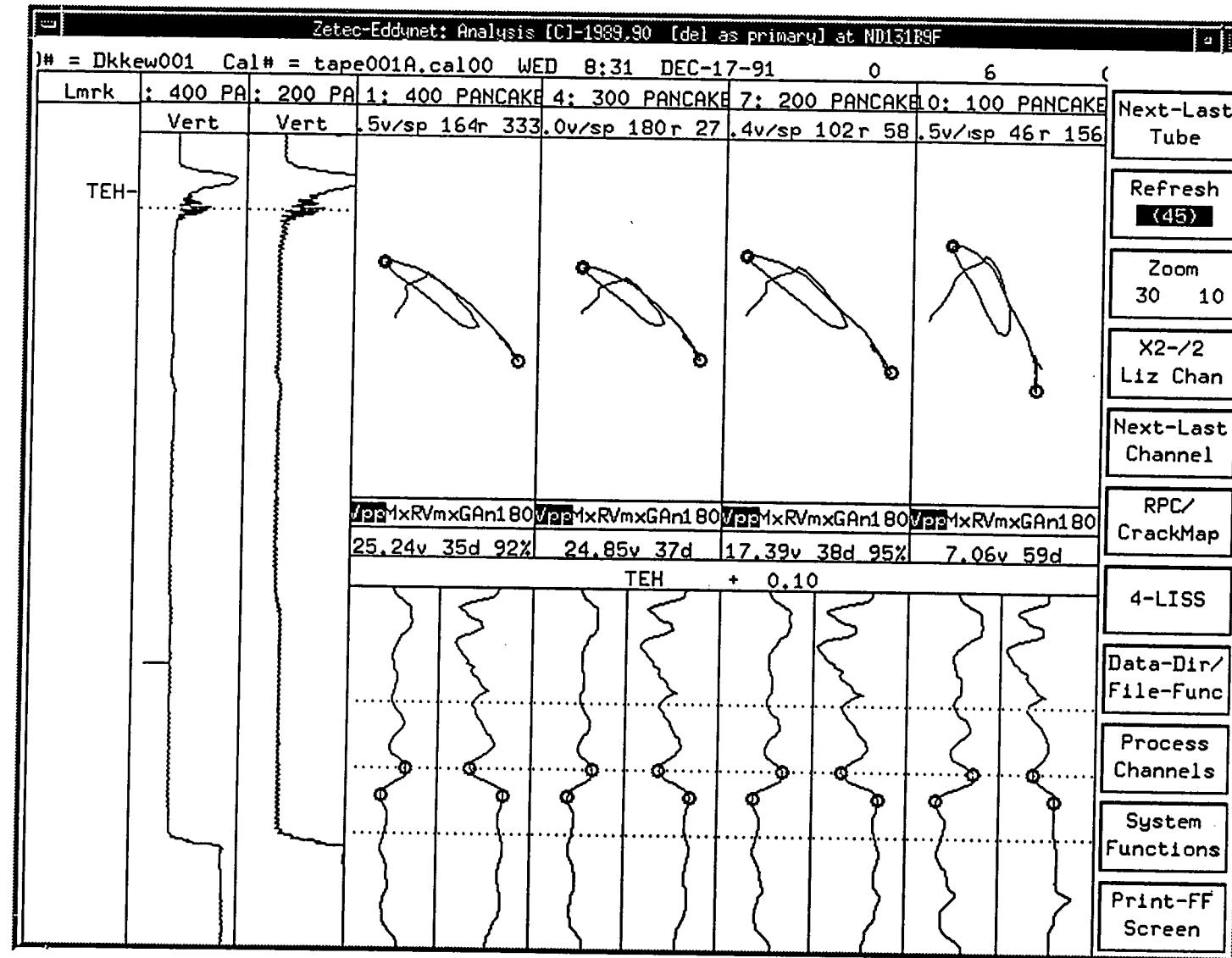


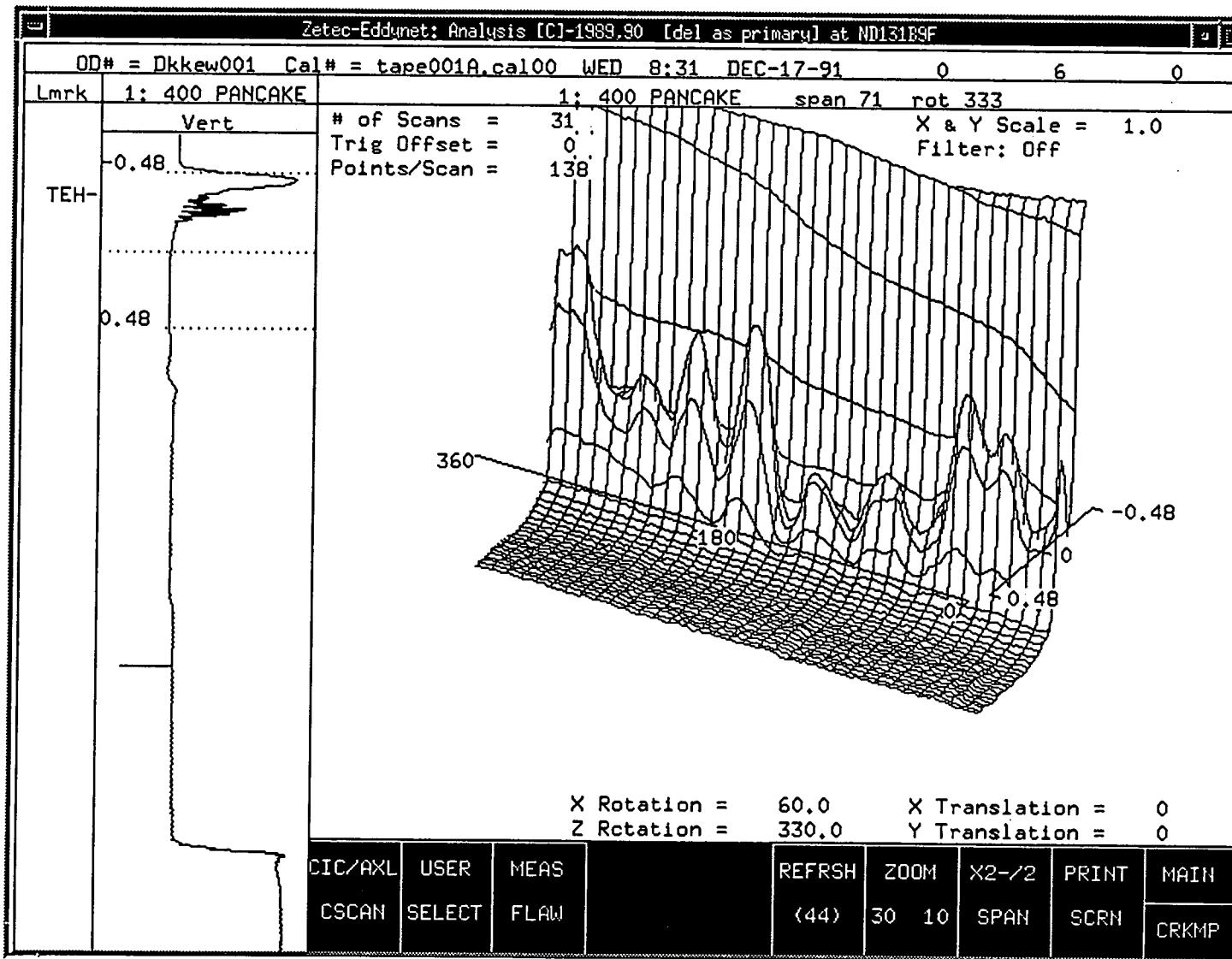


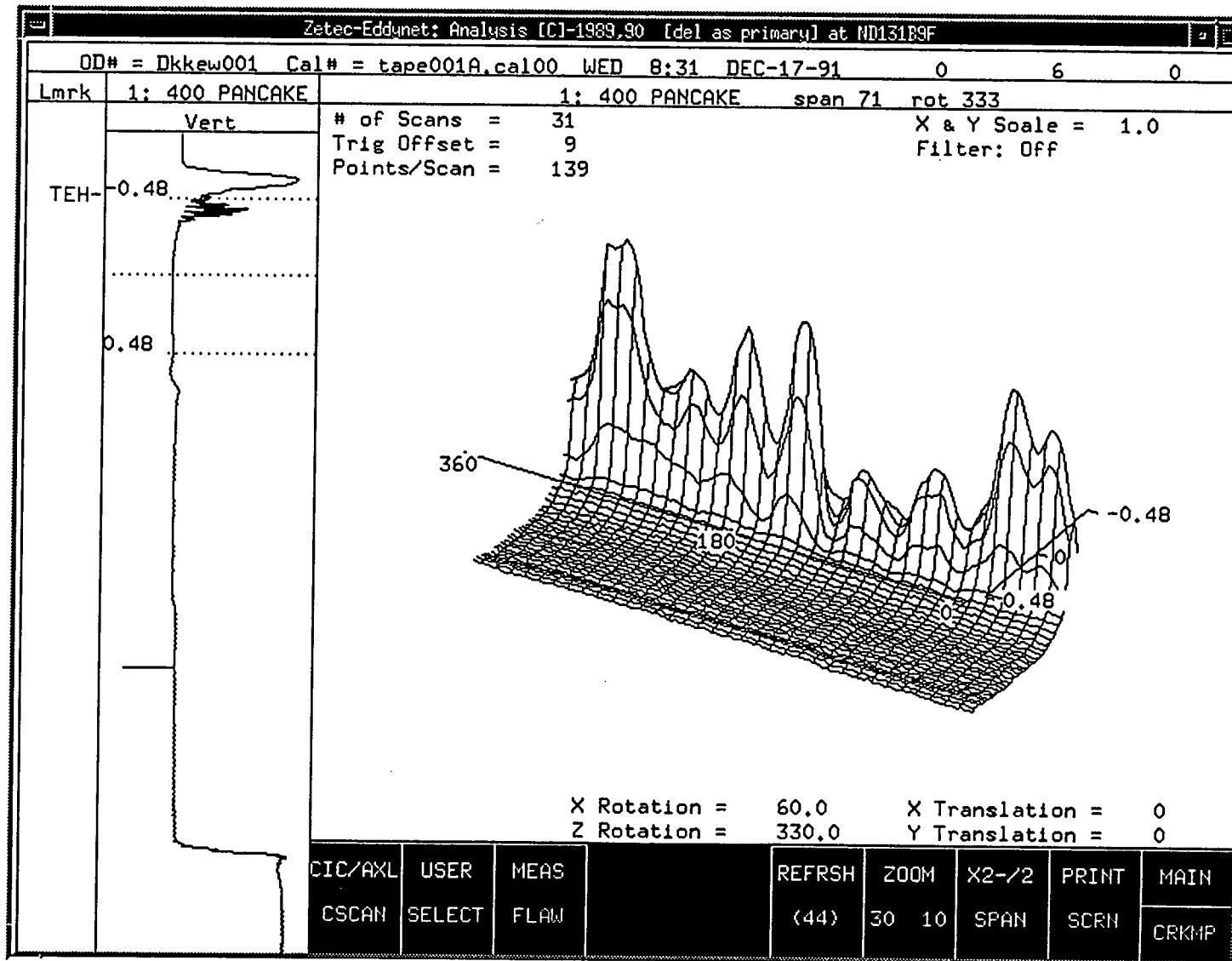


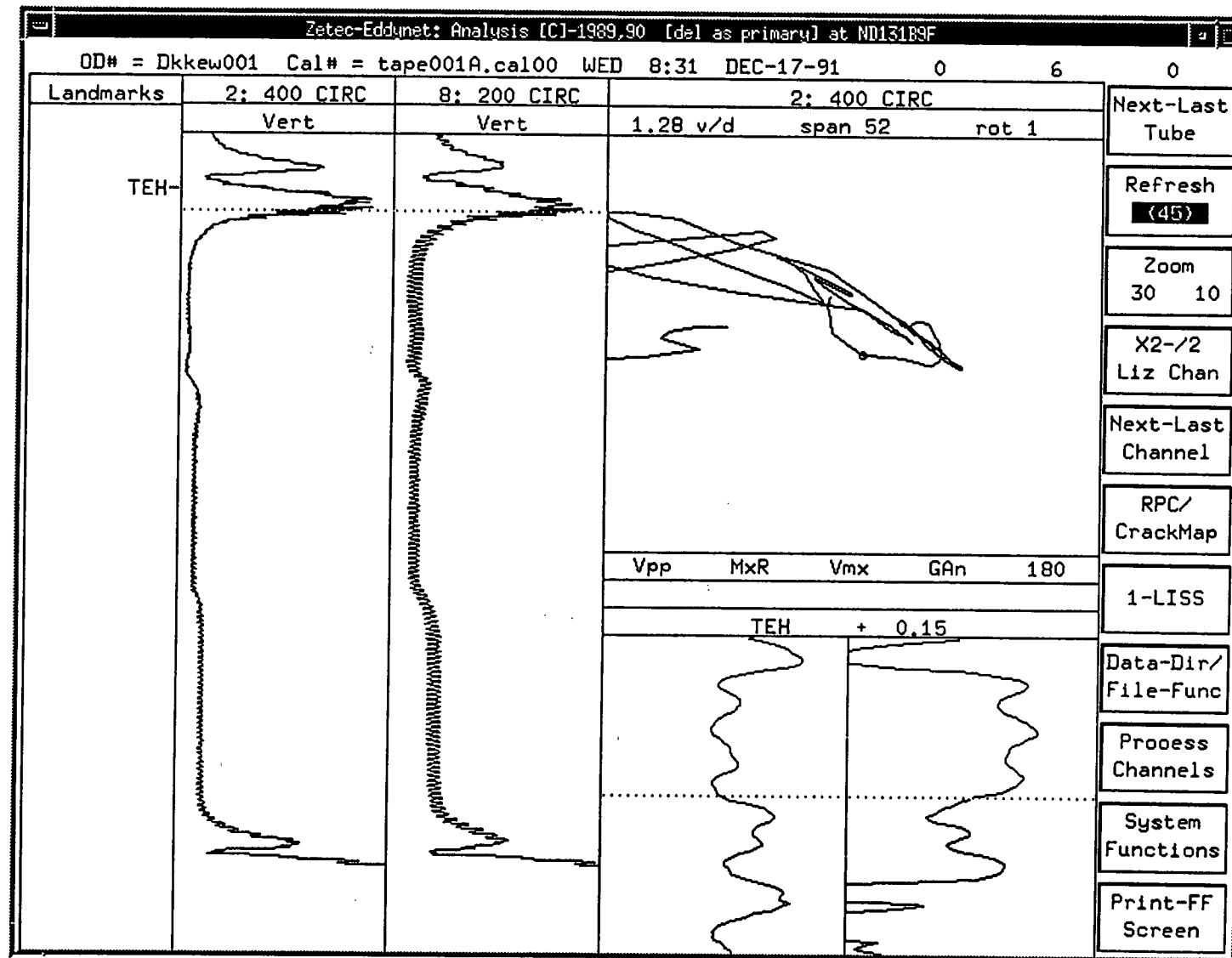


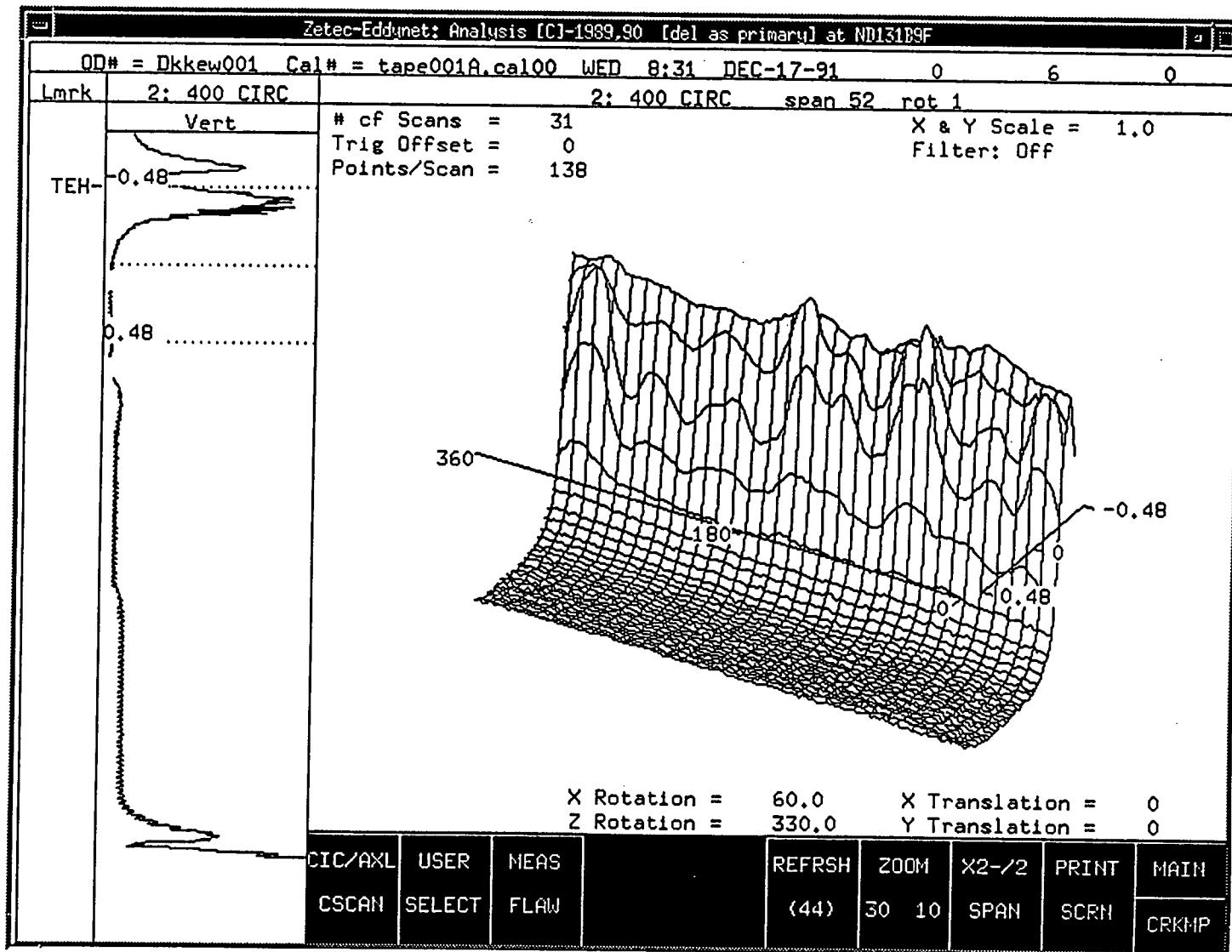


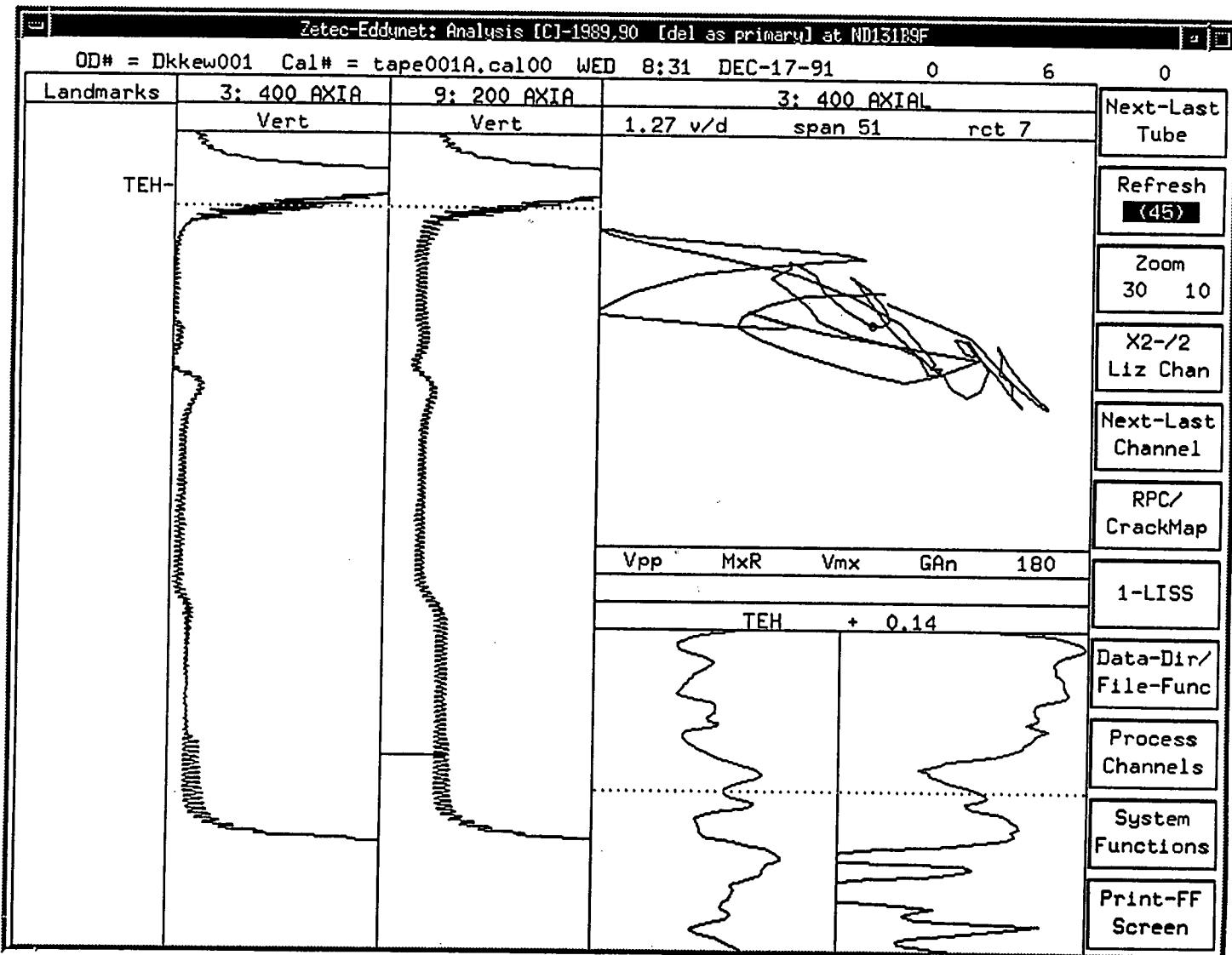


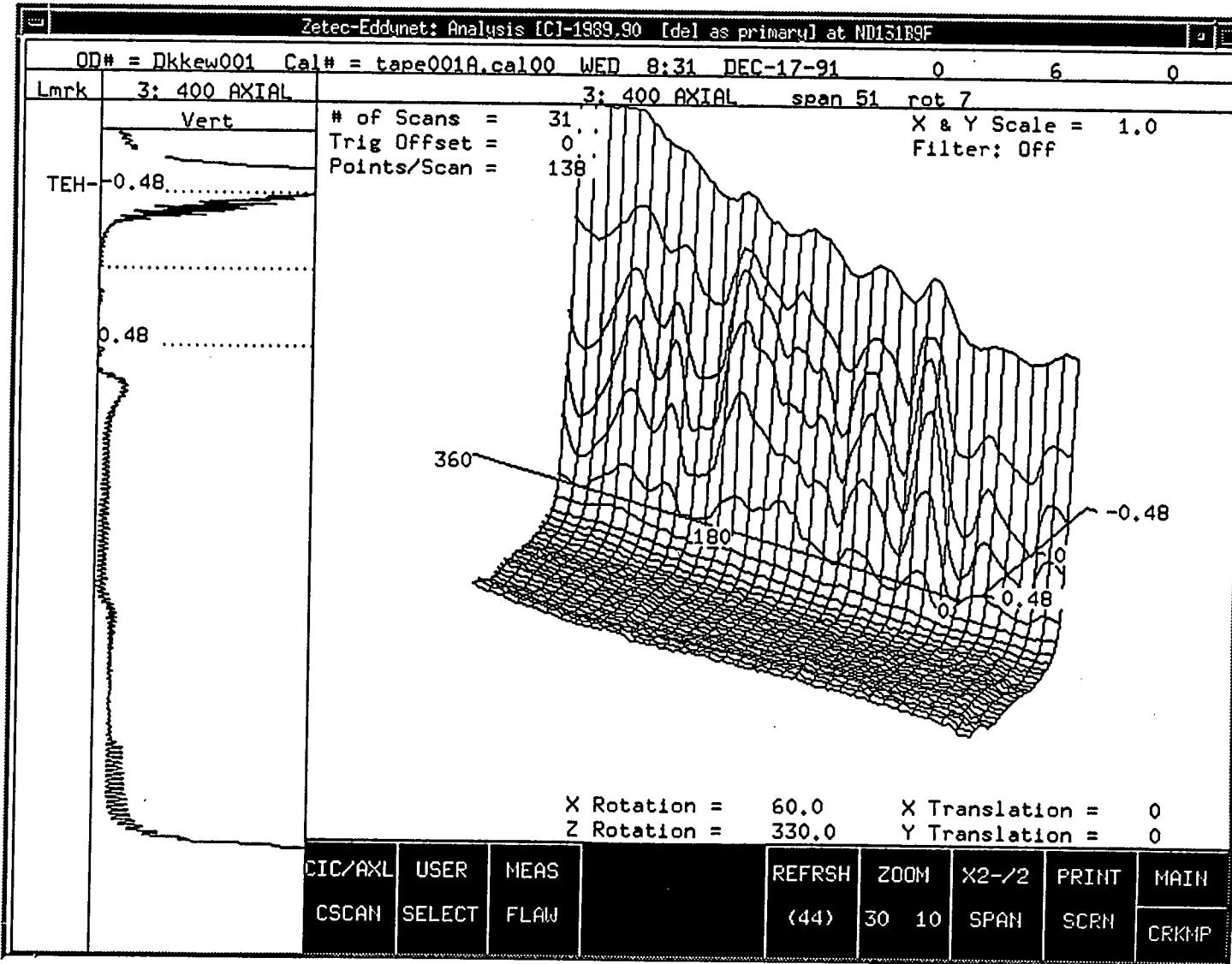


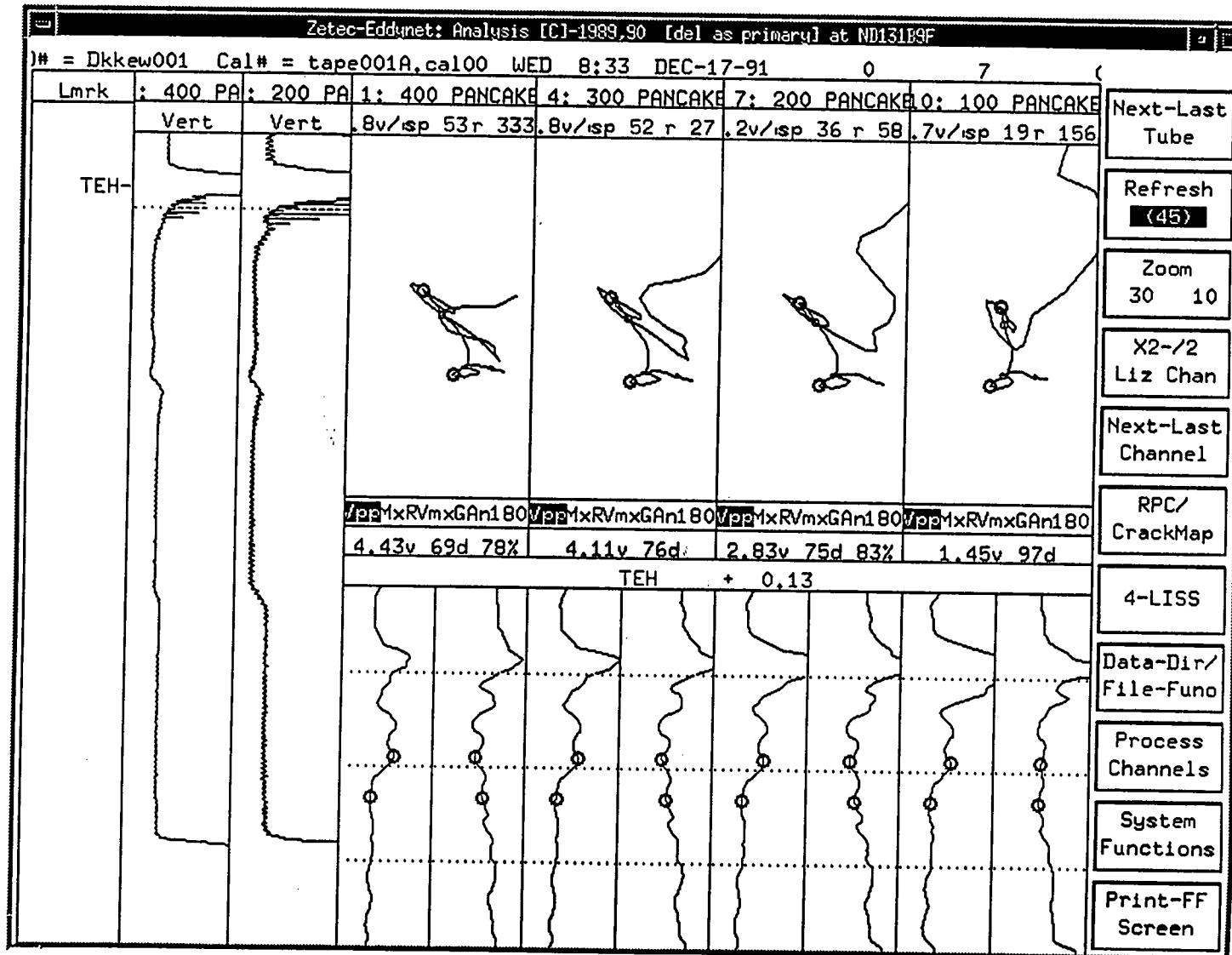








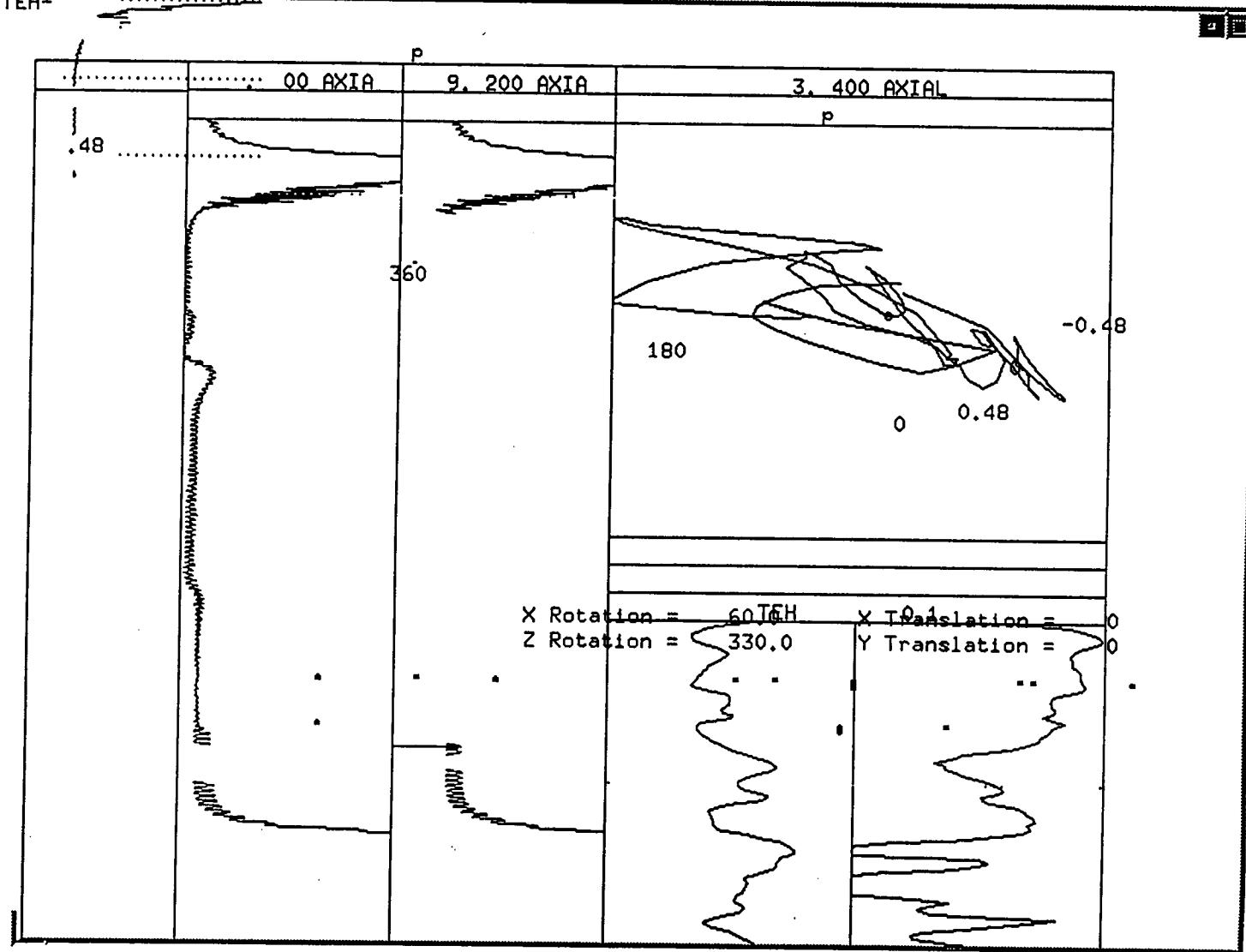


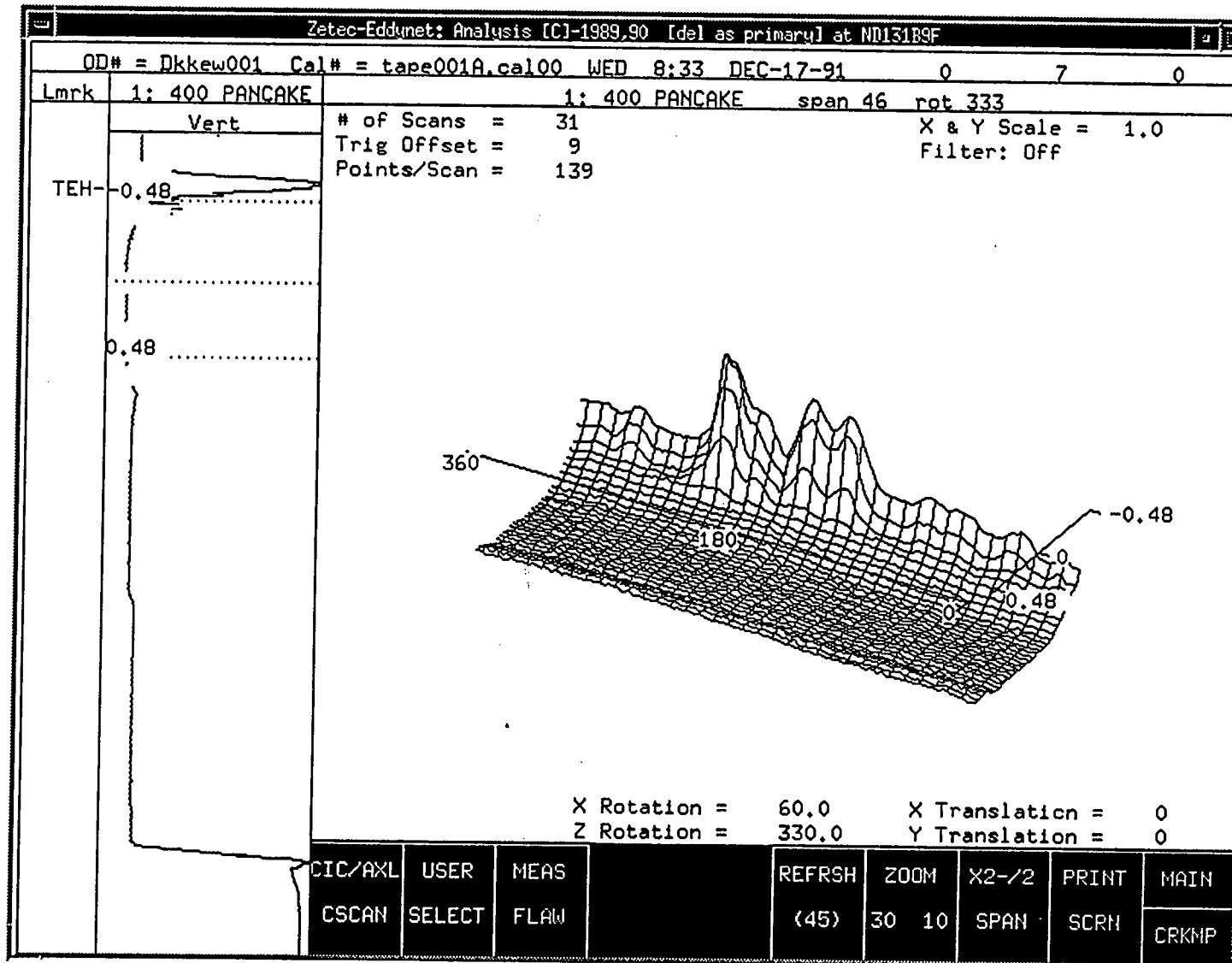


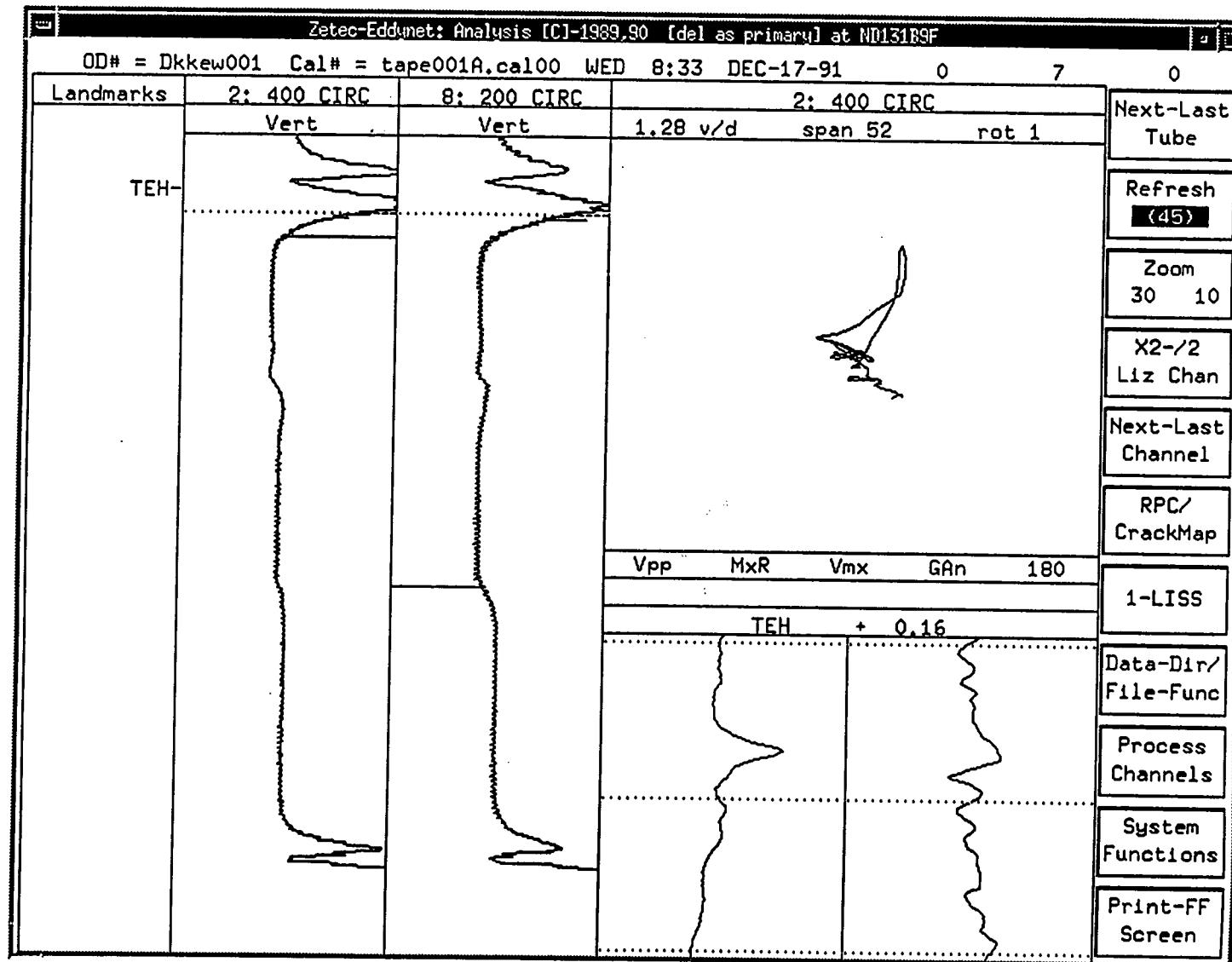
Zetec-Eddynet: Analysis [C]-1989,90 [del as primary] at ND131B9F

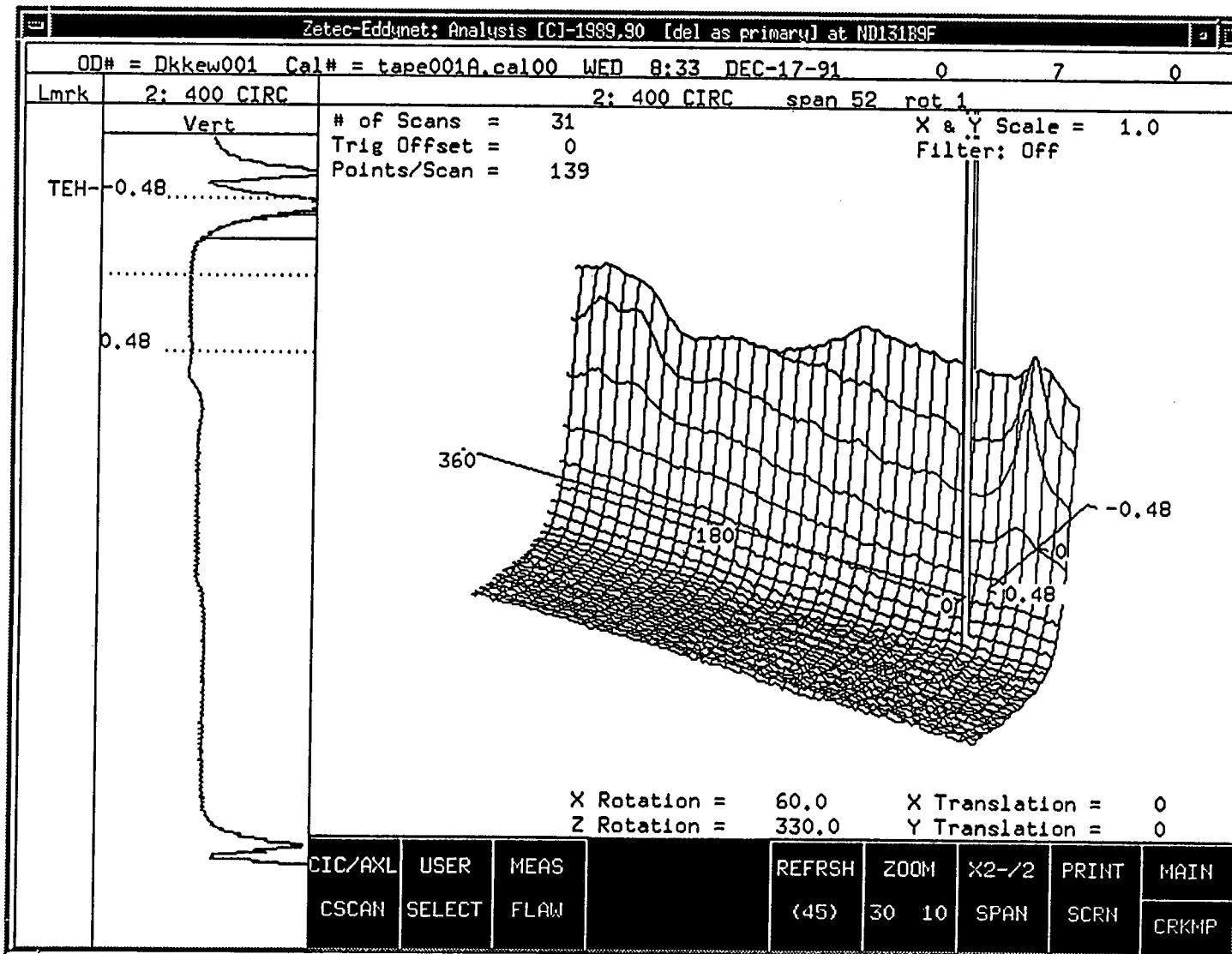
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 4 40 NCA 4 o
e # of Scans = 31.
Trig Offset = 9.
Points/Scan = 140
X & Y Scale = 1.0
Filter: Off

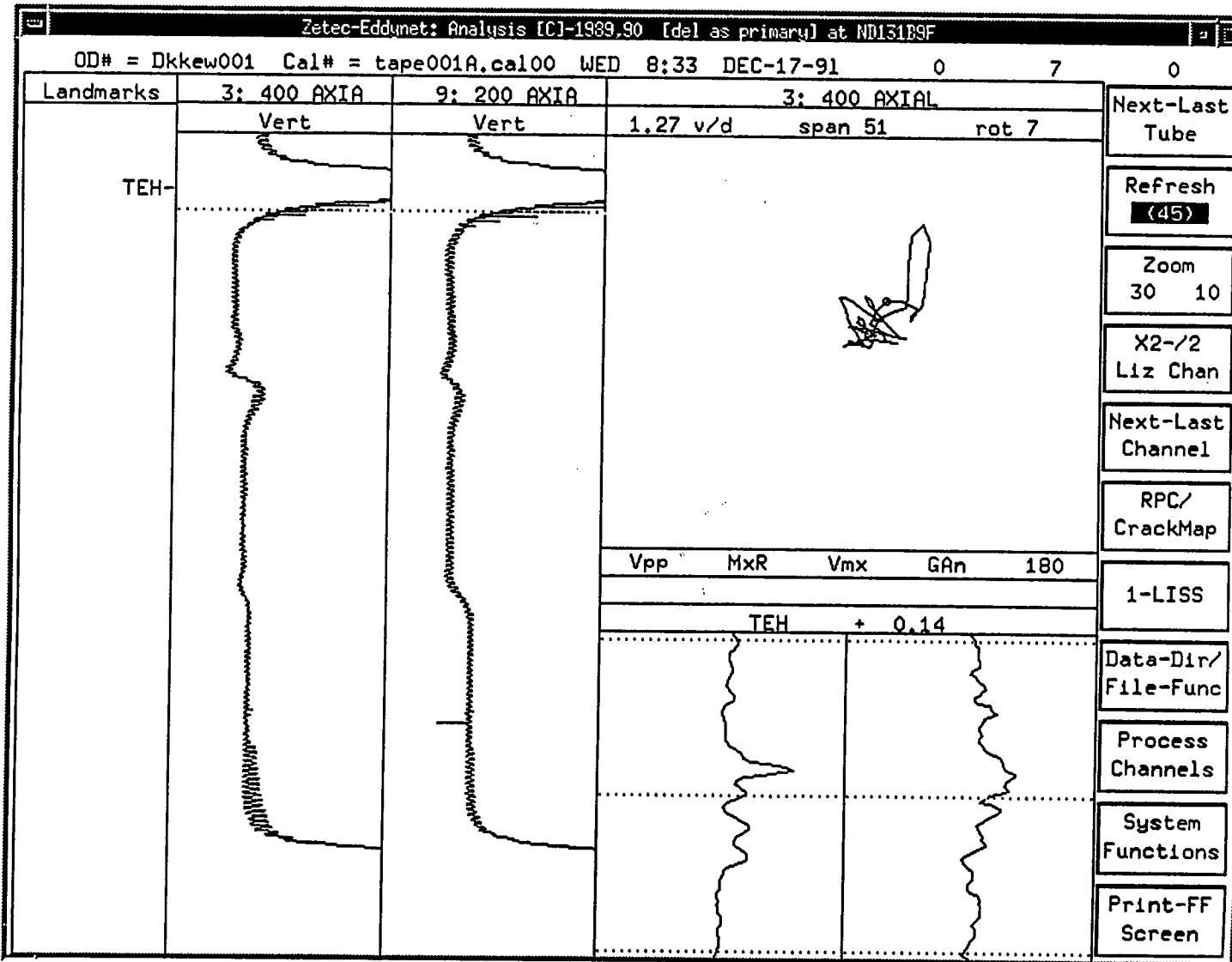
TEH-

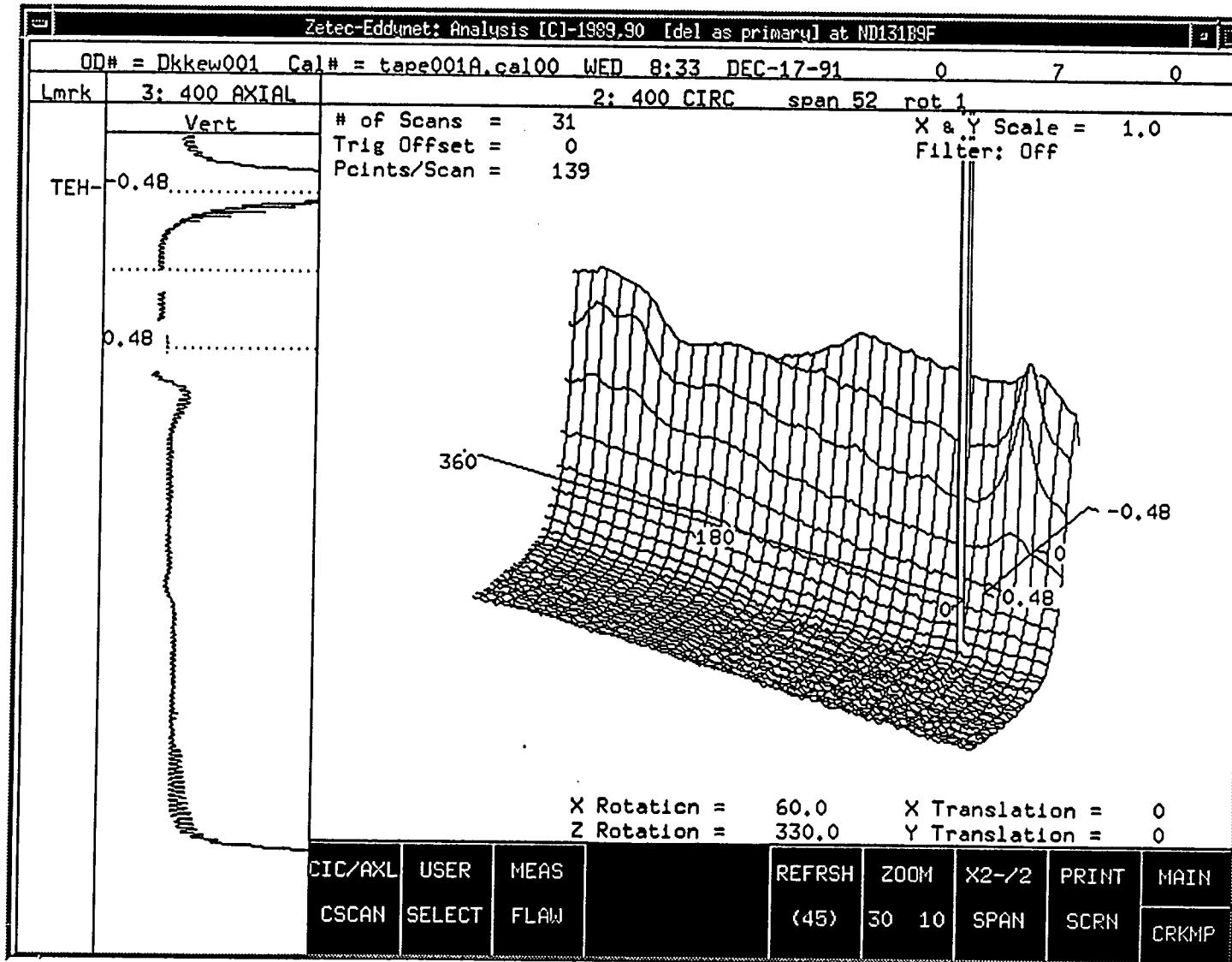


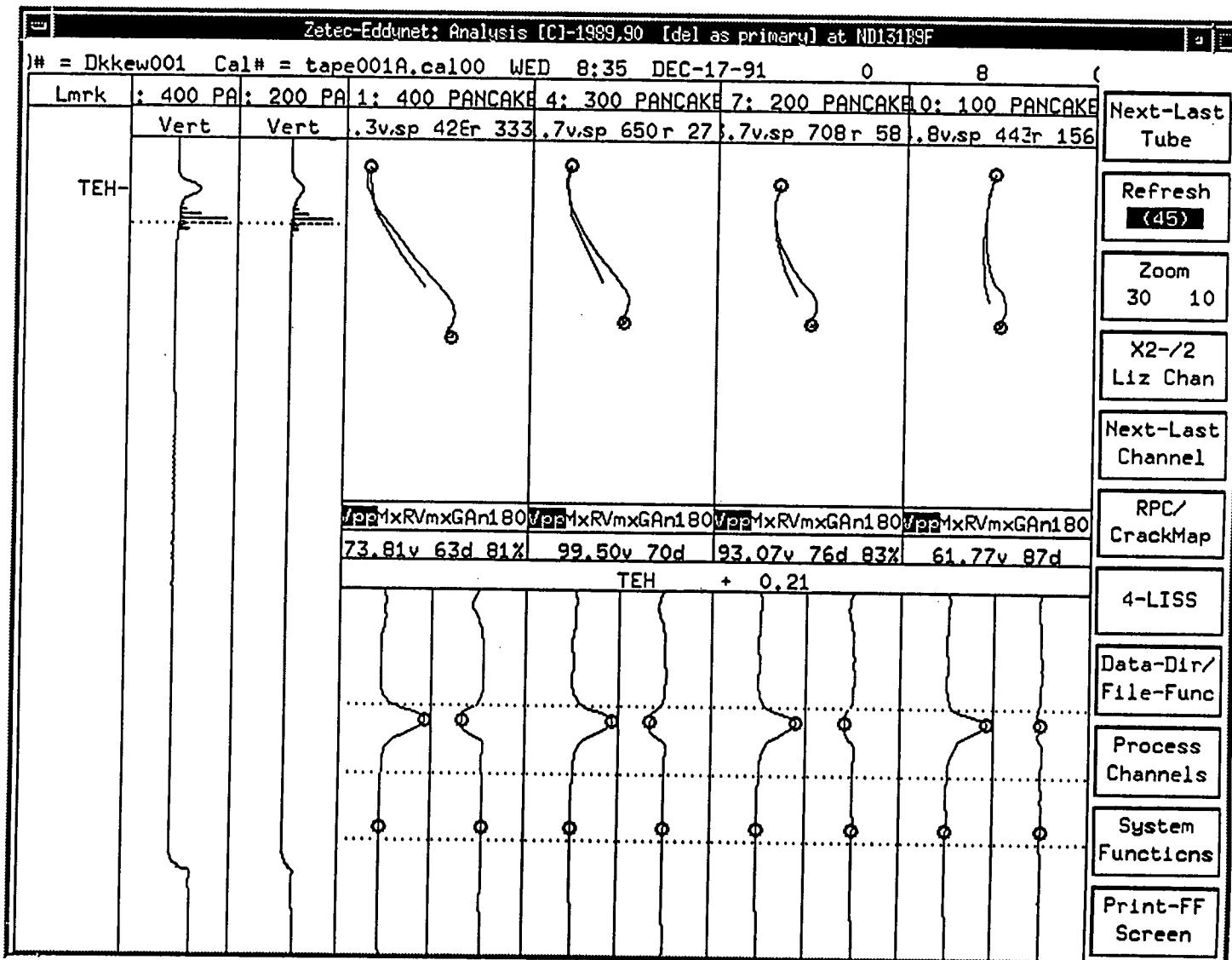


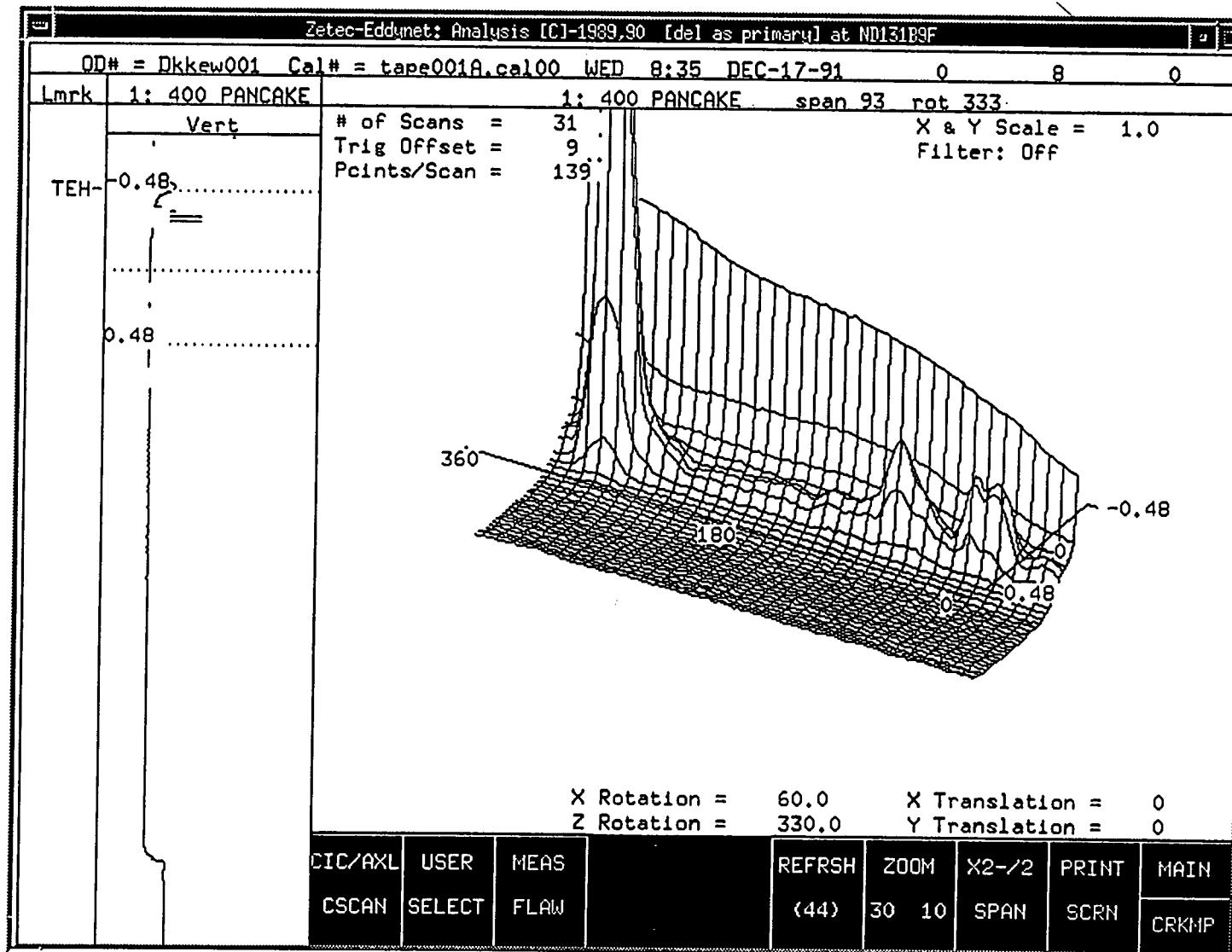


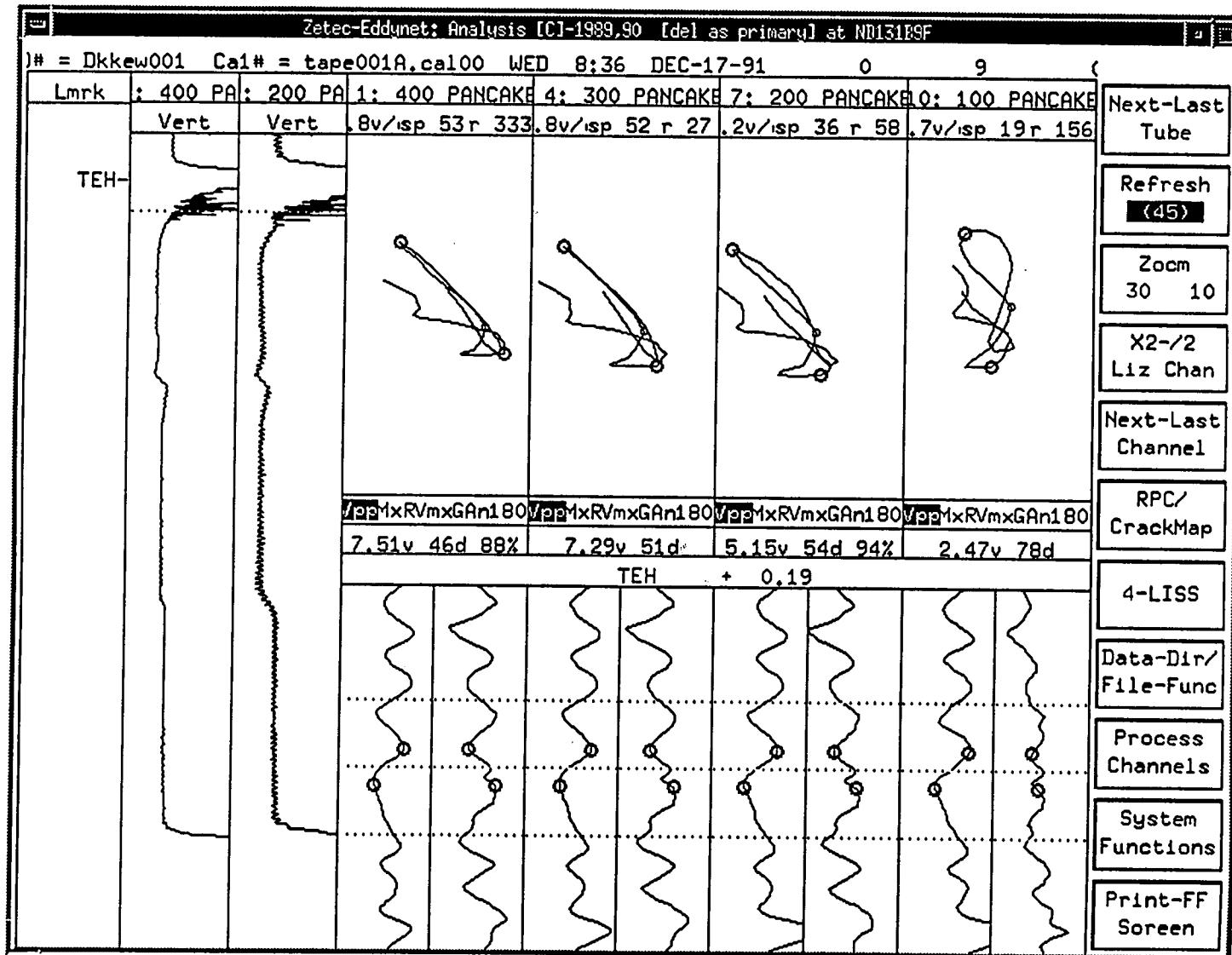


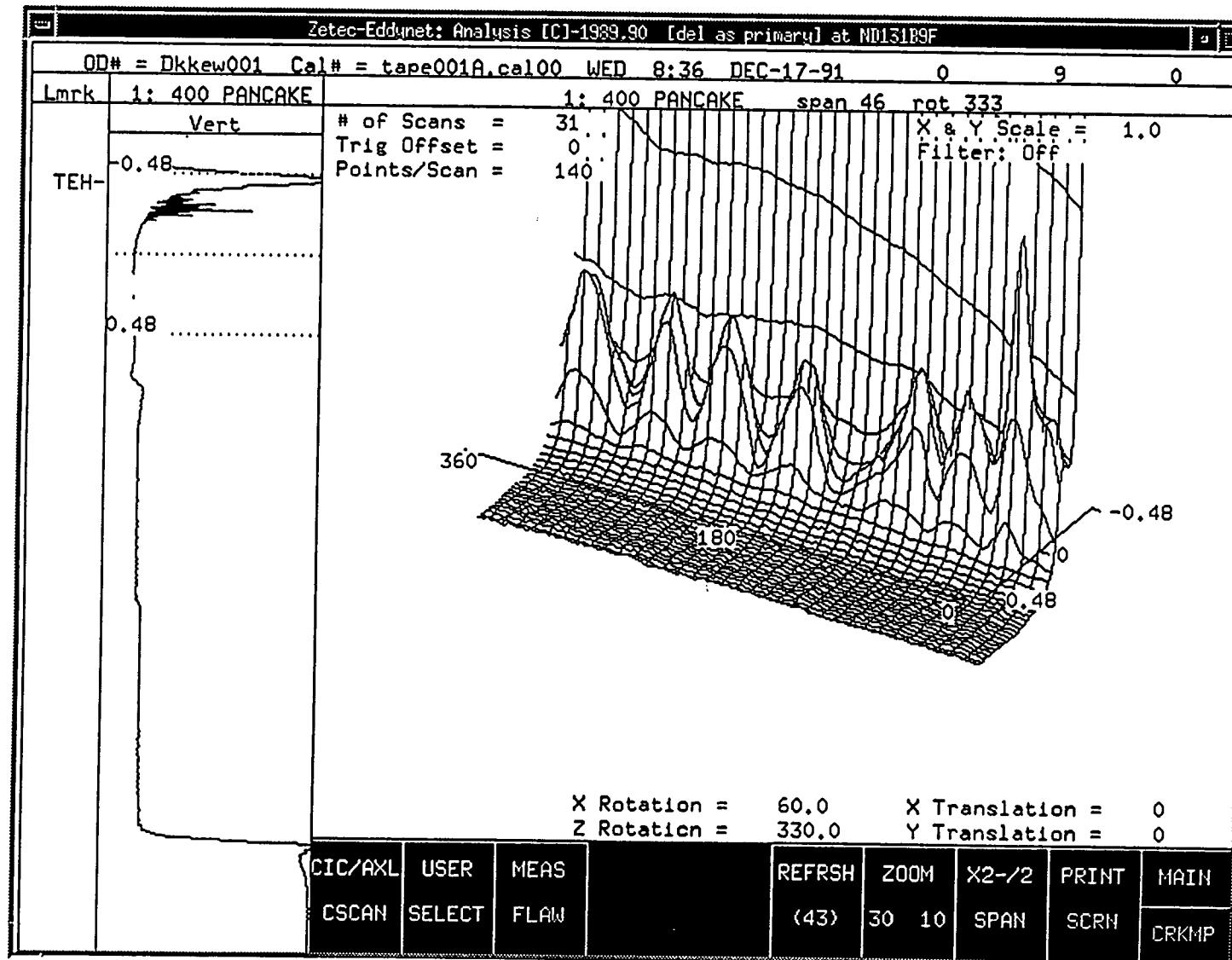


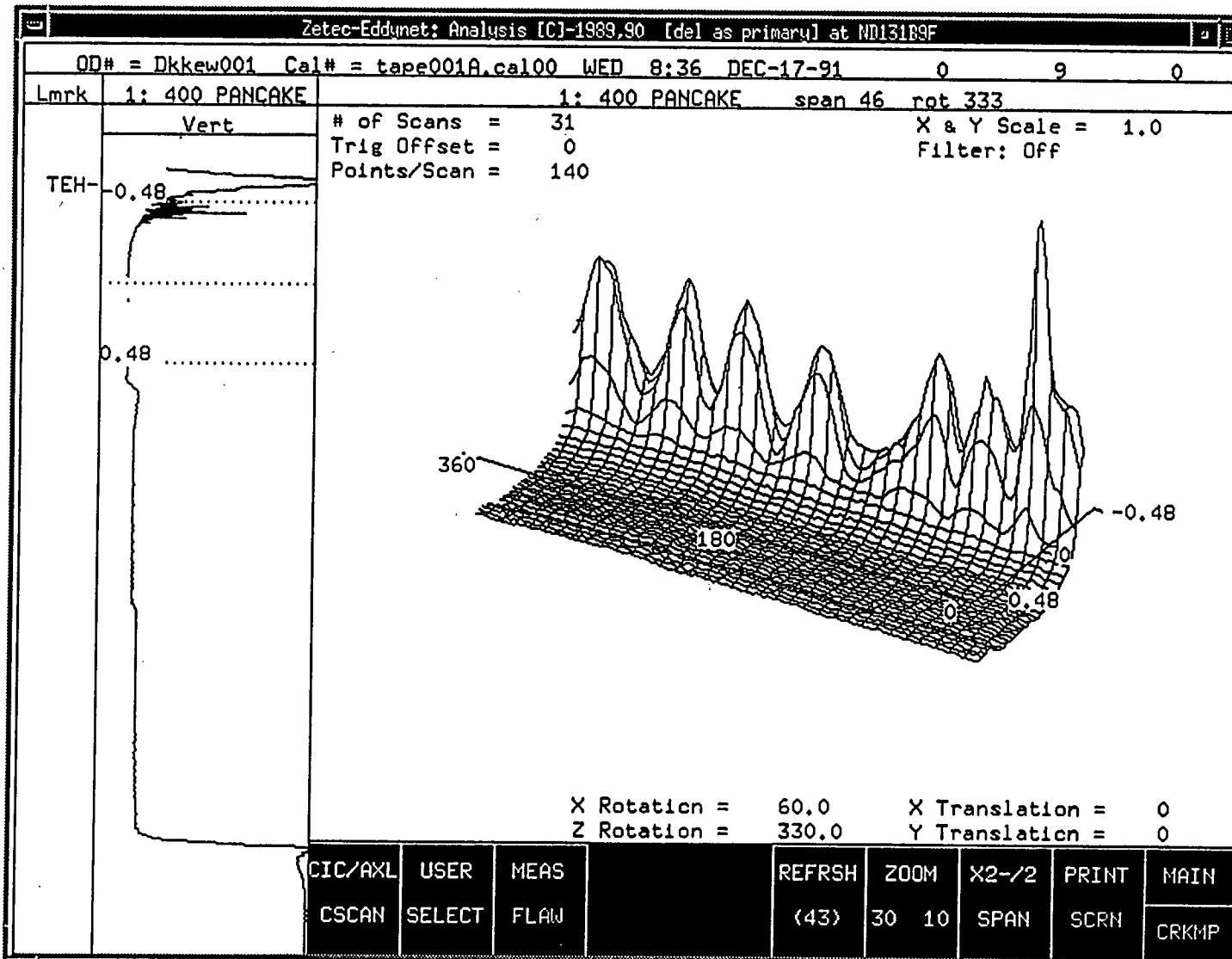


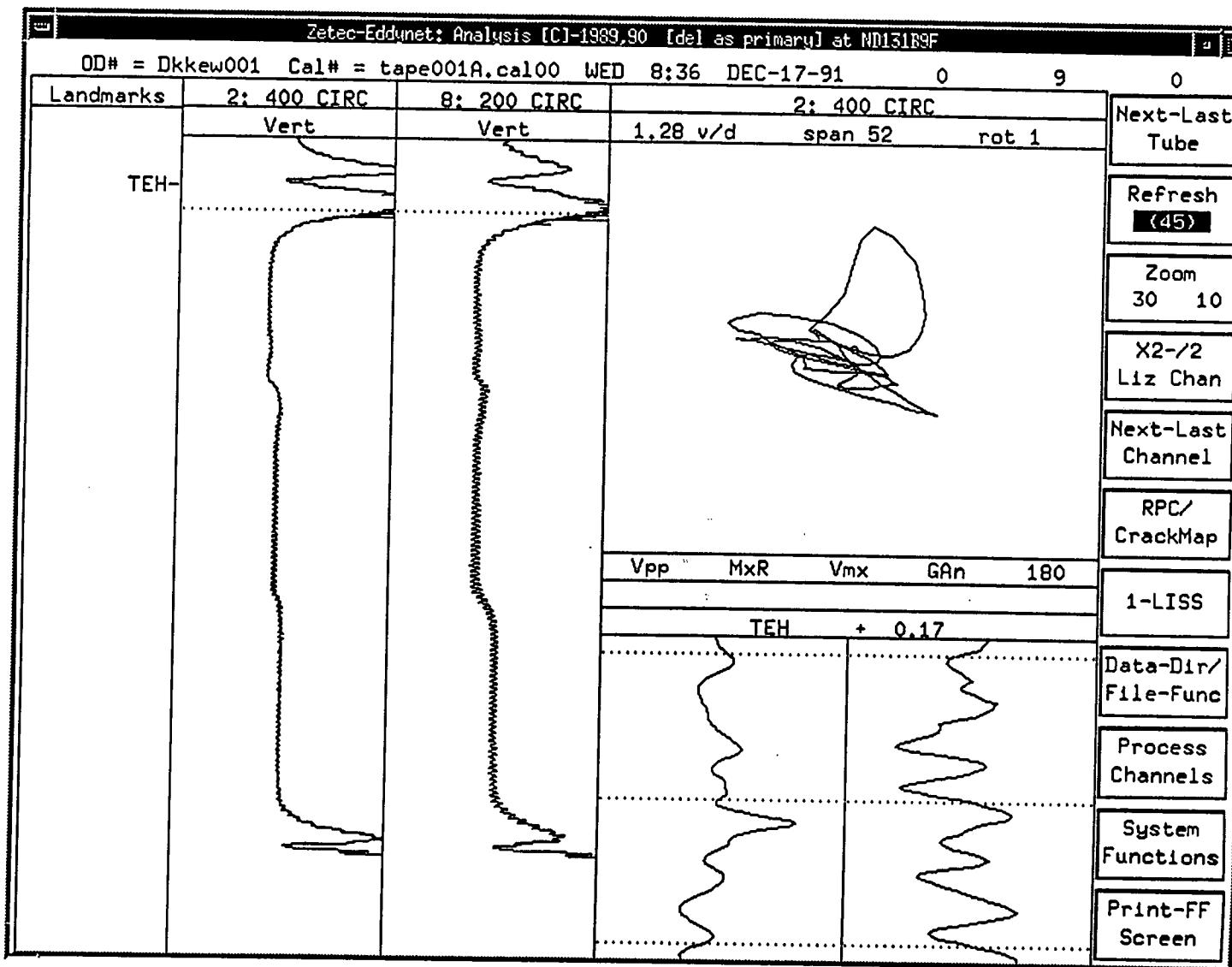


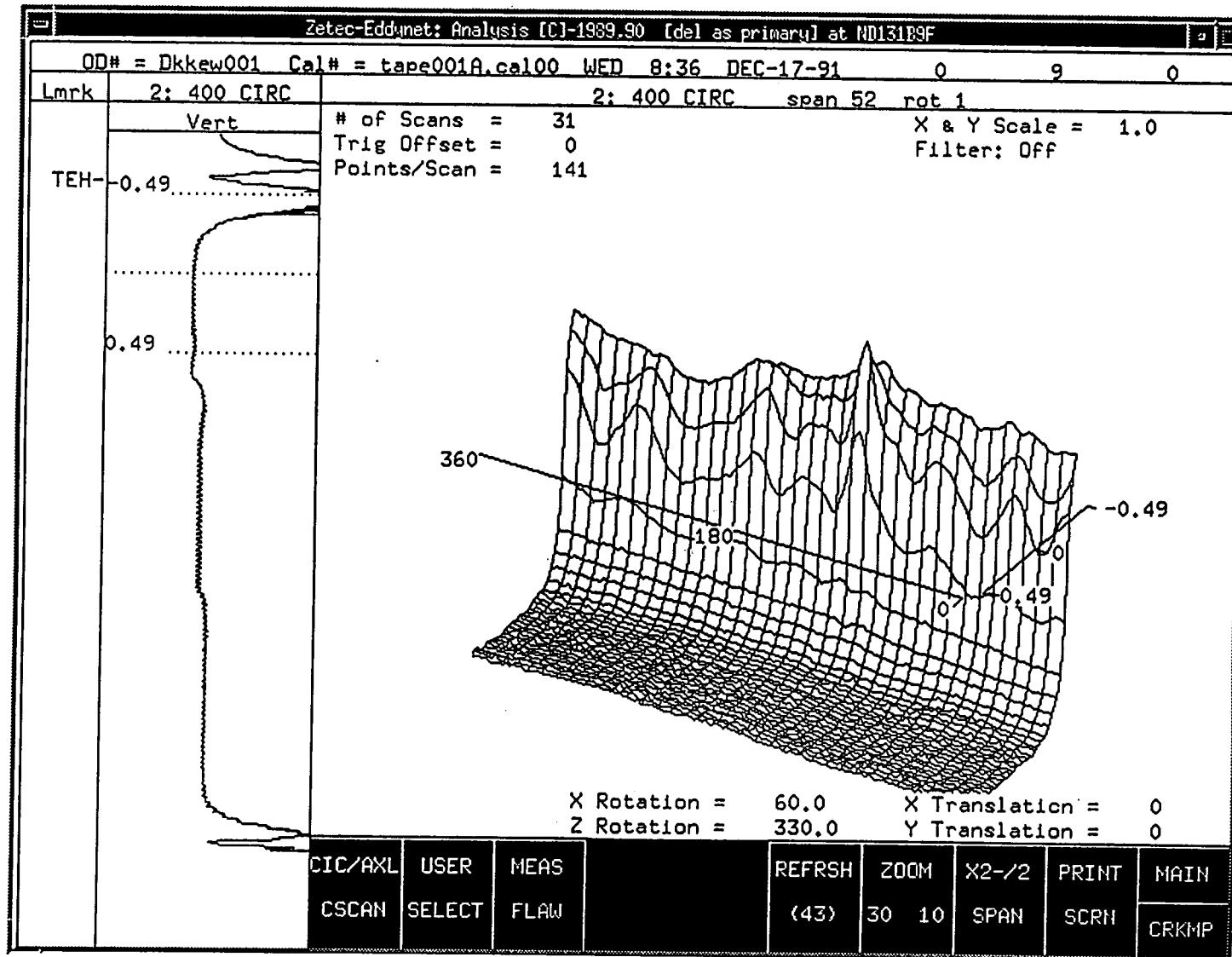


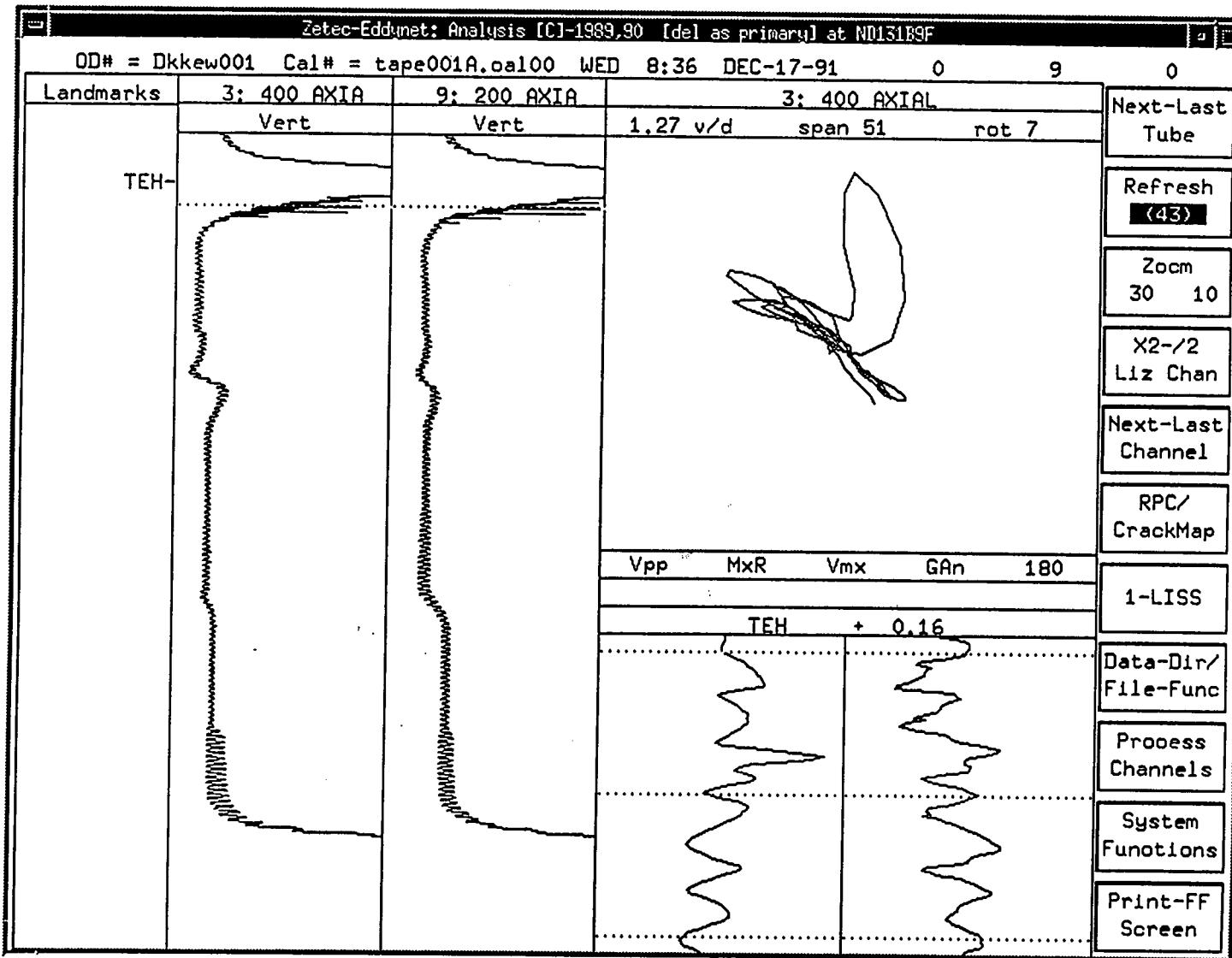


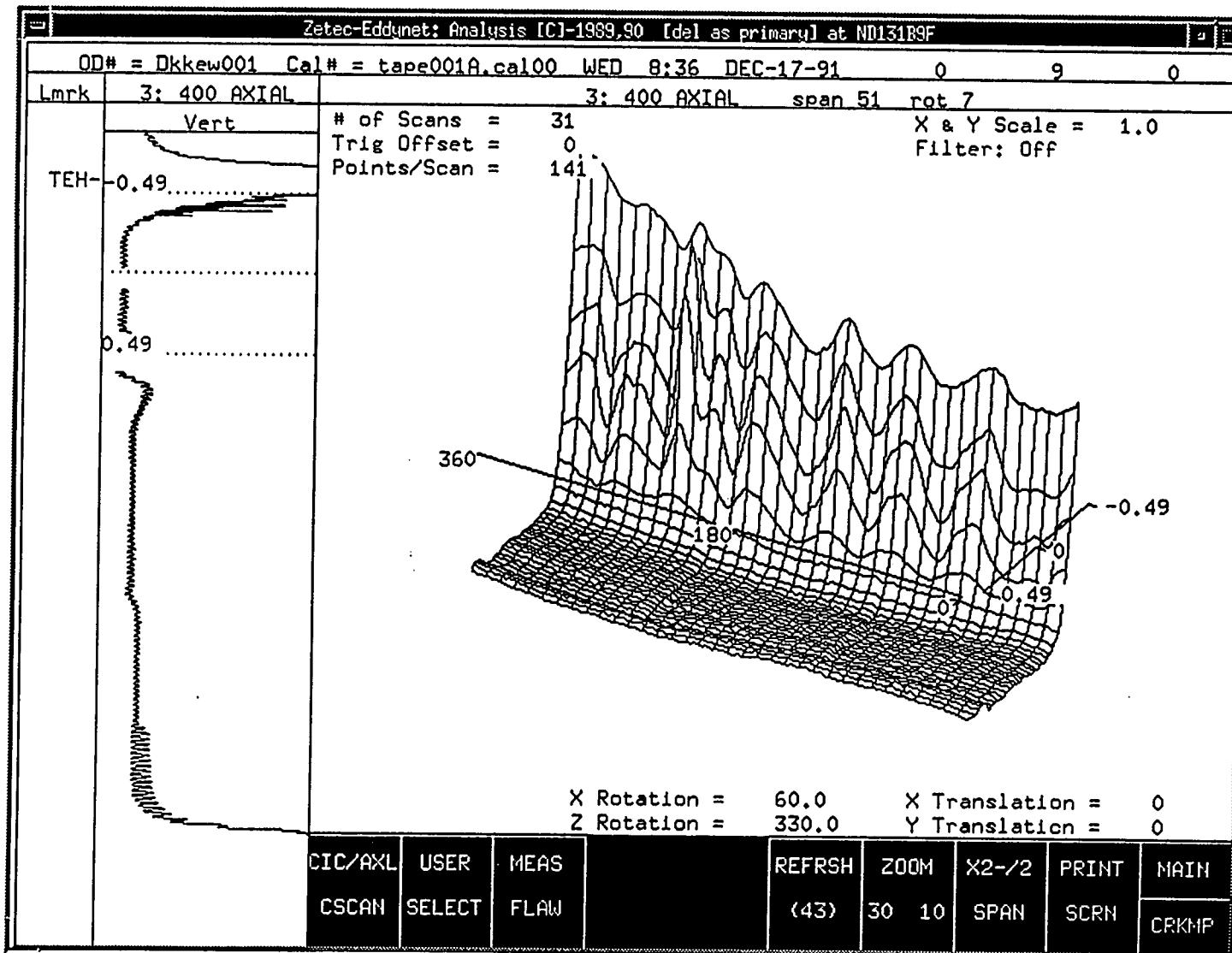


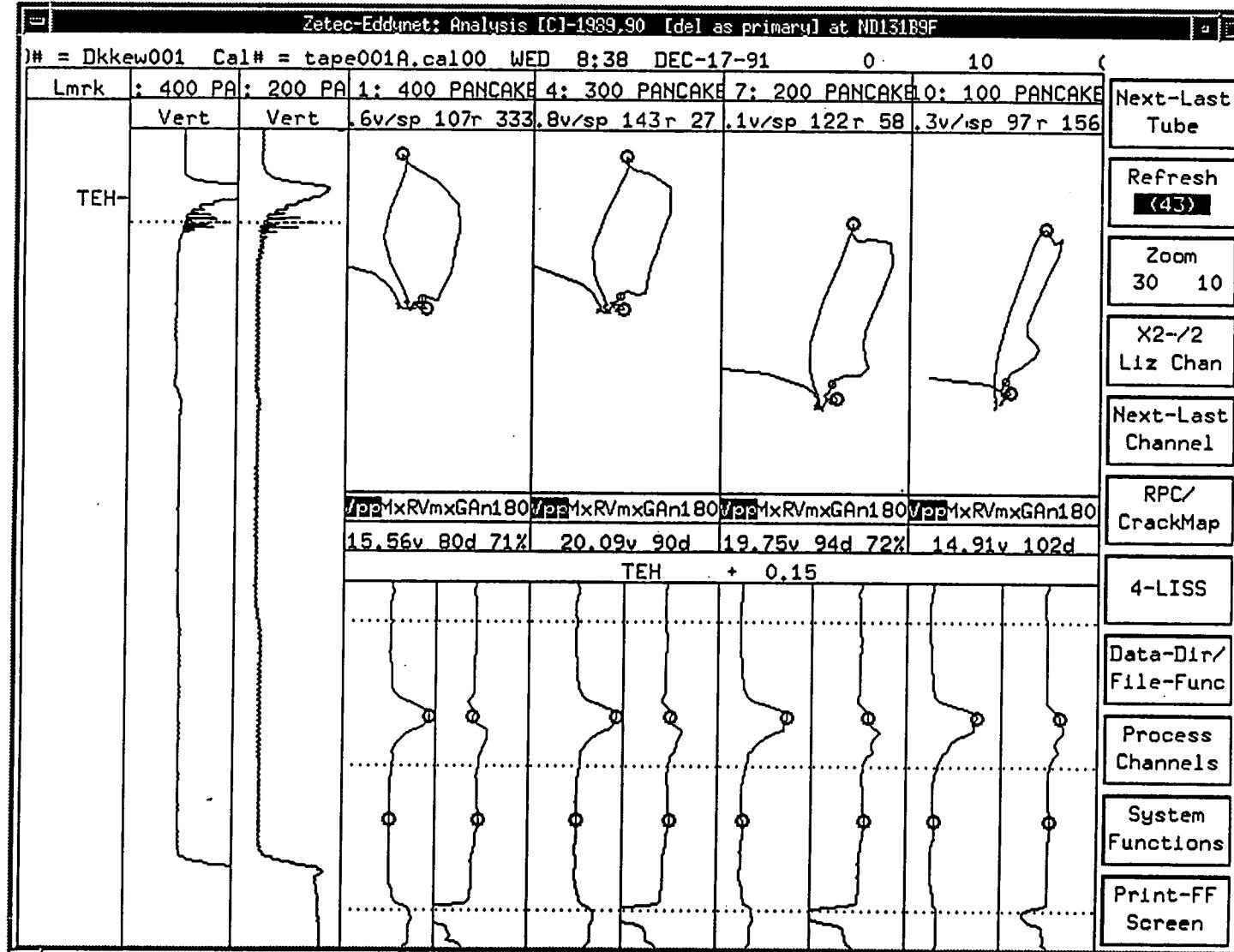


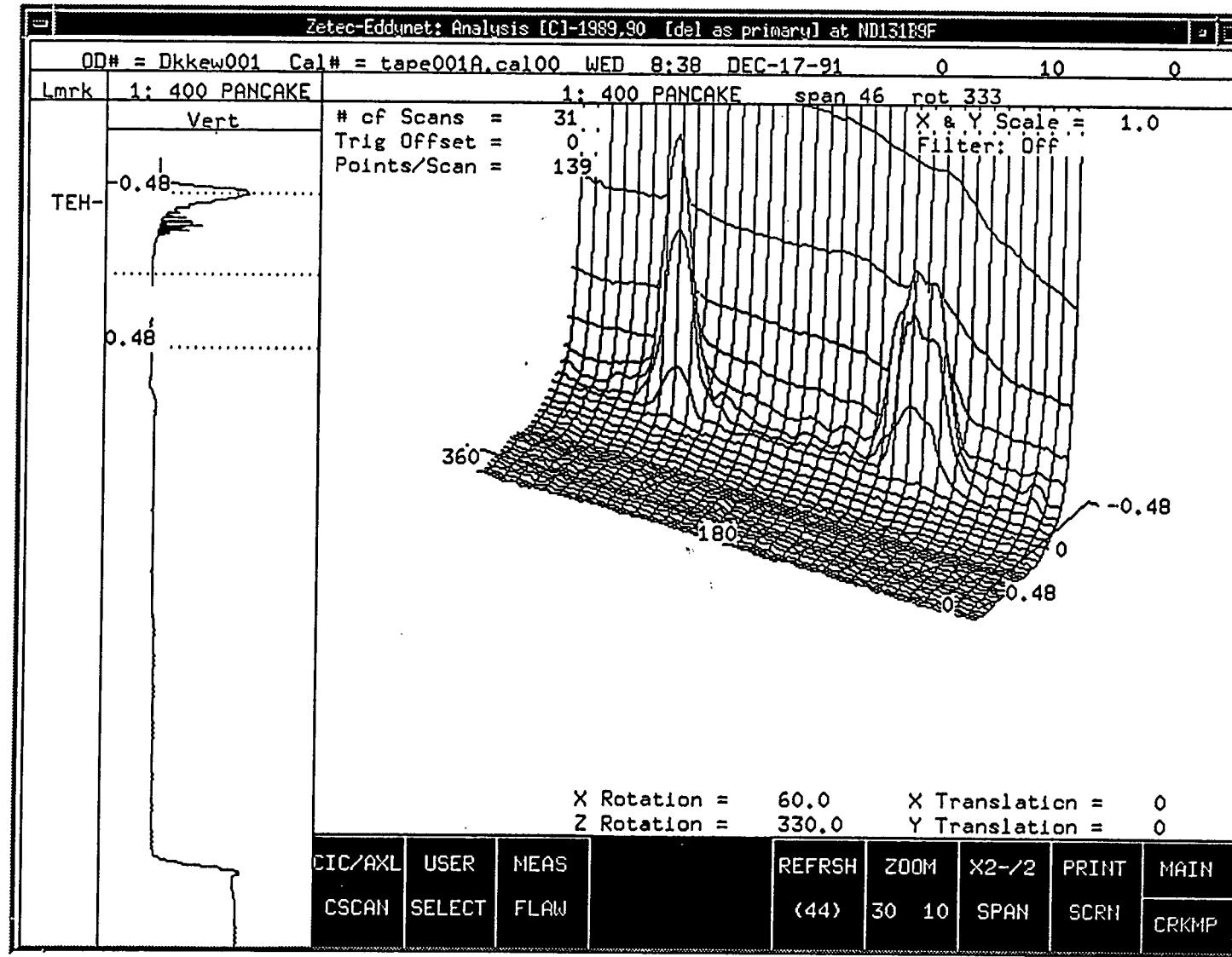


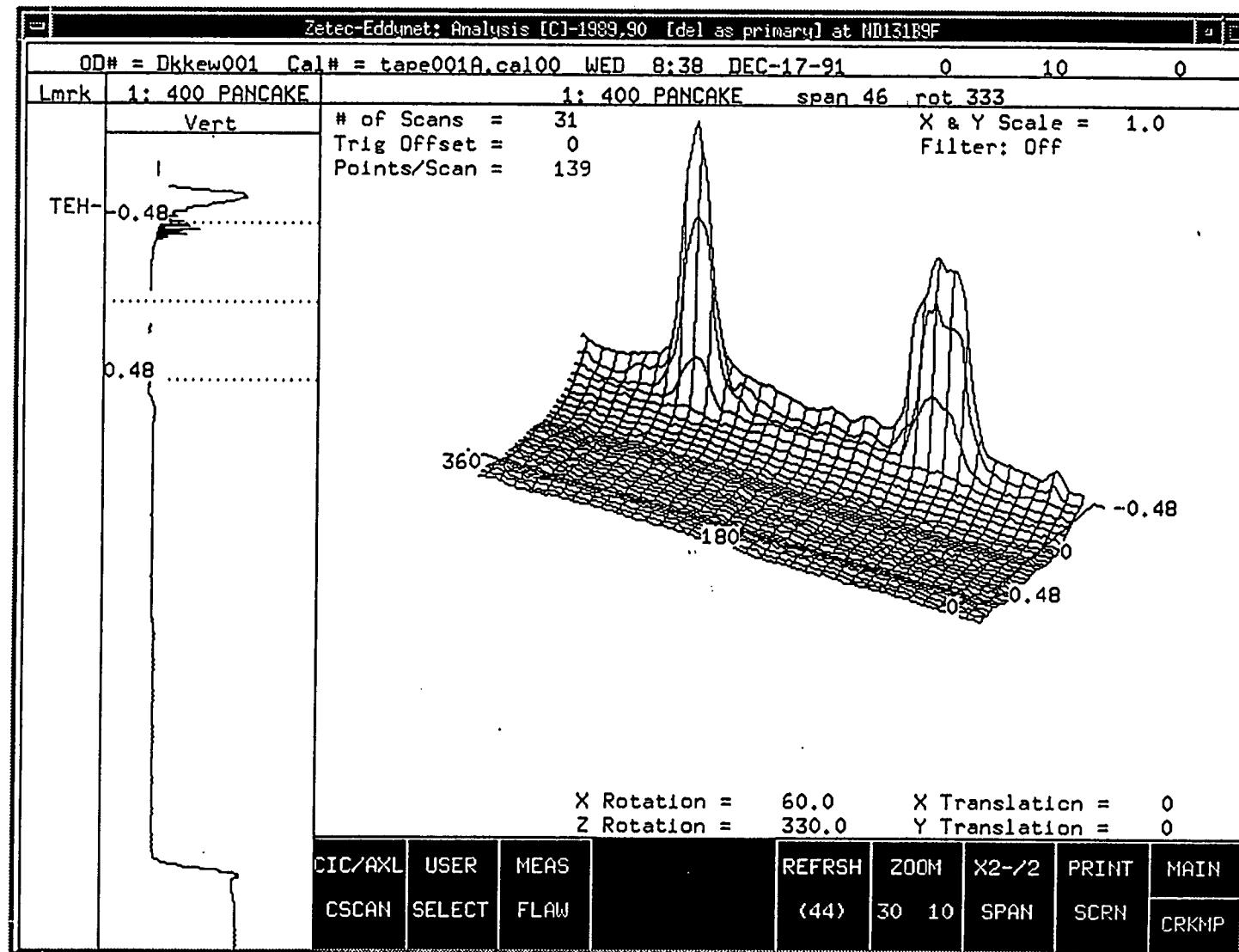


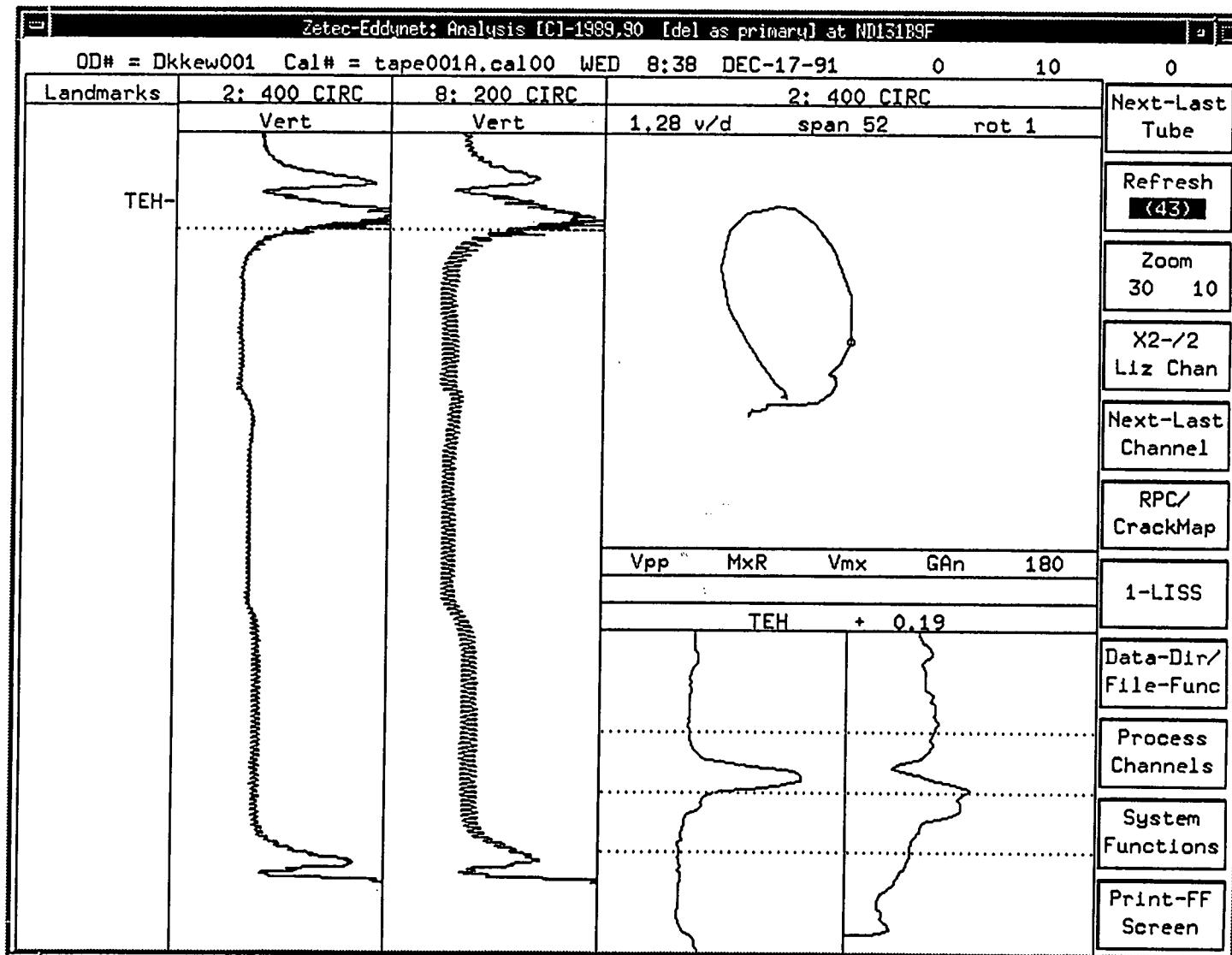


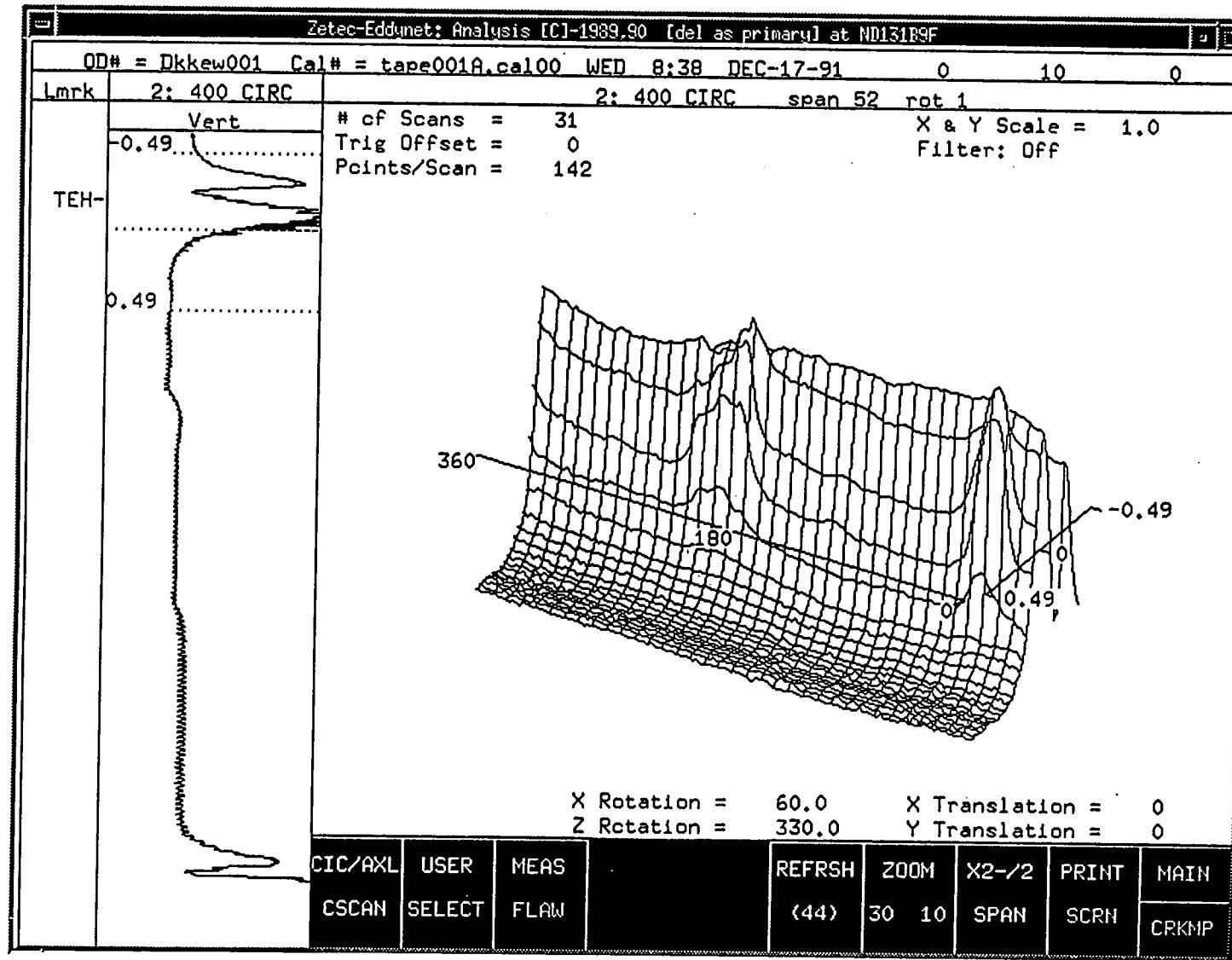


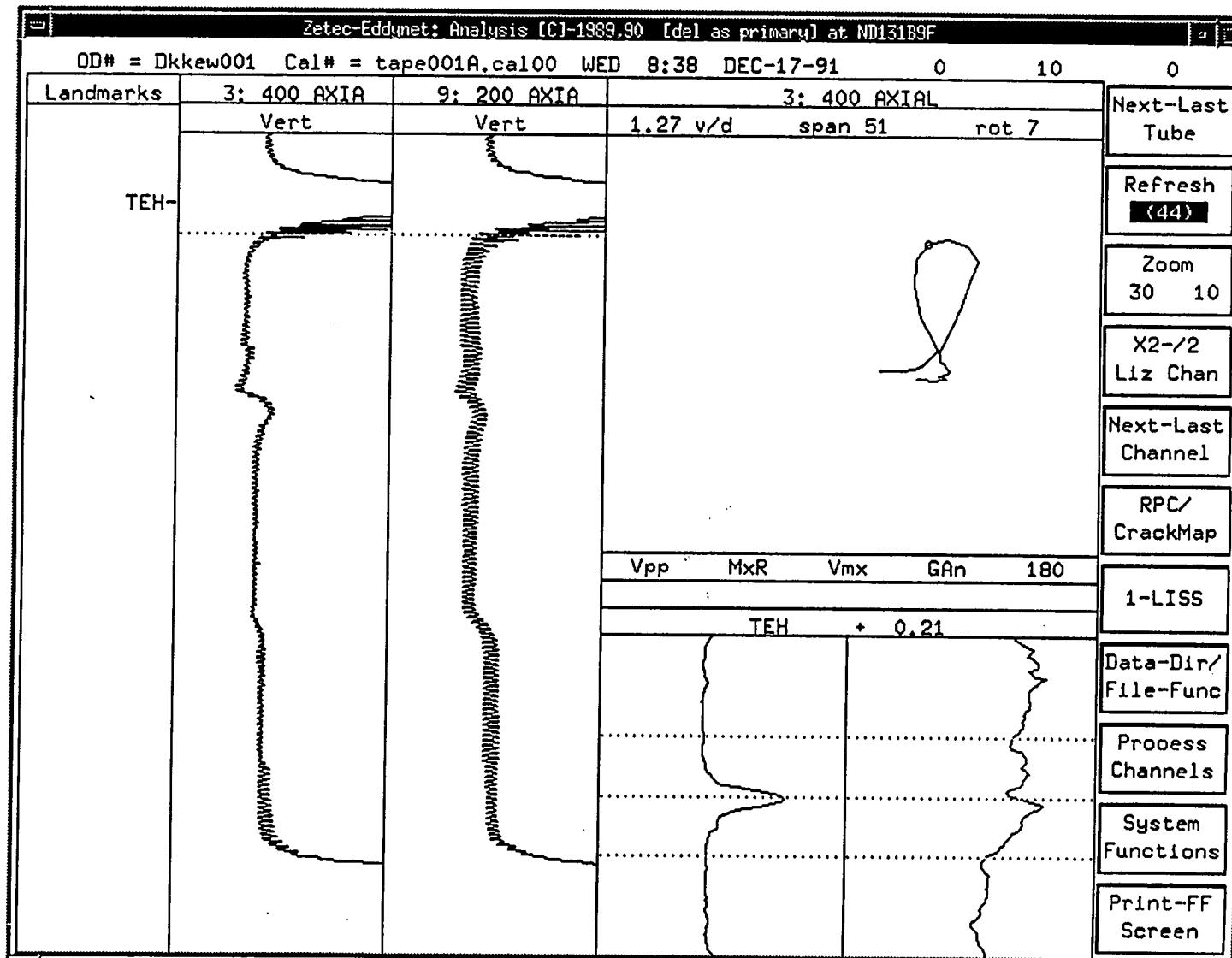






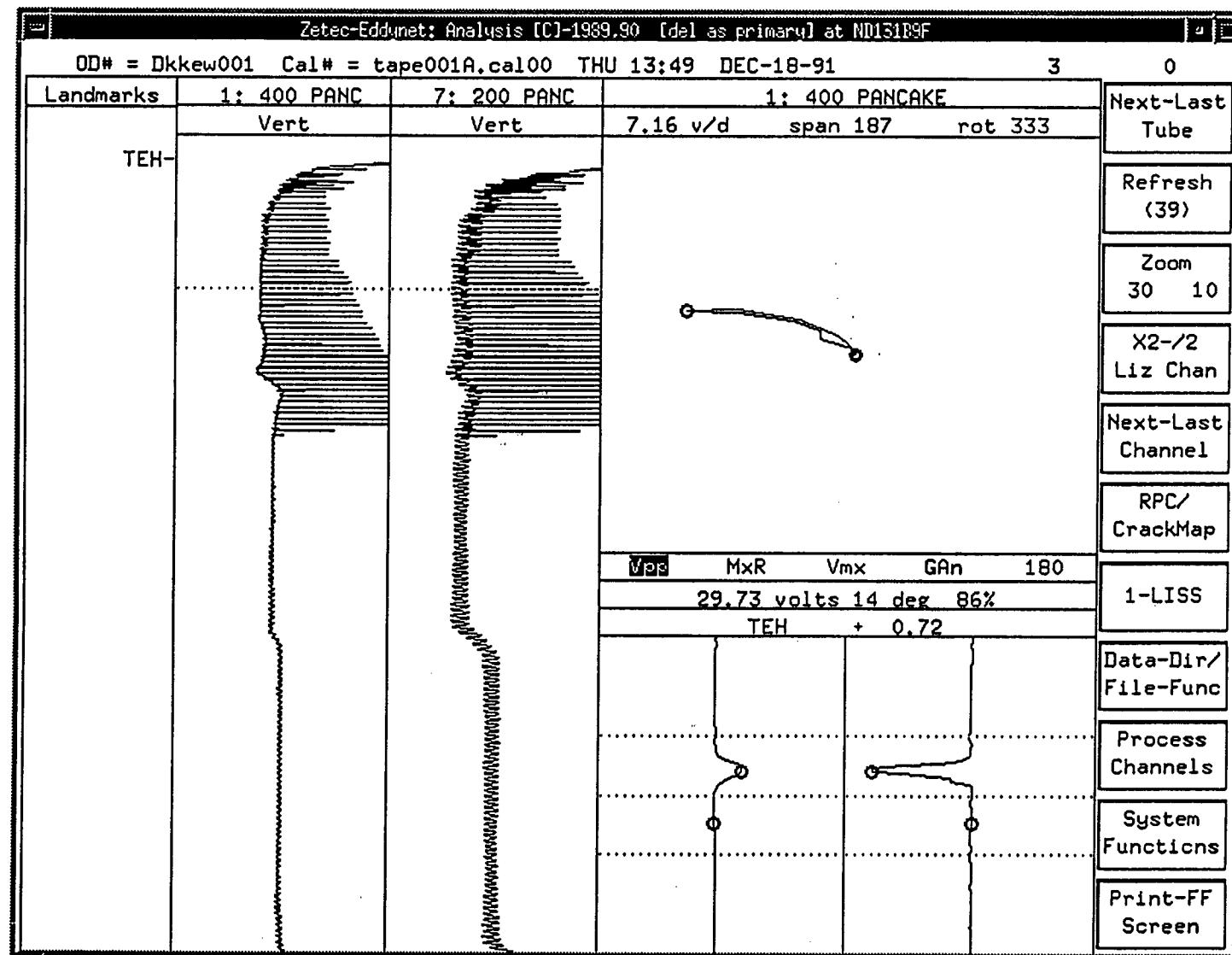


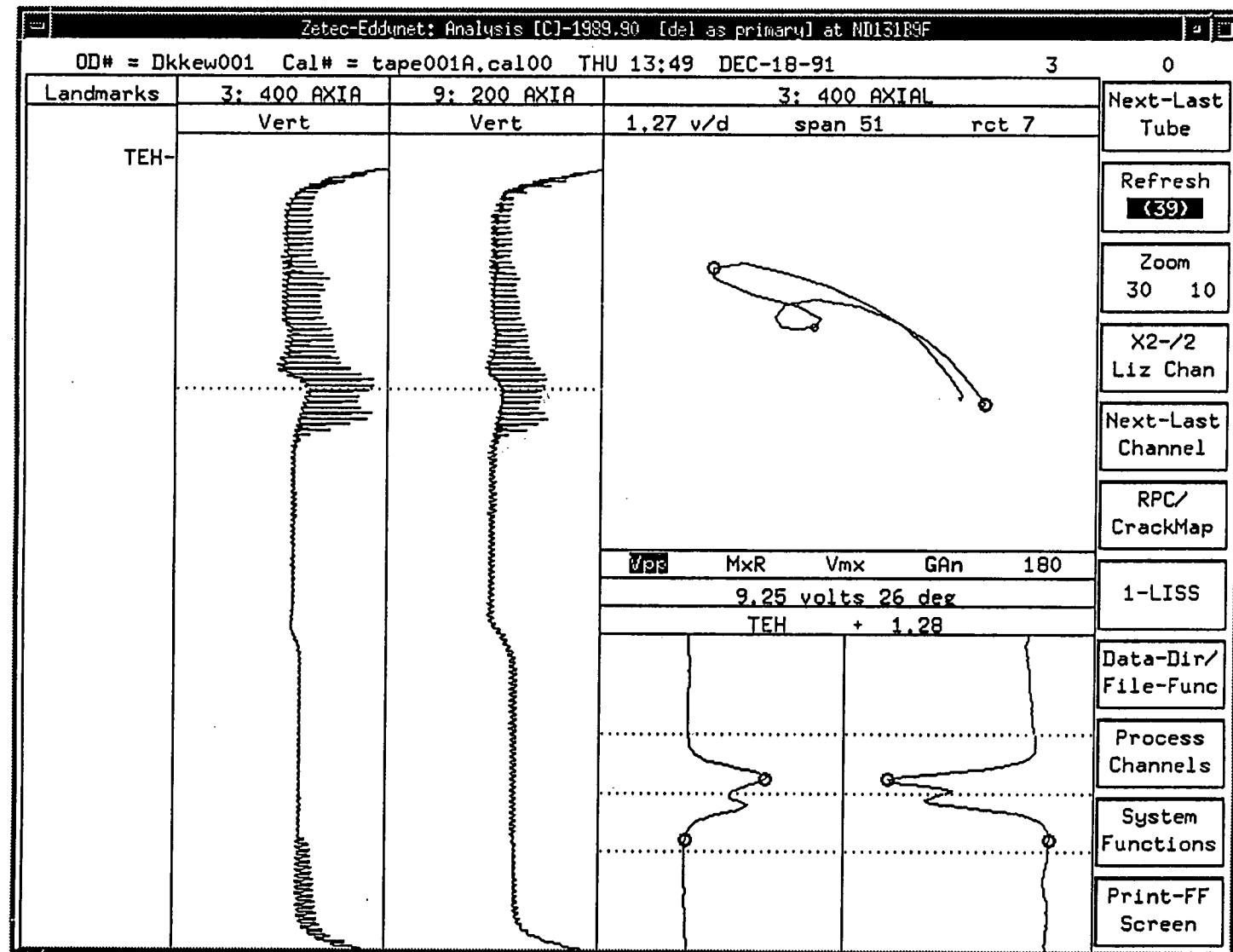


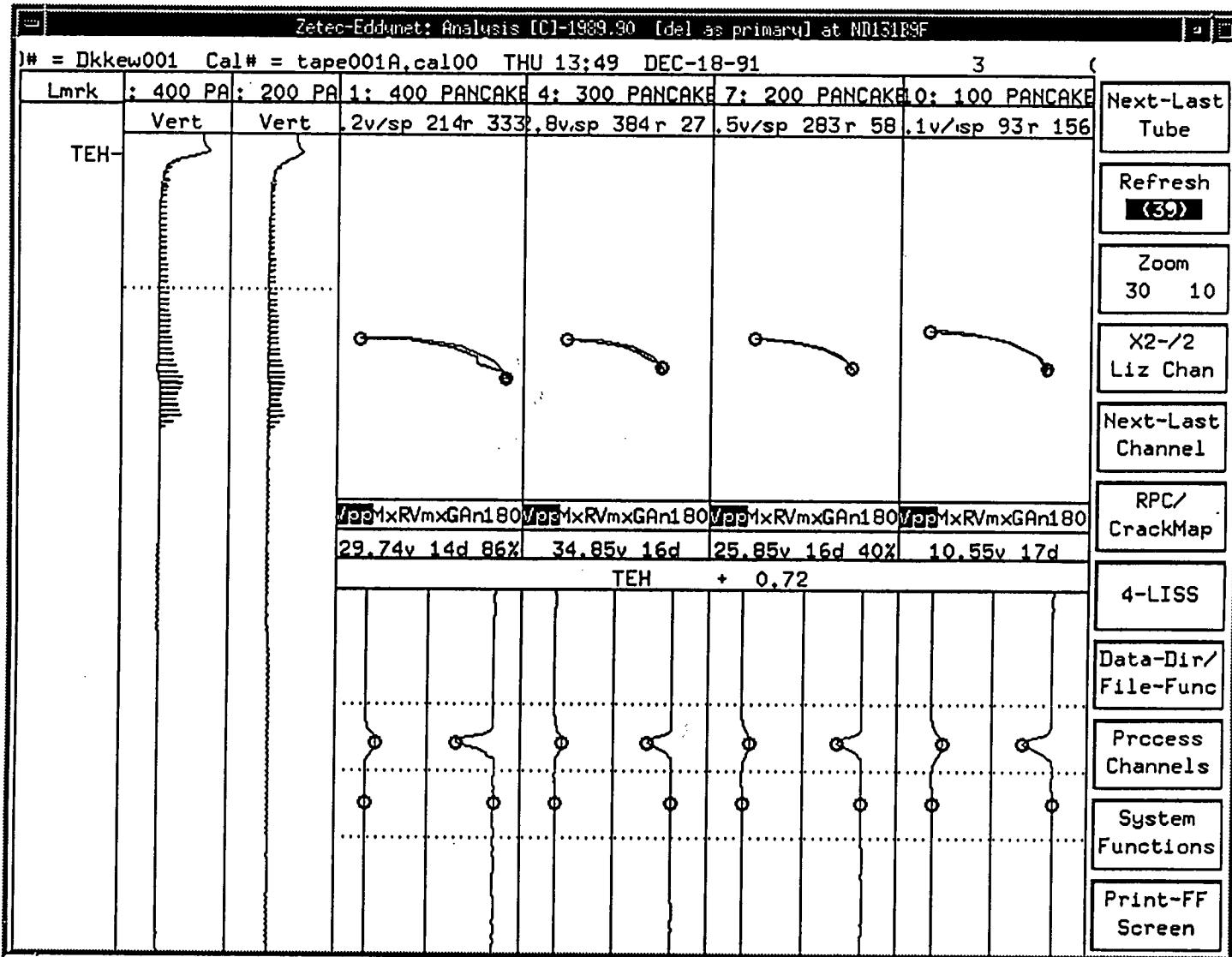


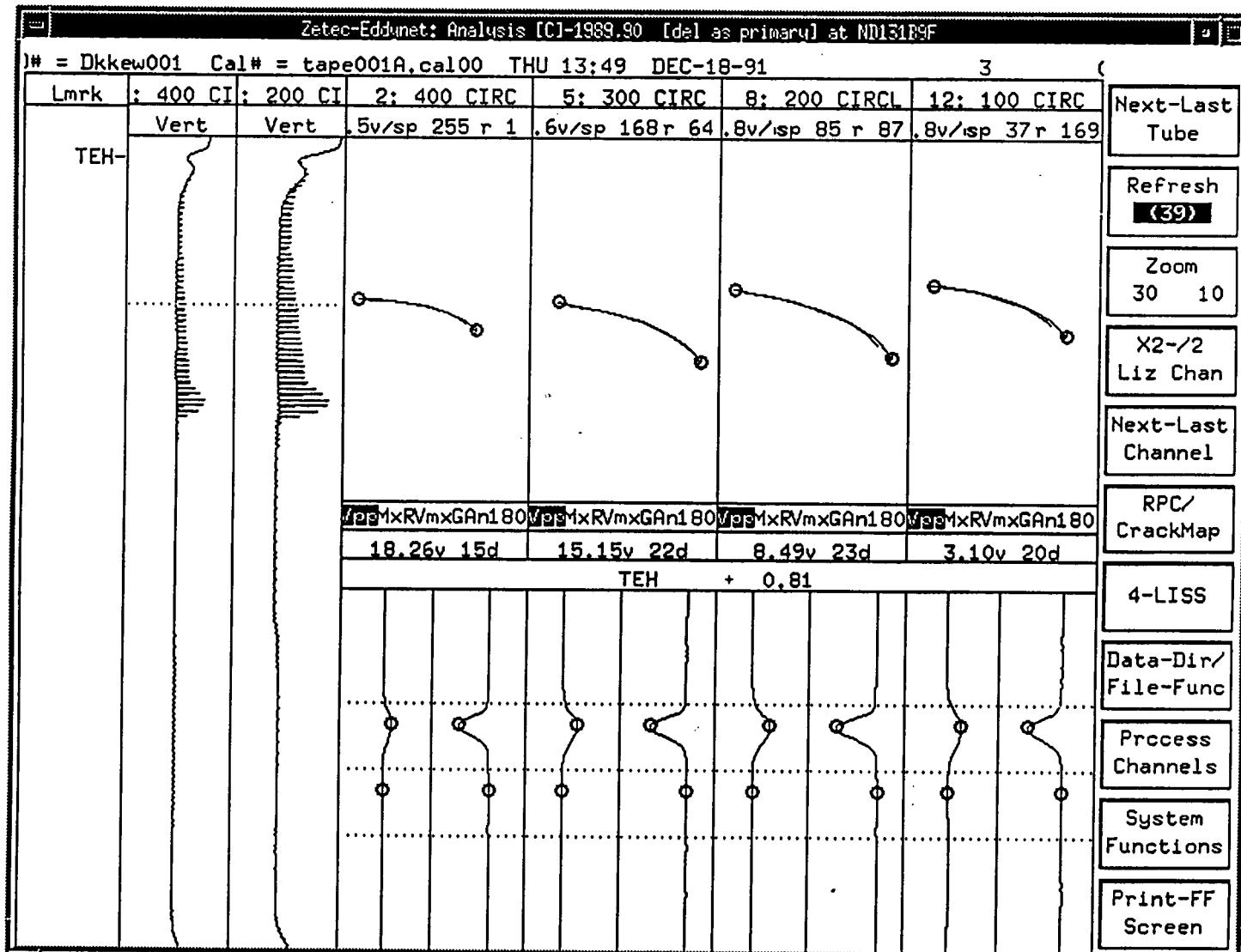
KEWAUNEE STEAM GENERATOR TUBES
EDDY CURRENT DATA ANALYSIS

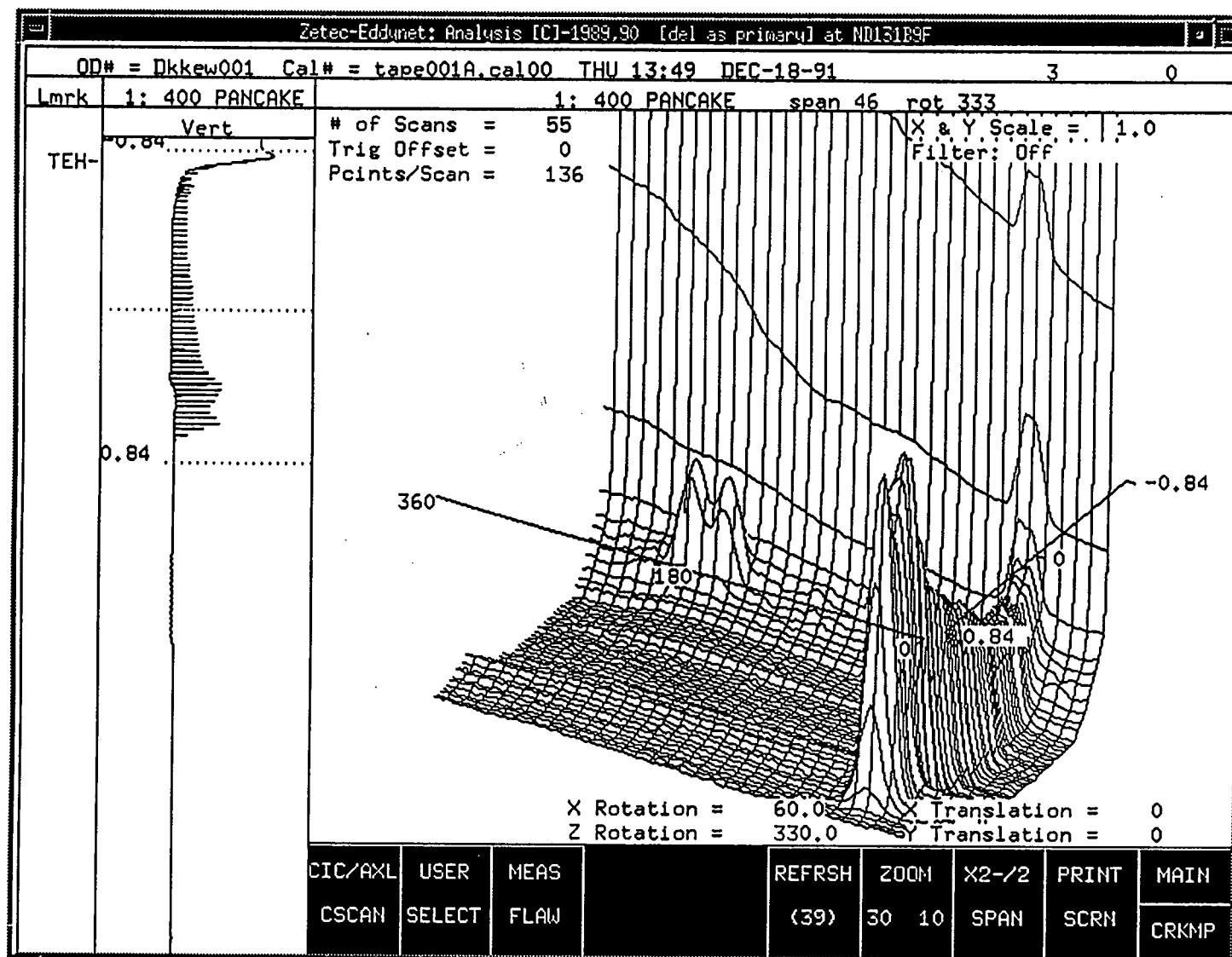
SECTION 6.0B - LAB SAMPLE EDDY CURRENT GRAPHICS
EXPANDED WELDED SAMPLES WITH EDM NOTCHES

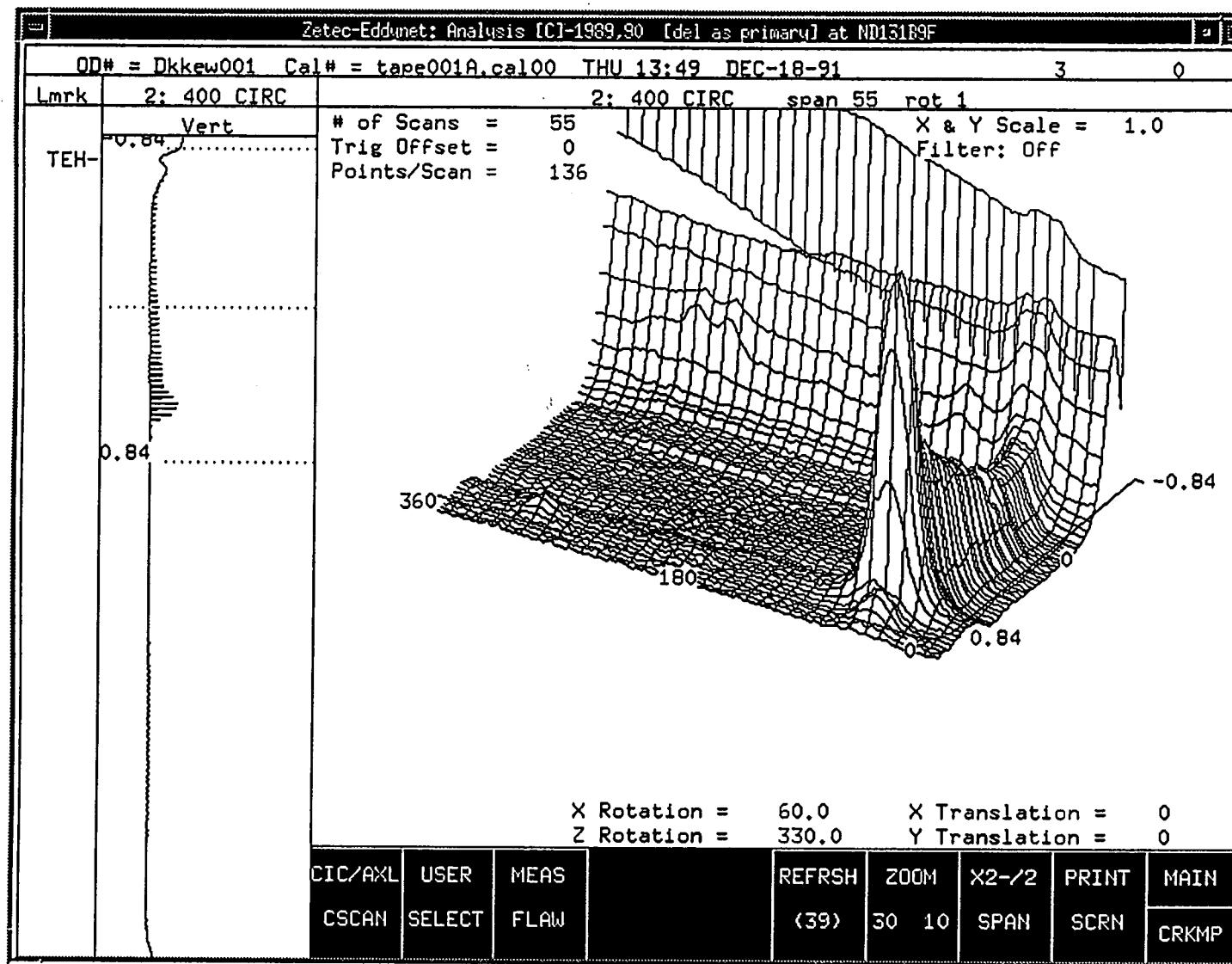


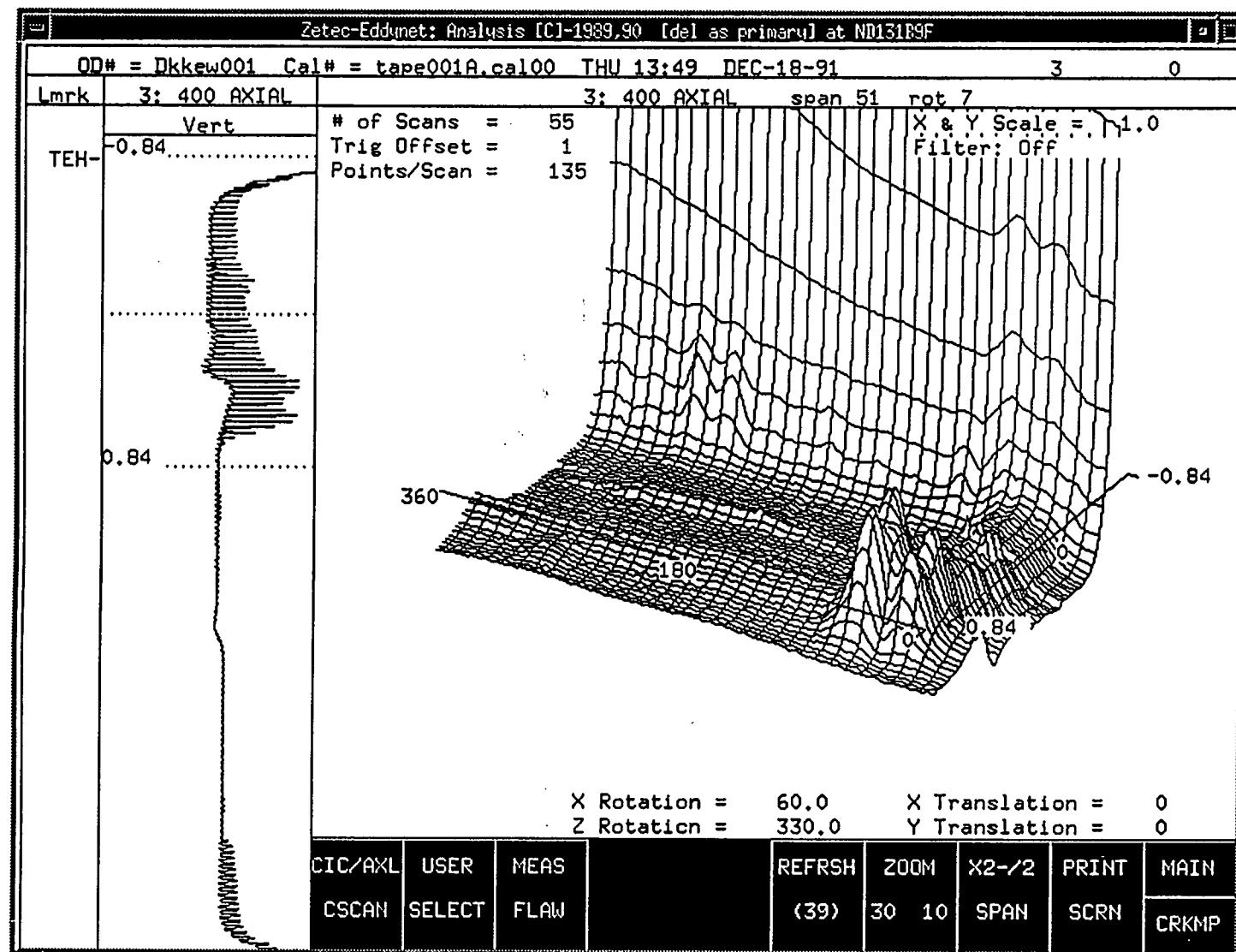


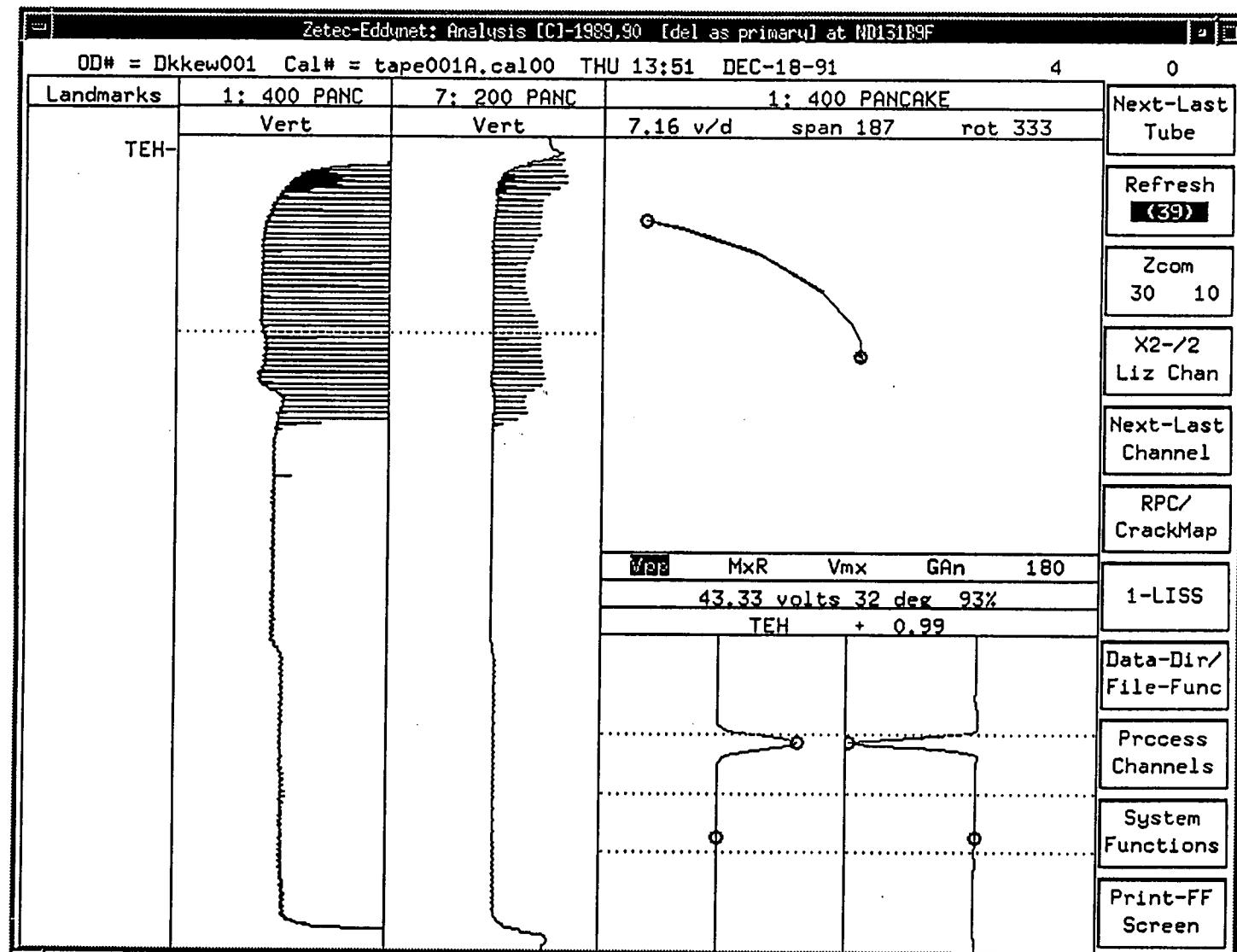


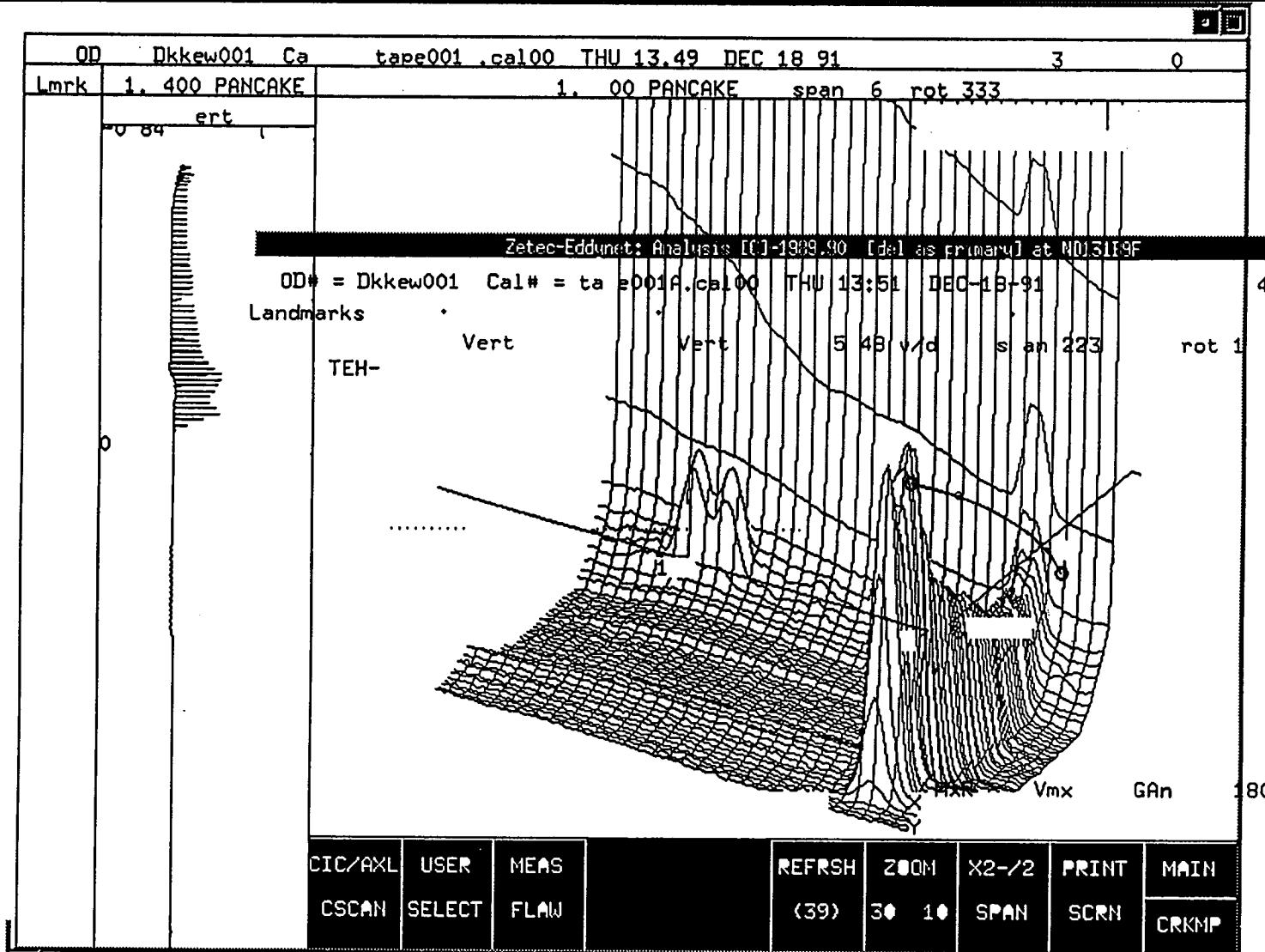




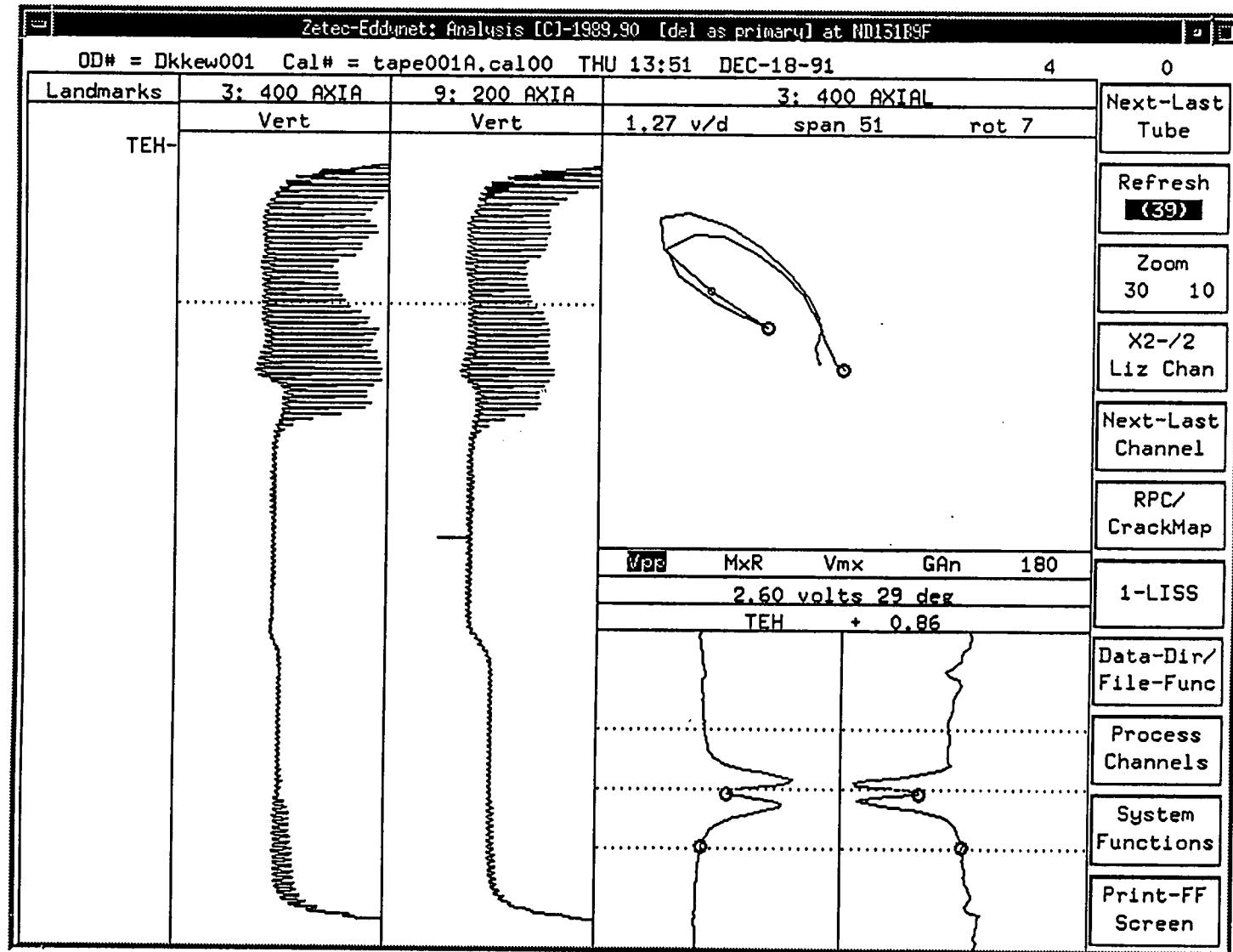


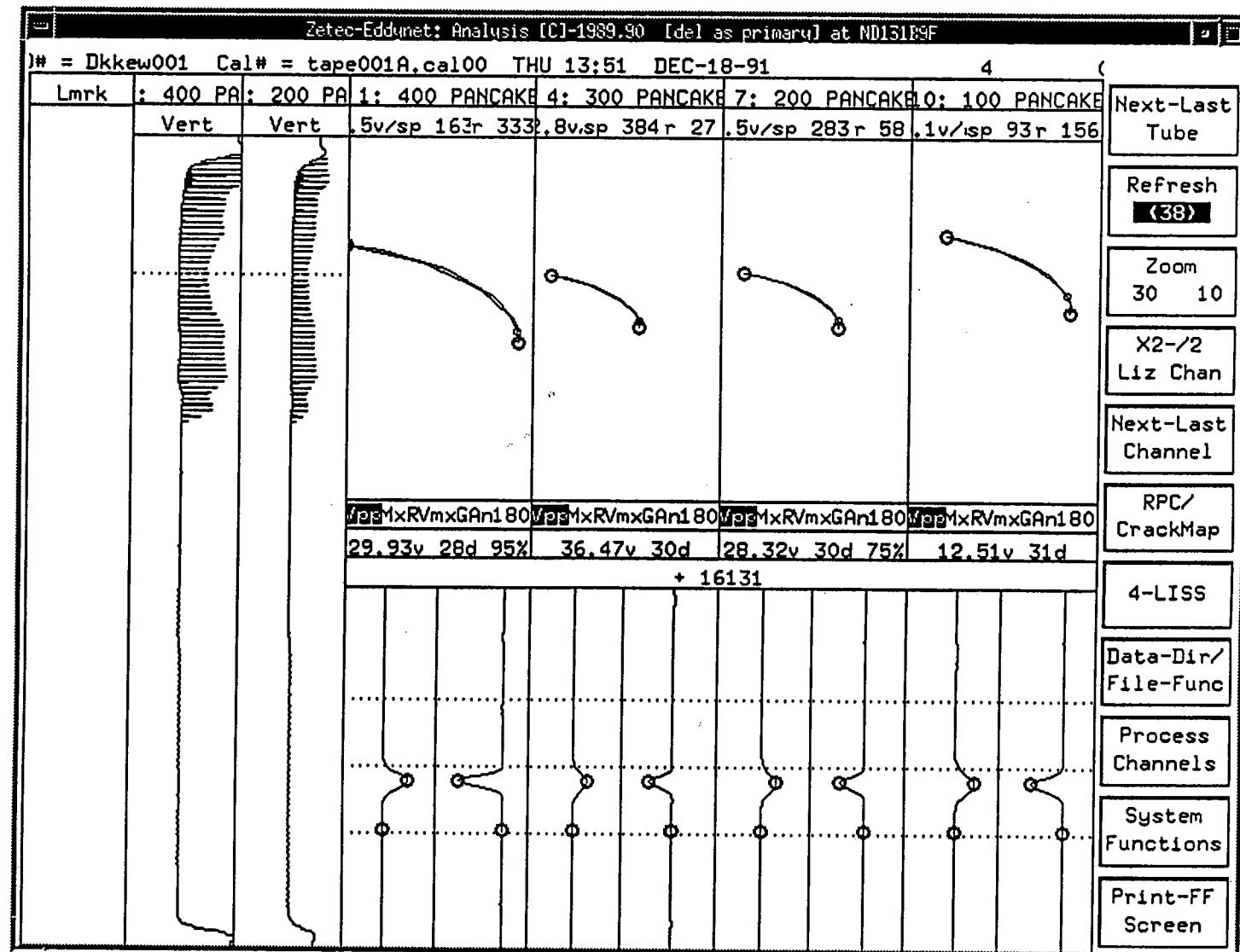


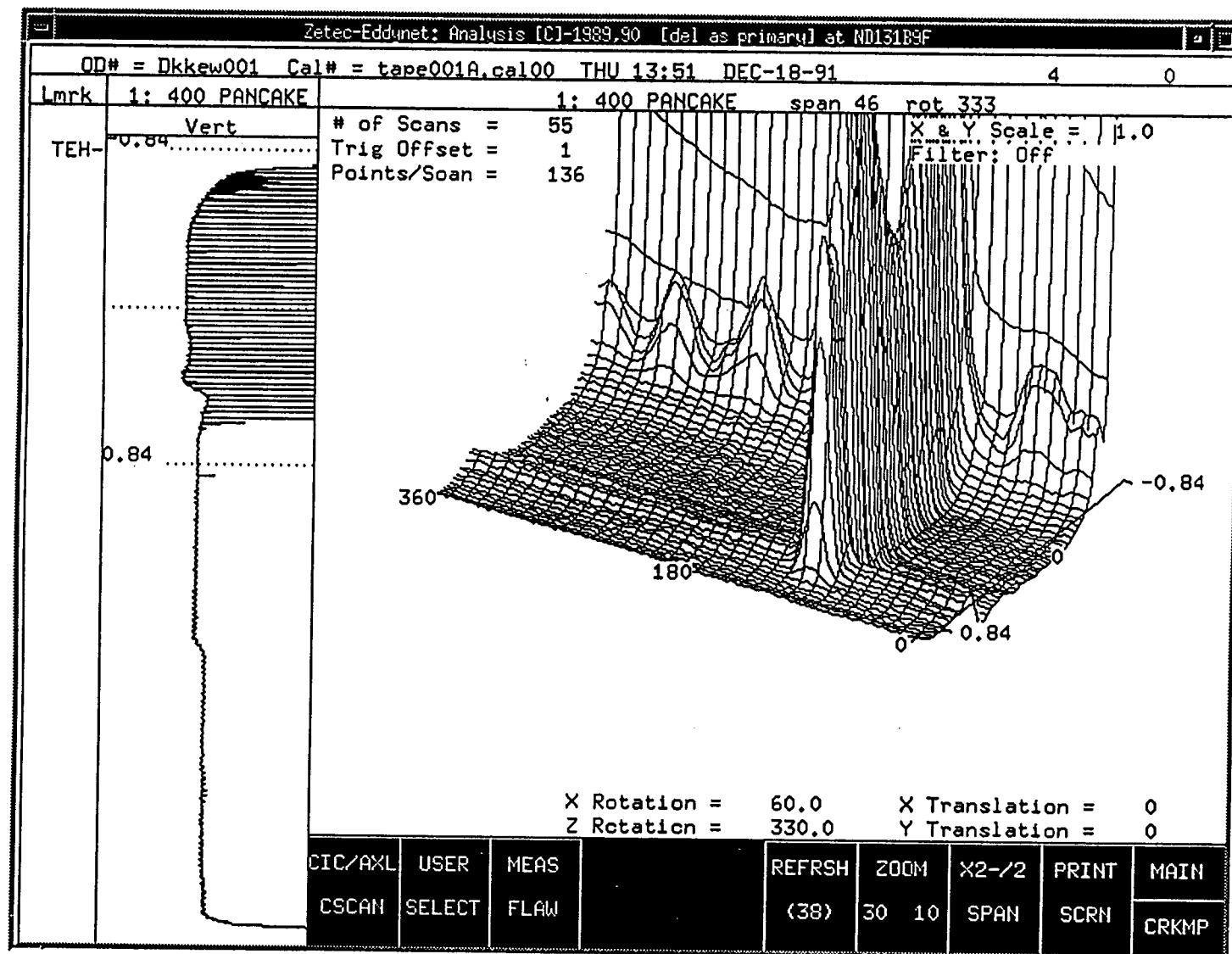


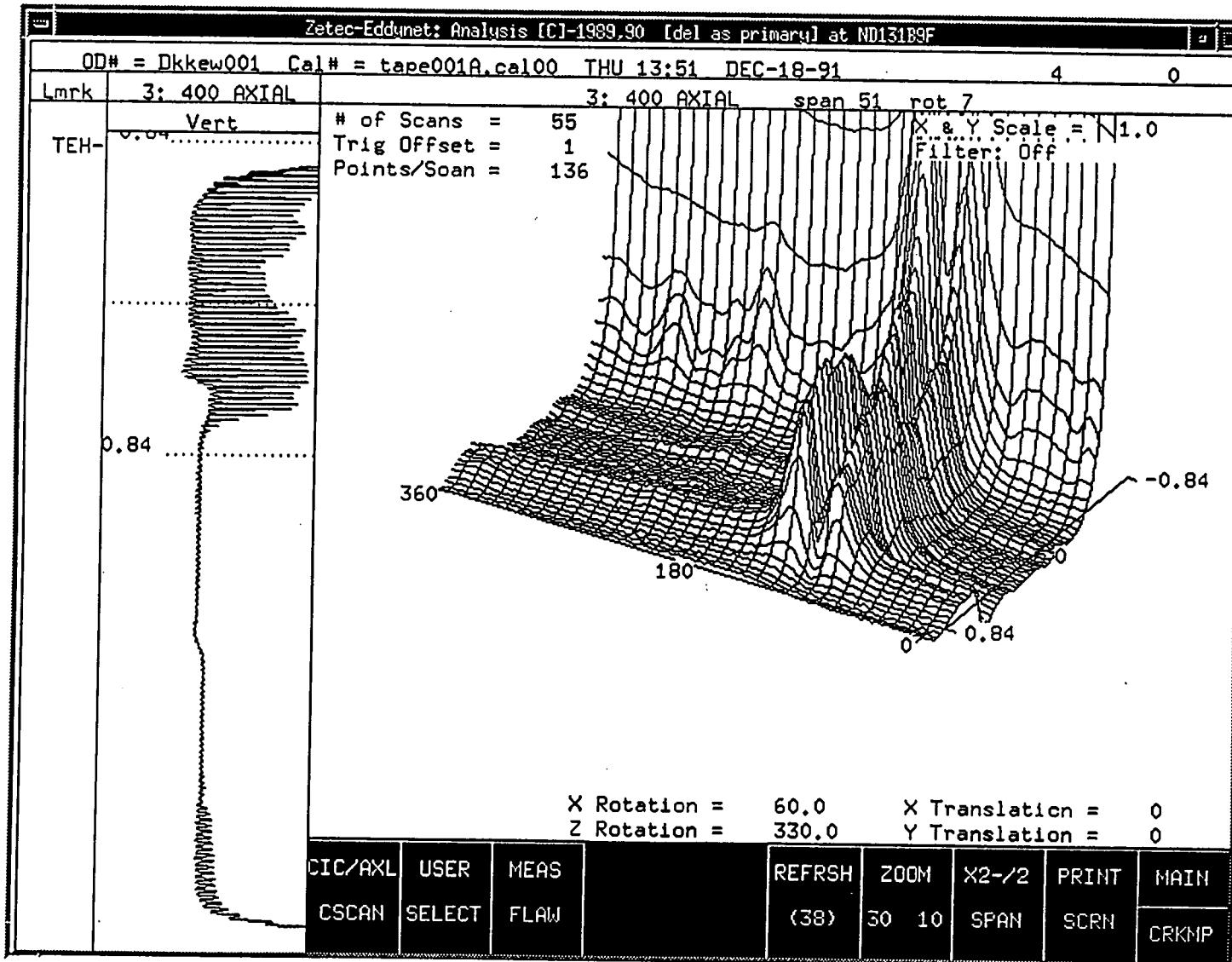


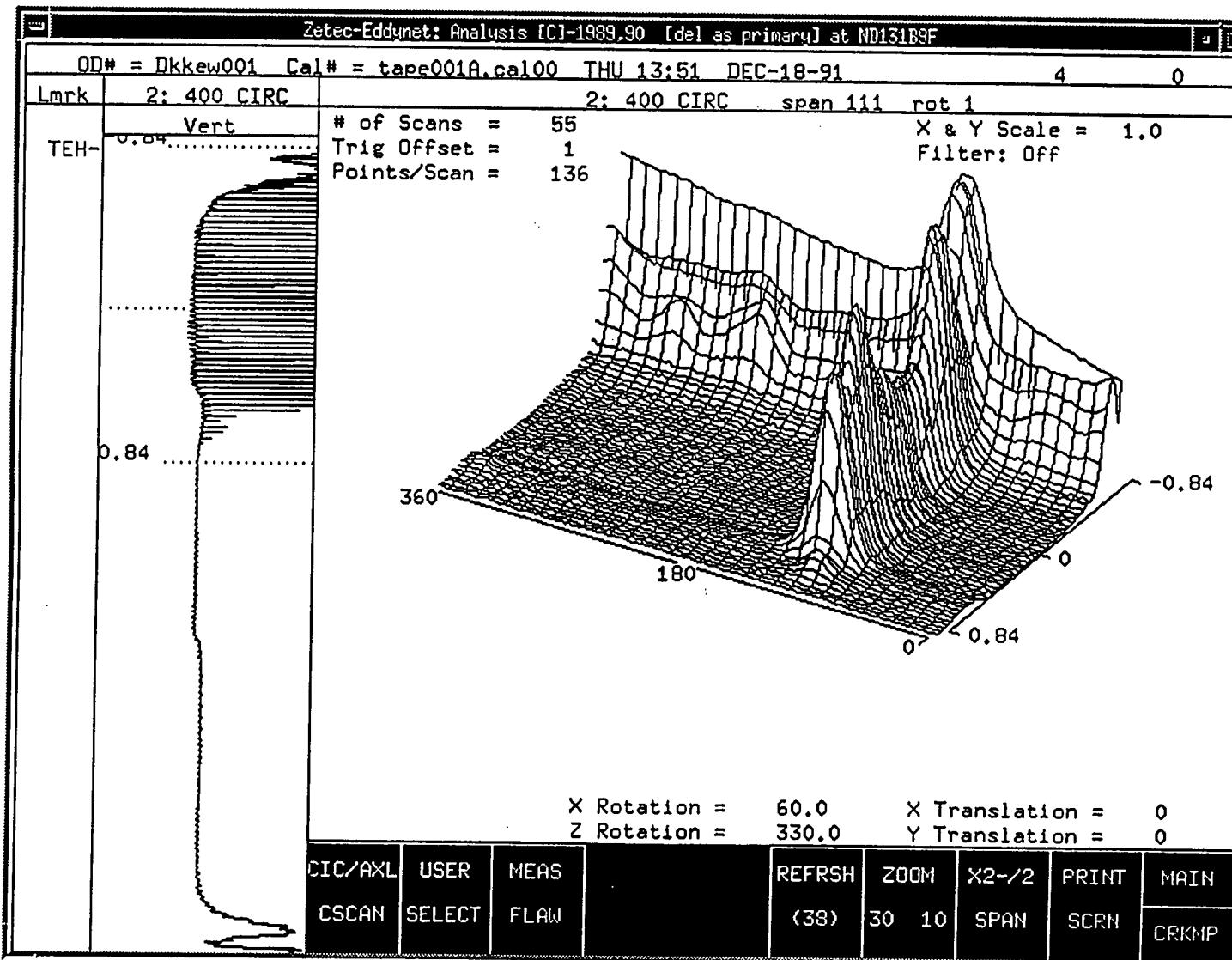
- 4 0 Next-Last Tube
- Refresh (39)
- Zoom 30 10
- X2-/2 Liz Chan
- Next-Last Channel
- RPC/ CrackMap
- 1-LISS
- Data-Dir/ File-Func
- Process Channels
- System Functions
- Print-FF Screen

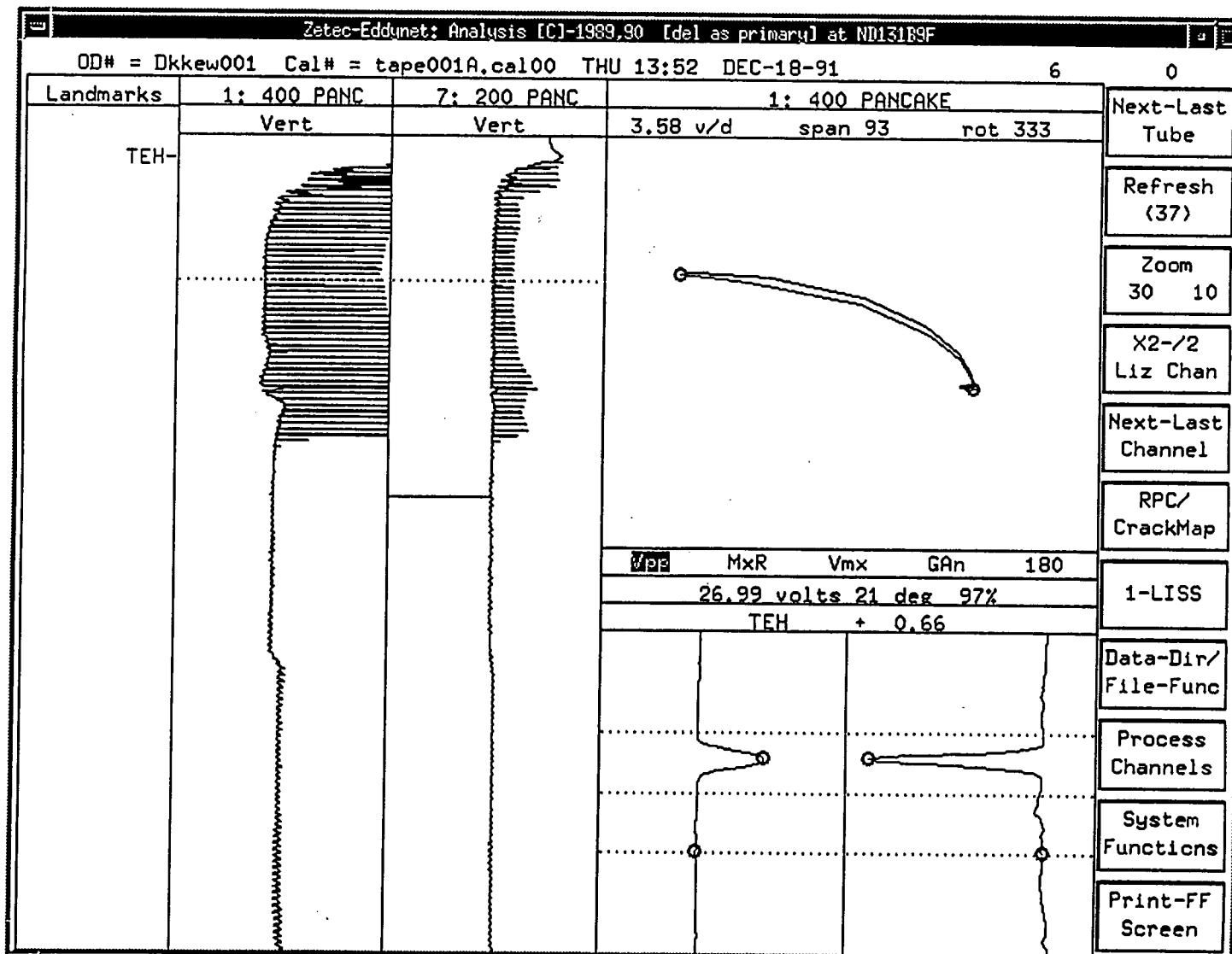


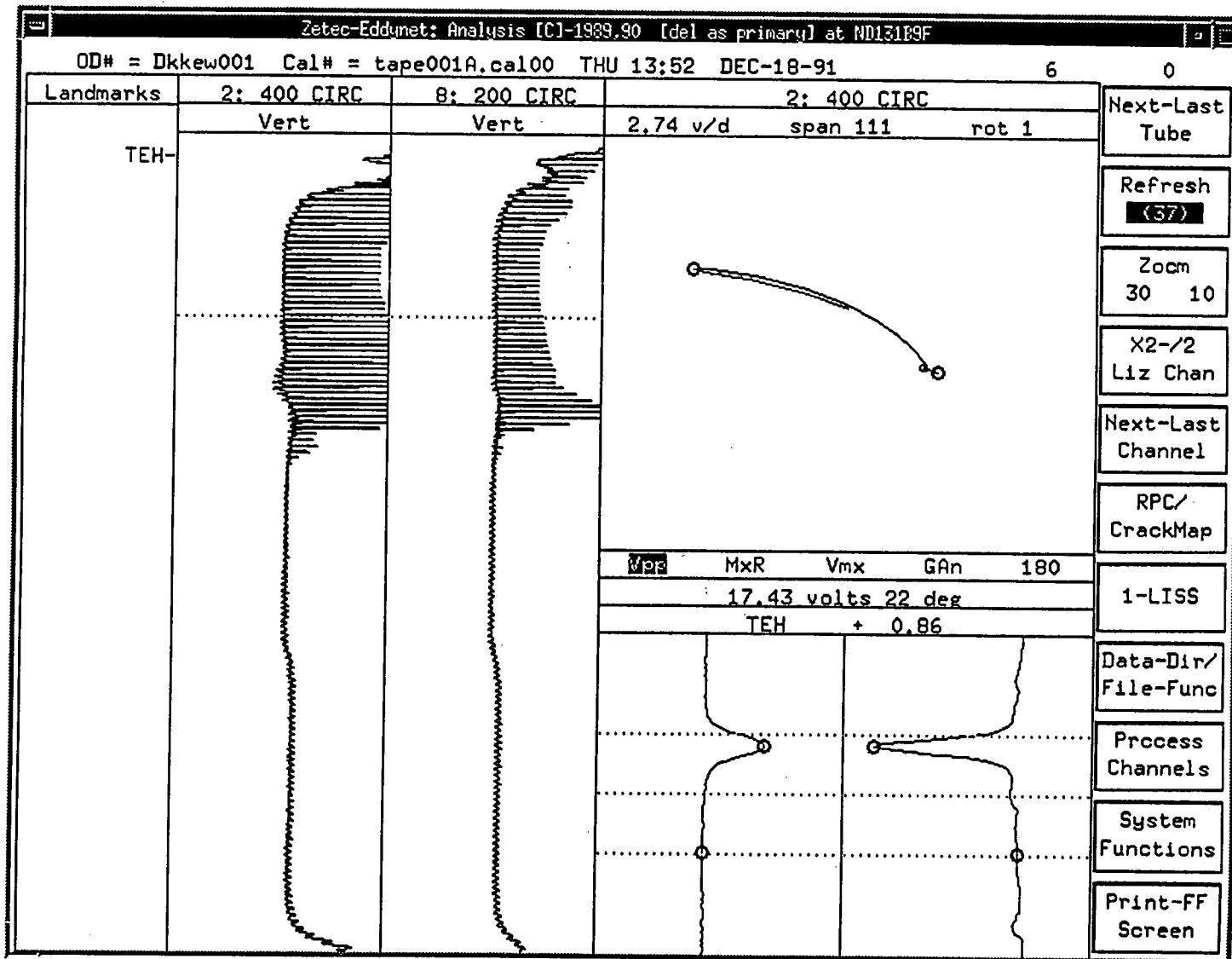


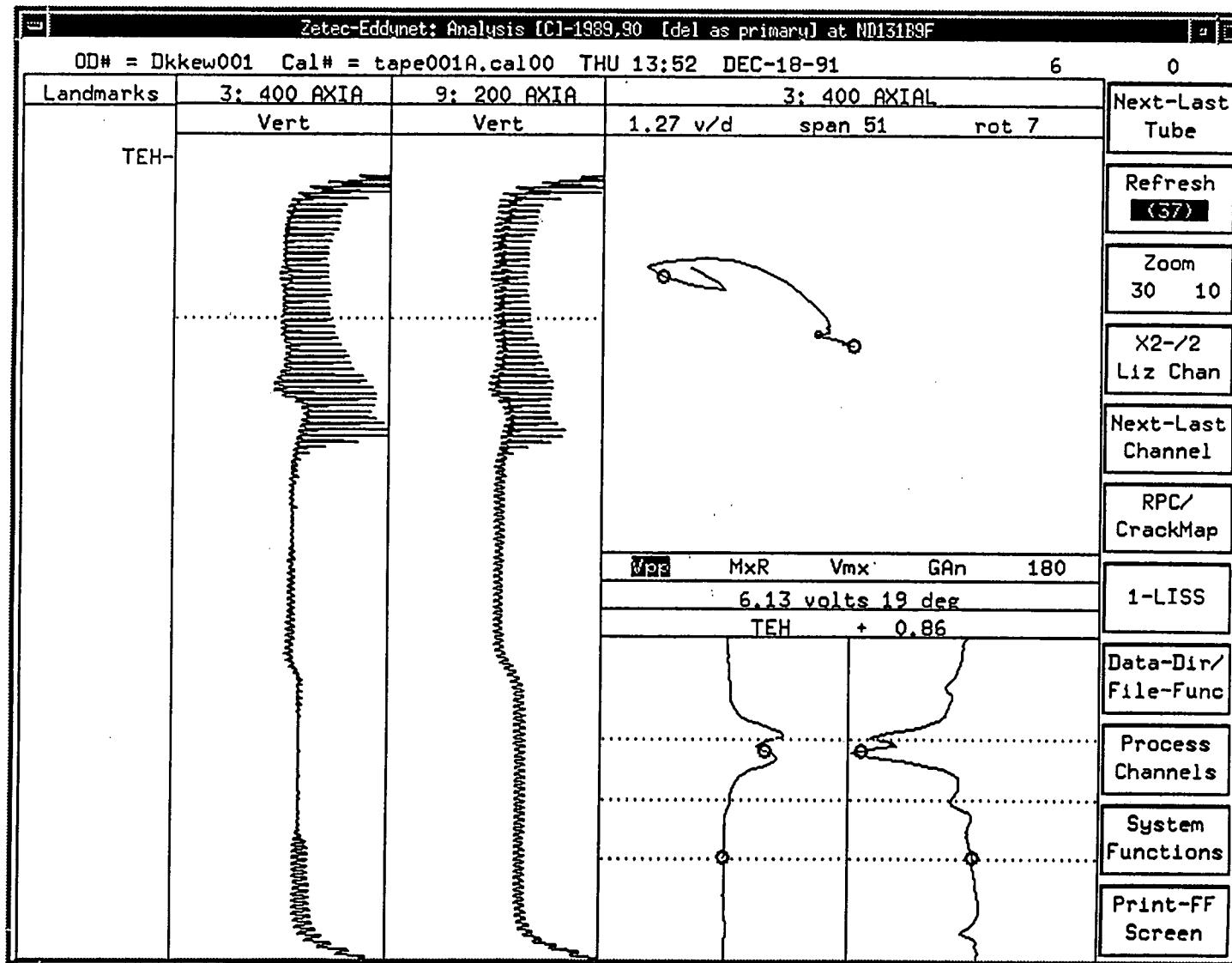


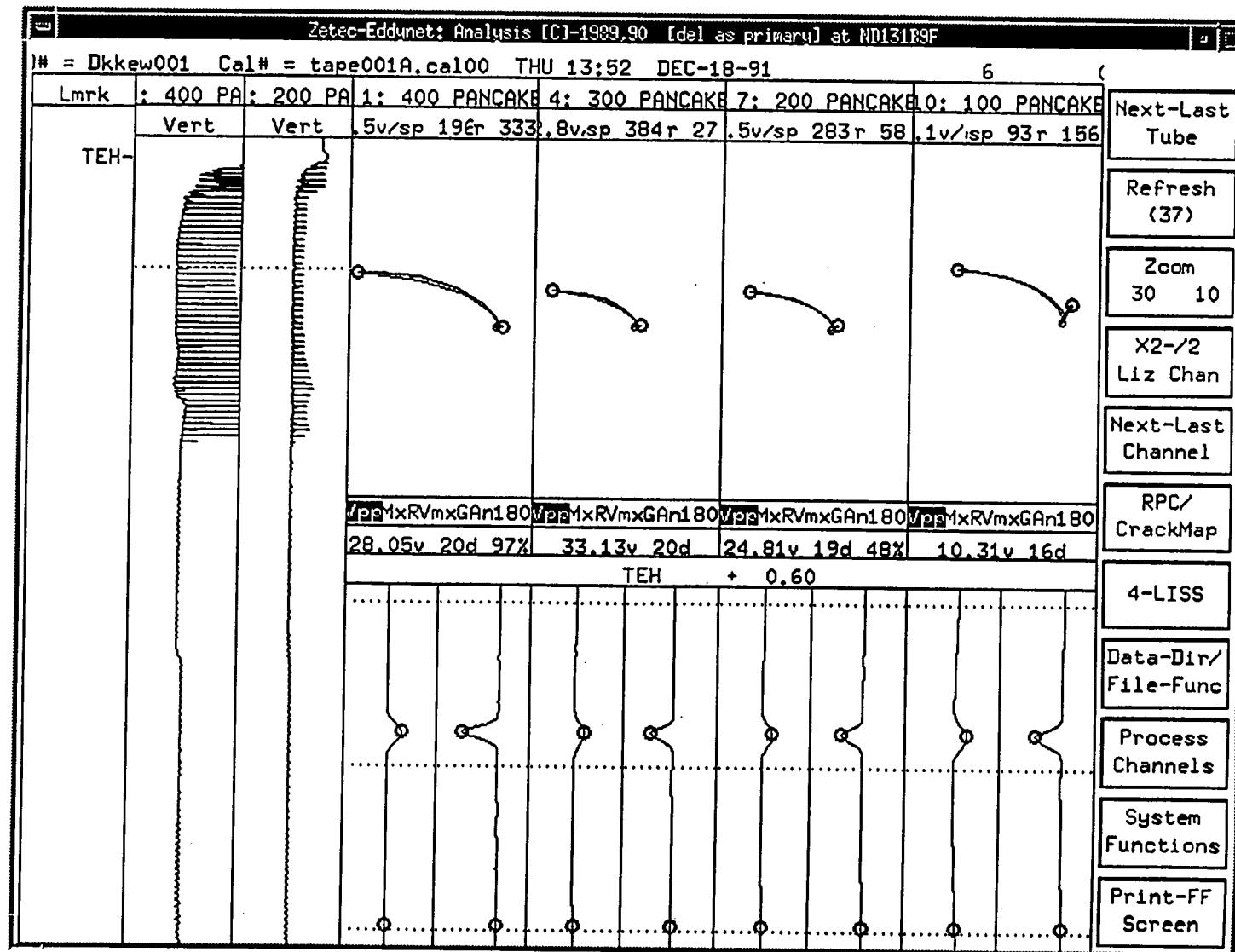


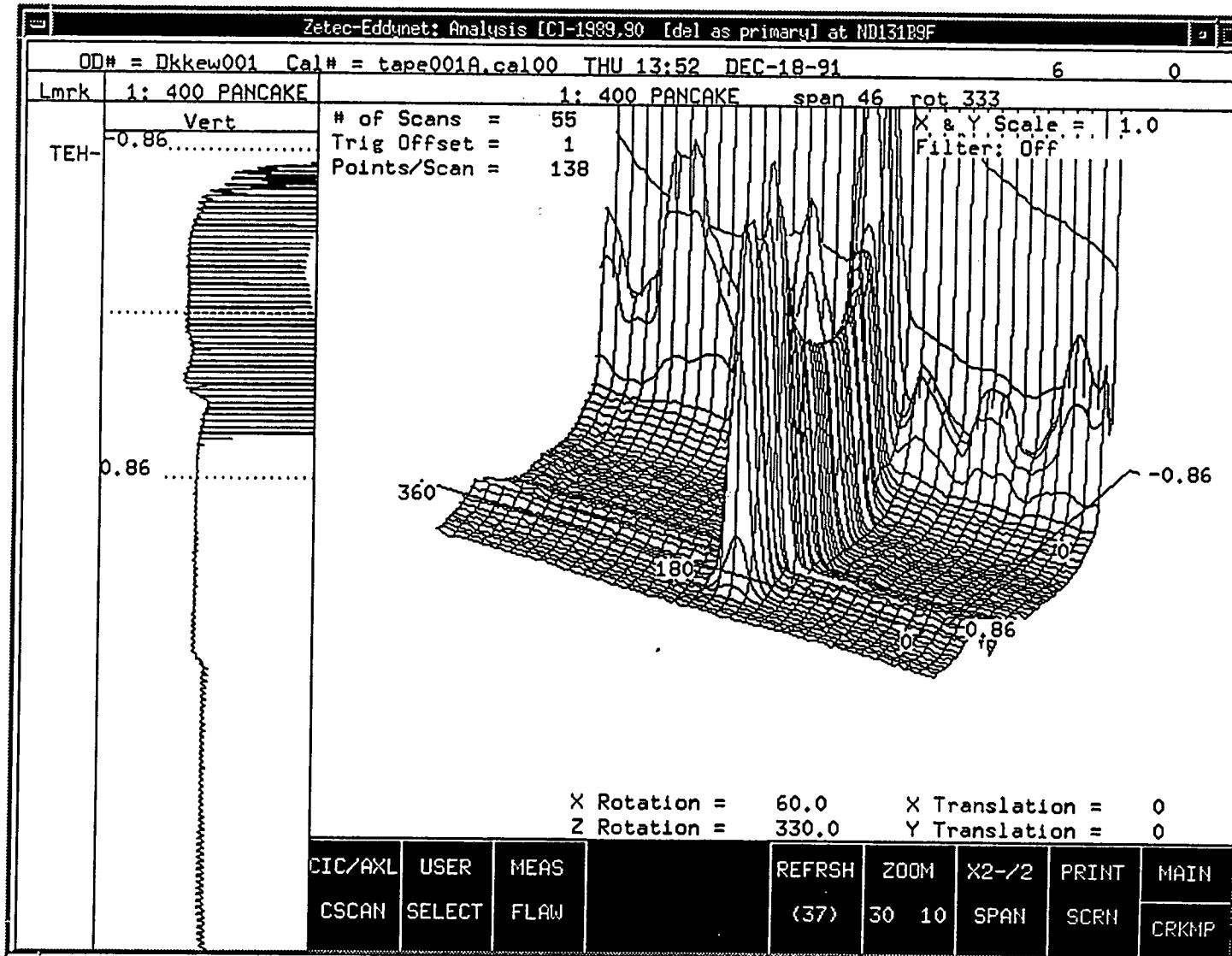


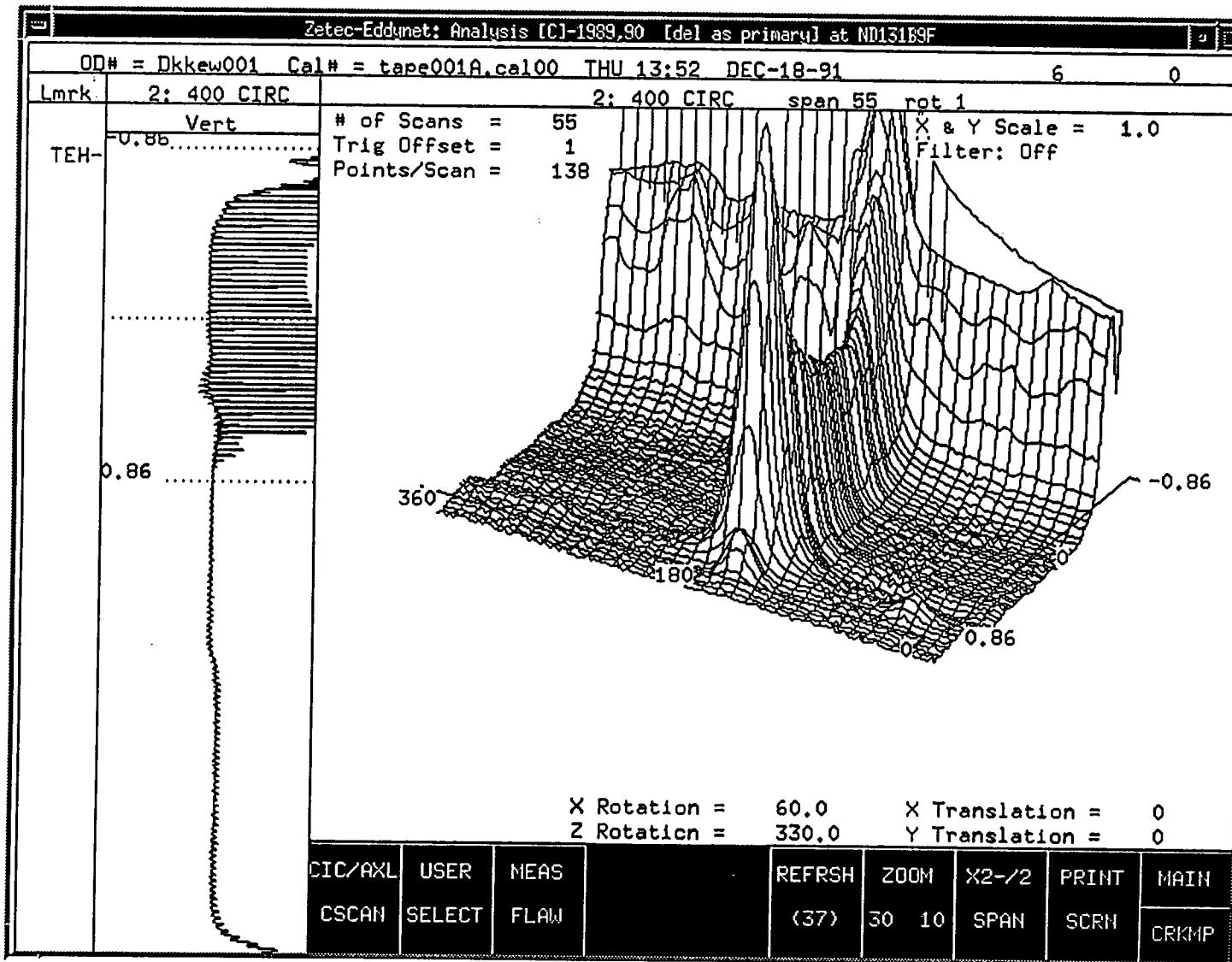


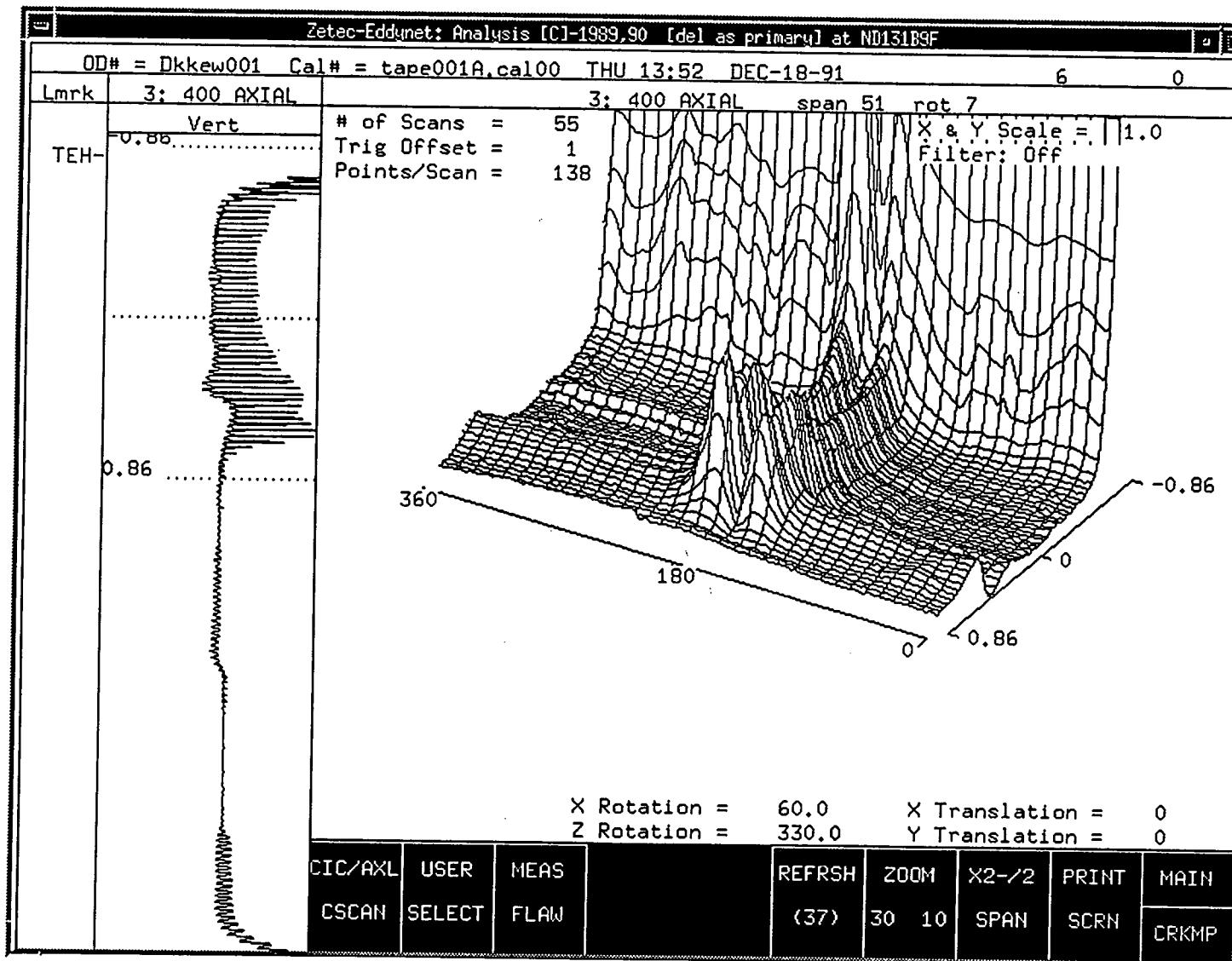


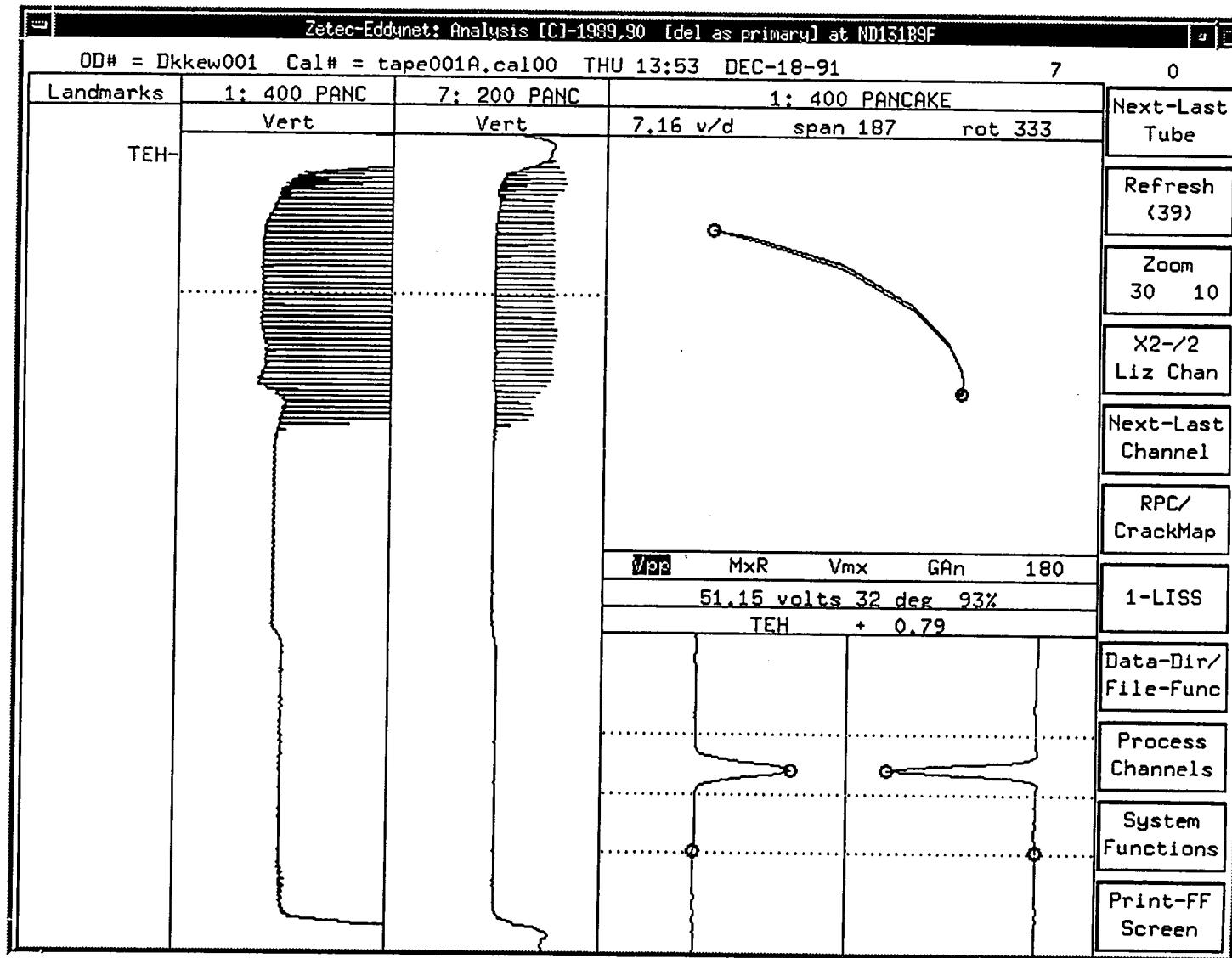


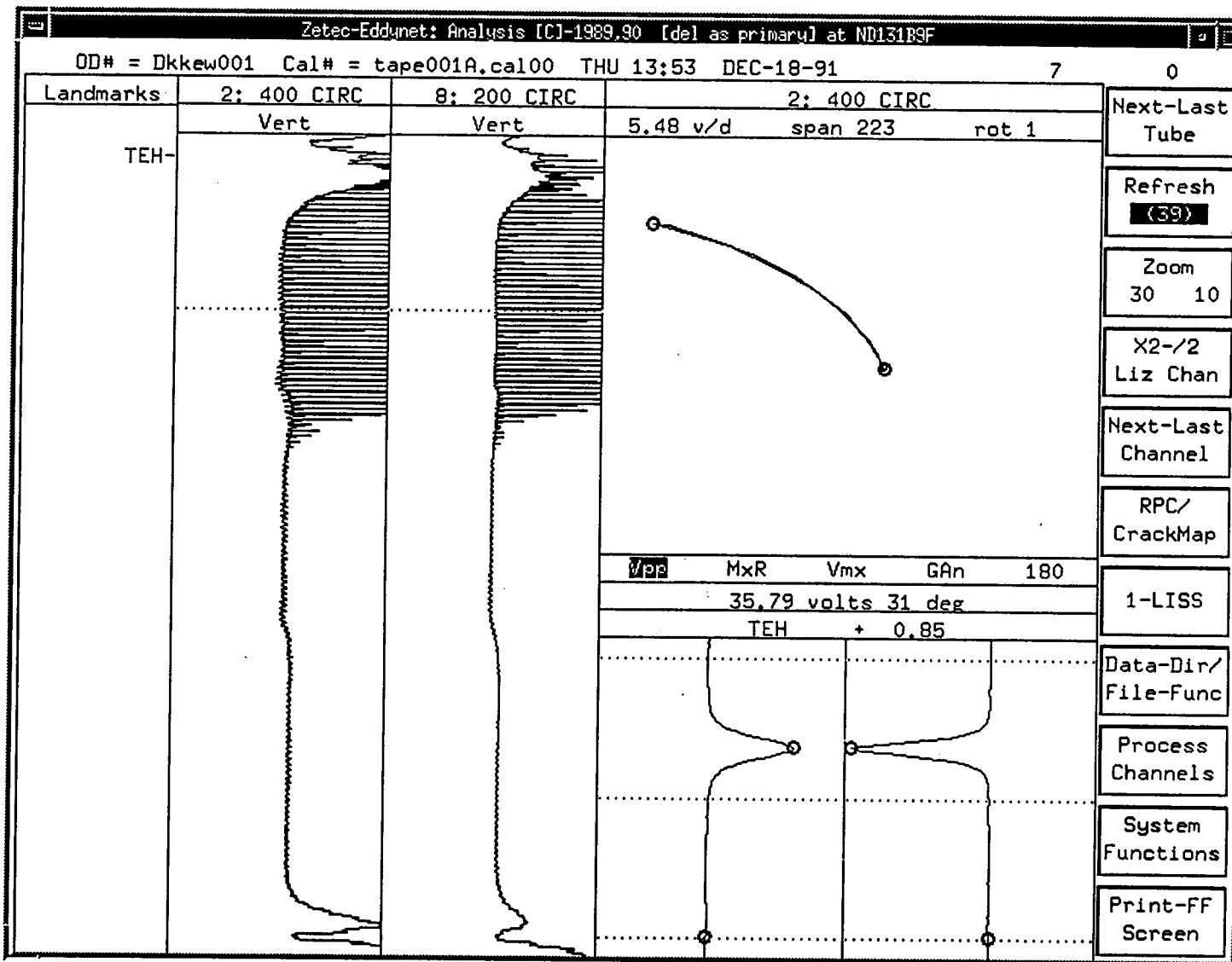


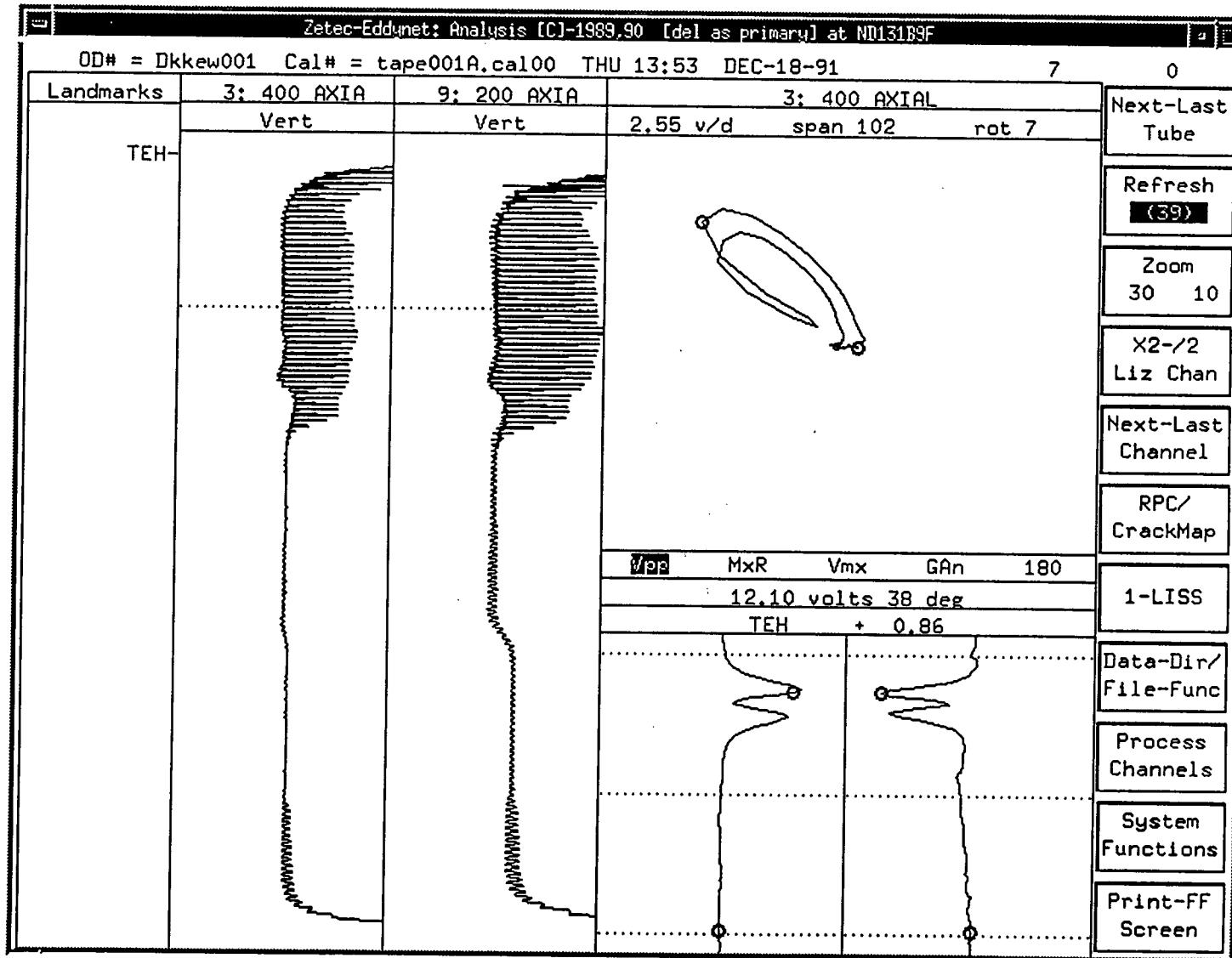


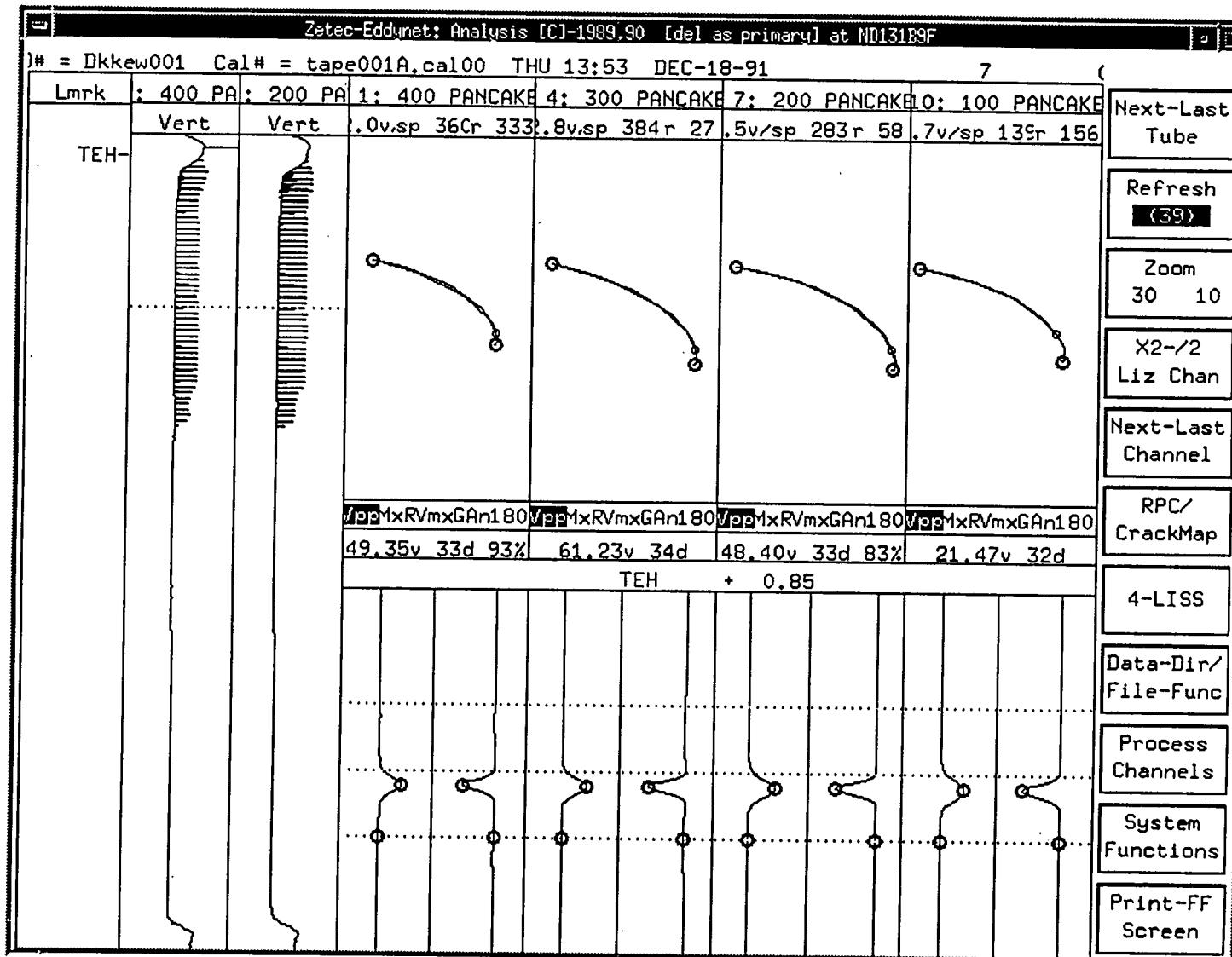


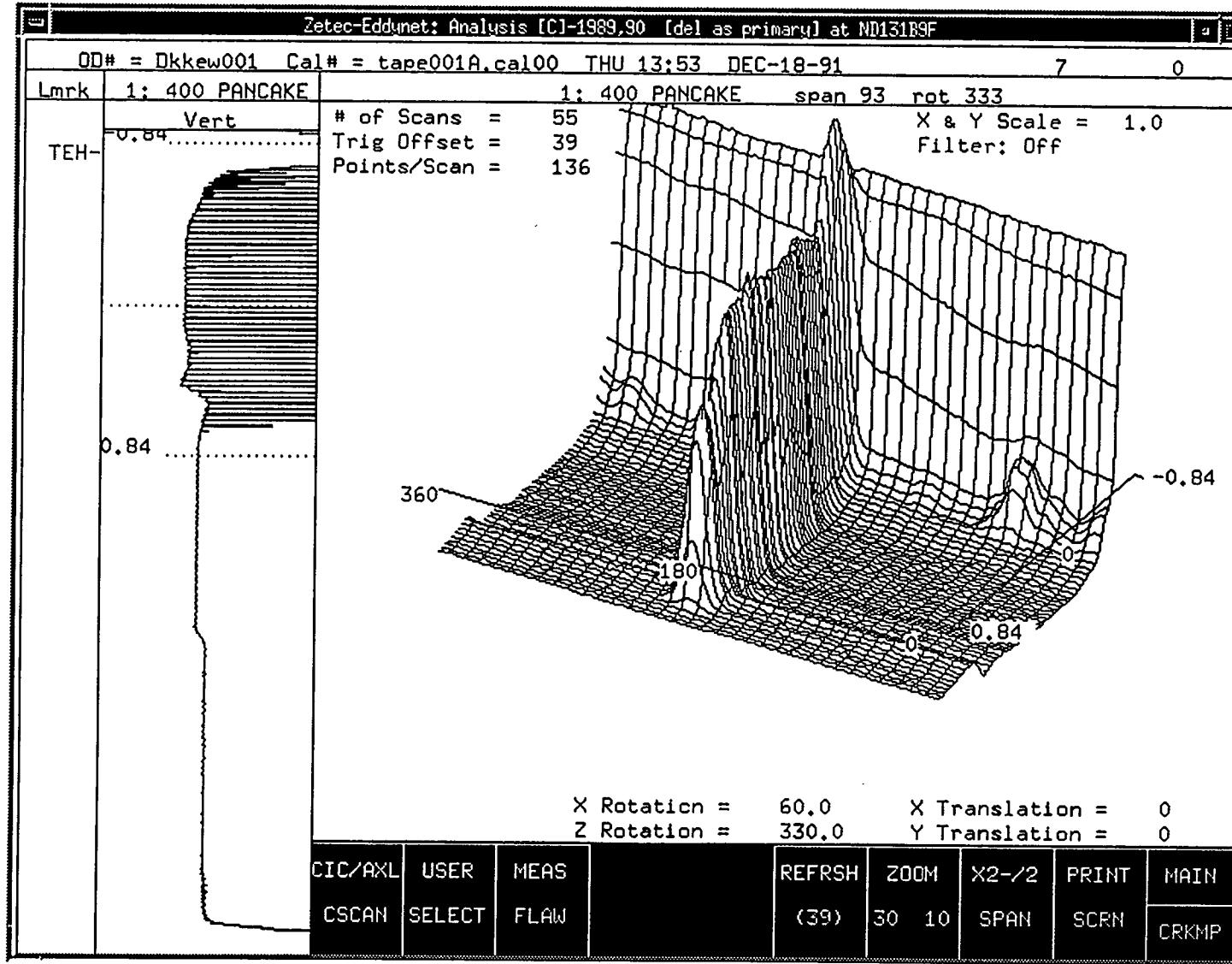






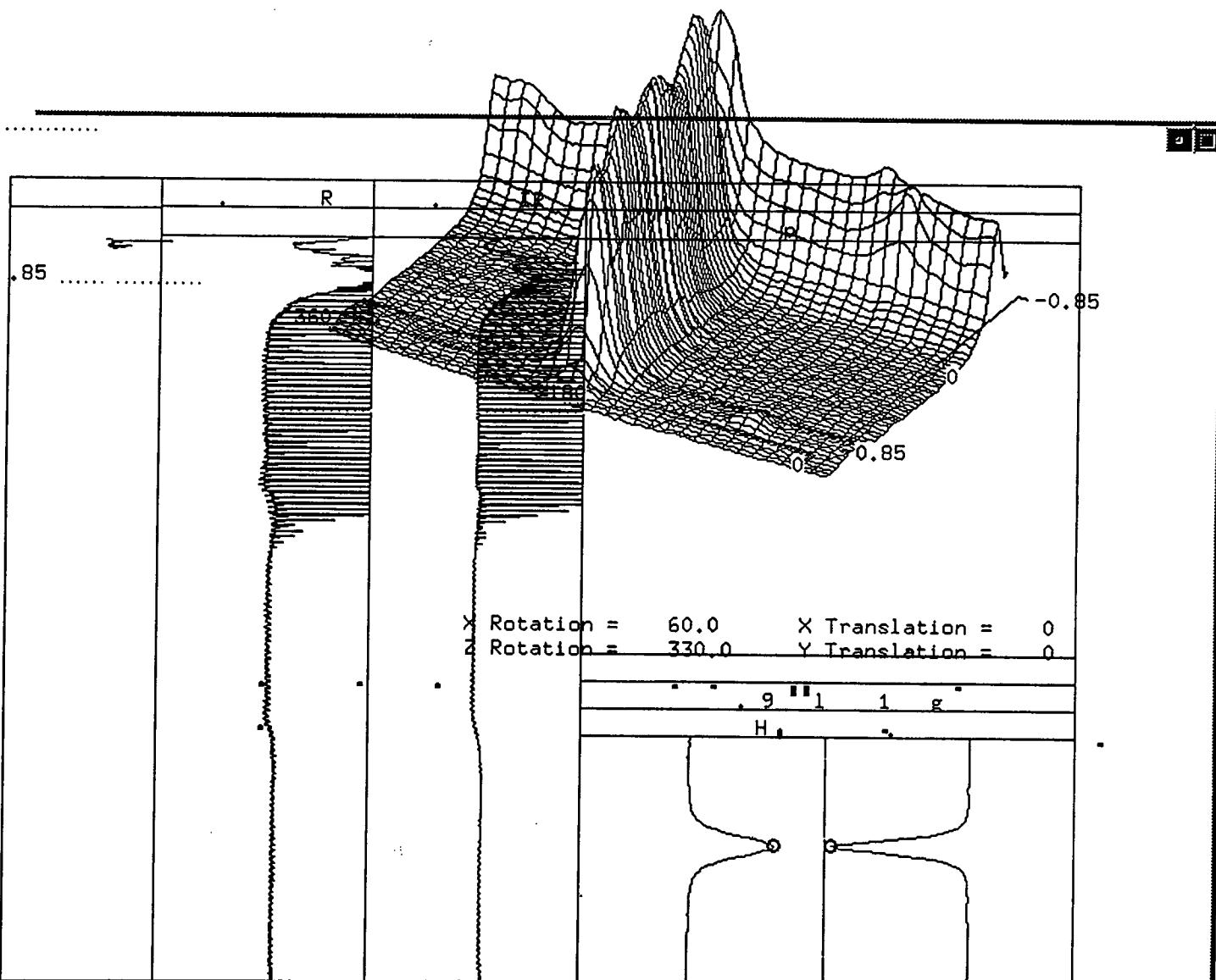


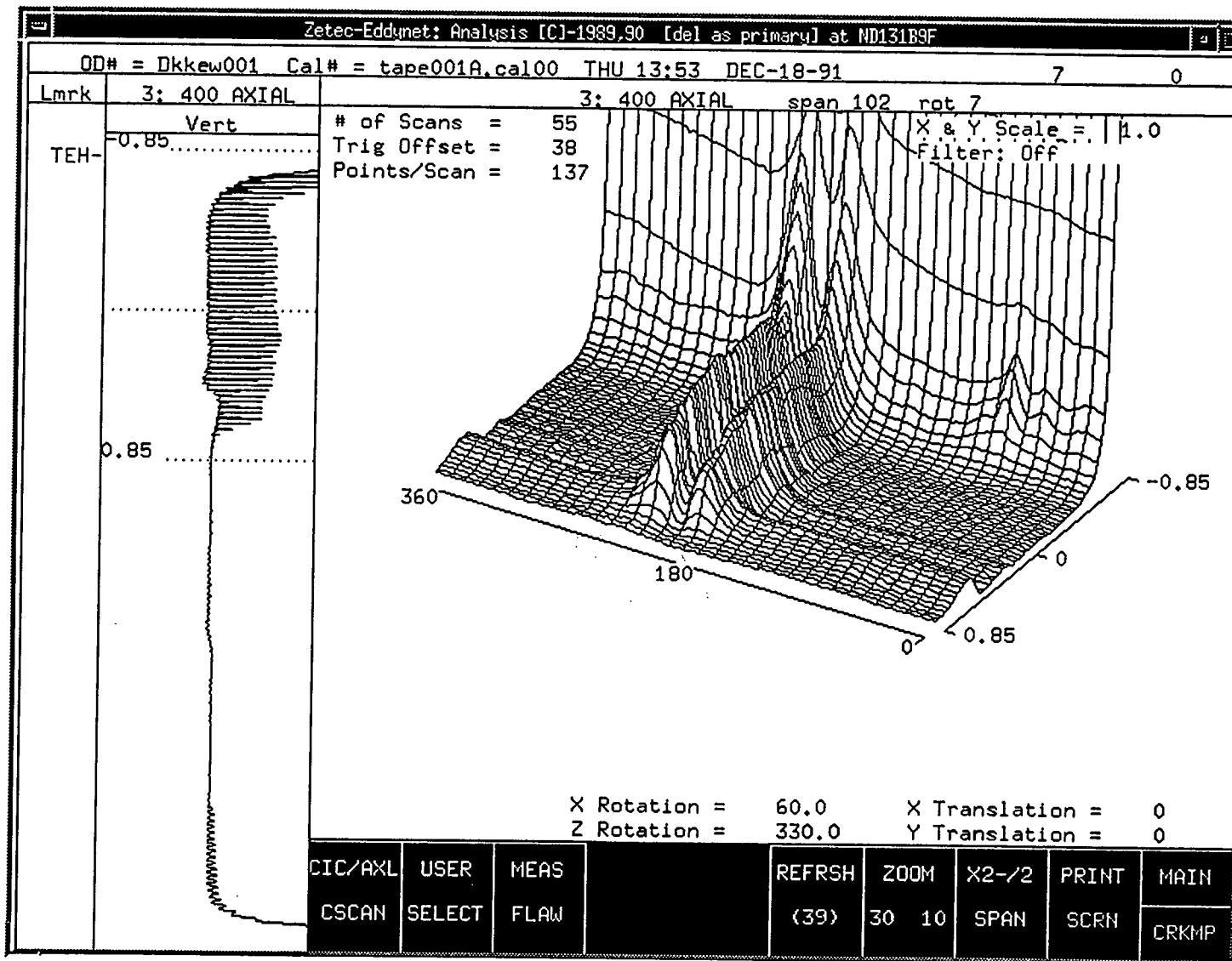


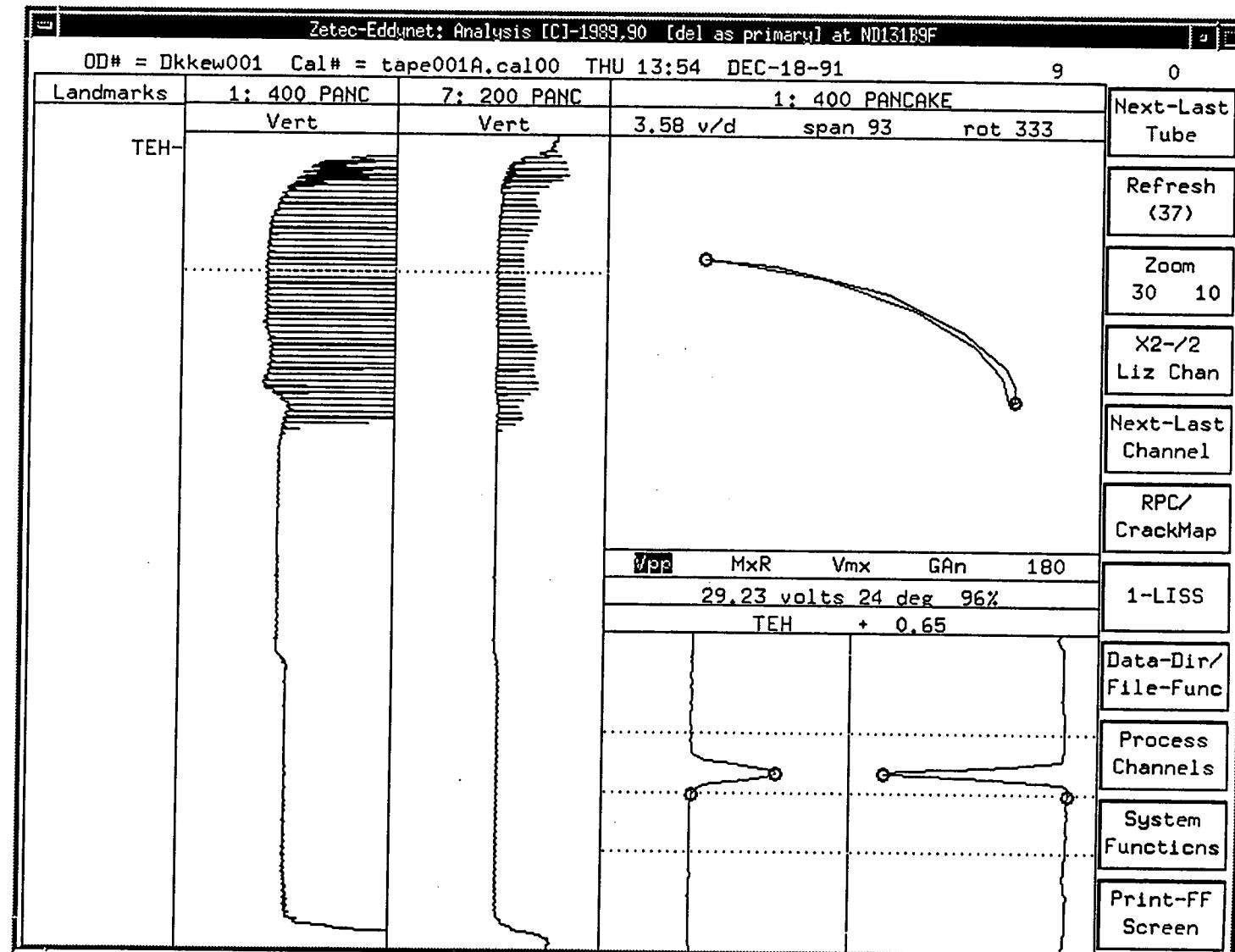


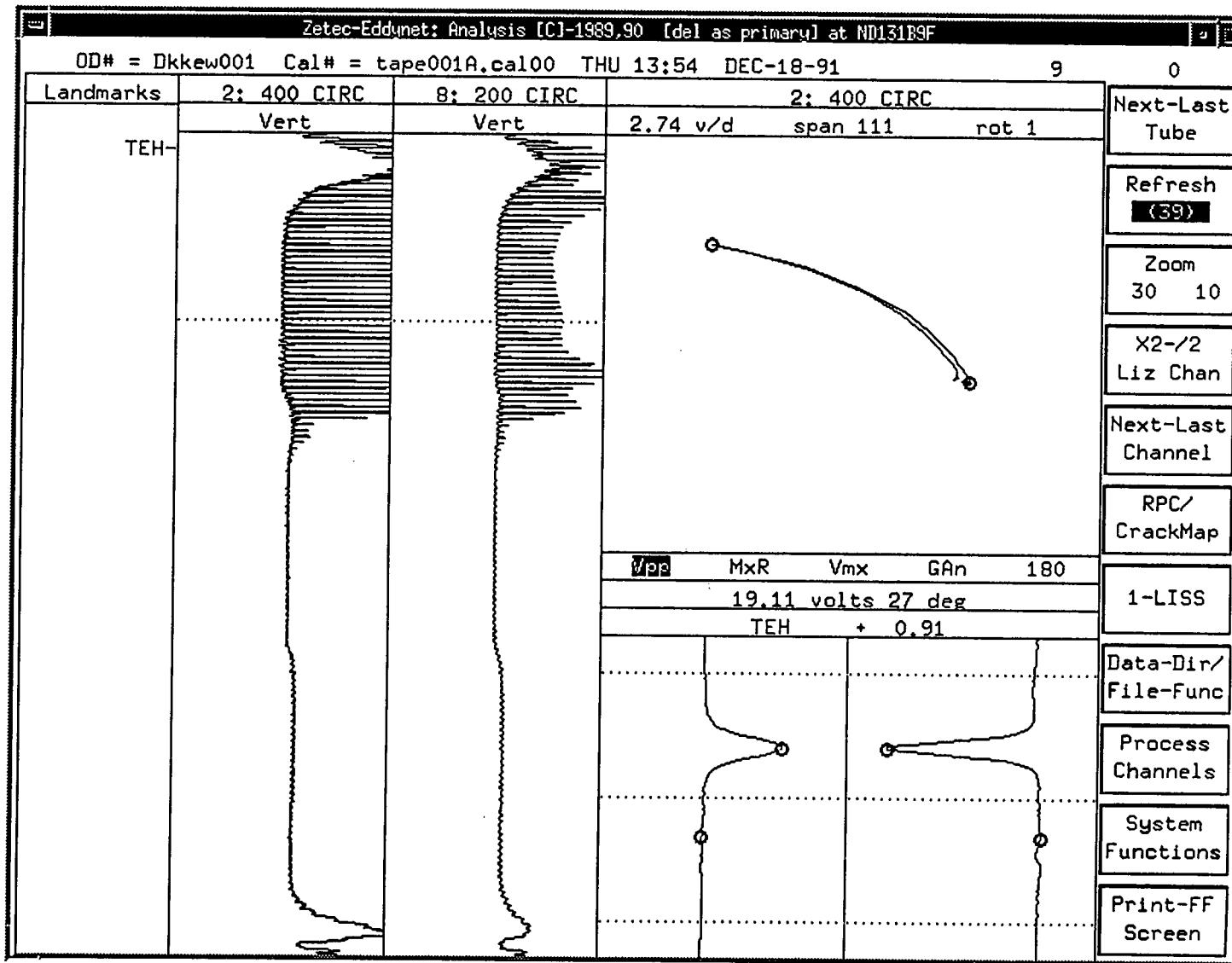
Zetec-EddyNet: Analysis [C]-1989,90 [del as primary] at ND131B9F

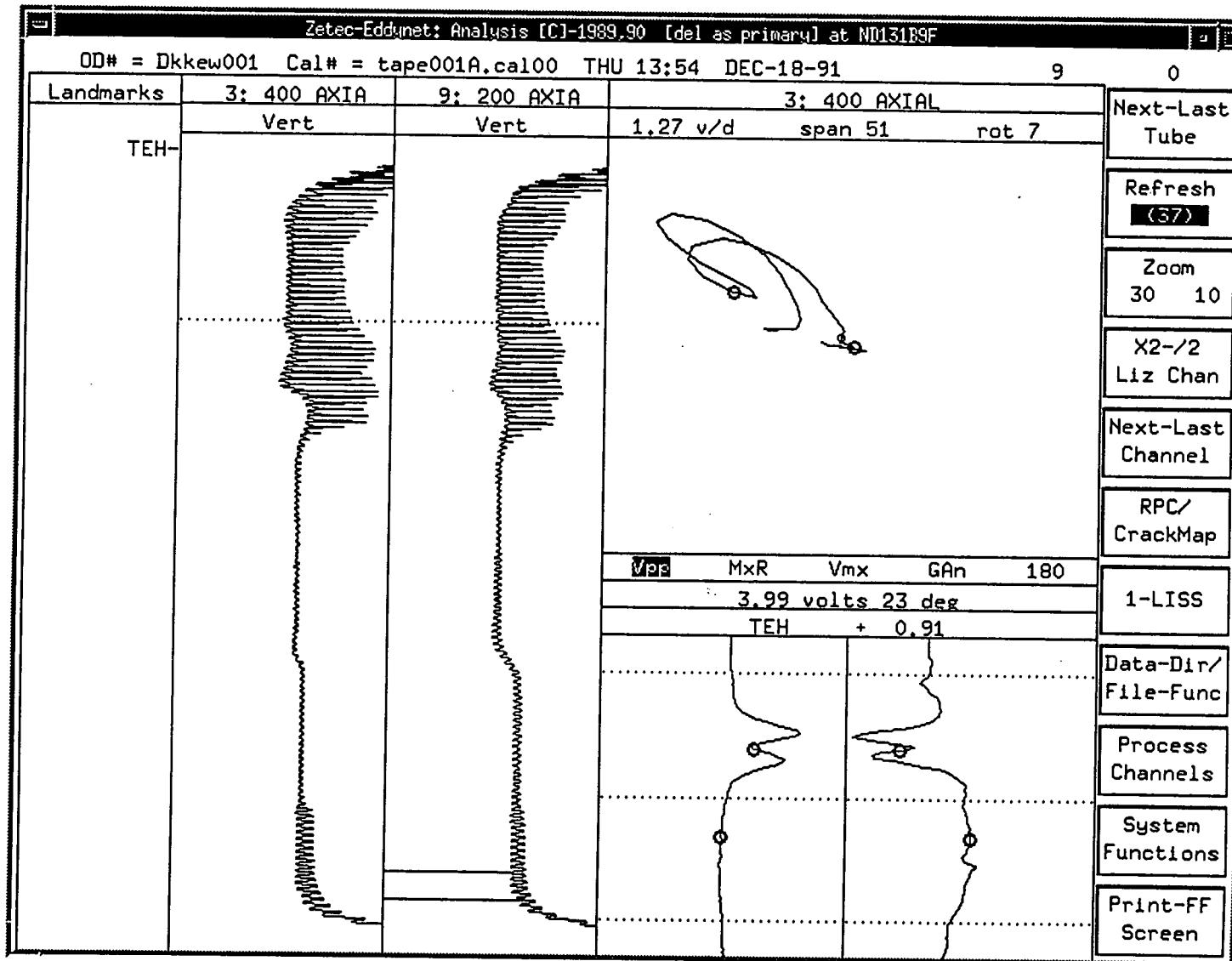
OD# = Dkkew 0 Ca # = ta e0 1 cal00 THU 13:53 D C-18-
 L r 2° 4 0 C • 4 0 IRC s a 111 rot
 V rt # of Scans = 55 X & Y Scale = 1.0
 TEH- • Trig Offset = 38 Filter: Off
 Points/Scan = 137

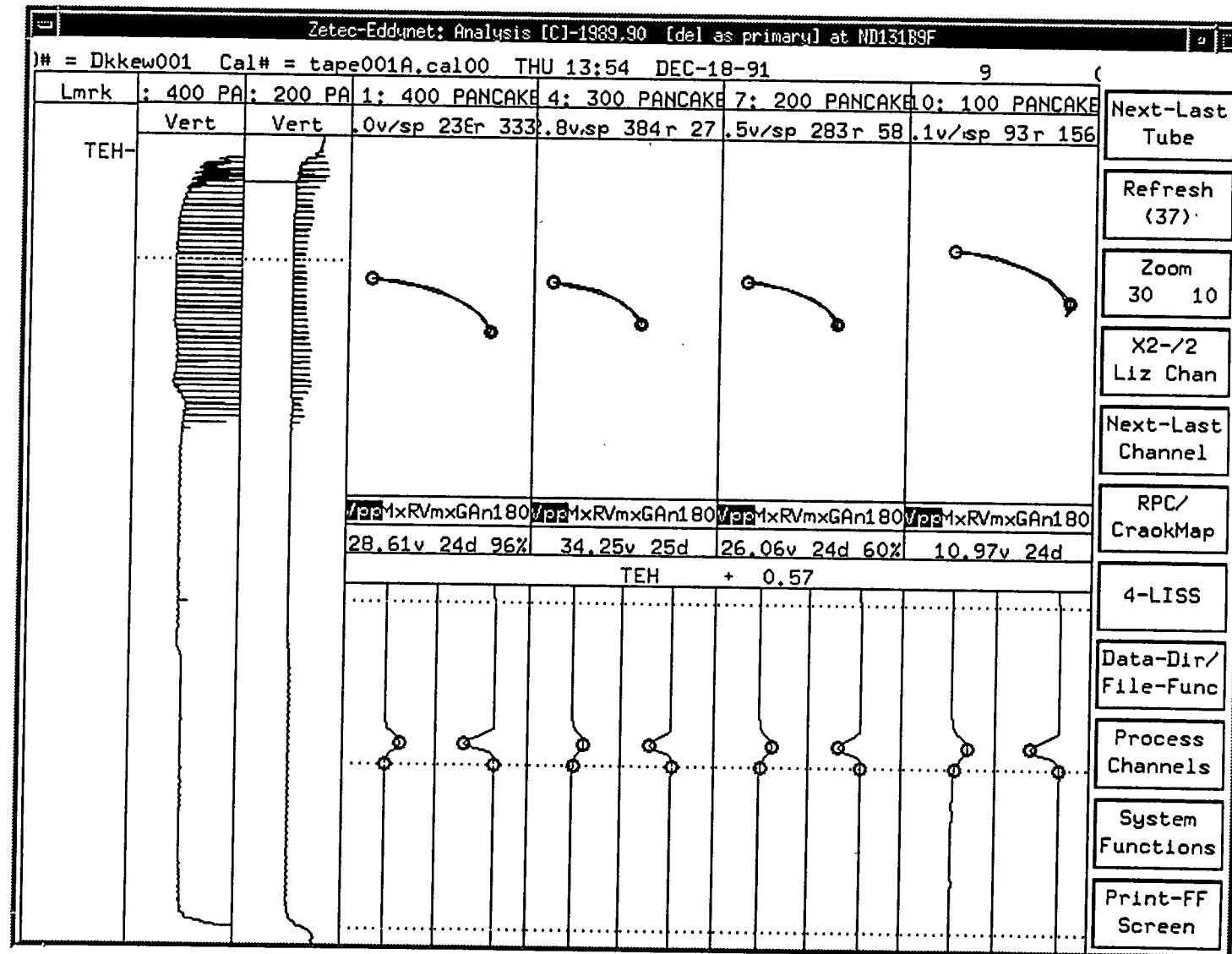


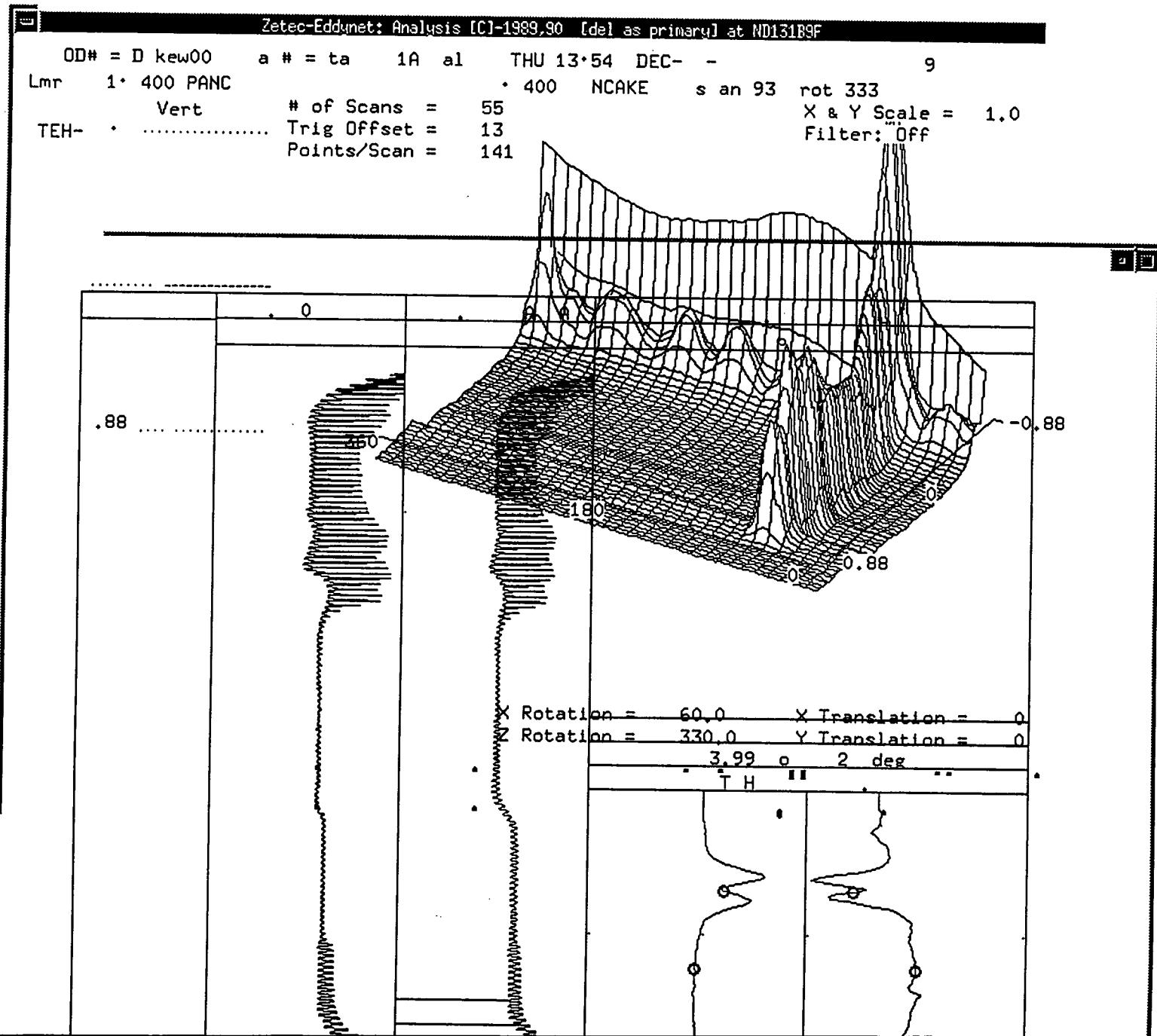


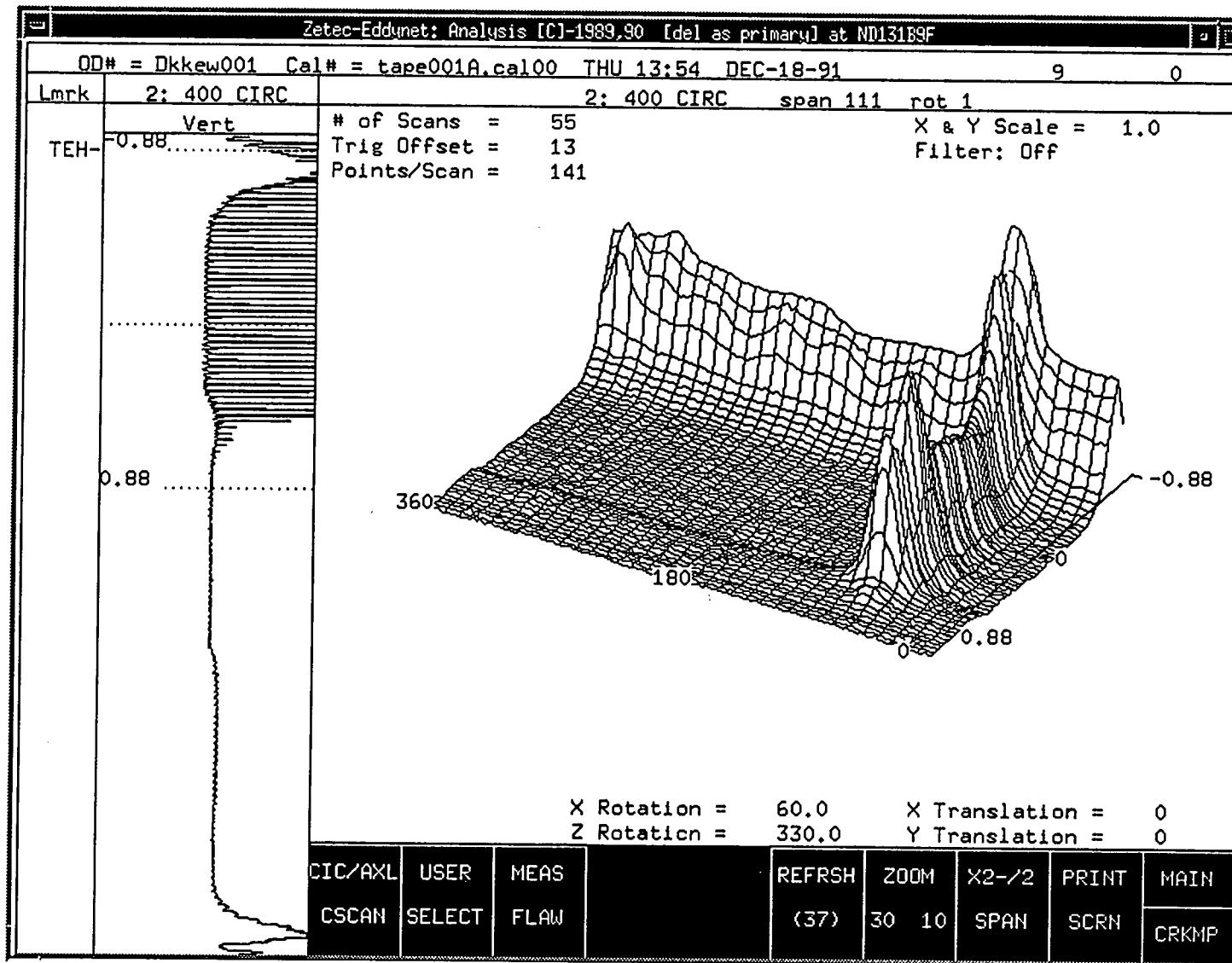


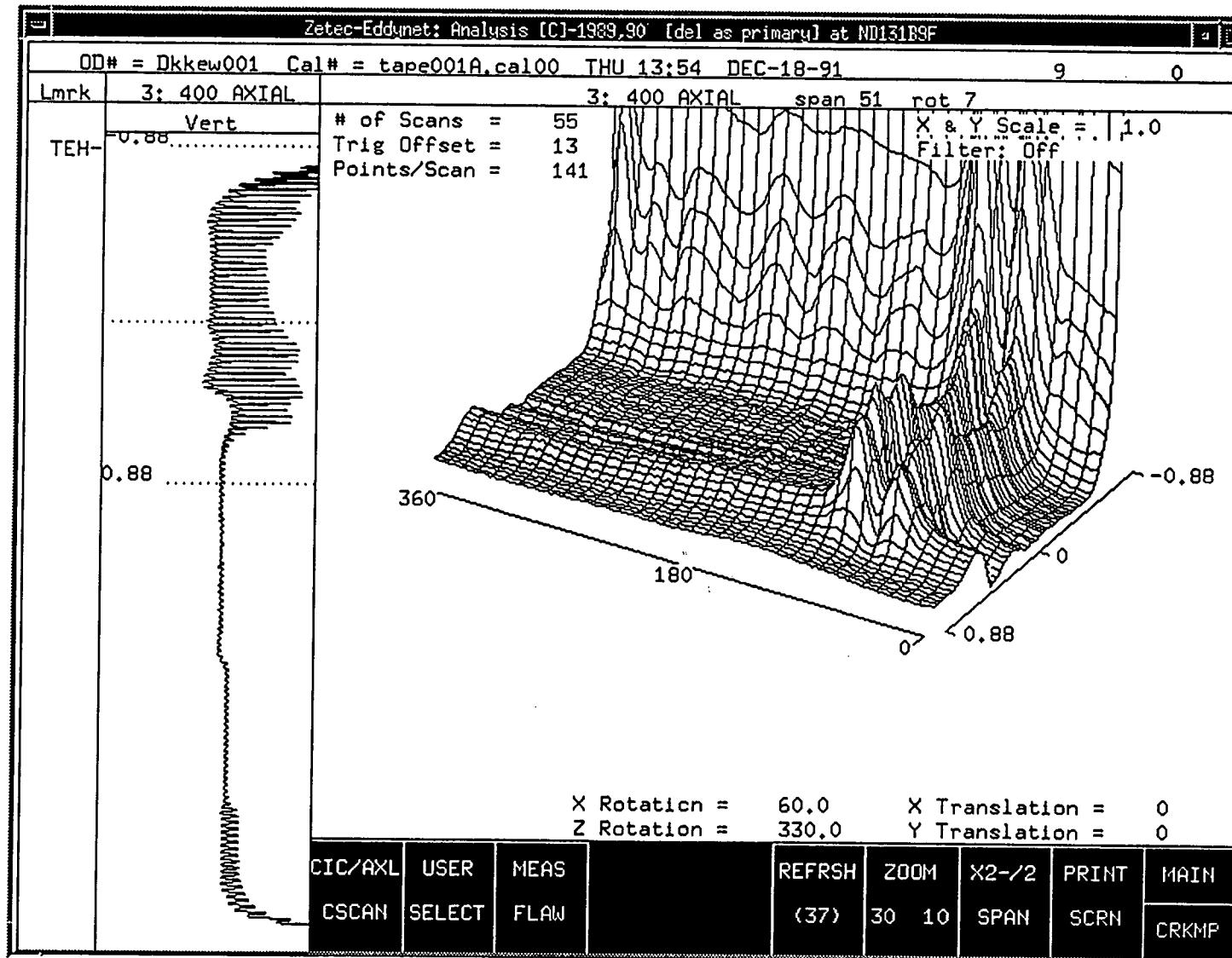


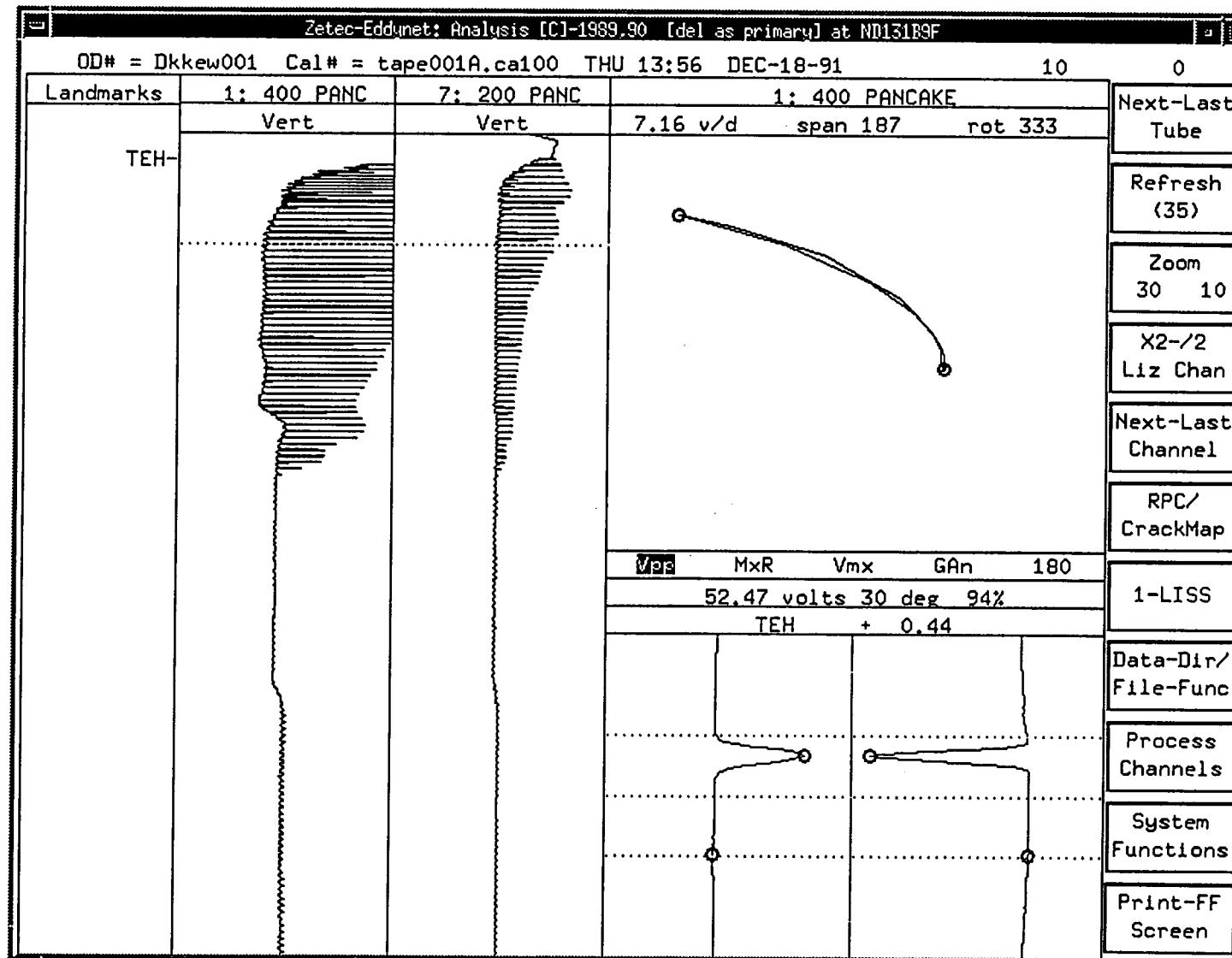


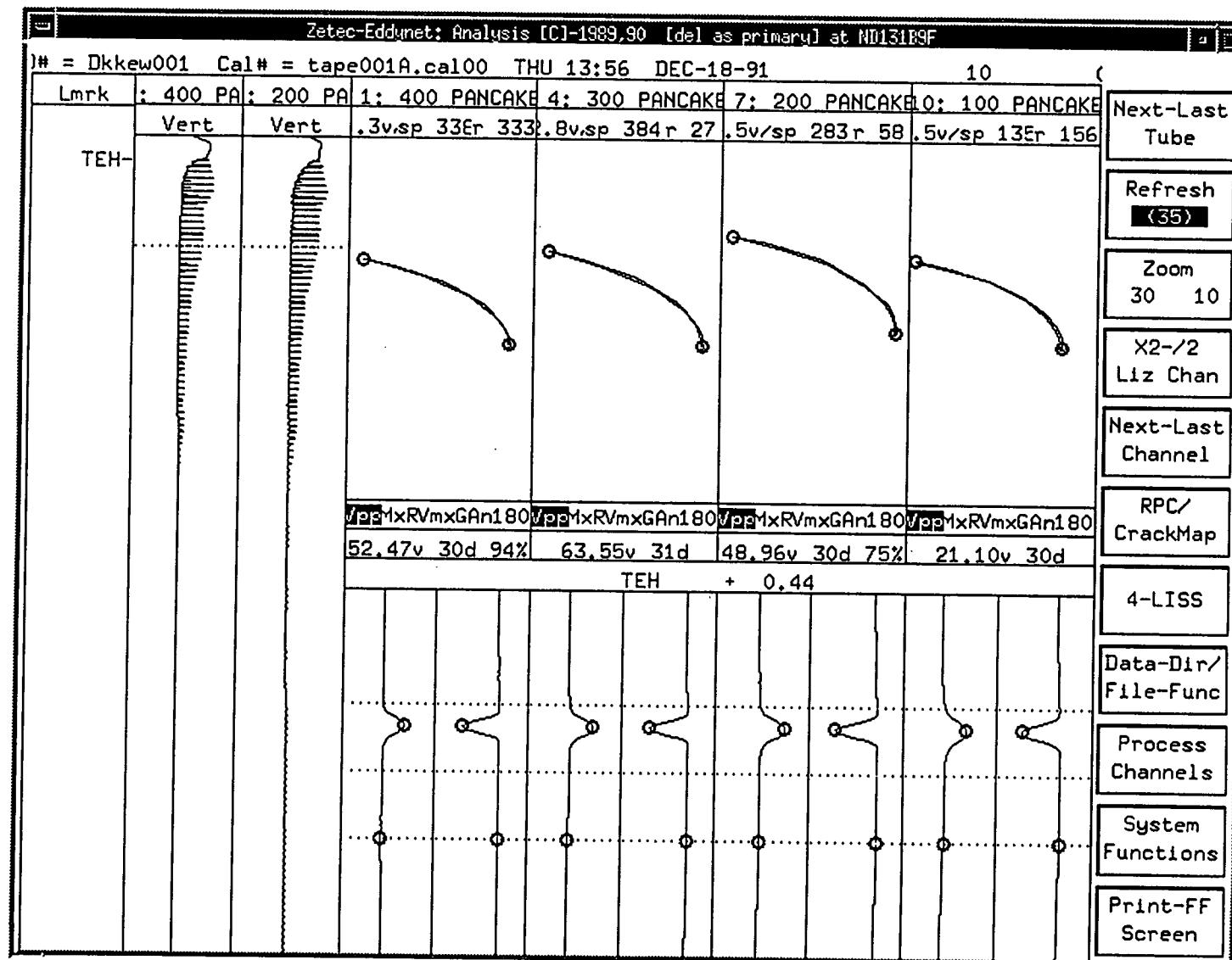


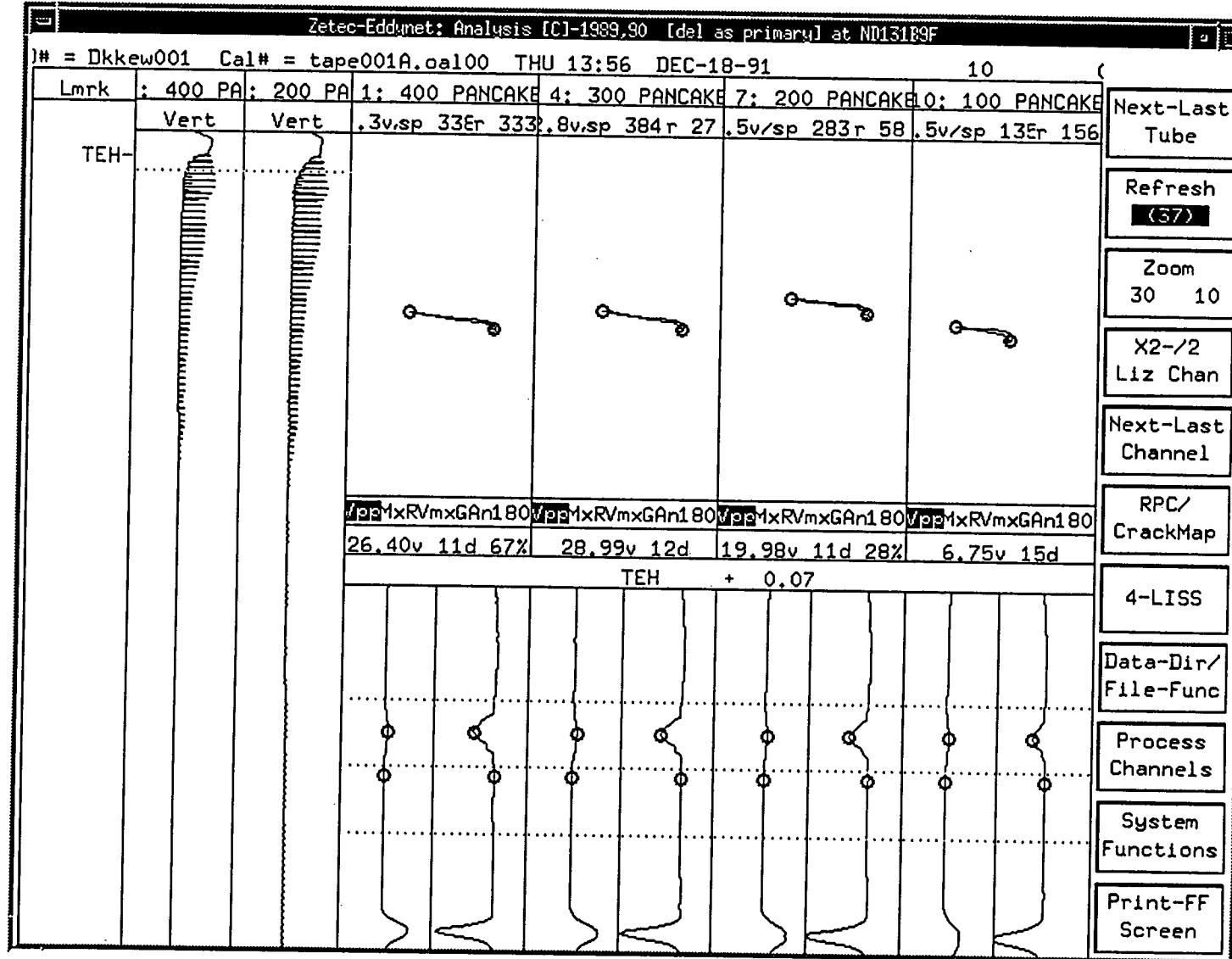


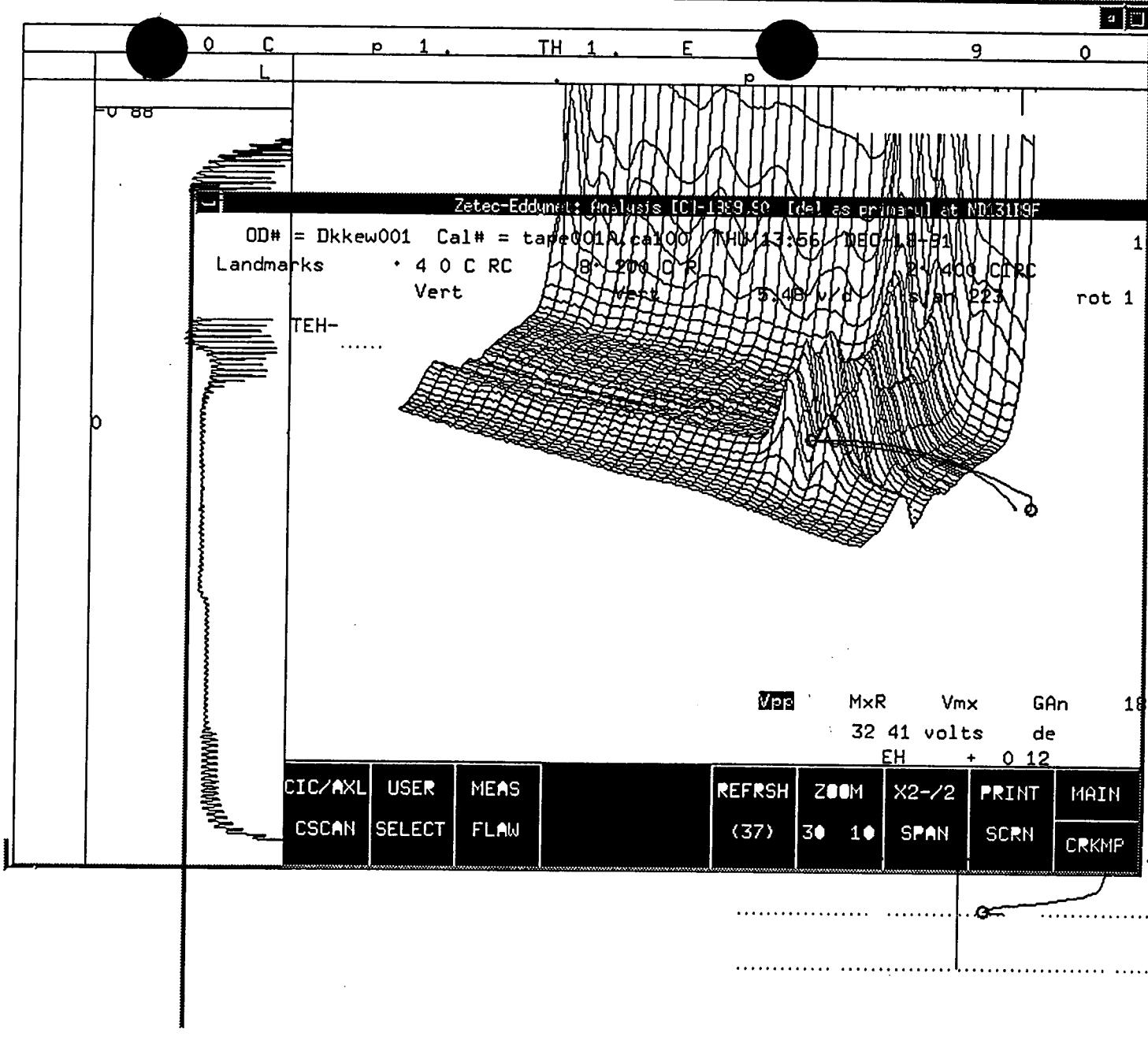




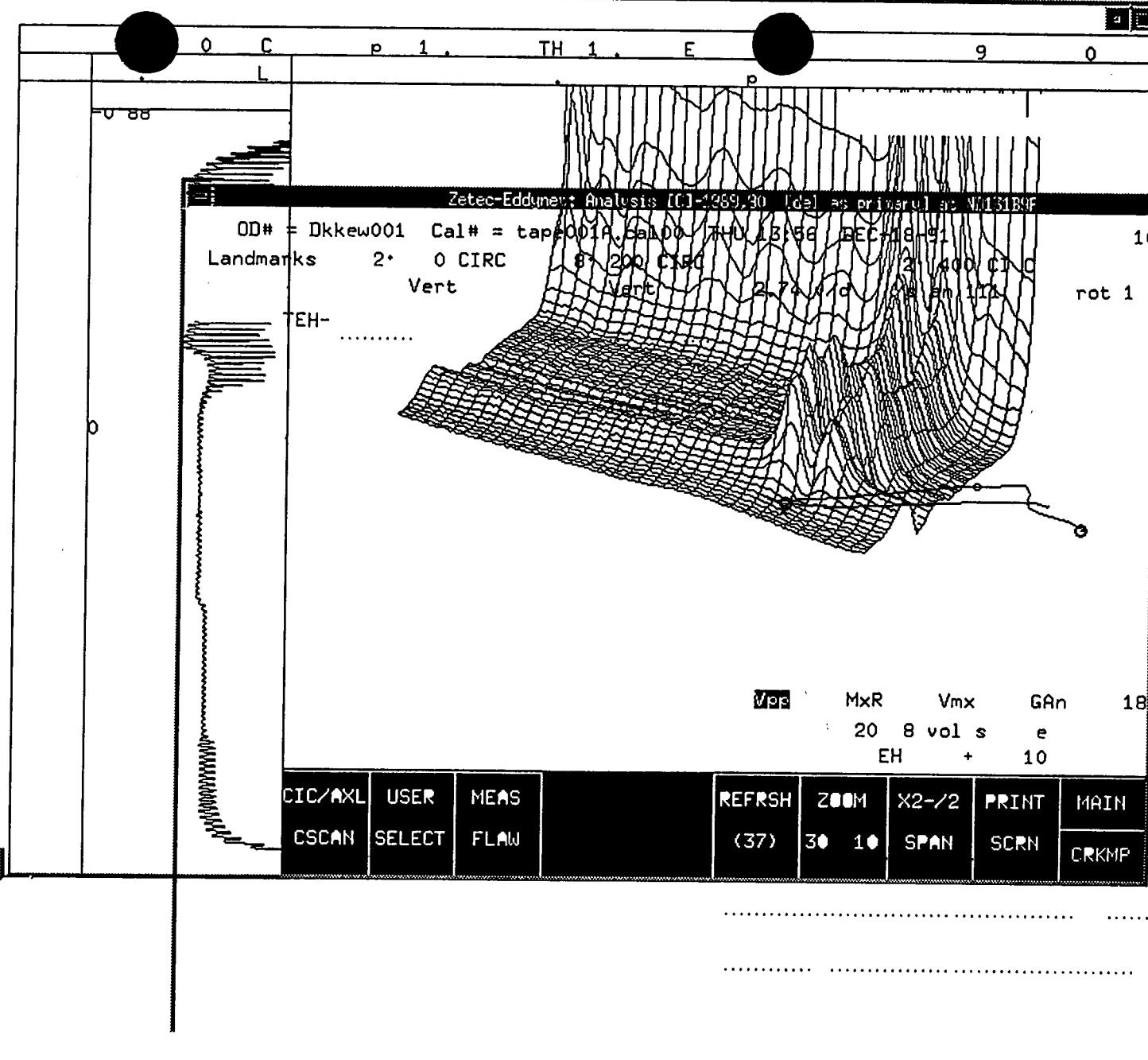




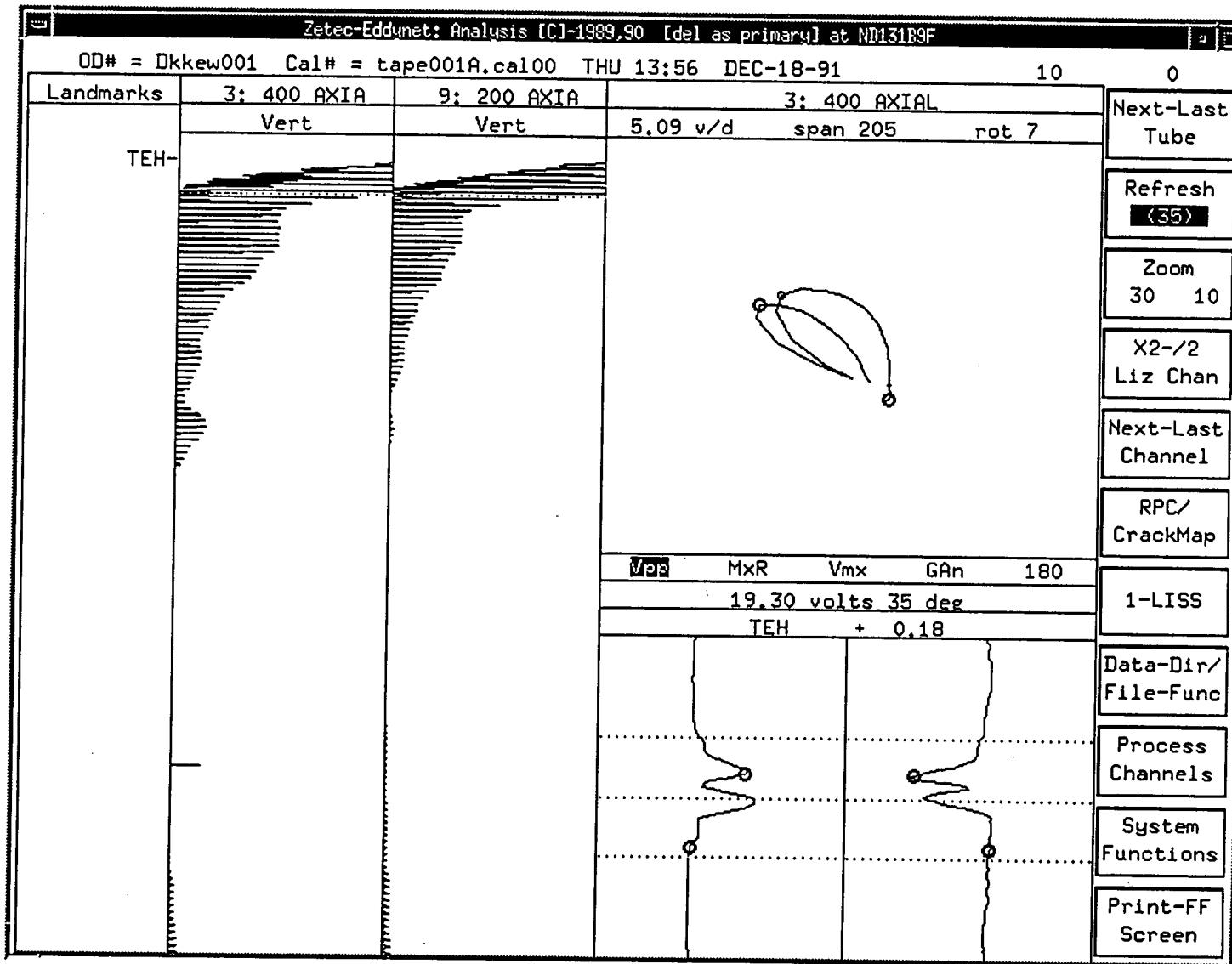


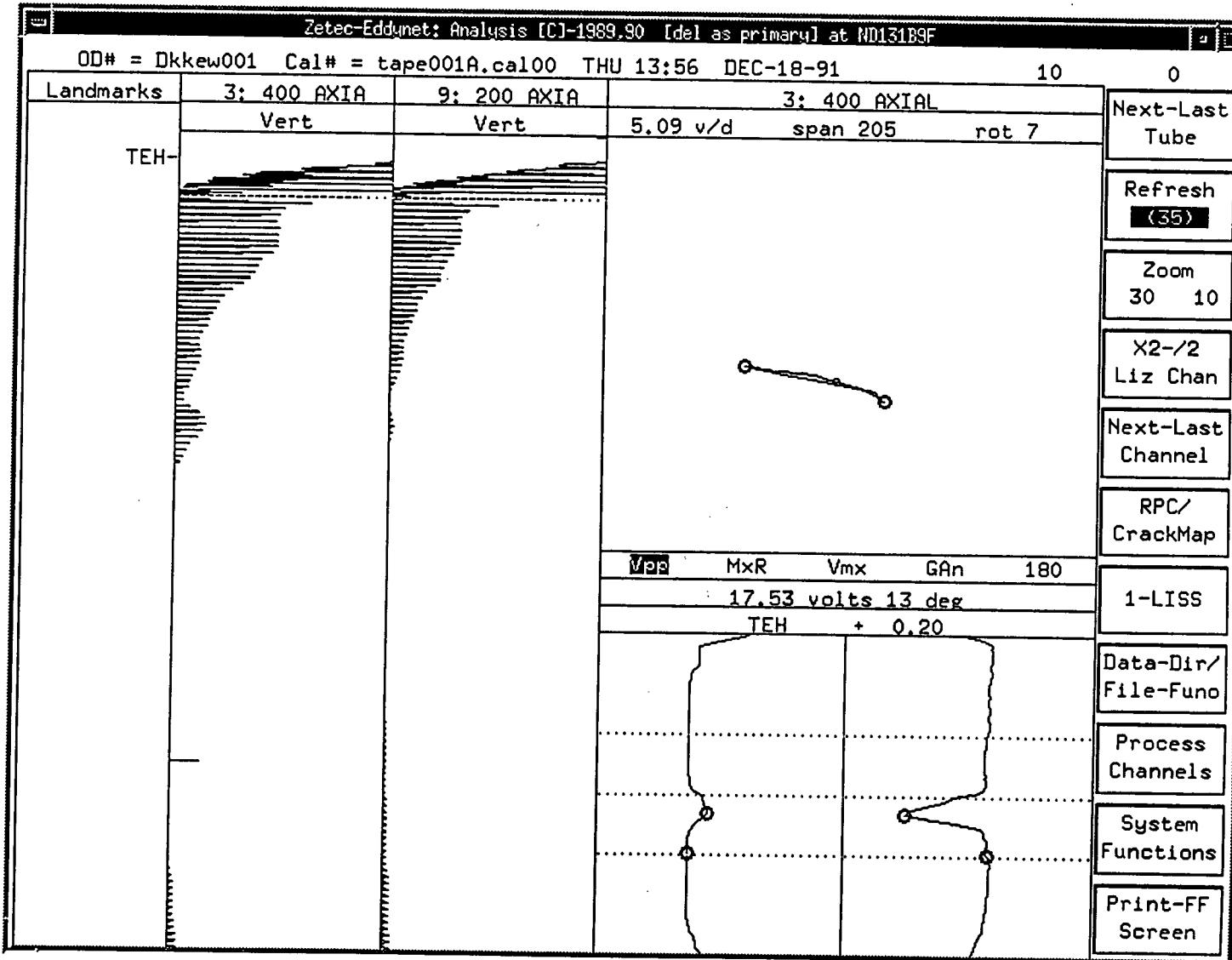


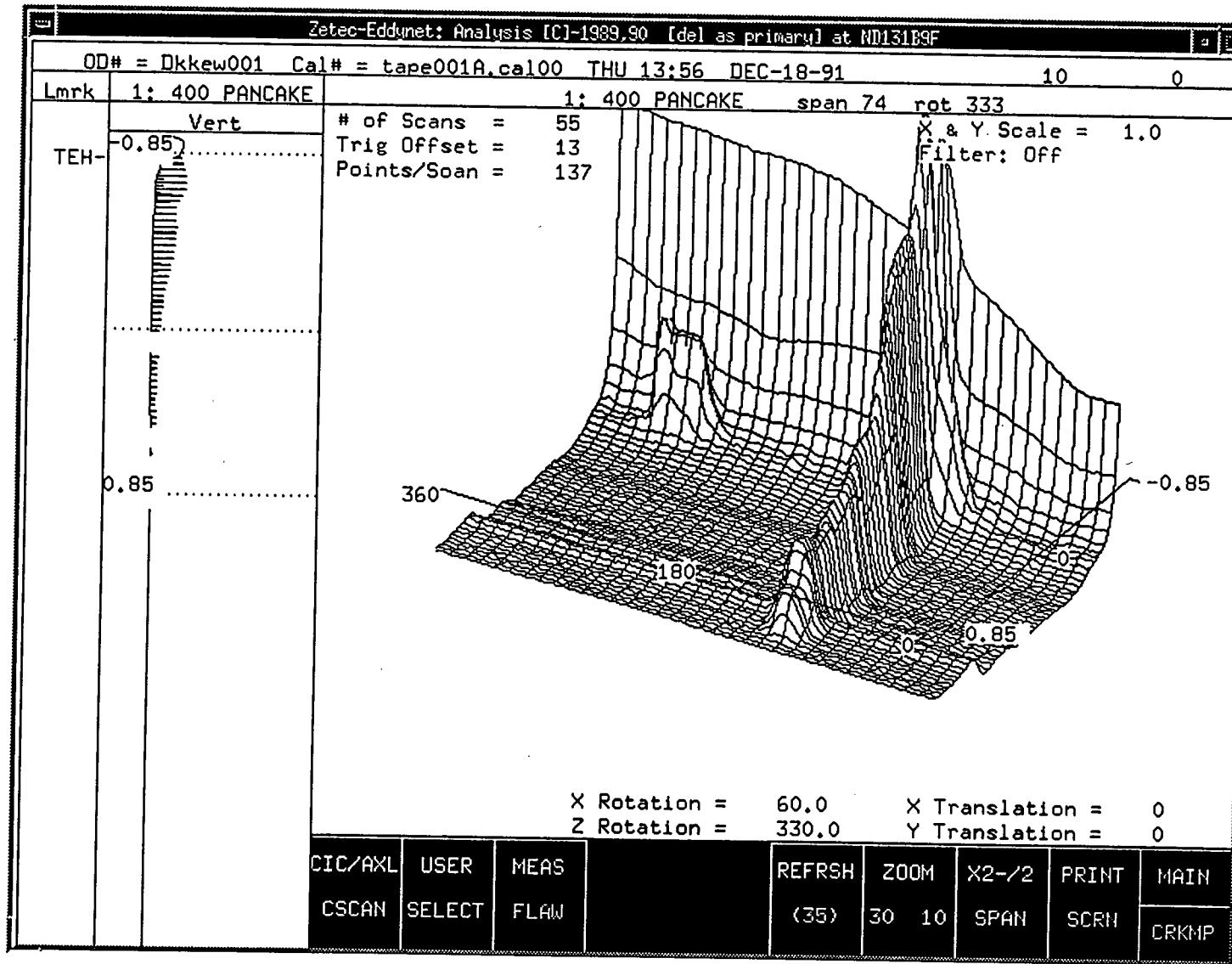
- 0 Next-Last Tube
- Refresh (37)
- Zoom 30 10
- X2-/2 Liz Chan
- Next-Last Channel
- RPC/ CrackMap
- 1-LISS
- Data-Dir/ File-Func
- Process Channels
- System Functions
- Print-FF Screen

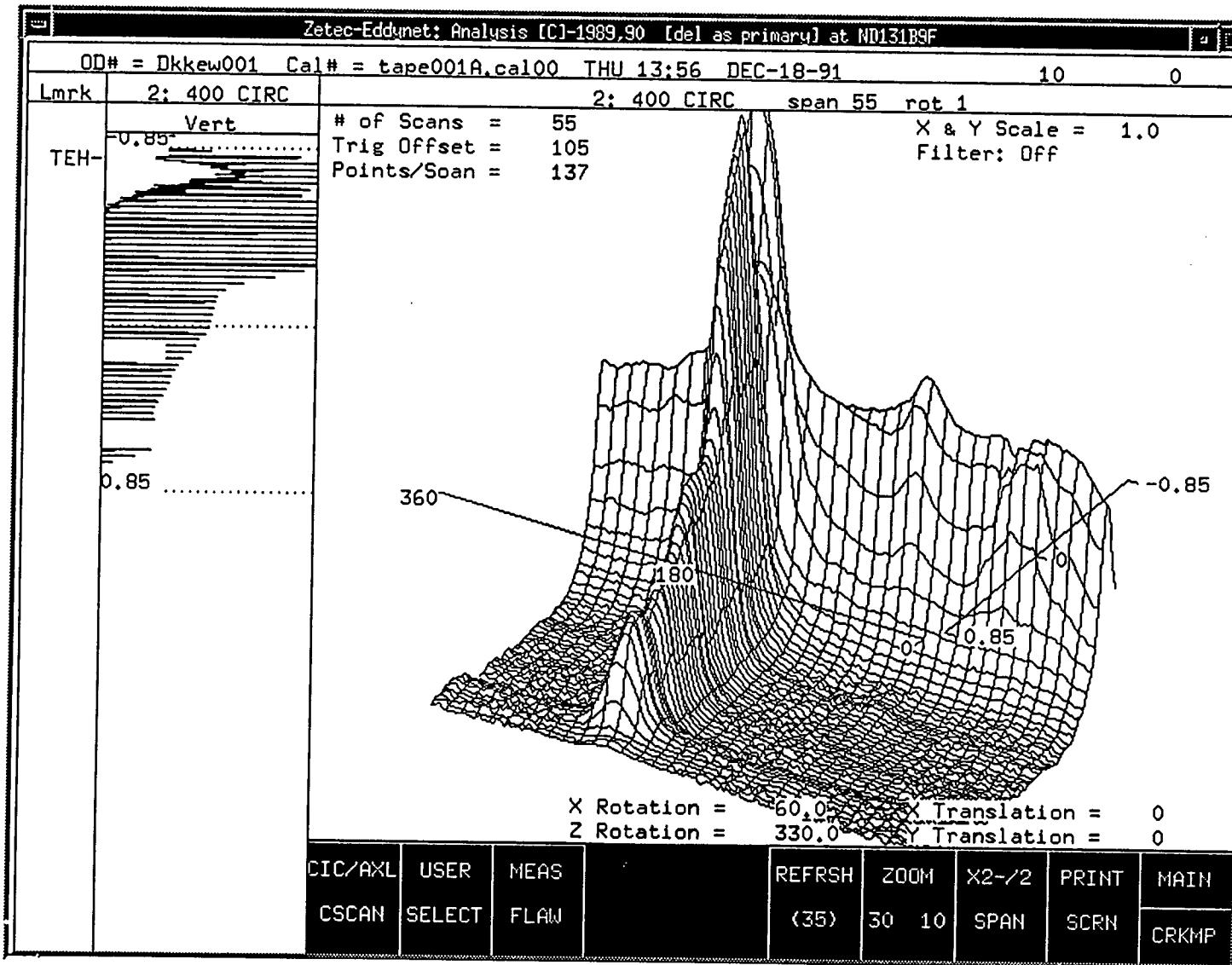


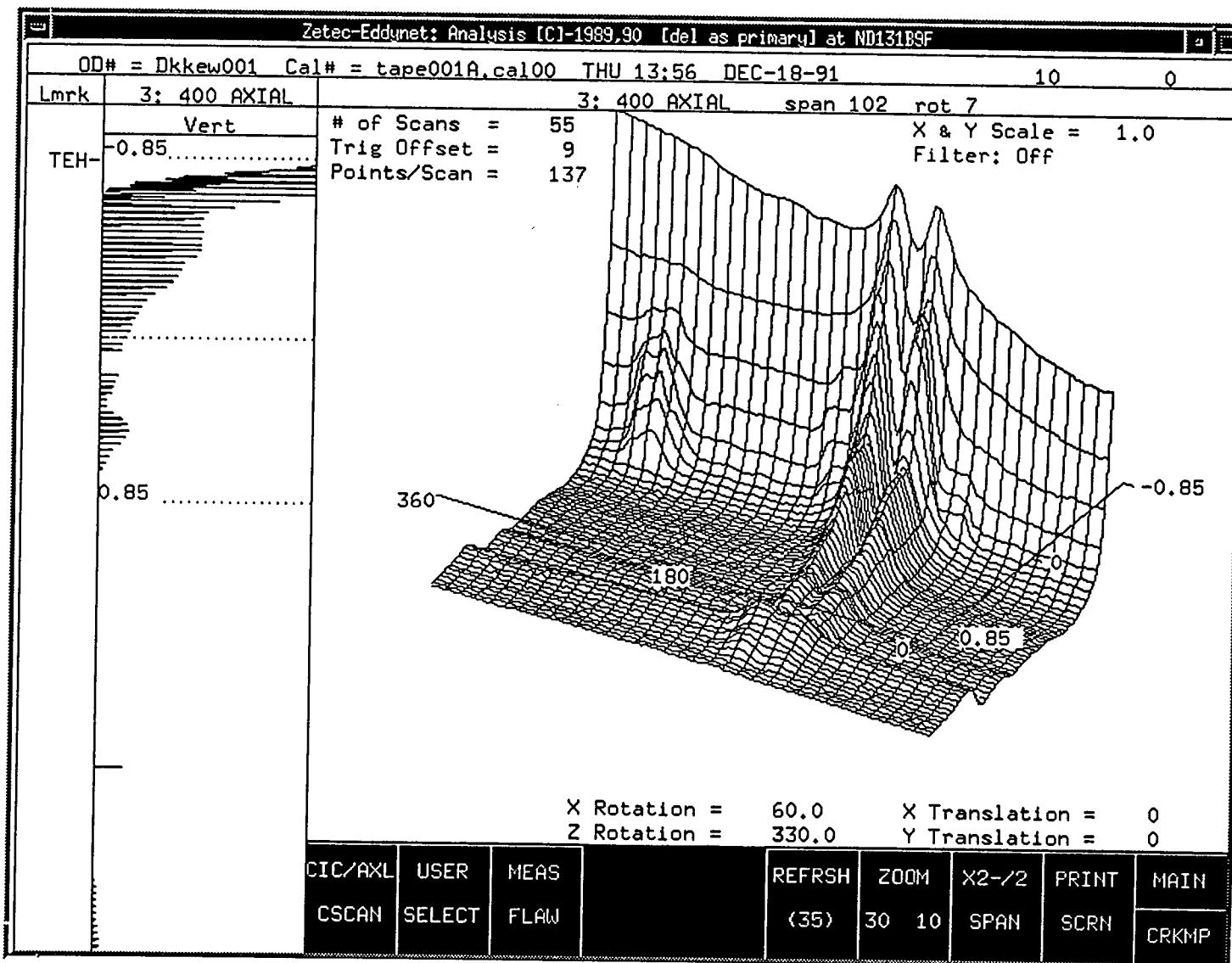
- Next-Last Tube
- Refresh (35)
- Zoom 30 10
- X2-/2 Liz Chan
- Next-Last Channel
- RPC/ CrackMap
- 1-LISS
- Data-Dir/ File-Func
- Process Channels
- System Functions
- Print-FF Screen











ATTACHMENT 3

LIQUID PENETRANT TEST REPORTS

Plant/Unit WINDSOR
Comp/System Slewing
Zone NA
Contract No. NA

PT No. 91-10
Procedure No. OP-9.4
Rev. No. 11
ST. No. NA Rev. NA

LIQUID PENETRANT EXAMINATION

| | <u>Brand Name</u> | <u>Type</u> | <u>Batch No.</u> | <u>Dwell Time</u> |
|------------|-------------------|-------------|------------------|-------------------|
| CLEANER: | Magniflux | SKC-NF | 90FOIK | 7 min |
| PENETRANT: | Magnaflux | SKC-HFT/S | 87KO18 | 10 min |
| REMOVER: | magnesflux | SKC-NF | 90FOIK | 10 min |
| DEVELOPER: | Magnsflux | SKD-NF | 89CO2K | 7 min |

Instructions: Completely describe ALL Indications.
If in the "as-welded" condition - so state.
If no indications were found - so state.

| EXAMINATION WELD/AREA | DESCRIPTION/REMARKS | ACCEPT | REJECT |
|-----------------------|---------------------|--------|--------|
| K-3 | NO INDICATIONS | | |
| K-4 | | X | NA |
| K-9 | | X | NA |
| K-6 | | X | NA |
| K-7 | | X | NA |

Component Temperature 84° F

Photograph: None Attached NA
Sketch: None Attached NA

EXAMINER P.K. Lang LEVEL III DATE 12-20-91

EXAMINER _____ DATE _____
LEVEL _____ RATE _____

REVIEWER _____ **DATE** _____

Authorized Inspection Agency

Authorized Inspection Agency _____ DATE _____

Page 1 of 1

Plant/Unit WINDSOR
Comp/System Sleevings
Zone NA
Contract No. NA

PT No. 91-11
Procedure No. OP. 9.4
Rev. No. 11
ST. No. NA Rev. NA

LIQUID PENETRANT EXAMINATION

| | <u>Brand Name</u> | <u>Type</u> | <u>Batch No.</u> | <u>Dwell Time</u> |
|------------|-------------------|-------------|------------------|-------------------|
| CLEANER: | Magniflux | SKC-NF | 90FO1K | 7 min |
| PENETRANT: | Magniflux | SKL-HFI'S | 87KO18 | 10 min |
| REMOVER: | Magniflux | SKC-NF | 90FO1K | 10 min |
| DEVELOPER: | Magniflux | SKD-NF | 90EO3K | 7 min |

Instructions: Completely describe ALL Indications.
If in the "as-welded" condition - so state.
If no indications were found - so state.

Component Temperature 71°F

Photograph: None Attached NA
Sketch: None Attached NA

EXAMINER P.K. Levy LEVEL III DATE 12-24-91
EXAMINER _____ LEVEL _____ DATE _____
REVIEWER _____ LEVEL _____ DATE _____
Authorized Inspection Agency _____ DATE _____

Page 1 of 1