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United States Nuclear Regulatory Commission
Attention: Document Control Desk
Washington, D.C. 20555

Serial No. 11-196
NL&OS/vlh R0
Docket No. 50-281
License No. DPR-37

VIRGINIA ELECTRIC AND POWER COMPANY (DOMINION)
SURRY POWER STATION UNIT 2
CYCLE 24 CORE OPERATING LIMITS REPORT, REVISION 0

Pursuant to Surry Technical Specification (TS) 6.2.C, enclosed is a copy of Dominion's Core Operating Limits Report (COLR) for Surry Unit 2 Cycle 24 Pattern UPG, Revision 0.

If you have any questions or require additional information, please contact Mr. Gary Miller at (804) 273-2771.

Sincerely,

A handwritten signature in black ink, appearing to read "C. L. Funderburk", followed by a horizontal line.

C. L. Funderburk, Director
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Dominion Resources Services, Inc. for
Virginia Electric and Power Company

Enclosure

Commitment Summary: There are no new commitments as a result of this letter.

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Serial No. 11-196
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CORE OPERATING LIMITS REPORT
Surry 2 Cycle 24 Pattern UPG
Revision 0

March 2011

Virginia Electric and Power Company
Surry Power Station Unit 2

1.0 INTRODUCTION

This Core Operating Limits Report (COLR) for Surry Unit 2 Cycle 24 has been prepared in accordance with the requirements of Surry Technical Specification 6.2.C.

The Technical Specifications affected by this report are:

TS 2.1 – Safety Limit, Reactor Core

TS 2.3.A.2.d – Overtemperature ΔT

TS 2.3.A.2.e – Overpower ΔT

TS 3.1.E - Moderator Temperature Coefficient

TS 3.12.A.1, TS 3.12.A.2, TS 3.12.A.3 and TS 3.12.C.3.b.1(b) - Control Bank Insertion Limits

TS 3.12.A.1.a, TS 3.12.A.2.a, and TS 3.12.G – Shutdown Margin

TS 3.12.B.1 and TS 3.12.B.2 - Power Distribution Limits

TS 3.12.F – DNB Parameters

TS Table 4.1-2A – Minimum Frequency for Equipment Tests: Item 22 – RCS Flow

2.0 REFERENCES

1. VEP-FRD-42, Rev. 2.1-A, “Reload Nuclear Design Methodology,” August 2003.

Methodology for:

TS 3.1.E - Moderator Temperature Coefficient

TS 3.12.A.1, TS 3.12.A.2, TS 3.12.A.3 and TS 3.12.C.3.b.1(b) - Control Bank Insertion Limit

TS 3.12.A.1.a, TS 3.12.A.2.a and TS 3.12.G – Shutdown Margin

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor and Nuclear Enthalpy Rise Hot Channel Factor

TS 3.12.F – DNB Parameters

TS Table 4.1-2A – Minimum Frequency for Equipment Tests: Item 22 – RCS Flow

2. WCAP-16009-P-A, “Realistic Large Break LOCA Evaluation Methodology Using the Automated Statistical Treatment of Uncertainty Method (ASTRUM),” (Westinghouse Proprietary), January 2005.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

3. WCAP-10054-P-A, “Westinghouse Small Break ECCS Evaluation Model Using the NOTRUMP Code,” (Westinghouse Proprietary), August 1985.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

4. WCAP-10079-P-A, "NOTRUMP, A Nodal Transient Small Break and General Network Code," (Westinghouse Proprietary), August 1985.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

5. WCAP-12610-P-A, "VANTAGE+ Fuel Assembly Report," (Westinghouse Proprietary), April 1995.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

6. WCAP-12610-P-A and CENPD-404-P-A, Addendum 1-A, "Optimized ZIRLO," (Westinghouse Proprietary), July 2006.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

7. VEP-NE-2-A, Rev. 0, "Statistical DNBR Evaluation Methodology," June 1987.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Nuclear Enthalpy Rise Hot Channel Factor

8. VEP-NE-3-A, Rev. 0, "Qualification of the WRB-1 CHF Correlation in the Virginia Power COBRA Code," July 1990.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Nuclear Enthalpy Rise Hot Channel Factor

9. DOM-NAF-2-A, Rev. 0.2-P-A, "Reactor Core Thermal-Hydraulics Using the VIPRE-D Computer Code," including Appendix B, "Qualification of the Westinghouse WRB-1 CHF Correlation in the Dominion VIPRE-D Computer Code," August 2010.

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Nuclear Enthalpy Rise Hot Channel Factor

10. WCAP-8745-P-A, "Design Bases for Thermal Overpower Delta-T and Thermal Overtemperature Delta-T Trip Function," September 1986.

Methodology for:

TS 2.3.A.2.d - Overtemperature ΔT

TS 2.3.A.2.e - Overpower ΔT

3.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in section 1.0 are presented in the following subsections. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.2.C.

3.1 Safety Limit, Reactor Core (TS 2.1)

3.1.1 The Reactor Core Safety Limits are presented in **Figure A-1**.

3.2 Overtemperature ΔT (TS 2.3.A.2.d)

$$\Delta T \leq \Delta T_0 \left[K_1 - K_2 \left(\frac{1 + t_1 s}{1 + t_2 s} \right) (T - T') + K_3 (P - P') - f(\Delta I) \right]$$

Where:

ΔT is measured RCS ΔT , °F.

ΔT_0 is the indicated ΔT at RATED POWER, °F.

s is the Laplace transform operator, sec^{-1} .

T is the measured RCS average temperature (T_{avg}), °F.

T' is the nominal T_{avg} at RATED POWER, $\leq 573.0^\circ\text{F}$.

P is the measured pressurizer pressure, psig.

P' is the nominal RCS operating pressure ≥ 2235 psig.

$$K_1 \leq 1.1425$$

$$K_2 \geq 0.01059 / ^\circ\text{F}$$

$$K_3 \geq 0.000765 / \text{psig}$$

$$t_1 \geq 29.7 \text{ seconds} \quad t_2 \leq 4.4 \text{ seconds}$$

$$f(\Delta I) \geq 0.0268 \{-24 - (q_t - q_b)\}, \text{ when } (q_t - q_b) < -24.0\% \text{ RATED POWER}$$

$$0, \text{ when } -24.0\% \text{ RATED POWER} \leq (q_t - q_b) \leq 8.0\% \text{ RATED POWER}$$

$$0.0188 \{(q_t - q_b) - 8.0\}, \text{ when } (q_t - q_b) > +8.0\% \text{ RATED POWER}$$

Where q_t and q_b are percent RATED POWER in the upper and lower halves of the core, respectively, and $q_t + q_b$ is the total THERMAL POWER in percent RATED POWER.

3.3 Overpower ΔT (TS 2.3.A.2.e)

$$\Delta T \leq \Delta T_0 \left[K_4 - K_5 \left(\frac{t_3 s}{1 + t_3 s} \right) T - K_6 (T - T') - f(\Delta I) \right]$$

Where:

ΔT is measured RCS ΔT , °F.

ΔT_0 is the indicated ΔT at RATED POWER, °F.

s is the Laplace transform operator, sec^{-1} .

T is the measured RCS average temperature (T_{avg}), °F.

T' is the nominal T_{avg} at RATED POWER, $\leq 573.0^\circ\text{F}$.

$$K_4 \leq \mathbf{1.0965} \quad K_5 \geq \mathbf{0.0198} / ^\circ\text{F} \text{ for increasing } T_{\text{avg}} \quad K_6 \geq \mathbf{0.001074} / ^\circ\text{F} \text{ for } T > T'$$
$$\geq \mathbf{0} / ^\circ\text{F} \text{ for decreasing } T_{\text{avg}} \quad \geq \mathbf{0} \text{ for } T \leq T'$$

$$t_3 \geq \mathbf{9.0} \text{ seconds}$$

$f(\Delta I)$ = as defined above for OT ΔT

3.4 Moderator Temperature Coefficient (TS 3.1.E)

3.4.1 The Moderator Temperature Coefficient (MTC) limits are:

+6.0 pcm/°F at less than 50 percent of RATED POWER, and

+6.0 pcm/°F at 50 percent of RATED POWER and linearly decreasing to 0 pcm/°F at RATED POWER

3.5 Control Bank Insertion Limits (TS 3.12.A.1, TS 3.12.A.2 and TS 3.12.C.3.b.1(b))

3.5.1 The control rod banks shall be limited in physical insertion as shown in **Figure A-2**.

3.5.2 The rod insertion limit for the A and B control banks is the fully withdrawn position as shown on **Figure A-2**.

3.5.3 The rod insertion limit for the A and B shutdown banks is the fully withdrawn position as shown on **Figure A-2**.

3.6 Shutdown Margin (TS 3.12.A.1.a, TS 3.12.A.2.a and TS 3.12.G)

3.6.1 Whenever the reactor is subcritical the shutdown margin (SDM) shall be $\geq \mathbf{1.77} \% \Delta k/k$.

3.7 Power Distribution Limits (TS 3.12.B.1 and TS 3.12.B.2)

3.7.1 Heat Flux Hot Channel Factor - FQ(z)

$$FQ(z) \leq \frac{CFQ}{P} K(z) \text{ for } P > 0.5$$

$$FQ(z) \leq \frac{CFQ}{0.5} K(z) \text{ for } P \leq 0.5$$

$$\text{where: } P = \frac{\text{THERMAL POWER}}{\text{RATED POWER}}$$

3.7.1.1 $CFQ = 2.5$

3.7.1.2 $K(z) = 1.0$ for all core heights, z

3.7.2 Nuclear Enthalpy Rise Hot Channel Factor - FΔH(N)

$$F\Delta H(N) \leq CFDH * \{1 + PFDH(1 - P)\}$$

$$\text{where: } P = \frac{\text{THERMAL POWER}}{\text{RATED POWER}}$$

3.7.2.1 $CFDH = 1.56$

3.7.2.2 $PFDH = 0.3$

3.8 DNB Parameters (TS 3.12.F and TS Table 4.1-2A)

3.8.1 Departure from Nucleate Boiling (DNB) Parameters shall be maintained within their limits during POWER OPERATION:

- Reactor Coolant System $T_{avg} \leq 577.0$ °F
- Pressurizer Pressure ≥ 2205 psig
- Reactor Coolant System Total Flow $\geq 273,000$ gpm (Tech Spec Limit) and $\geq 276,000$ gpm (COLR Limit)

Figure A-1

REACTOR CORE SAFETY LIMITS THREE LOOP OPERATION, 100% FLOW

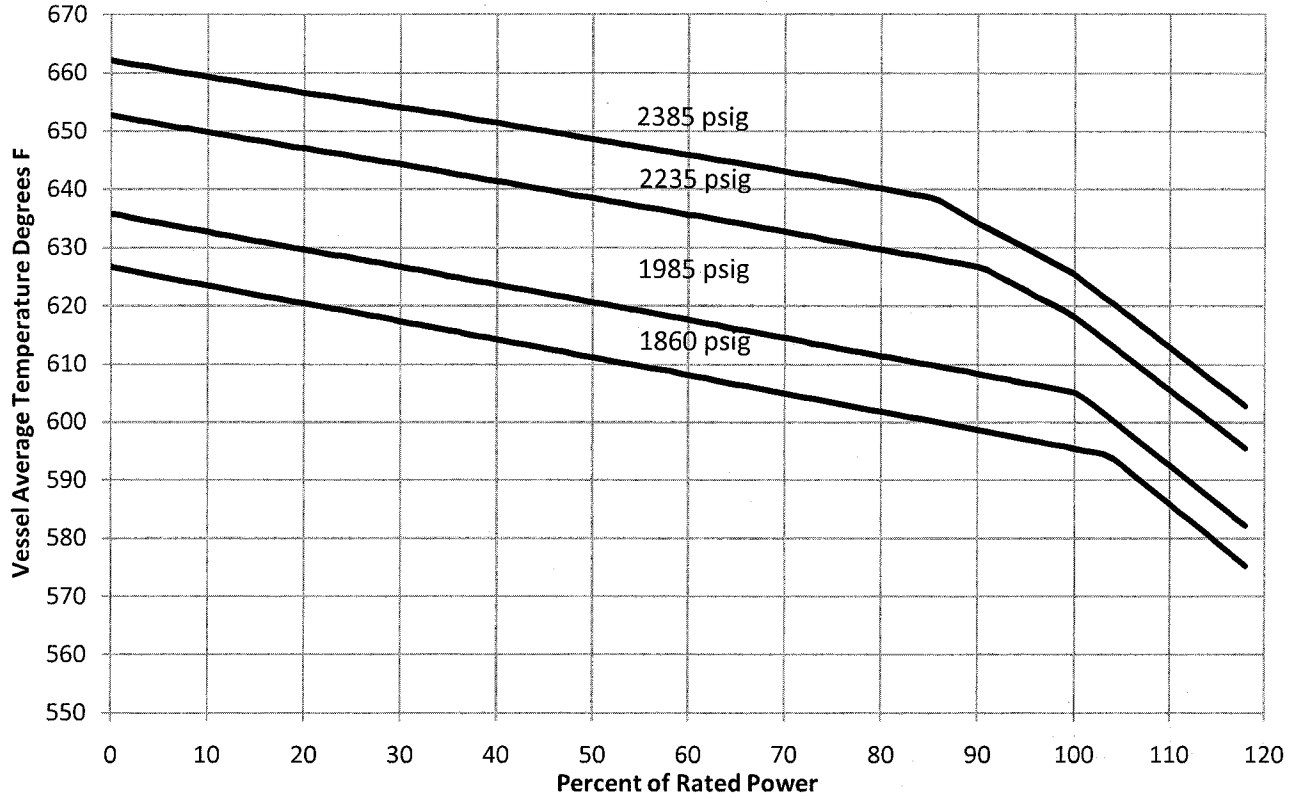


Figure A-2
Surry 2 Cycle 24
ROD GROUP INSERTION LIMITS

