

**ATTACHMENT 8  
LICENSE AMENDMENT REQUEST  
EXTENDED POWER UPRATE  
CORE OPERATING LIMITS REPORT  
MARKUPS**

**(For Information Only)**

**FLORIDA POWER & LIGHT  
ST. LUCIE UNIT 2**

This coversheet plus 12 pages

## LIST OF PAGES

### Core Operating Limits Report

5 of 18

6 of 18

8 of 18 (replaced by Proposed COLR Figure 3.1-1a)

Proposed COLR Figure 3.1-1a

12 of 18 (replaced by Proposed COLR Figure 3.2-3)

Proposed COLR Figure 3.2-3

14 of 18

15 of 18

16 of 18

17 of 18


18 of 18

heat rate  $LHR^M(z)$ . The incremental penalty factors (in excess of 2% margin decrease) are included in the  $W(z)$  function of Table 3.2-3.

Incore Detector Monitoring System

During operation, with the linear heat rate being monitored by the Incore Detector Monitoring System, the Local Power Density alarm setpoints shall be adjusted to less than or equal to the limits shown on Figure 3.2-1.

2.5 TOTAL INTEGRATED RADIAL PEAKING FACTOR -  $F_r^T$  (TS 3.2.3)

The calculated value of  $F_r^T$  shall be limited to  $\leq 1.70$ . 

The power dependent  $F_r^T$  limits are shown on Figure 3.2-3.

2.6 DNB Parameters (TS 3.2.5)


The following DNB-related parameters shall be maintained within the limits shown on Table 3.2-2:

- a. Cold Leg Temperature
- b. Pressurizer Pressure
- c. Reactor Coolant System Flow rate
- d. AXIAL SHAPE INDEX

 Total

2.7 Refueling Operations - Boron Concentration (TS 3.9.1)

With the reactor vessel head closure bolts less than fully tensioned or with the head removed, the boron concentration of all filled portions of the Reactor Coolant System and the refueling canal shall be maintained uniform and sufficient to ensure that the more restrictive of the following reactivity conditions is met:

- a. Either a  $K_{eff}$  of 0.95 or less, or
- b. A boron concentration of greater than or equal to 1720 ppm. 

2.8 SHUTDOWN MARGIN -  $T_{avg}$  Greater Than 200 °F (TS 3.1.1.1)

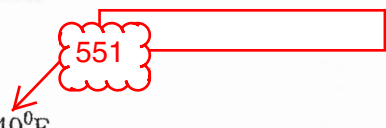
The SHUTDOWN MARGIN shall be greater than or equal to 3600 pcm.

2.9 SHUTDOWN MARGIN -  $T_{avg}$  Less Than or Equal To 200 °F (TS 3.1.1.2)

The SHUTDOWN MARGIN shall be greater than or equal to 3000 pcm.

Table 3.2-2

DNB MARGIN LIMITS

<u>PARAMETER</u>	<u>FOUR REACTOR COOLANT PUMPS OPERATING</u>
Cold Leg Temperature (narrow Range)	$535^{\circ}\text{F}^{**} \leq T \leq 549^{\circ}\text{F}$ 
Pressurizer Pressure*	$2225 \text{ psia} \leq P_{\text{PZR}} \leq 2350 \text{ psia}^{**}$
Reactor Coolant Flow Rate	$\geq 375,000 \text{ gpm}$
AXIAL SHAPE INDEX	Within the limits specified in Figure 3.2-4

\* Limit not applicable during either a THERMAL POWER ramp increase in excess of 5% of RATED THERMAL POWER or a THERMAL POWER step increase of greater than 10% of RATED THERMAL POWER.

\*\* Applicable only if power level  $\geq 70\%$  of RATED THERMAL POWER.



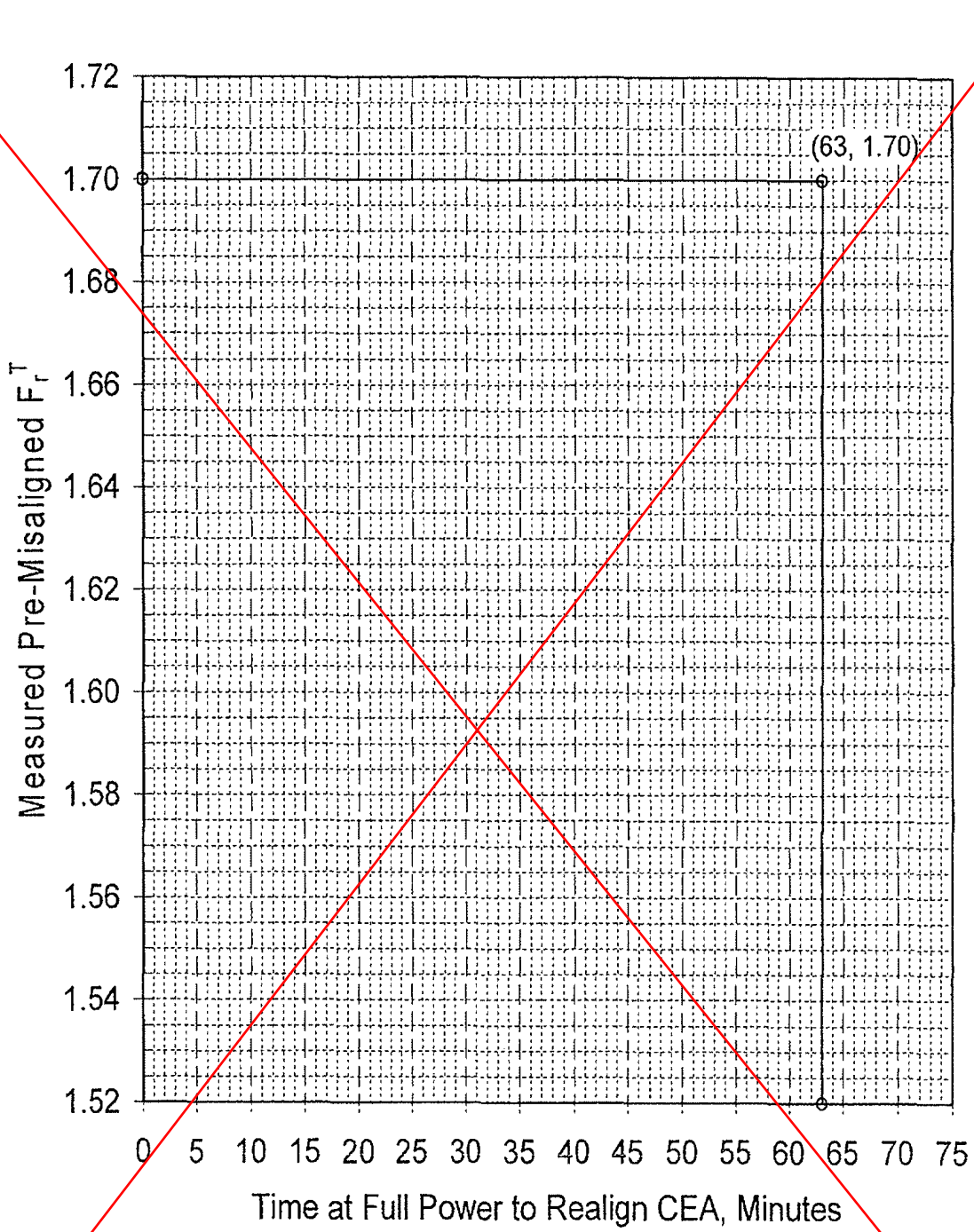


FIGURE 3.1-1a  
Allowable Time to Realign CEA vs. Initial  $F_r^T$

Proposed COLR Figure 3.1-1a

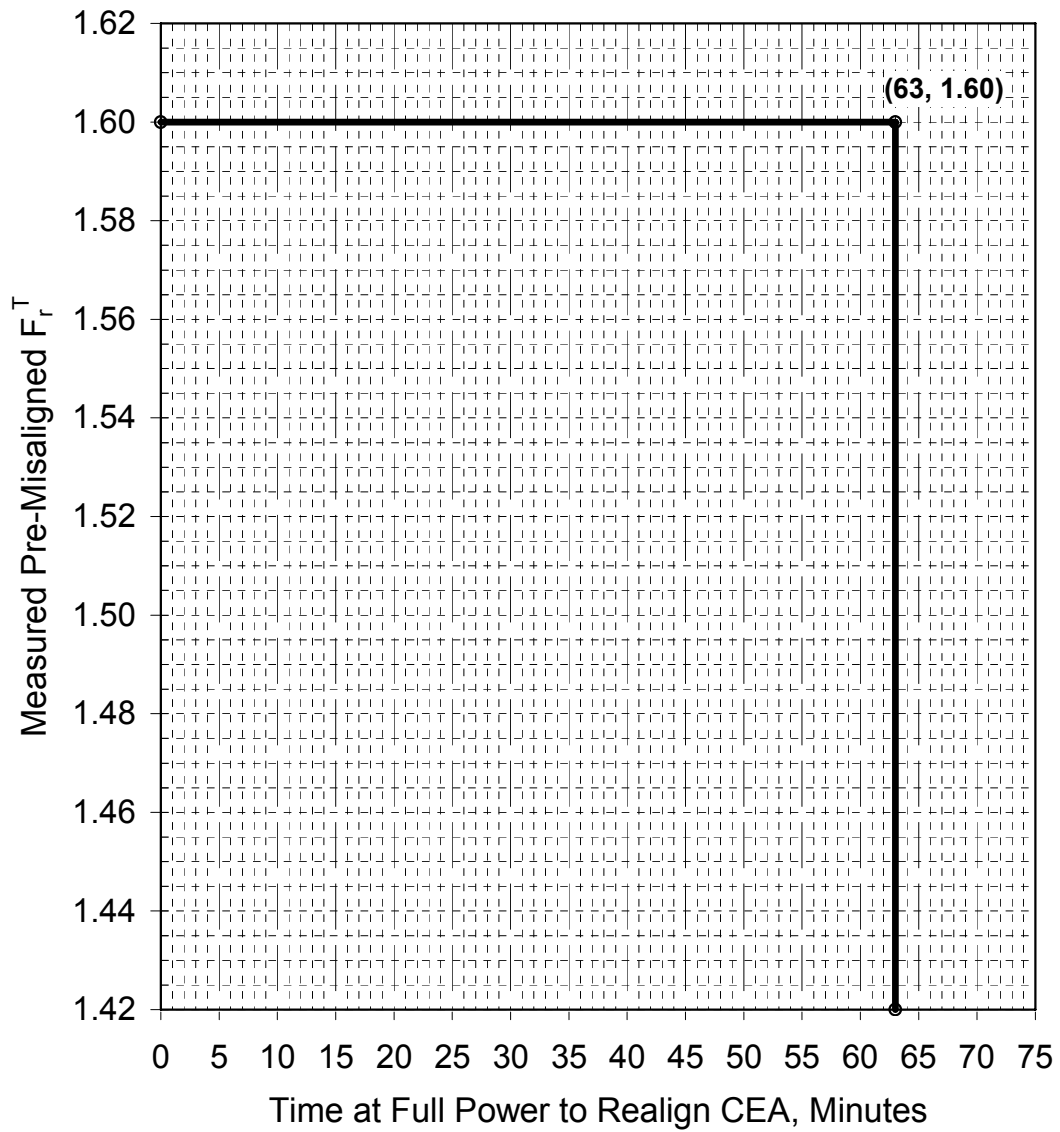


FIGURE 3.1-1a  
Allowable Time to Realign CEA vs. Initial  $F_r^T$

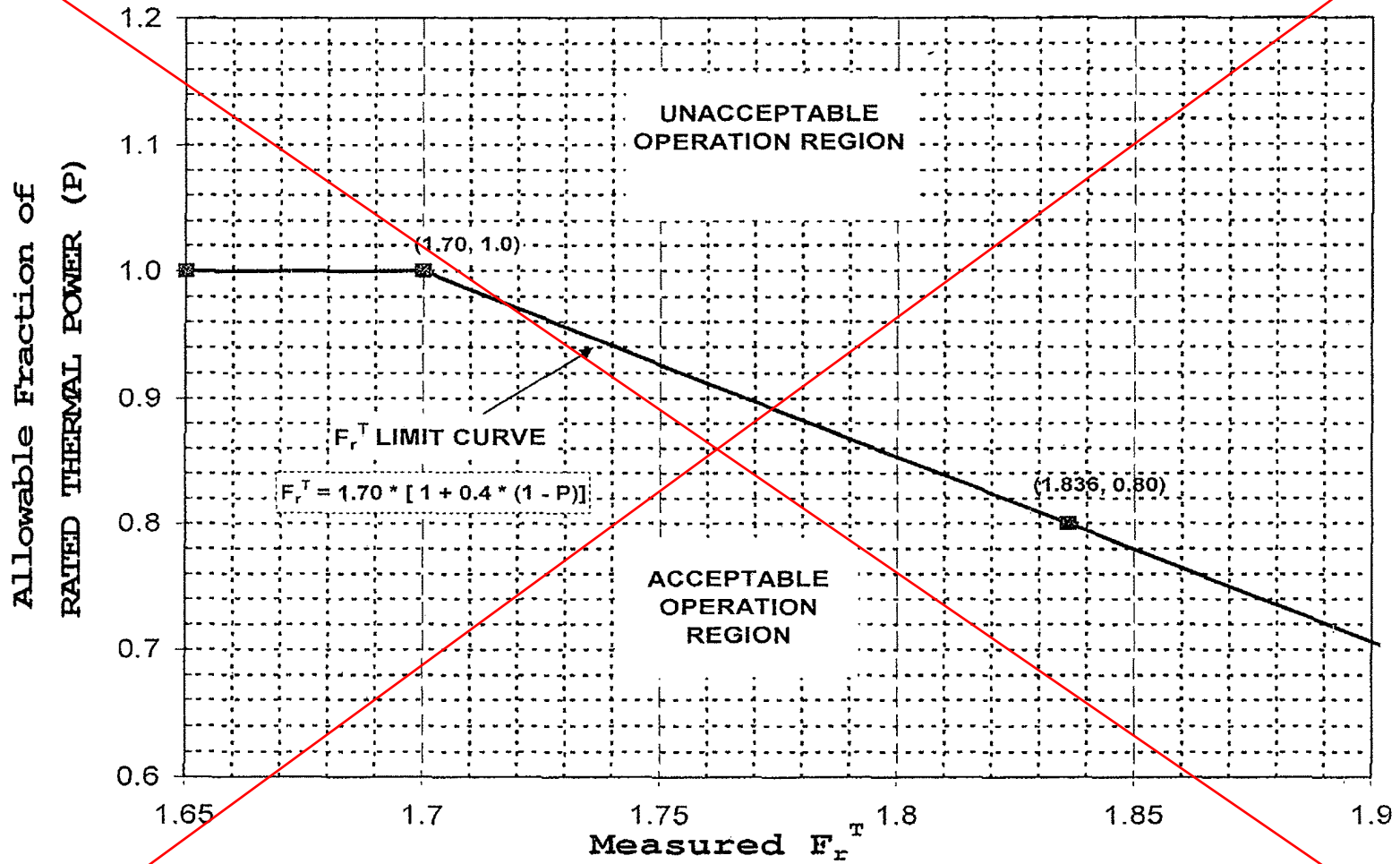


FIGURE 3.2-3  
Allowable Combinations of THERMAL POWER and  $F_r^T$   
(The expression specified in the Figure may be used for  $F_r^T$  at other power levels)

Proposed COLR Figure 3.2-3

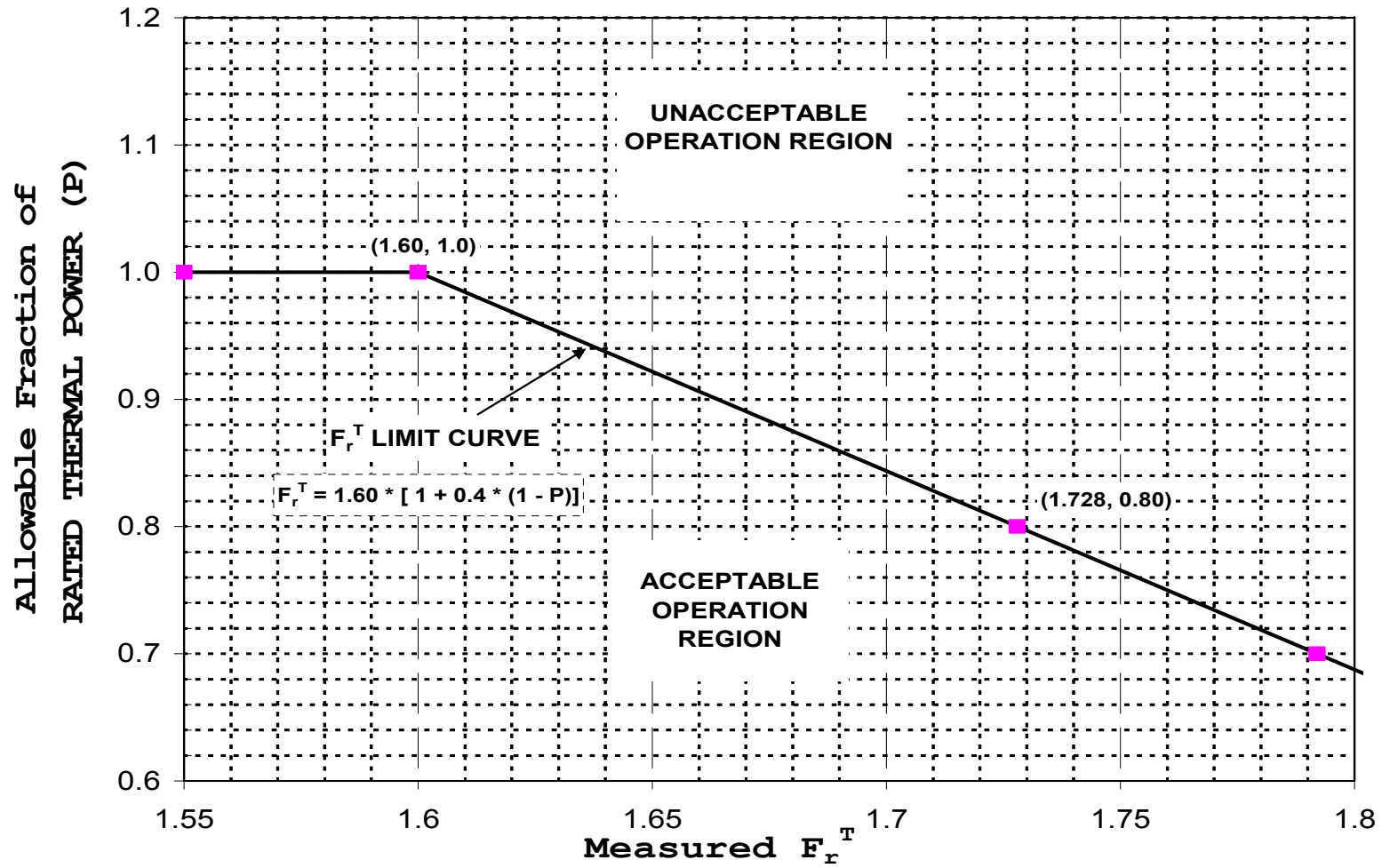


FIGURE 3.2-3  
Allowable Combinations of THERMAL POWER and  $F_r^T$   
(The expression specified in the Figure may be used for  $F_r^T$  at other power levels)

### 3.0 LIST OF APPROVED METHODS

The analytical methods used to determine the core operating limits are those previously approved by the NRC, and are listed below.

1. WCAP-11596-P-A, "Qualification of the PHOENIX-P/ANC Nuclear Design System for Pressurized Water Reactor Cores," June 1988 (Westinghouse Proprietary)
2. NF-TR-95-01, "Nuclear Physics Methodology for Reload Design of Turkey Point & St. Lucie Nuclear Plants," Florida Power & Light Company, January 1995 (NRC SER dated June 9, 1995), & Supplement 1, August 1997
3. → ~~CENPD 199 P, Rev. 1 P-A, "C-E Setpoint Methodology: CE Local Power Density and DNB-LSSS and LCO Setpoint Methodology for Analog Protection Systems," January 1986~~
4. → ~~CENPD 266 P-A, "The ROCS and DIT Computer Code for Nuclear Design," April 1983~~
5. CENPD-275-P, Revision 1-P-A, "C-E Methodology for Core Designs Containing Gadolinia-Urania Burnable Absorbers," May 1988, & Revision 1-P Supplement 1-P-A, April 1999
6. → ~~CENPD 188 A, "HERMITE: A Multi Dimensional Space Time Kinetics Code for PWR Transients," July 1976~~
7. → ~~CENPD 153 P, Rev. 1 P-A, "Evaluation of Uncertainty in the Nuclear Power Peaking Measured by the Self Powered, Fixed Incore Detector System," May 1980~~
8. CEN-123(F)-P, "Statistical Combination of Uncertainties Methodology Part 1: C-E Calculated Local Power Density and Thermal Margin/Low Pressure LSSS for St. Lucie Unit 1," December 1979
9. → ~~CEN 123(F) P, "Statistical Combination of Uncertainties Methodology Part 2: Combination of System Parameter Uncertainties in Thermal Margin Analyses for St. Lucie Unit 1," January 1980~~
10. CEN-123(F)-P, "Statistical Combination of Uncertainties Methodology Part 3: C-E Calculated Departure from Nucleate Boiling and Linear Heat Rate Limiting Conditions for Operation for St. Lucie Unit 1," February 1980
11. CEN-191(B)-P, "CETOP-D Code Structure and Modeling Methods for Calvert Cliffs Units 1 and 2," December 1981

DELETED

12. Letter, J. W. Miller (NRC) to J. R. Williams, Jr. (FPL), Docket No. 50-389, Regarding Unit 2 Cycle 2 License Approval (Amendment No. 8 to NPF-16 and SER), November 9, 1984 (Approval of CEN-123(F)-P (three parts) and CEN-191(B)-P)
13. → ~~CEN-371(F)-P, "Extended Statistical Combination of Uncertainties," July 1989~~
14. Letter, J. A. Norris (NRC) to J. H. Goldberg (FPL), Docket No. 50-389, "St. Lucie Unit 2 - Change to Technical Specification Bases Sections '2.1.1 Reactor Core' and '3/4.2.5 DNB Parameters' (TAC No. M87722)," March 14, 1994 (Approval of CEN-371(F)-P)
15. → ~~CENPD-161-P-A, "TORC Code, A Computer Code for Determining the Thermal Margin of a Reactor Core," April 1986~~
16. → ~~CENPD-162-P-A, "Critical Heat Flux Correlation for C-E Fuel Assemblies with Standard Spacer Grids Part 1, Uniform Axial Power Distribution," April 1975~~
17. → ~~CENPD-207-P-A, "Critical Heat Flux Correlation for C-E Fuel Assemblies with Standard Spacer Grids Part 2, Non-uniform Axial Power Distribution," December 1984~~
18. → ~~CENPD-206-P-A, "TORC Code, Verification and Simplified Modeling Methods," June 1981~~
19. CENPD-225-P-A, "Fuel and Poison Rod Bowing," June 1983
20. CENPD-139-P-A, "C-E Fuel Evaluation Model Topical Report," July 1974
21. CEN-161(B)-P-A, "Improvements to Fuel Evaluation Model," August 1989
22. CEN-161(B)-P, Supplement 1-P-A, "Improvements to Fuel Evaluation Model," January 1992
23. CENPD-132, Supplement 3-P-A, "Calculative Methods for the C-E Large Break LOCA Evaluation Model for the Analysis of C-E and W Designed NSSS," June 1985
24. CENPD-133, Supplement 5-A, "CEFLASH-4A, A FORTRAN77 Digital Computer Program for Reactor Blowdown Analysis," June 1985
25. CENPD-134, Supplement 2-A, "COMPERC-II, a Program for Emergency Refill-Reflood of the Core," June 1985
26. CENPD-135-P, Supplement 5, "STRIKIN-II, A Cylindrical Geometry Fuel Rod Heat Transfer Program," April 1977

DELETED

27. Letter, R. L. Baer (NRC) to A. E. Scherer (CE), "Evaluation of Topical Report CENPD-135, Supplement #5," September 6, 1978
28. CENPD-137, Supplement 1-P, "Calculative Methods for the C-E Small Break LOCA Evaluation Model," January 1977
29. CENPD-133, Supplement 3-P, "CEFLASH-4AS, A Computer Program for the Reactor Blowdown Analysis of the Small Break Loss of Coolant Accident," January 1977
30. Letter, K. Kniel (NRC) to A. E. Scherer (CE), "Evaluation of Topical Reports CENPD-133, Supplement 3-P and CENPD-137, Supplement 1-P," September 27, 1977
31. CENPD-138, Supplement 2-P, "PARCH, A FORTRAN-IV Digital Program to Evaluate Pool Boiling, Axial Rod and Coolant Heatup," January 1977
32. Letter, C. Aniel (NRC) to A. E. Scherer (CE), "Evaluation of Topical Report CENPD-138, Supplement 2-P," April 10, 1978
33. Letter, W. H. Bohlke (FPL) to Document Control Desk (NRC), "St. Lucie Unit 2, Docket No. 50-389, Proposed License Amendment, MTC Change from -27 pcm to -30 pcm," L-91-325, December 17, 1991
34. Letter, J. A. Norris (NRC) to J. H. Goldberg (FPL), "St. Lucie Unit 2 - Issuance of Amendment Re: Moderator Temperature Coefficient (TAC No. M82517)," July 15, 1992
35. Letter, J. W. Williams, Jr. (FPL) to D. G. Eisenhut (NRC), "St. Lucie Unit No. 2, Docket No. 50-389, Proposed License Amendment, Cycle 2 Reload," L-84-148, June 4, 1984
36. Letter, J. R. Miller (NRC) to J. W. Williams, Jr. (FPL), Docket No. 50-389, Regarding Unit 2 Cycle 2 License Approval (Amendment No. 8 to NPF-16 and SER), November 9, 1984 (Approval of Methodology contained in L-84-148)
- ~~37. Letter, A. E. Scherer Enclosure 1 P to LD 82-001, "CESEC Digital Simulation of a Combustion Engineering Nuclear Steam Supply System," December 1981~~
- ~~38. Safety Evaluation Report, "CESEC Digital Simulation of a Combustion Engineering Steam Supply System (TAC No.: 01142)," October 27, 1983~~
- ~~39. CENPD 282 P A, Volumes 1, 2, and 3, and Supplement 1, "Technical Manual for the CENTS Code," February 1991, February 1991, October 1991, and June 1993, respectively~~



40. ~~CEN 121(B)-P, "CEAW, Method of Analyzing Sequential Control Element Assembly Group Withdrawal Event for Analog Protected Systems," November 1979 (NRC SER dated December 21, 1999, Letter K. N. Jabbour (NRC) to T. F. Plunkett (FPL), TAC No. MA4523)~~
41. ~~CEN 133(B), "FIESTA, A One Dimensional, Two Group Space Time Kinetics Code for Calculating PWR Scram Reactivities," November 1979 (NRC SER dated December 21, 1999, Letter K. N. Jabbour (NRC) to T. F. Plunkett (FPL), TAC No. MA4523)~~
42. CEN-348(B)-P-A, Supplement 1-P-A, "Extended Statistical Combination of Uncertainties," January 1997
43. CEN-372-P-A, "Fuel Rod Maximum Allowable Gas Pressure," May 1990
44. ~~CENPD 183-A, "C E Methods for Loss of Flow Analysis," June 1984~~
45. ~~CENPD 190-A, "C E Method for Control Element Assembly Ejection Analysis," July 1976~~
46. ~~CENPD 199-P, Rev. 1 P-A, Supplement 2 P-A, "CE Setpoint Methodology", June 1998~~
47. ~~CENPD 382-P-A, "Methodology for Core Designs Containing Erbium Burnable Absorbers," August 1993~~
48. CEN-396(L)-P, "Verification of the Acceptability of a 1-Pin Burnup Limit of 60 MWD/KG for St. Lucie Unit 2," November 1989 (NRC SER dated October 18, 1991, Letter J. A. Norris (NRC) to J. H. Goldberg (FPL), TAC No. 75947)
49. CENPD-269-P, Rev. 1-P, "Extended Burnup Operation of Combustion Engineering PWR Fuel," July 1984
50. CEN-289(A)-P, "Revised Rod Bow Penalties for Arkansas Nuclear One Unit 2," December 1984 (NRC SER dated December 21, 1999, Letter K. N. Jabbour (NRC) to T. F. Plunkett (FPL), TAC No. MA4523)
51. CENPD-137, Supplement 2-P-A, "Calculative Methods for the ABB CE Small Break LOCA Evaluation Model," April 1998
52. CENPD-140-A, "Description of the CONTRANS Digital Computer Code for Containment Pressure and Temperature Transient Analysis," June 1976
53. ~~CEN 365(L), "Boric Acid Concentration Reduction Effort, Technical Bases and Operational Analysis," June 1988 (NRC SER dated March 13, 1989, Letter J. A. Norris (NRC) to W. F. Conway (FPL), TAC No. 69325)~~

DELETED



DELETED

54. ~~DP 456, F. M. Stern (CE) to E. Case (NRC), dated August 19, 1974, Appendix 6B to CESSAR System 80 PSAR (NRC SER, NUREG-75/112, Docket No. STN 50-470, "NRC SER - Standard Reference System, CESSAR System 80," December 1975)~~
55. CENPD-387-P-A, Revision 000, "ABB Critical Heat Flux Correlations for PWR Fuel," May 2000
56. CENPD-132, Supplement 4-P-A, "Calculative Methods for the CE Nuclear Power Large Break LOCA Evaluation Model," March 2001
57. CENPD-137, Supplement 2-P-A, "Calculative Methods for the ABB CE Small Break LOCA Evaluation Model," April 1998
58. CENPD-404-P-A, Rev. 0, "Implementation of ZIRLO™ Cladding Material in CE Nuclear Power Fuel Assembly Designs," November 2001
59. WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology" July 1985
60. WCAP-10216-P-A, Revision 1A, "Relaxation of Constant Axial Offset Control; FQ Surveillance Technical Specification," February 1994
61. WCAP-11397-P-A, (Proprietary), "Revised Thermal Design Procedure," April 1989
62. WCAP-14565-P-A, (Proprietary), "VIPRE-01 Modeling and Qualification for Pressurized Water Reactor Non-LOCA Thermal-Hydraulic Safety Analysis," October 1999
63. WCAP-14565-P-A, Addendum 1-A, Revision 0, "Addendum 1 to WCAP-14565-P-A Qualification of ABB Critical Heat Flux Correlations with VIPRE-01 Code," August 2004
64. Letter, W. Jefferson, Jr. (FPL) to Document Control Desk (USNRC), "St. Lucie Unit 2 Docket No. 50-389: Proposed License Amendment WCAP-9272 Reload Methodology and Implementing 30% Steam Generator Tube Plugging Limit," L-2003-276, December, 2003 (NRC SER dated January 31, 2005, Letter B. T. Moroney (NRC) to J. A. Stall (FPL), TAC No. MC1566)

65. WCAP-14882-P-A, "RETRAN-02 Modeling and Qualification for Westinghouse Pressurized Water Reactor Non-LOCA Safety Analyses," April 1999.
66. WCAP-7908-A, "FACTRAN-A FORTRAN IV Code for Thermal Transients in a UO2 Fuel Rod," December, 1989.
67. WCAP-7979-P-A, "TWINKLE - A Multi-Dimensional Neutron Kinetics Computer Code," January 1975.
68. WCAP-7588, Rev 1-A, "An Evaluation of the Rod Ejection Accident in Westinghouse Pressurized Water Reactors Using Special Kinetics Methods," January 1975.