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L-PI-11-004 TS 5.6.5.d

U S Nuclear Regulatory Commission ATTN: Document Control Desk Washington, DC 20555-0001

Prairie Island Nuclear Generating Plant Unit 1 Docket 50-282 License No. DPR-42

## <u>Core Operating Limits Report (COLR) for Prairie Island Nuclear Generating Plant</u> (PINGP) Unit 1, Cycle 26, Revision 3

Pursuant to the requirements of Technical Specification 5.6.5.d, the COLR for the PINGP Unit 1, Cycle 26, Revision 3, is attached. The limits specified in the attached COLR have been established using Nuclear Regulatory Commission (NRC) approved methodologies.

The COLR for Unit 1, Cycle 26, Revision 2, has been revised to align the Table 1 Mode 2 shutdown margin (SDM) with Figure 4. The vendor identified that Figures 3 and 4 had not been evaluated to confirm the SDM requirement specified in Table 1 for Mode 2 had been met. When the vendor performed the evaluation, it was determined that the Table 1 Mode 2 SDM requirement was more conservative than Figure 4 could support. The vendor determined that the SDM requirement used in the safety analyses, 1.9%, supports Figures 3 and 4. The COLR for Unit 1, Cycle 26, was revised to remove the excess conservatism in the Table 1 Mode 2 SDM value. This correction is limited to the COLR for Unit 1, Cycle 26, only and resulted in changes to the following sections:

- Revised the References section, item 30, to update the 50.59 Evaluation 1072, "Unit 1 Cycle 26 Core Reload" to revision 3.
- Revised Table 1 to update the shutdown margin value for Mode 2 from the overly conservative 2.0% to 1.9%, consistent with the safety analyses.

Additional minor editorial changes were made to the Reference section as follows:

- Replaced ZIRLO<sup>™</sup> with ZIRLO<sup>®</sup> in reference 9.
- Corrected the numbering sequence as reference 28 was previously used twice.

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# Summary of Commitments

This letter contains no new commitments and no revisions to existing commitments.

Mark A. Schimmel Site Vice President, Prairie Island Nuclear Generating Plant Northern States Power Company - Minnesota

Enclosure

cc: Administrator, Region III, USNRC Project Manager, Prairie Island, USNRC Resident Inspector, Prairie Island, USNRC State of Minnesota

# ENCLOSURE

# PRAIRIE ISLAND NUCLEAR GENERATING PLANT CORE OPERATING LIMITS REPORT UNIT 1 – CYCLE 26 REVISION 3

Record of Revision (6 pages)

PINGP COLR Unit 1 – Cycle 26, Revision 3 (21 pages)

# Core Operating Limits Report

# **Record of Revision**

 Unit	Cycle	Revision No.	Approval Date	Remarks
2	13	0	3 <b>/22/90</b>	Original Unit 2 Core Operating Limits Report, distributed with Technical Specification Revision 92.
1	14	0	3/22/90	Original Unit 1 Core Operating Limits Report, distributed with Technical Specification Revision 92.
		1	7/27/90	Incorporated expanded V(z) curves.
		2	9/27/90	Clarified rod insertion limit curve applicability.
		3	2/11/91	Incorporated revised $F_Q$ of 2.45 as a result of NRC approval of Westinghouse Topical Report WCAP-10924-P-A, Volume 1, Addendum 4, October 1990.
2	14	0	-	Not used.
		1	9/27/90	Updated to Unit 2 Cycle 14, incorporated expanded V(z) curves and clarified rod insertion limit curve applicability.
		2	2/11/91	Incorporated revised F <sub>Q</sub> of 2.45 as a result of NRC approval of Westinghouse Topical Report WCAP-10924-P-A, Volume 1, Addendum 4, October 1990.
1	15	0	6/25/91	Updated to Unit 1 Cycle 15.
2	15	0	3/9/92	Updated to Unit 2 Cycle 15 and clarified labeling of Figure 4. Clarified the actions to be taken if the nuclear enthalpy rise hot channel factor exceeds the Technical Specification limit.
1	16	0	12/28/92	Updated to Unit 1 Cycle 16, removed V(z) curves and replaced them with list of bounding V(z) values for three ranges of exposures.
 2	16	0	12/8/93	Updated to Unit 2 Cycle 16. Removed the multiple $V(z)$ curves and replaced them with a single figure with bounding $V(z)$ curves for four ranges of exposures. Incorporated additional discussion related to $V(z)$ and $K(z)$ .

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# Core Operating Limits Report

## **Record of Revision**

 Unit	Cycle	Revision No.	Approval Date	Remarks
2	16	1	11/3/94	The table containing the bounding V(z) values and Figure 2 updated to incorporate revised bounding V(z) values for the exposure range of 14-21.5 GWD/MTU. Figures 3 through 6 re- formatted.
1	17	0	6/17/94	Updated to Unit 1 Cycle 17. Removed the list of bounding V(z) values and replaced it with multiple V(z) curves. Incorporated additional discussion related to V(z) and K(z).
2	17	0	6/2/95	Updated to Unit 2 Cycle 17. Incorporated Table 1 and expanded Figure 2 with updated bounding V(z) values.
1	18	0	2/7/96	Updated to Unit 1 Cycle 18. Incorporated revised $F_{\Delta H}$ limit of 1.77. Incorporated Table 1 and updated Figure 2 with revised bounding V(z) values.
2	18	0	2/27/97	Updated to Unit 2 Cycle 18. Revised $F_{\Delta H}$ limit to 1.77. Updated Table 1 and Figures 2a through 2e with revised bounding V(z) values. Incorporated new Figures 2f and 2g with additional bounding V(z) values.
1	19	0	9/25/97	Updated to Unit 1 Cycle 19. Updated Table 1 and Figures 2a through 2f with revised bounding V(z) values.
2	19	0	12/17/98	Updated to Unit 2 Cycle 19. Updated Table 1 and Figures 2a through 2d with revised bounding V(z) values. Deleted Figures 2e, 2f and 2g.
1	20	<b>0</b>	5/13/99	Updated to Unit 1 Cycle 20. Updated Table 1 and Figures 2a through 2f with revised bounding V(z) values.
		1	8/4/00	Technical Specification Amendment 151: Relocate shutdown margin (SDM) requirements from Tech Specs and incorporate additional SDM requirements for Modes 3-6 from revised analysis of Uncontrolled Dilution event.

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# Core Operating Limits Report

# **Record of Revision**

	Unit	Cycle	Revision No.	Approval Date	Remarks
	2	20	0	5/31/00	Updated to Unit 2 Cycle 20. Updated Table 1 and Figures 2a through 2d with revised bounding V(z) values. Added new Table 2 and Figures 2e, 2f and 2g with additional bounding V(z) values. Added references to Tables 1 and 2 and to Figures 2e, 2f and 2g to discussion of heat flux hot channel factor limits. Added discussion clarifying applicability of axial flux difference limits when using Tables 1 and 2 and Figures 2a through 2g. Added discussion of two tier V(z) curve presented in Table 2 and Figure 2g.
			1	8/4/00	Technical Specification Amendment 142: Relocate shutdown margin (SDM) requirements from Tech Specs and incorporate additional SDM requirements for Modes 3-6 from revised analysis of Uncontrolled Dilution event.
	1	20	2	9/1/00	Revised to change axial flux difference target band.
	<b>1</b>	21	0	1/31/01	Updated to support refueling activities associated with Unit 1 Cycle 21. Revision 0 of the Unit 1 Cycle 21 COLR had to be issued prior to confirming the applicability of the LOCA analysis. Therefore, Revision 0 of the Unit 1 Cycle 21 COLR does not contain all of the operating limits necessary to support operation of Unit 1 Cycle 21.
-1 I -	<b>.1</b>	21	1	2/19/01	Updated to Unit 1 Cycle 21. Updated Tables 1 and 2 and Figures 2a through 2f with revised bounding V(z) values.
	1	21	2	10/02/02	Revised to support License Amendment 158 changes, including revision of all references to TS, revision of $F_Q$ symbols, addition of Table 4, ITC limits, DNB limits and refueling boron concentrations.
	2	21	0	2/06/02	Updated to Unit 2 Cycle 21.





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# Core Operating Limits Report

## **Record of Revision**

	Unit	Cycle	Revision No.	Approval Date	Remarks
	2	21	1	10/02/02	Revised to support License Amendment 149 changes, including revision of all references to TS, revision of $F_{Q}$ symbols, addition of Table 4, ITC limits, DNB limits and refueling boron concentrations. Also revised to include an additional V(z) curve to give greater $F_{Q}$ margin between 13.0 and 16.0 GWd/MTU.
	1	22	0	11/25/02	Updated to Unit 1 Cycle 22. Updated Tables 1 and 2 and Figures 2a through 2f with revised bounding V(z) values. Incorporated new Figure 2g with additional bounding V(z) values. Updated Table 3 with revised minimum shutdown margin limits. Deleted and revised text to eliminate duplication with the Technical Specifications and the Bases.
	2	22	0	9/19/03	Updated to Unit 2 Cycle 22. Updated Tables 1 and 2. A reduced number of exposure ranges were calculated in Table 1, therefore new Figures 2a through 2e with revised bounding V(z) values replaced Figures 2a through 2f. New Figure 2f replaced Figure 2g for the 2 tier band bounding V(z) values. Updated Table 3 with revised minimum shutdown margin limits. Deleted and revised text to eliminate duplication with the Technical Specifications and the Bases.
;	1	22	1	7/6/04	Revision to incorporate Westinghouse Safety Analysis Transition per LA 162/153. Revision 1 contains transitional values for the OP/OT $\Delta$ T Trip setpoints that will be used while the physical changes are implemented.
	2	22	1 <sup>1</sup>	7/6/04	Revision to incorporate Westinghouse Safety Analysis transition per LA 162/153. Revision 1 contains transitional values for the OP/OT $\Delta$ T Trip setpoints that will be used while the physical changes are implemented.
	2	22	2	7/12/04	Revised Fq limit from 2.4 to 2.5. Removed OP and OT delta-T setpoints based on NMC methodology and replaced with Westinghouse developed setpoints.



# Core Operating Limits Report

## Record of Revision

	Unit	Cycle	Revision No.	Approval Date	Remarks
	1	22	2	7/16/04	Revised Fq limit form 2.4 to 2.5. Removed OP and OT delta-T setpoints based on NMC methodology and replaced with Westinghouse developed setpoints.
	1	23	0	10/20/04	Updated to Unit 1 Cycle 23.
	2	23	0	-	Not used due to core redesign.
	2	23	1	5/19/05	Updated to Unit 2 Cycle 23 and to support redesign of Unit 2 Cycle 23 core.
•	1	23	1	7/11/05	Revised ITC upper limit from < 0 pcm/°F for power levels > 70% RTP to less than a line that slopes linearly from 0 pcm/°F at 70% RTP to -2.9 pcm/°F at 100% RTP. Revised the title of Figure 3 to reference T.S. 3.1.4 Condition B and revised the title of Figure 4 to reference T.S. 3.1.4 Condition A. Added references 24 and 25 to include the 50.59 screenings written to issue revision 1.
	1	24	0	5/10/06	Updated to Unit 1 Cycle 24.
	1	24	1	8/7/06	Updated Table 3 to reflect the correct $F_q^w(z)$ penalty factors.
	2	24	0	11/26/06	Updated to Unit 2 Cycle 24 Modes 5 and 6.
	2	24	1	12/6/06	Updated to Unit 2 Cycle 24 for Modes 1-6.
	2	24	2	9/4/07	Revised to support LA-179/169. Revised reference 24 to include the revision number (revision 0) and the correct date of the report (January 2005). Revised references 6a, 6b, 6c, and 8 to say 'Deleted.' These references referred to the old LBLOCA methodology and model.
	1	24	2	2/11/08	Updated Table 1 to reflect correct Shutdown Margin Requirements and added Figures 6A through 6H.



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# Core Operating Limits Report

## Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
2	24	3	2/11/08	Updated Table 1 to reflect correct Shutdown Margin Requirements and added Figures 6A through 6H.
1	25	0	2/24/08	Updated to Unit 1 Cycle 25
1	25	1	5/28/08	Updated Table 2 to reflect the correct W(z) at a burnup of 150 MWd/MTU and a core height of 6.20 feet
2	25	0	9/26/08	Updated for Unit 2 Cycle 25
1	26	0	9/24/09	Updated for Unit 1 Cycle 26
- 2	26	0	5/3/10	Updated for Unit 2 Cycle 26
2	26	1	5/17/10	Updated to include part power $W(z)$ factors
1	26	1	9/2/10	Updated for second set of W(z) factors
2	26	2	9/30/10	Updated for Measurement Uncertainty Recapture power uprate to 1677 MWth and for a second set of W(z) factors
1	26	2	9/30/10	Updated for Measurement Uncertainty Recapture power uprate to 1677 MWth
1	26	3	12/17/10	Updated SDM in Table 1 for Mode 2 to say 1.9.

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## **Core Operating Limits Report** Unit 1, Cycle 26 **Revision 3**

## PRAIRIE ISLAND NUCLEAR GENERATING PLANT

#### CORE OPERATING LIMITS REPORT

#### UNIT 1 - CYCLE 26

#### **REVISION 3**

12/11/10 Date:

Reviewed By:

Ι.

Lynn Johnson Supervisor, NSSS

Reviewed By: Hank Hoelscher

Supervisor, PWR Analyses

Date: 12 /15/10

Date: 12-17-19 Approved By: Thomas Roddey

Director, Site Engineering

Note: This report is not part of the Technical Specifications

This report is referenced in the Technical Specifications

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Core Operating Limits Report Unit 1, Cycle 26 Revision 3

# PRAIRIE ISLAND NUCLEAR GENERATING PLANT CORE OPERATING LIMITS REPORT

#### UNIT 1 - CYCLE 26

#### **REVISION 3**

This report provides the values of the limits for Unit 1 Cycle 26 as required by Technical Specification 5.6.5. These values have been established using NRC approved methodology and are established such that all applicable limits of the plant safety analysis are met. The Technical Specifications affected by this report are listed below:

- 1. 2.1.1 Reactor Core SLs
- 2. 3.1.1 Shutdown Margin (SDM)
- 3. 3.1.3 Isothermal Temperature Coefficient (ITC)
- 4. 3.1.5 Shutdown Bank Insertion Limits
- 5. 3.1.6 Control Bank Insertion Limits
- 6. 3.1.8 Physics Tests Exceptions MODE 2
- 7. 3.2.1 Heat Flux Hot Channel Factor  $(F_0(z))$
- 8. 3.2.2 Nuclear Enthalpy Rise Hot Channel Factor  $(F_{AH}^{N})$
- 9. 3.2.3 Axial Flux Difference (AFD)
- 3.3.1 Reactor Trip System (RTS) Instrumentation
  Overtemperature ΔT and Overpower ΔT Parameter Values for Technical
  Specification Table 3.3.1-1
- 11. 3.4.1 RCS Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
- 12. 3.9.1 Boron Concentration

#### 1. <u>2.1.1 Reactor Core Safety Limits</u>

Reactor Core Safety Limits are shown in Figure 1.

Reference Technical Specification 2.1.1.

2. <u>3.1.1 Shutdown Margin Requirements</u>

Minimum Shutdown Margin requirements are shown in Table 1.

Reference Technical Specification 3.1.1.

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#### 3. <u>3.1.3 Isothermal Temperature Coefficient (ITC)</u>

ITC Upper limit:

- a.  $< 5 \text{ pcm/}^{\circ}\text{F}$  for power levels < 70% RTP; and
- b. less than a line which slopes linearly from
  - i. 0 pcm/ $^{\circ}$ F at a power level = 70% RTP to
    - ii. -1.5 pcm/°F at a power level = 100% RTP
- ITC Lower limit: a. -43.15 pcm/°F

Reference Technical Specification 3.1.3.

4. <u>3.1.5 Shutdown Bank Insertion Limits</u>

The shutdown rods shall be fully withdrawn.

Reference Technical Specification 3.1.5.

## 5. <u>3.1.6 Control Bank Insertion Limits</u>

The control rod banks shall be limited in physical insertion as shown in Figures 2, 3, and 4.

The control rod banks withdrawal sequence shall be Bank A, Bank B, Bank C, and finally Bank D.

The control rod banks shall be withdrawn maintaining 128 step tip-to-tip distance.

Reference Technical Specification 3.1.6.

#### 3.1.8 Physics Tests Exceptions - MODE 2

6.

Minimum Shutdown Margin requirements during physics testing are shown in Table 1.

Reference Technical Specification 3.1.8.

#### 3.2.1 Heat Flux Hot Channel Factor (Fo(Z))

The Heat Flux Hot Channel Factor shall be within the following limits:

CFQ = 2.50

7.

K(Z) is a constant value = 1.0 at all elevations.

The HFP W(Z) values are provided in Table 2 and Table 4.

The W(Z) values in Table 2 are only applicable to Figure 5.

The W(Z) values in Table 4 are only applicable to Figure 6.

The data in Tables 2 and 4 should be used independently; cross interpolation or extrapolation between W(Z) sets is prohibited.

The  $F^{W}_{Q}(Z)$  Penalty Factors associated with Figure 5 and Table 2 are provided in Table 3.

The  $F^{W}_{Q}(Z)$  Penalty Factors associated with Figure 6 and Table 4 are provided in Table 5.

The Axial Flux Difference (AFD) Band in Figure 6 is more restrictive than the AFD Band in Figure 5. Prior to switching from Figure 6 to Figure 5,  $F^{W}_{Q}(Z)$  must be confirmed to meet Technical Specification requirements by one of the follow methods:

- Confirm F<sup>W</sup><sub>Q</sub>(Z) meets the Technical Specification Limit with the Table 2
  W(Z) values for the most recent surveillance performed.
- 2. Perform a new surveillance and confirm  $F^{W}_{Q}(Z)$  meets the Technical Specification Limit with the Table 2 W(Z) values.

The HFP W(Z) values are generated assuming that they will be used for full power surveillance. When a part power surveillance is performed, the W(Z) values should be multiplied by the factor 1/P, when P > 0.5. When P is  $\leq 0.5$ , the W(Z) values should be multiplied by the factor 1/(0.5), or 2.0. This is consistent with the adjustment in the F<sub>Q</sub>(Z) limit at part power conditions.

Reference 10 provides the basis for multiple sets of W(Z) curves.

#### Applicability: MODE 1

Reference Technical Specification 3.2.1.

8. <u>3.2.2 Nuclear Enthalpy Rise Hot Channel Factor ( $F_{AH}^{N}$ )</u>

The Nuclear Enthalpy Rise Hot Channel Factor shall be within the following limits:

 $F_{\Delta H} \le 1.77 \text{ x} [1 + 0.3(1 - P)]$  for all 422V+ type fuel assemblies, and

 $F_{\Delta H} \le 1.712 \text{ x} [1 + 0.3(1 - P)]$  for all OFA type fuel assemblies

where: P is the fraction of RATED THERMAL POWER at which the core is operating.

**Applicability: MODE 1** 

Reference Technical Specification 3.2.2.

## 9. <u>3.2.3 Axial Flux Difference (AFD)</u>

The indicated axial flux difference shall be maintained within the allowed operational space defined by Figure 5 or the more restrictive operational space as defined by Figure 6.

Both Figures 5 and 6 can be used any time during the cycle.

Prior to switching to the more restrictive AFD envelope (Figure 6), it should be confirmed that the plant is within the specified  $\overrightarrow{AFD}$  envelope

**Applicability:** MODE 1 with THERMAL POWER  $\geq$  50% RTP

Reference Technical Specification 3.2.3.

#### 10. 3.3.1 Reactor Trip System (RTS) Instrumentation

Overtemperature  $\Delta T$  and Overpower  $\Delta T$  Parameter Values for Technical Specification Table 3.3.1-1 (Note 1 and Note 2);

#### Overtemperature $\Delta T$ Setpoint

Overtemperature  $\Delta T$  setpoint parameter values:

$\Delta T_0$	Notes	Indicated A	ΔT	at RATED	THERMAL	POWER, %
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T = Average temperature, °F

 $T' = 560.0 \,^{\circ}F$ 

P = Pressurizer Pressure, psig

- P' = 2235 psig
- $K_1 \leq 1.17$
- $K_2 = 0.014 / {}^{\circ}F$
- $K_3 = 0.00100 / psi$

 $\tau_1 = 30$  seconds

 $\tau_2 = 4$  seconds

 $f(\Delta I) = A$ 

A function of the indicated difference between top and bottom detectors of the power range nuclear ion chambers. Selected gains are based on measured instrument response during plant startup tests, where  $q_t$  and  $q_b$  are the percent power in the top and bottom halves of the core respectively, and  $q_t + q_b$  is total core power in percent of RATED THERMAL POWER, such that

- (a) For  $q_t q_b$  within -13, +8 %  $f(\Delta I) = 0$
- (b) For each percent that the magnitude of  $q_t q_b$  exceeds +8% the  $\Delta T$  trip setpoint shall be automatically reduced by an equivalent of 1.73 % of RATED THERMAL POWER.
- (c) For each percent that the magnitude of  $q_t q_b$  exceeds -13 % the  $\Delta T$  trip setpoint shall be automatically reduced by an equivalent of 3.846 % of RATED THERMAL POWER.

#### Overpower AT Setpoint

Overpower  $\Delta T$  setpoint parameter values:

Indicated AT at RATED THERMAL POWER, %  $\Delta T_0$ = Т Average temperature, °F == T' 560.0 °F == K4 1.11  $\leq$ K5 === 0.0275/°F for increasing T; 0 for decreasing T K<sub>6</sub> === 0.002/°F for T > T'; 0 for  $T \le T'$ 10 seconds T3 ===

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11. <u>3.4.1 RCS Pressure, Temperature, and Flow - Departure from Nucleate Boiling (DNB)</u> Limits

The DNB Limits are: Pressurizer pressure limit = 2190 psia RCS average temperature limit =  $564^{\circ}F$ RCS total flow rate limit = 178,000 gpm

**Reference Technical Specification 3.4.1.** 

#### 12. <u>3.9.1 Refueling Boron Concentration.</u>

The boron concentration of the reactor coolant system and the refueling cavity shall be sufficient to ensure that the more restrictive of the following conditions is met:

- a)  $K_{eff} \leq 0.95$
- b) 2000 ppm
- c) The Shutdown Margin specified in Table 1

Reference Technical Specification 3.9.1.

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#### REFERENCES

#### (NRC Approved Methodologies for COLR Parameters)

- 1. NSPNAD-8101-A, "Qualification of Reactor Physics Methods for Application to Prairie Island," Revision 2, October 2000.
- 2. NSPNAD-8102-PA, "Prairie Island Nuclear Power Plant Reload Safety Evaluation Methods for Application to PI Units," Revision 7, July 1999.
- 3. NSPNAD-97002-PA, "Northern States Power Company's "Steam Line Break Methodology," Revision 1, October 2000.
- 4. WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July, 1985.
- 5.a WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model using the NOTRUMP Code," August, 1985.
- 5.b WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model using the NOTRUMP Code," Addendum 2 Revision 1, July 1997.
- 6. Not used.
- 7. WCAP-10924-P-A, Volume 1, Revision 1, and Volume 2, Revision 2, "Westinghouse Large Break LOCA Best Estimate Methodology," September 2005.
- 8. XN-NF-77-57-(A), XN-NF-77-57, Supplement 1 (A), "Exxon Nuclear Power Distribution Control for Pressurized Water Reactors Phase II," May 1981.
- 9. WCAP-13677-P-A, "10 CFR 50.46 Evaluation Model Report: W-COBRA/TRAC 2-Loop Upper Plenum Injection Model Update to Support ZIRLO<sup>®</sup> Cladding Options," February 1994.
- 10. NSPNAD-93003-A, "Prairie Island Units 1 and 2 Transient Power Distribution Methodology," Revision 0, April 1993.
- 11. NAD-PI-003, "Prairie Island Nuclear Power Plant Required Shutdown Margin During Physics Tests," Revision 0, January 2001.
- 12. NAD-PI-004, "Prairie Island Nuclear Power Plant  $F^{W}_{Q}(Z)$  Penalty With Increasing  $[F^{C}_{Q}(Z) / K(Z)$ Trend," Revision 0, January 2001.
- 13. WCAP-10216-P-A, Revision 1A, "Relaxation of Constant Axial Offset Control/ FQ Surveillance Technical Specification," February 1994.

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- 14. WCAP-8745-P-A, "Design Bases for the Thermal Overpower  $\Delta T$  and Thermal Overtemperature  $\Delta T$  Trip Functions," September 1986.
- 15. WCAP-11397-P-A, "Revised Thermal Design Procedure," April 1989.
- 16. WCAP-14483-A, "Generic Methodology for Expanded Core Operating Limits Report," January 1999.
- 17. WCAP-7588 Rev. 1-A, "An Evaluation of the Rod Ejection Accident in Westinghouse Pressurized Water Reactors Using Spatial Kinetics Methods," January 1975.
- 18. WCAP-7908-A, "FACTRAN A FORTRAN IV Code for Thermal Transients in a UO<sub>2</sub> Fuel Rod," December 1989.
- 19. WCAP-7907-P-A, "LOFTRAN Code Description," April 1984.
- 20. WCAP-7979-P-A, "TWINKLE A Multidimensional Neutron Kinetics Computer Code," January 1975.
- 21. WCAP-10965-P-A, "ANC: A Westinghouse Advanced Nodal Computer Code," September 1986.
- 22. WCAP-11394-P-A, "Methodology for the Analysis of the Dropped Rod Event," January 1990.
- 23. WCAP-11596-P-A, "Qualification of the PHOENIX-P/ANC Nuclear Design System for Pressurized Water Reactor Cores," June 1988.
- 24. WCAP-12910 Rev. 1-A, "Pressurizer Safety Valve Set Pressure Shift," May 1993.
- 25. WCAP-14565-P-A, "VIPRE-01 Modeling and Qualification for Pressurized Water Reactor Non-LOCA Thermal-Hydraulic Safety Analysis," October 1999.
- 26. WCAP-14882-P-A, "RETRAN-02 Modeling and Qualification for Westinghouse Pressurized Water Reactor Non-LOCA Safety Analyses," April 1999.
- 27. WCAP-16009-P-A, "Realistic Large-Break LOCA Evaluation Methodology Using the Automated Statistical Treatment Of Uncertainty Method (ASTRUM)," Revision 0, January 2005.
- 28. Caldon, Inc. Engineering Report-80P, "Improving Thermal Power Accuracy and Plant Safety While Increasing Operating Power Level Using the LEFM √<sup>™</sup> System," Revision 0, March 1997.
- 29. Caldon, Inc. Engineering Report-157P, "Supplement to Topical Report ER-80P: Basis for a Power Uprate With the LEFM √<sup>TM</sup> Check or CheckPlus<sup>TM</sup> System," Revision 5, October 2001.
- 30. 50.59 Evaluation 1072, Revision 3, "Unit 1 Cycle 26 Core Reload."

#### Table 1

#### Minimum Required Shutdown Margin, % Ap

	Number	r of Charging Pumps R	unning**
Mode 1*			
	0-1 Pump	2 Pumps	3 Pumps
0-22000 MWd/MTU		999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	

Mode 2*		₩ 1.8 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	
	0-1 Pump	2 Pumps	3 Pumps
0-22000 MWd/MTU	1.9	1.9	1.9

Physics Testing in Mode 2			
	0-1 Pump	2 Pumps	3 Pumps
0-22000 MWd/MTU	0.5	0.5	0.5

Mode 3	Tave ≥ 5	20 °F (Most Reac	tive Rod Out)
	0-1 Pump	2 Pumps	3 Pumps
0-22000 MWd/MTU	2.0	2.0	2.0

Mode 3	350 °F ≤ Tave < 520°F (Most Reactive Rod Out)				
·	0-1 Pump	2 Pumps	3 Pumps		
0 MWd/MTU	2.0	2.0	2.5		
12000 MWd/MTU	2.0	2.0	2.0		
22000 MWd/MTU	2.0	2.0 '	2.0		

Mode 4	200 °F < Tave < 350°F (Most Reactive Rod Out)					
	0-1 Pump	2 Pumps	3 Pumps			
0 MWd/MTU	2.0	4.0	6.5			
12000 MWd/MTU	2.0	3.0	4.5			
22000 MWd/MTU	2.0	2.0	2.5			

Operational Mode Definitions, as per TS Table 1.1-1.

For Mode 1 and Mode 2 with  $K_{eff} \ge 1.0$ , the minimum shutdown margin requirements are provided by the Rod Insertion Limits.

\*\* Charging pump(s) in service only pertains to steady state operations. It does not include transitory operations. For example, operations such as starting a second charging pump in order to secure the operating pump would fall under the one pump in service column.

## Table 1, Continued

## Minimum Required Shutdown Margin, % Ap

Number of Charging Pumps Running**						
Mode 5	$68^{\circ}F \leq Tave \leq 200^{\circ}F$ (Most Reactive Rod Out)					
	0-1 Pump	2 Pumps	3 Pumps			
0 MWd/MTU***	· 2.5	• 4.5	7.0			
12000 MWd/MTU	2.0	3.5	5.0			
22000 MWd/MTU	2.0	2.0	3.0			

Mode 6	68	$F^{\circ}F^{\circ} \leq Tave < 200^{\circ}F$ (A	RI)
e - maintir .	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU***	5.129	5.129	7.0
12000 MWd/MTU	5.129	5.129	5.129
22000 MWd/MTU	5.129	5.129	5.129

Mode 6	68	$^{\circ}F \leq Tave < 200^{\circ}F$ (A)	RO)
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU***	5.129	5.5	8.5
12000 MWd/MTU	5.129	5.129	7.0
22000 MWd/MTU	5.129	5.129	5.129

Operational Mode Definitions, as per TS Table 1.1-1.

\*\* Charging pump(s) in service only pertains to steady state operations. It does not include transitory operations. For example, operations such as starting a second charging pump in order to secure the operating pump would fall under the one pump in service column.

\*\*\* These values are also applicable for the Unit 1 Cycle 25 end of cycle.

	Height				BU [MWd/MTU]			
	[ft]	150	4000	8000	13000	16000	18000	20000
		AO = 0.70	AO = -1.71	AO = -3.30	AO = -4.80	AO = -0.04	AO = 0.81	AO = -0.10
[BOTTOM] 1	0.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
2	0.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
6	1.0	1.2964	1.2134	1.1709	1.1640	1.2375	1.2516	1.2658
7	1.2	1.2842	1.2042	1.1626	1.1552	1.2283	1.2411	1.2540
8	1.4	1.2702	1.1938	1.1534	1.1455	1.2182	1.2297	1.2411
9	1.6	1.2549	1.1825	1.1437	1.1353	1.2078	1.2178	1.2278
10	1.8	1.2383	1.1708	1.1336	1.1250	1.1972	1,2057	1.2141
11	2.0	1.2226	1.1581	1.1236	1.1146	1.1864	1.1932	1.2001
. 12	2.2	1.2083	1.1468	1.1129	1.1043	1.1755	1.1805	1.1855
13	2.4	1.1944	1.1388	1.1033	1.0942	1.1646	1.1677	1.1707
14	2.6	1.1802	1.1312	1.0995	1.0843	1.1536	1.1547	1.1558
15	2.8	1.1662	1.1236	1.0973	1.0746	1.1430	1.1404	1.1378
16	3.0	1.1513	1.1159	1.0955	1.0664	1.1308	1.1313	1.1319
17	3.2	1.1430	1.1109	1.0946	1.0643	1.1254	1.1313	1.1372
18	3.4	1.1423	1.1108	1.0945	1.0675	1.1290	1.1377	1.1464
19	3.6	1.1409	1.1115	1.0994	1.0752	1.1344	1.1471	1.1599
20	3.8	1.1389	1.1135	1.1047	1.0827	1.1389	1.1560	1.1730
21	4.0	1.1363	1.1158	1.1091	1.0893	1.1427	1.1636	1.1845
22	4.2	1.1328	1.1172	1.1130	1.0955	1.1455	1.1701	1.1947
23	4.4	1.1288	1.1181	1.1161	1.1008	1.1472	1.1753	1.2033
24	4.6	1.1264	1.1184	1.1185	1.1053	1.1479	1,1791	1.2102
25	4.8	1.1243	1.1178	1.1203	1.1104	1.1476	1.1815	1.2153
26	5.0	1.1216	1.1181	1.1210	1.1160	1.1461	1.1825	1.2190
27	5.2	1.1187	1.1212	1.1221	1.1214	1.1447	1.1822	1.2198
28	5.4	1.1151	1.1264	1.1263	1.1260	1.1451	1.1807	1.2163
29	5.6	1.1120	1.1314	1.1321	1.1292	1.1507	1.1816	1.2125
30	5.8	1.1167	1.1378	1.1386	1.1390	1.1595	1.1893	1.2191
31	6.0	1.1275	1.1459	1.1470	1.1543	1.1684	1.2016	1.2348
32	6.2	1.1358	1.1544	1.1583	1.1700	1.1759	1.2109	1.2459
33	6.4	1.1438	1.1618	1.1713	1.1848	1.1823	1.2191	1.2559
34	6.6	1.1509	1.1680	1.1833	1.1985	1.1876	1.2258	1.2639
35	6.8	1.1570	1.1751	1.1942	1.2111	1.1915	1.2307	1.2699
36	7.0	1.1621	1.1827	1.2039	1.2224	1.1941	1.2339	1.2736
37	7.2	1.1659	1.1891	1.2122	1.2321	1.1959	1.2351	1.2742
38	7.4	1.1684	1.1946	1.2189	1.2400	1.1971	1.2342	1.2713
39	7.6	1.1708	1.1995	1.2237	1.2460	1.1965	1.2311	1.2657
40	7.8	1.1720	1.2030	1.2266	1.2497	1.1941	1.2257	1.2573
41	8.0	1.1713	1.2046	1.2272	1.2511	1.1897	1.2179	12462
42	8.2	1.1690	1.2042	1.2255	1.2500	1.1835	1.2078	1.2321
43	8.4	1.1648	1.2018	1.2213	1.2462	1.1753	1.1952	1.2152
44	8.6	1.1590	1.1976	1.2149	1.2391	1.1640	1.1806	1.1972
45	8.8	1.1502	1.1902	1.2047	1.2327	1.1573	1.1689	1.1805
46	9.0	1.1482	1.1882	1.1999	1.2311	1.1576	1.1581	1.1586
47	9.2	1.1564	1.1945	1.2018	1.2328	1.1603	1.1481	1.1359
48	9.4	1.1612	1.1972	1.2056	1.2364	1.1612	1.1473	1.1334
49	9.6	1.1695	1.2032	1.2073	1.2379	1.1608	1.1454	1.1300
50	9.8	1.1774	1.2089	1.2117	1.2381	1.1588	1.1406	1.1224
51	10.0	1.1839	1.2132	1.2194	1.2412	1.1562	1.1401	1.1240
52	10.0	1.1896	1.2166	1.2259	1.2480	1.1560	1.1470	1.1379
53	10.2	1.1900	1.2158	1.2311	1.2528	1.1602	1.1524	1.1446
53	10.4	1.1900	1.2158	1.2374	1.2528	1.1656	1.1524	1.1542
55	10.8	1.2010	1.2154	1.2436	1.2639	1.1711	1.1688	1.1666
56	11.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

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# Table 2 - W(z) Values associated with Figure 5 (Top 10% and Bottom 8% excluded)\*

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	Height		BO [MWd/MTO]					
	[ft]	150	4000	8000	13000	16000	18000	20000
		AO = 0.70	AO = -1.71	AO = -3.30	AO = -4.80	AO = -0.04	AO = 0.81	AO = -0.10
57	11.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
58	11.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
59	11.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
60	11.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[TOP] 61	12.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

# Table 2 (cont) - W(z) Values associated with Figure 5 (Top 10% and Bottom 8% excluded)\*

\* Linear extrapolation based on a line between 18,000 MWD/MTU and 20,000 MWD/MTU is adequate for addressing burnups beyond 20,000 MWD/MTU.

#### Table 3

# $F^{W}_{Q}(Z)$ Penalty Factor associated with Figure 5 and Table 2

Cycle Burnup (MWD/MTU)	F <sup>W</sup> <sub>O</sub> (Z) Penalty Factor
14632	1.0200
14779	1.0203
14925	1.0202
15071	1.0200

 $F^{W}_{Q}(Z) = 1.020$  for all burnups except those listed above. Linear interpolation is adequate for intermediate cycle burnups.

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	Height	T		ur - Aler di Pindon kanalasan haran da sanadar sebukan da	BU [MWd/MTU]			
	[ft]	150	4000	8000	13000	16000	18000	20000
		AO = 0.70	AO = -1.71	AO = -3.30	AO = -4.80	AO = -0.04	AO = 0.81	AO = -0.10
[BOTTOM] 1	0.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
2	0.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
6	1.0	1.2724	1.1878	1.1447	1.0798	1.1713	1.2067	1.1863
7	1.2	1.2607	1.1790	1.1369	1.0737	1.1631	1.1972	1.1758
8	1.4	1.2471	1.1690	1.1281	1.0670	1.1540	1.1869	1.1645
9	1.6	1.2324	1.1583	1.1189	1.0602	1.1447	1.1764	1.1531
10	1.8	1.2166	1.1470	1.1094	1.0536	1.1353	1.1658	1.1417
11	2.0	1.2000	1.1353	1.0998	1.0472	1.1259	1.1551	1.1303
12	2.2	1.1830	1.1233	1.0901	1.0410	1.1166	1.1444	1.1189
13	2.4	1.1657	1.1114	1.0807	1.0353	1.1073	1.1336	1.1077
14	2.6	1.1483	1.0996	1.0715	1.0303	1.0980	1.1230	1.0969
15	2.8	1.1315	1.0875	1.0619	1.0241	1.0909	1.1117	1.0843
16	3.0	1.1134	1.0779	1.0562	1.0270	1.0844	1.1028	1.0814
17	3.2	1.1033	1.0749	1.0565	1.0385	1.0823	1.1017	1.0886
18	3.4	1.1031	1.0769	1.0617	1.0488	1.0886	1.1094	1.0955
19	3.6	1.1027	1.0835	1.0706	1.0592	1.0966	1.1175	1.1025
20	3.8	1.1026	1.0899	1.0793	1.0692	1.1041	1.1248	1.1133
21	4.0	1.1036	1.0957	1.0873	1.0787	1.1109	1.1321	1.1250
22	4.2	1.1057	1.1009	1.0947	1.0876	1.1169	1.1402	1.1351
23	4.4	1.1070	1.1055	1.1014	1.0959	1.1220	1.1491	1.1442
24	4.6	1.1079	1.1095	1.1073	1.1033	1.1259	1.1566	1.1520
25	4.8	1.1084	1.1125	1.1126	1.1101	1.1312	1.1628	1.1585
26	5.0	1.1084	1.1163	1.1170	1.1160	1.1369	1.1677	1.1635
27	5.2	1.1079	1.1212	1.1212	1.1214	1.1413	1.1714	1.1678
28	5.4	1.1073	1.1264	1.1263	1.1260	1.1449	1.1738	1.1746
29	5.6	1.1093	1.1314	1.1320	1.1292	1.1507	1.1745	1.1866
30	5.8	1.1167	1.1378	1.1386	1.1384	1.1595	1.1787	1.1984
31	6.0	1.1273	1.1459	1.1463	1.1512	1.1684	1.1854	1.2083
32	6.2	1.1358	1.1544	1.1535	1.1633	1.1759	1.1912	1.2170
33	6.4	1.1438	1.1618	1.1598	1.1747	1.1823	1.1958	1.2242
34	6.6	1.1509	1.1680	1.1680	1.1851	1.1876	1.1991	1.2298
35	6.8	1.1570	1.1737	1.1760	1.1944	1.1915	1.2008	1.2336
36	7.0	1.1621	1.1778	1.1827	1.2023	1.1940	1.2014	1.2357
37	7.2	1.1659	1.1808	1.1883	1.2091	1.1950	1.2013	1.2358
38	7.4	1.1684	1.1830	1.1937	1.2157	1.1942	1.2001	1.2339
<u>39</u> 40	7.6	1.1694	1.1844	1.1979	1.2206	1.1917	1.1971	1.2232
40 41	8.0	1.1687	1.1842	1.2003	1.2235	Concernance of the local day of the loca	1.1921	1.2143
		1.1662	i.1822	1.2010	1.2244	1.1806		1.2030
42	8.2	1.1618	1.1782	1.1996	1.2232	1.1721	<u>1.1760</u> 1.1651	1.1894
43	8.6	1.1553	And a second design of the sec	1.1961	and the second distance of the second distanc	1.1614	1.1515	1.1738
44 45		1.1472	1.1647	1.1908	1.2135		1.1415	1.1738
45	8.8	1.1353	1.1537	1.1818	1.2071	1.1361		1.1413
40	9.0 9.2	1.1295	1.1504	1.1779	1.2055	1.1275	1.1336	1.1413
47 48	9.2	1.1320	1.1597	1.1801			1.1097	1.1215
40	9.4	1.1393		1.1801	1.2071	1.1184	1.1003	1.1259
50	9.8		1.1711	Contraction of Contra			1.0993	1.1345
51	9.8	1.1509		1.1846	1.2107	1.1105	1.1028	1.1345
52	10.0	1.1545	1.1775	1.1909	1.2158	1.1144	1.1028	1.1410
53	10.2	1.1537	1.1825	1.2004	1.2260	1.1326	1.1043	1.1556
54	10.4	1.1564				1.1326	1.1052	1.1621
55	10.8	1.1573	1.1902	1.2161	1.2426	1.1445	1.1100	1.1682
56	11.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

# Table 4 - W(z) Values associated with Figure 6 (Top 10% and Bottom 8% excluded)\*

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	Height		BU [MWd/MTU]					
	[ft]	150	4000	8000	13000	16000	18000	20000
		AO = 0.70	AO = -1.71	AO = -3.30	AO = -4.80	AO = -0.04	AO = 0.81	AO = -0.10
57	11.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
58	11.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
59	11.6	1.0000-	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
60	11.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[TOP] 61	12.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

# Table 4 (cont) - W(z) Values associated with Figure 6 (Top 10% and Bottom 8% excluded)\*

Linear extrapolation based on a line between 18,000 MWD/MTU and 20,000 MWD/MTU is adequate for addressing \* burnups beyond 20,000 MWD/MTU.

#### Table 5

# $F^{W}_{Q}(Z)$ Penalty Factor associated with Figure 6 and Table 4

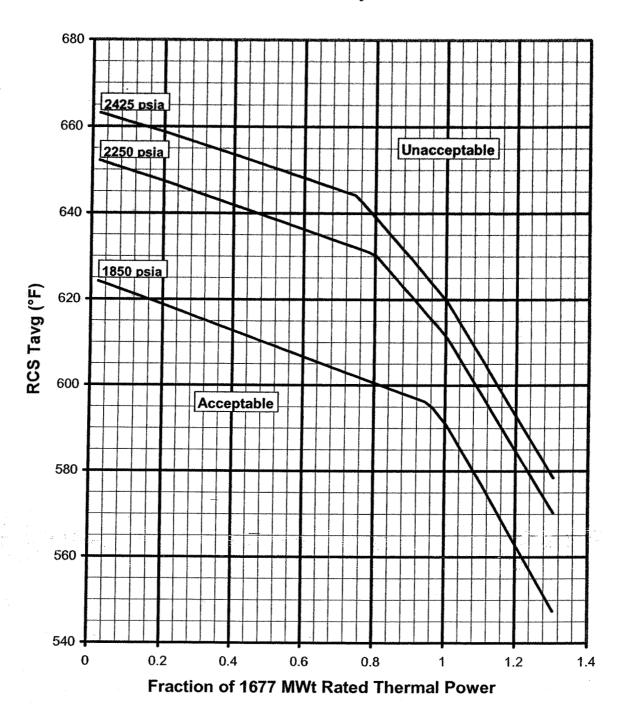
Cycle Burnup (MWD/MTU)	F <sup>W</sup> <sub>O</sub> (Z) Penalty Factor
15364	1.0200
15510	1.0215
15656	1.0232
15803	1.0212
15947	1.0200

 $F^{W}_{Q}(Z) = 1.020$  for all burnups except those listed above. Linear interpolation is adequate for intermediate cycle burnups.

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Core Operating Limits Report Unit 1, Cycle 26 Revision 3

# Figure 1



# **Reactor Core Safety Limits**

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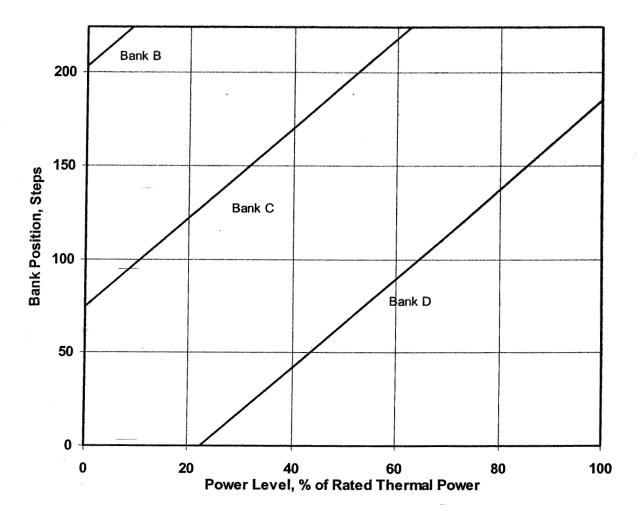


Figure 2 Rod Insertion Limit, 128 Step Tip-to-Tip

Bank Positions Given By:

- Bank D = (150 / 63) \* (P 100) + 185
- Bank C = (150 / 63) \* (P 100) + 185 + 128
- Bank B = (150 / 63) \* (P 100) + 185 + 128 + 128

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

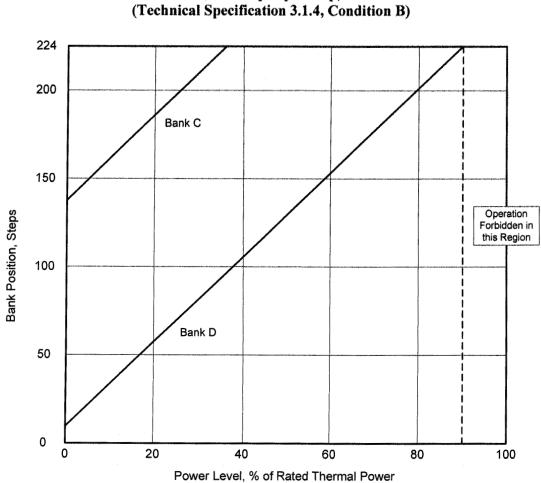


Figure 3 Rod Insertion Limit, 128 Step Tip-to-Tip, One Bottomed Rod (Technical Specification 3.1.4, Condition B)

Bank Positions Given By:

- Bank D = (150 / 63) \* (P 90) + 224
- Bank C = (150 / 63) \* (P 90) + 224 + 128

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

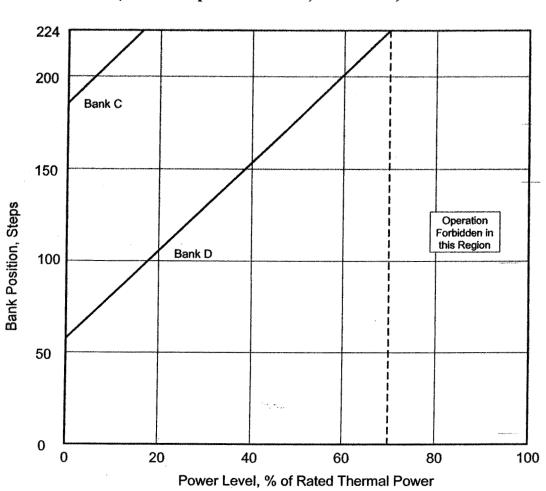


Figure 4 Rod Insertion Limit, 128 Step Tip-to-Tip, One Inoperable Rod (Technical Specification 3.1.4, Condition A)

Bank Positions Given By:

- Bank D = (150 / 63) \* (P 70) + 224
- Bank C = (150 / 63) \* (P 70) + 224 + 128

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

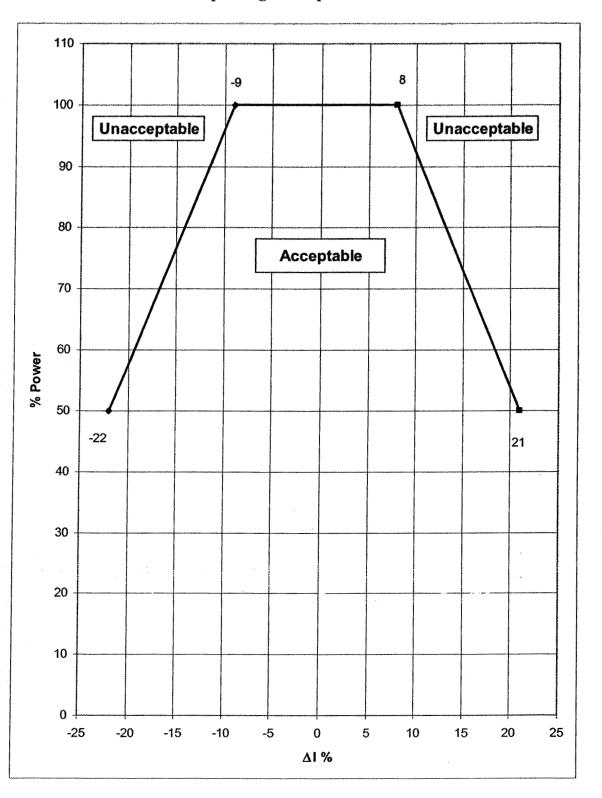


Figure 5 Flux Difference Operating Envelope associated with Table 2



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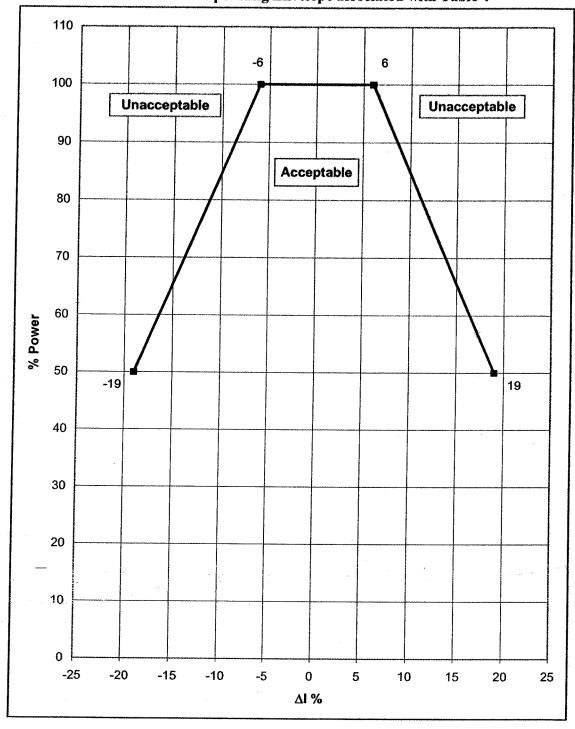


Figure 6 Flux Difference Operating Envelope associated with Table 4

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