

Dominion Resources Services, Inc.
Innsbrook Technical Center
5000 Dominion Boulevard, 2SE, Glen Allen, VA 23060



December 20, 2010

United States Nuclear Regulatory Commission
Attention: Document Control Desk
Washington, D.C. 20555

Serial No. 10-691
NL&OS/GDM: R0
Docket No. 50-281
License No. DPR-37

VIRGINIA ELECTRIC AND POWER COMPANY (DOMINION)
SURRY POWER STATION UNIT 2
CYCLE 23 CORE OPERATING LIMITS REPORT, REVISION 2

Pursuant to Surry Technical Specification (TS) 6.2.C, enclosed is a copy of Dominion's Core Operating Limits Report (COLR) for Surry Unit 2 Cycle 23 Pattern BOA, Revision 2. This revision to the COLR incorporates updates to TS references, reactor core safety limits, overtemperature ΔT and overpower ΔT setpoints, power distribution limits, and departure from nucleate boiling (DNB) parameters consistent with implementation of recently approved TS amendments 269 and 270.

If you have any questions or require additional information, please contact Mr. Gary Miller at (804) 273-2771.

Sincerely,

A handwritten signature in black ink, appearing to read "C. L. Funderburk", with a horizontal line extending to the right.

C. L. Funderburk, Director
Nuclear Licensing and Operations Support
Dominion Resources Services, Inc. for
Virginia Electric and Power Company

Enclosure

Commitment Summary: There are no new commitments as a result of this letter.

cc: U.S. Nuclear Regulatory Commission
Region II
Marquis One Tower
245 Peachtree Center Avenue, NE
Suite 1200
Atlanta, Georgia 30303-1257

Ms. K. R. Cotton
NRC Project Manager
U. S. Nuclear Regulatory Commission
One White Flint North
Mail Stop 8 G9A
11555 Rockville Pike
Rockville, MD 20852-2738

Dr. V. Sreenivas
NRC Project Manager
U. S. Nuclear Regulatory Commission
One White Flint North
Mail Stop 8 G9A
11555 Rockville Pike
Rockville, MD 20852-2738

NRC Senior Resident Inspector
Surry Power Station

Serial No. 10-691
Docket No. 50-281
Enclosure

COLR-S2C23, Revision 2

**CORE OPERATING LIMITS REPORT
Surry 2 Cycle 23 Pattern BOA**

1.0 INTRODUCTION

This Core Operating Limits Report (COLR) for Surry Unit 2 Cycle 23 has been prepared in accordance with the requirements of Technical Specification 6.2.C.

The Technical Specifications affected by this report are:

- TS 2.1 – Safety Limit, Reactor Core
- TS 2.3.A.2.d – Overtemperature ΔT
- TS 2.3.A.2.e – Overpower ΔT
- TS 3.1.E - Moderator Temperature Coefficient
- TS 3.12.A.1, TS 3.12.A.2, TS 3.12.A.3 and TS 3.12.C.3.b.1(b) - Control Bank Insertion Limits
- TS 3.12.A.1.a, TS 3.12.A.2.a, and TS 3.12.G – Shutdown Margin
- TS 3.12.B.1 and TS 3.12.B.2 - Power Distribution Limits
- TS 3.12.F – DNB Parameters
- TS Table 4.1-2A – Minimum Frequency for Equipment Tests: Item 22 – RCS Flow

2.0 REFERENCES

1. VEP-FRD-42, Rev. 2.1-A, “Reload Nuclear Design Methodology,” August 2003

Methodology for:

- TS 3.1.E - Moderator Temperature Coefficient
- TS 3.12.A.1, TS 3.12.A.2, TS 3.12.A.3 and TS 3.12.C.3.b.1(b) - Control Bank Insertion Limit
- TS 3.12.A.1.a, TS 3.12.A.2.a and TS 3.12.G – Shutdown Margin
- TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor and Nuclear Enthalpy Rise Hot Channel Factor
- TS 3.12.F – DNB Parameters
- TS Table 4.1-2A – Minimum Frequency for Equipment Tests: Item 22 – RCS Flow

2. WCAP-16009-P-A, “Realistic Large Break LOCA Evaluation Methodology Using the Automated Statistical Treatment of Uncertainty Method (ASTRUM),” (Westinghouse Proprietary), January 2005

Methodology for:

- TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

3. WCAP-10054-P-A, “Westinghouse Small Break ECCS Evaluation Model Using the NOTRUMP Code,” (Westinghouse Proprietary), August 1985

Methodology for:

- TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

4. WCAP-10079-P-A, "NOTRUMP, A Nodal Transient Small Break and General Network Code," (Westinghouse Proprietary), August 1985

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

5. WCAP-12610-P-A, "VANTAGE+ Fuel Assembly Report," (Westinghouse Proprietary), June 1990

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Heat Flux Hot Channel Factor

6. VEP-NE-2-A, Rev. 0, "Statistical DNBR Evaluation Methodology," June 1987

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Nuclear Enthalpy Rise Hot Channel Factor

7. VEP-NE-3-A, Rev. 0, "Qualification of the WRB-1 CHF Correlation in the Virginia Power COBRA Code," July 1990

Methodology for:

TS 3.12.B.1 and TS 3.12.B.2 - Nuclear Enthalpy Rise Hot Channel Factor

8. WCAP-8745-P-A, "Design Bases for Thermal Overpower Delta-T and Thermal Overtemperature Delta-T Trip Function," September 1986.

Methodology for:

TS 2.3.A.2.d - Overtemperature ΔT

TS 2.3.A.2.e - Overpower ΔT

3.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in section 1.0 are presented in the following subsections. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.2.C.

3.1 Safety Limit, Reactor Core (TS 2.1)

3.1.1 The Reactor Core Safety Limits are presented in **Figure A-1**.

3.2 Overtemperature ΔT (TS 2.3.A.2.d)

$$\Delta T \leq \Delta T_0 \left[K_1 - K_2 \left(\frac{1 + t_1 s}{1 + t_2 s} \right) (T - T') + K_3 (P - P') - f(\Delta I) \right]$$

Where:

ΔT is measured RCS ΔT , °F.

ΔT_0 is the indicated ΔT at RATED POWER, °F.

s is the Laplace transform operator, sec^{-1} .

T is the measured RCS average temperature (T_{avg}), °F.

T' is the nominal T_{avg} at RATED POWER, $\leq 573.0^\circ\text{F}$.

P is the measured pressurizer pressure, psig.

P' is the nominal RCS operating pressure ≥ 2235 psig.

$K_1 \leq 1.1425$

$K_2 \geq 0.01059 / ^\circ\text{F}$

$K_3 \geq 0.000765 / \text{psig}$

$t_1 \geq 29.7$ seconds

$t_2 \leq 4.4$ seconds

$f(\Delta I) \geq 0.0268 \{-24 - (q_t - q_b)\}$, when $(q_t - q_b) < -24.0\%$ RATED POWER

0, when -24.0% RATED POWER $\leq (q_t - q_b) \leq 8.0\%$ RATED POWER

$0.0188 \{(q_t - q_b) - 8.0\}$, when $(q_t - q_b) > +8.0\%$ RATED POWER

Where q_t and q_b are percent RATED POWER in the upper and lower halves of the core, respectively, and $q_t + q_b$ is the total THERMAL POWER in percent RATED POWER.

3.3 Overpower ΔT (TS 2.3.A.2.e)

$$\Delta T \leq \Delta T_0 \left[K_4 - K_5 \left(\frac{t_3 s}{1 + t_3 s} \right) T - K_6 (T - T') - f(\Delta I) \right]$$

Where: ΔT is measured RCS ΔT , °F.

ΔT_0 is the indicated ΔT at RATED POWER, °F.

s is the Laplace transform operator, sec^{-1} .

T is the measured RCS average temperature (T_{avg}), °F.

T' is the nominal T_{avg} at RATED POWER, $\leq 573.0^\circ\text{F}$.

$K_4 \leq 1.0965$

$K_5 \geq 0.0198$ /°F for increasing T_{avg}

$K_6 \geq 0.001074$ /°F for $T > T'$

≥ 0 /°F for decreasing T_{avg}

≥ 0 for $T \leq T'$

$t_3 \geq 9.0$ seconds

$f(\Delta I)$ = as defined above for OT ΔT

3.4 Moderator Temperature Coefficient (TS 3.1.E)

3.4.1 The Moderator Temperature Coefficient (MTC) limits are:

+6.0 pcm/°F at less than 50 percent of RATED POWER, and

+6.0 pcm/°F at 50 percent of RATED POWER and linearly decreasing to 0 pcm/°F at RATED POWER

3.5 Control Bank Insertion Limits (TS 3.12.A.1, TS 3.12.A.2 and TS 3.12.C.3.b.1(b))

3.5.1 The control rod banks shall be limited in physical insertion as shown in **Figure A-2**.

3.5.2 The rod insertion limit for the A and B control banks is the fully withdrawn position as shown on **Figure A-2**.

3.5.3 The rod insertion limit for the A and B shutdown banks is the fully withdrawn position as shown on **Figure A-2**.

3.6 Shutdown Margin (TS 3.12.A.1.a, TS 3.12.A.2.a and TS 3.12.G)

3.6.1 Whenever the reactor is subcritical the shutdown margin (SDM) shall be ≥ 1.77 % $\Delta k/k$.

3.7 Power Distribution Limits (TS 3.12.B.1 and TS 3.12.B.2)

3.7.1 Heat Flux Hot Channel Factor - FQ(z)

$$FQ(z) \leq \frac{CFQ}{P} K(z) \text{ for } P > 0.5$$

$$FQ(z) \leq \frac{CFQ}{0.5} K(z) \text{ for } P \leq 0.5$$

$$\text{where: } P = \frac{\text{THERMAL POWER}}{\text{RATED POWER}}$$

3.7.1.1 $CFQ = 2.32$

3.7.1.2 $K(z)$ is provided in Figure A-3

3.7.2 Nuclear Enthalpy Rise Hot Channel Factor - FΔH(N)

$$F\Delta H(N) \leq CFDH * \{1 + PFDH(1 - P)\}$$

$$\text{where: } P = \frac{\text{THERMAL POWER}}{\text{RATED POWER}}$$

3.7.2.1 $CFDH = 1.56$ for Surry Improved Fuel (SIF)

3.7.2.2 $PFDH = 0.3$

3.8 DNB Parameters (TS 3.12.F and TS Table 4.1-2A)

3.8.1 Departure from Nucleate Boiling (DNB) Parameters shall be maintained within their limits during POWER OPERATION:

- Reactor Coolant System $T_{\text{avg}} \leq 577.0 \text{ }^\circ\text{F}$
- Pressurizer Pressure $\geq 2205 \text{ psig}$
- Reactor Coolant System Total Flow Rate $\geq 273,000 \text{ gpm}$ and $\geq 276,000 \text{ gpm}$

Figure A-1

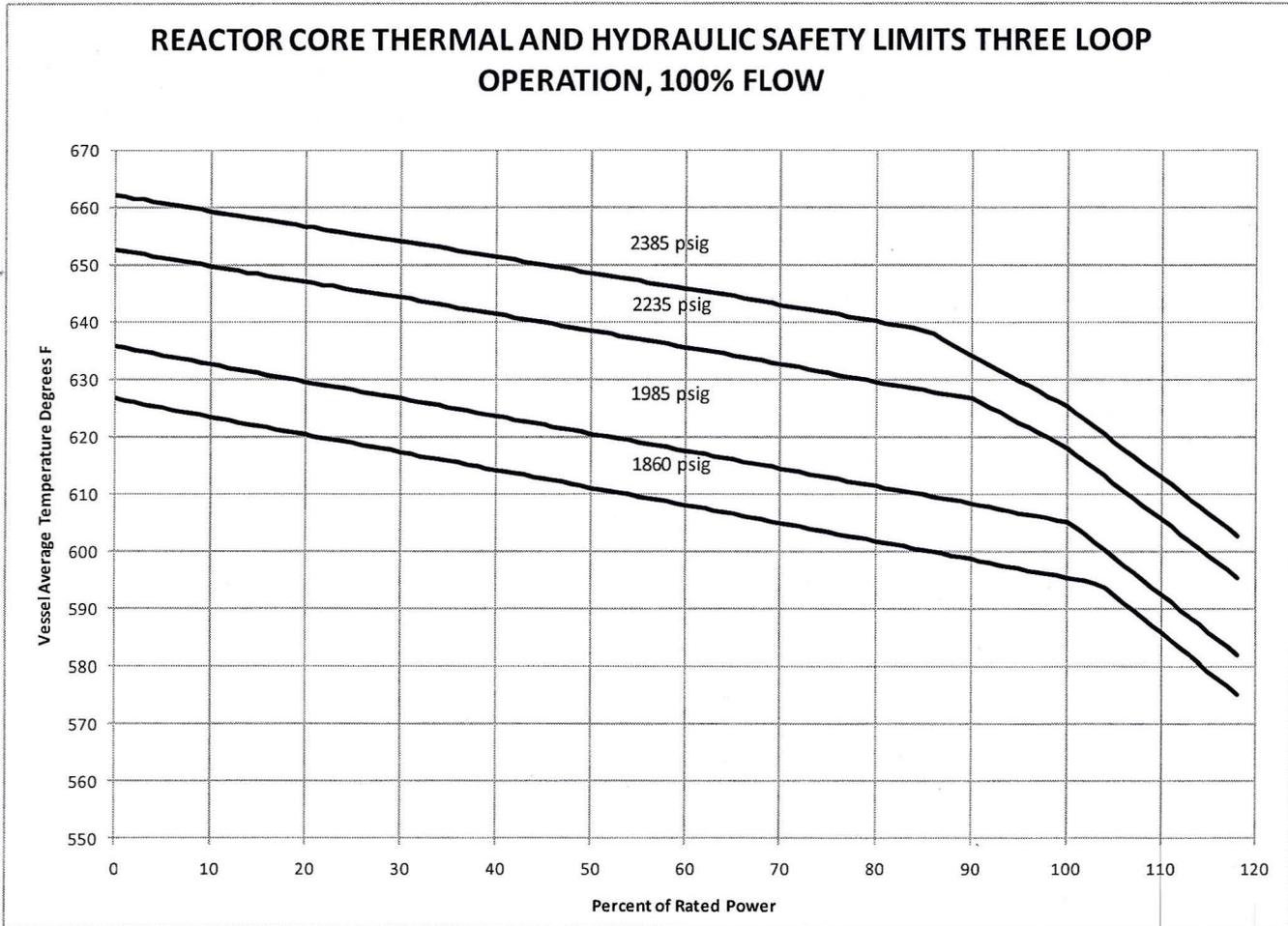


Figure A-2

SURRY UNIT 2 CYCLE 23 ROD GROUP INSERTION LIMITS

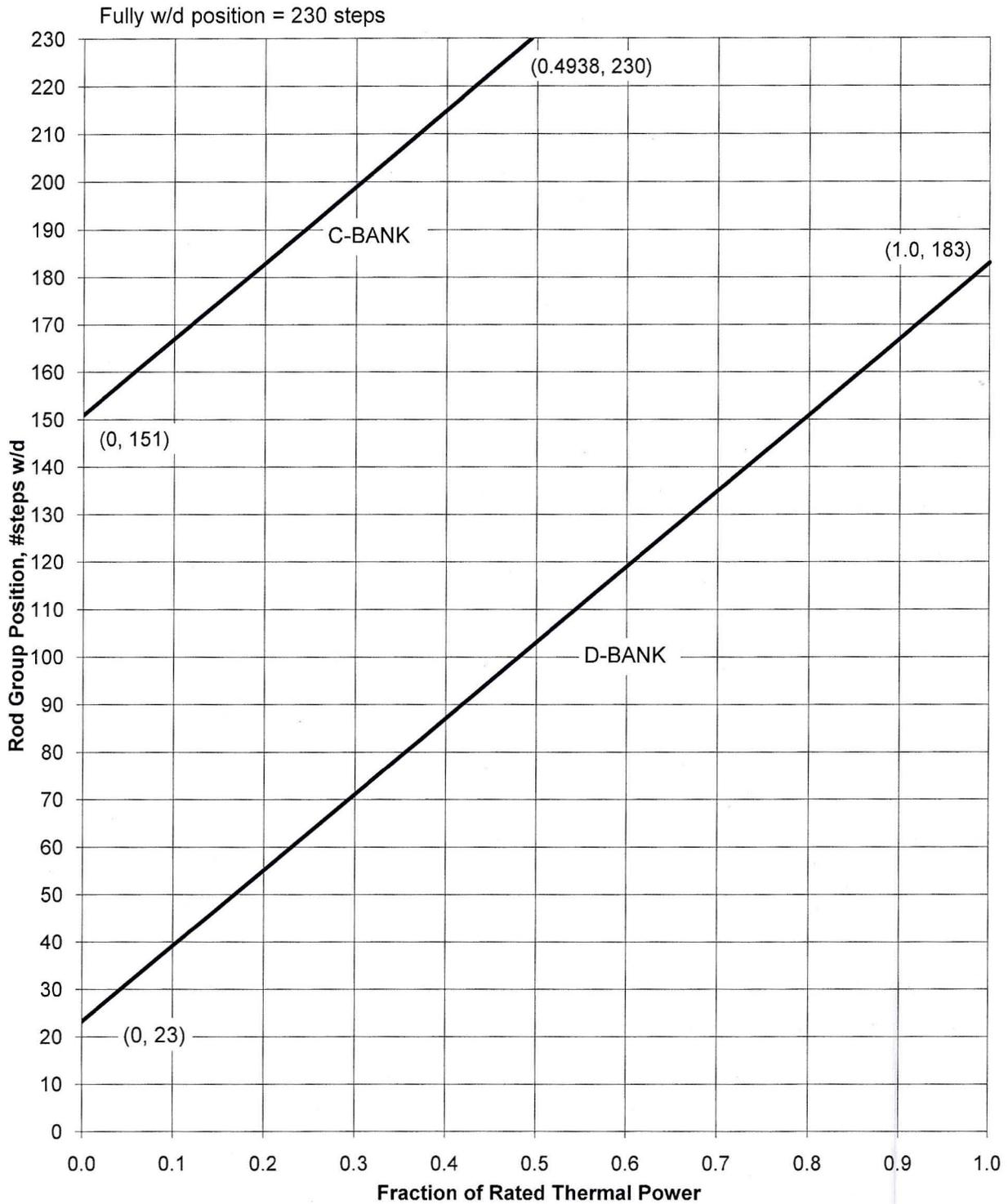


Figure A-3

