

ATTACHMENT 2

**Limerick Generating Station
Docket Nos. 50-352 and 50-353**

**License Amendment Request Regarding
TS Table 3.3.2-2, Item 4e, HPCI Equipment Room Delta Temperature High
Isolation Trip Setpoint and Allowable Value Change**

Loop Uncertainty Calculation TE-055-1N028B, dated 11/20/09

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Reviewer: AJMERA M.	Date: 11/17/09	
Approver: GEORGE RT	Date: 11/20/09	

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1.0 PURPOSE

This section includes the Objective, Limitations, Conclusions, and the Applicability Statement of this calculation.

1.1 Objective

The purpose of this calculation is to determine the Allowable Value (AV), Nominal Trip Setpoint (NTSP) and Actual Trip Setpoint (ATSP) for a high differential temperature steam source isolation by the Leak Detection System at the Limerick Generating Station (LGS). The increasing differential temperature signal is sensed by channel "B" of the High Pressure Coolant Injection (HPCI) Compartment Leak Detection Instrument, TE-055-1N028B & TE-055-1N029B.

This calculations is performed utilizing environmental conditions for a High Energy Line Break (HELB) accident scenario.

A summary of the calculation results may be found in Section 7.0 of this calculation.

Other redundant/mirror loops for which the results of this calculation are applicable may be found in Section 1.4, Applicability.

1.2 Limitations

The Max and Min Acceptable Limits calculated in Section 7.8 are not authorized for use in the PECO maintenance program by this revision of the calculation.

This calculation is produced utilizing the harsh environmental conditions for a HELB accident scenario. (See Section 2.2.5).

The appropriate use of this calculation to support design or station activities, other than those specified in Section 1.1 of this calculation, is the responsibility of the user.

1.3 Conclusions

The Upper Allowable Value of 108.5 DEGF was calculated by the software. The Upper Allowable Value is the result displayed in Section 7.7 of this calculation.

A Lower Allowable Value of 99.5 DEGF was determined using the calculation results and engineering judgement. The calculation produces an Upper Allowable Value of 108.5 DEGF. The Upper Allowable Value (108.5 DEGF) is subtracted from the Upper Analytical/Process Limit (113 DEGF) to obtain a value of 4.5 DEGF which represents a two (2) sigma one sided Loop Uncertainty which does not contain any instrument

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drift. This amount (4.5 DEGF) is then added to the Lower Analytical/Process Limit of 95 DEGF to obtain the 99.5 DEGF value (Lower Allowable Value).

An analysis of the proposed changes to the current station process setpoint values in relation to the results of this calculation has been performed and it has been concluded that the results of this calculation support the proposed changes to the current station setpoint values (Ref 4.15).

An Insulation Resistance (IR) Calculation for TE-055-1N028B Configuration 01 determined that the IR error associated with this instrument loop was insignificant (< 0.001% of loop span). It was therefore concluded that no IR effects would be included in this calculation. This IR Calculation resides in the IISCP software and is utilized as further justification for the position taken by PECO previously that IR concerns do not have any adverse effects on system operability at LGS.

The environmental conditions for the locations of the temperature elements for the redundant/mirror loops are the same/equivalent or not as harsh as those specified for the temperature element for this loop. Since the variables in this calculation are the same/equivalent or more restrictive, this calculation is valid for the redundant/mirror loops listed in Section 1.4.

1.4 Applicability

A data evaluation has been performed in order to determine which, if any, redundant/mirror instrument loops are bound by the results of this calculation (the "base" calculation). The data evaluation results validate that this "base" calculation is applicable to the following Loop Affiliation Numbers:

- * TE-055-1N028D Configuration 01
TE-055-1N029D
- * TE-055-2N028B Configuration 01
TE-055-2N029B
- * TE-055-2N028D Configuration 01
TE-055-2N029D

The results of this "base" calculation are bounding values for the instrument loops listed above based on such factors as instrument manufacturer and model number, instrument location environmental parameters, and actual installation and use of the instrument in the measurement of the process variable.

The only difference among the three redundant/mirror loops is the difference in environmental data for each loop due to the physical locations of each thermocouple, which does not introduce any additional uncertainty.

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2.0 DESIGN BASIS

This section includes the Technical Background and Design Input information relevant to this calculation.

2.1 Technical Background

High temperature in the space in which the HPCI steam lines are located outside the primary containment could indicate a breach in a HPCI steam line. The automatic closure of the HPCI isolation valve prevents the excessive loss of reactor coolant and the release of significant amounts of radioactive material from the nuclear system process barrier. When high temperatures occur in the HPCI steam line space, the inboard and outboard steam supply isolation valves are isolated.

Pairs of temperature elements monitor for high ventilation air differential temperature and compartment ambient temperature. One sensor of each pair is associated with one of the logic divisions; the other is associated with the other division.

2.2 Design Input

2.2.1 Calculation -1001 specifies 113.0 DEGF as the Upper Analytical/Process Limit (AL) and 95.0 DEGF as the Lower Analytical/Process Limit (AL) (Ref 4.11).

2.2.2 This calculation includes any applicable System Rerate Design/Operating Conditions and Impacts as a result of power rerate analyses per the guidelines contained in Specification NE-177 (Ref 4.6 & 4.8).

2.2.3 Additional margin of 4.5 DEGF was added to this calculation to support the setpoint recommended by Calculation -1001. Of this 4.5 DEGF, 4.5 DEGF is assigned margin to support the IISCP Loop Leave Alone Zone (LAZ) guidelines as discussed in Section 2.2.6 and to account for the calibration practices of the instrument channels.

The calibration practices of the instrument channels are accounted for by providing additional margin for M&TE beyond that in Section 6.2.2. This is done to provide 1% to account for the setting tolerance of the TIS. This also provides additional margin beyond that portion allocated in Section 6.2.1 to cover the 1% required accuracy for the TE. Setting Tolerance is not provided specifically for the TE since it is not calibratable.

2.2.4 Based on engineering judgement, S1 has been included as a process consideration. This consideration results in a conservatively rounded Allowable Value that supports the current Tech Spec revision request.

2.2.5 The selection of HELB environmental conditions for the performance of this calculation is based on engineering judgement and system knowledge. The environmental conditions for a HELB accident

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scenario are the most severe conditions to which the thermocouple sensors may be exposed and still be expected to perform their safety function.

- 2.2.6 The delta between the Allowable Value and the Actual Trip Set Point within this calculation is 4.5 DEGF which meets or exceeds the IISCP Program Guidance of greater than one times the LAZ (Ref 4.3)
- 2.2.7 The Setting Tolerances for the TIS in this calculation were reallocated from the region between AL and AV to the region between NTSP and ATSP in order to obtain the target Tech Spec setpoint. This reallocation was accomplished by assigning 0.0 to the Setting Tolerance of each instrument and verifying that the assigned margin amount was greater than one LAZ. Since the LAZ is equal to the square root of the sum of the squares of the Setting Tolerances, verification that the assigned margin is greater than one LAZ insures that the effects of the Setting Tolerances are included in the determination of the ATSP. No specific setting tolerance was provided for the T/C since it is not calibratable.
- 2.2.8 All other design inputs to this calculation are documented on the Supporting Data Sheet Attachments.

3.0 ASSUMPTIONS

- 3.1 Assumptions Not Requiring Confirmation
 - 3.1.1 None
- 3.2 Assumptions Requiring Confirmation
 - 3.2.1 None

4.0 REFERENCES

- 4.1 Limerick Generating Station Updated Final Safety Analysis Report (UFSAR), Revision 14 (dated 9/29/08)
 - Section 5.2.5.2.2 - Detection of Abnormal Leakage Outside the Primary Containment;
 - Section 7.6.1.3 - Leak Detection System - Instrumentation and Controls;
- 4.2 Limerick Generating Station Technical Specifications, Unit 1, Amendment 161, (dated 8/30/02)
 - Table 3.3.2-2 Item 4.e.
- 4.3 IISCP-PP-93-001, Revision 1 - Program Plan for the Implementation of Phase I of the PECO Improved Instrument Setpoint Control Program (IISCP) (Setpoint Methodology Reference).
- 4.4 M-171, Revision 0016, Limerick Generating Station Units 1&2

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Environmental Service Conditions Specification. (Location Data reference).

- 4.5 Master Calibration Sheets generated in accordance with PECO procedure IC-11-50014 for TE-055-1N028B dated 08/30/01, TE-055-1N029B dated 8/30/01, & TIS-025-101B dated 09/03/09.
- 4.6 Philadelphia Electric Letter from G.C. Storey to G.R. Hull General Electric Company, subject "Final OPL-3 for Limerick ARTS/MELLLA Analysis". This document contains Limerick 1 Reload 4(cycle 5) Resolved OPL-3 Forms that include ARTS/MELLLA at rerate conditions Dated 03/09/93. (Power Rerate Information Reference).
- 4.7 General Electric Design Specification Data Sheets (DSDS) A61-4040-L-004, Revision 0005 (Design Basis Reference).
- 4.8 NE-177, Revision 0001, Nuclear Safety Related Specification for Limerick Generating Station Units 1&2 Power Rerate Operating Conditions (Power Rerate Information Reference).
- 4.9 Calculation -1001 Revision 0004 "Compartment Temperature Transients for Steam and Water Leaks" (Analytical/Process Limit Reference)
- 4.10 Calculation -2208 Revision 0003 "RHR Compartment Pressurization due to Steam Line Break to RHR Hx" (Design Basis Reference).
- 4.11 Calculation LM-0400 Revision 0004 "HPCI and RCIC Pump Room Temperature Response Following a Small Break LOCA, Normal & Power Rerate Conditions" (Design Basis Reference).
- 4.12 Calculation LE-0036 Revision 0001 "Equivalency Evaluation between G.E. Numac LDM and Riley Temperature Instrumentation to demonstrate Accuracy and Support the use of existing Setpoints for the Steam Leak Detection System, LGS Units 1 and 2" (Vendor Information Reference)
- 4.13 Modification P-00212 Revision 0000 "HPCI/RCIC EQ Upgrade" (Design Basis Reference).
- 4.14 EQRR P-300 Revision "Pyco Temperature Elements" (Vendor Information Reference)

5.0 ATTACHMENTS

- 5.1 See Supporting Data Sheet Attachments located within this calculation.

6.0 ANALYSIS

6.1 Loop Effects

6.1.1 Loop ID No.: TE-055-1N028B

Configuration: 01

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6.1.2 Loop Function: STEAM LEAK DETECTION HPCI PIPEWAY

6.1.3 Configuration Description: HI DIFFERENTIAL TEMP TRIP

6.1.4 Loop Instrument List

<u>Device</u>	<u>ID Number</u>	<u>Function</u>	<u>Number</u>
1	TE-055-1N028B	IO	0
2	TE-055-1N029B	IO	0
3	TIS-025-101B	S	0

6.1.5 Device Dependency

<u>Device</u>	<u>Environment</u>	<u>Power</u>	<u>Calibration</u>	<u>Radiation</u>
1	A	A	A	A
2	A	A	A	A
3	B	B	B	B

6.1.6 Device Dependency References

Environmental: N/A
Power: N/A
Calibration: N/A
Radiation: N/A

6.1.7 PMA and PEA Effects

<u>Type</u>	<u>Magnitude</u>	<u>A/N</u>	<u>Sign</u>
PMA	0.00000	N	
PEA	0.00000	N	
IR	0.00000		

References

PMA:
PEA:
IR: SEE SECTION 1.3

6.1.8 Miscellaneous Random and Bias Effects

<u>Type</u>	<u>Magnitude</u>	<u>Dependent Instrument</u>	<u>Dependent Uncertainty</u>	<u>A/N</u>	<u>Sign</u>
S1	0.00992			N	R
S2	0.00000			N	
S3	0.00000			N	
R1	0.00000			N	
R2	0.00000			N	
R3	0.00000			N	

References

S1: SEE SECTION 2.2.4
S2:
S3:
R1:
R2:
R3:

6.1.9 Basis

Point of Interest: 0
Accident: HELB
Pressure Effects: Independent

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6.2 Device Effects

6.2.1 Device Accuracy (CA)

CA = va/S or Setting Tolerance (whichever is greater)

Where:

va = vendor's stated accuracy
S = instrument's calibrated span
R = instrument's range

6.2.1.1 TE-055-1N028B

va = $0.75\% \times S \times 0.66$
S = 300
R = $3.500e+002$
Setting tolerance = 0.00000
CA = 0.00495

6.2.1.2 TE-055-1N029B

va = $0.75\% \times S \times 0.66$
S = 300
R = $3.500e+002$
Setting tolerance = 0.00000
CA = 0.00495

6.2.1.3 TIS-025-101B

va = $1.0\% \times S \times 0.66$
S = 300
R = $3.500e+002$
Setting tolerance = 0.00000
CA = 0.00660

6.2.2 Device M&TE Allowance

MTE = CA + margin

Where:

CA = device calibration accuracy
margin = additional margin supplied by calculation originator

6.2.2.1 TE-055-1N028B

CA = 0.00495
Margin = 0.00000
MTE = 0.00495

6.2.2.2 TE-055-1N029B

CA = 0.00495
Margin = 0.00000
MTE = 0.00495

6.2.2.3 TIS-025-101B

CA = 0.00660
Margin = 0.00000

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MTE = 0.00660

6.2.3 Device Drift

$$D = vd * (\sqrt{tc * 1.25 / td}) / s$$

Where:

vd = vendor's stated drift specification
td = vendor's drift time specification
tc = instrument's calibration period
S = instrument's calibrated span
R = instrument's range

6.2.3.1 TE-055-1N028B

vd = 0.0
td = 1.0
tc = 731
S = 300
R = 3.500e+002
D = 0.00000

6.2.3.2 TE-055-1N029B

vd = 0.0
td = 1.0
tc = 732
S = 300
R = 3.500e+002
D = 0.00000

6.2.3.3 TIS-025-101B

vd = 0.233%*S*0.66
td = 31.
tc = 731
S = 300
R = 3.500e+002
D = 0.00835

6.2.4 Device Static Pressure

$SPE = \sqrt{SPz^2 + SPs^2}$ (for independent pressure effects)
 $SPE = SPz + SPs$ (for dependent pressure effects)
 $SPz = SPz * |Po - Pc| / S$
 $SPs = SPs * |Po - Pc| / S$

Where:

SPz = vendor's stated zero static pressure effect
SPs = vendor's stated span static pressure effect
Po = normal operating pressure
Pc = calibrated pressure
S = instrument's calibrated span
R = instrument's range

Note: Static pressure effects are relevant to sensors only.

6.2.4.1 TE-055-1N028B

SPS = 0.0

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SPZ = 0.0
 Po = 0.00
 Pc = 0.00000
 S = 300
 R = 3.500e+002
 SPs = 0.00000
 SPz = 0.00000
 SPE = 0.00000

6.2.4.2 TE-055-1N029B

SPS = 0.0
 SPZ = 0.0
 Po = 0.00
 Pc = 0.00000
 S = 300
 R = 3.500e+002
 SPs = 0.00000
 SPz = 0.00000
 SPE = 0.00000

6.2.4.3 TIS-025-101B

Sensor is not 'Y' (see attachment 9).

6.2.5 Device Over Pressure

$OPE = vope * |Pa - Pm| / S$ (for linear devices)
 $OPE = vope / S$ (for non-linear devices)

Where:

vope = vendor's stated over pressure effect
 Pa = maximum operating pressure
 Pm = instrument's design pressure
 S = instrument's calibrated span
 R = instrument's range
 X = $|Pa - Pm|$

Note: Over pressure effects are relevant to sensors only, where the maximum operating pressure is greater than instrument's design pressure.

6.2.5.1 TE-055-1N028B

vope = 0.0
 Pa = 0.00
 Pm = 0.00
 S = 300
 R = 3.500e+002
 OPE = 0.00000

6.2.5.2 TE-055-1N029B

vope = 0.0
 Pa = 0.00
 Pm = 0.00
 S = 300
 R = 3.500e+002
 OPE = 0.00000

6.2.5.3 TIS-025-101B

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Sensor is not 'Y' (see attachment 9).

6.2.6 Device Drift Temperature

$DTE = vte * dT / S$ (for linear devices)
 $DTE = vte / S$ (for non-linear devices)

Where:

vte = vendor specified temperature effect
 dT = (Normal Temp - 68° F)
 S = instrument's calibrated span
 R = instrument's range

6.2.6.1 TE-055-1N028B

vte = 0.0
 S = 300
 R = 3.500e+002
 Normal temp = 115.00
 DTE = 0.00000

6.2.6.2 TE-055-1N029B

vte = 0.0
 S = 300
 R = 3.500e+002
 Normal temp = 117.00
 DTE = 0.00000

6.2.6.3 TIS-025-101B

vte = 0.0
 S = 300
 R = 3.500e+002
 Normal temp = 82.00
 DTE = 0.00000

6.2.7 Device Accuracy Temperature

$ATE = vte * dT / S$ (for linear devices)
 $ATE = vte / S$ (for non-linear devices)

Where:

vte = vendor specified temperature effect
 dT = |accident temperature - normal temperature|
 S = instrument's calibrated span
 R = instrument's range

6.2.7.1 TE-055-1N028B

vte = 0.0
 S = 300
 R = 3.500e+002
 Normal temp = 115.00
 Accident temp = 306.83
 ATE = 0.00000

6.2.7.2 TE-055-1N029B

vte = 0.0
 S = 300

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$R = 3.500e+002$
 Normal temp = 117.00
 Accident temp = 307.89
 $ATE = 0.00000$

6.2.7.3 TIS-025-101B

$vte = 0.0$
 $S = 300$
 $R = 3.500e+002$
 Normal temp = 82.00
 Accident temp = 82.00
 $ATE = 0.00000$

6.2.8 Device Humidity

$HE = dH * vhe / S$ (for linear devices)
 $HE = vhe / S$ (for non-linear devices)

Where:

vhe = vendor's stated humidity specification
 S = instrument's calibrated span
 R = instrument's range
 dH = |accident humidity - normal humidity|

6.2.8.1 TE-055-1N028B

$vhe = 0.0$
 $S = 300$
 $R = 3.500e+002$
 Accident hum = 100.00
 Normal hum = 90.00
 $HE = 0.00000$

6.2.8.2 TE-055-1N029B

$vhe = 0.0$
 $S = 300$
 $R = 3.500e+002$
 Accident hum = 100.00
 Normal hum = 90.00
 $HE = 0.00000$

6.2.8.3 TIS-025-101B

$vhe = 0.0$
 $S = 300$
 $R = 3.500e+002$
 Accident hum = 90.00
 Normal hum = 90.00
 $HE = 0.00000$

6.2.9 Device Accuracy Radiation

$ARE = vre * DeltaRad / S$ (for linear devices)
 $ARE = vre / S$ (for non-linear devices)

Where:

vre = vendor specified radiation effect
 $DeltaRad$ = (accident radiation - normal radiation)
 S = instrument's calibrated span

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R = instrument's range

6.2.9.1 TE-055-1N028B

vre = 0.0
S = 300
R = 3.500e+002
Accident rad = 4.93000
Normal rad = 0.90500
ARE = 0.00000

6.2.9.2 TE-055-1N029B

vre = 0.0
S = 300
R = 3.500e+002
Accident rad = 1.76000
Normal rad = 0.90500
ARE = 0.00000

6.2.9.3 TIS-025-101B

Environmental qualifier is not 'Y' (see attachment 5).

6.2.10 Device Seismic

VSE = SRS * vse / S (for linear devices)
VSE = vse / S (for non-linear devices)

Where:

vse = vendor's stated seismic specification
S = instrument's calibrated span
R = instrument's range
SRS = seismic response envelope

6.2.10.1 TE-055-1N028B

Seismic class is not '1' in Pims (see attachment 5).

6.2.10.2 TE-055-1N029B

Seismic class is not '1' in Pims (see attachment 5).

6.2.10.3 TIS-025-101B

Seismic class is not '1' in Pims (see attachment 5).

6.2.11 Device Power

PSE = pss * pse / S

Where:

pse = vendor's stated power supply specification
pss = device power supply stability
S = instrument's calibrated span
R = instrument's range

6.2.11.1 TE-055-1N028B

pse = 0.0
S = 300

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R = 3.500e+002
pss = 0.000
PSE = 0.00000

6.2.11.2 TE-055-1N029B

pse = 0.0
S = 300
R = 3.500e+002
pss = 0.000
PSE = 0.00000

6.2.11.3 TIS-025-101B

pse = 0.0
S = 300
R = 3.500e+002
pss = 12.000
PSE = 0.00000

7.0 RESULTS

7.1 Loop Accuracy Allowance (AL)

AL_norm = A + OP + SP + PE
AL_accid = AL_norm + S (for S > TE + RE + AHE)
AL_accid = AL_norm + TE + RE + AHE (for S ≥ TE + RE + AHE)

Where:

A = $\sum CA^2$
TE = $\sum ATE^2$
OP = $\sum OPE^2$
SP = $\sum SPE^2$
RE = $\sum ARE^2$
AHE = $\sum HE^2$
S = $\sum VSE^2$
PE = $\sum PSE^2$
AL = 0.00009

7.2 Loop Drift Allowance (DL)

DL = DE + DT

Where:

DE = $\sum D^2$
DT = $\sum DTE^2$
DL = 0.00007

7.3 Loop Calibration Allowance (CL)

CL = V + M

Where:

V = $\sum (\text{setting tolerance})^2$
M = $\sum MTE^2$
CL = 0.00014

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7.4 TLU

$$\begin{aligned}
 (\text{Positive})\text{TLUp} &= [\text{IR} + \text{PMAp} + \text{PEAp} + \text{PCp} + \text{PMAo} + \text{PEAo} + \text{Pco} + \\
 &\quad \sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span} \\
 (\text{Negative})\text{TLUn} &= [-\text{PMAn} - \text{PEAn} - \text{PCn} - \text{PMAo} - \text{PEAo} - \text{PCo} + - \\
 &\quad \sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span}
 \end{aligned}$$

All other variables as previous defined.

$$\begin{aligned}
 \text{TLUp} &= 6.01696 \text{ DEGF} \\
 \text{TLUn} &= -6.01696 \text{ DEGF}
 \end{aligned}$$

7.5 NTSP

$$\begin{aligned}
 (\text{Increasing}) \text{NTSP} &= \text{limit} + [-\text{PMAn} - \text{PEAn} - \text{PCn} - \text{PMAo} - \text{PEAo} - \text{PCo} + \\
 &\quad (1.645 / \sigma) * -\sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span} \\
 (\text{Decreasing}) \text{NTSP} &= \text{limit} + [\text{IR} + \text{PMAp} + \text{PEAp} + \text{PCp} + \text{PMAo} + \text{PEAo} + \text{PCo} \\
 &\quad + (1.645 / \sigma) * \sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span}
 \end{aligned}$$

Where:

limit = loop analytical or process limit
limit = 113.00 DEGF

$$\begin{aligned}
 \sigma &= 2 \\
 \text{NTSP} &= 108.05105 \text{ DEGF}
 \end{aligned}$$

7.6 ATSP

$$\begin{aligned}
 (\text{Increasing}) \text{ATSP} &= \text{NTSP} + \text{margin} \\
 (\text{Decreasing}) \text{ATSP} &= \text{NTSP} - \text{margin}
 \end{aligned}$$

Where:

margin = additional margin supplied by calculation originator
margin = -4.05000
ATSP = 104.00105 DEGF

7.7 Allowable Value

$$\begin{aligned}
 (\text{Decreasing}) \text{AV} &= \text{limit} + [\text{IR} + \text{PMAp} + \text{PEAp} + \text{PCp} + \text{PMAo} + \text{PEAo} + \text{Pco} + \\
 &\quad (1.645 / \sigma) * \sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span} \\
 (\text{Increasing}) \text{AV} &= \text{limit} + [-\text{PMAn} - \text{PEAn} - \text{PCn} - \text{PMAo} - \text{PEAo} - \text{PCo} + \\
 &\quad (1.645 / \sigma) * -\sqrt{(\text{AL} + \text{CL} + \text{DL} + \text{PMAr} + \text{PEAR} + \text{PCr})}] * \text{Loop span}
 \end{aligned}$$

All other variables as previously defined.

$$\text{AV} = 108.50034 \text{ DEGF}$$

LOOP UNCERTAINTY CALCULATION			
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Reviewer: AJMERA M.	Date: 11/17/09		
Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 1: Session Data

Station: LG Unit: 1

Responsible Branch: LEDE

Safety Related (Y/N): Y

Description: HPCI EQUIPMENT ROOM DELTA TEMPERATURE - HIGH

System Number: 055

Structure: RX ENCL

Component: TE-55-1N28/29B TIS-2

Revision Description: LOWER AV & ATSP TO 108.5 & 104.0 PER ECR 09-00438

Vendor Calc Number: N/A

Revision: NA

Other Calculations: N

Provides info TO: N/A

Receives info FROM: LE-0036 -1001
LM-0400 -2208

Supercedes: N/A

- | | |
|---|-------------|
| 1. Accident type: | HELB |
| 2. Pressure effects dependent or independent (I/D): | Independent |
| 3. Process increasing, decreasing or neither (I/D/N): | Increasing |
| 4. Input point of interest: | 0 |
| 5. Include additional margin for actual setpoint calculation: | Yes |
| 6. Additional margin to be used: | -4.05000 |

LOOP UNCERTAINTY CALCULATION			
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Approver: GEORGE RT	Date: 11/20/09		

Attachment 2: Calculation Results

Device	F	N	Accuracy	Temperature		Humidity	Tol	Pwr Supp
				Normal	Accident			
TE-055-1N028B	IO	0	0.00495	0.00000	0.00000	0.00000	0.00000	0.00000
TE-055-1N029B	IO	0	0.00495	0.00000	0.00000	0.00000	0.00000	0.00000
TIS-025-101B	S	0	0.00660	0.00000	0.00000	0.00000	0.00000	0.00000

Device	F	N	SPE	Rad Acc	M&TE	Drift	Ovr Pres	Seismic
TE-055-1N028B	IO	0	0.00000	0.00000	0.00495	0.00000	0.00000	N/A
TE-055-1N029B	IO	0	0.00000	0.00000	0.00495	0.00000	0.00000	N/A
TIS-025-101B	S	0	N/A	N/A	0.00660	0.00835	N/A	N/A

Process Concerns						
	Positive	Normal	Offsetting	Positive	Accident	Offsetting
		Negative			Negative	
PMA	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
PEA	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
IR				0.00000		
Other	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Loop Results					
		Normal		Accident	
		Negative		Negative	
TLU*	6.01696	-6.01696		6.01696	-6.01696
AL		0.00009		0.00009	
	Increasing	Decreasing		Increasing	Decreasing
NTSP*	108.05105	N/A		108.05105	N/A
AV*	108.50034	N/A		108.50034	N/A
ATSP*	104.00105	N/A		104.00105	N/A

Additional Margin: -4.05000 DL: 0.00007 CL: 0.00014

* These values are in DEGF

LOOP UNCERTAINTY CALCULATION			
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Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 3: Loop Data

Loop Number: TE-055-1N028B

Instruments	Function	Num	1	2	3	4	5	6	7	8	9	10
TE-055-1N028B	IO	0	X	X								
TE-055-1N029B	IO	0	X	X								
TIS-025-101B	S	0	X									
TIS-025-101B	2	0		X								
		0										
		0										
		0										
		0										
		0										
		0										
Configuration Descriptions												
1: HI DIFFERENTIAL TEMP TRIP				6:								
2: DIFFERENTIAL TEMP IND				7:								
3:				8:								
4:				9:								
5:				10:								

Loop Description: STEAM LEAK DETECTION HPCI PIPEWAY

Originator: COLLIER KB

Date: 11/12/09

Revision: 00

ATTACHMENT 4: Loop Calibration Data

Loop Number: TE-055-1N028B

Configuration: 01

	Units	Min	Max	Normal	Trip
Process Temperature		0.00	0.00	0.00	0.00
Process Radiation		0.000e+000	0.000e+000	0.000e+000	0.000e+000
Process Humidity		0.00	0.00	0.00	0.00
Process Pressure		0.00	0.00	0.00	0.00
Loop Span	DEGF	-150.00	150.00	Sigma: 2	
	Value	Units			Value
Setpoint	104.00	DEGF	Loop Setting Limit		0.000
Reset	3.00	DEGF	Loop Leave Alone Zone		3.000
Allowable	108.5	DEGF	Loop Calculation Acc		0.000
Design/safety Limit	0.00		Calibration Frequency		731
Analytical/Proc Limit	113.00	DEGF			

Originator: COLLIER KB

Date: 11/13/09

Revision: 00

LOOP UNCERTAINTY CALCULATION			
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Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 5: Instrument Data

Component Id: TE-055-1N028B		Facility: LG	Unit: 1	System: 055
Description: HPCI COMPARTMENT LEAK DETECTION LEAK DET -- SHOWN ONP&ID 25				Function: IO 0
Type: I E	Manufacturer Code: P427		Model #: 102-9039	
Location: 015177109	Elevation: 177	Area: 015	Serial #: 01116	
QA Class: Q	Op Time: 1	Service Life: 40	EQ: Y	Seismic Class:
Tech Spec: Y	Tech Spec Ref: T3.3.2-2.4.E	Transient: NA	Reg Guide 1.97: N	
Power Supply Reg: 0.000		Tolerance: 0.000		
Loop Number: TE-055-1N028B		Loop Diagram: N/A		
Computer Address: N/A		P&ID: M-0025		
Installation Detail: N/A				
Calibration ST: ST-2-025-405-1		Calibration Proc: ST-2-025-405-1		
Functional ST: ST-2-055-611-1		Procedure #: IC-11-00001		
Response ST: N/A		Other:		
Mod Number:		Other:		
Signal From: PROCESS		Signal To: TIS-025-101B CH A4-1	Mod Rev:	
Alarms & Actions: N/A				
Instruction Book:				
Input Min: 50.00	Input Max: 350.00		Input Unit: DEGF	
Output Min: 0.391	Output Max: 8.064		Output Unit: MVDC	
HC: 0.000	Setting Tolerance: 0.00000	Leave Alone Zone: 0.01000		
HC Corrected:	SP Corrected:	Add. Margin: 0.00000		
MTE device				Period: 731
MTE Accuracy				
HC Reference: N/A		SP Reference: N/A		

Originator: COLLIER KB

Date: 11/12/09

Revision: 1

LOOP UNCERTAINTY CALCULATION			
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Reviewer: AJMERA M.	Date: 11/17/09		
Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 5: Instrument Data

Component Id: TE-055-1N029B		Facility: LG	Unit: 1	System: 055
Description: HPCI COMPARTMENT LEAK DETECTION LEAK DET -- SHOWN ONP&ID 25				Function: IO 0
Type: I E	Manufacturer Code: P427		Model #: 102-9039	
Location: 015201288	Elevation: 201	Area: 015	Serial #: 00573	
QA Class: Q	Op Time: 1	Service Life: 40	EQ: Y	Seismic Class:
Tech Spec: Y	Tech Spec Ref: T3.3.2-2.4.E	Transient: NA	Reg Guide 1.97: N	
Power Supply Reg: 0.000		Tolerance: 0.000		
Loop Number: TE-055-1N028B		Loop Diagram: N/A		
Computer Address: N/A		P&ID: M-0025		
Installation Detail: N/A				
Calibration ST: ST-2-025-405-1		Calibration Proc: ST-2-025-405-1		
Functional ST: ST-2-055-611-1		Procedure #: IC-11-00001		
Response ST: N/A		Other:		
Mod Number:		Other:		
Signal From: PROCESS		Signal To: TIS-025-101B CH A4-1	Mod Rev:	
Alarms & Actions: N/A				
Instruction Book:				
Input Min: 50.00	Input Max: 350.00		Input Unit: DEGF	
Output Min: 0.391	Output Max: 8.064		Output Unit: MVDC	
HC: 0.000	Setting Tolerance: 0.00000	Leave Alone Zone: 0.01000		
HC Corrected:	SP Corrected:	Add. Margin: 0.00000		
MTE device				Period: 732
MTE Accuracy				
HC Reference: N/A		SP Reference: N/A		

Originator: COLLIER KB

Date: 11/12/09

Revision: 1

LOOP UNCERTAINTY CALCULATION			
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Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 5: Instrument Data

Component Id: TIS-025-101B	Facility: LG	Unit: 1	System: 025
Description: STEAM LEAK DETECTION TEMP MONITOR DIV. 2/B1	Function: S 0		
Type: I S	Manufacturer Code: G080	Model #: 304A3714G004	
Location: 008289542	Elevation: 289	Area: 008	Serial #:
QA Class: Q	Op Time: N/A	Service Life: 000	EQ: N
Tech Spec: Y	Tech Spec Ref: T3.3.2-2.4	Transient: NA	Reg Guide 1.97: N
Power Supply Reg: 120.000	Tolerance: 12.000		
Loop Number: SEE REMARKS	Loop Diagram: N/A		
Computer Address: N/A	P&ID: M-0025		
Installation Detail: N/A			
Calibration ST: ST-2-025-405-1	Calibration Proc: ST-2-025-405-1		
Functional ST: SEE REMARKS	Procedure #: IC-11-00001		
Response ST: N/A	Other:		
Mod Number:	Other:		
Signal From: SEE REMARKS	Signal To: SEE REMARKS	Mod Rev:	
Alarms & Actions: SEE REMARKS			
Instruction Book: N-00E-68-00024 (GEK-97146)			
Input Min: 50.00	Input Max: 350.00	Input Unit: DEGF	
Output Min: 0	Output Max: 1	Output Unit:	
HC: 0.000	Setting Tolerance: 0.00000	Leave Alone Zone: 0.01000	
HC Corrected:	SP Corrected:	Add. Margin: 0.00000	
MTE device			Period: 731
MTE Accuracy			
HC Reference: N/A	SP Reference: N/A		

Originator: COLLIER KB

Date: 11/12/09

Revision: 4

LOOP UNCERTAINTY CALCULATION			
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Reviewer: AJMERA M.	Date: 11/17/09		
Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 6: Vendor Data

Manufacturer Code: P427 Model #: 102-9039

Function: IO 0

Reference: REFLECTS 2 SIGMA VALUE (CALC# LE-0065)							
Min	5.000e+001	Max	3.500e+002	Units	DEGF	Pressure	0.00
Accuracy Information							
Accuracy	0.75%*S*0.66						
Seismic	0.0						
Temperature	0.0						
Radiation	0.0						
Over Pressure	0.0						
Humidity	0.0						
Drift	0.0						
Time	1.0						
Power Supply	0.0						
Pressure Zero	0.0	Pressure Span				0.0	

Originator: KINCAID SC

Date: 07/06/01

Revision: 00

ATTACHMENT 6: Vendor Data

Manufacturer Code: P427 Model #: 102-9039

Function: IO 0

Reference: REFLECTS 2 SIGMA VALUE (CALC# LE-0065)							
Min	5.000e+001	Max	3.500e+002	Units	DEGF	Pressure	0.00
Accuracy Information							
Accuracy	0.75%*S*0.66						
Seismic	0.0						
Temperature	0.0						
Radiation	0.0						
Over Pressure	0.0						
Humidity	0.0						
Drift	0.0						
Time	1.0						
Power Supply	0.0						
Pressure Zero	0.0	Pressure Span				0.0	

Originator: KINCAID SC

Date: 07/06/01

Revision: 00

LOOP UNCERTAINTY CALCULATION			
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Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 6: Vendor Data

Manufacturer Code: G080 Model #: 304A3714G004

Function: S 0

Reference: GEK-97146, NE-68-24; REFLECTS 2 SIGMA VALUES (CALC# LE-0036)							
Min	5.000e+001	Max	3.500e+002	Units	DEGF	Pressure	0.00
Accuracy Information							
Accuracy	1.0%*S*0.66						
Seismic	0.0						
Temperature	0.0						
Radiation	0.0						
Over Pressure	0.0						
Humidity	0.0						
Drift	0.233%*S*0.66						
Time	31.						
Power Supply	0.0						
Pressure Zero	0.0	Pressure Span		0.0			

Originator: THOMAS RT

Date: 04/18/94

Revision: 00

LOOP UNCERTAINTY CALCULATION			
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Reviewer: AJMERA M.	Date: 11/17/09		
Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 7: Location Data

Location Code: 015177109

Description: UNIT 1 HPCI PUMP COMPT - REVISED BASED ON 94-08691

	Minimum	Normal	Trip LOCA	Trip HELB	Trip MSLB	Maximum
Temp	65.00	115.00	176.00	306.83	306.83	115.00
Radiation	2.580e+00	9.050e+05	4.930e+06	4.930e+06	4.930e+06	9.050e+05
Humidity	50.00	90.00	90.00	100.00	100.00	90.00
Pressure	14.69	14.69	14.70	17.64	17.64	14.69

Seismic Response Envelope: 0.00

Originator: GEORGE R T

Date: 10/29/96

Revision: 02

ATTACHMENT 7: Location Data

Location Code: 015201288

Description: UNIT 1 HPCI PIPING AREA

	Minimum	Normal	Trip LOCA	Trip HELB	Trip MSLB	Maximum
Temp	65.00	117.00	120.00	307.89	307.89	117.00
Radiation	2.580e+00	9.050e+05	1.760e+06	1.760e+06	1.760e+06	9.050e+05
Humidity	50.00	90.00	90.00	100.00	100.00	90.00
Pressure	14.69	14.69	14.70	21.34	21.34	14.69

Seismic Response Envelope: 0.00

Originator: THOMAS RT

Date: 05/02/94

Revision: 00

ATTACHMENT 7: Location Data

Location Code: 008289542

Description: ROOM 542, AUXILIARY EQUIPMENT ROOM

	Minimum	Normal	Trip LOCA	Trip HELB	Trip MSLB	Maximum
Temp	60.00	82.00	82.00	82.00	82.00	82.00
Radiation	5.000e-04	1.760e+02	1.890e+02	1.760e+02	1.760e+02	1.760e+02
Humidity	30.00	90.00	90.00	90.00	90.00	90.00
Pressure	14.70	14.70	14.70	14.70	14.70	14.70

Seismic Response Envelope: 0.00

Originator: CAROLAN JF

Date: 03/31/93

Revision: 00

LOOP UNCERTAINTY CALCULATION			
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Reviewer: AJMERA M.	Date: 11/17/09		
Approver: GEORGE RT	Date: 11/20/09		

ATTACHMENT 8: Process Concerns

<u>Consideration</u>	<u>Contribution to</u> <u>Uncertainty</u>	<u>Sign</u>	<u>A/N</u>			<u>Consideration</u> <u>References</u>
1 PMA	0.00000		N	Dependent	Dependent	
2 PEA	0.00000		N	<u>Device</u>	<u>Uncertainty</u>	
3 IR	0.00000					SEE SECTION 1.3
4 S1	0.00992	R	N			SEE SECTION 2.2.4
5 S2	0.00000		N			
6 S3	0.00000		N			
7 R1	0.00000		N			
8 R2	0.00000		N			
9 R3	0.00000		N			

ATTACHMENT 9: Device Dependencies

<u>Devices</u>	<u>Function</u>		<u>Dependency</u>				<u>Static</u>	<u>Calibration</u>	
			<u>Env</u>	<u>Pwr</u>	<u>Cal</u>	<u>Rad</u>	<u>Pressure</u>	<u>Humid</u>	<u>Sensor</u>
TE-055-1N028B	IO	0	A	A	A	A	0.00000	90.00	Y
TE-055-1N029B	IO	0	A	A	A	A	0.00000	90.00	Y
TIS-025-101B	S	0	B	B	B	B	0.00000	90.00	N

Dependency References

Env: N/A

Cal: N/A

Pwr: N/A

Rad: N/A

Cal Condition: N/A

Just: Maximum Normal Humidity for Location Code