Appendix A

ANSYS INPUT FILES

File name	Description
12AF_4sch80.inp	ANSYS model input file for location 12AF
14AF_4sch80.inp	ANSYS model input file for location 14AF
14AK_4sch80.inp	ANSYS model input file for location 14AK
AF13T_4sch80.inp	ANSYS model input file for location AF13T
tuesday_4sch80_bndng_EP.inp	ANSYS model input file for location between AF4T and AF5T

Information in this record was deleted in accordance with the Freedom of Information Act, Exemptions 7
FOIA/PA 2010-0334

J-3

1. **ISSUE IDENTIFICATION:**

1.1 Notification (Order)#: **20460078 (70109482 Op 0010)**

1.2 OpEval #: **10-005** Revision: **0**

General Information:

1.3 Affected Station(s): **Salem**

1.4 Unit(s): **2**

1.5 System: **Auxiliary Feedwater (AF)**

1.6 Component(s) Affected: **4" NPS Pipe 2AF1019 and 2AF1013**

1.7 Detailed description of what SSC is degraded or the nonconforming condition, by what means and when first discovered, and extent of condition for all similarly affected SSCs:

During S1R20 Unit 1 refueling outage, corrosion was found on the 4" Auxiliary Feedwater (AFW) buried piping that supplies the 12 and 14 steam generators. The corrosion exceeded the minimum wall criteria and the corrosion was seen on all excavated piping. This inspection was performed as part of planned buried pipe inspections during S1R20. This operability evaluation assesses the applicability of the findings to the Salem Unit 2 AFW piping

Unit 1 Buried AFW Piping:

Auxiliary Feedwater pipes connect to the #12 and #14 main feedwater lines in the outer penetration area. This location requires the #12 and #14 AFW pipes to travel approximately 30' underground along the edge of the containment building before entering the outer penetration area at elevation 94' 8" and 96' 2" for #12 and #14, respectively.

The Guided Wave inspections of the Salem Unit 1 #12 and #14 Auxiliary Feedwater (AFW) buried piping during Salem's S1R20 refueling outage revealed degraded pipe wall conditions due to external corrosion in excess of the design minimum wall thickness due to heavy external uniform corrosion. The apparent cause of the corrosion was the improper application (or lack) of the specified pipe coatings, X-Tru-Coat, an adhered polyethylene protection system, and Bitumastic, which was specified per drawings and pipe specifications to be applied at the welded joints. Visual inspections of this piping after excavation showed a lack of coating. The only remnant of coating found was a portion of coal tar which was approximately 9 inches in length and 7 inches in circumference. This piece of coating was in the shape of the 4 inch AFW piping and conformed to that same surface.

The piping is 4-inch NPS, Schedule 80, A106 Gr B seamless carbon steel. It is classified as Nuclear 3, Seismic Category I. Per the Pipe Specification S-C-MPOO-MGS-0001, SPS 54E, the design Pressure-Temperature limit is 1950 psi at 140 F. The nominal wall thickness is 0.337 inches ± 12.5%.

Using the Guided Wave inspection results to target specific pipe areas of the 12 and 14 AFW piping during S1R20, NDE Services initially performed confirmatory UT measurements on 378 grid areas. Approximately 76 percent of these UT measurements were non-conforming, having a minimum wall thickness less than the design minimum wall thickness of 0.278 inches. For the worst case UT measurements, the minimum wall thickness for the #12 AFW buried piping showed a 55 percent loss (0.152 inches). For the #14 AFW buried piping, the greatest loss was approximately 78 percent (0.077 inches). As of 4/19/2010 the following number of UT readings were taken:

<u>#14 AFW Line (Upper Pipe):</u> 8,904 readings total. 1,194 are below 0.278"

<u>#12 AFW Line (Lower Pipe):</u> 8,852 readings total. 192 readings are below 0.278".

Removal of sections of the Salem Unit 1 #12 and 14 AFW piping during S1R20 and subsequent visual examinations has validated that the corrosion identified above is external. These inspections also revealed that there is evidence of the X-Tru-Coat, an adhered polyethylene protection system <u>only on the thru wall portions</u> of the #12 and # 14 AFW piping where it passes into the fuel transfer tube area. It is obvious this coating system was not on the buried portions of these lines and validates that the corrosion is due to lack of coating. The ground fill of the AFW piping is not a harsh environment (harsh with regard to coating), and there does not appear to be a correlation between the missing/deterioration of coating and the buried pipe environment.

<u>Summary of Structural Integrity Associates (SIA) Finite Element Analysis Report</u>

The underground auxiliary feedwater piping at Salem, Unit 1 was designed to the t_{min} requirement given in the B31.1 Power Piping Code. B31.1 does not provide specific criteria for the evaluation of non-uniform wall thickness or local thinning. However, guidance for stress analysis may be taken from the ASME Code, Section III as described below.

The technical approach taken herein is based on the premise that while piping may have localized thinned regions that violate the design t_{min} requirements, the non-uniform wall thickness of the pipe cross-section may be shown to meet design stress allowables. This approach is possible for the pipe section exhibiting thinning when a remaining wall greater than t_{min} surrounds the thinned region. This approach is similar to the basis for qualifying pipe penetrations using branch reinforcement rules in the ASME Code.

Design requirements for Class 3 piping are provided in ND-3600 (similar to B31.1 rules) of the ASME Code, Section III [2]. More rigorous analyses are allowed under ND-3611.3:

> *"The specific design requirements of ND-3600 are based on a simplified engineering approach. A more rigorous analysis such as described in NB-3600 or NB-3200 may be used to calculate the stresses required to satisfy these requirements. These calculated stresses must be compared to the allowable stresses in this Subsection. In such cases, the designer shall include the appropriate justification for the approach taken in the Certified Design Report."*

Thus, NB-3200 design by analysis is employed. Based on the linear-elastic finite element analysis results which showed that the section of pipe between AF4T and AF5T was

bounding, it was required to perform additional analysis only for that section of pipe in order to show operability. The more rigorous analysis employed is described in Section NB3228.1, Limit Analysis. Specifically Section NB-3228.1 states that limits on Local Membrane Stress Intensity need not be satisfied at a specific location if it can be shown by limit analysis that the specified loadings do not exceed two-thirds of the lower bound collapse load. Also, NB-3228.1 states that the yield strength to be used in this calculation is 1.5Sm. In this evaluation, the value of yield strength is equal to 1.5S, where S is taken as the value of S_h, 15.0 ksi, from the original 1967 B31.1 Power Piping Code. Thus, a yield strength of 22.5 ksi is used.

The thinned section of pipe is modeled using the as-found wall thickness values for the region specified in S-TODI-2010-0005 which includes a minimum wall thickness of 0.077 inches. A pressure load of 1.5 times the specified design pressure is applied (1943 psi = 1.5*[1310psia-14.7psi]) to the pipe.

The results of the finite element analysis show that the thinned pipe in this section remains structurally stable at 1.5 times the specified design pressure and therefore passes the limit load analysis.

Unit 2 Buried AFW Piping:

At Salem Unit 2, the AFW discharge lines supplying the #22 and #24 SGs are also buried and run alongside the Unit 2 containment similar to the Unit 1 #12 and 14 AFW lines. The piping and coatings specified for Unit 2 AFW are identical to those in Salem Unit 1 AFW buried piping.

December 1994 Inspection

In December 1994, three areas of the buried Salem Unit 2 AFW piping were excavated due to a concern over water entering the Williamson penetration seals into Outer Penetration area. The concern was that this water could potentially be coming from a degraded buried #22 and/or #24 AFW line. Work order (941017262) created to excavate specific areas of the yard area containing these buried lines to rule out any degradation of the #22 or #24 AFW lines and prove that ground water was the source of the ingress.

Once excavation was complete in the three areas identified, coatings on these lines were inspected and photographs were taken. Per Report SCI-94-0877, the coal tar coating on the #22 and #24 Aux Feed lines appeared to be in excellent condition. It was noted that some of the coating had adhered very well and in other areas it had flaked off.

In one of the excavated areas, the coal tar coating was removed from the #22 and #24 AFW piping to allow for UT examination. These UT examinations revealed the following:

REFERENCE 1994 UT data

Upper AFW Pipe (#24):

No degradation of the piping was observed, with 50% of the piping at or above nominal thickness. No thickness readings below the manufacturer's tolerance of 87.5%. The lowest recorded value was 0.321" which was within the manufacturer's tolerance. Reference

Lower AFW Pipe (#22):
No degradation of the piping with 55% of the piping at or above nominal thickness, no thickness readings below the manufacturer's tolerance of 87.5%. The lowest recorded value was 0.306" which was within the manufacturer's tolerance. Reference

Post-inspection:
Any exposed carbon steel was prepped and recoated, and included the areas of minor flaking and sections where coating was removed for UT. All work was performed IAW work order instructions and station procedures. Two coats of Bitumastic 50 were applied over exposed metal surfaces IAW work order instructions. (See Report SCI-94-0877).

Recent AFW Excavation Inspection
On 4/22/2010, several areas were excavated to inspect a sampling of Unit 2 Aux Feed piping that was not part of the 1994 inspection. Salem Buried Pipe Program Engineer performed a visual inspection of the Salem Unit 2 Auxiliary Feedwater Buried Pipe for the No. 24 Aux Feed Train going to No. 24 Steam Generator. The subject pipe was unearthed in the Fuel Transfer Area just as it exits the building heading North towards the Outer Penetration. This 4" diameter pipe was completely exposed for an approximate 2 foot length at the wall penetration. Only the No. 24 line was exposed during this examination. The Bitumasitic coating was fully intact on the pipe, and showed no signs of deterioration or any flaking. Visual inspection included a look at the appearance, and running a hand over the pipe surface looking for loose coating or lack of adhesion. There was no loose coating or lack of adhesion, the coating was in excellent condition. WAITING FOR UT DATA FOR ELBOWS

Pooling Water
Notification 20459941 identified that pooling water was found in the area between Unit 2 containment and fuel handling building. Sampling results by chemistry detected measurable traces of ammonia. The results of an evaluation stated that the source of the water was not from the Unit 2 Auxiliary Feedwater system. reference

AFW Temperature Difference
On 4/20/2010 temperatures were taken on AF piping at various points upstream of the AF23 check valves. The purpose of this evolution was to determine if any of the AF lines is experiencing back leakage (which could be an indication of thru-wall leak). The results of the analysis shows that the temperatures measured seem appropriate for normal conduction of heat through the valve plug into fluid within the pipe. The pipe temperatures would be expected to stay elevated for longer lengths if there were a constant source of heated water moving through the pipe. Additionally, a review of operator log entries, SAP, and surveillance test results indicates that there has been no appreciable loss of inventory in the AFWST over the previous operating cycle.

Analysis

The piping is 4-inch NPS, Schedule 80, A106 Gr B seamless carbon steel. It is classified as Nuclear 3, Seismic Category I. Per the Pipe Specification S-C-MPOO-MGS-0001, SPS 54E, the design Pressure-Temperature limit is 1950 psi at 140 F. The nominal wall thickness is 0.337 inches.

To assess the available margin in the degraded Salem Unit 1 Piping, the maximum credible operating pressure was developed using all AFW system operating conditions (see SAP 70108698-0100). The resulting pressure is 1275 psi. The pipe wall t_{min} for this pressure is 0.185 inches. This operating pressure evaluation also applies to Salem Unit 2.

Since the AFW piping was found to be in good condition during 1994 inspection, and again during the current inspection, an average corrosion rate of 6 mils/year is conservatively assumed. The proposal is to perform excavation and inspections during the upcoming Unit 2 refueling outage (S2R18) scheduled for April 2011. This is a span of 16.5 years from the last inspection in 1994. The projected wall loss assuming a corrosion rate of 6 mils/per year is 0.099 mils (16.5 x 0.006). The projected wall thickness would be 0.207, which meets the minimum thickness requirement of 0.185 inches to support maximum credible operating pressure of 1275 psi Note that this projection assumes a nominal corrosion rate, even though spot inspections performed in 1994 and again in April 2010 showed that coating was intact and in good condition. Corrosion rate for sound coated carbon steel piping is zero.

Coating Life Span

Proper preparation of the carbon steel piping and application of the coating will ensure proper adherence to the piping. The recent inspections performed on 4/22/2010 of piping buried since construction showed that the coating was intact and in good condition, and the piping showed no indication of degradation or corrosion. Therefore, the coating is assumed to remain intact until next Unit 2 refueling outage.

In-service testing

The latest in-service testing for Unit 2 pumps and valves are provided below. Results of all testing was SAT.

Procedure	Component	Work Order	Date	Results
S2.OP-SO.AF-0005	21 & 22 Motor Driven Pumps	50114298	11/5/2009	SAT
S2.OP-SO.AF-0006	AF23 Stop Check Valves	50128109	01/24/2010	SAT
S2.OP-SO.AF-0007	23 Turbine Driven Pump	50113100	10/13/2009	SAT

Conclusion

Considering the positive inspection findings for both coatings and UT readings of the Salem Unit 2 #22 and #24 AFW buried lines, coupled with fact it is apparent that the Salem Unit 1 #12 and 14 AFW lines were not coated or improperly coated, there is reasonable assurance that the buried #22 and #24 AFW lines are protected from corrosion at this time by the coating system applied and are structurally sound, and the coating is assumed to remain intact until next Unit 2 refueling outage. Per the table above, recent In-service testing results for the AFW components were all SAT.

Based on the above information, it is concluded that Unit 2 AFW buried piping can perform its intended function until the next Unit 2 refueling outage (S2R18).

Future Actions and/or Compensatory Actions

Implement planned inspection per the buried pipe program in next outage of sufficient duration or S2R18. Perform Guided Wave examinations of the #22 and # 24 AFW buried piping during the next Unit 2 refueling outage – S2R18 As such, Guided Wave inspections of the Unit 2 AFW buried piping will be performed at locations to survey for areas of general or pitting corrosion. The results from the Guided Wave inspections will be used to target areas of interest for follow-up direct visual and confirmatory UT inspections to determine pipe minimum as-found wall thicknesses. Any portion of the piping if found unacceptable will be replaced.

2. EVALUATION:

2.1 Describe the safety function(s) or safety support function(s) of the SSC. As a minimum the following should be addressed, as applicable, in describing the SSC safety or safety support function(s):

UFSAR Section 10.4.7.2: Auxiliary Feedwater

The AFW System serves as a backup system for supplying feedwater to secondary side of the steam generators at times when the Main Feedwater System is not available. The AFW System is relied upon to prevent core damage and system overpressurization in the event of accidents such as a loss of normal feedwater or a secondary system pipe rupture, and to provide a means for plant cooldown.

Each unit is equipped with one turbine-driven and two motor-driven auxiliary feed pumps. Each motor-driven pump discharges to two steam generators with a normally isolated (21 and 22AF923 valves) cross-connect line joining the motor-driven pump discharge headers. The turbine-driven pump feeds all four steam generators. Feedwater flow is controlled from the Control Room by remotely operated flow control valves in the supply lines to each steam generator. In order to prevent a runout condition of the motor driven pumps the steam generator flow control valves (AF21's) modulates to control the motor-driven auxiliary feedwater pump discharge pressure.

The minimum performance limits required for the auxiliary feedwater pumps to satisfy the design bases analyses, as verified during quarterly (minimum flow/recirculation) and Full Flow Technical Specification Inservice Testing, are included below. Note that these values account for test instrumentation uncertainties.

S2.RA-ST.AF-0002 (*22AFP Min Flow Test)

Min Flow Test

21 motor-driven AFWP* _____ 160 gpm and 1369 psid

22 motor-driven AFWP _____ 160 gpm and 1389 psid

23 turbine-driven AFWP _____ 400 gpm and 1506 psid at 3600 rpm

S2.RA-ST.AF-0005 (*22 AFP Full Flow Test)

Full Flow Test

21 motor-driven AFWP _____ 440 gpm and 1184 psid

22 motor-driven AFWP* _____ 450 gpm and 1114 psid

23 turbine-driven AFWP _____ 880 gpm and 1269 psid at 3600 rpm

All auxiliary feed pumps normally take suction from the auxiliary feed storage tank. A safety grade, automatic low pressure trip is provided as backup protection for each pump in the event that tornado missile damage to the auxiliary feedwater storage tank results in loss of suction pressure. To protect against spurious activation, this trip will be made operable only during "tornado warnings" issued by the National Weather Service. The tank has sufficient capacity to allow residual heat removal for 8 hours. Backup water sources for the auxiliary feed pumps are the two demineralized water storage tanks (500,000 gallons capacity each), the two fire protection and domestic water storage tanks (350,000 gallons capacity each) and the station Service Water System, which must first have a spool piece installed. The quality of water from these sources is lower and is therefore intended for use only in the event of emergency situations.

- Does the SSC receive/initiate an RPS or ESF actuation signal?

YES. The Auxiliary Feedwater System (AFWS) is an Engineered Safeguards System (ESF). The motor driven auxiliary Feedwater pumps (MDAFPs) start automatically due to (1) trip of both main Feedwater pumps (LONF), (2) Safety Injection signal, and (3) a Low-Low signal from any one SG. The two MDAFPs are loaded onto the emergency diesel generators by the automatic load sequencer. The turbine driven auxiliary Feedwater pump (TDAFP) starts automatically on (1) a Low-Low level in two of the four SGs, (2) Loss of 125VDC control power, (3) Loss of Control Air, and (4) undervoltage on the reactor coolant pump group buses on 1 out 2 logic. For anticipated transients without scram (ATWS) events, which are not design basis transients analyzed in Chapter 15 of the FSAR, Westinghouse plants such as Salem have an ATWS Mitigation System Actuation Circuitry (AMSAC) to initiate a turbine trip an actuate auxiliary feedwater flow independent of the Reactor Protection System or the ESF Actuation System (ESFAS). When SG level drops below the AMSAC set point in 3 of 4 SGs, AMSAC initiates tripping the turbine, initiates AFWS, and isolates the SG blowdown and sample lines. AMSAC is non-safety related.

- Is the SSC in the main flow path of an ECCS or support system?

NO. The AFWS is not an Emergency Core Cooling System (ECCS) or an ECCS support system. The AFWS serves as a backup system supplying feedwater to the secondary side of the SGs when Main Feedwater system is unavailable. It is relied upon to prevent core damage and RCS overpressurization in certain design basis accidents such as Loss of Offsite Power (LOOP), LONF, Feedwater Line Break (FWLB), Main

Steam Line Break (MSLB), Steam Generator Tube Rupture (SGTR), or Loss of Coolant Accident (LOCA) by providing a means for plant cooldown from normal operating conditions to initiation of low pressure residual heat removal systems. It functions during startup, shutdown, and hot standby (HSB).

- Is the SSC used to:
  - Maintain reactor coolant pressure boundary integrity?

YES. The Auxiliary Feedwater system supplies water to the SGs for reactor decay heat removal when the normal Feedwater sources are unavailable due to loss of offsite power (LOOP) or other malfunction. By maintaining water levels in the SGs and thus ensuring an adequate heat sink, the AFWS functions to remove decay heat, reactor coolant pump heat, and sensible heat during plant cooldown. In addition, the AFW system functions to prevent overpressurization of the RCS, thereby protecting the reactor coolant pressure boundary (RCPB) integrity.

  - Shutdown the reactor?

NO. The AFWS does not provide a reactivity control safety function for shutting down of the reactor; although it does help to cooldown the reactor. The AFWS does not affect the rod control system or the alternative boron chemical shim system that control reactivity in the core. By providing the SG secondary side heat sink medium capable of receiving heat transfer from the reactor coolant system, the AFWS has an indirect positive reactivity effect by cooling and thus increasing the density of the reactor coolant neutron moderator.

  - Maintain the reactor in a safe shutdown condition?

YES. The licensing basis for safe shutdown at Salem is hot standby (HSB). The AFWS must perform its safe shutdown function to maintain the plant in HSB. The AFWS can be manually controlled to maintain HSB conditions until cooldown can be established. The AFWS is provided with sufficient water from the Auxiliary Feedwater Storage Tank (AFST) to allow the SGs to provide decay heat removal for 8 hours. In addition, backup water sources are provided from the Demineralized Water Storage Tanks (DWSTs), the Fire Protection Water Storage Tanks (FPWSTs), and a normally disconnected connection to the Service Water system for use in an emergency in the event of a seismic event that incapacitates AFST, DWSTs, and FPWSTs. During normal cooldown, each of the MDAFPs has the capacity to remove heat from the SGs at a sufficient rate to prevent RCS overpressurization and to maintain SG levels to prevent thermal cycling.

  - Prevent or mitigate the consequences of an accident that could result in offsite exposures comparable to 10 CFR 50.34(a)(1), 10 CFR 50.67(b)(2), or 10 CFR 100.11 guidelines, as applicable.

YES. The AFWS performs a safety function in mitigating design basis accidents, including LOOP, LONF, FWLB, MSLB, SGTR, and small break LOCA (SBLOCA) by supplying adequate feedwater to the secondary side of the Steam Generators to prevent overheating the reactor coolant system and to provide a means for achieving plant cooldown to initiation of the residual heat removal system. Depending on the design basis accident, the AFWS either maintains or limits feedwater to the SGs. For

the SBLOCA, LONF, and LOOP/LONF, the AFWS must maintain adequate feedwater. For the FWLB, the AFWS must preserve inventory while maintaining level. For the MSLB and SGTR events, the AFWS must limit feedwater flow as too much water delivery will result in overcooling the reactor coolant system or overpressurization of the containment.

- Does the SSC provide required support (i.e., cooling, lubrication, etc.) to a TS required SSC?

YES. During normal plant cooldown, the AFWS removes sufficient heat from the SGs to prevent overpressurization of the RCS and to maintain SG levels sufficient to prevent thermal cycling.

- Is the SSC used to provide isolation between safety trains, or between safety and non-safety ties?

NO. The AFWS does not perform an isolation function per se; however, whenever either the MDAFPs or the TDAFP automatically starts, a signal is sent to the isolation valves of the Steam Generator Blowdown and Sampling Systems to close. The isolation signal to the Sample System isolation valves can be bypassed using a keylocked switch located in the Control Room.

- Is the SSC required to be operated manually to mitigate a design basis event?

NO. The AFW pumps can be operated manually at their local control panel or from the main Control Room. Automatic initiation signals are designed to prevent system malfunction given a single failure. AFW flow is controlled from the Control Room using remotely-operated flow control valves (AF21's) in the supply lines to each SG. Safety-related flow indication to each SG is provided in the Control Room. The flow control valves have reduced capacity trim to limit the maximum flow under certain plant conditions.

- Have all specified safety functions described in TS been included?

YES. Salem T/Ss require that at least three independent AFW pumps, their associated manual activation switches in the Control Room, and their flow paths are operable in Modes 1 though 3. The two MDAFPs must be capable of being powered from separate vital busses and the TDAFP must be capable of being powered from an operable steam supply system. Operability of the AFWS ensures that the Reactor Coolant System can be cooled down to less than 350 F from normal operating conditions in the event of a total loss of offsite power (LOOP).

- Have all safety functions of the SSC required during normal operation and potential accident conditions been included?

YES. The AFWS safety functions include LONF, FWLB, MSLB, LOOP, and LOCA during accident conditions and plant cooldown during normal plant conditions. The AFWS supplies water to the SGs for reactor decay heat removal if the normal Feedwater sources are unavailable due to loss of offsite power or other malfunctions.

- **Is the SSC used to assess conditions for Emergency Action Levels (EALs)?**

NO. The AFWS is not used to assess conditions for EALs.

2.2 Describe the following, as applicable: (a) the effect of the degraded or nonconforming condition on the SSC safety function(s); (b) any requirements or commitments established for the SSC and any challenges to these; (c) the circumstances of the degraded/nonconforming condition, including the possible failure mechanism(s); (d) whether the potential failure is time dependent and whether the condition will continue to degrade and/or will the potential consequences increase; and (e) the aggregate effect of the degraded or nonconforming condition in light of other open OpEvals:

Table: List of Existing OpEvals

NUMBER	NOTF/ORDER	ENTRY DATE	DESCRIPTION	OWNER	STATUS	EXPECTED CLOSURE
07-033	80094618	9/07/07	S1/2 ECCS room cooler thermostats (DCP 80094618 and 80095613)	Bhardwaj	80094618-issued, need orders planned 80095613- issued, need orders planned	08/11
08-040	70087831	8/08/08	230V Motor Operated Valve – degraded voltage	Ciarlante	S1/S2 On-Line DCP 80099509 to be planned, scheduled, installed	12/23/10
09-09	60084229	4/07/09	CAA14/CAA17/CAA20	Hassler	Perform Inspections	5/31/10
09-019	60085180	8/10/09	SRW watertight door	Hassler	Replace door seal WW 0022	5/21/10
09-021	70103767	11/5/09	Can Liner	Curran	Repair In S2R18	S2R18
09-023	70104221	11/9/09	PZR Heater busses E & G 3 overheating	R. Smith	Procure new panel door design/ Implement new design	6/1/10
10-001	70106347	1/28/10	21 SI pump oil leak	Hummel	Develop repair plan Repair Oil Leak	9/27/10
10-002	60089385	03/19/10	#4 SW Bay Ventilation Temp Controller	Hayman	Perform repairs	4/27/10
10-003	20455408	3/25/10	22SW34 Valve failed ASME code reverse flow check	Hassler	Perform repairs	5/30/10
10-004	20457356	4/07/10	#3 SW Bay Vent temp controller for 1SWV3	Hayman	Perform repairs	9/30/10

A) THE EFFECT OF THE DEGRADED OR NONCONFORMING CONDITION ON THE SSC SAFETY FUNCTION(S)

The nonconforming condition potentially affects the structural integrity of the AFW discharge piping, reducing the margin of the Tmin wall thickness for a given pressure and would limit the maximum pressure to a value less than the design pressure. Based on an assumed constant corrosion rate, the wall thinning reduces the life expectancy of the buried pipe. If structural integrity is lost and a breach in the pipe occurs, the AFW system can no longer fully perform its design safety function. It should be noted that there has been no identified active leak reported.

B) ANY REQUIREMENTS OR COMMITMENTS ESTABLISHED FOR THE SSC AND ANY CHALLENGES TO THESE

The requirement associated with minimum wall thickness (Tmin) for buried AFW pipe is governed by the ANSI B31.1, 1967 Edition, Power Piping code.

C) THE CIRCUMSTANCES OF THE DEGRADED/NONCONFORMING CONDITION, INCLUDING THE POSSIBLE FAILURE MECHANISM(S)

The degradation of the auxiliary feed water piping at Unit 2 is substantially less than that at Unit 1. Based on the existing data, it is concluded that the AFW piping will be able to perform its intended design function at least until the next Unit 2 refueling outage (April 2011) when an extensive investigation will be performed. A complete loss of wall thickness would result in rupture in the pipe. Any rupture will result in loss of cooling of the steam generators.

D) WHETHER THE POTENTIAL FAILURE IS TIME DEPENDENT AND WHETHER THE CONDITION WILL CONTINUE TO DEGRADE AND/OR WILL THE POTENTIAL CONSEQUENCES INCREASE; AND

The potential failure of the pipe is time dependent based on the assumed corrosion rate. Based on earlier assessments of carbon steel corrosion due to exposure to brackish Service Water, the buried AFW pipe wall thickness will continue to degrade 6 mils per year until the pipe will no longer be capable of supporting the maximum credible operating pressure without margin to eminent failure.

E) THE AGGREGATE EFFECT OF THE DEGRADED OR NONCONFORMING CONDITION IN LIGHT OF OTHER OPEN OPEVALS (SEE TABLE OF OPEN OPEVALS ABOVE)

The aggregate impact of the non-conformance being evaluated was assessed against outstanding OpEVals listed in the Table above. Each of the ODs was reviewed in depth for the description of condition and the basis of the operability determination to determine if the non-conformance described in this OpEval will make any SSC covered in the other outstanding ODs inoperable or degraded. In conclusion, the OpEval discussed herein has no aggregate impact on any SSC safety function or other OD currently open.

		YES	NO
2.3	Is SSC operability supported? Explain basis (e.g., analysis, test, operating experience, engineering judgment, etc.):	[X]	[ ]

<u>Summary SIA Finite Element Analysis Report</u>

The preliminary analysis of the Salem Unit 1 underground auxiliary feedwater piping is complete. The analysis evaluated the region specified in S-TODI-2010-0005 which

includes a minimum wall thickness of 0.077 inches. A Limit Analysis was performed as described in NB-3228.1. NB-3228 allows relaxation of basic stress limits if plastic analysis is used. An elastic-perfectly plastic finite element analysis was performed and the results show that the criterion specified in NB-3228.1 is satisfied.

If 2.3 = NO, notify Operations Shift Management **immediately**.
If 2.3 = YES, clearly document the basis for the determination.

		YES	NO
2.4	Are compensatory measures and/or corrective actions required?	[X]	[X]

If 2.4 = YES, complete section 3.0 (if NO, N/A section 3.0).

Reference Documents:

2.4.1. Technical Specifications Section(s):

T/S 3/4.7 Plant Systems, LCO 3.7.1.2, Auxiliary Feedwater System

2.4.2. UFSAR Section(s):
3.7.3.9
3.9.4: Inservice Testing Pumps and Valves
10.4.7.2, Auxiliary Feedwater System
15.2.8, Loss of Normal Feedwater
15.2.9, Loss of Offsite Power to Station Auxiliaries (LOP)
15.3.1, Loss of Reactor Coolant from Small Ruptured Pipes (SBLOCA)
15.4.1, Major Reactor Coolant System Pipe Ruptures (LBLOCA)
15.4.2, Major Secondary System Pipe Rupture (MSLB)
15.4.3, Major Rupture of Main Feedwater Line (FWLB)
15.4.4, Steam Generator Tube Rupture (SGTR)

2.4.3. Other:
Technical Evaluation 70108698, Rev. 0
Technical Evaluation 20459941 Potential Water Sources Inner Mechanical Penetration
ANSI B31.1, 1967 Ed., Power Piping
DWG 205336 Sheet 1 Rev. 49
DWG 218233 Sheet 1 Rev. 11
S-C-MPOO-MGS-0001, SPS54, Rev. 6, Piping Schedule, Auxiliary Feedwater
S-C-AF-MDC-0445, Rev. 3, Auxiliary Feedwater System Hydraulic Analysis
S-C-F400-MDC-0096, Rev. 4 Auxiliary Feedwater Storage Tank (AFWST) Capacity
S-C-A900-MDC-005, Rev. 0, Pipe Wall Thickness Calculations (Info Only)
S2.OP-ST.AF-0002 Rev 18
S2.RA-ST.AF-0001 Rev. 6 (21 Aux Feed Pump)
S2.RA-ST.AF-0002 Rev. 9 (22 Aux Feed Pump)
S2.RA-ST.AF-0005 Rev. 9

SC.DE-BD.AF-0001(Q), Rev. 0, Auxiliary Feedwater System (Info Only)
[SIA Finite Element Analysis Report] S-TODI-2010-0005
SCI-94-877 LTR dated 12/16/1994 - Excavated Auxiliary feedwater Piping Walkdown/Disposition of Coating Requirements
20459689
Work Order 941017262
Duane Arnold Energy Center Relief Requests NDE-R004 and NDE-R007 (Info Only)

3. **ACTION ITEM LIST:**

If, through evaluating SSC operability, it is determined that the degraded or nonconforming SSC does **not** prevent accomplishment of the specified safety function(s) in the TS and the intention is to continue operating the plant in that condition, then record below, as appropriate, any required compensatory measures to support operability and/or corrective actions required to restore full qualification. For corrective actions, document when the actions should be completed (e.g., immediate, within next 13 week period, next outage, etc.) and the basis for timeliness of the action. Corrective action timeframes longer than the next refueling outage are to be explicitly justified as part of the OpEval or deficiency tracking documentation being used to perform the corrective action.

Compensatory Measure #1: **None** Responsible Dept./Supv.: Action Due: Action Tracking #:
Compensatory Measure #2: **None** Responsible Dept./Supv.: Action Due: Action Tracking #:

Corrective Action #1: **Perform Guided Wave examination and visual examination of the excavated area for the #22 and # 24 AFW buried piping during the next Unit 2 refueling outage – S2R18. The results from the Guided Wave inspections will be used to target areas of interest for follow-up direct visual and confirmatory UT inspections to determine pipe minimum as-found wall thicknesses. Replace if necessary, all non-conforming buried AFW piping. Work Order 60084161 is created to perform this task.** Responsible Dept./Supv.: **TBD** Action Due: **S2R18 Refueling Outage (April 2011)** Action Tracking #: **Work Order 60084161**
Corrective Action #2: Responsible Dept./Supv.: Action Due: Basis for timeliness of action: Action Tracking #:

4. **SIGNATURES:**

4.1 Preparer(s) **Mark Puher** Date **04/22/2010**

Robert Down Date **04/22/2010**

4.2 Reviewer Kiran Mathur Date **04/22/2010**
(10 CFR 50.59 screener qualified or active SRO license holder)

4.3 Sr. Manager Design Engr/Designee Concurrence _____ Date _____

4.4 Operations Shift Management Approval _____ Date _____

4.5 If the OpEval is to declare a Shutdown Safety System or component Operable but Degraded, then the following signatures are required: **(CAPR 70103591)**

Operations Director _____ Date _____

Engineering Director _____ Date _____

* Shutdown Safety Manager _____ Date _____

* When in Modes 4, 5, 6, Defueled (SA) or Modes 3, 4, 5 (HC).

4.6 Ensure the completed form is forwarded to the OEPM for processing and Action Tracking entry as appropriate.

5. **OPERABILITY EVALUATION CLOSURE:**

5.1 Corrective actions are complete, as necessary, and the OpEval is ready for closure

_____ Date _____
(OEPM)

5.2 Operations Shift Management Approval _____ Date _____

5.3 Ensure the completed form is forwarded to the OEPM for processing, Action Tracking entry, and cancellation of any open compensatory measures, as appropriate.

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Appendix A

ANSYS INPUT FILES

File name	Description
12AF_4sch80.inp	ANSYS model input file for location 12AF
14AF_4sch80.inp	ANSYS model input file for location 14AF
14AK_4sch80.inp	ANSYS model input file for location 14AK
AF13T_4sch80.inp	ANSYS model input file for location AF13T
tuesday_4sch80_bndng_EP.inp	ANSYS model input file for location between AF4T and AF5T

Ahmed, Mohammad I.

From: Romero, Martin [Mromero@Structint.com]

Sent: Wednesday, April 21, 2010 11:11 PM

To: Adair, Mark; Davies, Steven B.; Ahmed, Mohammad I.; Hennessy, Philip; Johnson, Alan A.

Cc: Gerber, Nancy; McGill, Bob; Bax, Rich; Jenson, Craig

Subject: Salem Unit 1 Underground Auxiliary feedwater Piping preliminary evaluation results

Hello:

The preliminary analysis of the Salem Unit 1 underground auxiliary feedwater piping is complete. A non-linear elastic-perfectly plastic finite element analysis was performed on the bounding location of the auxiliary feedwater piping and it was found to remain structurally stable using stress limits from the original B31.1 Power Piping Code. The following sections were evaluated: 12AF, 14AF, 14AK, AF13T, and a section of pipe between AF4T and AF5T. The section of pipe between AF4T and AF5T was found to be bounding based on a linear-elastic finite element analysis and required a more rigorous analysis described below.

The underground auxillary feedwater piping at Salem, Unit 1 was designed to the t_{min} requirement given in the B31.1 Power Piping Code. B31.1 does not provide specific criteria for the evaluation of non-uniform wall thickness or local thinning. However, guidance for stress analysis may be taken from the ASME Code, Section III as described below.

The technical approach taken herein is based on the premise that while piping may have localized thinned regions that violate the design t_{min} requirements, the non-uniform wall thickness of the pipe cross-section may be shown to meet design stress allowables. This approach is possible for the pipe section exhibiting thinning when a remaining wall greater than t_{min} surrounds the thinned region. This approach is similar to the basis for qualifying pipe penetrations using branch reinforcement rules in the ASME Code.

Design requirements for Class 3 piping are provided in ND-3600 (similar to B31.1 rules) of the ASME Code, Section III [2]. More rigorous analyses are allowed under ND-3611.3:

"The specific design requirements of ND-3600 are based on a simplified engineering approach. A more rigorous analysis such as described in NB-3600 or NB-3200 may be used to calculate the stresses required to satisfy these requirements. These calculated stresses must be compared to the allowable stresses in this Subsection. In such cases, the designer shall include the appropriate justification for the approach taken in the Certified Design Report."

Thus, NB-3200 design by analysis is employed. Based on the linear-elastic finite element analysis results which showed that the section of pipe between AF4T and AF5T was bounding, it was required to perform additional analysis only for that section of pipe in order to show operability. The more rigorous analysis employed is described in Section NB3228.1, Limit Analysis. Specifically Section NB-3228.1 states that limits on Local Membrane Stress Intensity need not be satisfied at a specific location if it can be shown by limit analysis that the specified loadings do not exceed two-thirds of the lower bound collapse load. Also, NB-3228.1 states that the yield strength to be used in this calculation is $1.5S_m$. In this evaluation, the value of yield strength is equal to 1.5S, where S is taken as the value of S_h, 15.0 ksi, from the original 1967 B31.1 Power Piping Code. Thus, a yield strength of 22.5 ksi is used.

The section of pipe between AF4T and AF5T is modeled using the as-found wall thickness values for the region specified in S-TODI-2010-0005 which includes a minimum wall thickness of 0.077 inches. A pressure load of 1.5 times the specified design pressure is applied (1943 psi = 1.5*(1310psia-14.7psi)) to the pipe.

The results of the finite element analysis show that the thinned pipe between AF4T and AF5T remains structurally stable at 1.5 times the specified design pressure and therefore passes the limit load analysis.

A draft calculation package will be transmitted Friday morning. If there are any questions, please do not hesitate to call me on my cell phone (408)218-2349.

Thank you,

Martin Romero, P.E.
Senior Consultant

An Assessment of "ASME Code, Section III, Design by Analysis Evaluation of a 4-inch Auxiliary Feedwater Piping" for Salem Generating Station, Unit 1.

Background

The licensee identified localized wall thinning in several regions of the buried auxiliary feedwater (AFW) piping at Salem Generating Station, Unit 1, based on the guided wave technology. The licensee excavated the affected piping regions and found significant external corrosion. Subsequently the licensee inspected the affected piping segments using straight beam ultrasonic testing to determine the pipe wall thickness. Several measurement locations showed pipe wall thicknesses less than the design minimum wall thickness. The licensee performed stress calculations to demonstrate that the degraded AFW piping still meets allowable stresses of the ASME B31.1 Code of Construction and that the piping was operable during past operation.

Discussion

Under ASME Section XI, a planar or laminar flaw is dispositioned by the acceptance standards of IWB-3515. If the flaw is within the acceptance standards of IWB-3515, the flaw can be left in service. If the flaw exceeds IWB-3514, the flaw may be accepted by analysis of IWB-3600 followed by 3 successive examinations. A pipe that contains a flaw that exceeds IWB-3600 will need to be repaired or replaced. The ASME Code, Section XI, is stringent in that it minimizes flaws from growing uncontrollably to rupture. A pin hole leak that is caused by wall thinning, in general, does not lead to pipe rupture [I believe that a pipe rupture is defined as when the leak rate from a crack is so large that the pump cannot provide sufficient makeup to achieve the intended function of the pipe]. Salem's AFE pipe degradation mechanism is wall thinning.

The ASME Code, Section XI, does not have requirements for analyzing wall thinning condition except in Code Case N-513-2. However, N-513-2 is not applicable to high energy line such as AFW line.
Code Case N-561-2, Alternative Requirements for Wall Thickness Restoration of Class 2 and High Energy Class 3 Carbon Steel Piping, provides guidance for high energy Class 3 piping. However, the NRC has not approved N-561 in Regulatory Guide 1.147, Revision 15.

Therefore, the licensee used the rules of the ASME Section III to satisfy 10 CFR 50.55a. Under the ASME Code, Section III, the same pipe would not need to be repaired as long as the pipe satisfies the allowable stresses of NB-3200 or NB-3600. The AFW piping is ASME Class 3 pipe and should follow the rule of ND-3000 for piping design. However, the licensee selected the rules of Class 1 piping, (i.e., NB-3200 and/or NB-3600) because rules in NB-3000 provide more detailed analysis procedures and allowables.

The licensee analyzed five pipe segments, 12AF, 14AF, 14AK, AF13T, AF4T/AF5T. The resultant stresses are shown on Pages 11 to 13 and page 16 of the report. As shown on those pages, each of the pipe segments has certain locations that exceed the allowable stresses. However, when the licensee linearized the stresses in all the nodes in the model and calculated a single stress, the linearized stress for each of the pipes is within the allowable as shown in Table 1 (page 8). In other words, even though localized stress at certain node in each of the pipes exceeds the allowable stress, the overall (global) stress of each of the pipe are within the allowable.

The licensee did not use the as-found pipe wall thickness (the thinnest wall thickness) for the entire pipe in calculating the stresses. For example, the licensee did not use 0.077 inch to calculate the stress for

the entire pipe segment. Instead, the licensee used the as-found wall thickness (0.077 inch) to calculate the local stresses at the node (location) where the wall thinning was found. For other nodal points of the pipe, the licensee used the nominal thickness or as-found pipe thickness at those nodes which may not be degraded. Although some pipe locations have severe wall thinning degradation, the licensee was able to demonstrate that the structural integrity of the pipe as a whole is acceptable.

Conclusion

The staff finds that the degraded AFW piping satisfies the requirements of ASME Code, Section III, NB-3213.10, NB-3221.2, and NB-3228.1. However, the staff concludes that the subject AFW piping is operable but degraded.

Recommendations

1. Page 4, last paragraph. The licensee stated that the worst wall thickness is 0.077 inch. Confirm that the minimum allowable pipe wall thickness is 0.190 inch as shown on page 5, second paragraph.

2. The stress analysis needs to include detailed pipe wall thickness measurements in all 5 subject AFW pipes so that the reviewer can understand the extent of the wall thinning.

Transmittal of Design Information
Transmittal Number: S-TODI-2010-0004

Date: 04/16/2010

To: Robert McGill
Structural Integrity Associates
5215 Hellyer Avenue, Suite 210
San Jose, CA 95138-1007

From: Arie Blum
Salem Design Engineering – Mechanical/ Structural
P.O. Box 236, M/C 29,
Hancocks Bridge, NJ 08038

Subject: Confirmation of design input information for Salem Unit 1, Underground Auxiliary Feedwater Piping

Follows are the description of the Attachments contained in this TODI:

Attachment 1 - Specification No. S-C-MPOO-MGS-001, Piping Schedule SP54

The piping is classified as Nuclear Class 3 and Seismic Class 1. The material is ASTM A106 Grade B. The maximum temperature is 140^{0}F. For the pressure see Attachment 2.

Attachment 2 – Technical Evaluation (TE) No. 70108698-005

The TE establishes the maximum credible operating pressure of 1275 psia. However, it is requested that the evaluation establishes a **maximum design pressure** for the Underground Auxiliary Feedwater piping based on its degraded condition, using ASME factor of 3.5 and 4.

Attachment 3 – Ultrasonic Thickness Examination record

The NDE data report is generated under work order number 60084266. As documented in this report the Pipe is 4" diameter with Nominal wall thickness of 0.337". It includes the UT data for the entire exposed Auxiliary Feedwater piping.

Intended use of the information being provided:

To generate analysis related to Salem Unit 1 Underground Auxiliary Feedwater Piping thinned wall piping, inspection/ evaluation scope during S1R20 refueling Outage.

Limitations on the use of the transmittal information:

This information is intended only to be used for Salem Unit 1 affected piping evaluation.

References:

(1) Notification 20456999
(2) PSEG Calculation 6S0-1882, Rev. 1
(3) PSEG Drawing AF-13A
(4) PSEG P&ID No. 205236

Signatures

Preparer: _____ Date: 04/16/2010
Arie Blum

Reviewer: _____ Date: 04/16/2010
Mohammad Ahmed

Approver: _____ Date: 04/16/2010
Phil Hennessy

ATTACHMENT 1

S-TODI-2010-004
P. 1 of 5

SPECIFICATION NO. S-C-MPOO-MGS-0001

PIPING SCHEDULE SPS54

AUXILIARY FEEDWATER

SERVICE: - Demineralized water (emergency - fresh water, demineralized water and salt water)

Group	A Pump Suction	B Alternate Pump Suction in yard	C Minimum flow Recirculation	D Pump Discharge up to level Control valve	E* Level Valve to Isolation Check valve
W.W.P., Maximum, psi	30 to 195	25	100	1950	1950
Normal, psi	30	25	100	1600	1195
W.W.T., Maximum, °F	120	120	130	120	140
Normal, °F	Ambient	Ambient	Ambient	Ambient	140
Seismic Design Class	1	3	1	1	1
Nuclear Class	3	None	3	3	3
PRIMARY SERVICE PRESSURE RATING:					
Pressure, lbs	150	150	150	900	900
Temperature, °F	500	500	500	850	850

* For piping between isolation check valve and steam generator feed line see Piping Schedule SPS16 Group A

SPECIFICATION NO. S-C-MPOO-MGS-0001

PIPING SCHEDULE SPS54

AUXILIARY FEEDWATER

PIPE:

MATERIAL

ASTM A106 Gr. B, seamless carbon steel, silicon killed.

ASTM A335 P22, seamless alloy steel.

Mill inspection and test reports required.

Check analysis and flattening test of one length of each lot required.

Flush piping with fresh water immediately after using salt water or demineralized water.

For protection of underground piping in the yard see page II-88 of Piping Schedule SPS28 of this specification. ``X-tru-coat'' may be used.

Dimensions

ANSI B36.10

For the 25 psi, 50 psi and 30 to 195 psi maximum systems:

Schedule 40 for 10 inch and smaller.

0.375 inch wall for 12 inch thru 16 inch

For the 1950 psi maximum systems:

Schedule 80 for 1 inch and 4 inch.

Schedule 160 for 1-1/2, 2, 2-1/2 and 3 inch sizes.

Schedule 120 for 6 inch thru 24 inch.

3/4 inch minimum size for 25 psi, 50 psi and 30 to 195 psi maximum systems.

1 inch NPS minimum size for 1950 psi maximum systems.

USER RESPONSIBLE FOR VERIFYING REVISION, STATUS AND CHANGES

SPECIFICATION NO. S-C-MPOO-MGS-0001

PIPING SCHEDULE SPS54

AUXILIARY FEEDWATER

FITTINGS AND FLANGES:

MATERIAL

ASTM A234 WPB and A234 WP22 seamless, for butt welding fittings.

ASTM A105 for forged socket welding fittings.

ASTM A182 F22 for forged chrome-moly alloy steel socket welding fittings.

ASTM A182 F316 for blind flange only and with Engineering's approval.

ASTM A181 Cl. 60 or ASTM A105 for flanges in the 25 psi, 50 psi and 30 to 195 psi maximum systems.

ASTM A105 for flanges in the 1950 psi maximum systems.

Mill inspection and test reports required.

Dimensions of fittings

ANSI B16.9 for butt welding fittings.

ANSI B16.11 for socket welding fittings.

Socket welding ends for 2 inch and smaller.

Butt welding ends for 2-1/2 inch and larger.

Dimensions of flanges

ANSI B16.5 for flanges.

All flanges to be welding neck type.

Facings for 25 psi, 50 psi and 30 to 195 psi maximum systems.

Raised face with stock spiral serrated finish.

Facings for 1950 psi maximum systems.

2-1/2 inch and smaller - large male and female.
3 inch and larger - small tongue and groove.

Contact facing machined per drawing 25057-L.

USER RESPONSIBLE FOR VERIFYING REVISION, STATUS AND CHANGES

PIPING SCHEDULE SPS54

AUXILIARY FEEDWATER

JOINTS:

Socket weld for 2 inch and smaller.

Butt welding for 2-1/2 inch and larger.

Full strength, full penetration, fusion welded in accordance with ASME Boiler and Pressure Vessel Code, Section III.

Stress relieving not required.

Heat treatment, welding and brazing as specified in applicable PSE&G Nuclear Welding and Brazing Manual, NC.ER-TM.ZZ-0002(Q).

Random magnetic particle examination of fillet welds, socket welds and welded branch connections over 4 inch pipe size for Nuclear Class 3 piping in accordance with Table A.7(b) of ANSI B31.7.

Random magnetic particle or liquid penetrant examination required for all Nuclear Class 3 welds 4 inch size and smaller. (Should not MT under 2 inch).

Hydrostatic pressure test of erected system shall be performed.

BOLTING:

MATERIAL

Alloy steel bolt-studs - ASTM A193 Gr. B7

Carbon steel nuts - ASTM A194 Gr. 2H

Dimensions

ANSI B18.2.1 - Heavy hex bolts.
ANSI B18.2.2 - Heavy hex nuts.
ANSI B1.1 - Threads

1 inch diameter and smaller - coarse thread series with fit specified in ANSI B1.1 standard.

1-1/8 inch diameter and larger - 8 pitch thread series, Class 2A for bolts and studs, Class 2B for nuts.

USER RESPONSIBLE FOR VERIFYING REVISION, STATUS AND CHANGES

BOLTING - (Cont'd)

Nuts shall be hot-forged or machined from hot-forged bars.

GASKETS:

For the 25 psi, 50 psi and 30 to 195 psi maximum systems

Sheet packing, 1/32 inch Garlock Blue-Gard Style 3400.

For the 1950 psi maximum systems

Flexitallic spiral-wound gaskets, style R-1 or RIR, with Type 304 S.S. and Flexite Super or Grafoil filler for large male and female flanged joints.

Flexitallic spiral-wound gaskets, style R-4, with Type 304 S.S. and Flexite Super or Grafoil filler for small tongue and groove joints.

Dimensions to conform to ANSI B16.5.

Piece Mark Identification---AF---(Prefix Station Unit No. to AF)

USER RESPONSIBLE FOR VERIFYING REVISION, STATUS AND CHANGES

Tech Eval prepared

**********Long Text Object Identification**********
Order 000070108698 Operation 0050 Confirmation 0008163337
Confirmation counter 00000001 Long text
****

Document #: 70108698-0050

TITLE: Maximum Pressure in Underground Auxiliary Feedwater Piping

REASON FOR EVALUATION / SCOPE:

Degradation was found in the underground Auxiliary Feedwater (AFW) piping prior to entering the Outer Penetration Area per Notification 20456999. This is the supply piping to 12 & 14 Steam Generators (SGs), downstream of the AFW pumps. This Technical Evaluation determines the maximum potential pressure in this piping for input into a subsequent evaluation on minimum wall.

DETAILED EVALUATION:

Auxiliary Feedwater Operation:

The AFW System provides flow to the SGs during plant cooldown and startup conditions for decay heat removal when the Main Feedwater (MFW) System is out of service. The AFW System also provides flow to the SGs during transient conditions such as Steam Line Break (SLB), Feedwater Line Break (FLB), Small Break Loss of Coolant Accident (SBLOCA), Loss of Normal Feedwater (LONF), Loss of Offsite Power (LOOP) and Station blackout (SBO). The system consists of two Motor Driven AFW Pumps (MDAFPs), each of which feeds two SGs, and one Turbine Driven AFW Pump (TDAFP), which feeds all four SGs. During plant cooldown and startup, operators manually control AFW flow via the AF21 control valves for the MDAFPs and via the AF11 control valves for the TDAFP. During transient conditions, the AF21 control valves are in automatic and control to maintain MDAFP discharge pressure; the AF11 control valves are full open.

The maximum potential pressure in the system would be with all the AFW pumps deadheaded. However, this is an unrealistic condition. The actual maximum system pressure is a function of the maximum potential SG pressure. Per Reference 3, the maximum SG pressure is assumed to be the lowest Main Steam (MS) safety valve setting (1070 psig - Reference 2) plus 3% accumulation, or 1102 psig (1117 psia).

The maximum system pressure would occur with all three pumps running on their design performance curves. Reference 3 provides a hydraulic analysis for the system transient conditions, using the AFW System hydraulic model. The SLB Inside Containment transient is analyzed with this pump

alignment for two conditions - no failures and MDAFP runout protection failure, which is a failure of one of the AF21 valves to the full open position. The actual maximum pressure in a particular SG supply line would occur for a failure of an AF21 valve to the full closed position, which maximizes pressure in the SG supply line that remains aligned to the associated MDAFP. This condition was not analyzed in Reference 3 as the parameter of concern was maximum total SG flow. As such, additional cases were run with 11AF21 closed, to maximize pressure in the 12 SG supply piping (Case A), and with 13AF21 closed, to maximize pressure in the 14 SG supply piping (Case B). For conservatism and simplicity, it was assumed that the remaining AF21 valves are full open. In reality they would be throttled to maintain MDAFP discharge pressure; however, determining their position is an iterative and cumbersome process. Case 4 from Reference 3 Proto-Flo database S-C-AF-MDC-0445-R3.DBD was modified accordingly. The pressure in the underground piping is assumed to be that from the nearest upstream node in the model, which are the tie-ins between the MDAFP and TDAFP discharges in the Auxiliary Building. The resulting pressures at these nodes are 1259 psia (1244 psig) for 12 SG supply (Case A) and 1270 psia (1255 psig) for 14 SG supply (Case B). The Proto-Flo output reports are included as Attachments 1 and 2, respectively. 1275 PSIG

During normal plant cooldown and startup, it is unlikely all three AFW pumps would be running. Furthermore, the AF21s and/or AF11s are manually throttled to control cooldown rate and/or maintain SG level, which reduces the downstream pressure and thus the pressure in the buried piping. Therefore, this condition is bounded by the SLB transient condition with respect to pressure in the buried piping.

Auxiliary Feedwater System Testing:

MDAFP and TDAFP full flow testing to the SGs is performed per References 7 & 8 during each Refueling Outage. The highest pump discharge pressure occurs for the TDAFP test. The TDAFP discharge pressure was originally base lined at 1250 psig in 1998 (WO #960829007). Since then the TDAFP discharge pressure has varied been between 1235 and 1248 psig. These pressures are bounded by the limiting SLB Case from above (Case B, 13AF21 fails closed). Furthermore, similar to normal plant cooldown and startup, the AF21s and AF11s are manually throttled during testing to set the required flow, and so the pressure in the buried piping to 12 and 14 SGs would be even less. Therefore, full flow testing is bounded by the SLB transient condition. During quarterly surveillance testing (References 4-6), the AF21s and AF11s are closed, with flow going through the respective pump recirculation line, and thus is not applicable to this evaluation.

Main Feedwater Operation:

During normal plant operation, the MFW System provides flow to the SGs, and the AFW System is isolated from the SGs. During this condition, there is a potential for back leakage through the AF23 stop check valves, which are located just upstream of

the AFW tie-ins to the MFW System. A leak check of these valves is performed quarterly per Reference 9. Trending of past test results finds no indication of significant leakage past these check valves. Test results found AFW line pressures typically around 25-30 psig with a MFW pressure of around 835-845 psig. A couple exceptions were for the test on 8/30/09, where the 12AF23 upstream pressure was 150 psig, and for the test on 3/1/10, where the 11AF23 and 12AF23 upstream pressures were about 115 psig. If these couple results were an indication of actual leakage, the AFW line pressure was still significantly below the MFW line pressure. Thus, even if the MFW System flow was low, with corresponding higher system pressure, the resulting AFW line pressure with any leakage past 12AF23 would still be very low compared to that with the AFW System in service.

CONCLUSIONS/FINDINGS:

The maximum potential pressure in the buried AFW piping during an accident is 1259 psia (1244 psig) for 12 SG supply and 1270 psia (1255 psig) for 14 SG supply. This occurs for a SLB Inside Containment transient with a single failure of an AF21 valve to the closed position, at the maximum potential SG pressure. For conservatism, the maximum operating line pressure in the buried AFW piping is set at 1275 psia

REFERENCES:

1. P&ID 205236, Revision 54, Unit 1 Auxiliary Feedwater

2. P&ID 205203, Sheet 1, Revision 77, Unit 1 Main, Reheat & Turbine By-Pass Steam

3. S-C-AF-MDC-0445, Revision 3, Auxiliary Feedwater System Hydraulic Analysis

4. S1.OP-ST.AF-0001, Revision 15, Inservice Testing - 11 Auxiliary Feedwater Pump

5. S1.OP-ST.AF-0002, Revision 16, Inservice Testing - 12 Auxiliary Feedwater Pump

6. S1.OP-ST.AF-0003, Revision 38, Inservice Testing - 13 Auxiliary Feedwater Pump

7. S1.OP-ST.AF-0005, Revision 11, Inservice Testing Auxiliary Feedwater Valves Mode 4-6

8. S1.OP-ST.AF-0007, Revision 19, Inservice Testing Auxiliary Feedwater Valves Mode 3

9. S1.OP-ST.AF-0006, Revision 10, Inservice Testing Auxiliary Feedwater Valves

10. UFSAR Section 10.4.7.2, Auxiliary Feedwater System; Section 15, Accident Analysis

ATTACHMENTS

1. Case A Proto-Flo Ouput Reports: SLB Inside Containment with 11AF21 Failing Close
2. Case B Proto-Flo Ouput Reports: SLB Inside Containment with 13AF21 Failing Close

NOTE: The complete Technical Evaluation, including attachments, has been submitted to Records Management, Document Number 70108698.

CO-PREPARER: Kevin King Date: See SAP

INDEPENDENT REVIEWER: Michael Crawford Date: See SAP

APPROVED: Alan Johnson Date: See SAP

ATTACHMENT 3

S-TQDI-2010-0004

P. 1 of 46

ILTRASONIC THICKNESS EXAMINATION RECORD

Under Ground Aux Feed Water Pipe

NDE Lab	Station	Unit	Outage	Order #	Procedure #	Rev.	Couplant Type	Couplant Batch	Exam Date
MISTRAS	Salem	1	RFO# 20	60084266	OU-AA-335-004	1	SONOTRACE 40	96243	

EXAMINATION AREA					MATERIAL			
Component I.D.	System	Location	Fab. Isometric	Elev.	(Type/Spec)	Dia. Size	Component Type	Surface Temp.
Aux. Feed Water		Yard	N/A	94'	P-1	4"	PIPE	AMBIENT

SEARCH UNIT DESCRIPTION				EQUIPMENT		WALL THICKNESS			Size	X	Y
Brand	Serial #	Size	Frequency	Instr. Brand/type	Serial #	Nominal	.875 Nom.	T min.			
									N/A		
anametric		0.312	5mhz	PANAMETRICS		0.337		0.278			
D 790RL				37 DL / PLUS							

alibration Block # 1 S/N		78897		Calibration Block Temp.	AMBIENT
Actual	Effective	Initial	Final		
0.100	0.100	0.100	0.100	CALIBRATION	TIME
0.200	0.200	0.200	0.200	Initial Calibration	
0.300	0.300	0.300	0.300	Calibration Check	
0.400	0.400	0.400	0.400	Final Calibration Check	
0.500	0.500	0.500	0.500		

alibration Block # 2 S/N				Calibration Block Temp.	
Actual	Effective	Initial	Final		
				Thermometer Serial #	Cal. Due

See pipe sketch for location of readings.

		File Name	Min. Thickness	Max. Thickness
IMITATIONS:	Readings taken through rough surface.	N/A		
	Thickness readings taken at intersections of 1" grid.			
COMMENTS:	Grinding was done to clean surface of AF13T rows 47 to 69.			

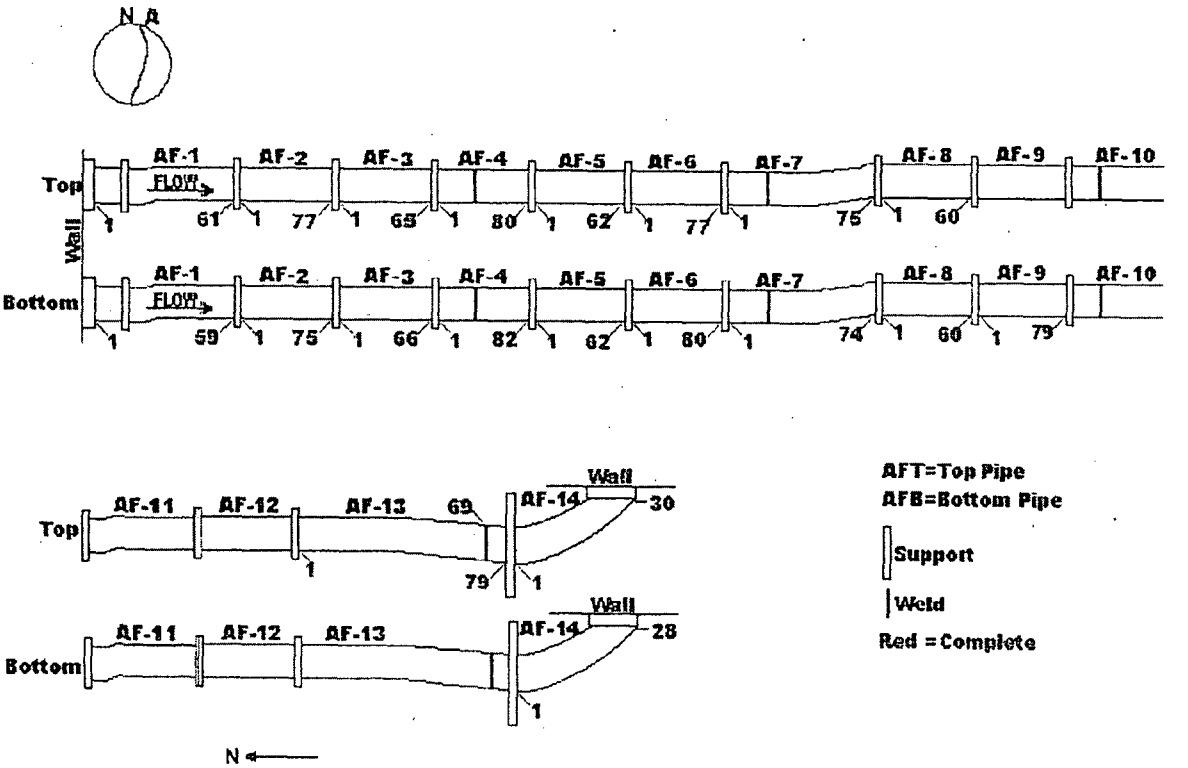
Notified: B. Montgomery

Attachment x Yes No

PSE&G Review: Adam Burke

Date: 4/15/10

SNT-TC-1A LEVEL II


N
Top
Wall
Bottom
FLOW
AF-1
AF-2
AF-3
AF-4
AF-5
AF-6
AF-7
AF-8
AF-9
AF-10
1
61
77
65
80
62
77
75
60
59
75
66
82
62
80
74
60
79
AF-11
AF-12
AF-13
AF-14
69
79
30
28
AFT=Top Pipe
AFB=Bottom Pipe
Support
Weld
Red = Complete

2 of 46

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF1T Lowest Reading 0.264 Highest reading 0.344

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.271	0.278	0.298	0.273	0.273	0.280	0.323	0.304	0.287	0.302	0.301	0.334	0.275	0.313
2	0.271	0.280	0.333	0.301	0.266	0.284	0.322	0.291	0.309	0.298	0.291	0.306	0.319	0.299
3	0.270	0.314	0.333	0.271	0.268	0.302	0.322	0.333	0.305	0.283	0.288	0.331	0.301	0.298
4	0.311	0.288	0.288	0.297	0.268	0.265	0.276	0.307	0.301	0.284	0.292	0.284	0.308	0.333
5	0.334	0.290	0.306	0.303	0.287	0.296	0.306	0.290	0.301	0.293	0.290	0.291	0.308	0.304
6	0.334	0.285	0.289	0.306	0.270	0.297	0.292	0.301	0.303	0.281	0.288	0.291	0.300	0.303
7	0.324	0.297	0.282	0.291	0.278	0.298	0.313	0.304	0.296	0.299	0.300	0.292	0.312	0.301
8	0.296	0.298	0.293	0.290	0.275	0.298	0.318	0.302	0.287	0.291	0.292	0.290	0.291	0.298
9	0.297	0.274	0.276	0.301	0.268	0.302	0.335	0.290	0.285	0.291	0.294	0.299	0.298	0.298
10	0.319	0.277	0.280	0.329	0.287	0.295	0.335	0.319	0.311	0.306	0.297	0.309	0.332	0.285
11	0.320	0.277	0.295	0.329	0.295	0.290	0.321	0.292	0.299	0.315	0.305	0.291	0.334	0.333
12	0.320	0.278	0.295	0.328	0.284	0.273	0.326	0.293	0.289	0.286	0.296	0.298	0.309	0.305
13	0.319	0.328	0.295	0.298	0.291	0.281	0.323	0.325	0.291	0.287	0.294	0.298	0.290	0.285
14	0.324	0.306	0.297	0.297	0.300	0.282	0.326	0.302	0.297	0.309	0.296	0.290	0.309	0.304
15	0.289	0.338	0.298	0.297	0.280	0.291	0.325	0.325	0.297	0.285	0.299	0.294	0.302	0.309
16	0.285	0.322	0.298	0.271	0.286	0.282	0.288	0.286	0.290	0.286	0.297	0.289	0.290	0.328
17	0.285	0.322	0.287	0.298	0.308	0.302	0.286	0.301	0.290	0.290	0.299	0.296	0.314	0.302
18	0.279	0.315	0.265	0.302	0.327	0.290	0.293	0.302	0.291	0.301	0.305	0.278	0.315	0.298
19	0.296	0.287	0.282	0.297	0.326	0.286	0.296	0.302	0.290	0.302	0.289	0.299	0.302	0.304
20	0.295	0.288	0.290	0.302	0.289	0.279	0.328	0.289	0.304	0.285	0.294	0.336	0.304	0.273
21	0.265	0.296	0.272	0.291	0.314	0.282	0.295	0.291	0.316	0.289	0.281	0.306	0.283	0.273
22	0.337	0.286	0.301	0.299	0.289	0.281	0.293	0.291	0.316	0.282	0.274	0.304	0.309	0.295
23	0.338	0.291	0.275	0.294	0.286	0.281	0.325	0.315	0.298	0.295	0.290	0.265	0.286	0.291
24	0.313	0.275	0.302	0.312	0.285	0.281	0.325	0.315	0.294	0.280	0.291	0.298	0.338	0.295
25	0.335	0.307	0.301	0.324	0.287	0.277	0.294	0.316	0.322	0.293	0.280	0.289	0.321	0.271
26	0.306	0.304	0.305	0.329	0.286	0.280	0.295	0.316	0.323	0.304	0.282	0.298	0.322	0.271
27	0.329	0.302	0.304	0.327	0.296	0.300	0.295	0.339	0.299	0.298	0.280	0.297	0.299	0.301
28	0.301	0.301	0.273	0.332	0.298	0.306	0.296	0.302	0.299	0.301	0.292	0.279	0.321	0.302
29	0.296	0.301	0.317	0.338	0.291	0.286	0.296	0.329	0.319	0.315	0.292	0.302	0.304	0.298
30	0.270	0.284	0.278	0.298	0.296	0.269	0.299	0.341	0.316	0.325	0.290	0.298	0.308	0.298
31	0.282	0.313	0.264	0.278	0.302	0.293	0.298	0.312	0.319	0.321	0.302	0.299	0.332	0.270
32	0.298	0.281	0.280	0.280	0.309	0.290	0.331	0.311	0.320	0.303	0.300	0.316	0.279	0.282
33	0.299	0.281	0.278	0.280	0.310	0.286	0.330	0.310	0.316	0.305	0.301	0.312	0.309	0.270
34	0.305	0.312	0.278	0.283	0.312	0.278	0.331	0.309	0.317	0.302	0.296	0.302	0.307	0.286
35	0.299	0.282	0.291	0.282	0.276	0.278	0.331	0.302	0.289	0.295	0.294	0.311	0.306	0.308
36	0.293	0.310	0.297	0.280	0.299	0.311	0.296	0.329	0.292	0.294	0.272	0.286	0.306	0.286
37	0.291	0.278	0.295	0.281	0.296	0.310	0.294	0.327	0.287	0.295	0.293	0.283	0.294	0.334
38	0.303	0.278	0.295	0.281	0.321	0.311	0.295	0.292	0.291	0.299	0.299	0.300	0.281	0.290
39	0.280	0.276	0.286	0.277	0.296	0.313	0.295	0.291	0.292	0.305	0.291	0.273	0.281	0.283
40	0.267	0.278	0.282	0.274	0.296	0.291	0.295	0.293	0.291	0.278	0.299	0.273	0.283	0.286
41	0.294	0.282	0.327	0.278	0.285	0.291	0.295	0.293	0.291	0.299	0.299	0.291	0.291	0.293
42	0.306	0.284	0.296	0.281	0.289	0.322	0.292	0.291	0.304	0.290	0.291	0.281	0.314	0.283
43	0.293	0.284	0.305	0.281	0.294	0.299	0.293	0.291	0.305	0.291	0.294	0.291	0.328	0.291
44	0.293	0.290	0.290	0.283	0.296	0.298	0.291	0.293	0.303	0.294	0.336	0.288	0.319	0.298
45	0.285	0.317	0.296	0.284	0.299	0.308	0.291	0.294	0.316	0.291	0.337	0.289	0.318	0.289
46	0.283	0.315	0.272	0.287	0.298	0.332	0.282	0.296	0.320	0.291	0.289	0.292	0.297	0.297
47	0.283	0.288	0.326	0.313	0.286	0.329	0.292	0.297	0.317	0.292	0.287	0.289	0.321	0.269
48	0.306	0.279	0.315	0.283	0.289	0.331	0.283	0.297	0.304	0.292	0.286	0.291	0.323	0.282
49	0.307	0.313	0.292	0.298	0.304	0.303	0.294	0.289	0.295	0.298	0.286	0.297	0.320	0.297
50	0.291	0.276	0.289	0.282	0.305	0.330	0.293	0.285	0.316	0.291	0.286	0.280	0.318	0.295
51	0.297	0.275	0.297	0.280	0.302	0.331	0.299	0.288	0.332	0.290	0.297	0.292	0.314	0.298
52	0.292	0.276	0.296	0.279	0.291	0.322	0.295	0.287	0.344	0.295	0.293	0.289	0.274	0.293
53	0.290	0.278	0.271	0.278	0.288	0.323	0.293	0.288	0.343	0.300	0.294	0.288	0.314	0.295
54	0.289	0.279	0.300	0.278	0.286	0.328	0.286	0.289	0.288	0.298	0.293	0.299	0.315	0.285
55	0.289	0.295	0.271	0.277	0.289	0.323	0.287	0.298	0.313	0.300	0.291	0.293	0.314	0.291
56	0.286	0.297	0.274	0.277	0.297	0.298	0.290	0.291	0.312	0.301	0.293	0.293	0.317	0.299
57	0.294	0.296	0.279	0.286	0.296	0.323	0.293	0.305	0.311	0.271	0.283	0.308	0.318	0.294
58	0.293	0.336	0.279	0.290	0.287	0.298	0.290	0.326	0.298	0.271	0.282	0.310	0.316	0.291
59	0.295	0.294	0.277	0.289	0.289	0.299	0.291	0.294	0.298	0.301	0.283	0.320	0.314	0.291
60	0.295	0.312	0.279	0.294	0.287	0.321	0.291	0.287	0.299	0.301	0.283	0.310	0.314	0.298
61	0.295	0.315	0.298	0.279	0.298	0.321	0.291	0.287	0.299	0.300	0.280	0.280	0.311	0.297

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF1B Lowest Reading 0.272 Highest reading 0.356

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.289	0.330	0.299	0.305	0.292	0.322	0.292	0.321	0.342	0.317	0.294	0.327	0.330	0.322
2	0.289	0.311	0.315	0.303	0.288	0.296	0.300	0.349	0.341	0.298	0.279	0.328	0.329	0.341
3	0.290	0.334	0.313	0.303	0.293	0.291	0.281	0.350	0.315	0.297	0.312	0.330	0.334	0.336
4	0.288	0.305	0.298	0.279	0.330	0.288	0.335	0.317	0.306	0.297	0.312	0.294	0.294	0.296
5	0.289	0.289	0.291	0.303	0.316	0.325	0.329	0.317	0.332	0.294	0.322	0.319	0.293	0.312
6	0.277	0.298	0.294	0.289	0.313	0.320	0.355	0.326	0.331	0.330	0.326	0.293	0.305	0.299
7	0.278	0.284	0.304	0.279	0.305	0.291	0.324	0.323	0.329	0.300	0.278	0.304	0.326	0.304
8	0.319	0.280	0.299	0.314	0.296	0.317	0.281	0.297	0.295	0.302	0.285	0.325	0.325	0.295
9	0.351	0.282	0.300	0.289	0.303	0.291	0.292	0.296	0.333	0.301	0.340	0.326	0.329	0.295
10	0.306	0.316	0.265	0.297	0.309	0.283	0.291	0.330	0.330	0.293	0.320	0.302	0.332	0.318
11	0.315	0.317	0.296	0.294	0.308	0.309	0.341	0.306	0.331	0.303	0.340	0.329	0.339	0.332
12	0.316	0.317	0.274	0.301	0.289	0.282	0.339	0.311	0.332	0.303	0.333	0.330	0.333	0.329
13	0.292	0.291	0.284	0.303	0.309	0.282	0.322	0.283	0.343	0.301	0.331	0.333	0.332	0.337
14	0.315	0.311	0.291	0.275	0.291	0.299	0.327	0.283	0.325	0.301	0.331	0.335	0.332	0.337
15	0.318	0.308	0.314	0.293	0.285	0.301	0.327	0.283	0.292	0.305	0.349	0.335	0.294	0.296
16	0.318	0.306	0.342	0.298	0.283	0.302	0.329	0.310	0.332	0.305	0.349	0.334	0.341	0.307
17	0.318	0.306	0.314	0.328	0.277	0.269	0.333	0.310	0.338	0.331	0.305	0.334	0.338	0.307
18	0.317	0.305	0.313	0.356	0.301	0.299	0.333	0.282	0.330	0.334	0.306	0.351	0.348	0.307
19	0.317	0.305	0.293	0.355	0.302	0.301	0.350	0.305	0.330	0.350	0.330	0.348	0.347	0.306
20	0.277	0.291	0.340	0.307	0.316	0.304	0.340	0.326	0.313	0.350	0.334	0.349	0.346	0.305
21	0.309	0.290	0.305	0.309	0.318	0.294	0.331	0.325	0.310	0.336	0.332	0.351	0.342	0.305
22	0.314	0.296	0.287	0.305	0.318	0.305	0.321	0.328	0.309	0.356	0.330	0.344	0.340	0.307
23	0.307	0.306	0.315	0.305	0.319	0.285	0.331	0.315	0.332	0.351	0.331	0.336	0.339	0.307
24	0.300	0.291	0.319	0.299	0.290	0.317	0.292	0.312	0.332	0.331	0.332	0.338	0.339	0.318
25	0.300	0.299	0.319	0.335	0.292	0.297	0.333	0.325	0.332	0.329	0.330	0.323	0.340	0.327
26	0.300	0.297	0.298	0.292	0.296	0.297	0.329	0.328	0.334	0.336	0.322	0.347	0.340	0.296
27	0.346	0.299	0.322	0.333	0.315	0.297	0.293	0.314	0.293	0.339	0.345	0.340	0.336	0.332
28	0.290	0.296	0.323	0.325	0.306	0.297	0.294	0.293	0.323	0.336	0.329	0.340	0.337	0.295
29	0.288	0.303	0.305	0.296	0.301	0.302	0.292	0.301	0.322	0.342	0.343	0.346	0.335	0.311
30	0.327	0.310	0.302	0.290	0.301	0.301	0.313	0.295	0.299	0.345	0.325	0.335	0.335	0.311
31	0.310	0.311	0.299	0.285	0.301	0.301	0.341	0.304	0.334	0.319	0.307	0.325	0.335	0.312
32	0.312	0.339	0.302	0.299	0.303	0.296	0.307	0.304	0.318	0.318	0.303	0.319	0.344	0.294
33	0.332	0.305	0.299	0.341	0.305	0.294	0.293	0.305	0.324	0.342	0.303	0.305	0.347	0.278
34	0.313	0.331	0.295	0.291	0.292	0.298	0.308	0.304	0.322	0.327	0.285	0.340	0.327	0.290
35	0.280	0.331	0.337	0.299	0.309	0.294	0.309	0.301	0.324	0.327	0.334	0.299	0.317	0.281
36	0.288	0.337	0.303	0.305	0.310	0.295	0.334	0.298	0.324	0.320	0.305	0.302	0.317	0.281
37	0.273	0.337	0.301	0.308	0.308	0.299	0.292	0.292	0.326	0.319	0.306	0.301	0.330	0.281
38	0.312	0.305	0.302	0.292	0.308	0.296	0.329	0.282	0.326	0.319	0.324	0.308	0.317	0.282
39	0.309	0.307	0.302	0.331	0.307	0.296	0.299	0.283	0.325	0.322	0.326	0.308	0.317	0.282
40	0.293	0.289	0.301	0.323	0.307	0.294	0.319	0.284	0.331	0.322	0.339	0.307	0.313	0.280
41	0.286	0.302	0.301	0.324	0.313	0.290	0.319	0.282	0.333	0.327	0.330	0.310	0.294	0.274
42	0.284	0.317	0.307	0.322	0.312	0.288	0.317	0.324	0.336	0.324	0.327	0.314	0.311	0.272
43	0.296	0.309	0.300	0.299	0.310	0.287	0.320	0.325	0.324	0.334	0.329	0.314	0.309	0.298
44	0.291	0.302	0.300	0.299	0.314	0.287	0.315	0.303	0.322	0.339	0.326	0.313	0.313	0.298
45	0.300	0.309	0.301	0.321	0.315	0.287	0.344	0.306	0.319	0.329	0.315	0.318	0.313	0.317
46	0.302	0.331	0.303	0.325	0.297	0.280	0.342	0.339	0.316	0.344	0.319	0.317	0.314	0.318
47	0.298	0.331	0.308	0.307	0.308	0.283	0.346	0.338	0.320	0.290	0.354	0.298	0.315	0.316
48	0.296	0.330	0.312	0.326	0.282	0.304	0.344	0.338	0.333	0.290	0.335	0.328	0.312	0.316
49	0.290	0.332	0.311	0.294	0.286	0.341	0.328	0.345	0.335	0.294	0.338	0.317	0.313	0.317
50	0.290	0.306	0.312	0.296	0.310	0.340	0.327	0.335	0.332	0.332	0.337	0.320	0.314	0.302
51	0.290	0.300	0.311	0.309	0.311	0.346	0.325	0.332	0.331	0.292	0.336	0.319	0.315	0.306
52	0.290	0.299	0.308	0.288	0.310	0.317	0.326	0.299	0.332	0.308	0.334	0.320	0.326	0.305
53	0.290	0.300	0.306	0.289	0.285	0.273	0.326	0.335	0.331	0.332	0.308	0.324	0.327	0.307
54	0.302	0.299	0.298	0.290	0.309	0.283	0.323	0.342	0.329	0.298	0.353	0.295	0.297	0.310
55	0.309	0.300	0.297	0.289	0.285	0.309	0.323	0.343	0.331	0.342	0.338	0.324	0.328	0.291
56	0.309	0.305	0.297	0.290	0.285	0.287	0.322	0.340	0.292	0.342	0.335	0.325	0.326	0.307
57	0.285	0.304	0.300	0.289	0.276	0.308	0.322	0.331	0.322	0.336	0.333	0.325	0.326	0.305
58	0.283	0.303	0.297	0.289	0.281	0.333	0.320	0.339	0.322	0.336	0.330	0.326	0.328	0.300
59	0.284	0.302	0.297	0.292	0.277	0.294	0.323	0.320	0.319	0.336	0.328	0.329	0.327	0.312

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF2T Lowest Reading 0.265 Highest reading 0.351

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.306	0.284	0.268	0.325	0.305	0.316	0.297	0.278	0.315	0.286	0.283	0.317	0.315	0.280
2	0.306	0.274	0.304	0.303	0.308	0.317	0.291	0.295	0.312	0.288	0.284	0.299	0.301	0.293
3	0.282	0.284	0.315	0.304	0.300	0.302	0.299	0.295	0.290	0.289	0.285	0.275	0.305	0.283
4	0.322	0.299	0.315	0.306	0.304	0.316	0.292	0.318	0.302	0.290	0.285	0.303	0.297	0.311
5	0.322	0.309	0.316	0.305	0.290	0.316	0.291	0.285	0.302	0.290	0.298	0.303	0.297	0.298
6	0.297	0.301	0.316	0.283	0.309	0.322	0.296	0.291	0.306	0.287	0.276	0.301	0.292	0.294
7	0.294	0.305	0.307	0.264	0.309	0.302	0.297	0.295	0.283	0.290	0.276	0.298	0.292	0.311
8	0.294	0.292	0.331	0.301	0.305	0.317	0.326	0.295	0.304	0.321	0.298	0.299	0.292	0.304
9	0.276	0.300	0.293	0.275	0.292	0.317	0.290	0.290	0.290	0.290	0.317	0.299	0.292	0.307
10	0.275	0.304	0.302	0.275	0.285	0.317	0.290	0.266	0.294	0.290	0.305	0.271	0.291	0.304
11	0.298	0.269	0.303	0.305	0.299	0.313	0.284	0.298	0.294	0.295	0.322	0.268	0.293	0.304
12	0.311	0.299	0.304	0.283	0.302	0.319	0.281	0.297	0.299	0.307	0.285	0.305	0.291	0.319
13	0.312	0.298	0.302	0.283	0.305	0.290	0.284	0.299	0.295	0.303	0.297	0.294	0.328	0.319
14	0.311	0.319	0.329	0.301	0.305	0.290	0.283	0.314	0.292	0.298	0.291	0.332	0.304	0.275
15	0.313	0.286	0.335	0.295	0.305	0.290	0.291	0.293	0.294	0.269	0.293	0.333	0.305	0.306
16	0.306	0.286	0.333	0.292	0.298	0.288	0.295	0.298	0.293	0.296	0.291	0.333	0.311	0.314
17	0.330	0.289	0.332	0.291	0.305	0.287	0.293	0.309	0.298	0.293	0.302	0.292	0.289	0.298
18	0.312	0.300	0.324	0.294	0.291	0.289	0.299	0.291	0.282	0.296	0.301	0.292	0.288	0.277
19	0.311	0.305	0.324	0.285	0.291	0.288	0.301	0.298	0.281	0.298	0.297	0.301	0.310	0.265
20	0.313	0.301	0.308	0.298	0.280	0.288	0.299	0.279	0.308	0.317	0.291	0.298	0.318	0.349
21	0.311	0.313	0.345	0.291	0.290	0.287	0.299	0.305	0.299	0.319	0.330	0.299	0.318	0.322
22	0.312	0.314	0.274	0.291	0.291	0.288	0.296	0.298	0.298	0.317	0.305	0.315	0.319	0.294
23	0.325	0.313	0.286	0.296	0.296	0.287	0.297	0.265	0.297	0.281	0.284	0.318	0.299	0.301
24	0.303	0.312	0.285	0.291	0.274	0.286	0.298	0.267	0.319	0.269	0.315	0.308	0.294	0.296
25	0.304	0.322	0.286	0.292	0.274	0.287	0.299	0.267	0.318	0.299	0.306	0.294	0.292	0.324
26	0.313	0.323	0.285	0.292	0.272	0.291	0.301	0.301	0.297	0.305	0.305	0.329	0.292	0.324
27	0.325	0.292	0.285	0.304	0.272	0.290	0.288	0.302	0.288	0.299	0.326	0.320	0.289	0.295
28	0.315	0.286	0.276	0.299	0.298	0.294	0.321	0.313	0.287	0.277	0.316	0.319	0.308	0.340
29	0.311	0.283	0.275	0.305	0.290	0.290	0.298	0.301	0.293	0.304	0.318	0.311	0.307	0.310
30	0.315	0.298	0.313	0.327	0.304	0.305	0.294	0.301	0.306	0.268	0.289	0.293	0.283	0.333
31	0.315	0.300	0.298	0.280	0.291	0.301	0.296	0.298	0.301	0.299	0.290	0.290	0.291	0.310
32	0.317	0.299	0.275	0.279	0.291	0.299	0.292	0.325	0.316	0.337	0.289	0.309	0.296	0.312
33	0.317	0.299	0.292	0.280	0.292	0.293	0.291	0.331	0.299	0.308	0.345	0.322	0.296	0.290
34	0.300	0.304	0.289	0.279	0.288	0.297	0.298	0.298	0.287	0.308	0.344	0.338	0.293	0.293
35	0.298	0.310	0.298	0.309	0.289	0.298	0.286	0.308	0.287	0.301	0.299	0.337	0.292	0.298
36	0.299	0.314	0.321	0.282	0.288	0.278	0.283	0.292	0.288	0.293	0.344	0.339	0.318	0.318
37	0.299	0.326	0.295	0.292	0.288	0.276	0.285	0.298	0.285	0.311	0.301	0.301	0.318	0.300
38	0.302	0.327	0.307	0.272	0.294	0.291	0.282	0.273	0.285	0.306	0.347	0.301	0.327	0.297
39	0.298	0.318	0.306	0.272	0.272	0.285	0.284	0.318	0.287	0.339	0.350	0.301	0.289	0.295
40	0.299	0.320	0.310	0.305	0.292	0.287	0.284	0.317	0.287	0.276	0.308	0.292	0.339	0.292
41	0.320	0.318	0.299	0.299	0.293	0.288	0.315	0.314	0.289	0.278	0.308	0.295	0.326	0.293
42	0.319	0.318	0.275	0.296	0.297	0.289	0.318	0.297	0.291	0.279	0.280	0.302	0.295	0.308
43	0.302	0.312	0.277	0.332	0.287	0.290	0.314	0.296	0.290	0.298	0.310	0.303	0.295	0.291
44	0.285	0.302	0.274	0.289	0.269	0.313	0.314	0.338	0.298	0.291	0.311	0.278	0.296	0.308
45	0.347	0.314	0.286	0.298	0.312	0.290	0.290	0.301	0.320	0.322	0.329	0.275	0.290	0.330
46	0.287	0.312	0.278	0.291	0.289	0.290	0.290	0.299	0.320	0.325	0.295	0.269	0.290	0.312
47	0.286	0.310	0.280	0.290	0.290	0.290	0.268	0.291	0.315	0.293	0.296	0.271	0.284	0.315
48	0.286	0.307	0.298	0.290	0.294	0.290	0.269	0.299	0.314	0.268	0.291	0.271	0.288	0.312
49	0.322	0.308	0.331	0.294	0.302	0.290	0.310	0.318	0.307	0.322	0.291	0.309	0.290	0.312
50	0.313	0.313	0.331	0.307	0.300	0.290	0.309	0.287	0.308	0.296	0.338	0.311	0.297	0.312
51	0.304	0.307	0.293	0.279	0.300	0.281	0.269	0.320	0.306	0.299	0.305	0.320	0.290	0.351
52	0.316	0.335	0.293	0.279	0.300	0.280	0.300	0.293	0.306	0.299	0.276	0.313	0.298	0.303
53	0.335	0.303	0.299	0.279	0.301	0.291	0.300	0.298	0.307	0.298	0.277	0.305	0.267	0.295
54	0.303	0.333	0.302	0.280	0.305	0.291	0.298	0.292	0.307	0.288	0.275	0.293	0.314	0.290
55	0.300	0.307	0.300	0.273	0.298	0.331	0.302	0.297	0.308	0.311	0.268	0.291	0.290	0.305
56	0.300	0.308	0.300	0.274	0.301	0.314	0.299	0.297	0.307	0.291	0.292	0.279	0.300	0.311
57	0.287	0.296	0.298	0.276	0.341	0.284	0.267	0.297	0.307	0.294	0.292	0.280	0.325	0.327
58	0.308	0.331	0.297	0.275	0.295	0.285	0.267	0.298	0.307	0.318	0.312	0.299	0.330	0.306
59	0.308	0.296	0.295	0.296	0.298	0.289	0.267	0.298	0.307	0.335	0.325	0.297	0.303	0.304
60	0.286	0.335	0.295	0.312	0.298	0.290	0.268	0.301	0.306	0.280	0.329	0.294	0.331	0.303
61	0.285	0.332	0.297	0.287	0.288	0.290	0.268	0.308	0.329	0.304	0.298	0.320	0.296	0.303
62	0.351	0.332	0.295	0.286	0.287	0.291	0.265	0.290	0.328	0.290	0.342	0.319	0.332	0.303
63	0.296	0.332	0.295	0.293	0.294	0.298	0.268	0.300	0.328	0.287	0.316	0.317	0.306	0.299
64	0.318	0.332	0.295	0.293	0.314	0.289	0.272	0.296	0.330	0.339	0.298	0.301	0.309	0.296
65	0.318	0.334	0.289	0.280	0.291	0.289	0.290	0.292	0.331	0.296	0.278	0.332	0.302	0.298
66	0.329	0.335	0.290	0.280	0.299	0.270	0.288	0.306	0.332	0.314	0.280	0.318	0.327	0.303
67	0.328	0.326	0.290	0.292	0.298	0.290	0.288	0.327	0.336	0.295	0.280	0.320	0.324	0.307

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF2T Lowest Reading 0.265 Highest reading 0.351

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.325	0.325	0.291	0.286	0.298	0.272	0.287	0.327	0.304	0.277	0.280	0.320	0.327	0.309
69	0.328	0.326	0.290	0.278	0.298	0.272	0.290	0.327	0.310	0.307	0.282	0.318	0.332	0.308
70	0.327	0.327	0.290	0.278	0.292	0.291	0.290	0.304	0.328	0.306	0.320	0.317	0.334	0.306
71	0.328	0.327	0.288	0.290	0.291	0.269	0.317	0.294	0.345	0.303	0.320	0.317	0.331	0.303
72	0.326	0.327	0.290	0.289	0.292	0.270	0.316	0.294	0.296	0.279	0.319	0.314	0.318	0.303
73	0.326	0.326	0.290	0.275	0.293	0.269	0.314	0.294	0.327	0.280	0.319	0.314	0.325	0.302
74	0.326	0.327	0.291	0.275	0.298	0.269	0.284	0.295	0.297	0.289	0.318	0.316	0.349	0.310
75	0.327	0.326	0.290	0.273	0.320	0.289	0.279	0.296	0.291	0.283	0.317	0.318	0.346	0.307
76	0.327	0.326	0.297	0.271	0.320	0.270	0.278	0.269	0.292	0.303	0.317	0.316	0.348	0.308
77	0.328	0.326	0.297	0.267	0.320	0.289	0.279	0.296	0.292	0.298	0.317	0.316	0.348	0.305

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF2B Lowest Reading 0.280 Highest reading 0.371

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.280	0.327	0.295	0.314	0.341	0.291	0.304	0.352	0.321	0.355	0.321	0.333	0.339	0.336
2	0.298	0.311	0.296	0.305	0.359	0.282	0.323	0.345	0.340	0.346	0.354	0.323	0.341	0.336
3	0.305	0.294	0.283	0.301	0.363	0.363	0.262	0.333	0.336	0.340	0.336	0.357	0.335	0.325
4	0.321	0.310	0.265	0.321	0.315	0.302	0.333	0.330	0.334	0.332	0.339	0.332	0.330	0.327
5	0.325	0.320	0.357	0.331	0.324	0.305	0.325	0.352	0.338	0.320	0.333	0.330	0.319	0.326
6	0.325	0.345	0.357	0.335	0.320	0.302	0.324	0.355	0.336	0.318	0.332	0.334	0.329	0.330
7	0.322	0.328	0.338	0.333	0.328	0.311	0.322	0.339	0.294	0.324	0.339	0.333	0.329	0.357
8	0.320	0.338	0.334	0.348	0.330	0.355	0.304	0.351	0.292	0.321	0.322	0.331	0.318	0.325
9	0.320	0.360	0.328	0.347	0.324	0.355	0.303	0.335	0.354	0.320	0.344	0.330	0.329	0.316
10	0.327	0.337	0.328	0.348	0.328	0.316	0.295	0.360	0.365	0.343	0.356	0.330	0.318	0.317
11	0.331	0.328	0.330	0.347	0.311	0.327	0.296	0.360	0.338	0.313	0.334	0.340	0.332	0.316
12	0.328	0.318	0.328	0.304	0.318	0.316	0.337	0.356	0.337	0.312	0.326	0.330	0.340	0.322
13	0.317	0.316	0.328	0.330	0.351	0.326	0.365	0.349	0.334	0.325	0.326	0.333	0.335	0.327
14	0.300	0.351	0.352	0.325	0.320	0.323	0.340	0.308	0.334	0.336	0.339	0.304	0.335	0.341
15	0.290	0.332	0.329	0.349	0.324	0.324	0.340	0.316	0.334	0.336	0.329	0.355	0.337	0.339
16	0.322	0.339	0.334	0.349	0.321	0.315	0.311	0.315	0.313	0.339	0.346	0.310	0.338	0.345
17	0.304	0.334	0.333	0.365	0.319	0.322	0.302	0.323	0.313	0.341	0.344	0.311	0.339	0.341
18	0.319	0.342	0.332	0.326	0.321	0.324	0.307	0.322	0.319	0.338	0.332	0.331	0.351	0.353
19	0.315	0.326	0.331	0.322	0.318	0.323	0.309	0.316	0.321	0.341	0.360	0.331	0.325	0.348
20	0.308	0.329	0.354	0.328	0.319	0.320	0.311	0.326	0.345	0.342	0.308	0.332	0.306	0.342
21	0.314	0.342	0.348	0.315	0.310	0.319	0.370	0.313	0.340	0.344	0.306	0.333	0.360	0.360
22	0.311	0.327	0.339	0.315	0.363	0.320	0.350	0.318	0.302	0.337	0.345	0.332	0.317	0.338
23	0.306	0.335	0.336	0.297	0.348	0.322	0.298	0.290	0.300	0.340	0.289	0.334	0.323	0.339
24	0.302	0.342	0.301	0.295	0.337	0.307	0.294	0.336	0.353	0.345	0.306	0.335	0.323	0.339
25	0.302	0.314	0.336	0.330	0.331	0.306	0.297	0.335	0.346	0.341	0.305	0.332	0.350	0.346
26	0.333	0.318	0.339	0.296	0.335	0.323	0.286	0.335	0.345	0.325	0.335	0.329	0.316	0.338
27	0.343	0.324	0.308	0.368	0.327	0.323	0.360	0.331	0.345	0.359	0.328	0.321	0.316	0.331
28	0.318	0.292	0.302	0.317	0.333	0.324	0.362	0.331	0.339	0.342	0.348	0.333	0.340	0.323
29	0.357	0.336	0.300	0.313	0.320	0.292	0.314	0.318	0.337	0.336	0.330	0.322	0.337	0.338
30	0.306	0.343	0.325	0.342	0.334	0.316	0.293	0.318	0.351	0.365	0.332	0.354	0.354	0.338
31	0.307	0.325	0.359	0.333	0.336	0.329	0.352	0.353	0.351	0.345	0.354	0.352	0.355	0.331
32	0.313	0.324	0.297	0.331	0.331	0.320	0.343	0.315	0.317	0.334	0.350	0.352	0.343	0.337
33	0.322	0.364	0.299	0.333	0.328	0.331	0.326	0.323	0.318	0.330	0.350	0.356	0.340	0.342
34	0.298	0.370	0.370	0.321	0.339	0.333	0.323	0.319	0.319	0.328	0.350	0.352	0.341	0.334
35	0.320	0.304	0.305	0.305	0.289	0.309	0.291	0.317	0.323	0.325	0.340	0.340	0.341	0.325
36	0.328	0.338	0.311	0.329	0.331	0.355	0.286	0.315	0.325	0.327	0.339	0.338	0.347	0.318
37	0.321	0.333	0.311	0.321	0.335	0.359	0.292	0.317	0.326	0.327	0.353	0.333	0.338	0.319
38	0.331	0.303	0.316	0.322	0.360	0.353	0.326	0.320	0.322	0.324	0.331	0.329	0.348	0.330
39	0.348	0.330	0.317	0.282	0.351	0.313	0.319	0.320	0.323	0.350	0.334	0.346	0.349	0.332
40	0.336	0.303	0.298	0.285	0.333	0.307	0.353	0.323	0.323	0.349	0.343	0.342	0.335	0.336
41	0.330	0.348	0.284	0.338	0.357	0.306	0.345	0.322	0.321	0.350	0.345	0.334	0.336	0.335
42	0.305	0.351	0.297	0.337	0.324	0.310	0.340	0.335	0.321	0.347	0.332	0.337	0.341	0.333
43	0.302	0.314	0.320	0.333	0.326	0.308	0.333	0.351	0.342	0.345	0.324	0.351	0.330	0.339
44	0.322	0.363	0.313	0.300	0.317	0.309	0.332	0.329	0.364	0.366	0.332	0.342	0.329	0.344
45	0.315	0.304	0.311	0.350	0.322	0.341	0.330	0.336	0.354	0.363	0.345	0.335	0.331	0.354
46	0.319	0.304	0.312	0.332	0.322	0.322	0.330	0.343	0.343	0.365	0.345	0.351	0.345	0.331
47	0.309	0.295	0.311	0.332	0.324	0.343	0.331	0.333	0.342	0.371	0.329	0.355	0.336	0.326
48	0.297	0.342	0.331	0.357	0.365	0.365	0.331	0.329	0.342	0.334	0.330	0.340	0.335	0.335
49	0.292	0.310	0.331	0.314	0.341	0.365	0.333	0.367	0.338	0.331	0.325	0.337	0.356	0.319
50	0.296	0.314	0.331	0.347	0.298	0.301	0.333	0.337	0.331	0.342	0.325	0.332	0.322	0.339
51	0.356	0.313	0.330	0.310	0.348	0.301	0.323	0.295	0.349	0.342	0.325	0.356	0.324	0.340
52	0.341	0.351	0.331	0.306	0.348	0.303	0.321	0.321	0.364	0.337	0.318	0.321	0.324	0.345
53	0.296	0.352	0.328	0.292	0.349	0.308	0.325	0.320	0.334	0.334	0.321	0.340	0.320	0.347
54	0.321	0.301	0.330	0.292	0.365	0.313	0.326	0.319	0.335	0.355	0.323	0.339	0.337	0.350
55	0.290	0.301	0.315	0.349	0.362	0.315	0.323	0.319	0.333	0.336	0.325	0.342	0.336	0.344
56	0.319	0.296	0.318	0.349	0.332	0.320	0.334	0.324	0.337	0.335	0.322	0.340	0.335	0.342
57	0.330	0.334	0.289	0.347	0.301	0.322	0.318	0.320	0.332	0.336	0.322	0.342	0.335	0.347
58	0.309	0.288	0.315	0.308	0.354	0.321	0.316	0.319	0.332	0.347	0.356	0.339	0.329	0.361
59	0.342	0.283	0.314	0.308	0.330	0.330	0.317	0.321	0.333	0.346	0.317	0.330	0.336	0.360
60	0.314	0.282	0.332	0.338	0.352	0.332	0.317	0.353	0.338	0.330	0.324	0.325	0.327	0.348
61	0.313	0.283	0.327	0.337	0.295	0.322	0.324	0.327	0.367	0.361	0.320	0.327	0.329	0.348
62	0.293	0.293	0.352	0.298	0.304	0.339	0.325	0.335	0.365	0.343	0.332	0.358	0.364	0.338
63	0.297	0.299	0.362	0.325	0.304	0.327	0.317	0.340	0.315	0.342	0.329	0.354	0.340	0.367
64	0.349	0.328	0.330	0.328	0.304	0.330	0.295	0.336	0.313	0.355	0.317	0.352	0.347	0.359
65	0.297	0.325	0.326	0.317	0.294	0.326	0.298	0.334	0.337	0.355	0.318	0.338	0.342	0.344
66	0.324	0.326	0.328	0.313	0.295	0.321	0.297	0.339	0.336	0.356	0.320	0.337	0.336	0.341
67	0.320	0.328	0.355	0.315	0.315	0.323	0.352	0.309	0.333	0.345	0.335	0.338	0.324	0.345

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF2B Lowest Reading 0.280 Highest reading 0.371

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.331	0.327	0.339	0.326	0.340	0.325	0.356	0.299	0.332	0.345	0.328	0.330	0.334	0.347
69	0.322	0.326	0.301	0.369	0.312	0.295	0.342	0.325	0.335	0.343	0.357	0.334	0.332	0.358
70	0.305	0.317	0.300	0.316	0.333	0.342	0.330	0.327	0.339	0.323	0.334	0.336	0.341	0.355
71	0.314	0.316	0.300	0.315	0.358	0.341	0.331	0.299	0.345	0.321	0.330	0.341	0.334	0.350
72	0.311	0.353	0.301	0.316	0.360	0.336	0.287	0.324	0.352	0.340	0.339	0.332	0.338	0.350
73	0.298	0.319	0.299	0.326	0.336	0.336	0.286	0.319	0.354	0.366	0.338	0.339	0.331	0.345
74	0.305	0.310	0.361	0.321	0.334	0.346	0.298	0.319	0.343	0.336	0.343	0.335	0.334	0.347
75	0.302	0.336	0.312	0.318	0.326	0.334	0.297	0.320	0.349	0.320	0.335	0.333	0.333	0.339

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF3T Lowest Reading 0.267 Highest reading 0.344

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.331	0.298	0.278	0.280	0.271	0.294	0.290	0.332	0.323	0.297	0.306	0.307	0.327	0.298
2	0.338	0.294	0.301	0.272	0.289	0.293	0.301	0.332	0.300	0.325	0.281	0.337	0.306	0.305
3	0.320	0.307	0.322	0.297	0.274	0.291	0.329	0.333	0.299	0.306	0.289	0.291	0.309	0.302
4	0.307	0.300	0.302	0.296	0.279	0.291	0.314	0.332	0.297	0.337	0.302	0.309	0.303	0.306
5	0.308	0.319	0.327	0.287	0.278	0.288	0.306	0.302	0.322	0.308	0.302	0.321	0.274	0.340
6	0.307	0.319	0.322	0.270	0.270	0.288	0.298	0.331	0.297	0.306	0.299	0.306	0.314	0.300
7	0.322	0.317	0.322	0.299	0.291	0.284	0.283	0.308	0.305	0.306	0.299	0.307	0.305	0.324
8	0.326	0.303	0.325	0.315	0.289	0.284	0.299	0.269	0.303	0.319	0.302	0.322	0.292	0.340
9	0.344	0.302	0.318	0.306	0.305	0.287	0.318	0.311	0.328	0.315	0.299	0.306	0.306	0.315
10	0.333	0.302	0.303	0.286	0.281	0.286	0.303	0.307	0.333	0.338	0.299	0.303	0.323	0.319
11	0.328	0.300	0.307	0.283	0.286	0.301	0.311	0.297	0.320	0.313	0.316	0.321	0.320	0.305
12	0.305	0.302	0.306	0.291	0.317	0.301	0.297	0.292	0.289	0.301	0.305	0.312	0.340	0.305
13	0.338	0.297	0.305	0.293	0.317	0.297	0.295	0.292	0.337	0.313	0.323	0.305	0.324	0.307
14	0.305	0.296	0.301	0.286	0.305	0.296	0.302	0.298	0.303	0.303	0.322	0.305	0.322	0.308
15	0.306	0.298	0.309	0.286	0.283	0.296	0.321	0.299	0.305	0.304	0.298	0.306	0.311	0.302
16	0.327	0.296	0.308	0.324	0.325	0.296	0.321	0.301	0.309	0.298	0.309	0.305	0.331	0.299
17	0.324	0.336	0.320	0.320	0.296	0.324	0.297	0.302	0.302	0.298	0.308	0.335	0.305	0.311
18	0.324	0.336	0.309	0.326	0.313	0.326	0.324	0.297	0.323	0.308	0.301	0.320	0.306	0.311
19	0.314	0.336	0.304	0.315	0.311	0.344	0.291	0.302	0.305	0.315	0.295	0.326	0.314	0.313
20	0.315	0.336	0.309	0.317	0.280	0.344	0.286	0.301	0.314	0.291	0.285	0.304	0.302	0.293
21	0.302	0.325	0.316	0.315	0.279	0.327	0.283	0.311	0.314	0.310	0.272	0.305	0.308	0.300
22	0.309	0.334	0.338	0.333	0.283	0.317	0.281	0.280	0.310	0.275	0.333	0.305	0.307	0.293
23	0.324	0.301	0.329	0.332	0.321	0.314	0.283	0.302	0.314	0.315	0.284	0.289	0.315	0.297
24	0.310	0.297	0.334	0.295	0.319	0.314	0.309	0.330	0.337	0.340	0.313	0.283	0.285	0.328
25	0.300	0.296	0.334	0.295	0.319	0.315	0.306	0.325	0.338	0.307	0.305	0.276	0.305	0.307
26	0.304	0.305	0.333	0.332	0.330	0.315	0.333	0.324	0.308	0.291	0.297	0.312	0.286	0.289
27	0.307	0.291	0.332	0.306	0.297	0.302	0.307	0.325	0.313	0.290	0.296	0.299	0.288	0.330
28	0.334	0.294	0.299	0.297	0.305	0.312	0.296	0.328	0.273	0.308	0.295	0.316	0.289	0.297
29	0.320	0.298	0.309	0.309	0.306	0.309	0.313	0.281	0.317	0.339	0.317	0.283	0.290	0.298
30	0.305	0.299	0.310	0.293	0.309	0.306	0.309	0.308	0.317	0.316	0.316	0.334	0.289	0.313
31	0.339	0.327	0.310	0.308	0.309	0.306	0.309	0.268	0.301	0.312	0.341	0.311	0.318	0.285
32	0.311	0.329	0.324	0.314	0.292	0.309	0.333	0.306	0.302	0.312	0.313	0.281	0.337	0.306
33	0.313	0.334	0.325	0.314	0.293	0.325	0.305	0.312	0.301	0.300	0.294	0.284	0.295	0.302
34	0.318	0.342	0.324	0.314	0.302	0.305	0.297	0.312	0.301	0.302	0.295	0.284	0.304	0.326
35	0.310	0.309	0.284	0.318	0.321	0.304	0.298	0.317	0.294	0.292	0.296	0.315	0.287	0.316
36	0.312	0.328	0.283	0.321	0.288	0.302	0.302	0.313	0.294	0.293	0.316	0.301	0.290	0.319
37	0.306	0.329	0.320	0.292	0.288	0.304	0.322	0.316	0.295	0.302	0.291	0.300	0.289	0.294
38	0.300	0.312	0.321	0.295	0.297	0.317	0.322	0.309	0.295	0.303	0.297	0.298	0.283	0.291
39	0.302	0.303	0.321	0.297	0.297	0.306	0.322	0.309	0.305	0.290	0.296	0.287	0.287	0.270
40	0.301	0.300	0.320	0.299	0.304	0.298	0.288	0.308	0.298	0.290	0.314	0.304	0.305	0.289
41	0.300	0.305	0.318	0.332	0.306	0.296	0.286	0.308	0.286	0.290	0.311	0.292	0.317	0.319
42	0.302	0.291	0.321	0.303	0.306	0.295	0.316	0.268	0.286	0.340	0.305	0.309	0.328	0.322
43	0.302	0.291	0.324	0.327	0.306	0.294	0.288	0.284	0.283	0.335	0.307	0.305	0.317	0.320
44	0.303	0.308	0.323	0.305	0.309	0.297	0.288	0.275	0.283	0.340	0.307	0.303	0.331	0.302
45	0.303	0.308	0.307	0.300	0.311	0.282	0.319	0.277	0.292	0.313	0.309	0.304	0.342	0.320
46	0.277	0.318	0.305	0.300	0.309	0.282	0.320	0.305	0.293	0.313	0.308	0.334	0.296	0.305
47	0.277	0.316	0.292	0.319	0.309	0.283	0.323	0.278	0.283	0.313	0.287	0.325	0.296	0.324
48	0.276	0.331	0.279	0.271	0.308	0.284	0.286	0.277	0.283	0.310	0.328	0.293	0.277	0.308
49	0.298	0.295	0.277	0.272	0.310	0.281	0.290	0.277	0.305	0.310	0.327	0.296	0.302	0.297
50	0.304	0.301	0.276	0.305	0.285	0.278	0.295	0.284	0.306	0.312	0.327	0.279	0.302	0.294
51	0.279	0.305	0.309	0.294	0.308	0.274	0.298	0.284	0.306	0.315	0.285	0.279	0.301	0.298
52	0.281	0.297	0.303	0.305	0.309	0.306	0.300	0.289	0.302	0.316	0.310	0.286	0.310	0.315
53	0.310	0.297	0.326	0.296	0.298	0.304	0.302	0.283	0.310	0.316	0.308	0.289	0.310	0.304
54	0.311	0.297	0.322	0.287	0.316	0.271	0.302	0.283	0.309	0.318	0.283	0.283	0.314	0.282
55	0.309	0.297	0.276	0.284	0.315	0.270	0.302	0.283	0.308	0.312	0.305	0.289	0.315	0.298
56	0.307	0.276	0.276	0.283	0.313	0.269	0.301	0.284	0.309	0.312	0.306	0.297	0.300	0.288
57	0.306	0.323	0.305	0.282	0.310	0.267	0.285	0.290	0.311	0.311	0.306	0.285	0.306	0.290
58	0.305	0.298	0.305	0.275	0.293	0.297	0.287	0.314	0.312	0.313	0.305	0.289	0.302	0.291
59	0.280	0.298	0.304	0.275	0.310	0.294	0.319	0.314	0.321	0.285	0.305	0.289	0.326	0.294
60	0.281	0.298	0.275	0.275	0.308	0.294	0.287	0.313	0.321	0.320	0.306	0.306	0.308	0.295
61	0.281	0.298	0.274	0.275	0.308	0.299	0.287	0.287	0.320	0.316	0.302	0.306	0.330	0.295
62	0.305	0.298	0.274	0.277	0.307	0.298	0.288	0.289	0.319	0.317	0.302	0.305	0.329	0.290
63	0.281	0.298	0.273	0.280	0.308	0.297	0.300	0.283	0.321	0.319	0.311	0.316	0.302	0.290
64	0.305	0.298	0.298	0.280	0.307	0.297	0.297	0.313	0.321	0.317	0.302	0.303	0.302	0.298
65	0.280	0.298	0.297	0.280	0.307	0.280	0.296	0.287	0.322	0.302	0.305	0.328	0.302	0.290

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF3B Component ID. Lowest Reading 0.294 Highest reading 0.369

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.306	0.297	0.303	0.353	0.305	0.335	0.336	0.316	0.325	0.321	0.364	0.326	0.331	0.338
2	0.308	0.327	0.314	0.340	0.340	0.333	0.335	0.314	0.323	0.324	0.322	0.324	0.367	0.316
3	0.336	0.320	0.331	0.330	0.339	0.342	0.357	0.322	0.335	0.367	0.327	0.361	0.312	0.363
4	0.349	0.335	0.343	0.325	0.325	0.351	0.354	0.363	0.356	0.336	0.318	0.307	0.357	0.346
5	0.321	0.315	0.338	0.328	0.349	0.336	0.351	0.331	0.333	0.325	0.316	0.309	0.317	0.317
6	0.323	0.325	0.331	0.356	0.339	0.302	0.337	0.351	0.330	0.336	0.317	0.316	0.313	0.316
7	0.343	0.321	0.310	0.351	0.368	0.304	0.339	0.326	0.352	0.357	0.324	0.315	0.337	0.318
8	0.349	0.359	0.318	0.342	0.337	0.332	0.338	0.324	0.335	0.351	0.320	0.301	0.333	0.356
9	0.342	0.333	0.346	0.326	0.338	0.332	0.311	0.326	0.349	0.323	0.313	0.302	0.311	0.336
10	0.325	0.364	0.347	0.361	0.336	0.344	0.322	0.344	0.327	0.319	0.320	0.339	0.301	0.351
11	0.335	0.307	0.358	0.330	0.316	0.337	0.321	0.368	0.321	0.331	0.365	0.295	0.316	0.353
12	0.353	0.326	0.367	0.350	0.319	0.359	0.308	0.310	0.316	0.316	0.329	0.318	0.322	0.356
13	0.323	0.325	0.329	0.318	0.347	0.333	0.311	0.324	0.338	0.320	0.295	0.319	0.322	0.358
14	0.339	0.325	0.337	0.349	0.342	0.330	0.315	0.345	0.341	0.325	0.300	0.335	0.317	0.338
15	0.346	0.343	0.296	0.327	0.337	0.323	0.315	0.336	0.366	0.312	0.336	0.335	0.320	0.336
16	0.354	0.345	0.339	0.333	0.322	0.356	0.338	0.353	0.318	0.336	0.324	0.301	0.316	0.337
17	0.319	0.298	0.328	0.332	0.325	0.326	0.337	0.307	0.318	0.317	0.349	0.302	0.322	0.338
18	0.336	0.347	0.304	0.332	0.322	0.342	0.338	0.333	0.311	0.327	0.348	0.323	0.322	0.341
19	0.347	0.335	0.343	0.306	0.338	0.333	0.357	0.333	0.315	0.358	0.336	0.342	0.319	0.343
20	0.321	0.336	0.340	0.305	0.326	0.368	0.322	0.333	0.323	0.328	0.328	0.348	0.346	0.343
21	0.334	0.334	0.329	0.321	0.327	0.344	0.319	0.333	0.327	0.348	0.336	0.347	0.345	0.324
22	0.339	0.301	0.351	0.324	0.327	0.328	0.318	0.331	0.325	0.340	0.316	0.347	0.310	0.324
23	0.327	0.308	0.342	0.351	0.330	0.325	0.336	0.328	0.325	0.335	0.365	0.325	0.312	0.327
24	0.336	0.303	0.349	0.348	0.331	0.325	0.339	0.342	0.337	0.359	0.318	0.319	0.313	0.332
25	0.327	0.294	0.342	0.342	0.336	0.335	0.325	0.331	0.338	0.356	0.312	0.318	0.313	0.366
26	0.344	0.294	0.356	0.357	0.364	0.332	0.317	0.327	0.354	0.351	0.356	0.307	0.339	0.319
27	0.360	0.297	0.357	0.366	0.361	0.329	0.316	0.322	0.351	0.347	0.321	0.308	0.338	0.319
28	0.333	0.303	0.352	0.335	0.359	0.327	0.313	0.304	0.311	0.334	0.320	0.308	0.338	0.324
29	0.339	0.305	0.352	0.325	0.355	0.337	0.338	0.323	0.312	0.306	0.303	0.309	0.364	0.325
30	0.342	0.339	0.356	0.343	0.351	0.322	0.333	0.321	0.309	0.324	0.304	0.311	0.341	0.326
31	0.339	0.336	0.334	0.355	0.356	0.330	0.333	0.328	0.334	0.323	0.354	0.329	0.313	0.324
32	0.324	0.338	0.343	0.352	0.341	0.331	0.343	0.343	0.329	0.349	0.304	0.363	0.312	0.323
33	0.347	0.362	0.347	0.332	0.334	0.325	0.330	0.338	0.322	0.323	0.305	0.299	0.339	0.328
34	0.361	0.317	0.341	0.332	0.334	0.321	0.331	0.301	0.347	0.320	0.354	0.305	0.312	0.338
35	0.355	0.316	0.366	0.308	0.349	0.323	0.327	0.335	0.355	0.329	0.327	0.323	0.309	0.308
36	0.358	0.359	0.357	0.328	0.343	0.335	0.320	0.345	0.331	0.330	0.296	0.321	0.309	0.317
37	0.309	0.327	0.341	0.362	0.340	0.334	0.321	0.327	0.343	0.334	0.349	0.323	0.308	0.325
38	0.335	0.311	0.327	0.348	0.325	0.343	0.332	0.327	0.347	0.329	0.342	0.309	0.312	0.332
39	0.333	0.335	0.335	0.319	0.321	0.322	0.330	0.331	0.368	0.330	0.329	0.340	0.313	0.344
40	0.327	0.328	0.327	0.339	0.336	0.346	0.334	0.333	0.324	0.353	0.331	0.342	0.315	0.310
41	0.332	0.307	0.315	0.333	0.319	0.318	0.345	0.342	0.306	0.320	0.329	0.335	0.327	0.364
42	0.309	0.314	0.306	0.358	0.341	0.320	0.341	0.342	0.308	0.319	0.323	0.332	0.325	0.331
43	0.308	0.343	0.309	0.323	0.332	0.338	0.341	0.340	0.322	0.319	0.320	0.332	0.345	0.345
44	0.329	0.333	0.362	0.316	0.353	0.332	0.342	0.332	0.315	0.320	0.318	0.325	0.331	0.344
45	0.354	0.313	0.329	0.303	0.330	0.352	0.344	0.333	0.301	0.337	0.324	0.333	0.337	0.343
46	0.339	0.362	0.313	0.334	0.331	0.336	0.341	0.333	0.295	0.309	0.320	0.329	0.336	0.334
47	0.351	0.334	0.342	0.348	0.340	0.336	0.354	0.329	0.336	0.326	0.320	0.330	0.337	0.333
48	0.335	0.344	0.321	0.314	0.319	0.342	0.347	0.328	0.311	0.321	0.333	0.327	0.353	0.332
49	0.345	0.324	0.327	0.321	0.329	0.330	0.346	0.320	0.363	0.321	0.325	0.328	0.353	0.331
50	0.341	0.324	0.328	0.340	0.352	0.361	0.358	0.320	0.358	0.341	0.328	0.319	0.329	0.359
51	0.337	0.343	0.329	0.350	0.325	0.364	0.349	0.323	0.334	0.341	0.328	0.315	0.337	0.358
52	0.357	0.326	0.335	0.315	0.348	0.355	0.339	0.348	0.333	0.336	0.322	0.314	0.323	0.357
53	0.335	0.325	0.326	0.325	0.326	0.334	0.350	0.347	0.329	0.340	0.359	0.329	0.328	0.369
54	0.340	0.363	0.336	0.337	0.311	0.331	0.347	0.324	0.327	0.349	0.358	0.328	0.331	0.363
55	0.330	0.322	0.358	0.337	0.350	0.355	0.342	0.323	0.335	0.350	0.359	0.356	0.360	0.366
56	0.354	0.353	0.338	0.335	0.314	0.344	0.335	0.347	0.323	0.328	0.326	0.358	0.351	0.346
57	0.360	0.330	0.337	0.327	0.324	0.344	0.330	0.348	0.331	0.328	0.328	0.329	0.323	0.347
58	0.350	0.326	0.348	0.325	0.310	0.351	0.338	0.358	0.331	0.317	0.324	0.333	0.320	0.344
59	0.347	0.326	0.323	0.320	0.361	0.343	0.341	0.354	0.321	0.329	0.347	0.331	0.318	0.345
60	0.348	0.330	0.312	0.310	0.360	0.342	0.340	0.318	0.320	0.326	0.344	0.329	0.314	0.341
61	0.348	0.332	0.328	0.321	0.317	0.355	0.334	0.339	0.319	0.327	0.345	0.325	0.340	0.342
62	0.368	0.326	0.313	0.318	0.317	0.351	0.333	0.334	0.321	0.345	0.339	0.317	0.337	0.333
63	0.364	0.335	0.348	0.328	0.316	0.355	0.335	0.335	0.339	0.345	0.331	0.332	0.336	0.342
64	0.335	0.343	0.337	0.333	0.358	0.353	0.332	0.336	0.326	0.333	0.333	0.331	0.308	0.339
65	0.366	0.319	0.339	0.341	0.322	0.346	0.332	0.339	0.321	0.345	0.335	0.330	0.307	0.339
66	0.308	0.350	0.317	0.321	0.323	0.348	0.334	0.340	0.337	0.352	0.340	0.353	0.332	0.338

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Unit: Salem 1 RFO 20 Date: 04/13/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF4T Component ID. Lowest Reading 0.260 Highest reading 0.358

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.304	0.316	0.348	0.295	0.278	0.287	0.334	0.279	0.317	0.310	0.325	0.316	0.298	0.314
2	0.311	0.318	0.350	0.293	0.290	0.291	0.297	0.317	0.325	0.297	0.283	0.303	0.297	0.307
3	0.332	0.306	0.351	0.289	0.333	0.278	0.323	0.316	0.317	0.274	0.310	0.298	0.298	0.302
4	0.335	0.300	0.307	0.312	0.332	0.301	0.338	0.323	0.314	0.288	0.301	0.296	0.268	0.302
5	0.322	0.317	0.301	0.312	0.271	0.302	0.293	0.319	0.316	0.292	0.294	0.284	0.311	0.298
6	0.298	0.352	0.293	0.283	0.274	0.327	0.313	0.323	0.324	0.294	0.308	0.269	0.319	0.294
7	0.283	0.287	0.328	0.290	0.299	0.307	0.300	0.308	0.315	0.298	0.269	0.279	0.297	0.302
8	0.271	0.297	0.270	0.344	0.261	0.309	0.278	0.300	0.302	0.316	0.291	0.298	0.268	0.305
9	0.318	0.355	0.272	0.337	0.263	0.286	0.330	0.301	0.297	0.318	0.302	0.335	0.268	0.311
10	0.302	0.323	0.268	0.339	0.278	0.275	0.312	0.303	0.311	0.294	0.310	0.286	0.267	0.299
11	0.301	0.304	0.318	0.311	0.272	0.314	0.311	0.266	0.303	0.294	0.283	0.285	0.312	0.297
12	0.290	0.301	0.310	0.318	0.271	0.282	0.301	0.266	0.313	0.298	0.276	0.312	0.287	0.306
13	0.287	0.272	0.283	0.339	0.265	0.318	0.299	0.294	0.309	0.275	0.270	0.312	0.309	0.296
14	0.267	0.292	0.283	0.310	0.291	0.273	0.299	0.313	0.275	0.306	0.314	0.277	0.329	0.293
15	0.273	0.297	0.328	0.306	0.292	0.296	0.291	0.317	0.285	0.308	0.271	0.281	0.303	0.292
16	0.262	0.283	0.301	0.291	0.285	0.314	0.292	0.312	0.323	0.309	0.280	0.275	0.288	0.293
17	0.296	0.282	0.302	0.291	0.332	0.273	0.308	0.310	0.263	0.296	0.304	0.308	0.289	0.297
18	0.294	0.283	0.320	0.299	0.264	0.332	0.309	0.298	0.267	0.329	0.278	0.288	0.307	0.299
19	0.264	0.288	0.295	0.298	0.292	0.318	0.270	0.339	0.269	0.297	0.281	0.301	0.291	0.295
20	0.314	0.307	0.302	0.299	0.296	0.291	0.275	0.316	0.263	0.300	0.294	0.269	0.265	0.292
21	0.316	0.289	0.305	0.272	0.296	0.265	0.267	0.320	0.264	0.305	0.286	0.274	0.321	0.291
22	0.265	0.299	0.305	0.305	0.264	0.263	0.297	0.314	0.281	0.309	0.291	0.318	0.287	0.295
23	0.294	0.355	0.322	0.281	0.300	0.299	0.296	0.309	0.266	0.313	0.313	0.293	0.315	0.297
24	0.270	0.350	0.273	0.299	0.270	0.278	0.300	0.311	0.270	0.312	0.286	0.292	0.314	0.299
25	0.270	0.320	0.310	0.321	0.268	0.280	0.298	0.285	0.287	0.321	0.298	0.314	0.287	0.295
26	0.288	0.309	0.321	0.290	0.292	0.306	0.273	0.297	0.301	0.307	0.303	0.320	0.314	0.291
27	0.285	0.314	0.344	0.291	0.294	0.310	0.284	0.301	0.276	0.309	0.303	0.288	0.337	0.291
28	0.269	0.331	0.293	0.294	0.282	0.311	0.299	0.309	0.306	0.310	0.278	0.308	0.314	0.308
29	0.324	0.294	0.272	0.305	0.291	0.264	0.311	0.266	0.297	0.319	0.279	0.311	0.296	0.312
30	0.323	0.323	0.354	0.267	0.328	0.295	0.308	0.308	0.294	0.321	0.281	0.303	0.295	0.314
31	0.285	0.338	0.330	0.324	0.321	0.296	0.288	0.310	0.298	0.322	0.280	0.328	0.299	0.311
32	0.300	0.306	0.292	0.301	0.292	0.305	0.291	0.307	0.303	0.315	0.278	0.280	0.302	0.314
33	0.317	0.306	0.294	0.297	0.291	0.302	0.261	0.318	0.314	0.291	0.283	0.304	0.305	0.315
34	0.274	0.335	0.305	0.329	0.290	0.279	0.264	0.320	0.322	0.321	0.288	0.326	0.301	0.273
35	0.279	0.309	0.322	0.326	0.295	0.283	0.269	0.310	0.345	0.318	0.285	0.303	0.298	0.266
36	0.331	0.309	0.275	0.267	0.317	0.308	0.280	0.316	0.343	0.347	0.272	0.278	0.298	0.265
37	0.295	0.331	0.299	0.295	0.313	0.280	0.285	0.320	0.293	0.319	0.347	0.277	0.309	0.298
38	0.290	0.336	0.290	0.298	0.262	0.274	0.279	0.291	0.323	0.319	0.282	0.285	0.313	0.294
39	0.328	0.342	0.276	0.304	0.297	0.302	0.328	0.293	0.314	0.320	0.283	0.314	0.282	0.298
40	0.309	0.357	0.296	0.277	0.299	0.300	0.268	0.297	0.286	0.324	0.282	0.333	0.280	0.300
41	0.310	0.326	0.298	0.269	0.296	0.274	0.269	0.322	0.315	0.328	0.286	0.306	0.276	0.305
42	0.303	0.347	0.356	0.261	0.274	0.273	0.315	0.276	0.313	0.295	0.322	0.301	0.274	0.314
43	0.308	0.341	0.332	0.267	0.304	0.303	0.310	0.305	0.284	0.299	0.329	0.329	0.276	0.322
44	0.335	0.348	0.286	0.263	0.265	0.316	0.288	0.325	0.282	0.297	0.325	0.305	0.283	0.328
45	0.336	0.348	0.330	0.268	0.283	0.326	0.290	0.312	0.285	0.320	0.324	0.303	0.303	0.341
46	0.327	0.349	0.284	0.262	0.321	0.274	0.298	0.283	0.321	0.318	0.322	0.301	0.330	0.348
47	0.308	0.349	0.330	0.276	0.295	0.316	0.306	0.306	0.326	0.312	0.321	0.304	0.286	0.312
48	0.278	0.286	0.283	0.261	0.284	0.354	0.311	0.311	0.325	0.292	0.295	0.322	0.300	0.311
49	0.307	0.280	0.288	0.269	0.264	0.264	0.284	0.316	0.325	0.292	0.306	0.289	0.286	0.276
50	0.332	0.321	0.309	0.316	0.263	0.273	0.327	0.310	0.321	0.299	0.309	0.287	0.295	0.304
51	0.322	0.294	0.336	0.299	0.292	0.297	0.279	0.311	0.296	0.302	0.312	0.285	0.283	0.282
52	0.337	0.309	0.350	0.278	0.267	0.290	0.268	0.316	0.325	0.302	0.315	0.306	0.285	0.336
53	0.289	0.303	0.335	0.271	0.279	0.296	0.289	0.323	0.273	0.308	0.303	0.307	0.291	0.329
54	0.344	0.303	0.336	0.279	0.262	0.281	0.337	0.302	0.274	0.316	0.305	0.338	0.296	0.329
55	0.300	0.306	0.316	0.280	0.321	0.289	0.315	0.297	0.303	0.326	0.282	0.308	0.301	0.299
56	0.332	0.350	0.342	0.290	0.287	0.299	0.302	0.298	0.306	0.327	0.300	0.315	0.305	0.318
57	0.291	0.352	0.315	0.318	0.290	0.292	0.302	0.297	0.311	0.331	0.281	0.304	0.290	0.317
58	0.330	0.321	0.317	0.283	0.327	0.278	0.316	0.298	0.312	0.304	0.290	0.310	0.284	0.316
59	0.311	0.285	0.320	0.323	0.289	0.280	0.313	0.339	0.314	0.302	0.318	0.329	0.287	0.311
60	0.304	0.290	0.351	0.288	0.307	0.265	0.325	0.302	0.317	0.307	0.312	0.288	0.288	0.313
61	0.300	0.291	0.346	0.319	0.327	0.274	0.317	0.308	0.318	0.311	0.280	0.329	0.292	0.312
62	0.321	0.321	0.316	0.293	0.293	0.275	0.285	0.292	0.301	0.315	0.283	0.310	0.290	0.321
63	0.335	0.289	0.340	0.320	0.313	0.282	0.288	0.309	0.277	0.304	0.329	0.295	0.289	0.322
64	0.319	0.319	0.316	0.314	0.281	0.290	0.318	0.313	0.297	0.342	0.302	0.294	0.299	0.304
65	0.315	0.287	0.322	0.287	0.319	0.285	0.321	0.330	0.309	0.306	0.315	0.290	0.294	0.328
66	0.317	0.293	0.353	0.282	0.317	0.283	0.320	0.305	0.288	0.322	0.315	0.308	0.286	0.303
67	0.315	0.297	0.356	0.279	0.321	0.267	0.292	0.323	0.284	0.330	0.339	0.310	0.288	0.302

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Unit: Salem 1 RFO 20 Date: 04/13/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF4T Component ID. Lowest Reading 0.260 Highest reading 0.358

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.315	0.290	0.336	0.315	0.273	0.265	0.308	0.325	0.281	0.280	0.307	0.285	0.302	0.299
69	0.325	0.290	0.332	0.292	0.273	0.260	0.332	0.306	0.279	0.319	0.279	0.283	0.299	0.297
70	0.312	0.354	0.332	0.300	0.294	0.262	0.315	0.306	0.313	0.306	0.278	0.309	0.299	0.293
71	0.327	0.326	0.332	0.303	0.283	0.296	0.329	0.315	0.306	0.291	0.269	0.309	0.297	0.290
72	0.321	0.326	0.324	0.307	0.279	0.294	0.329	0.306	0.275	0.298	0.300	0.290	0.289	0.286
73	0.326	0.358	0.347	0.288	0.305	0.271	0.322	0.285	0.266	0.311	0.299	0.293	0.296	0.281
74	0.323	0.332	0.314	0.273	0.274	0.266	0.305	0.292	0.287	0.309	0.299	0.283	0.307	0.281
75	0.321	0.309	0.308	0.307	0.271	0.311	0.297	0.297	0.283	0.325	0.305	0.284	0.308	0.280
76	0.344	0.309	0.281	0.318	0.308	0.316	0.318	0.303	0.292	0.332	0.346	0.285	0.300	0.279
77	0.349	0.335	0.310	0.324	0.297	0.271	0.320	0.311	0.296	0.315	0.304	0.286	0.299	0.282
78	0.347	0.354	0.309	0.325	0.285	0.312	0.319	0.322	0.308	0.309	0.295	0.318	0.298	0.280
79	0.347	0.356	0.278	0.328	0.320	0.290	0.294	0.307	0.310	0.315	0.294	0.305	0.308	0.308
80	0.347	0.294	0.299	0.355	0.288	0.294	0.316	0.298	0.295	0.305	0.298	0.314	0.309	0.305

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF4B Component ID. Lowest Reading 0.272 Highest reading 0.362

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.321	0.302	0.313	0.309	0.337	0.325	0.320	0.343	0.317	0.297	0.312	0.289	0.309	0.308
2	0.320	0.322	0.343	0.309	0.337	0.350	0.292	0.338	0.295	0.292	0.333	0.300	0.272	0.311
3	0.321	0.325	0.323	0.331	0.335	0.353	0.293	0.290	0.320	0.293	0.321	0.344	0.298	0.321
4	0.309	0.347	0.322	0.324	0.348	0.353	0.296	0.310	0.296	0.328	0.315	0.303	0.282	0.319
5	0.332	0.299	0.320	0.327	0.307	0.337	0.308	0.326	0.290	0.320	0.312	0.298	0.290	0.339
6	0.320	0.294	0.315	0.324	0.346	0.310	0.313	0.308	0.282	0.339	0.322	0.302	0.319	0.336
7	0.317	0.336	0.352	0.316	0.339	0.291	0.308	0.315	0.281	0.299	0.313	0.299	0.293	0.324
8	0.334	0.322	0.347	0.301	0.331	0.305	0.299	0.325	0.291	0.324	0.322	0.297	0.284	0.320
9	0.301	0.322	0.317	0.303	0.332	0.307	0.353	0.321	0.292	0.326	0.306	0.287	0.282	0.318
10	0.313	0.308	0.317	0.315	0.337	0.327	0.303	0.310	0.321	0.331	0.322	0.299	0.316	0.332
11	0.313	0.331	0.325	0.310	0.342	0.335	0.349	0.317	0.324	0.320	0.323	0.297	0.309	0.315
12	0.284	0.327	0.348	0.317	0.327	0.339	0.321	0.312	0.296	0.317	0.327	0.289	0.295	0.336
13	0.286	0.321	0.361	0.322	0.331	0.338	0.299	0.314	0.322	0.316	0.291	0.287	0.292	0.315
14	0.330	0.322	0.344	0.323	0.321	0.326	0.325	0.329	0.300	0.323	0.288	0.305	0.300	0.338
15	0.320	0.322	0.361	0.316	0.331	0.341	0.331	0.331	0.299	0.299	0.287	0.325	0.307	0.291
16	0.321	0.307	0.344	0.327	0.321	0.334	0.292	0.328	0.300	0.301	0.299	0.315	0.319	0.290
17	0.322	0.331	0.342	0.320	0.315	0.336	0.295	0.325	0.299	0.287	0.292	0.296	0.300	0.308
18	0.283	0.307	0.336	0.331	0.317	0.333	0.303	0.322	0.301	0.320	0.289	0.304	0.322	0.286
19	0.291	0.328	0.333	0.327	0.315	0.330	0.355	0.317	0.324	0.323	0.322	0.335	0.302	0.312
20	0.291	0.329	0.333	0.327	0.334	0.353	0.316	0.316	0.299	0.316	0.324	0.340	0.293	0.285
21	0.308	0.335	0.331	0.325	0.289	0.354	0.316	0.340	0.284	0.312	0.350	0.337	0.299	0.313
22	0.299	0.341	0.333	0.320	0.300	0.353	0.333	0.337	0.287	0.291	0.312	0.307	0.304	0.325
23	0.325	0.340	0.358	0.320	0.297	0.329	0.292	0.311	0.282	0.298	0.311	0.309	0.297	0.335
24	0.347	0.338	0.326	0.320	0.311	0.328	0.332	0.286	0.293	0.300	0.303	0.311	0.297	0.339
25	0.348	0.339	0.320	0.351	0.311	0.325	0.304	0.316	0.303	0.305	0.315	0.325	0.312	0.315
26	0.325	0.322	0.321	0.335	0.308	0.321	0.303	0.333	0.284	0.315	0.319	0.304	0.294	0.275
27	0.323	0.322	0.323	0.359	0.339	0.325	0.320	0.296	0.277	0.326	0.315	0.312	0.293	0.305
28	0.326	0.348	0.306	0.355	0.322	0.325	0.309	0.288	0.306	0.309	0.316	0.292	0.317	0.314
29	0.310	0.351	0.309	0.317	0.325	0.325	0.337	0.290	0.307	0.291	0.320	0.325	0.275	0.300
30	0.315	0.324	0.315	0.320	0.302	0.329	0.327	0.303	0.348	0.298	0.348	0.292	0.297	0.305
31	0.359	0.334	0.345	0.322	0.300	0.339	0.300	0.324	0.286	0.294	0.315	0.324	0.293	0.310
32	0.362	0.337	0.295	0.358	0.322	0.325	0.305	0.331	0.290	0.310	0.309	0.283	0.307	0.312
33	0.331	0.335	0.283	0.323	0.331	0.349	0.298	0.279	0.300	0.320	0.307	0.291	0.294	0.300
34	0.330	0.330	0.309	0.323	0.335	0.299	0.299	0.275	0.309	0.327	0.309	0.321	0.337	0.307
35	0.309	0.328	0.319	0.324	0.322	0.296	0.323	0.287	0.317	0.325	0.353	0.327	0.330	0.329
36	0.327	0.327	0.322	0.317	0.318	0.311	0.324	0.338	0.294	0.309	0.312	0.314	0.321	0.329
37	0.330	0.328	0.328	0.329	0.322	0.345	0.322	0.327	0.290	0.327	0.321	0.303	0.314	0.318
38	0.322	0.330	0.329	0.322	0.308	0.305	0.283	0.311	0.291	0.353	0.291	0.297	0.318	0.304
39	0.304	0.331	0.306	0.327	0.302	0.330	0.325	0.309	0.355	0.290	0.321	0.287	0.311	0.300
40	0.295	0.333	0.306	0.321	0.339	0.311	0.330	0.313	0.294	0.299	0.324	0.298	0.317	0.311
41	0.337	0.346	0.326	0.325	0.336	0.325	0.325	0.316	0.317	0.304	0.357	0.305	0.343	0.327
42	0.301	0.335	0.329	0.326	0.335	0.332	0.315	0.327	0.331	0.308	0.324	0.296	0.315	0.302
43	0.328	0.318	0.326	0.324	0.326	0.317	0.324	0.316	0.326	0.311	0.297	0.295	0.286	0.332
44	0.329	0.314	0.320	0.316	0.326	0.314	0.326	0.318	0.325	0.310	0.296	0.298	0.296	0.304
45	0.307	0.319	0.299	0.314	0.325	0.319	0.325	0.348	0.318	0.303	0.294	0.302	0.307	0.301
46	0.294	0.322	0.326	0.331	0.298	0.302	0.295	0.286	0.308	0.289	0.288	0.289	0.306	0.316
47	0.335	0.322	0.290	0.338	0.301	0.298	0.294	0.317	0.297	0.320	0.324	0.285	0.308	0.341
48	0.353	0.323	0.292	0.338	0.306	0.318	0.294	0.299	0.310	0.318	0.323	0.285	0.298	0.287
49	0.306	0.309	0.309	0.342	0.304	0.318	0.329	0.283	0.319	0.327	0.352	0.273	0.298	0.292
50	0.290	0.308	0.294	0.312	0.310	0.297	0.296	0.339	0.293	0.316	0.304	0.316	0.286	0.336
51	0.287	0.330	0.291	0.316	0.303	0.320	0.295	0.339	0.306	0.324	0.308	0.289	0.320	0.302
52	0.302	0.287	0.300	0.339	0.293	0.297	0.281	0.346	0.322	0.315	0.311	0.286	0.341	0.290
53	0.298	0.309	0.292	0.317	0.293	0.318	0.335	0.310	0.331	0.317	0.277	0.293	0.311	0.287
54	0.313	0.292	0.287	0.318	0.320	0.324	0.323	0.315	0.275	0.326	0.333	0.294	0.312	0.288
55	0.302	0.332	0.312	0.311	0.310	0.308	0.339	0.333	0.328	0.302	0.312	0.308	0.313	0.295
56	0.328	0.332	0.303	0.315	0.337	0.305	0.321	0.319	0.303	0.300	0.286	0.335	0.310	0.316
57	0.300	0.328	0.327	0.321	0.314	0.305	0.298	0.324	0.293	0.307	0.291	0.293	0.301	0.309
58	0.307	0.291	0.328	0.311	0.293	0.304	0.309	0.325	0.313	0.304	0.301	0.279	0.294	0.324
59	0.317	0.295	0.305	0.311	0.320	0.303	0.332	0.328	0.311	0.306	0.324	0.309	0.299	0.276
60	0.321	0.283	0.309	0.316	0.321	0.306	0.306	0.342	0.302	0.325	0.316	0.274	0.300	0.311
61	0.321	0.294	0.311	0.312	0.322	0.289	0.299	0.311	0.337	0.299	0.311	0.278	0.277	0.346
62	0.308	0.300	0.281	0.316	0.305	0.318	0.298	0.310	0.326	0.307	0.316	0.284	0.298	0.313
63	0.305	0.300	0.279	0.332	0.305	0.315	0.338	0.312	0.330	0.308	0.330	0.285	0.323	0.314
64	0.306	0.302	0.281	0.319	0.311	0.326	0.298	0.318	0.306	0.286	0.315	0.314	0.312	0.329
65	0.304	0.313	0.293	0.312	0.308	0.318	0.292	0.316	0.309	0.291	0.304	0.313	0.316	0.308
66	0.320	0.345	0.290	0.318	0.308	0.316	0.305	0.338	0.342	0.302	0.299	0.283	0.278	0.320
67	0.343	0.307	0.333	0.331	0.303	0.315	0.308	0.298	0.307	0.329	0.292	0.279	0.317	0.335

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF4B Component ID: Lowest Reading 0.272 Highest reading 0.362

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.302	0.305	0.317	0.346	0.302	0.309	0.338	0.276	0.311	0.300	0.298	0.289	0.296	0.311
69	0.344	0.351	0.319	0.312	0.301	0.314	0.315	0.275	0.337	0.308	0.297	0.323	0.284	0.334
70	0.346	0.351	0.305	0.292	0.284	0.328	0.337	0.309	0.314	0.310	0.305	0.320	0.289	0.325
71	0.345	0.295	0.302	0.292	0.289	0.298	0.325	0.298	0.307	0.329	0.325	0.337	0.284	0.299
72	0.301	0.291	0.302	0.290	0.318	0.289	0.298	0.296	0.322	0.327	0.326	0.286	0.296	0.338
73	0.299	0.281	0.295	0.276	0.322	0.308	0.300	0.289	0.308	0.325	0.303	0.325	0.302	0.344
74	0.302	0.283	0.289	0.277	0.323	0.312	0.306	0.285	0.326	0.297	0.294	0.292	0.280	0.308
75	0.296	0.294	0.282	0.320	0.320	0.311	0.308	0.280	0.325	0.302	0.303	0.327	0.297	0.313
76	0.308	0.281	0.310	0.306	0.320	0.316	0.324	0.293	0.302	0.298	0.323	0.326	0.286	0.310
77	0.309	0.279	0.309	0.310	0.336	0.281	0.293	0.301	0.329	0.306	0.325	0.294	0.304	0.331
78	0.311	0.295	0.315	0.285	0.333	0.303	0.317	0.328	0.293	0.329	0.327	0.336	0.319	0.309
79	0.281	0.286	0.313	0.275	0.330	0.287	0.318	0.327	0.304	0.326	0.299	0.310	0.314	0.308
80	0.315	0.288	0.313	0.285	0.328	0.289	0.317	0.323	0.323	0.305	0.288	0.312	0.318	0.294
81	0.286	0.303	0.310	0.289	0.328	0.316	0.314	0.322	0.300	0.301	0.289	0.325	0.322	0.326
82	0.289	0.303	0.310	0.327	0.328	0.320	0.339	0.316	0.294	0.313	0.299	0.322	0.312	0.294

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF5T Component ID. Lowest Reading 0.198 Highest reading 0.354

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.322	0.325	0.318	0.284	0.296	0.317	0.311	0.309	0.281	0.294	0.295	0.296	0.319	0.272
2	0.308	0.302	0.294	0.284	0.293	0.290	0.345	0.312	0.281	0.302	0.294	0.297	0.277	0.271
3	0.329	0.319	0.315	0.284	0.298	0.290	0.347	0.314	0.302	0.307	0.269	0.267	0.290	0.285
4	0.295	0.319	0.301	0.313	0.295	0.294	0.293	0.313	0.310	0.289	0.287	0.282	0.299	0.316
5	0.293	0.307	0.293	0.305	0.260	0.295	0.290	0.341	0.314	0.284	0.292	0.278	0.291	0.285
6	0.293	0.307	0.292	0.310	0.308	0.295	0.296	0.312	0.304	0.284	0.300	0.276	0.291	0.281
7	0.287	0.307	0.297	0.312	0.270	0.293	0.299	0.306	0.350	0.317	0.300	0.274	0.292	0.274
8	0.321	0.311	0.284	0.311	0.299	0.293	0.296	0.306	0.267	0.317	0.307	0.271	0.294	0.273
9	0.272	0.334	0.284	0.276	0.295	0.320	0.292	0.311	0.315	0.283	0.297	0.271	0.294	0.273
10	0.305	0.319	0.298	0.289	0.271	0.273	0.282	0.339	0.351	0.287	0.298	0.268	0.265	0.271
11	0.302	0.311	0.302	0.265	0.296	0.269	0.282	0.305	0.334	0.287	0.305	0.267	0.264	0.289
12	0.309	0.310	0.328	0.265	0.305	0.271	0.279	0.305	0.335	0.282	0.301	0.305	0.289	0.287
13	0.341	0.309	0.299	0.294	0.269	0.268	0.279	0.304	0.336	0.273	0.311	0.311	0.310	0.287
14	0.289	0.337	0.286	0.298	0.270	0.271	0.276	0.294	0.289	0.273	0.305	0.296	0.326	0.284
15	0.280	0.294	0.285	0.336	0.302	0.287	0.280	0.292	0.311	0.297	0.298	0.321	0.333	0.302
16	0.311	0.330	0.198	0.323	0.301	0.271	0.322	0.285	0.289	0.305	0.300	0.311	0.308	0.289
17	0.317	0.303	0.291	0.299	0.297	0.280	0.323	0.285	0.274	0.264	0.301	0.348	0.307	0.281
18	0.285	0.304	0.292	0.299	0.298	0.279	0.323	0.284	0.292	0.286	0.261	0.348	0.309	0.264
19	0.271	0.305	0.306	0.272	0.299	0.304	0.282	0.278	0.340	0.285	0.276	0.347	0.308	0.263
20	0.283	0.303	0.299	0.299	0.313	0.304	0.282	0.304	0.315	0.267	0.281	0.286	0.305	0.298
21	0.284	0.307	0.291	0.285	0.311	0.315	0.347	0.311	0.341	0.303	0.280	0.287	0.276	0.269
22	0.271	0.325	0.292	0.289	0.310	0.314	0.284	0.313	0.340	0.301	0.310	0.317	0.276	0.260
23	0.313	0.303	0.288	0.263	0.337	0.314	0.267	0.298	0.318	0.301	0.310	0.316	0.308	0.267
24	0.303	0.303	0.267	0.263	0.309	0.267	0.265	0.299	0.297	0.302	0.309	0.317	0.275	0.265
25	0.302	0.334	0.290	0.291	0.306	0.291	0.289	0.262	0.289	0.283	0.294	0.310	0.276	0.261
26	0.325	0.312	0.268	0.323	0.298	0.291	0.287	0.288	0.312	0.300	0.293	0.311	0.308	0.278
27	0.293	0.283	0.288	0.316	0.278	0.267	0.285	0.285	0.312	0.299	0.301	0.311	0.264	0.326
28	0.291	0.283	0.289	0.299	0.272	0.296	0.278	0.354	0.273	0.297	0.321	0.305	0.263	0.299
29	0.266	0.321	0.287	0.285	0.265	0.295	0.279	0.351	0.275	0.301	0.323	0.312	0.280	0.289
30	0.289	0.270	0.262	0.327	0.298	0.296	0.299	0.273	0.278	0.311	0.314	0.299	0.337	0.271
31	0.265	0.321	0.289	0.328	0.294	0.268	0.292	0.321	0.281	0.314	0.322	0.274	0.262	0.295
32	0.281	0.294	0.265	0.295	0.292	0.275	0.323	0.325	0.283	0.322	0.320	0.318	0.302	0.299
33	0.287	0.296	0.265	0.298	0.297	0.336	0.322	0.295	0.273	0.314	0.312	0.319	0.291	0.300
34	0.291	0.318	0.329	0.298	0.311	0.322	0.278	0.343	0.278	0.314	0.309	0.319	0.315	0.299
35	0.306	0.317	0.302	0.298	0.300	0.339	0.278	0.307	0.282	0.318	0.308	0.284	0.272	0.300
36	0.302	0.317	0.305	0.278	0.270	0.270	0.277	0.343	0.329	0.342	0.315	0.277	0.270	0.278
37	0.323	0.292	0.277	0.320	0.270	0.330	0.300	0.343	0.306	0.342	0.292	0.299	0.292	0.280
38	0.266	0.293	0.299	0.319	0.298	0.296	0.291	0.299	0.307	0.342	0.317	0.273	0.289	0.279
39	0.302	0.264	0.277	0.329	0.296	0.308	0.297	0.302	0.277	0.342	0.312	0.337	0.289	0.286
40	0.301	0.284	0.275	0.305	0.271	0.346	0.295	0.304	0.277	0.315	0.306	0.337	0.264	0.279
41	0.302	0.287	0.263	0.305	0.298	0.326	0.261	0.305	0.271	0.274	0.300	0.289	0.286	0.281
42	0.311	0.267	0.265	0.293	0.271	0.280	0.277	0.304	0.271	0.302	0.295	0.311	0.282	0.285
43	0.296	0.314	0.313	0.291	0.301	0.279	0.264	0.306	0.278	0.274	0.298	0.331	0.285	0.284
44	0.284	0.301	0.313	0.265	0.280	0.280	0.302	0.266	0.281	0.309	0.305	0.298	0.282	0.283
45	0.312	0.313	0.313	0.273	0.280	0.279	0.320	0.268	0.283	0.336	0.306	0.288	0.287	0.283
46	0.305	0.298	0.323	0.281	0.289	0.279	0.272	0.271	0.261	0.315	0.306	0.289	0.290	0.282
47	0.331	0.283	0.327	0.284	0.278	0.298	0.275	0.273	0.282	0.272	0.304	0.348	0.292	0.280
48	0.328	0.295	0.298	0.321	0.278	0.289	0.295	0.272	0.278	0.269	0.303	0.271	0.322	0.283
49	0.288	0.295	0.293	0.301	0.278	0.279	0.308	0.270	0.309	0.296	0.300	0.301	0.323	0.283
50	0.281	0.290	0.293	0.319	0.298	0.271	0.328	0.270	0.294	0.297	0.320	0.280	0.323	0.287
51	0.266	0.304	0.299	0.314	0.262	0.313	0.321	0.304	0.309	0.317	0.321	0.303	0.288	0.284
52	0.289	0.302	0.295	0.289	0.261	0.314	0.278	0.328	0.309	0.314	0.287	0.313	0.292	0.283
53	0.333	0.287	0.294	0.290	0.339	0.302	0.290	0.272	0.290	0.315	0.291	0.314	0.307	0.287
54	0.313	0.302	0.294	0.291	0.286	0.303	0.290	0.272	0.274	0.316	0.291	0.294	0.279	0.285
55	0.322	0.292	0.314	0.317	0.260	0.297	0.289	0.272	0.275	0.311	0.315	0.300	0.280	0.290
56	0.314	0.303	0.314	0.287	0.260	0.297	0.266	0.270	0.309	0.340	0.316	0.287	0.279	0.290
57	0.301	0.276	0.290	0.287	0.264	0.301	0.267	0.350	0.311	0.314	0.322	0.272	0.275	0.290
58	0.295	0.290	0.294	0.317	0.265	0.301	0.267	0.296	0.298	0.304	0.332	0.271	0.296	0.293
59	0.294	0.296	0.290	0.318	0.292	0.300	0.282	0.299	0.296	0.304	0.327	0.289	0.316	0.292
60	0.300	0.295	0.261	0.292	0.292	0.299	0.306	0.298	0.297	0.304	0.303	0.276	0.261	0.294
61	0.315	0.294	0.267	0.294	0.314	0.262	0.282	0.281	0.298	0.340	0.311	0.275	0.263	0.299
62	0.314	0.294	0.267	0.296	0.290	0.341	0.283	0.271	0.296	0.322	0.321	0.320	0.263	0.308

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF5B Component ID. Lowest Reading 0.272 Highest reading 0.394

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.319	0.303	0.310	0.326	0.334	0.303	0.277	0.332	0.351	0.372	0.333	0.310	0.307	0.340
2	0.334	0.307	0.309	0.328	0.351	0.297	0.369	0.330	0.381	0.382	0.298	0.309	0.351	0.369
3	0.331	0.314	0.353	0.309	0.349	0.322	0.323	0.347	0.378	0.275	0.274	0.310	0.347	0.356
4	0.298	0.379	0.359	0.364	0.349	0.393	0.343	0.343	0.339	0.350	0.307	0.309	0.310	0.344
5	0.323	0.355	0.363	0.352	0.378	0.389	0.362	0.341	0.340	0.378	0.303	0.306	0.374	0.377
6	0.347	0.335	0.372	0.350	0.367	0.358	0.351	0.382	0.340	0.364	0.294	0.305	0.361	0.308
7	0.378	0.332	0.332	0.341	0.387	0.353	0.350	0.379	0.336	0.284	0.295	0.303	0.337	0.333
8	0.301	0.313	0.339	0.348	0.330	0.340	0.295	0.343	0.385	0.360	0.345	0.323	0.324	0.362
9	0.330	0.320	0.339	0.317	0.363	0.338	0.356	0.342	0.292	0.277	0.343	0.330	0.323	0.350
10	0.368	0.335	0.334	0.325	0.314	0.350	0.379	0.374	0.298	0.331	0.338	0.353	0.320	0.316
11	0.372	0.384	0.363	0.321	0.375	0.340	0.345	0.326	0.281	0.328	0.359	0.356	0.328	0.314
12	0.306	0.359	0.346	0.385	0.374	0.340	0.379	0.325	0.335	0.357	0.345	0.344	0.355	0.328
13	0.354	0.369	0.367	0.336	0.323	0.338	0.317	0.330	0.337	0.356	0.348	0.301	0.343	0.327
14	0.333	0.371	0.299	0.360	0.319	0.339	0.312	0.335	0.375	0.373	0.349	0.274	0.344	0.326
15	0.322	0.312	0.329	0.328	0.331	0.348	0.297	0.337	0.351	0.336	0.345	0.276	0.363	0.320
16	0.311	0.308	0.330	0.325	0.379	0.339	0.287	0.347	0.320	0.357	0.324	0.292	0.322	0.333
17	0.342	0.280	0.351	0.328	0.322	0.351	0.372	0.366	0.383	0.355	0.323	0.338	0.355	0.338
18	0.350	0.279	0.378	0.336	0.326	0.346	0.366	0.291	0.345	0.361	0.336	0.342	0.316	0.318
19	0.378	0.304	0.380	0.348	0.357	0.338	0.346	0.301	0.347	0.366	0.340	0.363	0.326	0.290
20	0.354	0.326	0.368	0.392	0.367	0.351	0.375	0.292	0.337	0.373	0.346	0.314	0.311	0.335
21	0.338	0.345	0.377	0.371	0.335	0.344	0.348	0.298	0.359	0.380	0.330	0.337	0.341	0.302
22	0.368	0.299	0.351	0.374	0.336	0.374	0.319	0.275	0.387	0.359	0.331	0.340	0.327	0.328
23	0.314	0.306	0.284	0.305	0.342	0.342	0.347	0.302	0.291	0.385	0.332	0.338	0.283	0.302
24	0.321	0.392	0.285	0.363	0.344	0.382	0.360	0.291	0.326	0.325	0.338	0.324	0.277	0.329
25	0.360	0.284	0.363	0.359	0.340	0.361	0.336	0.297	0.352	0.326	0.339	0.344	0.302	0.356
26	0.354	0.338	0.352	0.380	0.310	0.380	0.342	0.300	0.291	0.355	0.337	0.374	0.278	0.333
27	0.310	0.301	0.332	0.389	0.363	0.363	0.338	0.278	0.353	0.325	0.385	0.358	0.303	0.360
28	0.307	0.375	0.368	0.375	0.361	0.360	0.337	0.332	0.325	0.348	0.329	0.359	0.299	0.333
29	0.311	0.354	0.333	0.307	0.359	0.358	0.284	0.365	0.337	0.360	0.337	0.365	0.345	0.340
30	0.346	0.381	0.343	0.342	0.383	0.386	0.280	0.298	0.331	0.298	0.345	0.345	0.278	0.338
31	0.335	0.315	0.338	0.369	0.358	0.332	0.279	0.290	0.387	0.290	0.332	0.347	0.330	0.333
32	0.359	0.314	0.342	0.361	0.360	0.334	0.276	0.321	0.365	0.283	0.363	0.378	0.334	0.290
33	0.387	0.331	0.349	0.342	0.352	0.380	0.348	0.314	0.299	0.338	0.344	0.342	0.328	0.296
34	0.363	0.330	0.379	0.339	0.349	0.382	0.371	0.313	0.334	0.336	0.320	0.379	0.358	0.336
35	0.338	0.337	0.333	0.341	0.339	0.354	0.366	0.314	0.330	0.283	0.335	0.319	0.317	0.377
36	0.333	0.331	0.356	0.281	0.348	0.388	0.342	0.326	0.338	0.293	0.321	0.310	0.358	0.319
37	0.339	0.369	0.341	0.358	0.328	0.385	0.293	0.327	0.338	0.277	0.322	0.311	0.307	0.293
38	0.344	0.381	0.339	0.306	0.330	0.353	0.296	0.330	0.341	0.373	0.326	0.312	0.283	0.326
39	0.342	0.350	0.336	0.280	0.334	0.354	0.303	0.308	0.322	0.371	0.323	0.313	0.278	0.326
40	0.340	0.317	0.307	0.355	0.332	0.372	0.349	0.308	0.334	0.305	0.332	0.291	0.274	0.342
41	0.324	0.304	0.310	0.292	0.342	0.373	0.299	0.328	0.351	0.383	0.366	0.321	0.351	0.290
42	0.317	0.361	0.302	0.298	0.347	0.382	0.297	0.324	0.372	0.337	0.336	0.311	0.352	0.334
43	0.314	0.299	0.301	0.340	0.348	0.380	0.298	0.383	0.315	0.298	0.300	0.344	0.326	0.295
44	0.336	0.298	0.315	0.332	0.368	0.394	0.334	0.355	0.320	0.378	0.296	0.306	0.321	0.350
45	0.346	0.299	0.317	0.330	0.363	0.341	0.364	0.374	0.349	0.340	0.304	0.303	0.293	0.345
46	0.342	0.379	0.320	0.350	0.381	0.361	0.367	0.359	0.313	0.326	0.305	0.303	0.291	0.361
47	0.337	0.392	0.323	0.348	0.369	0.334	0.342	0.357	0.363	0.334	0.281	0.306	0.333	0.365
48	0.364	0.362	0.324	0.342	0.371	0.359	0.348	0.333	0.377	0.342	0.358	0.307	0.325	0.337
49	0.355	0.374	0.320	0.353	0.384	0.352	0.348	0.392	0.363	0.346	0.355	0.325	0.330	0.322
50	0.326	0.344	0.317	0.358	0.383	0.369	0.292	0.354	0.323	0.351	0.300	0.325	0.352	0.347
51	0.374	0.349	0.318	0.349	0.334	0.369	0.320	0.371	0.317	0.352	0.297	0.326	0.333	0.307
52	0.337	0.393	0.328	0.353	0.326	0.358	0.376	0.321	0.356	0.352	0.272	0.330	0.340	0.334
53	0.341	0.353	0.330	0.374	0.370	0.319	0.360	0.350	0.353	0.377	0.294	0.377	0.294	0.328
54	0.339	0.337	0.326	0.340	0.349	0.388	0.355	0.349	0.336	0.357	0.291	0.301	0.310	0.332
55	0.296	0.342	0.329	0.345	0.355	0.356	0.322	0.292	0.274	0.357	0.285	0.324	0.307	0.341
56	0.344	0.375	0.328	0.334	0.383	0.389	0.322	0.296	0.344	0.341	0.338	0.333	0.307	0.327
57	0.361	0.344	0.289	0.332	0.367	0.359	0.320	0.312	0.355	0.311	0.325	0.367	0.296	0.332
58	0.309	0.279	0.345	0.333	0.333	0.388	0.296	0.296	0.328	0.341	0.307	0.353	0.315	0.326
59	0.322	0.347	0.343	0.357	0.335	0.365	0.364	0.281	0.339	0.350	0.283	0.333	0.317	0.324
60	0.346	0.339	0.331	0.334	0.329	0.353	0.296	0.283	0.321	0.368	0.308	0.330	0.331	0.308
61	0.324	0.337	0.368	0.337	0.349	0.344	0.323	0.303	0.337	0.356	0.309	0.290	0.364	0.276
62	0.362	0.339	0.330	0.374	0.363	0.347	0.330	0.298	0.327	0.330	0.369	0.274	0.327	0.287

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF6T Component ID. Lowest Reading 0.252 Highest reading 0.356

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.265	0.328	0.297	0.272	0.326	0.302	0.299	0.318	0.330	0.318	0.333	0.267	0.293	0.286
2	0.284	0.266	0.327	0.315	0.304	0.268	0.318	0.293	0.333	0.344	0.299	0.285	0.298	0.308
3	0.302	0.345	0.322	0.274	0.307	0.261	0.281	0.289	0.320	0.306	0.309	0.316	0.299	0.337
4	0.335	0.317	0.261	0.273	0.288	0.305	0.307	0.259	0.322	0.349	0.339	0.314	0.318	0.323
5	0.289	0.329	0.274	0.296	0.304	0.291	0.285	0.295	0.321	0.354	0.338	0.310	0.302	0.299
6	0.307	0.305	0.326	0.253	0.298	0.299	0.293	0.332	0.322	0.271	0.333	0.312	0.287	0.295
7	0.310	0.309	0.269	0.252	0.290	0.272	0.298	0.270	0.335	0.333	0.330	0.305	0.303	0.324
8	0.287	0.310	0.269	0.254	0.285	0.281	0.331	0.299	0.299	0.330	0.310	0.284	0.312	0.298
9	0.305	0.311	0.329	0.255	0.287	0.312	0.317	0.321	0.305	0.320	0.302	0.300	0.337	0.342
10	0.295	0.310	0.320	0.298	0.292	0.280	0.283	0.338	0.304	0.308	0.299	0.302	0.344	0.315
11	0.283	0.293	0.314	0.292	0.289	0.286	0.288	0.310	0.319	0.313	0.306	0.280	0.314	0.308
12	0.293	0.337	0.271	0.273	0.278	0.280	0.287	0.309	0.305	0.310	0.310	0.299	0.305	0.293
13	0.259	0.334	0.277	0.295	0.293	0.272	0.300	0.300	0.327	0.319	0.312	0.294	0.301	0.293
14	0.318	0.317	0.267	0.297	0.318	0.315	0.286	0.305	0.277	0.337	0.330	0.332	0.294	0.287
15	0.322	0.323	0.300	0.315	0.289	0.315	0.305	0.301	0.307	0.291	0.321	0.305	0.303	0.286
16	0.277	0.303	0.311	0.323	0.317	0.307	0.313	0.305	0.264	0.287	0.324	0.341	0.291	0.297
17	0.264	0.295	0.351	0.327	0.296	0.285	0.284	0.312	0.325	0.291	0.313	0.326	0.320	0.297
18	0.312	0.313	0.293	0.302	0.296	0.282	0.290	0.312	0.314	0.314	0.278	0.328	0.322	0.289
19	0.326	0.317	0.299	0.320	0.309	0.271	0.295	0.281	0.310	0.295	0.282	0.330	0.327	0.291
20	0.312	0.313	0.271	0.317	0.311	0.282	0.283	0.297	0.344	0.318	0.291	0.297	0.276	0.299
21	0.326	0.298	0.286	0.320	0.314	0.272	0.268	0.275	0.264	0.290	0.308	0.271	0.288	0.323
22	0.286	0.305	0.331	0.326	0.300	0.298	0.302	0.276	0.341	0.319	0.303	0.329	0.294	0.320
23	0.295	0.274	0.303	0.282	0.275	0.299	0.270	0.279	0.278	0.301	0.297	0.314	0.313	0.338
24	0.321	0.272	0.275	0.284	0.317	0.289	0.286	0.280	0.318	0.304	0.300	0.280	0.312	0.317
25	0.355	0.278	0.297	0.288	0.315	0.307	0.322	0.312	0.283	0.305	0.286	0.277	0.280	0.300
26	0.306	0.309	0.276	0.320	0.307	0.266	0.272	0.309	0.284	0.302	0.288	0.288	0.302	0.317
27	0.257	0.305	0.270	0.321	0.298	0.299	0.267	0.302	0.315	0.321	0.306	0.275	0.306	0.320
28	0.303	0.281	0.306	0.318	0.288	0.292	0.316	0.308	0.331	0.321	0.275	0.276	0.291	0.288
29	0.327	0.324	0.275	0.300	0.336	0.322	0.303	0.334	0.349	0.306	0.302	0.291	0.289	0.290
30	0.303	0.314	0.297	0.323	0.287	0.302	0.311	0.303	0.301	0.278	0.316	0.277	0.271	0.301
31	0.311	0.305	0.279	0.324	0.286	0.351	0.303	0.304	0.335	0.326	0.310	0.280	0.308	0.313
32	0.310	0.305	0.285	0.304	0.277	0.267	0.296	0.342	0.332	0.303	0.296	0.281	0.282	0.309
33	0.290	0.306	0.309	0.303	0.326	0.314	0.338	0.341	0.333	0.302	0.258	0.272	0.343	0.314
34	0.336	0.312	0.309	0.314	0.327	0.269	0.315	0.318	0.299	0.310	0.257	0.304	0.278	0.289
35	0.333	0.287	0.304	0.298	0.282	0.321	0.309	0.303	0.336	0.315	0.284	0.281	0.348	0.264
36	0.309	0.308	0.266	0.327	0.318	0.332	0.356	0.307	0.335	0.317	0.302	0.296	0.284	0.309
37	0.326	0.315	0.279	0.343	0.327	0.301	0.292	0.306	0.266	0.331	0.279	0.294	0.301	0.282
38	0.341	0.293	0.348	0.353	0.282	0.307	0.294	0.312	0.298	0.310	0.320	0.328	0.307	0.289
39	0.355	0.291	0.305	0.305	0.283	0.305	0.281	0.315	0.316	0.310	0.321	0.304	0.307	0.305
40	0.307	0.299	0.299	0.306	0.284	0.329	0.300	0.311	0.311	0.311	0.319	0.316	0.282	0.305
41	0.306	0.317	0.354	0.304	0.324	0.304	0.303	0.310	0.309	0.305	0.345	0.318	0.282	0.330
42	0.305	0.353	0.322	0.306	0.296	0.291	0.300	0.310	0.328	0.317	0.305	0.298	0.282	0.308
43	0.305	0.303	0.335	0.306	0.295	0.320	0.299	0.305	0.304	0.305	0.291	0.299	0.305	0.329
44	0.329	0.337	0.356	0.333	0.304	0.300	0.299	0.302	0.286	0.298	0.292	0.296	0.356	0.351
45	0.329	0.316	0.336	0.307	0.305	0.317	0.307	0.303	0.286	0.299	0.304	0.298	0.336	0.319
46	0.307	0.315	0.336	0.332	0.304	0.292	0.307	0.302	0.286	0.298	0.304	0.325	0.332	0.297
47	0.355	0.315	0.310	0.332	0.307	0.291	0.309	0.301	0.287	0.328	0.303	0.299	0.332	0.351
48	0.350	0.341	0.309	0.330	0.305	0.289	0.307	0.295	0.284	0.330	0.302	0.299	0.322	0.299
49	0.319	0.311	0.308	0.310	0.290	0.288	0.322	0.294	0.289	0.322	0.292	0.300	0.332	0.300
50	0.314	0.309	0.305	0.310	0.290	0.336	0.324	0.294	0.294	0.327	0.323	0.300	0.311	0.345
51	0.319	0.306	0.305	0.310	0.291	0.336	0.320	0.312	0.342	0.306	0.309	0.300	0.356	0.315
52	0.319	0.305	0.306	0.335	0.308	0.295	0.325	0.317	0.289	0.306	0.298	0.299	0.304	0.310
53	0.320	0.298	0.306	0.312	0.343	0.305	0.329	0.304	0.292	0.301	0.305	0.300	0.353	0.314
54	0.320	0.298	0.283	0.338	0.354	0.291	0.322	0.311	0.307	0.301	0.319	0.301	0.306	0.310
55	0.322	0.297	0.284	0.322	0.305	0.291	0.318	0.302	0.306	0.299	0.305	0.299	0.305	0.343
56	0.320	0.297	0.284	0.346	0.317	0.292	0.311	0.313	0.305	0.295	0.305	0.335	0.351	0.306
57	0.321	0.303	0.279	0.306	0.318	0.293	0.298	0.331	0.339	0.289	0.346	0.351	0.280	0.304
58	0.325	0.305	0.280	0.306	0.320	0.293	0.295	0.307	0.320	0.294	0.337	0.290	0.273	0.305
59	0.324	0.284	0.280	0.354	0.324	0.292	0.334	0.289	0.328	0.295	0.335	0.318	0.270	0.309
60	0.324	0.283	0.279	0.325	0.298	0.289	0.348	0.304	0.303	0.293	0.339	0.313	0.268	0.311
61	0.323	0.283	0.279	0.326	0.299	0.292	0.317	0.305	0.308	0.345	0.304	0.331	0.270	0.301
62	0.322	0.283	0.279	0.346	0.296	0.291	0.318	0.267	0.309	0.305	0.253	0.319	0.270	0.302
63	0.305	0.281	0.279	0.312	0.295	0.291	0.298	0.292	0.311	0.339	0.313	0.341	0.335	0.305
64	0.322	0.283	0.280	0.308	0.289	0.292	0.298	0.285	0.310	0.292	0.314	0.319	0.321	0.300
65	0.322	0.330	0.281	0.300	0.290	0.292	0.298	0.284	0.309	0.292	0.313	0.285	0.325	0.291
66	0.325	0.330	0.281	0.303	0.305	0.292	0.292	0.303	0.309	0.291	0.350	0.285	0.327	0.291
67	0.326	0.305	0.281	0.300	0.309	0.313	0.339	0.301	0.310	0.290	0.328	0.286	0.325	0.355

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF6T Component ID. Lowest Reading 0.252 Highest reading 0.356

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.326	0.286	0.282	0.300	0.309	0.312	0.317	0.302	0.308	0.291	0.327	0.287	0.327	0.289
69	0.326	0.290	0.283	0.301	0.289	0.301	0.287	0.300	0.311	0.294	0.305	0.288	0.345	0.289
70	0.324	0.288	0.281	0.301	0.294	0.298	0.293	0.300	0.341	0.322	0.304	0.284	0.332	0.289
71	0.325	0.288	0.281	0.304	0.294	0.291	0.291	0.299	0.302	0.350	0.304	0.284	0.329	0.290
72	0.322	0.324	0.282	0.300	0.294	0.292	0.289	0.299	0.341	0.322	0.302	0.287	0.322	0.333
73	0.320	0.324	0.282	0.301	0.294	0.291	0.269	0.301	0.321	0.293	0.274	0.286	0.323	0.327
74	0.324	0.292	0.282	0.301	0.296	0.293	0.270	0.302	0.334	0.319	0.275	0.332	0.314	0.355
75	0.293	0.289	0.277	0.340	0.297	0.294	0.270	0.296	0.339	0.320	0.274	0.283	0.312	0.349
76	0.293	0.290	0.278	0.303	0.303	0.294	0.298	0.292	0.305	0.320	0.289	0.282	0.312	0.265
77	0.293	0.299	0.278	0.305	0.306	0.302	0.300	0.300	0.305	0.319	0.270	0.308	0.298	0.266

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF6B Component ID. Lowest Reading 0.271 Highest reading 0.382

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.337	0.337	0.382	0.307	0.338	0.319	0.329	0.287	0.299	0.293	0.273	0.305	0.311	0.306
2	0.334	0.324	0.288	0.294	0.302	0.299	0.334	0.294	0.281	0.293	0.319	0.328	0.311	0.305
3	0.342	0.321	0.301	0.285	0.335	0.298	0.331	0.290	0.330	0.360	0.319	0.336	0.312	0.306
4	0.379	0.321	0.328	0.286	0.329	0.310	0.322	0.290	0.305	0.360	0.319	0.335	0.311	0.345
5	0.333	0.320	0.327	0.291	0.334	0.308	0.315	0.296	0.335	0.318	0.321	0.336	0.308	0.319
6	0.341	0.324	0.328	0.335	0.333	0.306	0.317	0.290	0.297	0.318	0.321	0.333	0.308	0.317
7	0.314	0.318	0.332	0.275	0.332	0.306	0.322	0.299	0.336	0.324	0.325	0.329	0.313	0.320
8	0.303	0.319	0.331	0.343	0.332	0.277	0.321	0.302	0.333	0.298	0.351	0.335	0.311	0.318
9	0.331	0.317	0.333	0.297	0.332	0.278	0.324	0.276	0.331	0.298	0.320	0.337	0.328	0.317
10	0.317	0.322	0.333	0.279	0.303	0.306	0.314	0.328	0.319	0.322	0.321	0.347	0.329	0.316
11	0.332	0.322	0.335	0.280	0.285	0.306	0.310	0.278	0.319	0.327	0.327	0.345	0.340	0.312
12	0.338	0.307	0.328	0.298	0.311	0.276	0.312	0.371	0.329	0.326	0.336	0.342	0.328	0.312
13	0.339	0.308	0.293	0.299	0.299	0.309	0.322	0.276	0.302	0.299	0.338	0.329	0.336	0.320
14	0.291	0.309	0.292	0.329	0.295	0.308	0.322	0.275	0.301	0.281	0.317	0.329	0.323	0.318
15	0.311	0.306	0.290	0.304	0.302	0.334	0.327	0.274	0.326	0.290	0.317	0.324	0.371	0.316
16	0.312	0.306	0.290	0.284	0.332	0.336	0.327	0.297	0.325	0.282	0.319	0.347	0.337	0.315
17	0.311	0.324	0.290	0.311	0.308	0.290	0.316	0.321	0.300	0.331	0.322	0.347	0.338	0.314
18	0.308	0.321	0.268	0.303	0.306	0.290	0.323	0.296	0.323	0.305	0.325	0.346	0.338	0.333
19	0.303	0.322	0.338	0.331	0.303	0.339	0.318	0.274	0.300	0.298	0.328	0.322	0.352	0.333
20	0.302	0.273	0.334	0.282	0.305	0.295	0.327	0.274	0.301	0.317	0.330	0.317	0.354	0.347
21	0.303	0.296	0.306	0.286	0.307	0.301	0.334	0.297	0.301	0.333	0.332	0.319	0.336	0.329
22	0.303	0.294	0.301	0.286	0.308	0.309	0.312	0.321	0.324	0.336	0.332	0.319	0.333	0.319
23	0.311	0.295	0.300	0.307	0.306	0.322	0.321	0.296	0.305	0.336	0.334	0.319	0.351	0.331
24	0.301	0.308	0.275	0.331	0.308	0.328	0.322	0.297	0.305	0.338	0.331	0.319	0.349	0.326
25	0.316	0.305	0.274	0.285	0.305	0.299	0.325	0.277	0.317	0.340	0.332	0.294	0.349	0.328
26	0.302	0.306	0.274	0.330	0.308	0.336	0.335	0.303	0.316	0.300	0.331	0.320	0.325	0.348
27	0.310	0.307	0.299	0.307	0.292	0.290	0.329	0.307	0.319	0.302	0.331	0.319	0.339	0.348
28	0.312	0.312	0.274	0.307	0.272	0.288	0.331	0.309	0.299	0.305	0.297	0.294	0.333	0.328
29	0.307	0.314	0.280	0.288	0.274	0.315	0.324	0.311	0.296	0.299	0.323	0.323	0.326	0.330
30	0.312	0.314	0.283	0.288	0.303	0.312	0.330	0.310	0.302	0.304	0.326	0.323	0.331	0.329
31	0.335	0.338	0.310	0.287	0.305	0.339	0.329	0.308	0.308	0.301	0.329	0.328	0.332	0.331
32	0.306	0.325	0.311	0.291	0.311	0.339	0.332	0.283	0.315	0.312	0.336	0.326	0.342	0.330
33	0.335	0.323	0.317	0.296	0.314	0.319	0.330	0.315	0.316	0.317	0.331	0.357	0.301	0.328
34	0.311	0.321	0.296	0.331	0.316	0.299	0.322	0.326	0.312	0.320	0.334	0.356	0.302	0.334
35	0.335	0.323	0.324	0.302	0.319	0.346	0.330	0.302	0.309	0.330	0.338	0.351	0.299	0.332
36	0.312	0.324	0.323	0.297	0.320	0.309	0.271	0.273	0.308	0.316	0.332	0.312	0.298	0.336
37	0.310	0.326	0.322	0.323	0.323	0.305	0.272	0.356	0.309	0.345	0.306	0.293	0.318	0.328
38	0.311	0.339	0.322	0.299	0.327	0.309	0.308	0.359	0.324	0.308	0.329	0.294	0.299	0.326
39	0.307	0.333	0.319	0.321	0.327	0.336	0.323	0.336	0.315	0.335	0.327	0.294	0.297	0.329
40	0.308	0.339	0.292	0.322	0.328	0.335	0.310	0.291	0.322	0.339	0.329	0.334	0.298	0.329
41	0.308	0.281	0.294	0.329	0.330	0.305	0.310	0.331	0.339	0.317	0.327	0.335	0.321	0.329
42	0.306	0.293	0.292	0.363	0.333	0.335	0.315	0.293	0.334	0.327	0.334	0.297	0.322	0.305
43	0.332	0.330	0.290	0.337	0.317	0.327	0.322	0.317	0.331	0.327	0.329	0.314	0.319	0.305
44	0.328	0.329	0.298	0.336	0.289	0.327	0.324	0.318	0.335	0.330	0.331	0.313	0.316	0.305
45	0.328	0.330	0.308	0.327	0.290	0.308	0.327	0.317	0.331	0.333	0.335	0.313	0.318	0.306
46	0.334	0.319	0.302	0.293	0.289	0.311	0.325	0.293	0.336	0.317	0.340	0.297	0.317	0.306
47	0.328	0.299	0.304	0.292	0.288	0.286	0.330	0.290	0.321	0.279	0.339	0.297	0.315	0.355
48	0.355	0.296	0.300	0.296	0.290	0.312	0.332	0.298	0.318	0.323	0.342	0.357	0.315	0.330
49	0.346	0.296	0.296	0.296	0.290	0.311	0.325	0.316	0.316	0.332	0.333	0.334	0.316	0.331
50	0.329	0.302	0.272	0.311	0.295	0.336	0.318	0.308	0.317	0.330	0.333	0.326	0.323	0.324
51	0.278	0.298	0.296	0.309	0.295	0.336	0.316	0.326	0.315	0.323	0.332	0.325	0.320	0.326
52	0.358	0.304	0.332	0.293	0.294	0.334	0.318	0.325	0.311	0.293	0.331	0.351	0.350	0.346
53	0.331	0.329	0.334	0.309	0.297	0.333	0.319	0.325	0.318	0.326	0.332	0.350	0.330	0.331
54	0.330	0.278	0.294	0.325	0.315	0.329	0.328	0.277	0.324	0.305	0.337	0.325	0.353	0.335
55	0.328	0.324	0.295	0.286	0.290	0.331	0.311	0.299	0.333	0.325	0.308	0.325	0.352	0.307
56	0.328	0.335	0.297	0.286	0.289	0.327	0.311	0.279	0.329	0.322	0.307	0.327	0.347	0.309
57	0.336	0.327	0.298	0.330	0.315	0.330	0.309	0.298	0.330	0.326	0.311	0.344	0.336	0.299
58	0.294	0.328	0.344	0.326	0.290	0.336	0.311	0.285	0.328	0.325	0.315	0.338	0.326	0.288
59	0.293	0.320	0.290	0.330	0.290	0.342	0.326	0.285	0.333	0.329	0.311	0.305	0.321	0.320
60	0.329	0.325	0.299	0.332	0.290	0.330	0.272	0.284	0.333	0.330	0.340	0.308	0.302	0.322
61	0.301	0.322	0.323	0.284	0.314	0.320	0.325	0.284	0.365	0.323	0.307	0.310	0.303	0.336
62	0.301	0.318	0.323	0.330	0.287	0.318	0.312	0.309	0.341	0.359	0.340	0.306	0.345	0.335
63	0.299	0.321	0.300	0.336	0.296	0.321	0.315	0.308	0.340	0.323	0.308	0.304	0.306	0.316
64	0.293	0.322	0.298	0.329	0.297	0.321	0.325	0.308	0.338	0.284	0.309	0.307	0.325	0.316
65	0.340	0.275	0.297	0.326	0.304	0.320	0.329	0.308	0.332	0.299	0.305	0.313	0.321	0.315
66	0.304	0.326	0.326	0.335	0.303	0.319	0.315	0.334	0.336	0.316	0.302	0.313	0.318	0.317
67	0.332	0.324	0.300	0.332	0.303	0.319	0.309	0.318	0.335	0.289	0.337	0.312	0.317	0.324

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF6B Component ID. Lowest Reading 0.271 Highest reading 0.382

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.324	0.322	0.298	0.311	0.302	0.327	0.326	0.296	0.335	0.309	0.338	0.313	0.317	0.349
69	0.321	0.323	0.298	0.314	0.281	0.322	0.338	0.318	0.316	0.328	0.341	0.316	0.293	0.326
70	0.326	0.319	0.274	0.307	0.280	0.328	0.324	0.320	0.273	0.329	0.321	0.328	0.298	0.325
71	0.334	0.320	0.323	0.275	0.296	0.325	0.329	0.277	0.318	0.314	0.342	0.330	0.300	0.356
72	0.325	0.322	0.300	0.289	0.302	0.319	0.328	0.317	0.289	0.314	0.321	0.335	0.301	0.340
73	0.329	0.279	0.272	0.290	0.323	0.317	0.346	0.317	0.305	0.291	0.322	0.333	0.309	0.321
74	0.323	0.348	0.323	0.335	0.341	0.321	0.330	0.320	0.343	0.317	0.325	0.334	0.314	0.294
75	0.327	0.272	0.324	0.338	0.342	0.328	0.337	0.311	0.296	0.317	0.321	0.332	0.309	0.298
76	0.327	0.368	0.311	0.332	0.296	0.328	0.332	0.288	0.296	0.320	0.299	0.332	0.307	0.300
77	0.330	0.279	0.309	0.331	0.315	0.317	0.305	0.293	0.271	0.339	0.299	0.308	0.313	0.301
78	0.317	0.290	0.279	0.272	0.314	0.318	0.284	0.297	0.298	0.281	0.301	0.310	0.312	0.298
79	0.321	0.289	0.300	0.294	0.312	0.311	0.283	0.290	0.299	0.339	0.306	0.310	0.317	0.299
80	0.318	0.287	0.306	0.335	0.318	0.325	0.335	0.299	0.293	0.305	0.305	0.308	0.317	0.320

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF7T Component ID. Lowest Reading 0.271 Highest reading 0.376

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.287	0.298	0.315	0.300	0.320	0.315	0.311	0.329	0.314	0.337	0.328	0.302	0.313	0.312
2	0.299	0.287	0.294	0.336	0.305	0.311	0.318	0.332	0.313	0.311	0.334	0.337	0.319	0.321
3	0.318	0.288	0.298	0.288	0.319	0.317	0.326	0.326	0.329	0.317	0.313	0.312	0.306	0.290
4	0.304	0.287	0.295	0.293	0.282	0.308	0.329	0.329	0.336	0.294	0.312	0.299	0.294	0.328
5	0.285	0.278	0.311	0.285	0.307	0.335	0.343	0.339	0.320	0.301	0.317	0.306	0.302	0.291
6	0.310	0.323	0.287	0.320	0.328	0.310	0.333	0.338	0.328	0.285	0.302	0.307	0.299	0.295
7	0.307	0.315	0.290	0.327	0.319	0.287	0.279	0.333	0.324	0.284	0.331	0.313	0.313	0.323
8	0.305	0.303	0.325	0.326	0.340	0.338	0.326	0.325	0.326	0.288	0.339	0.304	0.314	0.314
9	0.357	0.320	0.317	0.325	0.337	0.282	0.312	0.322	0.322	0.278	0.329	0.306	0.297	0.281
10	0.295	0.287	0.305	0.335	0.299	0.335	0.309	0.322	0.329	0.282	0.308	0.308	0.299	0.314
11	0.300	0.303	0.279	0.334	0.298	0.294	0.331	0.300	0.313	0.274	0.335	0.305	0.293	0.290
12	0.291	0.290	0.286	0.294	0.318	0.300	0.300	0.302	0.306	0.304	0.302	0.320	0.295	0.299
13	0.322	0.334	0.290	0.293	0.329	0.295	0.297	0.292	0.308	0.307	0.334	0.306	0.299	0.279
14	0.287	0.286	0.337	0.283	0.355	0.299	0.277	0.317	0.310	0.302	0.294	0.301	0.308	0.281
15	0.272	0.317	0.313	0.312	0.325	0.306	0.325	0.337	0.306	0.281	0.292	0.294	0.312	0.279
16	0.278	0.318	0.320	0.292	0.290	0.306	0.319	0.310	0.322	0.312	0.264	0.323	0.321	0.333
17	0.285	0.347	0.325	0.279	0.291	0.299	0.322	0.339	0.336	0.318	0.304	0.293	0.317	0.299
18	0.290	0.346	0.346	0.298	0.327	0.294	0.293	0.325	0.311	0.312	0.274	0.290	0.294	0.288
19	0.292	0.311	0.282	0.337	0.280	0.290	0.303	0.320	0.314	0.304	0.318	0.275	0.333	0.305
20	0.323	0.299	0.303	0.324	0.277	0.289	0.364	0.312	0.308	0.303	0.312	0.290	0.333	0.307
21	0.276	0.307	0.322	0.300	0.320	0.337	0.334	0.314	0.307	0.291	0.283	0.297	0.278	0.335
22	0.357	0.336	0.302	0.301	0.318	0.305	0.337	0.325	0.333	0.304	0.303	0.299	0.310	0.325
23	0.326	0.303	0.301	0.303	0.283	0.295	0.338	0.320	0.320	0.292	0.297	0.293	0.290	0.334
24	0.299	0.290	0.277	0.339	0.274	0.341	0.349	0.319	0.333	0.284	0.298	0.293	0.311	0.325
25	0.301	0.293	0.336	0.282	0.320	0.320	0.325	0.315	0.325	0.282	0.304	0.321	0.305	0.291
26	0.297	0.326	0.288	0.319	0.300	0.339	0.331	0.332	0.318	0.310	0.293	0.311	0.329	0.334
27	0.300	0.299	0.309	0.323	0.293	0.332	0.325	0.307	0.328	0.313	0.308	0.315	0.325	0.309
28	0.304	0.301	0.288	0.322	0.334	0.308	0.315	0.327	0.339	0.315	0.312	0.325	0.306	0.298
29	0.334	0.320	0.278	0.334	0.352	0.297	0.303	0.294	0.331	0.336	0.279	0.317	0.322	0.278
30	0.327	0.311	0.275	0.284	0.303	0.306	0.305	0.278	0.332	0.304	0.331	0.308	0.321	0.325
31	0.327	0.307	0.315	0.321	0.299	0.312	0.294	0.273	0.330	0.305	0.293	0.315	0.282	0.323
32	0.295	0.306	0.317	0.318	0.303	0.282	0.337	0.315	0.337	0.320	0.288	0.330	0.298	0.332
33	0.294	0.297	0.295	0.309	0.318	0.320	0.335	0.319	0.329	0.313	0.326	0.308	0.301	0.339
34	0.312	0.356	0.295	0.320	0.334	0.322	0.331	0.333	0.324	0.285	0.307	0.319	0.306	0.333
35	0.314	0.298	0.296	0.316	0.305	0.314	0.295	0.312	0.326	0.276	0.307	0.302	0.293	0.282
36	0.321	0.304	0.277	0.308	0.307	0.315	0.299	0.305	0.337	0.274	0.290	0.317	0.318	0.334
37	0.313	0.323	0.279	0.318	0.314	0.328	0.336	0.303	0.344	0.275	0.294	0.317	0.322	0.293
38	0.344	0.299	0.288	0.314	0.303	0.330	0.336	0.313	0.322	0.284	0.305	0.303	0.289	0.308
39	0.308	0.287	0.299	0.308	0.307	0.318	0.315	0.315	0.328	0.273	0.314	0.294	0.294	0.315
40	0.282	0.289	0.297	0.291	0.323	0.328	0.338	0.323	0.287	0.273	0.311	0.319	0.297	0.318
41	0.283	0.291	0.299	0.309	0.310	0.321	0.374	0.315	0.310	0.319	0.314	0.299	0.311	0.310
42	0.294	0.296	0.337	0.352	0.317	0.298	0.328	0.323	0.313	0.321	0.291	0.324	0.314	0.305
43	0.334	0.338	0.295	0.313	0.309	0.305	0.327	0.302	0.325	0.324	0.304	0.320	0.318	0.272
44	0.286	0.315	0.303	0.307	0.315	0.303	0.331	0.297	0.338	0.298	0.316	0.324	0.306	0.306
45	0.311	0.312	0.315	0.321	0.326	0.306	0.320	0.314	0.325	0.292	0.294	0.324	0.294	0.306
46	0.313	0.311	0.311	0.308	0.292	0.315	0.283	0.323	0.327	0.298	0.283	0.301	0.297	0.330
47	0.334	0.337	0.325	0.305	0.338	0.316	0.291	0.299	0.323	0.276	0.293	0.318	0.282	0.312
48	0.313	0.310	0.307	0.311	0.341	0.334	0.322	0.290	0.339	0.287	0.297	0.285	0.281	0.305
49	0.314	0.335	0.312	0.298	0.337	0.300	0.332	0.293	0.342	0.304	0.276	0.302	0.274	0.305
50	0.284	0.324	0.304	0.299	0.317	0.286	0.320	0.308	0.333	0.328	0.318	0.302	0.300	0.323
51	0.314	0.326	0.336	0.309	0.311	0.321	0.327	0.329	0.280	0.336	0.301	0.312	0.273	0.320
52	0.338	0.298	0.334	0.301	0.305	0.284	0.327	0.333	0.311	0.274	0.285	0.315	0.271	0.299
53	0.293	0.330	0.332	0.309	0.339	0.329	0.330	0.297	0.319	0.302	0.310	0.306	0.289	0.297
54	0.344	0.333	0.317	0.301	0.336	0.280	0.323	0.320	0.310	0.275	0.301	0.323	0.284	0.330
55	0.342	0.329	0.294	0.307	0.302	0.294	0.292	0.321	0.319	0.280	0.294	0.290	0.303	0.292
56	0.307	0.279	0.315	0.296	0.309	0.353	0.279	0.344	0.326	0.293	0.283	0.292	0.310	0.331
57	0.349	0.322	0.279	0.330	0.313	0.304	0.291	0.315	0.333	0.274	0.294	0.305	0.291	0.318
58	0.334	0.265	0.333	0.315	0.331	0.306	0.315	0.328	0.307	0.282	0.299	0.314	0.282	0.320
59	0.304	0.317	0.291	0.323	0.338	0.299	0.299	0.312	0.335	0.299	0.311	0.303	0.287	0.293
60	0.312	0.318	0.322	0.315	0.338	0.299	0.287	0.314	0.322	0.275	0.311	0.319	0.316	0.331
61	0.313	0.313	0.319	0.328	0.313	0.325	0.274	0.337	0.328	0.303	0.318	0.280	0.318	0.321
62	0.316	0.315	0.294	0.313	0.304	0.332	0.290	0.300	0.291	0.315	0.307	0.282	0.295	0.320
63	0.317	0.323	0.303	0.318	0.300	0.358	0.294	0.321	0.312	0.314	0.324	0.292	0.305	0.321
64	0.325	0.358	0.296	0.298	0.302	0.341	0.291	0.311	0.317	0.332	0.325	0.286	0.312	0.290
65	0.323	0.322	0.295	0.309	0.334	0.328	0.335	0.291	0.293	0.323	0.298	0.346	0.315	0.290
66	0.313	0.313	0.302	0.311	0.343	0.337	0.340	0.316	0.328	0.313	0.287	0.328	0.302	0.285
67	0.340	0.316	0.328	0.307	0.326	0.346	0.329	0.315	0.322	0.316	0.289	0.285	0.316	0.302

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF7T Component ID. Lowest Reading 0.271 Highest reading 0.376

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.315	0.310	0.289	0.317	0.331	0.309	0.338	0.319	0.309	0.318	0.276	0.325	0.315	0.298
69	0.319	0.308	0.309	0.311	0.313	0.328	0.327	0.322	0.299	0.326	0.331	0.308	0.306	0.276
70	0.324	0.318	0.337	0.290	0.314	0.342	0.337	0.304	0.315	0.319	0.299	0.286	0.301	0.307
71	0.328	0.306	0.303	0.321	0.287	0.322	0.333	0.337	0.321	0.316	0.298	0.338	0.320	0.329
72	0.326	0.302	0.298	0.306	0.307	0.327	0.353	0.338	0.304	0.325	0.321	0.306	0.295	0.325
73	0.329	0.289	0.301	0.307	0.319	0.323	0.305	0.339	0.324	0.320	0.276	0.301	0.312	0.335
74	0.330	0.307	0.306	0.307	0.322	0.376	0.321	0.336	0.321	0.323	0.306	0.317	0.279	0.333
75	0.325	0.315	0.307	0.313	0.318	0.329	0.301	0.316	0.313	0.324	0.323	0.318	0.295	0.307

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF7B Component ID. Lowest Reading 0.270 Highest reading 0.348

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.292	0.318	0.317	0.310	0.311	0.315	0.324	0.323	0.313	0.331	0.306	0.301	0.280	0.330
2	0.295	0.307	0.315	0.308	0.326	0.328	0.324	0.322	0.334	0.287	0.287	0.323	0.285	0.299
3	0.333	0.333	0.319	0.307	0.306	0.328	0.310	0.323	0.327	0.323	0.292	0.322	0.287	0.286
4	0.316	0.280	0.289	0.303	0.310	0.327	0.302	0.303	0.327	0.325	0.307	0.292	0.287	0.291
5	0.296	0.311	0.292	0.303	0.313	0.300	0.298	0.301	0.331	0.266	0.322	0.301	0.287	0.298
6	0.299	0.311	0.329	0.302	0.324	0.300	0.296	0.308	0.303	0.290	0.326	0.299	0.290	0.301
7	0.314	0.340	0.285	0.301	0.299	0.301	0.294	0.304	0.306	0.293	0.325	0.289	0.282	0.310
8	0.312	0.343	0.318	0.301	0.332	0.301	0.308	0.308	0.326	0.325	0.311	0.287	0.272	0.290
9	0.293	0.338	0.311	0.319	0.330	0.293	0.322	0.308	0.326	0.328	0.310	0.285	0.291	0.295
10	0.334	0.283	0.309	0.297	0.300	0.284	0.325	0.327	0.329	0.331	0.292	0.293	0.285	0.302
11	0.299	0.296	0.308	0.298	0.320	0.335	0.300	0.328	0.302	0.330	0.296	0.302	0.288	0.321
12	0.285	0.275	0.307	0.282	0.319	0.309	0.294	0.328	0.314	0.288	0.277	0.310	0.292	0.289
13	0.343	0.299	0.312	0.279	0.313	0.301	0.294	0.326	0.288	0.301	0.335	0.324	0.270	0.295
14	0.280	0.286	0.316	0.308	0.311	0.300	0.294	0.319	0.310	0.305	0.309	0.317	0.287	0.299
15	0.289	0.313	0.327	0.296	0.280	0.299	0.307	0.315	0.336	0.291	0.335	0.305	0.289	0.311
16	0.290	0.312	0.318	0.297	0.284	0.298	0.333	0.318	0.297	0.324	0.285	0.299	0.292	0.300
17	0.300	0.299	0.321	0.328	0.285	0.325	0.333	0.320	0.287	0.303	0.282	0.293	0.327	0.296
18	0.326	0.320	0.319	0.302	0.285	0.299	0.337	0.338	0.286	0.307	0.277	0.288	0.330	0.295
19	0.327	0.311	0.323	0.329	0.286	0.282	0.300	0.327	0.284	0.291	0.288	0.282	0.292	0.300
20	0.313	0.317	0.325	0.341	0.282	0.296	0.328	0.319	0.283	0.289	0.286	0.303	0.293	0.302
21	0.312	0.290	0.327	0.336	0.313	0.299	0.329	0.289	0.282	0.345	0.282	0.275	0.275	0.289
22	0.315	0.307	0.325	0.309	0.285	0.281	0.326	0.321	0.288	0.298	0.277	0.282	0.292	0.307
23	0.309	0.317	0.324	0.272	0.313	0.283	0.296	0.278	0.293	0.324	0.320	0.292	0.301	0.311
24	0.309	0.319	0.317	0.276	0.287	0.283	0.294	0.304	0.301	0.336	0.281	0.272	0.295	0.303
25	0.309	0.320	0.316	0.271	0.286	0.323	0.331	0.338	0.292	0.327	0.278	0.290	0.294	0.311
26	0.306	0.324	0.309	0.307	0.284	0.313	0.293	0.309	0.292	0.329	0.297	0.293	0.293	0.326
27	0.313	0.309	0.315	0.307	0.311	0.297	0.294	0.303	0.303	0.337	0.306	0.279	0.292	0.312
28	0.313	0.321	0.314	0.319	0.283	0.298	0.294	0.307	0.331	0.305	0.311	0.297	0.297	0.324
29	0.304	0.322	0.333	0.314	0.292	0.285	0.330	0.302	0.272	0.306	0.312	0.322	0.305	0.312
30	0.305	0.321	0.313	0.318	0.296	0.309	0.329	0.301	0.327	0.292	0.310	0.337	0.291	0.330
31	0.306	0.319	0.295	0.317	0.296	0.294	0.294	0.311	0.293	0.338	0.316	0.300	0.296	0.282
32	0.325	0.324	0.301	0.316	0.283	0.301	0.299	0.313	0.303	0.293	0.314	0.304	0.299	0.313
33	0.278	0.300	0.316	0.316	0.285	0.298	0.290	0.305	0.282	0.284	0.322	0.301	0.272	0.270
34	0.283	0.281	0.293	0.327	0.287	0.299	0.294	0.300	0.280	0.292	0.286	0.280	0.295	0.280
35	0.292	0.283	0.307	0.324	0.331	0.299	0.337	0.321	0.280	0.296	0.280	0.287	0.304	0.274
36	0.315	0.285	0.308	0.323	0.311	0.326	0.312	0.294	0.312	0.298	0.276	0.304	0.290	0.283
37	0.313	0.289	0.328	0.282	0.332	0.309	0.292	0.319	0.312	0.277	0.296	0.327	0.291	0.280
38	0.289	0.307	0.287	0.283	0.331	0.316	0.332	0.309	0.289	0.281	0.307	0.307	0.290	0.274
39	0.334	0.337	0.305	0.287	0.304	0.307	0.337	0.301	0.288	0.281	0.286	0.311	0.293	0.284
40	0.290	0.337	0.314	0.296	0.331	0.320	0.310	0.330	0.282	0.312	0.280	0.286	0.296	0.300
41	0.293	0.304	0.303	0.336	0.279	0.316	0.336	0.303	0.280	0.277	0.290	0.305	0.298	0.302
42	0.294	0.302	0.272	0.318	0.304	0.303	0.316	0.271	0.284	0.283	0.306	0.309	0.299	0.303
43	0.292	0.306	0.314	0.287	0.305	0.306	0.315	0.279	0.283	0.287	0.282	0.310	0.303	0.286
44	0.292	0.298	0.276	0.311	0.325	0.311	0.314	0.281	0.285	0.285	0.289	0.282	0.299	0.272
45	0.290	0.290	0.282	0.318	0.339	0.314	0.313	0.282	0.284	0.276	0.327	0.279	0.297	0.299
46	0.301	0.292	0.275	0.293	0.294	0.304	0.317	0.271	0.288	0.284	0.333	0.277	0.314	0.284
47	0.309	0.274	0.276	0.294	0.300	0.310	0.314	0.321	0.283	0.277	0.284	0.307	0.318	0.272
48	0.348	0.280	0.281	0.302	0.336	0.335	0.289	0.323	0.279	0.285	0.287	0.281	0.281	0.294
49	0.301	0.289	0.283	0.331	0.331	0.306	0.299	0.330	0.281	0.290	0.293	0.307	0.299	0.287
50	0.304	0.290	0.287	0.307	0.331	0.304	0.299	0.304	0.291	0.315	0.297	0.307	0.318	0.282
51	0.278	0.296	0.278	0.310	0.326	0.304	0.296	0.307	0.286	0.282	0.308	0.278	0.315	0.287
52	0.296	0.322	0.279	0.339	0.333	0.309	0.298	0.322	0.287	0.278	0.285	0.306	0.294	0.272
53	0.302	0.294	0.281	0.302	0.308	0.311	0.307	0.331	0.302	0.287	0.298	0.276	0.316	0.276
54	0.305	0.272	0.282	0.300	0.308	0.313	0.295	0.305	0.319	0.303	0.285	0.279	0.316	0.287
55	0.288	0.283	0.283	0.274	0.326	0.310	0.299	0.307	0.325	0.290	0.299	0.303	0.304	0.278
56	0.307	0.290	0.311	0.273	0.318	0.312	0.307	0.323	0.309	0.300	0.301	0.295	0.297	0.281
57	0.315	0.280	0.326	0.273	0.335	0.303	0.307	0.326	0.319	0.288	0.297	0.289	0.291	0.282
58	0.317	0.307	0.320	0.282	0.334	0.315	0.315	0.330	0.298	0.285	0.303	0.274	0.320	0.287
59	0.316	0.302	0.307	0.276	0.297	0.299	0.288	0.322	0.311	0.308	0.310	0.306	0.327	0.287
60	0.317	0.272	0.308	0.313	0.300	0.301	0.293	0.321	0.283	0.307	0.312	0.277	0.298	0.283
61	0.314	0.312	0.302	0.320	0.297	0.307	0.331	0.321	0.299	0.286	0.308	0.282	0.302	0.273
62	0.316	0.313	0.308	0.318	0.309	0.296	0.330	0.307	0.279	0.296	0.301	0.293	0.334	0.300
63	0.319	0.299	0.290	0.313	0.308	0.295	0.295	0.310	0.297	0.313	0.300	0.292	0.328	0.292
64	0.331	0.274	0.275	0.306	0.303	0.335	0.323	0.310	0.321	0.284	0.305	0.296	0.319	0.281
65	0.333	0.323	0.273	0.306	0.311	0.345	0.321	0.308	0.321	0.298	0.301	0.304	0.314	0.297
66	0.317	0.325	0.286	0.311	0.312	0.340	0.318	0.309	0.287	0.310	0.298	0.304	0.301	0.290
67	0.302	0.324	0.308	0.313	0.321	0.297	0.313	0.315	0.292	0.288	0.297	0.314	0.295	0.305

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF7B Component ID. Lowest Reading 0.270 Highest reading 0.348

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.334	0.300	0.310	0.317	0.310	0.293	0.309	0.314	0.314	0.298	0.296	0.306	0.276	0.305
69	0.306	0.276	0.284	0.309	0.278	0.299	0.307	0.322	0.330	0.303	0.296	0.297	0.302	0.321
70	0.307	0.300	0.311	0.309	0.334	0.305	0.307	0.323	0.333	0.302	0.339	0.296	0.334	0.306
71	0.331	0.327	0.313	0.310	0.272	0.293	0.333	0.330	0.331	0.311	0.296	0.303	0.307	0.318
72	0.341	0.311	0.314	0.295	0.340	0.322	0.328	0.333	0.330	0.329	0.318	0.278	0.308	0.287
73	0.318	0.322	0.295	0.299	0.312	0.320	0.331	0.321	0.267	0.347	0.315	0.282	0.292	0.304
74	0.343	0.319	0.298	0.300	0.314	0.318	0.328	0.323	0.299	0.321	0.285	0.271	0.297	0.283

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF8T Component ID. Lowest Reading 0.240 Highest reading 0.356

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.322	0.327	0.295	0.282	0.298	0.285	0.353	0.291	0.338	0.325	0.267	0.303	0.299	0.289
2	0.333	0.330	0.286	0.281	0.296	0.283	0.354	0.298	0.340	0.324	0.250	0.264	0.301	0.288
3	0.298	0.322	0.290	0.289	0.299	0.293	0.350	0.274	0.269	0.289	0.298	0.311	0.296	0.287
4	0.304	0.320	0.308	0.260	0.318	0.272	0.322	0.283	0.305	0.289	0.305	0.290	0.296	0.286
5	0.331	0.318	0.308	0.269	0.318	0.296	0.321	0.296	0.324	0.295	0.302	0.290	0.303	0.282
6	0.315	0.318	0.290	0.297	0.269	0.282	0.317	0.298	0.298	0.292	0.311	0.289	0.300	0.282
7	0.295	0.325	0.290	0.268	0.270	0.305	0.314	0.297	0.286	0.299	0.310	0.289	0.296	0.286
8	0.297	0.328	0.289	0.268	0.270	0.289	0.317	0.275	0.262	0.288	0.350	0.289	0.297	0.287
9	0.312	0.344	0.292	0.273	0.298	0.292	0.314	0.277	0.282	0.300	0.344	0.311	0.297	0.289
10	0.297	0.333	0.292	0.328	0.288	0.263	0.328	0.251	0.296	0.315	0.344	0.319	0.301	0.269
11	0.335	0.322	0.294	0.333	0.285	0.262	0.333	0.284	0.308	0.276	0.295	0.318	0.303	0.272
12	0.282	0.290	0.291	0.277	0.285	0.276	0.330	0.264	0.289	0.261	0.298	0.305	0.319	0.274
13	0.282	0.304	0.306	0.274	0.274	0.269	0.325	0.295	0.300	0.276	0.263	0.312	0.306	0.277
14	0.267	0.262	0.308	0.276	0.276	0.244	0.328	0.298	0.299	0.308	0.289	0.309	0.321	0.282
15	0.272	0.311	0.299	0.277	0.281	0.252	0.283	0.265	0.288	0.281	0.304	0.341	0.291	0.332
16	0.296	0.315	0.297	0.298	0.277	0.263	0.319	0.268	0.306	0.283	0.306	0.298	0.303	0.341
17	0.292	0.309	0.306	0.298	0.279	0.263	0.313	0.271	0.306	0.279	0.278	0.289	0.276	0.336
18	0.287	0.311	0.329	0.285	0.293	0.279	0.330	0.272	0.312	0.310	0.349	0.287	0.297	0.335
19	0.298	0.304	0.277	0.290	0.298	0.302	0.321	0.267	0.313	0.302	0.298	0.295	0.297	0.287
20	0.298	0.308	0.286	0.310	0.286	0.303	0.325	0.280	0.246	0.293	0.336	0.319	0.280	0.323
21	0.314	0.319	0.300	0.283	0.285	0.251	0.322	0.298	0.337	0.292	0.336	0.303	0.289	0.298
22	0.336	0.328	0.321	0.270	0.287	0.260	0.315	0.294	0.337	0.288	0.302	0.303	0.280	0.283
23	0.313	0.335	0.325	0.277	0.290	0.278	0.312	0.291	0.308	0.281	0.298	0.312	0.288	0.283
24	0.299	0.330	0.313	0.298	0.282	0.262	0.332	0.290	0.306	0.314	0.265	0.306	0.279	0.335
25	0.327	0.317	0.316	0.298	0.298	0.257	0.307	0.288	0.335	0.302	0.316	0.301	0.298	0.295
26	0.299	0.332	0.321	0.292	0.288	0.258	0.298	0.314	0.336	0.297	0.314	0.334	0.313	0.270
27	0.297	0.298	0.286	0.292	0.288	0.290	0.305	0.322	0.292	0.302	0.296	0.334	0.313	0.267
28	0.296	0.303	0.296	0.279	0.296	0.286	0.278	0.292	0.290	0.314	0.297	0.310	0.273	0.267
29	0.342	0.322	0.295	0.281	0.263	0.290	0.261	0.268	0.308	0.329	0.298	0.278	0.274	0.296
30	0.336	0.318	0.311	0.280	0.283	0.311	0.289	0.292	0.290	0.274	0.296	0.278	0.269	0.332
31	0.283	0.348	0.319	0.300	0.299	0.319	0.270	0.294	0.296	0.242	0.297	0.260	0.288	0.293
32	0.298	0.320	0.326	0.300	0.269	0.298	0.270	0.314	0.290	0.269	0.299	0.276	0.280	0.267
33	0.281	0.321	0.298	0.302	0.283	0.262	0.319	0.288	0.321	0.268	0.319	0.277	0.285	0.267
34	0.274	0.320	0.288	0.305	0.298	0.284	0.314	0.297	0.311	0.279	0.306	0.279	0.287	0.293
35	0.290	0.321	0.297	0.286	0.287	0.266	0.310	0.286	0.309	0.279	0.342	0.279	0.280	0.289
36	0.353	0.321	0.323	0.333	0.289	0.264	0.309	0.289	0.310	0.280	0.304	0.289	0.308	0.299
37	0.354	0.318	0.324	0.335	0.288	0.265	0.289	0.309	0.310	0.280	0.295	0.279	0.341	0.299
38	0.345	0.318	0.346	0.333	0.282	0.288	0.289	0.315	0.312	0.279	0.268	0.284	0.286	0.341
39	0.333	0.320	0.346	0.333	0.292	0.293	0.287	0.298	0.311	0.280	0.299	0.284	0.314	0.336
40	0.331	0.321	0.346	0.308	0.302	0.297	0.289	0.315	0.315	0.291	0.297	0.285	0.316	0.338
41	0.331	0.319	0.345	0.290	0.272	0.267	0.279	0.301	0.318	0.278	0.263	0.262	0.287	0.305
42	0.338	0.322	0.310	0.288	0.286	0.305	0.279	0.273	0.318	0.277	0.287	0.336	0.297	0.279
43	0.337	0.323	0.311	0.288	0.258	0.273	0.296	0.273	0.317	0.274	0.281	0.322	0.289	0.277
44	0.334	0.322	0.292	0.287	0.298	0.309	0.293	0.274	0.315	0.282	0.306	0.323	0.314	0.275
45	0.329	0.323	0.291	0.287	0.306	0.249	0.316	0.275	0.316	0.279	0.323	0.298	0.313	0.275
46	0.289	0.322	0.292	0.287	0.296	0.291	0.290	0.276	0.317	0.279	0.285	0.278	0.337	0.275
47	0.288	0.314	0.279	0.262	0.298	0.299	0.278	0.276	0.320	0.279	0.284	0.299	0.287	0.274
48	0.332	0.355	0.279	0.289	0.289	0.305	0.276	0.298	0.324	0.289	0.283	0.301	0.339	0.273
49	0.333	0.356	0.279	0.289	0.291	0.327	0.279	0.287	0.323	0.289	0.282	0.309	0.270	0.271
50	0.332	0.316	0.279	0.313	0.295	0.305	0.251	0.286	0.309	0.296	0.282	0.310	0.269	0.313
51	0.302	0.301	0.280	0.311	0.296	0.278	0.262	0.277	0.309	0.284	0.285	0.306	0.284	0.313
52	0.301	0.300	0.280	0.286	0.276	0.298	0.264	0.274	0.310	0.284	0.286	0.303	0.272	0.290
53	0.301	0.299	0.280	0.285	0.272	0.298	0.248	0.278	0.303	0.350	0.287	0.302	0.313	0.287
54	0.302	0.302	0.281	0.309	0.246	0.287	0.254	0.279	0.285	0.300	0.292	0.303	0.337	0.311
55	0.304	0.304	0.281	0.285	0.247	0.288	0.249	0.276	0.289	0.300	0.293	0.303	0.271	0.311
56	0.305	0.306	0.282	0.285	0.249	0.279	0.264	0.276	0.298	0.305	0.290	0.303	0.278	0.264
57	0.305	0.306	0.283	0.308	0.244	0.279	0.288	0.274	0.285	0.292	0.291	0.295	0.289	0.289
58	0.304	0.337	0.282	0.262	0.240	0.278	0.267	0.292	0.298	0.293	0.292	0.290	0.298	0.284
59	0.303	0.336	0.280	0.285	0.285	0.290	0.265	0.269	0.282	0.297	0.293	0.293	0.278	0.288
60	0.315	0.311	0.281	0.289	0.288	0.297	0.262	0.270	0.280	0.298	0.290	0.298	0.289	0.286

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF8B Component ID. Lowest Reading 0.263 Highest reading 0.352

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.313	0.307	0.304	0.307	0.333	0.315	0.343	0.310	0.312	0.338	0.333	0.334	0.305	0.285
2	0.314	0.299	0.332	0.313	0.333	0.315	0.337	0.309	0.310	0.315	0.330	0.332	0.306	0.276
3	0.266	0.301	0.305	0.302	0.334	0.333	0.328	0.296	0.314	0.327	0.329	0.339	0.307	0.305
4	0.313	0.308	0.305	0.302	0.294	0.316	0.331	0.312	0.339	0.304	0.329	0.325	0.308	0.304
5	0.326	0.301	0.319	0.270	0.304	0.318	0.328	0.291	0.337	0.312	0.352	0.331	0.306	0.287
6	0.324	0.305	0.319	0.267	0.301	0.318	0.330	0.343	0.342	0.343	0.324	0.341	0.304	0.302
7	0.329	0.297	0.318	0.316	0.300	0.336	0.322	0.342	0.321	0.292	0.329	0.324	0.335	0.330
8	0.316	0.304	0.312	0.296	0.321	0.332	0.317	0.344	0.323	0.290	0.333	0.319	0.336	0.330
9	0.313	0.278	0.318	0.344	0.282	0.331	0.310	0.307	0.329	0.289	0.336	0.328	0.272	0.286
10	0.339	0.304	0.309	0.338	0.290	0.326	0.310	0.342	0.322	0.290	0.327	0.326	0.332	0.290
11	0.304	0.303	0.323	0.318	0.300	0.325	0.310	0.312	0.320	0.289	0.326	0.334	0.263	0.294
12	0.306	0.304	0.319	0.314	0.294	0.300	0.309	0.313	0.321	0.294	0.326	0.294	0.296	0.307
13	0.305	0.279	0.303	0.320	0.327	0.331	0.322	0.307	0.341	0.325	0.331	0.290	0.334	0.308
14	0.302	0.282	0.302	0.327	0.341	0.325	0.327	0.282	0.318	0.295	0.328	0.284	0.297	0.304
15	0.301	0.282	0.287	0.322	0.319	0.308	0.325	0.306	0.318	0.275	0.330	0.282	0.309	0.292
16	0.297	0.312	0.298	0.322	0.322	0.308	0.325	0.282	0.332	0.292	0.332	0.283	0.309	0.326
17	0.297	0.341	0.306	0.334	0.341	0.309	0.325	0.304	0.328	0.289	0.308	0.295	0.309	0.315
18	0.299	0.298	0.296	0.321	0.321	0.331	0.325	0.313	0.309	0.306	0.307	0.299	0.279	0.342
19	0.325	0.323	0.298	0.328	0.340	0.328	0.331	0.311	0.317	0.338	0.296	0.326	0.350	0.295
20	0.300	0.312	0.347	0.324	0.332	0.312	0.345	0.295	0.317	0.308	0.297	0.293	0.301	0.336
21	0.304	0.317	0.342	0.321	0.335	0.311	0.344	0.295	0.312	0.305	0.296	0.328	0.316	0.312
22	0.300	0.320	0.293	0.321	0.323	0.343	0.350	0.295	0.315	0.304	0.296	0.325	0.307	0.339
23	0.293	0.320	0.291	0.314	0.332	0.288	0.298	0.321	0.314	0.308	0.294	0.327	0.295	0.305
24	0.297	0.319	0.295	0.316	0.302	0.292	0.298	0.297	0.312	0.333	0.293	0.349	0.295	0.304
25	0.300	0.310	0.296	0.325	0.346	0.293	0.309	0.297	0.310	0.332	0.297	0.325	0.299	0.304
26	0.300	0.322	0.327	0.311	0.300	0.265	0.300	0.297	0.312	0.332	0.300	0.321	0.317	0.326
27	0.322	0.332	0.319	0.322	0.300	0.331	0.297	0.303	0.312	0.295	0.303	0.329	0.317	0.344
28	0.325	0.345	0.323	0.331	0.301	0.315	0.293	0.305	0.328	0.297	0.301	0.300	0.318	0.279
29	0.325	0.337	0.332	0.324	0.305	0.308	0.302	0.305	0.321	0.331	0.298	0.305	0.317	0.319
30	0.301	0.331	0.320	0.328	0.338	0.308	0.302	0.302	0.328	0.323	0.300	0.305	0.337	0.338
31	0.307	0.334	0.326	0.323	0.337	0.348	0.304	0.309	0.325	0.319	0.323	0.304	0.345	0.316
32	0.308	0.333	0.323	0.328	0.339	0.328	0.302	0.315	0.324	0.328	0.336	0.300	0.288	0.330
33	0.300	0.343	0.310	0.337	0.300	0.335	0.299	0.319	0.326	0.319	0.308	0.351	0.290	0.333
34	0.326	0.326	0.341	0.335	0.331	0.333	0.299	0.320	0.344	0.322	0.310	0.314	0.320	0.322
35	0.327	0.310	0.315	0.332	0.324	0.328	0.296	0.320	0.331	0.318	0.316	0.289	0.336	0.319
36	0.321	0.309	0.317	0.328	0.323	0.334	0.321	0.317	0.332	0.317	0.312	0.325	0.301	0.328
37	0.285	0.308	0.317	0.344	0.326	0.330	0.315	0.318	0.335	0.319	0.315	0.332	0.301	0.310
38	0.284	0.311	0.314	0.321	0.326	0.324	0.321	0.318	0.334	0.325	0.281	0.326	0.306	0.324
39	0.286	0.312	0.328	0.325	0.329	0.335	0.317	0.328	0.332	0.294	0.314	0.336	0.306	0.316
40	0.324	0.313	0.311	0.324	0.333	0.316	0.316	0.324	0.311	0.294	0.313	0.329	0.307	0.338
41	0.341	0.314	0.310	0.351	0.330	0.319	0.313	0.323	0.316	0.296	0.313	0.328	0.329	0.301
42	0.303	0.318	0.311	0.327	0.326	0.317	0.339	0.323	0.322	0.302	0.323	0.328	0.329	0.326
43	0.302	0.312	0.326	0.330	0.323	0.328	0.333	0.321	0.319	0.335	0.328	0.330	0.327	0.326
44	0.299	0.316	0.321	0.324	0.325	0.328	0.332	0.319	0.309	0.312	0.345	0.330	0.323	0.325
45	0.297	0.312	0.309	0.326	0.325	0.334	0.317	0.326	0.306	0.311	0.342	0.318	0.307	0.326
46	0.297	0.340	0.311	0.324	0.320	0.331	0.320	0.328	0.327	0.309	0.315	0.317	0.321	0.331
47	0.297	0.318	0.308	0.327	0.315	0.334	0.322	0.333	0.350	0.306	0.316	0.313	0.319	0.346
48	0.292	0.328	0.337	0.331	0.290	0.329	0.328	0.331	0.290	0.305	0.317	0.317	0.320	0.335
49	0.294	0.332	0.305	0.329	0.292	0.323	0.327	0.330	0.286	0.333	0.318	0.320	0.321	0.314
50	0.332	0.325	0.320	0.322	0.293	0.321	0.333	0.333	0.297	0.335	0.329	0.319	0.318	0.322
51	0.323	0.322	0.321	0.320	0.314	0.321	0.323	0.331	0.298	0.341	0.331	0.328	0.319	0.333
52	0.323	0.346	0.306	0.320	0.317	0.321	0.323	0.335	0.299	0.341	0.328	0.330	0.319	0.339
53	0.282	0.325	0.315	0.322	0.319	0.333	0.326	0.321	0.300	0.284	0.303	0.316	0.324	0.339
54	0.334	0.319	0.324	0.324	0.346	0.323	0.330	0.301	0.300	0.283	0.304	0.324	0.327	0.326
55	0.327	0.320	0.321	0.325	0.324	0.318	0.330	0.305	0.293	0.283	0.305	0.330	0.323	0.324
56	0.322	0.327	0.320	0.325	0.320	0.317	0.329	0.307	0.298	0.345	0.319	0.322	0.347	0.328
57	0.303	0.341	0.317	0.324	0.317	0.314	0.346	0.313	0.294	0.322	0.323	0.322	0.319	0.327
58	0.316	0.334	0.313	0.326	0.321	0.322	0.341	0.307	0.321	0.319	0.322	0.338	0.304	0.311
59	0.347	0.328	0.325	0.321	0.348	0.319	0.318	0.341	0.328	0.348	0.325	0.308	0.322	0.309
60	0.317	0.302	0.316	0.313	0.347	0.318	0.318	0.311	0.268	0.336	0.290	0.306	0.335	0.313

Unit: Salem 1 RFO 20 Date: 04/14/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF9B Component ID. Lowest Reading 0.291 Highest reading 0.371

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.326	0.322	0.322	0.362	0.317	0.312	0.315	0.322	0.346	0.323	0.330	0.322	0.322	0.318
2	0.355	0.352	0.311	0.360	0.324	0.337	0.318	0.337	0.326	0.291	0.330	0.318	0.356	0.330
3	0.344	0.319	0.314	0.334	0.318	0.323	0.313	0.323	0.318	0.321	0.328	0.326	0.320	0.327
4	0.343	0.335	0.338	0.354	0.319	0.332	0.313	0.318	0.334	0.320	0.339	0.332	0.316	0.331
5	0.336	0.319	0.316	0.353	0.316	0.333	0.314	0.329	0.331	0.320	0.343	0.322	0.337	0.333
6	0.318	0.320	0.311	0.350	0.341	0.321	0.320	0.318	0.316	0.319	0.344	0.317	0.329	0.325
7	0.323	0.307	0.351	0.343	0.314	0.354	0.325	0.348	0.337	0.320	0.344	0.321	0.341	0.316
8	0.321	0.340	0.314	0.328	0.326	0.354	0.323	0.335	0.339	0.321	0.339	0.322	0.323	0.312
9	0.319	0.337	0.312	0.325	0.324	0.341	0.335	0.320	0.316	0.316	0.325	0.317	0.319	0.356
10	0.364	0.336	0.353	0.327	0.326	0.353	0.335	0.342	0.313	0.308	0.360	0.329	0.323	0.311
11	0.353	0.356	0.352	0.335	0.317	0.317	0.334	0.353	0.330	0.308	0.325	0.347	0.338	0.298
12	0.363	0.328	0.311	0.326	0.329	0.336	0.314	0.342	0.325	0.306	0.324	0.329	0.364	0.303
13	0.325	0.346	0.324	0.359	0.312	0.348	0.348	0.363	0.326	0.350	0.293	0.322	0.331	0.316
14	0.320	0.345	0.315	0.352	0.338	0.322	0.309	0.365	0.329	0.315	0.369	0.320	0.362	0.326
15	0.318	0.351	0.341	0.327	0.341	0.346	0.309	0.322	0.330	0.313	0.301	0.319	0.329	0.331
16	0.306	0.321	0.364	0.354	0.347	0.324	0.326	0.306	0.334	0.315	0.302	0.319	0.328	0.358
17	0.316	0.331	0.365	0.330	0.363	0.316	0.312	0.313	0.319	0.319	0.304	0.328	0.322	0.322
18	0.331	0.314	0.315	0.369	0.353	0.343	0.310	0.357	0.316	0.320	0.306	0.327	0.342	0.311
19	0.347	0.322	0.320	0.341	0.321	0.330	0.312	0.324	0.314	0.318	0.307	0.331	0.332	0.322
20	0.362	0.314	0.313	0.338	0.321	0.360	0.306	0.313	0.315	0.328	0.307	0.329	0.324	0.325
21	0.321	0.316	0.368	0.354	0.332	0.321	0.311	0.333	0.314	0.331	0.335	0.328	0.361	0.328
22	0.311	0.312	0.313	0.323	0.344	0.357	0.324	0.326	0.319	0.330	0.332	0.321	0.359	0.329
23	0.344	0.335	0.308	0.324	0.317	0.317	0.324	0.322	0.318	0.324	0.336	0.322	0.329	0.343
24	0.343	0.344	0.310	0.316	0.339	0.320	0.335	0.321	0.320	0.320	0.317	0.315	0.332	0.329
25	0.342	0.352	0.307	0.335	0.320	0.315	0.322	0.324	0.319	0.318	0.336	0.334	0.333	0.343
26	0.314	0.306	0.361	0.327	0.321	0.313	0.331	0.327	0.323	0.321	0.324	0.335	0.335	0.337
27	0.314	0.321	0.310	0.331	0.328	0.331	0.318	0.314	0.321	0.319	0.316	0.332	0.323	0.335
28	0.313	0.312	0.352	0.317	0.364	0.316	0.314	0.309	0.325	0.326	0.319	0.330	0.320	0.312
29	0.334	0.329	0.357	0.322	0.329	0.326	0.315	0.362	0.336	0.329	0.321	0.325	0.325	0.368
30	0.312	0.324	0.346	0.361	0.339	0.335	0.347	0.331	0.338	0.328	0.304	0.322	0.335	0.322
31	0.305	0.314	0.350	0.313	0.334	0.369	0.352	0.329	0.336	0.330	0.304	0.312	0.332	0.314
32	0.316	0.348	0.317	0.365	0.327	0.327	0.360	0.313	0.328	0.331	0.308	0.311	0.330	0.312
33	0.314	0.330	0.307	0.359	0.335	0.320	0.304	0.327	0.328	0.332	0.324	0.316	0.371	0.327
34	0.318	0.340	0.313	0.322	0.325	0.321	0.330	0.317	0.317	0.325	0.320	0.325	0.315	0.322
35	0.353	0.350	0.300	0.319	0.341	0.312	0.327	0.321	0.357	0.330	0.320	0.328	0.369	0.308
36	0.359	0.349	0.329	0.317	0.348	0.314	0.322	0.321	0.322	0.339	0.321	0.324	0.359	0.320
37	0.317	0.343	0.315	0.326	0.325	0.363	0.325	0.365	0.324	0.338	0.327	0.326	0.370	0.335
38	0.312	0.334	0.360	0.350	0.331	0.314	0.324	0.304	0.319	0.341	0.317	0.321	0.327	0.339
39	0.325	0.350	0.335	0.316	0.308	0.313	0.312	0.332	0.323	0.329	0.320	0.324	0.327	0.322
40	0.321	0.341	0.308	0.353	0.308	0.317	0.345	0.319	0.321	0.334	0.317	0.325	0.335	0.329
41	0.344	0.324	0.310	0.320	0.309	0.333	0.352	0.310	0.330	0.364	0.343	0.366	0.328	0.330
42	0.318	0.324	0.306	0.351	0.318	0.358	0.314	0.317	0.322	0.351	0.340	0.362	0.366	0.336
43	0.342	0.354	0.347	0.345	0.364	0.318	0.316	0.303	0.322	0.319	0.339	0.371	0.336	0.338
44	0.317	0.335	0.318	0.328	0.327	0.315	0.313	0.306	0.351	0.354	0.328	0.368	0.331	0.336
45	0.341	0.358	0.322	0.355	0.326	0.323	0.315	0.330	0.319	0.330	0.327	0.324	0.335	0.324
46	0.331	0.327	0.323	0.306	0.322	0.316	0.330	0.303	0.323	0.326	0.342	0.354	0.343	0.326
47	0.325	0.323	0.319	0.317	0.328	0.311	0.323	0.316	0.333	0.323	0.331	0.370	0.334	0.320
48	0.340	0.317	0.295	0.313	0.329	0.324	0.345	0.306	0.316	0.362	0.323	0.369	0.328	0.332
49	0.351	0.321	0.317	0.308	0.359	0.326	0.327	0.313	0.322	0.347	0.342	0.355	0.322	0.324
50	0.333	0.313	0.346	0.344	0.327	0.325	0.328	0.311	0.320	0.345	0.339	0.325	0.364	0.332
51	0.325	0.311	0.310	0.312	0.317	0.333	0.336	0.324	0.319	0.328	0.324	0.344	0.356	0.318
52	0.324	0.305	0.306	0.315	0.319	0.360	0.331	0.307	0.321	0.337	0.323	0.340	0.356	0.319
53	0.318	0.320	0.343	0.303	0.318	0.346	0.334	0.302	0.310	0.324	0.324	0.320	0.370	0.319
54	0.321	0.327	0.348	0.332	0.362	0.351	0.327	0.367	0.312	0.331	0.345	0.324	0.358	0.321
55	0.335	0.327	0.317	0.360	0.323	0.348	0.355	0.361	0.320	0.324	0.324	0.358	0.321	0.313
56	0.327	0.334	0.299	0.319	0.317	0.326	0.334	0.359	0.305	0.333	0.334	0.348	0.364	0.325
57	0.329	0.324	0.331	0.326	0.330	0.324	0.319	0.369	0.353	0.341	0.328	0.331	0.330	0.317
58	0.338	0.330	0.365	0.328	0.340	0.358	0.326	0.320	0.355	0.342	0.333	0.330	0.337	0.327
59	0.356	0.346	0.316	0.325	0.336	0.318	0.323	0.319	0.325	0.322	0.338	0.316	0.363	0.323
60	0.328	0.332	0.322	0.338	0.345	0.312	0.356	0.330	0.314	0.327	0.332	0.354	0.339	0.330
61	0.338	0.340	0.328	0.332	0.352	0.365	0.313	0.326	0.318	0.327	0.329	0.311	0.370	0.327
62	0.359	0.335	0.333	0.328	0.341	0.335	0.364	0.320	0.310	0.338	0.361	0.328	0.331	0.330
63	0.333	0.321	0.350	0.332	0.333	0.336	0.332	0.320	0.344	0.358	0.327	0.324	0.329	0.347
64	0.333	0.329	0.348	0.335	0.328	0.341	0.330	0.312	0.339	0.328	0.328	0.368	0.325	0.337
65	0.333	0.366	0.321	0.321	0.337	0.344	0.341	0.324	0.357	0.331	0.322	0.334	0.333	0.335
66	0.342	0.330	0.345	0.349	0.321	0.334	0.347	0.323	0.361	0.333	0.328	0.341	0.316	0.339
67	0.367	0.321	0.323	0.352	0.338	0.304	0.322	0.325	0.324	0.341	0.325	0.326	0.319	0.322

Unit: Salem 1 RFO 20 Date: 04/14/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF9B Component ID. Lowest Reading 0.291 Highest reading 0.371

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.342	0.325	0.329	0.336	0.329	0.346	0.322	0.313	0.320	0.321	0.318	0.337	0.334	0.323
69	0.356	0.330	0.332	0.323	0.339	0.331	0.321	0.316	0.311	0.322	0.326	0.342	0.324	0.326
70	0.347	0.325	0.325	0.324	0.327	0.339	0.350	0.318	0.327	0.324	0.338	0.331	0.331	0.332
71	0.325	0.322	0.364	0.337	0.335	0.322	0.320	0.325	0.317	0.327	0.330	0.354	0.333	0.331
72	0.325	0.363	0.361	0.335	0.337	0.337	0.359	0.321	0.334	0.329	0.326	0.343	0.330	0.329
73	0.322	0.358	0.314	0.339	0.359	0.334	0.319	0.325	0.316	0.322	0.323	0.331	0.326	0.320
74	0.321	0.333	0.319	0.338	0.353	0.350	0.328	0.310	0.325	0.335	0.357	0.324	0.334	0.362
75	0.335	0.360	0.363	0.338	0.321	0.337	0.364	0.330	0.313	0.329	0.331	0.323	0.340	0.315
76	0.329	0.336	0.329	0.343	0.334	0.332	0.323	0.333	0.309	0.331	0.335	0.330	0.338	0.326
77	0.361	0.351	0.321	0.333	0.325	0.319	0.309	0.323	0.371	0.322	0.349	0.336	0.340	0.342
78	0.316	0.363	0.318	0.337	0.332	0.305	0.317	0.326	0.322	0.325	0.341	0.325	0.362	0.333
79	0.319	0.339	0.334	0.339	0.326	0.367	0.315	0.327	0.322	0.337	0.330	0.340	0.341	0.342

Unit: Salem 1 RFO 20 Date: 04/14/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF13T Component ID. Lowest Reading 0.141 Highest reading 0.367

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.314	0.324	0.336	0.312	0.282	0.309	0.306	0.320	0.292	0.281	0.309	0.300	0.316	0.289
2	0.340	0.314	0.286	0.294	0.294	0.300	0.313	0.327	0.318	0.338	0.308	0.308	0.336	0.330
3	0.301	0.315	0.299	0.298	0.296	0.310	0.318	0.323	0.321	0.310	0.321	0.304	0.275	0.308
4	0.312	0.303	0.292	0.275	0.331	0.333	0.305	0.316	0.326	0.279	0.300	0.309	0.322	0.270
5	0.313	0.329	0.293	0.280	0.288	0.331	0.306	0.317	0.314	0.282	0.299	0.319	0.331	0.318
6	0.327	0.298	0.285	0.309	0.297	0.330	0.307	0.305	0.329	0.328	0.303	0.320	0.337	0.323
7	0.328	0.282	0.295	0.327	0.321	0.293	0.303	0.313	0.325	0.327	0.319	0.286	0.320	0.308
8	0.313	0.303	0.300	0.295	0.311	0.303	0.302	0.317	0.331	0.335	0.343	0.294	0.324	0.305
9	0.301	0.299	0.297	0.287	0.338	0.306	0.304	0.306	0.332	0.326	0.306	0.287	0.328	0.324
10	0.353	0.323	0.301	0.303	0.316	0.308	0.332	0.314	0.305	0.308	0.298	0.288	0.330	0.344
11	0.296	0.323	0.306	0.296	0.327	0.310	0.308	0.312	0.292	0.325	0.299	0.287	0.332	0.335
12	0.292	0.305	0.288	0.305	0.313	0.325	0.311	0.310	0.292	0.311	0.318	0.291	0.327	0.325
13	0.335	0.300	0.326	0.294	0.283	0.319	0.312	0.311	0.296	0.313	0.312	0.288	0.310	0.327
14	0.294	0.306	0.302	0.289	0.290	0.324	0.311	0.309	0.285	0.297	0.306	0.305	0.329	0.315
15	0.297	0.309	0.307	0.285	0.326	0.321	0.310	0.299	0.295	0.299	0.315	0.282	0.325	0.308
16	0.302	0.314	0.324	0.290	0.276	0.320	0.332	0.304	0.299	0.304	0.305	0.283	0.330	0.306
17	0.321	0.307	0.331	0.301	0.325	0.337	0.278	0.303	0.289	0.296	0.307	0.317	0.333	0.326
18	0.344	0.306	0.275	0.284	0.288	0.319	0.303	0.311	0.291	0.302	0.315	0.301	0.302	0.335
19	0.320	0.298	0.291	0.294	0.282	0.330	0.292	0.303	0.315	0.304	0.332	0.307	0.339	0.307
20	0.333	0.313	0.319	0.300	0.280	0.295	0.274	0.305	0.309	0.309	0.320	0.309	0.324	0.324
21	0.298	0.309	0.317	0.276	0.295	0.285	0.301	0.317	0.310	0.313	0.324	0.303	0.288	0.319
22	0.293	0.323	0.323	0.298	0.290	0.312	0.297	0.318	0.313	0.299	0.321	0.311	0.309	0.298
23	0.305	0.298	0.304	0.330	0.279	0.311	0.291	0.316	0.315	0.298	0.326	0.322	0.329	0.332
24	0.367	0.335	0.279	0.296	0.297	0.336	0.314	0.306	0.319	0.311	0.335	0.317	0.324	0.335
25	0.291	0.321	0.294	0.285	0.292	0.312	0.308	0.307	0.337	0.303	0.322	0.287	0.311	0.326
26	0.317	0.288	0.305	0.304	0.298	0.314	0.288	0.313	0.336	0.319	0.325	0.332	0.321	0.337
27	0.330	0.298	0.314	0.290	0.305	0.307	0.312	0.307	0.328	0.321	0.321	0.312	0.306	0.316
28	0.313	0.321	0.307	0.291	0.324	0.306	0.313	0.304	0.326	0.326	0.286	0.313	0.314	0.332
29	0.299	0.301	0.297	0.282	0.298	0.322	0.288	0.294	0.324	0.335	0.290	0.281	0.318	0.320
30	0.295	0.289	0.285	0.293	0.289	0.306	0.318	0.296	0.330	0.318	0.288	0.290	0.337	0.284
31	0.279	0.300	0.280	0.304	0.297	0.305	0.317	0.299	0.309	0.324	0.333	0.295	0.315	0.307
32	0.316	0.279	0.291	0.301	0.311	0.269	0.307	0.296	0.319	0.313	0.321	0.288	0.285	0.314
33	0.306	0.302	0.298	0.302	0.278	0.301	0.312	0.325	0.324	0.287	0.324	0.275	0.284	0.292
34	0.278	0.297	0.308	0.304	0.297	0.287	0.313	0.312	0.322	0.315	0.300	0.279	0.294	0.290
35	0.292	0.299	0.306	0.307	0.298	0.314	0.308	0.284	0.326	0.300	0.336	0.281	0.332	0.339
36	0.285	0.274	0.298	0.311	0.308	0.311	0.284	0.323	0.327	0.320	0.313	0.302	0.268	0.270
37	0.316	0.298	0.308	0.344	0.288	0.283	0.297	0.315	0.325	0.282	0.309	0.329	0.292	0.293
38	0.325	0.307	0.316	0.299	0.291	0.274	0.316	0.320	0.292	0.283	0.312	0.319	0.304	0.320
39	0.283	0.277	0.281	0.310	0.306	0.285	0.338	0.333	0.285	0.284	0.326	0.308	0.288	0.296
40	0.285	0.293	0.309	0.299	0.289	0.295	0.321	0.290	0.287	0.298	0.332	0.314	0.281	0.294
41	0.316	0.299	0.311	0.321	0.292	0.299	0.329	0.332	0.287	0.312	0.302	0.330	0.310	0.272
42	0.268	0.300	0.312	0.324	0.291	0.305	0.333	0.324	0.332	0.317	0.307	0.315	0.280	0.303
43	0.279	0.298	0.313	0.300	0.315	0.308	0.338	0.325	0.299	0.310	0.311	0.316	0.287	0.318
44	0.301	0.279	0.318	0.332	0.311	0.311	0.315	0.334	0.297	0.326	0.314	0.325	0.298	0.303
45	0.280	0.339	0.328	0.294	0.312	0.312	0.334	0.333	0.305	0.325	0.339	0.337	0.270	0.301
46	0.278	0.300	0.330	0.285	0.327	0.291	0.335	0.319	0.339	0.281	0.307	0.321	0.333	0.297
47	0.312	0.175	0.224	0.242	0.212	0.262	0.245	0.179	0.161	0.164	0.194	0.225	0.223	0.216
48	0.309	0.311	0.215	0.247	0.186	0.255	0.200	0.194	0.225	0.243	0.245	0.226	0.222	0.207
49	0.300	0.321	0.212	0.248	0.200	0.265	0.184	0.171	0.192	0.176	0.230	0.219	0.215	0.183
50	0.295	0.306	0.244	0.225	0.193	0.253	0.181	0.144	0.179	0.178	0.209	0.218	0.217	0.174
51	0.244	0.276	0.305	0.239	0.209	0.247	0.167	0.149	0.177	0.177	0.193	0.217	0.209	0.246
52	0.237	0.251	0.190	0.283	0.230	0.228	0.143	0.154	0.164	0.192	0.197	0.278	0.236	0.190
53	0.257	0.222	0.220	0.237	0.243	0.163	0.143	0.192	0.239	0.192	0.201	0.214	0.240	0.190
54	0.145	0.266	0.256	0.235	0.222	0.190	0.169	0.195	0.154	0.184	0.214	0.214	0.272	0.167
55	0.154	0.235	0.257	0.262	0.262	0.206	0.165	0.164	0.146	0.175	0.225	0.208	0.230	0.190
56	0.244	0.193	0.261	0.237	0.273	0.201	0.156	0.189	0.191	0.193	0.220	0.199	0.228	0.178
57	0.218	0.189	0.192	0.231	0.261	0.199	0.177	0.182	0.158	0.202	0.223	0.182	0.218	0.174
58	0.198	0.235	0.195	0.202	0.167	0.259	0.165	0.169	0.176	0.214	0.204	0.191	0.219	0.179
59	0.209	0.212	0.250	0.190	0.226	0.223	0.198	0.176	0.164	0.196	0.268	0.216	0.217	0.219
60	0.216	0.229	0.262	0.160	0.152	0.217	0.179	0.185	0.237	0.209	0.228	0.208	0.175	0.222
61	0.234	0.248	0.147	0.141	0.236	0.252	0.169	0.174	0.178	0.224	0.212	0.205	0.209	0.230
62	0.220	0.242	0.264	0.174	0.245	0.206	0.185	0.198	0.171	0.221	0.230	0.201	0.224	0.220
63	0.227	0.231	0.187	0.178	0.188	0.189	0.187	0.200	0.186	0.207	0.219	0.198	0.224	0.233
64	0.223	0.222	0.225	0.197	0.239	0.207	0.210	0.171	0.199	0.207	0.242	0.215	0.224	0.228
65	0.193	0.248	0.203	0.202	0.201	0.197	0.201	0.170	0.205	0.193	0.227	0.233	0.217	0.226
66	0.185	0.280	0.245	0.206	0.194	0.234	0.190	0.170	0.190	0.198	0.205	0.238	0.225	0.232
67	0.187	0.240	0.240	0.192	0.175	0.223	0.206	0.169	0.188	0.212	0.208	0.224	0.219	0.225

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Unit: Salem 1 RFO 20 Date: 04/14/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF13T Component ID. Lowest Reading 0.141 Highest reading 0.367

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
68	0.180	0.232	0.149	0.209	0.222	0.221	0.228	0.207	0.195	0.200	0.214	0.234	0.232	0.224
69	0.189	0.204	0.234	0.190	0.226	0.222	0.195	0.165	0.200	0.205	0.228	0.240	0.239	0.243
70	0.253	0.291	0.254	0.306	0.299	0.279	0.282	0.288	0.321	0.291	0.311	0.284	0.299	0.277
71	0.301	0.288	0.284	0.284	0.273	0.275	0.286	0.303	0.326	0.306	0.298	0.327	0.302	0.282
72	0.306	0.285	0.297	0.303	0.335	0.317	0.304	0.301	0.324	0.313	0.293	0.287	0.314	0.310
73	0.285	0.305	0.295	0.281	0.291	0.291	0.292	0.296	0.294	0.332	0.289	0.298	0.317	0.308
74	0.294	0.283	0.312	0.328	0.280	0.295	0.309	0.269	0.295	0.331	0.285	0.301	0.301	0.285
75	0.293	0.292	0.324	0.303	0.332	0.305	0.280	0.302	0.302	0.296	0.279	0.304	0.298	0.295
76	0.283	0.276	0.311	0.284	0.288	0.309	0.284	0.303	0.277	0.304	0.282	0.309	0.301	0.298
77	0.289	0.278	0.308	0.306	0.277	0.290	0.270	0.290	0.275	0.277	0.281	0.315	0.302	0.300
78	0.278	0.287	0.291	0.292	0.318	0.292	0.272	0.288	0.290	0.278	0.326	0.304	0.305	0.291
79	0.304	0.280	0.312	0.325	0.285	0.326	0.304	0.323	0.310	0.291	0.324	0.300	0.280	0.298

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Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF14B Component ID. Lowest Reading 0.271 Highest reading 0.344

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.306	0.339	0.339	0.291	0.292	0.303	0.298	0.294	0.335	0.305	0.282	0.316	0.285	0.302
2	0.290	0.297	0.328	0.321	0.292	0.336	0.296	0.290	0.274	0.299	0.300	0.307	0.299	0.299
3	0.298	0.291	0.294	0.308	0.290	0.304	0.293	0.294	0.273	0.307	0.335	0.306	0.298	0.279
4	0.301	0.292	0.291	0.309	0.299	0.291	0.298	0.277	0.306	0.306	0.321	0.277	0.294	0.290
5	0.299	0.331	0.301	0.340	0.293	0.293	0.293	0.290	0.304	0.299	0.321	0.275	0.294	0.318
6	0.289	0.279	0.296	0.339	0.305	0.294	0.293	0.302	0.281	0.294	0.326	0.298	0.295	0.323
7	0.309	0.273	0.314	0.320	0.278	0.295	0.290	0.338	0.289	0.308	0.323	0.298	0.342	0.324
8	0.298	0.281	0.302	0.308	0.278	0.299	0.295	0.303	0.306	0.292	0.278	0.328	0.316	0.300
9	0.298	0.331	0.297	0.308	0.304	0.298	0.289	0.303	0.311	0.309	0.276	0.286	0.317	0.301
10	0.299	0.293	0.280	0.285	0.281	0.292	0.289	0.271	0.305	0.311	0.326	0.305	0.297	0.307
11	0.289	0.296	0.298	0.286	0.289	0.296	0.304	0.293	0.279	0.301	0.325	0.306	0.297	0.285
12	0.291	0.282	0.302	0.339	0.291	0.297	0.309	0.283	0.281	0.291	0.328	0.305	0.296	0.294
13	0.290	0.294	0.293	0.339	0.305	0.297	0.309	0.315	0.285	0.274	0.308	0.309	0.275	0.292
14	0.299	0.293	0.292	0.294	0.282	0.302	0.311	0.281	0.294	0.311	0.278	0.309	0.295	0.295
15	0.298	0.296	0.289	0.271	0.337	0.339	0.308	0.281	0.300	0.312	0.277	0.303	0.293	0.273
16	0.305	0.328	0.341	0.273	0.337	0.322	0.289	0.287	0.303	0.315	0.290	0.299	0.307	0.272
17	0.306	0.305	0.284	0.300	0.305	0.306	0.299	0.296	0.295	0.280	0.305	0.303	0.299	0.291
18	0.289	0.295	0.292	0.335	0.298	0.275	0.291	0.294	0.299	0.304	0.286	0.298	0.295	0.276
19	0.289	0.291	0.297	0.335	0.292	0.322	0.305	0.300	0.300	0.279	0.295	0.326	0.301	0.288
20	0.287	0.289	0.292	0.300	0.294	0.290	0.288	0.295	0.304	0.282	0.324	0.329	0.294	0.299
21	0.289	0.330	0.297	0.328	0.293	0.292	0.287	0.293	0.285	0.294	0.323	0.306	0.289	0.272
22	0.280	0.279	0.299	0.276	0.295	0.292	0.289	0.324	0.282	0.292	0.302	0.305	0.293	0.274
23	0.292	0.315	0.322	0.290	0.328	0.297	0.294	0.320	0.281	0.284	0.298	0.302	0.297	0.301
24	0.316	0.287	0.295	0.282	0.277	0.280	0.300	0.278	0.278	0.281	0.298	0.316	0.281	0.290
25	0.290	0.289	0.298	0.290	0.278	0.300	0.301	0.278	0.278	0.303	0.305	0.274	0.284	0.301
26	0.278	0.294	0.298	0.282	0.292	0.299	0.294	0.289	0.282	0.279	0.303	0.293	0.297	0.274
27	0.290	0.295	0.295	0.296	0.279	0.311	0.297	0.335	0.306	0.296	0.343	0.279	0.290	0.293
28	0.300	0.294	0.296	0.284	0.279	0.290	0.296	0.334	0.307	0.302	0.344	0.283	0.304	0.291

31 07 46

Unit: Salem 1 RFO 20 Date: 04/11/10 T-MIN= 0.278 87.5% Nom. Wall= Nom. Wall = 0.337

ISI ID. AF14B Component ID. Lowest Reading 0.271 Highest reading 0.344

Color Code: 0.000 to T-MIN >T-MIN to 87.5% Nom Wall >87.5% Nom. Wall to Nom. Wall >Nom. Wall

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	0.306	0.339	0.339	0.291	0.292	0.303	0.298	0.294	0.335	0.305	0.282	0.316	0.285	0.302
2	0.290	0.297	0.328	0.321	0.292	0.336	0.296	0.290	0.274	0.299	0.300	0.307	0.299	0.299
3	0.298	0.291	0.294	0.308	0.290	0.304	0.293	0.294	0.273	0.307	0.335	0.308	0.298	0.279
4	0.301	0.292	0.291	0.309	0.299	0.291	0.298	0.277	0.306	0.306	0.321	0.277	0.294	0.290
5	0.299	0.331	0.301	0.340	0.293	0.293	0.293	0.290	0.304	0.299	0.321	0.275	0.294	0.318
6	0.289	0.279	0.296	0.339	0.305	0.294	0.293	0.302	0.281	0.294	0.326	0.298	0.295	0.323
7	0.309	0.273	0.314	0.320	0.278	0.295	0.290	0.338	0.289	0.308	0.323	0.298	0.342	0.324
8	0.298	0.281	0.302	0.308	0.278	0.299	0.295	0.303	0.306	0.292	0.278	0.328	0.316	0.300
9	0.298	0.331	0.297	0.308	0.304	0.298	0.289	0.303	0.311	0.309	0.276	0.286	0.317	0.301
10	0.299	0.293	0.280	0.285	0.281	0.292	0.289	0.271	0.305	0.311	0.326	0.305	0.297	0.307
11	0.289	0.296	0.298	0.286	0.289	0.296	0.304	0.293	0.279	0.301	0.325	0.306	0.297	0.285
12	0.291	0.282	0.302	0.339	0.291	0.297	0.309	0.283	0.281	0.291	0.328	0.305	0.296	0.294
13	0.290	0.294	0.293	0.339	0.305	0.297	0.309	0.315	0.285	0.274	0.308	0.309	0.275	0.292
14	0.299	0.293	0.292	0.294	0.282	0.302	0.311	0.281	0.294	0.311	0.278	0.309	0.295	0.295
15	0.298	0.296	0.289	0.271	0.337	0.339	0.308	0.281	0.300	0.312	0.277	0.303	0.293	0.273
16	0.305	0.328	0.341	0.273	0.337	0.322	0.289	0.287	0.303	0.315	0.290	0.299	0.307	0.272
17	0.306	0.305	0.284	0.300	0.305	0.306	0.299	0.296	0.295	0.280	0.305	0.303	0.299	0.291
18	0.289	0.295	0.292	0.335	0.298	0.275	0.291	0.294	0.299	0.304	0.286	0.298	0.295	0.278
19	0.289	0.291	0.297	0.335	0.292	0.322	0.305	0.300	0.300	0.279	0.295	0.326	0.301	0.288
20	0.287	0.289	0.292	0.300	0.294	0.290	0.288	0.295	0.304	0.282	0.324	0.329	0.294	0.299
21	0.289	0.330	0.297	0.328	0.293	0.292	0.287	0.293	0.285	0.294	0.323	0.306	0.289	0.272
22	0.280	0.279	0.299	0.276	0.295	0.292	0.289	0.324	0.282	0.292	0.302	0.305	0.293	0.274
23	0.292	0.315	0.322	0.290	0.328	0.297	0.294	0.320	0.281	0.284	0.298	0.302	0.297	0.301
24	0.316	0.287	0.295	0.282	0.277	0.280	0.300	0.278	0.278	0.281	0.298	0.316	0.281	0.290
25	0.290	0.289	0.298	0.290	0.278	0.300	0.301	0.278	0.278	0.303	0.305	0.274	0.284	0.301
26	0.278	0.294	0.298	0.282	0.292	0.299	0.294	0.289	0.282	0.279	0.303	0.293	0.297	0.274
27	0.290	0.295	0.295	0.296	0.279	0.311	0.297	0.335	0.306	0.296	0.343	0.279	0.290	0.293
28	0.300	0.294	0.296	0.284	0.279	0.290	0.296	0.334	0.307	0.302	0.344	0.283	0.304	0.291

ATTACHMENT 3
UT THICKNESS DATA SHEET
PAGE 1 OF 1

ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/15/2010 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 071474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 12:30cm Cal Check: N/A Cal Out time: 1:45cm

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Steve Walsh Level: II Date: 4/15/2010

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/14/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: PANAMETRICS
Model: 37DL Plus
Serial Number: 071474104

Transducer Information

Manufacturer: PANAMETRICS
Serial Number: 702375
Style: DUAL
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: AmbIENt
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 10:30 pm Cal Check: N/A Cal Out time: 12:15 am

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Mitch Wygand Level: II Date: 4/14/10

Reviewer: [signature] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/13/10 Page ____ of ____

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 051325610

Transducer Information

Manufacturer: Panametrics
Serial Number: 693612
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 12:00am Cal Check: N/A Cal Out time: 1:30am

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Mitch Wygand Level: II Date: 4/13/10

Reviewer: [signature] Date: 4/15/10

ANII: _____ Date: _____

ATTACHMENT 3
UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/12/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 051325610

Transducer Information

Manufacturer: Panametrics
Serial Number: 693612
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultrogel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 11:00pm Cal Check: N/A Cal Out time: 12:45am

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Mitch Wygant Level: II Date: 4/12/10

Reviewer: _____ Date: 4/15/10

ANII: _____ Date: _____

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THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/11/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 071474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 093325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 12:00 Am Cal Check: N/A Cal Out time: 2:00 Am

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Mitch Wygand Level: II Date: 4/11/10

Reviewer: Date: 4/15/10

ANII: Date:

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ATTACHMENT 3
UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/10/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: PANAMETRICS
Model: 37DL Plus
Serial Number: 071474104

Transducer Information

Manufacturer: PANAMETRICS
Serial Number: 702375
Style: DUAL
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 11:00pm Cal Check: N/A Cal Out time: 1:30 Am

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Mitch Wygand Level: II Date: 4/10/10

Reviewer: _____ Date: 4/15/10

ANII: _____ Date: _____

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ATTACHMENT 3
UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/10/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 0714 74104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: CS
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 8:30 AM Cal Check: _____ Cal Out time: 11:30 AM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Ken Underwood Level: II Date: 4/10/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

ATTACHMENT 3
UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/11/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 091474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 093325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 9:00 AM Cal Check: _____ Cal Out time: 11:30 AM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Neil Underwood Level: II Date: 4/11/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/11/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 0714474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: CS
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 1:00 PM Cal Check: _____ Cal Out time: 3:00 PM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Ken Underwood Level: II Date: 4/11/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

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THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/12/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model 37DL Plus
Serial Number 071474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp Ambient
Temp S/N N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 8:30 AM Cal Check: _____ Cal Out time: 11:00 AM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Jeremy Morgan Level: II Date: 4/12/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

ATTACHMENT 3
UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/12/10 Page ____ of ____

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 091474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: CS
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 1:00 PM Cal Check: _____ Cal Out time: 3:30 PM

Component Examination Information

System	Component Numbers	Component Comp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Jeremy Morgan Level: II Date: 4/12/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/13/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 07147410 4

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: C/S
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 8:00 AM Cal Check: _____ Cal Out time: 11:30 AM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Jeremy Morgan Level: II Date: 4/13/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/13/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: Panametrics
Model: 37DL Plus
Serial Number: 071474104

Transducer Information

Manufacturer: Panametrics
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 093225

Calibration Data

Calibration Block

Type: Step
Material: CS
Cal Blk S/N: 07-8897
Cal Blk Temp: Ambient
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 12:30PM Cal Check: _____ Cal Out time: 4:00PM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Jeremy Morgan Level: II Date: 4/13/10

Reviewer: [signature] Date: 4/15/10

ANII: _____ Date: _____

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UT THICKNESS DATA SHEET
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ULTRASONIC
THICKNESS
CALIBARATION DATA SHEET

Report Number: _____

Plant: Salem Unit: 1 Date: 4/14/10 Page ___ of ___

Procedure Number/Rev: OU-AA-335-004 Rev. 1 W/O # 60084266

Equipment Data

Instrument Information

Manufacturer: PANAMETRICS
Model: 37DL Plus
Serial Number: 0914 74104

Transducer Information

Manufacturer: PANAMETRICS
Serial Number: 702375
Style: Dual
Size: .434
Freq: 5 Mhz
Couplant: Ultragel II
Batch: 09325

Calibration Data

Calibration Block

Type: Step
Material: CS
Cal Blk S/N: 07-8897
Cal Blk Temp: AMBIENT
Temp S/N: N/A

Calibration Block Readings

Actual (T):	Measured (T):
.100	.100
.200	.200
.300	.300
.400	.400
.500	.500

Cal Time in: 7:30 AM Cal Check: _____ Cal Out time: 11:00 AM

Component Examination Information

System	Component Numbers	Component Temp	Acceptance Criteria	Inspection Results

Comments:

Examiner: Jeremy Morgan Level: II Date: 4/14/10

Reviewer: [illegible] Date: 4/15/10

ANII: _____ Date: _____