ES-301

Administrative Topics Outline FINAL

| Facility: McGuire | | Dat | e of Examination: | 8/2/10 |
|--|-------------------------------|-------------------------------------|---|----------------------|
| Examination Level: | RO | Op | erating Test Number: | N10-1 |
| Administrative Topic Type Code* Describe activity to be performed (see Note) | | erformed | | |
| Conduct of Operations | M, R | 2.1.37 (4.3) | Knowledge of procedures, guidelines or limitations associated with reactivity management | |
| | | JPM: | Perform an ECP | |
| Conduct of Operations | D, P, R | 2.1.25 (3.9) | Ability to interpret refe as graphs, curves, tab | |
| | | JPM: | Determine Boric Acid Addition to FWST | |
| Equipment Control | M, R | 2.2.12 (3.7) | Knowledge of Surveill | ance Procedures. |
| | , | JPM: | Perform a Manual NC Leakage Calculation | |
| Dediction Control | | 2.3.11 (3.8) | Ability to control radial | tion releases |
| Radiation Control | M, R | JPM: | Perform a Unit Vent Flow Calculation of a Containment Air Release | |
| NOTE: All items (5 total) retaking only the | | | oplicants require only 4 i are required. | tems unless they are |
| *Type Codes & Criteria: | (D)irect from (N)ew or (M) | bank (≤ 3 for R odified from bai | for, (0) or Class(R)oom (Os; \leq 4 for SROs & RO hk (\geq 1) (3) idomly selected) (1) | , |

RO Admin JPM Summary

- A1a This is a modified JPM using Bank JPM-RT-RB:073 as its basis. The operator will be told that Reactor Startup is an hour away, and provided with a set of initial conditions. The operator will be asked to perform an Estimated Critical Position (ECP) in accordance with OP/0/A/6100/06 (Reactivity Balance Calculation), Enclosure 4.2 (Estimated Critical Rod Position). During the course of the ECP, the operator will be given a set of power history conditions, and asked to perform a Shutdown Fission Product Correction calculation in accordance with OP/0/A/6100/06 (Reactivity Balance Calculation), Enclosure 4.8 (Shutdown Fission Product Correction Calculation) in support of the ECP. This is the same JPM as the SRO Exam.
- A1b This is a bank JPM, and previously used on the 2009 NRC Operating Test. The operator will be told that a leak, which is now isolated has lowered the FWST level to 440 inches, and that it has been decided to use the Recycle Holdup Tank (RHT) to refill the FWST. The operator will be told that Enclosure 4.4, (FWST Makeup Using the RHT), of OP/1/A/6200/014 (Refueling Water System) is in progress and completed through Step 3.9, and provided with Chemistry Data for the BAT and RHT. The operator will then be directed to determine the amount of Boric Acid needed to raise the FWST level to 480" using the RHT in accordance with Step 3.10 of Enclosure 4.4 of OP/1/A/6200/014 (Refueling Water System). The operator will be expected to calculate the amount of Boric Acid that must be added from the BAT to refill the FWST.
- A2 This is a modified JPM using Bank JPMs ADM-NRC-A2-05 and 12 as its basis. The operator will be told that Unit 1 is at 100% power, the Unit 1 OAC point M1L4554 is out of service, and that PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm. The operator will be given Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) with the necessary raw data compiled on a Data Sheet; and directed to complete the calculations within the Enclosure. The operator will be expected to complete all calculations, and identify any Technical Specification Limits that have been exceeded.
- A3 This is a modified JPM using Bank JPM ADM-NRC-A3-010 as its basis. The operator will be told that GWR Package # 2010013 for Unit 1 Containment Air Release is currently in use to conduct a series of Containment air releases, and that during the first release, conducted using Enclosure 4.2 (Air Release Mode With VQ Flow Monitor Operable) of OP/1/A/6450/017 (Containment Air Addition and Release), the Unit 1 VQ Monitor became inoperable. The operator will be told that the crew stopped the release and continued the air release using Enclosure 4.3 (Air Release Mode with VQ Flow Monitor Inoperable) of OP/1/A/6450/017 (Containment Air Addition and Release), and that three previous releases have been made; including the one which was made with the Unit 1 VQ Flow Monitor in operation. Finally, the operator will be provided with the pertinent data for the current release, and then be directed to calculate the volume released for the current release and to determine the total volume released from the Containment during all releases. The operator will be expected to calculate the volume of air released from the Containment during the final release, and determine the total volume of air released in the series of four releases.

ES-301

Administrative Topics Outline FINAL

Form ES-301-1

| Facility: McGuire | | Da | te of Examination: | 8/2/10 | |
|---|----------------------------------|--------------------------------------|--|------------------------|--|
| Examination Level: | SRO | Operating Test Number: | | N10-1 | |
| Administrative Topic (see Note) | Type Code* | | Describe activity to be performed | | |
| Conduct of Operations | M, R | 2.1.37 (4.6) | Knowledge of procedures, guidelines or limitations associated with reactivity management | | |
| | | JPM: | Perform an ECP | | |
| Conduct of Operations | D, P, R | 2.1.25 (4.2) | Ability to interpret reference materials, suc as graphs, curves, tables, etc. | | |
| | | JPM: | Determine Boric Acid | Addition to FWST | |
| | | 2.2.12 (4.1) | Knowledge of Surveillance Procedures. | | |
| Equipment Control | M, R | JPM: | Perform/Review a Manual NC leakage Calculation | | |
| . | | 2.3.11 (3.8) | Ability to control radia | tion releases | |
| Radiation Control | M, R | JPM: | Perform a Unit Vent Flow Calculation of a Containment Air Release | | |
| Emergency Procedures/Plan | N, R | 2.4.44 (4.4) | Knowledge of emerge action recommendation | | |
| | | JPM: | Provide an updated P | AR | |
| NOTE: All items (5 total) a only the administra | | | ants require only 4 items un | less they are retaking | |
| *Type Codes & Criteria: | (D)irect from b (N)ew or (M)o | ank (≤ 3 for ROs dified from bank | (0) or Class(R)oom (5) ; ≤ 4 for SROs & RO retake (≥ 1) (4) mly selected) (1) | es) (1) | |

SRO Admin JPM Summary

- A1a This is a modified JPM using Bank JPM-RT-RB:073 as its basis. The operator will be told that Reactor Startup is an hour away, and provided with a set of initial conditions. The operator will be asked to perform an Estimated Critical Position (ECP) in accordance with OP/0/A/6100/06 (Reactivity Balance Calculation), Enclosure 4.2 (Estimated Critical Rod Position). During the course of the ECP, the operator will be given a set of power history conditions, and asked to perform a Shutdown Fission Product Correction calculation in accordance with OP/0/A/6100/06 (Reactivity Balance Calculation), Enclosure 4.8 (Shutdown Fission Product Correction Calculation) in support of the ECP. This is the same JPM as the RO Exam.
- A1b This is a bank JPM, and previously used on the 2009 Operating Test. The operator will be told that a leak, which is now isolated has lowered the FWST level to 440 inches, below the Technical Specification Limit, and that it has been decided to use the Recycle Holdup Tank (RHT) to refill the FWST. The operator will be told that Enclosure 4.4 (FWST Makeup Using the RHT), of OP/1/A/6200/014 (Refueling Water System) is in progress and completed through Step 3.10, and provided with Chemistry Data for the BAT and RHT. The operator will then be directed to perform the Independent Verification (SRO aspect) of the calculation in Step 3.10 of Enclosure 4.4 to determine the amount of Boric Acid that must be added from the Boric Acid Tank (BAT), in order to raise the FWST Level to 480" using the RHT. The operator will discover two errors within the previous calculation, and determine the correct volume of Boric Acid to add. Following this, the operator will be given a makeup flowrate to the FWST and asked to identify the impact on the Technical Specification ACTION. The operator will be required to identify that ACTION C is applicable after one hour.
- A2 This is a modified JPM using Bank JPMs ADM-NRC-A2-05 and 12 as its basis. The operator will be told that Unit 1 is at 100% power, the Unit 1 OAC point M1L4554 is out of service, and that PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm. The operator will be given Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) with the necessary raw data compiled on a Data Sheet; and directed to complete the calculations within the Enclosure. The operator will be expected to complete all calculations in accordance with the provided Key, identify any Technical Specification Limits that have been exceeded, and (SRO aspect) identify with all Technical Specification ACTION.
- A3 This is a modified JPM using Bank JPM ADM-NRC-A3-010 as its basis. The operator will be told that GWR Package # 2010013 for Unit 1 Containment Air Release is currently in use to conduct a series of Containment air releases, and that during the first release, conducted using Enclosure 4.2 (Air Release Mode

| · · · · · · · · · · · · · · · · · · · | | |
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| E3-301 | | Form ES-301-1 |
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With VQ Flow Monitor Operable) of OP/1/A/6450/017 (Containment Air Addition and Release), the Unit 1 VQ Monitor became inoperable. The operator will be told that the crew stopped the release and continued the air release using Enclosure 4.3 (Air Release Mode with VQ Flow Monitor Inoperable) of OP/1/A/6450/017 (Containment Air Addition and Release), and that three previous releases have been made; including the one which was made with the Unit 1 VQ Flow Monitor in operation. Finally, the operator will be provided with the pertinent data for the current release, and then be directed to calculate the volume released for the current release and to determine the total volume released from the Containment during all releases. The operator will be expected to calculate the volume of air released from the Containment during the final release, and determine the total volume of air released in the series of four releases. This is the same JPM as the RO Exam.

A4 This is a new JPM. The operator will be placed in a post-accident condition with a Large Break LOCA with a release from the Containment. The operator will be told that a General Emergency has been declared, and provided with the initial Protective Action Recommendation (PAR). The operator will be given a subsequent set of plant conditions and meteorological data, and asked to provide an updated PAR in accordance with Enclosure 4.4 (Offsite Protective Recommendations) of RP/0/B/5700/029 (Notifications to Offsite Agencies from the Control Room). The operator will be expected to determine the Updated PAR for the subsequent conditions.

| Appendix C | Job Performance Measure | Form ES-C- |
|------------|-------------------------|------------|
| | Worksheet | |
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2010 Admin - JPM A1a RO/SRO 🐁

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| Appendix C | Pag | e 2 of 17 | Form ES-C-1 |
|---------------------|-----------------------|------------------|--|
| | Job Performance | Measure Workshee | t |
| | | | |
| Facility: | McGuire | Task No.: | 214OP_010 |
| Task Title: | Perform an ECP | JPM No.: | <u>2010 Admin - JPM A1a</u> <u>RO/SRO</u> |
| K/A Reference: | GK/A 2.1.37 (4.3/4.6) | | |
| Examinee: | | NRC Examiner | . |
| Facility Evaluator: | | Date: | |
| Method of testing | | | |
| Simulated Perform | nance: | Actual Perform | ance: X |
| Class | room X Simulator | Plant | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | Unit 1 startup in progress per OP/1/A/6100/001 (Controlling Procedure for Unit Startup). |
|---------------------|---|
| | All steps are complete up to determining the desired estimated critical rod height. |
| | The Unit tripped from 30% power, 70 hours ago. |
| | Prior to that the Unit had operated at 2 EFPD since the previous plant trip, which resulted in a shutdown lasting 24 hours. |
| | The following Cycle 21 conditions exist: |
| | • EFPD = 125 |
| | NC Boron = 1577 PPM Xenon Worth = 0 |
| | Samarium = 150 PCM greater than equilibrium |
| | It is intended to pull rods to criticality with criticality achieved in approximately 1 hour. |
| | Reactor Engineer Chad Adams has been contacted earlier today and has reported that there have been no unusual trends on ECPs. |
| | The OAC and REACT Program are unavailable. |
| Task Standard: | The Actual Estimated Critical Rod Position Bank for Xenon at time of Criticality agrees with the evaluator calculated ECP \pm 10 steps. |

| | Job Performance Measure Worksheet Calculator | |
|---------------------|--|--------------------|
| • | Calculator | |
| | | |
| General References: | OP/1/A/6100/001 (Controlling Procedure for Unit Start | up) |
| | OP/0/A/6100/006 (Reactivity Balance Calculation) | |
| | OP/1/A/6100/022 (Unit 1 Data Book – Cycle 21) | |
| | SOMP 01-02 (Reactivity Management) | |
| Handouts: | OP/0/A/6100/006 (Reactivity Balance Calculation) End (Estimated Critical Rod Position (ECP)) | closure 4.2 |
| | OP/0/A/6100/006 (Reactivity Balance Calculation) End (Fission Product Correction Calculation) | losure 4.8 |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, 7 Shutdown Fission Product Correction | able 6.7, |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, C Boron Concentration HZP, ARO, NO XENON, EQ Sm | • |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, C Differential Boron Worth, HZP, ARO, NO XENON, EQ | • |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, 7 and Samarium Worths. | able 6.9, Xenon |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, 7 Integral Rod Worth in Overlap, HZP, NO XENON. | able 6.3.A, |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, 7 Integral Rod Worth in Overlap, HZP, PEAK XENON. | able 6.3.B, |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, C Rod Insertion Limit as a Function of Power. | Graph 1.2, Control |
| | OP/1/A/6100/022 (Unit 1 Data Book), Enclosure 4.3, 1 Withdrawal Limits. | able 2.8, Rod |
| | The CRS has directed you to perform an ECP per End (Estimated Critical Rod Position (ECP)) of OP/0/A/610 Balance Calculation). | |
| Time Critical Task: | NO | |
| Validation Time: | 40 minutes | |

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(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue (Last Page of this JPM), and Handout all documents identified in the Handout section.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|--|-----|-----------------------------------|
| 1 | (Note prior to Step 3.1) All curves/tables used in this procedure are found in OP/1(2)/A/6100/022 (Unit One (Two) Core Data Book). These procedures will be referred to as the "Data Book." | The operator reads the Note and proceeds. | | |
| 2 | (Step 3.1) Record the following: (Step 3.1.1) | The operator records Unit <u>1</u> . | | |
| | Unit Cycle | The operator records Cycle <u>21</u> . | | |
| 3 | (Step 3.1.2) Recent trends on ECP. Reactor Engineer contacted Date | The operator recognizes that Chad Adams has been contacted. The operator records RE name as <u>Chad Adams</u> and <u>today's date</u> . | | |
| 4 | (Step 3.1.3) Date/Time of Shutdown. | The operator records <u>Date/Time</u> (70 hours ago) from current Date/Time. | | |
| 5 | (Step 3.1.4) Anticipated Date/Time of Criticality / | The operator records <u>today's date</u> and <u>1 hour</u> <u>from the time calculation</u> <u>is started</u> as the time of criticality. | | |

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Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|--|-----|-----------------------------------|
| 6 | (Step 3.1.5) Burnup: (P1457) | The operator records <u>125</u> <u>EFPD</u> . | | |
| 7 | (Step 3.1.6) NC System Boron Concentration: | | | |
| | (Step 3.1.6.1) If pulling rods to Criticality: (Step 3.1.6.1A) If OAC is unavailable, record the current NC System boron concentration. OR | The operator recognizes from initial conditions that OAC is unavailable and it is intended to pull rods to criticality. The operator records <u>1577</u> in Step 3.1.6.1A. | | |
| | (Step 3.1.6.1B) If OAC is available | The operator places <u>NA</u> in Step 3.1.6.1B. | | |
| 8 | (Step 3.1.6.2) If dilution to Criticality | The operator places <u>NA</u> in Step 3.1.6.2. | | |
| 9 | (Step 3.1.6.3) Record the Effective Boron Concentration: (Step 3.1.6.1A or Step 3.1.6.1B3 or 3.1.6.2) | The operator records <u>1577</u> ppm from Step 3.1.6.1A. | | |
| 10 | (Step 3.1.7) Xenon worth at anticipated time of Criticality (From OAC program Xenon Samarium – XESM or REACT Program). | The operator records <u>0</u> from initial conditions. | | |
| 11 | (Step 3.1.8) If burnup from Step 3.1.5 is > 0 EFPD, record the difference between equilibrium and present samarium worth (P1475, Samarium program on OAC or REACT). | The operator recognizes that burnup is > 0 EFPD and records <u>150</u> from initial conditions. | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 12 | (Step 3.1.9) If burnup from Step 3.1.5 is > 12 EFPD, perform Enclosure 4.8 to determine the fission product correction. | The operator recognizes that burnup is > 12 EFPD and that fission product correction is needed, and proceeds to Enclosure 4.8. | | |
| 13 | (Enclosure 4.8/Notes prior to Step 3.1) All curves /tables used in this procedure are found in OP/1(2)/A/6100/022 (Unit One (Two) Core Data Book). These procedures will be referred to as the "Data Book." Number of hours shutdown is the difference in time between the time the reactor went subcritical and the expected time of criticality. | The operator reads Notes, and proceeds. | | |
| 14 | (Step 3.1) Shutdown Fission Product Correction Calculation: (Step 3.1.1) If Unit operated > 3 EFPD from previous shutdown to current shutdown | The operator reviews power history and recognizes that the Unit did NOT operate > 3 EFPD from previous shutdown to current shutdown. The operator records an <u>NA</u> in Step 3.1.1, and proceeds to Step 3.1.2. | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 15 | (Step 3.1.2) If Unit operated < 1 EFPD from previous shutdown to current shutdown | The operator reviews power history and recognizes that the Unit operated > 1 EFPD from previous shutdown to current shutdown. Operator records an <u>NA</u> in Step 3.1.2, and proceeds to | | |
| | | Step 3.1.3. | | |
| *16 | (Step 3.1.3) If Unit operated between 1 EFPD and 3 EFPD from previous shutdown to current shutdown and current shutdown < 72 hours use Data Book Table 6.7 to determine the shutdown fission product correction based on the following: | The operator reviews power history and recognizes that the Unit operated between 1 EFPD and 3 EFPD from previous shutdown to current shutdown, and the current shutdown is < 72 hours. Operator proceeds to Step 3.1.3.1. | | |
| 17 | (Step 3.1.3.1) Previous Shutdown: (A) Number of hours during previous shutdown: hrs (B) Shutdown Fission Product Correction: ppm | The operator recognizes from initial conditions that the number of hours during the previous shutdown is 24, and records <u>24</u> . The operator addresses Data Book Table 6.7 and determines the Shutdown Fission Product Correction to be 10, and records <u>10</u> . | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|--|-----|-----------------------------------|
| 18 | (Step 3.1.3.2) Current Shutdown: (A) Number of hours since current shutdown: | The operator recognizes from initial conditions that the number of hours during the current shutdown to the time of the ECP is 71, and records <u>71</u> . | | |
| | hrs (B) Shutdown fission product correction: ppm | The operator addresses Data Book Table 6.7 and determines the shutdown fission product correction is 35, and records <u>34.5</u> . | | |
| 19 | (Step 3.1.3.3) Shutdown Fission product Correction: (Step 3.1.3.1B x 0.5) + (Step 3.1.3.2B) =ppm | The operator uses value determined in Step 3.1.3.1B and 3.1.3.2 and determines the Shutdown Fission Product Correction is 39.5 ppm. Operator records <u>39.5</u> (± 0.5). (10 x 0.5) + (34.5) = 40 ppm | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|--|-----|-----------------------------------|
| 20 | (Step 3.1.4) If Unit operated between 1 EFPD and 3 EFPD from previous shutdown to current shutdown and current shutdown > 72: | The operator reviews power history and recognizes that the Unit operated between 1 EFPD and 3 EFPD from previous shutdown to current shutdown, however, the current shutdown is < 72 hours. | | |
| | | Operator records an <u>NA</u> in Step 3.1.4. | | |
| | | Operator reports that the Shutdown Fission Product Correction factor is <u>39.5</u> (±0.5). | | |
| 21 | (Enclosure 4.2/Step 3.2) If desired, perform automated calculations using REACT | The operator recognizes from initial conditions that REACT is NOT available and proceeds to Step 3.3. | | |
| 22 | (Step 3.3) Manual Calculations: (Step 3.3.1) Boron Concentration: (Step 3.3.1.1) Determine the all rods out (ARO), hot zero power (HZP), no xenon, equilibrium samarium, boron concentration for present burnup from Step 3.1.5 (Data Book Graph 6.1) (Step 3.3.1.2) Record value | The operator addresses Data Book Graph 6.1. (NOTE: The operator should use chart at bottom, and NO interpolation is needed). The operator records <u>1818</u> | | |
| | (Step 3.3.1.2) Record Value in Table 4.2.1 Line A. | The operator records <u>1818</u> in Table 4.2.1 Line A. | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|---|-----|-----------------------------------|
| 23 | (Step 3.3.2) Differential Boron Worth: (Step 3.3.2.1) Determine the ARO differential boron worth for present burnup of step 3.1.5 (Data Book Graph 6.8) (Step 3.3.2.2) Record value in Table 4.2.1 Line B | The operator addresses Data Book Graph 6.8. (NOTE: Operator should use chart at bottom, and NO interpolation is needed). The operator records <u>-6.35</u> in Table 4.2.1 Line B. | | |
| 24 | (Step 3.3.3) Determine the Rod Inserted Worth: Step (3.3.3.1) Record values from Steps 3.1.6 - 3.1.9 in Table 4.2.1. | The operator records values from steps 3.1.6 - 3.1.9 in Table 4.2.1 as follows: C. Present Effective Boron Concentration: <u>1577</u> D. Xenon Worth: <u>0</u> E. Diff from Eq Sm Worth: <u>150</u> F. Fission Product Correction: <u>39.5 (±0.5)</u> | | |
| 25 | (Step 3.3.3.2) Complete Table 4.2.1, recording 0 for any N/A'd Reference Steps. | The operator records remaining values in Table 4.2.1, as follows: G. Reactivity Equivalent of Boron Difference (C - A) x B = <u>1530</u> . (1577 - 1818) x - 6.35 = 1530 pcm H. Reactivity Equivalent of Fission Product Correction F x B = <u>250.83</u> 39.5 x -6.35 = -250.83 Reactivity of Inserted Rods: (D + E + G) - H = <u>1931 (±4)</u> (0 + 150 + 1530) - (-)250.83 = 1931 | | |

Appendix C

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|--|-----|-----------------------------------|
| 26 | (Step 3.3.4) If result from Table 4.2.1 < 0 | The operator recognizes result from Table 4.2.1 > 0 and records <u>NA</u> in Step 3.3.4. | | |
| 27 | (Step 3.3.5) Peak xenon worth: (Step 3.3.5.1) Determine the peak xenon worth for present burnup from step 3.1.5 (Data Book Table 6.9) | The operator addresses Data Book Table 6.9. | | |
| | (Step 3.3.5.2) Record value in Table 4.2.2 Line C. | The operator records <u>3913</u> in Table 4.2.2 Line C. | | |
| 28 | (Step 3.3.6) Calculate the Estimated Critical Rod Positions: (Step 3.3.6.1) Record values from Step 3.1.7 and Table 4.2.1 in Table 4.2.2. | The operator records values in Table 4.2.2 as follows: A. Xenon Worth: <u>0</u> B. Reactivity of inserted rods: <u>1931</u> C. Peak Xenon Worth: <u>3913</u> D. Lower Band Reactivity Worth: <u>2681</u> E. Upper Band Reactivity Worth: 1181 | | |

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| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 29 | (Step 3.3.6.2) Complete Table 4.2.2. | The operator completes Table 4.2.2 as follows: The operator addresses Table 6.3.A of the Data Book and determines: F. No Xenon Rod Position for Reactivity of B - <u>Bank C</u> @ 35 steps, +2/-3 steps. G. No Xenon Rod Position for Reactivity of D - <u>Bank B</u> @ 39 steps, +2/-3 steps. H. No Xenon Rod Position for Reactivity of E - <u>Bank D</u> @ 3 steps, +2/-3 steps. The operator addresses Table 6.3.B of the Data Book and determines: I. Peak Xenon Rod Position for Reactivity of B - <u>Bank C</u> @ 49 steps, +2/-3 steps. J. Peak Xenon Rod Position fro Reactivity of D - <u>Bank B</u> @ 68 steps, +2/-3 steps. K. Peak Xenon Rod Position for Reactivity of E - <u>Bank D @ 26 steps, +2/-3</u> steps. | | |
| *30 | (Table 4.2.2) Estimated Critical Position | The operator records <u>Bank</u> <u>C @ 35 steps, +2/-3 steps.</u> [(I - F) x (A ÷ C)] + F. | | |
| *31 | (Table 4.2.2) Lower Limit of Band | The operator records <u>Bank</u> <u>B @ 39 steps, +2/-3 steps.</u> [(J - G) x (A ÷ C)] + G | | |

Appendix C

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Form ES-C-1

| r | P | | | |
|-------|--|---|-----|-----------------------------------|
| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
| *32 | (Table 4.2.2) Upper Limit of Band | The operator records <u>Bank</u> <u>D @ 3 steps, +2/-3 steps.</u> | | |
| | | [(K - H) x (A ÷ C)] + H | | |
| *33 | (Step 3.4) Check the following: | The operator addresses Graph 1.2 and determines | | |
| | (Step 3.4.1) Rod Positions of Table 4.2.2 or REACT output are greater than insertion limits per Data Book Graph 1.2. | rod positions are NOT greater than insertion limits. | | |
| | (Step 3.4.2) Rod positions of Table 4.2.2 or REACT Output are less than rod withdrawal limits per Data Book Table 2.8. | The operator addresses Table 2.8 and determines no withdrawal limits exist. | | |
| 34 | (Step 3.5) If Step 3.4 CANNOT be met, contact reactor Engineering. | The operator contacts Reactor Engineering. | | |
| | | Cue: | | |
| | | Reactor Engineering acknowledges. | | |
| 35 | Calculations performed By: (RO) | The operator records <u>Name</u> and <u>date</u> . | | |
| | Date | | | |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

| Appen | dix | С |
|-------|-----|---|
| | | |

Page 14 of 17 VERIFICATION OF COMPLETION

| Job Performance Measure No.: | <u> 2010 Admin - JP</u> | M A1a RO/SRO | |
|------------------------------|-------------------------|--------------|---|
| Examinee's Name: | | | |
| Date Performed: | | | |
| Facility Evaluator: | | | |
| Number of Attempts: | | | |
| Time to Complete: | | | |
| Question Documentation: | | | |
| | | | |
| | | | |
| | | | |
| Result: | SAT | UNSAT | - |

Examiner's Signature: Date:

Appendix C

Page 15 of 17 VERIFICATION OF COMPLETION

KEY:

Table 4.2.1: Rod Inserted Worth Calculation

| Description | Reference | Value |
|---|--|-----------------------------------|
| A. ARO, HZP, No Xenon, Eq. Samarium Boron | Step 3.3.1 | 1818ppm |
| B. ARO/DBW | Step 3.3.2 | -6.35pcm/ppm |
| C. Present Effective Boron Concentration | Step 3.1.6.3 | 1577ppm |
| D. Xenon Worth | Step 3.1.7 | 0pcm |
| E. Diff from Eq Sm Worth | Step 3.1.8 | 150pcm |
| F. Fission Product Correction | Step 3.1.9 | 39.5(±0.5)ppm |
| G. Reactivity Equivalent of Boron Difference | (C-A) x B (1577 - 1818) x -6.35 | 1530pcm |
| H. Reactivity Equivalent of Fission Product Correction | F x B 39.5 x -6.35 | -250.83pcm (-247.65 – (-) 254) |
| Reactivity of Inserted Rods | (D + E + G) –H (0 + 150 + 1530) – (-250.83) | 1930.83pcm (1927.65 - 1934) |

Appendix C

Page 16 of 17 VERIFICATION OF COMPLETION

KEY^(Cont'd):

Table 4.2.2: Estimated Critical Rod Positions

| Description | Reference | | Value |
|---|---|-------|-------------------|
| A. Xenon Worth | Step 3.1.7 | | 0pcm |
| B. Reactivity of inserted rods | Table 4.2.1 | | 1931±4pcm |
| C. Peak Xenon Worth | Step 3.3.5 | - | 3913pcm |
| D. Lower Band Reactivity Worth | B + 750 | | 2681pcm |
| E. Upper Band Reactivity Worth | B - 750 | | 1181pcm |
| F. No Xenon Rod Position for Reactivity of B | Data Book Table 6.3.A | BankC | 35+2/-3steps w/d |
| G. No Xenon Rod Position for Reactivity of D | Data Book Table 6.3.A | BankB | 39+2/-3steps w/d |
| H. No Xenon Rod Position for Reactivity of E | Data Book Table 6.3.A | BankD | 3+2/-3steps w/d |
| I. Peak Xenon Rod Position for Reactivity of B | Data Book Table 6.3.B | BankC | 48+2/-3steps w/d |
| J. Peak Xenon Rod Position for Reactivity of D | Data Book Table 6.3.B | BankB | 68+2/-3steps w/d |
| K. Peak Xenon Rod Position for Reactivity of E | Data Book Table 6.3.B | BankD | 26+2/-3steps w/d |
| Estimated Critical Position | [(I - F) x (A/C)] + F [(C48 – C35) x (0/3913)] + C35 | BankC | 35 +2/-3steps w/d |
| Lower Limit of Band | [(J - G) x (A/C)] + G [(B68 - B39) x (0/3913)] + B39 | BankB | 39+2/-3steps w/d |
| Upper Limit of Band | [(K - H) x (A/C)] + H [(D26 – D3) x (0/3913)] + D3 | BankD | 3 +2/-3steps w/d |

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| А | pp | end | dix | С |
|---|----|-----|-----|---|
|---|----|-----|-----|---|

| | Initial Conditions: | Unit 1 startup in progress per OP/1/A/6100/001 (Controlling Procedure for Unit Startup). |
|---|---------------------|---|
| | | All steps are complete up to determining the desired estimated critical rod height. |
| | | The Unit tripped from 30% power, 70 hours ago. |
| | | Prior to that the Unit had operated at 2 EFPD since the previous plant trip, which resulted in a shutdown lasting 24 hours. |
| | | The following Cycle 21 conditions exist: |
| | | EFPD = 125 NC Boron = 1577 PPM Xenon Worth = 0 |
| | | Samarium = 150 PCM greater than equilibrium |
| | | It is intended to pull rods to criticality with criticality achieved in approximately 1 hour. |
| | | Reactor Engineer Chad Adams has been contacted earlier today and has reported that there have been no unusual trends on ECPs. |
| | | The OAC and REACT Program are unavailable. |
| _ | | |
| | | |
| | | The CPS has directed you to perform an ECP per Englacy of 2 |

INITIATING CUE:

The CRS has directed you to perform an ECP per Enclosure 4.2 (Estimated Critical Rod Position (ECP)) of OP/0/A/6100/006 (Reactivity Balance Calculation).

Enclosure 4.2 Estimated Critical Rod Position (ECP)

1. Limits and Precautions

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- 1.1 The calculation shall be performed twice. A Licensed Reactor Operator performs the calculation. The second, independent calculation shall be performed by a Qualified Reactor Engineer as a separate verification of the original calculation (NSD 304).
- 1.2 Criticality should not be obtained outside the maximum window (\pm 750 pcm) of estimated critical control bank position.
- 1.3 Estimated critical rod position must be recalculated if criticality will not be achieved within ± 2 hours from previously anticipated time of criticality.
- 1.4 For Dilution to Criticality (Initial Startup for Cycle): The ECP shall be performed using the All Rods Out, HZP, 0 EFPD Critical Boron Concentration provided in the Data Book.
- 1.5 Rod Worths listed in Data Book Tables 6.3.A, 6.3.B and 6.3.3 do not need to be interpolated over EFPD. The worths are valid over the range given in each column.
- 1.6 The maximum allowable rod position is ARO and the minimum allowable rod position is 0.

2. Initial Conditions

2.1 None

3. Procedure

NOTE: All curves/tables used in this procedure are found in OP/1(2)/A/6100/022 (Unit One (Two) Data Book). These procedures will be referred to as the "Data Book."

- 3.1 Record the following:
 - □ 3.1.1
 Unit ____ Cycle ____

 □ 3.1.2
 Recent trends on ECP
Reactor Engineer contacted: ______ Date _____

 □ 3.1.3
 Date/Time of Shutdown: _____/_____

 □ 3.1.4
 Anticipated Date/Time of Criticality: _____/

 □ 3.1.5
 Burnup: (P1457)

| 3.1.6 | Enclosure 4.2 Estimated Critical Rod Position (ECP) NC System Effective Boron Concentration: | OP/ 0 /A/6100/006 Page 2 of 6 |
|---------|---|---|
| | 3.1.6.1 IF Pulling Rods to Criticality: | |
| | A. <u>IF</u> OAC is unavailable, record the current NC Boron Concentration | ppm |
| | B. <u>IF</u> OAC is available: | |
| | □ 1. Record B-10 Atom Percent, Best Estimate (P5613) | % |
| | □ 2. Record the current NC Boron Concentration | ppm |
| ş | □ 3. Calculate the Effective Boron C (Step 3.1.6.1B.2 x Step 3.1.6.1B.1)÷ | |
| | (x) ÷ 19.8 = | ppm |
| | 3.1.6.2 IF Dilution to Criticality, record All Roc Out, HZP, Critical Boron Concentration for 0 EFPD. (Databook Graph 6.1) | |
| | 3.1.6.3 Record the Effective Boron Concentration (Step 3.1.6.1A or Step 3.1.6.1B.3 or 3.1.6.2) = | on: ppm |
| □ 3.1.7 | Xenon worth at anticipated time of criticality (from OAC program Xenon Samarium - XESM or REACT program). | pcm |
| 3.1.8 | IF burnup from step 3.1.5 is > 0 EFPD, record the difference between equilibrium and present samarium worth (P1475, Samarium program on OAC or REACT). {MCEI-0400-150} | pcm |
| 3.1.9 | <u>IF</u> burnup from step 3.1.5 is > 12 EFPD, perform Enclosure 4.8 to determine the fission product correct | ppmb tion. |

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OP/**0**/A/6100/006 Page 3 of 6

Estimated Critical Rod Position (ECP)

- _ 3.2 <u>IF</u> desired, perform automated calculations using REACT (Reactivity Balance ECP module) by performing the following:
 - □ 3.2.1 Enter data from Section 3.1 into REACT and calculate, ensuring effective boron concentration from 3.1.6.3 is used as NC System Boron concentration.
 - \Box 3.2.2 Attach REACT output to this enclosure.
 - \square 3.2.3 N/A section 3.3 and go to step 3.4.

3.3 Manual Calculations:

- 3.3.1 Boron Concentration:
 - □ 3.3.1.1 Determine the all rods out (ARO), hot zero power (HZP), no xenon, equilibrium samarium, boron concentration for present burnup from Step 3.1.5 (Data Book Graph 6.1).
 - \Box 3.3.1.2 Record value in Table 4.2.1 Line A.
- 3.3.2 Differential Boron Worth:
 - □ 3.3.2.1 Determine the ARO differential boron worth for present burnup of step 3.1.5 (Data Book Graph 6.8)
 - \Box 3.3.2.2 Record value in Table 4.2.1 Line B.

OP/**0**/A/6100/006 Page 4 of 6

Estimated Critical Rod Position (ECP)

- Determine the Rod Inserted Worth: 3.3.3
 - □ 3.3.3.1 Record values from Steps 3.1.6 - 3.1.9 in Table 4.2.1.
 - Complete Table 4.2.1, recording 0 for any N/A'd Reference Steps. □ 3.3.3.2

| Description | Reference | Value | |
|---|------------------------|---------|--|
| A. ARO, HZP, No Xenon, Eq. Samarium Boron | Step 3.3.1 | ppm | |
| B. ARO DBW | Step 3.3.2 | pcm/ppm | |
| C. Present Effective Boron Concentration | Step 3.1.6.3 | ppm | |
| D. Xenon Worth | Step 3.1.7 | pcm | |
| E. Diff from Eq Sm Worth | Step 3.1.8 | pcm | |
| F. Fission Product Correction | Step 3.1.9 | ppm | |
| G. Reactivity Equivalent of Boron Difference | (C - A) x B () x | pcm | |
| H. Reactivity Equivalent of Fission Product Correction. | F x B | pcm | |
| Reactivity of Inserted Rods | (D + E + G) - H | | |
| | (+ +) | pcm | |

Table 4.2.1 Rod Inserted Worth Calculation

- 3.3.4 **IF** result from Table 4.2.1 < 0 perform the following:
 - Perform Enclosure 4.1 for an ECB. □ 3.3.4.1
 - □ 3.3.4.2 Exit this Enclosure.
- Peak xenon worth: 3.3.5
 - Determine the peak xenon worth for present burnup from step □ 3.3.5.1 3.1.5 (Data Book Table 6.9).

Record value in Table 4.2.2 Line C. □ 3.3.5.2

OP/**0**/A/6100/006 Page 5 of 6

Estimated Critical Rod Position (ECP)

- 3.3.6 Calculate the Estimated Critical Rod Positions:
 - \Box 3.3.6.1 Record values from Step 3.1.7 and Table 4.2.1 in Table 4.2.2.
 - \Box 3.3.6.2 Complete Table 4.2.2.

Table 4.2.2: Estimated Critical Rod Positions

| Description | Reference | Value |
|---|---|----------------|
| A. Xenon Worth | Step 3.1.7 | pcm |
| B. Reactivity of inserted rods | Table 4.2.1 | pcm |
| C. Peak Xenon Worth | Step 3.3.5 | - pcm |
| D. Lower Band Reactivity Worth | B + 750 | pcm |
| E. Upper Band Reactivity Worth | B - 750 | pcm |
| F. No Xenon Rod Position for Reactivity of B | Data Book Table 6.3.A | Bank steps w/d |
| G. No Xenon Rod Position for Reactivity of D | Data Book Table 6.3.A | Bank steps w/d |
| H. No Xenon Rod Position for Reactivity of E | Data Book Table 6.3.A | Bank steps w/d |
| I. Peak Xenon Rod Position for Reactivity of B | Data Book Table 6.3.B | Bank steps w/d |
| J. Peak Xenon Rod Position for Reactivity of D | Data Book Table 6.3.B | Bank steps w/d |
| K. Peak Xenon Rod Position for Reactivity of E | Data Book Table 6.3.B | Bank steps w/d |
| Estimated Critical Position | [(I - F) x (A÷C)] + F [() x (÷)] + | Bank steps w/d |
| Lower Limit of Band | [(J - G) x (A÷C)] + G [() x (÷)] + | Bank steps w/d |
| Upper Limit of Band | [(K- H) x (A÷C)] + H [() x (÷)] + | Bank steps w/d |

| Enclosure | 4.2 |
|-----------|-----|
|-----------|-----|

OP/**0**/A/6100/006 Page 6 of 6

Estimated Critical Rod Position (ECP)

- 3.4 Check the following:
 - □ 3.4.1 Rod Positions of Table 4.2.2 or REACT output are greater than insertion limits per Data Book Graph 1.2.
 - □ 3.4.2 Rod Positions of Table 4.2.2 or REACT output are less than rod withdrawal limits per Data Book Table 2.8.
- 3.5 **IF** Step 3.4 **CANNOT** be met, contact Reactor Engineering.

Reactor Engineer Contacted / Date / Time

Calculations Performed By: ______ (RO) Date: _____

Separate Verification By: ______ (QRE) Date: _____

- 3.6 <u>**WHEN**</u> criticality is achieved, record the following Actual Critical Data (with power leveled off at 10^{-8} amps on I/R):
 - □ 3.6.1 Critical Time _____
 - \Box 3.6.2 T_{avg} at Time of Criticality _____°F
 - □ 3.6.3 Critical Rod Position: Bank _____ at ____ steps w/d
 - □ 3.6.4 Critical Boron Concentration _____ ppm
- \Box 3.7 Request that Primary Chemistry obtain an NC system boron sample for ¹⁰B analysis.
- 3.8 **IF** criticality is achieved outside the upper or lower band rod position, generate a N coded Reactivity Management PIP.

PIP Number:

□ 3.9 Forward a copy of this Enclosure to Reactor Engineering.

End of Enclosure

1. Limits and Precautions

None

2. Initial Conditions

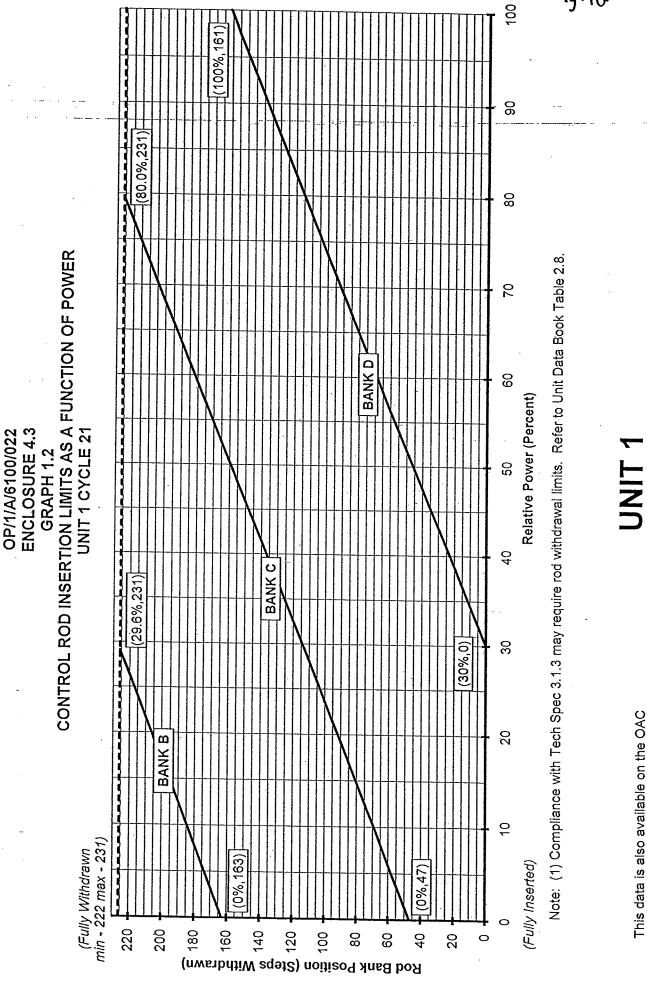
None

3. Procedure

| 1 | | | | | | | |
|-------|---|------------------|---|--|--|--|--|
| NOTE: | All curves/tables used in this procedure are found in OP/1(2)/A/6100/022 (Unit One (Two) Data Book). These procedures will be referred to as the "Data Book." | | | | | | |
| | 2. Number of hours shutdown is the difference in time between the time the reactor went subcritical and the expected time of criticality. | | | | | | |
| 3.1 | Shute | lown Fission Pro | oduct Correction Calculation: | | | | |
| | _ 3.1.1 | IF Unit op | erated > 3 EFPD from previous shutdown to current shutdown: | | | | |
| | | □ 3.1.1.1 | Use Data Book Table 6.7 to determine the shutdown fission product correction: | | | | |
| | | □ 3.1.1.2 | Number of hours shutdown hrs | | | | |
| | | □ 3.1.1.3 | Shutdown Fission Product Correction: ppm | | | | |
| | _ 3.1.2 | IF Unit op | erated < 1 EFPD from previous shutdown to current shutdown: | | | | |
| | | □ 3.1.2.1 | Use Data Book Table 6.7 to determine the shutdown fission product correction based on the number of hours since the first shutdown: | | | | |
| | | □ 3.1.2.2 | Number of hours since shutdown hrs | | | | |
| | | □ 3.1.2.3 | Shutdown Fission Product Correction: ppm | | | | |

| | Enclosure 4.8 | |
|-----------|--|-------------------------|
| | Fission Product Correction Calculation | Page 2 of 2 |
| current | t operated between 1 EFPD and 3 EFPD fror shutdown and current shutdown < 72 hours rmine the shutdown fission product correction | use Data Book Table 6.7 |
| 3.1.3.1 | Previous Shutdown: | |
| | \Box A. Number of hours during previous | shutdown: hrs |
| | □ B. Shutdown fission product correction | on: ppm |
| 3.1.3.2 | Current Shutdown: | |
| | \Box A. Number of hours since current shu | tdown: hrs |
| | □ B. Shutdown fission product correction | on: ppm |
| □ 3.1.3.3 | Shutdown Fission Product Correction: | |
| | (Step 3.1.3.1B x 0.5) + Step 3.1.3.2B = | : |
| | (x 0.5) + | ppm |
| | t operated between 1 EFPD and 3 EFPD from shutdown and current shutdown > 72 hours: | |
| □ 3.1.4.1 | Use Data Book Table 6.7 to determine product correction using the time of the | |

- \Box 3.1.4.2 Number of hours shutdown _____ hrs
- □ 3.1.4.3 Shutdown Fission Product Correction: _____ ppm



UNIT 1

Chg AG

UNIT 1

OP/1/A/6100/022 ENCLOSURE 4.3

TABLE 2.8

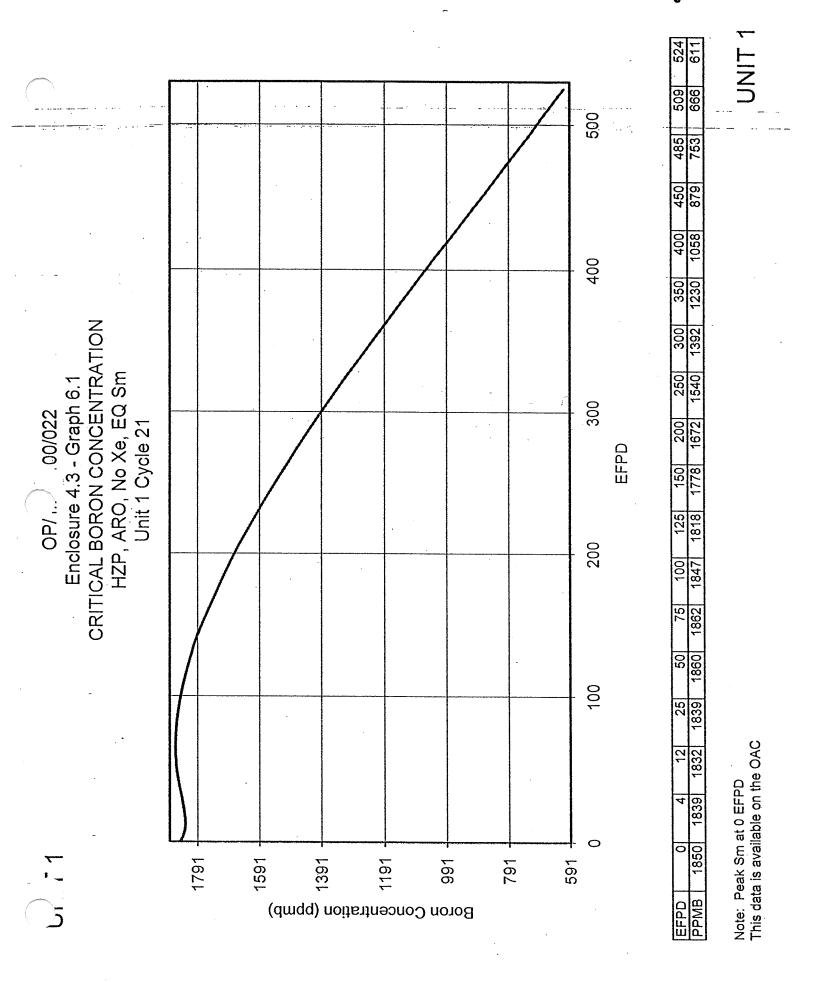
ROD WITHDRAWAL LIMITS

McGUIRE UNIT 1 CYCLE 21

McGuire Unit 1 is required to operate with a Moderator Temperature Coefficient within the limits of Tech Spec 3.1.3 and as shown in the McGuire Unit 1 Cycle 21 Core Operating Limits Report, MCEI-0400-232, Revision 0.

For McGuire Unit 1 Cycle 21, there are NO ROD WITHDRAWAL LIMITS.

UNIT 1



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Enclosure 4.3 - Table 6.3.A Integral Rod Worth in Overlap HZP, No Xenon

Unit 1 Cycle 21

| | • | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|-----------------------|-----------|-------------|---------------|----------------|----------------|-----------|----------|----------|
| Control Bank Position | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW | | |
| Step | s Withdra | wn * | | IRW | IRW | IRW | IRW | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 226 | 226 | 226 | 226 | 0 | 0 | 0 | 0 | 0 |
| 226 | 226 | 226 | 225 | 2 | 1 | 2 | 2 | 3 |
| 226 | 226 | 226 | 220 | 14 | 8 | 9 | 13 | 18 |
| 226 | 226 | 226 | 215 | 26 | 15 | 17 | 24 | 33 |
| 226 | 226 | 226 | 210 | 39 | 22 | 25 | 35 | 49 |
| 226 | 226 | 226 | 205 | 63 | 41 | 47 | 63 | 84 |
| 226 | 226 | 226 | 200 | 88 | 59 | 68 | 91 | 119 |
| 226 | 226 | 226 | 195 | 113 | 77 | 90 | 120 | 155 |
| 226 | 226 | 226 | 190 | 138 | 95 | 111 | 148 | 190 |
| 226 | 226 | 226 | 185 | 161 | 117 | 136 | 179 | 225 |
| 226 | 226 | 226 | 180 | 184 | 138 | 161 | 209 | 259 |
| 226 | 226 | 226 | 175 | . 207 | 160 | 186 | 240 | 294 |
| 226 | 226 | 226 | 170 | 230 | 181 | 211 | 271 | 329 |
| - ?^ _ | 226 | 226 | 165 | 250 | 202 | 235 | 296 | 355 |
| | 226 | 226 | 160 | 270 | 223 | 258 | 322 | 381 |
| <u> </u> | 226 | 226 | 155 | 290 | 245 | 281 | 347 | 407 |
| 6 | 226 | 226 | 150 | 311 | 266 | 305 | 373 | 433 |
| _226 | 226 | 226 | 145 | 327 | 286 | 325 | 392 | 450 |
| 226 | 226 | 226 | 140 | 344 | 306 | 345 | 412 | 467 |
| 226 | 226 | 226 | 135 | 361 | 326 | 366 | 431 | 484 |
| 226 | 226 | 226 | 130 | 378 | 346 | 386 | 450 | 501 |
| 226 | 226 | 226 | 125 | 393 | 364 | 404 | ·465 | 512 |
| 226 | 226 | 226 | 120 | 407 | . 383 | 421 | 479 | 522 |
| 226 | 226 | 226 | 116 | 418 | 398 | 435 | 490 | 531 |
| 226 | 226 | 226 | 110 | 433 | 418 | 454 | 504 | 540 |
| 226 | 226 | 221 | 105 | 454 | 438 | 473 | 523 | 561 |
| _226 | 226 | 216 | 100 | 475 | 459 | 492 | 542 | 583 |
| 226 | 226 | 211 | 95 | 514 | 491 | 527 | 584 | 637 |
| 226 | 226 | 206 | 90 | 553 | 524 | 562 | 627 | 692 |
| 226 | 226 | 201 | 85 | 593 | 557 | 596 | 670 | 747 |

NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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UNII 1

Enclosure 4.3 - Table 6.3.A Integral Rod Worth in Overlap HZP, No Xenon

Unit 1 Cycle 21

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| | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|-----------------------|------------|-------------|-----------------|----------------|----------------|---------------|----------|----------|
| Control Bank Position | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW | | |
| Steps Withdrawn * | | IRW | IRW | IRW | IRW | IRW | | |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | · · · · (PCM) | (PCM) | (PCM) |
| 226 | 226 | 196 | 80 | 632 | 589 | 631 | 712 | 801 |
| 226 | 226 | 191 | 75 | 670 | - 626 | 672 | 762 | 862 |
| 226 | 226 | 186 | 70 | 707 | 664 | 713 | 812 | 923 |
| 226 | 226 | 181 | 65 | 745 | 701 | 754 | 862 | 984 |
| 226 | 226 | 176 | 60 | 782 | . 739 | 795 | 911 | 1045 |
| 226 | 226 | 171 | 55 | 819 | 777 | 836 | 957 | 1097 |
| 226 | 226 | 166 | 50 | 856 | 816 | 878 | 1004 | 1148 |
| 226 | 226 | 161 | 45 | 893 | 855 | 919 | 1050 | 1200 |
| 226 | 226 | 156 | 40 | 930 · | 894 | 961 | 1096 | 1251 |
| 226 | 226 | 151 | 35 | 969 | 934 | 1002 | 1138 | 1295 |
| 226 | 226 | 146 | 30 | 1008 | 974 | 1043 | 1181 | 1338 |
| 226 | 226 | 141 | 25 | 1047 | 1014 | 1084 | 1224 | 1381 |
| 226 | 226 | 136 | 20 | 1086 | 1054 | 1125 | 1266 | 1425 |
| 225 | 226 | 131 | [.] 15 | 1124 | 1091 | 1162 | 1302 | 1457 |
| ~ _ | 226 | 126 | 10 | 1161 | 1129 | 1199 | 1338 | 1489 |
| 6 | 226 | 121 | 5 | 1198 | 1167 | 1236 | 1374 | 1522 |
| 226 | 226 | 116 | 0 | 1235 | 1205 | 1273 | 1410 | ` 1554 |
| 226 | 226 | 110 | 0 | 1269 | 1246 | 1312 | 1446 | 1583 |
| 226 | 221 | 105 | 0 | 1300 | 1282 | 1346 | 1477 | 1611 |
| 226 | 216 | 100 | 0 | 1330 | 1318 | 1380 | 1508 | 1639 |
| 226 | 211 | 95 | 0 | 1367 | 1360 | 1420 | 1547 | 1682 |
| 226 | 206 | 90 | 0 | 1404 | 1402 | 1461 | 1587 | 1725 |
| 226 | 201 | 85 · | 0 | 1441 | 1444 | 1501 | 1627 | 1769 |
| 226 | 196 | 80 | 0 | 1477 | 1486 | 1541 | 1666 | 1812 |
| 226 | 191 | 75 | 0 | 1523 | 1534 | 1589 | 1712 | 1859 |
| 226 | 186 | 70 | 0 | 1569 | 1583 | 1636 | 1758 | 1907 |
| 226 | 181 | 65 | 0 | 1614 | 1632 | 1683 | 1804 | 1954 |
| 226 | 176 | 60 | 0 | 1660 | 1680 | 1730 | 1850 | 2002 |
| 226 | 171 | 55 | 0 | 1719 | 1732 | 1781 | 1897 | 2044 |
| 226 | 166 | 50 | 0 | 1778 | 1784 | 1831 | 1944 | 2087 |

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*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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UNIT

UNII 1

Enclosure 4.3 - Table 6.3.A Integral Rod Worth in Overlap HZP, No Xenon

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Unit 1 Cycle 21

| | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|-----------|------------|--------|------|-------------|---------------|----------------|----------------|-----------|
| Contro | l Bank Po | sition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Step | s Withdrav | wn * | | IRW | IRW | IRW | IRW | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | ·(PCM) |
| 226 | 161 | · 45 | 0 | 1836 | 1837 | 1881 | 1991 | 2130 |
| 226 | 156 | 40 | 0 | 1895 | 1889 | 1932 | 2038 | 2172 |
| 226 | 151 | 35 | 0 | 1954 | 1933 | 1974 | 2076 | 2203 |
| 226 | 146 | 30 | 0 | 2013 | 1978 | 2016 | 2114 | 2234 |
| 226 | 141 | 25 | 0 | 2072 | 2022 | 2058 | 2151 | 2265 |
| 226 | 136 | 20 | 0 . | 2131 | 2066 | 2100 | 2189 | 2295 |
| 226 | 131 | 15 | 0 | 2168 | 2097 | 2127 | 2212 | 2312 |
| 226 | 126 | 10 | 0 | 2205 | 2127 | 2155 | 2235 | 2329 |
| 226 | 121 | 5 | 0 | 2241 | 2158 | 2183 | 2257 | 2346 |
| 226 | 116 | 0 | 0 | 2278 | 2188 | 2210 | 2280 | 2363 |
| 226 | 110 | 0 | 0. | 2300 | 2213 | 2233 | 2297 | 2375 |
| 221 | 105 | 0 | 0 | 2323 | 2236 | 2255 | 2317 | 2396 |
| 216 | 100 | 0 | 0 | 2347 | 2260 | 2276 | 2337 | 2416 |
| 211 | 95 | 0 | 0 | 2379 | 2291 | 2309 | 2374 | 2460 |
| <u> </u> | 90 | 0 | 0 | 2412 | 2323 | 2342 | 2411 | 2504 |
| | 85 | 0 | 0 | 2445 | 2355 | 2375 | 2448 | 2548 |
| <u>)6</u> | 80 | 0 | 0 | 2477 | 2387 | 2407 | 2485 | 2592 |
| 191 | 75 | 0 | 0 | 2510 | 2422 | 2445 | 2527 | 2639 |
| 186 | 70 | 0 | 0 | 2542 | 2457 | 2483 | 2569 | 2686 |
| 181 | 65 | 0 | 0 | 2574 | 2493 | 2521 | 2611 | 2732 |
| 176 | 60 | 0 | 0 | 2606 | 2528 | 2558 | 2653 | 2779 |
| 171 | 55 | 0 | 0 | 2640 | 2565 | 2596 | 2691 | 2816 |
| 166 | 50 | 0 | Ó | 2674 | 2601 | 2634 | 2730 | 2853 |
| 161 | 45 | 0 | 0 | 2708 | 2638 | 2673 | 2768 | 2890 |
| 156 | 40 | 0 | : 0 | 2742 | 2675 | 2711 | 2806 | 2928 |
| 151 | 35 | 0 | 0 | 2774 | 2710 | 2746 | 2839 | 2955 |
| 146 | 30 | 0 | 0 | 2807 | 2746 | 2781 | 2871 | 2982 |
| 141 | 25 | 0 | 0 | 2839 | 2782 | 2816 | 2903 | 3008 |
| 136 | 20 | 0 | 0 | 2871 | 2817 | 2852 | 2936 | 3035 |
| 131 | 15 | 0 | 0 | 2895 | 2848 | 2880 | 2959 | 3051 |

*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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Enclosure 4.3 - Table 6.3.A Integral Rod Worth in Overlap HZP, No Xenon

Unit 1 Cycle 21

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| | | | 1 | . 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|--------------|------------|---------|------|-------------|---------------|----------------|----------------|-----------|
| Contro | ol Bank Po | osition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Step | s Withdra | wn * | | IRW | IRW | IRW | IRW | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 126 | 10 | 0 | 0 | 2920 | 2878 | 2908 | 2981 | 3067 |
| 121 | 5 | 0 | 0 | 2944 | 2909 | 2937 | 3004 | 3083 |
| <u>116 ·</u> | θ. | 0 - | 0 | 2969 | 2939 | 2965 | 3027 | 3098 |
| 110 | 0 | 0 | 0 | 2988 | 2970 | 2993 | 3047 | 3110 |
| 105 | 0 | 0 | 0 | 3003 | 2994 | 3014 | 3060 | 3118 |
| _ 100 | 0 | 0 | 0 | 3018 | 3018 | 3035 | 3074 | 3126 |
| 95 | 0 | 0 | 0 | 3030 | 3039 | 3052 | 3084 | 3130 |
| 90 | 0 | 0 | 0 | 3042 | 3060 | 3069 | 3093 | 3134 |
| 85 | 0 | 0 | 0 | 3054 | 3081 | 3087 | 3103 | 3139 |
| 80 | 0 | 0 - | 0 | 3066 | 3102 | 3104 | 3112 | 3143 |
| 75 | 0 | 0 | 0 | 3074 | 3117 | 3115 | -3117 | 3145 |
| 70 | 0 | 0 | 0 | 3082 | 3131 | 3126 | 3123 | 3147 |
| 65 | 0 | 0 | 0 | 3090 | 3145 | 3137 | 3128 | 3149 |
| 60 | 0 | 0 | 0 | 3099 | 3160 | 3148 | 3133 | 3151 |
| | 0 | 0 | 0 | 3103 | 3167 | 3153 | 3135 | 3152 |
| \sim $-$ | 0 | 0 | 0 | 3108 | 3174 | 3159 | 3138 | 3153 |
| | 0 | 0 · | 0 | 3112 | 3182 | 3164 | 3140 | 3154 |
| 40 | 0 | 0 | 0 | 3117 | 3189 | 3170 | 3143 | 3155 |
| 35 | 0 | 0 | 0 | 3119 | 3192 | 3172 | 3144 | 3155 |
| 30 | 0 | 0 | 0 | 3121 | 3195 | 3174 | 3145 | 3156 |
| 25 | 0 | 0 | 0 | 3124 | 3198 | 3176 | 3146 | 3156 |
| 20 | Ó | 0 | 0 | 3126 | 3201 | 3179 | 3147 | 3156 |
| 15 | 0 | 0 | 0 · | 3127 | 3202 | 3179 | 3147 | 3156 |
| 10 | 0 | 0 | 0 | 3128 | 3203 | 3180 | 3147 | 3157 |
| 5 | 0 | 0 | 0 | 3129 | 3204 | 3180 | 3148 | 3157 |
| 0 | 0 | 0 | 0 | 3130 | 3205 | 3181 | 3148 | 3157 |

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'NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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UNIT '

Enclosure 4.3 - Table 6.3.A Integral Rod Worth in Overlap HZP, No Xenon

Unit 1 Cycle 21

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| | | • | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|----------|------|-------------------------|-----------|---------|------|-------------|---------------|-----------------|----------------|-----------|
| Control | | Shutdo | wn Bank F | osition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Bank | | Step | s Withdra | wn * | | IRW | IRW | IRW | IRW | IRW |
| Position | SD E | SD D | SD C | SD B | SD A | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 226 | 226 | 226 [¨] | 226 | 226 | 226 | 0. | - 0 | 0 | 0 | 0 |
| 0 | 226 | 226 | 226 | 226 | 226 | 3130 | 3205 | 3181 | 3148 | 3157 |
| 0 | 0 | 226 | 226 | 226 | 226 | 3985 | 4047 | 3973 | 3911 | 3907 |
| 0 | 0 | 0 | 226 | 226 | 226 | 4497 | 4671 | 4658 | 4614 | 4623 |
| . 0 | 0 | 0 | 0 | 226 | 226 | 5047 | 5361 | 5438 | 5429 | 5463 |
| 0 | 0 | 0 | 0 | 0 | 226 | 6289 | 6430 | 6420 | 6370 | 6394 |
| 0 | 0 | 0 | 0 | 0 | 0 | 6402 | 6563 | 6568 | 6525 | 6562 |

*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

UNIT

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Enclosure 4.3 - Table 6.3.B Integral Rod Worth in Overlap HZP, Peak Xenon

Unit 1 Cycle21

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| | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|------------------|-------------|--------|------|-------------|---------------|----------------|----------------|-----------|
| Contr | ol Bank Po | sition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Ste | ps Withdrav | wn * | | IRW | IRW " | · IRW | IRW | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 226 | 226 | 226 | 226 | 0 | 0 | 0 | 0 | 0 |
| 226 | 226 | 226 | 225 | 3. | 2 | 3 | 3 | 4 |
| 226 | 226 | 226 | 220 | 19 | 15 | 16 | 19 | 23 |
| 226 | 226 | 226 | 215 | 34 | 27 | 29 | 34 | 42 |
| 226 | 226 | 226 | 210 | 49 | 39 - | 42 | 50 | 61 |
| 226 | 226 | 226 | 205 | 81 | 69 | 75 | 88 | 103 |
| 226 | 226 | 226 | 200 | 113 | 99 | 109 | 126 | 145 |
| 226 | 226 | 226 | 195 | 144 | 129 | 142 | 163 | 187 |
| 226 | 226 | 226 | 190 | 176 | 159 - | 175 | 201 | 229 |
| 226 | 226 | 226 | 185 | 203 | 188 | 209 | 238 | 267 |
| 226 | 226 | 226 | 180 | 231 | 218 - | 243 | 274 | 305 |
| 226 · | 226 | 226 | 175 | 259 | 248 | 276 | 311 | . 343 |
| 226 | 226 | 226 | 170 | 286 | 278 | 310 | 347 | 381 |
| ک ر ا | 226 | 226 | 165 | 308 | 302 | 336 | 374 | 407 |
| ~ <u>.</u> | 226 | 226 | 160 | 330 | 326 | 362 | 400 | 432 |
| 26 | 226 | 226 | 155 | 352 | 350 | 389 | 427 | 458 |
| 226 | 226 | 226 | 150 | 373 | 375 | 415 | 453 | 484 |
| 226 | 226 | 226 | 145 | 390 | 393 | 434 | 470 | 499 |
| 226 | 226 | 226 | 140 | 407 | 412 | 452 | 487 | 514 |
| 226 | 226 | 226 | 135 | 423 | 430 | 471 | 504 | 529 |
| 226 | 226 | 226 | 130 | 440 | 449 | 489 | 521· | 544 |
| 226 | 226 | 226 | 125 | 453 | 463 | 502 | 532 | 553 |
| 226 | 226 | 226 | 120 | 466 | 478 | 515 | 542 | 561 |
| 226 | 226 | 226 | 116 | 477 | 489 | 525 · | 550 | 568 |
| 226 | 226 | 226 | 110 | 490 | 503 | 536 | 559 | . 574 |
| 226 | 226 | 221 | 105 | 512 | 523 | 556 | 580 | 599 |
| 226 | 22,6 | 216 | 100 | 534 | 543 | 575 | 601 | 623 |
| 226 | 226 | 211 | 95 | 580 | 587 | 625 | 658 | 689 |
| 226 | 226 | 206 | 90 | 627 | 630 | 674 | 715 | 755 |
| 226 | 226 | 201 | 85 | 674 | · 674 | 723 | 773 | 821 |

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*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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UNIT

UNIT 1

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Enclosure 4.3 - Table 6.3.B Integral Rod Worth in Overlap HZP, Peak Xenon

Unit 1 Cycle21

| | | | ••• | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|-------------------------|----------|------------|---------|------|-------------|---------------|----------------|----------------|-----------|
| | Contre | ol Bank Po | osition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| | Step | s Withdra | wn * | | IRW | IRW | IRW | IRW | IRW |
| | Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | . (PCM) | (PCM) | (PCM) |
| | 226 | 226 | 196 | 80 | . 720 | 718 | 773 | 830 | 887 |
| | 226 | 226 | 191 - | 75 | 761 | 763 | 827 | 894 | 958 |
| | 226 | 226 | 186 | 70 | 802 | 808 | 881 | 957 | 1028 |
| | 226 | 226 | 181 | 65 | 843 | 854 | 935 | 1021 | 1099 |
| _ | 226 | 226 | 176 | 60 | 884 | . 899 | 990 | 1084 | 1169 |
| : | 226 | 226 | 171 | 55 | 923 | 942 | 1038 | . 1137 | 1225 |
| _ | 226 | 226 | 166 | 50 | 961 | 984 | 1085 | 1189 | 1280 |
| | 226 | 226 | 161 | 45 | 1000 | 1027 | 1133 | 1242 | 1336 |
| | 226 | 226 | 156 | 40 | 1039 | 1070 | 1181 | - 1295 | 1392 |
| | 226 | 226 | 151 | 35 | 1079 | 1111 | 1224 | 1338 | 1433 |
| | 226 | 226 | 146 | 30 · | 1119 | 1153 | 1267 | - 1381 | . 1475 |
| | 226 | 226 | 141 | 25 | 1159 | 1194 | 1310 | 1424 | 1516 |
| | 226 | 226 | 136 | 20 | 1200 | 1236 | 1354 | 1467 | 1558 |
| | <u>م</u> | 226 | 131 | 15 | 1236 | 1271 | 1388 | 1498 | 1584 |
| , and the second second | <u>;</u> | 226 | 126 | 10 | 1272 | 1307 | 1423 | 1529 | 1610 |
| | _26 | 226 | 121 | 5 | 1308 | 1342 | 1457 | 1561 | 1636 |
| | 226 | 226 | 116 | 0 | 1344 | 1377 | 1492 | 1592 | 1662 |
| - | 226 | 226 | 110 | 0 | 1375 | 1410 | 1524 | 1618 | 1682 |
| | 226 | 221 | 105 | 0 | 1403 | 1439 | 1553 | 1645 | 1709 |
| | 226 | 216 | 100 | 0 | 1431 | 1468 | 1582 | 1673 | 1736 |
| | 226 | 211 | 95 | 0 | 1467 | 1506 | 1624 | 1721 | 1792 |
| _ | 226 | 206 | 90 | 0 | 1502 | .1544 | 1666 | 1769 | 1847 |
| | 226 | 201 | 85 | 0 | 1537 | 1582 | 1708 | 1817 | 1903 |
| _ | 226 | 196 | 80 | 0 | 1572 | 1620 | 1750 | 1866 | 1958 |
| | 226 | 191 | 75 | 0 | 1616 | 1666 | 1799 | 1918 | 2015 |
| | 226 | 186 | 70 | 0 | 1660 | 1713 | 1847 | 1970 | 2072 |
| | 226 | 181 | 65 | 0 | 1703 | 1759 | 1895 | 2022 | 2129 |
| | 226 | 176 | 60 | 0 | 1747 | 1806 | 1944 | 2074 | 2186 |
| _ | 226 | 171 | 55 | 0 | 1805 | 1862 | 1996 | 2121 | 2230 |
| _ | 226 | 166 | 50 | 0 | 1863 | 1919 | 2047 | 2168 | 2275 |

*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

UNIT 1

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Enclosure 4.3 - Table 6.3.B Integral Rod Worth in Overlap HZP, Peak Xenon

Unit 1 Cycle21

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| | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|-----------|------------|--------|------|-------------|---------------|----------------|----------------|-----------|
| Contr | ol Bank Po | sition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Step | os Withdra | wn * | | IRW | IRW | IRW | IRW - | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 226 | 161 | 45 | ·``0 | 1921 | 1975 | 2099 | 2215 | 2320 |
| 226 | 156 | 40 | 0 | 1979 | 2032 | 2151 | 2262 | 2364 |
| 226 | 151 | 35 | 0 | 2043 | 2085 | 2195 | 2298 | 2395 |
| 226 | 146 | 30 | 0 | 2106 | 2139 | 2239 | 2333 | 2425 |
| 226 | 141 | 25 | 0 | 2170 | 2193 | 2282 | 2368 | 2455 |
| 226 | 136 | 20 | 0 | 2233 | 2246 | 2326 | 2404 | 2485 |
| 226 | 131 | 15 | 0 | 2275 | 2279 | 2352 | 2423 | 2501 |
| 226 | 126 | 10 | 0 | 2316 | 2313 | 2378 | 2443 | 2516 |
| 226 | 121 | 5 | 0 | 2357 | 2346 | 2404 | 2463 | 2532 |
| 226 | 116 | 0 | 0 | 2398 | 2379 | . 2430 | 2482 | 2548 |
| 226 | - 110 | 0 | 0 | 2421 | 2401 | 2448 | 2496 | 2558 |
| 221 | 105 | 0 | 0 | 2445 | 2424 | 2469 | 2516 | 2579 |
| 216 | 100 | 0 | 0 | 2469 | 2447 | 2490 | 2536 | 2601 |
| 211 | 95 | 0 | 0 | 2503 | 2483 | 2529 | 2578 | 2646 |
| <u>کر</u> | 90 | 0 | 0 | 2536 | 2518 | 2567 | 2620 | 2692 |
| <u> </u> | 85 | 0 | 0 | 2570 | 2553 | 2606 | 2662 | 2738 |
| 96 | 80 | 0 | 0 | 2603 | 2588 | 2644 | 2704 | 2783 |
| 191 | 75 | 0 | 0 | 2637 | 2626 | 2685 | 2748 | 2828 |
| 186 | 70 | 0 | 0 | 2670 | 2664 | 2727 | 2791 | 2873 |
| | 65 | 0 | 0 | 2704 | 2702 | 2768 | 2835 | 2917 |
| 176 | 60 | 0 | 0 | 2738 | 2740 | 2809 | 2878 | 2962 |
| 171 | 55 | 0 | 0 | 2773 | 2778 | 2846 | 2913 | 2993 |
| 166 | 50 | 0 | 0 | 2808 | 2816 | 2882 | 2947 | 3025 |
| 161 | 45 | 0 | 0 | 2843 | 2854 | 2918 | 2981 | 3056 |
| 156 | 40 | 0 | 0 | 2878 | 2892 | 2955 | 3015 | 3088 |
| 151 | 35 | 0 | 0 | 2908 | 2923 | 2983 | 3038 | 3107 |
| 146 | 30 | 0 | 0 | 2938 | 2955 | 3010 | 3061 | 3126 |
| 141 | 25 | 0 | 0 | 2968 | 2987 | 3038 | 3084 | 3145 |
| 136 | 20 | 0 | 0 | 2998 | 3019 | 3066 | 3107 | 3164 |
| 131 | 15 | 0 | 0. | 3017 | 3039 | 3083 | 3120 | 3174 |

*NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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Enclosure 4.3 - Table 6.3.B Integral Rod Worth in Overlap HZP, Peak Xenon

Unit 1 Cycle21

| | | | 1 | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|----------|------------|---------|------|-------------|---------------|----------------|----------------|-----------|
| Contro | ol Bank Po | osition | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Step | s Withdra | wn * | | IRW | IRW | IRW | IRW | IRW |
| Bk A | Bk B | Bk C | Bk D | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 126 | 10 | 0 | 0 | 3035 | 3060 | 3100 | 3132 | 3184 |
| 121 | 5 | 0 | 0 | 3054 | 3081 | 3117 | 3145 | 3193 |
| 116 | 0 | • 0' | | 3072 | 3101 | 3134 | 3158 | 3203 |
| 110 | 0 | 0 | 0 | 3085 | 3118 | 3147 | 3167 | 3210 |
| 105 | 0 | 0 | 0 | 3094 | 3129 | 3156 | 3173 | 3213 |
| 100 | 0 | 0 | 0 | 3103 | 3140 | 3165 | 3179 | 3217 |
| 95 | 0 | 0 | 0 | 3110 | 3149 | 3170 | 3182 | 3219 |
| 90 | 0 | 0 | 0 | 3117 | 3157 | 3176 | 3185 | 3221 |
| 85 | 0 | 0 | 0 | 3123 | . 3165 | 3181 | 3189 | 3224 |
| 80 | 0 | 0 | 0 | 3130 | 3174 | 3187 | 3192 | 3226 |
| 75 | 0 | 0 - | 0 | 3134 | 3179 | 3190 | 3194 | 3226 |
| 70 | 0 | 0 | 0 | 3138 | 3183 | 3193 | 3195 | . 3227 |
| 65 | 0 | 0 | 0 | 3142 | 3188 | 3196 | 3196 | 3228 |
| 60 | 0 | 0 | 0 | 3146 | 3193 | 3198 | 3198 | 3229 |
| · • • | 0 | 0 | 0 | 3149 | 3196 | 3200 | 3199 | 3229 |
| <u> </u> | 0 | 0 | 0 | 3151 | 3199 | 3201 | 3199 | 3229 |
| | . 0 | 0 | 0 | 3153 | 3201 | 3203 | 3200 | 3230 |
| 40 | 0 | 0 | 0 | . 3156 | 3204 | 3204 - | 3201 | 3230 |
| 35 | . 0 | 0 | 0 | 3157 | 3205 | 3205 | 3201 | 3230 |
| <u> </u> | 0 | 0 | 0 | 3158 | 3206 | 3205 | 3201 | 3230 |
| 25 | 0 | 0 | 0 | 3160 | 3208 | 3206 | 3201 | 3230 |
| 20 | 0 | 0 | 0 | 3161 | 3209 | 3207 | 3202 | 3230 |
| 15 | 0 | 0 | 0 | 3161 | 3209 | 3207 | 3202 | 3230 |
| 10 | 0 | 0 | 0 | 3162 | 3210 | 3207 | 3202 | 3230 |
| 5 | 0 | 0 | 0 | 3162 | 3210 | 3207 | 3202 | 3231 |
| | 0 | 0 | 0 | 3163 | 3211 | 3208 | 3202 | 3231 |

NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

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Enclosure 4.3 - Table 6.3.B Integral Rod Worth in Overlap HZP, Peak Xenon

Unit 1 Cycle21

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| | | | | | | 4 EFPD | 100 EFPD | 200 EFPD | 300 EFPD | 400 EFPD |
|----------|------|--------|------------|----------|------|-------------|---------------|----------------|----------------|-----------|
| Control | • | Shutdo | wn Bank F | Position | | 0 - 50 EFPD | 51 - 150 EFPD | 151 - 250 EFPD | 251 - 350 EFPD | 351 - EOW |
| Bank | | Step | os Withdra | wn * | | IRW 1 | IRW | IRW | . IRW | IRW |
| Position | SD E | SD D | SD C | SD B | SD A | (PCM) | (PCM) | (PCM) | (PCM) | (PCM) |
| 226 | 226 | 226 | 226 | 226 | 226 | • | 0 | 0 | 0 | 0 |
| 0 | 226 | 226 | 226 | 226 | 226 | 3163 | 3211 | 3208 | 3202 | 3231 |
| -0 | 0 | 226 | 226 | 226 | 226 | 3925 | 3955 | 3916 | 3890 | 3906 |
| 0 | 0 | 0 | 226 | 226 | 226 | 4506 | 4639 | 4652 | 4643 | 4674 |
| . 0 | Ó | 0 | 0 | 226 | 226 | 5152 | 5424 | 5515 | 5539 | - 5598 |
| 0 | 0 | 0 | 0 | 0 | 226 | 6427 | 6542 | 6544 | 6523 | 6567 |
| 0 | 0 | 0 | 0. | 0 | 0 | 6612 | 6749 | 6762 | 6749 | 6813 |

NOTE: For actual ALL Rods out Overlap Data, see Enclosure 4.3, Section 1.13 of the Data Book

UNIT

UNIT 1

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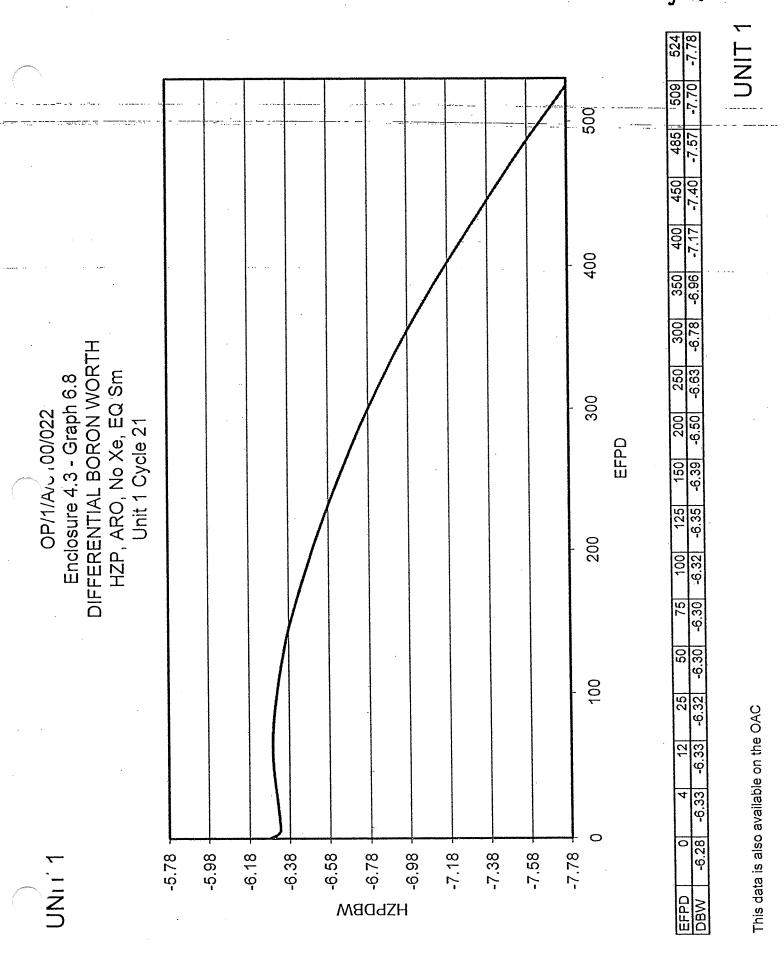
OP/ 1/A/6100/022 Enclosure 4.3 Table 6.7

Shutdown Fission Product Correction

| Tir | ne | Correction | · Ti | me | Correction | Τ | Tir | ne | Correction |
|---------|--------|------------|---------|--------|------------|-----|---------|--------|------------|
| (hours) | (days) | (ppm) | (hours) | (days) | (ppm) | | (hours) | (days) | (ppm) |
| 0 | 0.0 | 0 | 96 | 4.0 | 37 | | 192 | 8.0 | 46 |
| 8 | 0.3 | 3 | 104 | 4.3 | 38 | ' | 200 | 8.3 | 47 |
| 16 | 0.7 | 6 | 112 | 4.7 | . 39 | 1 | 208 | 8.7 | 47 |
| 24 | 1.0 | 10 | 120 | 5.0 | 39 | - | ,216 | 9.0 | 48 |
| 32 | 1.3 | . 14 | 128 | 5.3 | 40 | - | 224 | 9.3 | 49 |
| 40 | 1.7 | 18 | 136 | 5.7 | 41 | - | 232 | 9.7 | 49 |
| 48 | 2.0 | 23 | 144 | 6.0 | 41 | 1 | 240 | 10.0 | 50 |
| 56 | 2.3 | 27 | 152 | 6.3 | 42 | - | 480 | 20.0 | 53 |
| 64 | 2.7 | 31 | 160 | 6.7 | 43 | 1 - | 720 | 30.0 | 56 |
| 72 | 3.0 | 35 | 168 | 7.0 | 43 | - | 960 | 40.0 | 56 |
| 80 | 3.3 | 35 | 176 | 7.3 | 44 | - | 1200 | 50.0 | 56 |
| 88 | 3.7 | 36 | 184 | 7.7 | 45 | • | | | |

UNIT 1

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OP/1/A/6100/022 ENCLOSURE 4.3 TABLE 6.9

McGuire 1 Cycle 21

Xenon and Samarium Worths

| | HFP Equilibrium | HZP Peak | HFP Equilibrium |
|--------|-----------------|----------|-----------------|
| Burnup | Xenon | Xenon | Samarium |
| (EFPD) | _(pcm)_ | (pcm) | <u>(pcm)</u> |
| 0 | | - | 748 |
| 4 | 2523 | 3860 | 564 |
| 12 | _2519 | 3850 | 654 |
| 25 | 2523 | 3853 | 753 |
| 50 | 2534 | 3865 | 792 |
| 75 | 2548 | 3880 | 809 |
| 100 | 2564 | 3896 | 825 |
| 125 | 2580 | 3913 | 841 |
| 150 | 2597 | 3932 | 857 |
| 200 | 2632 | 3983 | 887 |
| 250 | 2668 | 4052 | 914 |
| 300 | 2706 | 4144 | 940 |
| 350 | 2744 | 4253 | 963 |
| 400 | 2783 | 4372 | 985 |
| 450 | 2822 | 4499 | 1006 |
| 485 | 2849 | 4603 | 1019 |
| 509 | 2868 | 4691 | 1028 |
| 524 | 2879 | 4738 | 1033 |
| | | | |



Chg AG Page 1 of 1

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JPM A1b RO

2010 Admin - JPM A1b RO

NUREG 1021, Revision 9

| Appendix C | Page 2 | of 8 | Form ES-C-1 |
|---------------------|--|----------------|--|
| | Job Performance Me | asure Workshee | t |
| | | | |
| Facility: | McGuire | Task No.: | 217MFW002 |
| Task Title: | Determine Boric Acid Addition to FWST | JPM No.: | <u>2010 Admin - JPM A1b</u> <u>RO</u> |
| K/A Reference: | GK/A 2.1.25 (3.9/4.2) | | |
| Examinee: | | NRC Examiner | , |
| Facility Evaluator: | | Date: | |
| Method of testing: | | | |
| Simulated Perform | ance: | Actual Perform | ance: X |
| Classr | oom X Simulator | Plant | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | • The plant was at 100% power when a leak developed on the FWST. |
|---------------------|---|
| | FWST Level dropped to 440 inches before leak was isolated. |
| | Enclosure 4.4, "FWST Makeup Using the RHT," of OP/1/A/6200/014, "Refueling Water System" is in progress and completed through Step 3.9. |
| | LCO 3.5.4, Refueling Water Storage Tank (RWST), was entered 10 minutes ago. |
| | Chemistry has provided the following information: |
| | BAT Boron Conc. = 7234 ppm |
| | RHT Boron Conc.= 1076 ppm |
| | FWST Make up Boron Concentration: Use COLR Minimum |

Task Standard:The operator will calculate the amount of Boric Acid that must be added
from the BAT to refill the FWST is 7,912 gallons +300/-75 gallons.

Required Materials: Calculator

General References: OP/1/A/6200/014, Refueling Water System

| Appendix C | Page 3 of 8 | Form ES-C-1 |
|---------------------|--|---------------------|
| | Job Performance Measure Worksheet | |
| | McGuire Core Operating Limits Report (Cycle 21) | |
| | McGuire U-1 Data Book | |
| | OMP 8-2, Component Verification Techniques | |
| Handouts: | Enclosure 4.4 of OP/1/A/6200/014, Refueling Wate for place-keeping through Step 3.9 as follows: | r System, marked up |
| | Initial Conditions 2.1 -2.3 are initialed. | |
| | • Procedure Step 3.1 – Checkbox is checked. | |
| | • Procedure Step 3.2 – Left blank (Conditional st | ep). |
| | Procedure Step 3.3 – initialed, Person Notified: present. | CHEMIST, date/time |
| | • Procedure Step 3.4 – NA, initialed. | |
| | • Procedure Step 3.5 – initialed. | |
| | • Procedure Step 3.6 – NA, initialed. | |
| | • Procedure Step 3.7 – NA, initialed. | |
| | • Procedure Step 3.8 – NA, initialed. | |
| | Procedure Step 3.9 – initialed, Person Notified: date/time: present. | R.P. TECH, |
| | McGuire 1 Cycle 21 Core Operating Limits Report | (Page 26 of 32) |
| | OP/1/A/6100/22, Enclosure 4.3, Curve 7.7, Refuelin Tank Level (Volume vs. Tank Level) | ng Water Storage |
| Initiating Cue: | Determine the amount of Boric Acid needed to rais 480" using the RHT in accordance with Step 3.10 c OP/1/A/6200/014, "Refueling Water System." | of Enclosure 4.4 of |
| Time Critical Task: | NO | |
| Validation Time: | 20 minutes | |
| | | |

C. C. Marine

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue (Last Page of this JPM), and Handout all three (3) identified Handout documents, marked up as described.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| *1 | (Step 3.10) Determine the amount of Boric Acid needed to raise makeup water to the limits specified in the Core Operating Limits Report (COLR). | The operator refers to the COLR, Section 2.13.1 on Page 26 of 32 and determines that the minimum boron concentration to be used in the calculation is 2675 ppm. The operator records <u>2675</u> ppm in the first line (Desired Page Concentration of | | |
| | | Boron Concentration of Addition from COLR) of the Doer Calculation in Step 3.10 of Enclosure 4.4. | | |
| *2 | (1 st Bullet) Desired Boron Concentration of Addition from COLR + 25 ppmB margin = Desired Boron Concentration | The operator adds an additional 25 ppm and determines Desired Boron Concentration to be 2700 ppm. The operator records 2700 ppm in the 2 nd line (Desired Boron Conc) of the Doer Calculation in Step 3.10 of Enclosure 4.4. | | |
| *3 | (2 nd Bullet) { <u>(Desired Cb) - (RHT Cb)</u> } (BAT Cb) - (RHT Cb) | The operator identifies Desired Cb = <u>2700</u> from previous Step and records. | | |
| | x {Desired Total Makeup Volume to FWST} | The operator recognizes that RHT Cb = <u>1076</u> ppm and records (Initial Conditions). | | |
| | = Desired BAT Volume | | | |

Appendix C

Page 5 of 8 PERFORMANCE INFORMATION

Form ES-C-1

| ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED |
|----------|--|---|---|
| | | | FOR UNSAT |
| | The operator recognizes | | |
| | that BAT Cb = <u>7234</u> ppm and records (Initial Conditions). | | |
| | The operator addresses OP/1/A/6100/22, Enclosure 4.3, Curve 7.7, and determines from graph that total makeup volume is 30,000 by comparing 480" volume of 390,000 gallons to the 440" volume of 360,000 gallons. | | |
| | The operator records <u>30,000 (+1300[#])</u> gallons. | | |
| | The operator calculates the Desired BAT Volume to be added to be 7,912 gallons +300/-75 gallons. | | |
| | The operator records <u>7,912</u> gallons <u>+300/-75</u> gallons as the Desired BAT Volume in the Doer Calculation. | | |
| | ELEMENTS | The operator recognizes that BAT Cb = 7234 ppm and records (Initial Conditions).The operator addresses OP/11/A/6100/22, Enclosure 4.3, Curve 7.7, and determines from graph that total makeup volume is 30,000 by comparing 480" volume of 390,000 gallons to the 440" volume of 360,000 gallons.The operator records 30,000 (+1300**) gallons.The operator calculates the Desired BAT Volume to be added to be 7.912 gallons +300/-75 gallons.The operator records 7.912 gallons $\pm 300/-75$ gallons as the Desired BAT Volume in | The operator recognizes that BAT Cb = 7234 ppm and records (Initial Conditions).The operator addresses OP/1/A/6100/22, Enclosure 4.3, Curve 7.7, and determines from graph that total makeup volume is 30,000 by comparing 480" volume of 390,000 gallons to the 440" volume of 360,000 gallons.The operator records 30,000 (+1300#) gallons.The operator calculates the Desired BAT Volume to be added to be 7.912 gallons +300/-75 gallons.The operator records 57.912 gallons ±300/-75 gallons as the Desired BAT Volume in |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

| Appendix C | Ap | pen | ıdix | С |
|------------|----|-----|------|---|
|------------|----|-----|------|---|

Page 6 of 8 VERIFICATION OF COMPLETION

Form ES-C-1

| Job Performance Measure No.: | <u> 2009 Admin - JPM A1b RO</u> |
|------------------------------|---------------------------------|
|------------------------------|---------------------------------|

Examinee's Name:

Date Performed:

Facility Evaluator:

Number of Attempts:

Time to Complete:

Question Documentation:

Result:

SAT UNSAT

Examiner's Signature: _____ Date: _____

Page 7 of 8 VERIFICATION OF COMPLETION

KEY:

Desired Boron Concentration from COLR + 25 ppmB = Desired Boron Concentration

2675 ppm (From COLR) + 25 ppmB = 2700 ppm

{(Desired Cb) - (RHT Cb)} x {Desired Total Makeup Volume to FWST} = Desired BAT Volume (BAT Cb) - (RHT Cb)

Given:

RHT Cb = **1076** ppm BAT Cb = **7234** ppm

Desired Total Makeup Volume to FWST = Overflow volume – Present volume (From Enclosure 4.3, Curve 7.7 of Unit 1 Core Data Book:) 390,000 gallons – 360,000 gallons (440") = **30,000** gallons[#]

#: If the operator uses develops a "gallons/inch" volume from the information block on Curve 7.7, the operator will determine the makeup volume to be 31,277 gallons.

Volume at 484 inches = 394,089 gallons Volume at 0 inches = 15,638 gallons

(394,089 gallons - 15,638 gallons)/484 inches = 781.92 gallons/inch

OR

Volume at 455.88 inches = 372,100 gallons Volume at 0 inches = 15,638 gallons

(372,100 gallons - 15, 638 gallons)/455.88 inches = 781.92 gallons/inch

Therefore, 781.92 gallons/inch x 40 inches = 31,276.80 gallons (This may be used as the makeup volume instead of 30,000 gallons).

If this volume is used, the calculation will result in a Desired BAT Volume below of 8132 gallons

So:

{(Desired Cb)-(RHT Cb)} x {Desired Total Makeup Volume to FWST} = Desired BAT Volume (BAT Cb)-(RHT Cb)

 $\{(2700)-(1076)\}$ x $\{30000\}$ = Desired BAT Volume (7234)-(1076)

{<u>1624</u>} x {30000} = Desired BAT Volume 6158

.26 x {30000} = Desired BAT Volume or **7,912** gallons +300/-75 gallons

OR between 7,837 and 8212 gallons



INITIAL CONDITIONS:

- The plant was at 100% power when a leak developed on the FWST.
- FWST Level dropped to 440 inches before leak was isolated.
- Enclosure 4.4, "FWST Makeup Using the RHT," of OP/1/A/6200/014, "Refueling Water System" is in progress and completed through Step 3.9.
- LCO 3.5.4, Refueling Water Storage Tank (RWST), was entered 10 minutes ago.
- Chemistry has provided the following information:
 - BAT Boron Conc. = 7234 ppm
 - RHT Boron Conc.= 1076 ppm
 - FWST Make up Boron Concentration: <u>Use COLR</u>
 <u>Minimum</u>

INITIATING CUE:

Determine the amount of Boric Acid needed to raise the FWST level to 480" using the RHT in accordance with Step 3.10 of Enclosure 4.4 of OP/1/A/6200/014, "Refueling Water System."

OP/**1**/A/6200/014 Page 1 of 9

FWST Makeup Using RHT

1. Limits and Precautions

- / 1.1 Maximum FWST Tech Spec temperature limit is 100°F.
- $\sqrt{1.2}$ Minimum FWST Tech Spec temperature limit is 70°F.
- $\sqrt{1.3}$ All electrically operated engineered safeguard valves must be operated electrically after any manual operation.
- $\sqrt{1.4}$ Maximum FWST level is 483 inches unless FWST overflow is required. (Overflows to SFP at 484 inches)
- $\sqrt{1.5}$ NC System sampling during makeup to the FWST is prohibited.

2. Initial Conditions

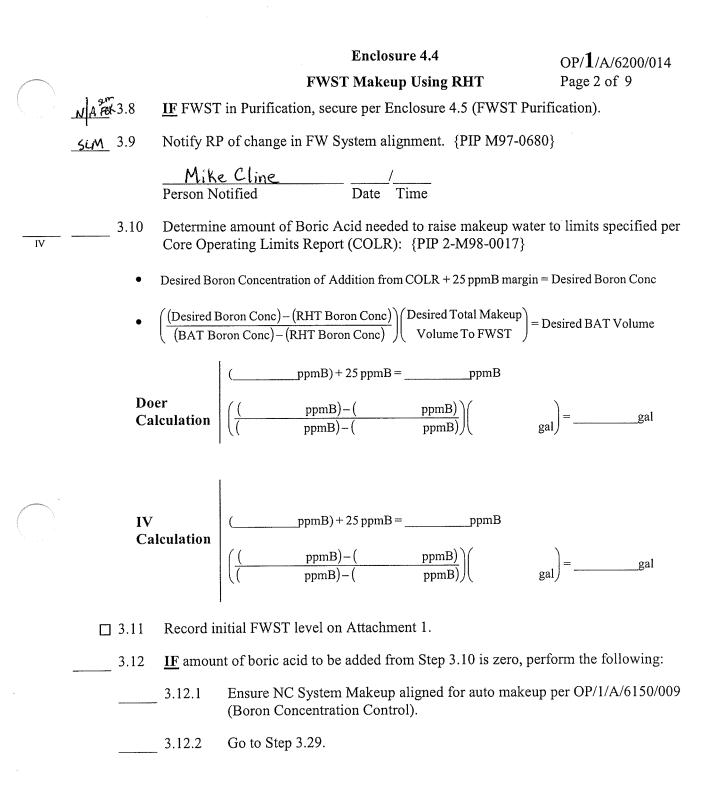
- <u>5LM</u> 2.1 Boron concentration control systems available per OP/1/A/6150/009 (Boron Concentration Control).
- 5LM 2.2 NB System aligned per OP/0/A/6200/003 (Boron Recycle System).
- 5LM 2.3 NI check valve test header alignment to FWST secured.

3. Procedure

- $\sqrt{3.1}$ Evaluate all outstanding R&Rs that may impact performance of this procedure.
 - 3.2 IF Emergency Boration Flow is needed, secure makeup to FWST.
- <u>SLM</u> 3.3 Notify Chemistry to sample RHT.

| Kevin Hodges | | / |
|-----------------|------|------|
| Person Notified | Date | Time |

- NAR 3.4 IF RHT is unacceptable for use, exit this enclosure.
- SEM 3.5 Ensure that a pre-job briefing has been performed that includes discussion of reactivity management concerns with this procedure.
- NATE 3.6 IF FWST in Recirculation per Enclosure 4.1 (FWST Recirculation Using 1A (1B) FWST Recirc Pump), stop the following:
 - 1A FWST Recirc Pump
 - 1B FWST Recirc Pump
- <u>NARE 3.7</u> <u>IF</u> FWST in Recirculation with #1 FWST Pump, secure per Enclosure 4.6 (FWST Recirculation Using Unit 1 FWST Pump).



| | | | Enclosure 4.4 | OP/ 1 /A/6200/014 | |
|------|--|---------------|--|----------------------------|--|
| | | | FWST Makeup Using RHT | Page 3 of 9 | |
| 3.13 | Add amo | ount of Boric | Acid calculated in Step 3.10 to FWST | ' from Blender as follows: | |
| | 3.13.1 | Ensure clos | sed one of the following: | | |
| | | • 1NI-96 | B (NI Chk Test Hdr C/I Outside) | | |
| | | OR | | | |
| | | • 1NI-99 | (Unit 1 NI Check Valve Test Hdr To | FWST Isol) | |
| | 3.13.2 | Ensure loc | ked closed, either: | | |
| | | _ 3.13.2.1 | 1NS-70 (1A & 1B NS HX Outlet To | FWST Throttle) | |
| | | | OR | | |
| | | 3.13.2.2 | Both of the following: | | |
| | | CV | • 1NS-8 (1B NS HX Outlet To FV | VST Isol) | |
| | | <u></u> | • 1NS-25 (1A NS HX Outlet To F | WST Isol) | |
| C |] 3.13.3 | Ensure clo | sed 1NB-5 (Unit 1 Boric Acid Blender 6, KK-51, S End U1 VCT Hallway) | To NB System Isol). | |
| | 3.13.4 | Open: | | | |
| | . <u></u> | | 72 (Unit 1 Boric Acid Blender To NB 74 (Unit 1 Boric Acid Blender To FW | | |
| | 3.13.5 Select "MANUAL" on "NC Sys M/U Controller". | | | | |
| | 3.13.6 | Ensure in | "STOP": | | |
| | | | M/U Water Pump M/U Water Pump | | |
| | _ 3.13.7 | IF both B | A Trans Pumps off, ensure in "AUTO" | one of the following: | |
| | | • 1A BA | Trans Pump | | |
| | | OR | | | |
| | | • 1B BA | Trans Pump | | |
| | | | | | |

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| Enclosure 4 | | Enclosure 4.4 | .4 OP/ 1 /A/6200/0 | | | |
|-------------|---|---|---------------------------|-----------------|----------------------------|--|
| | | FWST | Makeup Using R | HT | Page 4 of 9 | |
| | 3.13.8 | <u>IF</u> VCT is set up for following: | automatic makeup | , record curren | t Setpoint(s) (SP) for the | |
| | | • "Rx M/U Water I | Flow Control": | gpm | | |
| | | • "BA Flow Contro | ol": gi | om | | |
| | 3.13.9 | Place "Rx M/U Wate | r Flow Control" in | manual and c | lose. | |
| NOTE: | | Total Makeup Flow and Boric Acid Flow Counters must be reset for NC Makeup System to operate. | | | | |
| 3.14 | Ensure th | e following reset to ze | ro: | | | |
| | | Make Up Flow Count Acid Flow Counter | er | | | |
| 3.15 | Set Total | Set Total Makeup Flow Counter to desired value. | | | | |
| 3.16 | Set Boric | Set Boric Acid Flow Counter to desired value. | | | | |
| NOTE: | Valve leakage may occur causing input to the VCT. | | | | | |
| □ 3.17 | Monitor the following parameters: | | | | | |
| | • SM F | ressure | | | | |
| | | or Power | | | | |
| | TavgRod 1 | Motion | | | | |
| 3.18 | IF plant | parameters indicate oth | her than expected i | esponse, notif | y CRS. | |
| NOTE: | | el should be maintain (OAC Hi level alarm) | ed less than 481 in | ches unless FV | VST overflow is | |
| 3.19 | Momenta | arily select "START" of | on "NC System Ma | ake Up". | | |
| □ 3.20 | Check lit | "NC System Makeup | " red light. | | | |
| 3.21 | <u>IF</u> in "A | IF in "AUTO", ensure BA Trans Pump starts. | | | | |
| 3.22 | Place "B | Place "BA Flow Control" in manual and adjust to desired flow rate. | | | | |
| | | | | | | |

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| | Enclosure 4.4 | | Enclosure 4.4 | OP/ 1 /A/6200/014 | |
|------|---------------|----------------|---|--------------------------|--|
| | | | FWST Makeup Using RHT | Page 5 of 9 | |
| 3.23 | HOLD u | ntil desired a | amount of boric acid added then perform the | ne following: | |
| | 3.23.1 | IF in "AUT | ΓO", ensure off: | | |
| | | - | Trans Pump Trans Pump | | |
| | 3.23.2 | Flush flow | path for 5 minutes as follows: | | |
| | | 3.23.2.1 | Select "OFF" on "NC Sys M/U Controlle | er". | |
| | | 3.23.2.2 | Close "BA Flow Control". | | |
| | | 3.23.2.3 | Open "Rx M/U Water Flow Control". | | |
| | | 3.23.2.4 | Select "STOP" on the following: | | |
| | | | 1A BA Trans Pump1B BA Trans Pump | | |
| | | 3.23.2.5 | Select "AUTO" on one of the following: | | |
| | | | • 1A Rx M/U Water Pump | | |
| | | | OR | | |
| | | | • 1B Rx M/U Water Pump | | |
| | | 3.23.2.6 | Select "MANUAL" on "NC System M/L | J Controller". | |
| | | 3.23.2.7 | Momentarily select "START" on "NC Sy | ystem Make Up". | |
| | | 3.23.2.8 | Check lit "NC System Makeup" red light | | |
| | | 3.23.2.9 | Ensure Rx M/U Water Pump starts. | | |
| | | 3.23.2.10 | HOLD until flush complete then select " Makeup". | OFF" on "NC System | |
| 3.24 | Place in a | auto: | | | |
| | • "BA | Flow Contro | Ι" | | |

- "Rx M/U Water Flow control"
- 3.25 Close:

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- 1NV-172 (Unit 1 Boric Acid Blender To NB & FW Isol)
- 1NV-174 (Unit 1 Boric Acid Blender To FWST Isol)

FWST Makeup Using RHT

- 3.26 **IF** BAT to be in recirc, perform the following:
 - 3.26.1 Select "START" on one of the following:
 - IA BA Trans Pump

OR

- 1B BA Trans Pump
- □ 3.26.2 Go to Step 3.28.
- 3.27 Select "AUTO" on one of the following:
 - IA BA Trans Pump

OR

- 1B BA Trans Pump
- 3.28 Return the following controllers to values recorded in Step 3.13.8:
 - BA Flow Control (+/- 0.2 gpm)
 - Rx M/U Water Flow Control (+/- 0.2 gpm)
- 3.29 Select "AUTO" on "NC Sys M/U Controller".
 - 3.30 Momentarily select "START" on "NC System Make Up".
 - □ 3.31 Check lit "NC System Makeup" red light.

3.32 Open:

- 1FW-22 (NB To Unit 1 FW Pump Disch Hdr Isol)
- 1FW-24 (Unit 1 FW Pump Disch To FWST Isol)
- □ 3.33 Check closed 1FW-2 (Unit 1 FWST To Refueling Cavity Fill & Drn).

OP/**1**/A/6200/014 Page 7 of 9

FWST Makeup Using RHT

 Person Notified
 /

 Date
 Time

 3.34.1
 Operate the following as required:

 □
 1NB-126 (NB Evap Feed Pumps RHT Contents Transfer Isol)

 □
 1NB-127 (NB Evap Feed Pumps Disch Isol To U1 & U2 FWST)

 □
 3.34.2

 Operate both Recycle Evaporator Feed Pumps to complete makeup from RHT.

Notify Radwaste Chemistry to perform the following:

- 3.35 **HOLD** until FWST is at desired level.
- 3.36 Notify Radwaste Chemistry to operate Recycle Evaporator Feed Pumps as desired.

Person Notified / Date Time

3.37 Close:

3.34

- 1FW-22 (NB To Unit 1 FW Pump Disch Hdr Isol)
- 1FW-24 (Unit 1 FW Pump Disch To FWST Isol)
- 3.38 Notify Radwaste Chemistry to close:

Person Notified

□ 1NB-126 (NB Evap Feed Pumps RHT Contents Transfer Isol)

Date Time

- □ 1NB-127 (NB Evap Feed Pumps Disch Isol To U1 & U2 FWST)
- □ 3.39 Record final FWST level on Attachment 1.
- □ 3.40 Record in Auto Log final blender contents, either:
 - □ Rx Makeup Water

OR

□ Blend

OR

□ Boric Acid

OP/**1**/A/6200/014 Page 8 of 9

FWST Makeup Using RHT

- □ 3.41 Place routing stamp in remarks section of cover sheet, check (✓) "Engineering" and fill in "Attachment 1 only".
- ____ 3.42 <u>IF</u> desired to align for automatic NC System Makeup, align per OP/1/A/6150/009 (Boron Concentration Control).
 - 3.43 **IF** FWST Recirc Pump stopped in Step 3.6, start one of the following:
 - 1A FWST Recirc Pump

OR

- 1B FWST Recirc Pump
- _____ 3.44 <u>IF</u> FWST Recirculation with #1 FWST Pump is desired, place FWST in Recirculation per Enclosure 4.6 (FWST Recirculation Using Unit 1 FWST Pump).
- 3.45 <u>**IF**</u> FWST Purification is desired, place FWST in Purification per Enclosure 4.5 (FWST Purification).

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FWST Makeup Using RHT

OP/**1**/A/6200/014 Page 9 of 9

Attachment 1

FWST Makeup Data

| Initial FWST Level | inches | Date | Time |
|--------------------|--------|------|------|
| | | | |
| Final FWST Level | inches | Date | Time |
| Data Collected By | | | |

End of Enclosure

McGuire 1 Cycle 21 Core Operating Limits Report

2.11 RCS Pressure, Temperature and Flow Limits for DNB (TS 3.4.1)

2.11.1 The RCS pressure, temperature and flow limits for DNB are shown in Table 4.

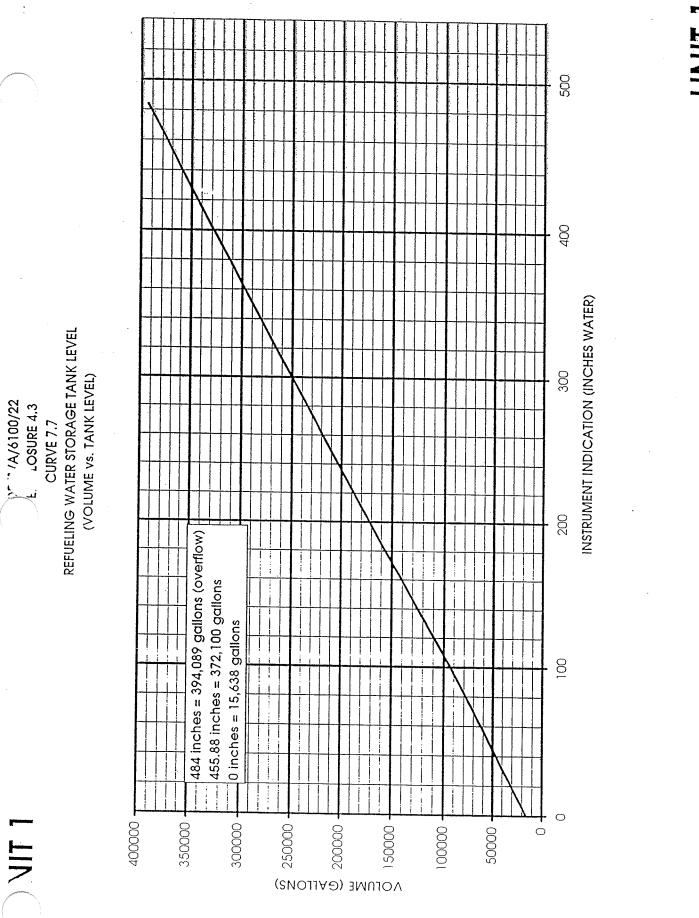
2.12 Accumulators (TS 3.5.1)

2.12.1 Boron concentration limits during MODES 1 and 2, and MODE 3 with RCS pressure >1000 psi:

| | Parameter | Limit | |
|------|--|--------------------|---|
| | Accumulator minimum boron concentration. | 2,475 ppm | • |
| | Accumulator maximum boron concentration. | 2 , 875 ppm | |
| 2.13 | Refueling Water Storage Tank - RWST (TS 3.5.4) | | |

2.13.1 Boron concentration limits during MODES 1, 2, 3, and 4:

| Parameter | Limit |
|-----------------------------------|-----------|
| RWST minimum boron concentration. | 2,675 ppm |
| RWST maximum boron concentration. | 2,875 ppm |



This data is also available on the OAC.

UNIT

JPM A1b SRO

| Appendix C | Page 2 of 10 | | Form ES-C-1 | |
|------------------------|--|----------------|---|--|
| | Job Performance Me | t | | |
| | | | | |
| Facility: | McGuire | Task No.: | 217MFW002 | |
| Task Title: | Determine Boric Acid Addition to FWST | JPM No.: | <u>2010 Admin - JPM A1b</u> <u>SRO</u> | |
| K/A Reference: | GK/A 2.1.25 (3.9/4.2) | | | |
| Examinee: | | NRC Examine | . | |
| Facility Evaluator: | | Date: | | |
| Method of testing: | | | | |
| Simulated Performance: | | Actual Perform | ance: X | |
| Classr | oom X Simulator | Plant | | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

Initial Conditions: The plant was at 100% power when a leak developed on the FWST. • FWST Level dropped to 440 inches before leak was isolated. • Enclosure 4.4, "FWST Makeup Using the RHT," of OP/1/A/6200/014, . "Refueling Water System" is in progress and completed through Step 3.9. LCO 3.5.4, Refueling Water Storage Tank (RWST), was entered 10 minutes ago. Chemistry has provided the following information: BAT Boron Conc. = 7234 ppm RHT Boron Conc.= 1076 ppm FWST Make up Boron Concentration: Use COLR Minimum The BOP has just completed the Doer Calculation of Step 3.10 of Enclosure 4.4, "FWST Makeup Using the RHT," and has asked you to perform an Independent Verification on the calculation.

> r Maria III. Maria

| Appendix C | Page 3 of 10 | Form ES-C- | | | |
|---------------------|---|----------------------|--|--|--|
| | Job Performance Measure Worksheet | | | | |
| | | | | | |
| Fask Standard: | The operator will calculate the amount of Boric Acid that must be added from the BAT to refill the FWST is 7,912 gallons +300/-75 gallons, determine that the BOP made two errors in the original calculation, and identify that Technical Specification ACTION C is now applicable. | | | | |
| Required Materials: | Calculator | | | | |
| | Reference Cart with all identified General References. | | | | |
| General References: | OP/1/A/6200/014, Refueling Water System | | | | |
| | McGuire Core Operating Limits Report (Cycle 21) | | | | |
| | McGuire U-1 Data Book | | | | |
| | McGuire Technical Specifications | | | | |
| | McGuire Selected Licensee Commitment Manual | | | | |
| | OMP 8-2, Component Verification Techniques | | | | |
| Handouts: | Enclosure 4.4 of OP/1/A/6200/014, Refueling Wat for place-keeping and the Doer Calculation of Ste | | | | |
| | Initial Conditions 2.1 -2.3 are initialed. | | | | |
| | Procedure Step 3.1 – Box checked. | | | | |
| | Procedure Step 3.2 – Left blank (Conditional s | step). | | | |
| | Procedure Step 3.3 – initialed, Person Notified present. | I: CHEMIST, date/tim | | | |
| | Procedure Step 3.4 – NA, initialed. | | | | |
| | • Procedure Step 3.5 – initialed. | | | | |
| | Procedure Step 3.6 – NA, initialed. | | | | |
| | • Procedure Step 3.7 – NA, initialed. | | | | |
| | Procedure Step 3.8 – NA, initialed. | | | | |
| | Procedure Step 3.9 – initialed, Person Notified date/time: present. | I: R.P. TECH, | | | |
| | Procedure Step 3.10 – initialed. | | | | |
| | Doer Calculation: | | | | |
| | (2875 ppmB + 25 ppmB = 2900 ppmB | | | | |
| | { <u>(2900 ppmB) – (1076 ppmB)</u> } {15,000} = 4443 g (7234 ppmB) – (1076 ppmB) | jal | | | |
| | McGuire 1 Cycle 21 Core Operating Limits Report | t (Page 26 of 32) | | | |
| | McGuire Technical Specifications | | | | |
| | OP/1/A/6100/22, Enclosure 4.3, Curve 7.7, Refue | ling Water Storage | | | |

| Appendix C | Page 4 of 10 | Form ES-C-1 | | |
|---------------------|---|-------------|--|--|
| | Job Performance Measure Worksheet | | | |
| Initiating Cue: | Perform the Independent Verification (IV) of the calculation in Step 3.10 of Enclosure 4.4 to confirm the amount of Boric Acid that must be added from the Boric Acid Tank (BAT), in order to raise the FWST Level to 480" using the RHT. | | | |
| | AFTER the calculations have been completed and verified in the FWST make up procedure, an 80 gpm Makeup is started to the FWST, and continues for 1 hour. | | | |
| | At the end of this 1 hour period: | | | |
| | What is the status of compliance with LCO 3.5.4? | | | |
| | FWST Temperature = 85 Deg | opm | | |
| Time Critical Task: | NO | | | |

Validation Time: 15 minutes

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue (Last Page of this JPM), and Handout all four (4) identified Handout documents, marked up as described.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| *1 | (Step 3.10) Determine the amount of Boric Acid needed to raise makeup water to the limits specified in the Core Operating Limits Report (COLR). | The operator refers to the COLR, Section 2.13.1 on Page 26 of 32 and determines that the minimum boron concentration to be used in the calculation is 2675 ppm, and <u>NOT 2875 ppm used</u> by BOP (1 st Error). The operator records <u>2675</u> ppm in the first line (Desired Boron Concentration of Addition from COLR) of the IV calculation in Step 3.10 | | |
| *2 | (1 st Bullet) Desired Boron Concentration of Addition from COLR + 25 ppmB margin = Desired Boron Concentration | of Enclosure 4.4. The operator adds an additional 25 ppm and determines Desired Boron Concentration to be 2700 ppm. The operator records <u>2700</u> ppm in the 2 nd line (Desired Boron Conc) of the IV calculation in Step 3.10 of Enclosure 4.4. | | |
| *3 | (2 nd Bullet) { <u>(Desired Cb) - (RHT Cb)</u> } (BAT Cb) - (RHT Cb) x {Desired Total Makeup Volume to FWST} = Desired BAT Volume | The operator identifies Desired Cb = 2700 from previous Step and records. The operator recognizes that RHT Cb = 1076 ppm and records Initial Conditions). | | |

Appendix C

Page 6 of 10 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|----------------|----------|--|-----|-----------------------------------|
| *3 (CONT'D) | | The operator recognizes that BAT Cb = <u>7234</u> ppm and records (Initial Conditions). | | |
| | | The operator addresses OP/1/A/6100/22, Enclosure 4.3, Curve 7.7, and determines from graph that total makeup volume is 30,000 by comparing 480" volume of 390,000 gallons to the 440" volume of 360,000 gallons. | | |
| | | The operator records <u>30,000 (+1300[#])</u> gallons; and <u>NOT 15,000 gallons</u> <u>used by the BOP (2nd <u>Error).</u></u> | | |
| | | The operator records <u>30,000 (+1300[#])</u> gallons in the IV Calculation. The operator calculates the Desired BAT Volume to be added to be <u>7,912</u> gallons +200/ 75 gallons | | |
| | | +300/-75 gallons. The operator records 7,912 gallons +300/-75 gallons as the Desired BAT Volume in the IV Calculation. | | |

Page 7 of 10 PERFORMANCE INFORMATION

Form ES-C-1

| | | | | |
|---------|---|--|-----|-----------------------------------|
| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
| *4 | (Technical Specification LCO 3.5.4) The RWST shall be OPERABLE. | The operator observes TS LCO 3.5.4 and determines that ACTION B was entered at the start of the JPM action was necessary within 1 hour to restore volume. | | |
| | | The operator determines that the FWST Volume TS Limit is 372,100 gallons. | | |
| | | The operator determines that 12,100 gallons must be added to the FWST to comply with this ACTION Statement, and that in one hour 4800 gallons will be added. | | |
| | | The operator identifies that ACTION C is now applicable. | | |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

| Appen | dix | С |
|-------|-----|---|
|-------|-----|---|

Page 8 of 10 VERIFICATION OF COMPLETION

Form ES-C-1

| Job Performance Measure No.: | 2010 Admin - JPM A1b SRO |
|------------------------------|--------------------------|
|------------------------------|--------------------------|

Examinee's Name:

Date Performed:

Facility Evaluator:

Number of Attempts:

Time to Complete:

Question Documentation:

Result:

SAT UNSAT

Examiner's Signature: Date: Page 9 of 10 VERIFICATION OF COMPLETION

KEY:

Desired Boron Concentration from COLR + 25 ppmB = Desired Boron Concentration

2675 ppm (From COLR) + 25 ppmB = 2700 ppm

{(Desired Cb) - (RHT Cb)} x {Desired Total Makeup Volume to FWST} = Desired BAT Volume (BAT Cb) - (RHT Cb)

Given:

RHT Cb = **1076** ppm BAT Cb = **7234** ppm

Desired Total Makeup Volume to FWST = Overflow volume – Present volume (From Enclosure 4.3, Curve 7.7 of Unit 1 Core Data Book:) 390,000 gallons – 360,000 gallons (440") = **30,000** gallons[#]

#: If the operator uses develops a "gallons/inch" volume from the information block on Curve 7.7, the operator will determine the makeup volume to be 31,277 gallons.

Volume at 484 inches = 394,089 gallons Volume at 0 inches = 15,638 gallons

(394,089 gallons - 15,638 gallons)/484 inches = 781.92 gallons/inch

OR

Volume at 455.88 inches = 372,100 gallons Volume at 0 inches = 15,638 gallons

(372,100 gallons - 15, 638 gallons)/455.88 inches = 781.92 gallons/inch

Therefore, 781.92 gallons/inch x 40 inches = 31,276.80 gallons (This may be used as the makeup volume instead of 30,000 gallons).

If this volume is used, the calculation will result in a Desired BAT Volume below of 8132 gallons

So:

{(Desired Cb)-(RHT Cb)} x {Desired Total Makeup Volume to FWST} = Desired BAT Volume (BAT Cb)-(RHT Cb)

 $\{(2700)-(1076)\}$ x $\{30000\}$ = Desired BAT Volume (7234)-(1076)

{<u>1624</u>} x {30000} = Desired BAT Volume 6158

.26 x {30000} = Desired BAT Volume or **7,912** gallons +300/-75 gallons

OR between 7,837 and 8212 gallons



INITIAL CONDITIONS: The plant was at 100% power when a leak developed on the FWST. FWST Level dropped to 440 inches before leak was isolated. Enclosure 4.4, "FWST Makeup Using the RHT," of OP/1/A/6200/014, "Refueling Water System" is in progress and completed through Step 3.9. LCO 3.5.4, Refueling Water Storage Tank (RWST), was entered 10 minutes ago. Chemistry has provided the following information: BAT Boron Conc. = 7234 ppm RHT Boron Conc.= 1076 ppm FWST Make up Boron Concentration: Use COLR Minimum The BOP has just completed the Doer Calculation of Step 3.10 of Enclosure 4.4, "FWST Makeup Using the RHT," and has asked you to perform an Independent Verification on the calculation. Perform the Independent Verification (IV) of the calculation in Step INITIATING CUE:

3.10 of Enclosure 4.4 to confirm the amount of Boric Acid that must be added from the Boric Acid Tank (BAT), in order to raise the FWST Level to 480" using the RHT.

AFTER the calculations have been completed and verified in the FWST make up procedure, an **80 gpm** Makeup is started to the FWST, and continues for **1 hour**.

At the end of this 1 hour period: What is the status of compliance with LCO 3.5.4?

· 4

FWST Temperature = 85 Deg FWST [B] = 2775 ppm

Enclosure 4.4

FWST Makeup Using RHT

1. Limits and Precautions

- 1.1 Maximum FWST Tech Spec temperature limit is 100°F.
- \checkmark 1.2 Minimum FWST Tech Spec temperature limit is 70°F.
- $\sqrt{1.3}$ All electrically operated engineered safeguard valves must be operated electrically after any manual operation.
- $\sqrt{1.4}$ Maximum FWST level is 483 inches unless FWST overflow is required. (Overflows to SFP at 484 inches)
- $\sqrt{1.5}$ NC System sampling during makeup to the FWST is prohibited.

2. Initial Conditions

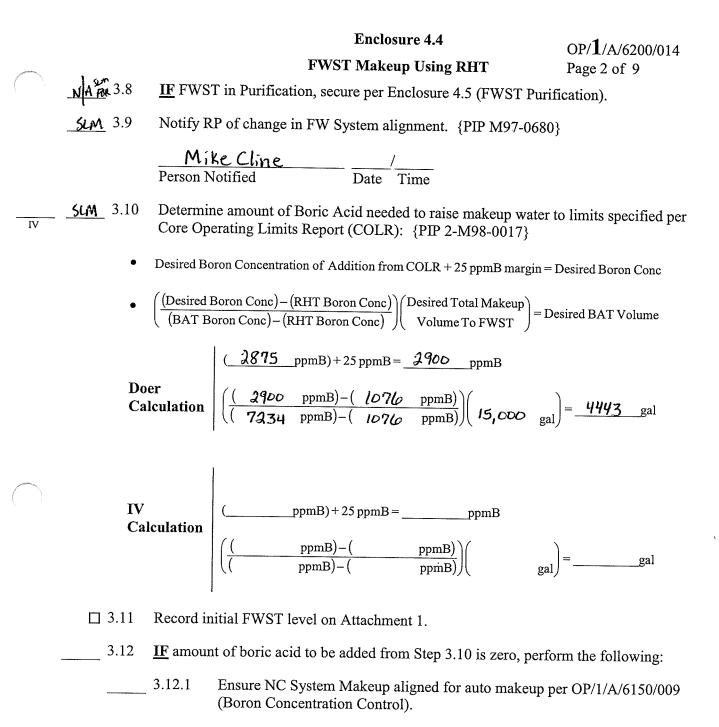
- <u>SLM</u> 2.1 Boron concentration control systems available per OP/1/A/6150/009 (Boron Concentration Control).
- <u>SLM</u> 2.2 NB System aligned per OP/0/A/6200/003 (Boron Recycle System).
- <u>SLM</u> 2.3 NI check valve test header alignment to FWST secured.

3. Procedure

- \checkmark 3.1 Evaluate all outstanding R&Rs that may impact performance of this procedure.
- 3.2 **IF** Emergency Boration Flow is needed, secure makeup to FWST.
- **SLM** 3.3 Notify Chemistry to sample RHT.

<u>Kevin Hodges</u> / Person Notified Date Time

- NATA 3.4 IF RHT is unacceptable for use, exit this enclosure.
- $\frac{5LM}{SRO}$ 3.5 Ensure that a pre-job briefing has been performed that includes discussion of reactivity management concerns with this procedure.
- **IF** FWST in Recirculation per Enclosure 4.1 (FWST Recirculation Using 1A (1B) FWST Recirc Pump), stop the following:
 - 1A FWST Recirc Pump
 - 1B FWST Recirc Pump
- NATE 3.7 IF FWST in Recirculation with #1 FWST Pump, secure per Enclosure 4.6 (FWST Recirculation Using Unit 1 FWST Pump).



_____ 3.12.2 Go to Step 3.29.

| | Enclosure 4.4 | OP/ 1 /A/6200/014 |
|---------------|---|---|
| | FWST Makeup Using RHT | Page 3 of 9 |
| ount of Boric | c Acid calculated in Step 3.10 to FWST | from Blender as follows: |
| Ensure clo | osed one of the following: | |
| • 1NI-96 | 6B (NI Chk Test Hdr C/I Outside) | |
| OR | | |
| • 1NI-99 | O (Unit 1 NI Check Valve Test Hdr To | FWST Isol) |
| Ensure loc | ked closed, either: | |
| _ 3.13.2.1 | 1NS-70 (1A & 1B NS HX Outlet To | FWST Throttle) |
| | OR | |
| 3.13.2.2 | Both of the following: | |
| | • 1NS-8 (1B NS HX Outlet To FW | /ST Isol) |
| <u> </u> | • 1NS-25 (1A NS HX Outlet To F | WST Isol) |
| | | To NB System Isol). |
| Open: | | |
| | | |
| Select "MA | ANUAL" on "NC Sys M/U Controller". | |
| Ensure in ' | 'STOP": | |
| | - | |
| IF both BA | A Trans Pumps off, ensure in "AUTO" | one of the following: |
| • 1A BA | Trans Pump | |
| OR | | |
| • 1B BA | Trans Pump | |
| | Ensure clo OR OR Ensure loc 3.13.2.1 3.13.2.2 CV Ensure clo (AB 733'+ Open: 1NV-1 Select "MA Ensure in ' Ensure in ' 1A Rx 1B Rx IF both BA OR | FWST Makeup Using RHT out of Boric Acid calculated in Step 3.10 to FWST Insure closed one of the following: - 1NI-96B (NI Chk Test Hdr C/I Outside) OR 0R - 1NI-999 (Unit 1 NI Check Valve Test Hdr To 1) Ensure locked closed, either: 3.13.2.1 3.13.2.1 1NS-70 (1A & 1B NS HX Outlet TO OR 3.13.2.2 Both of the following: CV - 0R 1NS-8 (1B NS HX Outlet To FW CV - 1NS-25 (1A NS HX Outlet To FW CV - Ensure closed 1NB-5 (Unit 1 Boric Acid Blender for NB W Open: - - 1NV-172 (Unit 1 Boric Acid Blender To FW Select "MANUAL" on "NC Sys M/U Controller" Ensure in "STOP": - 1A Rx M/U Water Pump IB Rx M/U Water Pump IF both BA Trans Pumps off, ensure in "AUTO" - 1A BA Trans Pump |

| | | | Enclo | sure 4.4 | | OP/ 1 /A/6200/014 |
|--------|---|------------------------------|------------------------------|--------------------|--------------|----------------------------|
| | | | FWST Make | up Using RHT | | Page 4 of 9 |
| | 3.13.8 | <u>IF</u> VCT is following: | set up for autom | atic makeup, ree | cord curren | t Setpoint(s) (SP) for the |
| | | • "Rx M/ | 'U Water Flow C | Control": | gpm | |
| | | • "BA Fle | ow Control": | gpm | | |
| | 3.13.9 | Place "Rx M | M/U Water Flow | v Control" in ma | nual and cl | ose. |
| NOTE: | Total Mal System to | keup Flow and operate. | nd Boric Acid F | low Counters m | ust be reset | for NC Makeup |
| 3.14 | Ensure th | he following | reset to zero: | | | |
| | | l Make Up Flo Acid Flow C | | | | |
| 3.15 | Set Total | Makeup Flo | w Counter to de | sired value. | | |
| 3.16 | Set Boric | c Acid Flow C | Counter to desire | ed value. | | |
| NOTE: | Valve leal | kage may occ | cur causing input | t to the VCT. | | |
| □ 3.17 | Monitor | the following | parameters: | | | |
| | • SM P | ressure | | | | |
| | | tor Power | | | | |
| | Tavg Rod M | Motion | | | | |
| 3.18 | | | dicate other than | a expected respo | nse, notify | CRS. |
| NOTE: | FWST lev required. (| el should be OAC Hi leve | maintained less el alarm) | than 481 inches | unless FW | ST overflow is |
| 3.19 | Momenta | rily select "S' | TART" on "NC | System Make U | p". | |
| □ 3.20 | Check lit | "NC System | Makeup" red lig | ;ht. | | |
| 3.21 | IF in "AU | JTO", ensure | BA Trans Pump | o starts. | | |
| 3.22 | Place "BA | A Flow Contro | ol" in manual ar | id adjust to desir | red flow rat | е. |
| | | | | | | |

FWST Makeup Using RHT

| 3.23 | HOLD until desired | amount of boric acid added then perform the following: | | |
|----------|--------------------|--|--|--|
| | | IF in "AUTO", ensure off: | | |
| | | A Trans Pump A Trans Pump | | |
| | 3.23.2 Flush flow | path for 5 minutes as follows: | | |
| | 3.23.2.1 | Select "OFF" on "NC Sys M/U Controller". | | |
| | 3.23.2.2 | Close "BA Flow Control". | | |
| | 3.23.2.3 | Open "Rx M/U Water Flow Control". | | |
| | 3.23.2.4 | Select "STOP" on the following: | | |
| | | 1A BA Trans Pump 1B BA Trans Pump | | |
| | 3.23.2.5 | Select "AUTO" on one of the following: | | |
| | | • 1A Rx M/U Water Pump | | |
| | | OR | | |
| | | • 1B Rx M/U Water Pump | | |
| | 3.23.2.6 | Select "MANUAL" on "NC System M/U Controller". | | |
| | 3.23.2.7 | Momentarily select "START" on "NC System Make Up". | | |
| | □ 3.23.2.8 | Check lit "NC System Makeup" red light. | | |
| | 3.23.2.9 | Ensure Rx M/U Water Pump starts. | | |
| | 3.23.2.10 | HOLD until flush complete then select "OFF" on "NC System Makeup". | | |
| 3.24 | Place in auto: | | | |

- "BA Flow Control"
- "Rx M/U Water Flow control"
- 3.25 Close:
 - 1NV-172 (Unit 1 Boric Acid Blender To NB & FW Isol)
- 1NV-174 (Unit 1 Boric Acid Blender To FWST Isol)

FWST Makeup Using RHT

3.26 **IF** BAT to be in recirc, perform the following:

- 3.26.1 Select "START" on one of the following:
 - IA BA Trans Pump

OR

- 1B BA Trans Pump
- □ 3.26.2 Go to Step 3.28.
- 3.27 Select "AUTO" on one of the following:
- 1A BA Trans Pump

OR

- 1B BA Trans Pump
- 3.28 Return the following controllers to values recorded in Step 3.13.8:
- BA Flow Control (+/- 0.2 gpm)
- Rx M/U Water Flow Control (+/- 0.2 gpm)
- 3.29 Select "AUTO" on "NC Sys M/U Controller".
- 3.30 Momentarily select "START" on "NC System Make Up".
- □ 3.31 Check lit "NC System Makeup" red light.

3.32 Open:

- 1FW-22 (NB To Unit 1 FW Pump Disch Hdr Isol)
- 1FW-24 (Unit 1 FW Pump Disch To FWST Isol)
- □ 3.33 Check closed 1FW-2 (Unit 1 FWST To Refueling Cavity Fill & Drn).

FWST Makeup Using RHT

| 3.34 | Notify Radwaste Chemistry to perform the following: | | | |
|--------|--|--|--|--|
| | Person Notified / Date Time | | | |
| | Person Notified Date Time | | | |
| | 3.34.1 Operate the following as required: | | | |
| | 1NB-126 (NB Evap Feed Pumps RHT Contents Transfer Isol) 1NB-127 (NB Evap Feed Pumps Disch Isol To U1 & U2 FWST) | | | |
| | 3.34.2 Operate both Recycle Evaporator Feed Pumps to complete makeup from RHT. | | | |
| 3.35 | HOLD until FWST is at desired level. | | | |
| 3.36- | Notify Radwaste Chemistry to operate Recycle Evaporator Feed Pumps as desired. | | | |
| | / | | | |
| | Person Notified <u>/</u> Date Time | | | |
| 3.37 | Close: | | | |
| | • 1FW-22 (NB To Unit 1 FW Pump Disch Hdr Isol) | | | |
| | • 1FW-24 (Unit 1 FW Pump Disch To FWST Isol) | | | |
| 3.38 | Notify Radwaste Chemistry to close: | | | |
| | Person Notified / Date Time | | | |
| | Person Notified Date Time | | | |
| | 1NB-126 (NB Evap Feed Pumps RHT Contents Transfer Isol) 1NB-127 (NB Evap Feed Pumps Disch Isol To U1 & U2 FWST) | | | |
| □ 3.39 | Record final FWST level on Attachment 1. | | | |
| □ 3.40 | Record in Auto Log final blender contents, either: | | | |
| | □ Rx Makeup Water | | | |
| | OR | | | |
| | □ Blend | | | |
| | OR | | | |
| | □ Boric Acid | | | |
| | | | | |

Unit 1

•

| | Enclosure 4.4 | OP/ 1 /A/6200/014 |
|--------|--|---------------------------|
| | FWST Makeup Using RHT | Page 8 of 9 |
| □ 3.41 | Place routing stamp in remarks section of cover sheet, check (\checkmark) in "Attachment 1 only". |) "Engineering" and fill |
| 3.42 | IF desired to align for automatic NC System Makeup, align per (Boron Concentration Control). | OP/1/A/6150/009 |
| 3.43 | IF FWST Recirc Pump stopped in Step 3.6, start one of the follo | owing: |
| | • 1A FWST Recirc Pump | |
| | OR | |
| · | • 1B FWST Recirc Pump | |
| 3.44 | IF FWST Recirculation with #1 FWST Pump is desired, place F per Enclosure 4.6 (FWST Recirculation Using Unit 1 FWST Pur | WST in Recirculation np). |
| 3.45 | IF FWST Purification is desired, place FWST in Purification per Purification). | Enclosure 4.5 (FWST |
| | | |

Enclosure 4.4

FWST Makeup Using RHT

OP/**1**/A/6200/014 Page 9 of 9

Attachment 1

FWST Makeup Data

| Initial FWST Level | inches | Date | Time |
|--------------------|---------|------|------|
| Final FWST Level | _inches | Date | Time |
| Data Collected By | | | |

End of Enclosure

McGuire 1 Cycle 21 Core Operating Limits Report

2.11 RCS Pressure, Temperature and Flow Limits for DNB (TS 3.4.1)

2.11.1 The RCS pressure, temperature and flow limits for DNB are shown in Table 4.

2.12 Accumulators (TS 3.5.1)

2.12.1 Boron concentration limits during MODES 1 and 2, and MODE 3 with RCS pressure >1000 psi:

| | Parameter | Limit | |
|-------|--|-----------|-------|
| · | Accumulator minimum boron concentration. | 2,475 ppm | · · · |
| | Accumulator maximum boron concentration. | 2,875 ppm | |
| 2.13 | Refueling Water Storage Tank - RWST (TS 3.5.4) | | |

2.13.1 Boron concentration limits during MODES 1, 2, 3, and 4:

| Parameter | Limit |
|-----------------------------------|-----------|
| RWST minimum boron concentration. | 2,675 ppm |
| RWST maximum boron concentration. | 2,875 ppm |

200 40 INSTRUMENT INDICATION (INCHES WATER) Cr '/A/6100/22 L. LOSURE 4.3 CURVE 7.7 REFUELING WATER STORAGE TANK LEVEL (VOLUME vs. TANK LEVEL) 300 200 484 inches = 394,089 gallons (overflow) 0 inches = 15,638 gallons 0000 ! 400000 350000 -0 300000 -VOLUME (GALLONS) 100000 0 , NIT 50000

This data is also available on the OAC.

UNIT 1

JPM A2 RO

2010 Admin - JPM A2 RO

NUREG 1021, Revision 9

| Appendix C | Page 2 | of 12 Form ES-0 |
|-----------------------|--|--|
| | Job Performance Me | asure Worksheet |
| | | |
| Facility: | McGuire | Task No.: |
| Task Title: | Perform a Manual NC Leakage Calculation | JPM No.: <u>2010 Admin - JPM /</u> RO |
| K/A Reference: | GK/A 2.2.12 (3.7) | |
| Examinee: | | NRC Examiner: |
| Facility Evaluator: | | Date: |
| Method of testing: | | |
| Simulated Perform | ance: | Actual Performance: XX |
| Classroom X Simulator | | Plant |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | Unit 1 is at 100% power. |
|---------------------|--|
| | The Unit 1 OAC point M1L4554 is out of service. |
| | PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm. |
| | A manual NC System leakage calculation is in progress in accordance with PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) |
| | Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) has been completed through Step 1.9. |
| Task Standard: | The operator will complete all calculations in accordance with the attached Key, and identify that the Unidentified RCS Leakage Technical Specification has been exceeded. |
| Required Materials: | None. |
| General References: | PT/1/A/4200/040 (Reactor Coolant Leakage Detection) PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) McGuire Unit 1 Technical Specifications |

| Appendix C | Page 3 of 12 | Form ES-C- |
|---------------------|---|-----------------------|
| | Job Performance Measure Worksheet | |
| Handouts: | PT/1/A/4150/001B (Reactor Coolant Leakage Calc follows: | culation) marked up a |
| | Step 7.1 – Initialed | |
| | Steps 8.1 through 8.5 – Initialed. | |
| | Step 12.1 Enclosure 13.2 Checkbox is checked. | |
| | PT/1/A/4150/001B (Reactor Coolant Leakage Calc 13.2 (NC Leakage Determinations Using Manual C up as follows: | , |
| | Step 1.1 – Checkbox is checked/Initialed. | |
| | Step 1.2 – Initialed. | |
| | Step 1.3 – Initialed. | |
| | Determine VCT Purge Status Checkbox is chec | ked. |
| | Secured Checkbox is checked. | |
| | NC System leakage calculation is in progress C | heckbox is checked. |
| | To refrain from sampling Checkbox is check | ed. |
| | Person Notified Mike Smith Today's Date/Time | |
| | Step 1.4 – Initialed. | |
| | NC System leakage calculation is in progress C | heckbox is checked. |
| | To check that NC sample Checkbox is check | ked. |
| | NC System sampling Checkbox is checked. | |
| | Person Notified Melvin Smith Today's Date/Time | e |
| | Step 1.5 – Initialed. | |
| | Step 1.6 – All Checkboxes checked/Initialed. | |
| | Step 1.7 – Initialed. | |
| | Step 1.7.1 – Initialed. | |
| | Step 1.7.2 – Initialed. | |
| | Step 1.8 – Initialed. | |
| | Step 1.9 – Initialed. | |
| | Enclosure 13.3 (NCDT Volume) of PT/1/A/4150/00 Leakage Calculation) | 1B (Reactor Coolan |
| | Enclosure 13.4 (PRT Volume) of PT/1/A/4150/001 Leakage Calculation) | 3 (Reactor Coolant |
| Initiating Cue: | Using Enclosure 13.2 (NC Leakage Determination Calculations), AND the attached Datasheet, compl Leakage Calculation, by performing Steps 1.10 and | ete the NC System |
| | Indicate whether or not a Technical Specification h | as been exceeded. |
| Time Critical Task: | NO | |

2010 Admin - JPM A2 RO

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|----|-----|------|--------|
| γĻ | per | ndix | C |

Page 4 of 12 Job Performance Measure Worksheet

Form ES-C-1

Validation Time: 20 minutes

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue, and associated Datasheet (Last two (2) Pages of this JPM); and Handout PT/1/A/4150/001B procedure body marked up as described, Enclosure 13.2 marked up as described, Enclosure 13.3 and Enclosure 13.4.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 1 | (Enclosure 13.2, Steps 1.10.1 through 13, 22, 26 and 1.11.1) Record raw data. | The operator transposes raw data from the Data Sheet provided. | | |
| 2 | (Enclosure 13.2, Step 1.10.14) Calculate change in NC System Tave: | The operator calculates the change in NC System Tave to be <u>0°F</u> , and records. | | |
| 3 | (Enclosure 13.2, Step 1.10.15) Calculate VCT Leakage Rate: | The operator calculates the VCT Leakage Rate to be <u>1.55 gpm</u> , and records. | | |
| 4 | (Enclosure 13.2, Step 1.10.16) Calculate PZR Leakage Rate: | The operator calculates the PZR Leakage Rate to be 0.02 gpm , and records. | | |
| 5 | (Enclosure 13.2, Step 1.10.17) Calculate Total Leakage: | The operator calculates the Total Leakage to be <u>1.57</u> <u>gpm</u> , and records. | | |

Page 6 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 6 | (Enclosure 13.2, Step 1.10.18) Using Enclosure 13.4 (PRT Volume), record the following: Initial PRT Volume Final PRT Volume | The operator uses Enclosure 13.4 and an initial PRT Level of 76.0 %, and determines that initial PRT Volume is <u>10636.1</u> <u>gal</u> , and records. The operator uses Enclosure 13.4 and interpolates a PRT Volume for 76.1% to be <u>10649.5</u> <u>gal</u> , and records. | | |
| 7 | (Enclosure 13.2, Step 1.10.19) Calculate PRT Leakage Rate: | The operator calculates the PRT Leakage Rate to be <u>.19 gpm</u> , and records. | | |
| 8 | (Enclosure 13.2, Step 1.10. 20) Using Enclosure 13.3 (NCDT Volume), record the following: Initial NCDT Volume Final NCDT Volume | The operator uses Enclosure 13.3 and an initial NCDT Level of <u>30.0%</u> , and determines that initial NCDT Volume is <u>105.9 gal</u> , and records. | | |
| | | The operator uses Enclosure 13.3 and a final NCDT Level of <u>33.0%</u> , and determines that final NCDT Volume is <u>116.2 gal</u> , and records. | | |
| 9 | (Enclosure 13.2, Step 1.10.21) Calculate NCDT Leakage Rate: | The operator calculates the NCDT Leakage Rate to be .14 gpm, and records. | | |
| 10 | (Enclosure 13.2, Step 1.10.23) Calculate Total Background Leakage: | The operator calculates the Total Background Leakage to be <u>0 gpm</u> , and records. | | |

Page 7 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|--|-----|-----------------------------------|
| *11 | (Enclosure 13.2, Step 1.10.24) Calculate Identified Leakage: | The operator calculates the Identified Leakage to be 0.33 (±10%) gpm , and records. | | |
| *12 | (Enclosure 13.2, Step 1.10.25) Calculate Unidentified Leakage: | The operator calculates the Unidentified Leakage to be 1.24 (±10%) gpm , and records. | | |
| *13 | (Enclosure 13.2, Step 1.10.26) Determine Total NC Pump #1 Seal Leakoff: | The operator calculates the Total NC Pumps #1 Seal Leakoff to be <u>12.8 (±10%)</u> <u>gpm</u> , and records. | | |
| *14 | (Enclosure 13.2, Step 1.10.27) Calculate Total Accumulative Leakage: | The operator calculates the Total Accumulative Leakage to be <u>14.37</u> (±10%) gpm, and records. | | |
| 15 | (Enclosure 13.2) Calculated By/ Date/Time: | The operator places their name in the Calculated by BLOCK, and signs. The operator enters the Date and Time. | | |

Appendix C

Page 8 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| | | | _ | |
|-------|---|--|-----|-----------------------------------|
| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
| *16 | Technical Specification LCO 3.4.13: RCS operational LEAKAGE shall be limited to: | The operator returns the completed Enclosure 13.2 and reports that LCO 3.4.13 has been exceeded because there is greater | | |
| | a. No pressure boundary LEAKAGE; | than 1 gpm unidentified LEAKAGE. | | |
| | b. 1 gpm unidentified LEAKAGE; | Examiner NOTE: | | |
| | c. 10 gpm identified LEAKAGE; | See KEY on Page 9 of this JPM. | | |
| | d. 389 gallons per day total primary to secondary LEAKAGE through all steam generators (SGs); and | | | |
| | e. 135 gallons per day primary to secondary LEAKAGE through any one steam generator (SG). | i | | |
| | APPLICABILITY: MODES 1, 2, 3, and 4. | | | |

Terminating Cue: Evaluation on this JPM is complete.

STOP TIME:

| Ap | pend | dix | С |
|-----------|------|-----|----------|
| · • • • • | | | <u> </u> |

Page 9 of 12 VERIFICATION OF COMPLETION

Form ES-C-1

| Job Performance Measure No.: | <u> 2010 Admin - JPI</u> | <u>M A2 RO</u> | |
|------------------------------|--------------------------|----------------|-----|
| Examinee's Name: | • | | |
| Date Performed: | | | |
| Facility Evaluator: | | | |
| Number of Attempts: | | | |
| Time to Complete: | | | |
| Question Documentation: | | | |
| | | | |
| | · · · | | |
| Decult | CAT | | |
| Result: | SAT | UNSAT | |
| Examiner's Signature: | | Da | te: |

Appendix C

Page 10 of 12 VERIFICATION OF COMPLETION

KEY:

Enclosure 13.2, Step 1.10.14 (JPM Step 2): Change in NC System Tave: $584.8^{\circ}F - 584.8^{\circ}F = 0^{\circ}F$

Enclosure 13.2, Step 1.10.15 (JPM Step 3): VCT Leakage Rate: (53.4% – 47.6%) x19.3 gallons/%/72 minutes = 1.55 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.16 (JPM Step 4): PZR Leakage Rate: (54.9% – 54.1%) x 132.5 gallons/% x .01613 /72 minutes = 0.02 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.17 (JPM Step 5): Total Leakage: 1.55 gpm + 0.02 gpm = 1.57 gpm

Enclosure 13.2, Step 1.10.18 (JPM Step 6): PRT Final Volume:

(10770.4-10636.1)/10 = 13.43/.1% PRT Level, 10636.1 + 13.43 = 10649.53 (gal)

Enclosure 13.2, Step 1.10.19 (JPM Step 7): Total PRT Leakage: (10649.5 gallons – 10636.1 gallons)/72 minutes = 0.19 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.21 (JPM Step 9): Total NCDT Leakage: (116.2 gallons – 105.9 gallons)/72 minutes = 0.14 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.23 (JPM Step 10): Total Background Leakage: (0 gpm + 0 gpm) = 0 gpm

Enclosure 13.2, Step 1.10.24 (JPM Step 11): Identified Leakage: (.19 gpm + .14 gpm + 0 gpm) = 0.33 gpm

Enclosure 13.2, Step 1.10.25 (JPM Step 12): Unidentified Leakage: (1.57 gpm - .33 gpm) = 1.24 gpm

Enclosure 13.2, Step 1.10.26 (JPM Step 13): Total NC Pumps #1 Seal Leakoff: (2.8 gpm + 3.6 gpm + 3.1 gpm + 3.3 gpm) = 12.8 gpm

Enclosure 13.2, Step 1.10.27 (JPM Step 14): Total Accumulative Leakage: (.33 gpm + 1.24 gpm + 12.8 gpm) = 14.37 gpm

LCO 3.4.13 (1 gpm unidentified LEAKAGE) has been exceeded.



| Appendix C | Form ES-C-1 |
|---------------------|---|
| | JPM CUE SHEET |
| | |
| INITIAL CONDITIONS: | Unit 1 is at 100% power. |
| | The Unit 1 OAC point M1L4554 is out of service. |
| | PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm. |
| | A manual NC System leakage calculation is in progress in accordance with PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) |
| | Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) has been completed through Step 1.9. |
| | |
| INITIATING CUE: | Using Enclosure 13.2 (NC Leakage Determination Using Manual Calculations), AND the attached Datasheet, complete the NC System Leakage Calculation, by performing Steps 1.10 and 1.11. |
| | Indicate whether or not a Technical Specification has been exceeded. |

Form ES-C-1

JPM CUE SHEET

Data Sheet

| Start Time | 0100 | |
|-------------------------------|--------------------------------|--------------|
| Stop Time | 0212 | |
| | | |
| | Initial | <u>Final</u> |
| VCT Level | 53.4 | 47.6 |
| Pzr Level | 54.9 | 54.1 |
| NC System Tave | 584.8 | 584.8 |
| PRT Level | 76.0 | 76.1 |
| NCDT Level | 30 | 33 |
| | | |
| NC Sample Purge Flow v | alue recorded in Autolog | 0 |
| Any quantified (measured) lea | akage that has been identified | 0 |
| | | |
| NC Pump 1A #1 S | Seal Leakoff Flow | 2.8 |
| | Seal Leakoff Flow | 3.6 |
| NC Pump 1C #1 \$ | Seal Leakoff Flow | 3.1 |
| NC Pump 1D #1 S | Seal Leakoff Flow | 3.3 |
| | | |
| 1EMF71 | 1.2 | |
| 1EMF72 | 1.7 | |
| 1EMF73 | 1.1 | |
| 1EMF74 | 1.9 | |

| Duke Energy |
|--|
| McGuire Nuclear Station |
| Reactor Coolant Leakage Calculation |

Procedure No. PT/1/A/4150/001 B

Revision No. 067

Electronic Reference No. MC0047QI

Continuous Use

PERFORMANCE

**⁴

(ISSUED) - PDF Format

| Revision History (significant issues, limited to one page) | | |
|--|---|--|
| Rev 067 | Changed format of procedure to split out calculation performed by OAC and performed by manual calculation. Combined leakage calculation using the OAC steps with current Enclosure 13.1 and renamed enclosure "NC Leakage Calculation Using OAC". Combined manual leakage calculation steps with Enclosure 13.2 and renamed enclosure "NC Leakage Determination Using Manual Calculation". Changed all references throughout procedure to include these format changes. Encl. 13.5. Added Independent Verification sign offs for calculation of seven day rolling average of Unidentified Leakage. {PIP M-09-1307} Revised current steps for determining if Tier Two or Tier Three Action levels exceeded to reference step numbers associated with determination. Intent is to clarify steps. Reworded steps that state "IF directed" by engineering to "IF advised" by engineering. Definition of "directed" changed with new fatigue rule. Added PIP M-09-1857 as an additional reference to NCP seal leakage basis. Modified steps that begin with "WHEN" to reflect NSD 704 Rev 016 requirements. | |
| Rev 066 | Body of procedure. Added a limit and precaution about manipulation of VA System during leakage calculation has an affect on VCT level. Re-worded Step 12.6.17. The leakage calculation is considered valid after 60 minutes but is preferred to run up to 3 hours. The step as written requires the operator to print calculation after 60 minutes when 1 of 3 conditions met. This is procedure use and adherence issue. Re-worded step to give operator flexibility to print calculation summary between 60 minutes and 3 hours. Re-worded Step 12.6.35. If operator performs section 12.6.16 to abort leakage calculation early, enclosure 13.1 is not performed. 12.6.35 directs operator to perform Encl. 13.5, however, this enclosure requires data from enclosure 13.1. Re-worded step to stipulate if unit at 100% RTP AND Encl. 13.1 completed, then perform Encl. 13.5. Procedure use and adherence issue. | |
| Rev 065 | Added step to make operator aware that if leakage calc ran for greater than 30 minutes but less than 60 minutes, the data can still be valid if it meets certain conditions. Added step to record status of VCT purge at beginning of procedure. Added steps to take NV-137A "hard" to VCT and back to "AUTO" prior to starting leakage calculation. Encl. 13.5. Reworded section if any Tier One, Two, or Three Action level is exceeded to make it easier to understand. | |

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Reactor Coolant Leakage Calculation

1. Purpose

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/ To determine NC System Leakage using the Operator Aid Computer (OAC) or manual calculations to ensure Tech Spec requirements met.

2. References

- ✓ 2.1 Tech Spec TS SR 3.4.13.1, 3.4.13.2, TS 3.4.15
- $\sqrt{2.2}$ SLC 16.9.7 Standby Shutdown System
- ./2.3 MCS-1274.00-00-0016 (License Renewal Basis Spec), Section 4.29
- ✓2.4 UFSAR Chapter 18 (Aging Management Program and Activities), Table 18-1, Reactor Coolant Operational Leakage Monitoring Program
- ✓ 2.5 SLC 16.7.6 Radiation Monitoring for Plant Operation
- √2.6 WCAP-16423-NP (Methodology for calculating Unidentified NC System leakage)
- √2.7 WCAP-16465-NP (Action levels and response guidelines for increasing Unidentifed NC System leakage less than Tech Spec limits)
- √2.8 MCC-1201.01-00-0053 (MNS Unit 1 & 2 NC Pump Response to Loss of Seal Cooling)

3. Time Required

 \checkmark 3.1 One operator for three hours every 72 hours.

4. Prerequisite Test

/None

5. Test Equipment

/None

6. Limits and Precautions

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- ✓ 6.1 NC System Tave, Reactor Power, Containment Temperature, and SM Pressure should remain constant during calculation.
- $\sqrt{6.2}$ Positioning values during calculation which could adversely affect results will invalidate the calculation.
- $\sqrt{6.3}$ Performing Leakage Calculation between 3 am and 8 am on Wednesdays may cause calculation to fail due to OAC weekly backup routine.
- ./6.4 Performing PT/1/A/4200/019 (ECCS Pump and Piping Vent) during calculation could adversely affect results and will invalidate the calculation.
- ★.5 Manipulation of VA System should be avoided while performing Leakage Calculation due to affect on VCT level.

7. Required Unit Status

51M 7.1 NC System filled and vented with a steam bubble in the Pzr.

8. Prerequisite System Conditions

- SLM 8.1 NC System Tave at steady state condition. $(\pm 0.5^{\circ}F)$
- Sign 8.2 Reactor Power at steady state condition. $(\pm 0.2\%)$
- 5iM 8.3 Main Steam pressure at steady state condition. (± 1%)
- **SUM** 8.4 NCDT and PRT will **NOT** need to be pumped down during calculation.

NOTE: ✓ Background leakage consists of known valve stem leakage and NC Sample Purge Flow.

- Sim 8.5 IF background leakage provided, data meets the following requirements:
 - Measured within last 7 days
 - Associated system conditions unchanged since calculated

9. Test Method

- IF OAC available for leakage calculation, NC System leakage is calculated using a water inventory balance around the NC System based on input data from the OAC. OAC NC System Leakage Calculation will be initiated once per 72 hours and will then run automatically for 3 hours. During the first 15 minutes of calculation, no correlation coefficient will be displayed.
- \sqrt{IF} elapsed time greater than 60 minutes, program data may be used for leakage calculation when one of the following sets of criteria met:
- ✓ "TOTAL LEAKAGE BEST" <u>NOT</u> between ±0.15 gpm and "TOTAL LEAKAGE CORRELATION COEFF" greater than 0.6

OR

"TOTAL LEAKAGE BEST" less than 0.15 gpm and "IDENTIFIED LEAKAGE BEST" greater than or equal to "BACKGROUND LEAKAGE".

OR

- ✓ TOTAL LEAKAGE BEST" less than 0.1 gpm
- IF plant stability can <u>NOT</u> be maintained <u>AND</u> elapsed time greater than 30 minutes, leakage calculation data may be used when absolute value for Total Leakage Correlation Coefficient greater than or equal to 0.50 and Identified Leakage Best greater than or equal to Background Leakage.
- **IF** OAC is partially or wholly unavailable, NC System leakage will be calculated manually. Initial data will be recorded followed by final data after 60 - 75 minute wait. Tank volume / gallon conversion and water densities are used in equations to determine NC System leakage.
- Individual NC Pump #1 Seal Leakoff flows will be recorded and compared to the maximum allowable limit of 4.0 gpm.
- Primary to Secondary Leakage will be recorded from EMF indication(s) or Chemistry sample and compared to a maximum of 135 gpd through any one steam generator or a maximum of 389 gpd through all steam generators.
- "TOTAL ACCUMULATIVE LEAKAGE" will be calculated using "IDENTIFIED LEAKAGE BEST", "UNIDENTIFIED LEAKAGE BEST" and "TOTAL NC PUMP SEAL LEAKOFF FLOWS".

10. Data Required

- A10.1 Enclosure 13.1 (NC Leakage Calculation Using OAC) or Enclosure 13.2 (NC Leakage Determination Using Manual Calculations).
- ∧10.2 <u>IF</u> Unit 1 at 100% RTP, Enclosure 13.5 (Evaluation of NC System Unidentified Leakage Results)
- ↓0.3 Indicate on cover sheet of this procedure under Remarks Section any special system alignments made for this calculation.

11. Acceptance Criteria

- $\sqrt{11.1}$ NC System Identified Leakage shall be limited to 10 gpm. (Reference TS 3.4.13)
- $\sqrt{11.2}$ NC System Unidentified Leakage shall be limited to 1 gpm. (Reference TS 3.4.13)
- √1.3 Total NC Pumps #1 Seal Leakoff shall be limited to 16.3 gpm. (Reference SLC 16.9.7) {PIP 04-3317}
- √1.4 Total Accumulative Leakage (sum of Identified Leakage, Unidentified Leakage, and NC Pumps #1 Seal Leakoff) shall be limited to 20 gpm. (Reference SLC 16.9.7) {PIP M99-3926}
- A1.5 Each NC Pump #1 Seal Leakoff flow shall be limited to a sustained value of less than
 4.0 gpm. (Reference SLC 16.9.7, MCC-1201.01-00-0053) {PIP 05-779, M-09-1857}
- $\sqrt{1.6}$ Primary to Secondary Leakage shall be limited to 135 gpd through any one steam generator and 389 gpd through all steam generators. (Reference TS 3.4.13)

12. Procedure

- 12.1 Perform one of the following:
 - □ Enclosure 13.1, NC Leakage Calculation Using OAC

OR

Enclosure 13.2, NC Leakage Determination Using Manual Calculations

PT/**1**/A/4150/001 B Page 7 of 7

13. Enclosures

• `

- 13.1 NC Leakage Calculation Using OAC
- 13.2 NC Leakage Determination Using Manual Calculations
- 13.3 NCDT Volume
- 13.4 PRT Volume
- 13.5 Evaluation of NC System Unidentified Leakage Results

End of Body

Enclosure 13.2 NC Leakage Determination Using Manual Calculations

1. Procedure

- ☑ 1.1 Evaluate all outstanding R&Rs that may impact performance of this procedure.
- **NOTE:** \checkmark **IF** Unit 1 in Mode 3 or 4, this procedure is **NOT** required until 12 hours of steady state operation have elapsed.
 - \checkmark The first calculation is considered the first calculation after 18:00 hrs for normal operation.
- <u>SUM</u>^{FOK} 1.2 <u>IF</u> more than one leakage calculation performed per shift, a brief explanation should be entered on Autolog indicating reason for repeating calculation.

NOTE: \checkmark A continuous vent is maintained on the PRT and a continuous purge is maintained on the VCT by Radwaste Chemistry.

- 54M 1.3 Notify Radwaste Chemistry of the following:
 - Determine VCT purge status:
 - \Box Active \blacksquare Secured
 - ☑ NC System leakage calculation is in progress
 - ✓ To refrain from sampling PRT, NCDT and VCT or changing vent (purge) status of PRT, NCDT and VCT {PIPM-00-0615}

<u>Mike Smith</u> / Person Notified Date Time

- 5LM 1.4 Notify Primary Chemistry of the following:
 - ☑ NC System leakage calculation is in progress
 - ☑ To check that NC Sample Purge Flow value is unchanged from the current Autolog entry (Prerequisite System Condition 8.5)
 - ☑ NC System sampling shall only be performed with permission from the Control Room

Melvin Smith / Notified Date Time Person Notified

<u>3100</u> 1.5 Ensure adequate VCT level to prevent auto makeup during calculation.

Enclosure 13.2 NC Leakage Determination Using Manual Calculations

PT/**1**/A/4150/001 B Page 2 of 10

NOTE: Leakage Calculation will be invalid if any valve in Step 1.6 or 1.7 is repositioned during calculation.

1.6 Check closed:

- ☑ 1NC-58A (PRT Spray Supply Block)
- ☑ 1NI-9A (NC Cold Leg Inj From NV)
- ☑ 1NI-10B (NC Cold Leg Inj From NV)
- ☑ 1NV-39A (A NC Pump Standpipe Fill)
- ☑ 1NV-55B (B NC Pump Standpipe Fill)
- ☑ 1NV-71A (C NC Pump Standpipe Fill)
- ☑ 1NV-87B (D NC Pump Standpipe Fill)
- ☑ 1NV-171A (BA Blender To VCT Inlet)
- ☑ 1NV-175A (BA Blender To VCT Outlet)
- ☑, 1NV-221A (NV Pumps Suct From FWST)
- ☑ 1NV-222B (NV Pumps Suct From FWST)
- <u>SLM</u> 1.7 IF 1NV-137A (NC Filters Otlt 3-Way Cntrl) in "AUTO", perform the following:
 - 3LM 1.7.1 Place 1NV-137A to "VCT" position.
 - <u>3LM</u> 1.7.2 <u>HOLD</u> until 1NV-137A indicates "VCT", <u>THEN</u> place 1NV-137A to "AUTO".
- SLM 1.8 Place "1WL-23 Mode Select" in "MAN".
- SIM 1.9 Close 1WL-23 (NCDT Pump Level Control).

Enclosure 13.2 NC Leakage Determination Using Manual Calculations

 \Box 1.10 Perform the following:

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| NOTE: IF available, the OAC should be used to obtain data required for calculation. | | | | |
|--|---|-----------------------------|--|--|
| □ 1.10.1 | Record Start Time: | | | |
| □ 1.10.2 | Record initial VCT Level (M1P0201): | % | | |
| □ 1.10.3 | Record initial PZR Level (M1P0200): | % | | |
| NOTE: <u>IF</u> Tave 1 and T_C . | ess than 530°F AND OAC unavailable, Tave must be calculat | ted using WR T _H | | |
| □ 1.10.4 | Record initial NC System Tave (M1P1479): | °F | | |
| □ 1.10.5 | Record initial PRT Level (M1P0202): | % | | |
| □ 1.10.6 | Record initial NCDT Level (M1P0203): | % | | |
| 1.10.7 | HOLD until 60 - 75 minutes elapsed. | | | |
| □ 1.10.8 | Record Stop Time: | | | |
| □ 1.10.9 | Record final VCT Level (M1P0201): | % | | |
| □ 1.10.10 | Record final PZR Level (M1P0200): | % | | |
| NOTE: <u>IF</u> Tave 1 and T_C . | ess than 530°F AND OAC unavailable, Tave must be calculat | ted using WR T _H | | |
| □ 1.10.11 | Record final NC System Tave (M1P1479): | •F | | |
| □ 1.10.12 | Record final PRT Level (M1P0202): | % | | |
| □ 1.10.13 | Record final NCDT Level (M1P0203): | % | | |

Enclosure 13.2 PT/**1**/A/4150/001 B NC Leakage Determination Using Manual Calculations

Page 4 of 10

| □ 1.10.14 | Calculate change in NC System Tave: | |
|-----------|---|-----|
| | $\frac{1}{10000000000000000000000000000000000$ | |
| □ 1.10.15 | | |
| | [Initial Level (%) - Final Level (%)] x (19.3 Gal/%) Stop Time - Start Time (Min) | |
| | [] x 19.3 Initial (Step 1.10.2) Final (Step 1.10.9) == | gpr |
| | Stop Time (Step 1.10.2) | |
| □ 1.10.16 | Calculate PZR Leakage Rate: | |
| | [Initial Level (%) - Final Level (%)] x (132.5 Gal/%) X (0.01613 ¹) Stop Time - Start Time (Min) | |
| |] x 132.5 x 0.01613 Initial (Step 1.10.3) Final (Step 1.10.10) = | gpm |
| Sto | p Time (Step 1.10.8) Start Time (Step 1.10.1) | |
| □ 1.10.17 | Calculate Total Leakage: | |
| | VCT Leakage Rate (Step 1.10.15) + = | gpm |
| □ 1.10.18 | Using Enclosure 13.4 (PRT Volume), record the following: | |
| | Initial PRT Volume: gal (Step 1.10.5) Final PRT Volume: gal (Step 1.10.12) | |
| □ 1.10.19 | Calculate PRT Leakage Rate: | |
| | | |

¹ Specific Volume for saturated liquid at PZR temperature.

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| | Enclosure 13.2 | PT/ 1 /A/4150/001 B |
|-------------------------------|--|--|
| | NC Leakage Determination Using Manual Calculations | |
| □ 1.10.20 | Using Enclosure 13.3 (NCDT Volume), record the fo | llowing: |
| | Initial NCDT Volume: gal (Step Final NCDT Volume: gal (Step | |
| □ 1.10.21 | Calculate NCDT Leakage Rate: | |
| Fi | | gpm |
| □ 1.10.22 | Record the following: | |
| | NC Sample Purge Flow value recorded in Autolo Any quantified (measured) leakage that has been | |
| □ 1.10.23 | Calculate Total Background Leakage: | |
| | $\frac{1}{\text{NC Purge (Step 1.10.22)}} + \frac{1}{\text{Quantified (Step 1.10.22)}} = \underline{\qquad} gpm$ | |
| □ 1.10.24 | Calculate Identified Leakage: | |
| PRT Leakage Rate (Step 1.10.1 | + + = 9) NCDT Leakage Rate (Step 1.10.21) Background Leakage (Step 1.10.23) | gpm ² (< 10 gpm) |
| □ 1.10.25 | Calculate Unidentified Leakage: | |
| Total Leakage (| Step 1.10.17) - Identified Leakage (Step 1.10.24) | gpm ² (< 1 gpm) |
| □ 1.10.26 | Determine Total NC Pump #1 Seal Leakoff flow: | |
| | NC Pump 1A #1 Seal Leakoff Flow | _ gpm ² (< 4.0 gpm) _ gpm ² (< 4.0 gpm) _ gpm ² (< 4.0 gpm) |

;

² Acceptance Criteria Value

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Enclosure 13.2 Calculations

NOTE:

PT/**1**/A/4150/001 B

Page 6 of 10 NC Leakage Determination Using Manual "0" should be entered below for any negative identified or unidentified value. □ 1.10.27 Calculate "Total Accumulative Leakage": $\frac{1}{\text{Identified (Step 1.10.24)}} + \frac{1}{\text{Unidentified (Step 1.10.25)}} + \frac{1}{\text{Total NC Seal Leakoff (Step 1.10.26)}} = \frac{1}{\text{Total Accumulative Leakage}} gpm^{3} (< 20 gpm)$ Determine Primary to Secondary Leakage by performing the following: 1.11 IF in Mode 1 AND greater than or equal to 40% RTP, record indication on the 1.11.1 following: 1EMF71: . _____ gpd 1EMF72: _____ gpd . _____ gpd 1EMF73: 1EMF74: _____ gpd ٠ IF any N-16 EMF inoperable, perform the following: 1.11.1.1 A. Notify Secondary Chemistry to provide Primary to Secondary leakage. ____ /____ Date Time Person Notified □ B. Record Primary to Secondary leakage as determined by _____ gpd ³ Secondary Chemistry: C. Record date and time Primary to Secondary leakage was determined (provided by Secondary Chemistry): Date / _____ Time IF in Mode 1 AND less than 40% RTP, perform the following: 1.11.2

> Notify Secondary Chemistry to provide Primary to Secondary 1.11.2.1 leakage.

> > _____ <u>/</u>_____ Date Time Person Notified

³ This value is a total primary to secondary leakage of all four S/Gs. A value of less than or equal to 135 gpd conservatively implies leakage through any one S/G is less than or equal to 135 gpd.

| | Enclosure 13.2 | рт/ 1 /А/4150/001 в |
|------------------------------|---|--------------------------------------|
| NC | C Leakage Determination Using Manual Calculations | Page 7 of 10 |
| □ 1.11.2.2 | Record Primary to Secondary leakage Secondary Chemistry: | as determined by gpd ⁴ |
| □ 1.11.2.3 | Record date and time Primary to Second etermined (provided by Secondary C | |
| | Date / Time | |
| 1.11.3 <u>IF</u> in M | odes 2, 3 or 4, perform the following: | |
| 1.11.3.1 | Notify Secondary Chemistry to provid leakage via grab sample. | e Primary to Secondary |
| | Person Notified/ | |
| | Person Notified Date | Time |
| □ 1.11.3.2 | Record Primary to Secondary leakage Secondary Chemistry grab sample: | |
| □ 1.11.3.3 | Record date and time Primary to Second time determined (provided by Secondary C | |
| | / Date Time | |
| Calculated By: | Date: | Time: |
| Checked By: | Date: | Time: |

e *

⁴ This value is a total primary to secondary leakage of all four S/Gs. A value of less than or equal to 135 gpd conservatively implies leakage through any one S/G is less than or equal to 135 gpd.

NC Leakage Determination Using Manual Calculations

 \Box 1.12 In Autolog, perform the following:

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| NOTE | • Calculations run during power escalation <u>AND</u> other than Mode 1 calculations should be identified as such. | | | |
|------|---|--|--|--|
| | • The first calculation is considered the first calculation after 18:00 hrs for normal operation. | | | |
| | 1.12.1 Enter the following values with any pertinent comments: | | | |
| | "IDENTIFIED" leakage (Step 1.10.24) "UNIDENTIFIED" leakage (Step 1.10.25) "TOTAL NC PUMPS #1 SEAL LEAKOFF" leakage (Step 1.10.26) "TOTAL" leakage (Step 1.10.27) "CALCULATION START TIME" Primary to Secondary leakage | | | |
| | 1.12.2 IF other than the first calculation for the day, record reason and any pertinent comments. | | | |
| NOTE | : Unidentified Leakage values are expected to be within ± 0.5 gpm for Manual Calculations. Exceeding ± 0.5 gpm does NOT invalidate leakage calculation. | | | |
| 1.1 | I3 IF unidentified leakage \underline{NOT} between ± 0.5 gpm, notify Primary System Engineer. | | | |
| | | | | |

Person Notified

Date Time

NC Leakage Determination Using Manual Calculations

- 1.14 Evaluate Acceptance Criteria per one of the following:
 - □ 1.14.1 Check Acceptance Criteria specified in Section 11 met.

OR

<u>IIF</u> Acceptance Criteria specified in Section 11 <u>NOT</u> met, perform the following:

| SRO | 1.14.2.1 | Log applicable Tech Spec or SLC. {PIP M-07-00393} |
|-----|-----------|--|
| SRO | 1.14.2.2 | <u>IF</u> Total NC Pumps #1 Seal Leakoff is greater than 16.3 gpm, declare SSF capability degraded. |
| | 1 1 4 2 3 | IF Total Accumulative Leakage is greater than 20 gpm OR Tota |

| | 1.14.2.3 | IF Total Accumulative Leakage is greater than 20 gpm OR Total |
|-----|----------|---|
| SRO | | NC Pumps #1 Seal Leakoff greater than 16.3 gpm, notify |
| | | Security of degraded SSF capabilities. |

| | / | |
|-----------------|------|------|
| Person Notified | Date | Time |

1.14.2.4IF any NC Pump #1 Seal Leakoff has a sustained value of greater
than OR equal to 4.0 gpm, notify SSS Engineer and Security of
degraded SSF capability.

| | | / |
|-----------------|------|------|
| Person Notified | Date | Time |

- 1.15 IF this is the second Leakage Calculation and elevated leakage is indicated, evaluate performing PT/1/A/4150/001 D (Identifying NC System Leakage).
- 1.16 Lower NCDT level less than 48%.
- 1.17 Close 1WL-23 (NCDT Level Control).
- 1.18 Place "1WL-23 Mode Select" to "AUTO".

| | Enclosure 13.2 | РТ/ 1 /А/4150/001 В |
|------|---|----------------------------|
| | NC Leakage Determination Using Manual Calculations | Page 10 of 10 |
| 1.19 | Notify Radwaste Chemistry of the following: | |
| | □ NC System leakage calculation is complete | |
| | □ PRT, NCDT and VCT sampling or venting may be initiated | {PIPM-00-0615} |
| | Person Notified / Date Time | |
| 1.20 | Notify Primary Chemistry of the following: | |
| | □ NC System leakage calculation is complete | |
| | □ NC System sampling may be initiated | |
| | Person Notified / | |
| 1.21 | IF Unit 1 at 100% RTP AND OAC is available, perform Enclos NC System Unidentified Leakage Results). | ure 13.5 (Evaluation of |

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End of Enclosure

Enclosure 13.3 NCDT Volume

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PT/**1**/A/4150/001 B Page 1 of 1

| NCDT LEVEL % | NCDT VOLUME | NCDT LEVEL % | NCDT VOLUME | NCDT LEVEL % | NCDT VOLUME |
|--------------|-------------|--------------|-------------|--------------|-------------|
| | (Gal) | | (Gal) | | (Gal) |
| 0 | 19.7 | 35 | 123.1 | 70 | 247.3 |
| 1 | 21.9 | 36 | 126.6 | 71 | 250.7 |
| 2 | 24.1 | 37 | 130.1 | 72 | 254.0 |
| 3 | 26.4 | 38 | 133.6 | 73 | 257.3 |
| 4 | 28.8 | 39 | 137.1 | 74 | 260.6 |
| 5 | 31.2 | 40 | 140.7 | 75 | 263.9 |
| 6 | 33.7 | 41 | 144.3 | 76 | 267.2 |
| 7 | 36.2 | 42 | 147.8 | 77 | 270.4 |
| 8 | 38.8 | 43 | 151.4 | 78 | 273.6 |
| 9 | 41.4 | 44 | 155.0 | 79 | 276.8 |
| 10 | 44.1 | 45 | 158.6 | 80 | 279.9 |
| 11 | 46.9 | 46 | 162.2 | 81 | 283.0 |
| 12 | 49.6 | 47 | 165.8 | 82 | 286.1 |
| 13 | 52.5 | 48 | 169.4 | 83 | 289.1 |
| 14 | 55.3 | 49 | 173.0 | 84 | 292.1 |
| 15 | 58.2 | 50 | 176.6 | 85 | 295.1 |
| 16 | 61.2 | 51 | 180.2 | 86 | 298.0 |
| 17 | 64.2 | 52 | 183.8 | 87 | 300.9 |
| 18 | 67.2 | 53 | 187.5 | 88 | 303.8 |
| 19 | 70.3 | 54 | 191.1 | 89 | 306.6 |
| 20 | 73.4 | 55 | 194.7 | 90 | 309.4 |
| 21 | 76.5 | 56 | 198.2 | 91 | 312.1 |
| 22 | 79.6 | 57 | 201.8 | 92 | 314.7 |
| 23 | 82.8 | 58 | 205.4 | 93 | 317.4 |
| 24 | 86.0 | 59 | 209.0 | 94 | 319.9 |
| 25 | 89.3 | 60 | 212.5 | 95 | 322.4 |
| 26 | 92.6 | 61 | 216.1 | 96 | 324.9 |
| 27 | 95.9 | 62 | 219.6 | 97 | 327.3 |
| 28 | 99.2 | 63 | 223.1 | 98 | 329.6 |
| 29 | 102.5 | 64 | 226.6 | 99 | 331.9 |
| 30 | 105.9 | 65 | 230.1 | 100 | 334.0 |
| 31 | 109.3 | 66 | 233.6 | | |
| 32 | 112.7 | 67 | 237.0 | | |
| 33 | 116.2 | 68 | 240.5 | | |
| 34 | 119.6 | 69 | 243.9 | | |

End of Enclosure

Enclosure 13.4 PRT Volume

. .

PT/**1**/A/4150/001 B Page 1 of 1

| PRT LEVEL % | PRT VOLUME (Gal) | PRT LEVEL % | PRT VOLUME (Gal) | PRT LEVEL % | PRT VOLUME (Gal) |
|-------------|---------------------|-------------|---------------------|-------------|---------------------|
| 0 | 303.2 | 35 | 4472.0 | 70 | 9799.8 |
| 1 | 371.9 | 36 | 4621.5 | 71 | 9942.5 |
| 2 | 445.6 | 37 | 4771.8 | 72 | 10084.0 |
| 3 | 523.9 | 38 | 4922.8 | 73 | 10224.1 |
| 4 | 606.7 | 39 | 5074.6 | 74 | 10362.9 |
| 5 | 693.6 | 40 | 5227.0 | 75 | 10500.3 |
| 6 | 784.5 | 41 | 5379.9 | 76 | 10636.1 |
| 7 | 879.0 | 42 | 5533.4 | 77 | 10770.4 |
| 8 | 977.0 | 43 | 5687.3 | 78 | 10903.1 |
| 9 | 1078.3 | 44 | 5841.7 | 79 | 11034.1 |
| 10 | 1182.7 | 45 | 5996.4 | 80 | 11163.3 |
| 11 | 1290.0 | 46 | 6151.4 | 81 | 11290.6 |
| 12 | 1400.2 | 47 | 6306.6 | 82 | 11416.0 |
| 13 | 1513.0 | 48 | 6461.9 | 83 | 11539.3 |
| 14 | 1628.4 | 49 | 6617.4 | 84 | 11660.6 |
| 15 | 1746.2 | 50 | 6772.9 | 85 | 11779.6 |
| 16 | 1866.2 | 51 | 6928.4 | 86 | 11896.2 |
| 17 | 1988.5 | 52 | 7083.8 | 87 | 12010.4 |
| 18 | 2112.9 | 53 | 7239.0 | 88 | 12122.0 |
| 19 | 2239.2 | 54 | 7394.1 | 89 | 12231.0 |
| 20 | 2367.5 | 55 | 7548.9 | 90 | 12337.0 |
| 21 | 2497.6 | 56 | 7703.4 | 91 | 12440.0 |
| 22 | 2629.4 | 57 | 7857.5 | 92 | 12539.9 |
| 23 | 2763.0 | 58 | 8011.2 | 93 | 12636.3 |
| 24 | 2898.1 | 59 | 8164.3 | 94 | 12729.2 |
| 25 | 3034.8 | 60 | 8316.9 | 95 | 12818.3 |
| 26 | 3172.9 | 61 | 8468.9 | 96 | 12903.4 |
| 27 | 3312.4 | 62 | 8620.3 | 97 | 12984.2 |
| 28 | 3453.3 | 63 | 8770.9 | 98 | 13060.5 |
| 29 | 3595.5 | 64 | 8920.7 | 99 | 13132.0 |
| 30 | 3738.9 | 65 | 9069.6 | 100 | 13198.3 |
| 31 | 3883.4 | 66 | 9217.7 | | |
| 32 | 4029.1 | 67 | 9364.8 | | |
| 33 | 4175.7 | 68 . | 9510.9 | | |
| 34 | 4323.4 | 69 | 9655.9 | | |

End of Enclosure

JPM A2 SRO

2010 Admin - JPM A2 SRO

NUREG 1021, Revision 9

| Appendix C | Page 2 | of 12 | Form ES-C-1 |
|---------------------|---|------------------|--|
| | Job Performance M | easure Worksheet | |
| | | | |
| Facility: | McGuire | Task No.: | |
| Task Title: | Perform/Review a Manual NC Leakage Calculation | JPM No.: | <u>2010 Admin - JPM A2</u> <u>SRO</u> |
| K/A Reference: | GK/A 2.2.12 (4.1) | | |
| Examinee: | | NRC Examiner | : |
| Facility Evaluator: | | Date: | |
| Method of testing: | | | |
| Simulated Perform | ance: | Actual Perform | ance: X |
| Classr | oom X Simulator | Plant | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | Unit 1 is at 100% power. |
|---------------------|---|
| | The Unit 1 OAC point M1L4554 is out of service. |
| | PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm. |
| | A manual NC System leakage calculation is in progress in accordance with PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) |
| | Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) has been completed through Step 1.9. |
| Task Standard: | The operator will complete all calculations in accordance with the attached Key, identify that the Unidentified RCS Leakage Technical Specification has been exceeded, and the required ACTION. |
| Required Materials: | None. |
| General References: | PT/1/A/4200/040 (Reactor Coolant Leakage Detection) PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) McGuire Unit 1 Technical Specifications |

| Appendix C | Page 3 of 12 | Form ES-C- |
|-----------------|---|------------------------|
| | Job Performance Measure Worksheet | |
| Handouts: | PT/1/A/4150/001B (Reactor Coolant Leakage Cal follows: | lculation) marked up a |
| | Step 7.1 – Initialed | |
| | Steps 8.1 through 8.5 – Initialed. | |
| | Step 12.1 Enclosure 13.2 Checkbox is checked. | |
| | PT/1/A/4150/001B (Reactor Coolant Leakage Cal 13.2 (NC Leakage Determinations Using Manual up as follows: | , |
| | Step 1.1 – Checkbox is checked/Initialed. | |
| | Step 1.2 – Initialed. | |
| | Step 1.3 – Initialed. | |
| | Determine VCT Purge Status Checkbox is che | cked. |
| | Secured Checkbox is checked. | |
| | NC System leakage calculation is in progress (| Checkbox is checked. |
| | To refrain from sampling Checkbox is check | ked. |
| | Person Notified Mike Smith Today's Date/Time | : |
| | Step 1.4 – Initialed. | |
| | NC System leakage calculation is in progress (| Checkbox is checked. |
| | To check that NC sample Checkbox is chec | cked. |
| | NC System sampling Checkbox is checked | |
| | Person Notified Melvin Smith Today's Date/Tim | ne |
| | Step 1.5 – Initialed. | |
| | Step 1.6 – All Checkboxes checked/Initialed. | |
| | Step 1.7 – Initialed. | |
| | Step 1.7.1 – Initialed. | |
| | Step 1.7.2 – Initialed. | |
| | Step 1.8 – Initialed. | |
| | Step 1.9 – Initialed. | |
| | Enclosure 13.3 (NCDT Volume) of PT/1/A/4150/00 Leakage Calculation) | 01B (Reactor Coolant |
| | Enclosure 13.4 (PRT Volume) of PT/1/A/4150/001 Leakage Calculation) | IB (Reactor Coolant |
| | McGuire Technical Specifications | |
| Initiating Cue: | Using Enclosure 13.2 (NC Leakage Determination Calculations), AND the attached Datasheet, comp Leakage Calculation, by performing Steps 1.10 ar the Acceptance Criteria. | lete the NC System |
| | Identify any Technical Specifications impacted an ACTION. | d any required |

2010 Admin - JPM A2 SRO

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| Ap | pendix | С |
|----|--------|---|
|----|--------|---|

Time Critical Task: NO

Validation Time: 25 minutes

Page 5 of 12 PERFORMANCE INFORMATION

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue, and associated Datasheet (Last two (2) Pages of this JPM); and Handout PT/1/A/4150/001B procedure body marked up as described, Enclosure 13.2 marked up as described, Enclosure 13.3 and Enclosure 13.4.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 1 | (Enclosure 13.2, Steps 1.10.1 through 13, 22, 26 and 1.11.1) Record raw data. | The operator transposes raw data from the Data Sheet provided. | | |
| 2 | (Enclosure 13.2, Step 1.10.14) Calculate change in NC System Tave: | The operator calculates the change in NC System Tave to be <u>0°F</u> , and records. | | |
| 3 | (Enclosure 13.2, Step 1.10.15) Calculate VCT Leakage Rate: | The operator calculates the VCT Leakage Rate to be <u>1.55 gpm</u> , and records. | | |
| 4 | (Enclosure 13.2, Step 1.10.16) Calculate PZR Leakage Rate: | The operator calculates the PZR Leakage Rate to be 0.02 gpm , and records. | | |
| 5 | (Enclosure 13.2, Step 1.10.17) Calculate Total Leakage: | The operator calculates the Total Leakage to be <u>1.57</u> <u>gpm</u> , and records. | | |

Page 6 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 6 | (Enclosure 13.2, Step 1.10.18) Using Enclosure 13.4 (PRT Volume), record the following: Initial PRT Volume Final PRT Volume | The operator uses Enclosure 13.4 and an initial PRT Level of 76.0 %, and determines that initial PRT Volume is <u>10636.1</u> <u>gal</u> , and records. The operator uses Enclosure 13.4 and interpolates a PRT Volume for 76.1% to be <u>10649.5</u> <u>gal</u> , and records. | | |
| 7 | (Enclosure 13.2, Step 1.10.19) Calculate PRT Leakage Rate: | The operator calculates the PRT Leakage Rate to be <u>.19 gpm</u> , and records. | | |
| 8 | (Enclosure 13.2, Step 1.10. 20) Using Enclosure 13.3 (NCDT Volume), record the following: Initial NCDT Volume Final NCDT Volume | The operator uses Enclosure 13.3 and an initial NCDT Level of <u>30.0%</u> , and determines that initial NCDT Volume is <u>105.9 gal</u> , and records. | | |
| | | The operator uses Enclosure 13.3 and a final NCDT Level of <u>33.0%</u> , and determines that final NCDT Volume is <u>116.2 gal</u> , and records. | | |
| 9 | (Enclosure 13.2, Step 1.10.21) Calculate NCDT Leakage Rate: | The operator calculates the NCDT Leakage Rate to be .14 gpm, and records. | | |
| 10 | (Enclosure 13.2, Step 1.10.23) Calculate Total Background Leakage: | The operator calculates the Total Background Leakage to be <u>0 gpm</u> , and records. | | |

Page 7 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| Г | 1 | | | |
|-------|---|--|-----|-----------------------------------|
| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
| *11 | (Enclosure 13.2, Step 1.10.24) Calculate Identified Leakage: | The operator calculates the Identified Leakage to be <u>0.33 (±10%) gpm</u> , and records. | | |
| *12 | (Enclosure 13.2, Step 1.10.25) Calculate Unidentified Leakage: | The operator calculates the Unidentified Leakage to be 1.24 (±10%) gpm , and records. | | |
| *13 | (Enclosure 13.2, Step 1.10.26) Determine Total NC Pump #1 Seal Leakoff: | The operator calculates the Total NC Pumps #1 Seal Leakoff to be <u>12.8 (±10%)</u> <u>gpm</u> , and records. | | |
| *14 | (Enclosure 13.2, Step 1.10.27) Calculate Total Accumulative Leakage: | The operator calculates the Total Accumulative Leakage to be <u>14.37</u> (±10%) gpm, and records. | | |
| 15 | (Enclosure 13.2) Calculated By/ Date/Time: | The operator places their name in the Calculated by BLOCK, and signs. The operator enters the Date and Time. | | |

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Page 8 of 12 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS |
|-------|---|---|-----|-----------|
| | | | 0,0 | REQUIRED |
| | | | | FOR UNSAT |
| *16 | Technical Specification LCO 3.4.13: RCS operational LEAKAGE shall be limited to: | The operator returns the completed Enclosure 13.2 and reports that LCO 3.4.13.b (1 gpm unidentified LEAKAGE) has been | | |
| | shan be innited to. | exceeded. | | |
| | a. No pressure boundary LEAKAGE; | The operator identifies that | | |
| | b. 1 gpm unidentified LEAKAGE; | CONDITION A is met, RCS Operational LEAKAGE not within limits for reasons | | |
| | c. 10 gpm identified LEAKAGE; | other than pressure boundary LEAKAGE or primary to secondary | | |
| | d. 389 gallons per day total primary to secondary LEAKAGE through all steam generators (SGs); and | LEAKAGE; AND that the REQUIRED ACTION is to Reduce LEAKAGE to within limits, within 4 hours. | | |
| | e. 135 gallons per day primary to secondary | Examiner NOTE: | | |
| | LEAKAGE through any one steam generator (SG). | See KEY on Page 10 of this JPM. | | |
| | APPLICABILITY: MODES 1, 2, 3, and 4. | , , | | |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

| Appendix C | А | pp | en | dix | С |
|------------|---|----|----|-----|---|
|------------|---|----|----|-----|---|

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Form ES-C-1

| Job Performance Measure No.: | 2010 Admin - JF | PM A2 SRO | |
|------------------------------|-----------------|-----------|----|
| Examinee's Name: | | | |
| Date Performed: | | | |
| Facility Evaluator: | | | |
| Number of Attempts: | 1 | | |
| Time to Complete: | | | |
| Question Documentation: | | | |
| | | | |
| | | | |
| | | | |
| Result: | SAT | UNSAT | |
| Examiner's Signature: | | Dat | e: |

Appendix C

Page 10 of 12 VERIFICATION OF COMPLETION

KEY:

Enclosure 13.2, Step 1.10.14 (JPM Step 2): Change in NC System Tave: $584.8^{\circ}F - 584.8^{\circ}F = 0^{\circ}F$

Enclosure 13.2, Step 1.10.15 (JPM Step 3): VCT Leakage Rate: (53.4% – 47.6%) x19.3 gallons/%/72 minutes = 1.55 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.16 (JPM Step 4): PZR Leakage Rate: (54.9% – 54.1%) x 132.5 gallons/% x .01613 /72 minutes = 0.02 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.17 (JPM Step 5): Total Leakage: 1.55 gpm + 0.02 gpm = 1.57 gpm

Enclosure 13.2, Step 1.10.18 (JPM Step 6): PRT Final Volume:

(10770.4-10636.1)/10 = 13.43/.1% PRT Level, 10636.1 + 13.43 = 10649.53 (gal)

Enclosure 13.2, Step 1.10.19 (JPM Step 7): Total PRT Leakage: (10649.5 gallons – 10636.1 gallons)/72 minutes = 0.19 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.21 (JPM Step 9): Total NCDT Leakage: (116.2 gallons – 105.9 gallons)/72 minutes = 0.14 gallons per minute (gpm)

Enclosure 13.2, Step 1.10.23 (JPM Step 10): Total Background Leakage: (0 gpm + 0 gpm) = 0 gpm

Enclosure 13.2, Step 1.10.24 (JPM Step 11): Identified Leakage: (.19 gpm + .14 gpm + 0 gpm) = 0.33 gpm

Enclosure 13.2, Step 1.10.25 (JPM Step 12): Unidentified Leakage: (1.57 gpm - .33 gpm) = 1.24 gpm

Enclosure 13.2, Step 1.10.26 (JPM Step 13): Total NC Pumps #1 Seal Leakoff: (2.8 gpm + 3.6 gpm + 3.1 gpm + 3.3 gpm) = 12.8 gpm

Enclosure 13.2, Step 1.10.27 (JPM Step 14): Total Accumulative Leakage: (.33 gpm + 1.24 gpm + 12.8 gpm) = 14.37 gpm

LCO 3.4.13.b (1 gpm unidentified LEAKAGE) has been exceeded, CONDITION A is met, RCS Operational LEAKAGE not within limits for reasons other than pressure boundary LEAKAGE or primary to secondary LEAKAGE; AND that the REQUIRED ACTION is to Reduce LEAKAGE to within limits, within 4 hours.



INITIAL CONDITIONS: Unit 1 is at 100% power.

The Unit 1 OAC point M1L4554 is out of service.

PT/1/A/4200/040 (Reactor Coolant Leakage Detection) has been completed showing that NCS Leakage is 1.6 gpm.

A manual NC System leakage calculation is in progress in accordance with PT/1/A/4150/001B (Reactor Coolant Leakage Calculation)

Enclosure 13.2 (NC Leakage Determination Using Manual Calculations) of PT/1/A/4150/001B (Reactor Coolant Leakage Calculation) has been completed through Step 1.9.

INITIATING CUE:Using Enclosure 13.2 (NC Leakage Determination Using Manual
Calculations), AND the attached Datasheet, complete the NC
System Leakage Calculation, by performing Steps 1.10 and 1.11,
AND evaluate the Acceptance Criteria.

Identify any Technical Specifications impacted and any required ACTION.

: • • • • į• •

JPM CUE SHEET

Data Sheet

| Start Time | 0100 | |
|---------------------------------|--------------------------------|--------------|
| Stop Time | 0212 | - Kales |
| | | |
| | | |
| | Initial | <u>Final</u> |
| VCT Level | 53.4 | 47.6 |
| Pzr Level | 54.9 | 54.1 |
| NC System Tave | 584.8 | 584.8 |
| PRT Level | 76.0 | 76.1 |
| NCDT Level | 30 | 33 |
| | | |
| NC Sample Purge Flow v | alue recorded in Autolog | 0 |
| | akage that has been identified | 0 |
| | | |
| NC Pump 1A #1 Seal Leakoff Flow | | 2.8 |
| | Seal Leakoff Flow | 3.6 |
| | Seal Leakoff Flow | 3.1 |
| NC Pump 1D #1 S | Seal Leakoff Flow | 3.3 |
| | | |
| 1EMF71 | Reading | 1.2 |
| 1EMF72 | | 1.7 |
| 1EMF73 | | 1.1 |
| 1EMF74 | Reading | 1.9 |

| Duke Energy | Procedure No. |
|--|----------------------------|
| McGuire Nuclear Station | рт/ 1 /А/4150/001 в |
| Reactor Coolant Leakage Calculation | Revision No. |
| | 067 |
| | |
| | |
| | |
| | Electronic Reference No |
| Continuous Use | MC0047QI |
| PERFORMANCE | |
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| Revision | Revision History (significant issues, limited to one page) | | | | |
|----------|---|--|--|--|--|
| Rev 067 | Changed format of procedure to split out calculation performed by OAC and performed by manual calculation. Combined leakage calculation using the OAC steps with current Enclosure 13.1 and renamed enclosure "NC Leakage Calculation Using OAC". Combined manual leakage calculation steps with Enclosure 13.2 and renamed enclosure "NC Leakage Determination Using Manual Calculation". Changed all references throughout procedure to include these format changes. Encl. 13.5. Added Independent Verification sign offs for calculation of seven day rolling average of Unidentified Leakage. {PIP M-09-1307} Revised current steps for determining if Tier Two or Tier Three Action levels exceeded to reference step numbers associated with determination. Intent is to clarify steps. Reworded steps that state "IF directed" by engineering to "IF advised" by engineering. Definition of "directed" changed with new fatigue rule. Added PIP M-09-1857 as an additional reference to NCP seal leakage basis. Modified steps that begin with "WHEN" to reflect NSD 704 Rev 016 requirements. | | | | |
| Rev 066 | Body of procedure. Added a limit and precaution about manipulation of VA System during leakage calculation has an affect on VCT level. Re-worded Step 12.6.17. The leakage calculation is considered valid after 60 minutes but is preferred to run up to 3 hours. The step as written requires the operator to print calculation after 60 minutes when 1 of 3 conditions met. This is procedure use and adherence issue. Re-worded step to give operator flexibility to print calculation summary between 60 minutes and 3 hours. Re-worded Step 12.6.35. If operator performs section 12.6.16 to abort leakage calculation early, enclosure 13.1 is not performed. 12.6.35 directs operator to perform Encl. 13.5, however, this enclosure requires data from enclosure 13.1. Re-worded step to stipulate if unit at 100% RTP AND Encl. 13.1 completed, then perform Encl. 13.5. Procedure use and adherence issue. | | | | |
| Rev 065 | Added step to make operator aware that if leakage calc ran for greater than 30 minutes but less than 60 minutes, the data can still be valid if it meets certain conditions. Added step to record status of VCT purge at beginning of procedure. Added steps to take NV-137A "hard" to VCT and back to "AUTO" prior to starting leakage calculation. Encl. 13.5. Reworded section if any Tier One, Two, or Three Action level is exceeded to make it easier to understand. | | | | |

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Reactor Coolant Leakage Calculation

1. Purpose

/ To determine NC System Leakage using the Operator Aid Computer (OAC) or manual calculations to ensure Tech Spec requirements met.

2. References

- ✓ 2.1 Tech Spec TS SR 3.4.13.1, 3.4.13.2, TS 3.4.15
- ✓ 2.2 SLC 16.9.7 Standby Shutdown System
- /2.3 MCS-1274.00-00-0016 (License Renewal Basis Spec), Section 4.29
- ✓2.4 UFSAR Chapter 18 (Aging Management Program and Activities), Table 18-1, Reactor Coolant Operational Leakage Monitoring Program
- ✓ 2.5 SLC 16.7.6 Radiation Monitoring for Plant Operation
- √2.6 WCAP-16423-NP (Methodology for calculating Unidentified NC System leakage)
- √2.7 WCAP-16465-NP (Action levels and response guidelines for increasing Unidentifed NC System leakage less than Tech Spec limits)
- √2.8 MCC-1201.01-00-0053 (MNS Unit 1 & 2 NC Pump Response to Loss of Seal Cooling)

3. Time Required

 $\sqrt{3.1}$ One operator for three hours every 72 hours.

4. Prerequisite Test

/None

5. Test Equipment

/_{None}

6. Limits and Precautions

- ✓ 6.1 NC System Tave, Reactor Power, Containment Temperature, and SM Pressure should remain constant during calculation.
- $\sqrt{6.2}$ Positioning values during calculation which could adversely affect results will invalidate the calculation.
- $\sqrt{6.3}$ Performing Leakage Calculation between 3 am and 8 am on Wednesdays may cause calculation to fail due to OAC weekly backup routine.
- √6.4 Performing PT/1/A/4200/019 (ECCS Pump and Piping Vent) during calculation could adversely affect results and will invalidate the calculation.
- ★.5 Manipulation of VA System should be avoided while performing Leakage Calculation due to affect on VCT level.

7. Required Unit Status

5LM 7.1 NC System filled and vented with a steam bubble in the Pzr.

8. Prerequisite System Conditions

- <u>SIM</u> 8.1 NC System Tave at steady state condition. $(\pm 0.5^{\circ}F)$
- <u>SLM</u> 8.2 Reactor Power at steady state condition. $(\pm 0.2\%)$
- <u>5LM</u> 8.3 Main Steam pressure at steady state condition. (± 1%)
- **SEM** 8.4 NCDT and PRT will **NOT** need to be pumped down during calculation.

NOTE: ✓ Background leakage consists of known valve stem leakage and NC Sample Purge Flow.

- <u>SLM</u> 8.5 <u>IF</u> background leakage provided, data meets the following requirements:
 - Measured within last 7 days
 - Associated system conditions unchanged since calculated

9. Test Method

IF OAC available for leakage calculation, NC System leakage is calculated using a water inventory balance around the NC System based on input data from the OAC. OAC NC System Leakage Calculation will be initiated once per 72 hours and will then run automatically for 3 hours. During the first 15 minutes of calculation, no correlation coefficient will be displayed.

 \sqrt{IF} elapsed time greater than 60 minutes, program data may be used for leakage calculation when one of the following sets of criteria met:

✓ "TOTAL LEAKAGE BEST" <u>NOT</u> between ±0.15 gpm and "TOTAL LEAKAGE CORRELATION COEFF" greater than 0.6

OR

"TOTAL LEAKAGE BEST" less than 0.15 gpm and "IDENTIFIED LEAKAGE BEST" greater than or equal to "BACKGROUND LEAKAGE".

OR

- ✓ TOTAL LEAKAGE BEST" less than 0.1 gpm
- **<u>IF</u>** plant stability can <u>NOT</u> be maintained <u>AND</u> elapsed time greater than 30 minutes, leakage calculation data may be used when absolute value for Total Leakage Correlation Coefficient greater than or equal to 0.50 and Identified Leakage Best greater than or equal to Background Leakage.
- JF OAC is partially or wholly unavailable, NC System leakage will be calculated manually. Initial data will be recorded followed by final data after 60 - 75 minute wait. Tank volume / gallon conversion and water densities are used in equations to determine NC System leakage.
- Individual NC Pump #1 Seal Leakoff flows will be recorded and compared to the maximum allowable limit of 4.0 gpm.
- Primary to Secondary Leakage will be recorded from EMF indication(s) or Chemistry sample and compared to a maximum of 135 gpd through any one steam generator or a maximum of 389 gpd through all steam generators.
- "TOTAL ACCUMULATIVE LEAKAGE" will be calculated using "IDENTIFIED LEAKAGE BEST", "UNIDENTIFIED LEAKAGE BEST" and "TOTAL NC PUMP SEAL LEAKOFF FLOWS".

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10. Data Required

- √10.1 Enclosure 13.1 (NC Leakage Calculation Using OAC) or Enclosure 13.2 (NC Leakage Determination Using Manual Calculations).
- ★10.2 <u>IF</u> Unit 1 at 100% RTP, Enclosure 13.5 (Evaluation of NC System Unidentified Leakage Results)
- ↓0.3 Indicate on cover sheet of this procedure under Remarks Section any special system alignments made for this calculation.

11. Acceptance Criteria

- $\sqrt{11.1}$ NC System Identified Leakage shall be limited to 10 gpm. (Reference TS 3.4.13)
- $\sqrt{1.2}$ NC System Unidentified Leakage shall be limited to 1 gpm. (Reference TS 3.4.13)
- √1.3 Total NC Pumps #1 Seal Leakoff shall be limited to 16.3 gpm. (Reference SLC 16.9.7) {PIP 04-3317}
- 1.4 Total Accumulative Leakage (sum of Identified Leakage, Unidentified Leakage, and NC Pumps #1 Seal Leakoff) shall be limited to 20 gpm. (Reference SLC 16.9.7) {PIP M99-3926}
- ▲1.5 Each NC Pump #1 Seal Leakoff flow shall be limited to a sustained value of less than
 4.0 gpm. (Reference SLC 16.9.7, MCC-1201.01-00-0053) {PIP 05-779, M-09-1857}
- √1.6 Primary to Secondary Leakage shall be limited to 135 gpd through any one steam generator and 389 gpd through all steam generators. (Reference TS 3.4.13)

12. Procedure

12.1 Perform one of the following:

□ Enclosure 13.1, NC Leakage Calculation Using OAC

OR

Enclosure 13.2, NC Leakage Determination Using Manual Calculations

13. Enclosures

- 13.1 NC Leakage Calculation Using OAC
- 13.2 NC Leakage Determination Using Manual Calculations
- 13.3 NCDT Volume
- 13.4 PRT Volume
- 13.5 Evaluation of NC System Unidentified Leakage Results

End of Body

: 1

NC Leakage Determination Using Manual Calculations

1. Procedure

- ☑ 1.1 Evaluate all outstanding R&Rs that may impact performance of this procedure.
- **NOTE:** \checkmark IF Unit 1 in Mode 3 or 4, this procedure is <u>NOT</u> required until 12 hours of steady state operation have elapsed.
 - ✓ The first calculation is considered the first calculation after 18:00 hrs for normal operation.

<u>SCM</u>^{FBK} 1.2 IF more than one leakage calculation performed per shift, a brief explanation should be entered on Autolog indicating reason for repeating calculation.

NOTE: \checkmark A continuous vent is maintained on the PRT and a continuous purge is maintained on the VCT by Radwaste Chemistry.

5LM 1.3 Notify Radwaste Chemistry of the following:

Determine VCT purge status:

 \Box Active \blacksquare Secured

- MC System leakage calculation is in progress
- ✓ To refrain from sampling PRT, NCDT and VCT or changing vent (purge) status of PRT, NCDT and VCT {PIPM-00-0615}

<u>Mike Smith</u> / Person Notified Date Time

- **SLM** 1.4 Notify Primary Chemistry of the following:
 - M NC System leakage calculation is in progress
 - ☑ To check that NC Sample Purge Flow value is unchanged from the current Autolog entry (Prerequisite System Condition 8.5)
 - ✓ NC System sampling shall only be performed with permission from the Control Room

<u>Melvin Smith</u> / Person Notified Date Time

31.5 Ensure adequate VCT level to prevent auto makeup during calculation.

NC Leakage Determination Using Manual Calculations

| NOTE:√ | Leakage Calculation will be invalid if any value in Step 1.6 or 1.7 is repositioned during calculation. |
|----------------|--|
| 1.6 | Check closed: |
| | INC-58A (PRT Spray Supply Block) INI-9A (NC Cold Leg Inj From NV) INI-10B (NC Cold Leg Inj From NV) INV-39A (A NC Pump Standpipe Fill) INV-55B (B NC Pump Standpipe Fill) INV-71A (C NC Pump Standpipe Fill) INV-87B (D NC Pump Standpipe Fill) INV-171A (BA Blender To VCT Inlet) INV-175A (BA Blender To VCT Outlet) |
| | INV-221A (NV Pumps Suct From FWST) INV-222B (NV Pumps Suct From FWST) |
| <u>slm</u> 1.7 | IF 1NV-137A (NC Filters Otlt 3-Way Cntrl) in "AUTO", perform the following: |
| SLM | 1.7.1 Place 1NV-137A to "VCT" position. |
| <u>_3LM</u> | 1.7.2 HOLD until 1NV-137A indicates "VCT", THEN place 1NV-137A to "AUTO". |
| <u>SLM</u> 1.8 | Place "1WL-23 Mode Select" in "MAN". |

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<u>SIM</u> 1.9 Close 1WL-23 (NCDT Pump Level Control).

Unit 1

3

NC Leakage Determination Using Manual Calculations

| □ 1.10 | Perform the following: |
|--------|------------------------|
|--------|------------------------|

| NOTE: <u>IF</u> availa | able, the OAC should be used to obtain data required for calculation | ion. | | | | |
|--|--|-------------------------|--|--|--|--|
| □ 1.10.1 | Record Start Time: | | | | | |
| □ 1.10.2 | Record initial VCT Level (M1P0201): | _% | | | | |
| □ 1.10.3 | Record initial PZR Level (M1P0200): | _% | | | | |
| NOTE: <u>IF</u> Tave and T _C . | less than 530°F AND OAC unavailable, Tave must be calculated | using WR T _H | | | | |
| □ 1.10.4 | Record initial NC System Tave (M1P1479): | °F | | | | |
| □ 1.10.5 | Record initial PRT Level (M1P0202): | | | | | |
| □ 1.10.6 | Record initial NCDT Level (M1P0203): | % | | | | |
| 1.10.7 | HOLD until 60 - 75 minutes elapsed. | | | | | |
| □ 1.10.8 | Record Stop Time: | | | | | |
| □ 1.10.9 | Record final VCT Level (M1P0201): | % | | | | |
| □ 1.10.10 | Record final PZR Level (M1P0200): | % | | | | |
| NOTE: <u>IF</u> Tave less than 530°F <u>AND</u> OAC unavailable, Tave must be calculated using WR T_H and T_C . | | | | | | |
| □ 1.10.11 | Record final NC System Tave (M1P1479): | °F | | | | |
| □ 1.10.12 | Record final PRT Level (M1P0202): | % | | | | |
| □ 1.10.13 | Record final NCDT Level (M1P0203): | % | | | | |

Unit 1

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| NOTE: <u>IF</u> chang be repeat | the in Tave greater than 0.25° F (0.1°F using OAC), calculation is invited. | valid and must |
|------------------------------------|--|----------------|
| □ 1.10.14 | Calculate change in NC System Tave: | |
| | Initial (Step 1.10.4) Final (Step 1.10.11) | |
| □ 1.10.15 | Calculate VCT Leakage Rate: | |
| | [Initial Level (%) - Final Level (%)] x (19.3 Gal/%) Stop Time - Start Time (Min) | |
| | [] x 19.3 | |
| | Initial (Step 1.10.2) Final (Step 1.10.9) = Stop Time (Step 1.10.8) Start Time (Step 1.10.1) | gpm |
| □ 1.10.16 | Calculate PZR Leakage Rate: | |
| | [Initial Level (%) - Final Level (%)] x (132.5 Gal/%) X (0.01613 ¹) Stop Time - Start Time (Min) | |
| [_ |] x 132.5 x 0.01613 Initial (Step 1.10.3) Final (Step 1.10.10) = | |
| Sto | pp Time (Step 1.10.8) Start Time (Step 1.10.1) | gpm |
| □ 1.10.17 | Calculate Total Leakage: | |
| | + = = | gpm |
| □ 1.10.18 | Using Enclosure 13.4 (PRT Volume), record the following: | |
| | Initial PRT Volume: gal (Step 1.10.5) Final PRT Volume: gal (Step 1.10.12) | |
| □ 1.10.19 | Calculate PRT Leakage Rate: | |
| | · | |
| | Final Volume (Step 1.10.18) Initial Volume (Step 1.10.18) | gpm |
| | Stop Time (Step 1.10.8) Start Time (Step 1.10.1) | |

¹ Specific Volume for saturated liquid at PZR temperature.

| | Enclosure 13.2 NC Leakage Determination Using Manual Calculations | PT/ 1 /A/4150/001 B Page 5 of 10 |
|-------------------------------|---|---|
| □ 1.10.20 | Using Enclosure 13.3 (NCDT Volume), record the following | llowing: |
| | Initial NCDT Volume: gal (Step Final NCDT Volume: gal (Step | 1.10.6) 1.10.13) |
| □ 1.10.21 | Calculate NCDT Leakage Rate: | |
| F | inal Volume (Step 1.10.20) Initial Volume (Step 1.10.20) = Stop Time (Step 1.10.8) Start Time (Step 1.10.1) | gpm |
| □ 1.10.22 | Record the following: | |
| | NC Sample Purge Flow value recorded in Autolog Any quantified (measured) leakage that has been i | ;: gpm dentified: gpm |
| □ 1.10.23 | Calculate Total Background Leakage: | |
| | $\frac{1}{\text{NC Purge (Step 1.10.22)}} + \frac{1}{\text{Quantified (Step 1.10.22)}} = gpm$ | |
| | Calculate Identified Leakage: | |
| PRT Leakage Rate (Step 1.10.1 | + + = 9) NCDT Leakage Rate (Step 1.10.21) Background Leakage (Step 1.10.23) | gpm ² (< 10 gpm) |
| □ 1.10.25 | Calculate Unidentified Leakage: | |
| Total Leakage (S | tep 1.10.17) Identified Leakage (Step 1.10.24) | _ gpm ² (< 1 gpm) |
| □ 1.10.26 | Determine Total NC Pump #1 Seal Leakoff flow: | |
| | NC Pump 1B #1 Seal Leakoff Flow + NC Pump 1C #1 Seal Leakoff Flow + NC Pump 1D #1 Seal Leakoff Flow + | $gpm^{2}(< 4.0 gpm)$ $gpm^{2}(< 4.0 gpm)$ $gpm^{2}(< 4.0 gpm)$ $gpm^{2}(< 4.0 gpm)$ $gpm^{2}(< 16.3 gpm)$ |

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² Acceptance Criteria Value

Unit 1

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Enclosure 13.2

NC Leakage Determination Using Manual Calculations

| | | | Calculations |
|---------------------|------------------|---|---|
| NOTE: | "0" shou | ld be entered | below for any negative identified or unidentified value. |
| | 1.10.27 | Calculate " | Fotal Accumulative Leakage": |
| Identified (Step 1. | + 10.24) Unio | dentified (Step 1.10 | + = gpm ³ (< 20 gpm) 25) Total NC Seal Leakoff (Step 1.10.26) Total Accumulative Leakage |
| 1.11 | Determin | e Primary to | Secondary Leakage by performing the following: |
| | 1.11.1 | IF in Mode following: | 1 AND greater than or equal to 40% RTP, record indication on the |
| | | 1EMF7 1EMF72 1EMF72 1EMF74 | 2: gpd 3: gpd |
| | | 1.11.1.1 | IF any N-16 EMF inoperable, perform the following: |
| | | | A. Notify Secondary Chemistry to provide Primary to Secondary leakage. <u>Person Notified</u> / <u>Date Time</u> |
| | | | Person Notified Date Time |
| | | | B. Record Primary to Secondary leakage as determined by Secondary Chemistry: gpd ³ |
| | | | C. Record date and time Primary to Secondary leakage was determined (provided by Secondary Chemistry): // |
| 1 | .11.2 | IF in Mode | Date Time 1 <u>AND</u> less than 40% RTP, perform the following: |
| . Nast | | 1.11.2.1 | Notify Secondary Chemistry to provide Primary to Secondary leakage. |
| | | | Person Notified / Date Time |

³ This value is a total primary to secondary leakage of all four S/Gs. A value of less than or equal to 135 gpd conservatively implies leakage through any one S/G is less than or equal to 135 gpd.

| | Enclosure 13.2 PT/1/A/4150/001 |
|--------------------------|---|
| NC | C Leakage Determination Using Manual Page 7 of 10 Calculations |
| □ 1.11.2.2 | Record Primary to Secondary leakage as determined by Secondary Chemistry: gpd ⁴ |
| □ 1.11.2.3 | Record date and time Primary to Secondary leakage was determined (provided by Secondary Chemistry): |
| | / Date Time |
| 1.11.3 <u>IF</u> in Mc | odes 2, 3 or 4, perform the following: |
| 1.11.3.1 | Notify Secondary Chemistry to provide Primary to Secondary leakage via grab sample. |
| | Person Notified / Date Time |
| | Person Notified Date Time |
| | |
| □ 1.11.3.2 | Record Primary to Secondary leakage as determined by Secondary Chemistry grab sample: gpd ⁴ |
| □ 1.11.3.2 □ 1.11.3.3 | |
| | Secondary Chemistry grab sample: gpd ⁴ Record date and time Primary to Secondary leakage was determined (provided by Secondary Chemistry): |
| | Secondary Chemistry grab sample: gpd ⁴ Record date and time Primary to Secondary leakage was |
| □ 1.11.3.3 | Secondary Chemistry grab sample: gpd ⁴ Record date and time Primary to Secondary leakage was determined (provided by Secondary Chemistry): |

⁴ This value is a total primary to secondary leakage of all four S/Gs. A value of less than or equal to 135 gpd conservatively implies leakage through any one S/G is less than or equal to 135 gpd.

NC Leakage Determination Using Manual Calculations

 \Box 1.12 In Autolog, perform the following:

| I | | |
|-------|--------------------------|---|
| NOTE: | • Calcu be ide | ulations run during power escalation <u>AND</u> other than Mode 1 calculations should entified as such. |
| | • The f opera | irst calculation is considered the first calculation after 18:00 hrs for normal tion. |
| | 1.12.1 | Enter the following values with any pertinent comments: |
| | | "IDENTIFIED" leakage (Step 1.10.24) "UNIDENTIFIED" leakage (Step 1.10.25) "TOTAL NC PUMPS #1 SEAL LEAKOFF" leakage (Step 1.10.26) "TOTAL" leakage (Step 1.10.27) "CALCULATION START TIME" Primary to Secondary leakage |
| | _ 1.12.2 | \underline{IF} other than the first calculation for the day, record reason and any pertinent comments. |
| NOTE: | Unidentif Calculation | fied Leakage values are expected to be within ± 0.5 gpm for Manual ons. Exceeding ± 0.5 gpm does NOT invalidate leakage calculation. |
| 1.13 | IF unide | ntified leakage NOT between +0.5 gpm, notify Primary System Engineer |

gp uly Prima System Engineer. цу

Person Notified

Date Time

Enclosure 13.2

NC Leakage Determination Using Manual Calculations

- 1.14 Evaluate Acceptance Criteria per one of the following:
 - □ 1.14.1 Check Acceptance Criteria specified in Section 11 met.

OR

- 1.14.2 IF Acceptance Criteria specified in Section 11 NOT met, perform the following:
 - Image: 1.14.2.1Log applicable Tech Spec or SLC. {PIP M-07-00393}Image: 1.14.2.2Image: 1.14.2.2Image: SROImage: 1.14.2.2Image: SRO
 - <u>IIF</u> Total Accumulative Leakage is greater than 20 gpm <u>OR</u> Total NC Pumps #1 Seal Leakoff greater than 16.3 gpm, notify Security of degraded SSF capabilities.

/ Date Time Person Notified

- 1.14.2.4IF any NC Pump #1 Seal Leakoff has a sustained value of greater
than OR equal to 4.0 gpm, notify SSS Engineer and Security of
degraded SSF capability.
 - Person Notified / Date Time
- 1.15 **IF** this is the second Leakage Calculation and elevated leakage is indicated, evaluate performing PT/1/A/4150/001 D (Identifying NC System Leakage).
- 1.16 Lower NCDT level less than 48%.
- 1.17 Close 1WL-23 (NCDT Level Control).
- 1.18 Place "1WL-23 Mode Select" to "AUTO".

| | Enclosure 13.2 | PT/ 1 /A/4150/001 B |
|------|---|----------------------------|
| | NC Leakage Determination Using Manual Calculations | Page 10 of 10 |
| 1.19 | Notify Radwaste Chemistry of the following: | |
| | □ NC System leakage calculation is complete | |
| | □ PRT, NCDT and VCT sampling or venting may be initiated | {PIPM-00-0615} |
| | Person Notified / Date Time | |
| 1.20 | Notify Primary Chemistry of the following: | |
| | □ NC System leakage calculation is complete | |
| | □ NC System sampling may be initiated | |
| 1.21 | IF Unit 1 at 100% RTP AND OAC is available, perform Enclose | ure 13.5 (Evaluation of |
| | NC System Unidentified Leakage Results). | |

End of Enclosure

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Enclosure 13.3 NCDT Volume

PT/**1**/A/4150/001 B Page 1 of 1

| NCDT LEVEL % | NCDT VOLUME (Gal) | NCDT LEVEL % | NCDT VOLUME (Gal) | NCDT LEVEL % | NCDT VOLUME (Gal) |
|--------------|----------------------|--------------|----------------------|--------------|----------------------|
| 0 | 19.7 | 35 | 123.1 | | 247.3 |
| 1 | 21.9 | 36 | 126.6 | 71 | 250.7 |
| 2 | 24.1 | 37 | 130.1 | 72 | 254.0 |
| 3 | 26.4 | 38 | 133.6 | 73 | 257.3 |
| 4 | 28.8 | 39 | 137.1 | 74 | 260.6 |
| 5 | 31.2 | 40 | 140.7 | 75 | 263.9 |
| 6 | - 33.7 | 41 | 144.3 | 76 | 267.2 |
| 7 | 36.2 | 42 | 147.8 | 77 | 270.4 |
| 8 | 38.8 | 43 | 151.4 | 78 | 273.6 |
| 9 | 41.4 | 44 | 155.0 | 79 | 276.8 |
| 10 | 44.1 | 45 | 158.6 | 80 | 279.9 |
| 11 | 46.9 | 46 | 162.2 | 81 | 283.0 |
| 12 | 49.6 | 47 | 165.8 | 82 | 286.1 |
| 13 | 52.5 | 48 | 169.4 | 83 | 289.1 |
| 14 | 55.3 | 49 | 173.0 | 84 | 292.1 |
| 15 | 58.2 | 50 | 176.6 | 85 | 295.1 |
| 16 | 61.2 | 51 | 180.2 | 86 | 298.0 |
| 17 | 64.2 | 52 | 183.8 | 87 | 300.9 |
| 18 | 67.2 | 53 | 187.5 | 88 | 303.8 |
| 19 | 70.3 | 54 | 191.1 | 89 | 306.6 |
| 20 | 73.4 | 55. | 194.7 | 90 | 309.4 |
| 21 | 76.5 | 56 | 198.2 | 91 | 312.1 |
| 22 | 79.6 | - 57 | 201.8 | 92 | 314.7 |
| 23 | 82.8 | 58 | 205.4 | 93 | 317.4 |
| 24 | 86.0 | 59. | 209.0 | 94 | 319.9 |
| 25 | 89.3 | 60 | 212.5 | 95 | 322.4 |
| 26 | 92.6 | 61 | 216.1 | 96 | 324.9 |
| 27 | 95.9 | 62 | 219.6 | 97 | 327.3 |
| 28 | 99.2 | 63 | 223.1 | 98 | 329.6 |
| 29 | 102.5 | 64 | 226.6 | 99 | 331.9 |
| 30 | 105.9 | 65 | 230.1 | 100 | 334.0 |
| 31 | 109.3 | 66 | 233.6 | | |
| 32 | 112.7 | 67 | 237.0 | | |
| 33 | 116.2 | -68 | 240.5 | | |
| 34 | 119.6 | 69 | 243.9 | | |

End of Enclosure

Enclosure 13.4 PRT Volume

PT/**1**/A/4150/001 B Page 1 of 1

| PRT LEVEL % | PRT VOLUME (Gal) | PRT LEVEL % | PRT VOLUME (Gal) | PRT LEVEL % | PRT VOLUME (Gal) |
|-------------|---------------------|-------------|---------------------|-------------|---------------------|
| 0 | 303.2 | 35 | 4472.0 | 70 | 9799.8 |
| 1 | 371.9 | 36 | 4621.5 | 71 | 9942.5 |
| 2 | 445.6 | 37 | 4771.8 | 72 | 10084.0 |
| 3 | 523.9 | 38 | 4922.8 | 73 | 10224.1 |
| 4 | 606.7 | 39 | 5074.6 | 74 | 10362.9 |
| 5 | 693.6 | 40 | 5227.0 | 75 | 10500.3 |
| . 6 | 784.5 | 41 | 5379.9 | 76 | 10636.1 |
| 7 | 879.0 | 42 | 5533.4 | 77 | 10770.4 |
| 8 | 977.0 | 43 | 5687.3 | 78 | 10903.1 |
| 9 | 1078.3 | 44 | 5841.7 | 79 | 11034.1 |
| 10 | 1182.7 | 45 | 5996.4 | 80 | 11163.3 |
| 11 | 1290.0 | 46 | 6151.4 | 81 | 11290.6 |
| 12 | 1400.2 | 47 | 6306.6 | 82 | 11416.0 |
| 13 | 1513.0 | 48 | 6461.9 | 83 | 11539.3 |
| 14 | 1628.4 | 49 | 6617.4 | 84 | 11660.6 |
| 15 | 1746.2 | 50 | 6772.9 | 85 | 11779.6 |
| 16 | 1866.2 | 51 | 6928.4 | 86 | 11896.2 |
| 17 | 1988.5 | 52 | 7083.8 | 87 | 12010.4 |
| 18 | 2112.9 | 53 | 7239.0 | 88 | 12122.0 |
| 19 | 2239.2 | 54 | 7394.1 | 89 | 12231.0 |
| 20 | 2367.5 | 55 | 7548.9 | 90 | 12337.0 |
| 21 | 2497.6 | 56 | 7703.4 | 91 | 12440.0 |
| 22 | -2629.4 | 57 · · · | 7857.5 | 92 | 12539.9 |
| 23 | 2763.0 | 58 | 8011.2 | 93 | 12636.3 |
| 24 | 2898.1 | 59 | 8164.3 | 94 | 12729.2 |
| 25 | 3034.8 | 60 | 8316.9 | 95 | 12818.3 |
| 26 | 3172.9 | 61 | 8468.9 | 96 | 12903.4 |
| 27 | 3312.4 | 62 | 8620.3 | 97 | 12984.2 |
| 28 | 3453.3 | 63 | 8770.9 | 98 | 13060.5 |
| 29 | 3595.5 | 64 | 8920.7 | 99 | 13132.0 |
| 30 | 3738.9 | 65 | 9069.6 | 100 | 13198.3 |
| 31 | 3883.4 | 66 | 9217.7 | | |
| 32 | 4029.1 | 67 | 9364.8 | | |
| 33 | 4175.7 | 68 - | 9510.9 | | |
| 34 | 4323.4 | 69 | 9655.9 | | |

End of Enclosure

JPM A3 RO/SRO

2010 Admin - JPM A3 RO/SRO

NUREG 1021, Revision 9

| Appendix C | Page 2 d | | Form ES-C-1 |
|---------------------|---|---------------------|------------------------------------|
| , ipperion e | Job Performance Me | | |
| | | | |
| Facility: | McGuire | Task No.: | |
| Task Title: | Perform a Unit Vent Flow Calculation of a Containment Air Release | | <u>n 2010 Admin -</u> A3 RO/SRO |
| K/A Reference: | GK/A 2.3.11 (3.8/3.8) | | |
| Examinee: | | NRC Examiner: | |
| Facility Evaluator: | | Date: | |
| Method of testing: | | | |
| Simulated Perform | ance: | Actual Performance: | X |
| Classr | oom <u>X</u> Simulator | _ Plant | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | GWR Package # 2010013 for Unit 1 Containment Air Release is currently in use to conduct a series of Containment air releases. |
|---------------------|---|
| | During the first release, conducted using Enclosure 4.2 (Air Release Mode With VQ Flow Monitor Operable) of OP/1/A/6450/017 (Containment Air Addition and Release), the Unit 1 VQ Monitor became inoperable. |
| | The crew stopped the release and continued the air release using Enclosure 4.3 (Air Release Mode with VQ Flow Monitor Inoperable) of OP/1/A/6450/017 (Containment Air Addition and Release). |
| | Three previous releases have been made; including the one which was made with the Unit 1 VQ Flow Monitor in operation. |
| | At 1743 on 8/4/10, containment pressure was 0.17 PSIG and a VQ release was initiated to reduce pressure to 0.12 PSIG per Step 3.8 of Enclosure 4.3. |
| | This release was secured at 1839 on 8/4/10 and the procedure was completed through step 3.7.1 for this release. |
| | RP has requested that the current GWR paperwork be closed out after the on-going release. |

| Appendix C | Page 3 of 11 | Form ES-C-1 |
|---------------------|--|-------------------------|
| | Job Performance Measure Worksheet | |
| Task Standard: | The operator will calculate the volume of air relea Containment during the final release, and determ air released in the series of four releases in accor provided KEY. | ine the total volume of |
| Required Materials: | Calculator | |
| General References: | OP/1/A/6450/017 (Containment Air Addition and I | Release) |

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| Appendix C | Page 4 of 11 Form ES- | -C- |
|------------|--|-----|
| | Job Performance Measure Worksheet | |
| Handouts: | Handout #1 - Enclosure 4.2 (Air Release Mode With VQ Flow Monit Operable) of OP/1/A/6450/017 (Containment Air Addition and Releas marked up as follows: | |
| | Step 2.1 – Initialed. | |
| | Step 2.2 – Initialed. | |
| | Step 2.3 – Initialed. | |
| | Step 2.4 – Initialed, GWR# 2010013 recorded. | |
| | Step 3.1 – Checkbox is checked and Initialed. | |
| | Step 3.2 – Initialed. | |
| | Step 3.2.1 – Initialed and CV initialed. | |
| | Step 3.2.2 – Initialed and CV initialed. | |
| | Step 3.2.3 – Initialed and Mike Cline /Date/Time Recorded consisten with first release Date/Time (8/4/10 0903). | t |
| | Step 3.3 – Initialed. | |
| | Step 3.3.1 – Initialed. | |
| | Step 3.3.2 – Checkbox is checked and Initialed. | |
| | Step 3.4 – Initialed and CV initialed. | |
| | Step 3.5 – Initialed. | |
| | Step 3.6 – Initialed. | |
| | Step 3.7 – Initialed. | |
| | Step 3.7.1 – Checkbox is checked and Initialed. | |
| | Step 3.7.2 – Checkbox is checked and Initialed. | |
| | Step 3.7.3 – Initialed and CV initialed, VQ Monitor flow is recorded as 1594, and Actual Volume Released is recorded as 15,940. | 5 |
| | Step 3.7.4 – Initialed. | |
| | Step 3.7.5 – Checkbox is checked and Initialed. | |
| | Step 3.8.1 – Checkbox is checked and Initialed. | |
| | Step 3.8.2 – Checkbox is checked and Initialed. | |
| | Step 3.8.3 – Checkbox is checked and Initialed. | |
| | Step 3.8.4 – Checkbox is checked and Initialed. | |
| | Step 3.8.5 – Both Checkbox' are checked and Initialed. | |
| | Step 3.8.6 – Initialed. | |
| | Step 3.9 – Initialed. | |

Page 5 of 11 Job Performance Measure Worksheet

Page 5 of 5 (Attachment 1) is marked up as follows: Sheet 1 of 1

| 1VQ-2B Open | | | | 1VQ-2B Closed | | |
|-------------|---------|---------------------------------------|-------------|---------------|---------|-------------|
| Doer | CV | VQ Flow Monitor Counting (√) | Date/Time | Doer | CV | Date/Time |
| Initial | Initial | | 8/4/10 0903 | Initial | Initial | 8/4/10 1016 |

Handout #2 - Enclosure 4.3 (Air Release Mode With VQ Flow Monitor Inoperable) of OP/1/A/6450/017 (Containment Air Addition and Release) marked up as follows:

- Step 2.1 Initialed.
- Step 2.2 Initialed.
- Step 2.3 Initialed.
- Step 2.4 Initialed, GWR# 2010013 recorded.
- Step 3.1 Checkbox is checked and Initialed.
- Step 3.2 Initialed.
- Step 3.2.1 Initialed and CV initialed.
- Step 3.2.2 Initialed and CV initialed.
- Step 3.2.3 Initialed and Person Notified/Date/Time Recorded consistent with <u>first</u> release Date/Time on Page 6 of 6.
- Step 3.3 Initialed.
- Step 3.4 Initialed and CV initialed.
- Step 3.5.1 Checkbox is checked and Initialed.
- Step 3.5.2 Checkbox is checked and Initialed.
- Step 3.5.3 Checkbox is checked and Initialed.
- Step 3.5.4 Both Checkbox' are checked and Initialed.
- Step 3.5.5 Checkbox is checked and Initialed.
- Step 3.5.6 Initialed.
- Step 3.6 NA and Initialed.
- Step 3.7 Initialed.
- Step 3.7.1 Checkbox is triple-checked and Initialed.
- Step 3.7.2-3 Checkbox is double-checked and Initialed.
- Step 3.8 Initialed.
- Step 3.9.1 through 3.9.3 Initialed.

Page 6 of 11

Job Performance Measure Worksheet

| 1VQ-2B Open | | | | 1VQ-2B Closed | | | | | |
|-------------|---------|-------------|-----------------------------|---------------|---------|-------------|----------------------------|-----------------------------|-----------------------------------|
| Doer | cv | Date/Time | Start Pressure (psig) | Doer | CV | Date/Time | Stop Pressure (psig) | Ft ³ Released | Total Ft ³ Released |
| Initial | Initial | 8/4/10 1117 | 0.21 | Initial | Initial | 8/4/10 1258 | 0.12 | 21,469.28 | 21,469.28 |
| Initial | Initial | 8/4/10 1432 | 0.19 | Initial | Initial | 8/4/10 1547 | 0.12 | 15,534.63 | 37,003.91 |
| Initial | Initial | 8/4/10 1743 | 0.17 | Initial | Initial | | 0.12 | | |

Page 6 of 6 (Attachment 1) is marked as follows: Sheet 1 of 1

Initiating Cue:You have been directed to calculate the volume released for this release
and complete all required paperwork starting with Step 3.7.2, AND,
since this is the last release perform Steps 3.9.4 through 3.9.8 of
Enclosure 4.3 to determine the total volume released from the
Containment.The CRS notified RP (Mike Cline) at 1840 on 8/4/10 that the release has
been terminated.
Complete all required paperwork.

Time Critical Task: NO

Validation Time: 15 minutes

Page 7 of 11 PERFORMANCE INFORMATION

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue (Last Page of this JPM), and Handouts #1 and #2.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|--|-----|-----------------------------------|
| 1 | (Enclosure 4.3, Step 3.7.2) Record stop date/time on Attachment 1 | The operator records <u>8/4/10</u> <u>1839</u> in the 1VQ-2B Closed Date/Time Block of Attachment 1. | | |
| 2 | (Step 3.7.3) Calculate volume released using the following and record on Attachment 1. | The operator uses Table 1 of Enclosure 4.3 and determines X to be <u>10.51</u> (Start Pressure of 0.17). | | |
| | Cu. Ft. Released = X + (YxZ) Where: | The operator uses Table 1 of Enclosure 4.3 and determines Y to be <u>201.1</u> (Start Pressure of 0.17). | | |
| | X and Y are from Table 1 Z is actual release duration in minutes from Attachment 1. | The operator uses Attachment 1 of Enclosure 4.3 and determines Z to be <u>56</u> (Stop Time of 1839 - Start Time of 1743). | | |
| | | The operator calculates volume released as follows: | | |
| * | | 10.51 + (201.1 x 56) = <u>11,272.11±1% (See KEY)</u> , and records this value in the 1VQ-2B Closed Cubic Ft Released Block of Attachment 1. | | |
| 3 | (Step 3.9.4) Ensure release stop date/time recorded on Attachment 1. | The operator ensures <u>8/4/10 1839</u> recorded in the 1VQ-2B Closed Date/Time Block of Attachment 1. | | |
| 4 | (Step 3.9.5) Notify RP that release has been terminated | The operator recognizes from the initial conditions that RP has been notified. | | |

Page 8 of 11 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|--|-----|-----------------------------------|
| 5 | (Step 3.9.6) Determine Total Cu. Ft Released on Attachment 1. | The operator adds the volume of this most recent release (11,272.11) to the total previously released on Attachment 1 (37,003.91) and determines that the total volume released is $\frac{48,276.02 \text{ ft}^3 \pm 1\%}{\text{KEY}}$. | | |
| | | The operator records this value in the 1VQ-2B Closed Total Cubic Ft Released Block of Attachment 1. | | |
| 6 | (Step 3.9.7) Record Total Cu. Ft Released from Attachment 1:ft ³ | The operator records <u>48,276.02</u> in the 1VQ-2B Closed Cubic Ft Released Block of Attachment 1. | | |
| 7 | (Step 3.9.8) IF Enclosure 4.2 (Air Release Mode With VQ Flow Monitor Operable) was used during this release, perform the following: (Step 3.9.8.1) Record Actual Volume Released from Enclosure 4.2, Step 3.7.3ft ³ (Step 3.9.8.2) Calculate Total Volume Released as follows: ft ³ +ft ³ =ft ³ Step 3.10.7 Step 3.10.8.1 Total Vol Rel | The operator observes Step 3.7.3 of Enclosure 4.2 and determines that $15,940$ ft ³ had been released when the VQ Monitor was operable, and records this value on Enclosure 4.3, Step 3.9.8.1. The operator adds the total volume released recorded in Step 3.9.7 ($48,276.02$) and the total volume released recorded in Step 3.9.8.1 ($15,940$), and determines the Total Volume Released for this series of Containment Air Releases is $64,216.02$ ft ³ $\pm 1\%$ (See KEY). | | |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

2010 Admin - JPM A3 RO/SRO

| Appendix C | Ap | penc | lix | С |
|------------|----|------|-----|---|
|------------|----|------|-----|---|

Page 9 of 11 VERIFICATION OF COMPLETION

| Job Performance Measure No.: | 2010 Admin - JPM A3 RO/SRO |
|------------------------------|----------------------------|
| Examinee's Name: | |
| Date Performed: | |
| Facility Evaluator: | |
| Number of Attempts: | |
| Time to Complete: | |
| Question Documentation: | |
| | |
| | |

| Result: | SAT | UNSAT | ····· |
|-----------------------|-----|-------|-------|
| | | | |
| | | | |
| Examiner's Signature: | | | Date: |

Page 10 of 11 VERIFICATION OF COMPLETION

KEY:

Enclosure 4.3, Attachment 1:

RED = filled in at start of JPM. GREEN = filled in during JPM performance

| 1VQ-2B Open | | | | 1VQ-2B Closed | | | | | | |
|-------------|---------|-------------|-----------------------------|---------------|---------|-------------|----------------------------|-----------------------------|-----------------------------------|--|
| Doer | cv | Date/Time | Start Pressure (psig) | Doer | cv | Date/Time | Stop Pressure (psig) | Ft ³ Released | Total Ft ³ Released | |
| Initial | Initial | 8/4/10 1117 | 0.21 | Initial | Initial | 8/4/10 1258 | 0.12 | 21,469,28 | 21,469,28 | |
| Initial | Initial | 8/4/10 1432 | 0.19 | Initial | Initial | 8/4/10 1547 | 0.12 | 15,534.63 | 37.003.91 | |
| Initial | Initial | 8/4/10 1743 | 0.17 | Initial | Initial | 8/4/10 1839 | 0.12 | 11,272.11 | 48,276.02 | |

Enclosure 4.3, Step 3.7.3 (JPM Step 2): Volume released, current release: $10.51 \text{ ft}^3 + (201.1 \text{ ft}^3/\text{min x 56 min}) = 11,272.11 \text{ ft}^3$

Enclosure 4.3, Step 3.9.7 (JPM Step 3): Total Volume released, during performance of Enclosure 4.3:

11,272.11 ft³ + 37,003.91 ft³ = 48,276.02 \pm 1% ft³ (47,793.26 - 48758.78)

Enclosure 4.3, Step 3.9.8.2 (JPM Step 5): Total Volume released, during performance of GW Permit: 48,276.02 ft³ + 15940 ft³ = 64,216.02 \pm 1% ft³ (63,573.86 - 64,858.18)

INITIAL CONDITIONS: GWR Package # 2010013 for Unit 1 Containment Air Release is currently in use to conduct a series of Containment air releases.

During the first release, conducted using Enclosure 4.2 (Air Release Mode With VQ Flow Monitor Operable) of OP/1/A/6450/017 (Containment Air Addition and Release), the Unit 1 VQ Monitor became inoperable.

The crew stopped the release and continued the air release using Enclosure 4.3 (Air Release Mode with VQ Flow Monitor Inoperable) of OP/1/A/6450/017 (Containment Air Addition and Release).

Three previous releases have been made; including the one which was made with the Unit 1 VQ Flow Monitor in operation.

At 1743 on 8/4/10, containment pressure was 0.17 PSIG and a VQ release was initiated to reduce pressure to 0.12 PSIG per Step 3.8 of Enclosure 4.3.

This release was secured at 1839 on 8/4/10 and the procedure was completed through step 3.7.1 for this release.

RP has requested that the current GWR paperwork be closed out after the on-going release.

INITIATING CUE:

You have been directed to calculate the volume released for this release and complete all required paperwork starting with Step 3.7.2, <u>AND</u>, since this is the last release perform Steps 3.9.4 through 3.9.8 of Enclosure 4.3 to determine the total volume released from the Containment.

The CRS notified RP (Mike Cline) at 1840 on 8/4/10 that the release has been terminated.

Complete all required paperwork.

Air Release Mode With VQ Flow Monitor Operable

1. Limits and Precautions

- $\sqrt{1.1}$ Containment Pressure Tech Spec limit is ± 0.3 psig.
- $\sqrt{1.2}$ All Engineered Safeguards Valves shall be cycled electrically after any manual operation.

2. Initial Conditions

- <u>SLM</u> 2.1 Per Tech Spec 3.9.4, movement of recently irradiated fuel assemblies within Containment, is <u>NOT</u> in progress. {PIP M-05-1608, PIP M-07-0033, CAPR}
- SLM 2.2 VQ Flow Monitor is operable.
- <u>SLM</u> 2.3 Containment pressure requires an air release.
- SLM 2.4 GWR # 2010013 has been issued.

3. Procedure

- ☑ 3.1 Evaluate all outstanding R&Rs that may impact performance of this procedure.
- SIM 3.2 IF 1EMF-39L monitoring release, perform the following:
- Fok SLM 3.2.1 Ensure 1EMF-39L Trip 1 setpoint set per GWR.
- FBK 3.2.2 Ensure 1EMF-39L Trip 2 setpoint set per GWR.
 - 3.2.3 Notify RP to update 1EMF-39L setpoints in EMF Setpoint Log.

| Mike Cline | 8/4/10 | / <u>090</u> 3 |
|-----------------|--------|----------------|
| Person Notified | Date | Time |

- <u>4</u>M 3.3 <u>IF</u> this is initial release <u>OR</u> directed to this enclosure from Enclosure 4.3, (Air Release Mode With VQ Flow Monitor Inoperable), perform the following:
 - **£**M 3.3.1 Reset VQ Flow Monitor.
 - \blacksquare 3.3.2 Record Release start date and time on GWR paperwork.
- FBK 3.4 Throttle 1VQ-4 (VQ To Unit Vent Control) 15% open.
 - SIM 3.5 Ensure 1VQ-2B (Cont Air Rel Outside Isol) closed.
 - 3.6 Open 1VQ-1A (Cont Air Rel Inside Isol).

OP/**1**/A/6450/017 Page 2 of 5

Air Release Mode With VQ Flow Monitor Operable

- <u>SEM</u> 3.7 <u>IF AT ANY TIME VQ</u> Flow Monitor stops counting <u>OR</u> becomes inoperable, perform the following:
 - ☑ 3.7.1 Ensure 1VQ-2B (Cont Air Rel Outside Isol) closed per Attachment 1.
 - \checkmark 3.7.2 Ensure release stop date / time recorded on Attachment 1.
- FbK 54 3.7.3 Record VQ Flow Monitor actual volume released as follows: {PIP 05-5685}

 $\frac{1594}{\text{VQ Flow Monitor}} \ge 10 = \frac{15,940}{\text{Actual Volume Released}} \text{ft}$

- 54 3.7.4 Reset VQ Flow Monitor.
 - ☑ 3.7.5 Exit this enclosure and go to Enclosure 4.3 (Air Release Mode With VQ Flow Monitor Inoperable).
- 3.8 Start initial VQ release as follows:
 - ☑ 3.8.1 Open 1VQ-2B (Cont Air Rel Outside Isol) per Attachment 1.
 - ☑ 3.8.2 Maintain a release rate less than 300 cfm by throttling 1VQ-4 (VQ To Unit Vent Control).
 - \checkmark 3.8.3 Record that VQ Flow Monitor is counting on Attachment 1.
 - ☑ 3.8.4 Record start date / time on Attachment 1.
 - 3.8.5 Record the following in Auto Log:
 - Release number
 - Start time
- 5LM 3.8.6 Ensure "Release Initiation" on GWR is completed.
- 3.9 To secure release, close 1VQ-2B (Cont Air Rel Outside Isol) per Attachment 1.
- 3.10 **IF AT ANY TIME** it is desired to throttle 1VQ-4 (VQ To Unit Vent Control) in subsequent releases, maintain release rate less than 300 cfm.
- 3.11 <u>IF</u> subsequent releases with existing GWR are required, maintain containment pressure less than 0.20 psig per Attachment 1.

Air Release Mode With VQ Flow Monitor Operable

- 3.12 **IF** desired to close out existing GWR, perform the following:
 - 3.12.1 Close 1VQ-1A (Cont Air Rel Inside Isol).
- _____ 3.12.2 Close 1VQ-4 (VQ To Unit Vent Control).

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C٧

- _____ 3.12.3 Ensure 1VQ-2B (Cont Air Rel Outside Isol) closed per Attachment 1.
 - 3.12.4 Ensure release stop date / time recorded on Attachment 1.
 - _____ 3.12.5 Notify RP that VQ release has been terminated and 1EMF-38, 1EMF-39, and 1EMF-40 setpoints need to be evaluated. {PIP 1-M97-1925}

| | Person Not | ified | <u>Da</u> | / te Time | | | |
|--------|------------|-------------------------------------|----------------------------|---------------|----------------------|------------------|-----------------|
| 3.12.6 | Record VQ | Flow Monitor | total vol | ume release | d as fol | lows: {PIP 05- | 5685} |
| | | x 10 = | | | ft ³ | | |
| | VQ Flow M | Monitor | Total V | olume Relea | sed | | |
| 3.12.7 | | re 4.3 (Air Rele this release, p | | | | Ionitor Inoperat | ole) was |
| | 3.12.7.1 | Record "Tota Attachment 1 | | Released" fro | om Encl | osure 4.3, | |
| | | | ft ³ | | | | |
| | 3.12.7.2 | Calculate Tot | al Volun | ne Released | as follo | ws: | |
| | | Step 3.12.6 | $_{-}$ ft ³ + _ | Step 3.12.7. | -1 ft ³ = | Total Vol Rel | ft ³ |

s:

Air Release Mode With VQ Flow Monitor Operable

| 3.12.8 | Record the following in Auto Log: |
|-------------|---|
| | Release number Stop time Volume released |
| □ 3.12.9 | Record release stop date / time on GWR. |
| □ 3.12.10 | Record and CV "Total Vol. Rel." on GWR. (Step 3.12.6 or Step 3.12.7.2) {PIP 05-5685} |
| 3.12.11 | Ensure "Release Completion" on GWR is completed. |
| □ 3.12.12 | Route GWR to SRO. |
| 3.12.13 | Reset VQ Flow Monitor. |

OP/**1**/A/6450/017 Page 5 of 5

Air Release Mode With VQ Flow Monitor Operable

Attachment 1

5? L

Sheet 1 of 1

| | | 1VQ-2B O | pen | | 1V0 | Q-2B Closed |
|------|---------------------------------------|---------------------------------------|---------------|---------------------------------------|-----|---------------|
| Doer | CV | VQ Flow Monitor Counting (√) | Date/Time | Doer | CV | Date/Time |
| SLM | FBK | √ | 8/4/10 / 0903 | FAR | SLM | 8/4/10 / 1016 |
| | | | | | | |
| | | | | | | |
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End of Enclosure

Air Release Mode With VQ Flow Monitor Inoperable

1. Limits and Precautions

- $\sqrt{1.1}$ Containment Pressure Tech Spec limit is ± 0.3 psig.
- $\sqrt{1.2}$ All Engineered Safeguards Valves shall be cycled electrically after any manual operation.

2. Initial Conditions

- <u>SLM</u> 2.1 Per Tech Spec 3.9.4, movement of recently irradiated fuel assemblies within Containment, is <u>NOT</u> in progress. {PIP M-05-1608, PIP M-07-0033, CAPR}
- SLM 2.2 VQ Flow Monitor is inoperable.
- **SLM** 2.3 Containment pressure requires an air release.
- SLM 2.4 GWR # 2010013 has been issued.

3. Procedure

CV

- \checkmark 3.1 Evaluate all outstanding R&Rs that may impact performance of this procedure.
- **SLM** 3.2 **IF** 1EMF-39L monitoring release, perform the following:
- FBK <u>SLM</u> 3.2.1 Ensure 1EMF-39L Trip 1 setpoint set per GWR.
- FOR SLM 3.2.2 Ensure 1EMF-39L Trip 2 setpoint set per GWR.
 - Sim 3.2.3 Notify RP to update 1EMF-39L setpoints in EMF Setpoint Log.

| Mike Cline | 8/4/10 | 1115 |
|-----------------|--------|------|
| Person Notified | Date | Time |

SLM 3.3 Open 1VQ-1A (Cont Air Rel Inside Isol).

NOTE: V 1VQ-4 (VQ To Unit Vent Control) is required to be in full open position for air releases with VQ Flow Monitor inoperable.

FBK SLM 3.4 Fully open 1VQ-4 (VQ To Unit Vent Control).

CV

Air Release Mode With VQ Flow Monitor Inoperable

3.5 Start initial VQ release as follows:

9

CV

- ☑ 3.5.1 Open 1VQ-2B (Cont Air Rel Outside Isol) per Attachment 1.
- ☑ 3.5.2 Record start date / time on Attachment 1.
- ☑ 3.5.3 Record start pressure on Attachment 1.
 - 3.5.4 Record the following in Auto Log:
 - ☑ Release number☑ Start time
- ☑ 3.5.5 Record release start date / time on GWR.
- 5. M 3.5.6 Ensure "Release Initiation" on GWR is completed.

NAME 3.6 IF AT ANY TIME VQ Flow Monitor becomes operable, perform the following:

- 3.6.1 Ensure 1VQ-2B (Cont Air Rel Outside Isol) closed per Attachment 1.
- 3.6.2 Ensure release stop date / time recorded on Attachment 1.
- 3.6.3 Record Total Cu. Ft. Released on Attachment 1. {PIP 05-5685}
 - □ 3.6.4 Exit this enclosure and go to Enclosure 4.2 (Air Release Mode With VQ Flow Monitor Operable).

Air Release Mode With VQ Flow Monitor I Inoperable

- **SLM** 3.7 **HOLD** until containment pressure reaches 0.12 psig, <u>THEN</u> secure VQ release as follows:
 - √ 3.7.1 Close 1VQ-2B (Cont Air Rel Outside Isol) per Attachment 1.
 - $\sqrt{12}$ 3.7.2 Record stop date / time on Attachment 1.
 - $\sqrt{12}$ 3.7.3 Calculate volume released using the following and record on Attachment 1: (Documentation of calculation <u>NOT</u> required)

Cu. Ft. Released = $X + (Y \times Z)$

Where: X and Y are from Table 1 Z is actual release duration in minutes from Attachment 1

 $\underbrace{\text{Table}}_{X \text{ (Table)}} ft^3 + (\underbrace{\text{Table}}_{Y \text{ (Table)}} ft^3 / \min X \underbrace{\text{Table}}_{Z \text{ (Release Duration)}} \min) = \underbrace{\text{min}}_{ft^3} ft^3$

| Table 1 |
|---------|
|---------|

| Start Pressure | Stop Pressure (Always 0.12) | X | Y |
|----------------|--------------------------------|--------------------|------------------------|
| (psig) | (psig) | (ft ³) | (ft ³ /min) |
| 0.12 | 0.12 | 0 | 0 |
| 0.13 | 0.12 | 0 | 188.29 |
| 0.14 | 0.12 | 0.64 | 191.71 |
| 0.15 | 0.12 | 2.39 | 194.98 |
| 0.16 | 0.12 | 5.60 | 198.10 |
| 0.17 | 0.12 | 10.51 | 201.10 |
| 0.18 | 0.12 | 17.31 | 203.99 |
| 0.19 | 0.12 | 26.13 | 206.78 |
| 0.20 | 0.12 | 37.07 | 209.47 |
| 0.21 | 0.12 | 50.21 | 212.07 |
| 0.22 | 0.12 | 65.57 | 214.60 |
| 0.23 | 0.12 | 83.20 | 217.06 |
| 0.24 | 0.12 | 103.09 | 219.44 |

Air Release Mode With VQ Flow Monitor Inoperable

- <u>Sim</u> 3.8 <u>IF</u> subsequent releases required, maintain containment pressure less than 0.20 psig per Attachment 1.
 - 3.9 **IF** it is desired to close out existing GWR, perform the following:
 - <u>sim</u> 3.9.1 Close 1VQ-1A (Cont Air Rel Inside Isol).
- Fok sum 3.9.2 Close 1VQ-4 (VQ To Unit Vent Control).
 - SLM 3.9.3 Ensure 1VQ-2B (Cont Air Rel Outside Isol) closed per Attachment 1.
 - 3.9.4 Ensure release stop date / time recorded on Attachment 1.
 - 3.9.5 Notify RP that VQ release has been terminated and 1EMF-38, 1EMF-39, and 1EMF-40 setpoints need to be evaluated. {PIP 1-M97-1925}

| | Person No | otified Date Time |
|---------|-----------|---|
| □ 3.9.6 | Determine | e Total Cu. Ft Released on Attachment 1. |
| □ 3.9.7 | Record To | otal Cu. Ft Released from Attachment 1: ft ³ |
| 3.9.8 | | sure 4.2 (Air Release Mode With VQ Flow Monitor Operable) was ng this release, perform the following: |
| | □ 3.9.8.1 | Record Actual Volume Released from Enclosure 4.2, Step 3.7.3: |
| | | ft ³ |
| | □ 3.9.8.2 | Calculate Total Volume Released as follows: |

 $\frac{1}{\text{Step 3.9.7}} \frac{\text{ft}^3 + \dots}{\text{Step 3.9.8.1}} \frac{\text{ft}^3 = \dots}{\text{Total Vol Rel}} \frac{\text{ft}^3}{\text{ft}^3}$

Air Release Mode With VQ Flow Monitor Inoperable

| 3.9.9 | Record the following in Auto Log: |
|----------|--|
| | Release number Stop time Volume released |
| □ 3.9.10 | Record release stop date / time on GWR. |
| □ 3.9.11 | Record and CV "Total Vol. Rel." on GWR. (Step 3.9.7 or Step 3.9.8.2) {PIP 05-5685} |
| 3.9.12 | Ensure "Release Completion" on GWR is completed. |
| | |

 \Box 3.9.13 Route GWR to SRO.

OP/**1**/A/6450/017 Page 6 of 6

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Air Release Mode With VQ Flow Monitor Inoperable

Attachment 1

Sheet 1 of 1

| | Total Cubic Ft Released | 21, 4leg.28 | 37,003.91 | | | | | | | | | | | | |
|---------------|--|-------------|--------------|---------------|------|------|------|------|------|------|------|------|------|------|--------------------------|
| | Cubic Ft Released per Step 3.7.3 | 21,469.28 | 15,534.63 | | | | | | | | | | | | Total Cu. Ft Released |
| 1VQ-2B Closed | Stop Pressure (psig) | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | |
| 1 | lime | 1,258 | 1547 | | • | | | | | | | | | | |
| | Date/Time | sjulio / | 8/4/10 /1547 | | | | | | | | | | | | |
| | CV | W7S | W7S | SLM | | | | | | | | | | | |
| | Doer | F&K | FOK | FBX | | | | | | | | | | | |
| | Start Pressure (psig) | 0.31 | 0.19 | 0,17 | | | | | | | | | | | |
| | me | Lm/ | 432 | 1743 | | | | | | | | | | | |
| 1VQ-2B Open | Date/Time | 21/h/8 | | 8/4/10 / 1743 | | | | | | | | | | | |
| IVG | CV | Fak | | | | | | | | | | | | | |
| | Doer | SLM | SLM | SLM | | | | | | | | | | | |

End of Enclosure Unit 1

JPM A4 SRO

2010 Admin - JPM A4 SRO

| Appendix C | Page | 2 of 11 | Form ES-C-1 |
|---------------------|------------------------|-------------------|----------------------------|
| | Job Performance | Measure Worksheet | |
| | | | |
| Facility: | McGuire | Task No.: | |
| Task Title: | Provide an Updated PAR | | 2010 Admin - JPM A4 SRO |
| K/A Reference: | GK/A 2.4.44 (4.4) | | |
| Examinee: | | NRC Examiner: | |
| Facility Evaluator: | | Date: | |
| Method of testing: | | | |
| Simulated Perforn | nance: | Actual Performan | ice: X |
| Class | room X Simulator | Plant | |

READ TO THE EXAMINEE

I will explain the initial conditions, which steps to simulate or discuss, and provide initiating cues. When you complete the task successfully, the objective for this Job Performance Measure will be satisfied.

| Initial Conditions: | A LOCA inside containment has occurred on Unit 1. |
|---------------------|--|
| | The crew implemented EP/1/A/5000/ECA-1.1 (Loss of Emergency Coolant Recirc) due to multiple ECCS component failures. |
| | A Containment Red Path and a Core Cooling Red Path have occurred. |
| | The Emergency Coordinator declared a General Emergency per RP/0/A/5700/000, Enclosure 4.1, EAL # 4.1.G.2 (Loss of Any two Barriers AND Potential loss of the third). |
| | An Emergency Notification Form, along with the initial PAR was sent at the appropriate time. |
| | The following conditions exist 1 hour after the start of the event: |
| | The radioactive release is still on-going. |
| | The wind speed is 9 mph. |
| | The wind direction is 158.9°. |
| | EMF51 A and B reading is 800 R/hr. |
| | A Radioactive Release is still in progress above normal limits. |
| | The OAC is NOT available. |

1

| Appendix C | Page 3 of 11 Form I | ES-C-1 |
|---------------------|---|--------|
| | Job Performance Measure Worksheet | |
| Task Standard: | The operator will determine the PAR for the current conditions to reflected on the provided KEY. | be as |
| Required Materials: | None | |
| General References: | RP/0/A/5700/000 (Classification of Emergency) | |
| | RP/0/B/5700/029 (Notifications to Offsite Agencies from the Cont Room) | rol |
| Handouts: | Initial Emergency Notification Form | |
| | Copy of Enclosure 4.4 (Offsite Protective Action Recommendatio RP/0/B/5700/029 (Notifications to Offsite Agencies from the Cont Room) marked up to step 2. | , |
| Initiating Cue: | Based on the present conditions, the OSM directs you to update to PAR by completing steps 2 through 12 of Enclosure 4.4 (Offsite Protective Action Recommendation) of RP/0/B/5700/029 (Notification Offsite Agencies from the Control Room). | |
| | Complete the Sections below as appropriate. | |
| Time Critical Task: | NO | |
| Validation Time: | 10 minutes | |

Page 4 of 11 PERFORMANCE INFORMATION

(Denote Critical Steps with an asterisk*)

Provide Candidate with Initial Conditions/Cue (Last Page of this JPM) and Handout the Initial Emergency Notification Form and Enclosure 4.4 of RP/0/B/5700/029 marked up to step 2.

START TIME:

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| 1 | (Enclosure 4.4, Step 1) If a General Emergency is declared, determine initial Protective Action Recommendation | The operator recognizes per the initial conditions this step is already complete. | | |
| *2 | (Step 2) If Wind Speed is less than or equal to | The operator recognizes that Wind Speed is greater than 5 mph, and proceeds to Step 3. | | |

Page 5 of 11 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|---|-----|-----------------------------------|
| *3 | (Step 3) If Wind Speed is greater than 5 mph, evacuate and shelter zones as shown in the table below based on wind direction | The operator uses the Table and determines that the applicable Wind Direction range is 157.6- 180.0°. | · · | |
| | Caution 1: Once a zone is selected for evacuation, it should not be removed. Caution 2: A short term release is any release that can be projected to be 3 hours or less in duration. An example would be a "puff release." A controlled release is one that can be started or stopped at the licensee's discretion, such as the venting of Containment for pressure control. If a release is short term and controlled, then sheltering in lieu of evacuation should be considered. | The operator observes that Sectors A, B, C, L, M, and N are recommended to be evacuated for a 2 mile radius, and 5 miles downwind. The operator observes that Sectors D, E, F, G, H, I, J, K, O, P, Q, R and S are recommended to be sheltered. The operator applies Caution 1, and recognizes that Sectors D, O and R have previously been evacuated, and although the Table recommends that they be sheltered, they must remain evacuated. The operator recognizes that Caution 2 does NOT apply. The operator recommends that Sectors A, B, C, D, L, M, N, O and R remain evacuated for a 2 mile radius, and 5 miles downwind; and that Sectors E, F, G, H, I, J, K, P, Q, and S are remain sheltered. | | |

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Page 6 of 11 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|---|---|-----|-----------------------------------|
| 4 | (Step 4) If notified by RP Dose Assessment that dose projections or field measurements indicate that thyroid dose will be greater than 5 Rem | The operator recognizes that no RP Dose Assessments have been made, and proceeds to Step 5. | | |
| 5 | (Step 5) For any other Protective Action Recommendation, Check E (Other), and record information | The operator recognizes that there are no other PARs, and proceeds to Step 6. | | |
| *6 | (Step 6) After the initial PARS are transmitted to offsite agencies, check for large fission product inventory in Containment as follows: | | | |
| | (Step 6.1) If the OAC is available | The operator recognizes that the OAC is NOT available and proceeds. | | |
| | (Step 6.2) If the OAC is unavailable, use the following EMFs: 1EMF51A, 1EMF51B | The operator recognizes that 1EMF51 A and B readings must be used. | | |
| | (Step 6.3) Check if Containment radiation level exceeds the following limits based on time after shutdown: | The operator uses the table in the Time after Shutdown column of 0-2 hours, and compares the 1EMF51A and B readings of 800 R/hr to the established limit of 864 R/hr determining that the Large Fission Product Inventory in Containment has NOT been met. | | |

Page 7 of 11 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|--|-----|-----------------------------------|
| *7 | (Step 7) If Containment radiation level exceeds limits in Step 6.3 | The operator recognizes that the radiation levels are NOT exceeded, and proceeds to Step 8. | | |
| 8 | (Step 8) A McGuire EPZ Map is located on Page 8 of 8, if it is desired to visually see zones evacuated or sheltered. | The operator acknowledges and proceeds to Step 9. | | |
| 9 | (Step 9) If notified by RP Dose Assessment that dose projections or field measurements indicate that thyroid dose will be greater than 5 Rem | The operator recognizes that no RP Dose Assessments have been made, and proceeds to Step 10. | | |
| 10 | (Step 10) On a continuing basis, evaluate specific plant conditions including: large fission product inventory in Containment, EMF 51 A/B readings, offsite dose projections, wind speed and wind direction, field monitoring team data, and assess the need to update Protective Action Recommendations made to the states and counties in the previous notification. | The operator acknowledges and proceeds to Step 11. | | |
| 11 | (Step 11) Review dose projections with the on-shift dose assessor (if available) to determine if Protective Action Recommendations are required beyond the 10- mile radius. | The operator recognizes that no Dose Assessments have been made, and proceeds to Step 12. | | |

Appendix C

Page 8 of 11 PERFORMANCE INFORMATION

Form ES-C-1

| STEPS | ELEMENTS | STANDARD | S/U | COMMENTS REQUIRED FOR UNSAT |
|-------|--|---|-----|-----------------------------------|
| *12 | (Step 12) If Protective Action Recommendations are required beyond 10 miles | The operator recognizes that no RP Dose Assessments have been made, and returns the completed PAR marked up as established on the KEY. | | |

Terminating Cue:

Evaluation on this JPM is complete.

STOP TIME:

| Appe | ndix | С |
|------|------|---|
|------|------|---|

Page 9 of 11 VERIFICATION OF COMPLETION

| Job Performance Measure No.: | <u> 2010 Admin - JPM A4 SRO</u> |
|------------------------------|---------------------------------|
|------------------------------|---------------------------------|

Examinee's Name:

Date Performed:

Facility Evaluator:

Number of Attempts:

Time to Complete:

Question Documentation:

Result:

SAT

UNSAT

Examiner's Signature: _____ Date:

ſ

Page 10 of 11 VERIFICATION OF COMPLETION

KEY:

| PROTECTIVE | E ACTION RECOMMENDATIONS: |
|------------|---|
| | Evacuate: A, B, C, D, L, M, N, O and R remain evacuated for a 2 mile radius, and 5 miles downwind |
| | Shelter: E, F, G, H, I, J, K, P, Q, and S |
| D | Consider the Use of KI (Potassium Iodide) in accordance with State Plans and Policy: NA |
| E | Other: NA |

Initial Conditions:

A LOCA inside containment has occurred on Unit 1.

The crew implemented EP/1/A/5000/ECA-1.1 (Loss of Emergency Coolant Recirc) due to multiple ECCS component failures.

A Containment Red Path and a Core Cooling Red Path have occurred.

The Emergency Coordinator declared a General Emergency per RP/0/A/5700/000, Enclosure 4.1, EAL # 4.1.G.2 (Loss of Any two Barriers AND Potential loss of the third).

An Emergency Notification Form, along with the initial PAR was sent at the appropriate time.

The following conditions exist 1 hour after the start of the event:

- The radioactive release is still on-going.
- The wind speed is 9 mph.
- The wind direction is 158.9°.
- EMF51 A and B reading is 800 R/hr.

A Radioactive Release is still in progress above normal limits.

The OAC is NOT available.

INITIATING CUE:

Based on the present conditions, the QSM directs you to update the PAR by completing steps 2 through 12 of Enclosure 4.4 (Offsite Protective Action Recommendation) of RP/0/B/5700/029 (Notifications to Offsite Agencies from the Control Room).

Complete the Sections below as appropriate.

| PROTECTIVE | E ACTION RECOMMENDATIONS: |
|------------|--|
| В | Evacuate: |
| С | Shelter: |
| D | Consider the Use of KI (Potassium lodide) in accordance with State Plans and Policy: |
| E | Other: |

| | FOR TRAINING USE ONLY | ENF Handout | ADMIN JPM A4 SRO |
|-----|---|---|---|
| | NUCLEAR POWER P | LANT EMERGENCY NOTIFICA | |
| 1. | ADRILL BACTUAL EVENT | | MESSAGE # / AUTHENTICATION # onfirmation Phone # (704) 875-6044 |
| | | | |
| 4. | EMERGENCY A UNUSUAL EVENT CLASSIFICATION: 4.1.G.2 BASED ON EAL# 4.1.G.2 | BALERT C SITE AREA EM | ERGENCY D GENERAL EMERGENCY roduct Barriers and Potential Loss of the Third |
| 5. | PROTECTIVE ACTION RECOMMENDATIONS: | ANONE | |
| | EVACUATE A, B, C, D, L, M, N, O and R | | |
| | SHELTER E, F, G, H, I, J, K, P, Q, and | 3 | |
| | D CONSIDER THE USE OF KI (POTASSIUM IOD | IDE) IN ACCORDANCE WITH STATE PLANS | AND POLICY. NA |
| | E OTHEF NA | | |
| 6. | EMERGENCY RELEASE: A None | B Is Occurring | C Has Occurred |
| 7. | RELEASE SIGNIFICANCE: A Not applicable | B Within normal operating limits C Abov | e normal operating limits D Under Evaluation |
| 8. | EVENT PROGNOSIS: | B Stable C Deg | rading |
| 9. | METEOROLOGICAL DATA: Wind D | irection* from <u>132.5</u> degrees | Wind Speed* mph |
| | * May not be available for Initial Precipi Notifications) | tation* None Stability | Class* A B C D E F G |
| 10. | A DECLARATION B TERMINATION | Time Event Start Time | Date Today / Today |
| 1 | FFECTED UNIT(S): 1 2 3 AI |] | |
| | , hit Status: (Unaffected Unit(s) Status Not Required for Initial | A U1 0 % Power Shutdown a | Time T minus 10 Date TODAY / TODAY / TODAY |
| | Notifications) | B U2 100 % Power Shutdown a | t: Time Date // |
| | | C U3% Power Shutdown at | :: Time Date // |
| 13. | REMARKS: | | |
| | | | |
| | FOLLOW-UP INFORMATION (Lines 1 | 4 through 16 Not Required for In | itial Notifications) |
| | | DATA. NOT REQUIRED IF LINE 6A IS SELEC | |
| 14. | RELEASE CHARACTERIZATION: TYPE: A Ele | vated B Mixed C Ground UNIT | S: A Ci B Ci/sec C µCi/sec |
| | MAGNITUDE: Noble Gases: | lodines: Particulate | s: Other: |
| | FORM: A Airborne Start Time: | Date: / / / | Stop Time Date // |
| | BLiquid Start Time: | Date: / / / / | |
| 15. | PROJECTION PARAMETERS: Projection Perio Projection performed: Time | | nated Release Duration:Hours |
| 16. | PROJECTED DOSE: <u>DISTANCE</u> | | Did CDE (mrem) |

Site boundary 2 Miles 5 Miles

17. APPROVED BY_____

NOTIFIED BY:

10 Miles Time: _____ Date ____ / ____ / ____ Title: Emergency Coordinator RECEIVED BY: Time: _____ Date ____ / ____ / ADMIN JPM A4 SRO FOR TRAINING USE ONLY

Offsite Protective Action Recommendations Page 1 of 8

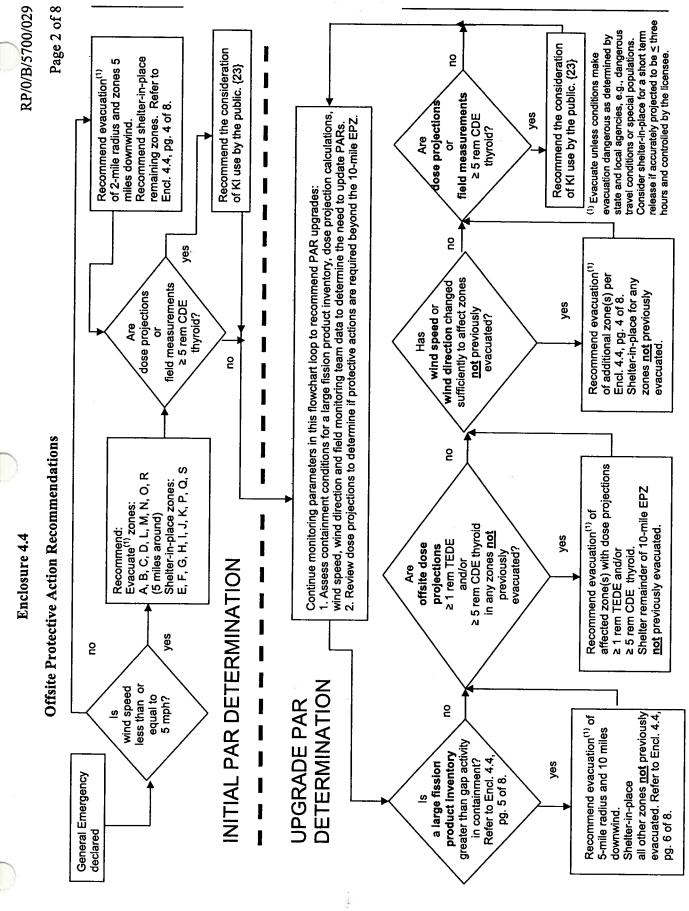
NOTE: 1. Protective Action Recommendations (PARs) for the public apply during a General Emergency, and include sheltering, evacuation and consideration of KI use. PARs are based on plant conditions independent of projected dose, and can also be based on projected dose. Protective Action Guides (PAGs) are levels of radiation dose at which prompt protective actions should be initiated and are based on EPA-400-R-92-001, <u>Manual of protective Action Guides and Protective Actions for Nuclear Incidents</u>. The projected dose PARs specified in this enclosure are based on the PAGs listed below. The PAG for KI is taken from <u>Potassium Iodide as a Thyroid Blocking Agent in Radiation Emergencies, FDA Guidance</u>, November 2001 and <u>Guidance for Industry, KI in Radiation Emergencies, Questions and Answers, FDA</u>, December 2002. {23}

PROTECTIVE ACTION GUIDES (PAGs)

| Total Effective Dose Equivalent (TEDE) | Committed Dose Equivalent (CDE) Thyroid | Recommendation |
|---|---|---|
| < 1 rem | < 5 rem | No Protective Action is required based on projected dose. |
| \geq 1 rem | ≥ 5 rem | Evacuate affected zones and shelter the remainder of the 10-mile EPZ not evacuated. |
| N/A | ≥ 5 rem | Consider the use of KI (potassium iodide) in accordance with State Plans and Policy. |

Projected Dose

2. IF desired, you may refer to the flow chart of page 2 of this enclosure. {PIP M-06-5137, C.A.3}



(

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Offsite Protective Action Recommendations

Page 3 of 8

- **<u>SLM</u>** 1. **IF** a General Emergency is declared, determine Initial Protective Action Recommendations as follows (PIP-M-02-6163):
 - ☑ 1.1 Obtain the wind speed and direction, use chart recorder 1EEBCR9100, point #5 (Average Lower Wind Speed) and point #8 (Average Upper Wind Direction).

Wind Direction (Point 8): <u>158.9°</u>

| Wind Speed (Point 5): 9 |
|-------------------------|
|-------------------------|

NAR 1.2 IF Chart Recorder unavailable, obtain wind direction from one of the following sources, preferred sequence:

DA. Unit 1 OAC:

- Average Upper Wind Direction M1P0847
- Average Lower Wind Speed M1P0848.
- B. DPC Meteorologist (9-704-382-0139 or 9-704-373-7896).
- □ C. National Weather Service in Greer, S.C. (9-864-879-1085 or 9-800-268-7785).
- 2. **IF** wind speed less than or equal to 5 MPH, recommend the following:

CAUTION: 1. Once a zone is selected for evacuation, it should not be removed. {PIP-M-03-3483}
2. A short term release is any release that can be projected to be 3 hours or less in duration. An example would be a "puff release". A controlled release is one that can be started and stopped at the licensee's discretion, such as the venting of Containment for pressure control. IF a release is short term and controlled, THEN sheltering in lieu of evacuation should be considered. {PIP-M-05-3631}

- 2.1 Evacuate zones A, B, C, D, L, M, N, O, R. (See Caution 2 above)
- 2.2 Shelter zones E, F, G, H, I, J, K, P, Q, S.

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Offsite Protective Action Recommendations

Page 4 of 8

- IF wind speed is greater than 5 MPH, evacuate and shelter zones as shown in the table below 3. based on wind direction:
- CAUTION: 1. Once a zone is selected for evacuation, it should not be removed. {PIP-M-03-3483} 2. A short term release is any release that can be projected to be 3 hours or less in duration. An example would be a "puff release". A controlled release is one that can be started and stopped at the licensee's discretion, such as the venting of Containment for pressure control. IF a release is short term and controlled, THEN sheltering in lieu of evacuation should be considered. {PIP-M-05-3631}

| W | ind Speed Greater than 5 Miles per I | Iour |
|--|--------------------------------------|---------------------------|
| Wind Direction (deg from N) Chart Recorder 1EEBCR9100 | | |
| Point # 8 Average Upper Wind | Evacuate* | Shelter |
| Direction | 2 Mile Radius-5 Mile Downwind | Remaining Sectors |
| 0.1 - 22.5 | B,C,D,L,M,O,R | A,E,F,G,H,I,J,K,N,P,Q,S |
| 22.6 - 45.0 | B,C,D,L,M,O,R | A,E,F,G,H,I,J,K,N,P,Q,S |
| 45.1 - 67.5 | B,C,D,L,M,O,R | A,E,F,G,H,I,J,K,N,P,Q,S |
| 67.6 – 90.0 | B,C,D,L,M,N,O,R | A,E,F,G,H,I,J,K,P,Q,S |
| 90.1 - 112.5 | B,C,L,M,N,O,R | A,D,E,F,G,H,I,J,K,P,Q,S |
| 112.6 - 135.0 | A,B,C,L,M,N,O,R | D,E,F,G,H,I,J,K,P,Q,S |
| 135.1 – 157.5 | A,B,C,L,M,N,O | D,E,F,G,H,I,J,K,P,Q,R,S |
| 157.6 - 180.0 | A,B,C,L,M,N | D,E,F,G,H,I,J,K,O,P,Q,R,S |
| 180.1 - 202.5 | A,B,C,L,M,N | D,E,F,G,H,I,J,K,O,P,Q,R,S |
| 202.6 - 225.0 | A,B,C,D,L,M,N | E,F,G,H,I,J,K,O,P,Q,R,S |
| 225.1 - 247.5 | A,B,C,D,L,M | E,F,G,H,I,J,K,N,O,P,Q,R,S |
| 247.6 - 270.0 | A,B,C,D,L,M | E,F,G,H,I,J,K,N,O,P,Q,R,S |
| 270.1 - 292.5 | A,B,C,D,L,M | E,F,G,H,I,J,K,N,O,P,Q,R,S |
| 292.6 - 315.0 | A,B,C,D,L,M | E,F,G,H,I,J,K,N,O,P,Q,R,S |
| 315.1 - 337.5 | B,C,D,L,M,R | A,E,F,G,H,I,J,K,N,O,P,Q,S |
| 337.6 - 360.0 | B,C,D,L,M,R | A,E,F,G,H,I,J,K,N,O,P,Q,S |

Protoctive Action Zames Determined

* See Cautions 1 and 2 above.

IF notified by RP Dose Assessment that dose projections or field measurements indicate that 4. Thyroid dose will be \geq 5 Rem, KI use by the General Public must be recommended in accordance with State Plans and Policy. {PIP-G-03-606}

5. For any other Protective Action Recommendation, check E (Other) and record information.

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Offsite Protective Action Recommendations

Page 5 of 8

- 6. After the Initial PARS are transmitted to offsite agencies, check for large fission product inventory in containment as follows:
- 6.1 **IF** the OAC is available, call up the following computer points based on need:

| Unit 1 OAC | Unit 2 OAC | |
|------------|------------|--|
| M1A0829 | M2A0829 | |
| M1A0835 | M2A0835. | |

6.2 **IF** the OAC is unavailable, use the following EMF's:

| Unit 1 | Unit 2 |
|---------|----------|
| 1EMF51A | 2EMF51A |
| 1EMF51B | 2EMF51B. |

□ 6.3 Check if containment radiation level exceeds the following limits based on time after shutdown:

| TIME AFTER SHUTDOWN (hours) | EMF51A(B) reading(R/HR) | |
|-----------------------------|-------------------------|--|
| >0-2 | 864 | |
| >2-4 | 624 | |
| >4-8 | 450 | |
| >8 | 265 | |

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Offsite Protective Action Recommendations

Page 6 of 8

- 7. IF containment radiation level exceeds limits in Step 6.3, perform the following:
 - \Box 7.1 Evacuate and shelter zones in the table below based on wind direction:

CAUTION: 1. Once a zone is selected for evacuation, it should not be removed. {PIP-M-03-3483}

 A short term release is any release that can be projected to be 3 hours or less in duration. An example would be a "puff release". A controlled release is one that can be started and stopped at the licensee's discretion, such as the venting of Containment for pressure control. <u>IF</u> a release is short term <u>and</u> controlled, <u>THEN</u> sheltering in lieu of evacuation should be considered. {PIP-M-05-3631}

| For Containment Radiation Levels Exceeding GAP Activity | | | |
|---|--------------------------------|-------------------|--|
| Wind Direction (deg from N) | | | |
| Chart Recorder 1EEBCR9100 | | | |
| | | | |
| Point # 8 Average Upper Wind | Evacuate* | Shelter | |
| Direction | 5 Mile Radius-10 Mile Downwind | Remaining Sectors | |
| 0.1 - 22.5 | A,B,C,D,E,F,L,M,N,O,R,S | G,H,I,J,K,P,Q | |
| 22.6 - 45.0 | A,B,C,D,E,L,M,N,O,Q,R,S | F,G,H,I,J,K,P | |
| 45.1 - 67.5 | A,B,C,D,E,L,M,N,O,Q,R,S | F,G,H,I,J,K,P | |
| 67.6 - 90.0 | A,B,C,D,L,M,N,O,P,Q,R,S | E,F,G,H,I,J,K | |
| 90.1 - 112.5 | A,B,C,D,K,L,M,N,O,P,Q,R,S | E,F,G,H,I,J | |
| 112.6 - 135.0 | A,B,C,D,I,K,L,M,N,O,P,Q,R,S | E,F,G,H,J | |
| 135.1 – 157.5 | A,B,C,D,I,K,L,M,N,O,P,Q,R | E,F,G,H,J,S | |
| 157.6 - 180.0 | A,B,C,D,I,J,K,L,M,N,O,P,R | E,F,G,H,Q,S | |
| 180.1 – 202.5 | A,B,C,D,G,H,I,J,K,L,M,N,O,P,R | E,F,Q,S | |
| 202.6 - 225.0 | A,B,C,D,G,H,I,J,K,L,M,N,O,P,R | E,F,Q,S | |
| 225.1 - 247.5 | A,B,C,D,F,G,H,I,J,L,M,N,O,R | E,K,P,Q,S | |
| 247.6 - 270.0 | A,B,C,D,F,G,H,I,J,L,M,N,O,R | E,K,P,Q,S | |
| 270.1 - 292.5 | A,B,C,D,E,F,G,H,J,L,M,N,O,R | I,K,P,Q,S | |
| 292.6 - 315.0 | A,B,C,D,E,F,G,L,M,N,O,R | H,I,J,K,P,Q,S | |
| 315.1 - 337.5 | A,B,C,D,E,F,G,L,M,N,O,R | H,I,J,K,P,Q,S | |
| 337.6 - 360.0 | A,B,C,D,E,F,L,M,N,O,R,S | G,H,I,J,K,P,Q | |

Protective Action Zones Determination

* See Cautions 1 and 2 above.

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Offsite Protective Action Recommendations

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- 8. A McGuire EPZ map is located on page 8 of 8, if it is desired to visually see zones evacuated or sheltered.
- 9. <u>IF</u> notified by RP Dose Assessment that dose projections or field measurements indicate that Thyroid dose will be ≥ 5 Rem, KI use by the General Public must be recommended in accordance with State Plans and Policy. {PIP-G-03-606}
- 10. On a continuing basis, evaluate specific plant conditions including: large fission product inventory in containment, EMF 51 A/B readings, offsite dose projections, wind speed and wind direction, field monitoring team data, and assess the need to update Protective Action Recommendations made to the states and counties in the previous notification.
- 11. Review dose projections with the on-shift dose assessor (if available) to determine if Protective Action Recommendations are required beyond the 10-mile EPZ.
 - 12. IF Protective Action Recommendations are required beyond 10 miles, notify the states and counties and request that they consider sheltering/evacuating the general populations located beyond the affected 10-mile EPZ.

RP/0/B/5700/029

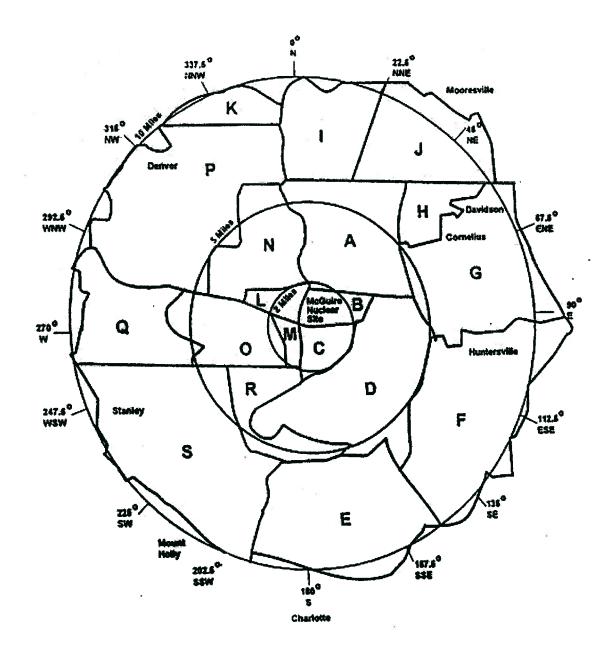
Offsite Protective Action Recommendations

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McGUIRE PROTECTIVE ACTION ZONES

(2 and 5 mile radius, inner circles)

10-MILE EPZ



1