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## RAGTIME: A FORTRAN 1V Implementation of a Time-Dependent Model for Radionuclides in Agricultural Systems

First Progress Report

**J,** C. Pleasant L. M. McDowell-Boyer **G, G.** KilIough



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#### RAGTIME: A FORTRAN IV IMPLEMENTATION OF A TIME-DEPENDENT MODEL FOR RADIONUCLIDES IN AGRICULTURAL SYSTEMS

#### FIRST PROGRESS REPORT

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#### NOTICE

This document contains information of a preliminary nature. It is subject to revision or correction and therefore does not represent a final report.

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#### HIGHLIGHTS

RAGTIME is a FORTRAN IV program that calculates radionuclide concentrations in food crops, beef, and milk which are contaminated as a result of deposition of radioactivity on an agricultural area. Contamination of these foods is assumed to occur as a result of the deposition of radioactivity onto the surface of above-ground food crops, pasture grass, the soil surface below crops, and the soil surface or root mat below pasture grass, with ingrowth of radioactive daughters being computed explicitly. The input source of radioactivity may be prescribed by the user as a step function for each nuclide in the chain. The model employs time-dependent interception fractions for deposition of activity on food crops; the interception fractions for deposition on pasture grass or pasture soil are at present constants, but the facility for use of time-dependent values is provided. Seasonal aspects of the transfer of radionuclides between various compartments of the model include the provision for specifying the dates of emergence and harvest for various crop categories.

The system of differential equations describing the model is solved by use of a discrete-variable numerical integration (the GEAR package), and the accuracy of this solution is monitored by comparing the total radioactivity in the system as calculated by the numerical procedure with that calculated by use of an explicit solution of the Bateman equations.

This report discusses the development of the model which is presently on-going, and thus, does not represent the final version envisioned for implementation. Output for a sample run of the current version is provided in this report.

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#### 1. INTRODUCTION

A number of terrestrial food-chain transport models have been developed over the past several years for use in assessing ingestion dose to man from aerially deposited radionuclides.' Included among these is a transport model described in the U. S. Nuclear Regulatory Commission's (USNRC) Regulatory Guide 1.109, a model which NRC considers acceptable for assessing terrestrial transport of radionuclides released during normal operation of light-water-cooled nuclear power plants.<sup>2</sup> Limitations of these models with respect to dynamic seasonal considerations as well as radioactive daughter ingrowth prompted model development work, the initial progress of which is reported here.

RAGTIME (Radionuclides in AGricultural systems: a TIME-dependent model) computes radionuclide concentrations in food crops, beef, and milk which are contaminated by radionuclide deposition. The model assumes a known rate of deposition of radioactivity (microcuries per square meter per day,  $\mu$ Ci m<sup>-2</sup> day<sup>-1</sup>) at a given environmental location and uses interception fractions  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$  to calculate radioactivity input rates to the model compartments representing aboveground food, the soil surface below the food crop, pasture grass, an<mark>c</mark> pasture soil or root mat, respectively, at that location. RAGTIME **s** basically an adaptation of the previously developed TERMOD code3 to consider both seasonality of agricultural processes and the dynamics of daughter ingrowth of radionuclides during food-chain transport. Because the development of RAGTIME is still in progress, some parameters and concepts believed to be inadequate for the intended use of this code have been carried over from TERMOD until appropriate revisions can be made.

The system of linear ordinary differential equations describing the model accounts explicitly for ingrowth of radioactive daughters and provides for an input source of each member of a radionuclide chain. This system is solved by use of the GEAR package<sup>4</sup> for solution of systems of ordinary differential equations. A subroutine, CHECK, of RAG-TIME provides a check on the accuracy of this solution. At each output

**I**

time, CHECK makes use of an explicit solution of the Bateman equations to calculate the total amount of radioactivity in the system; this value is compared with the total obtained by summing the amounts of radioactivity in all model compartments as computed by the GEAR subrouti ne.

In Sect. 2 of this report, we describe in broad outline the RAG-TIME methodology and present the equations which describe the model. Sections 3 and 4 provide details concerning the interception fractions  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$  and the transfer coefficients of the system. Section 5 is devoted to a discussion of the use of the GEAR package in solving the system of differential equations of the model and to a description of the way the Bateman equations are used. Finally, a description of the RAGTIME computer code is provided in Sect. 6, giving details regarding input, logical structure, and calls to the GEAR subroutines as well as the procedure employed by subroutine CHECK to monitor the accuracy of the numerical solution.

As mentioned previously, there are a number of limitations of the present version of the RAGTIME model which remain to be addressed. Principal among planned refinements is the inclusion of the seasonal cycle in the dairy and beef pathways. Aside from an example run for the <sup>90</sup>Sr-<sup>90</sup>Y chain, this report will not present a data base, the development of which is presently in progress. The present code uses an array of output times with a fixed size; whereas the integration interval may be of indefinite length, this fixed array limits the output density which is possible without recompilation. It may be desirable to remove this dependence on a fixed array in a future version.

Among planned revisions is the conversion of the RAGTIME code to the International System of Units (SI), thus effecting a change in the expression for radioactivity from curie (Ci) to becquerel (Bq), where

$$
1 \tCi = 3.7 \times 10^{10} Bq. \t(1.1)
$$

The current version of the code uses Ci to represent activity, and the following documentation is consistent with this convention although the output may easily be converted to Bq using the relationship given above.

#### 2. DESCRIPTION OF THE MODEL

The RAGTIME model is represented schematically in Fig. 2.1. The subscript i associated with the compartments  $E_i$ ,  $S_i$ ,  $P_i$ , etc. refers to the *ith* nuclide of a radionuclide decay chain. Certain of the transfer coefficients are nuclide-, or element-, dependent; this is also signified by the use of the subscript i, [e.g.,  $(\tau_{p,t})_i$ ]. The deposition source F<sub>i</sub> represents the input source of radioactivity corresponding to the ith nuclide of a radionuclide chain. This source strength may vary with time and may be represented in the computer code as a step function for each nuclide in the chain. The fractions of input radioactivity which are intercepted by above-ground crops, soil surface below the food crop, pasture grass, and pasture soil are represented by  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$ , respectively. These fractions may be time-dependent with respect to growth dynamics of the crop land or pasture. In Sect. 3.1, we describe models for calculation of time-dependent interception fractions  $S_1$  and  $S_2$ . The present version of the code uses values of  $S_3$  and  $S_4$  which are constant with respect to time; however, the same subroutine is used to return values for all interception fractions, so that a convenient method is available should the user desire to prescribe time-dependent values for  $S_3$  and  $S_4$ .

A general outline of the terrestrial pathways considered in RAG-TIME follows, along with a brief description of parameters used in implementing the computer simulation. A more rigorous definition and the rationale behind the particular quantifications used for each parameter are given in Sects. 3 and 4 of this report.

#### 2.1 Radioactivity Transfer to Crops

Radioactivity deposited on the surface of the above-ground food crop passes to the soil surface below the food crop with an environmental half-time of usually less than 30 days.<sup>5</sup> We have used 14 days for this value [ $\tau_{e,s}$  = 1n 2/(14 days) = 0.0495 day<sup>-1</sup>].<sup>3,6</sup> For transfer

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Fig. 2.1. Schematic representation of radioactivity transfer to food crops, milk, and beef as simulated by the RAGTIME computer code.

from the soil surface below the food crop to the subsurface soil pool, we have assumed a 1000-day environmental half-time, giving  $\tau_{S,D}$  = In  $2/(1000 \text{ days}) = 6.93 \times 10^{-4} \text{ day}^{-1}$ . Radioactivity in the subsurface soil pool is available for uptake by plant roots. The plant interior compartment T<sub>i</sub> simulates radioactivity which is transferred to the edible parts of crops as a result of root uptake.

In Sect. 3.2 and Appendix B, we describe a model for calcultion of a nuclide-and time-dependent rate coefficient  $(\tau_{n+1})$  representing this transfer of activity. We have assumed a loss rate of 4% per year from the subsurface soil compartment  $P_i$  to the soil compartment below the roots, H<sub>j</sub>, giving  $\tau_{p,h} = 0.04/(365 \text{ days}) = 1.096 \times 10^{-4} \text{ day}^{-1}$  (Refs. 3,7). The dotted lines from compartments **Ei** (surface of above-ground food crop) and  $T_i$  (plant interior) to (EH)<sub>i</sub> (crop holdup compartment) represent harvest of crops.

The level of radioactivity in all compartments associated with crops at a given time is dependent on the histories of both the deposition source strength and on the growth of these crops. The effect of crop growth upon the activity level on crop surfaces (compartment **Ei)** is simulated through use of the time-dependent interception fraction  $S_1$ . The time-dependent transfer coefficient  $(\tau_{p,t})_i$  serves this function with regard to the plant interior compartment  $T_i$ . Before the emergence of plants, the value of  $S_1$  is zero, as is that for  $(\tau_{p, t})_i$ . At harvest time, the entire food crop is assumed to be stored in a holdup compartment  $(EH)_i$ , after which time the radioactivity concentration level in this food is assumed to be affected only by the radioactivity decay process. Thus, the activity level in the compartments representing crops in the field (compartments  $E_i$  and  $T_i$ ) is zero except at times between the emergence and harvest of crops. Harvest of crops is simulated numerically by reinitialization of the state variables representing these compartments at harvest time, [i.e., the compartments E<sub>i</sub> and T<sub>i</sub> which represent activity associated with crops in the field are set to zero, and the compartment  $(EH)$ <sub>i</sub> representing harvested crops is assigned a value (in microcuries per kilogram) to reflect its receipt of all radioactivity from E<sub>i</sub> and T<sub>i</sub>].

#### 2.2 Radioactivity Transfer to Beef and Milk

As in the case of transfer from the surface of the above-ground food crop to the soil surface, we have assumed a 14-day environmental, or retention, half-time for the loss of radioactivity from pasture grass to pasture soil [ $\tau_{\text{a},\text{r}} =$  1n 2/(14 days) = 0.0495 day<sup>-1</sup>].<sup>3,6</sup> To account for uptake of radioactivity by pasture grass from soil, we have assumed a transfer rate of  $1\%$  per year from R<sub>i</sub> to G<sub>i</sub> [ $\tau_{r,\sigma}$  = 0.01/(365 days) = 2.74 x  $10^{-5}$  day<sup>-1</sup>].<sup>3,7</sup> As in the determination of  $\tau_{p-h}$ , a transfer rate of 4% per year from the pasture soil compartment  $R_i$  to the soil below the roots  $D_i$   $[\tau_{r,d} = 0.04/(365 \text{ days}) = 1.096 \times 10^{-4}$ day<sup>-1</sup>] was assumed.<sup>3,7</sup> The rate coefficient for loss of activity from pasture grass resulting from grass consumption **by.** a cow is denoted by  $\tau_{q,*}$ . The derivation of a value for this coefficient is discussed in Sect. 4.1. The beef compartment  $B_i$  represents the concentration of activity in the muscle of a steer and  $C_i$  simulates the concentration of activity in milk in the udder of a cow. It is not assumed that the total loss from the pasture grass compartment,  $G<sub>i</sub>$ , due to a cow's grass consumption is accounted for by gains to the beef and milk compartments  $B_i$  and  $C_i$ . Rather, the transfer coefficients  $(\tau_{q,b})_i$  and  $(\tau_{q,c})_i$ account for only portions of the total activity transferred to the cow through consumption of grass, those portions being the activity transferred to beef  $(B_i)$  and milk  $(C_i)$ , respectively. The remainder of the loss from G<sub>i</sub> due to a cow's consumption is considered only for the purpose of allowing a mass-balance check of total radioactivity in the system. This remainder, being the complement of  $(\tau_{g,b})_i$  and  $(\tau_{g,c})_i$ with respect to  $\tau_{g,*}$ , is indicated in Fig. 2.1 as a dashed line drawn to the compartment  $M_i^1$ . The compartment  $M_i^1$  is used only in connection with the performance of a mass-balance check. Details concerning the procedure used by the code to perform this check are given in Sects. 5.2 and 6.3.

The dotted lines from the beef and milk compartments  $B_i$  and  $C_i$  to the holdup compartments (BH)<sub>i</sub> and (CH)<sub>i</sub>, respectively, represent the effect of storage on the radionuclide concentration in these foods. At each output time, the computer prints, in addition to the activity concentrations of beef  $(B_i)$  and milk  $(C_i)$  at the given time, the concentration levels which these foods would reach if stored for a userspecified period of time  $(t_h^h$  for beef,  $t_c^h$  for milk). Thus, at a given output time t, (BH)<sub>i</sub> represents the activity concentration (µCi kg<sup>-1</sup>) of nuclide i in beef at time  $t + t_b^h$  which was stored from time t to time  $t + t_h^h$ , assuming a concentration level  $B_i$  at time  $t$ . The definition of  $(CH)$ ,  $(\mu C$ i liter<sup>-1</sup>) is similar. Since the determination of the values of (BH)<sub>i</sub> and (CH)<sub>i</sub> from those for B<sub>i</sub> and C<sub>i</sub> involves only the application of the process of radioactive decay (using the Bateman equations), the system of differential Eqs. (2.1) through (2.11) representing the model depicted in Fig. 2.1 does not contain equations corresponding to these holdup compartments. In Sect. 6.2 we present details concerning calls to a subroutine, RESDNS, which uses an explicit solution of the Bateman equations to calculate values for (BH)<sub>j</sub> and  $(CH)_\textbf{i}$ .

#### 2.3 The System of Equations

The following system of equations describes the transfer of deposited radioactivity to food crops, beef, and milk as depicted in Fig. 2.1. As pointed out in Sect. 2.2, the compartments  $(BH)_i$  and  $(CH)_i$  are not represented by differential equations since their values are calculated using only the Bateman equations (see Sect. **6.2).** Furthermore, the differential equation for the compartment  $M_i$ , which is used only in connection with a mass-balance check, is not included here but is discussed in Sect. 6.2. Definitions of the compartments used in the RAG-TIME model follow the system of equations. Descriptions of all other quantities used in these equations along with the values used for certain of those which represent constants (at present) are given in Table 2.1. Values of nuclide-dependent and crop-specific parameters for a sample run of RAGTIME are given in Appendix B (Table B.1) along with a description of how these values are derived from empirical data.

*Crop surface*

$$
\frac{dE_{i}}{dt} = S_{1}F_{i}(t) - (\lambda_{i}^{R} + \tau_{e,s})E_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{ij}E_{j}
$$
(2.1)

*Crop soil surface*

$$
\frac{dS_{i}}{dt} = S_{2}F_{i}(t) + \tau_{e,s}E_{i} - (\lambda_{i}^{R} + \tau_{s,p})S_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{i,j}S_{j}
$$
(2.2)

*Crop soil pooi*

$$
\frac{dP_i}{dt} = A\tau_{s,p}S_i - [\lambda_i^R + (\tau_{p,t})_i + \tau_{p,h}]P_i + \lambda_i^R \sum_{j=1}^{i-1} B_{ij}P_j
$$
 (2.3)

*Pasture grass*

$$
\frac{dG_i}{dt} = S_3 F_i(t) - (\lambda_i^R + \tau_{g,r} + \tau_{g,*}) G_i + \tau_{r,g} R_i + \lambda_i^R \sum_{j=1}^{i-1} B_{ij} G_j
$$
\n(2.4)

*Pasture soil*

$$
\frac{DR_{i}}{dt} = S_{4}F_{i}(t) + \tau_{g,r}G_{i} - (\lambda_{i}^{R} + \tau_{r,g} + \tau_{r,d})R_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{ij}R_{j}
$$
\n(2.5)

*Pasture soil sink*

$$
\frac{dD_{i}}{dt} = \tau_{r,d}R_{i} - \lambda_{i}^{R}D_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{ij}D_{j}
$$
 (2.6)

Milk

$$
\frac{dC_i}{dt} = (\tau_{g,c})_i G_i - (\lambda_i^R + \tau_{m11k}) C_i + \lambda_i^R \sum_{j=1}^{i-1} B_{ij} C_j
$$
 (2.7)

$$
\frac{dB_{i}}{dt} = (\tau_{g,b})_{i} G_{i} - [\lambda_{i}^{R} + \tau_{beef} + (\tau_{exc})_{i}]B_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{i,j} B_{j}
$$
(2.8)

*Interior of crops*

*Beef*

$$
\frac{d\mathsf{T}_{i}}{dt} = (\mathsf{t}_{p,t})_{i} \mathsf{P}_{i} - \lambda_{i}^{R} \mathsf{T}_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{i,j} \mathsf{T}_{j}
$$
(2.9)

*Crop soil sink*

$$
\frac{dH_{i}}{dt} = (\tau_{p,h}/A)P_{i} - \lambda_{i}^{R}H_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{i,j}H_{j}
$$
 (2.10)

*Stored crops*

$$
\frac{d(EH)}{dt} = -\lambda_{i}^{R}(EH)_{i} + \lambda_{i}^{R} \sum_{j=1}^{i-1} B_{ij}(EH)_{j}
$$
 (2.11)

The RAGTIME compartments are described as follows:

- E<sub>;</sub> Radioactivity present on the surface of the above<sup>.</sup> ground food crop per square meter of surface on which the crop is grown ( $\mu$ Ci m<sup>-2</sup>)
- $S_i$  Radioactivity present at the soil surface below food crops ( $\mu$ Ci m<sup>-2</sup>)
- P<sub>i</sub> Radioactivity present in the subsurface soil pool associated with one man's food supply  $(\mu C_i)$
- **G.** Radioactivity present in the pasture grass compart- **<sup>1</sup>**ment (pCi m-2 )
- R<sub>i</sub> Radioactivity present in the pasture soil from<br> **1** ground surface to the root donth of the grass  $(\mu$ Ci m<sup>-2</sup>)
- D<sub>i</sub> Radioactivity present in the pasture soil below the root depth  $(\mu$ Ci m<sup>-2</sup>)

- $C_i$  Concentration of radioactivity in the milk ( $\mu$ Ci liter-<sup>1</sup>)
- B. Concentration of radioactivity in beef (pCi **kg-1)**
- T<sub>i</sub> Radioactivity present in the interior of plants produced for human consumption ( $\mu$ Ci)
- H<sub>i</sub> Radioactivity present in the crop soil below the root depth ( $\mu$ Ci m<sup>-2</sup>)
- (EH). Concentration of radioactivity in food which is stored following harvest of crops (pCi **kg-")**
- (BH)<sub>i</sub> Concentration of radioactivity in the beef holdup compartment ( $\mu$ Ci  $kg^{-1}$ )
- **(CH)i** Concentration of radioactivity in the milk holdup compartment (pCi liter-')





## Table 2.1 (continued)



 $\mathcal{A}$ 

Symbol	FORTRAN Name	Description	Type $\alpha$
${}^{\intercal}$ r,d	TAURD	Transfer coefficient from $R_i$ to $D_i$ $(day^{-1})$	
$\mathfrak{r}_{r,g}$	TAURG	Transfer coefficient from $R_i$ to $G_i$ $($ (day $^{-1}$ )	
$\tau_{\text{s,p}}$	TAUSP	Transfer coefficient from $S_i$ to $P_i$ $(day^{-1})$	
	TIMBH	Holdup time for beef (days)	
$t_{b}^{h}$ $t_{c}^{h}$	TIMCH	Holdup time for milk (days)	
U	U	Milk capacity of the udder (liters)	
$V_c$	<b>VSUBC</b>	Dry weight consumption per day by a cow ( $kg$ day <sup>-1</sup> )	

Table 2.1 (continued)

 $\overline{a}_{N}$  type specified means parameter is nuclide- and time-independent.  $b$ Nuclide-dependent.

**C** Time-dependent.

 $d_{\mathsf{Cron}\text{-}s}$  perific parameters necessary to derive these quantities are described and quantified in Appendix B of this report.

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{2}\left(\frac{1}{2}\right)^2\right) \left(\frac{1}{2}\left(\frac{1}{2}\right)^2\right) \left(\frac{1}{2}\left(\frac{1}{2}\right)^2\right) \left(\frac{1}{2}\left(\frac{1}{2}\right)^2\right)$ 

 $\label{eq:2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2.$ 

a de la construcción de la constru<br>En 1930, el construcción de la con 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\$ 

 $\label{eq:2.1} \frac{1}{2} \sum_{i=1}^n \frac{1}{2} \sum_{j=1}^n \frac{$ 

 $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathcal{L}_{\text{max}}) = \mathcal{L}_{\text{max}}(\mathcal{L}_{\text{max}}) \,, \end{split}$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{dx}{(x^2+y^2)^2}\frac{dx}{(x^2+y^2)^2}dx\leq \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{dx}{(x^2+y^2)^2}dx=\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{dx}{(x^2+y^2)^2}dx$ 

 $\label{eq:2} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) = \frac{1}{2} \sum_{i=1}^{N} \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \,, \end{split}$ 

 $\label{eq:2.1} \frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\$ 

#### 3. PARAMETERS DESCRIBING TRANSFER TO CROPS

Modes of contamination of edible portions of crop plants include the interception and retention of aerially depositing radionuclides by crops as well as root uptake following deposition onto crop soils. In addition, interception and retention by crops of radionuclides resuspended from soil may contribute to the contamination of foodstuffs, although this pathway is not represented in the model at present. The relative importance of each of these modes of contamination will depend on many factors including the mobility of the radionuclide in soil, the availability of the nuclide for root uptake, the radiological half-life (-lives) involved, as well as the types of crops being considered.

In developing a model to describe these pathways of contamination, it is ncessary to consider seasonal cycles of crops (i.e., when the crops are and are not present during the year) as well as the time dependency of parameters describing contamination. Much of this time dependency is due to physiological and morphological changes in plants due to growth and maturation, and to changes which may be occurring in the chemical form of the radionuclide which is deposited either on plant or soil surfaces. Although time dependency due to chemical transformations has not been considered to date, the present model can potentially incorporate parameters of this type. At present, the time dependency of the interception parameters  $S_1$  and  $S_2$  (see Fig. 2.1) and of the root uptake parameter  $(\tau_{p,t})_i$  have been studied, and preliminary approaches to characterizing the dynamic nature of these parameters are discussed below.

 $A$  holdup compartment, (EH)<sub>i</sub>, is utilized in this model in order to account for radioactive decay and daughter buildup that may occur between harvest of crops and consumption by man (Fig. 2.1). The length of this interval is left to the user's discretion.

3.1 Time-dependent Aerosol Interception  $(S_1 \text{ and } S_2)$ 

The interception of airborne radionuclides by edible portions of crop plant will depend on these major factors:

- **1.** the surface area exposed to depositing particles,
- 2. the shape of the edible portion and its orientation to depositing particles, and
- 3. the particle density of the depositing material.

Because some of these parameters are specific for different plant species, edible crops have been divided into categories representing plant parts with similar morphological characteristics. The following categories have been recognized:

- 1. root crops and other crops with protected edible parts,
- 2. leafy vegetables,
- 3. exposed-grain crops,
- 4. cylindrical vegetables, and
- 5. spherical vegetables.

Ideally, empirical data regarding interception of airborne particles over the growth cycles of crops should be used to represent the time dependency of this mode of contamination. However, because data of this type are not readily available, certain simplifying assumptions were made to account for the factors affecting interception. It is hoped that the adequacy of these assumptions will be tested at a later date through validation studies and sensitivity analyses.

At present, we have attempted to model the dynamics of interception by assuming that interception is a direct function of the projected surface area of the edible portion, and that interception occurs at a **900** angle to the plane of the projected surface area. The time dependency of interception thus relies on the relationship of the projected surface area of the edible portion to the mass of that portion during plant growth. This relationship may be characterized either through the use of empirical data  $-$  for example, that obtained by the Stanford Research Institute<sup>9</sup> for several crops  $-$  or by assuming the density of the vegetative matter remains constant during growth and using geometric procedures to derive projected areas as a function of plant growth.

The mathematical representation of the crop compartment  $E_i$ , which intercepts depositing radionuclides, was given in Sect. 2.3 [Eq. (2.1)] as

$$
\frac{dE_{i}}{dt} = S_{1}F_{i}(t) - (\lambda_{i}^{R} + \tau_{e,s})E_{i} + \lambda_{i}^{R} \sum_{i=1}^{i-1} B_{ij}E_{j}.
$$

The fraction  $S_1$  of depositing radionuclides intercepted by the edible portion may be defined in two ways, depending on whether this fraction represents an empirically derived or theoretical (geometric) relationship with time. An empirical approach is

$$
S_1 = S_{\text{L}}^{\text{O}} \text{m}^{(1-\text{n}_{\text{L}})} \text{w} \tag{3.1}
$$

where

 $S_l^O$  and  $n_l$  = empirical constants,

m **=** time-dependent mass of the plant part (g dryweight),

 $w =$  number of plant parts per square meter.

An example of a time-dependent curve for m is given in Appendix B. This representation of  $S_1$  is adapted from a document prepared by the Stanford Research Institute,  $9$  which supplies values for the empirical constants  $S_1$  and n<sub>1</sub> for certain plant species. The empirical constants were derived for considerations of specific surface area  $(m^2 q^{-1})$ alone, for a given planting density w, and thus may be appropriate only for similar planting configurations. A geometric approach for estimating the relationship of  $S_1$  with time is provided by Miller, <sup>9</sup> where the change in projected surface area with time may be calculated by assigning a geometric configuration that best approximates the plant part of interest.

The output for a sample run of RAGTIME, which considers grains in compartment  $E_i$  (surface of above-ground crops) and is listed in Appendix B, was obtained by using the empirical approach for estimating the time dependency of  $S_1$ . Empirical constants, used in Eq. (3.1), are also available for edible parts of a few other plant species, including beans, cabbage, peppers, and squash.  $9$ 

The value of  $S_2$ , shown in Fig. 2.1, representing deposition of airborne radionuclides onto the soil surface below the food crop  $(S_i)$ is calculated hypersize that

 $S_2 = 1 - S_1$  (3.2)

It is recognized that this approach may overestimate the soil deposition since inedible parts of food crops will intercept depositing radionuclides. Radionuclides intercepted by inedible portions may all eventually reach the soil when the field is plowed following harvest, less any radioactive decay during retention on plant surfaces.

3.2 Time-dependent Root Uptake  $(\tau_{p,t})_i$ 

Time dependence of root uptake is especially important when considering radioactive daughter ingrowth and soil depletion of a particular radionuclide. It is expected that root uptake will be a function of the increase in biomass of a plant or plant part over time as well as of the physiological stage in the life cycle of the plant. Both biomass increase and physiologic maturation may involve active and passive processes by which plant tissues incorporate elements. Many essential elements are both actively and passively acquired, while other elements may only be passively acquired. Because many radionuclides are radioactive isotopes or chemical analogs of essential elements, root uptake rates should be described in an element-, as well as time-, dependent sense.

Literature reviewed to date indicates a paucity of data regarding time-dependent root uptake of most elements. What is available indicates that the shape of the uptake curve, however, is similar to that of the growth curve for some elements and crop species studied.  $10-16$ Therefore, the approach adopted in RAGTIME is either to characterize uptake rates by edible portions of crops on the basis of any empirical data available, or to assume that the uptake rate follows growth curve for the edible portion in the absence of empirical uptake data.

The uptake curve obtained via either of these two approaches is then adjusted such that the concentration in the edible portion for a chosen harvest time is related to the soil concentration at that time by the empirically derived concentration factor,  $B_{iv}$ . The value for  $B_{i,v}$  is obtained from empirical studies which measure the final crop concentration with respect to a soil concentration believed to be approximately constant throughout the growth cycle. Thus, for elements whose concentrations are significantly decreased in the root zone either by movement downward into the soil sink or uptake by crops, concentration factors derived from initial soil concentrations and final crop concentrations may not be appropriate.

## 3.3 Time-independent Parameters  $(\tau_{e,s}, \tau_{s,p} \text{ and } \tau_{p,h})$

Retention, both initial and long-term, of intercepted radionuclides will depend on $8$ 

- 1. the surface characteristics of the edible portion,
- 2. the particle size,
- 3. the wind velocity, and
- 4. the relative humidity and amount of rainfall.

The effect each of these will have on retention will vary from site to site, and thus, the value of  $\tau_{e,s}$ , the retention coefficient, may vary greatly. For the present, we have assumed an average, time-dependent value of  $\tau_{e,s}$  of 0.0495 day<sup>-1</sup>, consistent with that provided in TER-MOD,<sup>3</sup> until further research into this parameter can be undertaken.

The movement of radionuclides deposited on surface soil to the root zone has been characterized in TERMOD as  $\tau_{\rm g}$ . The definition and value of this parameter has been carried over to RAGTIME, pending future investigation into its appropriateness. It is possible that this parameter might best be described in a time-dependent sense, with empirical data being derived from soil distribution coefficients, or  $K_d$ 's, available in the literature. Because these  $K_d$ 's are elementspecific, it may also be necessary to incorporate nuclide-specificity into the definition of  $\tau_{s,p}$ .

The downward movement of radionuclides out of the root zone into the soil sink is again characterized by a time- and nuclide-independent parameter,  $\tau_{p,h}$ , adopted from TERMOD. As with  $\tau_{s,p}$ , further research into the appropriateness of the value and interpretation of this parameter is pending.

#### 4. PARAMETERS DESCRIBING TRANSFER TO BEEF AND MILK

Contamination of beef and milk may occur as a result of the interception or root uptake of depositing radionuclides by forage crops, and the subsequent ingestion by beef or dairy cattle. The RAGTIME code, to date, considers that this contamination occurs only through grazing of exposed pasture grasses by cattle. Thus, the loss and/or buildup of radionuclides present in stored feeds and hay, upon which cattle may depend for a large portion of the year, are not considered at this time. Furthermore, inhalation of radioactivity by cattle is not yet treated explicitly.

#### 4.1 Contamination of Pasture Grass

As with food crops (Sect. 3), pasture grass  $(G_i)$  may be contaminated through interception of depositing radionuclides, including resuspended particulates, and through root uptake of nuclides deposited on the soil or root mat  $(R_i)$  below the pasture grass. At present, a pasture exposed to depositing radionuclides is assumed to maintain an approximately constant plant biomass throughout the year, and that the interception fraction for grasses,  $S_3$ , remains constant. The assumed value of  $S_3$ , equal to 0.25, is equivalent to the value originally used in  $TERMOD, <sup>3</sup>$  and falls in the range of empirical measurements reported by Chamberlain<sup>17</sup> for initial retention (where sampling is done immediately after contamination) by grasslands. This parameter would be expected to vary with plant density and other environmental factors, and thus represents an average value here. The fraction,  $s_3$ , is applied directly to the aerosol source term,  $F_i$  (see Fig. 2.1), and thus the model does not explicitly account for interception of radionuclides resuspended from the soil or root mat below the pasture grass.

The fraction  $S_4$ , in Fig. 2.1, represents the fraction of depositing activity not initially intercepted by grass leaves and thus the fraction deposited on the surface soil or root mat below the leaves. Therefore, this value is assigned a constant value of 0.75, being defined as follows:

The value of the parameter  $\tau_{r,q}$ , representing additional input into the pasture grass compartment from surface soil, is consistent with the TERMOD value<sup>3</sup> adopted from a paper by Menzel,<sup>7</sup> which indicates that an upper limit for uptake of radionuclides in the surface soil by a single crop is 1%. Considered on an annual basis,  $\tau_{r,q}$  becomes 2.74  $\times$  10<sup>-5</sup> day<sup>-1</sup>.

Three aspects of root uptake by pasture grasses have not been considered at present. First, the element dependency of this parameter,  $\tau_{r,q}$ , has been neglected, yet may be quite important when root uptake is significant with respect. to foliar contamination. Second, an additional mode of root absorption of radionuclides which does not involve the soil may be quite significant. This latter mode of uptake involves the radionuclide availability for uptake from the root mat, which is a "thatch" of dead and decomposing tissues around the plant-base region in which grasses may root.<sup>7</sup> Finally, the time dependency of  $\tau_{r,q}$  has not been investigated. All of these aspects will be addressed as work continues on RAGTIME.

Loss of radionuclides from the grass compartment,  $G_i$  (see Fig. 2.1), may occur through ingestion of grass by grazing cattle  $(\tau_{q,x})$ , radioactive decay  $(\lambda_i^R)$ , and by weathering of surface-deposited radionuclides  $(\tau_{g,r})$ . The value of  $\tau_{g,r}$  is assumed to be equivalent to the weathering coefficient,  $\tau_{e,s}$ , discussed in Sect. 3, and thus represents a 14 day half-time for retention of intercepted materials. This value is consistent with data reported by Chamberlain<sup>17</sup> for grasslands, although it may vary with seasons and climatic factors. In particular, this weathering coefficient, when measured, will incorporate loss of surface material due to shedding of the protective leaf cuticle during plant growth,<sup>17</sup> thus suggesting a seasonal and species dependency of  $\tau_{g,r}$ . As with  $\tau_{e,s}$ ,  $\tau_{g,r}$  is assumed to be time independent until further research dictates that a different approach should be taken.

The value of  $\tau_{g,*}$  (day<sup>-1</sup>) will depend on the rate of loss of radionuclides in pasture grass through consumption by grazing beef and dairy cattle. For this model, an average ingestion rate,  $V_c$ , of 10 kg day $-1$  dry matter was assumed, consistent with the value used in TER-MOD. 3 Using this ingestion rate and a dry-weight areal grass density,  $D_{\alpha}$ , of 0.15 kg m<sup>-2</sup> (Ref. 3), we define the value of  $\tau_{\alpha}$  **\*** to be

$$
\tau_{g,*} = \frac{V_c}{A_g D_g} = \frac{6.67 \times 10^{-1} \text{ day}^{-1}}{A_g} , \qquad (4.2)
$$

where

 $A_q$  = pasture area per cow (m<sup>2</sup>).

At present, it is assumed that  $\tau_{q,*}$  is constant throughout the year. Further work on incorporating seasonal aspects into the model will modify this approach.

The rate of loss of radionuclides from the surface soil  $(R_i)$  beneath pasture grass is represented by the parameter  $\tau_{r,d}$ . As with the similarly defined parameter,  $\tau_{p,h}$ , for crop soil (Sect. 3), an elementindependent rate of 1.096 x  $10^{-4}$  day<sup>-1</sup> is used, as given in documentation of the TERMOD code.<sup>3</sup> Again, further research may indicate a more appropriate value or representation of this process.

#### 4.2 Contamination of Beef and Milk

Transfer of radionuclides from pasture grass to beef or milk is parameterized by  $(\tau_{a-b})_i$ , in m<sup>2</sup> kg<sup>-1</sup> day<sup>-1</sup>, or  $(\tau_{a-c})_i$ , in m<sup>2</sup> liter-<sup>1</sup> day $^{-1}$ , respectively (see Fig. 2.1). These parameters represent trans $\cdot$ fer rates and are assumed to be time independent pending further investigation into data available regarding their time dependency. Elementspecific values of  $(\tau_{g,b})$ ; and  $(\tau_{g,c})$ ; were calculated from empirically derived transfer coefficients, $^{18}, \, ^{19}$  (F<sub>f</sub>)<sub>i</sub> and (F<sub>m</sub>)<sub>i</sub>, which characterize the ratios between beef or milk concentrations of an element and the equilibrium concentration of that element in pasture grass or feed. By definition

- $F_f$  = the fraction of the daily intake of an element by a beef cow which appears per kg of flesh at time of slaughter (day  $kg^{-1}$ ), and
- F **=** the fraction of the daily intake of an element by a m dairy cow which appears per liter of milk at equilibdairy cow which appears per liter of milk at equilib-<br>rium (day liter<sup>-1</sup>).

Therefore, the empirical coefficients represent the theoretical coefficients only if pasture grass (or feed) is the only source of the element in question in the cow's diet. The parameter  $(\tau_{g,b})_i$  was derived by assuming that the concentration in beef at time of slaughter approximates an equilibrium concentration, given an equilibrium concentration in pasture grass. Thus, if  $(B_{\text{row}}^{\text{eq}})_{i}$  is taken to represent the equilibbium concentration of an element, i, in the muscle of a single cow ( $\mu$ Ci kg<sup>-1</sup>), and  $G_i^{eq}$  is the equilibrium concentration in grass ( $\mu$ Ci  $m^{-2}$ ), then from the equilibrium equation

$$
\frac{d(B_{\text{cow}})_{i}}{dt} = (\tau_{g,b})_{i} G_{i}^{eq} - (\tau_{\text{exc}})_{i} (B_{\text{cow}}^{eq})_{i} = 0, \qquad (4.3)
$$

it follows that

$$
\frac{(\mathsf{B}_{\mathsf{cow}}^{\mathsf{eq}})^{\mathsf{i}}}{\mathsf{G}_{\mathsf{i}}^{\mathsf{eq}}} = \frac{(\mathsf{t}_{\mathsf{g},\mathsf{b}})_{\mathsf{i}}}{(\mathsf{t}_{\mathsf{exc}})_{\mathsf{i}}},\tag{4.4}
$$

where

 $(\tau_{\text{exc}})_i$  = loss rate of the element, i, from the muscle of a steer  $(\text{day}^{-1})$ . Since

$$
(\tau_{g,b}) = \frac{(\text{B}_{\text{cow}}^{\text{eg}})^{\dagger}}{\text{G}_{\text{i}}^{\text{eq}}} (\tau_{\text{exc}})_{\text{i}}
$$
 (4.5)

24

and

$$
(F_f)_i = \frac{(B_{cow}^{eq})_i}{(G_i^{eq} \times V_c / D_g)}
$$

where

$$
V_c = \text{dry-weight grass consumption per day by a cow (10 kg day-1),}
$$

D<sub>g</sub> = dry-weight areal grass density (0.15 kg m<sup>-2</sup>),

it follows that the expression for  $(\tau_{q,b})_i$  is related to  $(F_f)_i$  by:

$$
(\tau_{g,b})_i = \frac{(F_f)_i (\tau_{exc})_i V_c}{D_g} \qquad (4.7)
$$

Assuming the animal's diets to consist solely of pasture grass, the loss rate of the element from the muscle of a steer,  $(\tau_{exc})_i$ , may be interpreted to represent both the element-specific metabolic turnover, as well as the element-independent dilution of the concentration due to increase in muscle mass during growth. This approach has been adopted from the TERMOD code<sup>3</sup> for the present, but will probably be revised to reflect a dynamic, rather than steady-state, approach to modeling this pathway as model development progresses. In doing so, the dilution due to growth may be handled explicitly rather than incorporated into a term such as  $(\tau_{\text{exc}})_{\text{i}}$ .

Similarly for  $(\tau_{q,c})_i$ , representing transfer of element, i, to milk  $(C_i)$ ,

$$
(\tau_{g,c})_i = \frac{(F_m)_i (\tau_{milk}) V_c}{D_g} , \qquad (4.8)
$$

where

$$
\tau_{\text{milk}} =
$$
 the element-independent loss rate from the udder (2 day<sup>-1</sup>).

 $(4.6)$ 

. The value of  $\tau_{\mathsf{milk}}$  in this case corresponds to the frequency of milking, assumed to be twice daily, and other losses are considered negli- .gible. Equation (4.8) was derived in a manner similar to Eq. (4.7), from

$$
\frac{d(C_{\text{cow}})_i}{dt} = (\tau_{g,c})_i G_i^{\text{eq}} - \tau_{\text{milk}}(C_{\text{cow}}^{\text{eq}})_i = 0,
$$
\n(4.9)

and

$$
(F_m)_i = \frac{(c_{\text{cow}}^{\text{eq}})_i}{(G_i^{\text{eq}} \times V_c / D_g)}
$$
(4.10)

Again, dynamics related to maturation and milking practices for a single cow have been neglected at this time, but will be considered as model development progresses.

The equation describing radionuclide concentrations in the beef compartment as whole [Eq. (2.8)], given in Sect. 2.3 of this report, as

$$
\frac{dB_{i}}{dt} = (\tau_{g,b})_{i} G_{i} - [\lambda_{i}^{R} + \tau_{beef} + (\tau_{exc})_{i}]B_{i} + \lambda_{i}^{R} \sum_{i=1}^{i-1} B_{i,j} B_{j}
$$

differs from that for a single cow given in Eq. (4.3) due to the presence of an additional element-independent loss parameter,  $\tau_{\text{beef}}$ . The interpretation of this aspect of the beef compartment has been adopted here from TERMOD,<sup>3</sup> in that the compartmental equation considers losses from beef in the herd as a whole by including the term,  $\tau_{\text{beef}}$ , to account for slaughter of contaminated cattle. This interpretation then implies instantaneous replacement of the slaughtered portion with uncontaminated cattle and a subsequent reduction or loss of radioactivity from the compartment. The uncontaminated cattle then begin to accumulate radioactivity at a rate determined by  $(\tau_{q,b})_i$ . If, however, the
radionuclide concentration in the beef compartment is to be used as an indication of man's radiation exposure via ingestion of beef, the present methodology may underestimate concentrations in beef of cattle being slaughtered. That is, this latter portion of the herd will likely be the more mature segment which has been exposed to contaminated pasture for the greatest length of time, although the concentration calculated will be an average of all members of the herd. In light of this potential deficiency, work is ongoing to revise the homogeneous herd concept, where uncontaminated and contaminated beef are indiscriminately mived to produce an average concentration in **the** beef which may be lower than that in cattle ready for slaughter.

The milk compartment may also be interpreted to represent concentrations in milk obtained from the dairy herd as a whole. In this case, however, instantaneous replacement of milk removed from the udder by uncontaminated milk does not result in a reduction in concentration below that to which man might be exposed, because each lactating cow, as well as the herd, is subject to this same removal process. That is, while slaughtering will not affect the radionuclide concentration in beef of any particular cow, milking will affect the concentration in milk of each individual lactating cow in the herd, and thus can be considered when considering the herd as a whole.

For both milk and beef compartments, radionuclide loss and buildup of daughters due to radioactive decay during storage prior to human consumption is considered. Compartments  $(CH)$ <sub>i</sub> and  $(BH)$ <sub>i</sub>, representing concentrations of each nuclide in milk and beef, respectively, following storage were devised to provide this information.

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\$  $\label{eq:2.1} \frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt$  $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) & = \frac{1}{2} \sum_{i=1}^{N} \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \\ & = \frac{1}{2} \sum_{i=1}^{N} \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{$  $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) &= \mathcal{L}_{\text{max}}(\mathbf{r}) \$ 

## 5. SOLUTION OF THE SYSTEM OF DIFFERENTIAL EQUATIONS

#### 5.1 Use of the GEAR Subroutine

The system of differential Eqs. (2.1) through (2.11) is solved in the RAGTIME code by use of the GEAR package<sup>4</sup> for solution of systems of ordinary, differential equations. The subroutine CALC of RAGTIME makes a call to the subroutine GEAR of the GEAR package at each output time to determine the values of the state variables,

 $E_i$ ,  $S_i$ ,  $P_i$ ,  $G_i$ ,  $R_i$ ,  $D_i$ ,  $C_i$ ,  $B_i$ ,  $T_i$ ,  $H_i$ , and (EH)<sub>i</sub>,

where  $i = 1$  to n (the number of nuclides in the chain) at the given time. In the notation of the GEAR package, the system of differential Eqs. (2.1) through (2.11), with i varying from 1 to n, has the form

 $dY/dT = F(Y,T)$ 

where  $Y = [Y(1), Y(2), ..., Y(N)]$  is the state vector at time T, with N representing the number of state variables. The present version of RAGTIME uses  $N = 12 \times n$  state variables ( $n =$  the number of nuclides in the chain). The correspondence between RAGTIME state variable names and those used in the GEAR package is shown in Table 5.1.

The user of the GEAR package furnishes a subroutine DIFFUN(N,T,Y, YDOT) which computes the function YDOT **=** F(Y,T), the right-hand side of the system of ordinary differential equations, where N, T, and Y are as described above. The correspondence indicated above between RAGTIME state variable names and those used by the GEAR package implies a similar correspondence between the two notations for derivatives (Table 5.2).

The notation used in subroutine CALC of RAGTIME for a call to the GEAR subroutine for values of the state variables at the time TOUT is

CALL GEAR (DIFFUN, PEDERV, N, TO, HO, YO, TOUT, APS, MF, INDEX)



 $\ddot{\phi}$ 

Table **5.1** Definition of RAGTIME state variables in terms of GEAR package notation

RAGTIME derivatives	GEAR package notation
$dE_i/dt$	$YDØT[12(i - 1) + 1]$
$ds_i/dt$	$YDØT[12(i - 1) + 2]$
$dP_i/dt$	$YDØT[12(i - 1) + 3]$
$dG_i/dt$	$YDØT[12(i - 1) + 4]$
$dR_i/dt$	YDØT[12(i - 1) + 5]
$dD_i/dt$	$YDØT[12(i - 1) + 6]$
$dC_i/dt$	$YDØT[12(i - 1) + 7]$
$dB_i/dt$	$YDØT[12(i - 1) + 8]$
$d(EH)$ <sub>i</sub> /dt	$YDØT[12(i - 1) + 9]$
$dT_i/dt$	$YDØT[12(i - 1) + 10]$
$dH_i/dt$	$YDØT[12(i - 1) + 11]$

Table **5.2** Definition of RAGTIME derivatives in terms of GEAR package notation

 $\overline{a}$ 

where the parameters have the following meanings:

- (1) DIFFUN is the name of the subroutine described above, which is declared external in subroutine CALC.
- (2) PEDERV is also a subroutine which is declared external in CALC. Under certain options available to the user of the GEAR subroutine, this subroutine is used to define the N by N Jacobian matrix of partial derivatives. However, under the option used by RAGTIME, PEDERV is a dummy subroutine.
- (3) N is the number of state variables (i.e.,  $N = 12$  x n in our case).
- (4) TO is the initial value of T, the time variable (used only on the first call).
- (5) HO is the step size for T (used only on the first call).
- (6) YO is a vector of length N  $(= 12 \times n)$  containing the initial values of Y. This vector is used for input only on the first call.
- (7) TOUT is the value of T at which output is desired.
- (8) EPS is the relative error bound (used only on the first call unless  $IMDEX = -1$ ).
- (9) MF is a parameter used to indicate the basic method to be used for integration (Adams method or the stiff method of GEAR) and the method of iteration.
- (10) INDEX is an integer used to indicate the type of call. Initially, INDEX is set to 1. The value returned for INDEX is 0 unless the integration was halted for some reason. For meanings of the values  $-1$ ,  $-2$ ,  $-3$ , or  $-4$ , for an output value of INDEX, see a listing of the GEAR package.

#### 5.2 Use of the Bateman Equations as a Check

Since RAGTIME uses a numerical method for solution of the system of differential Eqs. (2.1) through (2.11), it is desirable to have a procedure for checking the accuracy of this solution. Fortunately, it is possible to calculate the total amount of radioactivity in the system at any given time using an explicit solution of the Bateman equations. This value can then be compared with the corresponding value calculated by summing the amounts of radioactivity in the various compartments of the model as calculated by use of the GEAR package. Close agreement of these two values is a necessary but not sufficient condition that the numerical solution of the model equations is accurate to the degree desired. In particular, one should keep in mind that a large relative error in a compartment whose radioactivity contribution is small compared to other compartments would be masked by this summing procedure. Nevertheless, the comparison of total radioactivity as calculated in these two ways provides valuable assistance in evaluating the numerical method since, as most practitioners of numerical analysis would admit, the use of such methods is still largely an empirical science. In particular, this comparison can provide guidance for the selection of appropriate options and parameter values to be used in calls to the GEAR subroutine.

The Bateman equations describe the decay process of a radionuclide chain. Consider a chain of radionuclide species indexed  $i = 1, \ldots, n$ in a comparment into which the exogenous inflow rate of the ith species is given by  $I_i(t)(\mu C_i \, \text{day}^{-1})$  and which is subject to first-order removal processes with removal constant,  $\lambda_i^B$  (day<sup>-1</sup>). Then the following system of differential equations describes the decay process in this compartment:

$$
\frac{dA_i}{dt} = -(\lambda_i^R + \lambda_i^B)A_i + \lambda_i^R \sum_{j=1}^{i-1} B_{ij}A_j + I_i(t), \quad i = 1, ..., n \quad (5.1)
$$

where

 $A_i(t)$  = radioactivity ( $\mu$ Ci) of the ith nuclide at time t (day), decay constant (day<sup>-1</sup>) for the ith nuclide, **1**  $\lambda_1^B$  = removal constant (day<sup>-1</sup>) for the ith nuclide,  $B_{i,j}$  = radioactive branching ratio from species j to species i, j < i,  $I_i(t)$  = exogenous inflow rate for species i ( $\mu$ Ci day<sup>-1</sup>).

For the purpose of checking the total amount of activity in the RAGTIME compartments against the value as predicted using the Bateman equations, we may regard the total exogenous inflow rate for species i into the system to be the product of the deposition source  $F_i(t)$  ( $\mu$ Ci m<sup>-2</sup>  $day^{-1}$ ) and the quantity

$$
S_1 A + S_2 A + S_3 A_{\alpha} + S_4 A_{\alpha} = (S_1 + S_2)A + (S_3 + S_4)A_{\alpha},
$$
 (5.2)

where

A = soil surface area  $(m^2)$  assumed for the above-surface food crop,

 $A_{r}$  = soil surface area ( $m^{2}$ ) assumed for the pasture grass g compartment.

Subroutine CHECK of RAGTIME makes a call to subroutine TRAFUN for the purpose of calculation of the total radioactivity in the system at various times. TRAFUN requires that the function representing the exogenous input rate be a step function of time, which dictates that  $F_i(t)$  be a step function. Furthermore, TRAFUN requires that the exogenous input rate be prescribed as a doubly dimensioned array rather than as a FORTRAN function. We thus reserve for Sect. 6.3 an explicit description of the call by CHECK to TRAFUN, in order to make use of our description in Sect. 6.1 of the doubly dimensioned inflow rate matrix FF which is defined in subroutine INPUT and whose values are used to define both the deposition source function  $F_i(t)$  [in FORTRAN,  $F(I,T)$ ] and the doubly dimensioned exogenous input rate matrix P which is used as an input parameter to TRAFUN.

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\pi} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\pi}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt$  $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))\leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))\leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))$  $\label{eq:2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2}$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^n}\frac{1}{\sqrt{2\pi}}\frac{1$  $\langle \bullet \rangle$  $\frac{1}{2}$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\pi}}\frac{dx}{\sqrt{2\$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac$ 

# 6. THE RAGTIME CODE

### 6.1 Input

The subroutine INPUT reads values for user-supplied data required by RAGTIME. The first value read is that for NUMNUC, the number of nuclides in the chain. Next read are the names of the nuclides [NAMNUC(I), I **=** 1 to NUMNUC] and the initial ground deposition source (microcuries per square meter) for each nuclide [FO(I), I **=** 1 to NUM-NUC]. Following these steps values are read for MP and for the arrays

$$
TIMEP(KP)
$$
,  $KP = 1$  to  $MP$ 

and

FF(I,KP), 
$$
I = 1
$$
 to NUMBER, KP = 1 to MP

where

FF(I,KP) = inflow rate of species I (microcuries  $m^{-2}$  day<sup>-1</sup>) for the time interval TIMEP(KP) to TIMEP(KP+1) if KP **<** MP,

 $FF(I, MP)$  = inflow rate at times subsequent to TIMEP(MP).

The matrix FF defines the exogenous input of radioactivity into the system. This matrix is used to define values of the fallout source function  $F_1(t)$  [in FORTRAN, FUNCTIØN  $F(I,T)$ ]. Also FF is used in subroutine CHECK to define the exogenous input rate matrix P as discussed in Sects. 5.2 and 6.3. Next read are the number (NUMBRA) of and values for the radioactive branching ratios. The FORTRAN notation  $B(I,J)$  is used to denote the radioactive branching ratio from species **J** to species **l(J <** I). If NUMBRA **= 0,** no branching ratios are read. If NUMBRA **>** 1, then one card is read for each nonzero branching ratio, the READ statement and its associated FØRMAT being

READ(RDR,50) PARNUC,DAUNUC,BRATIO

50 FORMAT(A8,5X,A8,5X,E13.6)

where PARNUC is the name of the "parent" and DAUNUC the name of the "daughter." For example, the card



is used to input the branching ratio 1.0 from  $210B$ i to  $210P_0$ . The input subroutine assigns the value BRATIØ to the element  $B(I,J)$  of the matrix of branching ratios in such a manner that  $B(1, J)$  represents the branching ratio from the nuclide NAMNUC(J) to NAMNUC(I).

Following input of the branching ratios, information regarding desired output times is read. The entire integration interval is specified as consisting of a number (NINTVL) of subintervals, with INCR(I) denoting the interval between successive output times for the subinter-. val indexed by I. The right endpoint of the subinterval indexed by I is denoted by  $ENDTIM(I)$ . The READ statement and its associated FØRMAT statement for input of these quantities is

READ(RDR,90) INCR(I),ENDTIM(I)

90 FORMAT(E13.6,16)

In subroutine CALCIN, the arrays INCR and ENDTIM are used to define values for the entire array of output times  $\text{TIM}(I)$ ,  $I = 1$  to NTIM.

Values for the radionuclide-dependent parameters listed in Table **6.1** are read next. For definitions of these parameters, see Table 2.1. One card is read for each of these parameters, the cards being read in the order indicated in Table 6.1 for each value of I, with I varying from 1 to NUMNUC. The format for each card is (1OX,E13.7).

We now consider the input of nuclide-independent parameters. The main program of RAGTIME handles any number of radionuclide chains. The first executable statement of MAIN is

### READ(RDR,10) NCHAIN

10 FORMAT(1OX,12)

Parameter symbol	FORTRAN name
$\lambda_i^{\rm R}$	LAMRR(1)
$(E_m)_i$	FSUBM(I)
$(F_f)$	FSUBF(1)
$B_{\text{iv}}$	BSUBIV(I)
$(\tau_{\text{exc}})_{i}$	TAUEXC(I)

Table 6.1 Radionuclide-dependent input parameters for RAGTIME

where NCHAIN is the number of chains to be considered. Following this read statement, the main program makes calls to the subroutine INPUT, OUTDAT, CALCIN, HARVST, CALC, and CHECK in this order for each chain under consideration. In order to avoid the necessity of inputting the nuclide-independent parameters for each chain, a flag, IFLAG, is set in MAIN and passed as a parameter in the call to INPUT [CALL INPUT(IFLAG)] to enable a branch to be made around the input of these parameters for calls subsequent to the first one. Values are read for the nuclideindependent parameters listed in Table 6.2. For definitions of these parameters, see Table 2.1. One card is read for each of these parameters, the format being (10X,E13.7).

The final segment of code in INPUT reads values for certain GEAR subroutine parameters (see Sect. 5.1).

### 6.2 Logical Structure of the Code

After calling subroutine INPUT for input of data related to a given chain, the main program calls OUTDAT for a printout of these data. Next a call is made to subroutine CALCIN, which calculates the values of certain coefficients used in the system of differential Eqs. (2.1) through (2.11). These coefficients, the numbers of the equations in which they occur, and their FORTRAN designations are as follows:

Parameter symbol	FORTRAN name
Α	A
$A_g$	ASUBG
$\sf d$	SMALLD
$\mathsf{D}_{\mathsf{g}}$	<b>DSUBG</b>
$M_{b}$	<b>MSUBB</b>
ρ	RH <sub>0</sub>
$\tau_{\text{beef}}$	TAUBEF
$\tau_{\mathsf{milk}}$	TAUMLK
$^{\tau}$ e, s	TAUES
$\mathfrak{r}_{\mathfrak{g},\mathfrak{r}}$	TAUGR
$\tau_{\rm p\,,\,h}$	<b>TAUPH</b>
$\mathfrak{r}_{r,\mathfrak{d}}$	TAURD
$\mathfrak{r}_{\mathfrak{r},\mathfrak{g}}$	TAURG
$\mathfrak{r}_{\mathsf{s,p}}$	TAUSP
U	U
$V_c$	VSUBC
$t_b^h$ $t_c^h$	TIMBH
	TIMCH

Table 6.2 Nuclide-independent input parameters for RAGTIME

l.



Subroutine CALCIN also defines values of the array of output times TIM(I),  $I = 1$  to NTIM as discussed in Sect. 6.1. Following the call to CALCIN, the main program calls subroutine HARVST in which emergence and harvest times for crop plants are specified. The FORTRAN name for the number of harvests considered is NHARV. Subroutine HARVST assigns values to NHARV and to the arrays EMERGE(I), I **=** 1 to NHARV, and HAR- $TIM(I)$ ,  $I = 1$  to NHARV, where

EMERGE(I) = date (days) for Ith emergence time for plants, HARTIM(I) = date (days) for  $I<sub>th</sub>$  harvest time for plants.

After calling HARVST, MAIN calls subroutine CALC which serves the following functions  $[(1)-(4)]$ :

- (1) Initializes and prints definitions of compartments  $E_i$ ,  $S_i$ ,  $P_i$ ,  $G_i$ ,  $R_i$ ,  $C_i$ ,  $B_i$ ,  $T_i$ ,  $(EH)$ <sub>i</sub>,  $(BH)$ <sub>i</sub>, and  $(CH)$ <sub>i</sub>.
- (2) Assigns values to GEAR subroutine parameters INDEX, TO, HO, and N (Sect. 5.1).
- (3) Assigns values to the arrays TR(INUC), TB(INUC), and PRORAT (INUC), INUC **=** 1 to NUMNUC, where



TB(INUC) = biological half-time (days) of nuclide INUC (a large value is assigned to approximate a biological removal factor of zero),

PRORAT(INUC) **=** (constant) production rate for nuclide INUC.

These arrays are used as input parameters to the subroutine RESDNS, which is called by CALC for calculation (using an explicit solution of the Bateman equations) of the radioactivity level in the holdup compartments  $(BH)$ ; and (CH)<sub>;</sub> as discussed in Sect. 2.2. The array PRØRAT is used to specify the production rate in compartment  $(BH)$ <sub>i</sub> and is therefore assigned zero values since no exogenous input is assumed for this compartment.

(4) Following steps (1) through (3), subroutine CALC executes a loop,

**DO** 4 1 = 1,NTIM

in which the values of the state variables defined by Eqs. (2.1) through (2.11) as well as the holdup compartments (BH)<sub>i</sub> and (CH)<sub>i</sub> are computed and printed. At each time TØUT = TIM(I), a call is made to the GEAR subroutine,

CALL(DIFFUN,PEDERV,N,TO,HO,YO,TOUT,EPS,MF,INDEX)

for calculation of values of the state variables  $E_i$ ,  $S_i$ ,  $P_i$ ,  $G_i$ ,  $R_i$ ,  $D_i$ ,  $C_i$ ,  $B_i$ ,  $T_i$ ,  $H_i$  and (EH)<sub>i</sub>, where  $i = 1$  to the number (NUMNUC) of nuclides in the chain. These values are returned in the array YO, with the same

correspondence between RAGTIME state variable names and GEAR package names as indicated in Sect.  $5.1$ ; for example, the value of  $E_i$  is given by YO[12(i - 1) + 1].

At each output time, CALC calculates and saves in the array TØTUCI the total activity in the system corresponding to each nuclide. We define

 $T\varnothing TUCI(I, INUC) = total activity (microcuries) in the system$ corresponding to nuclide INUC at time TIM(I).

If we assume A square meters of land devoted to crop production and  $A_{\alpha}$ square meters of pasture grass, the appropriate multiplicative factors for converting the values in the various compartments to microcuries are given in Table 6.3. The values of these conversion factors are obvious for all except compartments  $C_i$ ,  $B_i$ , and  $(EH)_i$ . For the milk compartment  $C_i$ , we assume one cow for each  $A_q$  square meters of pasture grass, with an udder capacity of U liters per cow. Similarly, the conversion factor for the beef compartment follows from our assumption of  $M_b$  kilograms of muscle per steer, with one steer per  $A_a$  square meters of pasture grass. The conversion factor  $M_f^0/1000$  for the crop holdup compartment (EH)<sub>i</sub> is based on the definition

 $M_f^0$  = total mass (grams) of crop per A m<sup>2</sup> at harvest time.

The compartment  $M_i^{\dagger}$  is used only in connection with a mass-balance check. This compartment serves to account for the loss to the system of activity from the beef and milk compartments  $B_i$  and  $C_i$  as well as the complement of the activity represented by transfer coefficients  $(\tau_{g,b})_i$  and  $(\tau_{g,c})_i$  with respect to  $\tau_{g,*}$ . The differential equation for  $M_i$  is



Table 6.3 Conversion factors used to convert compartmental concentrations to total activity

$$
\frac{dM_{i}^{i}}{dt} = \tau_{\text{beef}} M_{b} B_{i} + \tau_{\text{milk}} U C_{i} - \lambda_{i}^{R} M_{i}^{i} + \left[ V_{c} / D_{g} - (\tau_{g,b})_{i} M_{b} - (\tau_{g,c})_{i} U \right] G_{i},
$$
\n(6.1)

where

 $M_h$  = mass of muscle on a steer at time of slaughter (kg),  $U = milk capacity of the udder (liters).$ 

The other parameters were defined and discussed in Sects. 2, 3, and 4 of this report. The first two terms on the right-hand side of this equation represent gains to  $M_i^{\text{t}}$  resulting from losses to compartments  $B_i$ and  $C_i$  through slaughter of cattle and milking of cows, respectively. The third term accounts for radioactive decay in  $M_i^1$ . The last term represents the loss to compartments G<sub>i</sub> which is not accounted for by the terms  $(\tau_{g,b})_iG_i$  and  $(\tau_{g,c})_iG_i$  in Eqs. (2.7) and (2.8), respective- $\frac{1}{2}$ .

With MFO as the FORTRAN name for **Mf,** the FORTRAN statement defining  $I\emptyset TUCI(I,1)$  is therefore

TOTUCI(I,1) **=** YO(1)\*A **+** YO(2)\*A **+** YO(3) **+** YO(4)\*ASUBG 1 +  $YO(5)$ \*ASUBG +  $YO(6)$ \*ASUBG +  $YO(7)$ \*U +  $YO(8)$ \*MSUBB 2 **+** YO(9)\*(MFO/1000.) **+** YO(1O) **+** YO(11)\*A **+** YO(13),

(6.2)

the generalization for TOTUCI(I,INUC) being obvious.

After defining values of the array TOTUCI(I,INUC) for a given I and for INUC **=** 1 to NUMNUC, calls are made to subroutine RESDNS for the calculation of values of the beef and milk holdup compartments  $(BH)_i$ and  $(CH)$ <sub>;</sub>. The statements executing these calls are

CALL RESDNS(TIMBH, NUMNUC, TR, TB, B, PRØRAT, QOBEF, QBEF, QWIGL, IDIM)

where TIMBH, TIMCH, NUMNUC, TR, TB, B (matrix of branching ratios) and PRØRAT are as defined previously. On input, the arrays QOBEF and QOMLK contain the values in the beef and milk compartments  $B_i$  and  $C_i$ , respectively, at the current time  $TM(1)$ . The concentration levels ( $\mu$ Ci  $kg^{-1}$ ) which beef and milk would reach if stored for the period of time (days) specified by TIMBH and TIMCH are returned in the arrays QBEF and QMLK, respectively. The array QWIGL contains residence values (µCi-days) on output and is not used by RAGTIME. The parameter IDIM specifies the maximum dimensions for the matrix of branching ratios as defined in RESDNS (REAL BRANCH(IDIM,IDIM)). Following these calls to RESDNS, values of the various compartments, including the holdup compartments for beef and milk, are printed for the current time.

The final section of code within the I-loop determines whether or not the current time, TIM(I), is a harvest time, and if so, reinitializes the state variables  $E_i$ ,  $T_i$ , and (EH)<sub>i</sub> to simulate harvest. First the following call is made to subroutine QUERY:

### CALL QUERY(TIM(I),IANS)

This subroutine searches the array of harvest times, HARTIM, and returns IANS = 1 if TIM(I) is a harvest time, IANS = 0 if not. If TIM(I) is a harvest time, the crop holdup compartment (EH)<sub>i</sub> is reinitialized to the value

total activity (µCi) in compartments E<sub>;</sub> and T<sub>i</sub> AE<sub>i</sub> + T<sub>i</sub> total mass (kg) of crop at harvest time  $M_f^U \times 0.001$ (6.3)

after which the compartments  $E_i$  and  $T_i$  are set to zero. After completion of the I-loop, control returns to the main program.

As pointed out in Sect. 5.1, the system of differential Eqs. (2.1) through (2.11) is defined in subroutine DIFFUN. The GEAR package makes calls to DIFFUN for values of YDOT at various times as described in Sect. 5.1. The deposition source function  $F_i(t)$  of Eqs. (2.1), (2.2),

 $(2.4)$ , and  $(2.5)$  is defined by means of the FORTRAN function  $F(I, T)$ . This function is defined in terms of the inflow rate matrix

FF(I,KP), 
$$
I = 1
$$
 to NUMBER,  $KP = 1$  to MP

as. described in Sect. 6.1..

The final subroutine called by MAIN is subroutine CHECK. Details concerning this subroutine are discussed in the following section.

### 6.3 Subroutine CHECK

The last subroutine called by MAIN is subroutine'CHECK. This subroutine calculates and prints values of



and the percentage error

(T0TUCI(ITIM,INUC)) - ACT(INUC,ITIM)\*100./ACT(INUC,ITIM)

for times TIM(ITIM), ITIM **= 1** to NTIM. The call to TRAFUN is as follows:

CALL TRAFUN(NUMNUC,TR,TB,B,MP,TIMEP,P,NTIM,RTIM,AWIGL,ACT,IDIM)

The meanings of NUMNUC, TR (radioactive half-lives), TB (biological half-times), B (matrix of branching ratios), MP (Sect. 6.1), TIMEP (Sect. 6.1), NTIM (number of output times), and IDIM are as defined previously. The array RTIM is a real array whose values are the same as those for the double precision array TIM of output times. The matrix

P(INUC,KP), INUC **=** 1 to NUMNUC, KP **=** 1 to MP

defines the total exogenous input rate of each nuclide to the system for each of the time intervals TIMEP(KP), KP **= 1** to MP. From the definition of the inflow rate matrix FF (Sect. **6.1)** and our assumption of A square meters of crop production land and  $A_{\alpha}$  square meters of pasture land, it follows that the correct expression for P(INUC,KP) is

P(INUC,KP) **=** FF(INUC,KP)\*((S1 **+** S2)\*A + **(S3** + S4)\*ASUBG)

Subroutine TRAFUN returns in the array ACT the total activity levels as computed using the Bateman equations. After the call to TRAFUN, the values of the arrays TOTUCI and ACT as well as the percentage errors are printed.

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APPENDIX A LISTING OF RAGTIME SOURCE CODE AND JOB CONTROL LANGUAGE

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{$ 

 $\label{eq:2} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3} \frac{1}{\sqrt{2}}\,d\mu\,d\mu\,.$  $\label{eq:2} \frac{1}{2} \sum_{i=1}^n \frac{1}{2} \sum_{j=1}^n \frac{1}{$ 

 $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) & = \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r})$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \frac{1}{\sqrt{2}}\left(\frac{$  $\label{eq:2.1} \frac{d\mathbf{r}}{d\mathbf{r}} = \frac{1}{2} \sum_{i=1}^n \frac{d\mathbf{r}}{d\mathbf{r}} \, \mathbf{r}_i \, \mathbf$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2}d\mu$ 

an<br>Marangan

LEVEL 21.8 ( JUN 74 ) 0S/560 FORTRAN H COMPILER OPTIONS - NAME= MAIN, OPT=02, LINECNT=60, SIZE=0000K, SOURCE, EBCDIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF SUBROUTINE INPUT (IFLAG) ISN 0002 **C**  $\mathsf C$  $\overline{c}$ SUBROUTINE INPUT INPUTS ALL THE DATA  $\mathsf{C}$  $\mathbf c$ COMMON /HOLTIM/ TIMBH, TIMCH TSN 0003 COMMON /INFLOW/ MP, TIMEP(30), FF(15,30) **ISN 0004** ISN 0005 COMMON /BRANCH/ B(15,15) COMMON /DEP/ LAMRR(15), FSUBM(15), TAUEXC(15), FSUBF(15), BSUBIV(15) ISN 0006 COMMON /INDEP/ A, ASUBG, DSUBG, MSUBB, TAUBEF, TAUMLK, TAUES, TAUGR, ISN 0007  $\Delta$ TAUPH, TAURD, TAURG, TAUSP, U, VSUBC, SMALLD, RHO ISN 0008 COMMON /NAMES/ NAMNUC(15) **ISN 0009** COMMON /NUMBRS/ NUMNUC COMMON /TIME/ TIM(365), INCR(30), ENDTIM(30), NINTVL, NTIM ISN 0010 COMMON /SOURCE/ FO(15) ISN 0011 COMMON /GPARAM/ EPS, MF ISN 0012 ISN 0013 COMMON /IODEV / PTR, RDR C  $\bar{c}$  $\mathsf{C}$ DOUBLE PRECISION NAMNUC, PARNUC, DAUNUC, TIM, EPS ISN 0014 ISN 0015 INTEGER ENDTIM.PTR.RDR ISN 0016 REAL MSUBB, INCR, LAMRR  $\mathbf c$  $\mathsf C$  $\mathsf C$  $C$ \*\*\*  $C***$ NUMNUC - THE NUMBER OF NUCLIDES IN THE CHAIN BEING STUDIED  $C***$ READ (RDR, 10) NUMNUC ISN 0017 ISN 0018  $\pm 10$  FORMAT (I5)  $C***$ NAMNUC - ARRAY OF THE NAMES OF THE NUCLIDES IN THE CHAIN.  $C***$  $C***$ - INITIAL GROUND DEPOSITION SOURCE FOR NUCLIDE(I)  $F<sub>0</sub>$  $C$  \* \* \* WHERE I VARIES FROM 1 TO THE NUMBER OF NUCLIDES **IMICROCURIES PER SQUARE METERI**  $C***$  $C$ \*\*\* ISN 0019  $00$  30 I = 1, NUMNUC READ (RDR, 20) NAMNUC(I), FO(I) ISN 0020 FORMAT (A8, E13.6) ISN 0021  $20$ 50 CONTINUE ISN 0022  $\mathbf{c}$  $C***$ INFLOW RATES FOR VARIOUS SPECIES  $C***$  $C***$ READ VALUES FOR THE ARRAYS  $C***$  $C***$ TIMEP(KP), KP=1 TO MP, AND  $C***$ FF(I,KP), I=1 TO NUMNUC, KP=1 TO MP, WHERE  $C$ \*\*\* FF(1,KP) = INFLOW RATE OF SPECIES I (UCI/M\*\*2-DAY) FROM  $C***$  $C***$ TIMEP(KP) TO TIMEP(KP+1) IF KP .LT. MP  $C$ \*\*\* AND FELL, MPI IS THE RATE AT TIMES SUBSEQUENT TO  $C***$ TIMEP(MP). ISN 0025 READ (RDR.200) MP ISN 0024 200 FORMAT (15)

00 201 1=1, NUMNUC<br>00 201 KP=1, MP ISN 0025 ISN 0026 201 READ (RCR, 202) TIMEP (KP), FF(I, KP) ISN 0027 ISN 0028 202 FORMAT(E13.6,2X, E13.6)  $\mathbf c$ C c MATRIX CONTAINING BRANCHING RATIOS INITIALIZED TO ZERO  $\mathbf c$  $\mathbf c$  $\mathbb C$  $C \neq \pm \pm \pm \sqrt{2}$  $C$ \*\*\*  $\mathbf{R}$ - MATRIX CONTAINING THE BRANCHING RATIOS.  $C \# \# \#$ ISN 0029  $DO 40 I = 1, NUMNUC$ **ISN 0030**  $DO 4O J = 1$ , NUMNUC ISM 0031  $B(I, J) = 0.0$ ISN 0032 40 CONTINUE  $\mathbf{C}$ Ċ  $\mathsf{C}$ BRANCHING RATIOS FILLED IN MATRIX  $\mathbf c$ \*  $\mathbf c$  $\mathsf{C}$  $C***$  $C***$ PARNUC - PARENT NUCLIDE  $C$ \*\*\* **DAUNUC** - DAUGHTER NUCLIDE  $C***$ BRATIO - BRANCHING RATIO  $C***$ PARNOD - INDEX INTO MATRIX B  $C***$ REPPESENTS PARENT NUCLIDE  $f$  \*\*\* DAUNOD - INDEX INTO MATRIX B  $C***$ REPRESENTS DAUGHTER NUCLIDE  $C$ \*\*\* NUMBRA - NUMBER OF NONZERO BRANCHING RATIOS  $C$ \*\*\* ISN 0033 READ (RDR, 10) NUMBRA ISN 0034 IF (NUMBRA.EQ.0) GO TO 160 ISN 0056 DO 70  $I = 1$ , NUMBRA ISN 0037 READ (RDR,50) PARNUC, DAUNUC, BRATIO ISN 0038  $50$ FORMAT (A8,5X,48,5X,E15.6)  $\mathsf{C}$  $\mathsf{C}$ LOOP TO SET APPROPRIATE INDICES INTO MATRIX 8 C  $\mathbf c$  $\mathsf{C}$ C ISN 0039 00 60 J = 1, NUMNUC IF(PARNUC.EQ.NAMNUC(J)) PARNOD = J<br>IF(DAUNUC.EQ.NAMNUC(J)) DAUNOD = J ISN 0040 ISN 0042 ISN 0044 CONTINUE 60 ISN 0045 B(DAUNOD, PARNOD) = BRATIO ISN 0046 70 CONTINUE ISN 0047 80 CONTINUE  $C \times \times \times$ NINTVL - NUMBER OF INTERVALS SPECIFYING OUTPUT TIMES  $C***$  $C***$ INCR(I) - STEPSIZE FOR INTERVAL I  $C***$ ENDTIM(I) - RIGHT ENDPOINT OF INTERVAL I (DAY) NOTE THAT ENDTIM(1) SHOULD BE AN INTEGRAL MULTIPLE OF INCR(1)  $C$ \*\*\*  $C***$ AND FOR I GREATER THAN 1, ENDTIM(I) - ENDTIM(I-1) SHOULD BE AN  $C****$ INTEGRAL MULTIPLE OF INCRIII.











 $\mathcal{A}^{\mathcal{A}}$ 

 $\sim$ 

 $\mathcal{A}^{\mathcal{A}}$ 





 $\frac{1}{2}$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\frac{1}{2}$ 

 $\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 

 $\mathcal{L}_{\text{eff}}$ 

 $\frac{1}{2}$ 

 $\sim 10^6$ 

 $\hat{\boldsymbol{\beta}}$ 

 $\hat{\mathcal{A}}$ 

 $\hat{\boldsymbol{\beta}}$ 

 $\frac{c}{c}$  $00 2 1=1, NINTVL$ <br>  $[M1 = I-1$ <br>  $IF(I - EQ-1) START=0.0$  $-15N$  0026 ISN 0027 ISN 0028 IF(I.NE.1) START= ENDTIMIIM1) ISN 0030 TSN 0052 NUMSUB = (ENOTIM(I)-START) / INCR(I)  $NTIM = NTIM + NUMSUB$  $\mathsf{C}$ ISN 0034<br>ISN 0035  $003$   $J=1, NUMSUB$ .<br>II = NPREV + J  $5$  TIM(II) = START + J\*INCR(I) ISN 0056  $\mathsf{C}$ NPREV = NUMSUB + NPREV ISN 0037  $\sim 20\,$ 2 CONTINUE ISN 0058  $\mathsf{C}$  $\mathsf{C}$ - RETURN ISN 0039  $\mathsf{EMD}$ ISN 0040






65

 $\sim$ 

C TRILUIDI=RAD, HALF-LIFE (DAY) OF HUCLIDE INUC.<br>C TRILUIDI=BIO, HALF-LIFE (DAY) OF NUCLIDE INUC. USE LARGE VALUE TO C APPROXIMATE A BIO. PEMBVAL FACTOR OF ZERO. ISN 0073 L0G2=DL0G12.0001 ISN 0074 OU 300 ' PNUC=1, NUMNUC TRIINUCJ=LOG2/ORLEtLANAR(INUC)) ISN 0075 ISN 0076 TBIINUCJ=1.0E50 C PROPATITNUCJ=CONSTANT PRODUCTION RATE FOR NUCLIDE THUD. ISN 0077 PRORAT(INUC)=0.0 ISN 0078 200 CONTINUE  $\mathcal{L}$ ISN 0079  $OD 4 1=1+NTIM$ IF IK .NE. KOUNTE OP TO 160 TSN 0080 C PRINT HEADING T5N 0082 WRITE (PTR, I) (MAMNUCIJ), J=1, NUMNUC) FORMAT (FIGONTENTS OF COMPARTMENTS AT VARIOUS TIMES',//, ISN 0085 WRITE (PTR.2) ESN 0084 ISM 0085 2 FORMAT(\*OTIME\*,T17,\*E\*,T28,\*S\*,T39,\*P\*,T50,\*G\*,T61,\*P\*,T72,\*C\*, T83, '8', T94, 'T', T105, 'EH!, T116, 'SH', T125, 'CH') ISN 0086 WRITE (PTP,3) ISN 0087 3 FURMATE\* (DAYS)\*+T13+\*(UCT/SQLM)\*+T24+\*(UCI/SQLM)\*+T37+\*(UCT)\*+  $C = T46 + 10C1750 + 1111 + 157 + 10C1750 + 111 + 168 + 10C17111 + 130 + 10C17K611$  $(1591, 1001)$ , TI03, TOCI/KGI (, TI14, TOCI/KGI (, TI23, TOCI/L) () C IF T=1, PRINT VALUES OF COMPARTMENTS AT TIME ZERD. IF (1.NE.1) GO TO 200 ISM 0088 TSN 0090  $T1 \text{ME} = 0.000$ C FIRST NUCLIDE IN CHAIN WRITE (PTR, 11) TIME, YOI1), YO(2), YO(3), YO(4), YO(5), YO(7), ISN 0091 YO(8), YO(10), YO(9), OBEF(1), ONLK(1) IF (NUMNUC.EQ.1) GO TO 200 1.94 0092 C REMAINING NUCLIDES IN CHAIN **ESN 0094** DO 201 INUC=2, NUMNUC NPREV=12\*fINUC-L) TSN 0095 TSN 0096 WRITE (PTR,12) YO(NPREV+1), YO(NPREV+21, YO(NPREV+3), W YOLNPREV+41.YOLNPREV+51.YOLNPREV+71. YOLNPREV+81.<br>W YOLNPREV+101.YOLNPREV+91.QBEFLINUC1.QMLKLINUC1 ISN 0097 201 CONTINUE ISN 0098  $200 K = 0$ C IF I=1, ADD 1 TO K TO ACCOUNT FOR PRINTING COMPARTMENT VALUES C AT TIME ZERO.  $15N.0099$ IF (I.EQ.1) K=K+1 160 CONTINUE ISN 0101  $TOUT = TIM11$ ISM 0102 ISN 0105 TOWT = TOUT CALL GEARIDIFFUN, PEDERV, N. TO, HO, YO, TOUT, EPS, MF, INDEX) ISN 0104 ISN 0105 IF (INDEX.EQ.0) GO TO 6 WRITE (PTR.7) TOWT.INDEX 15N 0107 7 FORMAT( OINTEG, WAS NOT COMPLETED TO TOWT="+E10.3,", INDEX= "+13) **ISN 0108** ISN 0109  $GO$   $TO$   $B$  $\mathsf C$  $\mathfrak{C}$  $\xi$ THE FOLLOWING STATEMENTS ARE USED TO CALCULATE THE TOTAL AMOUNT OF  $\dot{\mathbb{C}}$ PADIOACTIVITY IMICROCURTES) IN THE SYSTEM FOR EACH NUCLIDE IN THE  $\mathbb C$ CHAIN.  $\tilde{c}$  $\mathbb C$ TOTUCILI, INUCI = RADIOACTIVITY FOR NUCLIDE WITH INDEX JNUC  $\bar{C}$ 



 $\bar{z}$ 

 $\sim 10^7$ 

 $\alpha$ 

 $\mathcal{L}$ 

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LEVEL 21.8 ( JUN 74 ) 0S/360 FORTRAN H COMPILER OPTIONS - NAME=  $MAIN, OPT=02, LIMECMT=60, SIZE=0000K,$ SOURCE, EBCOIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF ISN 0002 SUBROUTINE DIFFUNIN, T, Y, YOOTI  $\mathbf c$  $\mathbf c$  $\mathbf c$  $\mathbf c$ COMPUTES THE RIGHT HAND SIDE OF YDDT=F(Y,T)  $\mathbf C$  $\mathsf{C}$  $\mathsf{c}$ ISN 0003 DIMENSION TAUPT(15) ISN 0004 COMMON /INDEP/ A, ASUBG, DSUBG, MSUBB, TAUBEF, TAUMLK, TAUES, TAUGR, TAUPH, TAURD, TAURG, TAUSP, U, VSUBC, SMALLD, RHO ISN 0005 COMMON/LMDA/LAMR (15), LAMC(15), LAMB(15), LAMA(15), C LAMS(15), LAMG(15) COMMON /DEP/ LAMRR(15), FSUBM(15), TAUEXC(15), FSUBF(15), SSUBIV(15) ISN 0006 ISN 0007 COMMON /PARAM/ TAUGC (15), TAUGB (15) COMMON /NUMBRS/NUMNUC ISN 0008 ISN 0009 COMMON /BRANCH/ B(15,15) **TSN 0010** COMMON /IODEV / PTR, RDR  $\mathsf C$  $\mathbf c$  $\mathbf c$ ISN 0011 DOUBLE PRECISION T, YINI, YOOTINI ISN 0012 REAL LAMBH, LAMCH, MSUBB, LAMRR, II, LAMR, LAMC, LAMB, LAMA, LAMS, LAMG, IIPRIM, LAMPI  $\star$ ISN 0013 INTEGER RDR, PTR  $\mathsf C$  $\mathbf{c}$  $\mathbf c$ THE STATE VARIABLES ARE  $\mathsf{C}$  $\mathsf C$  $Y(NPREV+1) = E$  $\mathsf{C}$  $Y(NPREV+2) = S$  $\mathbf c$  $Y(NPREV+3) = P$  $\mathsf{C}$  $Y(NPREV+4) = G$  $\mathsf{C}$  $Y(NPREV+5) = R$  $\mathfrak{c}$  $Y(NPREV+6) = 0$  $\mathsf{C}$  $Y(NPREV+7) = C$  $\mathsf C$  $Y(NPREV+8) = 8$  $\ddot{\text{c}}$  $Y(NPREV+9) = EH$  $\mathsf{C}$  $YINPREV+101 = T$  $\epsilon$  $Y(NPREV+11) = H$  $Y(NPREV+12) = MPRIME$  $\mathbf c$  $\mathsf C$ WHERE NPREV =  $0, 1, 2, \ldots$ , NUMNUC-1  $\mathbf c$  $\mathsf C$  $\tilde{c}$ TIME (T) IS SOMETIMES REQUIRED TO BE IN SINGLE PRECISION (X). C ISN 0014  $X = T$ ISN 0015 CALL SVALIX, S1, S2, S3, S4) ISN 0016 CALL TIMDEP(X, TAUPT)  $\mathbf{c}$ ISN 0017 DO 1 I=1, NUMNUC C NPREV =  $NO$ . OF PREVIOUS FOUATIONS  $NPREV = (1-1)*12$ ISN 0018 C CALCULATE CONTRIBUTION FROM PREDECESSORS IN THE CHAIN. ISN 0019  $SUM1 = 0.0$ **ISN 0020** SUM2 =  $0.0$ 



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### LEVEL 21.8 t JUN 74 **1 OS/360** FORTRAN H



LEVEL 21.8 **(** JUN 74 ) 0S/360 FORTRAN H COMPILER OPTIONS - NAME= MAINOPT=O2,LINECNT=60,SIZE=OOOOK, SOURCE,EBCDIC,NOLIST,NODECK,LO D,MAP,NDED IT,ID,NoXREF ISN 0002 SUBPOUTINE CHECK C CALCULATES AND PRINTS VALUES OF C C TOTUCI(ITIM,!NUC) **=** TOTAL ACTIVITY DUE TO NUCLIDE INUC AT TIME ITIM C AS CALCULATED BY SUBROUTINE CALC USING THE CALC USING THE CALCULATED BY SUBROUTINE C GEAR SUBROUTINE C ACT(INUC<sub>t</sub> ITIM) = TOTAL ACTIVITY DUE TO NUCLIDE INUC AT TIME ITIM<br>C AS CALCULATED BY SUBROUTINE TRAEUN, USING THE AS CALCULATED BY SUBROUTINE TRAFUN, USING THE C BATEMAN EQUATIONS C AS WELL AS THE PERCENTAGE ERROR C C (TOTUCI(ITIM,INUC) - ACT(TNUC,ITIMIU\*100. **/** ACT(IN'ICITIMI C C FOR TIMES TIMCITIM), ITIM=1 TO **NTIM.** r ISN 0003 DIMENSION TR(15),TB(15),ACT(15,365),P(15,30),RELER(15),RTIM(365),<br>  $*$  AWIGL(15,365)  $\boldsymbol{\pi}$ ISN 0004 COMMON /INFLOW/ MP,TIMEP(30),FF(15,301 **ISN 0005 COMMON /BRANCH/ B(15,15)**<br>ISN 0006 COMMON /MCHECK/ TOTUCT(3 **ISN** 0006 COMMON /MCHECKI TrTUCI(365,151 ISN 0007 **COMMON /DEP/ LAMPR(15),FSUBM(15),TAUEXC(15),FSUBF(15),BSUBIV(15)**<br>ISN 0008 COMMON /INDEP/ A,ASUBG,DSUBG,MSUBB,TAUBEF,TAUMLK,TAUES,TAUGR, COMMON /INDEP/ A, ASUBG, DSUBG, MSUBB, TAUBEF, TAUMLK, TAUES, TAUGR, \* TAUPHTA'JRDTAURG,TAUSP,U,VSUBC,SMALLD,RHO I SN 0009 COMMON /NUMBRS/ NUMNUC **ISN** 0010 COMMON /TIME/ TIM(365?,1NCR(30),ENDTIM(3O),NINTVL,NTIM **ISN** 0011 COMMON **/IODEV** / PTR,RDR **C ISN 0012** DOUBLE PRECISION TIM, LOG2<br> **ISN 0013** INTEGER ENDTIM, PTR, RDR **ISN 0013** INTEGER ENDTIM,PTR,RDR<br>ISN 0014 9EAL MSUBB,INCR,LAMRR REAL MSUBB, INCR, LAMRR C IDIM IS THE MAXIMUM FIRST D!MENSION FOR THE ARFAYS ACT, P, AND AWIGL. C IT CORRESPONDS TO THE MAXIMUM NUMBER OF NUCLIDES IN A CHAIN. ISN 0015 DATA IDIM **/15/**  $\mathcal{C}$ C PRINT HEADINGS FOR TIME, TOTAL ACTIVITY COMPUTED BY THE GEAR C SUBROUTINE, TOTAL ACTIVITY COMPUTED USING BATEMAN EQUATIONS, SUBROUTINE, TOTAL ACTIVITY COMPUTED USING BATEMAN EQUATIONS, AND C RELATIVE ERROR. C ISN 0016 WRITE (PTP,100) ISN 0017 **100** FORMAT ('I',52X,'COMPARISON OF TOTAL ACTIVITY' / \* '0',1IOX,'TIME (DAYSI',9ZX,'TOTAL ACTIVITY (MICROCURIESI', \* 12X,'TOTAL ACTIVITY (MICROCURIFS)',8X,'PERCENTAGE ', \* 'ERROR' **/ \*I** ',35X,'\*\*\* GEAR SUBROUTINE \*\*\*',17X,'\*\*\* BATEMAN ', \* 'EQUATIONS \*\*\*'? C C C DEFINE INPUT PARAMETERS FOR SUBROUTINE TRAFUN C C TP(INUC) =RADIOACTIVE HALF-LIFE (DAY) OF NUCLIDE I. C TB(INUC) =BIOLOGICAL HALF-LIFE (DAY) OF NUCLIDE I (USE LARGE VALUE C **TC** APPROXIMATE A BIOLOGICAL REMOVAL FACTOR OF ZERO.) C P(INUC,KPI=SOURCE STRENGTH (MICROCURIES/DAYI FOR NUCLIDE I C FROM TIMEP(KP) TO TIMEP(KP+1) IF KP .LT. MP AND P(INUC, MP) = C SOURCE STRENGTH AT TIMES SUBSEQUENT TO TIMEPIMP). BRANCH(I,J)



LEVEL 21.8 **(** JUN 74 **)** OS/350 FORTRAN H COMPILER OPTIONS - NAME=  $MAIN, OPT=02, LINECNT=60, SLZE=0000K,$ ISN 0002 C C MICROCURIE-CAYS QWIGL OF N SPECIES OF A RADIONUCLIDE C CHAIN. C (rAYS) FOR THE I-TH NUCLIDE AND CONSTANT PRODUCTION  $\mathbf c$ C QADIOACTIVE HALF-LIFE OF THE I-TH NUCLIDE. THE INITIAL  $\mathcal{C}$ C FRACTION OF SPECIES J WHICH DISINTEGRATES TO SPECIES I C WHERE J IS LESS THAN I. THUS ALL NON-ZERO ENTRIES IN  $\mathbf{C}$ Ç C ALL DIMENSIONS OF SIZE 20 CORRESPOND TO N, THE NUMBER OF C RADIOACTIVE SPECIES IN THE CHAIN. C C c<br>c SOURCE, EBCOIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF SUBROUTINE RESONS(T,N,TR,TB, BRANCH, P,Q0,Q,QWIGL, IDIM) THIS SUBROUTINE COMPUTES THE MICROCUP.IES **0** AND THE CHAIN. EVALUATION IS AT TIME T (DAYS) IN A COMPARTMENT WITH FIRST-ORDER PEMOVAL PROCESSES WITH HALF-TIME TB(Il RATE P(1) (MICROCURIES/DAY). TR(I) (DAYS) IS THE BURDEN IS QO(I) (MICROCURIES). BRANCH(I, J) IS THE BRANCH ARE BELOW THE MAIN DIAGONAL. IDIM IS THE MAXIMUM FIRST DIMENSION FOR THE ARRAYS ACT, P, AND AWIGL. IT CORRESPONDS TO THE MAXIMUM NUMBER OF NUCLIDES IN A CHAIN. ISN 0003 I SN 0004 ISN 0005 ISN 0007 ISN 0008 ISN 0009 ISN 0010 ISN 0011 ISN 0012 ISN 0013 ISN 0014 **I** SN 0015 ISN 0016 ISN **0017 ISN** 0019 ISN 0020 ISN 0021 ISN 0023 ISN 0024 ISN 0025 ISN 0026 ISN 0027 ISN 0029 **ISN** 0030 REAL TR(N), TB(N), BRANCH(IDIM,IDIM), P(N), QO(N), Q(N), QWIGL(N) DOUBLE PRECISION LM(20),LMRf20),D(20),C(20,20),  $$$   $LOG2$ , TEMPQ, TEMPQW, EXLI, EX1LI, EXPFUN, EXPF1 IF (T.GT.O.0) GO TO 10  $DO 5 I=1. N$ **Q(1)=00(1)** OWIGL(I)=0.O **5** CONTINUE GO TO 120 10 LOG2=DLOG12.0DO) C COMPUTE DECAY AND REMOVAL CONSTANTS FROM HALF-TIMES. **DO** 20 I=l,N LMR(I)=LOG2/DBLE(TR(I)) LM(I)=LOG2/DBLEITB(I)) **+** LMR(I) 20 CONTINUE C IF TWO LM(I) ARE NEARLY EQUAL, SEPARATE THEM. C C SKIP SEPARATION ROUTINE IF N=1. IF(N.EQ.1) GO TO 45 C C BEGINNING OF SEPARATION ROUTINE.. C  $N1=N-1$ C KODE IS A SWITCH FOR WHICH THE VALUE I MEANS ANOTHER C PASS SHOULD BE MADE. KODE=I 25 IF (KODE.NE.1) GO TO 45 KODE=O C BEGIN PASS. **00** 40 K=1,NI  $K1=K+1$ DO 35 L=KI,N C IF LM(L) AND LM(KI ARE NEARLY EQUAL, SEPARATE THEM. IF (DABS(LM(L)/LM(KI-l.ODO\*.GE.1.0O-61 GO TO 35 LM(L)=LM(K)\*I.O0001DO  $K$ OD $F=1$ 

ISN 0031

35 CONTINUE



 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{$ 

 $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}))\leq \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}))$ 

 $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}),\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}))$ 

 $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}})) = \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$  and  $\mathcal{L}^{\text{max}}_{\text{max}}$ 

#### LEVEL.21.8 ( JUN 74 )

#### OS/360 FORTRAN H

## COMPILER OPTIONS - NAME= MAIN, OPT=02,LINECNT=60,SIZE=0000K,<br>SQURCE,EBCOIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,NOXREF<br>DOUBLE PRECISION FUNCTION EXPEUNITI ISN 0002





LEVEL 21.8 ( JUN 74 *I* OS/360 FORTRAN H

#### COMPILER OPTIONS - NAME=  $MAIN<sub>0</sub>OPT=02<sub>0</sub> LINECNT=60<sub>0</sub> SIZE=0000K<sub>0</sub>$ SOURCE, EBCDIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF ISN 0002 SUBROUTINE TRAFUNIN, TR, TB, BRANCH, MP, TIMEP, P, MA, TIMEA, AWIGL, ACT, \* IDIM) C TRAFUN SUGGESTS TRANSFER FUNCTION. C WE ARE CONSIDERING N RADIOACTIVE SPECIES **IN** A CHAIN IN A BIOLOGICAL C COMPARTMENT. TRII) AND TB(Il ARE THE RADIOACTIVE HALF-LIFE (DAYS) C AND BIOLOGICAL HALF-TIME (DAYS), RESPECTIVELY, OF THE I-TH SPECIES <sup>C</sup>**IN** THE COMPARTMENT. BPANCH(I,J) IS THE BRANCHING RATIO OF SPECIES C J TO SPECIES I, WHERE J IS LESS THAN I. THE INFLOW RATE OF EACH **C SPECIES** IS GIVEN AS A DISCRETE FUNCTION OF TIME BY THE ARRAYS C TIMEP (DAYS) **AND** P (MICROCURIES/DAY). P(I,KP) IS THE INFLOW RATE C OF SPECIES I FROM TIMEP(KP) TO TIMEP(KP+1), AND P(I,MP) IS THE C RATE AT TIMES SUBSEQUENT TO TIMEP(MP). AWIGL(IKAI IS THE C CUMULATED ACTIVITY (MICROCURIE-DAYSI IN THE COMPARTMENT UP TO C T!MEA(KA). THE TIME ARRAYS MUST BE ARRANGED **IN** INCREASING ORDER. C ACT(I,KA) IS THE ACTIVITY FOR NUCLIDE I (MICROCURIES) IN THE C COMPARTMENT AT TIMEA{KA). C  $\mathsf{C}$ C IT CORRESPONDS TO THE MAXIMUM NUMBER OF NUCLIDES IN A CHAIN. C C ISN 0003 **ISN** 0004 ISN 0005  $\epsilon$  $\mathsf{C}$ C  $\mathbf{c}$ C  $\mathsf{C}$ ISN 0006 ISN 0007 **ISN** 0008 ISN 0009 ISN 0010 ISN 0011 ISN 0012 **ISN** 0013 ISN 0014 I SN 0015 C IF KP=l, SET INITIAL TOTAL ACTIVITY IN THE SYSTEM EQUAL TO THAT C DETERMINED BY FOIL1, I=1 TO N AND S1, S2, S3, S4. ISN 0016 C C CALCULATE TOTAL INITIAL ACTIVITY (MICROCURIES) IN RAGTIME COMPARTMENT C E,S,G AND R IDIM IS THE MAXIMUM FIRST DIMENSION FOR THE ARRAYS ACT, P, AND AWIGL. THE MAXIMUM DIMENSION 20 FOR THE ARRAYS PTEMP, ATEMP AND AWTEMP CORRES PONDS TO N (THE NUMBER OF RADIOACTIVE NUCLIDES IN THE CHAIN). REAL TR(N),TB(N),BRANCH(IDIM,IDIM|,ACT(IDIM,365) REAL TIMEP(30),P(IDIM,30),TIMEA(MA),AWIGL(IDIM,3651 REAL PTEMP(20),ATEMP(20),AWTEMP(20) FOR EACH TIMEP(KPI AND THE CORRESPONDING COLUMN P(\*,KP) OF RATES, USE RESID ITERATIVELY TO CALCULATE THE CONTRIBUTION TO AWIGL(\*,KA) AT TIME TIMEA(KA). FIRST INITIALIZE AWIGL AND ACT TO ZERO. COMMON /INDEP/ A, ASURG, DSUBG, MSUBB, TAUBEF, TAUMLK, TAUES, TAUGR, \* TAUPH, TAURD, TAURG, TAUSP, U, VSUBC, SMALLD, RHO COMMON /SOURCE/ FO(15) CALL ZEROM(IDIM, MA, AWIGL CALL ZEROM(IDIM, MA, ACT 00 25 KP=1,MP DO **10** I=l,N PTEMP(I)=P(I,KP) **10** CONTINUE DO 20 KA=I,MA CALL ZEROV(N,ATEMP) IF (KP .NE. **1)** GO TO 40 TZERO **=** 0.0 CALL SVAL(TZERO, S1, S2, S3, S4) **00** 41 I=1,N 41 ATEMP(I) = **(fSIS+2)\*A +** (S3+S4)\*ASUBGI \* FOIl) 40 CALL ZEROV(N,AWTEMP) I SN **0018** ISN 0019 I SN 0020 **I** SN 0021 I SN 0022

ISN 0023 ISN 0024 **ISN** 0026 ISN 0028

Tl=TIMEPIKPI

IF (TL.GT.TIMEA(KAJ) GO TO 20<br>TE (KP.(T.MP) 72=TIMEP(KP+1) IF IKP.LT.MP) T2=TIMEP(KP+1) IF (KP.EQ.MP) T2=TIMEA(KA)



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### LEVEL 21.8 ( JUN 74 )

#### OS/360 FORTRAN H

### COMPILER OPTIONS - NAME= MAIN, OPT=02, LINECNT=60, SIZE=0000K,<br>SOURCE, EBCOIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF<br>SUBROUTINE ZEROM(N, M, A) ISN 0002



#### 05/560 FORTRAN H

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## COMPILER OPTIGNS - NAME= MAIN, OPT=02, LINECNT=60, SIZE=0000K,<br>SOUPCE, EBCOIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF<br>SUBROUTINE ZEROV(N, V) ISN 0002





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### OS/360 FORTRAN H





ISN 0013 END

COMPILER OPTIONS - NAME= MAIN, OPT=02, LINECNT=60, SIZE=0000K, SOURCE, EBCOIC, NOLIST, NODECK, LOAD, MAP, NOEDIT, ID, NOXREF C C RAGTIME C ...........-- **- ---** C C PROGRAM AUTHORS **:** J.C.PLEASANT, L.M.MCDOWELL-BOYER, AND G.G.KILLOUGH C HEALTH AND SAFETY RESEARCH DIVISION<br>C COMPARENT ON A RIDGE NATIONAL LABORATORY C CONSTRUCT ON BAK RIDGE NATIONAL LABORATORY<br>CONSTRUCT OAK RIDGE, TENNESSEE 37830 OAK RIDGE, TENNESSEE  $\epsilon$ **C --- -- --** C C PTR IS USED TO REPRESENT THE UNIT NUMBER ASSOCIATED WITH THE LINE<br>C PRINTER, RDR IS USED TO REPRESENT THE UNIT NUMBER ASSOCIATED WITH C PRINTER, RCP IS USED TO REPRESENT THE UNIT NUMBER ASSOCIATED WITH C THE CARD READER. THE CARD READER.  $\mathsf C$ ISN 0002 COMMON / IODEV / PTR<sub>7</sub>RDR<br>ISN 0003 INTEGER PTR<sub>7</sub>RDR INTEGER PTR, RDR<br>RDR = 5  $\begin{array}{ccc} \text{ISM} & 0004 & \text{RDR} & = & 5 \\ \text{ISM} & 0005 & \text{PTR} & = & 6 \end{array}$ ISN 0005 PTR **= 6 C iSN** 0006 IFLAG **= 0**  $\frac{c}{c}$ 

C. IFLAG IS A PARAMETER PASSED IN SUBROUTINE INPUT WHICH DIRECTS<br>C. THE FLOW OF THE PROGRAM. IF IFLAG IS SET TO ZERO, THE ENTIRE C THE FLOW OF THE PROGRAM. IF IFLAG IS SET TO ZERO, THE ENTIRE<br>C SUBROUTINE IS EXECUTED AND IFLAG IS SET EQUAL TO ONE. THIS C SUBROUTINE IS EXECUTED AND IFLAG IS SET EQUAL TO ONE.<br>C FNABLES A BRANCH TO BE MADE AROUND THE PORTION OF CODE C ENABLES A BRANCH TO BE MADE AROUND THE PORTION OF CODE THAT WPUTS<br>C THE NUCLIDE INDEPENDENT PARAMETERS ON SUCCESSIVE CALLS FOR THE C THE NUCLIDE INDEPENDENT PARAMETERS ON SUCCESSIVE CALLS FOR THE C VARIOUS CHAINS BEING STUDIED. VARIOUS CHAINS BEING STUDIED. C

#### **ISN 0007** READ (RDR,10) NCHAIN<br>ISN 0008 10 FORMAT (10X,12) ISN 0008 **10** FORMAT (1OX,12) **C ISN 0009 DO 20 I = 1, NCHAIN**<br> **ISN 0010** CALL INPUT (IFLAG) **ISN 0010** CALL INPUT iIFLAGI CALL OUTDAT ISN 0012<br>
ISN 0012 CALL CALCIN<br>
ISN 0013 CALL HARVST **ISN 0013** CALL HARVST<br>ISN 0014 CALL CALC **ISN 0014** CALL CALC<br> **ISN 0015** CALL CHEC **ISN 0015** CALL CHECK<br>ISN 0016 20 CONTINUE **20 CONTINUE C**

**ISN** 0017 STOP

**ISN 0018** 

LEVEL 21.8 ( JUN 74 **) OS/)60** FORTRAN H

 $\label{eq:2} \frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{$ 

 $\label{eq:2.1} \frac{d\mathbf{r}}{dt} = \frac{1}{2} \left( \frac{d\mathbf{r}}{dt} + \frac{d\mathbf{r}}{dt} \right) \left( \frac{d\mathbf{r}}{dt} + \frac{d\mathbf{r}}{dt} \right) \left( \frac{d\mathbf{r}}{dt} + \frac{d\mathbf{r}}{dt} \right)$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{d\mu}{\sqrt{2\pi}}\left(\frac{d\mu}{\mu}\right)^2\frac{d\mu}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{d\mu}{\sqrt{2\pi}}\left(\frac{d\mu}{\mu}\right)^2\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{\sqrt{2\pi}}\frac{d\mu}{$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{$ 

 $\label{eq:2} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) = \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \end{split}$ 

### Job Control Language (JCL) for RAGTIME

Job control language varies from one computer installation to another. For execution of RAGTIME on the IBM 360/91 at Oak Ridge National Laboratory, the following JCL arrangement has been used:

//jobname **JOB** (charge no.),'X-1O 7509 PLEASANT' //\*CLASS CPU91=44S,I0=2.8,REGI0N=270K  $\overline{X}$ RØUTE  $\overline{X}$ EQ CPU91 // EXEC FØRTHCLG, REGION.GØ=270K, PARM.GØ='EU=-1' //!ORT.SYSIN DD *\_\**

source decks (RAGTIME MAIN and subroutines)

//LKED.GEAR **DD** DSN=T.GGK05716.GEAR,DISP=SHRUNIT=SPDA, *//* DCB=(RECFM=FB,LRECL=80,BLKSIZE=800) //LKED.SYSIN **DD** m INCLUDE GEAR

//GO.FTO3FOO1 DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=1000) //GO. FTO1FOO1 DD **\***

data deck

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The underline *(\_)* is used to indicate a space. The JCL shown above makes use of compiled code for GEAR stored in the system as a catalogued data set and made available to the Linkage Editor through the JCL statements comprehended by the brace. If the subroutines of the GEAR package are to be compiled along with RAGTIME, they should be included with the source decks and the JCL statements in the brace deleted. The additional compilation time would require that the limits on the CLASS card be revised. We note also that other sets of input data (e.g., radionuclide chains with more than two species or multiple problems within one job) will require longer running times. Moreover, the running times will vary greatly with the model of IBM system and other local factors.

 $\label{eq:2} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$ 

 $\label{eq:2} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1}{\sqrt{2}}\sum_{j=1}^n\frac{1$  $\label{eq:2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2}$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\frac$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac$ 

### APPENDIX B SAMPLE RUN OF THE RAGTIME CODE

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{1/2}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{1/2}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{1/2}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{1/2}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\$  $\label{eq:2.1} \frac{1}{2}\int_{\mathbb{R}^3}\left|\frac{d\mathbf{r}}{d\mathbf{r}}\right|^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\mathbf{r}^2\,d\math$  $\mathcal{L}(\mathcal{A})$  .  $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{$  $\label{eq:2} \frac{1}{2} \int_{\mathbb{R}^3} \frac{1}{\sqrt{2}} \, \mathrm{d} \mu \, \mathrm$  $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2}$  $\label{eq:2} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{$ 

 $\frac{1}{2}$  $\label{eq:2.1} \mathcal{L}_{\mathcal{A}}(x,y) = \mathcal{L}_{\mathcal{A}}(x,y) = \mathcal{L}_{\mathcal{A}}(x,y) = \mathcal{L}_{\mathcal{A}}(x,y) = \mathcal{L}_{\mathcal{A}}(x,y) = \mathcal{L}_{\mathcal{A}}(x,y)$  $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\$ 

 $\label{eq:2.1} \begin{split} \mathcal{L}^{(1)}(x) &= \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \\ &= \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \mathcal{L}^{(1)}(x) \end{split}$ 

#### APPENDIX B

Output from a sample run of the currently implemented version of RAGTIME is provided in this appendix. Values for all state variables are listed, and concentrations in grains, milk, and beef are plotted versus time in Fig. B.1, B.2, and B.3. A number of parametric values had to be specified and options chosen to complete this run (see Table B.1). Table B.2 exhibits a listing of the data cards used for the sample run.

Following is a brief description of values and options specified for the sample run conducted, which considers a chronic deposition term (F<sub>i</sub>) of 1  $\mu$ Ci <sup>90</sup>Sr per m<sup>2</sup> per day, beginning 70 days prior to emergence of the grain. Compartment  $E_i$ , representing direct contamination of the surface of above-ground food crops through interception of depositing radionuclides, was considered to consist only of grain crops. In doing so, the time-dependent intercepting efficiency of the edible portion of the crop, the grain, was modeled using empirical values describing projected surface area as a function of plant mass, rather than using the geometric approach (see Sect. 3 discussion). Both empirical values and plant growth curves were obtained mainly from work documented by Miller' of the Stanford Research Institute. An equation describing the mass m of the grain per plant (grams/plant) was adopted from Miller; at any time  $t \geq t_0$ ,

$$
m = m_f^0 \left[ 1 - e^{-a} \tau^{(t^2 - t_0^2)} \right],
$$
 (B.1)

where  $m_f^0$  = final mass of grain at harvest (grams/plant);  $t_0$  = time of emergence of grain (days), and  $a_T =$  growth coefficient (day<sup>-2</sup>). All of these input parameters represent averages for a number of grain varieties. For the sample run of RAGTIME, the following values were used:

$$
m_f^0 = 1 \text{ gram/plant}
$$
  
\n
$$
t_0 = 70 \text{ days}
$$
  
\n
$$
a_x = 1.24 \times 10^{-4} \text{ day}^{-2}
$$



Fig. B.1. Predicted concentrations of Sr and  $90$ Y in grain vs time (1 µCi m<sup>-2</sup> day<sup>-1</sup> deposition of  $90$ Sr).



Fig. B.2. Predicted concentrations of 9 "Sr and <sup>9</sup> 0Y in milk vs time (1 **pCi** m-2 day-' deposition of <sup>90</sup>Sr)

 $\overline{6}$ 



Fig. B.3. Predicted concentrations of  $90$ Sr and  $90$ Y in beef vs time (1  $\mu$ Ci m<sup>-2</sup> day<sup>-</sup> riy. b.b. Prt<br>deposition of <sup>90</sup>Sr).

 $98\,$


 $\sim$ 

Table B.1. Values of parameters and other quantities used in sample run of RAGTIME for the <sup>90</sup>Sr, <sup>90</sup>Y decay chain

 $\mathcal{L}^{(1)}$ 



Table B.1 (continued)

 $\sqrt{ }$ 

 $100$ 

Parameter	FORTRAN name	Specific for	Value used	Reference or section of report containing discussion
$\tau_{\text{beef}}$	TAUBEF		3.81 x 10 <sup>-3</sup> day <sup>-1</sup>	4
$\tau_{e,s}$	<b>TAUES</b>		0.0495 day $-1$	4, 7
$\tau_{\text{exc}}$	TAUEXC(I)		2.0 x $10^{-3}$ day <sup>-1</sup> for $90$ Sr, 2.0 x 10 <sup>-3</sup> day <sup>-1</sup> for $90$ Y	$\overline{4}$
$^{\tau}$ q, *			$V_c/(A_qD_q) = 6.67 \times 10^{-3}$ day <sup>-1</sup>	Sect. 4.1
$(\tau_{q,b})_i$	TAUGB(I)		$[(F_f)_{i}(\tau_{exc})_{i}V_{c}]/D_{a}$	Sect. 4.2
$(\tau_{q,c})_i$	TAUGC(I)		$[(F_m)_i \tau_{m11k}V_c]/D_q$	Sect. 4.2
$\mathfrak{r}_{\mathfrak{g},\mathfrak{r}}$	TAUGR		$0.0495$ day <sup>-1</sup>	4, 7
$\tau_{\text{milk}}$	TAUMLK		2 day <sup><math>-1</math></sup>	$\overline{4}$
$\tau_{p,h}$	<b>TAUPH</b>		$1.096 \times 10^{-4}$ day <sup>-1</sup>	4, 8
$(\tau_{p,t})_i$	TAVPT(I)	grains	$\begin{bmatrix} \mathsf{M}_{\mathrm{f}}^0\dot{\mathsf{U}}(\mathrm{t})\mathsf{B}_{\mathsf{i}\,\mathsf{V}} \end{bmatrix}/(10\,,000\,$ x Adp)	App. B
$\tau_{r,d}$	<b>TAURD</b>		$1.096 \times 10^{-4}$ day <sup>-1</sup>	4,8
$\mathfrak{r}_{r,g}$	TAURG		2.74 $\times$ 10 <sup>-5</sup> day <sup>-1</sup>	Sect. 4.1
	<b>TAUSP</b>		6.93 x $10^{-4}$ day <sup>-1</sup>	Sect. 2.1
$\begin{matrix} \tau_{s,p} \\ t_h^h \end{matrix}$	<b>TIMBH</b>		20 days	5

Table B.1 (continued)



Table B.1 (continued)

 $^a$ The subscript i used with parameter names refers to the i $\it{th}$  nuclide (i = 1 for  $^{90}$ Sr,  $i = 2$  for  $90$ <sup>y</sup>)

 $\hat{A}$ 

ro



The specified values were derived from a minimum of data, for the grain of one variety of wheat, and thus may not be the best values to use for other simulations.

We have made use of Eq. (B.1) in deriving time-dependent values for the interception fraction  $S_1$  and a normalized version of this equation in the derivation of values for the transfer coefficient  $(\tau_{p, t})_i$ . The fraction  $S_1$  may be viewed as the ratio of the projected surface area  $(m^2)$  of the grain to the area  $(m^2)$  of the land on which the crop is grown. Thus,  $S_1$  is related to the specific area,

$$
S_{L} = \frac{projected surface area of grain (m2)}{mass of grain (grams)}
$$

by the equation

$$
S_1 = S_1 \text{mw} \tag{B.2}
$$

where  $m = mas$  of grain per plant (grams), and  $w = number$  of plants per square meter of land. The specific area, S<sub>1</sub>, may be fitted to an equation of the form

$$
s_L = s_L^0 \text{ m} \tag{B.3}
$$

in which  $S^0_L$  and  $n_L$  are empirical constants and m is the time-dependent mass of the grain per plant as given in Eq. (B.1). This model is adopted from ref. 1 (p. 177). Using the values  $s_L^0 = 0.00075$  and  $n_L =$ 0.455 from this document, the value of  $S_1$  is calculated from Eqs. (B.2) and (B.3) to be

 $S_1 = 0.00075 \text{ m}^0 \cdot 545 \text{ w}$ 

For the root uptake compartment  $T_i$ , again only grains were considered in the sample run. The rate (microcuries day<sup>-1</sup>) at which radioactivity is absorbed by plant roots is represented in Eq. (2.9) by **I** the term  $(\tau_{p,t})_i^p$ , where  $P_i$  represents the radioactivity (µCi) present in the subsurface soil pool associated with one man's food supply. As in our discussion of Eq. (B.1), it follows that the total mass (grams), as time  $t \geq t_0$ , of grain in compartment T<sub>i</sub> is given by  $M_f^0U(t)$ , where

$$
U(t) = 1 - e^{-a} t^{2} - t_{0}^{2}
$$
 (B.4)

**0** and  $\texttt{M}_{\texttt{f}}^{\textsf{U}}$  = total mass (grams) of crop at harvest time grown on land associated with one man's food supply. The rate of root absorption of radioactivity,  $(\tau_{n-t})$ ,  $P_i$  (microcuries day<sup>-1</sup>) is assumed to be the product of the rate of increase of grain mass  $\texttt{M}_{\texttt{f}}^{\textsf{U}}(\texttt{t})(\texttt{grams day}^{-1})$  and the radioactivity concentration in grain (microcuries gram<sup>-1</sup>), the latter quantity being approximated by

$$
\frac{B_{\text{i}v}P_{\text{i}}}{\text{mass (grams) of soil}} = \frac{B_{\text{i}v}P_{\text{i}}}{10,000 \times \text{Adp}}
$$
\n(B.5)

where  $B_{i} =$  concentration of nuclide i per unit fresh weight in plant ( $\mu$ Ci kg<sup>-1</sup>) divided by concentration of nuclide per unit dry weight in soil ( $\mu$ Ci kg<sup>-1</sup>); A = soil area used for crop production, chosen as  $10^3$  $m^2$  here; d = plow depth, assumed to be 20 cm; and  $p =$  soil density, assumed to be 1.4  $q cm^{-3}$  (dry weight). This derivation then leads to the equation

$$
(\tau_{p,t})_i = \frac{M_f^0}{10,000 \times \text{Ad}\rho} , \qquad (8.6)
$$

where

$$
\dot{U}(t) = 2a_t t \cdot e^{-a_t (t^2 - t_0^2)}
$$
 (B.7)

Factors describing growth rate [i.e.,  $\dot{U}(t)$  and  $a_{\tau}$ ] were again derived from empirical data available for grains<sup>1</sup> and are consistent with those used in estimating interception of airborne radionuclides by grains. Values of  $B_{iv}$  (see Table B.1) were derived from empirically obtained data for the elements Sr and  $Y. 2, 3$ 

For compartments  $B_i$  and  $C_i$ , respectively representing beef and milk concentrations of 90Sr and 90Y, all parameters were defined and assigned values in Sect. 4 of this document, with the exception of  $(\tau_{\text{exc}})_{i}$ ,  $(\mathsf{F}_{\mathsf{f}})_{i}$ ,  $(\mathsf{F}_{\mathsf{m}})_{i}$ ,  $t_{\mathsf{b}}^{\mathsf{h}}$ , and  $t_{\mathsf{c}}^{\mathsf{h}}$ . A constant value of 0.002 day<sup>-1</sup>, adopted from TERMOD,<sup>4</sup> has temporarily been assigned to  $(\tau_{exc})_i$ . This value for  $(\tau_{\text{exc}})$ ; represents the fractional weight gain per day for a mature steer, and thus implies that dilution of the elemental concentration is due only to growth. In this sense, it represents the lower limit for  $(\tau_{\text{avc}})_{i}$ , and thus may underestimate loss from the beef compartment because metabolic turnover, which may be element-specific, is neglected. Values for F<sub>f</sub> and F<sub>m</sub> (Table B.1) were taken from a review of literature concerning uptake of these elements by cattle and subsequent transfer to meat and milk, respectively.

The holdup times for compartments B<sub>i</sub> and C<sub>i</sub> were specified using values either given in, or derived from, the U. S. Nuclear Regulatory Commission's (USNRC) Regulatory Guide  $1.109$  (October, 1977).<sup>5</sup> The assumed time between slaughter and consumption of beef  $(\mathbf{t}_{\mathsf{h}}^{\mathsf{h}})$  was 20 days, and between milking and milk consumption (t<sup>h</sup>) was 2 days, the latter representing one-half of the total time given for transfer from feed, through milk, to man. For compartments  $E_i$  and  $T_i$ , holdup times were not specified, but rather the concentrations after harvest are printed at each output time so that the value of this parameter is left to the user's discretion.

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 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{$ 

 $\label{eq:2.1} \mathbf{E} = \mathbf{E} \left[ \mathbf{E} \left( \mathbf{E} \right) \mathbf{E} \right] \mathbf{E} \left( \mathbf{E} \right)$ 

 $\mathcal{L}(\mathcal{L}(\mathcal{L}))$  and  $\mathcal{L}(\mathcal{L}(\mathcal{L}))$  . The contribution of the contribution of  $\mathcal{L}(\mathcal{L})$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\$ 

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 $\label{eq:1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{dx}{dx}dx.$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\frac{1}{\sqrt{2\pi}}\sum_{i=1}^n\$