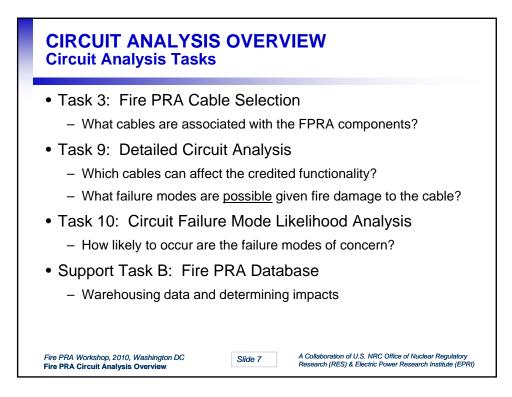
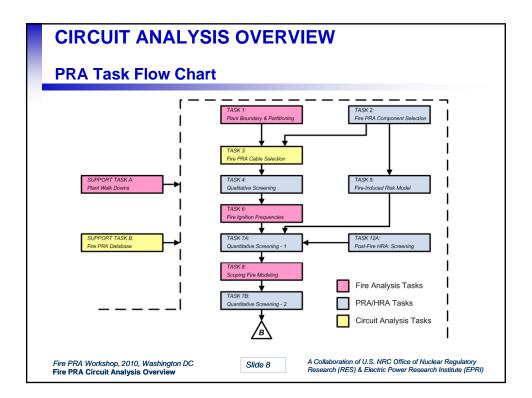
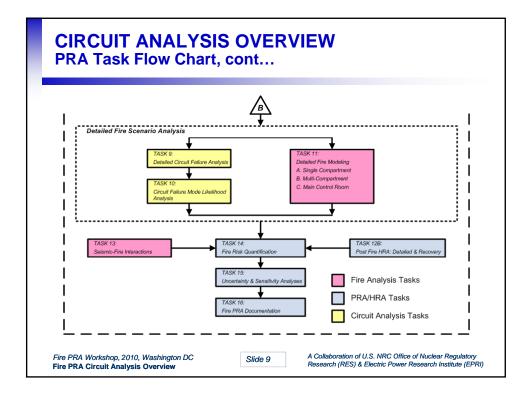
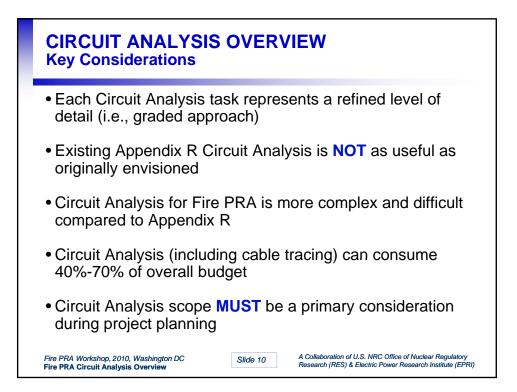


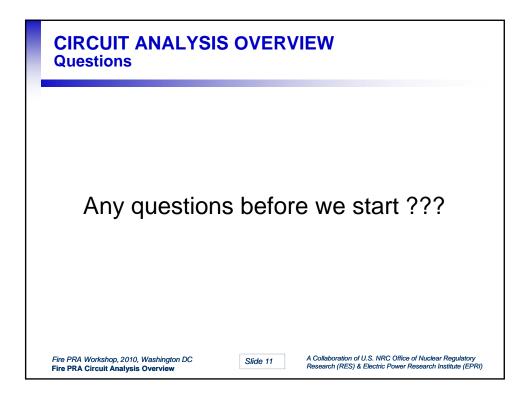
| - | Tuesday | Wednesday | Thursday | Friday |
|-------|---------------------------------------|--------------------------|---|---|
| 8:30 | · · · · · · · · · · · · · · · · · · · | weunesuay | inuisuay | Thuay |
| 8:45 | | | | |
| 9:00 | | Presentation - Detailed | Presentation - Fire PRA | Exercises - Work Task 10 |
| 9:15 | | Circuit Failure Analysis | Database | Sample Problems |
| 9:30 | | (Task 9) | | |
| 9:45 | | | Break | Break |
| 10:00 | General Session - | | | |
| 10:15 | Introduction to all Modules | Break | - Fire PRA Database | Discussion - Task 10 |
| 10:30 | | | (continued) | Sample Problems |
| 10:45 | | Presentation - Task 3 & | | |
| 11:00 | | Task 9 Sample Problem | n : | D : |
| 11:15 | | Definition and Examples | Discussion - Open, Q&A, | Discussion - Summary and Conclusions |
| 11:30 | | | etc. | Conclusions |
| | LUNCH BREAK | LUNCH BREAK | LUNCH BREAK | LUNCH BREAK |
| 13:00 | | | | |
| 13:15 | Presentation - Fire PRA | | | |
| 13:30 | Circuit Analysis Overview | | Presentation - Circuit Failure Mode Likelihood | |
| 13:45 | | | Analysis (Task 10) | |
| | Presentation - Fire PRA | Exercises - Work Task 3 | Analysis (Task 10) | |
| | Circuit Analysis Summary | & Task 9 Sample Problems | | |
| _ | Break | | Break | |
| 14:45 | Presentation - Fire PRA | | - Circuit Failure Mode | General Session - Closing: All Modules |
| | Cable Selection (Task 3) | | Likelihood Analysis | Closing: All Modules |
| 15:15 | | | (continued) | |
| | Break | Break | Break | |
| 16:00 | | | - Circuit Failure Mode | |
| 16:15 | - Fire PRA Cable Selection | Discussion - Task 3 & | Likelihood Analysis (cont.) | |
| 16:30 | (continued) | Task 9 Sample Problems | Presentation - Task 10 | |
| 16:45 | | | Sample Problems | |
| 17:00 | ADJOURN | ADJOURN | ADJOURN | ADJOURN |

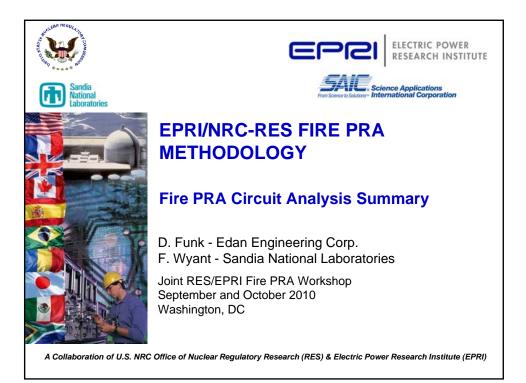


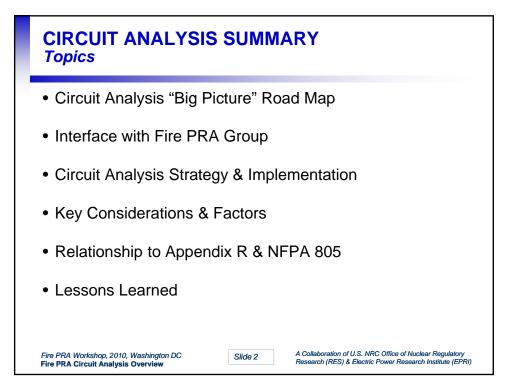


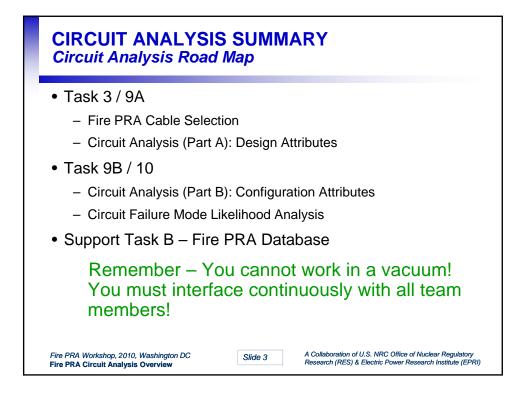


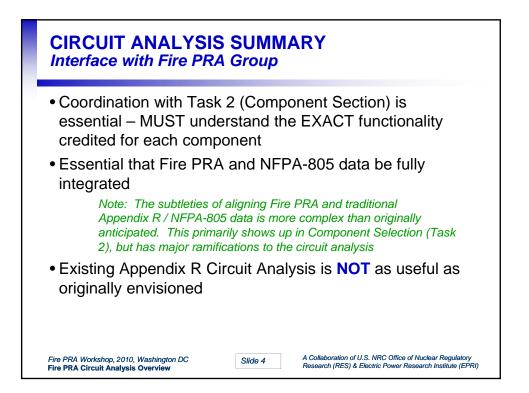


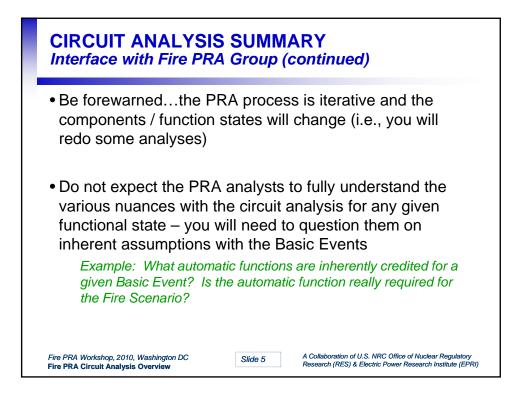


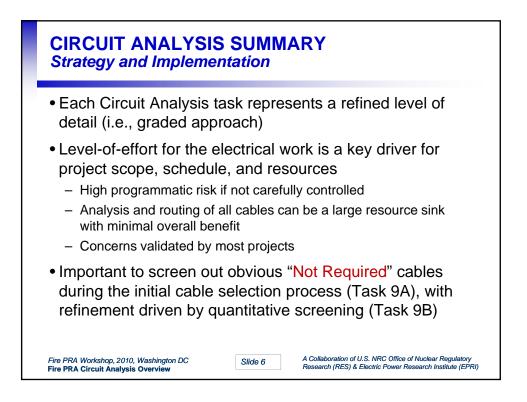


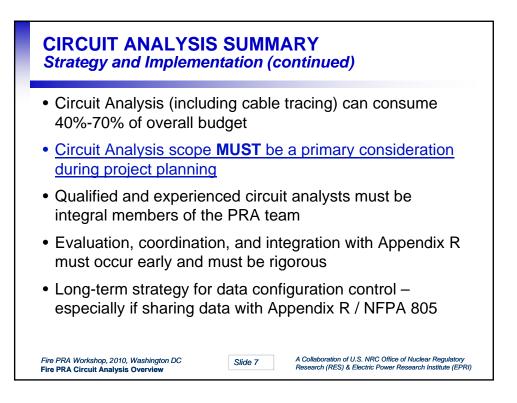


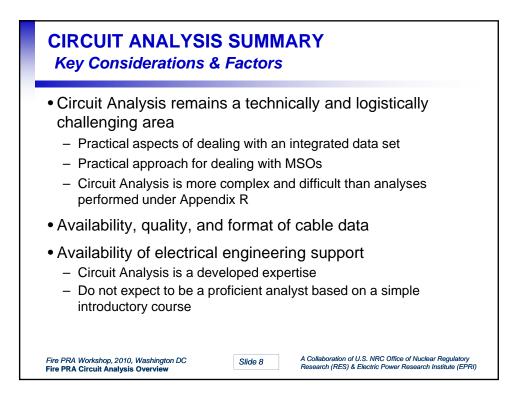


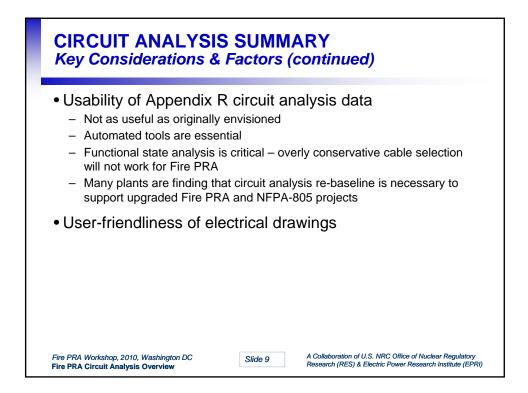


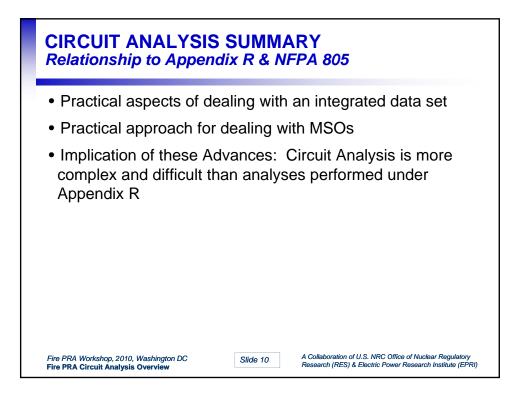


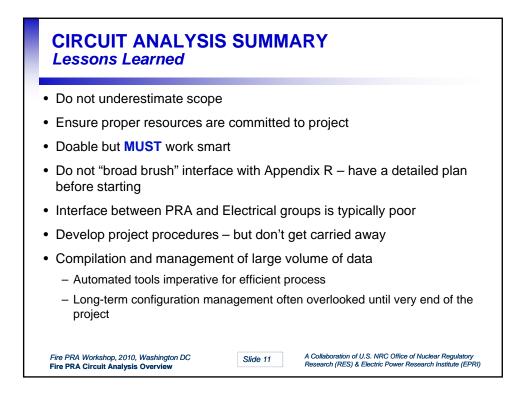


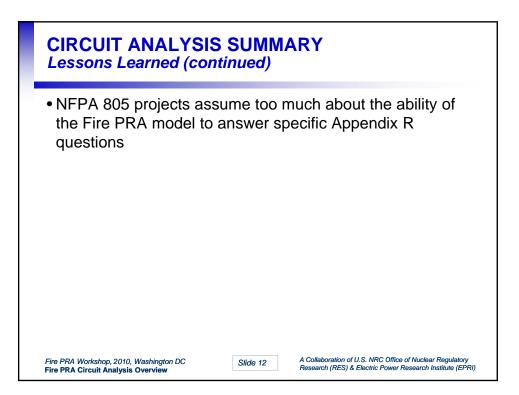


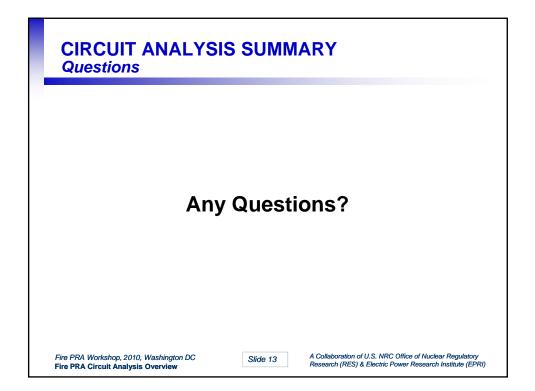




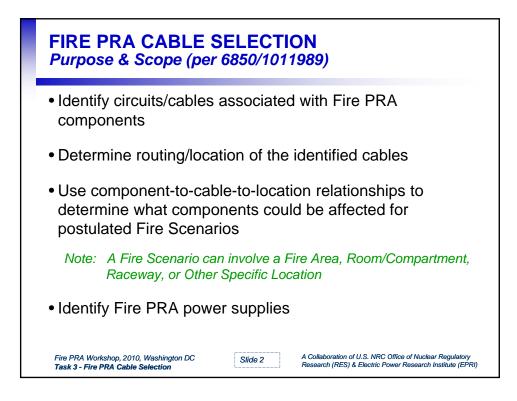


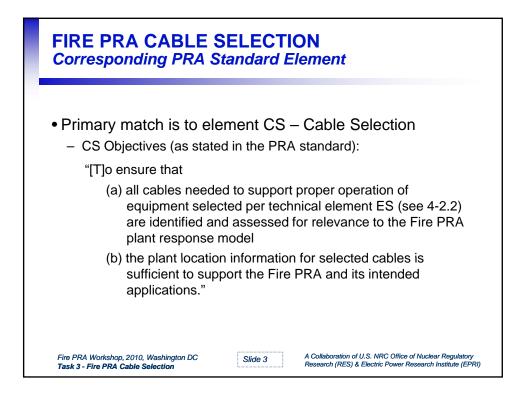


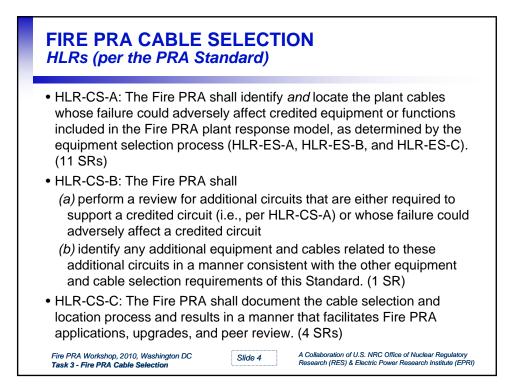


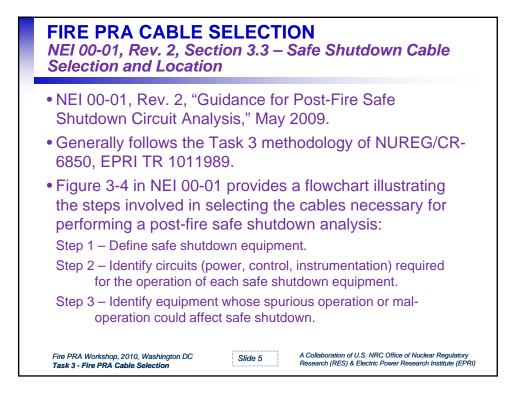


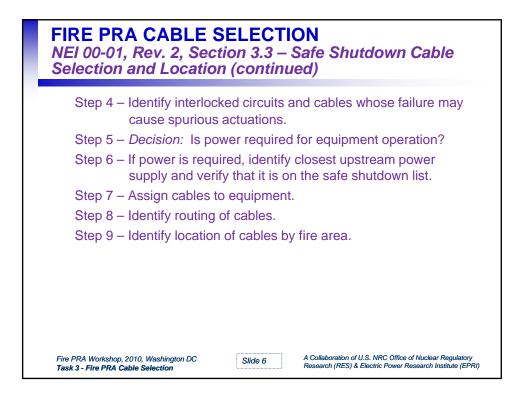


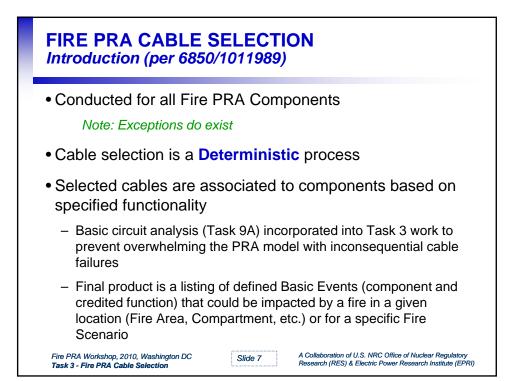


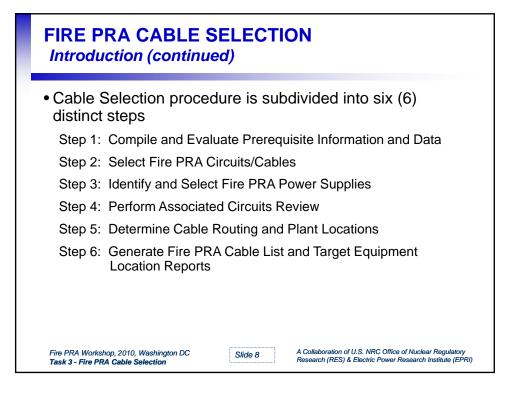


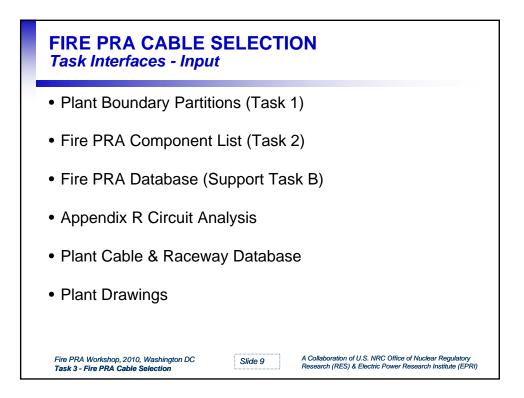


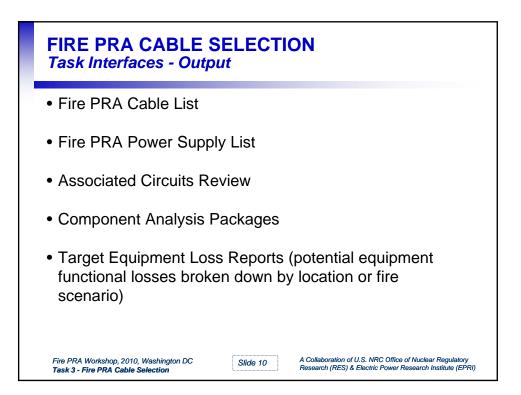


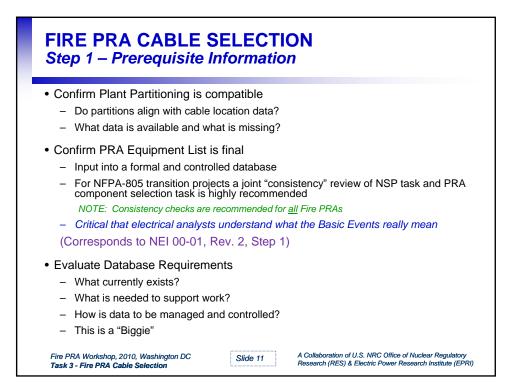




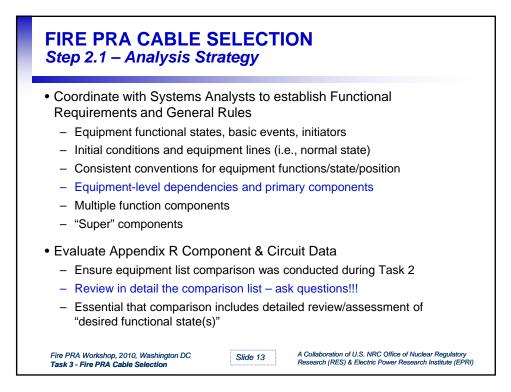


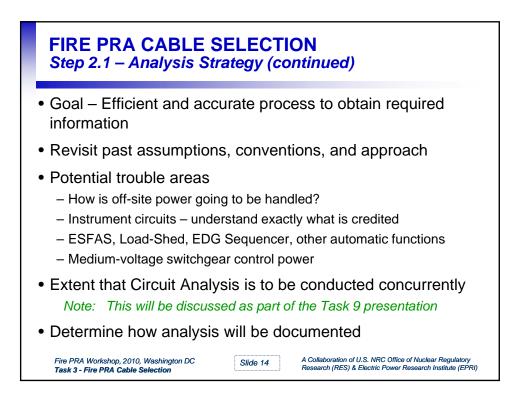


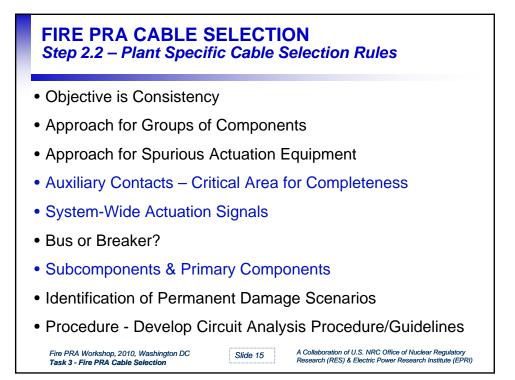


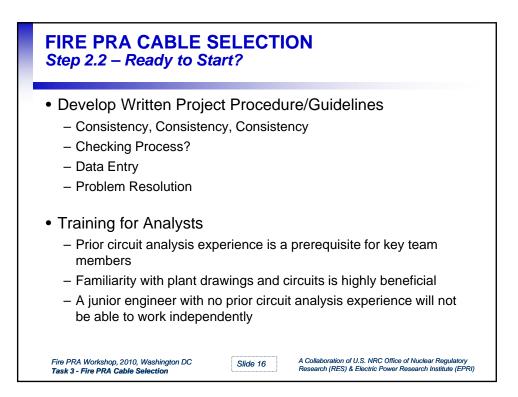


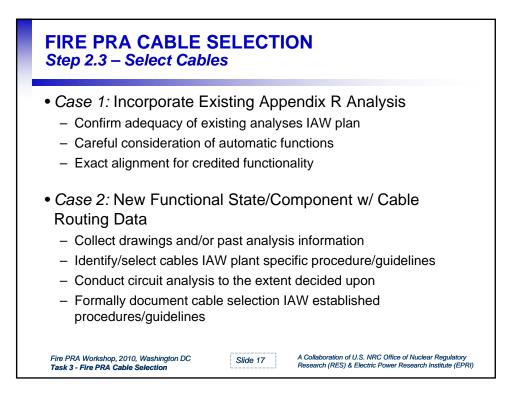
FIRE PRA CABLE SELECTION Step 2 – Select Fire PRA Cables Analysis Cases Appendix R Component with same functional requirements Must consider which (if any) automatic features are included in the existing analysis Aligning existing analyses to Fire PRA Basic Events is not straightforward - Appendix R Component with *different* functional requirements - Non-Appendix R Component with cable location data Non-Appendix R Component without cable location data Analysis Sub-Steps - Step 2.1: Analysis Strategy - Step 2.2: Plant Specific Rules - Step 2.3: Select Cables Corresponding PRA Standard SRs: CS-A1, A3 Corresponding NEI 00-01, Rev. 2, Steps: 2 & 4 • A Collaboration of U.S. NRC Office of Nuclear Regulatory Fire PRA Workshop, 2010, Washington DC Slide 12 Task 3 - Fire PRA Cable Selection Research (RES) & Electric Power Research Institute (EPRI)

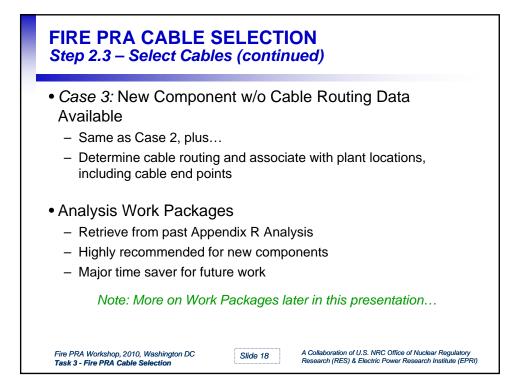


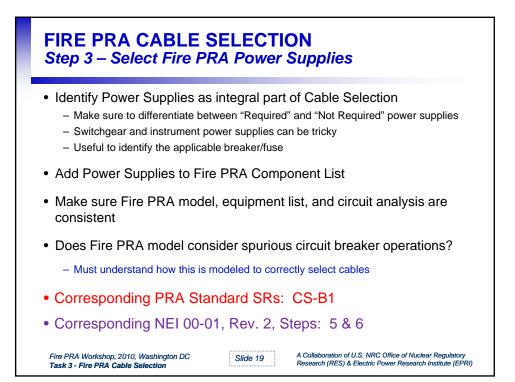


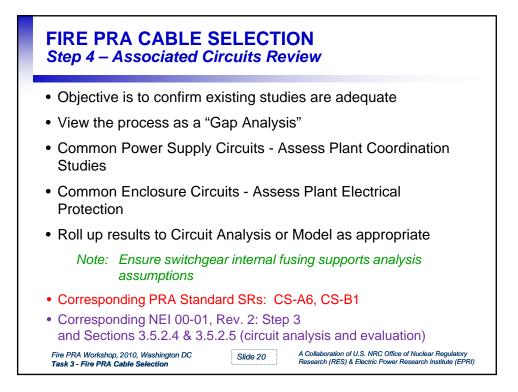


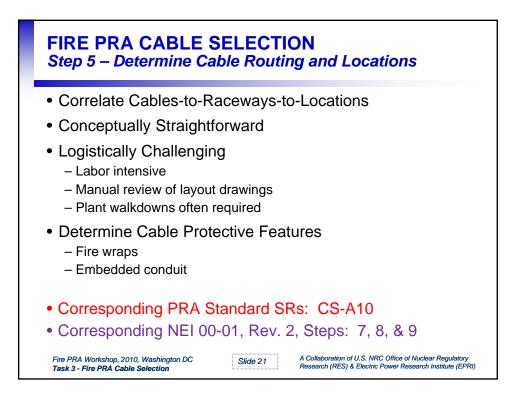


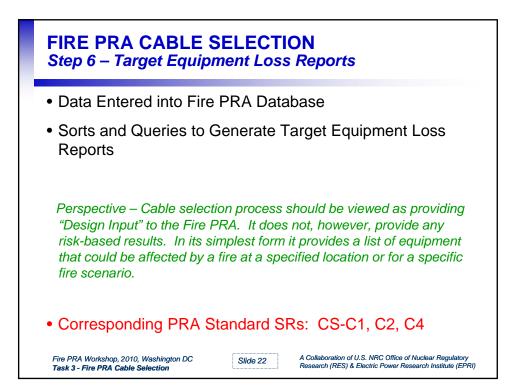


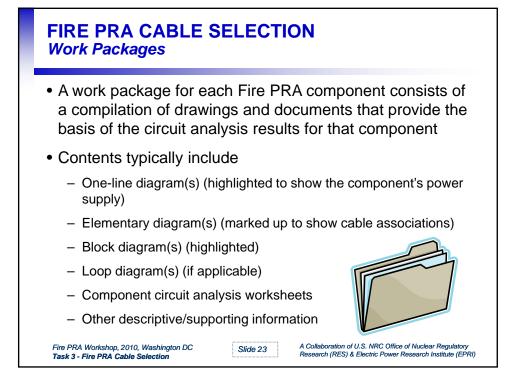


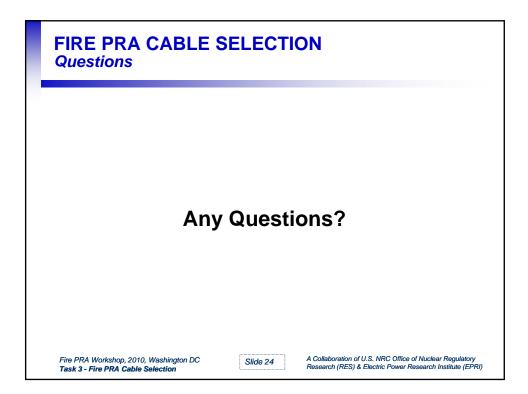






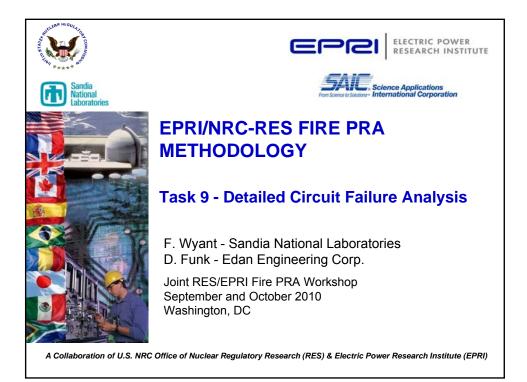


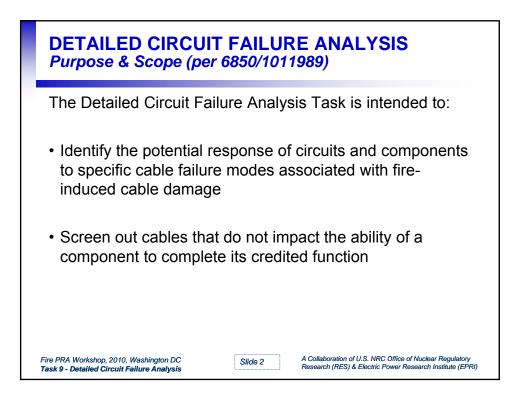


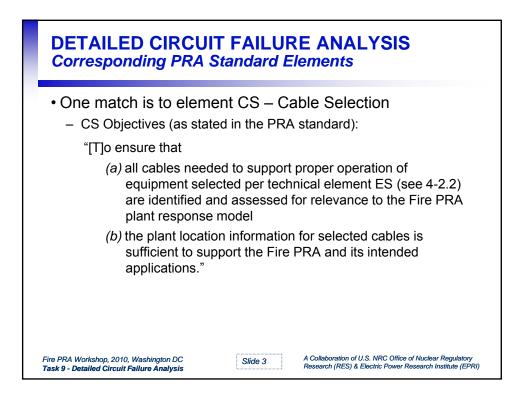


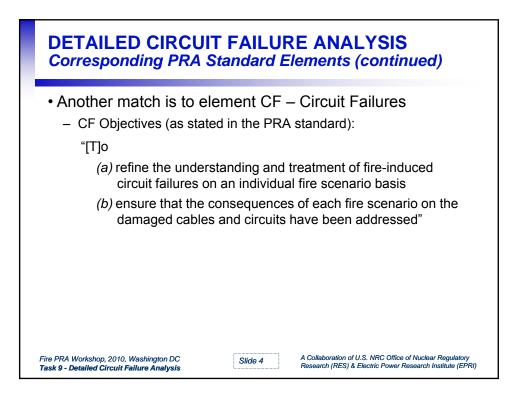
| NLG/ | /CR | -68 | 50, EPR | for the CS technical element to I TR 1011989 | |
|-----------|-----|--|--|--|--|
| Technical | HLR | SR | 6850/1011989 | Comments | |
| Element | | | Sections that | | |
| | | | cover SR | | |
| CS | Α | The F | The Fire PRA shall identify and locate the plant cables whose failure could adversely affect credited equipment or | | |
| | | functions included in the Fire PRA plant response model, as determined by the equipment selection process (HLR-ES-A | | | |
| | | HLR-B | S-B, and HLR-ES-C |). | |
| | | 1 | 3.5.2 | | |
| | | 2 | 9.5.2 | Covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 3 | 3.5.2, 9.5.2 | Also covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 4 | 3.5.3 | | |
| | | 5 | 9.5.2 | Covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 6 | 3.5.4, 9.5.2 | Also covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 7 | 9.5.2 | Covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 8 | 9.5.2 | Covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 9 | 9.5.2 | Covered in "Detailed Circuit Failure Analysis" chapter | |
| | | 10 | 3.5.5 | | |
| | | 11 | 3.5.5 | | |
| | В | The F | ire PRA shall | | |
| | | | | r additional circuits that are either required to support a credited circuit (i.e., per HLR-CS-A) or | |
| | | | | rersely affect a credited circuit | |
| | | | | nal equipment and cables related to these additional circuits in a manner consistent with the | |
| | | othe | equipment and c | ble selection requirements of this Standard | |
| | | 1 | 3.5.3, 3.5.4 | | |
| | С | The Fire PRA shall document the cable selection and location process and results in a manner that facilitates Fire PRA | | | |
| | | appli | cations, upgrades, | and peer review. | |
| | | 1 | 3.5.6 | | |
| | | 2 | 3.5.6 | | |
| | | 3 | 3.5.6 | | |
| | | 4 | 3.5.6 | | |

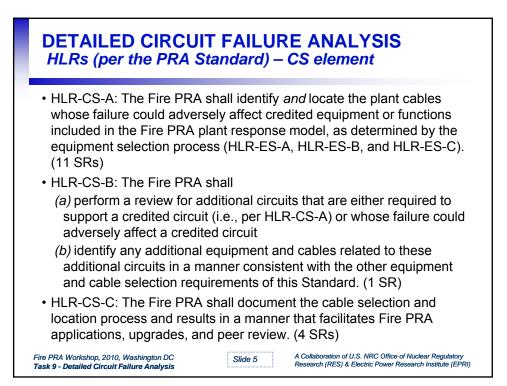
| FIRE I | PRA | CABL | E SELECTION | NC |
|-----------------|------------|-----------------|--------------|---|
| | | | | own Cable Selection to |
| | | 550 EDE | TD 1011000 | |
| VUREG/ | CK-00 | 550, EPR | I TR 1011989 | |
| | | | | |
| NEI 00-01. | NEI 00-01. | 6850/1011989 | Comments | |
| Rev. 2, | Figure 3-4 | Sections that | | |
| Section | Step | cover step | | |
| 3.3 - Safe | 1 | 3.5.1 | | |
| Shutdown | 2 | 3.5.2 | | |
| Cable | 3 | 3.5.4 | | |
| Selection | 4 | 3.5.2 | | |
| and | 5 | 3.5.3 | | |
| Location | 6 | 3.5.3 | | |
| | 7 | 3.5.5 | | |
| | 8 | 3.5.5 | | |
| | 9 | 3.5.5 | | |
| | | | | |
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| | | 0.14/ | | A Collaboration of U.S. NRC Office of Nuclear Regulatory |
| Task 3 - Fire I | | 0, Washington L | C Slide 26 | Research (RES) & Electric Power Research Institute (EPRI) |
| | | Geleculli | | |

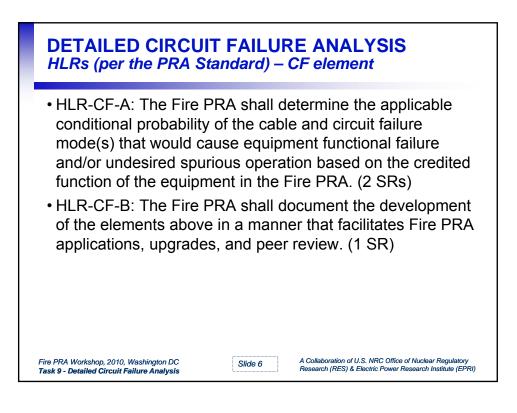


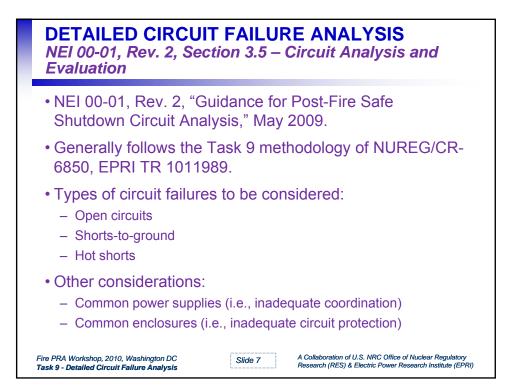


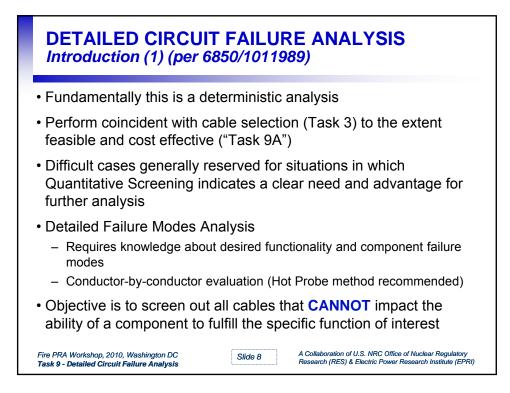


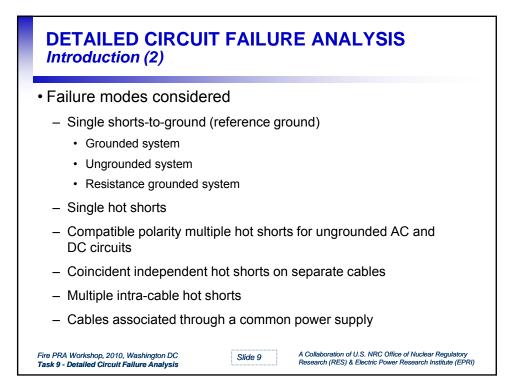


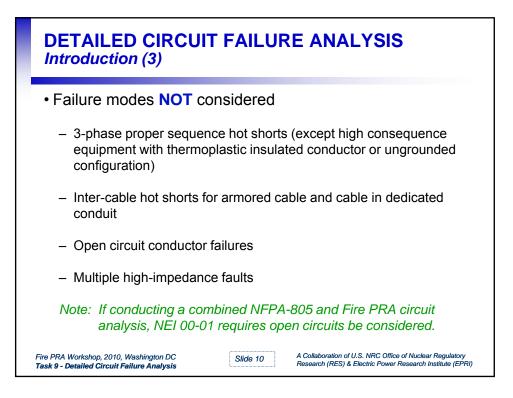


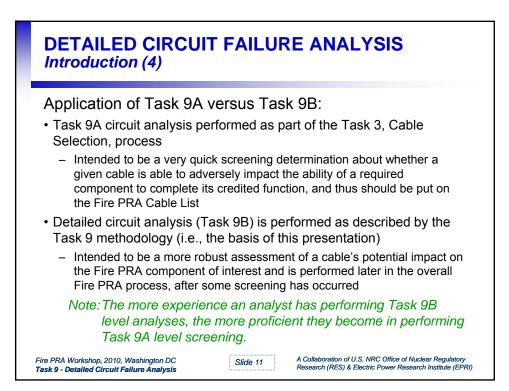


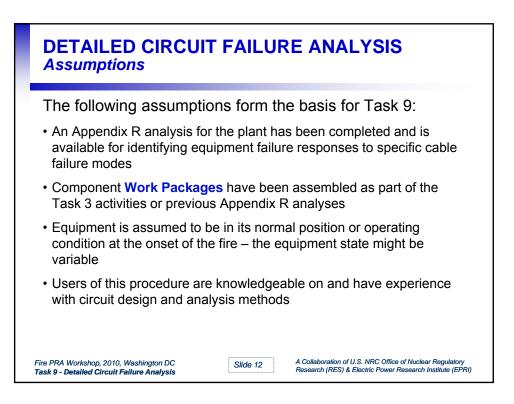


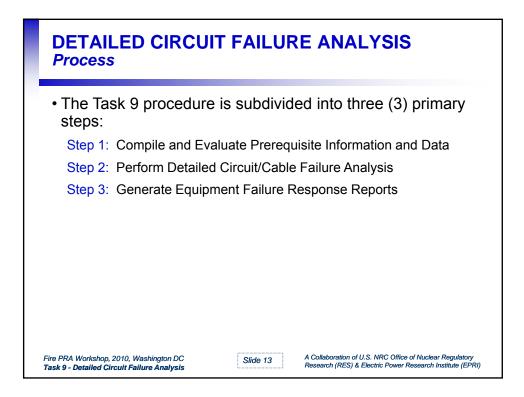


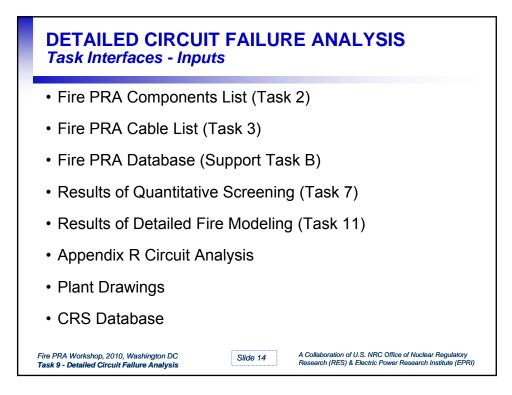


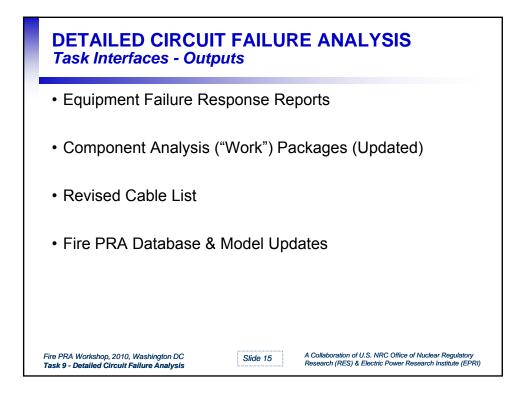


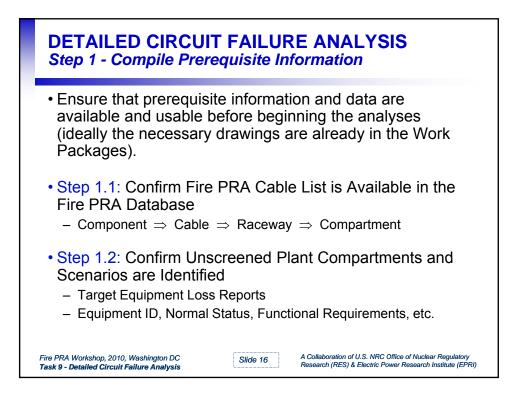


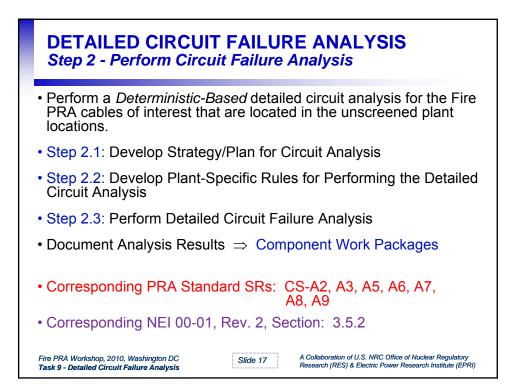


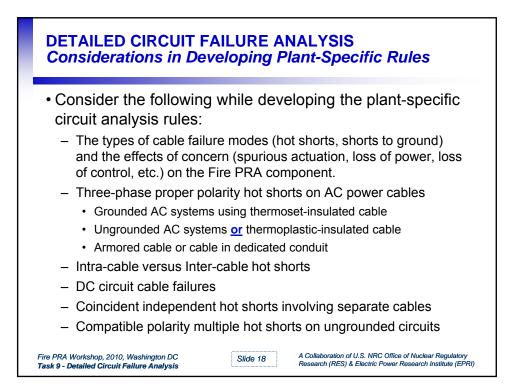


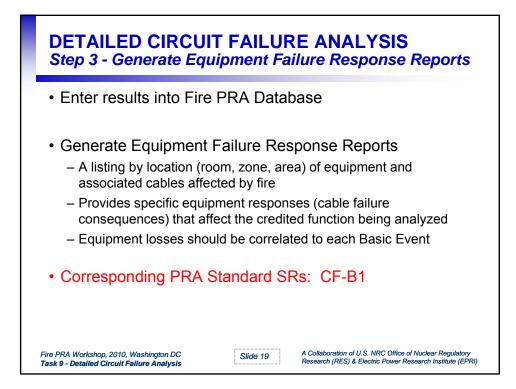


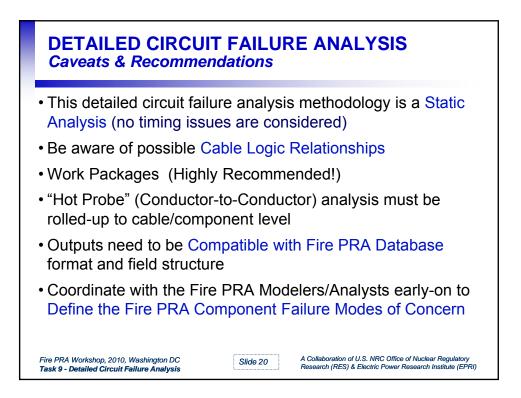


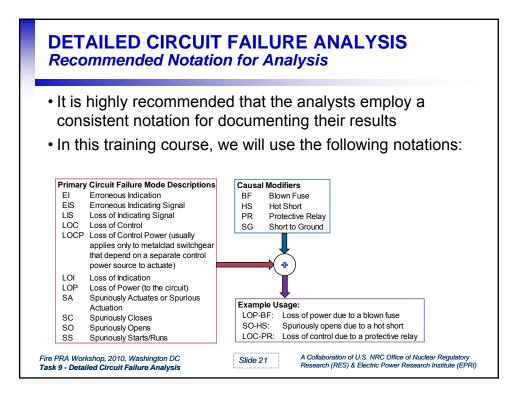


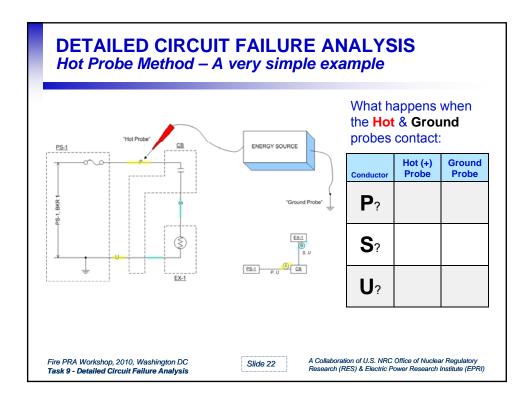


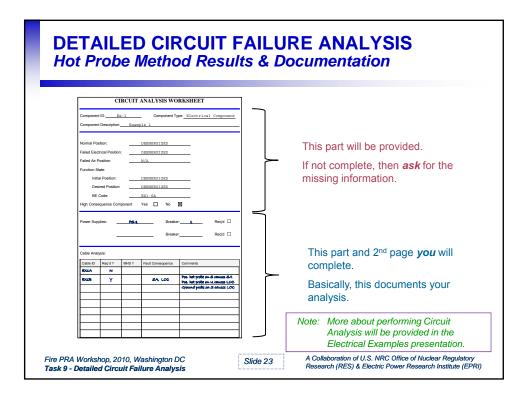


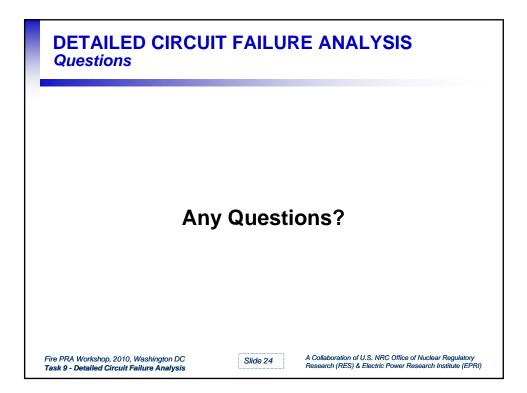


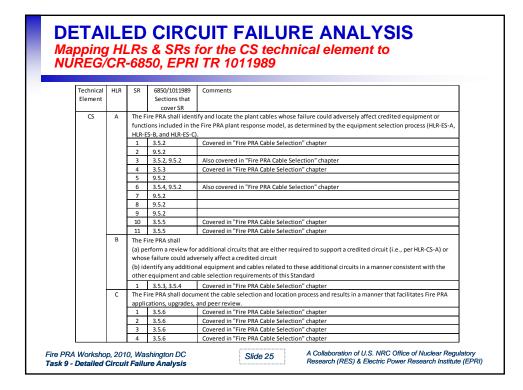


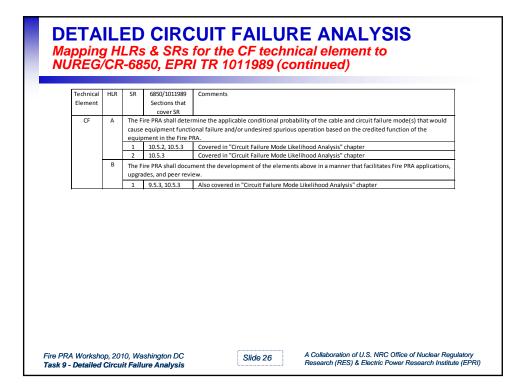












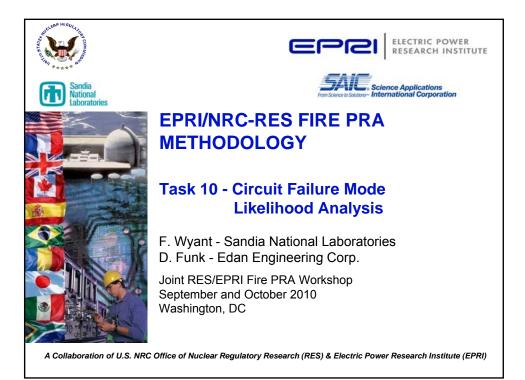
DETAILED CIRCUIT FAILURE ANALYSIS Mapping NEI 00-01, Rev. 2, Circuit Analysis and Evaluation to NUREG/CR-6850, EPRI TR 1011989

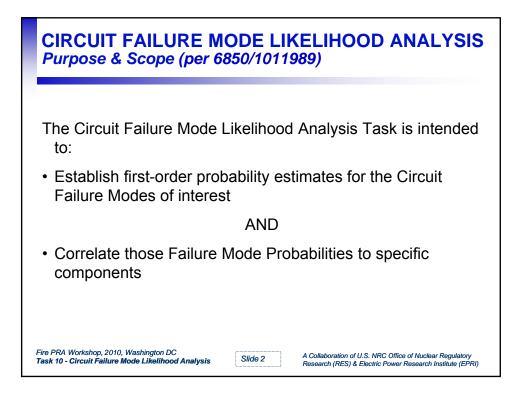
| NEI 00-01, | NEI 00-01, | 6850/1011989 | Comments |
|------------|-----------------|---------------|--|
| Rev. 2, | Section 3.5.2 - | Sections that | |
| Section | Types of | cover step | |
| | Circuit | | |
| | Failures | | |
| 3.5 - | 3.5.2.1: Due to | | |
| Circuit | an Open | N/A | Open circuits not considered in 6850/1011989 as discussed in 9.5.2 |
| Analysis | Circuit | | |
| and | 3.5.2.2: Due to | | |
| Evaluation | a Short-to- | 9.5.2 | |
| | Ground | | |
| | 3.5.2.3: Due to | 9.5.2 | |
| | a Hot Short | 9.5.2 | |
| | 3.5.2.4: Due to | | |
| | Inadequate | 3.5.4 | Covered in "Fire PRA Cable Selection" chapter |
| | Circuit | 3.3.4 | Covered In File PKA Cable Selection Chapter |
| | Coordination | | |
| | 3.5.2.5: Due to | | |
| | Common | 3.5.4 | Covered in "Fire PRA Cable Selection" chapter |
| | Enclosure | 3.3.4 | Covered in The FRA Cable Selection Chapter |
| | Concerns | | |

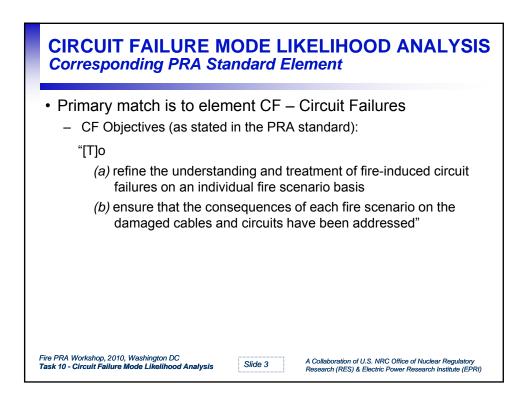
Fire PRA Workshop, 2010, Washington DC Task 9 - Detailed Circuit Failure Analysis

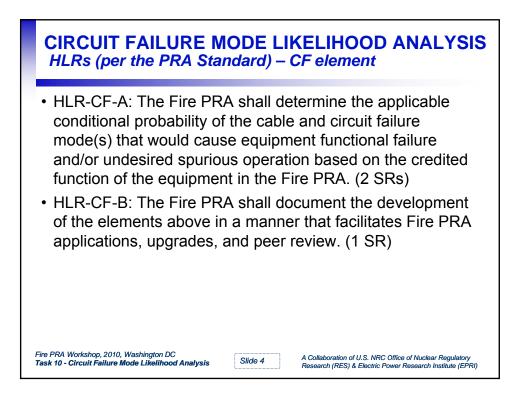
Slide 27

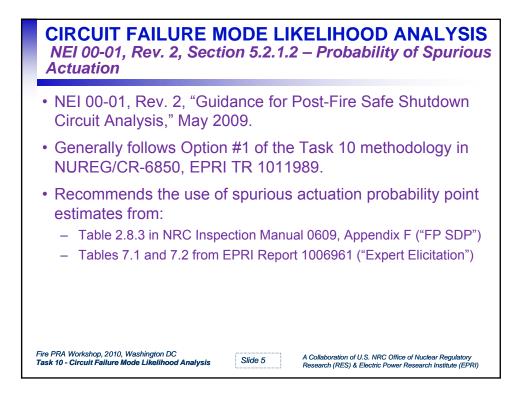
A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

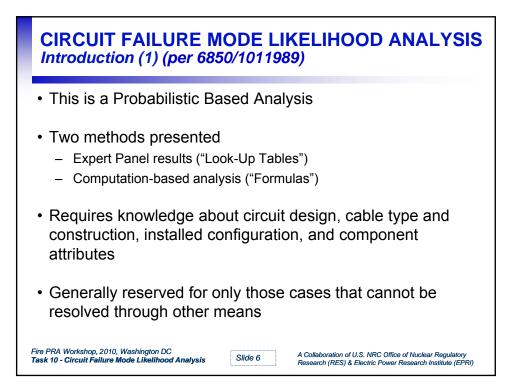












CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS *Introduction (2)*

Caveats:

- Our knowledge is greatly improved but <u>Uncertainties Are Still High</u>
 Very limited data for many issues
- For this reason, implementing guidance is intended to be Conservative
- Practical implementation is challenging
- Further analysis of existing test data and follow-on tests would be beneficial:
 - · Reduce uncertainties, including conservatisms as appropriate
 - · Solidify key influence factors

Fire PRA Workshop, 2010, Washington DC Task 10 - Circuit Failure Mode Likelihood Analysis

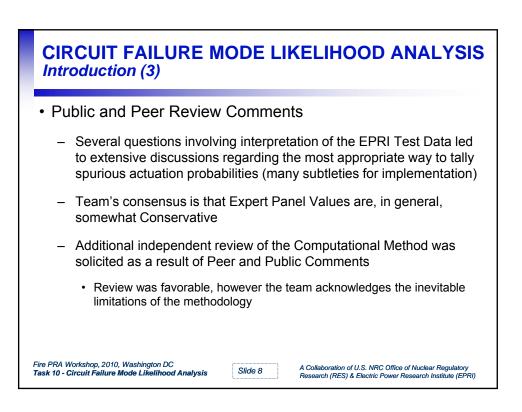
- Incorporate time as a factor (FAQ 08-0051, for AC circuits only; Status: Closed)
- Incorporate "End-Device" functional attributes and states (e.g., latching circuits vs. drop-out design)

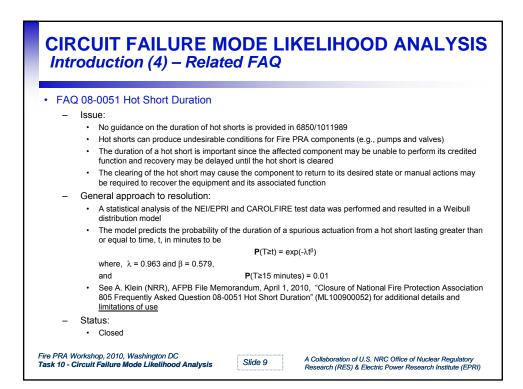
A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

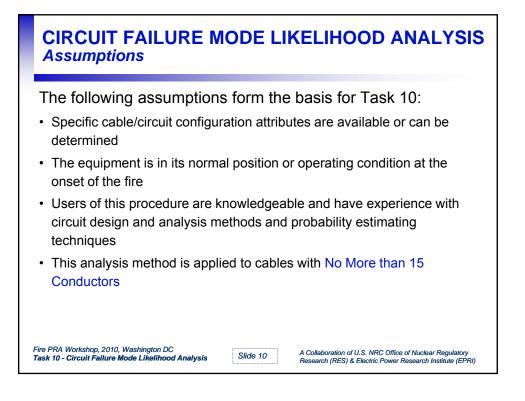
- Expert elicitation to produce refined spurious operation probabilities (planned for 2010)
- Computation-based method (formula) is an extrapolation of existing data; validation remains to be done. Conservatism has not been established.

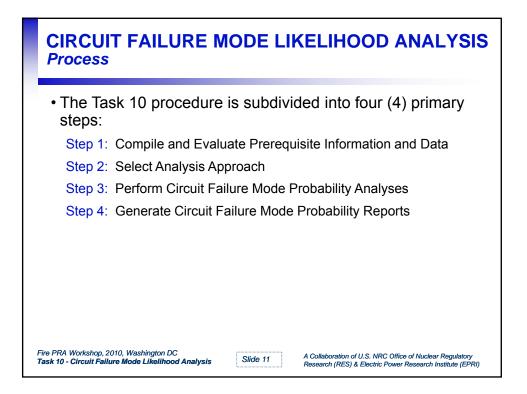
Slide 7

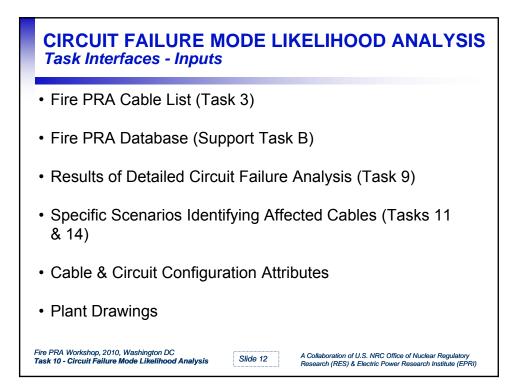
· Probabilities of sufficient quality to move ahead

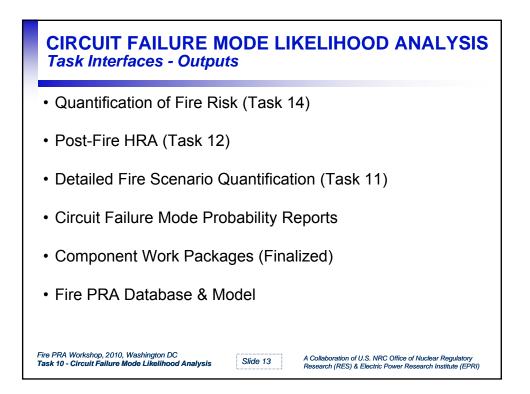


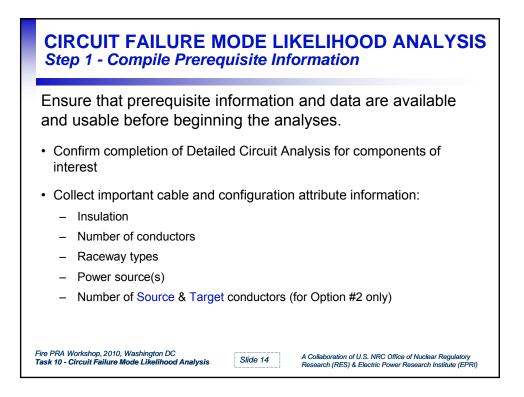


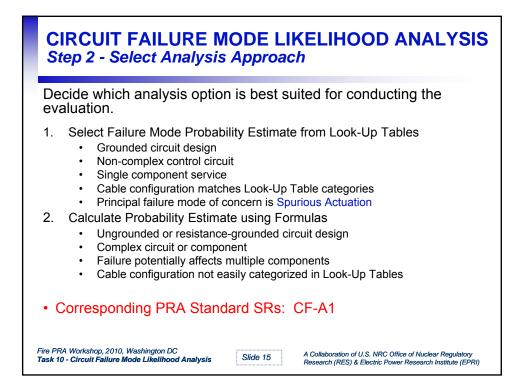


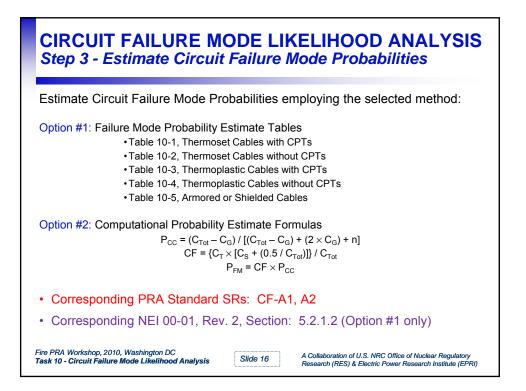


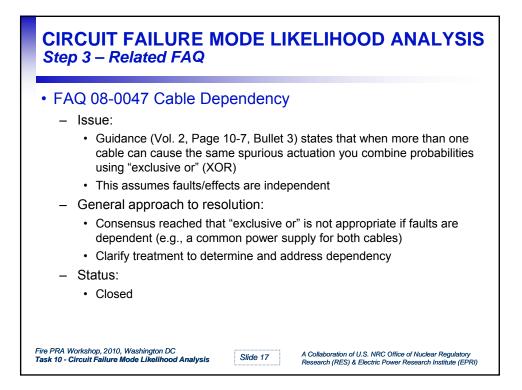


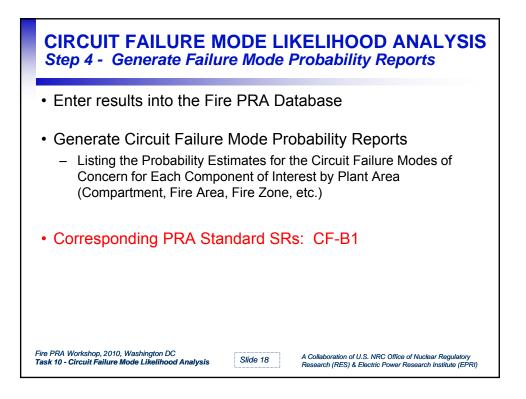


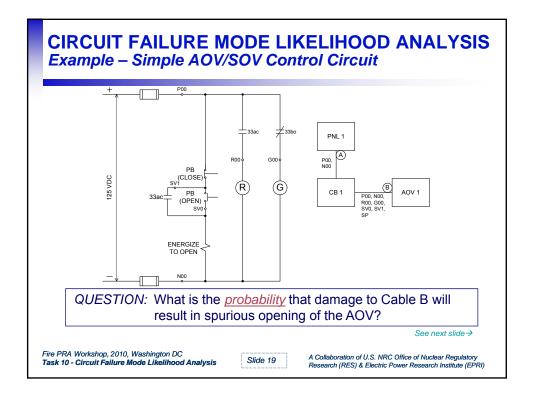




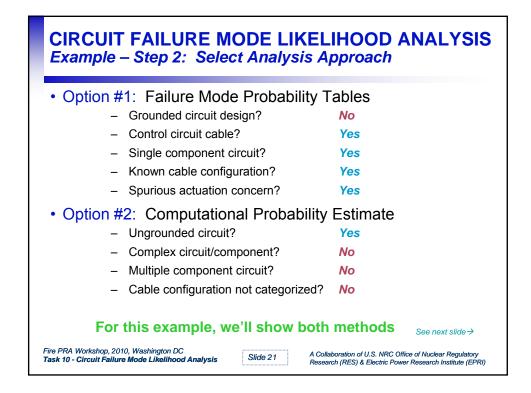




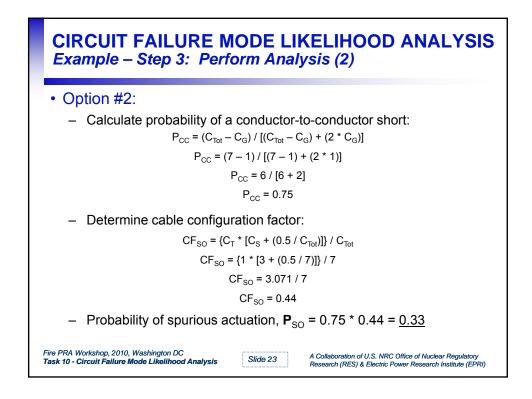


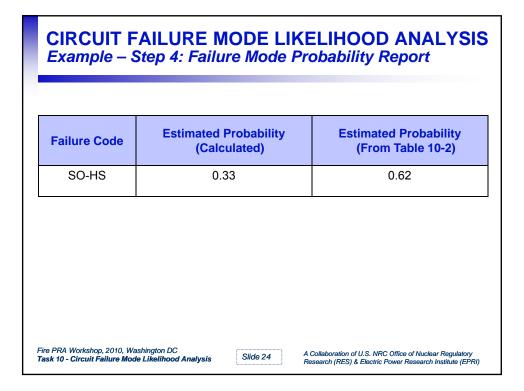


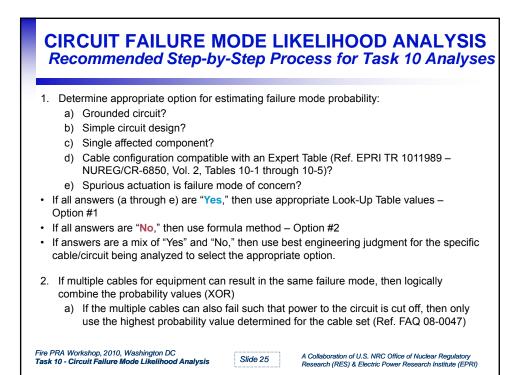
| CIRCUIT FAI Example – Ste | _ | - | | D ANALYSIS |
|---|---------|----------------------------------|---------------------------------------|--|
| Detailed circuit | analys | is completed & | & documented | ? Yes |
| | Cable | +125 VDC Hot Probe | -125 VDC Reference Ground Probe | |
| | Α | LOP-FB | LOP-FB | |
| | в | LOP-FB, EI-HS, SO-HS | LOP-FB, LOC | |
| Collect importat _ Cable insulat | | e and configur <i>Thermos</i> | | |
| Number of co | onducto | ors? Seven | | |
| Raceway typ | e? | Tray | | |
| Power source | e? | Ungroun | ded DC bus (r | no CPT) |
| Number of so | ource & | target conducto | ors? 3 sources | s, 1 target |
| | | Ū. | | See next slide -> |
| Fire PRA Workshop, 2010, Washing Task 10 - Circuit Failure Mode Like | | ysis Slide 20 | | RC Office of Nuclear Regulatory c Power Research Institute (EPRI) |

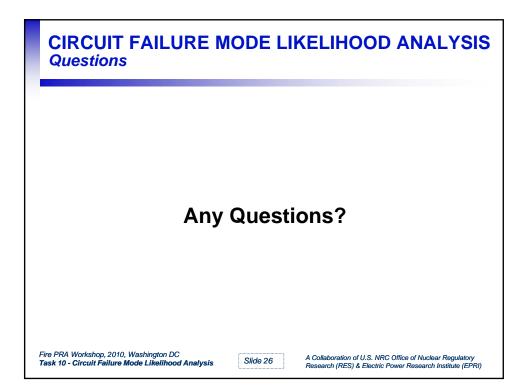


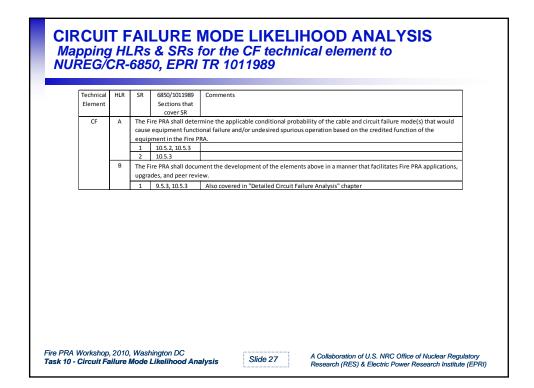
| Example – StOption #1: | e to Use? Table 10-2, T | vsis (1) | |
|---|---|------------------------------------|--|
| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
| Tray | $\begin{array}{l} M/C \mbox{ Intra-cable} \\ 1/C \mbox{ Inter-cable} \\ M/C \rightarrow 1/C \mbox{ Inter-cable} \\ M/C \rightarrow M/C \mbox{ Inter-cable} \end{array}$ | 0.60 0.40 0.20 0.02 - 0.1 | 0.20 - 1.0 0.1 - 0.60 0.1 - 0.40 |
| Conduit | $\begin{array}{l} M/C \mbox{ Intra-cable} \\ 1/C \mbox{ Inter-cable} \\ M/C \rightarrow 1/C \mbox{ Inter-cable} \\ M/C \rightarrow M/C \mbox{ Inter-cable} \end{array}$ | 0.15 0.1 0.05 0.01 – 0.02 | 0.05 - 0.25 0.025 - 0.15 0.025 - 0.1 |
| - SO Probab ire PRA Workshop, 2010, Washi ask 10 - Circuit Failure Mode L | | A Collaboration of U.S. NF | 60*0.06) See next slide → RC Office of Nuclear Regulatory c Power Research Institute (EPRI) |







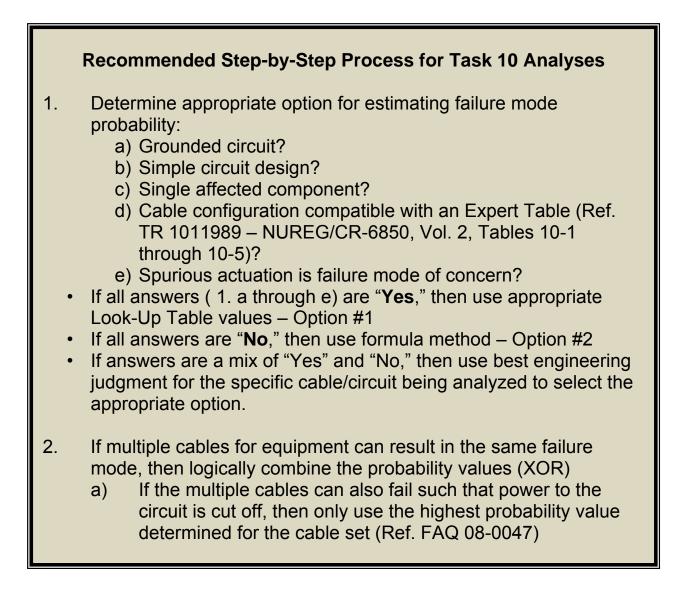




| | NEI 00-01, Rev. 2, Section | NEI 00-01 – Probability of Spurious | 6850/1011989 Sections that cover step | Comments |
|---|---|---|---|--|
| | Section | Actuation | coverstep | |
| | 5 – Risk Signifi- cance Analysis | 5.2.1.2 | 10.5.3 | NEI 00-01, Rev. 2, only recommends use of tables to determine spurious actuation probability estimates. NUREG/CR-6850, EPRI TR 1011989 also offers formula method. |
| - | | | | |
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Task 10: Circuit Failure Mode Likelihood Analysis Methodology Summary

This document summarizes the process for determining the probability, or likelihood, of a particular circuit failure mode occurrence. It includes the five Failure Mode Probability Estimate Tables employed under the Option #1 analysis approach, and the Option #2 Computational Probability Estimate formulas. **Important!** Please refer to the complete discussion of this methodology provided in NUREG/CR-6850, EPRI 1011989, "EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities; Volume 2: Detailed Methodology," Final Report, September 2005, when applying this methodology in non-classroom situations.



Selecting the Analysis Approach

1. Option #1: Failure Mode Probability Estimate Tables

Tables of probability estimates would appropriately be used for cables that meet the following criteria:

- The circuit is of a grounded design (including impedance grounded systems with ground fault trip capability),
- The cable is part of the control circuit for a typical component (e.g., non-complex MOVs, SOVs, pumps),
- The cable is associated with a single component,
- The cable configuration is known and can be readily associated with one of the defined configurations in Tables 1 through 5, and
- The principal hot short failure mode of concern is a spurious operation of the component.
- 2. Option #2: Computational Probability Estimates

Use of the probability estimate formulas are recommended for cases where:

- The circuit is ungrounded or is impedance grounded without ground fault trip capability,
- The cable is part of a relatively complex circuit or component,
- The cable is associated with or can influence the behavior of multiple components (e.g., safeguards actuation signal, bus shed scheme, etc.),
- The cable configuration is not easily categorized into one of the defined configurations contained in Tables 10-1 through 10-5.

Performing the Circuit Failure Mode Probability Analyses

Option #1: Failure Mode Probability Estimate Tables

- 1. Categorize the circuit of interest based on its configuration attributes.
- 2. From the appropriate table (Tables 10-1 to 10-5), select the probability estimates for the failure modes of concern.
- 3. If the cable failure mode can occur due to different cable interactions, the probability estimate is taken as the simple sum of both estimates. For example, if a particular thermoset cable failure mode can be induced either by an intra-cable shorting event (P = 0.30) or by an inter-cable shorting event (P = 0.03; mid-range of 0.01–0.05), the overall probability of that failure mode is estimated to be 0.33.

| Table 10-1 |
|---|
| Failure Mode Probability Estimates Given Cable Damage |
| Thermoset Cable with Control Power Transformer (CPT) |

| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
|-----------------|--|--|--|
| Tray | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.30 0.20 0.10 0.01 – 0.05 | 0.10 – 0.50 0.05 – 0.30 0.05 – 0.20 |
| Conduit | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.075 0.05 0.025 0.005 - 0.01 | 0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05 |

M/C: Multi-conductor cable

1/C: Single conductor cable

Intra-cable: An internally generated hot short. The source conductor is part of the cable of interest Inter-cable: An externally generated hot short. The source conductor is from a separate cable

Table 10-2Failure Mode Probability Estimates Given Cable DamageThermoset Cable without CPT

| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
|-----------------|--|------------------------------------|--|
| Тгау | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.60 0.40 0.20 0.02 – 0.1 | 0.20 - 1.0 0.1 - 0.60 0.1 - 0.40 |
| Conduit | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.15 0.1 0.05 0.01 – 0.02 | 0.05 - 0.25 0.025 - 0.15 0.025 - 0.1 |

| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
|-----------------|--|--|--|
| Тгау | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.30 0.20 0.10 0.01 – 0.05 | 0.10 - 0.50 0.05 - 0.30 0.05 - 0.20 |
| Conduit | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.075 0.05 0.025 0.005 – 0.01 | 0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05 |

Table 10-3Failure Mode Probability Estimates Given Cable DamageThermoplastic Cable with CPT

Table 10-4Failure Mode Probability Estimates Given Cable DamageThermoplastic Cable without CPT

| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
|-----------------|--|------------------------------------|--|
| Тгау | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.60 0.40 0.20 0.02 – 0.1 | 0.20 - 1.0 0.1 - 0.60 0.1 - 0.40 |
| Conduit | M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable | 0.15 0.1 0.05 0.01 – 0.02 | 0.05 - 0.25 0.025 - 0.15 0.025 - 0.1 |

Table 10-5Failure Mode Probability Estimates Given Cable DamageArmored or Shielded Cable

| Raceway Type | Description of Hot Short | Best Estimate | High Confidence Range |
|-----------------|-----------------------------|------------------|-----------------------------|
| With CPT | M/C Intra-cable | 0.075 | 0.02 – 0.15 |
| Without CPT | M/C Intra-cable | 0.15 | 0.04 - 0.30 |

3. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the probability estimates associated with all affected cables should be considered when deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

 $P_{\text{Component failure Cable A}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$

Option #2: Computational Probability Estimates

Application of this calculational method is more complex and is only recommended for cases where Option #1 cannot reasonably be applied. The intent is to give the analyst a means of refining the estimated circuit failure mode probabilities based on the most important characteristics of the cable/circuit under study.

This computational method involves applying circuit failure mode probability estimation formulas. The following discussions provide only the minimum definition of the failure mode likelihood estimation formulas and their terms. For a complete discussion of the technical basis, detailed explanations, and examples of usage, please refer to Appendices J and K in Volume 2 of EPRI 1011989, NUREG/CR-6850.

The probability of occurrence for a specific hot short failure mode (P_{FM}) is estimated by the formula:

 $P_{FM} = CF \times P_{CC,}$

Where:

 P_{FM} = The probability that a specific hot short failure mode of interest will occur in a specific circuit given a fire of sufficient intensity to cause cable damage,

- P_{CC} = The probability that a conductor-to-conductor short will occur prior to a short-toground or short to a grounded conductor, and
- CF = A configuration factor applied to P_{CC} to account for the relative number of source conductors and target conductors. Target conductors are those conductors of a circuit that, if contacted by an electrical source of proper magnitude and voltage, will result in abnormal energization of the circuit, component or device of concern. Source conductors represent energized conductors that are a potential source of electrical energy.
- 1. Calculate P_{CC} as follows:

| Cables in trays: | $P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 1]$ |
|----------------------------------|--|
| Cables in conduit ¹ : | $P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 3]$ |
| Ungrounded systems: | $\mathbf{P}_{\mathrm{CC}} = (\mathbf{C}_{\mathrm{Tot}} - C_G) / \left[(\mathbf{C}_{\mathrm{Tot}} - C_G) + (2 \times C_G) \right]$ |
| Where: | |

- $C_{Tot} =$ The total number of conductors in the cable of interest (including spares), and
- C_G = The number of grounded (or common) conductors in the cable of interest. The analyst should determine the number of grounded/common conductors based on the circuit configuration (contact positions, etc.) that represent the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

Note: For ungrounded AC and DC systems, C_G represents the number of return conductors to the power source associated with the circuit of interest (e.g., the negative polarity conductors for an ungrounded 125 VDC circuit)

2. Calculate CF as follows.

Non-armored cables: $CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$

Armored cables: $CF = (C_T \times C_S) / C_{Tot}$

Where:

- C_S = The total number of source conductors in the cable under evaluation,
- C_T = The total number of target conductors in the cable², and
- C_{Tot} = The total number of conductors in the cable, as before.

¹ Armored and shielded cable should use the equation for conduit.

² Target conductors are only those cable conductors capable of forcing the component or circuit into the undesired state or condition of interest. For example, the target conductors associated with causing a spurious operation of the component will likely differ from target conductors associated with causing a loss of control condition.

Note: CF should be ≤ 1.0 . If the calculated value of CF is greater than 1, then set CF = 1. In practical applications it is highly unlikely that the calculated value of CF will ever exceed 1. For this to occur, virtually all conductors in the cable would need to be either a source conductor or target conductor.

Note: The analyst should determine the number of target and source conductors based on the circuit configuration (contact positions, etc.) that represents the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

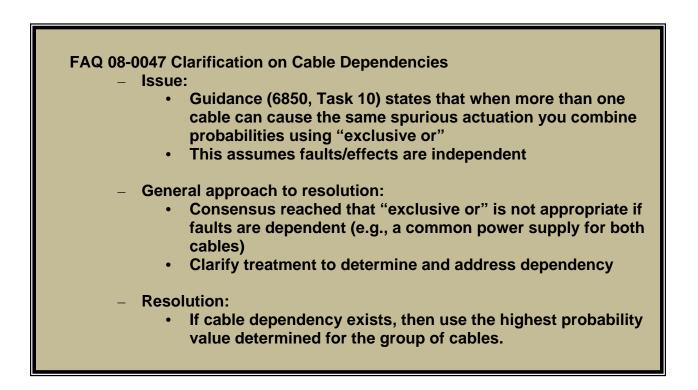
3. Calculate P_{FM} as follows:

 $P_{FM} = CF \times P_{CC},$

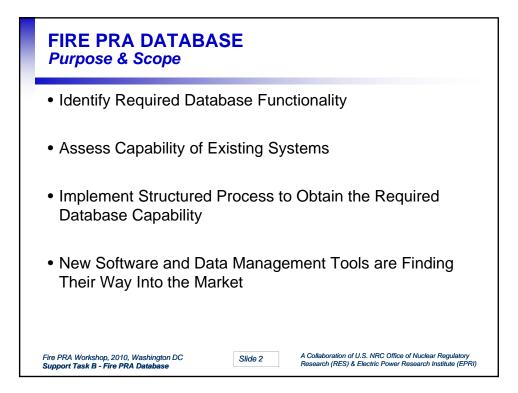
where CF and P_{CC} are determined using the formulas discussed above.

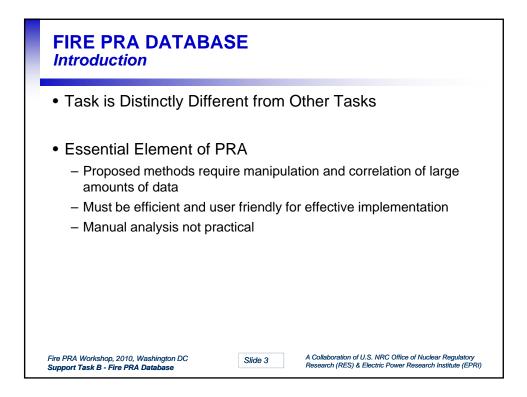
4. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the probability estimates associated with all affected cables should be considered in deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

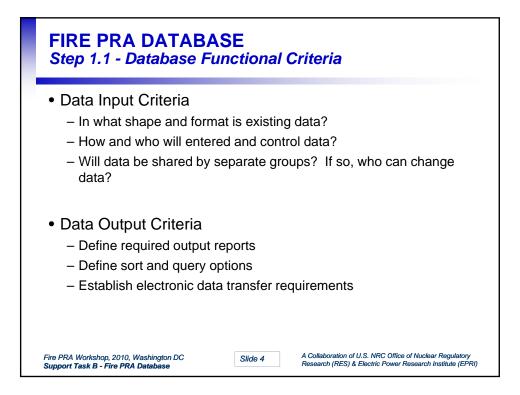
 $P_{\text{Component failure Cable A}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$

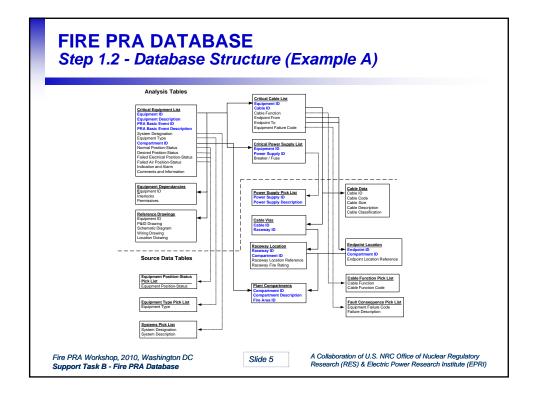


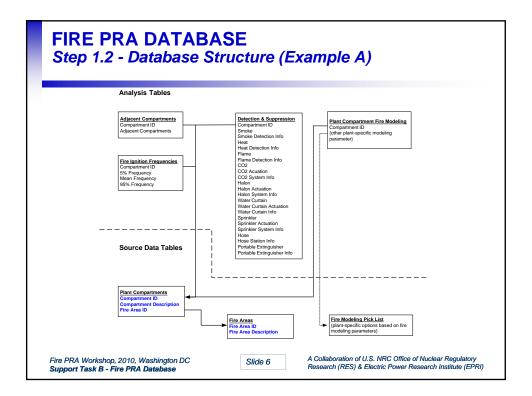


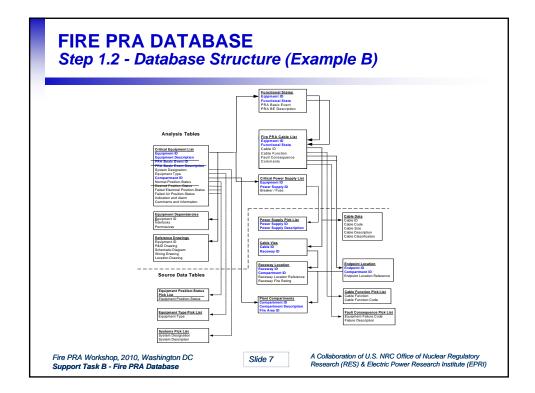


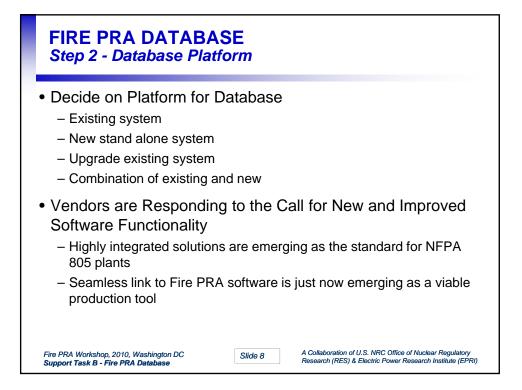


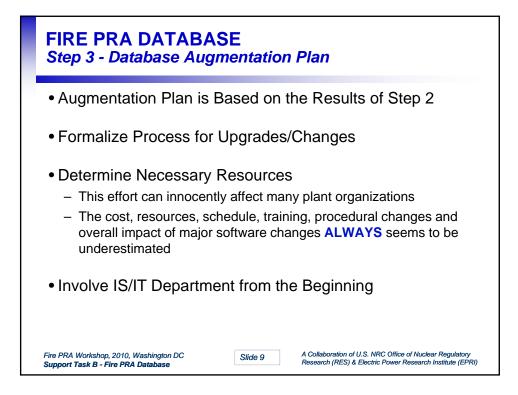


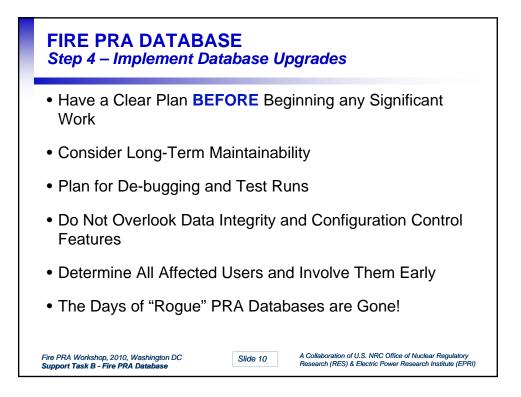


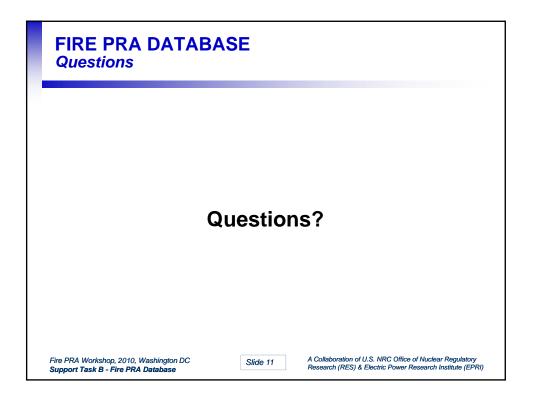


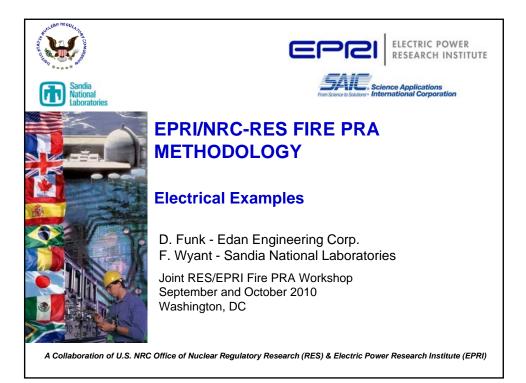


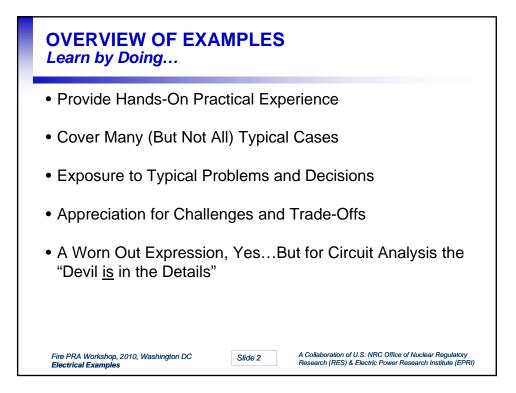












HANDS-ON EXERCISES Example Circuit Analysis Problem Set

| Example No. | Component | Description of Example | Function State |
|----------------|------------------------|---|---------------------------------------|
| 1 | AOV-8879B | Easy AOV circuit with desired change of state to failsafe position | Open - Closed |
| 2 | AOV-8879B | Easy AOV circuit with desired position to maintain energized state | Open - Open |
| 3 | MOV-8888 | Easy MOV circuit with desired position to maintain initial state | Open - Open |
| 4 | MOV-8888 | Easy MOV circuit with desired change of state | Open - Closed |
| 5 | MOV-11 | DC MOV control circuit with desired change of state | Close - Open |
| 6 | MOV-15 | Double pole DC motor control circuit with desired change of state - | 6a: Close - Throttled |
| 0 | MOV-15 | remote and local operation | 6b: Close - Throttled Local |
| 7 | AOV-2869A | Hard AOV circuit with desired position to maintain initial state | Closed - Closed |
| 8 | AOV-2869A | Hard AOV circuit with desired change of state | Closed - Open |
| 9 | MOV-8706A | Hard MOV with desired position to maintain initial state | Closed - Closed |
| 10 | MOV-8706A | Hard MOV circuit with desired change of state | Closed - Open |
| 11 | ANN-1 | Annunciator Circuit | Available – Nonspurious |
| 12 | HPI-B | 4.16 kV Motor | Standby – On |
| 13 | COMP-1 | 480 V Motor | Cycle - Cycle |
| 14 | MCC-1B | 480V MCC | Energized - Energized |
| 15 | LC-B | 480V Load Center | Energized - Energized |
| 16 | 52-DF01 | 4.16 kV OSP Breaker | Closed - Closed |
| 17 | FCV 605A | Instrument control signal to flow control valve | Closed - Modulate |
| 18 | TTR2 | Instrument loop – temperature indicator | Available - Available |
| | Workshop, 2010, Washir | | f U.S. NRC Office of Nuclear Regulate |

