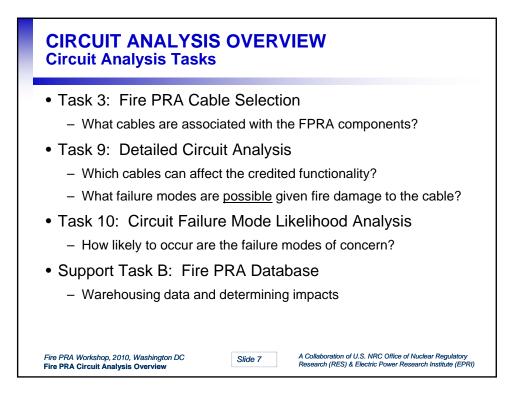
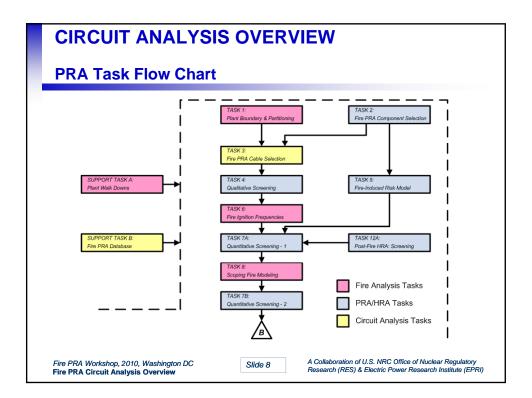
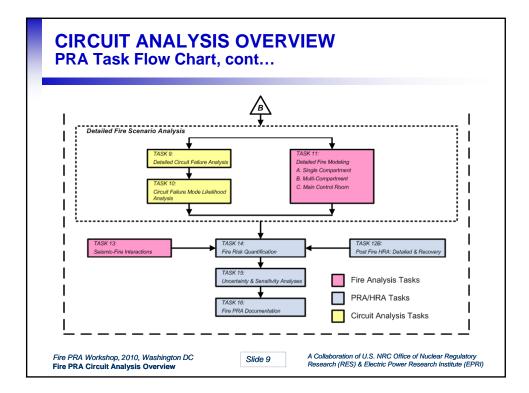
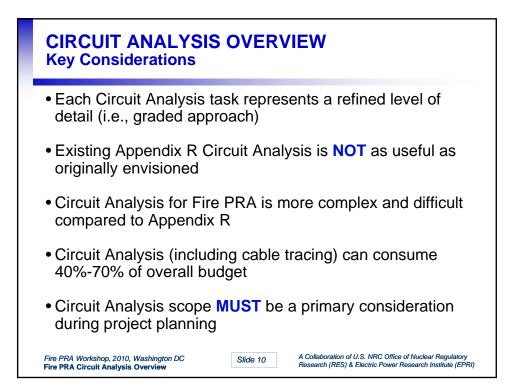


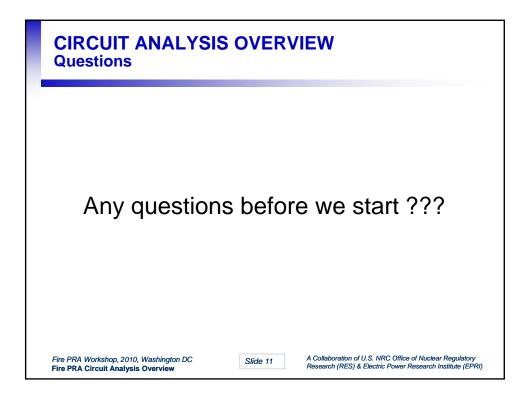
-	Tuesday	Wednesday	Thursday	Friday
8:30	· · · · · · · · · · · · · · · · · · ·	weunesuay	inuisuay	Thuay
8:45				
9:00		Presentation - Detailed	Presentation - Fire PRA	Exercises - Work Task 10
9:15		Circuit Failure Analysis	Database	Sample Problems
9:30		(Task 9)		
9:45			Break	Break
10:00	General Session -			
10:15	Introduction to all Modules	Break	- Fire PRA Database	Discussion - Task 10
10:30			(continued)	Sample Problems
10:45		Presentation - Task 3 &		
11:00		Task 9 Sample Problem	n :	D :
11:15		Definition and Examples	Discussion - Open, Q&A,	Discussion - Summary and Conclusions
11:30			etc.	Conclusions
	LUNCH BREAK	LUNCH BREAK	LUNCH BREAK	LUNCH BREAK
13:00				
13:15	Presentation - Fire PRA			
13:30	Circuit Analysis Overview		Presentation - Circuit Failure Mode Likelihood	
13:45			Analysis (Task 10)	
	Presentation - Fire PRA	Exercises - Work Task 3	Analysis (Task 10)	
	Circuit Analysis Summary	& Task 9 Sample Problems		
_	Break		Break	
14:45	Presentation - Fire PRA		- Circuit Failure Mode	General Session - Closing: All Modules
	Cable Selection (Task 3)		Likelihood Analysis	Closing: All Modules
15:15			(continued)	
	Break	Break	Break	
16:00			- Circuit Failure Mode	
16:15	- Fire PRA Cable Selection	Discussion - Task 3 &	Likelihood Analysis (cont.)	
16:30	(continued)	Task 9 Sample Problems	Presentation - Task 10	
16:45			Sample Problems	
17:00	ADJOURN	ADJOURN	ADJOURN	ADJOURN

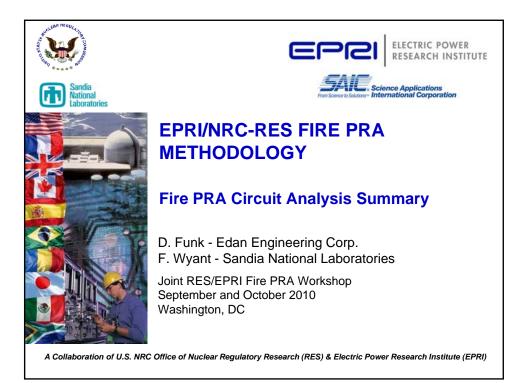


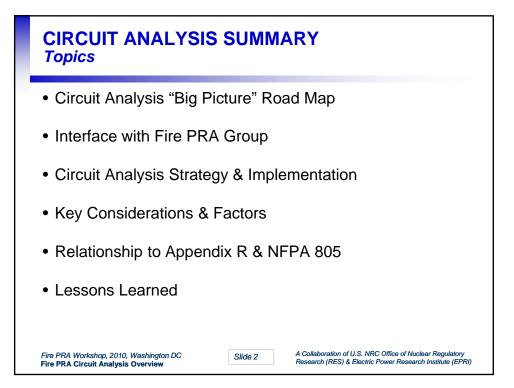


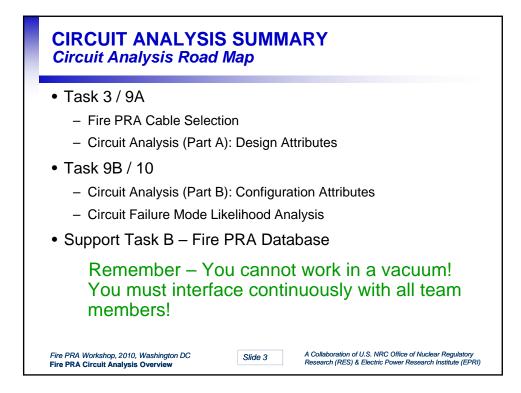


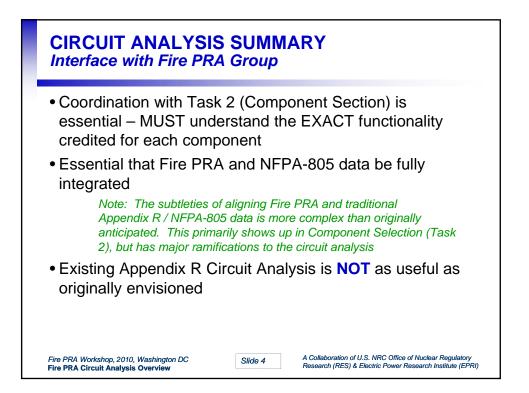


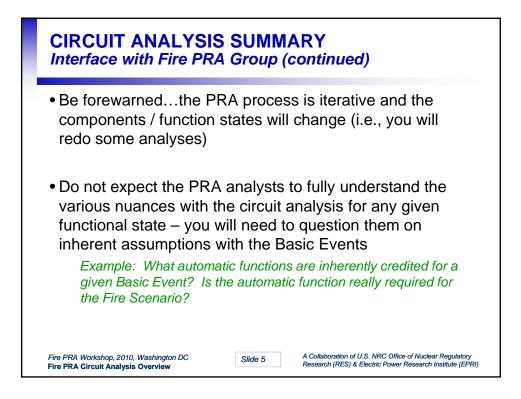


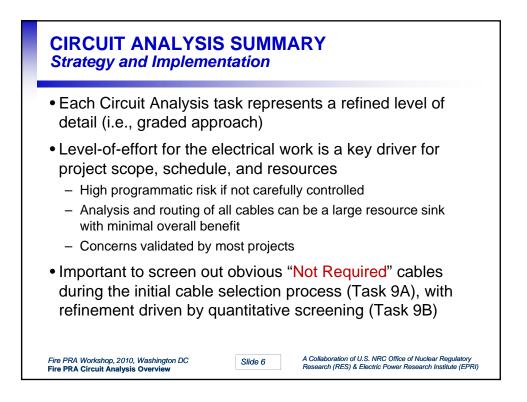


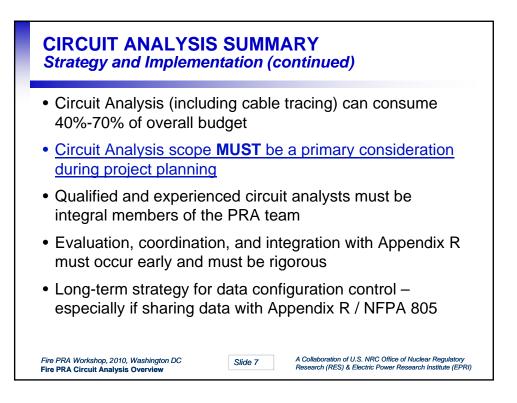


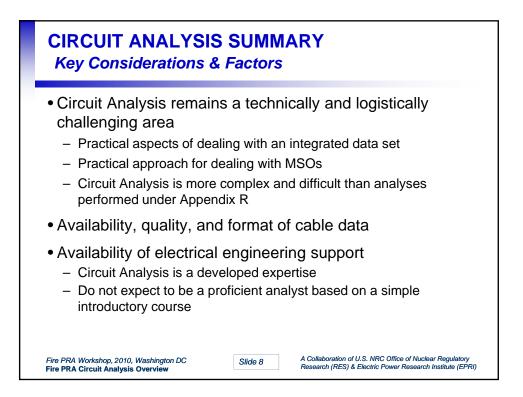


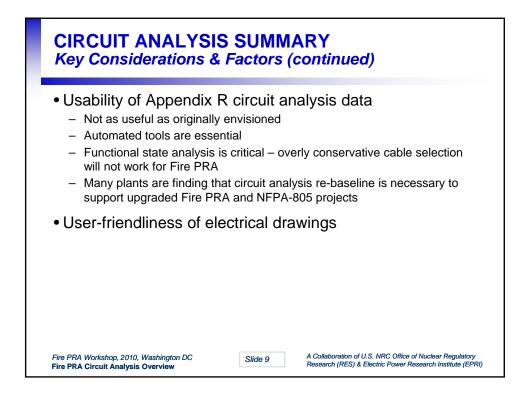


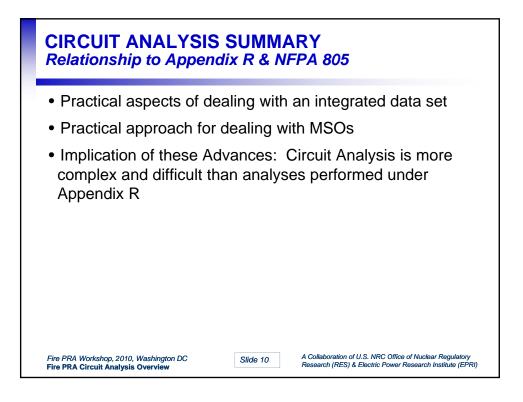


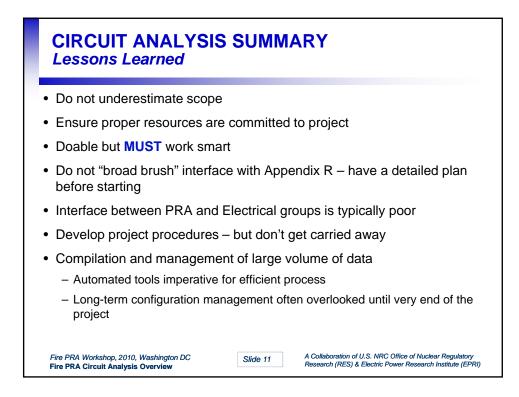


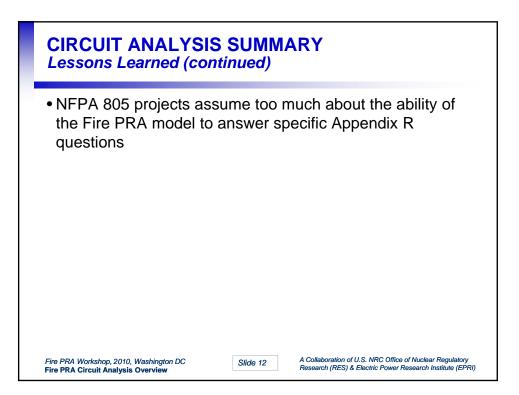


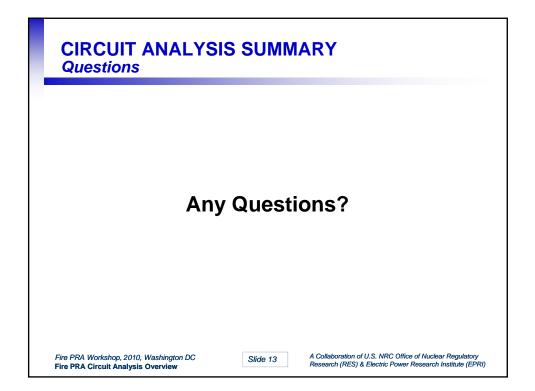




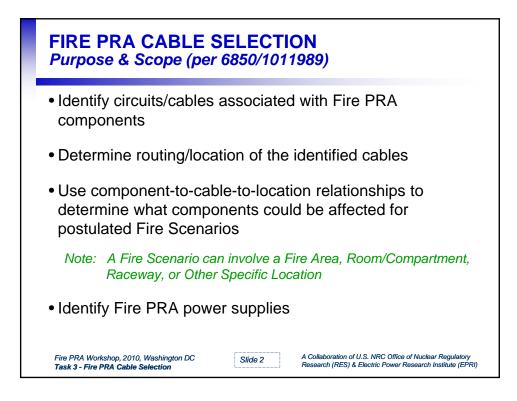


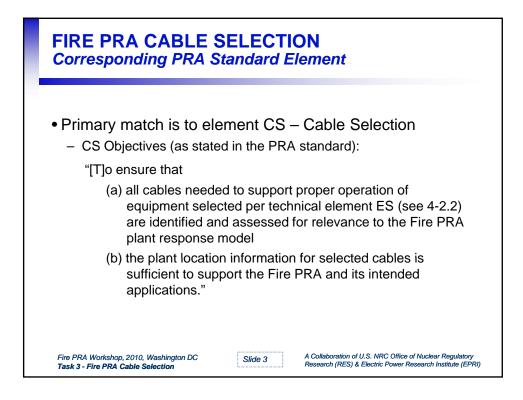


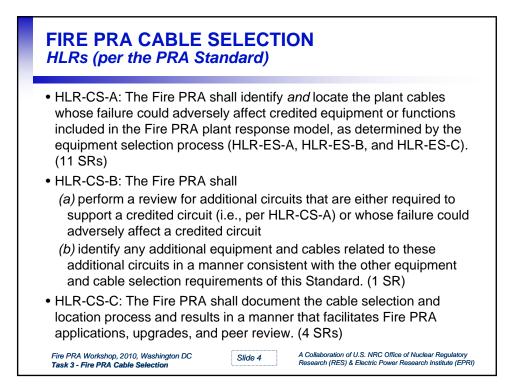


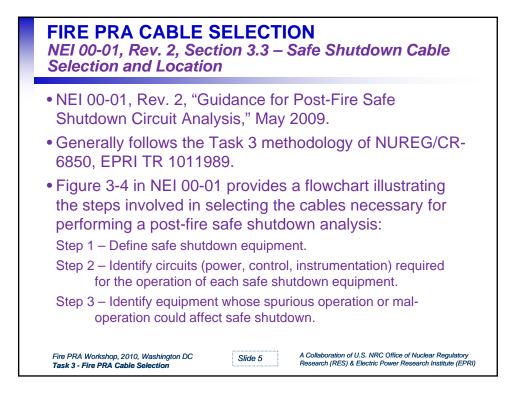


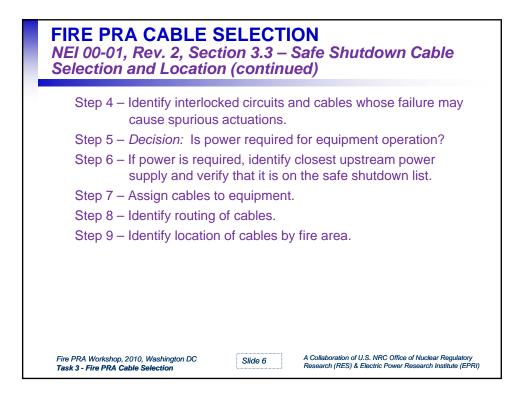


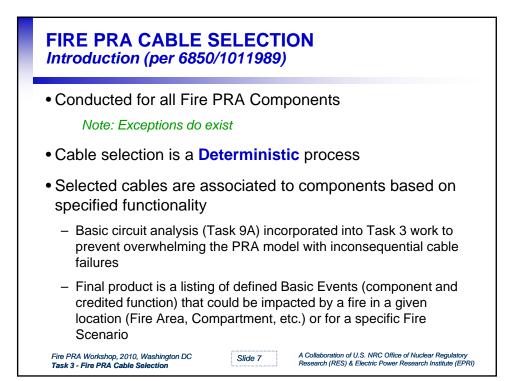


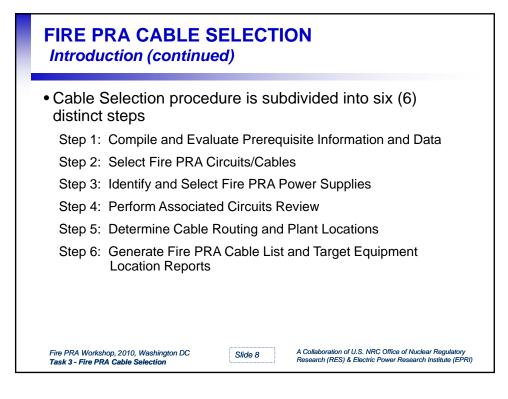


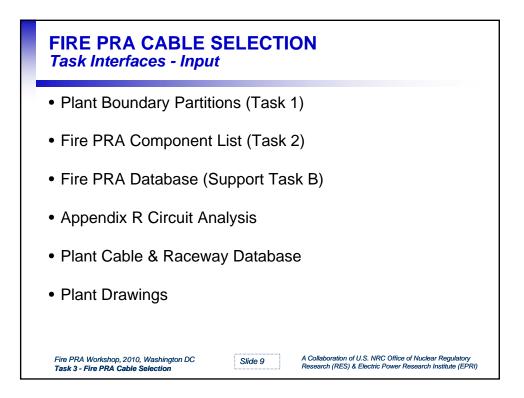


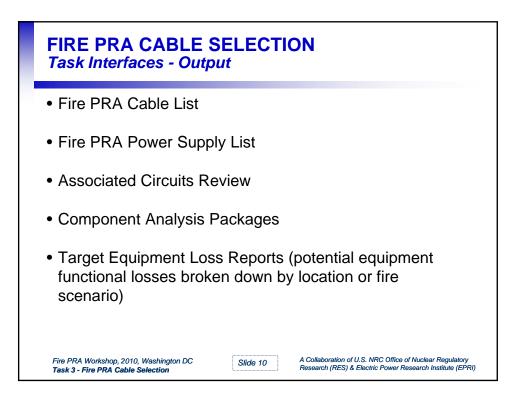


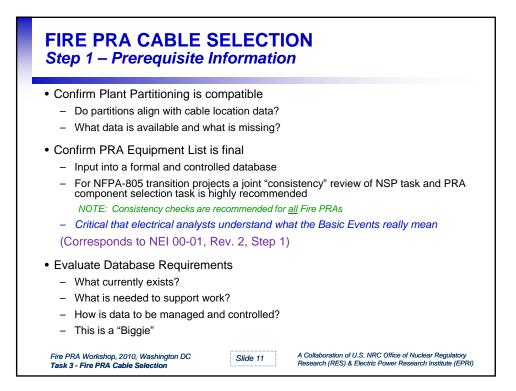




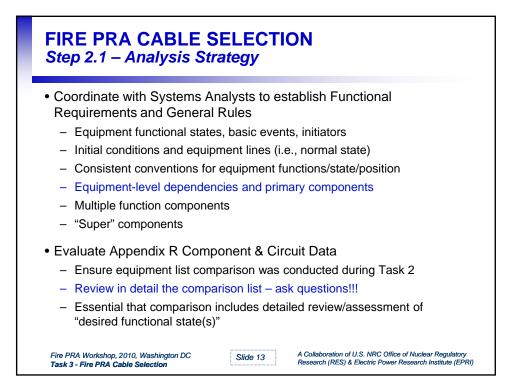


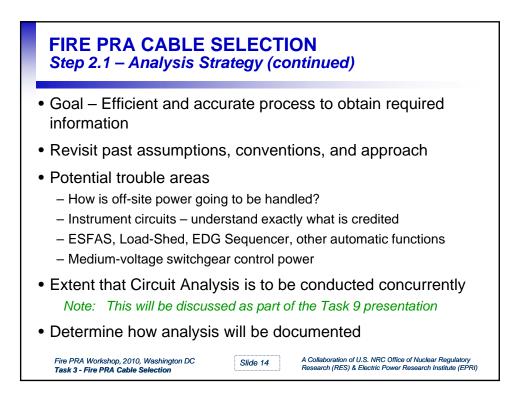


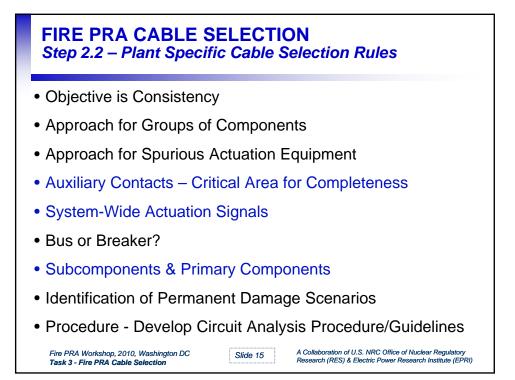


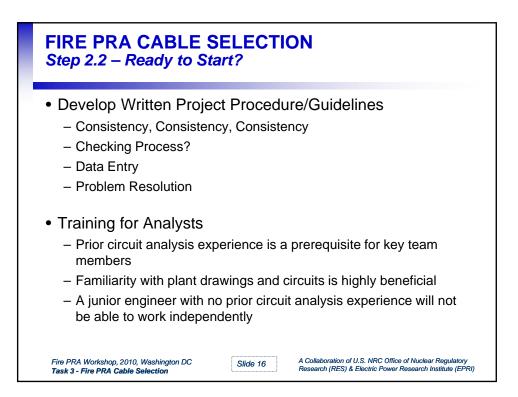


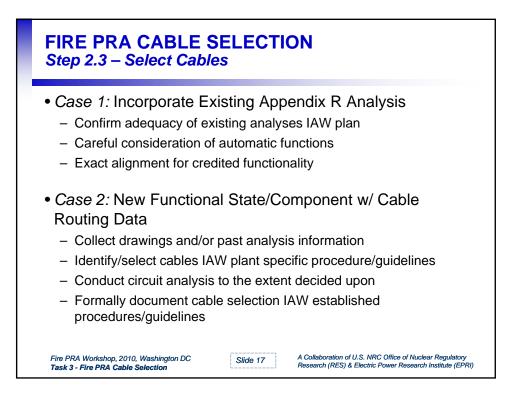
FIRE PRA CABLE SELECTION Step 2 – Select Fire PRA Cables Analysis Cases Appendix R Component with same functional requirements Must consider which (if any) automatic features are included in the existing analysis Aligning existing analyses to Fire PRA Basic Events is not straightforward - Appendix R Component with *different* functional requirements - Non-Appendix R Component with cable location data Non-Appendix R Component without cable location data Analysis Sub-Steps - Step 2.1: Analysis Strategy - Step 2.2: Plant Specific Rules - Step 2.3: Select Cables Corresponding PRA Standard SRs: CS-A1, A3 Corresponding NEI 00-01, Rev. 2, Steps: 2 & 4 • A Collaboration of U.S. NRC Office of Nuclear Regulatory Fire PRA Workshop, 2010, Washington DC Slide 12 Task 3 - Fire PRA Cable Selection Research (RES) & Electric Power Research Institute (EPRI)

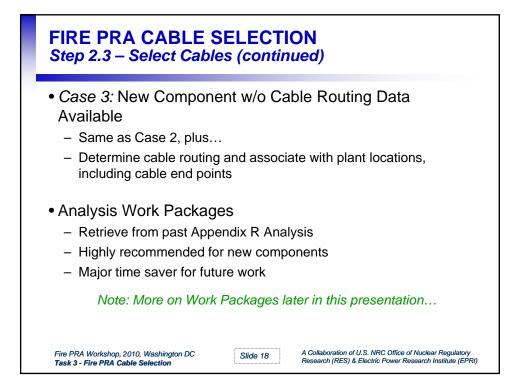


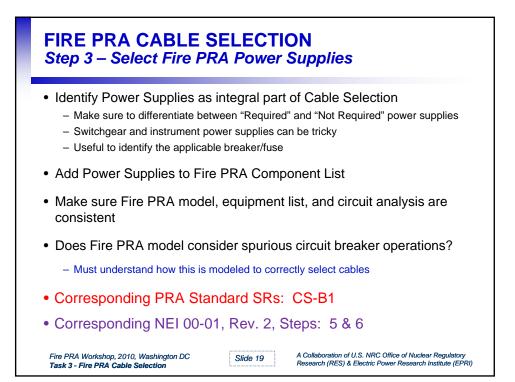


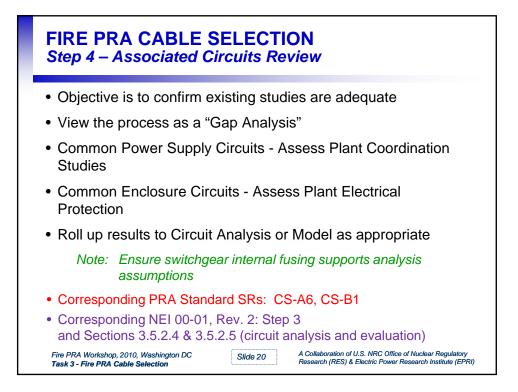


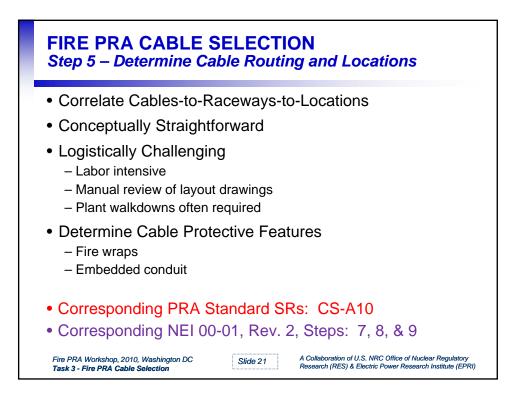


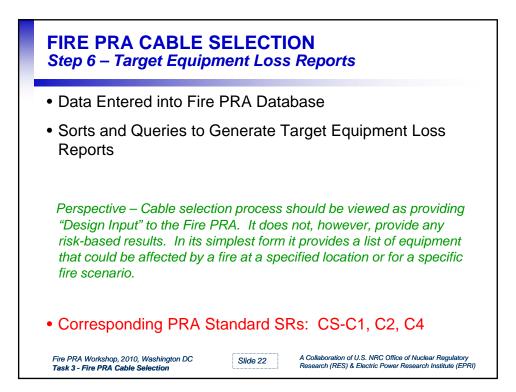


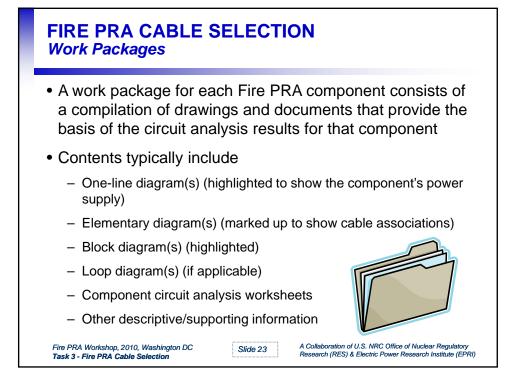


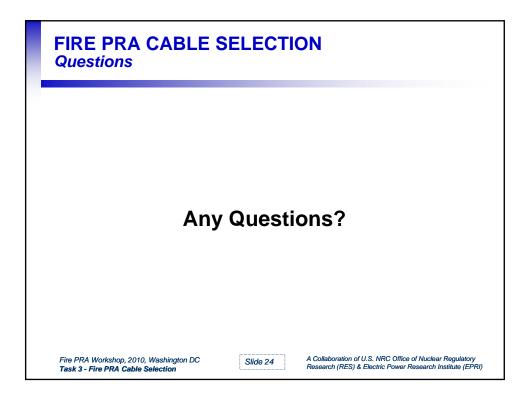






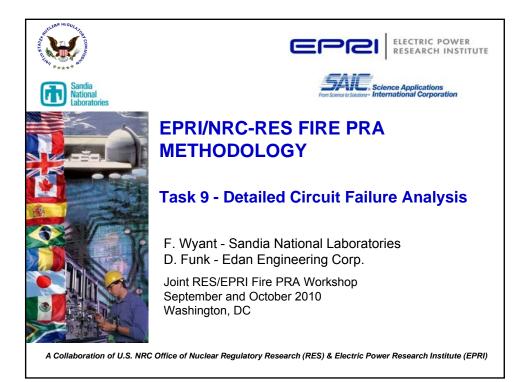


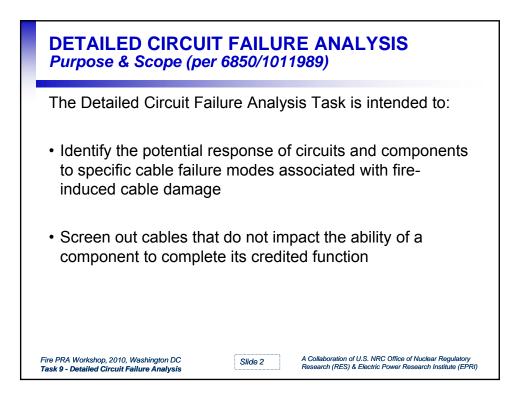


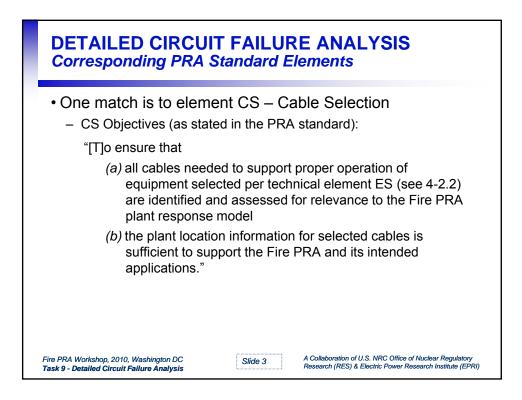


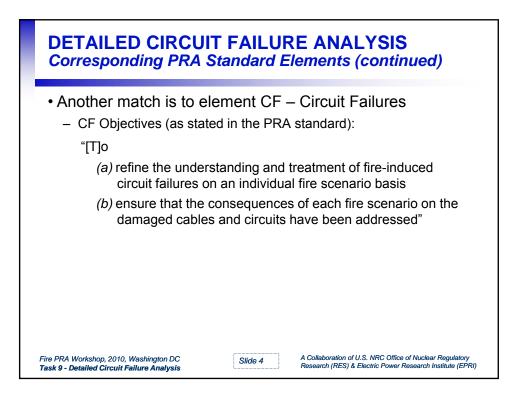
NLG/	/CR	-68	50, EPR	for the CS technical element to I TR 1011989	
Technical	HLR	SR	6850/1011989	Comments	
Element			Sections that		
			cover SR		
CS	Α	The F	The Fire PRA shall identify and locate the plant cables whose failure could adversely affect credited equipment or		
		functions included in the Fire PRA plant response model, as determined by the equipment selection process (HLR-ES-A			
		HLR-B	S-B, and HLR-ES-C).	
		1	3.5.2		
		2	9.5.2	Covered in "Detailed Circuit Failure Analysis" chapter	
		3	3.5.2, 9.5.2	Also covered in "Detailed Circuit Failure Analysis" chapter	
		4	3.5.3		
		5	9.5.2	Covered in "Detailed Circuit Failure Analysis" chapter	
		6	3.5.4, 9.5.2	Also covered in "Detailed Circuit Failure Analysis" chapter	
		7	9.5.2	Covered in "Detailed Circuit Failure Analysis" chapter	
		8	9.5.2	Covered in "Detailed Circuit Failure Analysis" chapter	
		9	9.5.2	Covered in "Detailed Circuit Failure Analysis" chapter	
		10	3.5.5		
		11	3.5.5		
	В	The F	ire PRA shall		
				r additional circuits that are either required to support a credited circuit (i.e., per HLR-CS-A) or	
				rersely affect a credited circuit	
				nal equipment and cables related to these additional circuits in a manner consistent with the	
		othe	equipment and c	ble selection requirements of this Standard	
		1	3.5.3, 3.5.4		
	С	The Fire PRA shall document the cable selection and location process and results in a manner that facilitates Fire PRA			
		appli	cations, upgrades,	and peer review.	
		1	3.5.6		
		2	3.5.6		
		3	3.5.6		
		4	3.5.6		

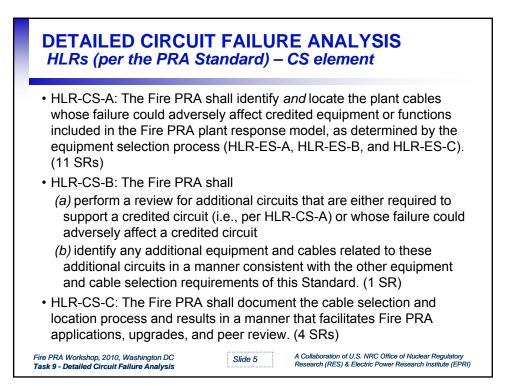
FIRE I	PRA	CABL	E SELECTION	NC
				own Cable Selection to
		550 EDE	TD 1011000	
VUREG/	CK-00	550, EPR	I TR 1011989	
NEI 00-01.	NEI 00-01.	6850/1011989	Comments	
Rev. 2,	Figure 3-4	Sections that		
Section	Step	cover step		
3.3 - Safe	1	3.5.1		
Shutdown	2	3.5.2		
Cable	3	3.5.4		
Selection	4	3.5.2		
and	5	3.5.3		
Location	6	3.5.3		
	7	3.5.5		
	8	3.5.5		
	9	3.5.5		
		0.14/		A Collaboration of U.S. NRC Office of Nuclear Regulatory
Task 3 - Fire I		0, Washington L	C Slide 26	Research (RES) & Electric Power Research Institute (EPRI)
		Geleculli		

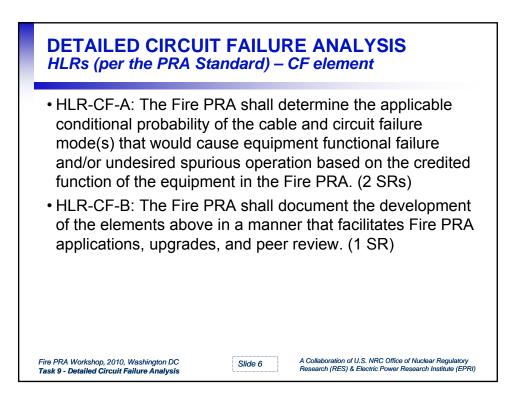


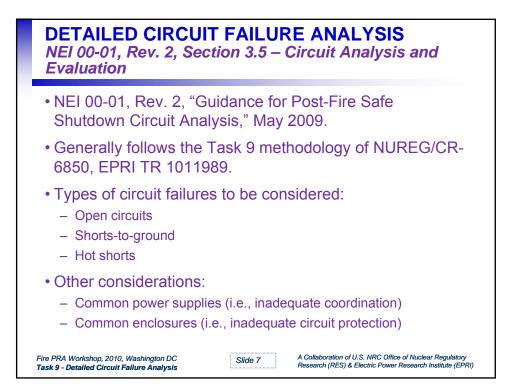


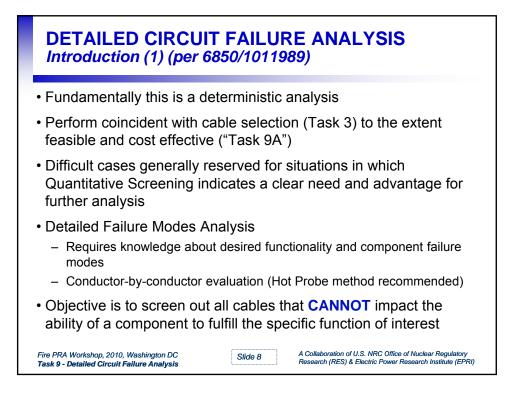


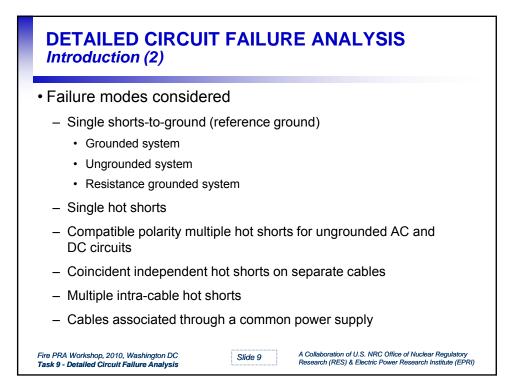


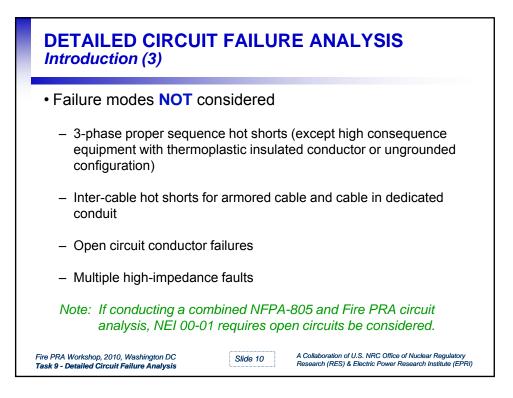


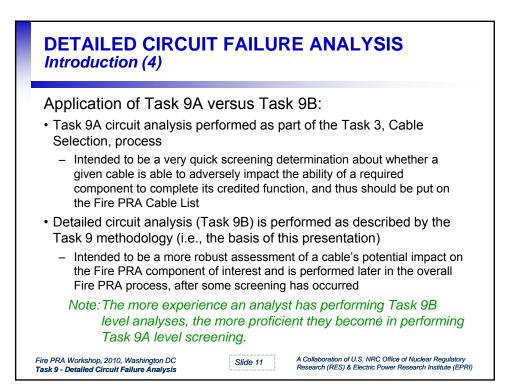


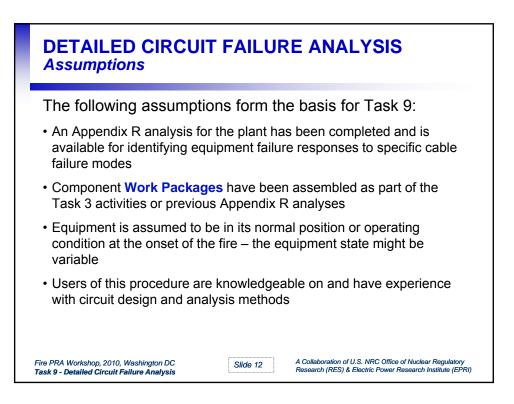


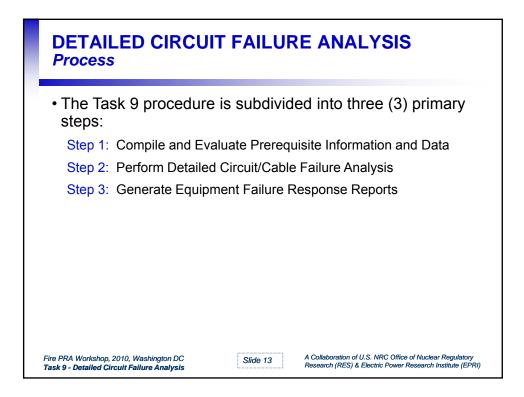


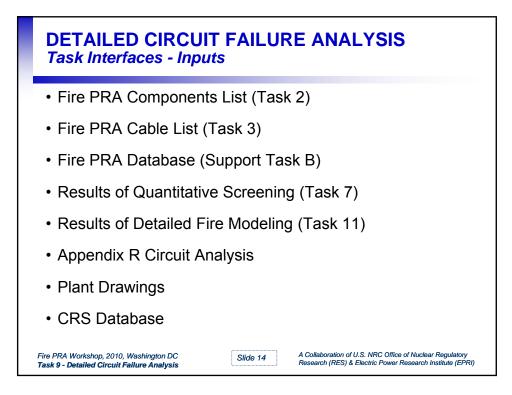


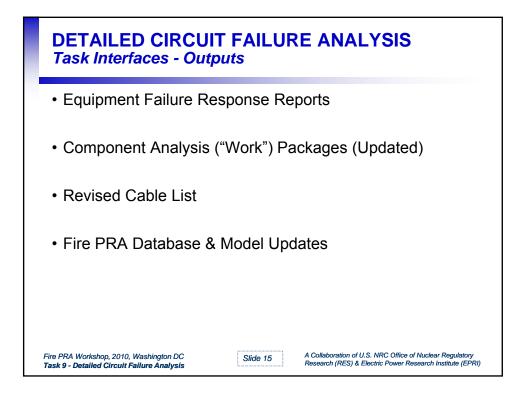


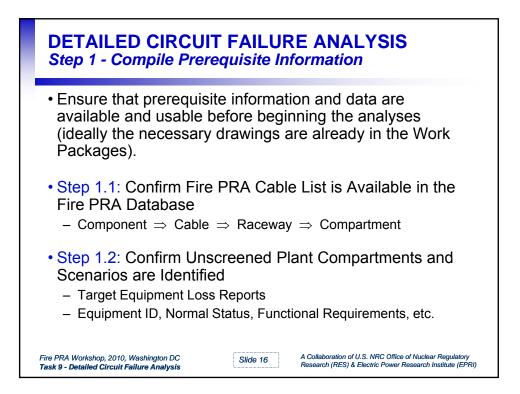


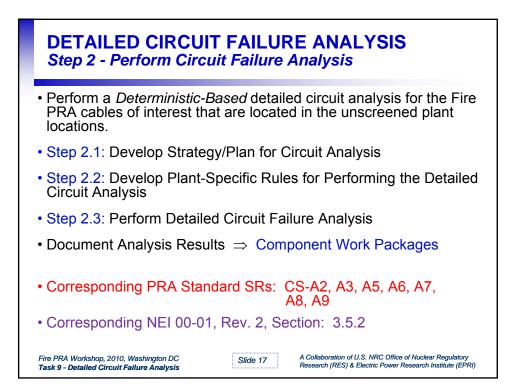


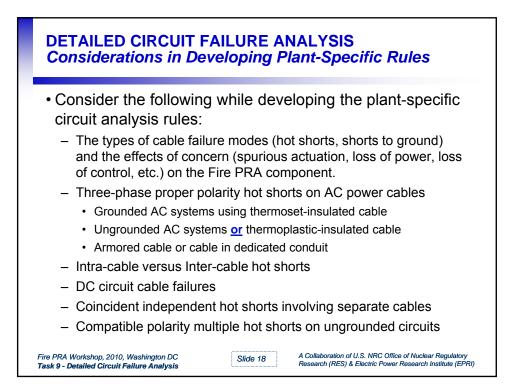


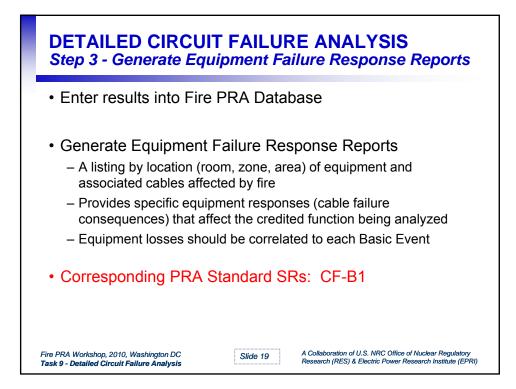


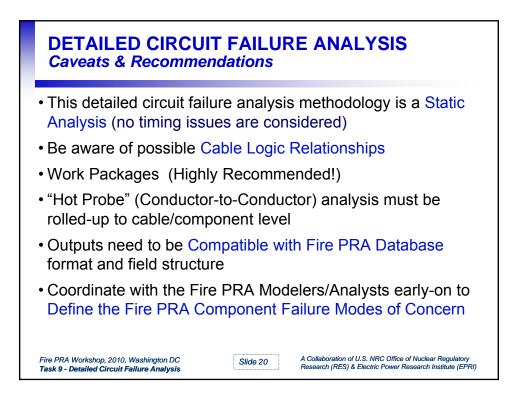


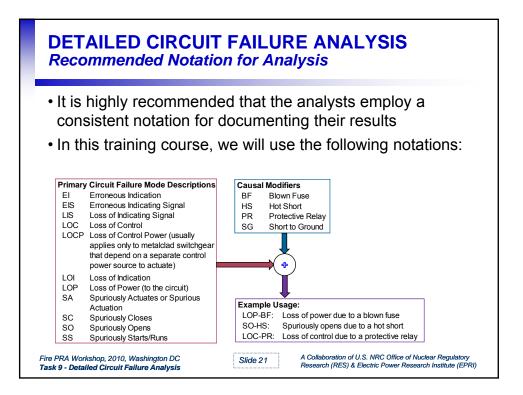


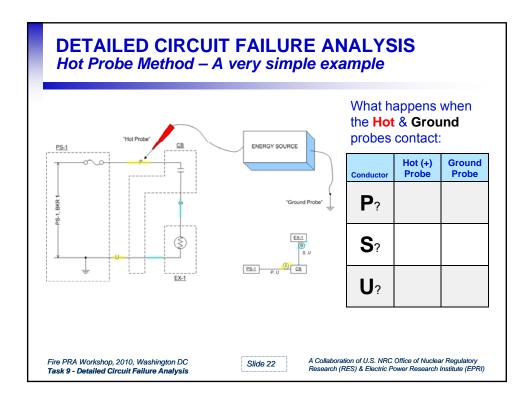


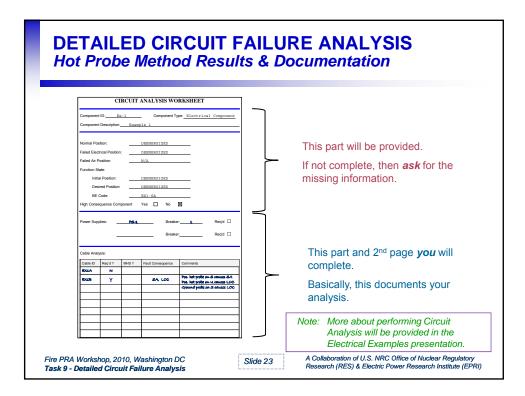


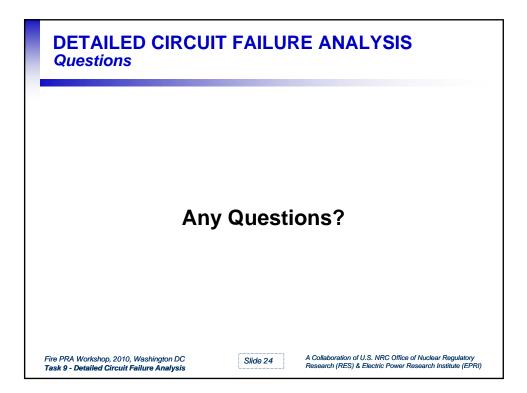


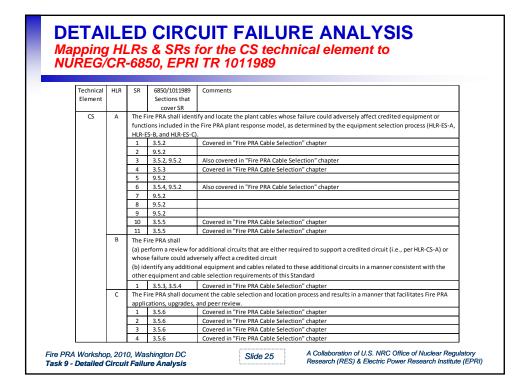


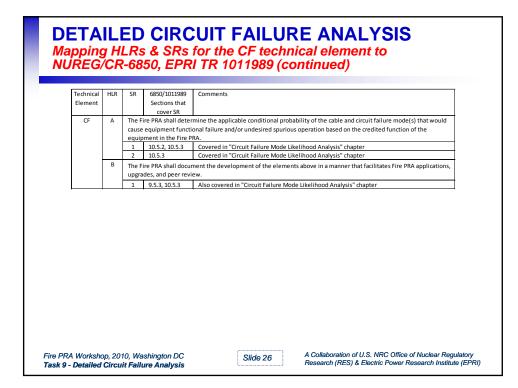












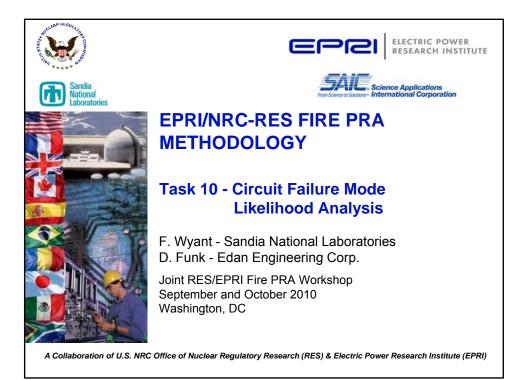
DETAILED CIRCUIT FAILURE ANALYSIS Mapping NEI 00-01, Rev. 2, Circuit Analysis and Evaluation to NUREG/CR-6850, EPRI TR 1011989

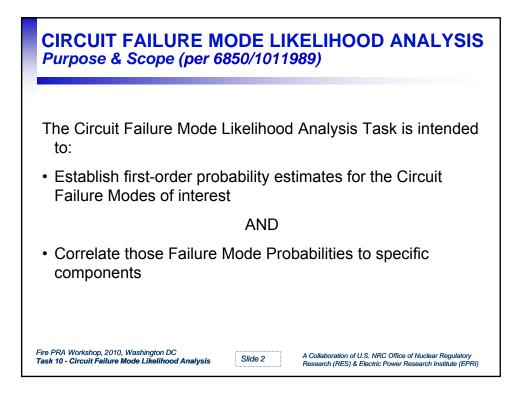
NEI 00-01,	NEI 00-01,	6850/1011989	Comments
Rev. 2,	Section 3.5.2 -	Sections that	
Section	Types of	cover step	
	Circuit		
	Failures		
3.5 -	3.5.2.1: Due to		
Circuit	an Open	N/A	Open circuits not considered in 6850/1011989 as discussed in 9.5.2
Analysis	Circuit		
and	3.5.2.2: Due to		
Evaluation	a Short-to-	9.5.2	
	Ground		
	3.5.2.3: Due to	9.5.2	
	a Hot Short	9.5.2	
	3.5.2.4: Due to		
	Inadequate	3.5.4	Covered in "Fire PRA Cable Selection" chapter
	Circuit	3.3.4	Covered In File PKA Cable Selection Chapter
	Coordination		
	3.5.2.5: Due to		
	Common	3.5.4	Covered in "Fire PRA Cable Selection" chapter
	Enclosure	3.3.4	Covered in The FRA Cable Selection Chapter
	Concerns		

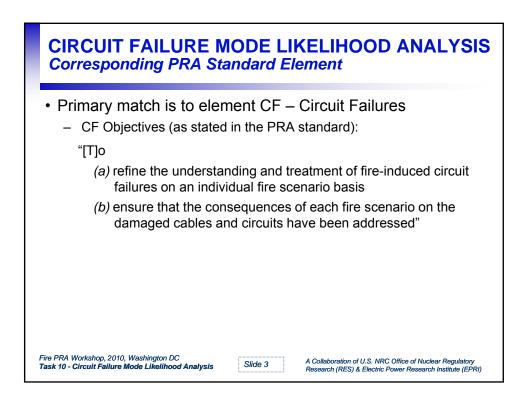
Fire PRA Workshop, 2010, Washington DC Task 9 - Detailed Circuit Failure Analysis

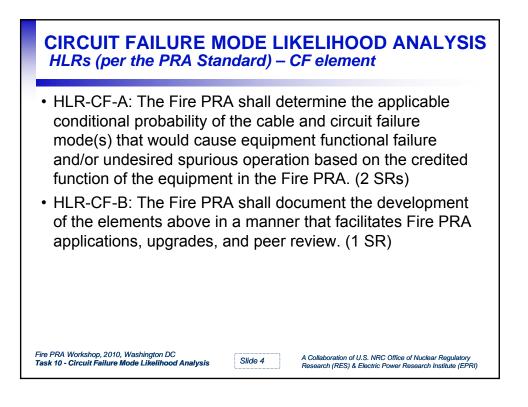
Slide 27

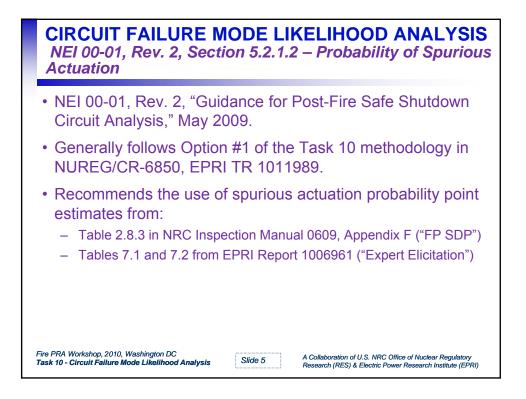
A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

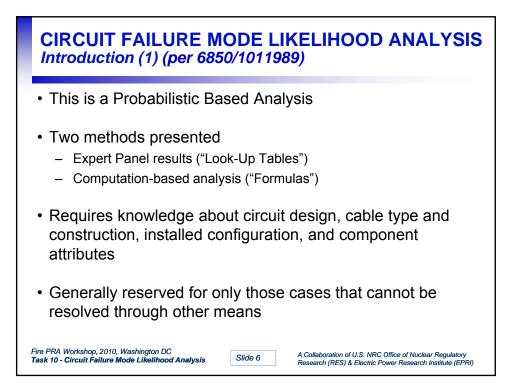












CIRCUIT FAILURE MODE LIKELIHOOD ANALYSIS *Introduction (2)*

Caveats:

- Our knowledge is greatly improved but <u>Uncertainties Are Still High</u>
 Very limited data for many issues
- For this reason, implementing guidance is intended to be Conservative
- Practical implementation is challenging
- Further analysis of existing test data and follow-on tests would be beneficial:
 - · Reduce uncertainties, including conservatisms as appropriate
 - · Solidify key influence factors

Fire PRA Workshop, 2010, Washington DC Task 10 - Circuit Failure Mode Likelihood Analysis

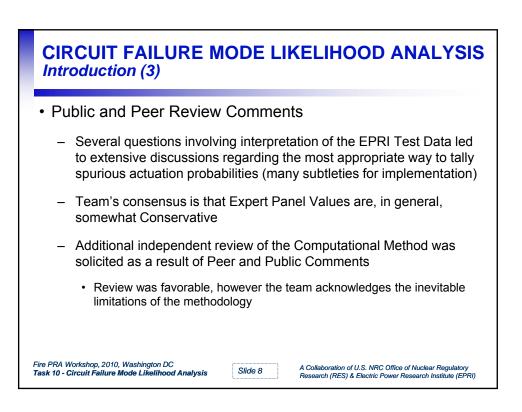
- Incorporate time as a factor (FAQ 08-0051, for AC circuits only; Status: Closed)
- Incorporate "End-Device" functional attributes and states (e.g., latching circuits vs. drop-out design)

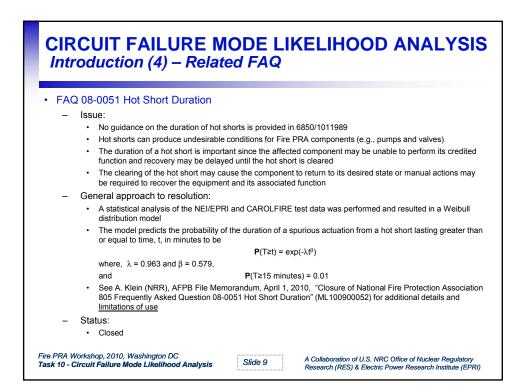
A Collaboration of U.S. NRC Office of Nuclear Regulatory Research (RES) & Electric Power Research Institute (EPRI)

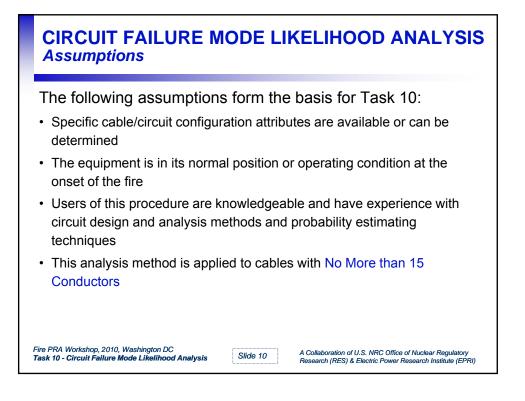
- Expert elicitation to produce refined spurious operation probabilities (planned for 2010)
- Computation-based method (formula) is an extrapolation of existing data; validation remains to be done. Conservatism has not been established.

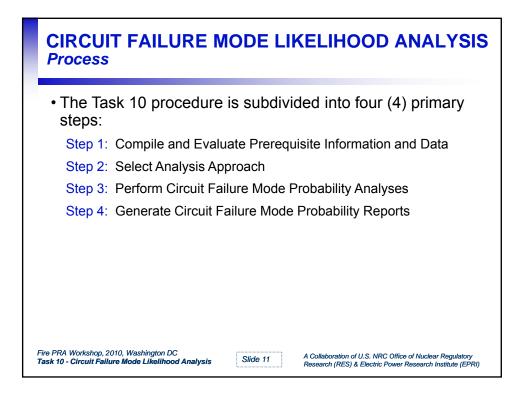
Slide 7

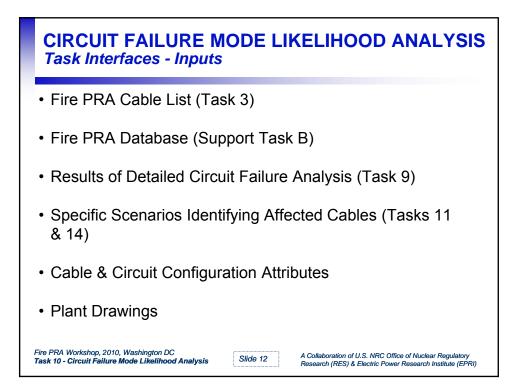
· Probabilities of sufficient quality to move ahead

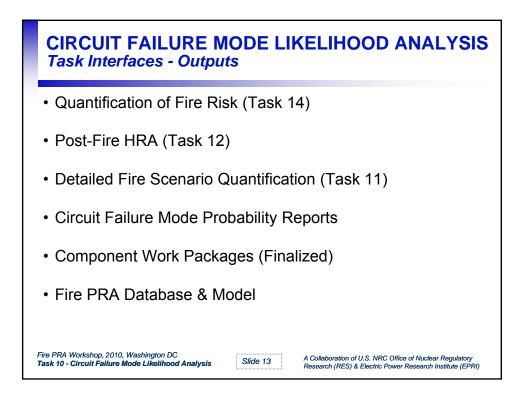


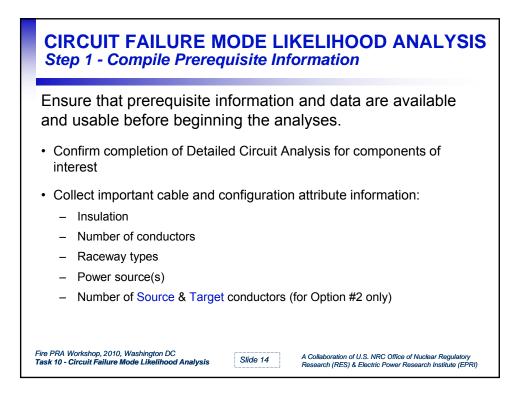


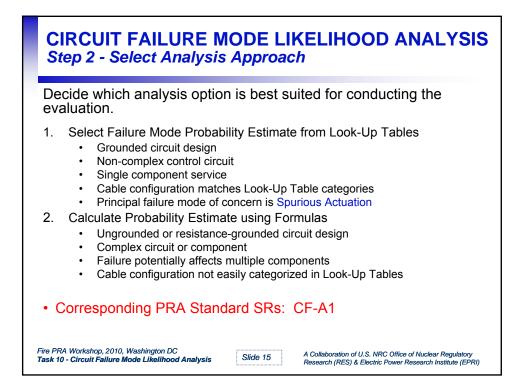


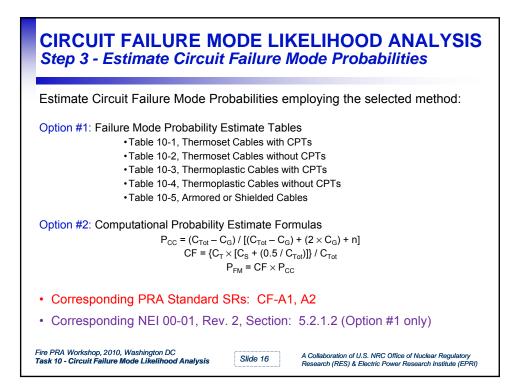


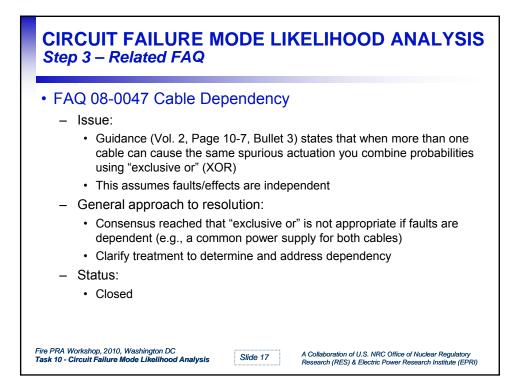


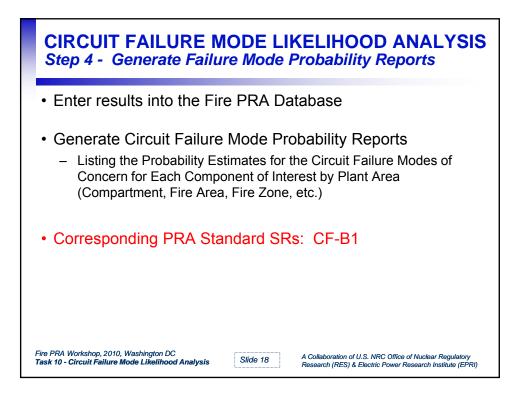


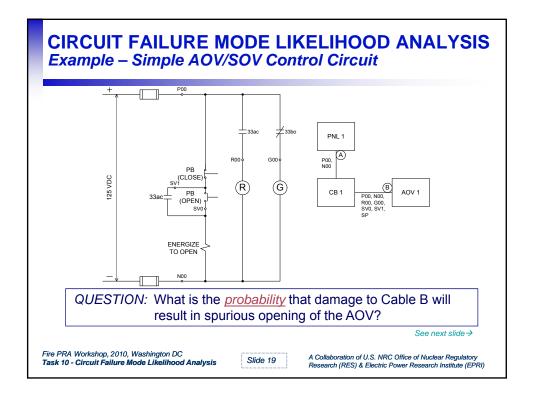




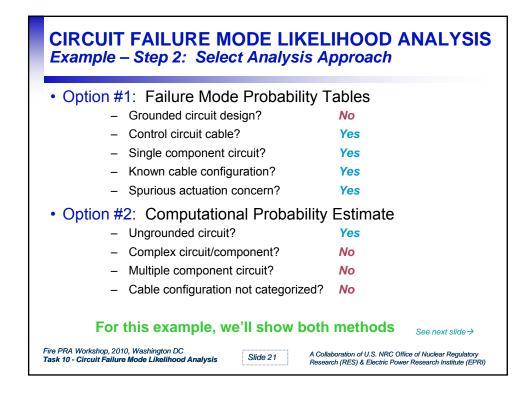




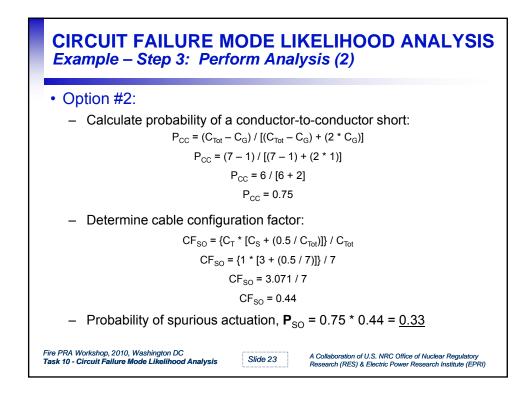


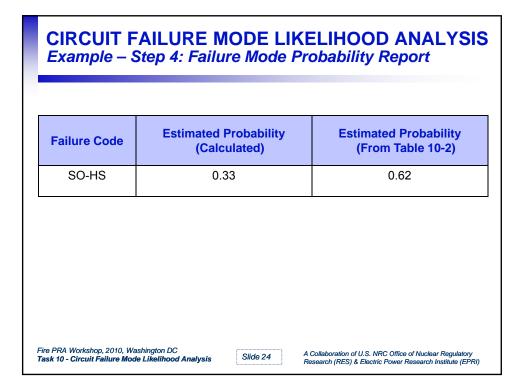


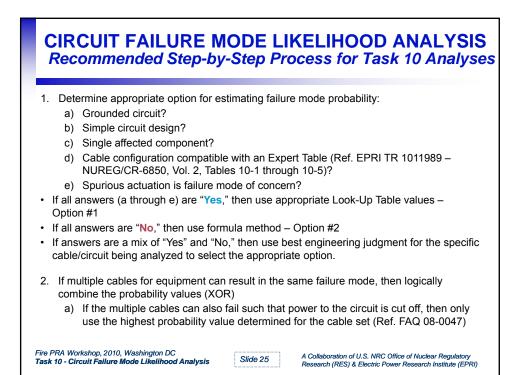
CIRCUIT FAI Example – Ste	_	-		D ANALYSIS
Detailed circuit	analys	is completed &	& documented	? Yes
	Cable	+125 VDC Hot Probe	-125 VDC Reference Ground Probe	
	Α	LOP-FB	LOP-FB	
	в	LOP-FB, EI-HS, SO-HS	LOP-FB, LOC	
Collect importat _ Cable insulat		e and configur <i>Thermos</i>		
 Number of co 	onducto	ors? Seven		
 Raceway typ 	e?	Tray		
 Power source 	e?	Ungroun	ded DC bus (r	no CPT)
 Number of so 	ource &	target conducto	ors? 3 sources	s, 1 target
		Ū.		See next slide ->
Fire PRA Workshop, 2010, Washing Task 10 - Circuit Failure Mode Like		ysis Slide 20		RC Office of Nuclear Regulatory c Power Research Institute (EPRI)

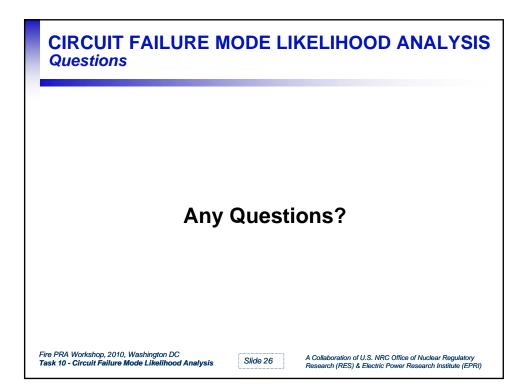


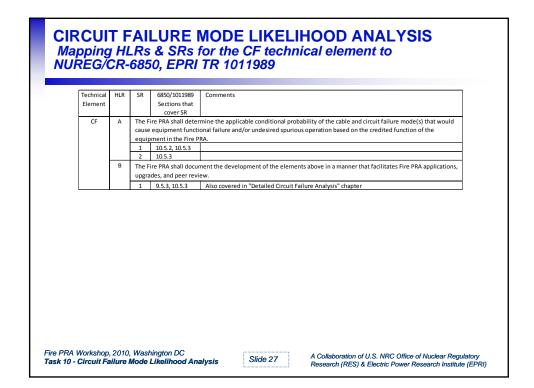
Example – StOption #1:	e to Use? Table 10-2, T	vsis (1)	
Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	$\begin{array}{l} M/C \mbox{ Intra-cable} \\ 1/C \mbox{ Inter-cable} \\ M/C \rightarrow 1/C \mbox{ Inter-cable} \\ M/C \rightarrow M/C \mbox{ Inter-cable} \end{array}$	0.60 0.40 0.20 0.02 - 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	$\begin{array}{l} M/C \mbox{ Intra-cable} \\ 1/C \mbox{ Inter-cable} \\ M/C \rightarrow 1/C \mbox{ Inter-cable} \\ M/C \rightarrow M/C \mbox{ Inter-cable} \end{array}$	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1
- SO Probab ire PRA Workshop, 2010, Washi ask 10 - Circuit Failure Mode L		A Collaboration of U.S. NF	60*0.06) See next slide → RC Office of Nuclear Regulatory c Power Research Institute (EPRI)







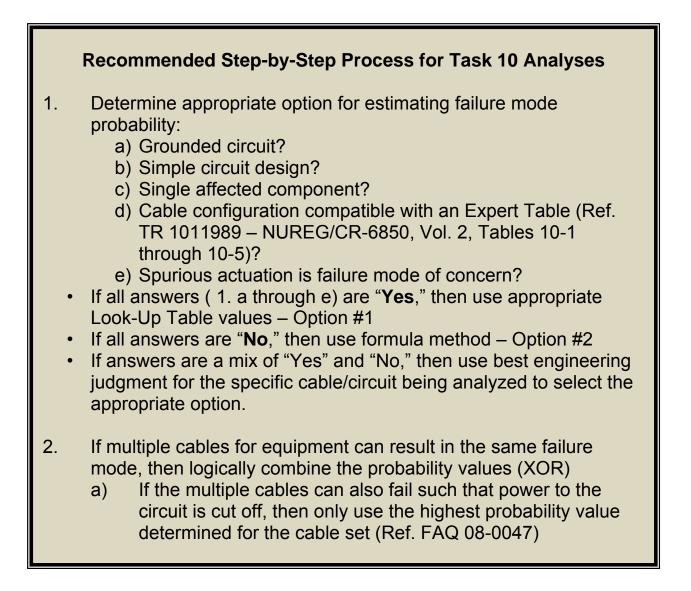




	NEI 00-01, Rev. 2, Section	NEI 00-01 – Probability of Spurious	6850/1011989 Sections that cover step	Comments
	Section	Actuation	coverstep	
	5 – Risk Signifi- cance Analysis	5.2.1.2	10.5.3	NEI 00-01, Rev. 2, only recommends use of tables to determine spurious actuation probability estimates. NUREG/CR-6850, EPRI TR 1011989 also offers formula method.
-				

Task 10: Circuit Failure Mode Likelihood Analysis Methodology Summary

This document summarizes the process for determining the probability, or likelihood, of a particular circuit failure mode occurrence. It includes the five Failure Mode Probability Estimate Tables employed under the Option #1 analysis approach, and the Option #2 Computational Probability Estimate formulas. **Important!** Please refer to the complete discussion of this methodology provided in NUREG/CR-6850, EPRI 1011989, "EPRI/NRC-RES Fire PRA Methodology for Nuclear Power Facilities; Volume 2: Detailed Methodology," Final Report, September 2005, when applying this methodology in non-classroom situations.



Selecting the Analysis Approach

1. Option #1: Failure Mode Probability Estimate Tables

Tables of probability estimates would appropriately be used for cables that meet the following criteria:

- The circuit is of a grounded design (including impedance grounded systems with ground fault trip capability),
- The cable is part of the control circuit for a typical component (e.g., non-complex MOVs, SOVs, pumps),
- The cable is associated with a single component,
- The cable configuration is known and can be readily associated with one of the defined configurations in Tables 1 through 5, and
- The principal hot short failure mode of concern is a spurious operation of the component.
- 2. Option #2: Computational Probability Estimates

Use of the probability estimate formulas are recommended for cases where:

- The circuit is ungrounded or is impedance grounded without ground fault trip capability,
- The cable is part of a relatively complex circuit or component,
- The cable is associated with or can influence the behavior of multiple components (e.g., safeguards actuation signal, bus shed scheme, etc.),
- The cable configuration is not easily categorized into one of the defined configurations contained in Tables 10-1 through 10-5.

Performing the Circuit Failure Mode Probability Analyses

Option #1: Failure Mode Probability Estimate Tables

- 1. Categorize the circuit of interest based on its configuration attributes.
- 2. From the appropriate table (Tables 10-1 to 10-5), select the probability estimates for the failure modes of concern.
- 3. If the cable failure mode can occur due to different cable interactions, the probability estimate is taken as the simple sum of both estimates. For example, if a particular thermoset cable failure mode can be induced either by an intra-cable shorting event (P = 0.30) or by an inter-cable shorting event (P = 0.03; mid-range of 0.01–0.05), the overall probability of that failure mode is estimated to be 0.33.

Table 10-1
Failure Mode Probability Estimates Given Cable Damage
Thermoset Cable with Control Power Transformer (CPT)

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Tray	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.30 0.20 0.10 0.01 – 0.05	0.10 – 0.50 0.05 – 0.30 0.05 – 0.20
Conduit	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.075 0.05 0.025 0.005 - 0.01	0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05

M/C: Multi-conductor cable

1/C: Single conductor cable

Intra-cable: An internally generated hot short. The source conductor is part of the cable of interest Inter-cable: An externally generated hot short. The source conductor is from a separate cable

Table 10-2Failure Mode Probability Estimates Given Cable DamageThermoset Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Тгау	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.60 0.40 0.20 0.02 – 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Тгау	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.30 0.20 0.10 0.01 – 0.05	0.10 - 0.50 0.05 - 0.30 0.05 - 0.20
Conduit	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.075 0.05 0.025 0.005 – 0.01	0.025 - 0.125 0.0125 - 0.075 0.0125 - 0.05

Table 10-3Failure Mode Probability Estimates Given Cable DamageThermoplastic Cable with CPT

Table 10-4Failure Mode Probability Estimates Given Cable DamageThermoplastic Cable without CPT

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
Тгау	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.60 0.40 0.20 0.02 – 0.1	0.20 - 1.0 0.1 - 0.60 0.1 - 0.40
Conduit	M/C Intra-cable 1/C Inter-cable M/C \rightarrow 1/C Inter-cable M/C \rightarrow M/C Inter-cable	0.15 0.1 0.05 0.01 – 0.02	0.05 - 0.25 0.025 - 0.15 0.025 - 0.1

Table 10-5Failure Mode Probability Estimates Given Cable DamageArmored or Shielded Cable

Raceway Type	Description of Hot Short	Best Estimate	High Confidence Range
With CPT	M/C Intra-cable	0.075	0.02 – 0.15
Without CPT	M/C Intra-cable	0.15	0.04 - 0.30

3. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the probability estimates associated with all affected cables should be considered when deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

 $P_{\text{Component failure Cable A}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$

Option #2: Computational Probability Estimates

Application of this calculational method is more complex and is only recommended for cases where Option #1 cannot reasonably be applied. The intent is to give the analyst a means of refining the estimated circuit failure mode probabilities based on the most important characteristics of the cable/circuit under study.

This computational method involves applying circuit failure mode probability estimation formulas. The following discussions provide only the minimum definition of the failure mode likelihood estimation formulas and their terms. For a complete discussion of the technical basis, detailed explanations, and examples of usage, please refer to Appendices J and K in Volume 2 of EPRI 1011989, NUREG/CR-6850.

The probability of occurrence for a specific hot short failure mode (P_{FM}) is estimated by the formula:

 $P_{FM} = CF \times P_{CC,}$

Where:

 P_{FM} = The probability that a specific hot short failure mode of interest will occur in a specific circuit given a fire of sufficient intensity to cause cable damage,

- P_{CC} = The probability that a conductor-to-conductor short will occur prior to a short-toground or short to a grounded conductor, and
- CF = A configuration factor applied to P_{CC} to account for the relative number of source conductors and target conductors. Target conductors are those conductors of a circuit that, if contacted by an electrical source of proper magnitude and voltage, will result in abnormal energization of the circuit, component or device of concern. Source conductors represent energized conductors that are a potential source of electrical energy.
- 1. Calculate P_{CC} as follows:

Cables in trays:	$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 1]$
Cables in conduit ¹ :	$P_{CC} = (C_{Tot} - C_G) / [(C_{Tot} - C_G) + (2 \times C_G) + 3]$
Ungrounded systems:	$\mathbf{P}_{\mathrm{CC}} = (\mathbf{C}_{\mathrm{Tot}} - C_G) / \left[(\mathbf{C}_{\mathrm{Tot}} - C_G) + (2 \times C_G) \right]$
Where:	

- $C_{Tot} =$ The total number of conductors in the cable of interest (including spares), and
- C_G = The number of grounded (or common) conductors in the cable of interest. The analyst should determine the number of grounded/common conductors based on the circuit configuration (contact positions, etc.) that represent the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

Note: For ungrounded AC and DC systems, C_G represents the number of return conductors to the power source associated with the circuit of interest (e.g., the negative polarity conductors for an ungrounded 125 VDC circuit)

2. Calculate CF as follows.

Non-armored cables: $CF = \{C_T \times [C_S + (0.5 / C_{Tot})]\} / C_{Tot}$

Armored cables: $CF = (C_T \times C_S) / C_{Tot}$

Where:

- C_S = The total number of source conductors in the cable under evaluation,
- C_T = The total number of target conductors in the cable², and
- C_{Tot} = The total number of conductors in the cable, as before.

¹ Armored and shielded cable should use the equation for conduit.

² Target conductors are only those cable conductors capable of forcing the component or circuit into the undesired state or condition of interest. For example, the target conductors associated with causing a spurious operation of the component will likely differ from target conductors associated with causing a loss of control condition.

Note: CF should be ≤ 1.0 . If the calculated value of CF is greater than 1, then set CF = 1. In practical applications it is highly unlikely that the calculated value of CF will ever exceed 1. For this to occur, virtually all conductors in the cable would need to be either a source conductor or target conductor.

Note: The analyst should determine the number of target and source conductors based on the circuit configuration (contact positions, etc.) that represents the normal operating state of the component. If this information is unavailable or indeterminate, the worst-case conditions should be assumed.

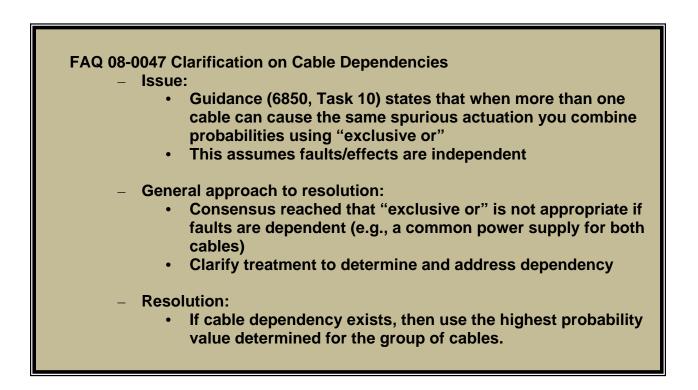
3. Calculate P_{FM} as follows:

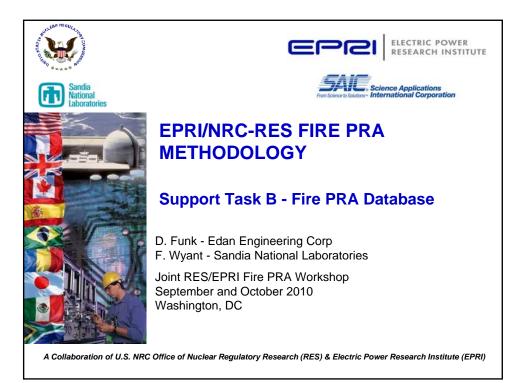
 $P_{FM} = CF \times P_{CC},$

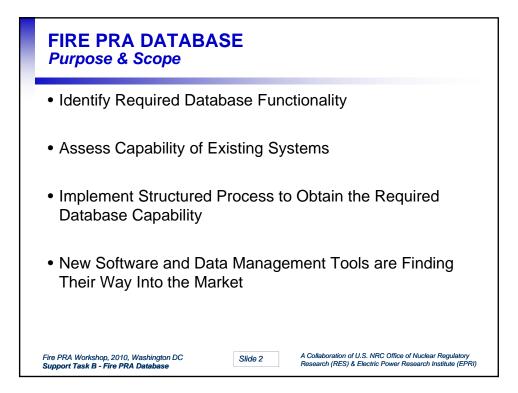
where CF and P_{CC} are determined using the formulas discussed above.

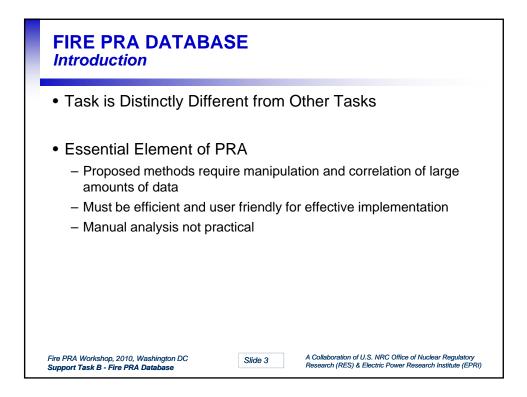
4. When more than one cable can cause the component failure mode of concern, and those cables are within the boundary of influence for the scenario under investigation, the probability estimates associated with all affected cables should be considered in deriving a failure estimate for the component. In general, the probabilities should be combined as follows:

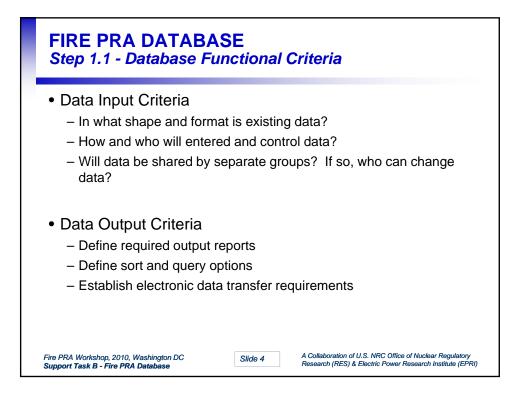
 $P_{\text{Component failure Cable A}} = (P_{\text{Failure Cable A}}) + (P_{\text{Failure Cable B}}) - (P_{\text{Failure Cable A}})(P_{\text{Failure Cable B}})$

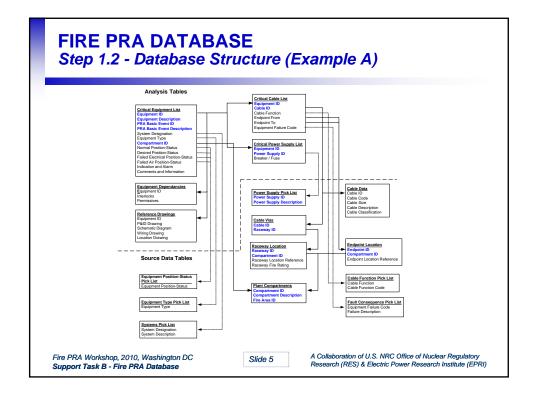


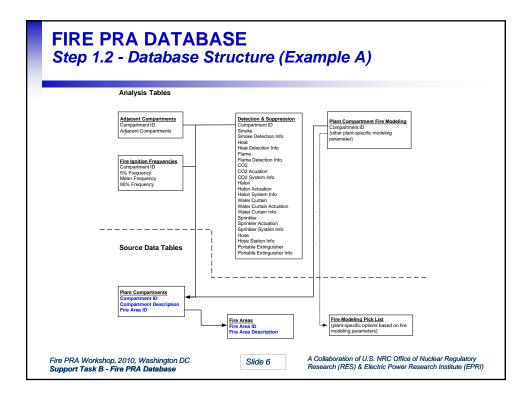


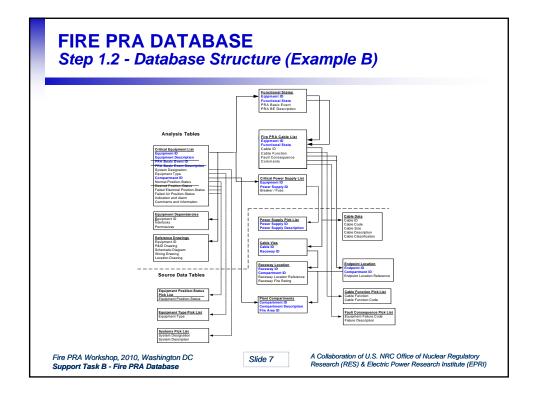


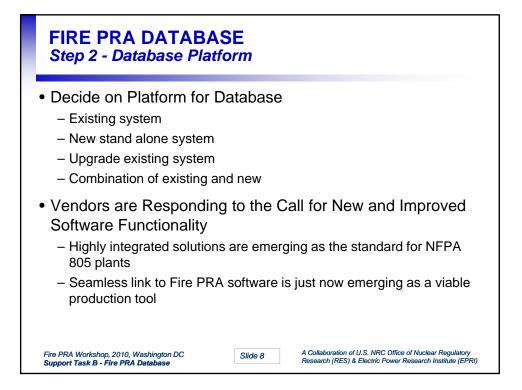


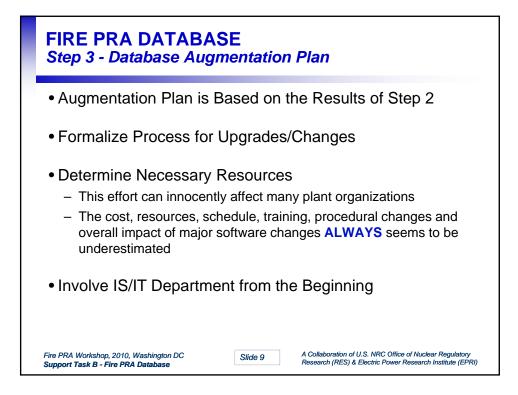


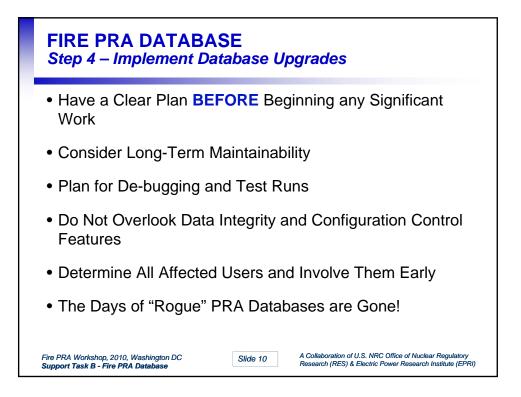


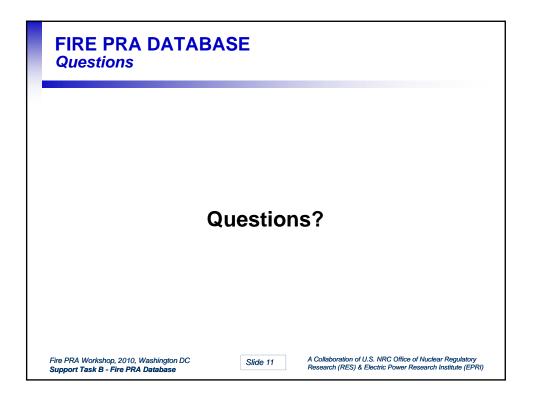




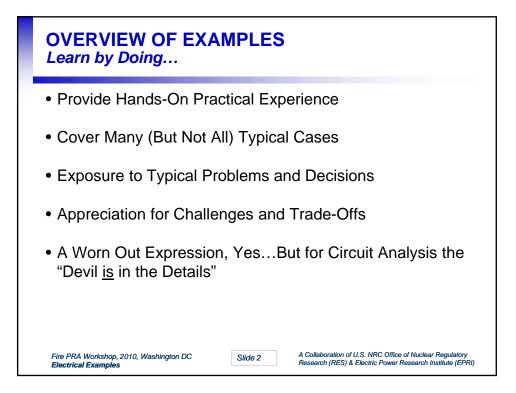












HANDS-ON EXERCISES Example Circuit Analysis Problem Set

Example No.	Component	Description of Example	Function State
1	AOV-8879B	Easy AOV circuit with desired change of state to failsafe position	Open - Closed
2	AOV-8879B	Easy AOV circuit with desired position to maintain energized state	Open - Open
3	MOV-8888	Easy MOV circuit with desired position to maintain initial state	Open - Open
4	MOV-8888	Easy MOV circuit with desired change of state	Open - Closed
5	MOV-11	DC MOV control circuit with desired change of state	Close - Open
6	MOV-15	Double pole DC motor control circuit with desired change of state -	6a: Close - Throttled
0	MOV-15	remote and local operation	6b: Close - Throttled Local
7	AOV-2869A	Hard AOV circuit with desired position to maintain initial state	Closed - Closed
8	AOV-2869A	Hard AOV circuit with desired change of state	Closed - Open
9	MOV-8706A	Hard MOV with desired position to maintain initial state	Closed - Closed
10	MOV-8706A	Hard MOV circuit with desired change of state	Closed - Open
11	ANN-1	Annunciator Circuit	Available – Nonspurious
12	HPI-B	4.16 kV Motor	Standby – On
13	COMP-1	480 V Motor	Cycle - Cycle
14	MCC-1B	480V MCC	Energized - Energized
15	LC-B	480V Load Center	Energized - Energized
16	52-DF01	4.16 kV OSP Breaker	Closed - Closed
17	FCV 605A	Instrument control signal to flow control valve	Closed - Modulate
18	TTR2	Instrument loop – temperature indicator	Available - Available
	Workshop, 2010, Washir		f U.S. NRC Office of Nuclear Regulate

