

Engineering and constructing a better tomorrow

November 16, 2009

From: Jon Honeycutt, Staff Professional

For for A

Reviewed By: Steve Kiser, Principal Professional

Subject:

Report of SPT Energy – MACTEC CME 55 Track (RAL) Hammer Serial No. MEC-21 Automatic Hammer WORK INSTRUCTION No. 8 (DCN:NAP-077) North Anna 3 Project Louisa County, Virginia MACTEC Project No. 6468-09-2473

Jonathan Honeycutt, of MACTEC Engineering and Consulting, Inc. (MACTEC), performed energy measurements on the drill rig at the subject site per the referenced Work Instructions. This memorandum summarizes the field testing activities and presents the results of the energy measurements.

SPT Energy Field Measurements

SPT energy measurements were made on September 1, 2009, during drilling of Boring M-30(DH) at the referenced site. The testing was performed by Jonathan Honeycutt from approximately 4:05 PM to 4:45 PM on September 1 under clear skies with a temperature of about 75 degrees Fahrenheit. The boring was drilled by MACTEC personnel using equipment from the MACTEC Raleigh office. The drilling equipment consisted of a CME 55 model track drill rig with an SPT automatic hammer. The drilling tools consisted of AW-J-sized drilling rods and a 2foot long split-barrel sampler. Mud rotary drilling techniques were used to advance the boring at the time of energy testing. The drill rig operator during sampling was Mr. Thomas Hahn. Energy measurements were recorded during sampling at the depth intervals shown in Table 1.

The energy measurements were performed with a Pile Driving Analyzer (PDA) model PAX (Serial No. 3622L), and calibrated accelerometers (Serial Nos. K983 and K0686) and strain gages (Serial Nos. AW#75/1 and AW#75/2). A steel drill rod, 2 feet long and instrumented with dedicated strain gages, was inserted at the top of the drill rod string immediately below the SPT hammer. The inserted rod was also instrumented with two piezoresistive accelerometers that were bolted to the outside of the rod. The instrumented rod insert had a cross-sectional area of approximately 1.22 square inches and an outside diameter of approximately 1.75 inches at the gage location. The drill rods included in the drill rod string were hollow rods in 5 to 10 foot long sections, with an outside and inside diameter of approximately 1.75 and 1.375 inches, respectively. The recommended operation rate of the hammer is not known. Due to the closed hammer system, the hammer lubrication condition and anvil dimensions could not be observed.

18 Pages Total

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Page 38 of 55 DCN#NAP299

DCN NAP306

Calibration Records

The calibration records for all the above are filed in DCN NAP-223.

Calculations for EFV

The work was done in accordance with ASTM D 4633-05. The strain and acceleration signals were converted to force and velocity by the PDA. The maximum energy transmitted to the drill rod string (EFV), as measured at the location of the strain gages and accelerometers, was calculated by the PDA using the equation shown below:

 $EFV = \int F(t) * V(t) * dt$

Where: EFV = Transferred energy (EFV equation), or Energy of FV F(t) = Calculated force at time t V(t) = Calculated velocity at time t

As recommended by ASTM D4633-05, the force-velocity method of energy calculation was used. The equation shown above for calculating EFV, integrated over the complete wave event, measures the total energy content of the event using both force and velocity measurements. The EFV values associated with each blow analyzed are tabulated in the attached PDIPLOT tables and are also shown graphically in the PDIPLOT charts.

Calculations for ETR

The ratio of the measured transferred energy (EFV) to the theoretical potential energy of the SPT system (140 lb weight with the specified 30 inch fall) is the ETR. The ETR values (as percent of the theoretical value) are shown in Table 1.

Comparison of ETR to Typical Energy Transfer Ratio Range

Based on a research report published by the Florida Department of Transportation (FDOT) (Report WPI No. 0510859, 1999), the average ETR measured for automatic hammers is 79.6%. The standard deviation was 7.9%; therefore, the range of ETRs within one standard deviation of the average was reported to be 71.7% to 87.5%. This range of ETRs was also consistent with other research that was cited in the FDOT research paper; however, maximum and minimum ETR values of up to 98% and 56%, respectively, were reported in the literature. The ETR values shown in Table 1 are generally within the range of typical values for automatic hammers as reported in the literature.

Discussion

Based on the field testing results, observations from the SPT energy measurements are summarized below:

• The data obtained by the PDA are generally consistent between individual hammer blows and between the sample depths tested. In general, the first and last one (and sometimes two or more) hammer blow records recorded by the PDA produced poor quality data (which is relatively common) and, as such, the record(s) was(were) not used in the data reduction. This may result in more or less hammer blows evaluated for ETR than what is shown on the boring logs.

- The average energy transferred from the hammer to the drill rods for each individual depth interval using the EFV method ranged from 302 foot-pounds to 317 foot-pounds. These average energy transfers correspond to energy transfer ratios (ETR) of 86.3% to 90.6% of the theoretical energy (350 foot-pounds) of the SPT hammer.
- The average at each depth interval was calculated as the transferred energy for each analyzed blow of the depth intervals divided by the total number of hammer blows analyzed. The overall average energy transfer of the SPT system (for all the depth intervals tested) was 306.1 foot-pounds, with an average ETR of 87.4%.

Attachments:Page 4 Table 1 - Summary of SPT Energy Measurements - 1 PagePage 5 - 6 Work Instruction No. 8 DCN:NAP 077- 2 Pages (without attachments)Pages 7 Record of SPT Energy Measurement - 1 PagePages 8 - 17 PDIPLOT Output - 10 PagesPage 18 Force-Velocity Plot - 1 Page

| TABLE 1 | | | | | | | | |
|--|--|--|--|--|--|--|--|--|
| SUMMARY OF SPT ENERGY MEASUREMENTS (ASTM D4633-05) | | | | | | | | |
| North Anna 3 Project | | | | | | | | |
| Louisa County, Virginia | | | | | | | | |
| MACTEC Project No. 6468-09-2473 | | | | | | | | |

| Automatic Hammer Serial Number and Rig Model | Rig Owner | Rig Operator | Boring No. Tested | Date Tested | Drill Rod Size | Sample Depth (feet) | SPT Blow Count (blows per six inches) | No. of Blows Analyzed | Average Measured Energy (Average EFV) (ft-lbs) ^a | Ènergy Transfer Ratio (%) ^b (Average ETR) |
|--|-----------|--------------|-------------------|-------------|----------------|---------------------|--|-----------------------|---|---|
| | | | | | | 11.1 - 12.6 | 4 - 6 - 6 | 16 | 304 | 86.9% |
| MEC-21 | MACTEC | Thomas Hahn | M 20 | | AW-J | 13.7 - 15.2 | 4 - 7 - 7 | 19 | 302 | 86.3% |
| (CME 55 | Raleigh | | (DH) | 9/1/2009 | | 18.7 - 20.2 | 6 - 7 - 6 | 19 | 317 | 90.6% |
| Track) | Traioigii | | | | | 23.7 - 25.2 | 7 - 8 - 10 | 25 | 307 | 87.7% |
| | | | | | | 28.7 - 30.2 | 11 - 14 - 15 | 40 | 303 | 86.6% |
| | | | | Ave | rage for Rig: | 306.1 | 87.4% | | | |

^aMeasured Energy is energy based on the EFV method, as outlined in ASTM D4633-05, for each blow recorded by the PDA. In some cases, the initial and final one to two blows produced poor quality data, and were not used to calculate the Average Measured Energy. This may result in more or less blows evaluated for ETR than what is shown on the boring logs.

EFV = EMX * 1000 lbs/kip, where EMX equals the maximum transferred energy measured by the PDA (see attached PDA data).

^bEnergy Transfer Ratio is the Measured Energy divided by the theoretical SPT energy of 350 foot-pounds (140 pound hammer falling 2.5 feet). The average EFV and ETR values may differ slightly and insignificantly from those in the PDIPLOT tables due to roundoff.

Page 41 of 55 DCN#NAP299 Date: 11-16-09 Checked By: Prepared By: Date: 11-16-09 For With Permission

DCN NAP306

Work Instruction No. 8 North Anna 3 Project MACTEC Engineering and Consulting, Inc. Project Number: 6468-09-2473

| Issued To: | Jonathan Honeycutt, Stev | re Kiser | Rev. No0 | |
|-------------|--------------------------|-------------|------------------------------|--|
| Issued By: | D. Steven Copley, P.E. | 050 8-31-09 | Date: <u>August 31, 2009</u> | |
| Valid From: | August 31, 2009 | | To: <u>August 31, 2010</u> | |
| | | | | |

Task Description: Perform SPT Energy Measurements

Applicable Technical Procedures or Plans, or other reference:

- Geotechnical Work Plan (complete copy of current revision available at Field Office), Section 4.2 and Attachment 2

 Drilling and Sampling Procedures (attached)
- Engineering Specification for Subsurface Investigation and Laboratory Testing, No. 25161-500-3PS-CY00-Q0001, Rev. 000, Issued for use August 21, 2009, Section 3.3 Drilling Equipment (attached)
- 3. ASTM D 4633-05 (attached)

<u>Specific Instructions</u> (note attachments where necessary): Perform energy measurements for each drill rig on site in general accordance with ASTM D 4633-05. Consult with Site Manager as to schedule for performing the measurements. Hammer weights have been checked, and records will be available on site. All rigs are using automatic hammer systems. Confirm that automatic hammer system is being operated within manufacturer's recommendations or in a typical operating fashion as observed from watching one or two SPT measurements prior to measuring energy. Check each drill rig using all hammer/rod combinations that it will be using. Depths for measurements should be coordinated with the Site Manager. See Site Manager for current boring logs of holes drilled, if available, and use these to plan most effective field measurement program. Submit copies of calibration records for equipment to Principal Professional for review prior to beginning work on site.

Confirm with Site Manager that approval of equipment calibration records have been received prior to beginning field testing. If unexpected conditions are encountered that affect measurements, contact Site Manager or Principal Professional immediately.

Report Format: Prepare standard report in accordance with ASTM D 4633-05 requirements.

Specific Quality Assurance Procedures Applicable: 10CFR21; NQAP 16-01 Procedure For Conforming To Federal Regulation 10CFR21; QAP 20-1; QAP 25-1; Section 306 of the Energy Reorganization Act of 1974. Current revisions apply; copies available in Field Office.

Hold Points or Witness Points: None

<u>Records</u>: All records generated shall be considered QA Records.

Page 1 of 15 DCN NAP077 Page 42 of 55 DCN#NAP299

Volume 1, Revision 0

Page 138 of 148

DCN NAP306

| Reviewed and Approved By (Note: Only one signature required for issuance): | | | | | | | | | |
|--|---------|--------|---------|--|--|--|--|--|--|
| Project Manager: | Date: | | | | | | | | |
| Principal Professional: D. Agreen Copley | | Date: | 8-31-09 | | | | | | |
| Site Manager: | _ Date: | | | | | | | | |
| No. of Pages:15 | | DCN: _ | NAP077 | | | | | | |

QA Form 24-1 Revised 8/12/2009

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Page 2 of 15 DCN AP077 Page 43 of 55 DCN#NAP299 DCN NAP306

Volume 1, Revision 0

2801 YORKMONT ROAD, SUITE 100 D CHARLOTTE, NC 28208 Telephone: (704) 357-8600 / Facsimile: (704) 357-8638

RECORD OF SPT ENERGY MEASUREMENT

| • | GENERAL INFORMA | TION | DRILL RIG DATA | | | | | | |
|----------------------|----------------------|---|----------------|---------------------|--|------|----------|--------------|-----|
| PROJECT: | North Anna 3 Project | | | MAKE: CME | | | | | |
| LOCATION: | Virginia | | | MODEL: | | .55 | BARL | | |
| PROJECT NO .: | 6468-09-2473 | : | | SERIAL NO | .: | me | E/~21 | | |
| DATE: | 911/200 | 59 | , | HAMMER TYPE: 104. | | | 4. | | |
| WEATHER: | Sumine | TOF | | ROPE CONDITION: N/A | | | <u> </u> | | |
| INSPECTOR: | TIL | | • . | ROD SIZE: | | AW-J | | | |
| DRILLING COMPANY: | MACTEC - Pale | ĥ | | NO. OF SHI | EAVES: | N/A | • | | |
| | () PEIE | 20 | | | | | | | |
| | | | BORING | DATA | | | | | |
| BORING NUMBER: | M-30(D) | <u>+)</u> | | | | | | | |
| DEPTH DRILLED: | Vari | | | | | | | | |
| TIME DRIVEN: | 4:05 pm - | | | | | | | | |
| RIG OPERATOR: | THAHN | | | | | | • | • | |
| HAMMER OPERATOR: | N/ | Α | | | | | | | |
| PDA PAK SERIAL NO.: | 362 | 2L | | | | | | | |
| INSTR. ROD AREA: | 1.22:N2 | · · · | | | | | | | |
| ACCEL. SERIAL NOS .: | · 41-k983: | A2-K0686. | | | | | | | |
| STRAIN SERIAL NOS .: | 75AW # | 1/2 | | | | | | | |
| | SAMPLE | SPT | | | | | | | |
| ŧ | DEPTH | N-VALUE | | | | | | 1 4 | |
| : | (feet) | (bpf) | | | | | | | |
| | 11 1 12 1- | 4-6-6 | | | | | | | |
| · · | 16,1-12,0 | 1.0-0 | | | 1 | | | | |
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| | 13.7-15.2 | 4-7-7 | | ·. | | | | | |
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| | 10 7-20 2 | 1-2-6 | | | 1 | | | | |
| | 1317-20 id | 0 7 0 | | | | | | | |
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| | 13.7-25.2 | 7-8-10 | | | | | | | |
| | | | | | | | | | |
| | 707.207 | 11-14-15 | | | | | | | |
| | 20.1-30.04 | | | | | | | | |
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| | | مورد موسوم المراجع الم | | | | | | | |
| REMARKS: | Testing performed in | accordance with | | | | | | | |
| | ASTM D 4633-05 | | | | | | | | |
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| | Reviewed By: | an a shine that a state of the | | | A None of Concession, Name of Street, or Str | | 1 | -age 44 of 5 | O 🥼 |
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DCN NAP306

19



MACTEC Engineering and Consulting, Inc. - Case Method Results

Page 45 of 55 DCN#NAP299

Test date: 1-Sep-2009

PDIPLOT Ver. 2008.1 - Printed: 16-Nov-2009

| MACTEC Engin Case Method F | neering and C Results | PDIPLO | T Ver. 2008.1 | Pa - Printed: 16- | age 1 of 1 Nov-2009 | | | | |
|---|--|----------------------------|-------------------------------|----------------------|------------------------|--------------|--------------------------------------|--|----------------------------------|
| NORTH ANNA OP: JNH | 3 Project - BC | Serial No. MEC | C-21; CME 55 Test date: 1- | (T.Hahn) Sep-2009 | | | | | |
| AR: 1.22 in LE: 16.60 f WS: 16,807.9 f | n^2 t /s | | | ` | | | | SP: 0 EM: 30 JC: | 0.492 k/ft3 0,000 ksi 0.70 |
| CSX: Max Mea TSX: Tension VMX: Maximuu FMX: Maximuu FVP: Force/Ve | asured Compr Stress Maxim m Velocity m Force elocity proport | . Stress um ionality | | | | | BPM: B EF2: E ETR: E EMX: N | lows per Minu nergy of F^2 nergy Transfe lax Transferre | ute er Ratio ed Energy |
| BL# | CSX | TSX | VMX | FMX | FVP | BPM | EF2 | ETR | EMX |
| | ksi | ksi | f/s | kips | [] | ** | k-ft | (%) | k-ft |
| 2 | 21.6 | 14.9 | 16.3 | 26 | 0.8 | 1.9 | 0.251 | 81.8 | 0.286 |
| 3 | 20.5 | 12.4 | 15.9 | 25 | 0.8 | 60.2 | 0.246 | 84.7 | 0.297 |
| 4 | 21.2 | 11.9 | 15.4 | 26 | 0.9 | 58.4 | 0.243 | 90.0 | 0.315 |
| 5 | 21.1 | 9.5 | 14.6 | 26 | 0.9 | 58.7 | 0.244 | 90.8 | 0.318 |
| 6 | 19.3 | 9.9 | 15.2 | 24 | 0.8 | 58.6 | 0.242 | 91.3 | 0.320 |
| 7 | 20.6 | 7.9 | 13.6 | 25 | 0.9 | 58.6 | 0.236 | 85.1 | 0.298 |
| 8 | 20.9 | 8.2 | 13.9 | 25 | 0.9 | 58.8 | 0.235 | 89.6 | 0.314 |
| 9 | 20.8 | 8.5 | 13.5 | 25 | 0.9 | 58.5 | 0.234 | 88.5 | 0.310 |
| 10 | 20.4 | 8.3 | 13.8 | 25 | 0.8 | 58.9 | 0.233 | 84.4 | 0.295 |
| 11 | 21.0 | 8.6 | 13.9 | 26 | 0.8 | 58.7 | 0.234 | 85.7 | 0.300 |
| 12 | 19.3 | 8.2 | 13.7 | 24 | 0.8 | 58.9 | 0.235 | 87.3 | 0.306 |
| 13 | 18.0 | 9.0 | 13.8 | 22 | 0.8 | 58.6 | 0.235 | 87.3 | 0.306 |
| 14 | 20.2 | 8.6 | 13.9 | 25 | 0.8 | 58.9 | 0.228 | 85.3 | 0.298 |
| 15 | 18.7 | 8.8 | 14.0 | 23 | 0.8 | 58.4 | 0.235 | 88.9 | 0.311 |
| 16 | 19.7 | 8.5 | 14.0 | 24 | 0.8 | 58.8 | 0.231 | 86.2 | 0.302 |
| 17 | 20.7 | 7.8 | 14.2 | 25 | 0.8 | 58.9 | 0.230 | 83.2 | 0.291 |
| Average | 20.3 | 9.5 | 14.4 | 25 | 0.8 | 55.2 | 0.237 | 86.9 | 0.304 |
| | | | | Total nur | nber of blows | analyzed: 16 |) | | |

Time Summary

Drive 1 minute 44 seconds

3:54:35 PM - 3:56:19 PM (9/1/2009) BN 1 - 18



MACTEC Engineering and Consulting, Inc. - Case Method Results

Page 47 of 55 DCN#NAP299

Volume 1, Revision 0

Page 143 of 148

MACTEC Engineering and Consulting, Inc. - Case Method Results

PDIPLOT Ver. 2008.1 - Printed: 16-Nov-2009

NORTH ANNA 3 Project - BORING M-30(DH) (18.7' - 20.2' sample)



Page 49 of 55 DCN#NAP299

Test date: 1-Sep-2009



| | Results | | PDIPLOT Ver. 2008.1 - Printea: 16-Nov-2009 | | | | | | |
|--|--|------------------------------|---|------|-----|------|-------|------------------------|---------------------------------|
| NORTH ANN OP: JNH | A 3 Project - BC | DRING M-30(I | Rig Serial No. MEC-21; CME 55 (T.Hahn) Test date: 1-Sep-2009 | | | | | | |
| AR: 1.22 in^2 LE: 29.20 ft WS: 16.807.9 f/s | | | | | | | | SP: 0 EM: 30 JC: | 0.492 k/ft 0,000 ksi 0.70 |
| CSX: Max M TSX: Tensio VMX: Maxim FMX: Maxim FVP: Force/ | easured Compr n Stress Maxim um Velocity um Force /elocity proport | BPM: EF2: ETR: EMX: | Blows per Minute Energy of F ² Energy Transfer Ratio Max Transferred Energy | | | | | | |
| BL# | CSX | TSX | VMX | FMX | FVP | BPM | EF2 | ETR | EMX |
| | ksi | ksi | f/s | kips | П | ** | k-ft | (%) | k-f |
| 2 | 21.6 | 13.5 | 13.2 | 26 | 0.9 | 1.9 | 0.249 | 85.9 | 0.30 |
| 3 | 21.0 | 10.9 | 13.7 | 26 | 0.9 | 58.3 | 0.251 | 89.1 | 0.31 |
| 4 | 19.2 | 10.9 | 13.3 | 23 | 0.8 | 58.4 | 0.256 | 90.3 | 0.31 |
| 5 | 21.0 | 11.5 | 13.0 | 26 | 0.9 | 58.7 | 0.255 | 89.6 | 0.31 |
| 6 | 20.3 | 11.9 | 13.7 | 25 | 0.8 | 58.3 | 0.254 | 87.2 | 0.30 |
| 7 | 21.0 | 11.2 | 14.1 | 26 | 0.8 | 58.8 | 0.251 | 87.7 | 0.30 |
| 8 | 21.1 | 11.1 | 14.0 | 26 | 0.8 | 58.7 | 0.255 | 87.7 | 0.30 |
| 9 | 20.6 | 9.9 | 12.5 | 25 | 0.9 | 58.6 | 0.254 | 91.2 | 0.31 |
| 10 | 21.0 | 9.6 | 13.1 | 26 | 0.9 | 58.6 | 0.253 | 86.8 | 0.30 |
| 11 | 20.7 | 9.9 | 12.1 | 25 | 1.0 | 58.5 | 0.252 | 85.9 | 0.30 |
| 12 | 20.2 | 10.0 | 13.2 | 25 | 0.9 | 58.7 | 0.249 | 84.7 | 0.29 |
| 13 | 19.4 | 11.1 | 12.9 | 24 | 0.8 | 58.6 | 0.255 | 82.0 | 0.28 |
| 14 | 19.3 | 11.2 | 12.5 | 24 | 0.8 | 58.4 | 0.252 | 86.0 | 0.30 |
| 15 | 20.1 | 10.2 | 13.4 | 25 | 0.8 | 58.5 | 0.257 | 86.2 | 0.30 |
| 16 | 22.0 | 9.8 | 12.7 | 27 | 1.0 | 58.4 | 0.257 | 87.8 | 0.30 |
| 17 | 20.3 | 9.3 | 13.3 | 25 | 0.9 | 58.7 | 0.252 | 85.7 | 0.30 |
| 18 | 21.5 | 9.7 | 13.9 | 26 | 0.9 | 58.3 | 0.258 | 89.7 | 0.31 |
| 19 | 19.9 | 8.2 | 12.6 | 24 | 0.8 | 58.6 | 0.261 | 87.0 | 0.30 |
| 20 | 21.1 | 9.1 | 13.1 | 26 | 0.9 | 58.4 | 0.251 | 92.3 | 0.32 |
| 21 | 21.0 | 9.4 | 12.0 | 26 | 0.8 | 58.9 | 0.255 | 88.6 | 0.31 |
| 22 | 19.1 | 8.3 | 12.9 | 23 | 0.8 | 58.3 | 0.257 | 92.0 | 0.32 |
| 23 | 21.6 | 9.6 | 13.5 | 26 | 0.9 | 58.7 | 0.254 | 88.2 | 0.30 |
| 24 | 20.4 | 8.8 | 13.5 | 25 | 0.8 | 58.3 | 0.260 | 87.7 | 0.30 |
| 25 | 19.9 | 8.3 | 13.7 | 24 | 0.8 | 58.7 | 0.257 | 87.8 | 0.30 |
| 26 | 19.5 | 8.0 | 13.4 | 24 | 0.8 | 58.3 | 0.259 | 85.5 | 0.29 |
| | | | | | | | | | |

Time Summary

Page 51 of 55 DCN#NAP299

Drive 50 seconds

4:23:26 PM - 4:24:16 PM (9/1/2009) BN 1 - 27

Page 52 of 55 DCN#NAP299



PDIPLOT Ver. 2008.1 - Printed: 16-Nov-2009

MACTEC Engineering and Consulting, Inc. - Case Method Results

Test date: 1-Sep-2009

Page 53 of 55 DCN#NAP299

| MACT Case | EC Engineer Method Resu | ing and Cor Ilts | isulting, Inc. | | | Page 1 of PDIPLOT Ver. 2008.1 - Printed: 16-Nov-2009 | | | | |
|--------------------------------------|---|--|-----------------------|-----------------|-----------------|---|----------------------|------------------------------|---|--------------------------------------|
| NORT OP: JI | TH ANNA 3 P NH | roject - BOR | RING M-30(E | OH) (28.7' - 30 | .2' sample) | | Rig S | Serial No. ME | EC-21; CME 55 Test date: 1- | 5 (T.Hahn) ∙Sep-2009 |
| AR: LE: | 1.22 in^2 34.20 ft | | | | | | | | SP: (EM: 30 | 0.492 k/ft3 0,000 ksi |
| CSX: TSX: VMX: FMX: FVP: | 6,807.9 f/s Max Measur Tension Stre Maximum V Maximum Force/Veloc | red Compr. S ess Maximur elocity orce ity proportion | Stress n nality | | | | | BPM: EF2: ETR: EMX: | JC: Blows per Min Energy of F^2 Energy Transf Max Transferr | 0.70 ute er Ratio ed Energy |
| | BL# | CSX | TSX | VMX | FMX | FVP | BPM | EF2 | ETR | EMX |
| | - | ksi | ksi | f/s | kips | [] | ** | k-ft | (%) | k-ft |
| | 2 | 19.0 | 11.2 | 12.5 | 23 | 0.8 | 1.9 | 0.273 | 84.2 | 0.295 |
| | 3 | 19.5 、 | 9.6 | 12.7 | 24 | 0.8 | 58.1 | 0.285 | 85.9 | 0.301 |
| | 4 | 19.2 | 11.4 | 12.8 | 23 | 0.8 | 59.0 | 0.285 | 84.4 | 0.295 |
| | 5 | 21.1 | 12.4 | 14.2 | 26 | 0.8 | 59.0 | 0.273 | 85.9 | 0.301 |
| | 6 | 20.6 | 10.7 | 12.6 | 25 | 0.8 | 58.8 | 0.279 | 86.4 | 0.302 |
| | 7 | 20.3 | 11.4 | 13.0 | 25 | 0.9 | 58.7 | 0.275 | 84.5 | 0.296 |
| | 8 | 18.8 | 11.8 | 13.6 | 23 | 0.8 | 58.7 | 0.277 | 86.9 | 0.304 |
| | 9 | 20.7 | 10.5 | 14.1 | 25 | 0.8 | 58.9 | 0.272 | 85.6 | 0.300 |
| | 10 | 19.6 | 11.5 | 13.0 | 24 | 0.8 | 58.8 | 0.276 | 85.1 | 0.298 |
| | 11 | 21.2 | 8.9 | 12.6 | 26 | 0.9 | 58.6 | 0.271 | 82.0 | 0.287 |
| | 12 | 20.3 | 10.8 | 13.0 | 25 | 0.8 | 58.9 | 0.273 | 85.1 | 0.298 |
| | 13 | 21.0 | 8.8 | 12.3 | 26 | 1.0 | 58.4 | 0.274 | 82.9 | 0.290 |
| | 14 | 20.4 | 9.1 | 13.7 | 25 | 0.8 | 58.9 | 0.267 | 85.1 | 0.298 |
| | 15 | 21.1 | 10.3 | 12.6 | 26 | 0.9 | 58.5 | 0.269 | 84.1 | 0.294 |
| | 16 | 21.5 | 9.8 | 12.7 | 26 | 0.9 | 58.8 | 0.273 | 84.6 | 0.296 |
| | 17 | 18.5 | 7.9 | 12.7 | 23 | 0.8 | 58.4 | 0.277 | 82.9 | 0.290 |
| | 18 | 21.3 | 9.7 | 13.0 | 26 | 0.9 | 58.7 | 0.270 | 86.4 | 0.302 |
| | 19 | 21.5 | 8.9 | 12.0 | 26 | 0.8 | 58.6 | 0.272 | 85.7 | 0.300 |
| | 20 | 20.7 | 8.9 | 12.0 | 25 | 1.0 | 58.9 | 0.266 | 83.8 | 0 293 |
| | 21 | 18.6 | 6.9 | 13.7 | 23 | 0.8 | 58.5 | 0.270 | 86.5 | 0.200 |
| | 22 | 19.7 | 7.0 | 12.5 | 20 | 0.0 | 58.7 | 0.270 | 85.8 | 0.000 |
| | 23 | 20.8 | 7.3 | 11.0 | 25 | 0.0 | 58.7 | 0.270 | 81.6 | 0.000 |
| | 20 | 20.0 | 7.0 | 12.6 | 25 | 0.0 | 58.5 | 0.272 | 84.6 | 0.200 |
| | 25 | 21.0 | 6.8 | 11.0 | 20 | 0.7 | 58.6 | 0.200 | 04.0 | 0.230 |
| | 25 | 21.0 | 0.0 | 12.9 | 20 | 0.7 | 50.0 | 0.270 | 03.0 | 0.293 |
| | 20 | 20.6 | 6.7 | 12.0 | 22 | 0.0 | 59.0 | 0.209 | 04.0 | 0.290 |
| | 20 | 20.0 | 7.4 | 12.2 | 20 | 0.9 | 50.0 | 0.202 | 03.5 | 0.292 |
| | 20 | 10.0 | 7.4 | 12.7 | 23 | 0.0 | 50.7 | 0.273 | 00.0 | 0.303 |
| | 29 | 20.9 | 0.2 | 11.7 | 25 | 1.0 | 58.0 | 0.266 | 84.0 | 0.296 |
| | 30 | 19.7 | 0.0 | 12.0 | 24 | 0.9 | 58.0 | 0.266 | 85.6 | 0.300 |
| | 31 | 20.3 | 0.4 | 11.9 | 25 | 1.0 | 58.7 | 0.263 | 85.1 | 0.298 |
| | 32 | 19.2 | 7.0 | 13.7 | 23 | 0.8 | 58.4 | 0.269 | 89.9 | 0.315 |
| | 33 | 19.2 | 6.2 | 12.9 | 23 | 0.8 | 58.7 | 0.270 | 89.2 | 0.312 |
| | 34 | 19.7 | 6.3 | 11.3 | 24 | 1.0 | 58.6 | 0.263 | 86.7 | 0.304 |
| | 35 | 19.3 | 5.8 | 12.8 | 24 | 0.8 | 58.7 | 0.266 | 89.3 | 0.312 |
| | 36 | 20.7 | 6.0 | 12.2 | 25 | 0.7 | 58.5 | 0.262 | 93.0 | 0.325 |
| | 37 | 21.0 | 6.5 | 12.2 | 26 | 0.7 | 58.5 | 0.264 | 95.7 | 0.335 |
| | 38 | 19.0 | 5.4 | 12.8 | 23 | 0.8 | 58.5 | 0.266 | 92.5 | 0.324 |
| | 39 | 21.0 | 6.0 | 13.2 | 26 | 0.7 | 58.7 | 0.264 | 95.8 | 0.335 |
| | 40 | 21.3 | 7.0 | 13.0 | 26 | 0.7 | 58.4 | 0.270 | 99.7 | 0.349 |
| | 41 | 21.0 | 6.1 | 11.8 | 26 | 0.8 | 58.5 | 0.269 | 88.8 | 0.311 |
| Avera | ige | 20.2 | 8.3 | 12.7 | 25 Total nur | 0.8 nber of blows | 57.2 analvzed: 40 | 0.270 | 86.6 | 0.303 |

Time Summary

Drive 2 minutes 41 seconds

4:32:18 PM - 4:34:59 PM (9/1/2009) BN 1 - 41



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PDI-CURVES - Printed: 11/16/2009

Page 148 of 148

Page 55 of 55 DCN#NAP299 DCN NAP306