Depth Interval (Feet)	ISFSI Site	Power Block Site
	Refraction Velocities Compressive Wave (Vp) ⁽¹⁾ (feet/second)	Refraction Velocities Compressive Wave (Vp) ⁽¹⁾ (feet/second)
5-50	2700-6500	2350-5700
	Suspension Velocities Compressive Wave (Vp) ⁽²⁾ (feet/second)	Downhole Velocities Compressive Wave (Vp) ⁽³⁾ (feet/second)
5-50 50-200	4500-9100 7300-12700	2450-9800 5690-15000
	Suspension Velocities Shear Wave (Vs) ⁽²⁾ (feet/second)	Downhole Velocities Shear Wave (Vs) ⁽⁴⁾ (feet/second)
10-30 30-150	3400-4800 3100-5400	2200-4400 2600-5400

Table 21-7. Comparison of seismic wave velocities in the ISFSIstudy area and at the DCPP power block

⁽¹⁾ Velocities reported for rock below thin soil layer or surface disturbed zone (John A. Blume & Associates, 1968)

⁽²⁾ Averaged from WLA 1998 borings

(3) Averaged from 1967 and 1977 borings DDH-1 through 4 and DDH-A through D (URS/John A. Blume & Associates, 1977)

⁽⁴⁾ LTSP envelope (PG&E, 1988)



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FIGURE 21-8 CHRONOLOGY OF STRATIGRAPHY GEOLOGIC PROCESSES AT THE IS STUDY AREA	AND FSI

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Explanation

⊛P-x	Petrographic sample location	
• UC-x	Unconfined test sample location	
• Tx-x	Triaxial test sample location	
+ DS-x	Direct shear test sample location	
cla, N22°W, 25°S, 1/2"	Clay bed, with strike, dip, and thickness (where known) (Table 21-3)	
bd, N61°W, 16'S	Bedding, with strike, dip, and thickness (where known) (Table 21-1)	
I	Friable (weak) dolomite or sandstone zones	
[]	Percent recovery of core run	
	Rock Quality Designation (Deere, and Miller, 1966) of core run; length of recovered intact core over 4 inches divided by length of core run. Low RQD is indicative of closely spaced joints, high RQD is indicative of moderate to widely spaced joints.	

BORING 01-H

- Note:1. Explanation is general. Not all features apply to every boring.
- Note: 2. Only those claybeds that are greater than 1/4" thick are shown
- Note: 3. Coring began 1' to 3' below grade level to allow for installation of borehole casing.

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FIGURE 21-10 SUMMARY LOGS OF BORINGS NEAR SOUTHWEST END OF ISFSI SITE

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- Note:1. Explanation is general. Not all features apply to
- Note: 2. Only those claybeds that are greater than 1/4" thick
- Note: 3. Coring began 1' to 3' below grade level to allow for installation of borehole casing.

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SUMMARY LOGS OF BORINGS AT ISFSI SITE

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BORING 98BA-1

Note:1.	Explanation is general.	Not all features apply to
	every boring.	

- Note: 3. Coring began 1' to 3' below grade level to allow for installation of borehole casing.

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FIGURE 21-12 SUMMARY LOGS OF BORINGS NEAR EAST END OF ISFSI SITE

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Calculation 52.27.100.731, Rev. 0, Attachment A, Page 476f 185



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0 25 50 75 100 feet

Calculation 52.27.100.731, Rev. 0, Attachment A, Page 52 of 185

Notes 1. Location of cross section shown on Figures 21-3 and 21-4. Nearby borings are projected to cross section.

2. See Figure 21-13 for explanation of geologic units.

3. Horizontal scale = vertical scale.

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FIGURE 21-17b CROSS SECTION D-D'

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0 25 50 75 100 leet

Calculation 52.27.100.731, Rev. 0, Attachment A, Page 464 of 185

Notes 1. Location of cross section shown on Figures 21-3 and 21-4. Nearby borings are projected to cross section.

2. See Figure 21-13 for explanation of geologic units.

3. Horizontal scale = vertical scale

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FIGURE 21-18b CROSS SECTION E-E'

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Exploratory boring core from ISFSI study area laid out in stratigraphic succession for studying geologic correlation of bedrock units. Photo roll JGH R5.

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FIGURE 21-28 CORE BOXES FROM ISFSI STUDY AREA LAID OUT IN STRATIGRAPHIC ORDER

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Clay bed within dolomite (Tof_{b-1}) with sample tube in trench T-14B. Photo roll JLB-8.

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FIGURE 21-29 CLAY BED IN TRENCH T-14B

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Calculation 52.27.100.731, Rev. 0, Attachment A, Page 167 of 185





Clay bed in boring 00BA-1 at 55 feet. Note tight contacts with bounding rock, and low dip angle. Photo roll JLB-8

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FIGURE 21-30 CLAY BED AT 55 FEET IN BORING	00BA-1
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Typical appearance of clay bed and bedding laminations in a section of core at 130 feet from boring 01-I, south of the ISFSI. Clay bed occurs within Tof_{b-1} . Photo roll 01JLB-ba.

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FIGURE 21-31 CLAY BED AT 130 FEET IN BORING 01-I

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Minor fault in trench T-1 juxtaposing friable sandstone (Tof_{b-2a}) on left against dolomite (Tof_{b-1}) on the right. Photo roll JLB-2.

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FIGURE 21-32 MINOR FAULT IN TRENCH T-1

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Thin-to medium-bedded dolomite (Tof_{b-1}) exposed in the roadcut of Reservoir Road directly southwest of the ISFSI. Note the laminations and bedding parting surfaces in the dolomite. Gray zones in the rock are believed to be petroliferous stains. Photo roll JLB4-3.

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FIGURE 21-33 BEDDED DOLOMITE ON RESERVOIR ROAD

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Friable dolomite (Tof_{b-1a} ; left part of photo) in contact with closely-fractured dolomite (Tof_{b-1} ; right part of photo) in trench T-20A. Shear fabric in dolomite at the contact indicates the presence of a minor fault. Photo roll JGH 2-1.

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FIGURE 21-34 MINOR FAULT IN TRENCH T-20A

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Outcrop of thick to massive bedded, weathered sandstone (Tof_{b-2}), directly west of the ISFSI. Photo roll JLB OLD-2.

DIABLO CANYON ISFSI FIGURE 21-35 SANDSTONE OUTCROP IN THE ISFSI STUDY AREA	

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Typical dolomite (Tof_{b-1}) and thin clay beds exposed in trench T-11C. Clay beds are subhorizontal and define bedding. Photo roll 01JLB-1.

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FIGURE 21-36 CLAY BEDS AND DOLOMITE IN TRENCH T-11C

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Equal-angle lower hemisphere plot.

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Northward view of Diablo Creek Road cut showing steeply dipping minor faults in dolomite of unit Tof_{b-1} . Slickensides and mullions on the fault plane indicate primarily strike-slip displacement, but bedding also suggests a component of down-to-the- east vertical separation of approximately 3 to 6 feet. These faults are located along projection of faults exposed in trenches at the ISFSI, approximately 800 feet to the southeast, that have similar strike and slickenside/mullion rakes. Photo roll JLB5/16-1.

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FIGURE 21-39 MINOR FAULTS ALONG DIABLO CREEK ROAD

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Calculation 52.27.100.731, Rev. 0, Attachment A, Page 180 of 185

Explanation

Percent recovery of core run

Rock Quality Designation of core run

Geologic contact

-

3.0-inch NX wireline coring

Shear wave (Vs) velocity

Compression wave (Vp) velocity

Note: Boring logged in 1977 by D.W. Frames. Casing used for the upper 18.5 feet. Downhole logging performed by Bruce Redpath.

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Velocity profile from PG&E, 1989, Response to NRC Question 19 dated December 13, 1988.

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FIGURE 21-43 SUMMARY LOG OF **1977 POWER BLOCK BORING DDH-D**

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Borings 98BA-1 and 98BA-4





Note: Average velocity profiles interpreted from data

R1 - R2 = Receiver-to-receiver velocity (3.3-foot spacing) S-R1 = Source-to-receiver velocity (10.3-foot spacing)

Calculation 52.27.100.731, Rev. 0, Attachment A, Page 181 of 185

Boring 98BA-3

