

EPRI

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Estimation of Carbon-14 in Nuclear Power Plant Gaseous Effluents

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EPRI Project Objectives

- Review international research and development & data related to Carbon-14 generation and release.
- Review Carbon-14 generation and release mechanisms in nuclear power plants.
- Provide utilities with methodology for accurately estimating carbon-14 generation and release from specific nuclear power plants.
- Benchmark 2-BWRs, 2-W PWRs, 1-CE PWR, 1-B&W PWR

Calculation of Reactor Coolant C-14 Source Term

- Production reactions
- Target concentrations
- Neutron cross-sections
- Neutron fluxes
- Target quantity in neutron flux

Production of C-14 in Coolant

Nuclear Reactions (in order of importance)

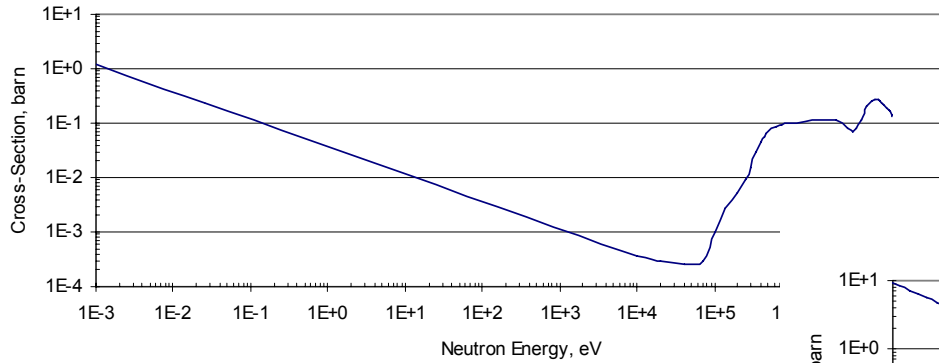
Reaction	Target Abundance (%)	Target Concentration
$^{17}\text{O} (n,\alpha) ^{14}\text{C}$	0.038	1.27E22 atoms $^{17}\text{O}/\text{kg H}_2\text{O}$
$^{14}\text{N} (n,p) ^{14}\text{C}$	99.632	4.28E19 atoms $^{14}\text{N}/\text{kg H}_2\text{O}$ - ppm N
$^{13}\text{C} (n,\gamma) ^{14}\text{C}$	1.07	5.36E17 atoms $^{13}\text{C}/\text{kg H}_2\text{O}$ - ppm C

Possible Chemical Forms Produced from In-Core ^{14}C Production Reactions

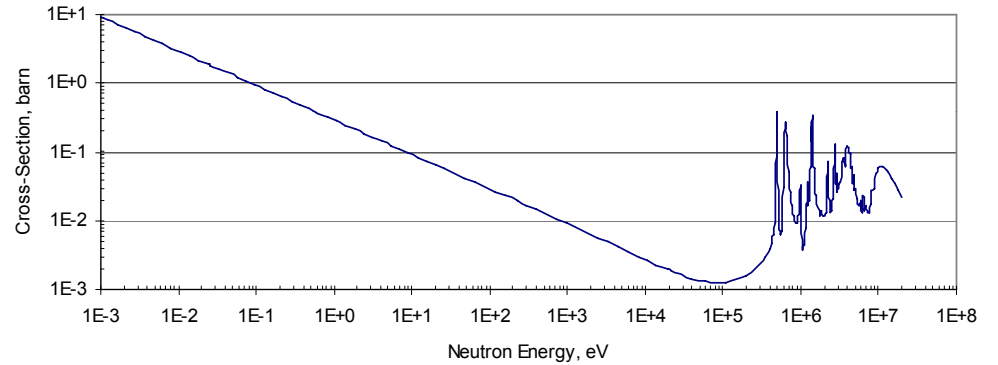
Single Carbon Atom Species		Environment
CO_2	Carbon Dioxide	Oxidizing
CO	Carbon Monoxide	↓
HCOOH	Formic Acid	
$\text{H}_2\text{C}=\text{O}$	Formaldehyde	
CH_3OH	Methanol	
CH_4	Methane	Reducing

C-14 Production Cross-Sections

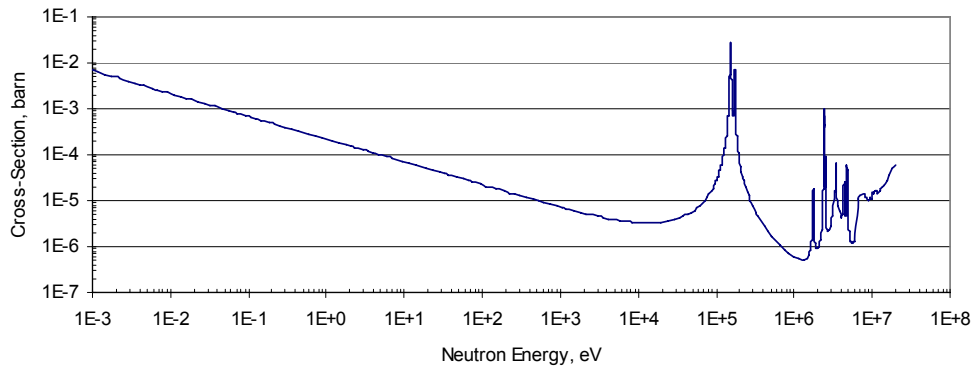
Cross-Section for $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction



Cross-Section for $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction

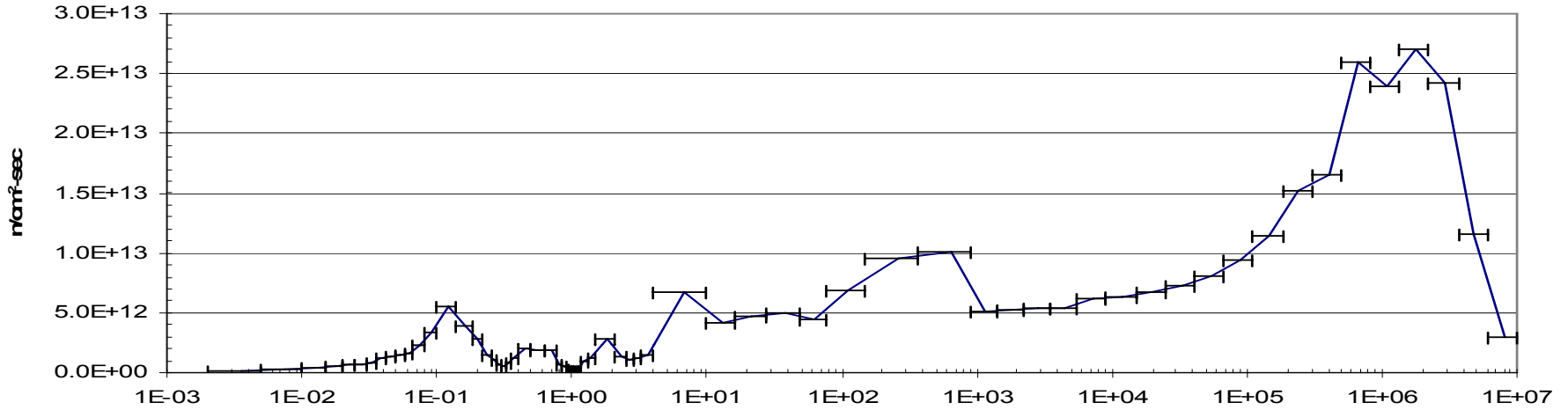


Cross-Section for $^{13}\text{C}(n,\gamma)^{14}\text{C}$ Reaction

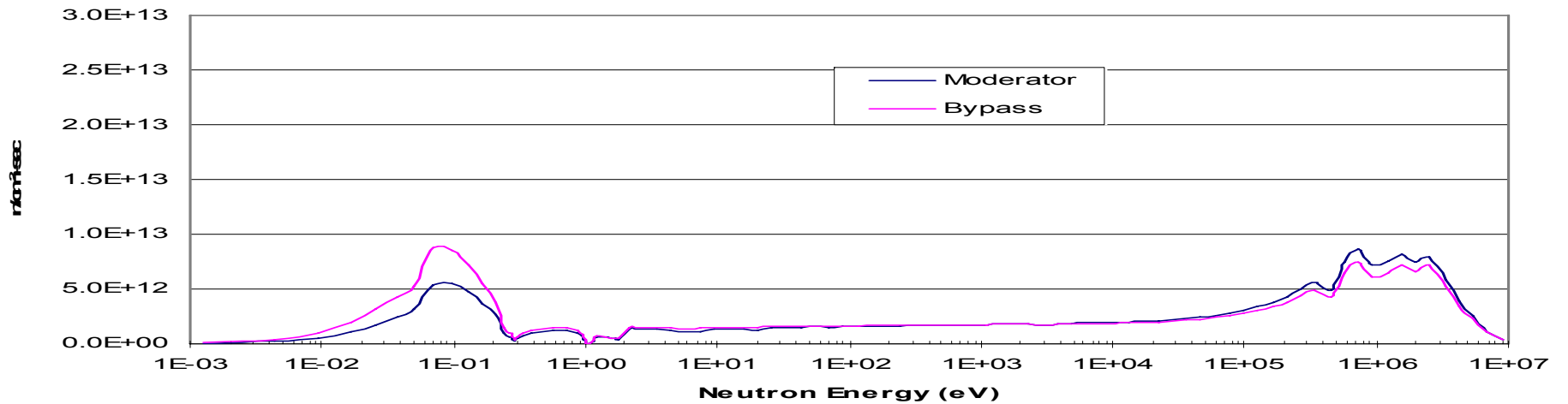


Examples of Neutron Flux Spectra

PWR Neutron Flux - 16 GWd/MTU



BWR Neutron Flux Distribution - 20 GWd/MTU



“Effective Mass” of Coolant in Active Core

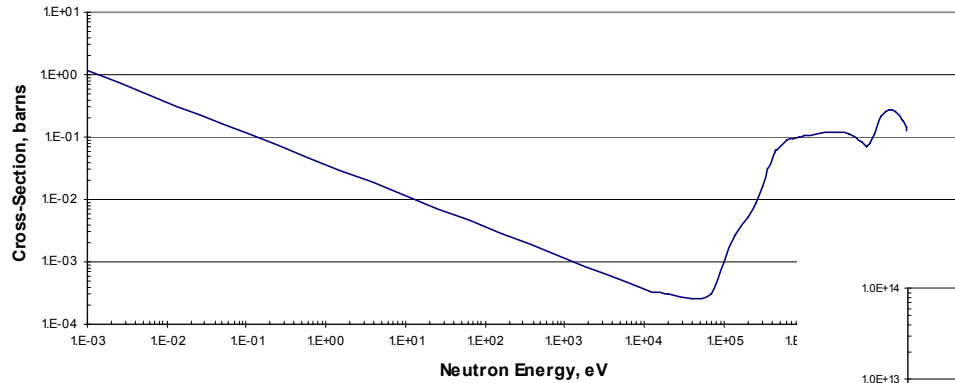
• BWR	BWR-GALE Code	39,000 kg
	Limerick UFSAR	33,975 kg
	GE Vessel Drawings	
	2894 MW _T , 624 Fuel Assemblies	24,630 kg
	3579 MW _T , 748 Fuel Assemblies	29,755 kg
	3579 MW _T , 732 Fuel Assemblies	27,805 kg
	Oyster Creek, 1860 MWt, 560 Fuel Assemblies	26,254 kg
	1593 MW _T , 368 Fuel Assemblies	15,830 kg
	Bonka, 1972	33,000 kg
	Fowler , 1976, 3579 MW _T BWR/6	39,500 kg
• PWR	Helmholz (Braidwood 1)	14,100 kg
	Bonka (1976)	13,400 kg
	Fowler (1976) - 3479 MW _T CE Plant	13,700 kg

- Need site specific value to calculate individual unit source term.

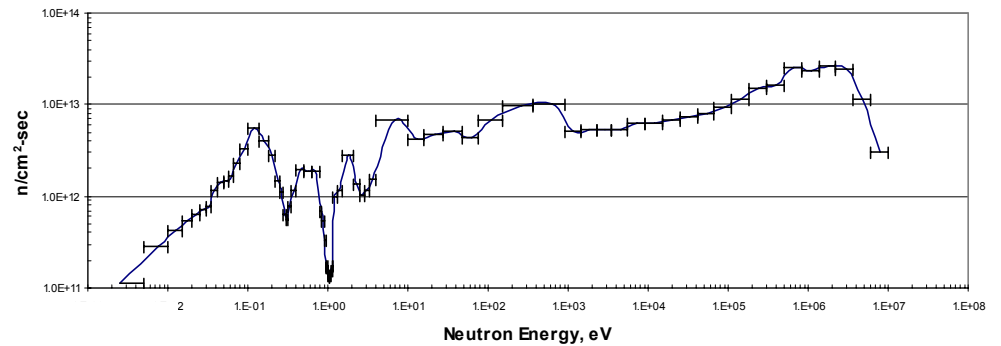
Example Calculation at 16 GWd/MTU

$^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction

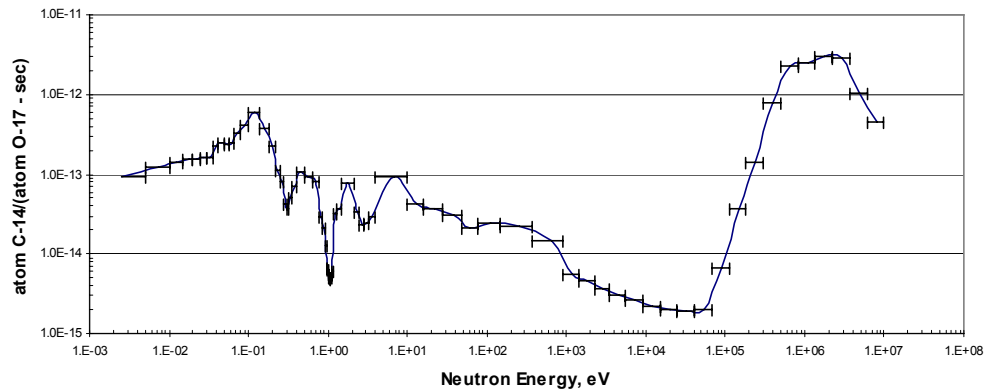
O-17 (n,alpha) C-14 Production Reaction



Average Neutron Flux (16,000 MWD/MTU) - PWR



C-14 Production from the O-17(n,alpha)C-14 Reaction



PWR Source Term Example - $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction

PWR “Effective Cross-Sections” for the $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction

Neutron Group	Group Energy	“Effective Cross-Section”, b
Thermal	≤ 0.625 eV	0.1189
Intermediate	> 0.625 eV - < 1 MeV	0.0183
Fast	≥ 1 MeV	0.1504

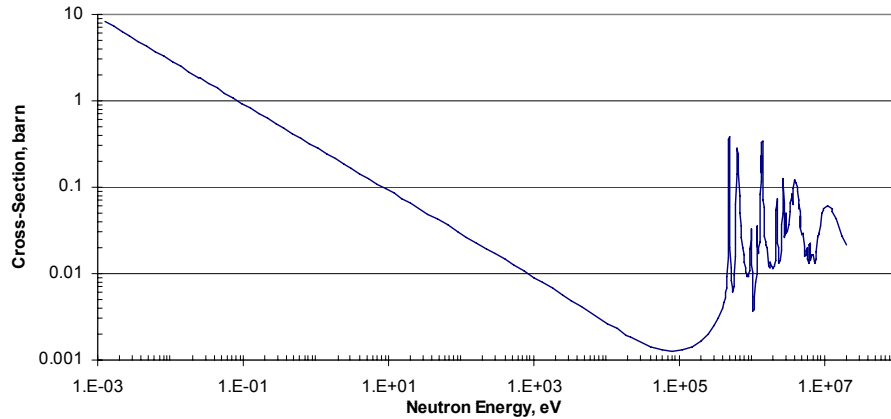
- C-14 production per kilogram of water is $2.475\text{E-}5$ $\mu\text{Ci/sec-kg}$
- For the 1178 MW_e ($\sim 3549 \text{ MW}_{\text{TH}}$) PWR with an estimated coolant mass of 14,100 kg, the total production for this reactor would be approximately:

$$\begin{aligned}
 2.475\text{E-}5 * 14,100 &= 0.349 \mu\text{Ci/sec} \\
 &= 11.0 \text{ Ci/yr} &= 9.35 \text{ Ci/GW}_e\text{-yr} \\
 &= 13.1 \text{ kBq/MWh}_{\text{TH}} &= 0.354 \mu\text{Ci/MWh}_{\text{TH}}
 \end{aligned}$$

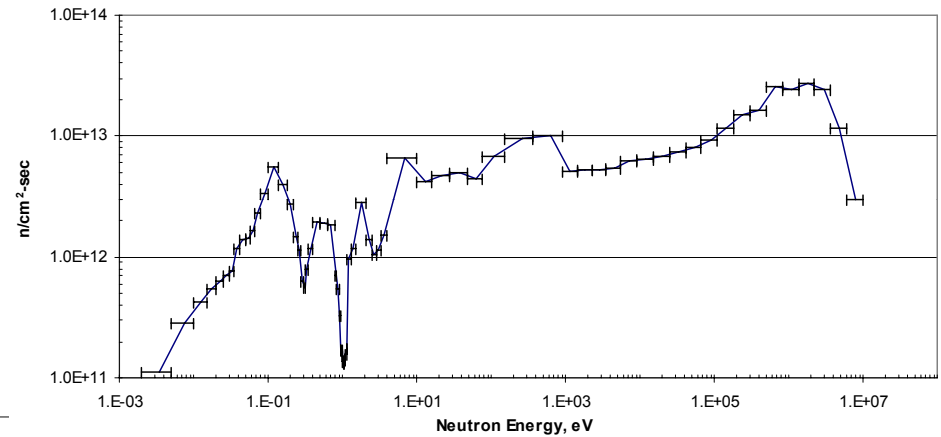
Example Calculation at 16 GWd/MTU

$^{14}\text{N}(n,p)^{14}\text{C}$ Reaction

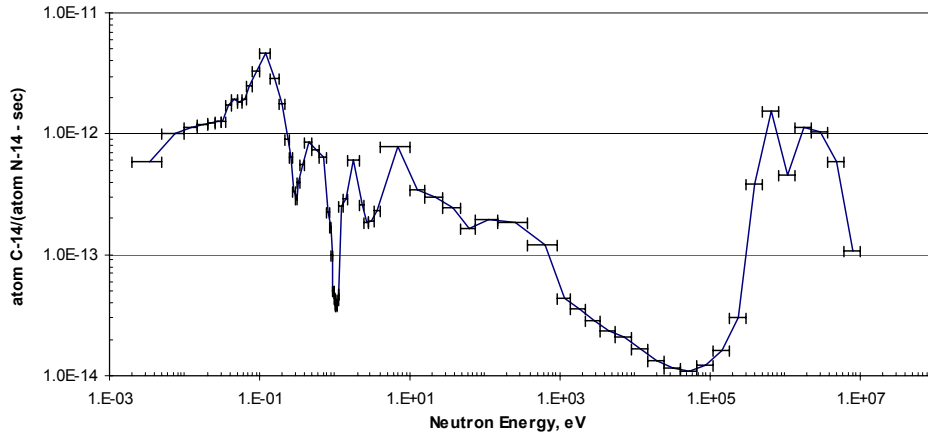
N-14 (n,p) C-14 Cross Section



PWR Neutron Flux



Production of C-14 by the N-14 (n,p) C-14 Reaction in a PWR



PWR Source Term Example - $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction

PWR “Effective Cross-Sections” for the $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction

Neutron Group	Group Energy	“Effective Cross-Section”, b
Thermal	≤ 0.625 eV	0.9519
Intermediate	> 0.625 eV - < 1 MeV	0.0358
Fast	≥ 1 MeV	0.0505

- C-14 production rate per kilogram of water with 1.0 ppm dissolved nitrogen:

$$2.10\text{E-}7 \text{ } \mu\text{Ci/sec-kg-ppm N}$$

- At a coolant mass in the core flux of 14,100 kg, the production rate for this reactor would be:

$$2.10\text{E-}7 * 14,100 = 2.96\text{E-}3 \text{ } \mu\text{Ci/sec-ppm N or } 0.09 \text{ Ci/yr-ppm N}$$

PWR Source Term Example

- For the 1178 MW_e (~3549 MW_{TH}) PWR with an estimated coolant mass of 14,100 kg and 2 ppm N:
 - $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction = 11.0 Ci/yr
 - $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction = 0.18 Ci/yr
 - Total = 12.8 Ci/yr

BWR Source Term Example - $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction

“Effective Cross-Sections” for the $^{17}\text{O}(n,\alpha)^{14}\text{C}$ reaction

		“Effective Cross-Section”, b	
Neutron Group	Group Energy	Moderator	Bypass
Thermal	≤ 0.625 eV	0.1328	0.1387
Intermediate	> 0.625 eV - < 1 MeV	0.0238	0.0222
Fast	≥ 1 MeV	0.1106	0.1106

- C-14 Production:

<u>Moderator Region</u>	<u>Bypass Region</u>
$1.75\text{E-}5$ $\mu\text{Ci/sec-kg}$	$2.05\text{E-}5$ $\mu\text{Ci/sec-kg}$
- For example, one large $3579 \text{ MW}_{\text{TH}}$ BWR, is estimated to have 17,100 kg of coolant in the bypass region and 12,650 kg of coolant in the moderator region. The total production for this reactor would be:

$$\begin{aligned}
 1.75\text{E-}5 * 12,655 + 2.05\text{E-}5 * 17,100 &= 0.572 \mu\text{Ci/sec} \\
 &= 18.0 \text{ Ci/yr} \\
 &= 21.3 \text{ kBq/MWhth} \\
 &= 0.575 \mu\text{Ci/MWhth}
 \end{aligned}$$

BWR Source Term Example - $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction

“Effective Cross-Sections” for the $^{14}\text{N}(n,p)^{14}\text{C}$ reaction

Neutron Group	Group Energy	“Effective Cross-Section”, b	
		Moderator	Bypass
Thermal	≤ 0.625 eV	1.0560	1.0903
Intermediate	> 0.625 eV - < 1 MeV	0.0384	0.0423
Fast	≥ 1 MeV	0.0479	0.0478

- C-14 production per kilogram of water with 1.0 ppm dissolved nitrogen

Moderator Region

2.15E-7 $\mu\text{Ci}/\text{sec}\cdot\text{kg}\cdot\text{ppm N}$

Bypass Region

3.23E-7 $\mu\text{Ci}/\text{sec}\cdot\text{kg}\cdot\text{ppm N}$

- For example, one large 3579 MW_{th} BWR is estimated to have 17,100 kg of water in the bypass region and 12,655 kg of water in the moderator region.
- The total production for this reactor would be:

$$2.15\text{E-}7 \cdot 12,655 + 3.23\text{E-}7 \cdot 17,100 = 8.24\text{E-}3 \mu\text{Ci}/\text{sec}\cdot\text{ppm N} \text{ or } 0.26 \text{ Ci}/\text{yr}\cdot\text{ppm N}$$

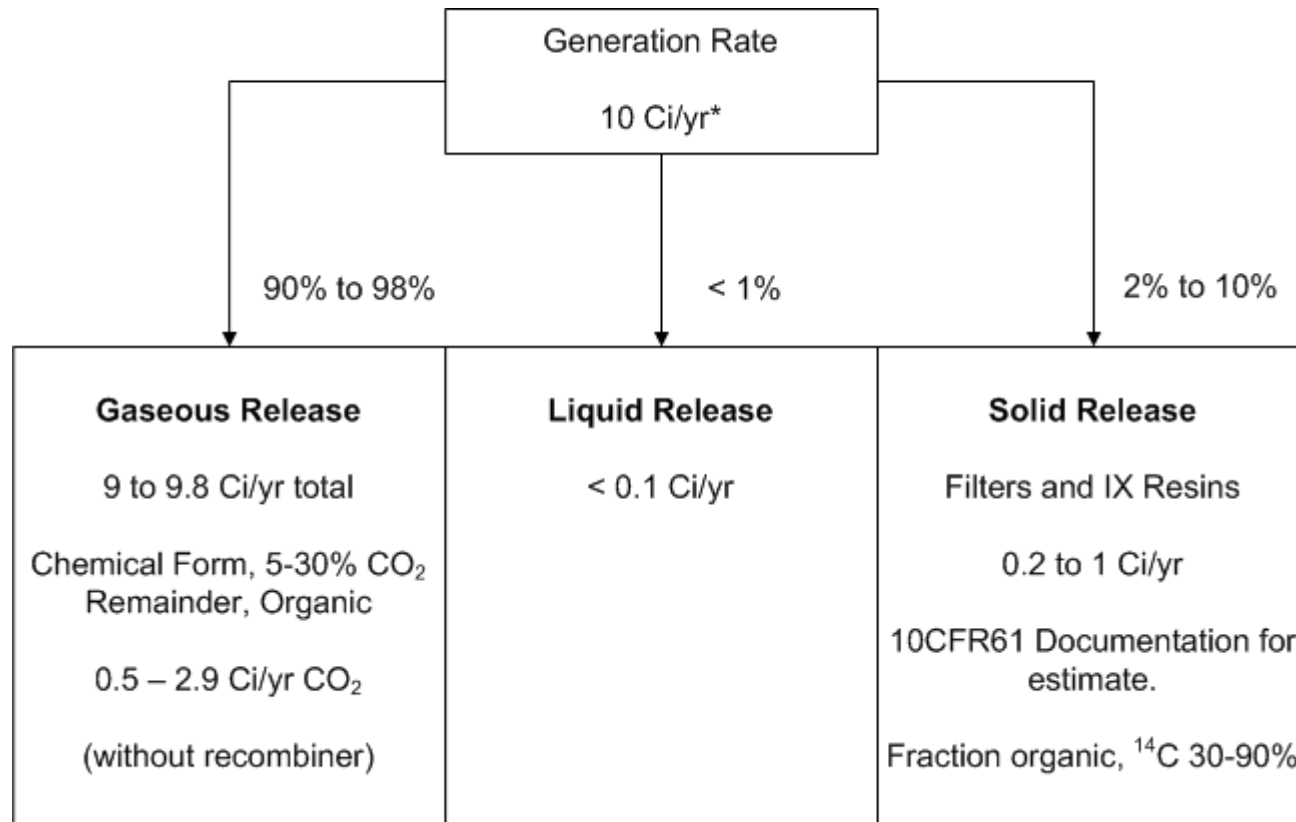
BWR Source Term Example

- 3579 MW_{TH} BWR, is estimated to have 17,100 kg of coolant in the bypass region and 12,650 kg of coolant in the moderator region:
 - $^{17}\text{O}(n,\alpha)^{14}\text{C}$ Reaction = 18.0 Ci/yr
 - $^{14}\text{N}(n,p)^{14}\text{C}$ Reaction = Negligible
 - Total = 18.0 Ci/yr

What Do We Need To Do To Estimate the C-14 Source Term?

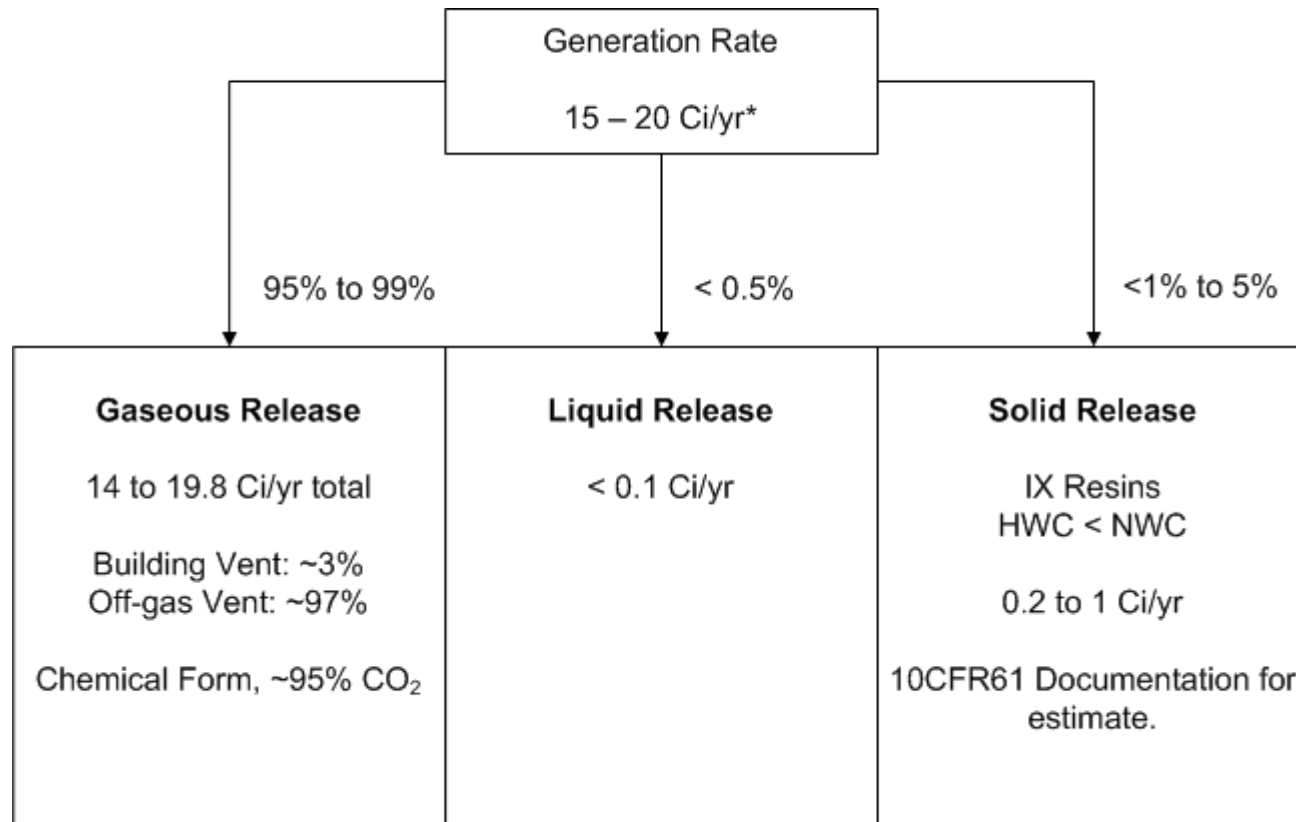
- Core “Average” Neutron Flux
 - BOC, Mid-cycle, EOC
 - Three energy groups
 - Thermal ≤ 0.625 eV
 - Intermediate > 0.625 eV - < 1.0 MeV
 - Fast ≥ 1.0 MeV
- Use “Effective Cross-Sections” in the three neutron energy groups
- “Effective Mass” of coolant in active core
 - Suggest use mass from “bottom” of active core to “top” of active core
 - BWR → must consider moderator and bypass regions
- Concentration of Nitrogen in the coolant (for PWR; BWR negligible.)
- Calculate BOC, mid-cycle and EOC C-14 source term
 - Average the three values

Simplistic PWR Transport Model



*Unit Specific

Simplistic BWR Transport Model



*Unit Specific

Current Status

- Calculation methodology for generation established.
- Collecting operational data from U.S. utilities to conduct example estimations and compare with available carbon-14 data.
- Draft methodology to be available in Fall 2010.



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