



JUN 01 2010

L-PI-10-049
TS 5.6.5.d

U S Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555-0001

Prairie Island Nuclear Generating Plant Unit 2
Docket 50-306
License No. DPR-60

Core Operating Limits Report (COLR) for Prairie Island Nuclear Generating Plant (PINGP) Unit 2, Cycle 26, Revision 0

Pursuant to the requirements of Technical Specification 5.6.5.d, the COLR for the PINGP Unit 2, Cycle 26, Revision 0, is attached. The limits specified in the attached COLR have been established using Nuclear Regulatory Commission (NRC) approved methodologies.

The COLR has been updated for the Unit 2, Cycle 26 core reload. The following changes were made:

- Revised Section 3.1.3, Isothermal Temperature Coefficient (ITC), ITC Lower limit, for Unit 2, Cycle 26.
- Revised Section 3.2.1, Heat Flux Hot Channel Factor ($F_Q(Z)$), to add a paragraph on how the $W(Z)$ values are generated.
- Revised Section 3.2.2, Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$), $F_{\Delta H}$ limits, for Unit 2, Cycle 26.
- Revised Section 3.4.1, RCS (Reactor Coolant System) Pressure, Temperature, and Flow – Departure from Nucleate Boiling (DNB) Limits, Pressurizer pressure limit, for Unit 2, Cycle 26.
- Revised the References section, adding items 7, 9, 11, and 12.
- Revised the References section, item 28, to replace the previous reference with the new reference to the 50.59 evaluation for Unit 2 Cycle 26 Core Reload.
- Revised Table 1, Minimum Required Shutdown Margin, for Unit 2, Cycle 26.
- Revised Table 2, $W(z)$ Values, for Unit 2, Cycle 26.
- Revised Table 3, $F_Q^W(Z)$ Penalty Factor, for Unit 2, Cycle 26.

Summary of Commitments

This letter contains no new commitments and no revisions to existing commitments.

 For M. Schimmel

Mark A. Schimmel
Site Vice President, Prairie Island Nuclear Generating Plant
Northern States Power Company - Minnesota

Enclosure

cc: Administrator, Region III, USNRC
Project Manager, Prairie Island, USNRC
Resident Inspector, Prairie Island, USNRC
State of Minnesota

ENCLOSURE

**PRAIRIE ISLAND NUCLEAR GENERATING PLANT
CORE OPERATING LIMITS REPORT
UNIT 2 – CYCLE 26
REVISION 0**

Record of Revision (6 pages)

Unit 2 – Cycle 26, Revision 0 (18 pages)

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
1	13	0	3/22/90	Original Unit 2 Core Operating Limits Report, distributed with Technical Specification Revision 92.
1	14	0	3/22/90	Original Unit 1 Core Operating Limits Report, distributed with Technical Specification Revision 92.
		1	7/27/90	Incorporated expanded V(z) curves.
		2	9/27/90	Clarified rod insertion limit curve applicability.
		3	2/11/91	Incorporated revised F_Q of 2.45 as a result of NRC approval of Westinghouse Topical Report WCAP-10924-P-A, Volume 1, Addendum 4, October 1990.
2	14	0	-	Not used.
		1	9/27/90	Updated to Unit 2 Cycle 14, incorporated expanded V(z) curves and clarified rod insertion limit curve applicability.
		2	2/11/91	Incorporated revised F_Q of 2.45 as a result of NRC approval of Westinghouse Topical Report WCAP-10924-P-A, Volume 1, Addendum 4, October 1990.
1	15	0	6/25/91	Updated to Unit 1 Cycle 15.
2	15	0	3/9/92	Updated to Unit 2 Cycle 15 and clarified labeling of Figure 4. Clarified the actions to be taken if the nuclear enthalpy rise hot channel factor exceeds the Technical Specification limit.
1	16	0	12/28/92	Updated to Unit 1 Cycle 16, removed V(z) curves and replaced them with list of bounding V(z) values for three ranges of exposures.
2	16	0	12/8/93	Updated to Unit 2 Cycle 16. Removed the multiple V(z) curves and replaced them with a single figure with bounding V(z) curves for four ranges of exposures. Incorporated additional discussion related to V(z) and K(z).

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
2	16	1	11/3/94	The table containing the bounding V(z) values and Figure 2 updated to incorporate revised bounding V(z) values for the exposure range of 14-21.5 GWD/MTU. Figures 3 through 6 re-formatted.
1	17	0	6/17/94	Updated to Unit 1 Cycle 17. Removed the list of bounding V(z) values and replaced it with multiple V(z) curves. Incorporated additional discussion related to V(z) and K(z).
2	17	0	6/2/95	Updated to Unit 2 Cycle 17. Incorporated Table 1 and expanded Figure 2 with updated bounding V(z) values.
1	18	0	2/7/96	Updated to Unit 1 Cycle 18. Incorporated revised $F_{\Delta H}$ limit of 1.77. Incorporated Table 1 and updated Figure 2 with revised bounding V(z) values.
2	18	0	2/27/97	Updated to Unit 2 Cycle 18. Revised $F_{\Delta H}$ limit to 1.77. Updated Table 1 and Figures 2a through 2e with revised bounding V(z) values. Incorporated new Figures 2f and 2g with additional bounding V(z) values.
1	19	0	9/25/97	Updated to Unit 1 Cycle 19. Updated Table 1 and Figures 2a through 2f with revised bounding V(z) values.
2	19	0	12/17/98	Updated to Unit 2 Cycle 19. Updated Table 1 and Figures 2a through 2d with revised bounding V(z) values. Deleted Figures 2e, 2f and 2g.
1	20	0	5/13/99	Updated to Unit 1 Cycle 20. Updated Table 1 and Figures 2a through 2f with revised bounding V(z) values.
		1	8/4/00	Technical Specification Amendment 151: Relocate shutdown margin (SDM) requirements from Tech Specs and incorporate additional SDM requirements for Modes 3-6 from revised analysis of Uncontrolled Dilution event.

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
2	20	0	5/31/00	Updated to Unit 2 Cycle 20. Updated Table 1 and Figures 2a through 2d with revised bounding V(z) values. Added new Table 2 and Figures 2e, 2f and 2g with additional bounding V(z) values. Added references to Tables 1 and 2 and to Figures 2e, 2f and 2g to discussion of heat flux hot channel factor limits. Added discussion clarifying applicability of axial flux difference limits when using Tables 1 and 2 and Figures 2a through 2g. Added discussion of two tier V(z) curve presented in Table 2 and Figure 2g.
		1	8/4/00	Technical Specification Amendment 142: Relocate shutdown margin (SDM) requirements from Tech Specs and incorporate additional SDM requirements for Modes 3-6 from revised analysis of Uncontrolled Dilution event.
	20	2	9/1/00	Revised to change axial flux difference target band.
1	21	0	1/31/01	Updated to support refueling activities associated with Unit 1 Cycle 21. Revision 0 of the Unit 1 Cycle 21 COLR had to be issued prior to confirming the applicability of the LOCA analysis. Therefore, Revision 0 of the Unit 1 Cycle 21 COLR does not contain all of the operating limits necessary to support operation of Unit 1 Cycle 21.
1	21	1	2/19/01	Updated to Unit 1 Cycle 21. Updated Tables 1 and 2 and Figures 2a through 2f with revised bounding V(z) values.
1	21	2	10/02/02	Revised to support License Amendment 158 changes, including revision of all references to TS, revision of F _Q symbols, addition of Table 4, ITC limits, DNB limits and refueling boron concentrations.
2	21	0	2/06/02	Updated to Unit 2 Cycle 21.

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
2	21	1	10/02/02	Revised to support License Amendment 149 changes, including revision of all references to TS, revision of F_Q symbols, addition of Table 4, ITC limits, DNB limits and refueling boron concentrations. Also revised to include an additional $V(z)$ curve to give greater F_Q margin between 13.0 and 16.0 GWd/MTU.
1	22	0	11/25/02	Updated to Unit 1 Cycle 22. Updated Tables 1 and 2 and Figures 2a through 2f with revised bounding $V(z)$ values. Incorporated new Figure 2g with additional bounding $V(z)$ values. Updated Table 3 with revised minimum shutdown margin limits. Deleted and revised text to eliminate duplication with the Technical Specifications and the Bases.
2	22	0	9/19/03	Updated to Unit 2 Cycle 22. Updated Tables 1 and 2. A reduced number of exposure ranges were calculated in Table 1, therefore new Figures 2a through 2e with revised bounding $V(z)$ values replaced Figures 2a through 2f. New Figure 2f replaced Figure 2g for the 2 tier band bounding $V(z)$ values. Updated Table 3 with revised minimum shutdown margin limits. Deleted and revised text to eliminate duplication with the Technical Specifications and the Bases.
1	22	1	7/6/04	Revision to incorporate Westinghouse Safety Analysis Transition per LA 162/153. Revision 1 contains transitional values for the OP/OT ΔT Trip setpoints that will be used while the physical changes are implemented.
2	22	1	7/6/04	Revision to incorporate Westinghouse Safety Analysis transition per LA 162/153. Revision 1 contains transitional values for the OP/OT ΔT Trip setpoints that will be used while the physical changes are implemented.
2	22	2	7/12/04	Revised F_Q limit from 2.4 to 2.5. Removed OP and OT delta-T setpoints based on NMC methodology and replaced with Westinghouse developed setpoints.

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
1	22	2	7/16/04	Revised Fq limit from 2.4 to 2.5. Removed OP and OT delta-T setpoints based on NMC methodology and replaced with Westinghouse developed setpoints.
1	23	0	10/20/04	Updated to Unit 1 Cycle 23.
2	23	0	-	Not used due to core redesign.
2	23	1	5/19/05	Updated to Unit 2 Cycle 23 and to support redesign of Unit 2 Cycle 23 core.
2	23	1	7/11/05	Revised ITC upper limit from < 0 pcm/°F for power levels $> 70\%$ RTP to less than a line that slopes linearly from 0 pcm/°F at 70% RTP to -2.9 pcm/°F at 100% RTP. Revised the title of Figure 3 to reference T.S. 3.1.4 Condition B and revised the title of Figure 4 to reference T.S. 3.1.4 Condition A. Added references 24 and 25 to include the 50.59 screenings written to issue revision 1.
1	24	0	5/10/06	Updated to Unit 1 Cycle 24.
1	24	1	8/7/06	Updated Table 3 to reflect the correct $F_q^w(z)$ penalty factors.
2	24	0	11/26/06	Updated to Unit 2 Cycle 24 Modes 5 and 6.
2	24	1	12/6/06	Updated to Unit 2 Cycle 24 for Modes 1-6.
2	24	2	9/4/07	Revised to support LA-179/169. Revised reference 24 to include the revision number (revision 0) and the correct date of the report (January 2005). Revised references 6a, 6b, 6c, and 8 to say 'Deleted.' These references referred to the old LBLOCA methodology and model.
2	24	2	2/11/08	Updated Table 1 to reflect correct Shutdown Margin Requirements and added Figures 6A through 6H.

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Core Operating Limits Report

Record of Revision

Unit	Cycle	Revision No.	Approval Date	Remarks
2	24	3	2/11/08	Updated Table 1 to reflect correct Shutdown Margin Requirements and added Figures 6A through 6H.
1	25	0	2/24/08	Updated to Unit 1 Cycle 25
1	25	1	5/28/08	Updated Table 2 to reflect the correct W(z) at a burnup of 150 MWd/MTU and a core height of 6.20 feet
2	25	0	9/26/08	Updated for Unit 2 Cycle 25
1	26	0	9/24/09	Updated for Unit 1 Cycle 26
2	26	0	5/3/10	Updated for Unit 2 Cycle 26

PRAIRIE ISLAND NUCLEAR GENERATING PLANT

CORE OPERATING LIMITS REPORT

UNIT 2 – CYCLE 26

REVISION 0

Reviewed By: *Lynn Johnson* Date: 5-2-10
Lynn Johnson
Supervisor, NSSS

Reviewed By: *Clifford Zamiat* Date: 5/2/10
FOR Hank Hoelscher
Hank Hoelscher
Supervisor, PWR Analyses

Approved By: *Dave Kettering* Date: 5/3/10
Dave Kettering
Director, Site Engineering

Note: This report is not part of the Technical Specifications
This report is referenced in the Technical Specifications

PRAIRIE ISLAND NUCLEAR GENERATING PLANT
CORE OPERATING LIMITS REPORT
UNIT 1 - CYCLE 26
REVISION 0

This report provides the values of the limits for Unit 2 Cycle 26 as required by Technical Specification Section 5.6.5. These values have been established using NRC approved methodology and are established such that all applicable limits of the plant safety analysis are met. The Technical Specifications affected by this report are listed below:

- 1 2.1.1 Reactor Core SLs
- 2 3.1.1 Shutdown Margin (SDM)
- 3 3.1.3 Isothermal Temperature Coefficient (ITC)
- 4 3.1.5 Shutdown Bank Insertion Limits
- 5 3.1.6 Control Bank Insertion Limits
- 6 3.1.8 Physics Tests Exceptions - MODE 2
- 7 3.2.1 Heat Flux Hot Channel Factor ($F_Q(z)$)
- 8 3.2.2 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$)
- 9 3.2.3 Axial Flux Difference (AFD)
- 10 3.3.1 Reactor Trip System (RTS) Instrumentation
Overtemperature ΔT and Overpower ΔT Parameter Values for Table 3.3.1-1
- 11 3.4.1 RCS Pressure, Temperature, and Flow - Departure from Nucleate
Boiling (DNB) Limits
- 12 3.9.1 Boron Concentration

1 2.1.1 Reactor Core Safety Limits

Reactor Core Safety Limits are shown in Figure 1.

Reference Technical Specification section 2.1.1.

2 3.1.1 Shutdown Margin Requirements

Minimum Shutdown Margin requirements are shown in Table 1.

Reference Technical Specification section 3.1.1.

3. 3.1.3 Isothermal Temperature Coefficient (ITC)

ITC Upper limit:

- a. < 5 pcm/ $^{\circ}$ F for power levels $< 70\%$ RTP; and
- b. less than a line which slopes linearly from
 - i. 0 pcm/ $^{\circ}$ F at a power level = 70% RTP to
 - ii. -1.5 pcm/ $^{\circ}$ F at a power level = 100% RTP

ITC Lower limit:

- a. -43.15 pcm/ $^{\circ}$ F

Reference Technical Specification section 3.1.3.

4. 3.1.5 Shutdown Bank Insertion Limits

The shutdown rods shall be fully withdrawn.

Reference Technical Specification section 3.1.5.

5. 3.1.6 Control Bank Insertion Limits

The control rod banks shall be limited in physical insertion as shown in Figures 2, 3, and 4.

The control rod banks withdrawal sequence shall be Bank A, Bank B, Bank C, and finally Bank D.

The control rod banks shall be withdrawn maintaining 128 step tip-to-tip distance.

Reference Technical Specification section 3.1.6.

6. 3.1.8 Physics Tests Exceptions - MODE 2

Minimum Shutdown Margin requirements during physics testing are shown in Table 1.

Reference Technical Specification section 3.1.8.

7. 3.2.1 Heat Flux Hot Channel Factor ($F_Q(Z)$)

The Heat Flux Hot Channel Factor shall be within the following limits:

$$CFQ = 2.50$$

$K(Z)$ is a constant value = 1.0 at all elevations.

$W(Z)$ values are provided in Table 2.

$F_Q^W(Z)$ Penalty Factors are provided in Table 3.

The $W(Z)$ values are generated assuming that they will be used for full power surveillance. When a part power surveillance is performed, the $W(Z)$ values should be multiplied by the factor $1/P$, when $P > 0.5$. When P is ≤ 0.5 , the $W(Z)$ values should be multiplied by the factor $1/(0.5)$, or 2.0. This is consistent with the adjustment in the $F_Q(Z)$ limit at part power conditions.

Applicability: MODE 1

Reference Technical Specification section 3.2.1

8. 3.2.2 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$)

The Nuclear Enthalpy Rise Hot Channel Factor shall be within the following limits:

$$F_{\Delta H} \leq 1.77 \times [1 + 0.3(1 - P)] \text{ for all 422V+ type fuel assemblies, and}$$

$$F_{\Delta H} \leq 1.708 \times [1 + 0.3(1 - P)] \text{ for all OFA type fuel assemblies}$$

where: P is the fraction of RATED THERMAL POWER at which the core is operating.

Applicability: MODE 1.

Reference Technical Specification section 3.2.2

9. 3.2.3 Axial Flux Difference (AFD)

The indicated axial flux difference, in % flux difference units, shall be maintained within the allowed operational space defined by Figure 5.

Applicability: MODE 1 with RATED THERMAL POWER \geq 50% RTP.

Reference Technical Specification section 3.2.3.

10. 3.3.1 Reactor Trip System (RTS) Instrumentation

Overtemperature ΔT and Overpower ΔT Parameter Values for Table 3.3.1-1;

Overtemperature ΔT Setpoint

Overtemperature ΔT setpoint parameter values:

- ΔT_0 = Indicated ΔT at RATED THERMAL POWER, %
- T = Average temperature, °F
- T' = 560.0 °F
- P = Pressurizer Pressure, psig
- P' = 2235 psig
- K_1 \leq 1.17
- K_2 = 0.014 /°F
- K_3 = 0.00100 /psi
- τ_1 = 30 seconds
- τ_2 = 4 seconds
- f(ΔI) = A function of the indicated difference between top and bottom detectors of the power range nuclear ion chambers. Selected gains are based on measured instrument response during plant startup tests, where q_t and q_b are the percent power in the top and bottom halves of the core respectively, and $q_t + q_b$ is total core power in percent of RATED THERMAL POWER, such that
 - (a) For $q_t - q_b$ within $-13, +8$ % f(ΔI) = 0
 - (b) For each percent that the magnitude of $q_t - q_b$ exceeds $+8\%$, the ΔT trip setpoint shall be automatically reduced by an equivalent of 1.73 % of RATED THERMAL POWER.
 - (c) For each percent that the magnitude of $q_t - q_b$ exceeds -13 % the ΔT trip setpoint shall be automatically reduced by an equivalent of 3.846 % of RATED THERMAL POWER.

Overpower ΔT Setpoint

Overpower ΔT setpoint parameter values:

- ΔT_0 = Indicated ΔT at RATED THERMAL POWER, %
- T = Average temperature, °F
- T' = 560.0 °F
- K_4 \leq 1.11
- K_5 = 0.0275/°F for increasing T; 0 for decreasing T
- K_6 = 0.002/°F for $T > T'$; 0 for $T \leq T'$
- τ_3 = 10 seconds

11. 3.4.1 RCS Pressure, Temperature, and Flow - Departure from Nucleate Boiling (DNB) Limits

Pressurizer pressure limit = 2190 psia
RCS average temperature limit = 564°F
RCS total flow rate limit = 178,000 gpm

Reference Technical Specification section 3.4.1.

12. 3.9.1 Refueling Boron Concentration.

The boron concentration of the reactor coolant system and the refueling cavity shall be sufficient to ensure that the more restrictive of the following conditions is met:

- a) $K_{\text{eff}} \leq 0.95$
- b) 2000 ppm
- c) The Shutdown Margin specified in Table 1

Reference Technical Specification section 3.9.1.

REFERENCES
(NRC Approved Methodologies for COLR Parameters)

1. NSPNAD-8101-A, "Qualification of Reactor Physics Methods for Application to Prairie Island," Revision 2, October 2000.
2. NSPNAD-8102-PA, "Prairie Island Nuclear Power Plant Reload Safety Evaluation Methods for Application to PI Units," Revision 7, July 1999.
3. NSPNAD-97002-PA, "Northern States Power Company's "Steam Line Break Methodology," Revision 1, October 2000.
4. WCAP-9272-P-A, "Westinghouse Reload Safety Evaluation Methodology," July, 1985.
- 5.a WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model using the NOTRUMP Code," August, 1985.
- 5.b WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model using the NOTRUMP Code," Addendum 2 Revision 1, July 1997.
- 6.a Not used.
- 6.b Not used.
- 6.c Not used.
7. WCAP-10924-P-A, Volume 1, Revision 1, and Volume 2, Revision 2, "Westinghouse Large Break LOCA Best Estimate Methodology," September 2005.
8. XN-NF-77-57-(A), XN-NF-77-57, Supplement 1 (A), "Exxon Nuclear Power Distribution Control for Pressurized Water Reactors Phase II," May 1981.
9. WCAP-13677-P-A, "10 CFR 50.46 Evaluation Model Report: W-COBRA/TRAC 2-Loop Upper Plenum Injection Model Update to Support ZIRLO™ Cladding Options," February 1994.
10. NSPNAD-93003-A, "Prairie Island Units 1 and 2 Transient Power Distribution Methodology," Revision 0, April 1993.
11. NAD-PI-003, "Prairie Island Nuclear Power Plant Required Shutdown Margin During Physics Tests," Revision 0, January 2001.
12. NAD-PI-004, "Prairie Island Nuclear Plant $F^W_Q(Z)$ Penalty With Increasing $[F^C_Q(Z)/K(Z)]$ Trend," Revision 0, January 2001.

13. WCAP-10216-P-A, Revision 1A, "Relaxation of Constant Axial Offset Control/ FO Surveillance Technical Specification," February 1994.
14. WCAP-8745-P-A, "Design Bases for the Thermal Overpower ΔT and Thermal Overtemperature ΔT Trip Functions," September 1986.
15. WCAP-11397-P-A, "Revised Thermal Design Procedure," April 1989.
16. WCAP-14483-A, "Generic Methodology for Expanded Core Operating Limits Report," January 1999.
17. WCAP-7588 Rev. 1-A, "An Evaluation of the Rod Ejection Accident in Westinghouse Pressurized Water Reactors Using Spatial Kinetics Methods," January 1975.
18. WCAP-7908-A, "FACTRAN – A FORTRAN IV Code for Thermal Transients in a UO₂ Fuel Rod," December 1989.
19. WCAP-7907-P-A, "LOFTRAN Code Description," April 1984.
20. WCAP-7979-P-A, "TWINKLE – A Multidimensional Neutron Kinetics Computer Code." January 1975.
21. WCAP-10965-P-A, "ANC: A Westinghouse Advanced Nodal Computer Code," September 1986.
22. WCAP-11394-P-A, "Methodology for the Analysis of the Dropped Rod Event," January 1990.
23. WCAP-11596-P-A, "Qualification of the PHOENIX-P/ANC Nuclear Design System for Pressurized Water Reactor Cores," June 1988.
24. WCAP-12910 Rev. 1-A, "Pressurizer Safety Valve Set Pressure Shift," May 1993.
25. WCAP-14565-P-A, "VIPRE-01 Modeling and Qualification for Pressurized Water Reactor Non-LOCA Thermal-Hydraulic Safety Analysis," October 1999.
26. WCAP-14882-P-A, "RETRAN-02 Modeling and Qualification for Westinghouse Pressurized Water Reactor Non-LOCA Safety Analyses," April 1999.
27. WCAP-16009-P-A, "Realistic Large-Break LOCA Evaluation Methodology Using the Automated Statistical Treatment Of Uncertainty Method (ASTRUM)," Revision 0, January 2005.
28. 50.59 Evaluation 1076, "Unit 2 Cycle 26 Core Reload."

Table 1

Minimum Required Shutdown Margin, % $\Delta\rho$

Number of Charging Pumps Running**			
Mode 1*			
	0-1 Pump	2 Pumps	3 Pumps
0 – 25000 MWd/MTU	-	-	-
Mode 2*			
	0-1 Pump	2 Pumps	3 Pumps
0 – 25000 MWd/MTU	2.0	2.0	2.0
Physics Testing in Mode 2			
	0-1 Pump	2 Pumps	3 Pumps
0 – 25000 MWd/MTU	0.5	0.5	0.5
Mode 3 $T_{ave} \geq 520\text{ }^\circ\text{F}$ (Most Reactive Rod Out)			
	0-1 Pump	2 Pumps	3 Pumps
0 – 25000 MWd/MTU	2.0	2.0	2.0
Mode 3 $350\text{ }^\circ\text{F} \leq T_{ave} < 520\text{ }^\circ\text{F}$ (Most Reactive Rod Out)			
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU	2.0	2.0	2.5
12000 MWd/MTU	2.0	2.0	2.0
25000 MWd/MTU	2.0	2.0	2.0
Mode 4 $200\text{ }^\circ\text{F} < T_{ave} < 350\text{ }^\circ\text{F}$ (Most Reactive Rod Out)			
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU	2.0	4.0	6.5
12000 MWd/MTU	2.0	3.0	5.0
25000 MWd/MTU	2.0	2.0	2.5

Operational Mode Definitions, as per TS Table 1.1-1.

* For Mode 1 and Mode 2 with $K_{eff} \geq 1.0$, the minimum shutdown margin requirements are provided by the Rod Insertion Limits.

** Charging pump(s) in service only pertains to steady state operations. It does not include transitory operations. For example, operations such as starting a second charging pump in order to secure the operating pump would fall under the one pump in service column.

Table 1, Continued

Minimum Required Shutdown Margin, % $\Delta\rho$

Number of Charging Pumps Running**			
Mode 5			
68°F ≤ T_{ave} ≤ 200°F (Most Reactive Rod Out)			
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU***	2.5	4.5	7.0
12000 MWd/MTU	2.0	3.5	5.5
25000 MWd/MTU	2.0	2.0	2.5

Mode 6			
68°F ≤ T_{ave} < 200°F (ARI)			
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU***	5.129	5.129	7.0
12000 MWd/MTU	5.129	5.129	5.5
25000 MWd/MTU	5.129	5.129	5.129

Mode 6			
68°F ≤ T_{ave} < 200°F (ARO)			
	0-1 Pump	2 Pumps	3 Pumps
0 MWd/MTU***	5.129	5.5	9.0
12000 MWd/MTU	5.129	5.129	7.0
25000 MWd/MTU	5.129	5.129	5.129

Operational Mode Definitions, as per TS Table 1.1-1.

** Charging pump(s) in service only pertains to steady state operations. It does not include transitory operations. For example, operations such as starting a second charging pump in order to secure the operating pump would fall under the one pump in service column.

*** These values are also applicable for the Unit 2 Cycle 25 end of cycle.

Table 2 - W(z) Values (Top 10% and Bottom 8% excluded)*

	Height	BU [MWd/MTU]					
		150	6000	13000	16000	20000	22000
[BOTTOM]	[ft]	AO = -0.59	AO = -2.31	AO = -4.61	AO = -0.38	AO = 0.44	AO = -0.64
1	0.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
2	0.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
6	1.0	1.2691	1.2113	1.1684	1.2172	1.2369	1.2421
7	1.2	1.2579	1.2022	1.1592	1.2093	1.2276	1.2318
8	1.4	1.2449	1.1917	1.1488	1.2004	1.2173	1.2207
9	1.6	1.2307	1.1803	1.1378	1.1911	1.2067	1.2093
10	1.8	1.2168	1.1683	1.1264	1.1814	1.1958	1.1978
11	2.0	1.2031	1.1557	1.1148	1.1715	1.1846	1.1860
12	2.2	1.1890	1.1431	1.1031	1.1615	1.1732	1.1741
13	2.4	1.1747	1.1301	1.0917	1.1514	1.1616	1.1619
14	2.6	1.1603	1.1168	1.0807	1.1413	1.1498	1.1496
15	2.8	1.1463	1.1102	1.0696	1.1314	1.1371	1.1376
16	3.0	1.1317	1.1062	1.0674	1.1207	1.1270	1.1226
17	3.2	1.1250	1.1037	1.0700	1.1152	1.1247	1.1164
18	3.4	1.1268	1.1038	1.0756	1.1161	1.1296	1.1282
19	3.6	1.1281	1.1031	1.0818	1.1187	1.1332	1.1386
20	3.8	1.1286	1.1038	1.0877	1.1213	1.1406	1.1476
21	4.0	1.1288	1.1046	1.0930	1.1236	1.1490	1.1561
22	4.2	1.1282	1.1054	1.0977	1.1250	1.1556	1.1632
23	4.4	1.1271	1.1076	1.1017	1.1256	1.1613	1.1690
24	4.6	1.1254	1.1097	1.1050	1.1256	1.1656	1.1736
25	4.8	1.1230	1.1112	1.1078	1.1243	1.1684	1.1789
26	5.0	1.1202	1.1120	1.1098	1.1241	1.1712	1.1836
27	5.2	1.1165	1.1126	1.1117	1.1263	1.1743	1.1868
28	5.4	1.1127	1.1149	1.1148	1.1298	1.1759	1.1886
29	5.6	1.1143	1.1206	1.1184	1.1354	1.1774	1.1890
30	5.8	1.1192	1.1281	1.1224	1.1461	1.1827	1.1930
31	6.0	1.1259	1.1349	1.1319	1.1585	1.1913	1.2017
32	6.2	1.1334	1.1422	1.1468	1.1690	1.2002	1.2106
33	6.4	1.1400	1.1532	1.1605	1.1787	1.2075	1.2178
34	6.6	1.1460	1.1640	1.1735	1.1872	1.2133	1.2237
35	6.8	1.1507	1.1738	1.1857	1.1944	1.2176	1.2278
36	7.0	1.1559	1.1825	1.1967	1.2002	1.2202	1.2308
37	7.2	1.1619	1.1901	1.2064	1.2044	1.2209	1.2332
38	7.4	1.1668	1.1962	1.2146	1.2070	1.2197	1.2343
39	7.6	1.1721	1.2008	1.2212	1.2077	1.2164	1.2333
40	7.8	1.1764	1.2037	1.2258	1.2064	1.2110	1.2300
41	8.0	1.1791	1.2046	1.2283	1.2031	1.2032	1.2245
42	8.2	1.1803	1.2035	1.2286	1.1976	1.1932	1.2164
43	8.4	1.1798	1.2002	1.2264	1.1900	1.1810	1.2061
44	8.6	1.1775	1.1950	1.2221	1.1802	1.1653	1.1953
45	8.8	1.1736	1.1858	1.2137	1.1682	1.1561	1.1868
46	9.0	1.1679	1.1810	1.2098	1.1588	1.1497	1.1790
47	9.2	1.1633	1.1834	1.2134	1.1574	1.1417	1.1675
48	9.4	1.1666	1.1945	1.2267	1.1621	1.1419	1.1536
49	9.6	1.1776	1.2042	1.2386	1.1653	1.1444	1.1530
50	9.8	1.1922	1.2145	1.2515	1.1696	1.1470	1.1552
51	10.0	1.2054	1.2242	1.2646	1.1728	1.1490	1.1581
52	10.2	1.2182	1.2307	1.2748	1.1745	1.1501	1.1666
53	10.4	1.2301	1.2374	1.2862	1.1858	1.1521	1.1790
54	10.6	1.2407	1.2393	1.2963	1.1987	1.1597	1.1903
55	10.8	1.2507	1.2417	1.3060	1.2104	1.1690	1.1981
56	11.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

Table 2 - Continued

	Height [ft]	BU [MWD/MTU]					
		150 AO = -0.59	6000 AO = -2.31	13000 AO = -4.61	16000 AO = -0.38	20000 AO = 0.44	22000 AO = -0.64
57	11.2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
58	11.4	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
59	11.6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
60	11.8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[TOP] 61	12.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

* Linear extrapolation based on a line between 20,000 MWD/MTU and 22,000 MWD/MTU is adequate for addressing burnups beyond 22,000 MWD/MTU.

Table 3

$F^w_{Q(Z)}$ Penalty Factor

Cycle Burnup (MWD/MTU)	$F^w_{Q(Z)}$ Penalty Factor
15133	1.0200
15278	1.0209
15424	1.0200

$F^w_{Q(Z)} = 1.020$ for all burnups except those listed above. Linear interpolation is adequate for intermediate cycle burnups.

Figure 1

Reactor Core Safety Limits

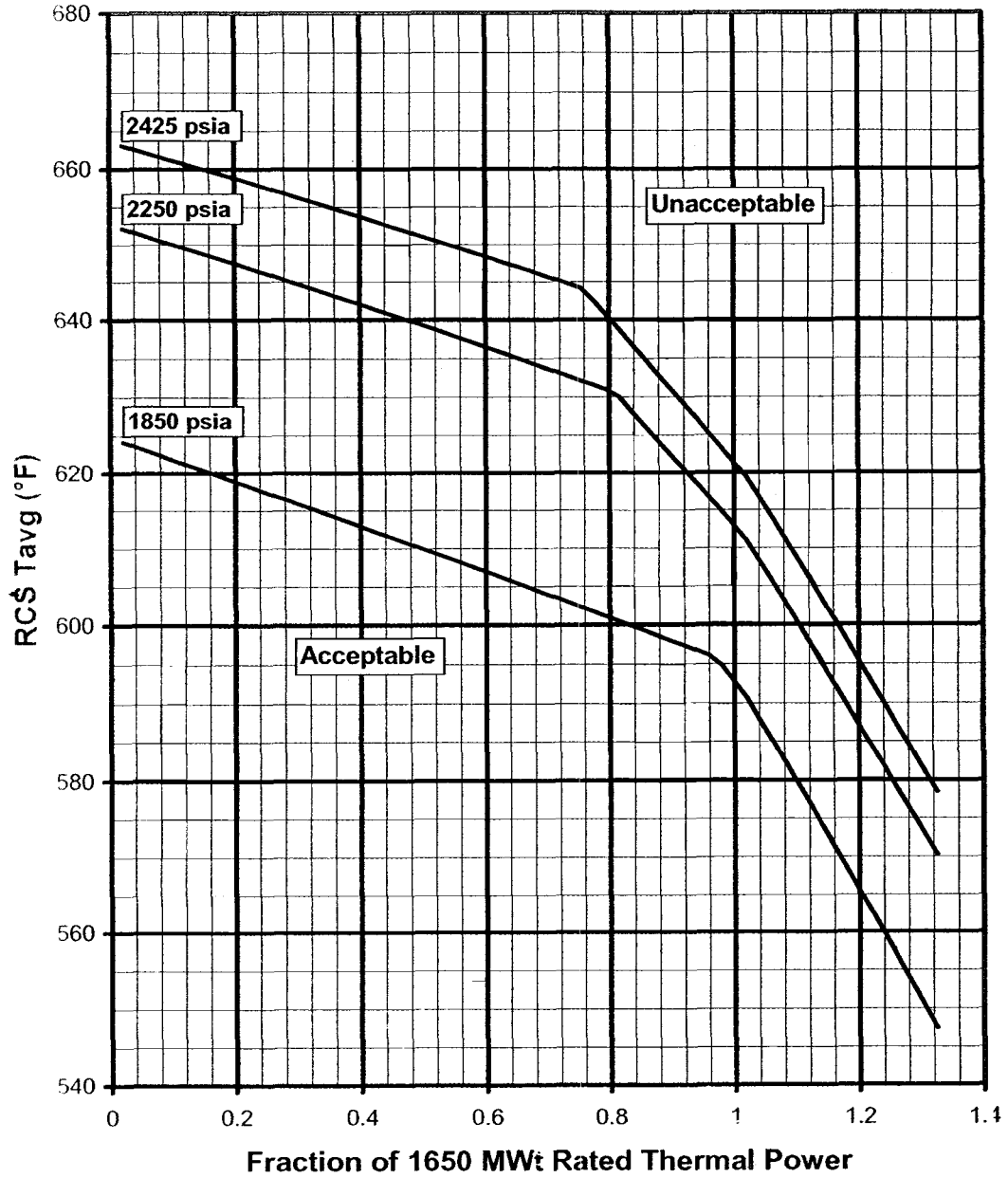
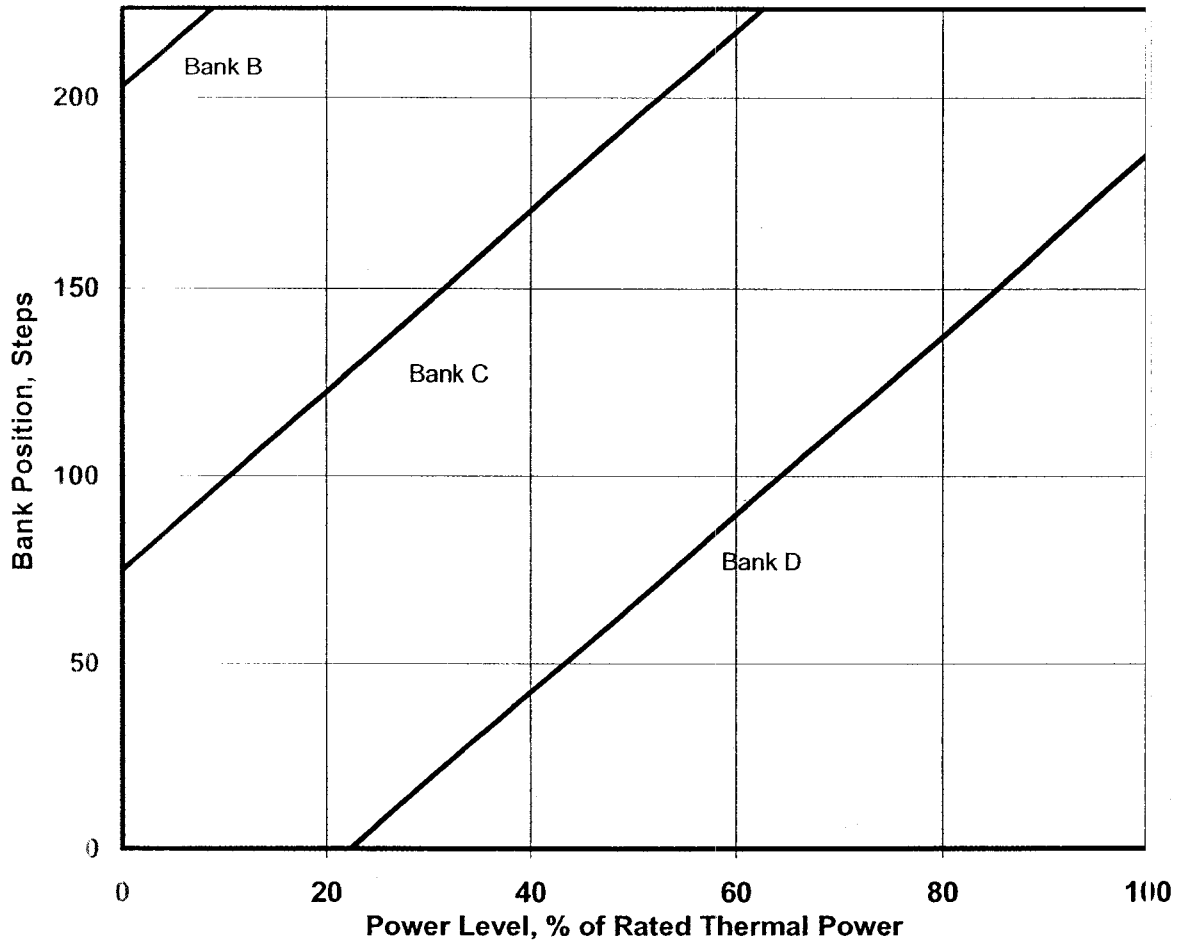


Figure 2
Rod Insertion Limit, 128 Step Tip-to-Tip

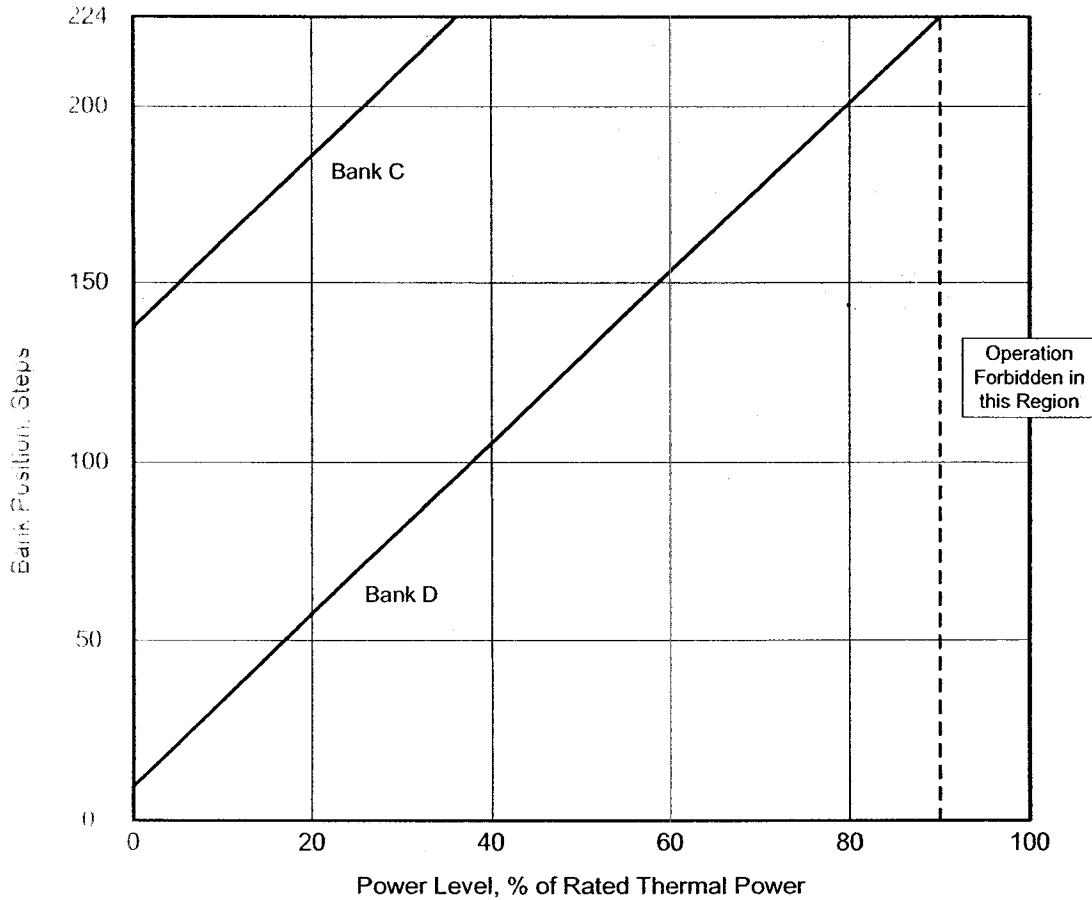


Bank Positions Given By:

- Bank D = $(150 / 63) * (P - 100) + 185$
- Bank C = $(150 / 63) * (P - 100) + 185 + 128$
- Bank B = $(150 / 63) * (P - 100) + 185 + 128 + 128$

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

Figure 3
Rod Insertion Limit, 128 Step Tip-to-Tip, One Bottomed Rod
(Technical Specification 3.1.4, Condition B)

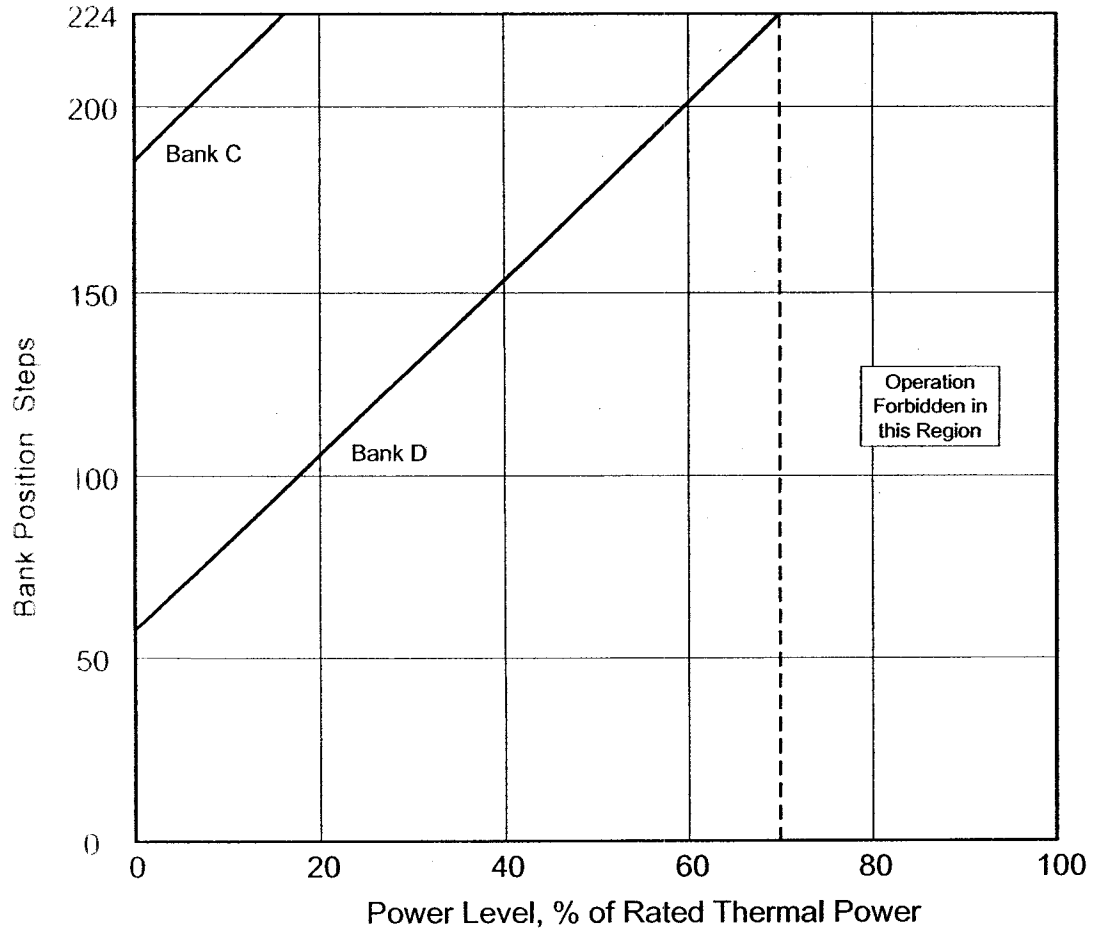


Bank Positions Given By:

- Bank D = $(150 / 63) * (P - 90) + 224$
- Bank C = $(150 / 63) * (P - 90) + 224 + 128$

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

Figure 4
Rod Insertion Limit, 128 Step Tip-to-Tip, One Inoperable Rod
(Technical Specification 3.1.4, Condition A)



Bank Positions Given By:

- Bank D = $(150 / 63) * (P - 70) + 224$
- Bank C = $(150 / 63) * (P - 70) + 224 + 128$

NOTE: The top of the active fuel height corresponds to 224 steps. The ARO parking position may be any position above 224 steps.

Figure 5
Flux Difference Operating Envelope

