2009 ANNUAL MONITORING REPORT / PERFORMANCE REVIEW FOR HOMESTAKE'S GRANTS PROJECT PURSUANT TO NRC LICENSE SUA-1471 AND DISCHARGE PLAN DP-200

FOR:

U.S. NUCLEAR REGULATORY COMMISSION AND NEW MEXICO ENVIRONMENT DEPARTMENT

BY:

HOMESTAKE MINING COMPANY OF CALIFORNIA GRANTS, NEW MEXICO

AND

HYDRO-ENGINEERING, LLC CASPER, WYOMING

MARCH, 2010

GEORGE L. HOFFMAN, P.E. 5831 N.M. HYDROLOGIST

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0 EXECUTIVE SUMMARY AND INTRODUCTION

1.1 EXECUTIVE SUMMARY

Homestake Mining Company of California manages a ground water restoration program as defined by Nuclear Regulatory Commission (NRC) License SUA-1471, and New Mexico Environment Department (NMED), DP-200 permit. The restoration program is a dynamic on-going strategy based on a restoration plan, which began in 1977, and is scheduled to be completed in 2015.

Homestake's long-term goal is to restore the ground water aquifer to levels as close as practicable to the up-gradient background levels. A ground water collection area (see shaded area on Figure 2.1-1, Page 2.1-11) has been established and is bounded by a down-gradient perimeter of injection/infiltration wells and trenches. Alluvial ground water that flows beneath the tailings enters this collection area. All ground water in the alluvial aquifer that is within the collection area is eventually captured by the collection well system. Once ground water quality restoration within the zone is complete and approved by the agencies, the site is to be transferred to the U.S. Department of Energy, which will have the responsibility for long-term site care and maintenance.

The data reported within this document represent the results of the monitoring program during 2009. This is a yearly reporting requirement. A similar report has been submitted to the agencies each year since 1983 (see list in Section 1.2).

The restoration program is designed to remove target contaminants from the ground water by flushing the alluvial aquifer with deep-well supplied fresh water or water produced from the reverse osmosis (R.O.) plant. A series of collection wells is used to collect the contaminated water, which is pumped to the R.O. plant for treatment or, alternatively, reported to the evaporation ponds.

Historically, the contaminants are found in two different aquifer systems. The aquifer system of primary concern is the alluvial system, which averages approximately 100 feet in depth, and extends generally north to south encompassing the San Mateo alluvial aquifer. In addition, a second aquifer system is found within the Chinle formation underlying the San Mateo alluvium. It is comprised of three separate aquifers designated as the Upper, Middle and Lower Chinle aquifers. The Hydro-Engineering 2003b report should be reviewed for details of the geologic setting and aquifer conditions on the site. The Upper and Middle Chinle aquifers subcrop beneath the alluvial system near the project site. Slight to moderately elevated concentrations of constituents of concern

have been observed in the Upper, Middle and Lower Chinle aquifers near their subcrops with the overlying alluvial system.

The restoration program, as described above, is made up of injection and collection well systems. R.O. product water, or fresh water pumped from deep wells, is injected in a series of wells or infiltration trenches arranged to form a continuous injection line across the site. The injection line creates a hydraulic barrier that results in containment of the contaminants within the collection area. The contaminated ground water is pumped and collected from a series of wells within the collection area. The collected aquifer water is pumped to the R.O. plant or to two large lined evaporation ponds for passive and forced (spray) evaporation.

In the years from 1977 to the present, the combination of injection wells and the upgradient collection system has gradually continued the withdrawal of the contaminated ground water plume up-gradient of the current hydraulic barrier which assists in aquifer restoration of ground water concentrations to or below background levels.

An average of 556 gallons per minute (gpm) was pumped into the alluvial fresh-water injection systems in 2009. An additional 75 gpm of fresh water was injected into the Upper and Middle Chinle aquifer systems. An average rate of 171 gpm of R.O. product water was injected into the alluvial aquifer in 2009, in addition to the fresh-water injection program. Production of significant quantities of R.O. product water started in July of 1999 with consistent operation during 2000 through 2009 except during equipment repair periods.

In 2009, the average collection rate for the alluvial aquifer was maintained at 251 gpm. An additional 45 gpm was pumped from the alluvial aquifer and re-injected within the collection area. The Upper Chinle aquifer collection program consisted of pumping wells CE2, CE5, CE6, CE11 and CE12 at an average rate of 122 gpm in 2009. The up-gradient alluvial aquifer collection system was estimated at 96 gpm in 2009, while average rates of 52 and 56 gpm were pumped from the Large Tailings Pile toe drains and in situ tailings pile dewatering, respectively.

The continuing evaluation of the performance of the Grants restoration system, including the 2009 results, shows that sulfate, TDS, chloride, uranium, selenium and molybdenum are still the key constituents of interest at this site. Successful restoration of ground water quality with respect to these key constituents will also accomplish restoration for other constituents. The monitoring program has shown that any low levels of nitrate, radium-226, radium-228, vanadium and thorium-230 are also reduced when the key constituents are restored in a particular area.

Data relating to key constituents currently being restored at the site have been reviewed and statistically evaluated to determine upgradient background water quality. These background water quality levels have been accepted by NRC, EPA and NMED; the NRC has set site standards based on the background water quality and accordingly amended the Radioactive Material license to reflect those standards. It should be noted that these site standards are utilized throughout this report for comparison purposes in discussing restoration progress.

Observed alluvial background concentrations of key constituents at the Grants site were similar to those in previous years. The only areas where sulfate, TDS and chloride concentrations exceed the alluvial site standard are small localized areas east of Valle Verde plus the large area in close proximity to the Large and Small Tailings Piles in the Grants Project area.

Uranium concentrations exceed the alluvial site standard of 0.16 mg/l within the collection area near the tailings. There are also four wells in Felice Acres and one well in Murray Acres subdivision that contain concentrations of uranium exceeding the site standard. Ground water withdrawal for irrigation is being used to further reduce uranium levels that exceed the standard in an area southwest of Felice Acres in Section 3 and in the western half of Section 27 and Section 28. Collection of water from one well in Murray Acres is being used to reduce uranium concentrations in that area.

Selenium concentrations also exceed the relevant site standard in the collection area near the Large Tailings Pile and southeast of the Small Tailings Pile. None of the sampled subdivision wells contained selenium concentrations above the site standard.

Molybdenum concentrations above the site standard of 0.1 mg/l are not present in the sampled subdivision wells. The wells exhibiting elevated molybdenum concentrations are all located near the Large and Small Tailings Piles, to the southeast of the Small Tailings Pile, and in an area in central Section 27. Migration of this constituent has been limited due to natural retardation within the alluvial aquifer.

Nitrate concentrations are compared to the alluvial site standard of 12 mg/l. Areas to the west of the Large Tailings Pile contain higher nitrate concentrations above the site standard, but these levels are likely natural given their location. Nitrate concentrations in the area of the Large and

Small Tailings Piles and to the east are likely caused by tailings seepage. A small area southeast of Valle Verde area exceeds the nitrate alluvial site standard. Water quality with respect to this constituent should easily be remediated through the ongoing restoration program.

All radium values in the alluvial aquifer outside of the tailings perimeter were less than the site standard. This demonstrates that radium is only a constituent of concern under the Large Tailings Pile.

None of the vanadium concentrations measured in 2009 exceeded the alluvial site standard. Concentrations of this constituent have been adequately restored to below the site standard except for levels immediately under the Large Tailings Pile.

Thorium levels observed in 2009 were less than the site standard except levels in the alluvium immediately under the Large Tailings Pile. The mobility of this constituent has been very limited and is found in close proximity to the tailings. However, the analytical results for this constituent vary significantly at the low observed levels that are approaching laboratory detection limits. Slightly higher values should not be given any significance until they are supported by additional monitoring. The monitoring records for thorium indicate that it is a minor constituent of concern at the Grants site.

Fresh-water injection into Upper Chinle well CW13, east of the East Fault, continued in 2009. This injection has maintained higher water levels in the Upper Chinle aquifer east of the East Fault which in turn has allowed continued operation of the nearby Upper Chinle collection wells.

Fresh-water injection continued in 2009 in Upper Chinle well CW5 just north of Broadview Acres and also in Upper Chinle wells CW4R and CW25. This injection has resulted in gradient reversal within the Upper Chinle, thereby forcing ground water from this area back to the north toward the tailings piles. Collection from Upper Chinle well CE2 was initiated in 1999 and continued through 2009. Collection in Upper Chinle wells CE5, CE6, CE11 and CE12 was started in 2006. This collection is used in conjunction with injection wells CW4R, CW5 and CW25 to restore ground water quality in this area. Injection into well CW25 was started in 2000 and continued through 2009.

All sulfate, chloride and TDS concentrations in the Upper Chinle aquifer are below the site standards except for samples from wells CE7 and CE13. Therefore, the Upper Chinle aquifer

only requires restoration with respect to TDS, chloride and sulfate in a localized area near the Large Tailings Pile.

Uranium concentrations in eleven Upper Chinle wells exceeded the Upper Chinle site standard in 2009. Restoration of these elevated values should result from CE2, CE5, CE6, CE11 and CE12 well collection and the CW4R, CW5 and CW25 well injection efforts.

Selenium concentrations in the Upper Chinle aquifer exceed the site standard in five wells in the mixing zone. The site standards for selenium for the Upper Chinle mixing zone and the Upper Chinle non-mixing zone are 0.14 and 0.06 mg/l, respectively.

The concentrations of molybdenum exceeded the site standard in four wells near the tailings in the Upper Chinle aquifer and six more to the south of the Collection Ponds during 2009. Restoration for these locations should occur from continued CE2, CE5, CE6, CE11 and CE12 well collection and CW4R, CW5 and CW25 well injection activities.

All nitrate concentrations observed in 2009 for the Upper Chinle mixing zone were less than the nitrate site standard. This indicates that nitrate is not a constituent of concern in this aquifer.

None of the Upper Chinle wells contain a radium-226 plus radium-228 value above 5 pCi/l. Two wells near the Large Tailings Pile exceeded the site standard for vanadium concentrations from the 2009 sampling in the Upper Chinle aquifer. The highest measured thorium-230 concentration near the Large Tailings Pile in the Upper Chinle aquifer wells during 2009 was 0.2 pCi/l at well CE13. This is consistent with the low observed concentrations in the overlying alluvial aquifer.

The direction and rate of ground water flow in the Middle Chinle aquifer in 2009 is very similar to that of past years. Fresh-water injection into well CW14 started in December of 1997. Fresh-water injection into wells CW30 and CW46 started in 2004. The fresh water is building up a mound of ground water in this area, which will result in a reversal of the flow of Middle Chinle water back toward the alluvial subcrop. Wells 493, 498, CW44 and CW45 are being used for irrigation supply, which will increase the flow in the Middle Chinle aquifer from Broadview and Felice Acres to the south. Additionally, well CW28 was added as a supply well for fresh-water injection in 2002 but had not been used for the last few years but was used in 2009.

Water quality in the Middle Chinle aquifer is generally good. All sulfate concentrations are less than the site standards except for exceedance in the mixing zone area at wells CW24 and

WR25. All TDS concentrations in the Middle Chinle aquifer are less than the standards except for two TDS values in Felice Acres that are slightly above the non-mixing zone background value and one TDS value in a well west of the West Fault. None of the chloride concentrations exceed the Middle Chinle site standard. Uranium concentrations in the western portion of Felice Acres are above site standards due to the alluvial recharge to the Middle Chinle aquifer just south of Felice Acres. Continued irrigation use of this water by Homestake will reduce these elevated concentrations in western Felice Acres. The uranium background is also exceeded in well CW1 north of the LTP and wells CW17, CW35 and WR25 west of the West Fault. The non-mixing zone selenium site standard is slightly exceeded in well CW28 which is located east of the East Fault and also well 493 in Broadview and Felice Acres. Uranium site standards of 0.18 and 0.07 mg/l, respectively, were set for the mixing and non-mixing zones in the Middle Chinle aquifer, while selenium site standards are 0.14 and 0.07 mg/l. Molybdenum concentration in well CW17 is the only Middle Chinle value above the mixing zone standard of 0.10 mg/l.

Nitrate, radium, vanadium and thorium-230 concentrations in the Middle Chinle aquifer are at less than significant levels for each of the constituents except for the nitrate level in well CW17. Hence, uranium and selenium are considered the important constituents relative to restoration needs for the Middle Chinle aquifer system.

Concentrations of major constituents in the Lower Chinle aquifer generally increase in the down-gradient direction due to the slow movement of water in the fractured shale. All sulfate, TDS and chloride concentrations are less than the site standards except in far-down-gradient areas, where natural concentrations exceed the non-mixing zone site standard. These exceedances result because there is only limited background data for the far-down-gradient areas of the Lower Chinle aquifer, and there is a naturally occurring deterioration of Lower Chinle water quality in the down-gradient direction. The uranium site standard in the Lower Chinle aquifer is exceeded in six wells. The three wells where concentrations exceed the mixing zone site standard of 0.18 mg/l are located near the subcrop of the Lower Chinle aquifer with the alluvial aquifer. Concentrations in three non-mixing zone wells exceed the site standard of 0.03 mg/l.

Concentrations of selenium do not exceed the standards in the two zones for the Lower Chinle aquifer. All molybdenum concentrations in the Lower Chinle aquifer are less than the site standard. None of the Lower Chinle nitrate concentrations exist at a significant level. All radium, vanadium and thorium-230 concentrations in the Lower Chinle aquifer in 2009 were at low levels for these constituents.

1.2 INTRODUCTION

This report, as required by the New Mexico Environment Department (NMED) discharge plan DP-200 and the Nuclear Regulatory Commission (NRC) License SUA-1471, presents results of the 2009 annual ground water monitoring program at Homestake's Grants Project. Homestake Mining Company (HMC) conducted uranium milling operations five miles northeast of Milan, New Mexico from 1958 to 1990 (see Figure 1.2-1). Referred to as the Grants Project or Grants site, HMC deposited uranium tailings from the alkaline (high pH) Grants mills into two unlined piles (Large and Small Tailings Piles) that overlie San Mateo alluvium. The San Mateo alluvium is simply referred to as the alluvium or alluvial aquifer in this report. In 1977, due to initial concerns about ground water selenium levels, HMC installed a system of wells and pumps in order to inject fresh water into the alluvium at the property boundary and to withdraw contaminated water from the alluvium near the tailings.

Previous monitoring reports have been published in quarterly, semi-annual and annual reports¹, which were presented to the NMED and the NRC.

Four subdivisions, Broadview Acres, Murray Acres, Felice Acres and Pleasant Valley Estates, are adjacent to the HMC site. These subdivisions are shown on many of the various report figures found in this report.

Monitoring data for ground water west of the project site is included in the 1995 through 2009 reports (see Appendix A for water levels and Appendix B for water quality). This area has been designated the "West Area" and was so labeled on the figures in the annual reports prior to 2003. The 2003 through 2009 annual reports combine the project site and West Area figures on one 11 x 17 inch set of figures.

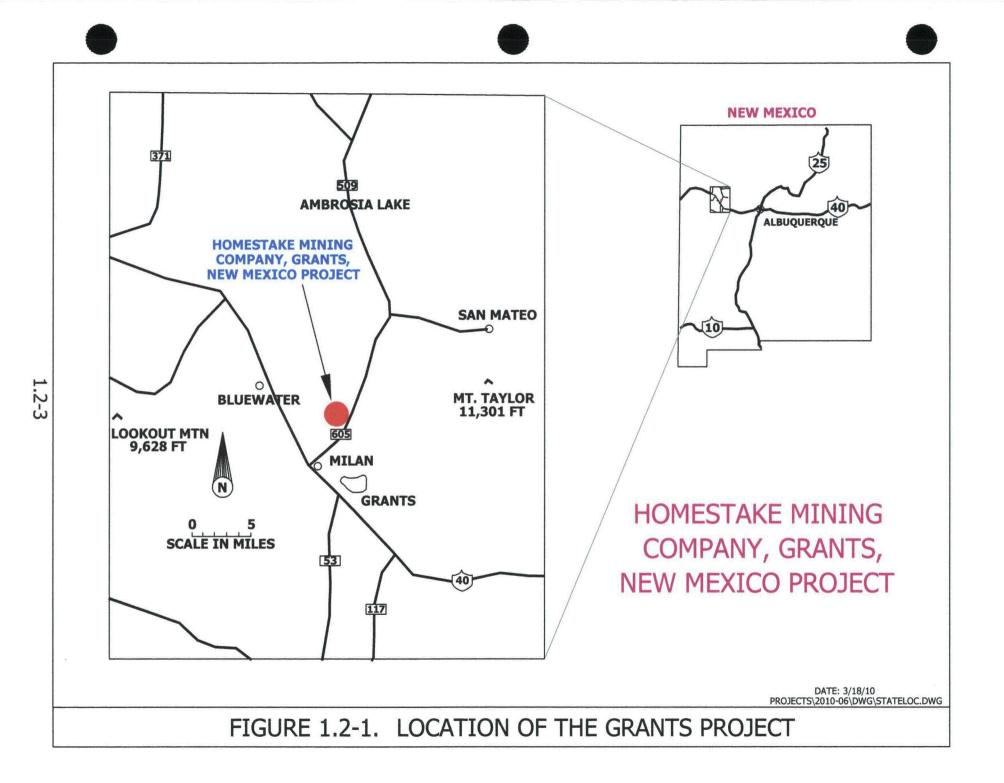
The annual ALARA audit, required as an NRC license condition, is presented in Appendix C. Additionally, a report of an annual inspection of the tailings piles and pond dikes must be submitted per license condition and is presented in Appendix D. Appendix E provides an annual land-use survey discussion for the immediate Grants site area; this was an added license condition beginning in 2002. The annual radon flux survey report for the Large and Small Tailings Piles is

¹ See Hydro-Engineering 1983b, 1983c, 1984a, 1984b, 1984c, 1985a, 1985b, 1985c, 1985d, 1986a, 1986b, 1986c, 1987a, 1987b, 1988a, 1988b, 1990, 1991, 1992, 1993a, 1994, 1995, 1996, 1997, 1998, 1999, 2000a, 2001a, 2002, 2003a, 2004, 2005, 2006, 2007, 2008 and 2009.

presented in Appendix F of this report.

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2.0 OPERATIONS

2.1 CURRENT OPERATIONS SUMMARY

The annual precipitation of 8.8 inches on site in 2009 is below the normal precipitation for Grants, New Mexico. These below normal conditions in an extended drought have resulted in a continuing natural decline in water levels regionally and at the Grants site.

The Grants Project ground water remediation system consists of collection of contaminated ground water near the tailings piles and down-gradient injection of fresh water and R.O. product water. These collection and injection systems continued to operate in 2009, along with the reverse osmosis (R.O.) plant, which is used to treat and manage the majority of collected ground water. The R.O. plant produces product water that is of much better quality than the natural alluvial water, and it is used as injection water in some areas of the Grants Project restoration program. Figure 2.1-1 on page 2.1-11 shows the location of the present (end of 2009) injection and collection systems along with their starting dates of operation. Water collected from the site is pumped to the R.O. plant or discharged into lined collection ponds or one of two lined evaporation ponds (light blue areas).

The area where ground water flow is controlled by the fresh-water injection and collection systems is called the "Collection Area" and is shown by the yellow cross-hatched pattern on Figure 2.1-1. All of the alluvial ground water within the collection area converges to the collection wells.

2.1.1 R.O. PLANT

The R.O. plant utilizes a lime/caustic pre-treatment and clarification unit. Blowdown (sludge) from the pre-treatment unit discharges to the West Collection Pond with the treated water feeding the two 300 gpm low-pressure R.O. units. The brine from the No. 1 low-pressure unit feeds a 75-gpm high-pressure R.O. unit. The No. 2 R.O. unit is a single stage, low pressure 300 gpm system. The R.O. product water from the two units is discharged to a series of injection wells. The brine from the R.O. plant is discharged to the evaporation ponds. Other miscellaneous flows and blowdown from the R.O. plant are pumped to the West Collection Pond for recycle to the R.O. plant.

The R.O. plant inputs and output of R.O. product water for injection are listed in the following tabulation:

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	R.O. I	Plant Performance (GPN	M)		
Year	In	(2000-2009) put	Output		
	Collection Wells	Tailings Collection	R.O. Injection	Brine and Blowdowr	
2000	274	0.	204	70	
2001	276	5	222	59	
2002	383	5	288	100	
2003	338	4	266	76	
2004	293	12.2	249	64	
2005	250	6.4	198	49	
2006	257	2.1	184	48	
2007	262	0.0	204	55	
2008	264	3.1	194	60	
2009	251	0.3	171	60	

Aquifer restoration results continue to show that the R.O. product water injection is much more effective than the fresh water in reducing the uranium and molybdenum concentrations within the alluvial aquifer.

2.1.2 COLLECTION

The 2009 alluvial aquifer collection rate was very similar to the 2008 rate. In general, the R.O. plant was operated on a single unit 300 gpm basis during 2009; each of the two R.O. units were operated alternatively to allow single unit operation while the other unit was on a backwash cleaning cycle.

Up-gradient alluvial aquifer collection continues north of County Road 63. Wells P2, P3 and P4 were used to collect upgradient alluvial aquifer water (brown triangle symbol on Figure 2.1-1) for transfer to the drainage system farther west until April 6, 2009 and then pumped as a source to the

tailings flushing program for the remainder of the year. This collection well reduces the quantity of alluvial water flowing into the tailings area. Upper Chinle aquifer collection continued from wells CE2, CE5, CE6, CE11 and CE12 in 2009 (gold X symbols located south of the collection ponds), and this water was used as injection supply water for the Large Tailings Pile (LTP) flushing program described later in Section 2.1.5.

2.1.2.1 ALLUVIAL AQUIFER

Figure 2.1-1 shows the locations of five lines of alluvial aquifer collection wells (red x symbols). The S and D-lines are adjacent to the Large Tailings Pile and the K and C-lines are adjacent to the Small Tailings Pile. No new wells were added to the alluvial collection system in 2009. The L-line south of the Small Tailings Pile continued to operate in 2009 and includes collection wells 521, 522 and 639 which are located on the east side of Highway 605 (see Figure 4.1-1 for location). Alluvial water is pumped from these lines of collection wells to the R.O. plant or, depending on water quality, it is pumped to re-injection wells. Figure 2.1-2 on page 2.1-12 graphically presents collection rates for the last ten years at the Grants Project. The alluvial collection system operated at an average rate of 251 gpm in 2009. Additionally, an average of 45 gpm was extracted from the alluvium for re-injection in 2009.

2.1.2.2 UP-GRADIENT ALLUVIAL WATER

Collection of alluvial water up-gradient of the tailings piles started in January of 1993 and continued through 2009. Wells P2, P3 and P4 were pumped in 2009 (see Figure 2.1-1). This upgradient water was transferred to the next drainage channel to the west until April 9, 2009 when this pumping was switched to the supply for tailings flushing. The pumping of this up-gradient water prevents some of the alluvial water from entering the Grants Project area at the north side of the Large Tailings Pile and helps maintain the gradient reversal. The collection rate for this effort averaged 96 gpm during 2009 (see Figure 2.1-2). Monthly rates were not measured for the up-gradient wells, and therefore only the yearly average is presented for 2001 through 2009 on Figure 2.1-2.

2.1.2.3 UPPER CHINLE AQUIFER

Figure 2.1-2 shows the collection rate for Upper Chinle collection wells CE2, CE5, CE6, CE11 and CE12, which are located on the south side of the collection ponds. Collection from Upper Chinle well CE2 started in 1999 and is expected to continue for several years. Collection from wells CE5 and CE6 started in August 2006 while pumping from wells CE11 and CE12 was initiated in October of 2006. These wells were used to supply water to the Large Tailings Pile for the tailings flushing program during 2009. The yearly average collection rate from the Upper Chinle was 122 gpm.

2.1.2.4 QUANTITY OF CONSTITUENTS COLLECTED FROM THE ALLUVIAL AQUIFER

Table 2.1-1 (page 2.1-17) presents the quantities of chemical constituents extracted from the ground water system, the tailings piles and the toe drains. The ground water collection system has produced an average pumping rate of 259 gpm for the entire period between 1978 and 2009. The portion of the collection water that has been re-injected into the alluvial aquifer is not included in the values in Table 2.1-1. The quantity of constituents removed in 2009 was computed by multiplying the average concentration of a particular constituent for each source of water (ground water, toe drains and tails collection) by the volume of water pumped for each that year.

2.1.3 INJECTION

The fresh-water and R.O. injection systems, which aid in the reversal of the ground water gradients back toward the collection wells, consist of lines of injection wells, which are oriented generally along the east, south and west perimeter of the two tailings piles and evaporation pond complex (see green and blue circles on Figure 2.1-1).

In 2003, approximately 2100 feet of four-inch corrugated slotted polyethylene pipe was installed at a depth of approximately 6 feet below land surface west of the Large Tailings Pile to serve as a horizontal injection line (see green line on Figure 2.1-1). A filter sock was placed over the pipe thus negating the need for a sandpack. Water is currently being injected into this injection line (S injection line) at three locations. The 2009 injection rate for this horizontal injection line is included in the Broadview and Murray Acres injection rates, and was approximately 128 gpm for the year.

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In July 2004, two 250 foot sections of injection line (EBA1 and EBA2) were added south of collection well 522 east of Highway 605 (see Figure 2.1-1 for location). The average injection rate for these two lines is estimated at 20 gpm and is included in the Broadview and Murray Acres injection rate.

A 400-foot extension to the S injection line was added on the north end of this line in 2005. Five EMA injection lines were added southwest of the Large Tailings while three ETA injection lines were added east of the Large Tailings in 2005 (see Figure 2.1-1).

2.1.3.1 BROADVIEW AND MURRAY ACRES

The Broadview Acres injection system started in 1977 with the G line on the north side of this subdivision. Injection into the majority of the G-line wells was discontinued in mid-April of 2000 in order to supply more water to injection wells near the collection area. The J-line, wells X1 through X10, and wells X28 through X31 are also considered part of the Broadview Acres injection system. Fresh water was injected into wells X13 through X27, 1A and 1E in 2009. Alluvial fresh-water injection wells 523 and 524 were added to the Broadview Acres injection system in 2002 (see Figure 4.1-1).

All wells adjacent to the northeast corner and to the north and east of Murray Acres are included in the Murray Acres injection system. This system includes all of the M and WR series injection wells. The M line of the Murray Acres injection system was initially used in 1983. Injection into the M-line west of well WR1R was discontinued at the end of September of 2000, and injection into the WR-line, north of WR10, began at this time. The horizontal injection line, west of the Large Tailings Pile, (S. Inj. Line) was added to this system on August 25, 2003. Fresh-water injection into lines ETA1, ETA2 and ETA3 started in July of 2005 while injection into EMA1 with fresh water started in December, 2005.

Figure 2.1-3 (page 2.1-14) presents fresh-water injection rates for the last nine years. An average of 556 gpm, or a total of 291 million gallons, was injected during 2009.

2.1.3.2 R.O. PRODUCT

The R.O. product water injection system supplies water to the X wells to the south and east of the Small Tailings Pile. Until October, 2005, R.O. product water was discharged into the X line and

injected into wells X1 through X10, X28 through X31 and into wells K2, K6, KA through KE, KM, KN, C4, C13, C5, C3R and PM. Fresh-water injection was commenced after that date for these wells. R.O. product was switched to injection lines EMA2 through EMA5 in October 2005. Figure 2.1-3 shows the rates of R.O. product water injection, which averaged 171 gpm in 2009 for a total of 90 million gallons.

2.1.3.3 UPPER CHINLE AQUIFER

Hydro-Engineering 2003b should be reviewed for a detail discussion of the geologic setting for the Chinle aquifers. From 1984 through early 1995, the Upper Chinle injection system consisted of injecting fresh water into Upper Chinle well CW5, located on the north side of Broadview Acres. This effort restored most of the area in the Upper Chinle aquifer between the two faults. Injection into well CW5 was resumed in April of 1997 and continues at present to complete the restoration of this aquifer.

In order to maintain head in the Upper Chinle aquifer east of the East Fault, injection of fresh water into well CW13, an Upper Chinle well, was begun in June, 1996. Injection into Upper Chinle well CW25, located on the western edge of the Upper Chinle outcrop east of Murray Acres, began in 2000. Injection into CW25 will increase the head in the Upper Chinle aquifer and force flow in the Upper Chinle back toward collection well CE2. Injection into Upper Chinle well 944 started in June of 2002, and injection into well CW4R started in 2003. The red squares on Figure 2.1-3 present monthly average injection rates into Upper Chinle wells 944, CW4R, CW5, CW13 and CW25, with an overall 2009 average of 55 gpm.

2.1.3.4 MIDDLE CHINLE AQUIFER

Injection of San Andres fresh water into Middle Chinle well CW14 was started in December of 1997. This injection was initiated to prevent northward movement of alluvial water that recharges the Middle Chinle on the south side of Felice Acres. The injection rate averaged 20 gpm in 2009 (see Figure 2.1-3). This injection has prevented the movement of constituents further to the north and allows up-gradient collection from wells 482, 483, 493, 498, CW44 and CW45.

2.1.3.5 SECTIONS 28 AND 29

A test of fresh-water injection was initiated in late 1999 and continued through January of 2000 by pumping San Andres well 951, which is located in Section 20, (see Figure 2.1-1 for location of supply well 951). This water was subsequently injected into alluvial wells 682, 656, 894, 633 and 655 (see Figure 4.1-1 for location). This fresh-water injection in Sections 28 and 29 was resumed in March of 2002 to impede movement of ground water with modest contaminant concentrations in Section 28 until ongoing irrigation water extraction can reduce these low concentrations. Eight injection lines were added in 2005 in Sections 27 and 28 to replace the injection wells and adjust the location of this injection. Injection into lines NPV1 through NPV5 (5 of the 8 injection lines) was started on July 27, 2005 while injection into NPV6 was started in December 2005. This injection rate averaged 333 gpm for 2009 with a total injected volume of 174 million gallons. Figure 2.1-3 presents the monthly injection rates into wells and injection lines located in Sections 28 and 29.

2.1.3.6 SECTIONS 35 AND 3

Fresh-water injection in the southwestern quarter of Section 35 was initiated in late 2002 utilizing production from Upper Chinle well CW18 and Middle Chinle well CW28. This water was injected into alluvial wells 641, 642, 848 and 868 (see Figure 4.1-1 for location).

Fresh-water injection into alluvial wells 643, 863, 865 and 866, located in the northeast portion of Section 3 was initiated in 2003. Injection into Middle Chinle wells CW30 and CW46 was added to this program in 2004 (see Figure 2.1-1). Seven injection lines in Section 3 and two injection lines in Felice Acres were also added in 2004. Two additional injection lines, FA1 in central Felice Acres and WFA1 west of Felice Acres, were added in 2005. These injection wells and lines were supplied with water by San Andres well 943 in 2009 while well CW28 supplied injection water for wells 848 and 868.

Figure 2.1-3 presents the combined monthly injection rates for Sections 34, 35 and 3 fresh-water injection lines and wells (see brown diamond symbols on Figure 2.1-3). This injection effort is associated with the ground water restoration of the Sections 3 and 35 areas. Water collected from wells in Section 3 and 35 is used for the irrigation program. During 2009, the yearly average injection rate in Sections 34, 35 and 3 was 225 gpm.

2.1.4 **RE-INJECTION**

Alluvial water containing relatively low concentrations of contaminants is collected and is then injected into areas of the alluvial aquifer near the Large Tailings Pile with higher concentrations of contaminants in order to enhance restoration in this area. This aspect of the restoration plan at the Grants sites is referred to as the collection for re-injection program. The lower-concentration water will be as effective (see sulfate, uranium, selenium and molybdenum concentrations in plots for wells T and TA – see report Sec. 4.3) as fresh water during the initial stages of restoration, and therefore, re-injection is a beneficial use of this slightly contaminated ground water. Water collected from the L-line to the south of the Small Tailings Pile and wells 521, 522 and 639 was used for re-injection into the alluvial aquifer and tailings in 2009. The total collection for re-injection rate in 2009 averaged 45 gpm. Re-injection into alluvial wells X11, X12, D2 through D4, DAA, DAB, DL, DW, DY, DF, DG and DX was roughly 91 percent of the rate or 41 gpm. The monthly re-injection rates are depicted on Figure 2.1-2 as collection for re-injection use (COL/RE-INJ). Some of the collection for re-injection water was re-injected into the Large Tailings Pile wells in 2009. Approximately 9 percent of the yearly average is estimated to have been injected into the tailings.

2.1.5 TAILINGS CONDITIONS

Tailings wells were installed in the Large Tailings Pile beginning in 1994, and wells have been periodically added through 2009. Six additional tailings injection wells were drilled in 2009 and no additional monitoring wells. Eleven additional or replacement 5 inch dewatering well was also drilled in 2009. Data collected from these wells has been used to estimate the amount of drainable water in the re-contoured, stabilized tailings. The tailings wells are also a primary component of the tailings dewatering program. With the exception of some testing of dewatering options in 1999, no dewatering of the tailings occurred in 1998 and 1999 due to limited available capacity in the evaporation ponds. The complete dewatering program was restarted in 2000 and operated through mid-April 2002. Dewatering rates were reduced through the remainder of 2002 and 2003 due to limited available storage in the evaporation ponds. The dewatering wells were operated near capacity starting in April of 2004 and throughout 2005 and 2006. Dewatering rates were restricted in 2007, 2008 and 2009 due to limited available storage in the evaporation ponds.

Figure 2.1-4 (page 2.1-14) shows the locations of tailings wells that were available for pumping in 2009. The cumulative volume of tailings water pumped from 1995 through 2009 is presented on Figure 2.1-5. A total volume of 301 million gallons of water had been removed from the tailings via dewatering wells by the end of 2009. Of that total, 29 million gallons were pumped from the tailings in 2009. The yearly average collection rate from the tailings wells was 56.1 gpm in 2009.

Wells CE2, CE5, CE6, CE11, CE12, CW1, CW2, P2, P3 and P4 have been used to supply water for flushing the Large Tailings Pile in 2009. A total of 147 million gallons were injected into the tailings in 2009 from these wells, which is an average rate of 280 gpm. Additionally, 4 gpm of the alluvial collection for re-injection was injected into the tailings for a total tailings injection rate of 284 gpm. This injection for tailings flushing allows larger extraction rates from the tailings dewatering wells and reduces contaminant concentrations in the tailings.

Table 2.1-1 presents the quantity of constituents collected from the tailings wells since dewatering began in 1995. Tables B.1-1 and B.1-2 of Appendix B present chemical analyses of tailings well water during 2009.

2.1.6 TOE DRAIN CONDITIONS

A series of toe drains have been installed around the Large Tailings Pile to intercept perched ground water seeping from the tailings into the alluvium. The locations of the toe drains and their associated sumps are shown on Figure 2.1-4. Nine sumps are located around the perimeter of the Large Tailings Pile that are utilized for collection of toe seepage. Two of these sumps are tied to the old tailings decant towers (East and West reclaim sumps).

Figure 2.1-5 shows that 320 million gallons of water have been pumped from the toe drains. Approximately 52 gpm of water was collected from the toe drains in 2009, which is slightly greater than the 2008 rate. This increase in rate is due to the less dewatering from tailings, which offsets the injection of water in the tailings.

Table 2.1-1 also presents the 2009 quantity of constituents collected from the toe drains (see Tables B.2-1 and B.2-2 of Appendix B for toe drain sump water-quality results for 2009).

2.1.7 LINED EVAPORATION PONDS

The use of lined evaporation collection ponds (East Collection Pond and West Collection Pond) began in October of 1986 when the two ponds were constructed. The No. 1 Large Evaporation Pond, located on the Small Tailings Pile, began receiving water in November of 1990. Usage of the No. 2 Large Evaporation Pond began in March of 1996.

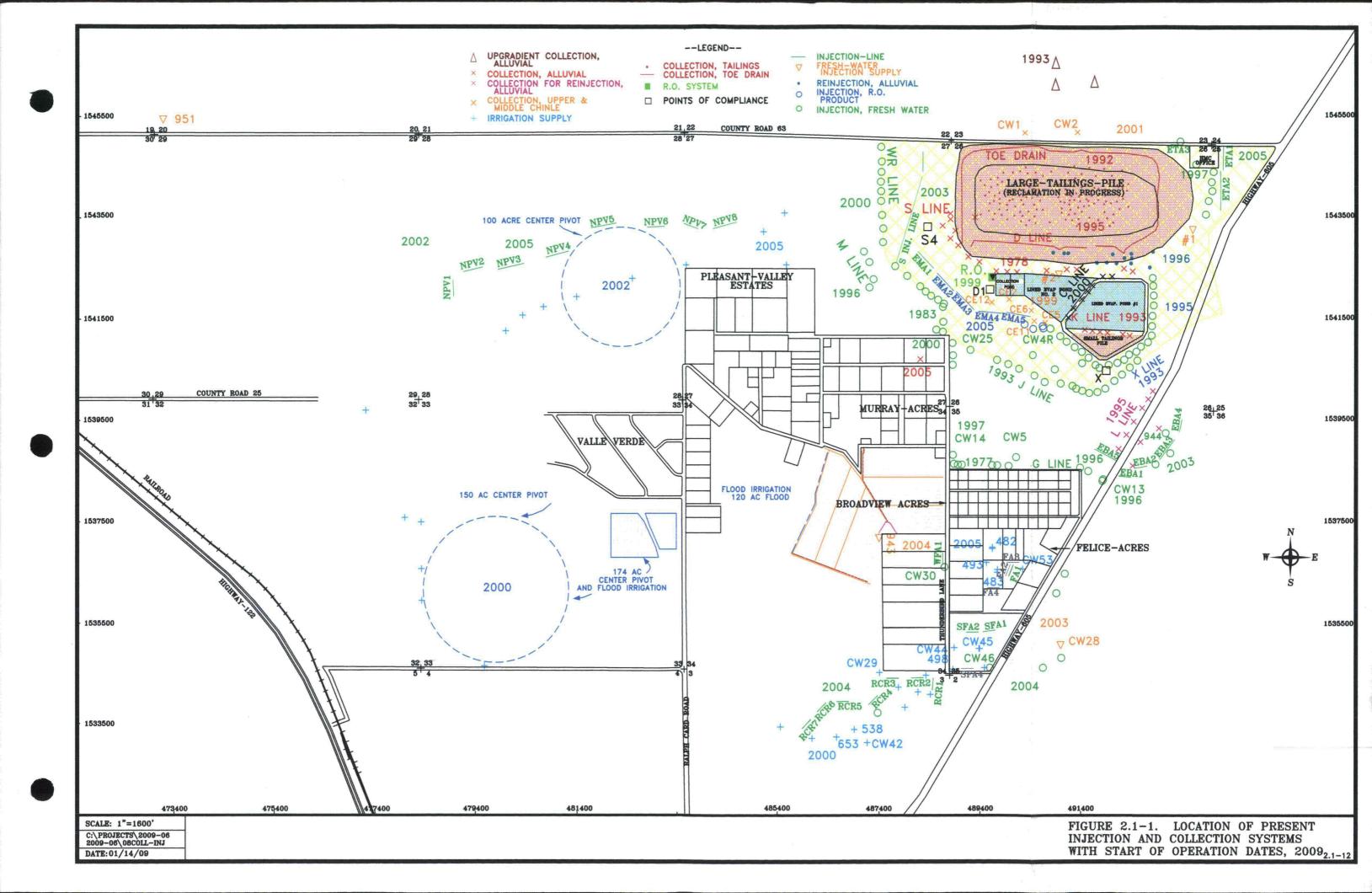
The water from the well collection system and some water from the tailings dewatering wells and toe drains is pumped to the R.O. plant as feed water. The majority of the extracted tailings water is reported directly to the No. 2 Evaporation Pond for subsequent evaporation. Excess water is transferred from the East Collection Pond to the No. 2 Evaporation Pond. When necessary, water is transferred from the No. 2 Evaporation Pond to the No. 1 Evaporation Pond. This transfer is mainly through the turbo mister evaporation spray system. Both ponds use spray systems to enhance evaporation. A total of 90 million gallons (average rate of 171 gpm) of water was delivered to the evaporation pond system in 2009 in addition to the 11 million gallons (average rate of 21 gpm) of precipitation added to the pond. The net evaporation from the evaporation system averaged 152 gpm in 2009, compared to 169 gpm in 2008.

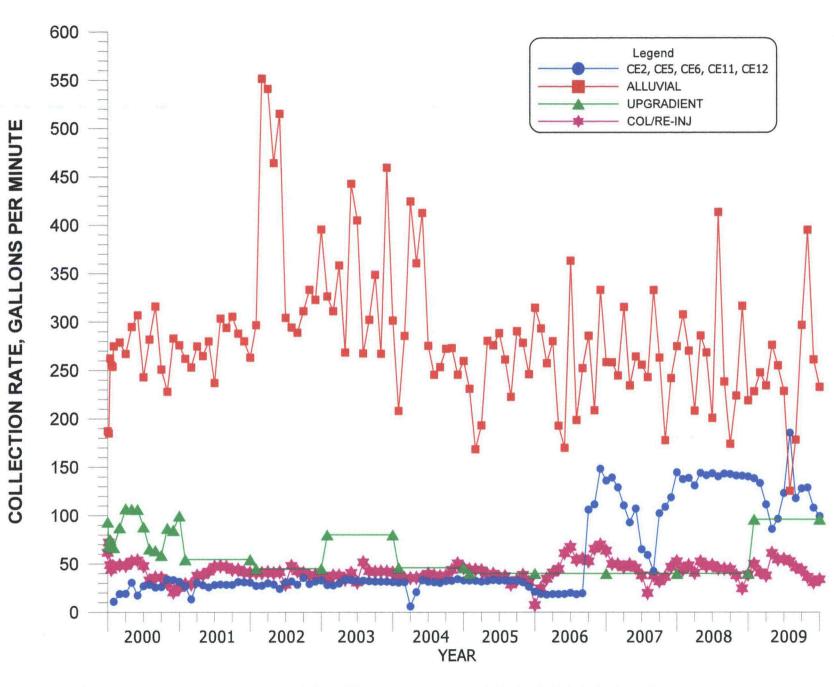
Water quality samples results collected from the No. 1 and No. 2 Large Evaporation Ponds, the East Collection Pond (E COLL POND), and the West Collection Pond (W COLL POND) are presented in Tables B.3-1 and B.3-2 of Appendix B.

2.1.8 IRRIGATION

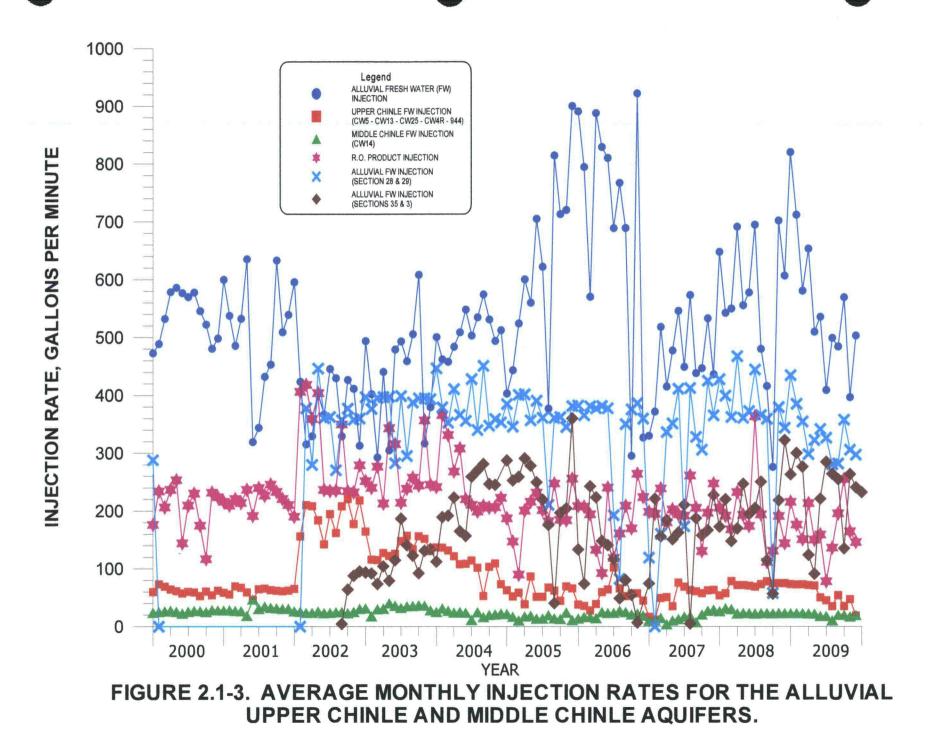
Four irrigation systems were operated in 2009 (see Figure 2.1-1 for locations). The 150-acre center pivot in the southwest quarter of Section 33 and 120 acres of flood irrigation in the eastern half of Section 34 were used for the eighth full irrigation season; the 100 acre center pivot in Section 28 was operated for the sixth irrigation season. The 24 acre flood irrigation in the eastern portion of Section 33 was operated in 2009. Figure 4.1-1 shows the supply wells for these irrigated areas. In 2009, wells 482, 483, 490, 491, 493, 496, 498, 538, 540, 541, 631, 632, 647, 649, 653, 657, 658, 862, 863, 865, 866, 996, CW29, CW42, CW44, CW45 and CW53 were used for the irrigation supply to the areas in Sections 33 and 34. Water from these supply wells is collected into a common piping system and is used on only one irrigation area at a time. Wells 634, 659, 881, 886, 890, M16, MO, MR and MS were used to supply the Section 28 pivot irrigation. These four areas were

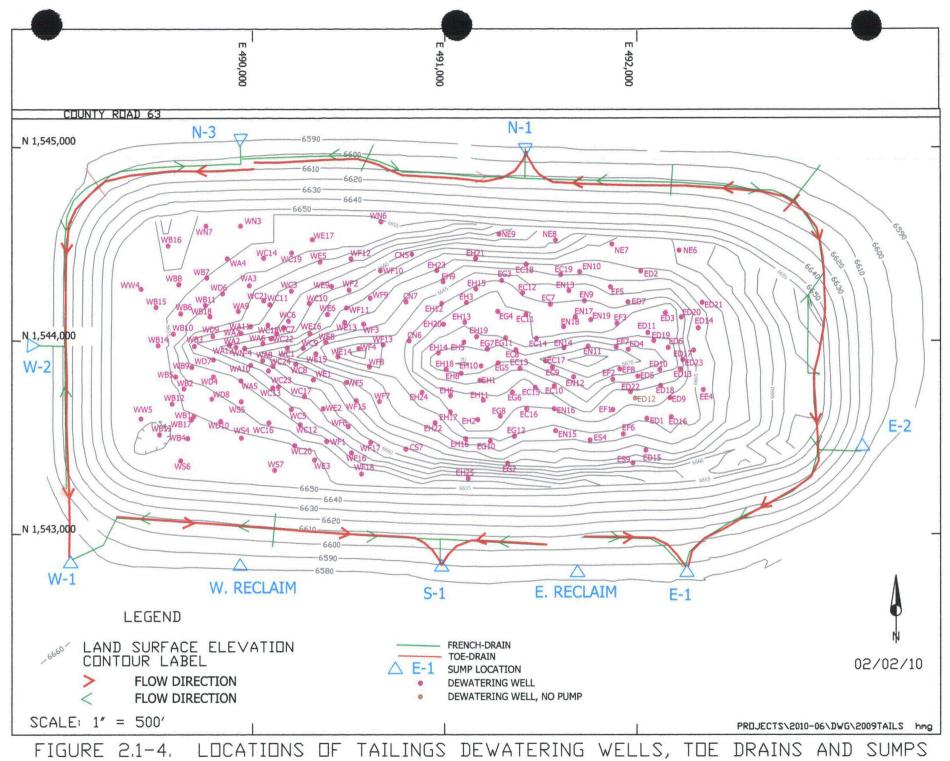
successfully irrigated during the entire 2009 growing season with 2 hay cuttings produced from the center pivot irrigation within Section 33 and the flood area in Section 34. Only 1 hay cutting was produced from Section 28 center pivot and no cutting was done on the Section 33 flood area. A total of 731 Ac-Ft of water was applied to the four irrigation areas in 2009. The average uranium and selenium concentrations applied to the Section 33/34 fields were 0.24 and 0.05 mg/l for uranium and selenium respectively in 2009 while the average values for Section 28 were 0.39 and 0.07 mg/l, respectively.











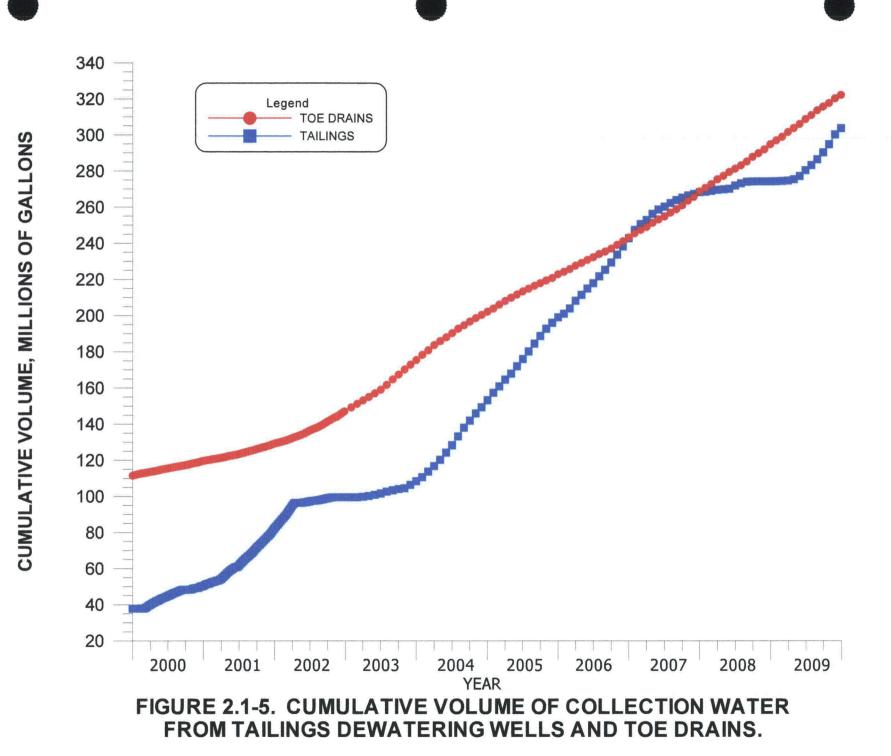
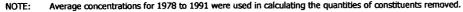




TABLE 2.1-1. QUANTITIES OF CONSTITUENTS COLLECTED.

YEAR	SOURCE	TOTAL VOLUME PUMPED	SULFATE CONC.		URANIU CONC.			MOLYBDENUM (MO) CONC. AMT.		M (SE) MT.
		(GAL)	(MG/L)	(LB)	(MG/L)	(LB)	(MG/L)	(LB)	(MG/L)	(LB)
1978	G.W.	27670033	5200	1200620	35	8081	40	9236	2	46
1979	G.W.	46371629	5200	2012095	35	13543	40	15478	2	774
1980	G.W.	39385860	5200	1708978	35	11503	40	13146	2	65
1981	G.W.	91613183	5200	3975155	35	26756	40	30578	2	1529
1982	G.W.	159848025	5200	6935910	35	46684	40	53353	2	266
1983	G.W.	167018540	5200	7247043	35	48778	40	55746	2	278
1984	G.W.	203258522	5200	8819519	35	59362	40	67842	2	3393
1985	G.W.	194074421	5200	8421015	35	56680	40	64777	2	323
1986	G.W.	199326030	5200	8648886	35	58214	40	66530	2 2	332 301
1987	G.W.	180881740	5200	7848576	35 35	52827 48615	40 40	60374 55560	2	277
1988	G.W.	166460826 175780800	5200 5200	7222843 7627243	35	51337	40	58671	2	293
1989 1990	G.W. G.W.	164378919	5200	7132508	35	48007	40	54865	2	274
1990	G.W.	171497720	5200	7441397	35	50086	40	57242	2	286
1992	G.W.	128398849	4925	5276234	27.2	29134	35.9	38419	1.60	171
1992	TOE	8544670	12117	864006	53.2	3793	106.5	7595	1.73	12
1993	G.W.	115795020	5011	4841203	28.1	27130	45.4	43885	1.47	142
1993	TOE	18357680	12117	1856262	53.2	8150	106.5	16315	1.73	26
1994	G.W.	98294087	4423	3624762	26.0	21146	27.3	22349	1.42	116
1994	TOE	18337680	12117	1854240	53.2	8141	106.5	16299	1.73	26
1995	G.W.	108306398	3256	2 9 42827	16.1	14553	19.2	17355	1.65	149
1995	TOE	17711370	11370	1680500	54.6	8069	94.4	13952	2.25	33
1995	TAILS	5905740	8191	403680	36.1	1778	89.7	4420	0.15	105
1996	G.W.	122064160	3899	3967919	20.9	21225	26.8	27259	1.92	195
1996	TOE	15431810	11537	1484295	46.4	5970	105.0	13509	1.29	16 1
1996	TAILS	9181390	9434	722129	40.2	3077	108.0	8236 25887	0.18 3.17	245
1997	G.W.	94465562	4955	3836678	26.9	20892 419	33.4 100.0	10040	0.81	243
1997	TOE	12029390 21292900	11094 10284	1113808 1827575	41.8 45.8	8139	92.4	16420	0.14	2
1997 1998	TAILS G.W.	74459130	5088	3161866	29.6	18385	34.8	21625	1.85	115
1998	TOE	10321780	9870	850257	42.5	3665	95.2	8203	0.73	6
1999	G.W.	117752408	3363	3305027	16.6	16314	14.8	14545	2.06	202
1999	TOE	8809890	11560	849976	54.3	3993	106.0	7794	0.46	3
1999	TAILS	120550	9420	9478	40.9	41	111.5	112	0.19	(
2000	G.W.	146609842	3358	4108868	18.8	23004	20.6	25206	1.94	237
2000	TOE	8032870	9734	652590	58.6	3929	118.0	7911	0.34	2
2000	TAILS	12446810	97 10	1008685	37.8	3927	127.0	13193	0.30	3
2001	G.W.	144925056	2770	3350438	19.6	23707	21.4	25884	1.65	199
2001	TOE	9606280	9935	796529	43.1	3455	95.7	7673	0.78	6
2001	TAILS	31465370	8688	2281555	34.6	9086	89.2	23425	0.19 1.23	5 206
2002	G.W.	201357360	2748	4618092	14.9	25040	16.7 88.7	28065 13307	0.76	200
2002	TOE	17975520	9210 7670	1381718	33.4 23.5	5011 3495	40.8	6067	0.12	1
2002	TAILS	17817840 177727419	2417	1140588 3585168	13.8	20470	15.5	22991	0.73	108
2003 2003	G.W. TOE	28418871	9457	2243048	35.6	8444	78.9	18714	4.35	103
2003	TAILS	8890076	9800	727126	28.0	2078	92.0	6826	0.30	2
2003	G.W.	154422720	2272	2931913	11.3	14633	16.6	21386	0.79	101
2004	TOE	26720928	8007	1787722	31.9	7115	67.6	15102	2.78	62
2004	TAILS	44745696	6360	2377848	23.1	8637	60.9	22769	0.20	7
2005	G.W.	130810679	2478	2705346	11.8	12883	15.5	16922	0.59	64
2005	TOE	20704320	8228	1421784	43.5	7517	87.5	15120	2.63	45
2005	TAILS	45685786	4389	1673497	18.7	7130	56.3	21467	0.18	6
2006	G.W.	132406109	1990	2199072	9.6	10609	14.3	15802	0.73	80
2006	TOE	20374782	7432	1263796	38.0	6462	76.2	12958	1.09	18
2006	TAILS	43707760	4278	1560550	17.6	6420	51.9	18932	0.14	5
2007	G.W.	137707200	2420	2781316	10.3	11838	16.7	19193	0.52	- 59
2007	TOE	25037779	6829	1427024	31.9	6666	67.3	14063	1.20	25
2007	TAILS	24561680	4130	846616	19.9	4079	61.1	12525	0.15 0.61	3 69
2008	G.W.	137145174	2672	3058408	11.5	13163	16.5 68.5	18886 14945	1.58	34
2008	TOE	26140850	7847	1711992	31.6	6894 705	68.5 42.8	2126	0.24	1
2008	TAILS	5950324	4671	231968	16.0 15.5	795 16766	42.8 19.1	20660	0.24	· 91
2009	G.W.	131564160	3145	3401818 1771396	15.5 35.0	7957	69.9	15891	0.85	18
2009 2009	TOE TAILS	27238830 29403070	7792 3850	1771396 944782	35.0 13.7	3362	38.6	9472	0.81	5
2009	INLS	25403070	3030	544/02	13.7	3302	50.0	2.12		•
JM G.W.		4,341,777,581		149,938,744		921,363		1,089,718		58,750
JM TOE		319,795,300		25,010,943		105,649		229,390		4,600
JM TAILS	5	301,174,992		15,756,079		62,044		165,990		463
The Letter						1,089,056		1,485,098		63,813



Average concentrations for 1978 to 1991 were used in calculating the quantities of constituents removed. Concentrations from the collection wells have gradually decreased from 1978 through 1991. G.W. = Ground water; TOE = Toe drains on edge of tailings; TAILS = Large tailings collection wells

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2.2 FUTURE OPERATION

Ground water quality restoration in 2010 will continue as a combination of fresh-water and R.O. product injection to maintain the overall piezometric gradient reversal between the lines of injection (M Line, WR Line, J Line and X Line) and contaminated water collection near the tailings piles. The reverse osmosis (R.O.) plant can be operated at a rate of up to 600 gpm but is projected to operate at an average rate of approximately 350 gpm in 2010 due to present limitations on pond storage capacity. When the plant is operated at full capacity, approximately 380 gpm of R.O. product is produced for injection into the alluvium and approximately 150 gpm of brine reject is discharged to the evaporation ponds. A larger collection rate and use of the very good quality R.O. product for injection will continue to enhance the progress in restoration.

Water collected from the alluvial and Chinle aquifers, where there are relatively low levels of selenium and uranium, will continue to be collected and used for re-injection in the initial phase of restoration of some areas. This re-injection will occur in the alluvium, where concentrations are greater than those of the injected water, until such time as injection with San Andres fresh water or R.O. product water will better complete the restoration. Use of the low-concentration re-injection water will be limited to areas up-gradient of the J, WR and X injection lines. For the purpose of this document, the reversal zone is called the collection area. To date, re-injection has occurred in wells X5 through X27, 1A, C4, D2 through D4 and DAA, DAB, DL, DW, DY, DF, DG, DQ, DX and K and a few tailings wells.

Collection from Upper Chinle wells CE2, CE5, CE6, CE11 and CE12 will continue to intercept contaminants in this aquifer. Injection into Upper Chinle wells 944, CW4R, CW5, CW13 and CW25 is planned to continue to control the direction of flow in these areas of the Upper Chinle aquifer.

Injection into well CW14 will be continued in order to build the head in this area of the Middle Chinle aquifer. This will prevent alluvial water from flowing into this portion of the Middle Chinle aquifer.

Irrigation with water from Sections 3, 27, 28, 32, 33 and 35 is planned to be continued in 2010. Fresh-water well injection lines in Section 28 will continue to be utilized in 2010 to restore these areas of low level aquifer contamination. Fresh-water injection will be continued in Sections

35 and 3 in 2010 to complement the use of water for irrigation and assist in final aquifer restoration in this area.

Subject to review and approval, alternative restoration for contaminated water with small concentrations will be evaluated in 2010. The removal of uranium in zeolite beds will be tested to enable the water after treatment to be used in the restoration program. Insitu treatment will be tested to evaluate the treatment of ground water in the aquifer. Insitu bio-remediation will be tested by adding a carbon source to reduce small concentrations. Phosphate precipitation will be tested to evaluate the removal of small concentrations from the ground water. An additional insitu treatment will be the use of a reductant to cause the precipitation of uranium in the ground water.

SECTION 3

1

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GROUND WATER MONITORING FOR HOMESTAKE'S GRANTS PROJECT

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3.0

3.1

SITE STANDARDS AND BACKGROUND CONDITIONS ALLUVIAL SITE STANDARDS

Ten water-quality site standards (U, Se, Mo, SO4, Cl, TDS, NO3, Ra226 + Ra228, Th230 and V) have been set for the alluvial aquifer at the Homestake site by the United States Nuclear Regulatory Commission (NRC) and the site Radioactive Materials License was amended accordingly. These site standards were established on the basis of defining the full range in alluvial aquifer background concentration values for these constituents. The procedures used to establish background concentrations and subsequent setting of appropriate site standards were reviewed and approved by NRC, EPA and the New Mexico Environmental Department (NMED). Adjustment of the site standards to account for the full range in natural background concentrations was important in assuring that appropriate site standards are set in relation to background concentrations.

The NRC alluvial aquifer site standards are shown in Table 3.1-1 and will be incorporated in the New Mexico Environment Department (NMED) DP-200 Discharge Plan when the permit is renewed. Alluvial site standards for the Grants Project are applicable at three points of compliance; these Point of Compliance (POC) wells are S4, D1, and X (see Figure 2.1-1 for locations).



TABLE 3.1-1. GRANTS PROJECT ALLUVIAL SITESTANDARDS.

Constituents		
	NRC License Site Standards	New Mexico Site Standards*
Uranium	0.16	0.16
Selenium	0.32	0.32
Molybdenum	0.10	1.0**
Vanadium	0.02	
RA-226 + Ra-228	5	30
Thorium-230	0.3	
Sulfate	1500	1500
Chloride	250	250
TDS	2734	2734
Nitrate	12	12

NOTE: All concentrations are in mg/l except: Ra-226 + Ra-228 and Th-230, which are in pCi/l.

* = Pending NMED renewal of DP-200 Discharge Plan

****** = New Mexico Irrigation Standard

3.2

ALLUVIAL BACKGROUND WATER QUALITY

Background alluvial aquifer water-quality conditions at the Grants site are those found up-gradient or north of the Large Tailings Pile. These conditions in the San Mateo alluvium have been monitored since 1976. Ground water flow in the San Mateo alluvial system is generally from the northeast to the southwest (see Figure 3.2-1). Lobo Creek joins San Mateo Creek in the Felice Acres subdivision area at the Homestake site, although neither creek has a well-defined surface flow channel in this area. Surface-water flow occurs only after extreme precipitation events and then generally only within some reaches of the channels.

Hydrographs of up-gradient wells that have been used to define the background hydrologic conditions of the alluvial aquifer are presented in Section 4 of this report. Wells DD, DD2, P, P1, P2, P3, P4, Q, R and ND, located just north of the Large Tailings Pile, have been used for monitoring alluvial background water quality and are called the near up-gradient wells. An additional near up-gradient well, DD2, was drilled in 2008.

Additional alluvial background wells located farther north have also been sampled (wells 914, 920, 921, 922 and 950, see Figure 3.2-1 for locations). Information gathered from these wells has been used to further define the piezometric surface and water-quality conditions in the upgradient alluvial aquifer, and these wells are referred to as the far up-gradient wells.

Figure 3.2-1 presents the latest 2009 water-quality data for the near and far-up-gradient alluvial background wells for six parameters: sulfate, uranium, selenium, chloride, TDS and nitrate. Sulfate concentrations for the wells varied from 450 to 1610 mg/l in 2009. Uranium concentrations also varied over a large range, from less than 0.003 to 0.25 mg/l. The new upgradient monitoring well DD2 has the highest near upgradient uranium concentration and would have resulted in a higher site standard if its values had been used in setting the standard. Selenium concentrations also varied over a large range, from less than 0.005 to 0.72 mg/l.

Chloride concentrations in water sampled in 2009 from the up-gradient wells ranged from a low of 44 mg/l to a high of 94 mg/l. The TDS concentrations varied from 1080 to 2760 mg/l. Nitrate concentrations also vary naturally over a large range in the alluvial aquifer, and ranged from less than 0.1 to 20.2 mg/l in 2009. Molybdenum concentrations varied from less than 0.03 to 0.04



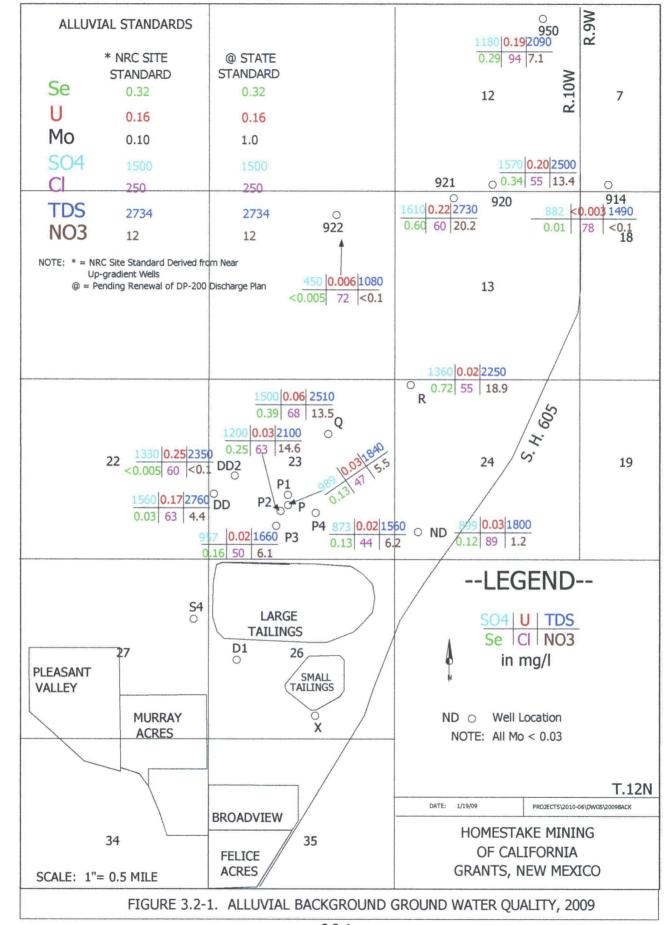
mg/l. Concentration versus time plots for up-gradient wells DD, DD2, P, P4, Q and R are presented later in Section 4.3 of this report.

The 95th percentile of the historical background alluvial aquifer water-quality data for the Grants site was defined by ERG (1999a and 1999b). These documents, along with a hydrologic support document (Hydro-Engineering 2001c), were submitted to the NRC in 2001 with a request to adjust some of the site standards based on the full range of natural background conditions. The 95th percentile was used to define the upper limit of background. Background data for a ten year period of 1995 through 2004 was used to determine the 95th percentile values. The cumulative database for all of the background wells more adequately defines background concentrations, and this expanded database, based on near-up-gradient wells, was utilized in the two ERG (1999a and 1999b) studies. A tabulation of alluvial standards for the Grants Project area constituents is included in Figure 3.2-1.

The range in concentrations in the alluvial up-gradient wells¹ sampled during 2009 is tabulated in Table 3.2-1 with a list of the site standards. These site standards were established from data from the near up-gradient wells². The following table (Table 3.2-1) summarizes the 2009 data for near up-gradient and far up-gradient wells for constituents of concern where site standards have been set for the Grants site. As shown by the present data, there is a large natural areal variability in the background water quality. Naturally occurring background variation is illustrated by the uranium concentrations, where concentrations in 2009 varied from less than 0.003 to 0.25 mg/l.

TABLE 3.2-1	2009 BACK	GKUUN				UIVI				
		PARAMETERS								
	Se	U	Mo	SO4	Cl	TDS	NO ₃			
NRC Site Standard	0.32	0.16	0.10	1500	250	2734	12			
Pending NMED Standard	0.32	0.16	1.0	1500	250	2734	12			
	NEAR U	P-GRADI	ENT WE	LLS	J		L			
DD	0.03	0.17	< 0.03	1560	63	2760	4.4			
DD2	< 0.005	0.25	< 0.03	1330	60	2350	<0.1			
ND	0.12	0.03	<0.03	899	89	1800	1.2			
Р	0.13	0.03	< 0.03	989	47	1840	5.5			
P2	0.25	0.03	< 0.03	1200	63	2100	14.6			
P3	0.16	0.02	<0.03	957	50	1660	6.1			
P4	0.13	0.02	< 0.03	873	44	1560	6.2			
Q	0.39	0.06	< 0.03	1500	68	2510	13.5			
R	0.72	0.02	< 0.03	1360	. 55	2250	18.9			
······································	FAR UP	-GRADIE	ENT WEL	LS	I		I			
914	0.01	< 0.003	< 0.03	882	78	1490	<0.1			
920	0.34	0.20	< 0.03	1570	55	2500	13.4			
921	0.60	0.22	< 0.03	1610	60	2720	.20.2			
922	< 0.005	0.006	0.04	450	72	1080	<0.1			
950	0.29	0.19	< 0.03	1180	94	2090	7.1			

¹Wells DD, DD2, ND, P, P2, P3, P4, Q, R, 914, 920, 921, 922 and 950 ²Wells DD, ND, P, P1, P2, P3, P4, Q and R



3.2-4

3.3 CHINLE SITE STANDARDS

Eight water quality site standards (U, Se, Mo, SO4, Cl, TDS, NO3, and V) have been set for the Chinle aquifers at the Homestake site by the NRC. The site standards were also established based on the full range of background concentration in the Chinle aquifers for these constituents. The procedures accepted and used to establish these site standards can result in a minor amount of observed natural concentrations exceeding the site standards.

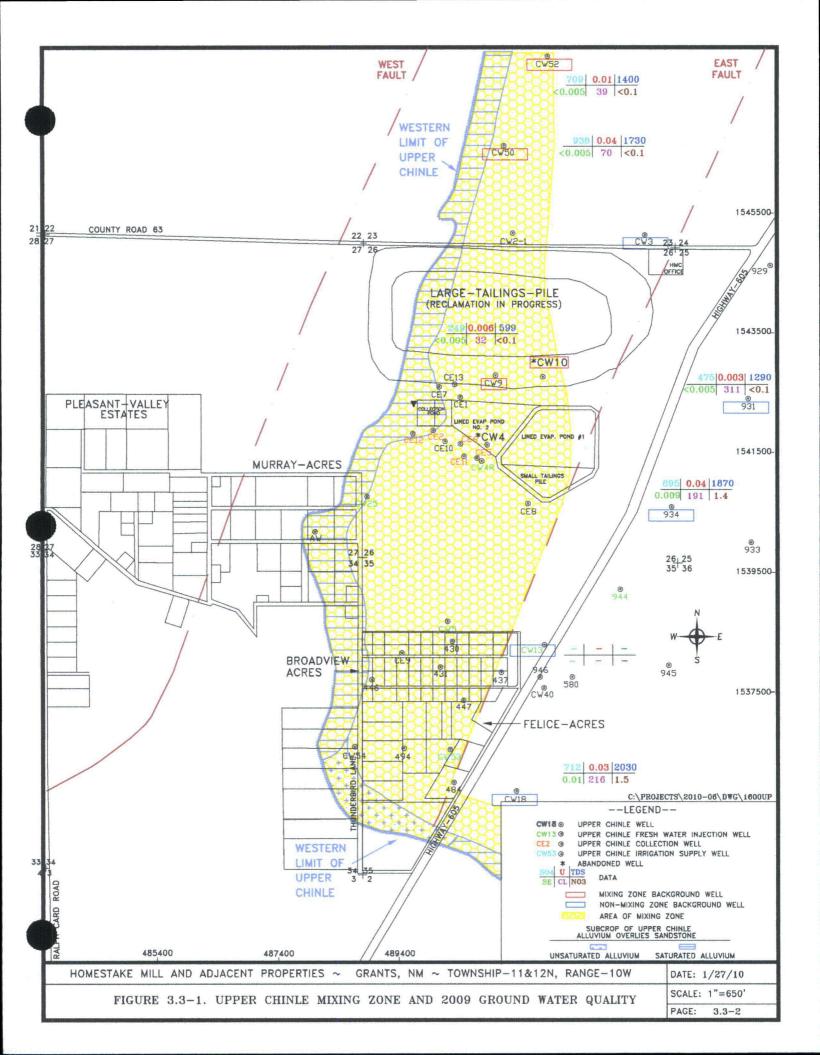
Site standards have been established for the Chinle mixing zone, Upper Chinle nonmixing zone, Middle Chinle non-mixing zone and Lower Chinle non-mixing zone. Separate site standards exist for each of these four Chinle aquifer zones. Figures 3.3-1 through 3.3-3 show the Upper Chinle, Middle Chinle and Lower Chinle aquifers with the portion of the aquifer in the mixing zone and the remainder that is in the non-mixing zone. Figure 3.3-1 presents the location of the Upper Chinle mixing-zone (yellow pattern) and the wells used in the analysis of background values. Wells within the mixing zone that were used in the mixing-zone background calculations have a red box around the well name. Wells used to define the Upper Chinle non-mixing zone are indicated by a light blue rectangular box around their name.

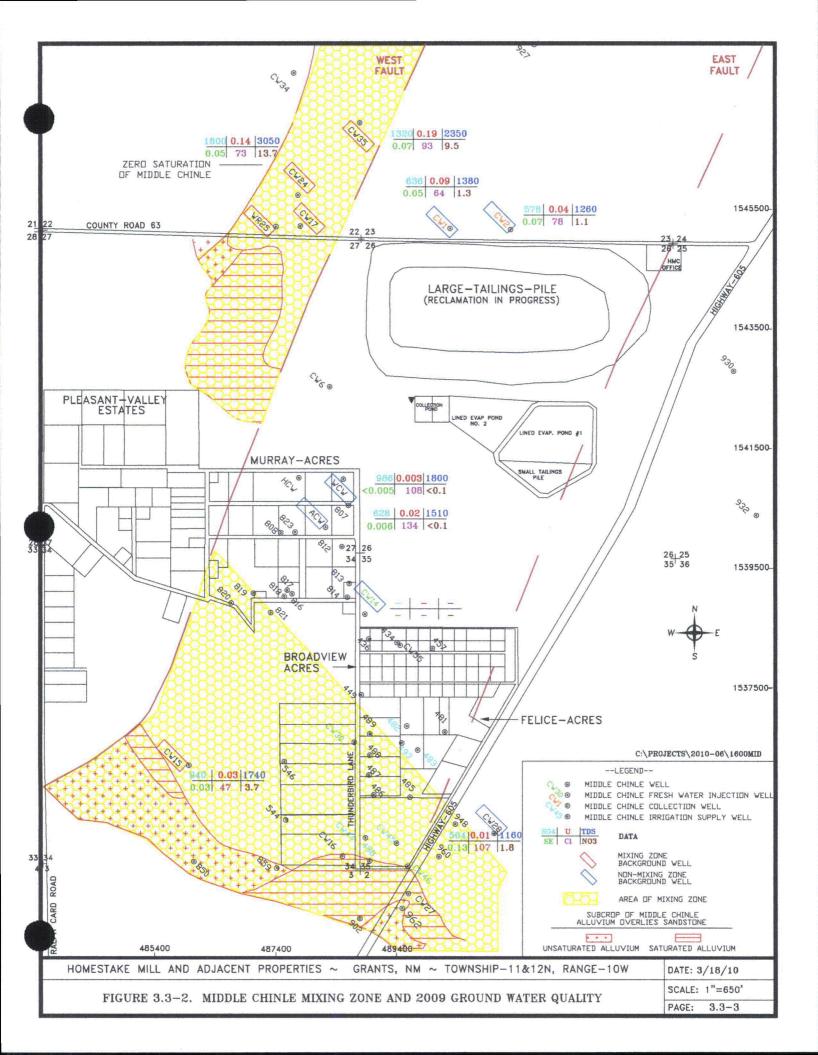
Table 3.3-1 below presents the Chinle site standards for the four Chinle aquifer zones.

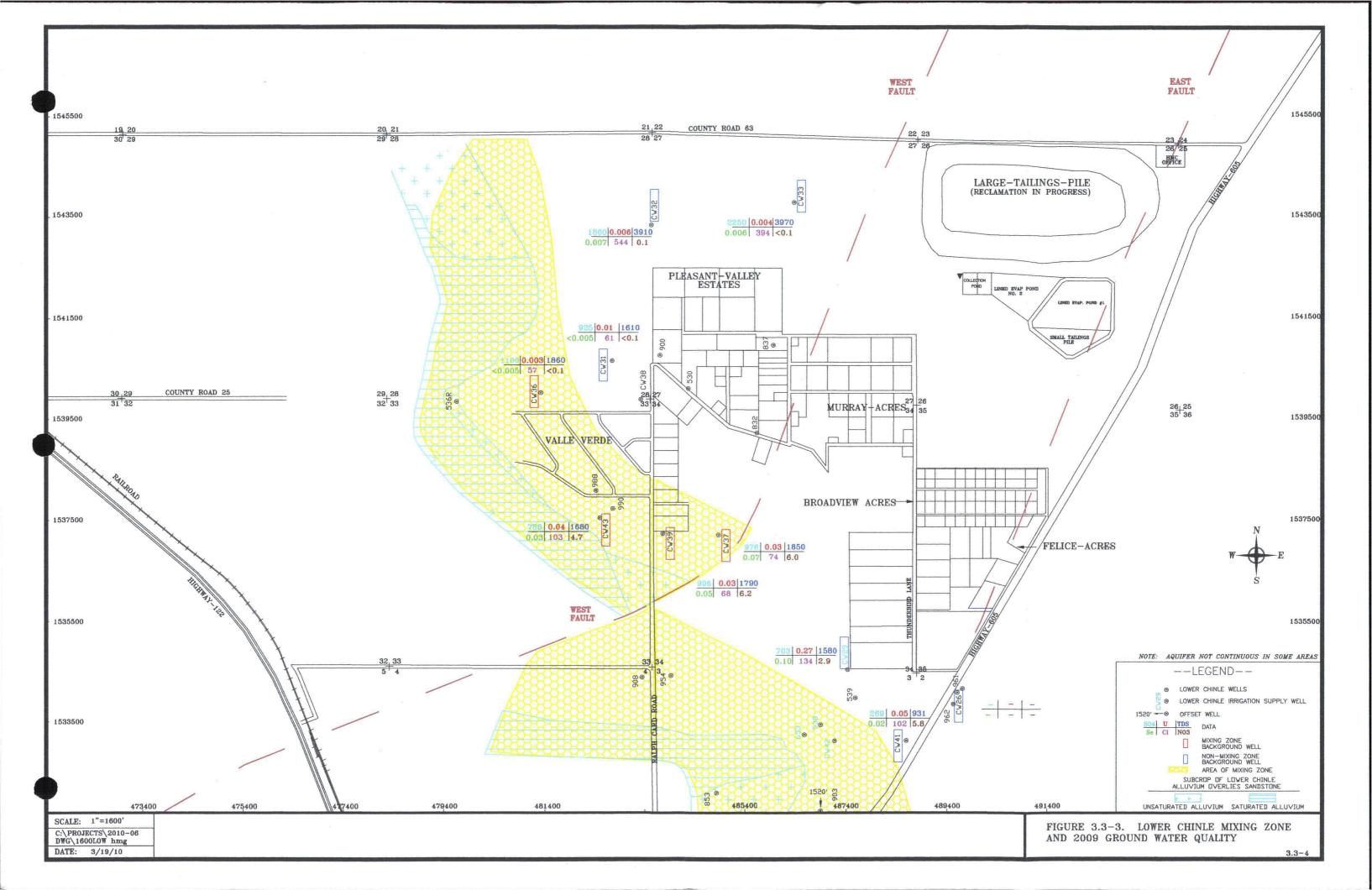
		CONSTITUENT, concentrations in mg/l except Thorium-230 and Ra226+Ra228 in pCi/l.								
Aquifer Zone	Selenium	Uranium	Molybdenum	TDS	Sulfate	Chloride	Nitrate	Vanadium	Thorium-230	Ra-226 +Ra-228
Chinle Mixing	0.14	0.18	0.10	3140	1750	250	15	0.01	*	*
Upper Chinle Non-Mixing	0.06	0.09	0.10	2010	914	412	*	0.01	*	*
Middle Chinle Non-Mixing	0.07	0.07	0.10	1560	857	250	*	*	*	*
Lower Chinle Non-Mixing	0.32	0.03	0.10	4140	2000	634	*	*	*	*

TABLE 3.3-1. GRANTS PROJECT - CHINLE SITE STANDARDS

* Background water quality analyses for constituent determined that site standard is not necessary.







3.4

CHINLE BACKGROUND WATER QUALITY

The Chinle aquifer background water quality has been analyzed and presented to the NRC and NMED in Hydro-Engineering 2003b and ERG 2003. The background concentrations for the mixing zones in the Upper, Middle and Lower Chinle aquifers were grouped together to develop a mixing zone background level. The non-mixing zone water chemistry data for each of the three aquifers were analyzed separately. Table 3.4-1 presents the site standards that resulted from the analysis and related discussions with NRC, EPA and NMED concerning agreement on the standards. Figure 3.3-1 also presents the 2009 data collected from these background wells for selected parameters of sulfate, uranium, TDS, selenium, chloride and nitrate. This data is presented in a format similar to that used for the alluvial background data. The data for wells CW3, CW17 and WR25 are not presented on Figures 3.3-1 and 3.3-2 because concentrations are not natural in these wells for 2009. Table 3.4-1 also presents the 2009 data for the Chinle mixing zone background wells and the Upper, Middle and Lower Chinle non-mixing zone wells separated by their category.

The Middle Chinle mixing zone is presented in Figure 3.3-2 with a yellow pattern. Five wells are shown in the Middle Chinle mixing zone, and these wells were included with the Upper Chinle and Lower Chinle mixing-zone wells in establishing the mixing-zone background values. Six wells shown on Figure 3.3-2 were used to establish the Middle Chinle non-mixing zone background levels. This figure also presents the 2009 data collected for these background wells.

Figure 3.3-3 presents the Lower Chinle mixing zone in a yellow pattern. This figure also shows which wells were used to establish the background concentrations in the mixing and nonmixing zones of the Lower Chinle aquifer. The 2009 data for the Lower Chinle wells previously used to define background concentrations are also presented on Figure 3.3-3. The Lower Chinle non-mixing zone background levels are somewhat problematic, because the water quality tends to deteriorate naturally as the ground water moves down-gradient. Therefore, the expected natural water quality deterioration is a function of the distance from the Lower Chinle subcrop beneath the alluvium to a particular point within the aquifer.

	CONSTITUENT, concentrations in mg/l							
Aquifer Zone	Selenium	Selenium Uranium Molybdenum TDS Sulfate Chloride Nitrate Vana						Vanadium
		CI	HINLE SITE ST	ΓANDA	RDS			
Chinle Mixing	0.14	0.18	0.10	3140	1750	250	15	0.01
Upper Chinle								
Non-Mixing	0.06	0.09	0.10	2010	914	412	*	0.01
Middle Chinle								
Non-Mixing	0.07	0.07	0.10	1560	857	250	*	*
Lower Chinle								
Non-Mixing	0.32	0.03	0.10	4140	2000	634	*	*
		CHI	NLE MIXING	ZONE V	VELLS			
CW9	< 0.005	0.01	<0.03	599	249	32	<0.1	-
CW50	< 0.005	0.04	<0.03	1730	938	70	<0.1	<0.01
CW52	<0.005	0.01	<0.03	1400	709	39	<0.1	<0.01
CW15	0.03	0.03	< 0.03	1740	940	47	3.7	-
CW24	0.05	0.14	< 0.03	3050	1800	73	13.7	-
CW35	0.07	0.19	<0.03	2350	1320	93	9.5	-
CW36	<0.005	0.003	<0.03	1860	1100	57	<0.1	-
CW37	0.07	0.03	<0.03	1850	976	74	6	-
CW39	0.05	0.03	<0.03	1790	996	68	6.2	-
CW43	0.03	0.04	<0.03	1680	788	103	4.7	-
	¹ U	PPER CH	INLE NON-MI	XING Z	ONE WE	ELLS		
934	0.009	0.04	<0.03	1870	695	191	1.4	-
CW18	0.01	0.03	<0.03	2030	712	216	1.5	-
	M	DDLE CH	IINLE NON-M	IXING 2	ZONE W	ELLS		
ACW	0.006	0.02	<0.03	1510	628	134	<0.1	-
CW1	0.05	0.09	0.04	1380	636	64	1.3	-
CW2	0.07	0.04	<0.03	1260	578	78	1.1	-
CW28	0.13	0.01	<0.03	1160	504	107	1.8	-
WCW	<0.005	0.003	<0.03	1800	986	108	<0.1	-
		OWER CH	INLE NON-MI	XING 2	CONE WI	ELLS		
CW26	,0.1	-	<0.03	-	-	-	-	
CW29	0.1	0.27	<0.03	1580	703	134	2.9	-
CW31	<0.005	0.01	<0.03	1610	925	61	<0.1	-
CW32	0.007	0.006	<0.03	3910	1860	544	0.1	-
CW33	0.006	0.004	<0.03	3970	2250	394	<0.1	-
CW41	0.02	0.05	<0.03	931	269	102	5.8	-

TABLE 3.4-1. 2009 BACKGROUND WELL DATA - CHINLE

* Background water quality analyses for constituent determined that site standard is not necessary.

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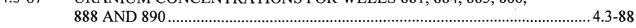
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ALLUVIAL AQUIFER MONITORING

This section presents 2009 monitoring results for the alluvial aquifer. The alluvial aquifer immediately underlies the Grants Project site and is therefore the most important ground water system at the Grants Project site. The section describing well completions is presented first, and is followed by several report sections presenting water-level and water-quality information.

4.1 ALLUVIAL WELL COMPLETIONS

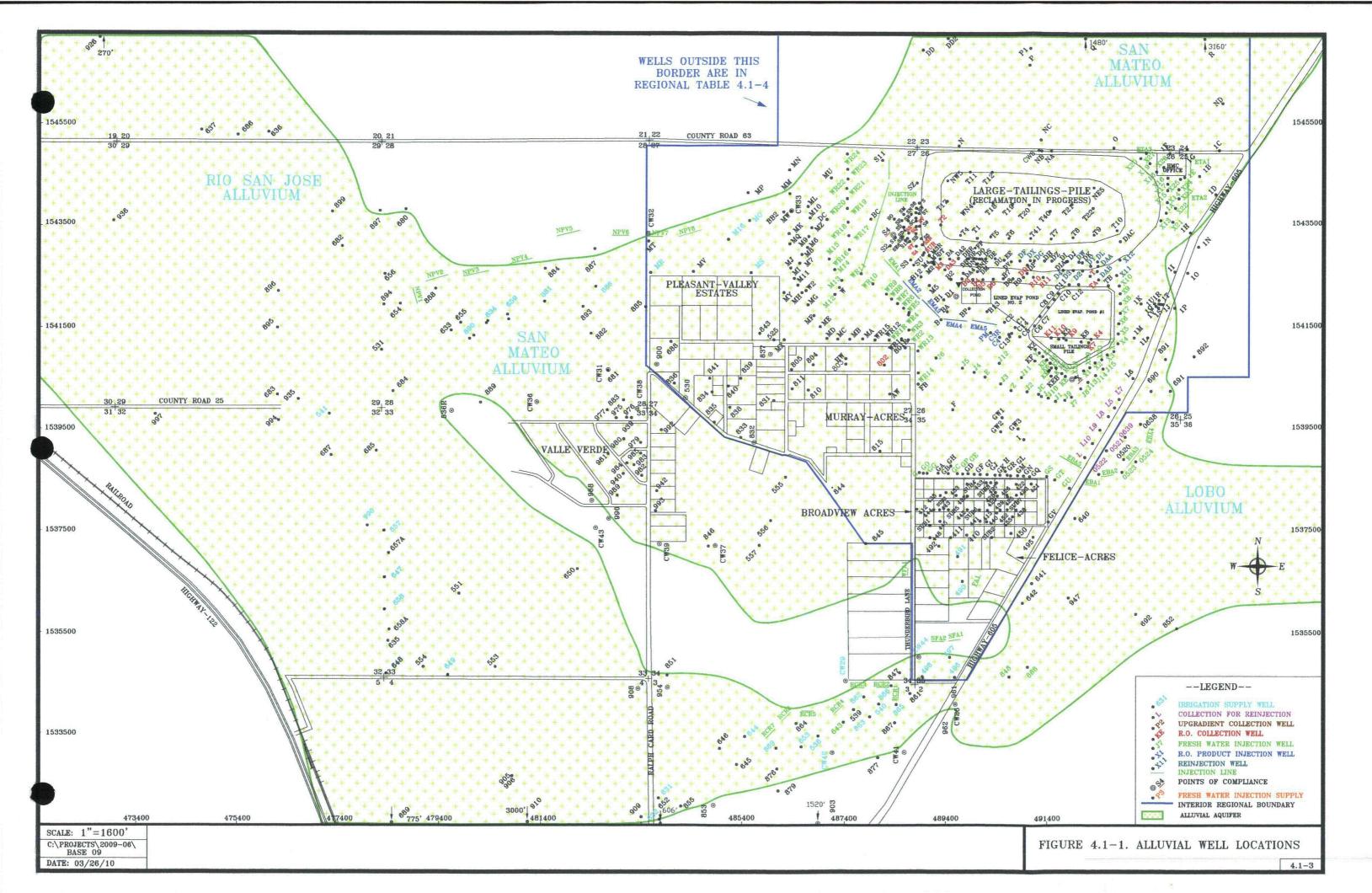
Ten new alluvial wells, 551, 553, 554, T13, T14, T15, T16, T23, T36 and T39 were installed in 2009; four additional infiltration lines, FA2, FA3, FA4 and SFA4 were installed during the year. Operational status and other characteristics of the new and previously installed alluvial wells and infiltration lines are discussed in this section. Figure 4.1-1 shows the locations of the alluvial wells near the Homestake Grants Project with the operational status for each well and infiltration line for 2009. Wells labeled in black were used only for monitoring and black labeled infiltration lines were not used in 2009. This figure is plotted at a scale of 1'' = 1600'.

Alluvial wells 914, 920, 921, 922 and 950 are located outside of the area presented on Figure 4.1-1. These upgradient wells are shown on Figure 3.2-1 in the previous report section.

The currently active injection and collection wells are labeled with different colors on Figure 4.1-1 so that they can be distinguished from monitoring wells. This figure also shows the wells used for irrigation water supply during the 2009 irrigation season. Table 4.1-1 presents basic well data for alluvial wells located on the Grants Project that have been used to define the alluvial ground water hydrology. Many additional alluvial wells outside of the Grants Project have also been used for that purpose. The basic well data table presents the location, well depth, casing diameter, water-level information, depth to the base of the alluvium and casing perforation intervals for each well.

Table 4.1-2 presents the same type of basic well data for alluvial wells in the Broadview and Felice Acres subdivisions. These two subdivisions are located just south of the Homestake property. Figure 4.1-1 shows the locations of the subdivision wells. Table 4.1-3 presents similar basic data for alluvial wells located in Murray Acres and Pleasant Valley Estates subdivisions.

Table 4.1-4 presents data for regional wells located outside of the subdivisions and the immediate Homestake property around the tailings sites (Grants Project). Wells outside the area delineated with a heavy blue boundary line on Figure 4.1-1 are considered to be regional wells; data for these wells are presented in this table. Over 100 alluvial wells are included on the regional table, which brings the total number of alluvial wells used to characterize this site to more than 400. The wells are listed in numerical or alphabetical order based on their well names.



· · ·

	North. Coord.		WELL DEPTH . (FT-MP)	CASI DIA (IN	М		ATER LE DEPTH (FT-MP)	ELEV.		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)		SATURATED THICKNESS
0690	15402	79 4	93465	65.0	5.0	12/14/2	2009	38.15	6543.91	2.5	6582.06	55	6524.6 A	25-65	19.3
0691	15402	76 4	93860	66.0	5.0	12/14/2	2009	44.17	6544.64	2.9	6588.81	55	6530.9 A	26-66	13.7
0891	15409	04 4	93751	54.0	5.0	7/27/2	009	33.56	6547.56	2.1	6581.12	50	6529.0 A	24-54	18.5
0892	15409	54 4	94317	50.0	5.0	12/19/2	2002	41.96	6545.25	2.0	6587.21	42	6543.2 A	30-50	2.0
1A	15437	90 4	93768	61.0	5.0	11/4/2	800	38.40	6547.03	2.9	6585.43	47	6535.5 A	39-51	11.5
1B	15445	02 4	94412	51.8	5.0	10/30/2	001	38.70	6545.72	1.5	6584.42	50	6532.9 A	20-50	12.8
1C	15450	18 4	94799	52. 9	5.0	9/28/2	000	43.26	6544.73	2.5	6587.99	43	6542.5 A	34-54	2.2
1D	15441	42 4	94752	42.9	5.0	12/3/2	005	26.42	6559.55	2.2	6585.97	40	6543.8 A	22-42	15.8
1E	15444	81 49	94116	51.4	5.0	11/4/2	800	27.96	6556.35	2.1	6584.31	43	6539.2 A	34-54	17.1
1F	15449	52 49	93831	61.8	5.0	11/5/2	800	42.03	6545.35	1.8	6587.38	54	6531.6 A	30-60	13.8
1G	15450	34 49	94170	57.5	5.0	11/4/2	800	40.46	6546.61	2.3	6587.07	48	6536.8 A	35-55	9.8
1H	15433	63 49	94266	55.4	5.0	11/4/2	800	55.08	6531.31	1.8	6586.39	43	6541.6 A	25-55	0.0
11	15426	27 49	93928	49.8	5.0	7/27/2	009	35.43	6562.92	1.3	6598.35	35	6562.1 A	27-47	0.8
1J	15419	86 49	93695	50.3	5.0	2/23/2	009	38.81	6546.59	1.8	6585.40	· 40	6543.6 A	30-50	3.0
1K	15419	92 49	93275	55.6	5.0	2/23/2	009	36.11 t	6548.02	1.0	6584.13 ·	47	6536.1 A	30-55	11.9
hL	15412	56 49	93416	53.4	5.0	11/4/2	008	27.46	6551.15	3.1	6578.61	40	6535.5 A	35-55	15.6
1M	15413	27 49	93133	43.1	5.0	11/4/2	008	26.94	6548.59	1.3	6575.53	33	6541.2 A	25-54	7.4
1N .	154310	00 49	94396	45.6	5.0	7/27/2	009	32.81	6558.04'	2.4	6590.85	25	6563.5 A	15-44	0.0
10	154259	92 49	94175	44.0	5.0	7/27/2	009	43.72	6551.22	0.8	6594.94	29	6565.1 A	14-34	0.0
1P	154190	02 49	93924	52.8	5.0	7/27/2	009 :	37.02	6548.22	2.6	6585.24	35	6547.6 A	20-40	0.6
1Q	154199	93 49	93619	56.0	5.0	2/23/2	009	37.41	6545.70	1.9	6583.11	56	6525.2 A	36-56	20.5
1R	154207	71 49	93623	56.0	5.0	2/23/2	009 :	37.70	6548.29	1.3	6585.99	56	6528.7 A	36-56	19.6
1S	154192	20 49	93614	56.0	5.0	2/23/2	009 3	36.20	6545.79	1.5	6581.99	56	6524.5 A	36-56	21.2
1T	154199	90 49	93656	56.0	5.0	1/19/2	009 :	37.04	6547.87	1.7	6584.91	56	6527.2 A	36-56	20.7
1U	154200)1 49	93542	44.2	4.0	7/27/2	009 3	38.27	6547.95	3.2	6586.22		A	-	
1V	154198	32 49	3579	61.4	5.0	12/28/20	009 3	37.40	6547.54	1.7	6584.94		A	• ·	
' A1	154236	65 49	91539	55.6	4.0	1/12/1	994 4	15.29	6527.86	1.1	6573.15	55	6517.1 A	37-57	10.8
' A2	154235	56 49	91539	46.4	4.0	12/23/19	991 4	47.98	6525.42	1.1	6573.40		— A	27-47	-
в	154168	34 48	9311	68.6	4.0	12/28/20	009 3	35. 9 8	6534.92	2.4	6570.90	60	6508.5 A	49-69	26.4
B1	154207	'1 48	9370	90.9	5.0	12/9/20	009 3	38.55	6533.10	0.6	6571.65	82	6489.1 A	62-82	44.1
B2	154247	75 48	9515	83.0	5.0	10/17/20	006 4	12.08	6532.17	2.0	6574.25	72	6500.3 A	55-75	31.9
ВЗ ,	154248	60 48	9731	87.0	5.0	7/14/20	008 6	68.00	6506.29	2.6	6574.29	77	6494.7 A	58-78	11.6
B4	154247	'1 48	9942	88.8	5.0	7/14/20	008 6	64.98	6509.68	7.4	6574.66	82	6485.3 A	63-83	24.4
B5	154247	4 49	0141	91.0	5.0	7/14/20	008 5	57.60	6515.86	1.4	6573.46	81	6491.1 A	62-82	24.8 ·
B 6	154247	8 49	0341	90.0	5.0	12/5/20	000 4	8.94	6528.75	2.0	6577.69	80	6495.7 A	63-83	33.1
87	154248	8 49	0540	87.0 [.]	5.0	7/14/20	008 4		6528.52	2.2	6574.40	77	6495.2 A	53-78	33.3
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(cont'd.)

			WELL	. c	ASING	W	IATER LE	VEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.	EAS COO			DIAM (IN)		DEPTH (FT-MP)	ELEV.	L)	LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS (FT-LSD)	SATURATEI THICKNESS
88	15424	488	490734	87.0) 5.0	6/15/2	2005	40.30	6535.45	2.3	6575.75	77	6496.5 A	53-78	39.0
B9	1542	514	490935	86.0) 5.0	6/15/2	2005	40.03	6536.14	2.2	6576.17	76	6498.0 A	51-78	38.2
B10	1542	517	491133	84.8	5.0	7/14/2	8008	48.91	6527.86	2.3	6576.77	75	6499.5 A	51-78	28.4
B11	1542	517	491329	84.9	5.0	7/14/2	800	53.00	6524.39	2.2	6577.39	77	6498.2 A	42-80	26.2
B12	1542	524	488915	100.0	5.0	12/9/2	009	39.91	6533.11	2.2	6573.02	91	6479.8 A	30-100	53.3
B13	15418	341	490223	80.0	5.0	12/9/2	009	36.47	6533.57	3.1	6570.04	72	6494.9 A	30-80	38.6
BA	15418	335	489440	86.0	5.0	12/28/2	009 3	39.00	6532.58	1.7	6571.58	76	6493.9 A	64-78	38.7
BB2	15437	791	486213	56.6	4.0	11/15/2	002	53.36	6520.44	0.6	6573.80		A	42-62	
BC	15436	655	487910	82.8	4.0	12/9/2	009	1.00	6533.61	2.6	6574.61	75	6497.0 A	63-83	36.6
BP	15418	882	489841	85.4	4.0	8/26/2	009	12.10	6530.20	3.0	6572.30	75	6494.3 A	40-85	35.9
С	15417	62	490854	79,7	4.0	5/16/1	994 4	1.50	6529.34	0.3	6570.84	75	6495.5 A	59-79	33.8
C1	15415	533	490780	76.0	5.0	7/29/2	009 3	32.80	6539.06	0.8	6571.86	67	6504.1 A	41-68	35.0
C2	15416	530	490566	76.0	5.0	7/29/2	009 2	28.00	6537.02	0.9	6565.02	66	6498.1 A	42-67	38.9
C3	15413	44	490481	75.0	5.0	6/20/1	994 3	36.20	6532.33	0.9	6568.53	65	6502.6 A	45-67	29.7
C3R	15413	38	490472	75.0	5.0	3/7/2	002	8.00	6551.29	2.0	6569.29	66	6501.3 A	43-68	50.0
C4	15413	48	490675	75.0	5.0	10/2/2	000 3	9.66	6531.18	1.3	6570.84	66	6503.5 A	46-66	27.6
C5	15413	44	490869	72.0	5.0	10/21/2	009 3	2.60	6537.25	0.8	6569.85	62	6507.1 A	43-63	30.2
C6	15415	33	491142	80.8	5.0	11/4/2	009 4	8.43	6536.46	1.6	6584.89	72	6511.3 A	34-74	25.2
C7	15417	34	491280	72.4	5.0	11/4/2	009 4	8.13	6536.31	1.5	6584.44	61	6521.9 A	25-65	14.4
C8	15419	06	491415	78.1	5.0	11/4/2	009 4	7.51	6536.98	1.6	6584.49	67	6515.9 A	31-71	21.1
C9	15420	75	491545	77.0	5.0	11/4/2	009 4	6.54	6538.01	1.5	6584.55	65	6518.1 A	27-67	20.0
C10	15421	82	491629	71.6	5.0	11/4/2	009 4	7.00	6538.26	2.7	6585.26	65	6517.6 A	30-70	20.7
C11	15423	76	491844	6 8 .2	5.0	11/4/20	009 4	7.51	6533.87	2.4	6581.38	60	6519.0 A	35-65	14.9
C12	15423	75	492029	63.5	5.0	11/4/20	009 3	8.41	6542.14	2.6	6580.55	55	6523.0 A	34-64	19.2
C13	15413	94	490655	63.0	5.0	11/9/20	005 3	0.00	6540.01	2.0	6570.01	63	6505.0 A	36-70	35.0
C14	15414	13	490713	63.0	5.0	11/9/20	005 2	9.95	6539.74	2.0	6569.69	63	6504.7 A	36-70	35.0
D	15421	27	490118	89.7	4.0	7/28/19	986 . 4	8.04	6524.85	0.8	6572.89	90	6482.1 A	71-91	42.8
D1	15421	40	489615	8 9.4	4.0	7/13/20	009 3	9.30	6531.60	1.0	6570.90	80	6489.9 A	58-90	41.7
D2	15426	41	492107	70.0	5.0	11/29/19	999	0.50	6579.67	3.0	6580.17	62	6515.2 A	40-7 0	64.5
D3	15426	46	491917	80.0	5.0	11/29/19	999	0.50	6579.63	2.5	6580.13	72	6505.6 A	40-80	74.0
D4	15426	52	491724	78.0	5.0	11/29/19	99	0.50 (6578.93	2.5	6579.43	70	6506.9 A	48-78	72.0
DA	15428	64	489488	99.1	5.0	12/4/19	97 6	1.40 (6524.15	3.0	6585.55	90	6492.6 A	50-100	31.6
DA2	15428	81	489656	82.1	5.0	1/13/19	95 5	1.11 (6536.18	2.8	6587.29	83	6501.5 A	64-74	34.7
DA3	15426	64	489390	81.0	5.0	7/14/20	08 5	4.10 (6520.26	2.6	6574.36	72	6499.8 A	30-81	20.5
DA4	154259	98	489756	81.0	5.0	6/26/20	02 7	6.50 6	6497.47	1.7	6573.97	71	6501.3 A	31-81	0.0
DAA	15427:	33	492411	62.7	5.0	12/5/20	00	2.00 6	6578.60	2.2	6580.60	54	6524.4 A	30-60	54.2
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(cont'd.)

			WELL	CASIN	G	w	ATER LE	VEL		MP ABOVE	" t	DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	, ,
	NORTH. COORD.		DEPTH	DIAM (IN)			DEPTH (FT-MP)	ELEV.	L)	LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS	SATURATE THICKNES
DAB	15426	533 49	92399	65.1	5.0	12/5/2	000	0.50	6579.38	2.3	6579.88	56	6521.6 A	30-60	57.8
DAC	15432	218 49	92851	67.7	5.0					4.1	6620.36	45	6571.3 A	20-30	
DB	15428	374 48	39842	73.2	5.0	9/8/1	998	66.15	6523.33	0.5	6589.48		A	55-85	
DBR	15428	377 48	39855	55.6	5.0	1/25/1	995	52.19	6536.97	4.8	6589.16		A	-	
DC	15436	646 48	37060	64.1	4.0	12/9/2	009	38.94	6532.37	2.7	6571.31		A	45-65	
DD	15469	89 48	38943	78.5	4.0	9/21/2	009	52.76	6539.83	1.9	6592.59	83	6507.7 A	40-80	32.1
DD2	15474	39 48	39251	94.3	5.0	9/21/2	009	51.12	6542.16	2.0	6593.28		A		
DE	15428	377 49	90193	70.2	5.0	10/5/1	998	63.70	6527.65	0.8	6591.35	80	6510.6 A	60-90	17.1
DF	15428	39 49	90869	88.5	5.0	5/23/2	002	65.06	6525.53	0.6	6590.59		— A	65-95	
DG	15428	339 49	91157	88.9	5.0	5/23/2	002	59.80	6531.98	0.4	6591.78		A	65-95	
DH	15428	35 49	91365	61.7	5.0	12/24/1	991 9	52.65	6538.69	4.8	6591.34		A	65-95	
DI	15428	321 49	91788	86.1	5.0	12/9/1	997 9	57.87	6531.75	2.3	6589.62	75	6512.3 A	35-85	19.4
DiA	15428	21 49	1793		4.0	12/23/1	991 !	50.41	6543.22	1.4	6593.63		A	-	
DJ	15428	21 49	1793	85.7	5.0	8/24/1	988 4	46.87	6542.69	0.7	6589.56	· 75	6513.9 A	35-85	28.8
DK	15427	99 49	2094	65.4	5.0	12/23/1	991 4	43.58	6542.33	0.7	6585.91	55	6530.2 A	35-55	12.1
L	15428	13 49	2398	64.4	5.0	12/5/2	000	2.00	6582.87	2.9	6584.87	55	6527.0 A	35-55	55.9
DM	15426	28 49	0035	62.8	5.0	12/14/2	000 8	52.00	6523.08	3.0	6575.08		A	-	-i
DN	15427	76 49	0020	66.7	4.0	12/14/2	000 8	51.52	6525.14	3.7	6576.66		A	- `	
DNR	15427	79 49	0031	79.7	4.0	12/5/2	000 8	51.80	6525.26	3.3	6577.06		A	-	
DO	15428	74 49	0049	75.8	5.0	12/5/2	000 6	55.20	6525.13	1:6	6590.33	75	6513.7 A	65-75	[.] 11.4
DP	15427	54 49	1012	79.8	5.0	6/26/2	002 5	53.46	6526.25	3.5	6579.71	-	A	-	·
DQ	15425	92 49	1006	85.3	5.0	7/11/2	002 4	18.10	6528.33	2.2	6576.43		— A	-	
DR	15428	84 48	9966	87.8	5.0	12/5/2	000 E	6.05	6524.78	2.7	6590.83	85	6503.1 A	65-85	21.6
DS	15428	76 49	0118	87.0	5.0	8/2/1	999 e	65.22	6523.59	.9	6588.81	77	6510.9 A	62-77 ·	12.7
DT	15428	71 48	9293	72.3	5.0	12/5/2	000 5	59.80	6524.01	2.7	6583.81	99	6482.1 A	59-99	41.9
DU	15428	79 49	0380	84.6	5.0	7/6/1	988 5	51.56	6539.51	2.9	6591.07	81	6507.2 A	61-81	32.3
DV	15428	26 49	0702	80.0	5.0	8/28/20	006 5	64.64	6530.96	2.9	6585.60	77	6505.7 A	60-80	25.3
DW	15428	18 49	2029	73.4	5.0	12/5/20	000	2.50	6586.16	3.6	6588.66	59	6526.1 A	45-60	60.1
DX	15428	38 49	1074	90.0	6.0	8/2/19	999 6	61.80	6530.18	1.0	6591.98	80	6511.0 A	60-90	19.2
DY	15427	37 49	2271 (65.7	5.0	12/5/20	000	1.50	6579.11	2.3	6580.61	56	6522.3 A	15-65	56.8
DZ	15428	34 49	1501	81.8 [.]	5.0	12/28/20	009 5	i0.05	6540.48	2.2	6590.53		A	-	
E	15405	53 49	0187 6	61.7	4.0	12/5/20	000	2.00	6566.94	1.7	6568.94	60	6507.2 A	44-64	59.7
EE	15428	53 49	0523	91.2	5.0	1/31/19	95 4	5.26	6542.85	0.6	6588.11	80	6507.5 A	50-90	35.3
F	15399			63.8	4.0	12/14/20			6532.06		6564.82	62	6501.6 A		30.4
FB	15404	17 48	8857 (62.0	4.0	9/14/20			6530.66		6565.66	58	6505.7 A	43-58	25.0
ΥF	15428		0017		4.0	6/21/19			6535.46		6576.54	124	6452.3 A		83.1
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			WELL	CA	SING	W	ATER LI	EVEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.		DEPTH (FT-MP)		AM N)	DATE	depth (FT-MP)	ELEV. (FT-MS		LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS (FT-LSD)	SATURATE
G	15386	72 48	8890	78.3	4.0	12/13/2	004	4.00	6559.09	2.0	6563.09	75	6486.1 A	50-80	73.0
GA	15386	57 48	9255		4.0	12/9/2	009	35.33	6527.46	1.8	6562.79	62	6499.0 A	45-65	28.5
GB	15386	54 48	9456	65.2	4.0	4/3/2	000	4.00	6558.99	1.9 [·]	6562.99	64	6497.1 A	45-65	61.9
GC	15386	50 48	9654		4.0	12/11/2	003	33.82	6531.35	2.5	6565.17	78	6484.7 A	60-80	46.7
GD	153864	46 48	9855	مەن	4.0	12/4/1	995	0.50	6565.12	1.8	6565.62	72	6491.8 A	55-75	73.3
GE	153863	37 48	9972	117:0	4.0	12/11/2	003	34.61	6531.66	2.4	6566.27	65	6498.9 A	50-120	32.8
GF	153863	32 49	0097	119.2	4.0	12/9/2	009	36.75	6529.26	1.8	6566.01	67	6497.2 A	50-120	32.1
GG	153866	52 48	9055	58.7	4.0	4/3/2	000	4.00	6559.13	1.8	6563.13	57	6504.3 A	48-68	54.8
GH	153880	07 48	9509	69.2	4.0	12/9/2	009	34.48	6528.28	1.3	6562.76	67	6494.5 A	55-65	33.8
GI	153863	31 49	0218	119.0	4.0	4/3/2	000	4.00	6561.85	1.5	6565.85	67	6497.4 A	50-120	64.5
GJ	153862	29 490)382 ·	119.2	4.0	4/3/2	000	4.00	6562.15	2.0	6566.15	65	6499.2 A	50-120	63.0
GK	153862	22 490)482 ·	115.7	4.0	12/9/2	009	36.10	6530.66	2.4	6566.76	67	6497. 4 A	50-120	33.3
GL	153861	4 490)701 [·]	119.3	4.0	4/3/2	000	4.00	6563.15	2.1	6567.15	71	6494.1 A	50-120	69.1
GM	153860)5 490)824 ·	118.2	4.0	4/3/2	000	4.00	6563.65	2.1	6567.65	69	6496.6 A	50-120	67.1
GN	153860)2 490)9 4 4 ·	116.5	4.0	7/22/2	009	36.68	6531.29	1.8	6567.97	70	6496.2 A	50-120	35.1
GO	153866	63 488	3973	122.3	4.0	4/3/20	000	4.00	6559.00	1.6	6563.00	75	6486.4 A	50-120	72.6
GP	153864	9 489	752 1	121.4	4.0	12/5/20	000	5.00	6559.87	2.1	6564.87	68	6494.8 A	50-120	65.1
GQ	153859	9 491	067	70.0	4.0	12/9/20)09	1.70	6566.46	0.9	6568.16	71	6496.3 A	50-70	70.2
GR	153861	9 490	619	85.0	4.0	12/23/19	91 :	36.55	6528.66	1.0	6565.21	75	6489.2 A	50-85	39.5
GS	153859	7 491	408	86.4	5.0	12/5/20	000 :	33.00	6541.31	2.0	6574.31	80	6492.3 A	50-85	49.0
GT	153853	4 491	565	84.0	5.0	12/5/20	00	8.30	6567.87	2.1	6576.17	76	6498.1 A	60-84	69.8
GU	153836	7 491	854	80.0	5.0	3/7/20	02 ⁻	15.00	6560.65	2.0	6575.65	73	6500.7 A	60-80	60.0
GV	153770	1 491	428	83.0	5.0	12/9/20	109 - 5	51.08	6526.30	2.5	6577.38	74	6500.9 A	62-82	25.4
GW1	153975	5 490	530	73.0	5.0	12/9/20	09 3	33.25	6532.02	1.0	6565.27	65	6499.3 A	48-73	32.8
GW2	153947	1 490	497	75.0	5.0	12/9/20	09 3	34.35	6531.73	1.0	6566.08	68	6497.1 A	47-75	34.7
GW3	153953	2 490	835	72.0	5.0	5/4/19	93 3	34.42	6531.86	1.0	6566.28	62	6503.3 A	45-72	28.6
Н	153870	3 490	582	69.3	4.0	12/23/19	91 3	37.93	6528.65	1.8	6566.58	69	6495.8 A	50-70	32.9
	153931	9 490	954	70.0	4.0	6/22/20	09 3	3.39	6533.81	1.6	6567.20	68	6497.6 A	52-72	36.2
ļ	154017	4 491	302	65.6	4.0	12/5/20	00	6.00	6564.19	3.4	6570.19	56	6510.8 A	46-68	53.4
J1	154008	2 491	585	57.0	6.0	12/5/20	00 1	8.80	6553.05	3.8	6571.85	55	6513.1 A	50-57	40.0
12	154027	1 491	013	58.0	6.0	12/5/20	00 2	6.00	6544.19	2.9	6570.19	55	6512.3 A	50-58	31.9
13	1540414		499	70.0	6.0	12/5/20			6541.74	2.6	6569.14	66	6500.5 A		41.2
14	1540643			80.0	6.0	12/5/20			6551.52	3.9	6569.52	68	6497.6 A		53.9
15	1540728		747	65.0	6.0	12/5/20			6559.24	2.8	6569.79	61	6506.0 A		53.2
16	1540919			67.0	6.0	12/5/20			6563.00	3.7	6570.10	65	6501.4 A		61.6
17	1540168			61.9	5.0	12/5/20			6550.88	2.1	6570.38	53	6515.3 A		35.6
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			WELL	CASI	NG	W	ATER LE	VEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.		T. DEPTH	DIA	M		DEPTH (FT-MP)	ELEV.		LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS	SATURATE
J8	15403	318	492064	63.2	5.0	12/5/2	000	23.30	6547.49	2.4	6570.79	52	6516.4 A	35-61	31.1
J9	15401	01	491759	68.0	5.0	12/5/2	000	24.60	6546.60	2.0	6571.20	58	6511.2 A	36-68	35.4
J10	15401	38	491436	66.0	5.0	12/5/2	000	18.00	6552.91	3.5	6570.91	36	6531.4 A	66-	21.5
J 1 1	15405	545	490909	66.0	5.0	12/5/2	000	12.00	6557.86	2.0	6569.86	55	6512.9 A	36-66	45.0
J12	15408	27	490466	70.0	5.0	12/5/2	000	18.44	6551.86	3.0	6570.30	60	6507.3 A	40-70	44.6
J13	15404	51	492218	55.0	5.0	2/5/2	002	4.00	6564.40	1.8	6568.40	46	6520.6 A	15-55	43.8
J14	15405	85	492367	55.0	5.0	2/5/2	002	12.90	6556.08	1.7	6568.98	44	6523.3 A	15-55	32.8
J15	15407	'19	492521	55.0	4.0	2/5/2	002	3.10	6566.53	2.2	6569.63	46	6521.4 A	15-55	45.1
JC	15402	15	491240	60.0	5.0	12/5/2	000	22.10	6546.34	1.8	6568.44	50	6516.6 A	35-55	29.7
к	15407	'30	491590	61.7	4.0	8/12/2	002	2.00	6571.51	3.8	6573.51	60	6509.7 A	44-64	61.8
K2	15407	36	491587	58.9	4.0	7/15/2	005 ·	19.40	6552.81	2.5	6572.21	58	6511.7 A	46-56	41.1
K3	15407	'44	491571	56.7	2.0	7/15/2	005	19.20	6551.47	1.3	6570.67	·	A	53-58	·
K4	15412	11	492371	86.2	5.0	10/6/2	009 8	B1.40	6520.62	2.5	6602.02	80	6519.5 A	65-85	1.1
K5	15412	69	491935	86.4	5.0	10/6/2	009	52.79	6548.94	2.8	6601.73	80	6518.9 A	55-85	30.0
K6	15406	89	491459	58.0	5.0	3/6/2	002 ⁻	13.00	6557.07	2.0	6570.07	·	— A	33-58	
7	15412	32	492237	86.0	5.0	10/6/2	009 - 6	65.24	6536.29	2.0	6601.53	79	6520.5 A	56-86	15.8
K8	15412	50	492081	86.0	5.0	10/6/2	009 8	58.22	6542.27	2.0	6600.49	78	6520.5 A	66-86	21,8
K9	15412	87	491787	86.0	5.0	10/6/2	009 6	65.48	6534.86	2.0	6600.34	79	6519.3 A	56-86	15.5
K10	15413	05	491638	87.0	5.0	10/6/2	009 7	76.60	6524.21	2.0	6600.81	81	6517.8 A	47-87	6.4
K11	15413	25	491490	84.0	5.0	10/6/2	009 7	73.70	6526.91	2.0	6600.61	78	6520.6 A	64-84	6.3
KA	15409	59	491331	67.8	5.0	8/12/2	002 1	13.00	6559.19	1.9	6572.19	65	6505.3 A	42-72	53.9
КВ	15408	93	491406	61.8	5.0	8/12/2	002	0.60	6571.05	0.8	6571.65	60	6510.9 A	40-70	60.2
кс	15408	26	491477	68.6	5.0	8/12/2	002	0.50	6569.81	0.7	6570.31	59	6510.6 A	42-72	59.2 ·
KD	15406	27	491701	62.1	5.0	8/12/2	002	1.10	6569.12	0.6	6570.22		A	40-70	
KE	15405	66	491776	60.8	5.0	8/12/2	002	9.10	6563.18	2.5	6572.28		A	40-70	
KEB	15405	70	491487	59.9	5.0	7/20/2	009 2	25.21	6544.52	1.5	6569.73	50	- 6518.2 A	40-60	26.3
KF	15408	70	491169	63.5	5.0	7/20/2	009 2	28.49	6541.72	2.2	6570.21	50	6518.0 A	30-60	23.7
KM	15406	71	491444	52.4	5.0	3/6/2	002 1	2.20	6557.57	2.2	6569.77		— A	-	
KN	15407	34	491492	50.1	5.0	10/11/2	002	8.36	6561.23	2.3	6569.59		— A	-	
κz	15411	00	491183	58.4	5.0	12/28/20	009 3	3.16	6538.56	1.2	6571.72		A	-	
L	15389	70	492150	67.0	4.0	10/6/20	009 5	50.13	6524.84	0.8	6574.97	59	6515.2 A	46-66	9.7
L5	153994	46	492730	60.2	5.0	10/6/20	009 2	28.00	6548.07	1.3	6576.07	50	6524.8 A	25-55	23.3
L6	15405	26	493110	51.1	5.0	10/6/20	009 2	8.31	6546.33	2.1	6574.64	50	6522.5 A	25-55	23.8
L7	15401	13	492842	67.8	5.0	10/6/20)09 6	5.00	6511.61	2.3	6576.61	62	6512.3 A	36-66	0.0
L8	15397			73.9	5.0	10/6/20		1.00	6525.49	2.1	6576.49	65	6509.4 A		16.1
9	15395			74.9	5.0	10/6/20		2.06	6535.17	2.2	6577.23	64	6511.0 A		24.1
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	•		WELL	. Ç/	ASING	w	ATER LE	VEL		MP Above		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.	EAST. COORD.	DEPTH (FT-MP		DIAM (IN)	DATE	Depth (FT-MP)		L)	lsd (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS (FT-LSD)	SATURATE THICKNES
L10	15392	50 492	2310	74.2	5.0	10/6/2	009	46.81	6530.02	2.0	6576.83	63	6511.8 A	53-73	18.2
M1	15427	97 489	9157	103.4	4.0	1/3/1	989	79.80	6505.17	1.5	6584,97	120	6463.5 A	66-106	41 .7
M2	15427	85 489	9159	40.4	4.0	1/20/1	995 3	34.85	6541.41	1.4	6576.26		A	-	
М3	15428	05 489	9151	105.3	4.0	7/14/2	008 (60.23	6515.87	1.0	6576.10		A	79-99	
M3R	15429	26 489	9078	115:0	5.0	12/15/2	004	50.70	6529.56	2.1	6580.26	108	6470.2 A	55-115	59.4
M4	15428	04 489	9134	81.8	5.0	10/31/2	000	56.72	6521.54	3.7	6578.26		A	78-82	
M5	15423	60 489	080	92.3	5.0	12/9/2	009 4	42.02	6533.32	3.2	6575.34	84	6488.1 A	60-90	45.2
M6	15430	97 486	674	110.0	5.0	12/9/2	009 6	52.16	6512.88	2.2	6575.04	65	6507.9 A	60-110	5.0
M7	15427	90 486	523	83.0	5.0	12/9/2	009 . 5	57.91	6514.94	2.4	6572.85	71	6499.4 A	63-83	15.5
M8	15429	60 486	567	83.0	5.0	9/5/2	000 3	33.71	6541.52	2.4	6575.23	57	6515.8 A	53-83	25.7
M9	15433	10 486	699	103.0	5.0	12/9/2	009 C	53.21	6513.60	3.5	6576.81	78	6495.3 A	63-103	18.3
M10	15436	77 486	5723	88.0	5.0	12/9/2	009 e	61.20	6512.16	2.3	6573.36	86	6485.1 A	58-88	27.1
M11	15423	58 486	486	118.0	, 5.0	12/8/2	003 5	53.98	6519.24	3.2	6573.22	109	6461.0 A	58-118	58.2
M12	15421	74 487	209	124.0	5.0	12/5/2	000	3.87	6569.64	2.5	6573.51	118	6453.0 A	57-124	116.7
M13	15424	50 487	336	117.0	5.0	12/5/2	000 2	9.81	6546.35	3.0	6576.16	108	6465.2 A	57-117	81.2
M14	15426	61 487	216	117.0	5.0	12/5/2	000 2	9.42	6547.75	2.7	6577.17	109	6465.5 A	57-117	82.3
M15	154287	72 487	094	102.0	5.0	12/5/2	000	3.71	6575.37	3.5	6579.08	93	6482.6 A	52-102	92.7
M16	15432	52 485	112	93.3	5.0	12/10/2	009 6	i1.54	6509.05	1.4	6570.59	100	6469.2 A	60-100	39.9
MA	154129	90 487	767	85.0	4.0	12/9/2	009 4	2.40	6529.82	1.0	6572.22	. 85	6486.2 A	70-85	43.6
MB	154129	96 487	512	90.0	4.0	9/5/2	000	2.05	6570.01	1.0	6572.06	. 85	6486.1 A	60-90	84.0
мс	154130	487	264	100.0	4.0	12/9/20)09 4	5.06	6527.00	1.0	6572.06	95	6476.1 A	70-100 ⁻	50.9
MD	154131	1 487	050	105.0	4.0	9/5/20	00	2.00	6569.46	1.0	6571.46	105	6465.5 A	75-105	104.0
ME	154153	486	934	105.0	4.0	9/5/20	000	1.61	6569.31	1.0	6570.92	105	6464.9 A	75-105	104.4
MF	154175	67 486	808	110.0	4.0	12/9/20	09 4	8.43	6523.85	1.0	6572.28	110	6461.3 A	90-110	62.6
MG	154197	2 486	694	110.0	4.0	9/5/20	000	1.72	6571.36	1.0	6573.08	110	6462.1 A	90-110	109.3
MH	154220	8 486	569	110.0	4.0	12/9/20	09 5	2.75	6521.17	1.0	6573.92	110	6462.9 A	90-110	58.3
MI	154248	6 486	413	110.0	4.0	9/5/20	000	2.24	6574.03	1.0	6576.27	110	6465.3 A	90-110	108.8
MJ	154268	2 486	350	60.0	4.0	12/9/20	09 5	4.07	6518.87	1.8	6572.94	60	6511.1 A	40-60	7.7
MK	154337	3 486	324	57.0	4.5	12/3/20	108 5	9.90	6513.89	1.5	6573.79	92	6480.3 A	-	33.6
ML	154390	2 486	691	76.0	5.0	12/9/20	109 5 ¹	0.29	6522.41	2.3	6572.70	80	6490.4 A	56-76	32.0
MM	154415	4 486	324	63.0	5.0	9/5/20	00	3.46	6573.99	2.4	6577.45	50	6525.1 A	33-63	48.9
MN	154461	3 486	325	63.0	5.0	12/18/19	96 64	4.15	6513.41	1.9	6577.56	42	6533.7 A	23-63	0.0
٥N	154362	0 485	518	88.0	4.5	12/10/20	09 6	3.48	6509.41	2.0	6572.89	80	6490.9 A	45-85	18.5
MP	154416	4 4854	492	80.0	5.0	12/18/19	96 63	2.66	6511.82	2.1	6574.48	50	6522.4 A	33-63	0.0
٨Q	154317	3 4863	326	98.0	5.0	12/9/20			6510.06	1.6	6574.30	88	6484.7 A		25.4
٨R	154260			100.0		12/10/20			6500.29		6566.26	100	6464.5 A		35.8
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(cont'd.)

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	NORTH.	E A CT	W		CASING			R LEVEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	COORD.	COOR	DE: D. (FT	ртн - M P)	DIAM (IN)	DATE		TH ELE MP) (FT-N		LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)		SATURATEI THICKNESS
MS	15426	607	485570	82	.0 5.0	0 12/10/	2009	61.25	6509.42	1.5	6570.67	89	6480.2 A	52-82	29.3
MT	15432	221	483531	98	.0 4.	5 10/14/	2009	55.04	6512.39	2.3	6567.43	87	6478.1 A		34.3
MU	15444	61	487143	80	.0 5.0) 12/9/	2009	37.20	6536.99	1.5	6574.19	72	6500.7 A		36.3
ΜV	15426	18	484418	105	.0 4.5	5 12/8/	2008	67.55	6502.23	1.3	6569.78	95	6473.5 A		28.7
MW	15438	02	486346	85	.0 5.0) 12/9/	2009	65.91	6509.00	1.9	6574.91	83	6490.0 A		19.0
MX	15412	87	486244	103	.0 5.0) 12/14/	2009	52.00	6516.61	1.7	6568.61	94	6472.9 A	63-103	43.7
MY	15422	00	486213	112	.0 5.0	12/14/	2009	57.26	6516.30	3.0	6573.56	102	6468.6 A	72-112	47.7
MZ	15434	85	486757	92	.0 5.0) 12/9/	2009	65.49	6511.15	3.0	6576.64	84	6489.6 A	60-92	21.5
N	15451	01 4	489665	92	.0 4.0	11/3/2	2008	44.48	6539.49	0.9	6583.97	80	6503.1 A	54-94	36.4
NA	15450	00 ·	491488	91	.4 5.0	10/28/2	2008	49.67	6541.31	1.1	6590.98	80	6509.9 A	50-90	31.4
NB	15450	00 4	491296	96.	4 5.0	10/28/2	2008	48.31	6544.99	3.5	6593.30	.80	6509.8 A	50-90	35.2
NC	15452	20	491282	95.	.0 4.0	12/14/2	2009	44.91	6540.92	0.8	6585.83	. 85	6500.0 A	65-95	40.9
ND	15459	27 4	494872	70.	0 4.0	9/21/2	2009	45.70	6547.19	1.1	6592.89	65	6526.8 A	50-70	20.4
NE5	154423	79 4	192332	`' 156.	8 5.0	4/3/2	007	57.00	6610.00	3.2	6667.00	150 150	T 6513.8 A	50-110 🛒 / 135-155	
W5	15444(08 4	189433	149.	8 5.0	5/29/2	007	42.72	6614.86	2.7	6657.58	155		39-79	·
												155	6499.9 A	119-159	115.0
0	154506	60 4	92725	69.	9 4.0	10/28/2	800	43.61	6544.22	1.3	6587.83	77	6509.5 A	40-70	34.7
Р	154669)1 4	91058	109.1	1 4.0	9/15/2	009	47.88	6539.38	1.7	6587.26	107	6478.6 A	82-112	60.8
P1	154701	74	91060	105.	0 6.0	11/28/2	000	55.75	6536.72	0.8	6592.47	105	6486.7 A	60-105	50.1
P2	154655	5 4	90912	105.0	6.0	3/6/2	009	60.18	6529.61	0.9	6589.79	105	6483.9 A	60-105	45.7
P3	154615	i9 4	90785	95.0) 5.0	12/10/2	009	49.24	6540.71	2.2	6589.95	85	6502.8 A	55-95 ,	38.0
P4	154650	4 4	91899	92.0) 5.0	12/10/2	009	47.76	6541.76	3.6	6589.52	84	6501.9 A	52-92	39.8
PM	154142	64	90292	81.9	9 4.0	1/12/2	004	12.33	6555.09	1.8	6567.42		A	-	
Q	154869	34	92153 、	98.3	3 4.0	10/12/2	009	47.03	6546.79	2.3	6593.82	100	6491.5 A	72-102	55.3
R	155037	2 4	94514	85.0	4.0	10/12/2	009	41.70	6562.33	0.3	6604.03	95	6508.7 A	60-90	53.6
S	154387	1 4	88816	72.2	2 4.0	12/9/2)09	44.11	6537.06	2.0	6581.17	75	6504.2 A	52-72	32.9
51	154328	8 4	88401	85.0	2.0	9/28/20	09	40.97	6534.22	5.3	6575.19	85	6484.9 A	60-85	49.3
S2	154312	7 4	B8299	100.0	3.0	12/28/20	09	39.82	6533.90	2.0	6573.72	100	6471.7 A	90-100	62.2
S3	154285	7 4	88714	122.6	5.0	12/9/20	09	41.98	6532.80	6.2	6574.78	116	6452.6 A	80-120	80.2
64	1543344	4 48	38359	112.4	5.0	12/9/20	09	40.48	6534.81	2.3	6575.29	108	6465.0 A	50-110	69.8
55	1543269	9 48	38923	115.0	5.0	12/28/20	09	46.61	6528.08	1.0	6574.69	105	6468.7 A		59.4
55R	1543150) 48	38938	115.0	5.0	6/29/20	09	7.48	6573.01	1.9	6580.49	109	6469.6 A		103.4
66	154351	5 48	38874	113.2	5.0	1/3/20	00	55.85	6524.22	1.3	6580.07	105	6473.8 A		50.5
67	1543763	3 48	8874	97.0	5.0	1/4/19	99	57.38	6522.51	1.0	6579.89	82	6496.9 A		25.6
68	1543968	3 48	8879	43.8	5.0	8/22/19	95	43.28	6537.06		6580.34	40	6539.3 A		0.0

(cont'd.)

			WELI		ASING	w	ATER LE			MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.		dept . (FT-M		DIAM (IN)	DATE	DEPTH (FT-MP)		L)	LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS (FT-LSD)	SATURATE
S11	15447	793 4	88150	76.2	5.0	12/9/2	009 3	32.57	6545.82	1.9	6578.39	70	6506.5 A	48-78	3 9.3
S12	15432	297 4	88628	93.0	5.0	12/9/2	009 2	26.30	6552.55	2.1	6578.85	80	6496.7 A	53-93	55.8
SA	15431	22 4	88811	123.7	5.0	6/29/2	009 4	45.77	6534.54	1.0	6580.31	115	6464.3 A	100-130	70.2
SB	15433	371 4	88811	125.0	5.0	2/23/2	009 4	48.50	6532.59	0.9	6581.09	115	6465.2 A	100-130	67.4
SC	15436	617 4	88815	105.4	5.0	12/5/2	000 క	57.11	6521.69	1.2	6578.80	103	6474.6 A	55-105	47.1
SD	15434	90 4	B8564	90.1	5.0	2/23/2	009 4	4 1.50	6536.81	0.6	6578.31	107	6470.7 A	50-110	66.1
SD4	15434	97 4	88556	95.0	5.0	2/23/2	009 4	46.17	6532.60	1.1	6578.77	95	6482.7 A	45-95	49.9
SE	15433	801 4	88550	111.8	5.0	2/23/2	009	7.88	6570.11	0.5	6577.99	88	6489.5 A	50-90	80.6
SE4	15433	08 4	B 85 60	105.3	2.0	2/23/2	009 4	45.78	6532.22		6578.00		A	-	
SE6	15432	44 4	88615	92.0	5.0	12/28/2	009	0.24	6578.67	2.3	6578.91		A	-	-
SM	15437	48 48	38566	86.0	5.0	12/28/2	009 4	12.26	6536.48	0.7	6578.74		A	-	
SN	15437	52 48	38716	67.5	4.0	12/28/2	009 4	13.63	6535.63	1.1	6579.26		A	-	
so	15436	52 48	38381	92.3	5.0	12/28/2	009 4	3.57	6535.22	0.6	6578.79		A	-	
SP	15436	30 48	38531	94,4	4.0	12/28/2	009 4	3.28	6535.38	2.0	6578.66		A	-	
SQ	15435	07 48	38814	95.0	5.0	6/29/2	009 5	59.50	6519.70	0.9	6579.20	95	6483.3 A	55-95	36.4
SR	15436	11 48	38669	95.0	5.0	9/21/2	007 4	7.54	6531.65	0.8	6579.19	95	6483.4 A	50-90	48.3
SS	15433	74 48	38666	101.0	5.0	2/23/2	009 4	8.66	6529.72	1.2	6578.38	90	6487.2 A	51-101	42.5
ST	15432	15 48	38688	97.0	5.0	2/23/2	009 4	8.90	6530.41	2.2	6579.31	96	6481.1 A	55-97	49.3
* SU	15429	46 48	8953	110.0	5.0	9/5/19	995 3	5.60	6542.50	0.7	6578.10	110	6467.4 A	50-110	75.1
SUR	15429	91 48	8968	115.0	5.0	7/14/2	008 5	8.28	6522.44	2.6	6580.72	106	6472.1 A	35-115	50.3
sv	15436	76 48	8813	78.2	6.0	6/29/20	009 4	5.66	6533.59	1.7	6579.25	100	6477,6 A	55-105	56.0
SW	15437	83 48	88812	81.9	6.0	5/19/20	008 5	0.31	6530.98	2.9	6581.29	75	6503.4 A	35-80	27.6
SX	15445	10 48	9025	45.0	5.0					1.0	6581.49	40	6540.5 A	20-40	
SZ	15443	67 48	8833	62.6	5.0	12/9/20	009 3	6.79	6544.68	2.2	6581.47	60	6519.3 A	40-70	25.4
T	15425	36 49	2260	70.2	4.0	8/24/20	009 3	4.30	6544.93	2.4	6579.23	68	6508.8 A	61-71	36.1
T1	15432	85 49	0027	<u> </u>	5.0	12/6/20	002 10	2.40	6561.51	1.0	6663.91	161	6501.9 A	121-171	59.6
T2	15435	38 48	9303	186.0	5.0	8/24/20	009 12	1.38	6543.44	1.6	6664.82	180	6483.2 A	100-186	60.2
Τ4	15433	40 48	9699	205.0	5.0	8/24/20	09 7	0.26	6587.48	2.9	6657.74	175	6479.8 A	145-205	107.6
T5	15433	07 49	0289	182.0	5.0	8/24/20	009 11	9.29	6538.04	3.1	6657.33	151	6503.2 A	122-182	34.8
T6	15432	82 49	0655	160.0	5.0	8/24/20	09 12	0.88	6537.89	2.9	6658.77	156	6499.9 A	130-160	38.0
T7	15432	72 49	1484	160.0	5.0	1/26/20)09 11	9.60	6540.07	2.0	6659.67	142	6515.7 A	130-160	24.4
T8	15432	96 49	1914	162.0	5.0	1/26/20	009 12	0.00	6541.61	2.6	6661.61	158	6501.0 A	132-162	40.6
Т9	154334	47 49	2337	141.0	5.0	8/24/20	09 11	9.76	6544.19	3.3	6663.95	138	6522.7 A	121-141	21.5
T10	154343			148.0	5.0	8/24/20			6553.56		6659.96	142	6515.7 A	108-148	37.9
T11	154458			193.0	5.0	8/24/20			6540.29		6656.81	160	6494.1 A	113-193	46.2
T12	154458			200.0	5.0	8/24/20			6574.42		6657.23	170	6484.7 A		89.7
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(cont'd.)

	NODTU	EAST. COORD.			CASING	w	ATER LE			MP ABOVE	/E MPELEV.	DEPTH TO Base of Alluvium (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)		SATURATED THICKNESS
	NORTH. COORD.			epth T-MP)	DIAM (IN)	DATE	(FT-MP)	ELEV. (FT-MS	L)	LSD (FT)					
T13	15445	34	490619	160	.0 5.0						6657.37	160	A	120-160	
T14	15445	65 [.]	491071	155	.0 5.0						6660.13	155	A	125-155	
T15	15444	80	491953	150	.0 5.0						6665.29	150	A	120-150	
T16	15442	76	492718	140	.0 5.0					660.0	6659.98	132	-132.0 A	120-140	
T17	15440	80	489430	183	.0 5.0	1/28/2	009 1	20.38	6536.53	2.6	6656.91	170	6484.3 A	143-183	52.2
T18	15439	77	490333	195	.0 5.0	1/28/2	009 1	23.36	6541.80	2.9	6665.16	162	6500.3 A	115-195	41.5
T19	15439	58	490722	167	.0 5.0	1/28/2	009 1	24.48	6543.28	2.5	6667.76	162	6503.3 A	137-167	40.0
T20	15439	35	491048	170	.0 5.0	1/28/2	009 1	29.86	6540.83	1.5	6670.69	162	6507.2 A	140-170	33.6
T21	15439	51	491882	170	.0 5.0	1/28/2	009 1	09.60	6560.40	1.3	6670.00	163	6505.7 A	140-170	54.7
T22	15438	76	492311	165	.0 5.0	8/24/2	009 1	10.84	6556.35	2.1	6667.19	160	6505.1 A	120-165	51.3
T23	15439	01	492805	140	.0 5.0						6661.11	140	A	120-140	-
T36	15437	35	489688	170	.0 5.0						6655.44	170	A	130-170	
T39	15444	98	491669	150	.0 5.0						6665.31	150	A	120-150	
T40	15438	19	491466	170	.0 5.0	1/28/2	009 1	28.86	6541.41	2.3	6670.27	165	6503.0 A	140-170	38.4
T41	15432	78	491079	160	0 5.0	1/26/2	009	83.00	6576.96	3.2	6659.96	155	6501.8 A	130-160	75.2
A	15424	71	492426	62	4 5.0	9/21/2	009	35.31	6544.99	2.4	6580.30	55	6522.9 A	35-65	22.1
тв	15423	51	492616	64	4 5.0	9/21/2	009	38.01	6545.56	1.9	6583.57	55	6526.7 A	35-65	18.9
W	15423	02	487297	99.	3 4.0	12/9/2	009 4	45.15	6526.99	0.3	6572.14	117	6454.8 A	58-118	72.1
W2	15422	51	486654	79.	1 4.0	3/2/1	998	56.21	6515.29	0.9	6571.50		A	-	
WN4	15439	58	489961	142.	4 5.0	12/2/2	009	66.80	6595.98	3.0	6662.78	165	T	40-100	
												165	6494.8 A	50-190	101.2
WR1	15412		488529	-	5.0	6/27/1	989 . 4	46.54	6521.86	0.8	6568.40		A	-	
WR1R	154130)2	488536	85.	0 5.0	12/5/2	000	28.62	6539.85	0.0	6568.47	85	6483.5 A	-	56.4
WR2	15412	30	488678	94.	1 5.0	12/5/2	000	2.52	6566.07	0.9	6568.59	85	6482.7 A	65-95	83.4
WR3	154149	90	488671	82.	3 5.0	12/5/20)00 :	32.96	6536.58	2.7	6569.54	83	6483.8 A	63-93	52.7
WR4	15417	38	488678	62.	0 5.0	12/5/20	, 000	1.92	6570.89	0.0	6572.81		A	-	
WR5	15418	13	488683	72.	4 5.0	12/5/20)00 (38.69	6532.54	0.6	6571.23	80	6490.6 A	60-80	41.9
WR6	154190)2	488566	96.	8 5.0	12/5/20	00	3.04	6569.99	1.3	6573.03	84	6487.7 A	55-85	82.3
WR7	154199	97	488456	97.	3 5.0	12/5/20	000 . 3	38.91	6534.82	2.0	6573.73	84	6487.8 A	55-85	47.0
WR8	154209	95	488328	110.	2 5.0	11/10/20	08 2	26.40	6546.20	0.4	6572.60	100	6472.2 A	50-100	74.0
WR9	154218	85	488217	111.	3 5.0	12/5/20	000 4	16.82	6526.23	0.8	6573.05	100	6472.3 A	50-100	54.0
WR10	154238	39	487961	120.	6 5.0	1/29/20	03 -	14.84	6558.35	0.7	6573.19	110	6462.5 A	60-110	95.9
WR11	154258	6	487728	120.	5 5.0	1/29/20	103 1	4.88	6559.61	0.3	6574.49	110	6464.2 A	60-110	95.4
WR12	154128	10	488277	96.	7 4.0	11/12/20	07 3	80. 8 5	6537.34	1.1	6568.19	85	6482.1 A	55-85	55.2
WR13	154106	8	488861	70.1	0 5.0	12/5/20	00 1	8.98	6550.19	3.2	6569.17	60	6506.0 A	50-60	44.2
WR14	154063	8	488863	70.	0 5.0	5/28/20	03 1	5.50	6551.41	2.3	6566.91	61	6503.6 A	50-60	47.8

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TABLE 4.1-1. WELL DATA FOR THE HOMESTAKE ALLUVIAL WELLS.

(cont'd.)

			WELL	CAS	SING	w	ATER LE	VEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	North. Coord.		DEPTH (FT-MP)		AM		DEPTH (FT-MP)	ELEV.	-)	LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)		SATURATE THICKNES
WR15	15412	280 48	8016	70.0	4.0	5/28/2	003	10.90	6560.29	0.0	6571.19	75	6496.2 A	60-75	64.1
WR16	15430)51 48	7495 1	22.3	5.0	1/29/2	003	6.54	6566.24	1.9	6572.78	100	6470.9 A	40-120	95.4
WR17	15433	328 48	7485 1	24:4	5.0	1/29/2	003	2.45	6570.64	2.2	6573.09	75	6495.9 A	40-120	74.7
WR18	15435	597 48	7465	73.6	5.0	1/29/2	003	2.97	6569.94	2.2	6572.91	70	6500.7 A	20-70	69.2
WR19	15438	573 48	7458	87:8	5.0	1/29/2	003	3.31	6571.62	2.2	6574.93	74	6498.7 A	25-85	72.9
WR20	15440	59 48	7449 1	02,3	5.0	1/29/2	003	3.98	6570.49	2.1	6574.47	80	6492.4 A	42-102	78.1
WR21	15442	41 48	7449	88.9	5.0	1/29/2	003	6.28	6569.77	2.1.	6576.05	77	6497.0 A	28-88	72.8
WR22	15444	34 48	7462	91,5	5.0	1/29/2	003	3.44	6574.45	2.4	6577.89	86	6489.5 A	30-90	85.0
WR23	15446	32 48	7445	94:3	5.0	1/29/2	003	1.72	6574.75	2.2	6576.47	77	6497.3 A	32-92	77.5
WR24	15449	38 48	7438	89.2	5.0	1/29/2	003	2.04	6586.63	3.0	6588.67	82	6503.7 A	50-90	83.0
х	15405	12 49	1892	50:7	4.0	12/28/2	009 2	28.92	6542.69	1.7	6571.61		A	-	
X1	15406	71 49	2129	54.0	5.0	8/12/2	002	7.50	6654.71	3.9	6662.21	47	6611.3 A	37-47	43.4
X2	15408	36 49	2363	53.0	6.0	8/12/2	002	2.50	6569.43	1.9	6571.93	45	6525.0 A	40-45	44.4
X3	15409	92 493	2599	52.0	5.0	8/12/2	002	2.50	6570.78	2.0	6573.28	42	6529.3 A	32-42	41.5
X4	15412	10 49:	2814	54.0	5.0	8/12/2	002 [·]	3.10	6563.84	3.2	6576.94	45	6528.7 A	37-45	35.1
X5	15414	08 493	2821	44:0	6.0	8/12/2	002	7.80	6569.81	3.6	6577.61	35	6539.0 A	24-36	30.8
X6	15416	09 49:	2828	46.0	6.0	8/12/2	002	8.00	6570.72	3.5	6578.72	. 35	6540.2 A	22-37	30.5
X7	15418	08 493	2851	56.0	6.0	12/5/2	000	8.60	6571.83	3.4	6580.43	45	6532.0 A	32-46	39.8
X8	15420	07 492	2852	61.0	5.0	12/5/20	000 1	3.00	6568.76	3.4	6581.76	51 ·	6527.4 A	32-52	41.4
X9	15421	94 492	2852	61.0	5.0	12/5/20	000 2	27.00	6555.92	3.6	6582.92	51	6528.3 A	24-52	27.6
X10	15423	52 492	2835	61.0	5.0	8/12/20	002	4.00	6578.43	3.6	6582.43	53	6525.8 A	30-55	52.6
X11	15425	53 492	2782	57.0	5.0	12/5/20	000	0.50	6581.50	3.0	6582.00	53	6526.0 A	17-57	55.5
X12	15428	61 492	2852	57.0	5.0	12/5/20	000	0.50	6582.83	3.0	6583.33	53	6527.3 A	17-57	55.5
X13	15436	40 493	8665	56.0	5.0	4/9/20	002 4	0.76	6546.18	2.5	6586.94	51	6533.4 A	16-56	12.7
X14	15440	02 493	3777 .	56.0	5.0	4/9/20	002 3	9.80	6546.40	2.1	6586.20	49	6535.1 A	16-56	11.3
X15	15442	22 493	8800	57.0	5.0	4/9/20	002 4	0.54	6542.37	2.3	6582.91	51	6529.6 A	17-57	12.8
X16	15444	73 493	795	47.0 ·	5.0	4/9/20	02 4	0.64 6	6544.15	2.3	6584.79	47	6535.5 A	22-47	8.7
X17	15443	56 493	793	55.0	5.0	4/9/20	002 4	1.06 6	6544.78	3.3	6585.84	48	6534.6 A	35-55	10.2
X18	154459	93 493	569	57.0	5.0	10/20/20	09 3	7.76 6	548.32	2.9	6586.08	49	6534.2 A	37-57	14.1
X19	15447	53 493	437 (63.0	5.0	11/17/20	06 3	2.46 6	6552.74	4.2	6585.20	56	6525.1 A	33-63	27.7
X20	15448	55 493	256 7	71.0	5.0	11/17/20	06 4	0.15 €	545.58	5.0	6585.73	64	6516.8 A	31-71	28.8
X21	154360	06 493	894 5	55.Ó	5.0	12/5/20	100 3	8:99 6	547.34	2.7	6586.33	51	6532.6 A	35-55	14.7
X22	154387	74 493	946 5	56.0	5.0	12/5/20	00 3	9.21 6	546.49	2.6	6585.70	50	6533.1 A	36-56	13.4
X23	154406	64 494	012 5	56.0	5.0	12/5/20	00 3	8.96 6	546.98	2.8	6585.94	47	6536.1 A	36-56	10.8
X24	154424	4 494	011 5	56.0	5.0	12/5/20	00 3	9.94 €	545.78	2.6	6585.72	46	6537.1 A	36-56	8.7
X25	154444	15 494	042 5	53.0	5.0	12/5/20			546.22		6585.63	46	6536.9 A	33-53	9.3

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TABLE 4.1-1. WELL DATA FOR THE HOMESTAKE ALLUVIAL WELLS.

(cont'd.)

WELL NAME		WELL ST. DEPTH ORD. (FT-MP)	CASING DIAM (IN)	DE	er level PTH elev. -MP) (FT-MSL)	MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)	CASING PERFOR- ATIONS (FT-LSD)	SATURATED
X26	1544693	493702	53.0 5.0	12/5/2000	35.34 6552.30	2.8	6587.64	43	6541.8 A	33-53	10.5
X 2 7	1544953	493374	71.0 5.0	11/17/2006	39.75 6545.55	6.0	6585.30	64	6515.4 A	31-71	30.2
X28	1540545	491971	56.0 5.0	8/12/2002	8.30 6561.66	2.0	6569.96	48	6520.0 A	16-56	41.7
X29	1540735	492256	51.0 5.0	8/12/2002	4.00 6566.03	2.0	6570.03	43	6525.0 A	11-51	41.0
X30	1540897	492493	51.0 5.0	8/12/2002	3.00 6569.53	2.0	6572.53	43	6527.5 A	11-51	42.0
X31	1541052	492731	51.0 5.0	8/12/2002	8.00 6566.13	2.0	6574.13	44	6528.1 A	11-51	38.0
Y	1541025	491256	60.8 4.0	10/15/2002	15.20 6557.68	2.4	6572.88	57	6513.5 A	54-59	44.2
Z	1540290	490701	73.9 4.0	12/5/2000	5.00 6564.22	0.6	6569.22	68	6500.6 A	60-70	63.6

Note: A = Alluvial Aquifer, Base

M = Middle Chinle Aquifer, Top

T = Tailings Aquifer, Base

* = Well Abandoned

? = Uncertain Identity

TABLE 4.1-2. WELL DATA FOR THE ALLUVIAL AQUIFER BROADVIEW AND FELICE ACRES WELLS.

			WELL	CASING		• • • • • •	TER LE	VEL		MP ABOVE		DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD.		DEPTH (FT-MP)	DIAM (IN)			DEPTH	ELE\		LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)		SATURATE
						·····		Br	oadview						
0410	15374	59 48	9882 1	05:0	6.0	5/25/20	05	40.47	6519.19	0.0	6559.66	75	6484.7 A	90-105	34.5
0411	15374	00 48	9510	70.0	6.0	8/7/19	96	35.10	6524.90	0.0	6560.00	70	6490.0 A	65-70	34.9
0412	15379	40 48	8830		6.0					0.0	6561.00		A	-	
0413	15379	00 49	0100			4/27/19	94	35.25	6530.75	0.0	6566.00		A	-	
0421	15384	50 49	1100	88.0	5.0	1/30/19	96	37.58	6534.42	0.9	6572.00	92	6479.1 A	72-102	55.3
0422	15384	40 49	0810	80.0	4.0	4/6/19	94 :	32.82	6537.18	0.0	6570.00	75	6495.0 A	60-80	42.2
0423	15382	23 49	0926							0.0	6570.00		A	-	
0425	15384	30 49	0630	90.0	6.0	4/7/19	94 :	32.42	6534.58	0.0	6567.00	71	6496.0 A	50-90	38.6
0426	15382	30 49	0620 1	00.0		11/10/19	81 :	30.65	6534.35	0.0	6565.00	80	6485.0 A	80-100	49.4
0427	15384	50 49	0410 1	21.0	6.0	4/12/19	94 :	35.00	6535.00	0.0	6570.00	81	6489.0 A	62-120	46.0
0428	15383	67 49	0435 1	10.0	4.0					0.0	6570.00	66	6504.0 A	83-104	
0429	15382	10 49	0430 1	00.0	6.0	9/1/19	95 :	37.21	6532.79	0.0	6570.00	74	6496.0 A	58-75	36.8
0430	15384			45.0						0.0	6568.00	72	6496.0 A	-	
												72	6433.0 U	-	
0431	15380	45 49	0090 1	30.0	6.0	4/12/19	94 :	35.00	6533.00	0.0	6568.00	60	6508.0 A	125-130	25.0
												60	6450.0 U	125-130	83.0
0432	15382	10 48	9840							0.0	6565.00		A	-	
0433	15382	20 489	9620	90.0	4.0	5/2/199	97 3	36.05	6527.95	1.5	6564.00	75	6487.5 A	58-84	40.5
0435	15382	20 489	9300	85.0	6.0	3/25/200)3 3	34.48	6526.52	1.3	6561.00 .	85	6474.7 A	-	51.8
0438	15378	54 490	0840 1	20.0	4.0		_			0.0	6571.00	105	6466.0 A	70-100	
0439	153794	10 490	0490	97.0	4.0	8/7/199	96 3	39.80	6527.20	0.0	6567.00	75	6492.0 A	77-97	35.2
0440	153770	00 490	0230		•	. •				0.0	6566.00		A	-	
0441	153772	20 490	0090 1	16.0	6.0	1/30/199	95 3	35.19	6530.81	0.0	6566.00	78	6488.0 A	106-116	42.8
0442	153794	10 489	9840 1	0.00	4.0	8/7/199	6 3	87.15	6527.85	0.0	6565.00	80	6485.0 A	70-100	42.8
0443	153794	10 489	9280		4.0					0.0	6561.00	75	6486.0 A	60-80	
0444	153794	10 489	9180	30.0	4.0	5/18/199	4 2	28.84	6532.16	0.0	6561.00		A	-	
0445	153772	20 489	300 1	0.80	5.0					0.0	6561.00	79	6482.0 A	75-105	
0446	153783	io 488	960 1	10.0 (5.0	9/8/198	33 4	1.28	6518.72	0.0	6560.00	60	6500.0 U	60-95	18.7
												60	6500.0 A	60-95	18.7
0447	153749	0 490	480 14	1 2.0 (5.0	4/11/198	5 4	1.18	6526.82	0.0	6568.00	80	6488.0 A	120-142	38.8
												80	6430.0 U	120-142	96.8
0448	153740	0 489	100			-	-			0.0	6561.00		A	-	
0450	153744	8 490	763	´ 6	5.0	1/25/199	54	2.29	6528.71	0.0	6571.00	85	6486.0 A	70-105	42.7
0451	153770	0 490	600			-				0.0	0.00		A	-	
0452	153788	0 490	420 10	0.0 4	l.0	8/7/199	64	1.20	6525.80	0.8	6567.00	85	6481.2 A	40-100	44.6

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TABLE 4.1-2. WELL DATA FOR THE ALLUVIAL AQUIFER BROADVIEW AND FELICE ACRES WELLS.

	North. Coord.		T. D	VELL Epth T-MP)	CASING DIAM (IN)			R LEVEL PTH ELEV MP) (FT-M		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)	CASING PERFOR- ATIONS (FT-LSD)	SATURATEI THICKNESS
0453	15383	75	`490300) 11	0.0 4	4.0	7/1/2002	34.93	6533.07	0.9	6568.00	80	6487.1 A	60-110	46.0
* 0454	15379;	20	489025	5	4	1 .0				0.0	0.00		— A	-	
0455	153780	04	490737	,	0.0		~						— A	-	
0456	153824	40	490060) 30	0.0 8	5.0					6559.00		—A	-	-
SUB1	153762	20	489100)	4	1.0	4/20/2009	35.16	6525.84	0.0	6561.00		— A	-	<u> </u>
SUB2	153739	92	490370	1	4	1.0	5/4/2004	40.10	6527.47	0.0	6567.57		A	-	
SUB3	153828	80	489420	8	4.0 (6.0	12/14/2009	31.08	6525.99	0.0	6557.07	72	6485.1 A	56-72	40.9
SUB4	153844	40	489840) 10	0.0	1 .0	9/21/1978	49.11	6515.89	0.0	6565.00	78	6487.0 A	60-85	28.9
SUB5	153794	40	489470	8	6.0 4	1.0				0.0	6562.31	66	6496.3 A	55-80	
SUB6	153794	40	490090	8	2.0 4	1.0				0.0	6566.00	80	6486.0 A	52-82	
SUB7	153794	40	490630	9	3.0 4	1.0				0.0	6568.00	85	6483.0 A	78-98	
SUB8	153848	50	490210	15	D.O 8	5.0				0.0	6568.00	72	6496.0 A	60-90	
SUB9										0.0	0.00		A		
								<u>Feli</u>	ce Acres	,					
481	153835	50	490180	320).0 4	.0		-		0.0	6568.00	110 110	6458.0 A 6298.0 M		
0482	153698	31	489579	260).0 5	i.0	12/10/2009	38.37	6524.29	0.0	6562.66	80 80	6482.7 A 6352.7 M		41.6 171.6
0483	153658	36	489753	280).O 5	i.0	10/6/2009	53.11	6509.55	0.0	6562.66	40 40 40	6522.7 A 6497.7 U 6326.7 M	-	0.0 11.9 182.9
0490	153655	53	489752	6	3.0 4	.0	12/14/2009	38.98	6523.44	0.0	6562.42	75	6487.4 A	20-80	36.0
0491	153703	31	489658	63	3.0 4	.0	12/10/2009	40.41	6522.21	0.0	6562.62	40	6522.6 A	30-63	0.0
0492	153722	20	489280	60).0 4	.0	4/12/2006	35.46	6525.22	1.2	6560.68	55	6504.5 A	40-60	20.7
0495	153740	00	497100							0.0	6571.00		A	-	
0496	153465	50	489603	93	3.0 5	.0	12/14/2009	57.43	6505.09	1.6	6562.52	86	6474.9 A	53-93	30.2
0497	153503	39	489503	94	l.0 5	.0	12/14/2009	56.79	6505.83	2.0	6562.62	89	6471.6 A	64-94	34.2
0498	153466	51	488953	150).0 6	.0	12/14/2009	60.60	6499.99	2.0	6560.59	80 80	6478.6 M 6478.6 A		21.4 21.4
CW44	153504	18	488891	208	8.0 6	.0	12/10/2009	63.93	6496.81	2.5	6560.74	94 94	6464.2 A 6428.2 M		32.6 68.6

(cont'd.)

Note: A = Alluvial Aquifer, Base

M = Middle Chinle Aquifer, Top

T = Tailings Aquifer, Base

* = Well Abandoned

? = Uncertain Identity

TABLE 4.1-3. WELL DATA FOR THE ALLUVIAL AQUIFER MURRAY ACRES AND PLEASANT VALLEY WELLS.

	NORTH. COORD.	EAST. COORD.	WELL DEPTH (FT-MP	1 [ASING DIAM (IN)			LEVEL H ELEV P) (FT-M		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)	CASING PERFOR- ATIONS (FT-LSD)	SATURATEL THICKNESS
					- <u>-</u>				Murray				<u> </u>		
* 0801	15410	20 48	8600	100.0	4.0	7/15/2	2004	39.20	6528.53	0.0	6567.73	85	6482.7 A	80-100	45.8
0801F	15410	96 48	8431	90.0	5.0	11/4/2	2004	41.01	6528.04	3.0	6569.05	82	6484.1 A	60-90	44.0
0802	15407	65 48	8277	98.0	6.0	12/28/2	2009	37.51	6525.21	2.0	6562.72	81	6479.7 A	75-81	45.5
0803	154080	00 48	7430		6.0	9/19/1	1983	84.86	6476.14	0.0	6561.00	85	C	85-180	-
												85	6476.0 A	85-180	0.1
0804	154079	90 48	6790	137.0	6.0	2/24/2	2009	46.20	6515.80	0.0	6562.00	85	6477.0 A	125-136	38.8
0805	15408	18 48	6241	140.0	5.0	10/6/1	994	59.34	6507.66	0.0	6567.00	110	6457.0 A	100-140	50.7
0810	154024	44 48	6563	105.0	6.0					0.0	6562.00	81	6481.0 A	75-101	
081 1	154032	20 48	6373	140.0	4.0					0.0	6563.00	110	6453.0 A	100-140	
0815	153909	0 48	8100	255.0	4.0	5/22/1	991	29.14	6526.12	0.0	6555.26		A	-	
0844	153837	6 48	7002	75.0	4.0	12/12/2	2009	36.64	6519.49	1.2	6556.13	70	6484.9 A	35-75	34.6
0845	153728	0 48	7833	65.0	4.0	12/12/2	2009	36.72	6520.33	1.7	6557.05	55	6500.4 A	45-65	20.0
AW	154023	5 48	8015	156.0	6.0	12/14/2	2009	35.09	6528.34	0.1	6563.43	63	6500.3 A	-	28.0
												63	6463.3 U	66-155	65.0
HW	154092	0 48	7435	115.0	6.0	11/9/1	994	40.00	6517.00	0.0	6557.00	95	6462.0 A	60-94	55.0
								Pleas	sant Valle	¥					
0525	154128	3 48	6020		4.5	7/12/2	002	55.36	6514.64		6570.00		A	-	
0688	154125	7 48	3955	105.0	5.0	12/14/2	009	60.92	6501.70	2.9	6562.62	95	6464.7 A	65-105	37.0
0831	154009	0 48	6030			9/6/1	983	54.95	6506.05	0.0	6561.00		A	-	
0833	153933	5 48	5445	110.0	6.0	12/10/1	996	46.61	6511.39	0.0	6558.00	103	6455.0 A	60-90	56.4
0834	154025	9 48	4847	100.0	4.0					0.0	6560.00	80	6480.0 A	60-80	
0835	153961	0 48	4795	98.0	5.0	5/2/2	000	49.74	6509.26	0.0	6559.00	94	6465.0 A	73-94	44.3
0836	154025	0 48	4010	90.0	4.0					0.0	6558.00	80	6478.0 A	65-80	_
0838	154060	0 48	5640	100.0		7/22/1	995	49.03	6513.97	0.0	6563.00		A	-	
0839	154078	2 48	5371	100.0	5.0	12/19/1	994	50.00	6510.00	0.0	6560.00	94	6466.0 A	80-96	44.0
0840	154044	0 48	5360	98.0	6.0	9/8/1	983	47.32	6513.68	0.0	6561.00	94	6467.0 A	73-94	46.7
08À1	154083	5 48	5020	100.0		7/22/1	995	54.66	6506.34	0.0	6561.00		A	-	
0843	154141	1 48	5738	120.0	4.0	6/27/1	989	52.40	6517.60	0.0	6570.00	112	6458.0 A	100-110	59.6

Note: A = Alluvial Aquifer, Base

M = Middle Chinle Aquifer, Top

T = Tailings Aquifer, Base

* = Well Abandoned

? = Uncertain Identity

	North. Coord.		. DE	ell Pth -MP)	CASING DIAM (IN)	D			EVEL ELEV) (FT-M		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)		SATURATED THICKNESS
0520	15389	34	492935	7	5.0 5	01	2/14/20	09	51.92	6534.10	0.3	6586.02	68	6517.7 A	35-75	16.4
0521	15391	04	492588	7	5.0 5	0	9/23/20	09	52.33	6532.11	2.5	6584.44	65	6516.9 A	35-75	15.2
0522	15386	40	492437	7	7.0 5	0	9/23/20	09	52.68	6527.85	2.8	6580.53	68	6509.7 A	37-77	18.1
0523	15386	80	492896	7	4.0 5	0	9/10/20	02	2.00	6584.79	3.0	6586.79	62	6521.8 A	34-74	63.0
0524	15388	89	493173	7	8.0 5	0	1/28/20	03	3.47	6586.88	3.0	6590.35	70	6517.4 A	33-78	69.5
0531	15410	86	478262			1	0/30/19	96	79.24	6474.55	2.0	6553.79		A	-	
0532	15187	00	482400	21	4.0 -						0.0	6515.00		A	-	
* 0533				19	5.0 -						0.0	6520.00		A	-	
0538	15334	86	486899	17	0.0 6	01	2/12/20	09	81.12	6467.82	2.0	6548.94	95	6451.9 A	50-90	15.9
													95	6413.9 L	130-170	53.9
0539	15340	14	487596	21	0.0 6.	01	2/12/20	09	84.25	6471.07	2.0	6555.32	100	6453.3 A		17.8
													100	6453.3 A		17.8 92.8
0540	45044	0 5	400004			~ 4	0140100		co oo	0407.00	0.7	6555 0 4	100	6378.3 L		
0540	15341		488091				2/10/20		68.29	6487.62	2.7	6555.91	80	6473.2 A		14.4
0541	15398		477236	120			2/12/20		91.35	6464.27	2.0	6555.62			78-118	
0551	15362		479881	13!			2/14/20		00.07	6447.23	2.1	6547.30	115	6430.2 A		17.0
0553	15349		480563	130			2/14/20		04.42	6443.06	2.0	6547.48	128	6417.5 A		25.6 13.6
0554 0555	15349		479107	140			2/14/20	19 1	06.30	6440.87	1.9	6547.17	118	6427.3 A		13.0
			_	100									100		60-90	_
0556			_	100				_					95		60-90	
0557			-		5.0 5.								55		45-65	
0631	15322		483756	118			2/12/200		96.25	6444.85	2.2	6541.10	109	6429.9 A		15.0
0632	15318		483767	11(2/10/200		99.02	6442.28	1.4	6541.30	102	6437.9 A		4.4
0633	15414		479642				2/10/200		73.33	6484.23	0.0	6557.56	95	6462.6 A		21.7
0634	15416		480362	103			2/10/200)9	70.21	6489.86	2.8	6560.07	95	6462.3 A		27.6
0635	15353		478401		3.0 12.							6546.25		A		
0636	15453		476038	123			9/23/200		05.60	6467.84	2.3	6573.44	119	6452.1 A		15.7
0637	15454		474710	124			9/23/200		11.88	6463.32	2.5	6575.20	118	6454.7 A		8.6
0638	153962		493265		5.0 5.		2/14/200		46.74	6538.82	0.0	6585.56	65	6520.6 A		18.3
0639	15393		492961).0 5.		9/23/200		62.91	6524.97	2.5	6587.88	71	6514.4 A		10.6
0640	153779		491961		.0 5.		2/14/200		53.38	6526.59	2.2	6579.97	77	6500.8 A		25.8
0641	153649		491110	95			2/28/200		51.75	6521.61	2.5	6573.36	87	6483.9 A		37.8
0642	15361()4 4	490932	95	.0 5.) 2	2/28/200)7	52.61	6519.27	2.4	6571.88	89	6480.5 A		38.8
0643	153376	60 4	487386	108	.0 5.) 1(0/16/200)2	75.89	6475.44	1.5	6551.33	93	6456.8 A	58-108	18.6
0644	153348	81 4	485450	110	.0 5.0) 12	2/10/200	9	85.55	6458.35	2.0	6543.90	102	6439.9 A	55-110	18.4
0645	153292	24 4	\$85282	80	.0 5.) 12	2/11/200	6	80.00	6463.79	2.5	6543.79	70	6471.3 A	60-80	0.0

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(cont'd.)	
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	100		WELL	CASING)	W	ATER L	EVEL		MP ABOV	E	DEPTH TO BASE OF	ELEV. TO BASE OF	CASING PERFOR-	
	NORTH. COORD. C		DEPTH (FT-MP)	DIAM (IN)		DATE	Depth (Ft-Mp			LSD (FT)	MP ELEV. (FT-MSL)	ALLUVIUM (FT-LSD)	ALLUVIUM (FT-MSL)	ATIONS	SATURATED THICKNESS
0646	1533246	6 484	953 10	0.0	5.0	10/7/20)09	90.60	6452.75	1.5	6543.35	91	6450.9 A	60-100	1.9
0647	1536623	3 4783	308 14	0.0	4.5	12/9/20	009 1	05.96	6445.95	1.4	6551.91	132	6418.5 A	80-140	27.4
0648	1534730	478 3	843 12	0.0	4.5	12/9/20	09 1	20.00	6427.79	2.0	6547.79	120	6425.8 A	80-120	2.0
0649	1534730	479 7	798 12	4.0	4.5	12/9/20	09 1	03.18	6440.11	0.3	6543.29	115	6428.0 A	84-124	12.1
0650	1536779	4821	35 10	9.0	4.5	12/12/20	09	82.03	6465.08	2.2	6547.11	103	6441.9 A	89-109	23.2
0652	1531170) 4837	79 8	8.0	5.0	12/10/20	09	86.24	6451.91	1.5	6538.15	79	6457.7 A	60-88	0.0
0653	1533283	4865	70 20	6.0	6.0	12/10/20	09	79.85	6465.12	1.6	6544.97	97	6446.4 A	69-206	18.8
												97	6408.4 L	•	56.8
0654	1541994		36 12	0.0	4.5	12/10/20	09	72.78	6477.72	1.4	6550.50	106	6443.1 A	60-120	34.6
0655	1541620		30 9	6.0	8.0	12/14/20	09	72.61	6485.57		6558.18	88	A	21-84	
0656	1542578	4783	33 8	B.O a	8.0	10/23/20	07	75.10	6478.97		6554.07	88	A	6-88	
0657	1537497	4783	92 12	B.O f	6.0	12/9/20	09 10	01.92	6449.89	2.2	6551.81	120	6429.6 A	87-128	20.3
0657A	1537083	4784	12 3	5.0 12	2.0	4/13/19	99 :	37.00	6512.00		6549.00		A	17-35	
0658	1535922	4784	36 130).0 6	6.0	12/9/200	09 10	08.11	6442.07	0.4	6550.18	129	6420.8 A	89-130	21.3
0659	1541689	4807	72 10 [.]	1.0 4	.5	12/10/200)9 6	59.58	6490.59	2.0	6560.17	97	6461.2 A	61-101	29.4
0680	1543850	47874	46 80).0 4	.5	10/25/199	96 7	77.39	6481.48	2.0	6558.87	75	6481.9 A	50-80	0.0
0681	1540676	48273	34 117	.0 6	0.0	9/24/199	98 6	64.18	6496.34	2.1	6560.52	111	6447.4 A	67-117	48.9
0682	1543125	47748	39 94	.0 4	.0	9/29/200	9 8	4.97	6469.00	2.8	6553.97	102	6449.2 A	54-94	19.8
0683	1540198	47621	7 120	.0 6	.0	12/14/200	9 9	0.53	6465.51	2.0	6556.04	140	6414.0 A	80-120	51.5
0684	1540273	47849	9 143	.0 6	.0	10/20/200	98	7.34	6465.94	2.0	6553.28	118	6433.3 A	83-143	32.7
0685	1539098	47817	0 100	.0 4	.5	12/12/200	9 9	8.10	6458.47	1.7	6556.57	116	6438.9 A	60-100	19.6
0686	1545319	47543	8 115	.0 4	5	9/23/200	9 11	4.70	6464.10	1.8	6578.80	136	6441.0 A	75-115	23.1
0687	1539011	47727	6 102	.0 6	0	12/12/200	99	6.68	6459.28	2.2	6555.96	120	6433.8 A	62-102	25.5
0689	1530024	47847	8 80	.0 4.	5	11/24/200	88	3.65	6458.37	2.6	6542.02	75	6464.4 A	60-80	0.0
0692	1535892	49317	5 90.	0 5.	0	7/15/200	9 6	7.00	6517.82	2.5	6584.82	80	6502.3 A	58-90	15.5
0846	1537219	48473	0 75.	0 4.	0	12/12/2009	9 4	5.58	6503.34	0.8	6548.92	65	6483.1 A	40-65	20.2
0847	1534736	48850	8 92.	0 5.	0 ·	11/22/1996	ວີ 53	3.88	6504.39	2.6	6558.27	80	6475.7 A	52-92	28.7
0848	1534634	49066	D 92.	0 5.	0	2/28/2007	7 60).78	6511.71	2.7	6572.49	91	6478.8 A	52-92	32.9
0851	1534692	483909	9 91.	0 5.0	0	12/1/2008	89	9.13	6457.31	3.3	6546.44	80	6463.1 A	1-91	0.0
0852	1535610	493989	9 74.	0 5.0	0 1	1/22/1996	6 73	3.26	6516.88	2.5	6590.14	70	6517.7 A	54-74	0.0
0855	1532111	484184	l 105.0) 5.0)	2/24/2009	93	8.94	6447.17	2.1	6541.11	97	6442.0 A 7	0-105	5.2
0861	1534332	488702	2 100.0) 5.0)	8/19/2009	71	.13	6488.72	2.3	6559.85	65	6492.6 A 5		0.0
0862	1534265	487800) 110.() 5.0) 1	2/10/2009	65	.55	6490.63	3.3	6556.18	97	6455.9 A 6	3-103	34.7
0863	1533867	487912	! 110.() - 5.0)	9/12/2007	96	.08	6460.48	2.5	6556.56	94	6460.1 A 6		0,4
0864	1533735	486464	95.0) 5.0)	10/7/2009	75	.84	6470.88	1.9	6546.72	78	6466.9 A 4		4.0
0865	1534123	488429	97.0	5.0		7/20/2009	68	.30	6488.48		6556.78	88	6466.6 A 3		21.9

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(cont'd.)

	NORTH. COORD.		WELL DEPTH (FT-MP)	CASING DIAM (IN)	DA	DEI	R LEVEL PTH ELEV -MP) (FT-MS		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)	PERFOR- ATIONS	SATURATED THICKNESS
0866	15344	94 48	8340 1	20.0	i.0 9/	11/2009	101.00	6457.12	1.8	6558.12	80	6476.3 A	33-113	0.0
0867	15337	62 48	8409	B8.0 S	5.0 12/	10/2009	71.78	6484.12	2.0	6555.90	86	6467.9 A	48-88	16.2
0868	15348	48 49	1033 1	03.0 5	i.0 2/	28/2007	62.10	6512.64	2.2	6574.74	94	6478.5 A	53-103	34.1
0869	15332	51 48	6073	94.0 (i.0 12/	10/2009	83.88	6460.61	1.7	6544.49	99	6443.8 A	44-94	16.8
* 0870	15326	80 48	4906	93.0 5	.0 1/	11/1996	68.56	6475.60	1.9	6544.16	95	6447.3 A	69-89	28.3
0871	15336	03 48	5400 1	0.00	5.0 1/	11/1996	66.86	6477.85	2.4	6544.71	93	6449.3 A	60-100	28.5
* 0872	15330	92 48	5407 1	0.00	5.0 1/	11/1996	65.80	6477.51	1.8	6543.31	96	6445.5 A	55-100	32.0
* 0873	15332	86 48	4505 1	0.0	i.0 1/	11/1996	67.55	6475.46	1.9	6543.01	96	6445.1 A	60-100	30.3
* 0874	15339	68 48	4925 1	05.0 5	i.0 1/	11/1996	68.68	6476.66	2.2	6545.34	110	6433.1 A	55-105	43.5
* 0875	15327	85 48	3634 1	25.0 5	i.0 1/	11/1996	69.85	6472.99	1.7	6542.84	116	6425.1 A	65-125	47.9
0876	15328	53 48	6088 9	95.0 5	.0 12/	10/2009	85.74	6458.52	1.9	6544.26	85	6457.4 A	58-88	1.2
0877	15330	68 48	8067 .	70.0 5	.0 8/	18/1998	63.58	6489.50	1.9	6553.08	65	6486.2 A	58-68	3.3
0879	15324	01 48	6104	70.0 5	.0 12/	10/2009	69.20	6475.35	2.2	6544.55	62	6480.4 A	48-68	0.0
0881	15420	34 48	1478 9	96.0 4	.5 12/	10/2009	73.26	6491.78	2.0	6565.04	103	6460.0 A	76-96	31.7
0882	15414	04 48	2396 11	10.0 4	.5 11/	18/2008	68.21	6492.95	2.0	6561.16	98	6461.2 A	70-110	31.7
1883	15400	97 . 48	3039 10	0.0 5	.0 12/	14/2009	62.00	6495.13	1.9	6557.13	96	6459.3 A	60-90	35.9
0884	15426	77 48	1498 9	90.0 5	.0 6/2	22/2009	74.66	6491.44	1.0	6566.10	85	6480.2 A	58-88 ·	11.3
0885	15419	19 48	3474 10	0.0 5	.0 12/	10/2009	65.25	6499.39	1.5	6564.64	95	6468.1 A	70-100	31.3
0886	15423	27 48	2487 9	90.0 5	.0 1,2/	0/2009	68.78	6495.77	1.5	6564.55	87	6476.1 A	60-90	19.7
0887	15430	63 48	2469 6	67 <i>.</i> 0 5	.0 6/	6/2009	57.54	6510.19	1.5	6567.73	60	6506.2 A	42-67	4.0
0888	15422	85 479	9335 10)5.0 5	.0 12/	0/2009	75.70	6481.63	1.1	6557.33	90	6466.2 A	75-105	15.4
0889	15400	47 48	0222 6	5.0 5	.0 10/2	24/1996	63.31	6486.32	1.5	6549.63	60	6488.2 A	35-65	0.0
0890	15413	65 480	0088 10)1.0 5	.0 12/ ⁻	0/2009	72.87	6485.56	1.7	6558.43	93	6463.7 A	81-101	21.8
0893	15419	34 482	2244 9	8.0 4	.5 12/	0/2009	68.80	6495.17	2.1	6563.97	93	6468.9 A	78-98	26.3
0894	15419	76 478	3317 7	' 8.0 4	.5 11/	6/2005	77.40	6476.89	3.0	6554.29	97	6454.3 A	58-78	22.6
0895	15415	21 476	6222 10	94.0 5	.0 9/2	29/2009	86.00	6467.84	2.4	6553.84	116	6435.4 A	61-101	32.4
0896	15422	46 476	5237 11	3.0 5	.0 9/2	9/2009	87.14	6468.47	2.0	6555.61	117	6436.6 A	73-113	31.9
0897	15438	19 478	3237 9	3.0 4	.0 9/2	7/1998	83.28	6478.97	2.0	6562.25	70	6490.3 A	63-93	0.0
0899	15438	01 477	7288 11	0.0 4	.0 9/*	6/2009	101.78	6469.06	2.0	6570.84	120	6448.8 A	70-110	20.2
0905	15327	00 480	0850 12	20.0 5	.0 11/	3/2006	0.00	6545.00	0.0	6545.00	120	6425.0 A	100-120	120.0
0906	15329	00 48 0	0450		8/2	9/1995	74.65	6462.75	0.0	6537.40	·	A	-	
0909	15319	00 483	3400 14	0.0 4	.0 5	7/2009	92.20	6446.70	0.0	6538.90	112	6426.9 A	80-135	19.8
0910	15288	00 481	1150 13	8.0 5	.0				0.0	6535.00	132	6403.0 A	120-134	
0912	14710	00 478	3250						0.0	6530.00	-	A	-	
0913	155580	00 500	950	8	.0 1/2	4/1996	38.40	6604.60	0.3	6643.00		A	•	
0914	155550	00 500	0850	6	.0 5	6/2009	42.87	6599.13	1.4	6642.00		—A	-	

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	North. Coord.		WELL DEPTH (FT-MP)	CAS DIA (IN	١M			.EVEL 1 ELE\ 2) (FT-M		MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)		SATURATE THICKNESS
0915	15526	50 49	9650 1	00.0	4.0	6/19/2	006	30.00	6595.00	0.0	6625.00	70	6555.0 A	55-85	40.0
0916	15523	50 49	9600 1	60.0	4.0	5/7/2	009	36.63	6588.37	0.0	6625.00		A	45-70	
0917	15422	00 51	4600							0.0	6800.00		A	-	
0920	15558	00 49	6900		7.0	5/11/1	994	33.40	6594.20	0.7	6627.60		A	-	
0921	15554	00 49	5800		5.0	5/6/2	009	39.05	6584.95	1.9	6624.00		A	-	
0922	15552	00 49	2500		6.0	5/6/2	009	58.83	6562.87	1.7	6621.70		— A	-	
0924	15475	00 43	8900 1	35.0	4.0					0.0	6592.90	112	6480.9 A	94-114	
0925	15486	00 48	0800 1	50.0	4.0					0.0	6601.40	140	6461.4 A	126-141	
0926	15475	00 47	2700 1	34.0	4.0					0.0	6596.90	132	6464.9 A	123-132	
0935	15401	15 47	6629 3	00.0	16.0	10/20/2	009	93.00	6465.12	2.6	6558.12	125	6430.5 A	95-132	34.6
0936	15436	21 47	2978 1	60.0	5.0					0.0	6573.38	160	6413.4 A	100-160	
0939	15397	51 48	3202	97.0	8.0	7/25/1	996	59.31	6497.69	2.3	6557.00		. — A	-	
0940	15386	51 48	3040	70.0		· 7/24/1	996	57.30	6495.70	8.8	6553.00		A	-	
0942	15383	06 48	3703 1	00.0	6.0					0.0	6550.20	95	6455.2 A	85-95	
0947	15362	06 49	1841 1	00.0	4.0	7/27/19	994	54.63	6520.55	0.0	6575.18	95	6480.2 A	70-100	40.4
0950	15604	00 49	3300	81.0	5.0	7/12/20	000	25.70	6631.30	0.5	6657.00		A	-	
0952	15345	50 47	7800 1	40.0						0.0	6550.00		— A	-	
0975	15397	53 483	2896							0.0	6556.00		A	-	
0976	15397	51 483	3100 1	15.0						0.0	0.00		A	-	
0977	15399	00 482	2720			12/9/19	995	61.47	6495.53	1.0	6557.00		A	-	
0979	15388	50 483	B110 1	05.0	5.0	7/10/20	002	57.56	6493.44	0.0	6551.00	100	6451.0 A	90-100	42.4
0980	15393	30 483	8050			11/8/19	995	57.70	6497.30	0.0	6555.00		— A	-	
0981	153904	10 483	3740	-			—			0.0	6554.00		- A	-	
0982	15386	10 483	1400	10.0	5.0					0.0	6551.00	105	6446.0 A	90-105	
0983	153859	90 483	100							0.0	6552.00		A	-	
0984	153875	50 482	2950 1	03.0	5.0					0.0	6551.00	98	6453.0 A	88-98	
0985	153904	8 483	380 1	15.0	5.0	7/18/19	996	58.75	6492.25	0.0	6551.00	102	6449.0 A	90-110	43.3
0989	153822	20 482	920			11/2/19	995	58.10	6494.90	1.0	6553.00		· A	-	
0992	153951	0 483	790 10	0.00	5.0				_	0.0	6552.00	95	6457.0 A	85-95	
0993	153792	20 483	677 10	02.0	5.0					0.0	6550.00	98	6452.0 A	85-98	
0994	153970	0 476	240 14	14.0	6.0	10/2/20	09	94.90	6460.10	0.0	6555.00		A	95-110	
0996	153762	1 477	989 13	38.0	5.0	12/12/20	09 1	03.73	6448.79	1.7	6552.52	136	6414.8 A	126-136	34.0
0997	153982	1 473	807			3/12/19	96	76.90	6491.40	0.0	6568.30		A	-	
0999	152423	0 480	187 18	85.0						0.0	6527.00		A	•	
1012	-				6.0					0.0	0.00		A	-	
1013	-				4.0					0.0	0.00		A	-	

(cont'd.)

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WELL NAME	NORTH. COORD.	EAST. COORD.	WELL DEPTH (FT-MP)	CASIN DIAM (IN)			ATER LE DEPTH (FT-MP)			MP ABOVE LSD (FT)	MP ELEV. (FT-MSL)	DEPTH TO BASE OF ALLUVIUM (FT-LSD)	ELEV. TO BASE OF ALLUVIUM (FT-MSL)	CASING PERFOR- ATIONS (FT-LSD)	SATURATED
1014				~~~	9.0					0.0	0.00		—A	-	
1015	•				6.0					0.0	0.00		A	-	
1018					5.0					0.0	0.00		A	-	
1020					5.0	1/18/1	996	15.17	-15.17	0.0	0.00		A	-	
1021						1/18/1	996	18.00	-18.00	0.0	0.00		A	-	

(cont'd.)

 $(x_{i},y_{i}) = (x_{i},y_{i}) = (x_{i},y_{i}$

Sec. 19 1. 1

Note: A = Alluvial Aquifer, Base

M = Middle Chinle Aquifer, Top

T = Tailings Aquifer, Base

* ≈ Well Abandoned

? = Uncertain Identity

4.2

ALLUVIAL WATER LEVELS

4.2.1 WATER-LEVEL ELEVATION - ALLUVIAL

This section presents information necessary to evaluate the direction of ground water flow in the alluvial aquifer. Water-level elevations are used to quantify the gradient of the alluvial water table, which in turn can be used to interpret the direction of ground water flow.

Figure 4.2-1 presents the Fall of 2009 alluvial aquifer water-level elevation contours for the Grants Project area near Homestake's tailings. The alluvial aquifer limits are based on the 2009 water-level elevation map and base of the alluvium map. This recent adjustment in the alluvial aquifer limits resulted in only small changes in the limits of the alluvial aquifer. Locations of the alluvial wells, with their respective well names listed adjacent to the well symbol, are plotted on Figure 4.1-1 in the previous section. The 2009 ground water flow patterns in the alluvial aquifer are very similar to those observed in the Fall of 2008. The ridge in the piezometric surface west of the Large Tailings Pile is attributable to continued injection of water into the injection line in 2009 (see Figure 4.1-1 for location of the injection line). The hydraulic ridge on the southeast side of the Small Tailings Pile decreased in 2009 due to some of these injection wells being down a portion of the year. The water-level elevations and flow directions indicate the extent of the area of the alluvial aquifer from which ground water is drawn by the collection system. The area of collection is between the fresh-water injection area and the collection wells, where ground water is flowing back to the collection wells. The area underlying the Large Tailings Pile is also within the collection area, because alluvial ground water in this area flows to the collection wells.

The water-level elevations in Section 3 were overall fairly steady in 2009 with the fresh water injection and irrigation supply water pumping in this section (see Figure 4.2-1). Water-level changes continued an overall decline in Section 33 (see the western half of Figure 4.2-1), because seven irrigation supply wells are located in this area. The water levels in Section 28 overall increased in 2009 due to the fresh water injection in central Section 28.

Several wells were drilled in the area of the zero saturation boundaries to better define the limits of the alluvial aquifer. However, there are occurrences of limited saturation in the Chinle shale below the alluvium, indicating that there may be zones of perched water in the upper part of the Chinle shale. These wells have been used to help define where the zero saturation boundary of the alluvium occurs and the water levels in these wells may not be representative of the alluvial aquifer.

Flow in the San Mateo alluvium is naturally diverted either west through the western portion of Section 28 or south/southwest through Section 35 around the area where the base of the alluvium is elevated. There is no alluvial saturation where the elevation of the base of the alluvium is above the water table. Further downgradient, the San Mateo alluvial water then mixes with the Rio San Jose alluvial water flowing from the northwest. The combined flow continues to flow in a southerly direction. The gradient of the alluvial water surface in the Rio San Jose alluvium has been increased somewhat due to irrigation water withdrawal, but it is still relatively flat due to its large transmitting ability. San Mateo alluvial ground water that flows through the northern portion of Section 3 (see Figure 4.2-1) joins the Rio San Jose ground water system in the eastern portion of Section 4.

Water-level data for the alluvial wells are presented in Appendix A as Table A.1-1 (HMC alluvial wells), Table A.1-2 (Murray Acres, Broadview Acres, Felice Acres, and Pleasant Valley Estates alluvial wells) and Table A.1-3 (regional alluvial wells).

4.2.2 WATER-LEVEL CHANGE - ALLUVIAL

Figure 4.2-2 presents well locations and indicates the grouping of wells for presentation on water-level elevation versus time plots. The figure number of the water-level elevation plots for each group of wells is shown by the well groupings in the black boxes depicted on Figure 4.2-2. The colors used for the well name and well symbol on Figure 4.2-2 correspond with those used on the water-level elevation plots. Time plots (Figures 4.2-3 through 4.2-18) present the last ten years of data to illustrate the recent trends.

Water levels in the alluvial aquifer have been fairly stable during the last year. Figure 4.2-3 presents water-level elevation data for up-gradient wells DD, ND, NC, P, Q and R. A very slight increasing trend was observed in up-gradient wells during 2009.

Water-level elevation data are presented for two sets of wells monitored for the purpose of detection of a reversal of water-surface gradient near the S line of the collection system. These wells (SP and SO) are located just northeast of the majority of the S line of collection wells. Figure 4.2-4 graphically illustrates that the alluvial hydraulic gradient is very

flat in the area of wells SM, SN, SO and SP. Water-level rises were observed in wells SN, SO and SP in 2003 and 2004 due to injection of fresh water into the injection line with an overall increase in 2009. The water levels actually indicate a very flat gradient between wells SP and SO for 2009. The injection of water into the injection line has caused slightly more rise in well SP than SO. The head is larger near the injection line than near wells SP and SO. The water levels between wells SM and SN shows a slight reversal in the water level elevation.

Wells S2 and S5 are the two reversal wells down-gradient of the S line of collection wells (see Figures 4.1-1 and 4.2-2 for their location). Recent data from these two wells indicate a very good reversal of the ground water flow direction due to the collection wells near well S5 and the rise in water levels caused by the injection line (see Figure 4.2-5). The injection line water caused a larger water level rise in well S1 than in well S2. This data shows that a strong reversal has been maintained between wells S2 and S5.

Figure 4.2-6 presents water-level elevation data for a group of wells located west of the S line of collection wells. Water-level elevations in each of these wells were maintained higher in 2009 due to the injection into the injection line. Water levels overall were steady in well S11 in 2009 with a small increase in the remainder of these wells.

The alluvial water levels north of Murray Acres gradually increased in 2009 in wells MO, MQ, MS, MY and W except during the pumping period for irrigation supply (see Figure 4.2-7).

Wells B and BA are monitored in order to define the reversal in the ground water gradient between the M and J injection lines and the D collection line. Figure 4.2-8 presents water-level elevation data for wells B and BA and indicates a continued ground water reversal. Water levels in this area sharply rose after the addition of the R.O. product injection into the new EMA injection lines until the second quarter of 2006 when the water levels overall declined until mid-2008 when the level steadily rose for the remainder of the year and generally gradually declined in 2009.

Figure 4.2-9 presents water-level elevation plots for alluvial wells B13, C2, D1, M5 and S3, which are located near the lined collection ponds and to the northwest of these ponds. This plot shows that the water levels generally increased or were steady in each of these wells in 2009.

Water-level elevations in the alluvial aquifer near the Small Tailings collection system are presented on Figure 4.2-10 for reversal wells DZ and KZ. Well DZ is near the D collection line and well KZ is close to the K injection line and, therefore, is naturally downgradient of well DZ. This plot shows that, during late 2009, the reversal of the ground water gradient was lost between the line of injection and line of collection. The injection wells on the south side of the Small Tailings Pile were turned off during the pushing of material at the base of the tailings dike back up on the dike slope. These injection wells have been turned back on and should re-establish the reversal.

Figure 4.2-11 presents water-level elevation data for wells C10, C12, L6 and TA. This data reflects the changes in water levels near the north and east sides of the Small Tailings Pile. Injection of R.O. product and fresh water has caused the higher water-level elevations observed in well L6 but steady to gradually declining levels occurred in 2009. The water level in other wells were steady in 2009 except during the pumping of well C10.

Figure 4.2-12 shows the water-level elevation plots for wells I, KEB, KF and X. Water levels slightly declined or were steady in these wells in 2009.

Water-level elevations in the alluvial aquifer south of the Broadview Acres injection system varied in 2009 due to pumping in Felice Acres for the irrigation supply (see water levels for wells 490, 497, GH and SUB1 on Figure 4.2-13). Water levels overall were steady or gradually declined in the wells in 2009.

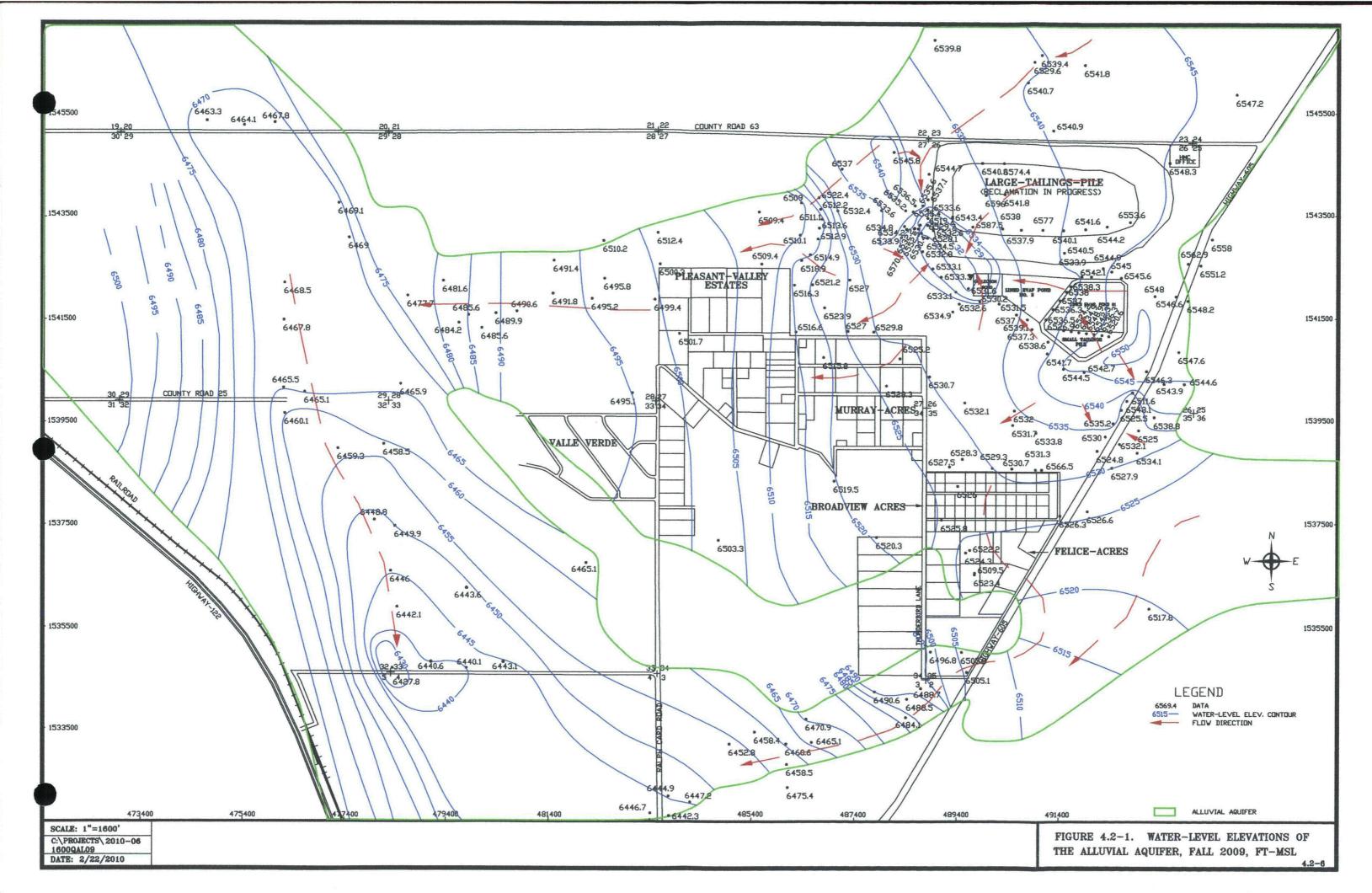
Water levels in the Murray Acres and Pleasant Valley areas were fairly steady in alluvial wells 688, 844, 846, FB and MX during 2009 (see Figure 4.2-14).

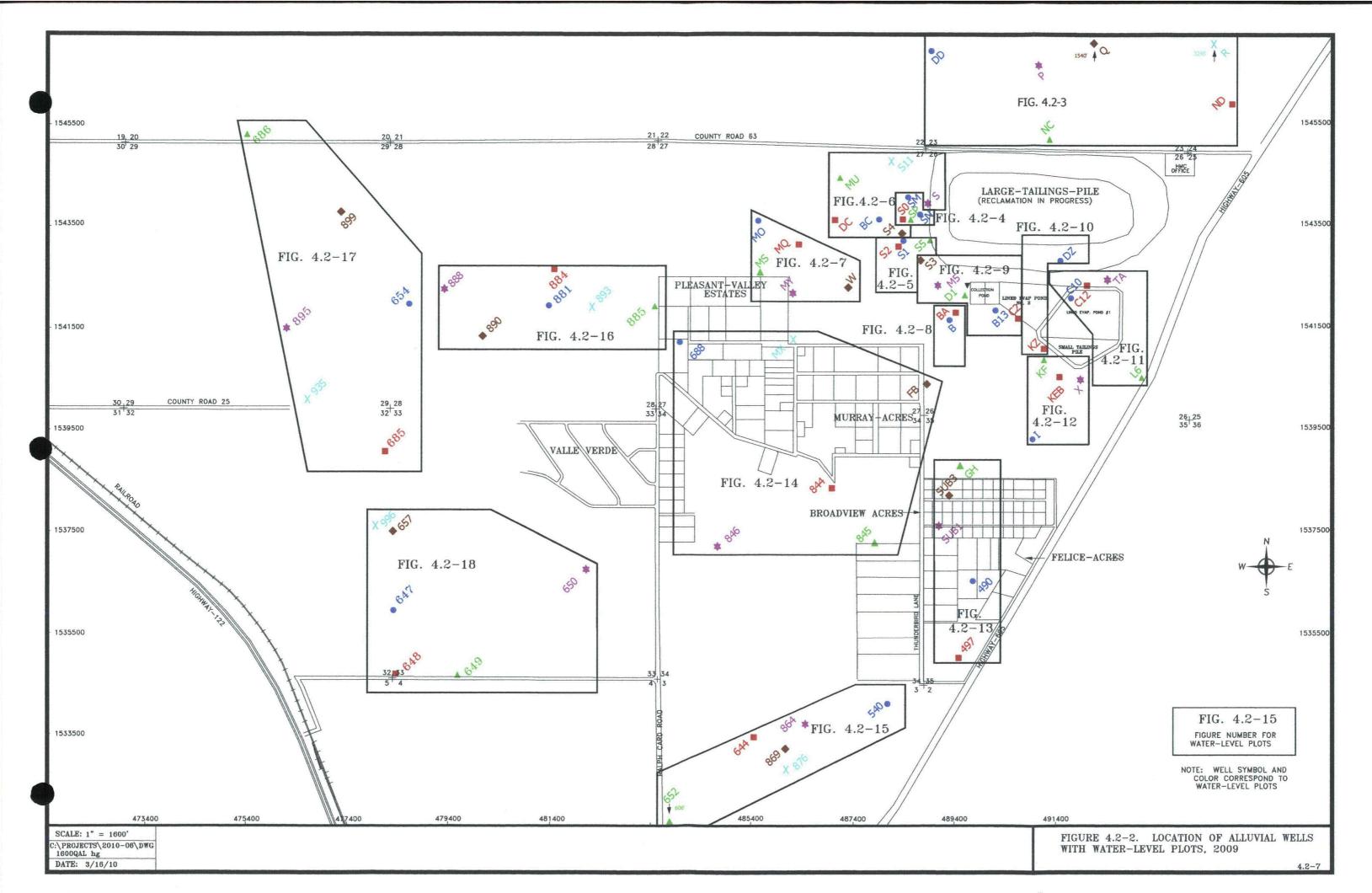
Figure 4.2-15 presents water-level hydrographs for six wells in Section 3. Water levels were overall steady in 2009 in these wells after the irrigation season except for a gradual rise in wells 864 and 876.

Water-level hydrographs for six wells in the Section 28 area are presented on Figure 4.2-16. Wells 881 and 890 were used as irrigation supply wells. Late season water levels in 2009 were slightly above those at a similar time in recent years due to the fresh water injection in this area. Figure 4.2-17 presents the water- level time plots for the group of wells west and southwest of the Section 28 irrigation supply wells. Some rise in water levels in wells 654, 685,

895 and 935 was observed in 2009 due to the Section 28 injection. Water levels in wells 686 and 899 which are northwest of the injection area gradually declined.

Figure 4.2-18 presents the water-level plots for the Section 33 wells shown on Figure 4.2-2. Wells 647, 649, 657 and 996 are irrigation supply wells, and therefore, their water levels are influenced by the periodic withdrawal of water from these wells. The observed water levels during December of 2009 were slightly higher than those observed in previous years at this time except for a steady level in well 649 and a gradual decline in well 648. The water level rises indicate the recharge in 2009 was better than in recent years.





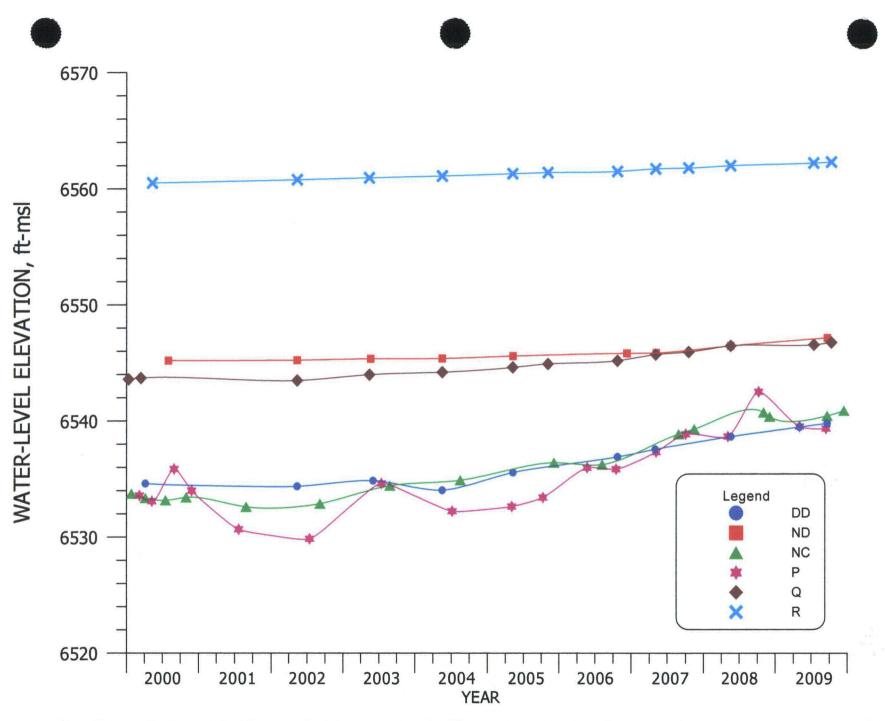
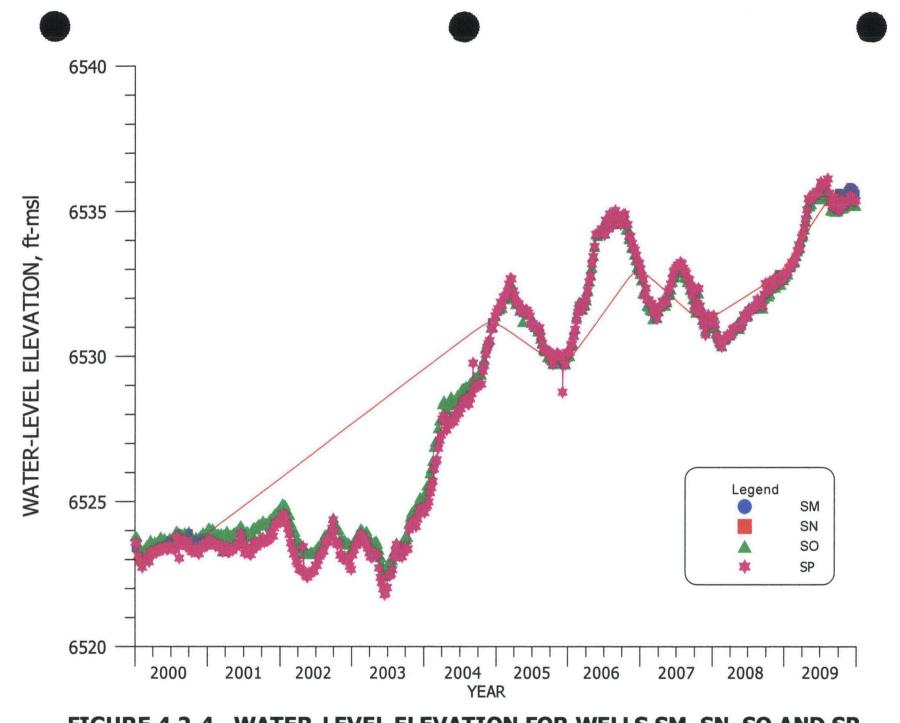
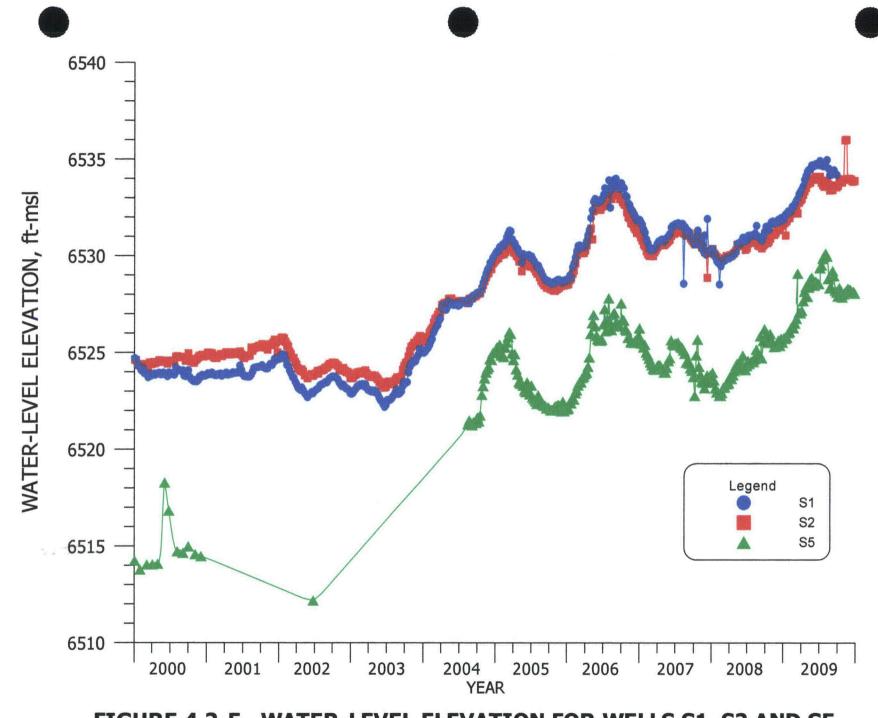


FIGURE 4.2-3. WATER-LEVEL ELEVATION FOR WELLS DD, ND, NC, P, Q AND R.









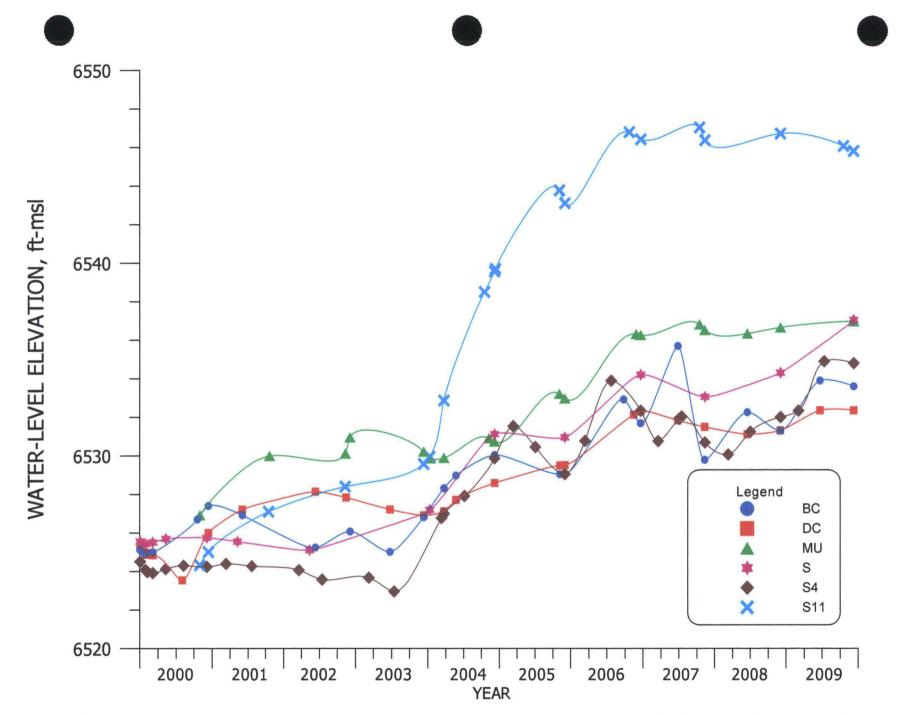


FIGURE 4.2-6. WATER-LEVEL ELEVATION FOR WELLS BC, DC, MU, S, S4 AND S11.

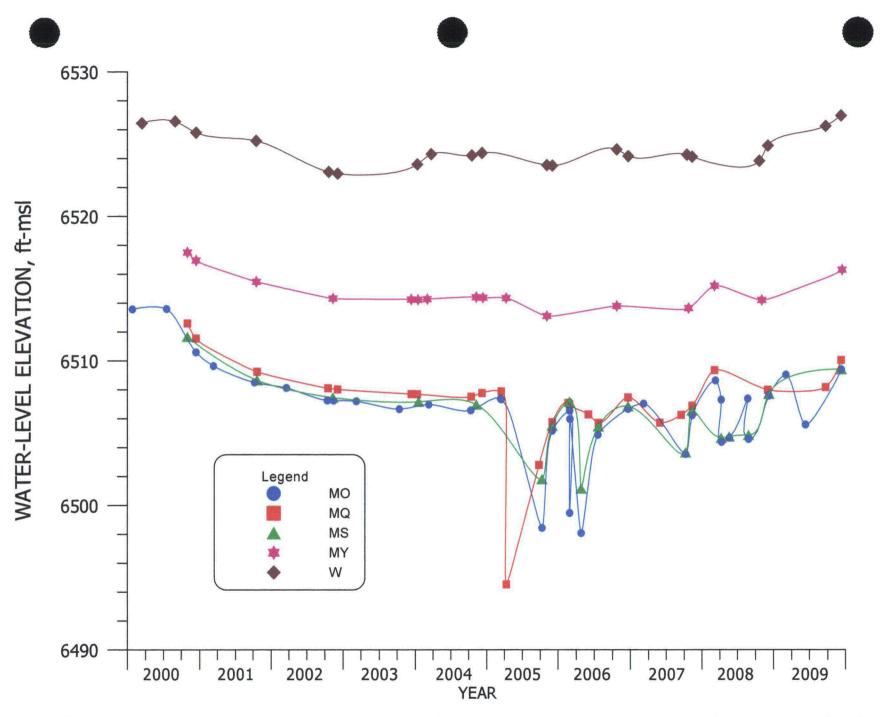
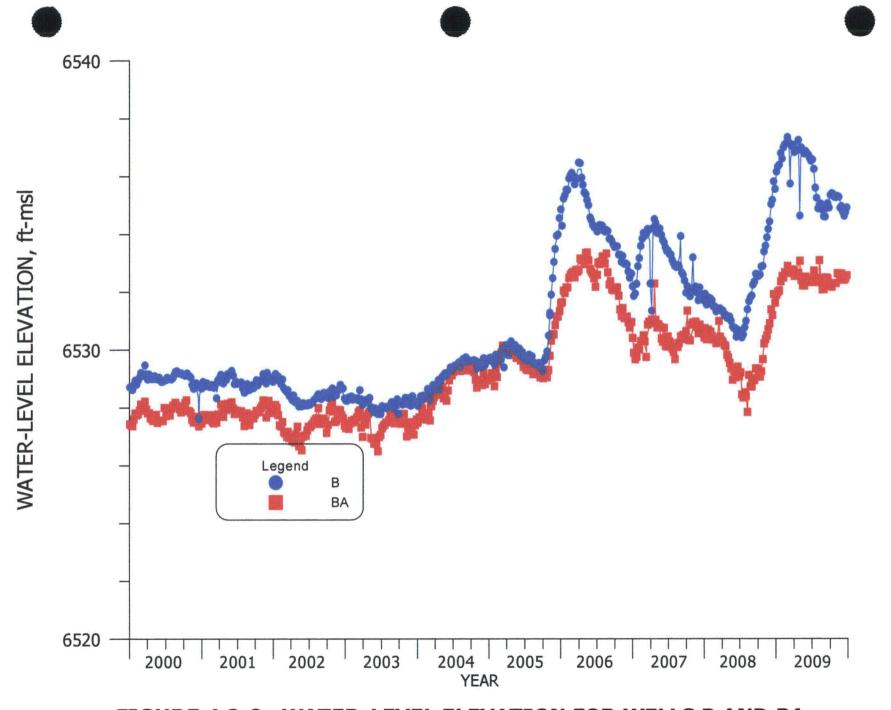
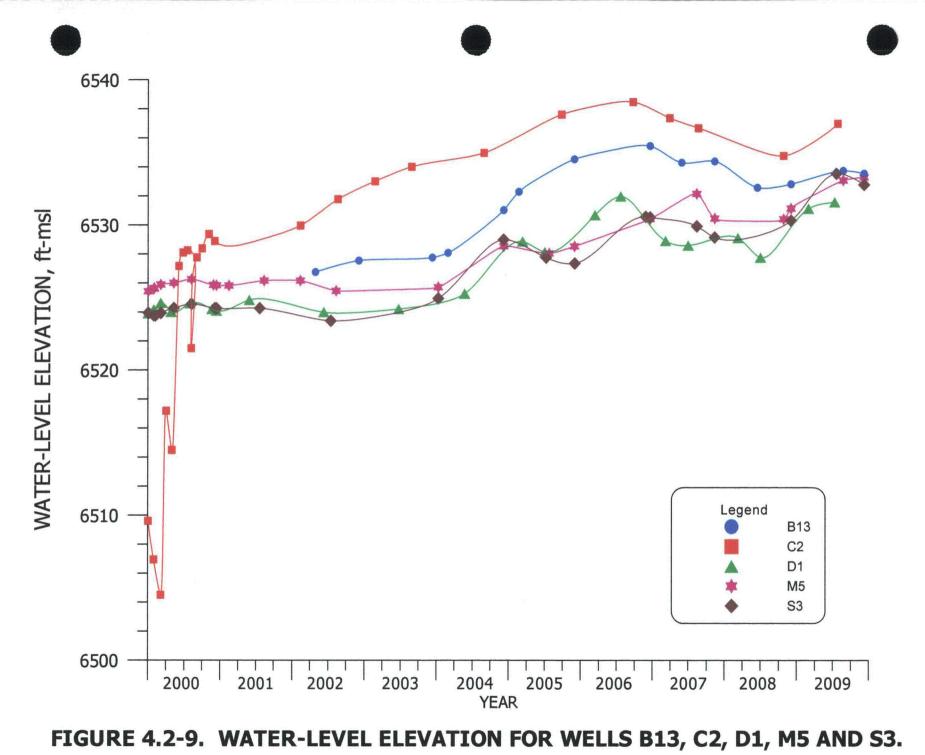
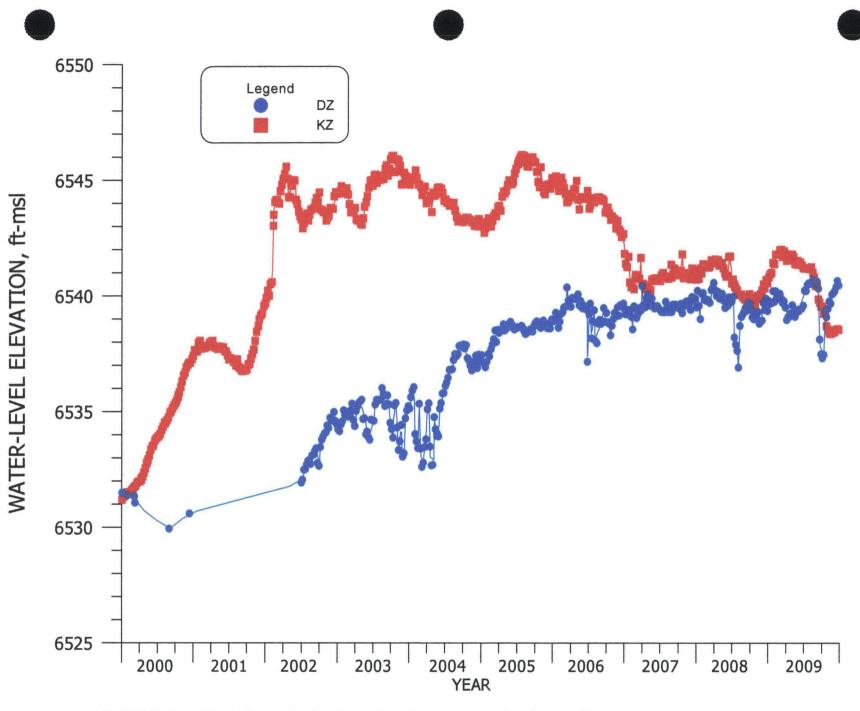


FIGURE 4.2-7. WATER-LEVEL ELEVATION FOR WELLS MO, MQ, MS, MY AND W.

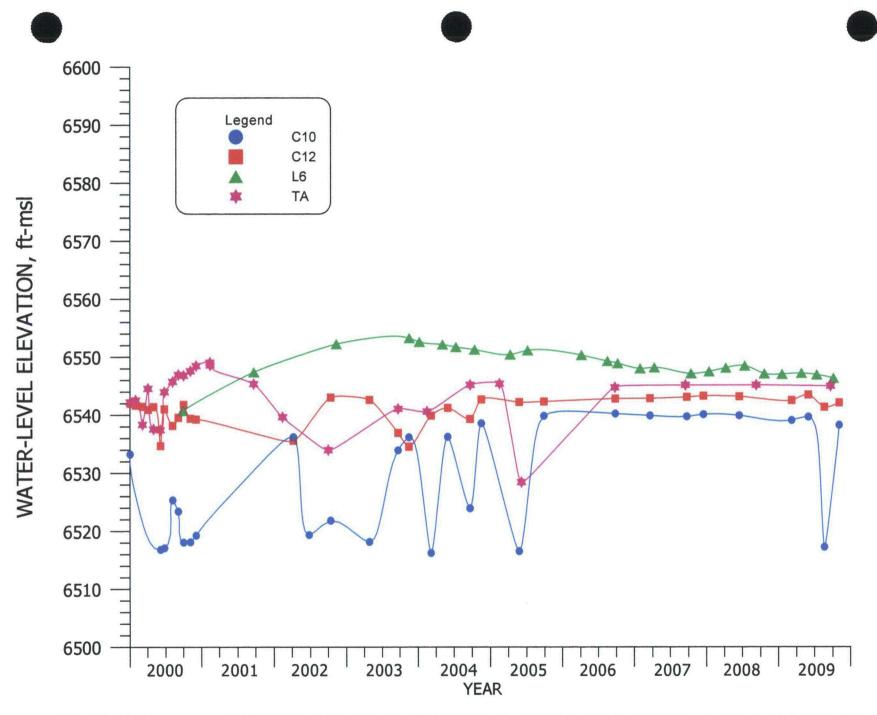














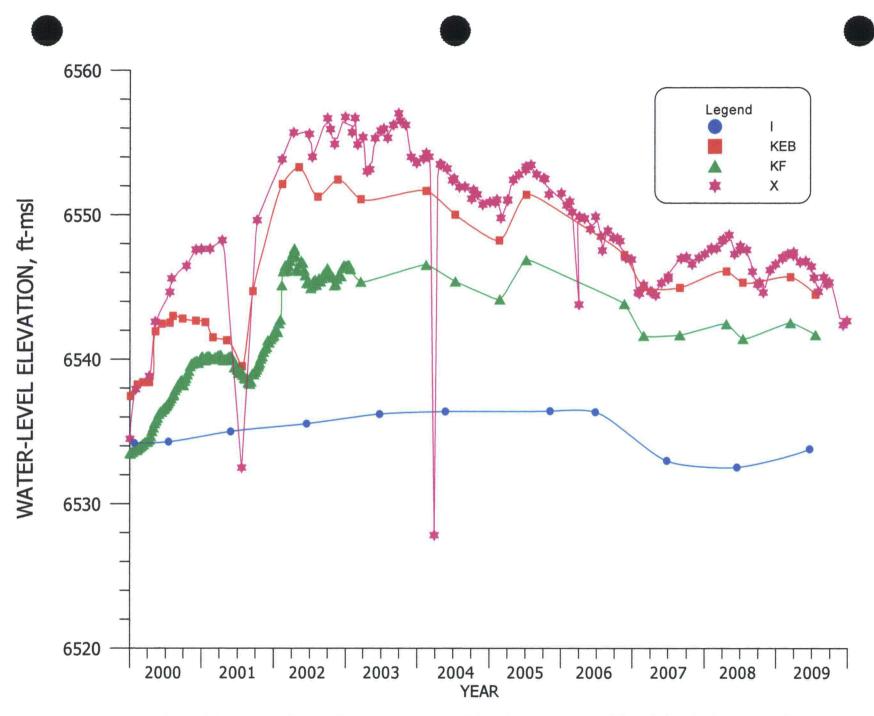
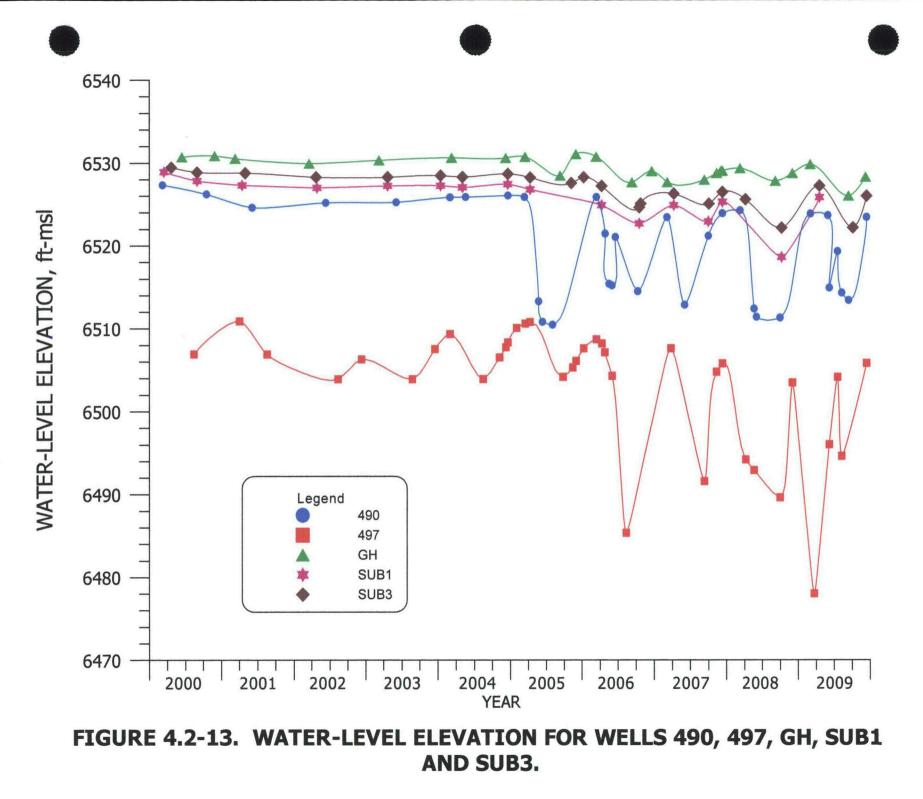
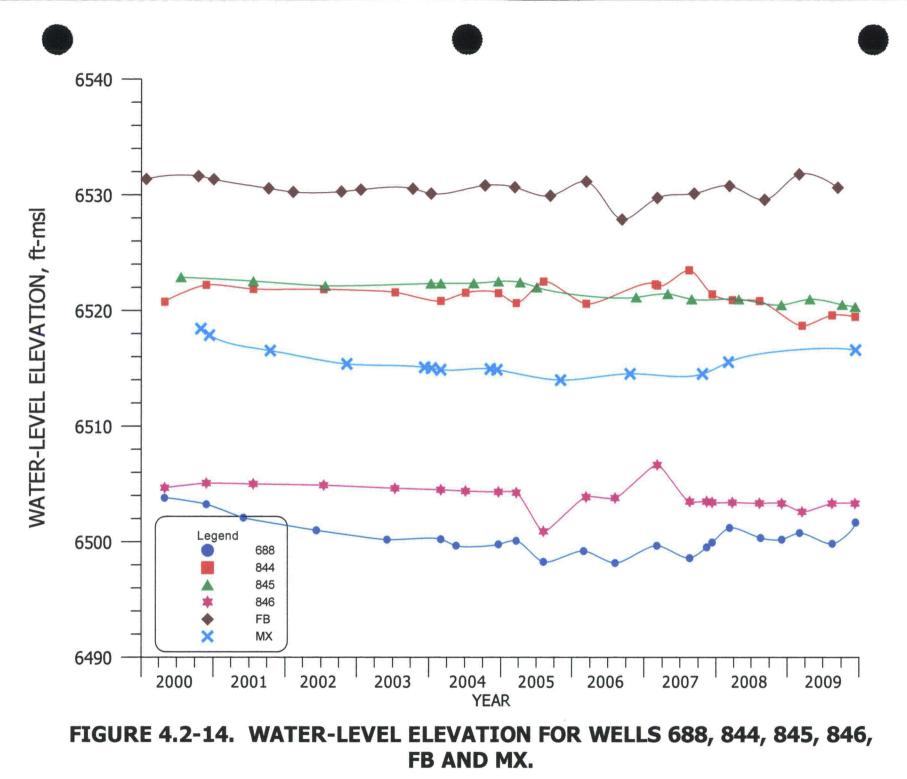
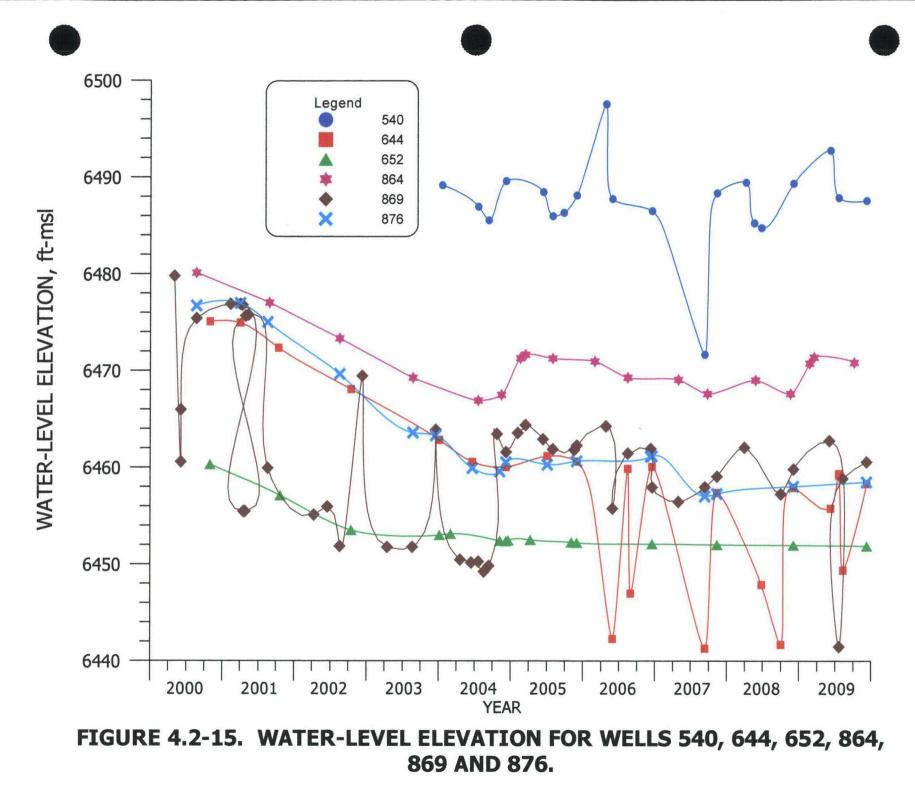
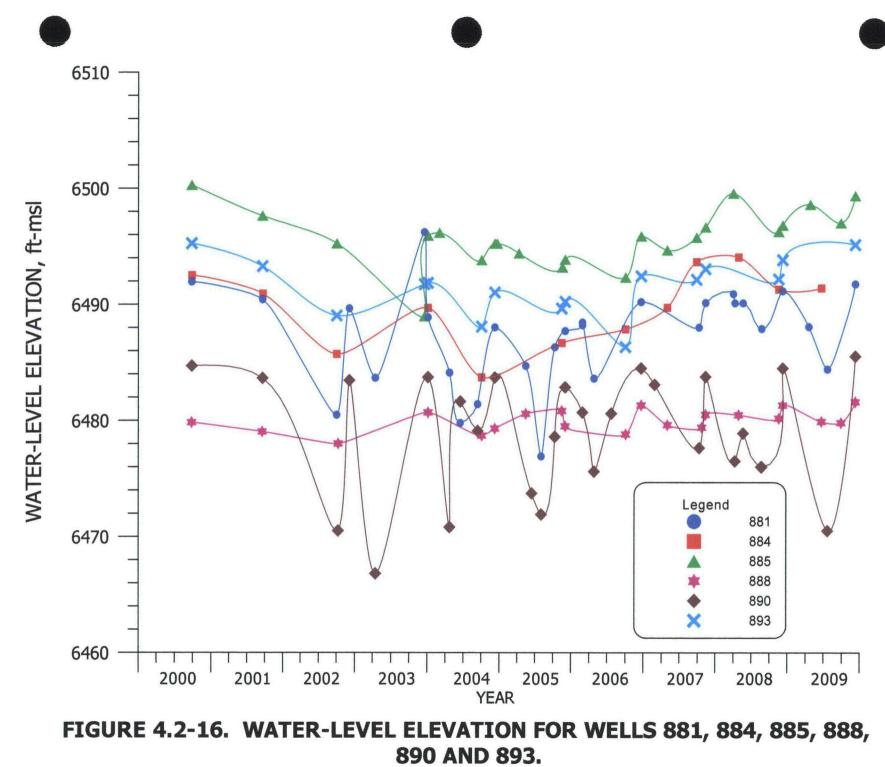


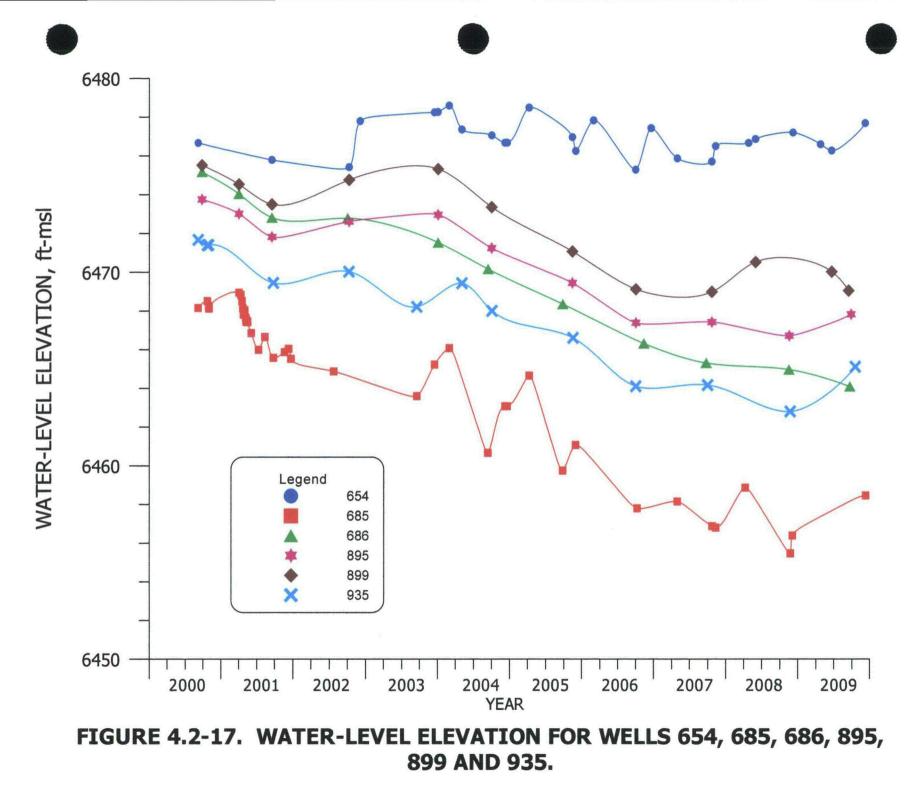
FIGURE 4.2-12. WATER-LEVEL ELEVATION FOR WELLS I, KEB, KF AND X.

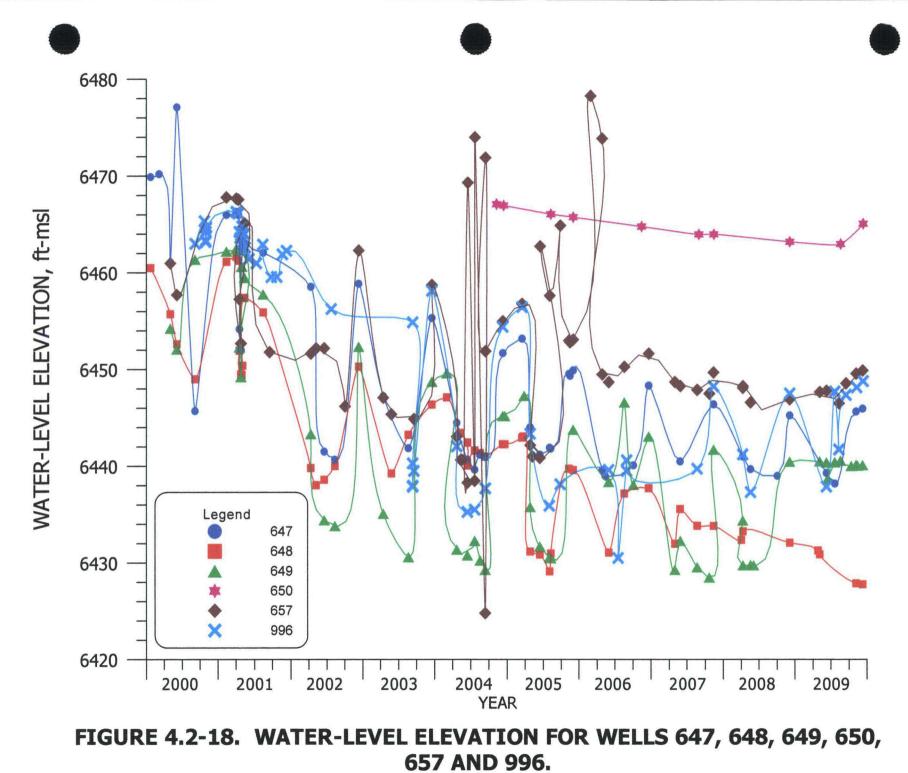












4.3

ALLUVIAL WATER QUALITY

This section presents the 2009 water-quality data for the alluvial aquifer. The major constituents that are typically measured at this site are sulfate, chloride and TDS. Sulfate concentrations are used as the primary indicator of contaminant remediation. Selenium, uranium and molybdenum are the metals of concern at this site. Nitrate, radium, chromium, vanadium and thorium are also discussed in the monitoring report, but these constituents are of only minor concern at the Grants site. Tables B.4-1 through B.4-6 in Appendix B present the 2009 alluvial water-quality data for each well. The most recent monitoring values were used for the concentration contour figures presented in this section.

Colored patterns are used on the figures to delineate where concentration limits exceed the NRC site standards for each of the constituents. The standard is presented in the legend of the respective figure for each parameter. A greater than sign was added in front of the numeric value to note that the pattern shows where the standard is exceeded.

4.3.1 SULFATE - ALLUVIAL

Sulfate has been used as the primary indicator constituent for this site, because concentrations are large in the tailings solution. Concentrations of sulfate in the alluvial aquifer for 2009 are presented on Figure 4.3-1. Background concentrations observed in 2009 ranged from 450 to 1610 mg/l. An updated statistical evaluation of the background sulfate concentration with data for a ten year period (1995 - 2004) showed that concentrations as great as 1500 mg/l could occur naturally at this site and is, therefore, the site standard. Areas where sulfate concentrations exceed 1500 mg/l are shown with a green pattern on Figure 4.3-1. Two wells in west-central portion of Section 34 and one in western Broadview Acres slightly exceed the site standard. As shown, sulfate concentrations in two small areas underlying the Large Tailings Pile still locally exceed 10,000 mg/l. A significant reduction in sulfate concentration was achieved along the restoration zone in Section 28 in 2009. The observed sulfate concentrations in the four adjacent subdivisions were less than 1000 mg/l in 2009, except for a value of 1540 mg/l measured in a water samples collected from well SUB3. Sulfate concentrations were fairly stable in Section 3 in 2009. Sulfate concentrations exceeded 1000 mg/l in the southwest portion of Murray Acres, southern Pleasant Valley Estates, eastern Valle Verde and to the southeast of Valle Verde. Sulfate concentrations also exceeded 1000 mg/l

adjacent to the zero saturation boundary in the northern portion of Section 27 (see Figure 4.3-1). Down-gradient of the Grants Project site, the sulfate concentrations are all within the natural range of background except for the three wells previously mentioned and, therefore, no waterquality restoration with respect to sulfate is necessary beyond the immediate Grants Project area except for these three wells.

Plots of constituent concentrations versus time have been prepared for the alluvial aquifer for sulfate, TDS, chloride, uranium, selenium, molybdenum and nitrate. The groupings of wells used for these plots are shown on Figure 4.3-2. The figure numbers for each of the well groupings that correspond with the sulfate concentration versus time plots are indicated. The color and symbol used for each well are the same as those used in the time plots for each constituent. Figure numbers for the time plots of other constituents are not shown on this map; however, it is useful for the other time-concentration plots because the color, symbol and well groupings are consistent.

Figure 4.3-3 presents sulfate concentrations plotted versus time for up-gradient wells DD, DD2, P, P4, Q and R. A gradual increase occurred in the up-gradient well DD in the 2008 and 2009 values compared to recent yearly concentrations. Overall steady sulfate concentrations have been observed in wells P and P4 in 2009. A very gradual increasing trend was observed in well Q and R during 2009. The historical values for these wells show similar periods of short term increasing and decreasing trends in the alluvial aquifer. The changes in sulfate concentration in these wells are well within the range previously observed for sulfate in the up-gradient wells. Some of these increases could be due to the influx of ground water with higher sulfate concentrations into this area up-gradient of Homestake's background wells.

Sulfate concentrations immediately west of the Large Tailings Pile in alluvial wells NC and S4 were fairly steady in 2009 (see Figure 4.3-4). The sulfate concentrations for well S2 increased in 2005 through 2007 but decreased in 2008 and increased in 2009. A decrease in sulfate in well S11 was observed in 2009 with a value very similar to that observed in 2005. The 2007 value was more than two times the TDS value and therefore an error.

Figure 4.3-5 presents sulfate concentrations plotted versus time for alluvial wells BC, DC, ML, MO and W situated further west of the Large Tailings Pile. Sulfate concentrations were fairly stable in alluvial wells BC, DC and W in 2009, while concentrations in wells MO and ML were increasing. Samples from BC and DC are thought to have been switched in 2007.

Figure 4.3-6 presents sulfate concentration versus time plots for alluvial wells B, D1, M3 and M5. Overall, sulfate concentration in wells B and D1 gradually decreased in 2009. An increase in wells M3 and M5 were observed.

Figure 4.3-7 presents time plots of sulfate concentrations for wells B5, T, T2, T8 and TB. The sulfate concentrations in wells T and TB were fairly steady during 2009. Sulfate concentrations in wells B5 and T2 were increasing in 2009 while sulfate concentrations in well T8 declined.

Figure 4.3-8 presents plots of sulfate concentration versus time for alluvial wells on the west side of the Small Tailings Pile. Sulfate concentration was relatively stable in well C5 in 2009, while an increase in well C2 was observed. A gradual declining trend was measured in wells C8 and C11.

Figure 4.3-9 presents sulfate concentrations versus time for alluvial wells on the south side of the Small Tailings Pile. Sulfate concentrations in these wells were all small in 2009 with small variation except for an increase in well X. This increase is likely due to more fresh water injection near this well. The small changes in sulfate concentrations are due to the switching to fresh water injection in this area in place of the R.O. product injection. R.O. product water injection had reduced sulfate concentrations in these wells to very low levels over the previous years.

Figure 4.3-10 shows the sulfate concentrations for the Small Tailings Pile collection wells K4, K7, K9 and K10. Small decreases to steady values were observed in these wells during 2009 except for a larger decrease in sulfate in well K10.

Time plots of sulfate concentrations in collection wells located southeast of the Small Tailings Pile are presented on Figure 4.3-11. This figure shows a reasonably steady sulfate concentration in 2009 in wells L, L6, L7, L8 and L9, while levels decreased in well L10.

Figure 4.3-12 presents sulfate concentration time plots for Broadview Acres alluvial wells GH, SUB1, SUB2 and SUB3. A decrease was observed in wells SUB1 and SUB2 in 2009 while a small increase was observed in wells GH and SUB3. A very gradual increase in sulfate concentration was observed in well GH in 2008 and 2009.

Figure 4.3-13 presents sulfate concentrations versus time for Felice Acres alluvial wells 490, 491, 496 and 497. The sulfate concentrations in 491, 496 and 497 wells were fairly



steady in 2009. The sulfate concentrations in well 490 increased in late 2009 after decreasing in the early part of the year.

Figure 4.3-14 contains time plots of sulfate concentrations for Murray Acres and Pleasant Valley Estates alluvial wells 688, 802, 844, 846 and FB. This plot shows that sulfate concentrations in water taken from alluvial well 846 decreased in 2009. Concentrations were fairly steady in alluvial wells 688, 844 and FB during 2009 while a small decline was observed in well 802.

Figure 4.3-15 presents the sulfate concentration time plots for six wells in Section 3 (see Figure 4.3-2 for the location of these wells). Sulfate concentrations in each of these Section 3 alluvial wells have been fairly steady over the last several years with a gradual decline being observed in wells 644, 646 and 869.

The sulfate concentrations in water from six wells near the Section 28 center pivot irrigation system are presented on Figure 4.3-16. The decline that occurred in monitoring wells 884 and 888 leveled in 2008 due to the influence of fresh water injection in Section 28. Sulfate concentrations in these two wells were fairly steady in 2009. A sulfate decline continued in well 886 in 2009 but has not started in well 881 as a result of fresh water injection.

Figure 4.3-17 presents sulfate concentrations with time for six wells located to the west of the Section 28 irrigation area. The sulfate concentrations in these wells remained fairly stable during 2009.

The time variations of sulfate concentrations in water sampled from four irrigation supply wells in Section 33 and one new monitoring well located on the southwest edge of the Section 33 Center Pivot are plotted on Figure 4.3-18. Sulfate concentrations in each of these wells were fairly steady in 2009 with a small increase observed in wells 647, 649, 657 and 658.

4.3.2 TOTAL DISSOLVED SOLIDS - ALLUVIAL

Total dissolved solids (TDS) concentration contours for the alluvial aquifer during 2009 are presented on Figure 4.3-19. The alluvial background TDS concentrations measured upgradient of the Large Tailings Pile in 2009 varied from 1080 to 2760 mg/l. Based on an updated statistical analysis, TDS concentration must exceed 2734 mg/l before it is considered elevated beyond the naturally occurring range. A light green pattern is shown on Figure 4.3-19 to indicate where the TDS concentrations exceed 2734 mg/l. None of the observed concentrations in the west half of this figure exceed this level. The TDS concentrations near the tailings exceed 2734 mg/l for a distance of approximately 700 feet to the west of the Large Tailings Pile. Some TDS concentrations underlying the Large Tailings area exceed 20,000 mg/l. A zone of 2000 mg/l or greater TDS concentration extends to the west of the Large Tailings Pile into the eastern portion of Section 28 (see Figure 4.3-19). An additional area of TDS concentrations greater than 2000 mg/l exists in the southern portion of Pleasant Valley Estates, the western portion of Murray Acres, the eastern portion of Valle Verde and to the south and southwest of this area. The only other area of TDS concentrations above 2000 mg/l are small areas in western Broadview Acres and one small area in Section 3. Only the areas closely proximal to the two tailings piles and small areas west of the Large Tailings and small areas east of Valle Verde require ground water quality restoration with respect to TDS.

TDS-time concentration plots were developed for the same grouping of wells as those prepared for sulfate (see Figure 4.3-2 for groupings of wells with TDS plots). Figure 4.3-20 presents the TDS concentrations versus time for the up-gradient wells. TDS concentrations had very slightly increased in well DD in 2009 over the values observed in the last few years. TDS concentrations in the remainder of the upgradient wells remained fairly steady in 2009 except for a very gradual increase in well Q in the last few years.

Figure 4.3-21 presents TDS concentrations plotted versus time for wells NC, S2, S4, S11 and ST. This plot shows an increase in concentration in 2009 for well S2. Steady concentrations in TDS are noted in the remainder of the wells.

TDS concentrations were relatively stable in water collected from wells DC and W during 2009 (see Figure 4.3-22). Increasing concentrations have been observed in 2009 in wells BC, MO and ML. The variations in wells BC and DC in 2007 and 2008 indicate the 2007 samples for these two wells were switched.

TDS concentrations in water sampled from wells B, D1, M3 and M5 are presented in Figure 4.3-23. TDS concentrations increased in 2009 in wells M3 and M5. The decrease in well B and increase in wells M3 and M5 are likely due to the influence of R.O. product injection lines.

Figure 4.3-24 presents TDS concentrations for wells B5, T, T2, T8 and TB. Fairly steady concentration was observed in well TB in 2009, while an increase was observed in wells B5, T and T2 and a decrease was observed in well T8.

Figure 4.3-25 presents time concentration plots for the wells on the west side of the Small Tailings Pile. The concentrations in these wells were fairly steady in 2009 except for an increase in TDS in well C2 and small decreases in wells C8 and C11.

TDS concentrations versus time for four wells just south of the Small Tailings Pile are presented in Figure 4.3-26. This figure shows continued low and slightly variable concentrations in these wells in 2009 except and an increase in well X. This increase is thought to be due to fresh water injection moving to well X.

Figure 4.3-27 presents plots of TDS concentrations for four wells on the south side of the No. 1 Evaporation Pond on top of the Small Tailings Pile. Samples from these alluvial wells have shown a very small decrease in TDS concentrations in 2009 except for well K10 which had a larger TDS decline.

TDS concentrations in water taken from the L line of wells are presented in Figure 4.3-28. TDS concentrations are gradually decreasing or steady with time in each of the wells except for a small increase in well L6.

Figure 4.3-29 presents the TDS concentrations versus time for the Broadview Acres wells. This plot shows a gradual decline in TDS concentrations in 2009 in wells SUB1 and SUB2 and an increase in values from wells GH and SUB3.

The TDS concentrations in the Felice Acres alluvial wells 490, 491 and 497 were fairly steady in 2009 (see Figure 4.3-30). The TDS concentrations in 496 gradually increased in 2009.

TDS concentrations for the Murray Acres and Pleasant Valley Estates alluvial wells are presented in Figure 4.3-31. Steady TDS concentrations were observed in these wells in 2009 except for a gradual decline in well 802.

Figure 4.3-32 presents time plots of TDS concentrations for six wells located in Section 3. Overall, TDS concentrations have been relatively steady over the last few years in these wells, except the 2007 value for well 646 which may be an analytical outlier.

The TDS concentrations for the Section 28 irrigation supply and monitoring wells were also stable in 2009 (see Figure 4.3-33) except for a decline in well 886. The observed decline in well 886 is likely due to the effects of freshwater injection proximal to these wells. The total change in the TDS due to the freshwater injection appears to have occurred in wells 884 and 888 in 2007.

TDS concentrations in alluvial wells in Section 29 and adjacent areas are presented on Figure 4.3-34. TDS concentrations in these wells in 2009 were fairly steady except for a very gradual rise in well 531.

Figure 4.3-35 presents TDS concentrations in the Section 33 alluvial wells. This plot shows fairly steady concentrations in the Section 33 wells in 2009 with a very gradual increase in TDS in wells 647, 649 and 658.

4.3.3 CHLORIDE - ALLUVIAL

Chloride concentration is another important indicator of tailings seepage because of the conservative nature of this constituent and the fact that up-gradient concentrations are low. Chloride concentrations measured during 2009 in the alluvial aquifer near the tailings are presented on Figure 4.3-36. Up-gradient chloride concentrations in the alluvial aquifer varied from 44 to 94 mg/l in 2009. The fresh-water injection systems have used water with chloride concentrations of approximately 200 mg/l, whereas the R.O. product chloride concentration is less than 10 mg/l. The alluvial aquifer around and underlying the Large and Small Tailings Piles contains chloride concentrations in excess of the State drinking water standard of 250 mg/l (site standard). Measurement of chloride concentration in alluvial ground water is useful in defining areas where the R.O. product water has migrated in the alluvial aquifer. A light green pattern on Figure 4.3-36 is used to illustrate where concentrations exceed 250 mg/l. The limited areal extent of the green pattern on this figure shows that the need for ground water-quality restoration with respect to chloride is limited to the immediate area of the tailings and one well west of the tailings. Chloride concentrations in the alluvial water in the western half of Figure 4.3-36 have not typically exceeded 250 mg/l. However, chloride concentrations were measured in samples collected from most of these wells in 2009.

Figure 4.3-37 presents chloride concentrations versus time for the six up-gradient wells. Analysis of the data on this figure shows overall steady chloride concentrations in 2009 in these wells.

Figure 4.3-38 presents time plots of chloride concentration for wells NC, S2, S4, S11 and ST. Fairly steady chloride levels were measured in these wells in 2009 except for a small increase in wells S2 and ST.



Chloride concentrations in wells BC and DC were steady in 2009 compared to their 2006 and 2008 values (see Figure 4.3-39). The 2007 samples for wells BC and DC are thought to be switched. Fairly steady chloride levels were observed in the three other wells.

Plots of chloride concentration for wells B, D1, M3 and M5 are presented on Figure 4.3-40. The chloride concentration in well D1 is similar to the fresh water injection concentration but gradually declined in 2008 and 2009. An increase in concentrations in well M3 was observed in 2009. The chloride concentration in wells B and M5 were fairly steady in 2009.

Chloride concentrations in wells B5, T, T2, T8 and TB are presented on Figure 4.3-41. Chloride concentration in well T8 decreased in 2009. An increase in concentration in collection wells B5 and T2 was observed. A gradual increase was observed in collection well T while chloride concentration in the sample from well TB was fairly steady in 2009.

Chloride concentrations in alluvial wells on the west side of the Small Tailings Pile are presented on Figure 4.3-42. This figure shows stable chloride concentrations in these wells.

All of the chloride concentrations on the south side of the Small Tailings Pile remained very low in 2009 but have been variable due to the switch to fresh water injection. This reflects the changes from the removal of R.O. product water injection in this area (see Figure 4.3-43). The chloride concentrations in water from the K wells (see Figure 4.3-44) have been steady and low in 2009 except for a small decline in well K10.

The chloride concentrations in water collected from the L line wells are presented in Figure 4.3-45. The chloride concentrations have generally been fairly steady in these wells in 2009 except for a decline in concentrations in wells on the south end of the L wells at wells L and L10. With respect to chloride concentration, the quality of water has been restored in the vicinity of the L wells.

Figure 4.3-46 presents time plots of chloride concentrations in the Broadview Acres wells with the concentrations very similar to the fresh water chloride concentration. A gradual increasing trend has been observed the last few years in well GH.

Figure 4.3-47 presents the chloride concentration-time plots for the four Felice Acres wells. The 2009 chloride concentrations are fairly similar to previous chloride concentrations except for an overall decline in irrigation supply well 491 and a gradual increase in well 496.

The large increase in early 2008 in well 491 is supported by other parameters from this sample but this value may be an outlier.

Chloride concentration plots for the Murray Acres and Pleasant Valley Estates wells are presented on Figure 4.3-48. Chloride concentrations are very similar to the fresh water injection concentration with small increases in concentrations for wells FB and 846.

The plots of chloride concentration versus time in Section 3 wells are presented on Figure 4.3-49. Chloride concentrations were similar in 2009 in these wells to their historic values with a very gradual increase in well 631.

Figure 4.3-50 presents plots of the variation of chloride concentrations with time in Section 28 wells. Decline in chloride concentration was observed in well 886 in 2009. This decline is due to the lower chloride concentration from fresh water injection in the area and will likely stabilize at a similar level to the chloride in wells 884 and 888.

Chloride concentrations in the Section 29 monitoring wells are presented on Figure 4.3-51. Chloride concentrations in samples from these wells are similar to the concentration of the nearby fresh water injection with a lower chloride concentration. The water in injection supply well 951 typically has a chloride concentration of approximately 80 mg/l. A small increase was observed in well 531.

Figure 4.3-52 presents time plots of chloride concentrations in the Section 33 wells. The 2009 chloride concentrations slightly increased in wells 647, 649, 657 and 658.

4.3.4 URANIUM - ALLUVIAL

Uranium is considered an important ground water constituent at this site due to the significant levels in the tailings seepage. Uranium data and contours for 2009 are presented on Figure 4.3-53. Background uranium concentrations during 2009 varied from less than 0.003 to 0.25 mg/l, and the alluvial site standard is 0.16 mg/l. The light green pattern on Figure 4.3-53 shows where uranium concentrations exceed 0.16 mg/l, the statistical upper range of background from previous statistical analysis of the 1995-2004 data.

Uranium concentrations exceed background in the area of the Large and Small Tailings Piles, and to the west extending into Section 28. Uranium concentrations in Sections 28 and 29 also reflect a contribution from the Rio San Jose alluvial system in Section 20, but these levels have decreased to less than 0.16 mg/l. The zones of moderately elevated concentrations

join together and the combined area extends down-gradient approximately one mile into Section 33.

Uranium concentrations greater than 0.16 mg/l are also present near the L collection wells south of the Small Tailings Pile. Uranium concentrations in the L wells were overall slightly reduced in 2009.

An additional area where uranium concentrations in the alluvium are greater than 0.16 mg/l exists in Felice Acres and to the southwest into Section 3 (see Figure 4.3-53). The area of elevated concentrations extends approximately 3500 feet to the southwest of the southwest corner of Felice Acres. Uranium concentrations in this area were generally reduced in 2009. The uranium concentrations in another small area in the northeast portion of Murray Acres at well 802 exceed 0.16 mg/l. Concentrations in this area reduced in 2009. Additional restoration is needed in each of these areas with respect to uranium concentrations.

Uranium concentration plots were prepared in order to illustrate changes that result from the corrective action program and other factors. Figure 4.3-2 shows the grouping and location of the alluvial wells used for the uranium-time plots. The figure numbers shown on Figure 4.3-2 correspond to the sulfate time plots. The same grouping of wells was used for the uranium plots, and their symbols and colors are the same as those used on other time plots.

Figure 4.3-54 presents uranium concentrations plotted versus time for up-gradient wells DD, DD2, P, P4, Q and R. The uranium concentrations in these wells have been fairly steady during the last few years. Data for new upgradient well DD2 which is near well DD has a slightly higher uranium concentration than the site standard. The site standard of 0.16 mg/l is shown in the legend on Figure 4.3-53.

A decrease in uranium concentrations was observed in 2009 for wells S4 and ST (see Figure 4.3-55). Uranium concentrations remained low in wells NC and S11. Uranium increased in well S2.

Figure 4.3-56 presents the uranium concentration time plots for alluvial wells west of the Large Tailings Pile. Uranium concentrations are low with a large increase in well BC in 2005 and 2006 and slightly lower concentrations in 2008 and 2009. Well BC is completed in a low permeability area of the alluvial aquifer and responded slowly to restoration. The 2007 samples from wells BC and DC are thought to have been switched. Steady concentrations were observed in wells DC and MO in 2009. A small increase was observed in well W.

Figure 4.3-57 presents time plots of uranium concentrations for alluvial wells B, D1, M3 and M5. Fairly steady uranium concentrations were observed in wells B, D1 and M5 in 2009. Uranium concentrations in well M3 increased in 2009.

Plots of uranium concentration versus time are presented on Figure 4.3-58 for alluvial wells B5, T, T2, T8 and TB. Small concentrations were observed in water from wells T and TB during 2009. Uranium concentration in collection wells B5 and T2 increased while a decline was observed in water from well T8.

Figure 4.3-59 presents plots of uranium concentration versus time for collection wells on the west side of the Small Tailings Pile. Uranium concentrations in wells were fairly steady in 2009 in these wells except for a small decline in wells C8 and C11.

Figure 4.3-60 presents uranium concentrations for wells on the south side of the Small Tailings Pile. Uranium concentrations are low in each of these wells, due to the injection of R.O. product and fresh water into this area.

Uranium concentrations in wells K4, K7, K9 and K10 were reasonably steady in 2009 (see Figure 4.3-61) except for a decline in wells K4 and K10.

Uranium concentrations in water from alluvial wells L, L6, L7, L8, L9 and L10 are presented on Figure 4.3-62. Uranium concentrations were fairly steady in 2009 in all of these wells.

Figure 4.3-63 presents uranium concentrations versus time for four Broadview Acres alluvial wells: GH, SUB1, SUB2 and SUB3. Uranium concentrations in each of these wells were steady in 2009 except for a very gradual increase in well GH and a decline in well SUB2.

Figure 4.3-64 presents the uranium concentration time plots for Felice Acres wells 490, 491, 496 and 497. An overall decrease in concentration was observed in well 491 in 2009 with fairly steady levels in wells 490, 496 and 497.

Figure 4.3-65 presents uranium concentrations for wells in the Murray Acres and Pleasant Valley Estates subdivision areas. Uranium concentrations continued to gradually decline in well 802 in 2009 and are expected to continue to gradually decrease with time. Uranium concentrations in the remainder of the wells in this area are low.

The uranium concentrations for six wells in Section 3 southwest of Felice Acres are plotted on Figure 4.3-66. The uranium concentrations in the western well 631 have been low throughout the period of record. Uranium concentrations overall were very gradually declining

for the last few years in well 862. The concentration at the leading edge of the uranium plume, as demonstrated by the values measured in wells 644 and 646 declined in well 644 but increased in well 646 in 2009. The steady to gradual increasing concentration in irrigation well 869 shows that additional restoration is needed in central Section 3. The uranium concentration in monitoring well 864 overall declined in 2009 indicating that fresh water injection is starting to decrease these concentrations.

Uranium concentrations from six Section 28 wells are plotted on Figure 4.3-67. A declining trend had been observed in concentrations in wells 884 and 888 during the last few year and 2009 values show a very gradual declining trend. An overall decline was also observed in well 886 which is thought to be due to the fresh water injection. Concentrations from irrigation supply wells 881 and 890 and monitoring well 885 were overall steady in 2009.

Uranium concentration time plots for wells in the eastern area of Section 29 are presented on Figure 4.3-68. The uranium concentrations to the north of Section 29 (well 686) were steady in 2009. Well 686 is located in the Rio San Jose alluvial system up-gradient of its confluence with the San Mateo alluvial system. Fairly steady concentration was noted in alluvial wells 895 and 935 in the southern portion of Section 29. The uranium concentration in well 531 increased in 2009.

Uranium concentrations in wells located in Section 33 are relatively small and are plotted on Figure 4.3-69. Concentrations have remained low with steady values in wells 647, 648, 649 and 658 during 2009. The concentrations in well 657 are slightly higher than the other Section 33 wells.

4.3.5 SELENIUM - ALLUVIAL

Selenium is an important constituent at the Grants Project site because, like uranium, it is present in significant concentrations in the tailings water. Figure 4.3-70 presents a map of the spatial distribution of selenium concentrations throughout the site. The upper limit of background based on statistical analysis and the site standard is 0.32 mg/l. Selenium concentrations upgradient of the site varied from less than 0.005 and 0.72 mg/l in 2009. Concentrations that exceed 0.32 mg/l are considered indicative of seepage impacts, while smaller concentrations are within the range of natural variation. A green pattern is superimposed on the concentration contour figure to show where concentrations exceed 0.32 mg/l. A 0.1 mg/l

selenium concentration contour extends to the western edge of Section 27. Selenium concentrations in excess of 0.1 mg/l were measured southwest of Felice Acres in two areas of Section 3 with the one of these areas extending to its western border. All selenium concentrations in the alluvial aquifer in all of the nearby subdivisions are less than 0.1 mg/l.

Selenium concentrations exceeding 0.32 mg/l were measured in wells around the Large and Small Tailings Piles and extend approximately 800 feet to the west of the Large Tailings Pile and also extend to the south of the Small Tailings Pile in the area near the eastern edge of the L collection wells. This shows that only the area near the tailings pile and the area near some of the L collection wells needs additional restoration in order to reduce selenium concentration.

Figure 4.3-2 presents the location and grouping of wells for selenium concentration plots. The symbols and colors used on Figure 4.3-2 are the same as those used on each constituent time plot.

Figure 4.3-71 presents plots of selenium concentration versus time for up-gradient wells DD, DD2, P, P4, Q and R. There has been an increasing selenium concentration trend in up-gradient well R which is the farthest near-up-gradient well from the tailings. The data in 2009 indicates that this trend is continuing but the trend is expected to cease because the maximum selenium value measured in the far upgradient wells is similar to the selenium in well R. A smaller increasing trend has also been observed in the data for well Q. The 2009 concentrations in wells P, P4, DD and DD2 were steady.

Figure 4.3-72 shows low selenium concentrations in wells NC, S4 and S11 during 2009. An increase in selenium concentration was observed in well S2 in 2009. A decline in selenium concentration was observed in well ST to a very low values in 2009.

Figure 4.3-73 presents selenium concentrations for wells BC, DC, ML, MO and W. Selenium concentrations have remained low in all of these wells except for an overall decrease in wells DC, ML and W. Selenium in well BC was slightly higher in 2009. As previously mentioned, 2007 data for wells BC and DC are believed to have been switched.

Selenium concentrations in water from alluvial wells located southwest of the Large Tailings Pile are plotted on Figure 4.3-74. This figure shows a small selenium concentration in wells B and M5 in 2009 and a decrease in well D1. A small increase in concentration was observed for data from well M3 after a larger increase in 2007.

Figure 4.3-75 presents plots of selenium concentrations for wells B5, T, T2, T8 and TB. A gradual increasing trend in selenium was noted for well T in 2008 with overall steady levels in 2009. Small selenium increases in wells B5, T2 and TB were observed during 2009.

The selenium concentrations for collection wells located on the west side of the Small Tailings Pile are plotted on Figure 4.3-76. Selenium concentrations in samples collected from wells C1, C2 and C5 were small in 2009. Steady concentrations were observed in wells C8 and C11 in 2009.

Figure 4.3-77 presents selenium concentrations for wells KEB, KF, KZ and X, which are located on the south side of the Small Tailings Pile. Only small concentrations were measured in water taken from these wells and this is attributed to restoration by injection of R.O. product and fresh water in this area.

Selenium concentrations in wells K4 and K10 decreased in 2009 (see Figure 4.3-78). Concentrations in 2009 in collection wells K7 and K9 were fairly steady.

Figure 4.3-79 presents selenium concentration for wells L, L6, L7, L8, L9 and L10. Fairly steady selenium concentrations with time were observed in these wells during 2009.

Figures 4.3-80 and 4.3-81 present selenium concentration plots for the Broadview Acres and Felice Acres alluvial wells. These plots show that the selenium concentrations have been reduced and maintained at low levels for the last several years in these two subdivisions except for a higher value in early 2008 in well 491. The early value in well 491 in 2008 appears to be an outlier.

Selenium concentrations are presented for wells in the Murray Acres and Pleasant Valley Estates areas on Figure 4.3-82. This plot shows continuing low selenium concentrations in monitoring wells in this area of the alluvial aquifer.

Selenium concentrations for six wells in Section 3 are plotted on Figure 4.3-83. Well 631 is located in the western portion of Section 3. Selenium concentrations in this well, and wells 646 and 869, decreased slightly in 2009. Concentrations in wells 644 and 862 were steady in 2009. An increasing trend has been observed in well 864 in 2008 which is thought to be due to fresh water forcing higher concentrations to move toward the irrigation supply wells but the 2009 values show a decline.

The selenium concentrations in alluvial water in Section 28 have been fairly steady with time. Figure 4.3-84 presents the selenium concentrations from the Section 28 alluvial wells. A significant decline was observed in concentration in well 884 in 2006 due to the fresh water injection in this area and this decline ceased in 2008 and 2009 at a very low value. Small decreases were observed in irrigation supply well 886 likely due to injection water reaching this well.

Figure 4.3-85 displays selenium concentrations in wells in Section 29 and in wells 686 and 541, which are located to the north and south of Section 29, respectively. Fairly steady and small selenium concentrations were observed in 2009 in these wells and the remainder of the Section 29 wells.

Selenium concentrations from wells in Section 33 are presented on Figure 4.3-86. The data demonstrated small and steady selenium concentrations in 2009 in these wells.

4.3.6 MOLYBDENUM - ALLUVIAL

This section discusses the molybdenum concentrations in the alluvial aquifer at the Grants Project during 2009. Figure 4.3-87 is a spatial presentation of the concentration data and contours. Molybdenum concentrations in alluvial water in the west area of this figure have typically been less than 0.03 mg/l and, therefore, samples from the western wells are not routinely analyzed for molybdenum. Numerous samples were taken from these wells in 2009 to update the molybdenum database. The movement of molybdenum in the alluvial aquifer is dramatically attenuated in comparison to that of selenium and uranium. Molybdenum concentrations exceed 100 mg/l near the Large Tailings Pile and a 10 mg/l contour extends around most of the Large Tailings Pile and the western portion of the Small Tailings Pile.

The light green pattern on Figure 4.3-87 shows the area where molybdenum concentrations exceed 0.10 mg/l, the site standard. A molybdenum concentration of 0.10 mg/l is considered the threshold of significance for this constituent at this site. Significant molybdenum concentrations extend approximately 1000 feet west of the Large Tailings Pile and also to the southeast of the Small Tailings Pile to the L collection wells. Concentrations in five wells in the central portion of Section 27 exceed the molybdenum site standard of 0.10 mg/l. Concentrations in none of the alluvial wells in the subdivisions exceed 0.10 mg/l of molybdenum.



Figure 4.3-88 presents molybdenum concentration for the up-gradient wells DD, DD2, P, P4, Q and R. Concentrations have remained low in these six wells in 2009.

Steady molybdenum concentrations were observed in well S4 in 2009, while the molybdenum concentrations in well S2 was fairly steady (see Figure 4.3-89). Molybdenum concentrations in wells NC and S11 were small and steady in 2009. A decrease was observed in well ST in 2009.

Figure 4.3-90 presents time plots of molybdenum concentration for wells BC, DC, ML, MO and W. Molybdenum concentrations in each of these wells were small in 2009 except for higher value in well BC. Concentrations in this well were gradually declining, assuming the 2007 samples from wells BC and DC were switched, but increased in 2009.

Figure 4.3-91 displays molybdenum concentrations for wells B, D1, M3 and M5. Molybdenum concentrations in well M3 increased in 2009. Stable concentrations with time were observed in well B. A decrease was observed in well M5 while the 2009 values from well D1 were fairly steady in 2009.

Figure 4.3-92 presents molybdenum concentrations for wells B5, T2, T8, T and TB. A decrease in the molybdenum concentration in well T8 was observed in 2009. The molybdenum concentrations in wells T and TB were fairly steady in 2009 while the values in wells B5 and T2 increased.

Molybdenum concentrations in wells on the west side of the Small Tailings Pile are presented on Figure 4.3-93. Molybdenum concentration declined in the water in well C11 in 2009 and gradually increased in well C8.

Figure 4.3-94 presents molybdenum concentrations for wells on the south side of the Small Tailings Pile. Small molybdenum concentrations continued to be observed in wells KEB, KF, KZ and X during the last year.

Figure 4.3-95 shows decreasing molybdenum concentrations in wells K4, K7 and K10 in 2009 and a small increase in well K9.

Figure 4.3-96 presents molybdenum concentrations in wells L, L6, L7, L8, L9 and L10, which are located further to the southeast of the Small Tailings Pile. Molybdenum concentrations were generally very gradually declining or steady in these wells during 2009.

Molybdenum concentrations in alluvial wells located in Broadview Acres and Felice Acres are plotted on Figures 4.3-97 and 4.3-98, respectively. The molybdenum concentrations in Broadview wells GH, SUB1, SUB2 and SUB3 have been low for the last several years. Molybdenum concentrations in wells 490, 491, 496 and 497 in Felice Acres were reasonably steady for 2009.

Figure 4.3-99 presents the molybdenum concentrations for wells in the Murray Acres and the Pleasant Valley Estates areas. This plot shows that molybdenum concentrations have remained low in these alluvial wells.

Molybdenum concentration plots for the irrigation area wells have been updated. Figures 4.3-100 through 4.3-103 present the molybdenum concentration time plots for the Section 3, Section 28, Section 29 and Section 33 wells, respectively. All of the molybdenum concentrations have remained low in wells located in these areas in 2009. Molybdenum concentrations have migrated into Section 27 and could possibly have migrated into eastern Section 28 in a small area.

4.3.7 NITRATE - ALLUVIAL

The presence of relatively large nitrate concentrations up-gradient of the Grants site has resulted in a site standard of 12 mg/l (see Table 3.1-1). A statistical analysis of the upgradient data 1995 through 2004 produced the nitrate concentration of 12 mg/l based on the 95th percentile of background. Upgradient nitrate concentrations varied from less than 0.1 to 20.2 mg/l in 2009. Figure 4.3-104 presents nitrate concentrations measured in 2009 in the alluvial aquifer. The nitrate concentrations north and up-gradient of the tailings ultimately impact the nitrate concentrations down-gradient of the Large Tailings Pile in the northern portion of Sections 27 and 28. It is difficult to determine whether seepage from the tailings has any significant impact on the nitrate concentrations in this area, because the naturally higher concentrations indistinguishable from background. The nitrate concentrations in the northern portion of Section 27 did exceed 12 mg/l in 2009. Some of these larger nitrate concentrations could be caused by the higher historical nitrates upgradient of the site.



Grants Reclamation Project 2009 Annual Report Monitoring / Performance Review Nitrate concentrations exceed 12 mg/l in an area on the south and northeast sides of the Large Tailings Pile which are all likely due to seepage from the tailings. Small areas of nitrates above 12 mg/l also exist east of the Small Tailings and south of Pleasant Valley. Nitrate concentrations in all of the alluvial subdivision wells are below 12 mg/l. Areas where water-quality restoration is required with respect to nitrate are shown by the green patterns on Figure 4.3-104. Restoration of nitrate should occur prior to the restoration of some other key parameters in these areas.

Plots of nitrate concentration over time were prepared for the alluvial wells that are listed on Figure 4.3-2. Figure 4.3-105 presents the nitrate concentrations for the background wells. Concentrations in these wells have been relatively stable except for a gradual increasing trend over the last several years in well R and well Q for the last four years. Nitrate concentrations in wells Q and R declined or were steady in 2009 which may be an indication that they have reached their peak. The present nitrate concentrations in wells Q and R exceed the site standard which shows that higher nitrate concentrations upgradient of the site are entering the near-up-gradient area. Well Q nitrate concentrations have exceeded the site standard in only 2008 and 2009. The recent increases in well Q fit the travel time between wells R and Q.

The nitrate concentrations in wells NC, S2, S4, S11 and ST, immediately west of the Large Tailings Pile, are plotted on Figure 4.3-106. This figure shows small and steady concentrations in 2009 for wells NC, S4, S11 and ST and increasing concentrations in well S2.

Figure 4.3-107 presents the nitrate concentrations for wells BC, DC, ML, MO and W. Nitrate concentrations were marginally higher in 2009 in well MO in 2009. Nitrate concentrations were lower in wells BC, DC and W. An increasing trend was observed in well ML

Nitrate concentrations in the group of wells southwest of the Large Tailings Pile are presented as time plots on Figure 4.3-108. All of the concentrations in these wells are small with a small decrease observed in wells D1 and M3.

Figure 4.3-109 presents nitrate concentrations in wells B5, T, T2, T8 and TB. Nitrate concentrations were fairly steady in these wells in 2009.

Nitrate concentrations in wells on the west side of the Small Tailings Pile are plotted on Figure 4.3-110. Fairly steady and small nitrate concentrations were observed in these wells in 2009 except well C11 which has a larger value and overall increased in 2009. Figure 4.3-111 shows nitrate concentrations for wells on the south side of the Small Tailings Pile. All of the nitrate concentrations in these wells are low and steady.

The nitrate concentrations in the K and L series wells are presented on Figures 4.3-112 and 4.3-113, respectively. Concentrations in recent samples have been very small in all of these wells.

Nitrate concentrations in the Broadview Acres wells are presented on Figure 4.3-114. Small and relatively steady nitrate concentrations were measured in water from these wells with time.

Nitrate concentrations for the Felice Acres wells are presented on Figure 4.3-115, with reasonably steady concentrations over time except the higher value in early 2008 in well 491.

Nitrate concentrations in Murray Acres and Pleasant Valley Estates wells are presented on Figure 4.3-116. Nitrate concentrations in well 846 are higher than the other four wells shown on this figure and show an increase in 2009. The nitrate concentration in the remainder of these wells was fairly steady in 2009.

Nitrate concentrations in Section 3 wells are presented on Figure 4.3-117. The nitrate concentrations in these wells were low in 2009.

Nitrate concentrations for the Section 28 wells are presented on Figure 4.3-118. A small decrease was observed in well 886 in 2009. The nitrate concentrations in wells 888 and 890 were reasonably steady while an increase was observed for well 885.

Figure 4.3-119 presents nitrate concentrations in wells 531, 654, 685, 686, 895 and 935. The nitrate concentrations have been decreasing or steady over the last few years in each of these wells. The large increase in well 686 in 2007 is thought to be an error and the 2006, 2008 and 2009 data indicate it is an outlier.

Nitrate concentrations in the Section 33 wells are presented on Figure 4.3-120, and, in these wells, nitrate concentrations were steady in 2009.

4.3.8 RADIUM-226 AND RADIUM-228 - ALLUVIAL

Figure 4.3-121 presents radium concentrations for the alluvial ground water in the Grants Project area. Radium concentrations are very small in the alluvial aquifer except directly underneath the Large Tailings Pile. The monitoring program for radium has been scaled back,

because radium is not present in significant concentrations in the alluvial aquifer. The radium-226 concentrations are printed horizontally in black, while the radium-228 values are shown at a 45° angle and in magenta. The State standard for radium-226 plus radium-228 is 30 pCi/l, while the NRC site standard is 5 pCi/l. Measured activities of radium-226 in alluvial wells beneath the Large Tailings Pile exceed 50 pCi/l in some areas and therefore exceeded the site standard in 2009. No significant radium-228 values were measured in 2009, similar to the 2008 results. No radium concentrations outside of the Large Tailings Pile area are in exceedance of the standard. Past data has shown that radium is not mobile in the alluvial aquifer at this site. The laboratory started in 2008 reporting negative and zero values for the radionuclides instead of a less than value. These very low results should be considered non-detect values.

4.3.9 VANADIUM - ALLUVIAL

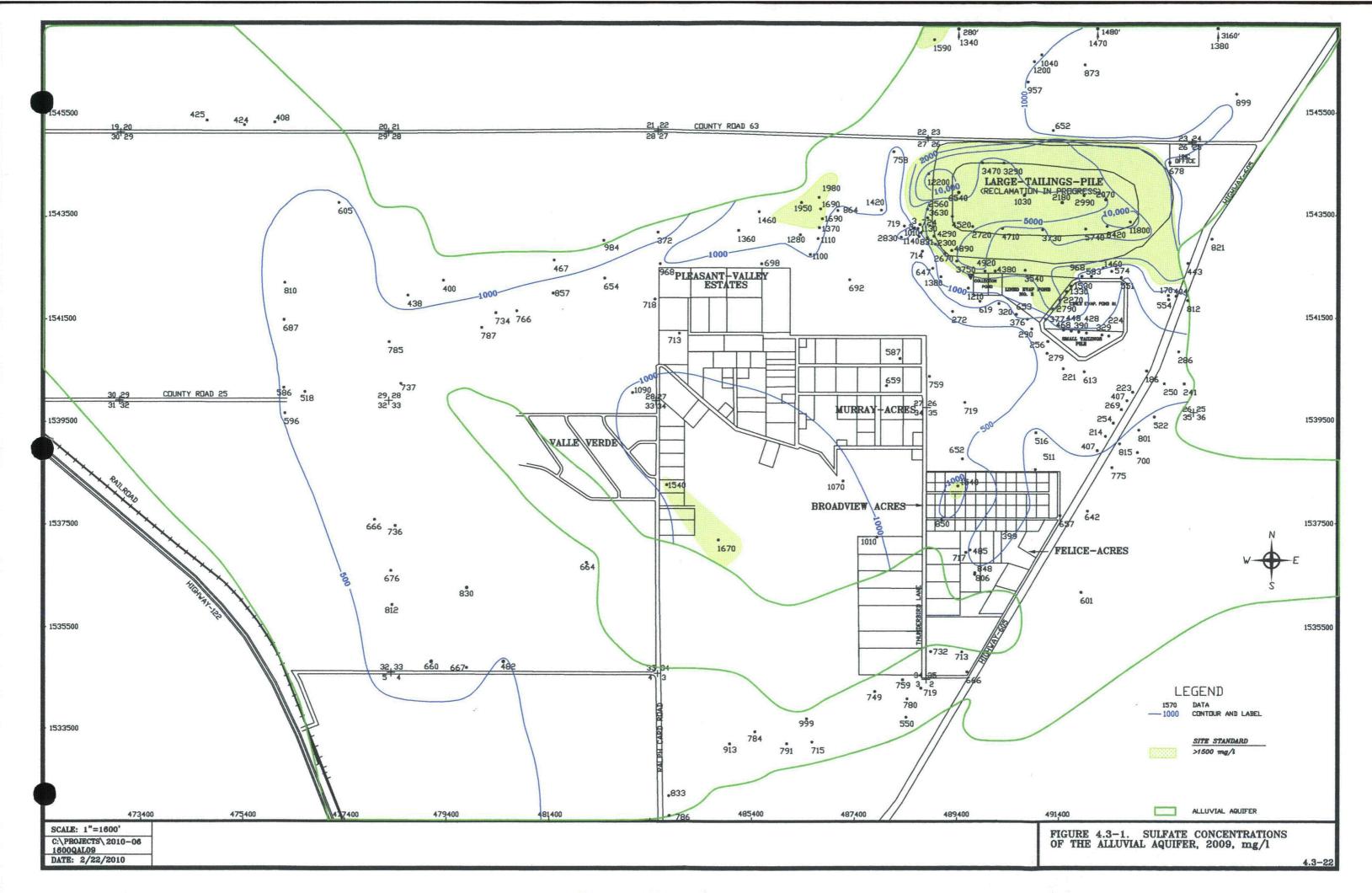
Vanadium concentrations measured in 2009 are shown on Figure 4.3-122. None of the vanadium concentrations in the POC wells exceeded the site standard of 0.02 mg/l. POC well X was the only POC well that routinely contained a vanadium concentration above the site standard prior to restoration of that area. Therefore, none of the POC wells are expected to contain vanadium concentrations above the site standard of 0.02 mg/l in the future. Injection of R.O. product water has effectively restored ground water quality in the area near well X. Vanadium concentrations in 2004, in eight alluvial wells located within the footprint of the Large Tailings Pile, were above the site standard for vanadium. The ongoing corrective action program will restore vanadium concentrations in this area. All of the 2009 measurements were less than the detection limit.

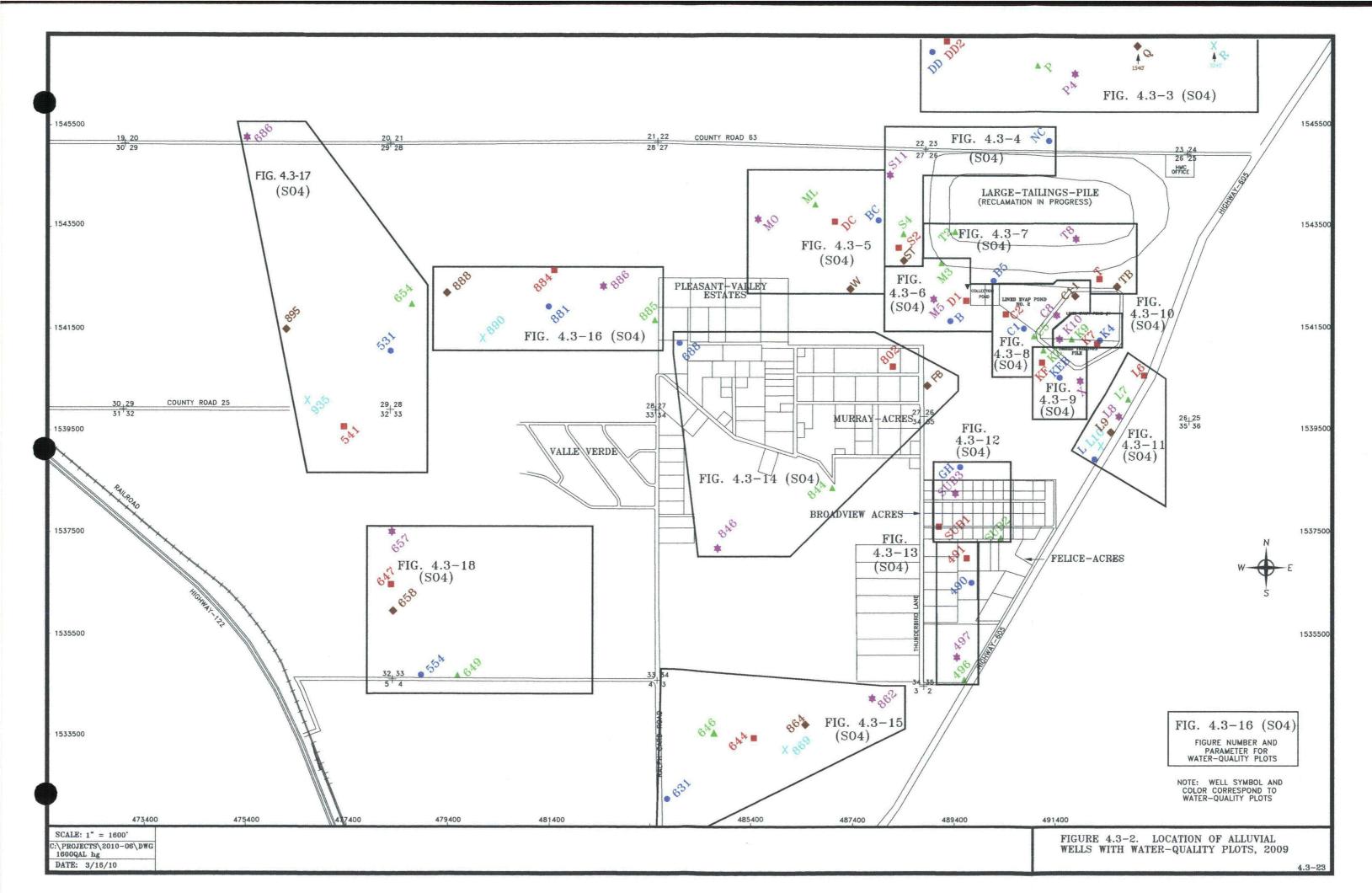
4.3.10 THORIUM-230 - ALLUVIAL

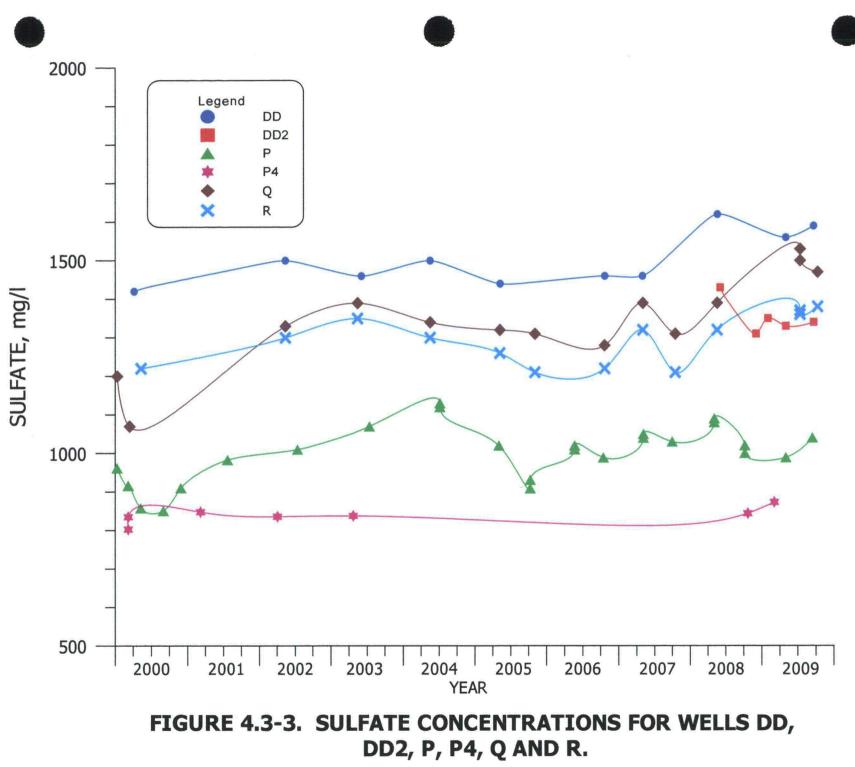
Figure 4.3-123 presents the 2009 thorium-230 concentrations in the alluvial aquifer. Thorium-230 concentrations are low at this site. The very low site standard of 0.3 pCi/l was established to reflect the low background concentrations. The thorium-230 activity was significant in some of the alluvial wells underneath the Large Tailings Pile in 2004. Thorium-230 has not been mobile in the alluvial aquifer except in the immediate vicinity of the tailings. The site standard for thorium-230 was exceeded in 2004 in ten wells in the alluvial aquifer underneath the Large Tailings Pile. This area is within the collection area, and additional

restoration will result from the ongoing collection/injection programs. Thorium-230 levels in wells 490, 649, 659, 688, 802, 846, M16, SUB1, SUB2 and SUB3, the three POC wells and upgradient wells were measured in 2009. All values in 2009 were less than the site standard. Therefore, only the alluvial aquifer underneath the Large Tailings Pile needs restoration relative to this parameter.

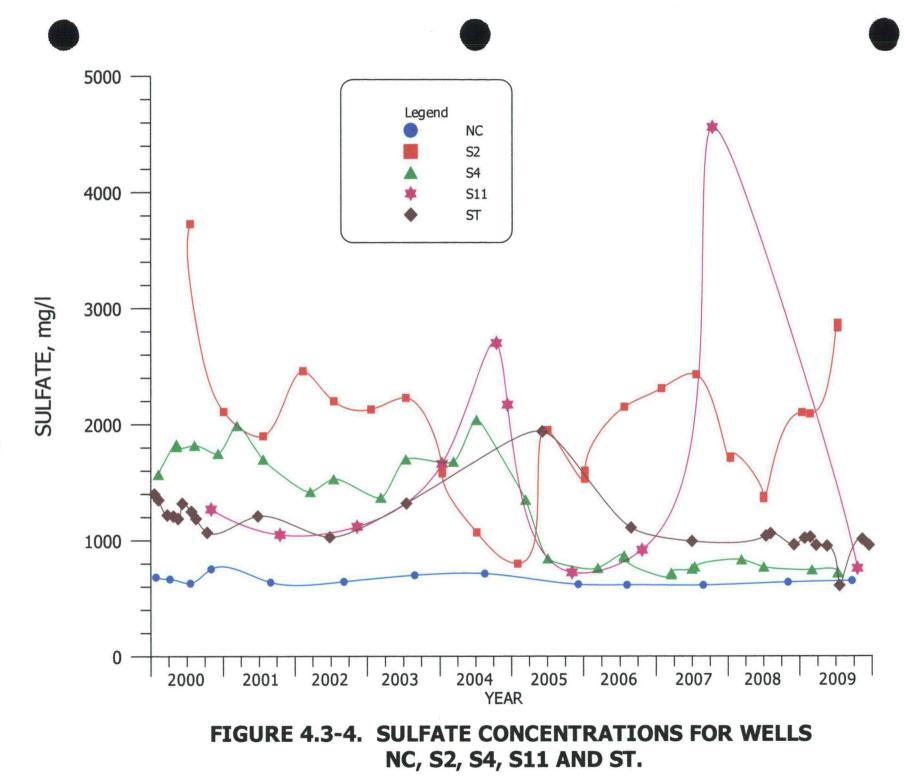


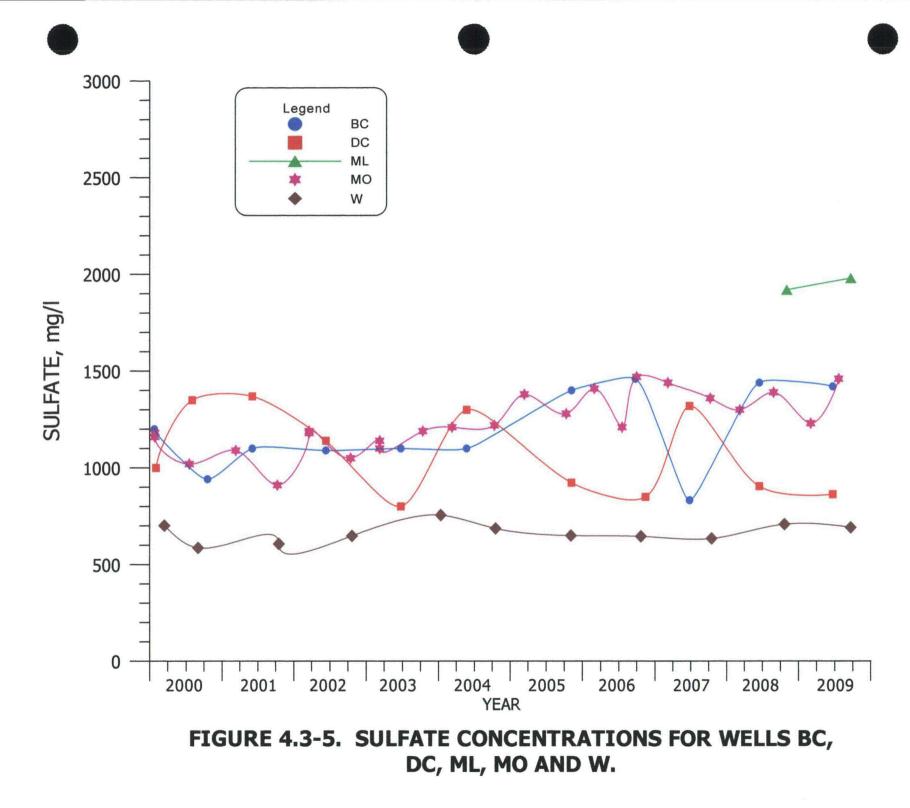


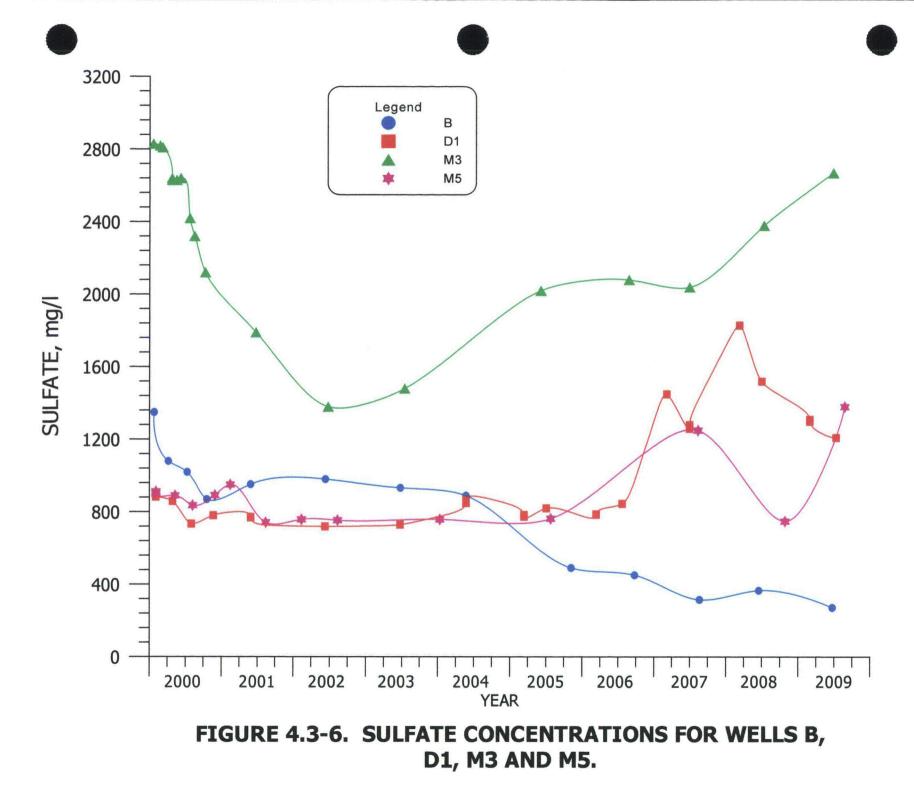


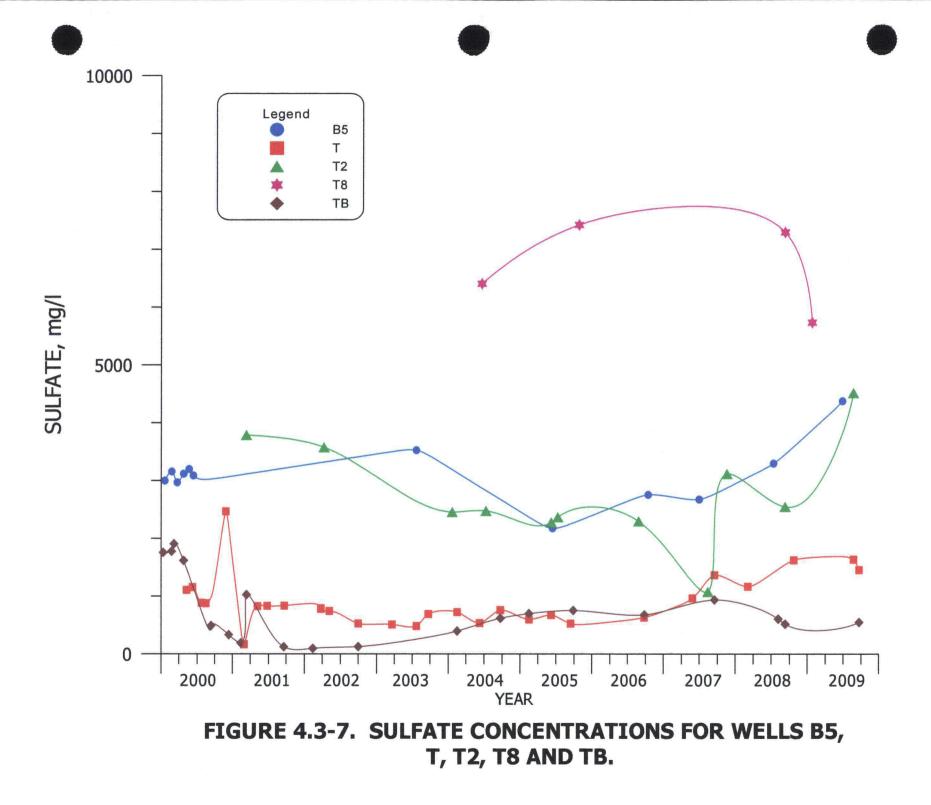


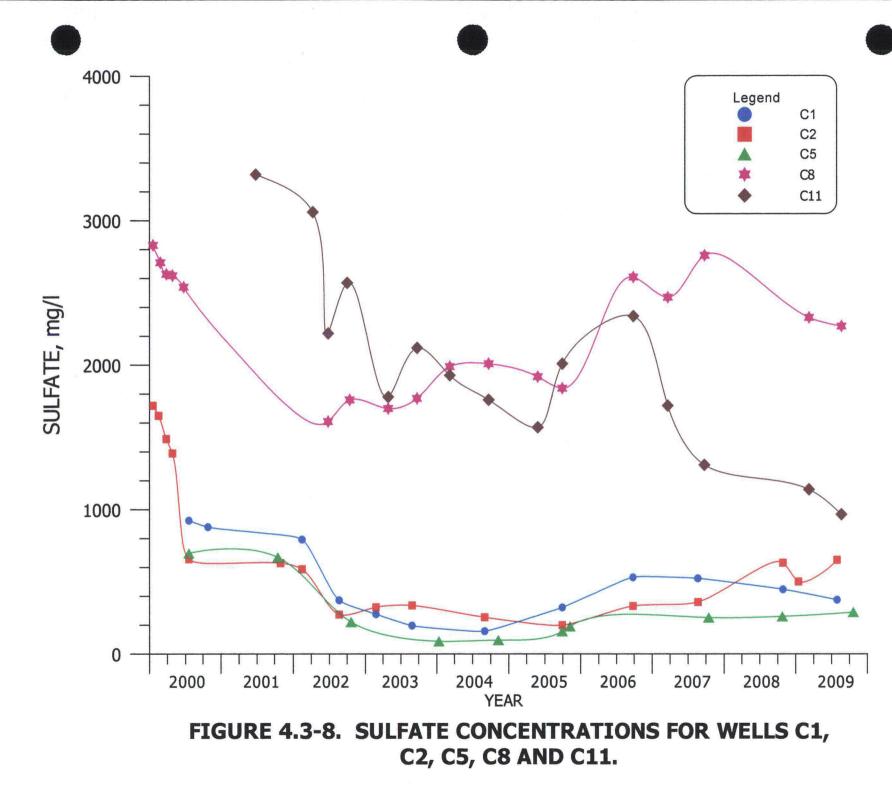


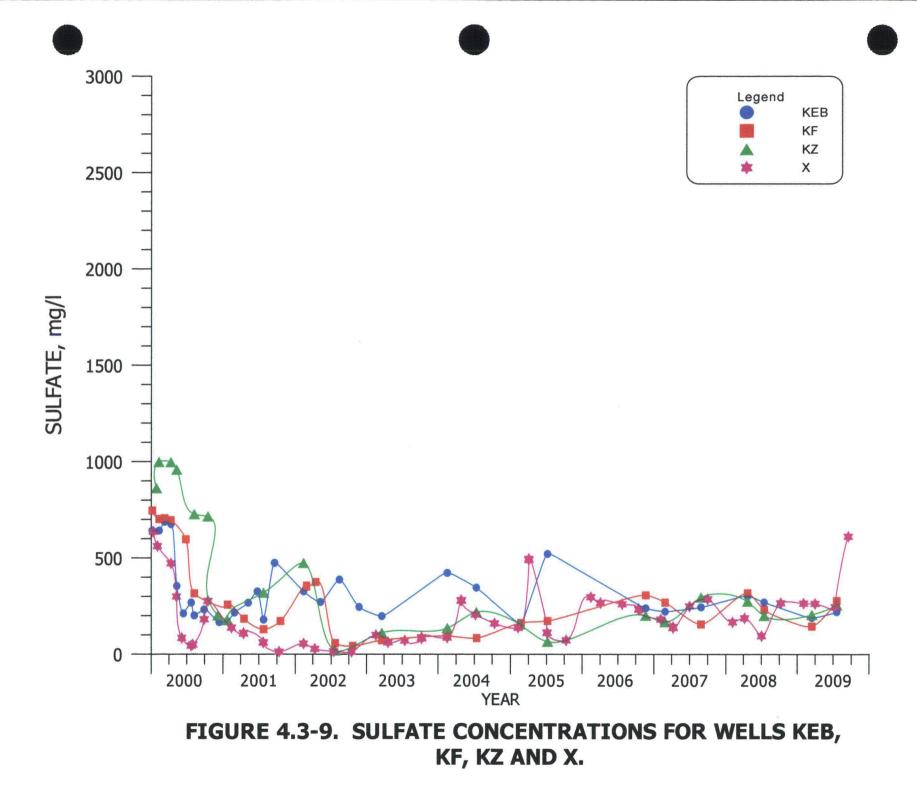


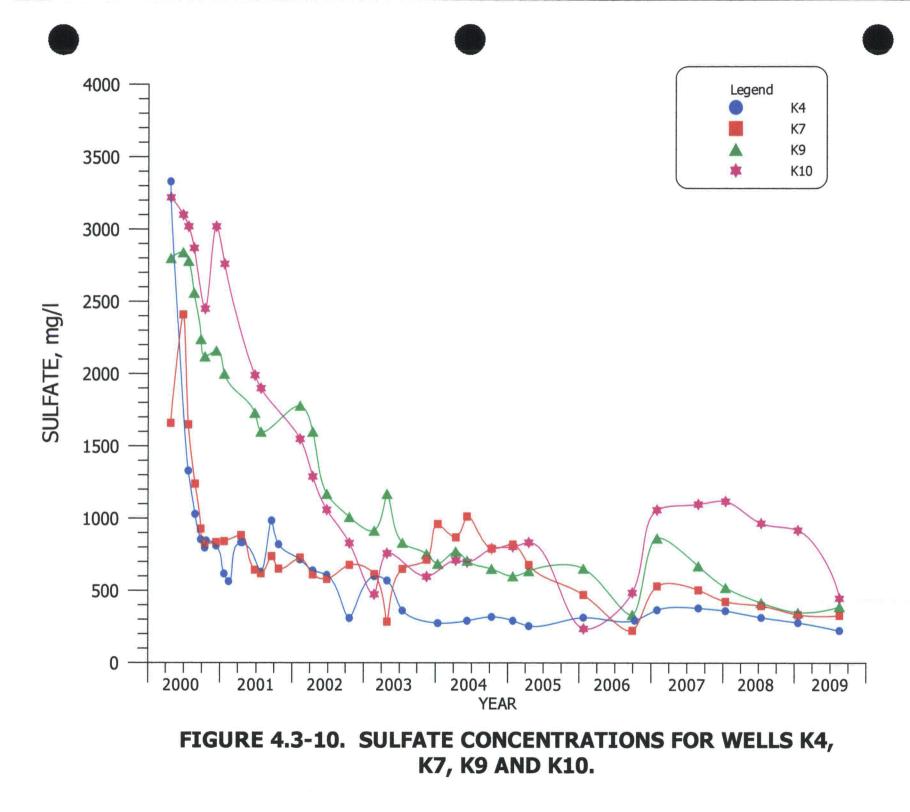




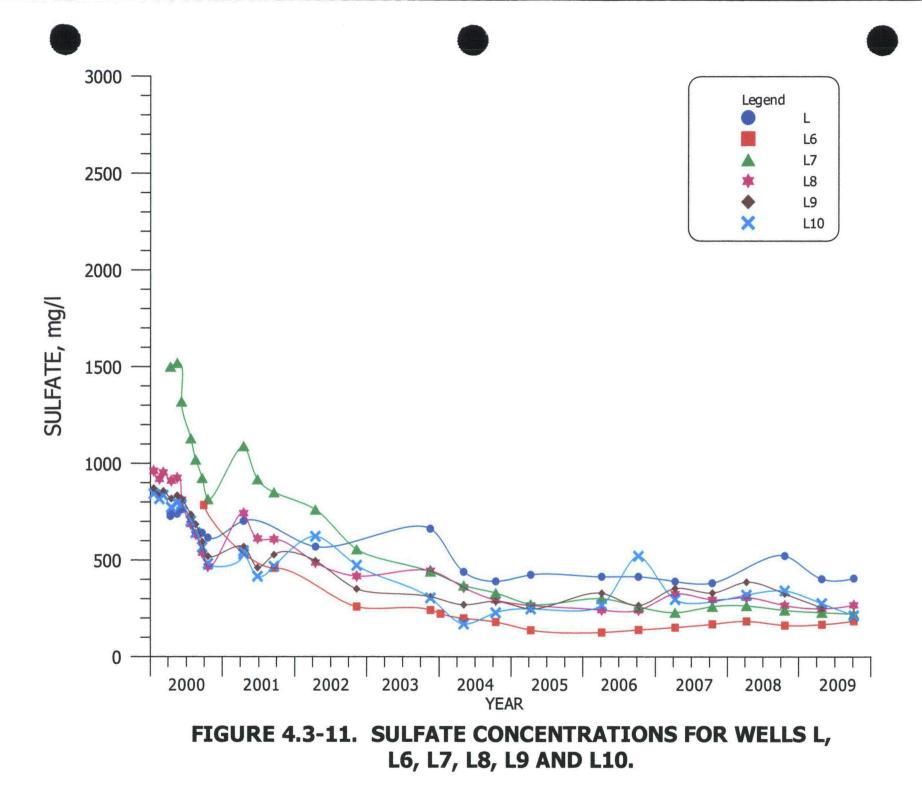


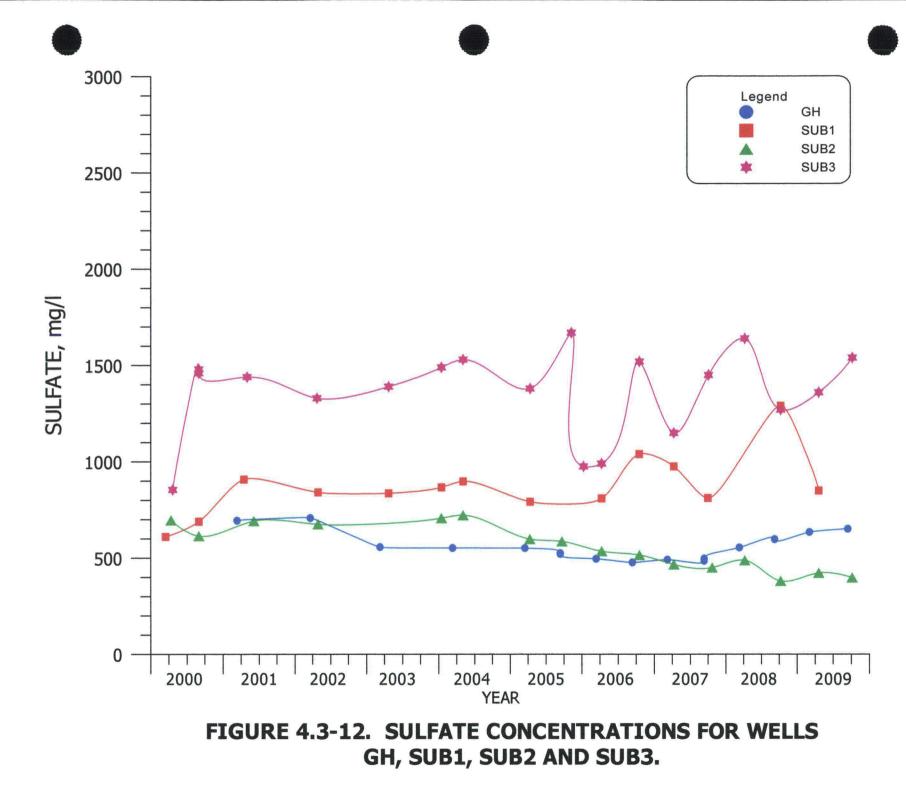


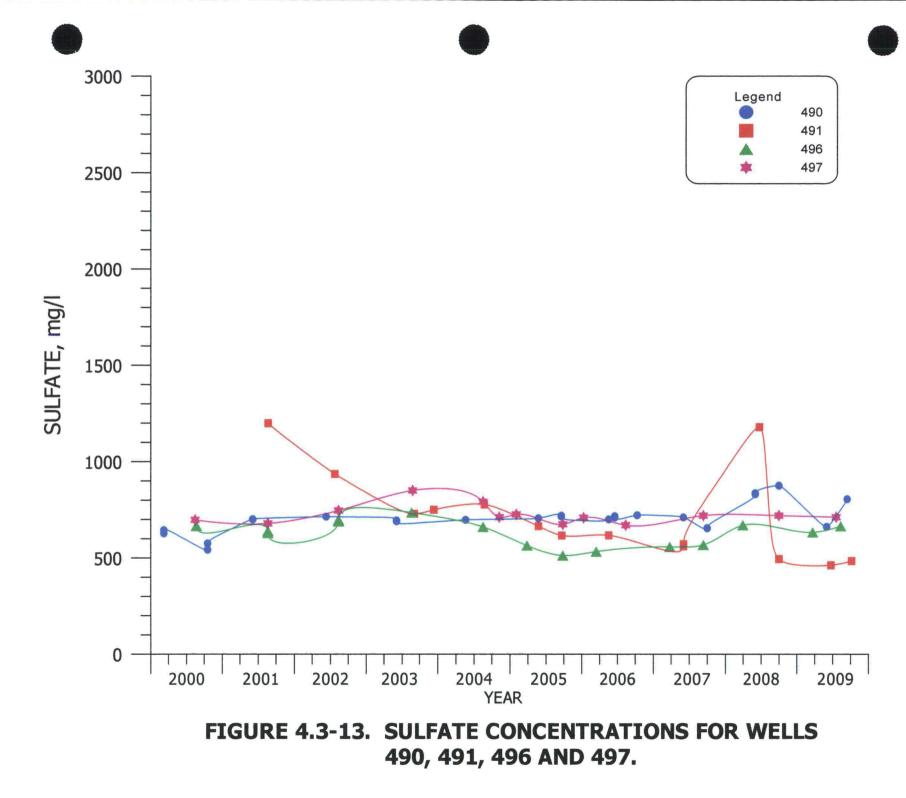


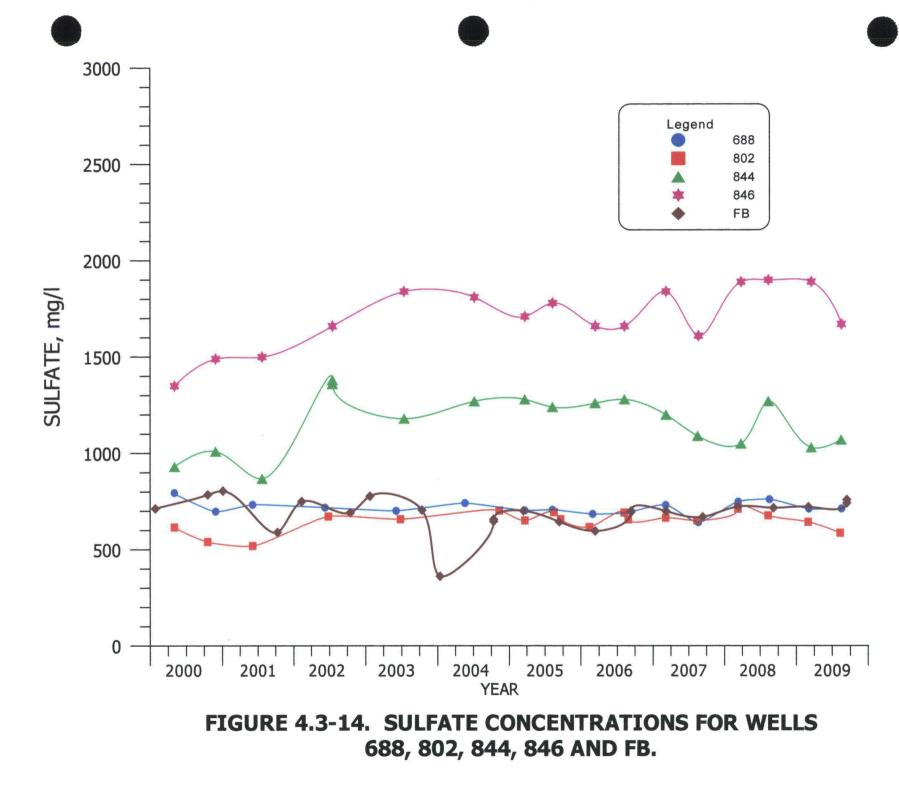


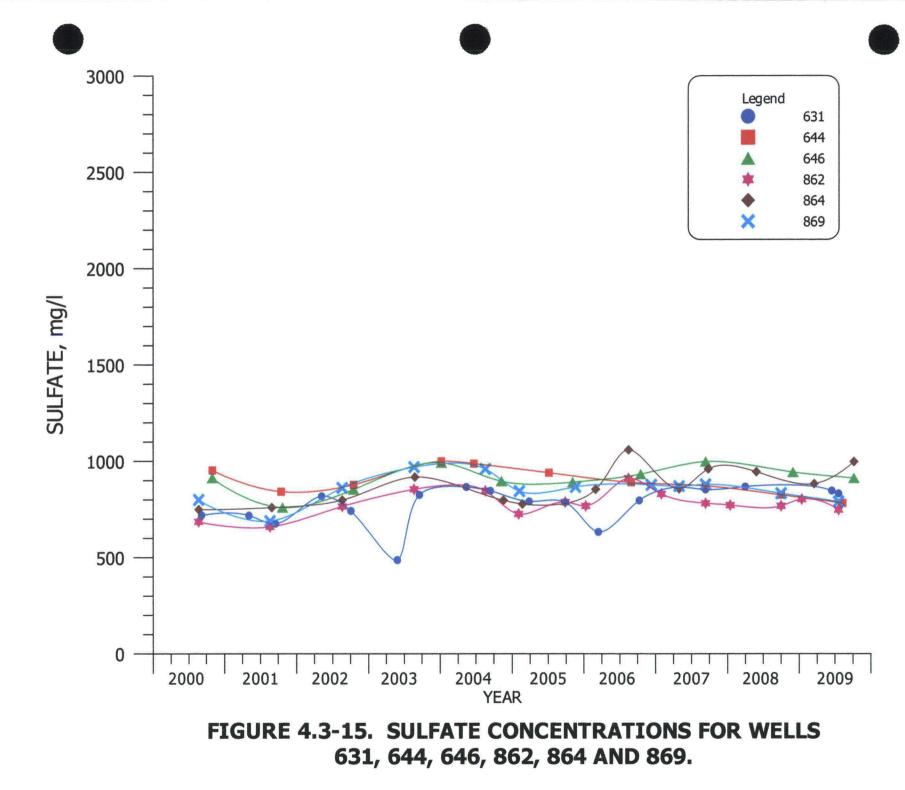
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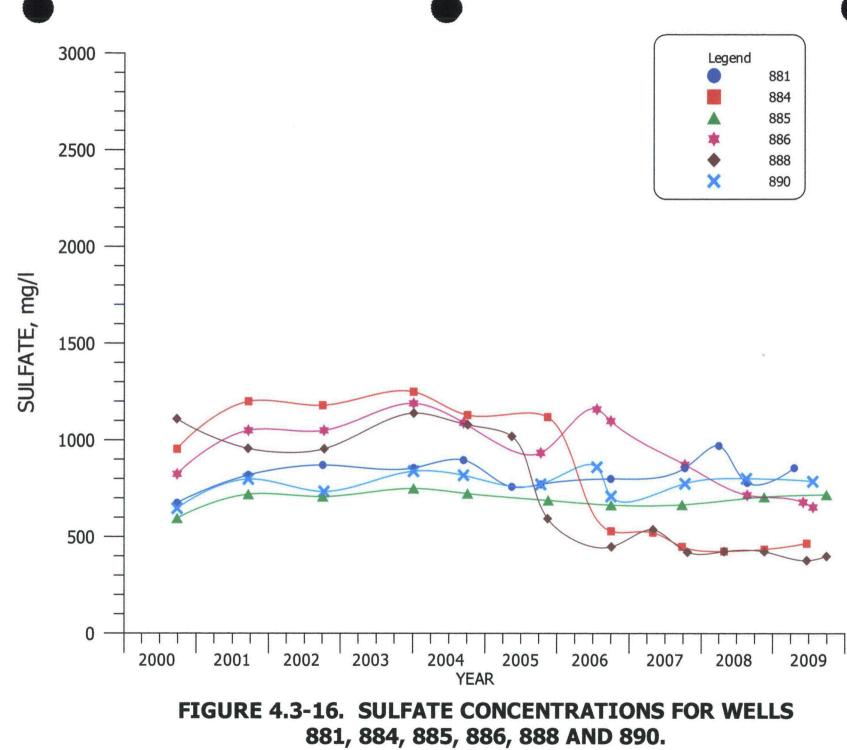


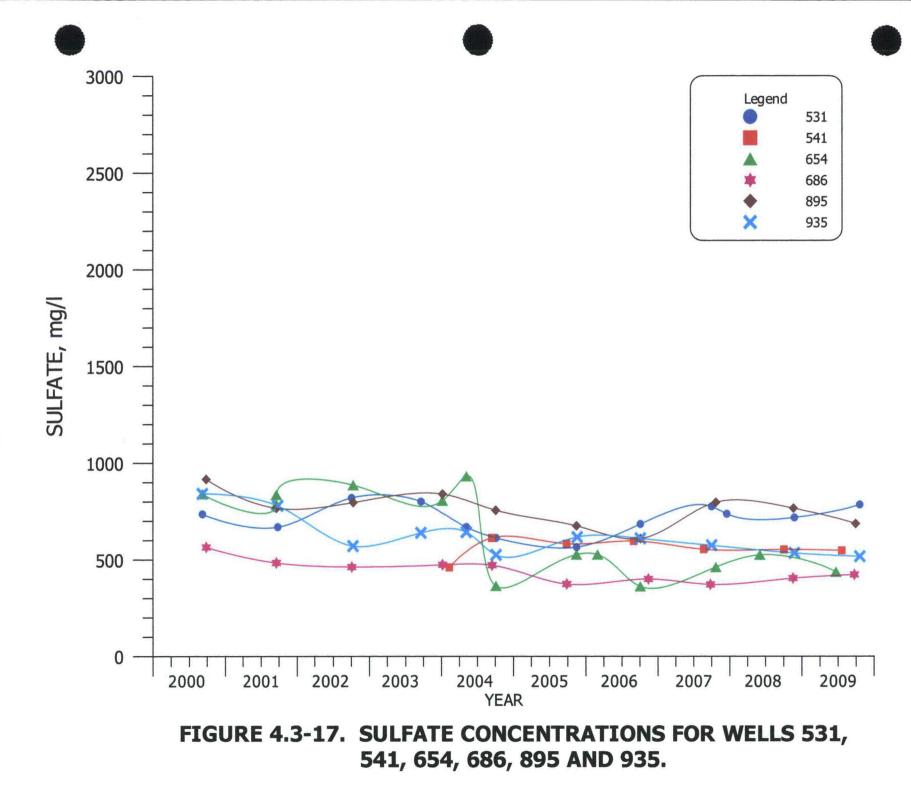


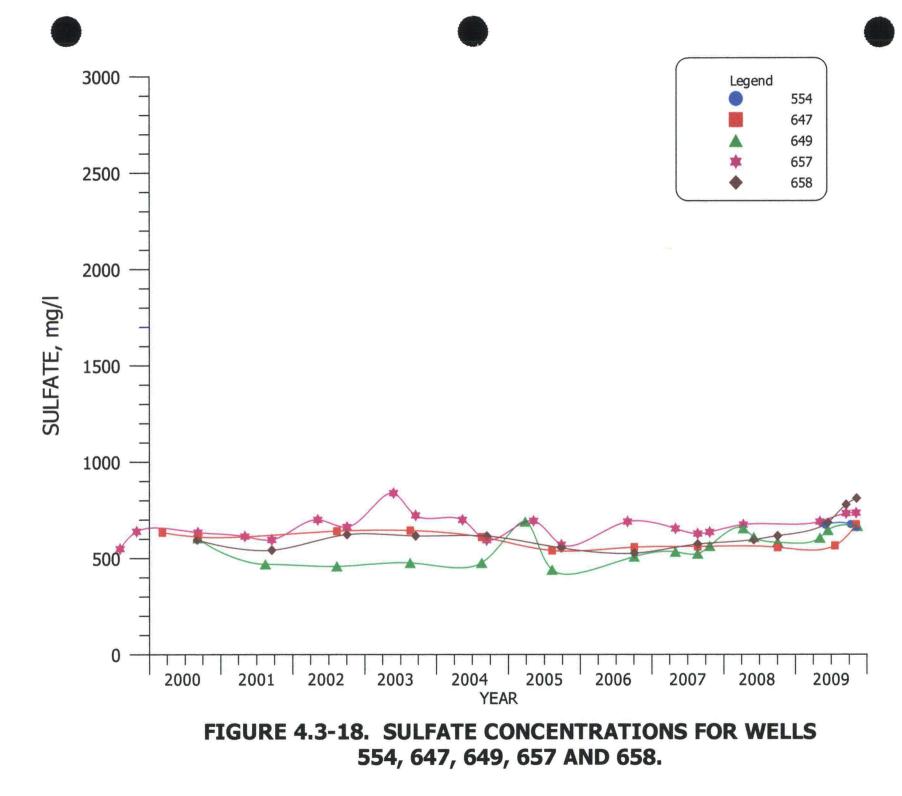




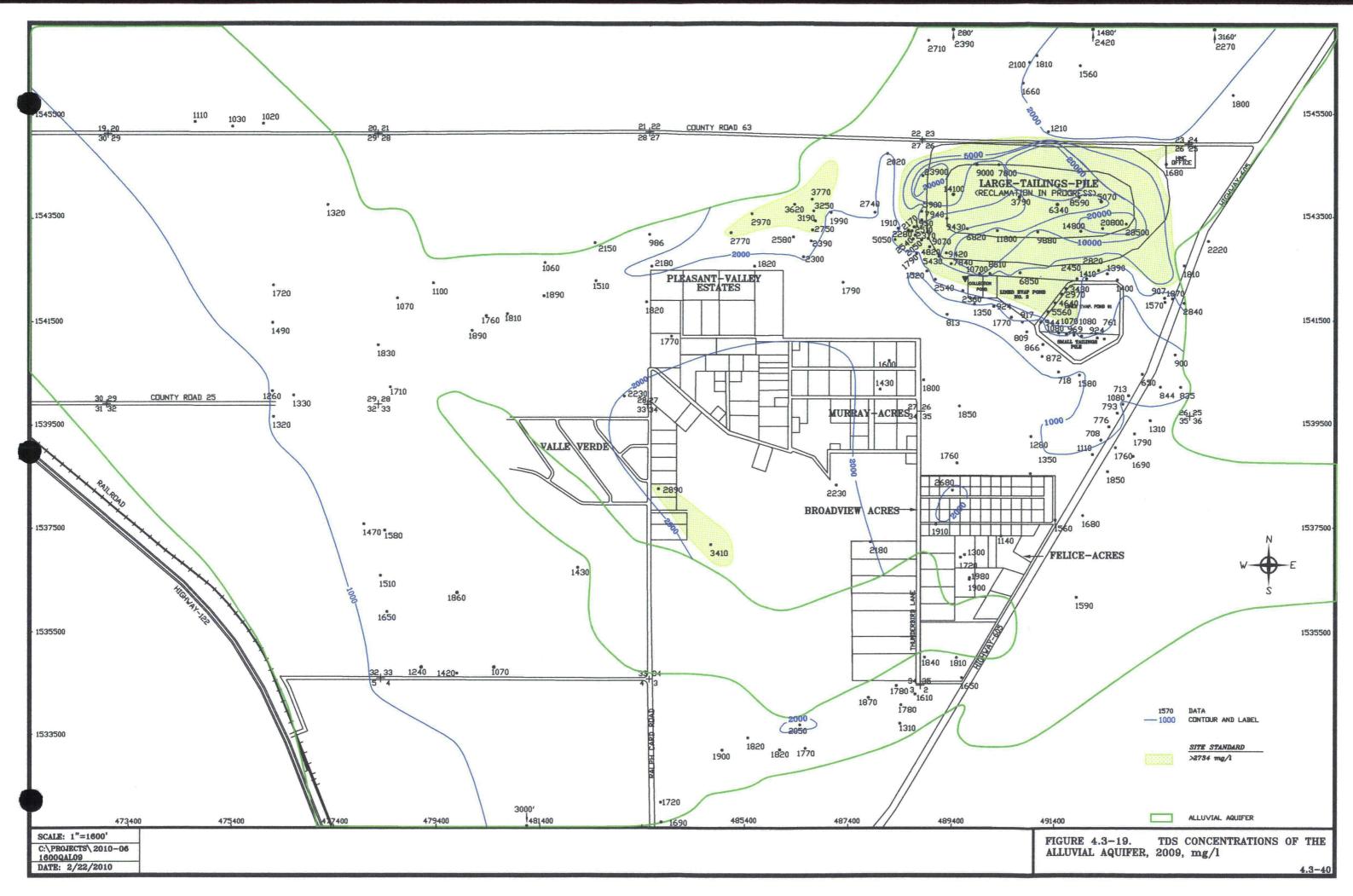


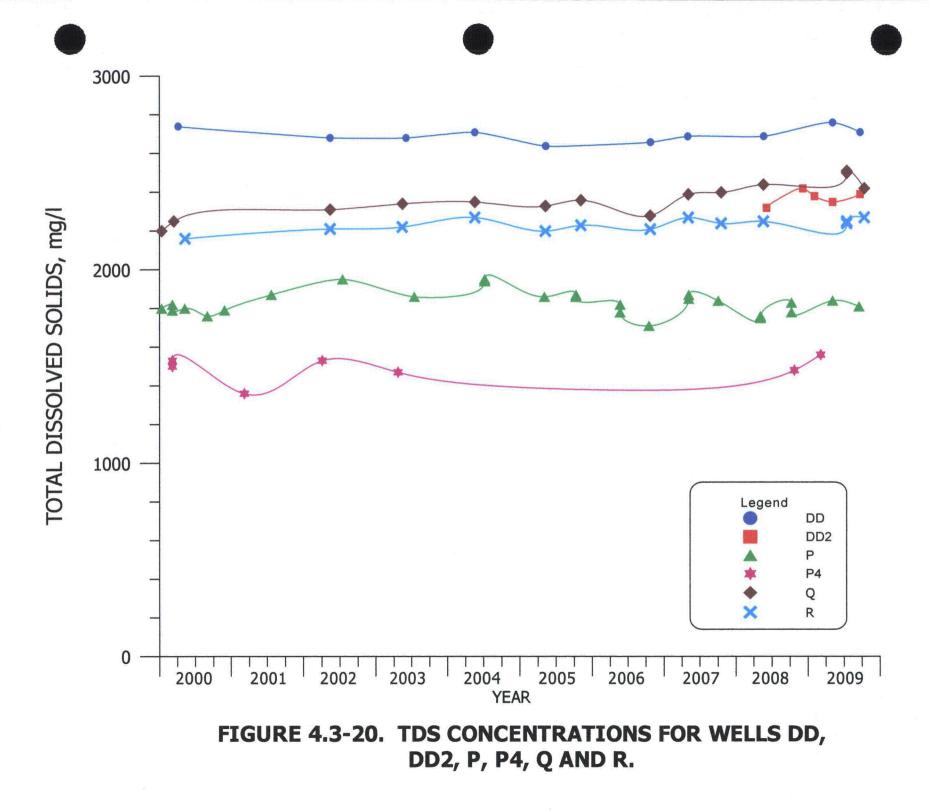


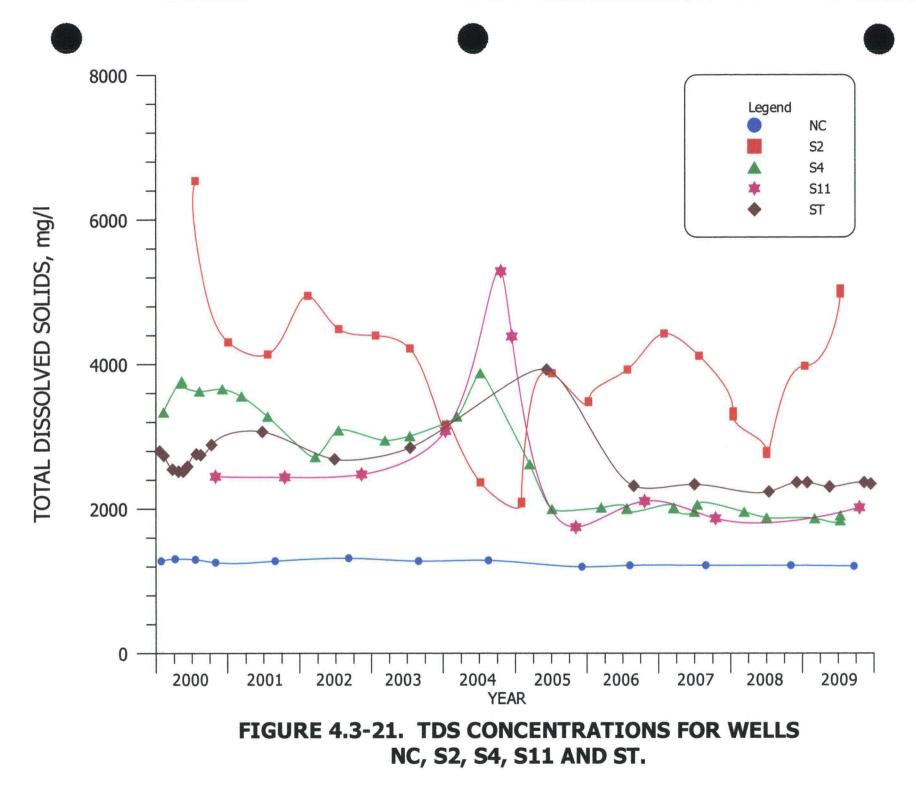


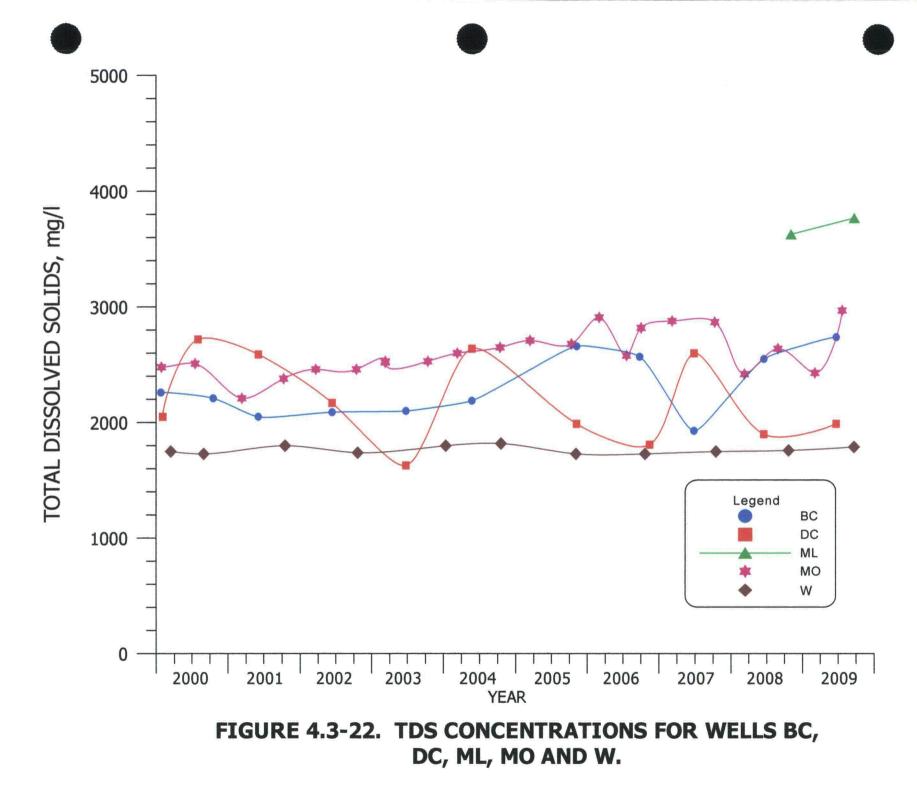


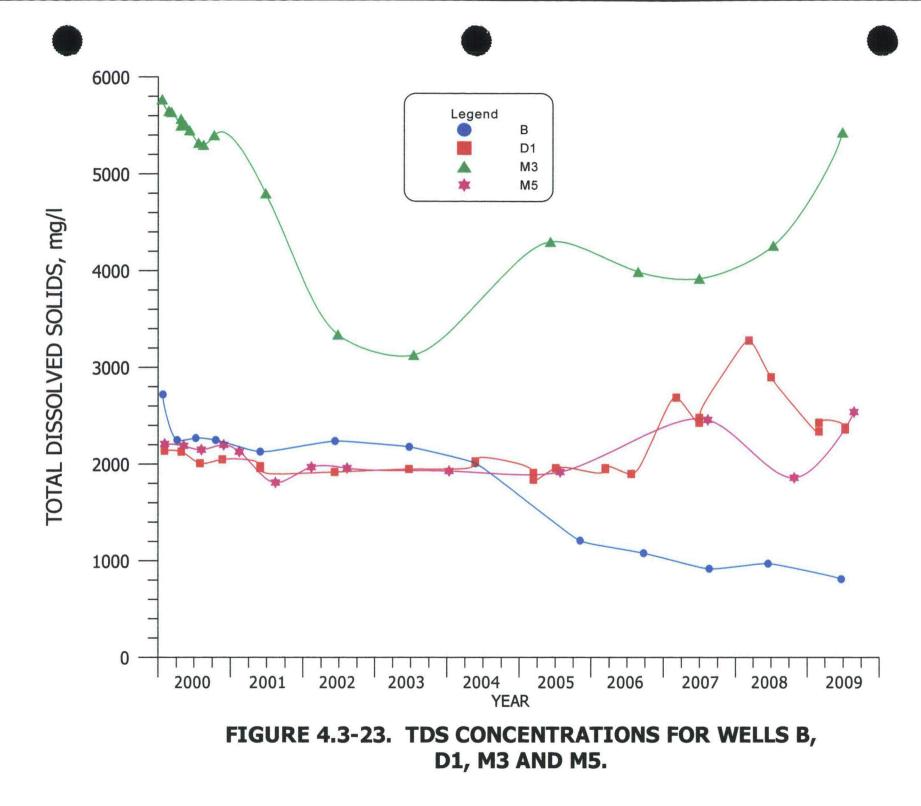
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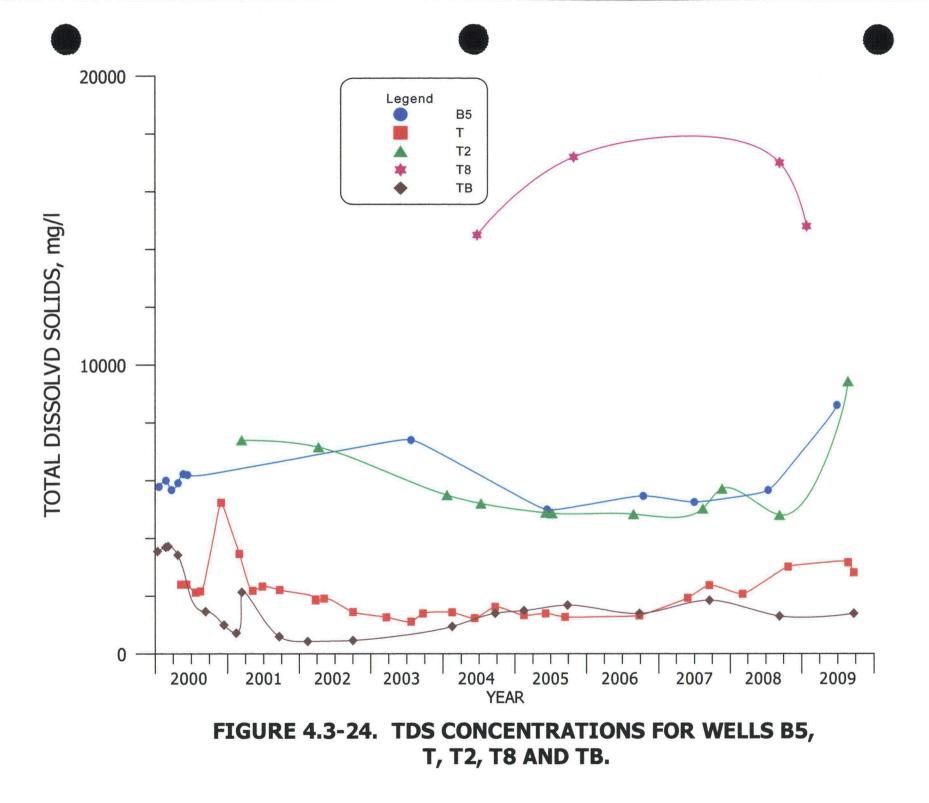


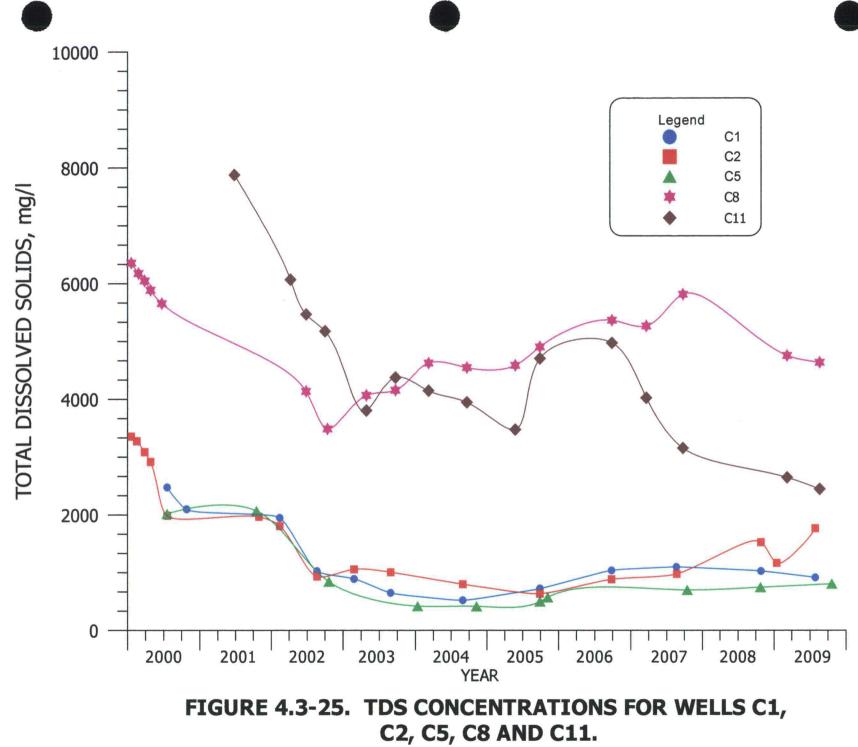


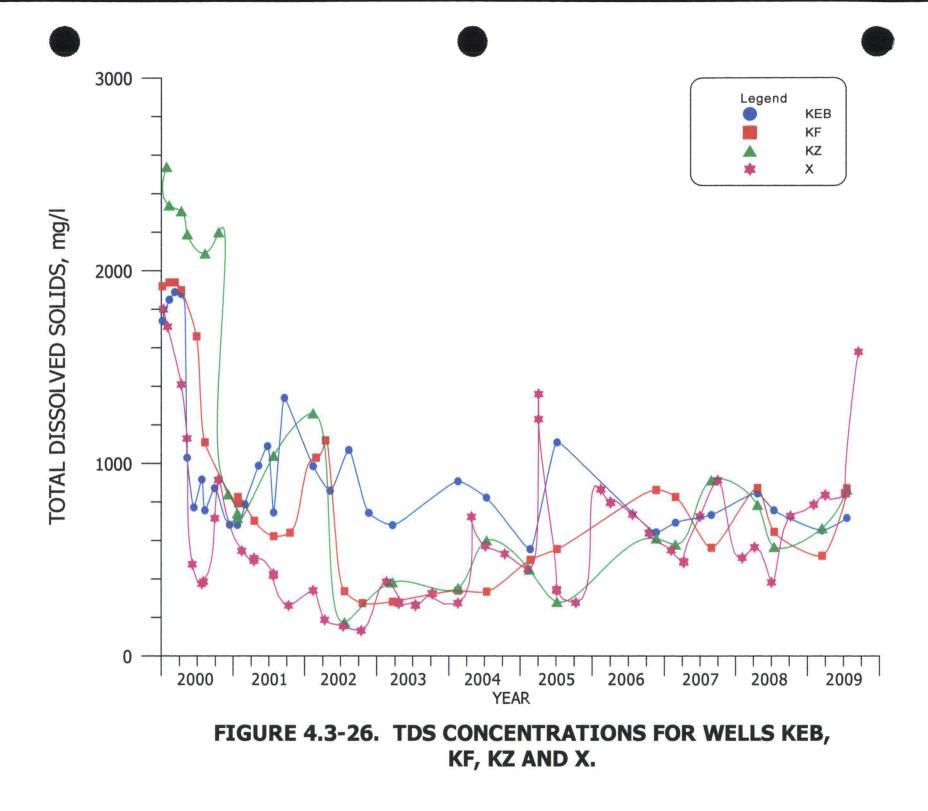


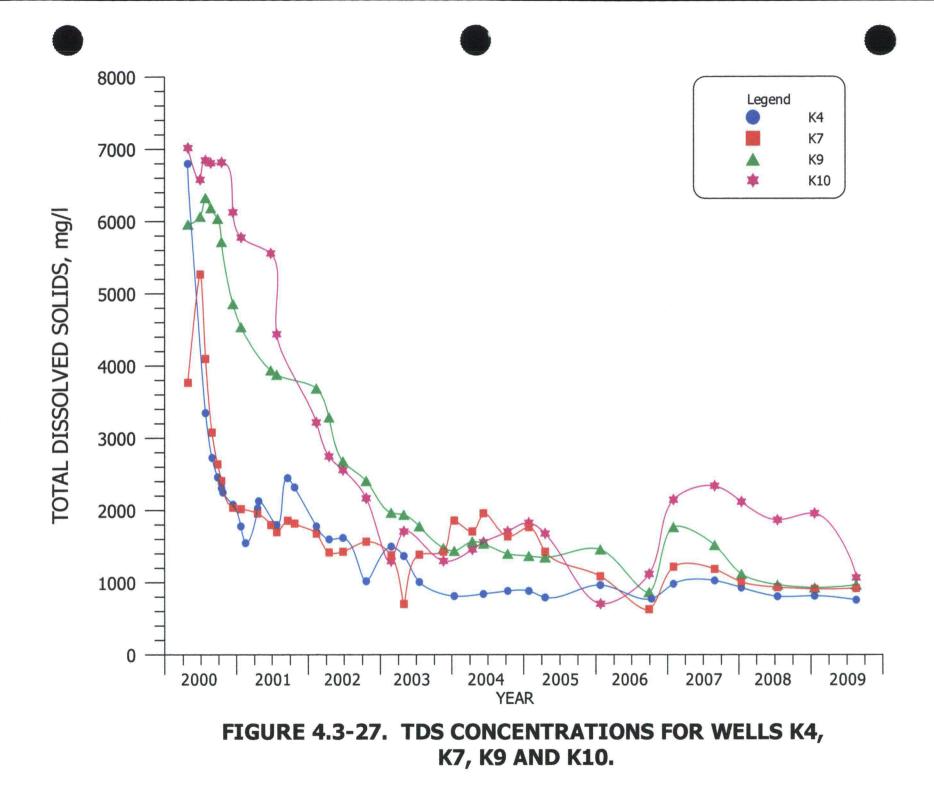


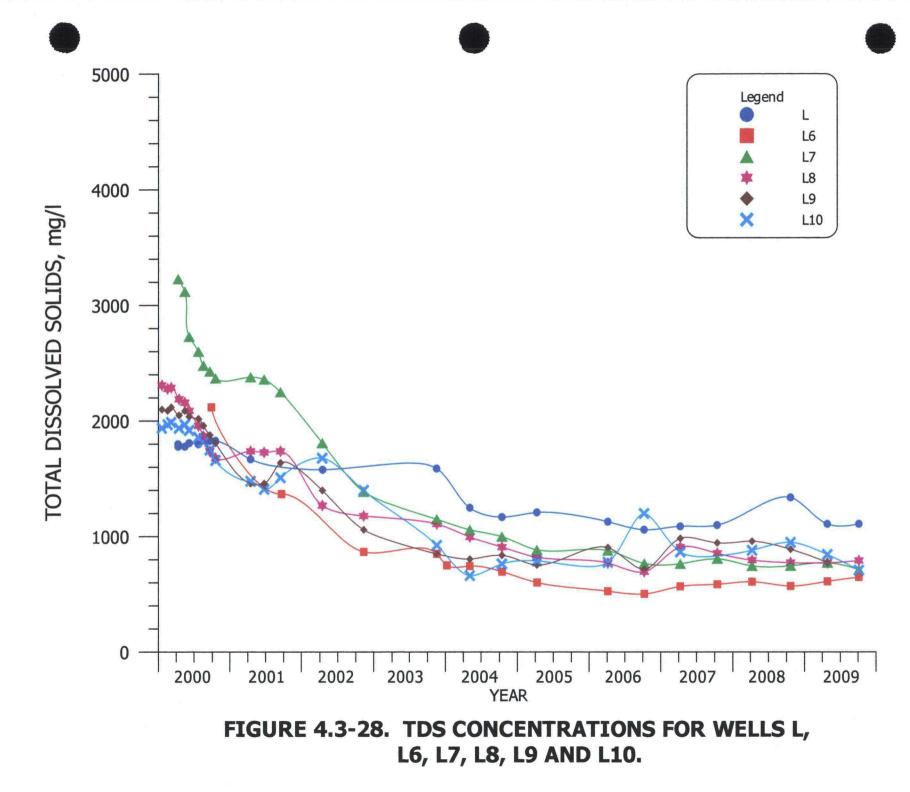


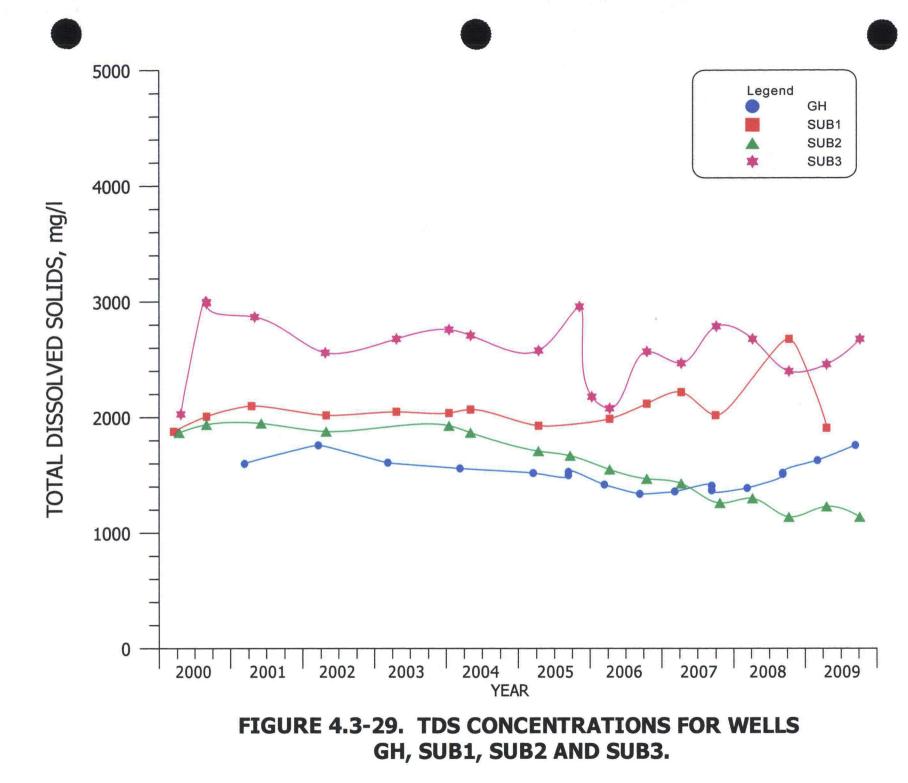


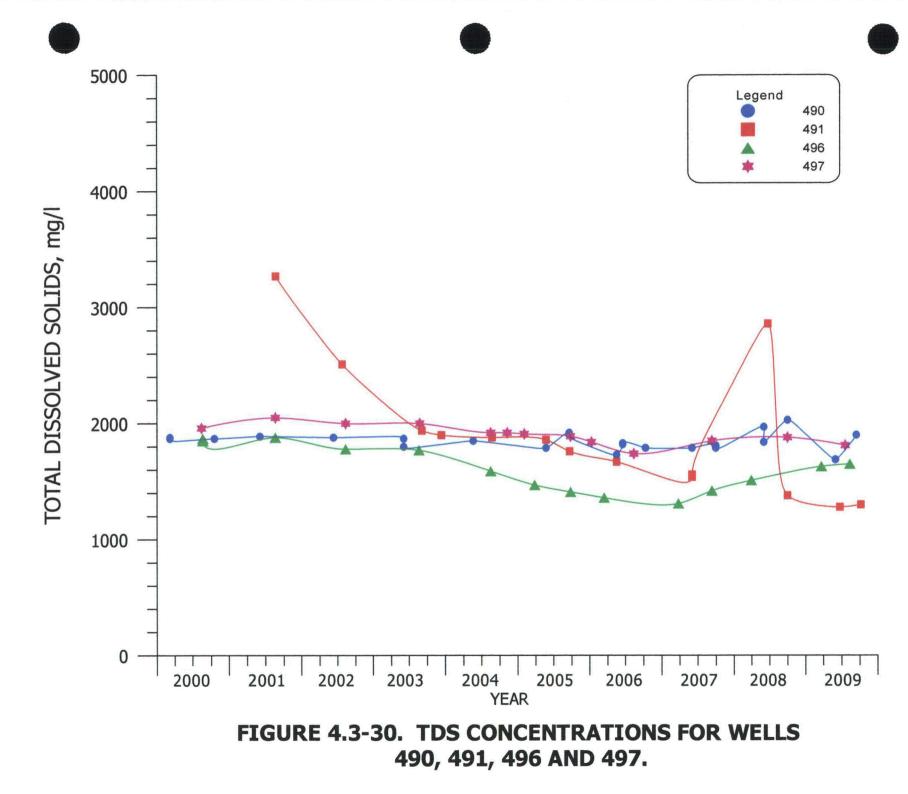


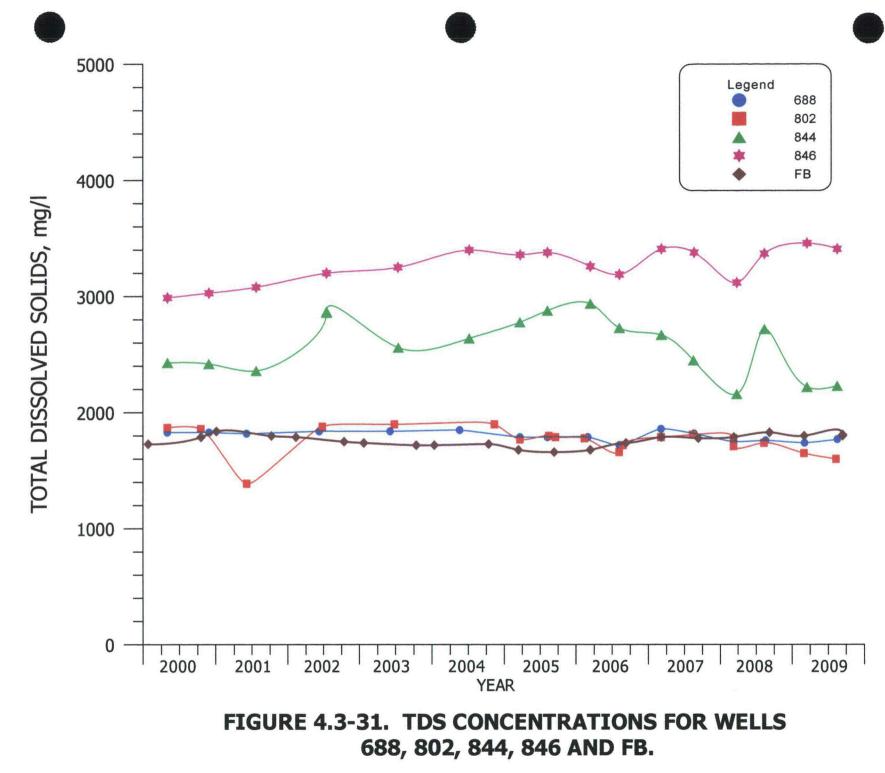


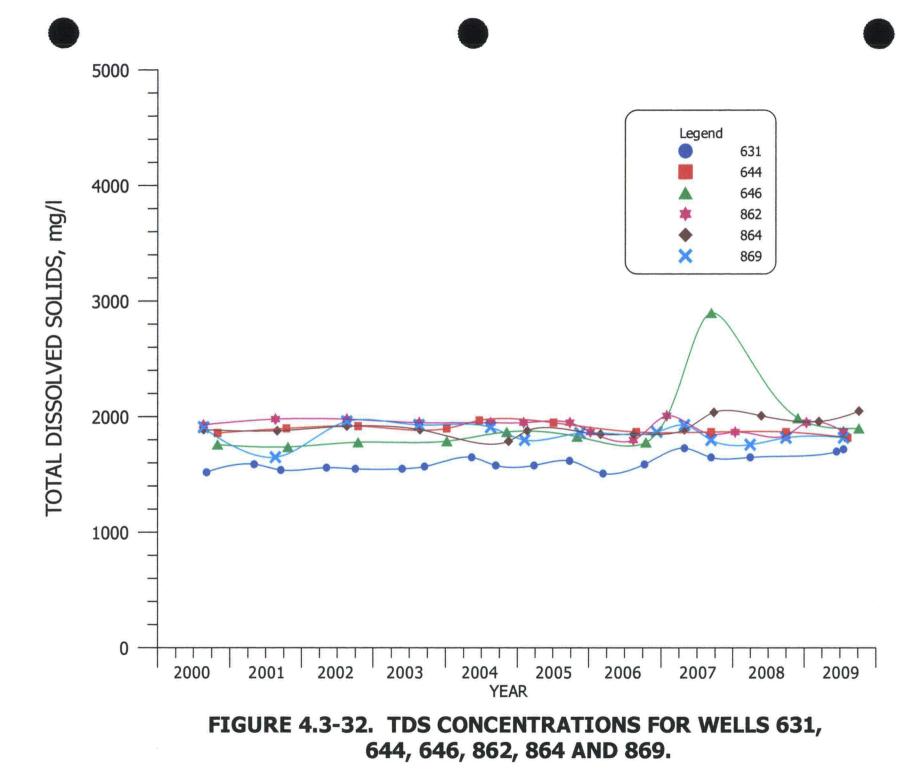


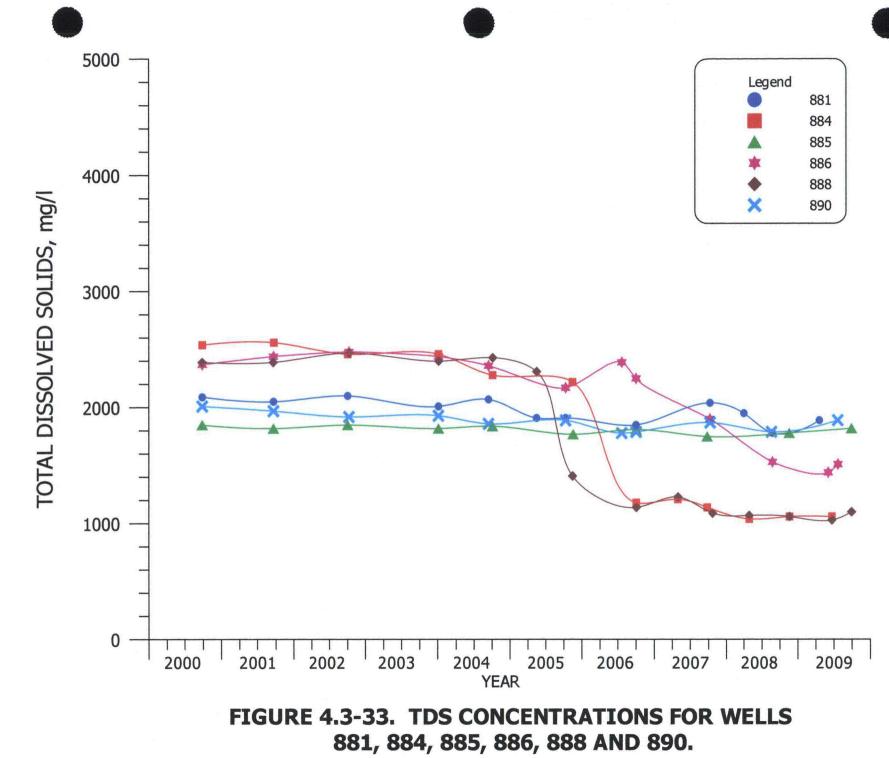


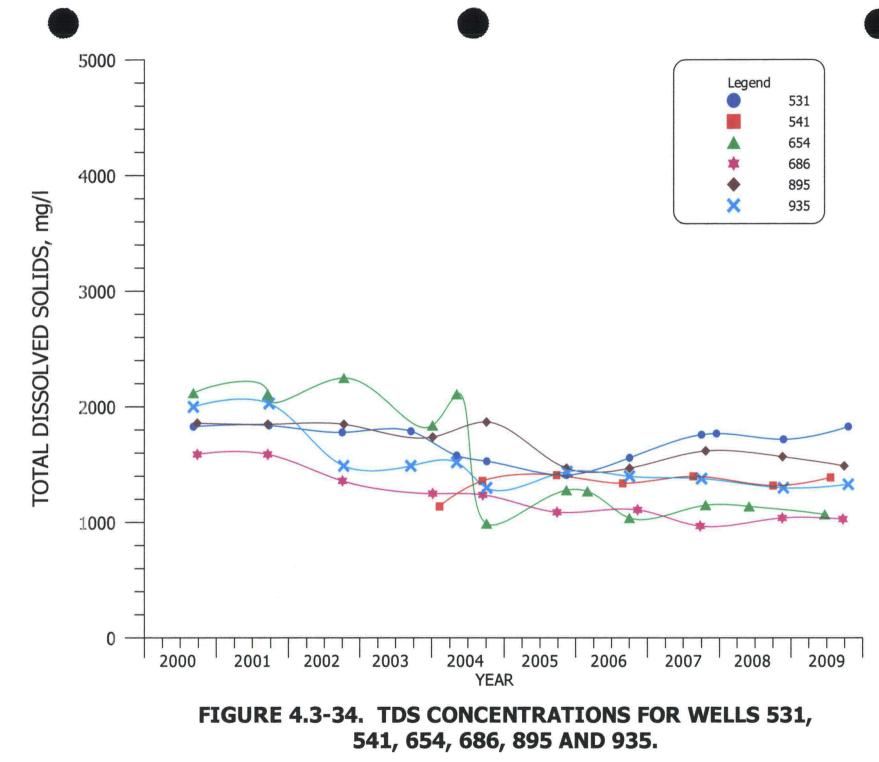


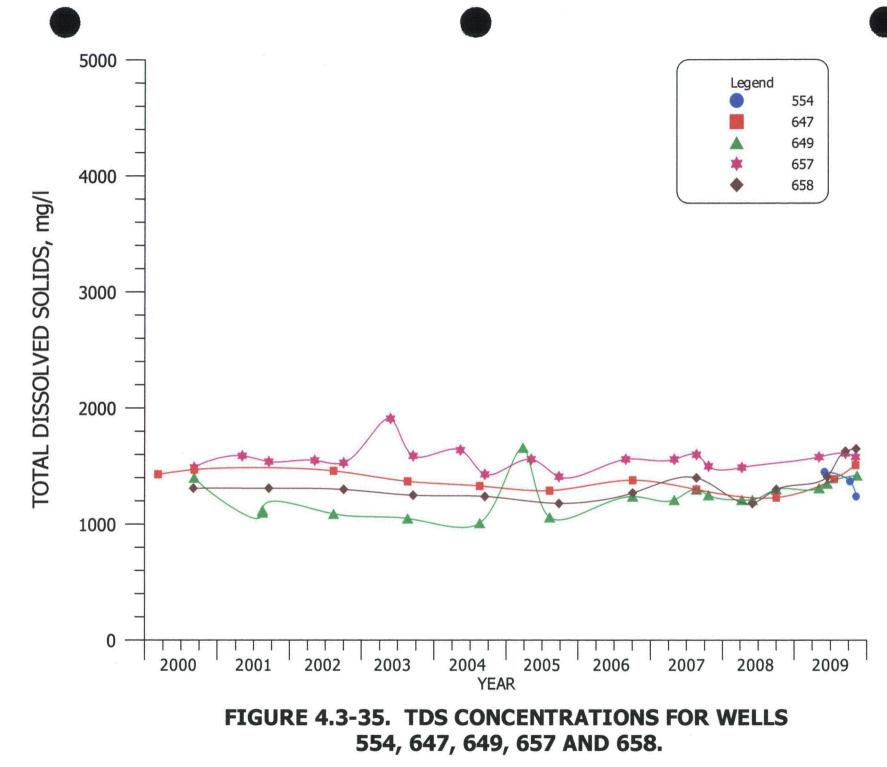


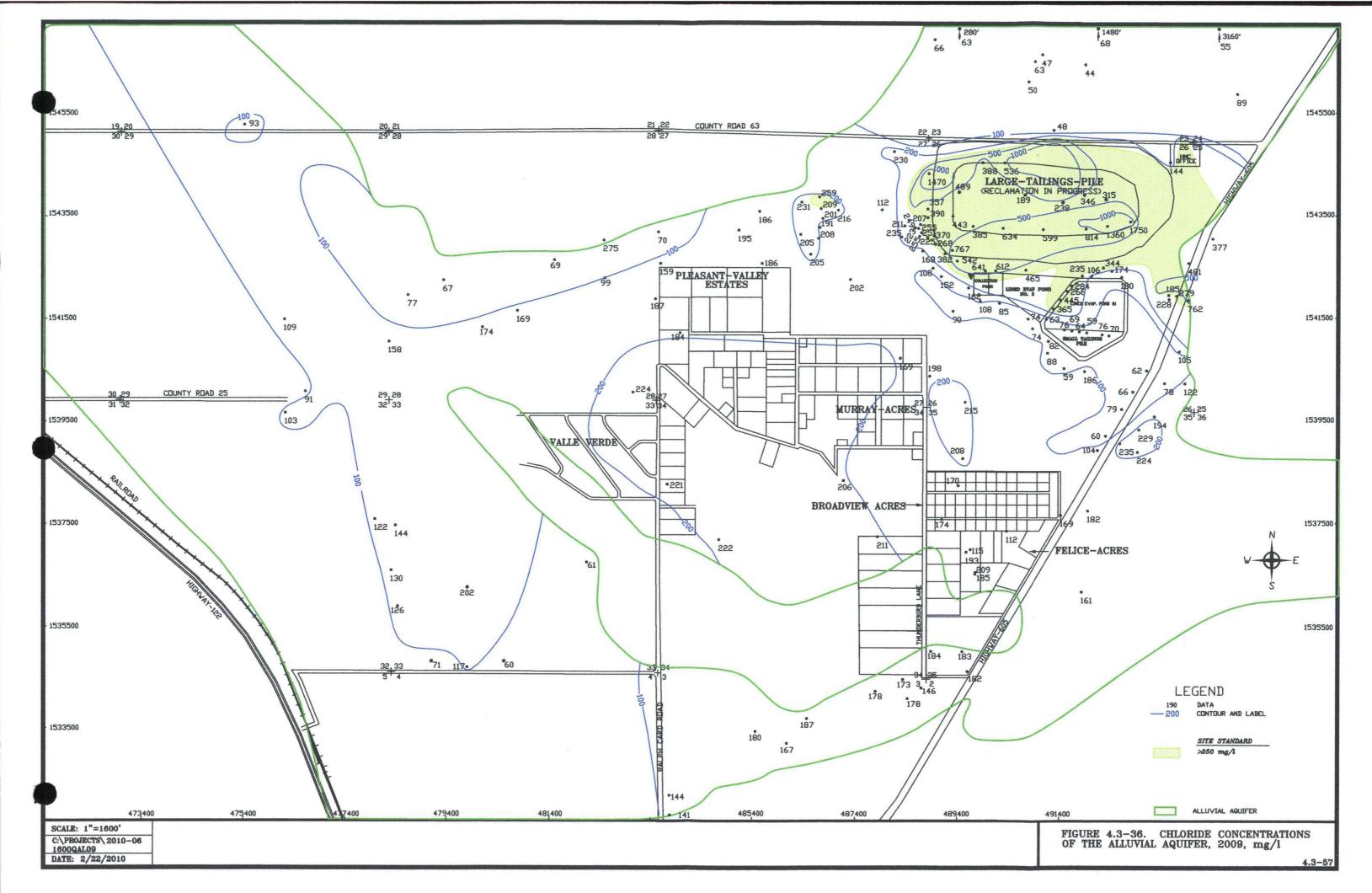


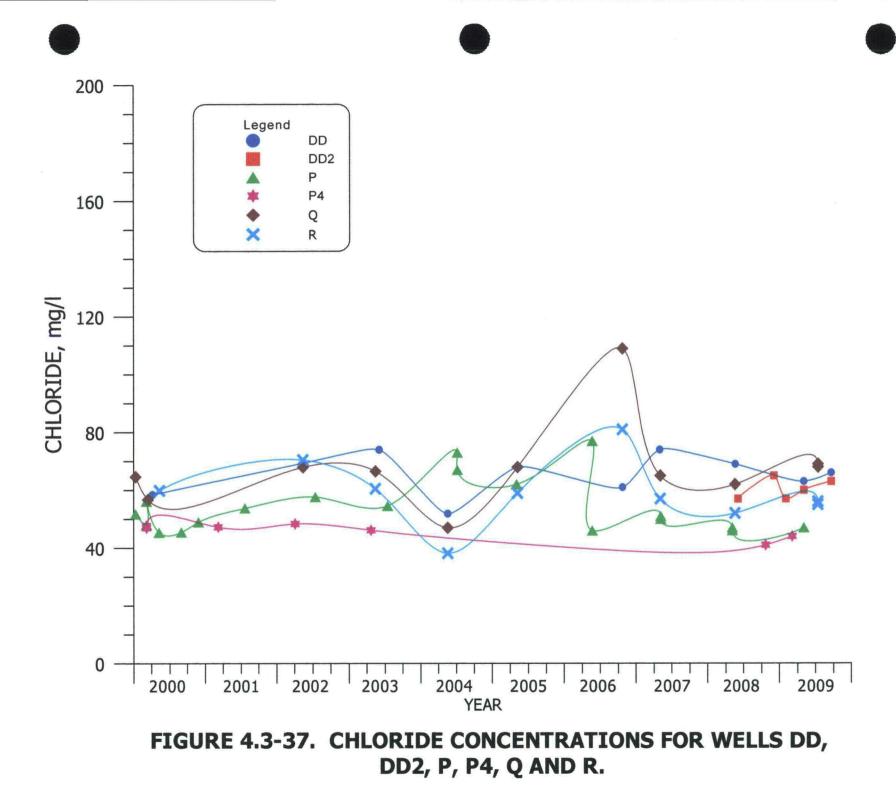


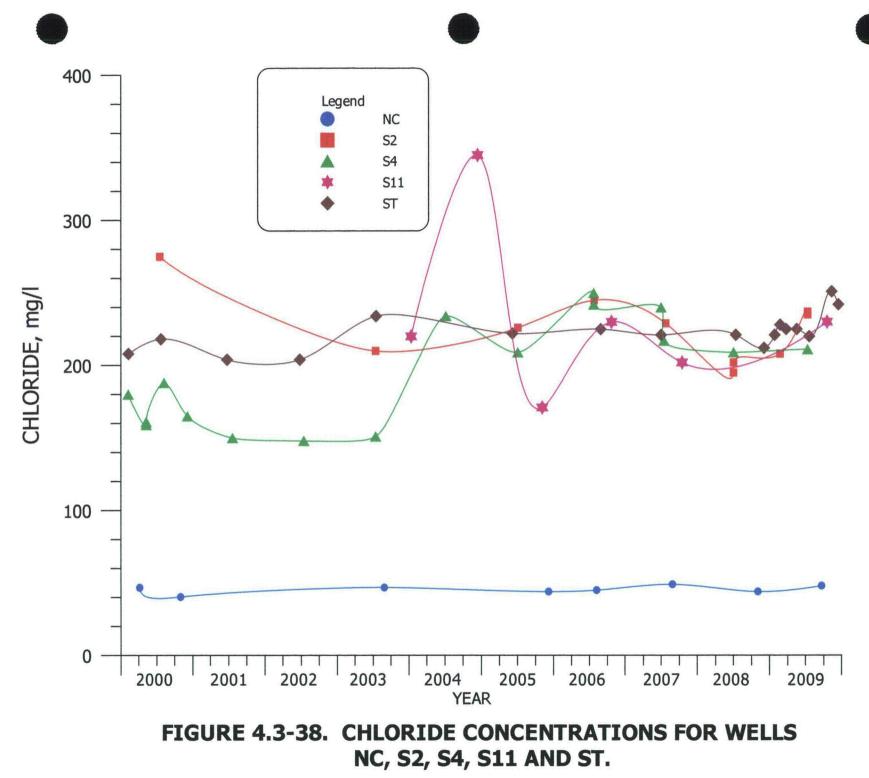












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