UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

April 12, 2010

Mr. Barry S. Allen
Site Vice President
FirstEnergy Nuclear Operating Company
Davis-Besse Nuclear Power Station
Mail Stop A-DB-3080
5501 North State Route 2
Oak Harbor, OH 43449-9760

SUBJECT: DAVIS-BESSE NUCLEAR POWER STATION UNIT 1 – SUMMARY OF MARCH 18, 2010, CONFERENCE CALL REGARDING THE SPRING 2010 REFUELING OUTAGE STEAM GENERATOR INSERVICE INSPECTIONS (TAC NO. ME3427)

Dear Mr. Allen:

On March 18, 2010, the U.S. Nuclear Regulatory Commission (NRC) staff participated in a conference call with FirstEnergy Nuclear Operating Company (FENOC) staff, regarding the spring 2010, refueling outage, steam generator inspections at the Davis-Besse Nuclear Power Station, Unit 1. A summary of the notes by the NRC staff of the March 18, 2010, conference call is enclosed. In addition, a handout provided by FENOC to support the conference call is also enclosed. The NRC staff did not identify any issues that would require follow-up action at this time; however, the staff asked to be notified in the event any unusual conditions were detected during the remainder of the outage.

If you have any questions, please call me at (301) 415–3867.

Sincerely,

Michael Mahoney, Project Manager
Plant Licensing Branch III-2
Division of Operating Reactor Licensing
Office of Nuclear Reactor Regulation

Docket No. 50-346

Enclosures:
1. Summary of conference call
2. DBNPS Steam Generator Inspections data March 18, 2010

cc w/encl: Distribution via Listserv

CONFERENCE CALL SUMMARY
DAVIS-BESSE NUCLEAR POWER STATION REGARDING
SPRING 2010, REFUELING OUTAGE, STEAM GENERATOR INSPECTION RESULTS

On March 18, 2010, the staff of the Steam Generator Tube Integrity and Chemical Engineering Branch of the Division of Component Integrity participated in a conference call with FirstEnergy Nuclear Operating Company (the licensee), regarding the ongoing steam generator (SG) inspection activities at Davis-Besse Nuclear Power Station (DBNPS) Unit 1.

There are two Babcock and Wilcox once-through steam generators (OTSG), designated 1-B and 2-A, at DBNPS. Each SG has approximately 15,500 Alloy 600 tubes in the mill-annealed condition. The tubes have a nominal outside diameter of 0.625 inches and a nominal wall thickness of 0.037 inches. Both OTSG 1-B and 2-A contain tubes with sleeves.

Additional clarifying information or information not included in the document (Enclosure 2) provided by the licensee is summarized below.

> At the time of the call, DBNPS SGs had operated for 21.2 effective full power years. In the recently completed cycle, they operated for 717 effective full power days. SG 2A has 625 (or 4 percent) tubes plugged, 199 sleeves, and 131 repair rolls. SG 1B has 279 (or 1.8 percent) tubes plugged, 212 sleeves, and 31 repair rolls. These two SGs are scheduled to be replaced in 2014 during refueling outage 18.
>
> The primary-to-secondary leakage rate during the recently completed cycle (Cycle 16) was approximately 0.02 gallons per day, until April 2009. In April 2009, the plant was shut down and restarted for maintenance on a pressurizer safety valve. After the plant restart, the primary-to-secondary leak rate increased from 0.02 to 0.1 gallons per day. This increase in leak rate was suspected to be the result of a welded plug that cracked during the shutdown/startup transient. Due to the low leak rate, a secondary side pressure test was not performed.
>
> No exceptions were taken to the industry Pressurized-Water Reactor Steam Generator Examination Guidelines.
>
> In the Table, "Steam Generator Inspection Data – March 18, 2010: Davis-Besse 16RFO Eddy Current Exam Scope" (Enclosure 2, page 1) provided by the licensee:
>
>> The periphery auxiliary feedwater (AFW) header-to-tube gap analysis is performed to determine if the position of the AFW header is changing relative to the inservice tubing. The analysis is performed with a bobbin coil and was approximately 95 percent complete at the time of the call. The AFW header does not appear to be moving.
>>
>> The "full length bobbin examination of all in-service non-sleeved tubing" includes the non-sleeved portion of sleeved tubes.
>>
>> The full length bobbin examination of 100 percent of sleeves is a bobbin exam of the sleeves only.

NSRT means non-stress relieved roll transition.

The +Point™ inspection of in-service stress relieved lower tube roll expansions and tube ends in SG 1-B included the second roll above the original roll, because primary water stress corrosion cracking (PWSCC) had been found between the two rolls in the heel transition of the upper roll.

The 50 percent +Point™ coil inspection of the defined lower tubesheet sludge pile region tubes was from three inches above to three inches below the tubesheet, unless the sludge pile went higher than 3 inches above the top of the tubesheet (in which case the entire portion of the tube in the sludge pile was examined).

The geometric distortions are small indentations in the sleeves.

All installed rolled plugs are made from Alloy 690.

In the table titled "Davis-Besse 16 RFO March 2010: Axial Indications" (Enclosure 2, page 2):

The first four entries should state "Reroll Transition PWSCC" instead of "Roll Transition PWSCC" (Primary Water Stress-Corrosion Cracking), and these indications were found in the heel of the roll transition.

The repair rolls installed at Davis-Besse are 1 5/8 inches long, which is longer than the 1 inch required by the topical report that was used for obtaining approval of the repair rolls.

At the time of the call, the licensee had completed more than 95 percent of the tubesheet exams.

Groove intergranular attack (IGA) was found in the free span of 1-B SG. The Groove IGA was a form of outside diameter stress-corrosion cracking and there was sufficient margin on the tubes (R73C60 and R73C64) that structural integrity was maintained, despite the long length of the groove IGA. All Groove IGA detected during the refueling outage was found with the bobbin coil. None of these indications were scheduled to be in-situ pressure tested since they did not pass the screening criteria based on +Point™ voltage or depth. A tertiary review of the bobbin data was performed to increase the probability of detecting Groove IGA.

In the table titled "Davis-Besse 16 RFO March 2010: 2.C (7) Steam Generator Tube Circumferential Crack Report" (Enclosure 2, page 3):

The indications listed as "Roll Trans[ition] PWSCC [primary water stress-corrosion cracking]" are in the heel transition of the repair roll (i.e., reroll transition PWSCC).

32 Roll Trans PWSCC indications were detected in the lower tube end in SG 1-B. These indications are located in the heel transition of the second (upper) roll.

The 0.105 gallon per minute leak rate indicated in row 136, tube 1 is a 50/50 estimate.
The volumetric (VOL) IGA indications are in repair rolls.

The tube end PWSCC indication is in the weld's heat affected zone.

In the table titled "Davis-Besse 16 RFO March 2010: Volumetric Indications (Not in Previously Rerolled Tubes)"
(Enclosure 2, page 4), the portion in parentheses "(Not in Previously Rerolled Tubes)" should be deleted.

The indications in this table are also in the previous table titled, "2.C(7) Steam Generator Tube Circumferential Crack Report."

Both indications shown in the table are located in a repair roll.

In the table titled "Davis-Besse 16 RFO March 2010: New Tube End Indications (Not in Previously Rerolled Tubes)" (Enclosure 2, pages 5 through 7):

There are 92 indications in SG 2-A and 43 indications in SG 1-B. Many of these tubes will be repaired by re-rolling. The potential for these indications to leak will be addressed in the condition monitoring and operational assessment.

In the table titled "Davis-Besse 16 RFO March 2010: Top 10 Wear Calls by Bobbin Depth" (Enclosure 2, page 8):

The licensee has never had to plug any tubes as a result of a wear indication. The upper 95th percentile growth rate was 1.84 percent per effective full power year. There is a slight increase in the number of wear scars, which the licensee attributes to the power uprate that was implemented during the last operating cycle. The increase in wear scars falls within the bounds that were predicted prior to implementation of the power uprate. All the new indications are within 4 to 6 percent through-wall.

At the time of the call, the licensee was projecting that they would plug approximately 180 tubes and repair approximately 120 tubes using the rolling process. The licensee was still performing special interest examinations at the time of the call.

No in-situ pressure testing was scheduled, but the licensee stated that they would notify the staff if their plans changed. If any in-situ pressure testing would be performed, the licensee was planning on performing it on Sunday, March 21, 2010.

Manual and automatic analysis for loose parts had not detected any loose parts. Inspections with the +Point™ coil at the lower tube sheet (LTS) had not revealed any loose parts. No degradation due to loose parts had been found. To date, no potential loose part indications had ever been found at Davis-Besse with eddy current testing. The licensee attributes this condition to the spray plates through which the incoming feedwater must pass that have very small holes and act to keep out debris.

SG secondary side inspections were performed on the auxiliary feedwater header in SG 1-B during this outage as part of the 10-year inspection program. The inspections were performed through the upper secondary manway and some auxiliary feedwater spray nozzles. These inspections had just started, but the licensee did not expect to find anything based on eddy current examination. The licensee stated they would inform the staff if anything was found.

The licensee stated that when compared to the last outage, there was an increase in wear that they attributed to the power uprate. There was also an increase in the occurrence of LTS heel transition cracking in SG 1-B.

A VT-1 inspection of installed plugs revealed a cracked welded plug in SG 1-B. The plug was scheduled to be replaced with a rolled plug, but that would be the last procedure performed in the SG since removal of the old plug generates debris.

The licensee predicts closeout of eddy current testing in the SGs by Sunday, March 21, 2010, and repairs will be made on Monday and Tuesday.

Per license condition 2.C.7 – the licensee notified the staff of the results of their assessment. They found no circumferential cracking inboard of the repair rolls. Circumferential cracking in an original roll was found (as shown on page 3 of 8 in Enclosure 2) with an estimate leakage of 0.105 gallons per day.

Some of the installed plugs have a thermal cycle limit of 170 cycles. The plant has currently undergone 110 actual thermal cycles.

The welded plug that cracked had signs of poor fusion in the weld. The cracked plug was compared to the other 17 manufacturer-installed plugs and the licensee noted that all the other plugs had better weld quality than the plug that cracked. The cracks in the plug were very small and there was no concern for plug ejection.

The staff did not identify any issues that required follow-up action at this time; however, the staff asked to be notified in the event that any unusual conditions were detected during the remainder of the outage.

Davis-Besse Steam Generator Inspection Data – March 18, 2010

Davis Besse 16RFO Eddy Current Exam Scope	SG 2-A	SG 1-B
Inspection of all newly installed repair rolls.	100 estimate	100 estimate
Periphery AFW Header to tube gap analysis to determine if the header is moving.	366	396
Full length bobbin examination of all in-service non-sleeved tubing.	14832	15178
Full length bobbin examination of 100% sleeves.	199	212
+Point™ exam of the sleeve at the point of entry (USE) and parent tube pressure boundary portion extending approximately 6 inches past the sleeve end (LSE) of 100% of the sleeves (the parent tube between the bottom of the upper most sleeve roll and the top of the middle sleeve roll may be excluded from inspection since it is not a pressure boundary).	199	212
+Point™ inspection of non-sleeved in-service upper tube roll expansions (100%) including non stress relieved upper repair roll expansions and factory re-rolls.	14633	14966
+Point™ coil examination of 50% of the non-sleeved in-service tubes in the upper tube sheet region from tube end including tube end, upper roll expansion and crevice to upper tube sheet exit.	7317	7483
+Point™ inspection of 20% of the in-service stress relieved lower tube roll expansions and tube ends in OTSG 2-A. (including tube 127-67 with NSRT)	3126	0
+Point™ inspection of in-service stress relieved lower tube roll expansions and tube ends in S/G 1-B 100%.	0	15178
+Point™ coil examination of the tubes bordering the sleeve region.	89	80
+Point™ coil examination of all of the flaw-like indications (I codes, TWD per the DA, and new dents) reported from bobbin.	550 estimate	530 estimate
+Point™ coil examination of all Non Quantifiable Signal (NQS) and Manufacturing Burnish Mark (MBM) indications above 10S-2".	220 estimate	240 estimate
+Point™ coil examination of all dent indications below 14S (100% sample of all previously reported and new dents using a ≥2.5 volt bobbin threshold).	350 estimate	300 estimate
+Point™ coil examination of all dent indications greater than or equal to 1 volt above 14S in the non-periphery region.	330 estimate	430 estimate
+Point™ coil examination of all dent indications greater than or equal to 0.5 volts above 14S in the periphery region.	29 estimate	19 estimate
+Point™ coil sample inspection of 50% of the defined lower tubesheet sludge pile region tubes.	1447	1709
Sleeve Bobbin and +Point™ coil inspection of all previously identified geometric distortions (40 tubes SG 1-B).	0	40
+Point™ coil inspection of all previously identified and new magnetic stain (MAG) indications (23 tubes SG 1-B)	0	23
+Point™ inspection of 20% of the Hot Leg rolled Plugs.	121	54
Visual Welded Plug Exam (VT-1) (100%)	33	19
Visual Plug exams of all Plugs in Upper and Lower (100%)	1250	558
Total Exams	45191	57727

ENCLOSURE 2

Results as of : 11:23 AM,3/18/2010

Davis-Besse 16 RFO March 2010
Axial Indications

SG	Count	Row	Tube	Ind	Volts	TSP	Inch1	Probe	Depth	Ax Len	Deg Mode
2-A	1	117	103	SAI	2.14	UTE	-2.55	520PP	86	0.61	Roll Transition PWSCC
2-A	2	114	112	SAI	0.68	UTE	-1.36	520PP	52	0.17	Roll Transition PWSCC
2-A	3	63	12	SAI	0.57	UTE	-1.48	520PP	80	0.19	Roll Transition PWSCC
2-A	4	25	47	SAI	0.80	UTE	-1.54	520PP	46	0.20	Roll Transition PWSCC
2-A	5	132	2	MAI	0.55	UTE	-3.20	520PP	65	0.19	ReRoll Transition PWSCC
2-A	6	125	14	MAI	1.26	UTE	-2.92	520PP	95	0.26	ReRoll Transition PWSCC
2-A	7	124	101	MAI	0.78	UTE	-2.82	520PP	69	0.18	ReRoll Transition PWSCC
2-A	8	118	105	SAI	2.42	UTE	-2.77	520PP	68	0.17	ReRoll Transition PWSCC
2-A	9	116	111	MAI	2.13	UTE	-3.16	520PP	96	0.34	ReRoll Transition PWSCC
2-A	10	94	3	MAI	2.09	UTE	-3.02	520PP	97	0.31	ReRoll Transition PWSCC
2-A	11	92	3	SAI	2.76	UTE	-3.14	520PP	98	0.27	ReRoll Transition PWSCC
2-A	12	92	9	SAI	1.44	UTE	-3.04	520PP	53	0.34	ReRoll Transition PWSCC
2-A	13	91	10	SAI	1.87	UTE	-3.03	520PP	86	0.22	ReRoll Transition PWSCC
2-A	14	87	122	MAI	1.02	UTE	-3.26	520PP	73	0.27	ReRoll Transition PWSCC
2-A	15	85	31	MAI	1.23	UTE	-3.21	520PP	78	0.25	ReRoll Transition PWSCC
2-A	16	80	12	MAI	1.26	UTE	-3.05	520PP	97	0.49	ReRoll Transition PWSCC
2-A	17	68	4	MAI	0.71	UTE	-3.13	520PP	48	0.26	ReRoll Transition PWSCC
2-A	18	65	1	SAI	1.52	UTE	-3.13	520PP	36	0.17	ReRoll Transition PWSCC
2-A	19	32	83	MAI	0.43	UTE	-3.56	520PP	83	0.14	ReRoll Transition PWSCC
2-A	20	24	18	SAI	1.20	UTE	-3.18	520PP	72	0.22	ReRoll Transition PWSCC
2-A	21	19	75	MAI	0.63	UTE	-3.58	520PP	53	0.27	ReRoll Transition PWSCC
2-A	22	83	74	SAI	0.15	UTS	-17.79	520PP	1	0.15	Groove IGA
2-A	23	65	1	SAI	0.14	15S	-1.10	520PP	1	0.15	Groove IGA
1-B	24	111	48	MAI	0.83	LTE	1.54	520PP	57	0.20	Roll Transition PWSCC
1-B	25	52	93	SAI	0.58	UTE	-1.10	520PP	48	0.21	Roll Transition PWSCC
1-B	26	52	95	SAI	0.63	UTE	-1.17	520PP	62	0.17	Roll Transition PWSCC
1-B	27	48	93	SAI	0.75	UTE	-1.32	520PP	62	0.12	Roll Transition PWSCC
1-B	28	46	33	SAI	0.89	LTE	1.41	520PP	68	0.21	Roll Transition PWSCC
1-B	29	41	103	SAI	0.55	LTE	1.31	520PP	91	0.35	Roll Transition PWSCC
1-B	30	31	31	SAI	0.80	LTE	1.81	520PP	99	0.21	Roll Transition PWSCC
1-B	31	56	104	MAI	0.64	UTE	-3.75	520PP	98	0.14	ReRoll Transition PWSCC
1-B	32	43	92	MAI	3.05	UTE	-2.95	520PP	81	0.27	ReRoll Transition PWSCC
1-B	33	36	99	SAI	0.93	UTE	-4.89	520PP	67	0.15	ReRoll Transition PWSCC
1-B	34	35	88	MAI	0.98	UTE	-2.80	520PP	76	0.15	ReRoll Transition PWSCC
1-B	35	30	14	MAI	0.67	UTE	-2.94	520PP	66	0.37	ReRoll Transition PWSCC
1-B	36	73	60	SAI	0.32	15S	39.78	520PP	34	2.91	Groove IGA
1-B	37	73	64	SAI	0.23	15S	28.03	520PP	61	2.54	Groove IGA

Davis-Besse 16RFO March 2010

2.C(7) Steam Generator Tube Circumferential Crack Report

S/G	Count	Row	Tube	Ind	Volts	TSP	Inch	Probe	%TW	Ci Ext	Degradation Mechanism	Section a	Section b	Section c
2-A	1	15	10	SCI	0.54	UTE	-3.78	520PP	43	0.23	Roll Trans PWSCC		x	
2-A	2	16	27	SCI	1.18	UTE	-3.61	520PP	75	0.53	Roll Trans PWSCC		x	
2-A	3	19	15	MCI	0.56	UTE	-3.64	520PP	62	0.42	Roll Trans PWSCC		x	
2-A	4	26	22	SCI	0.71	UTE	-3.64	520PP	50	0.25	Roll Trans PWSCC		x	
2-A	5	93	7	SVI	0.16	UTE	-4.07	520PP	2	0.28	VOL IGA in Roll		x	
2-A	6	93	7	SVI	0.19	UTE	-4.1	520PP	1	0.16	VOL IGA in Roll		x	
2-A	7	136	1	SCI	1.71	UTE	-0.38	520PP	96	0.28	Tube End PWSCC		x	0.105gpm
1-B	8	44	72	SCI	0.2	LTE	1.59	520PP	76	0.12	Roll Trans PWSCC		x	
1-B	9	44	73	SCI	0.57	LTE	1.88	520PP	49	0.16	Roll Trans PWSCC		x	
1-B	10	44	75	SCI	0.44	LTE	1.77	520PP	68	0.18	Roll Trans PWSCC		x	
1-B	11	45	74	SCI	0.34	LTE	1.62	520PP	46	0.16	Roll Trans PWSCC		x	
1-B	12	45	74	SCI	0.43	LTE	1.63	520PP	46	0.18	Roll Trans PWSCC		x	
1-B	13	46	74	SCI	0.23	LTE	1.55	520PP	34	0.16	Roll Trans PWSCC		x	
1-B	14	46	74	SCI	0.43	LTE	1.59	520PP	99	0.27	Roll Trans PWSCC		x	
1-B	15	46	74	SCI	0.56	LTE	1.63	520PP	53	0.37	Roll Trans PWSCC		x	
1-B	16	47	77	SCI	0.52	LTE	1.73	520PP	50	0.21	Roll Trans PWSCC		x	
1-B	17	47	77	SCI	0.85	LTE	1.72	520PP	96	0.25	Roll Trans PWSCC		x	
1-B	18	48	77	SCI	0.46	LTE	1.65	520PP	95	0.23	Roll Trans PWSCC		x	
1-B	19	49	25	MCI	0.48	LTE	1.62	520PP	76	0.25	Roll Trans PWSCC		x	
1-B	20	49	78	SCI	0.42	LTE	1.64	520PP	67	0.18	Roll Trans PWSCC		x	
1-B	21	50	74	SCI	0.3	LTE	1.59	520PP	85	0.18	Roll Trans PWSCC		x	
1-B	22	50	74	SCI	0.66	LTE	1.6	520PP	99	0.96	Roll Trans PWSCC		x	
1-B	23	50	77	SCI	0.71	LTE	1.63	520PP	76	0.53	Roll Trans PWSCC		x	
1-B	24	51	76	SCI	0.57	LTE	1.44	520PP	89	0.27	Roll Trans PWSCC		x	
1-B	25	51	78	SCI	0.62	LTE	1.34	520PP	98	0.3	Roll Trans PWSCC		x	
1-B	26	53	77	SCI	0.55	LTE	1.47	520PP	98	0.25	Roll Trans PWSCC		x	
1-B	27	58	98	SCI	0.44	LTE	1.31	520PP	50	0.18	Roll Trans PWSCC		x	
1-B	28	59	76	SCI	0.47	LTE	1.24	520PP	66	0.3	Roll Trans PWSCC		x	
1-B	29	60	80	SCI	0.58	LTE	1.38	520PP	97	0.23	Roll Trans PWSCC		x	
1-B	30	62	30	SCI	0.33	LTE	1.59	520PP	99	0.19	Roll Trans PWSCC		x	
1-B	31	91	72	SCI	0.34	LTE	1.6	520PP	88	0.18	Roll Trans PWSCC		x	
1-B	32	91	72	SCI	0.42	LTE	1.47	520PP	83	0.18	Roll Trans PWSCC		x	
1-B	33	92	74	SCI	0.46	LTE	1.66	520PP	55	0.18	Roll Trans PWSCC		x	
1-B	34	92	74	SCI	0.57	LTE	1.57	520PP	81	0.18	Roll Trans PWSCC		x	
1-B	35	94	72	SCI	0.33	LTE	1.5	520PP	60	0.18	Roll Trans PWSCC		x	
1-B	36	103	33	SCI	0.51	LTE	1.6	520PP	88	0.28	Roll Trans PWSCC		x	
1-B	37	106	31	SCI	0.47	LTE	1.57	520PP	99	0.19	Roll Trans PWSCC		x	
1-B	38	110	61	SCI	0.28	LTE	0.45	520PP	100	0.18	Tube End PWSCC		x	
1-B	39	111	29	SCI	0.27	LTE	1.64	520PP	69	0.18	Roll Trans PWSCC		x	
1-B	40	111	29	SCI	0.53	LTE	1.66	520PP	89	0.62	Roll Trans PWSCC		x	

Results as of : 11:23 AM,3/18/2010

Davis-Besse 16 RFO March 2010

Volumetric Indications (Not in Previously Rerolled Tubes)

SG	Row	Tube	Ind	Volts	TSP	Inch1	Probe	Depth	Ax Len	Circ Len	Deg Mode
2-A	93	7	SVI	0.16	UTE	-4.07	520PP	2	0.20	0.28	VOL IGA in Roll
2-A	93	7	SVI	0.19	UTE	-4.10	520PP	1	0.14	0.16	VOL IGA in Roll

Results as of : 11:23 AM,3/18/2010

Davis-Besse 16 RFO March 2010
New Tube End Indications (Not in Previously Rerolled Tubes)

SG	Count	Row	Tube	Ind	Volts	TSP	Inch1	Probe
2-A	1	55	1	SAA	0.83	UTE	-0.25	520PP
2-A	2	115	112	SAA	1.09	UTE	-0.31	520PP
2-A	3	115	113	MAA	0.79	UTE	-0.30	520PP
2-A	4	114	112	SAA	1.46	UTE	-0.27	520PP
2-A	5	114	111	SAA	1.10	UTE	-0.31	520PP
2-A	6	2	20	SAA	2.10	UTE	-0.27	520PP
2-A	7	11	37	SAA	1.15	UTE	-0.32	520PP
2-A	8	147	44	SAA	1.55	UTE	-0.22	520PP
2-A	9	20	72	MAA	2.25	UTE	-0.29	520PP
2-A	10	4	27	SAA	1.77	UTE	-0.22	520PP
2-A	11	27	81	SAA	1.20	UTE	-0.25	520PP
2-A	12	28	81	SAA	1.24	UTE	-0.27	520PP
2-A	13	94	6	SAA	1.21	UTE	-0.23	520PP
2-A	14	93	8	MAA	2.23	UTE	-0.24	520PP
2-A	15	92	7	SAA	1.94	UTE	-0.28	520PP
2-A	16	66	3	SAA	1.31	UTE	-0.25	520PP
2-A	17	65	2	SAA	2.73	UTE	-0.26	520PP
2-A	18	129	7	MAA	1.63	UTE	-0.27	520PP
2-A	19	11	4	SAA	1.20	UTE	-0.25	520PP
2-A	20	106	105	SAA	1.55	UTE	-0.29	520PP
2-A	21	108	112	SAA	1.08	UTE	-0.24	520PP
2-A	22	135	70	MAA	1.99	UTE	-0.31	520PP
2-A	23	137	69	SAA	1.30	UTE	-0.31	520PP
2-A	24	96	6	SAA	1.55	UTE	-0.38	520PP
2-A	25	27	94	SAA	1.27	UTE	-0.23	520PP
2-A	26	28	82	SAA	1.43	UTE	-0.27	520PP
2-A	27	149	17	SAA	1.59	UTE	-0.20	520PP
2-A	28	23	19	MAA	1.82	UTE	-0.27	520PP
2-A	29	14	8	SAA	1.79	UTE	-0.27	520PP
2-A	30	21	31	SAA	1.14	UTE	-0.20	520PP
2-A	31	133	4	SAA	2.33	UTE	-0.26	520PP
2-A	32	134	4	SAA	0.90	UTE	-0.28	520PP
2-A	33	84	8	MAA	2.12	UTE	-0.24	520PP
2-A	34	81	11	SAA	1.50	UTE	-0.28	520PP
2-A	35	72	115	SAA	0.91	UTE	-0.21	520PP
2-A	36	81	32	SAA	0.86	UTE	-0.25	520PP
2-A	37	66	113	SAA	1.61	UTE	-0.32	520PP
2-A	38	126	44	SAA	1.17	UTE	-0.21	520PP
2-A	39	126	10	MAA	2.17	UTE	-0.23	520PP
2-A	40	132	6	SAA	1.52	UTE	-0.26	520PP
2-A	41	96	2	MAA	1.64	UTE	-0.29	520PP
2-A	42	25	47	MAA	1.11	UTE	-0.29	520PP
2-A	43	150	1	SAA	2.86	UTE	-0.28	520PP
2-A	44	90	7	SAA	1.80	UTE	-0.27	520PP
2-A	45	90	3	SAA	1.49	UTE	-0.26	520PP
2-A	46	95	9	MAA	1.05	UTE	-0.27	520PP
2-A	47	96	8	MAA	2.83	UTE	-0.26	520PP
2-A	48	94	26	SAA	1.08	UTE	-0.21	520PP
2-A	49	110	3	SAA	1.95	UTE	-0.18	520PP
2-A	50	100	7	SAA	1.09	UTE	-0.25	520PP

Davis-Besse 16 RFO March 2010
New Tube End Indications (Not in Previously Rerolled Tubes)

SG	Count	Row	Tube	Ind	Volts	TSP	Inch1	Probe
2-A	51	28	19	SAA	1.40	UTE	-0.26	520PP
2-A	52	7	13	MAA	1.72	UTE	-0.22	520PP
2-A	53	122	13	SAA	0.89	UTE	-0.22	520PP
2-A	54	87	10	SAA	0.99	UTE	-0.26	520PP
2-A	55	87	8	SAA	1.74	UTE	-0.27	520PP
2-A	56	86	11	SAA	1.61	UTE	-0.29	520PP
2-A	57	67	2	SAA	2.31	UTE	-0.27	520PP
2-A	58	24	33	SAA	1.90	UTE	-0.28	520PP
2-A	59	24	19	MAA	2.01	UTE	-0.22	520PP
2-A	60	19	35	SAA	0.86	UTE	-0.23	520PP
2-A	61	92	8	SAA	2.43	UTE	-0.25	520PP
2-A	62	92	6	MAA	2.08	UTE	-0.26	520PP
2-A	63	99	3	SAA	1.75	UTE	-0.28	520PP
2-A	64	91	9	MAA	1.58	UTE	-0.25	520PP
2-A	65	91	121	SAA	1.81	UTE	-0.19	520PP
2-A	66	21	48	SAA	1.77	UTE	-0.24	520PP
2-A	67	19	71	MAA	1.65	UTE	-0.20	520PP
2-A	68	10	61	SAA	1.50	UTE	-0.28	520PP
2-A	69	17	70	SAA	1.63	UTE	-0.24	520PP
2-A	70	10	36	MAA	1.51	UTE	-0.27	520PP
2-A	71	26	95	SAA	1.84	UTE	-0.27	520PP
2-A	72	127	76	MAA	1.62	UTE	-0.21	520PP
2-A	73	36	42	SAA	0.86	UTE	-0.16	520PP
2-A	74	36	26	SAA	1.51	UTE	-0.07	520PP
2-A	75	79	28	SAA	0.79	UTE	-0.28	520PP
2-A	76	85	10	SAA	1.69	UTE	-0.28	520PP
2-A	77	83	6	SAA	1.26	UTE	-0.31	520PP
2-A	78	68	9	SAA	1.46	UTE	-0.28	520PP
2-A	79	130	93	SAA	0.43	UTE	-0.16	520PP
2-A	80	137	74	SAA	0.89	UTE	-0.18	520PP
2-A	81	105	6	MAA	1.73	UTE	-0.26	520PP
2-A	82	89	7	MAA	1.69	UTE	-0.26	520PP
2-A	83	88	7	SAA	1.34	UTE	-0.26	520PP
2-A	84	13	41	SAA	2.25	UTE	-0.21	520PP
2-A	85	13	67	SAA	1.73	UTE	-0.20	520PP
2-A	86	14	41	SAA	1.00	UTE	-0.21	520PP
2-A	87	114	109	SAA	0.91	UTE	-0.27	520PP
2-A	88	81	10	SAA	1.67	UTE	-0.26	520PP
2-A	89	58	9	SAA	1.70	UTE	-0.26	520PP
2-A	90	103	18	MAA	1.92	UTE	-0.13	520PP
2-A	91	146	49	MAA	2.22	UTE	-0.22	520PP
2-A	92	147	46	SAA	2.18	UTE	-0.30	520PP
1-B	93	102	10	SAA	1.25	UTE	-0.32	520PP
1-B	94	28	12	SAA	1.07	UTE	-0.30	520PP
1-B	95	31	14	MAA	1.77	UTE	-0.27	520PP
1-B	96	20	54	MAA	2.78	UTE	-0.17	520PP
1-B	97	84	116	SAA	2.13	UTE	-0.26	520PP
1-B	98	104	114	SAA	0.97	UTE	-0.25	520PP
1-B	99	61	29	SAA	1.16	UTE	-0.29	520PP
1-B	100	110	45	SAA	1.04	UTE	-0.20	520PP
1-B	101	18	57	SAA	0.94	UTE	-0.27	520PP

Davis-Besse 16 RFO March 2010

New Tube End Indications (Not in Previously Rerolled Tubes)

SG	Count	Row	Tube	Ind	Volts	TSP	Inch1	Probe
1-B	102	18	55	SAA	1.68	UTE	-0.25	520PP
1-B	103	20	83	SAA	1.19	UTE	-0.21	520PP
1-B	104	45	90	SAA	1.58	UTE	-0.29	520PP
1-B	105	53	94	MAA	1.83	UTE	-0.18	520PP
1-B	106	53	96	SAA	1.25	UTE	-0.18	520PP
1-B	107	29	65	SAA	2.46	UTE	-0.16	520PP
1-B	108	40	89	MAA	1.24	UTE	-0.11	520PP
1-B	109	48	96	SAA	1.06	UTE	-0.27	520PP
1-B	110	50	92	SAA	1.23	UTE	-0.11	520PP
1-B	111	53	97	SAA	0.86	UTE	-0.19	520PP
1-B	112	27	12	MAA	1.61	UTE	-0.21	520PP
1-B	113	33	68	SAA	1.86	UTE	-0.33	520PP
1-B	114	117	40	SAA	1.08	UTE	-0.23	520PP
1-B	115	43	105	MAA	2.56	UTE	-0.28	520PP
1-B	116	132	76	SAA	1.27	UTE	-0.22	520PP
1-B	117	30	66	MAA	1.18	UTE	-0.36	520PP
1-B	118	8	42	SAA	3.18	UTE	-0.14	520PP
1-B	119	29	83	SAA	2.65	UTE	-0.35	520PP
1-B	120	121	5	SAA	1.18	UTE	-0.33	520PP
1-B	121	121	4	SAA	2.08	UTE	-0.30	520PP
1-B	122	19	56	SAA	2.15	UTE	-0.18	520PP
1-B	123	19	75	SAA	2.23	UTE	-0.16	520PP
1-B	124	47	74	SAA	1.00	UTE	-0.43	520PP
1-B	125	14	51	SAA	1.27	UTE	-0.24	520PP
1-B	126	100	78	SAA	1.30	UTE	-0.42	520PP
1-B	127	61	80	SAA	3.18	UTE	-0.20	520PP
1-B	128	113	110	SAA	2.28	UTE	-0.28	520PP
1-B	129	108	106	SAA	1.08	UTE	-0.21	520PP
1-B	130	36	102	SAA	0.81	UTE	-0.33	520PP
1-B	131	43	93	SAA	1.74	UTE	-0.23	520PP
1-B	132	43	106	SAA	0.57	UTE	-0.22	520PP
1-B	133	59	94	SAA	2.33	UTE	-0.32	520PP
1-B	134	56	77	SAA	1.80	UTE	-0.15	520PP
1-B	135	60	99	SAA	1.38	UTE	-0.19	520PP

Results as of : 11:23 AM,3/18/2010

Davis-Besse 16 RFO March 2010

Top 10 Wear Calls By Bobbin Depth

SG	Row	Tube	Depth	Volts	TSP	Inch1	Prev Depth
2-A	147	36	23	0.98	10S	0.61	22
2-A	16	2	21	1.34	13S	-0.68	28
2-A	84	32	20	0.80	09S	0.63	14
2-A	52	1	20	0.95	13S	-0.70	12
2-A	146	34	19	0.75	10S	0.59	14
2-A	43	1	18	0.93	13S	-0.66	14
2-A	12	1	17	0.91	13S	-0.68	17
2-A	150	27	17	0.97	10S	-0.78	16
2-A	146	33	17	0.99	10S	0.60	20
1-B	2	27	17	0.66	12S	0.66	14

Results as of : 11:23 AM,3/18/2010

Mr. Barry S. Allen
Site Vice President
FirstEnergy Nuclear Operating Company
Davis-Besse Nuclear Power Station
Mail Stop A-DB-3080
5501 North State Route 2
Oak Harbor, OH 43449-9760

SUBJECT: DAVIS-BESSE NUCLEAR POWER STATION UNIT 1 – SUMMARY OF MARCH 18, 2010, CONFERENCE CALL REGARDING THE SPRING 2010 REFUELING OUTAGE STEAM GENERATOR INSERVICE INSPECTIONS (TAC NO. ME3427)

Dear Mr. Allen:

On March 18, 2010, the U.S. Nuclear Regulatory Commission (NRC) staff participated in a conference call with FirstEnergy Nuclear Operating Company (FENOC) staff, regarding the spring 2010, refueling outage, steam generator inspections at the Davis-Besse Nuclear Power Station, Unit 1. A summary of the notes by the NRC staff of the March 18, 2010, conference call is enclosed. In addition, a handout provided by FENOC to support the conference call is also enclosed. The NRC staff did not identify any issues that would require follow-up action at this time; however, the staff asked to be notified in the event any unusual conditions were detected during the remainder of the outage.

If you have any questions, please call me at (301) 415--3867.

Sincerely,
/RA/
Michael Mahoney, Project Manager
Plant Licensing Branch III-2
Division of Operating Reactor Licensing
Office of Nuclear Reactor Regulation

Docket No. 50-346

Enclosures:
1. Summary of Conference Call
2. DBNPS Steam Generator Inspections data March 18, 2010
cc w/encl: Distribution via Listserv

DISTRIBUTION:
PUBLIC
LPL3-2 R/F
RidsNrrDorlLpl3-2 Resource
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ADAMS Accession No. ML100970031 NRR-106 *By Memo Dated

OFFICE	NRR/LPL3-2/PM	NRR/LPL3-2/LA	NRR/DCI/CSGB/BC	NRR/LPL3-2/BC
NAME	MMahoney	THarris	RTaylor	SCampbell
DATE	04/08/10	04/08/10	03/23/10*	04/12/10

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