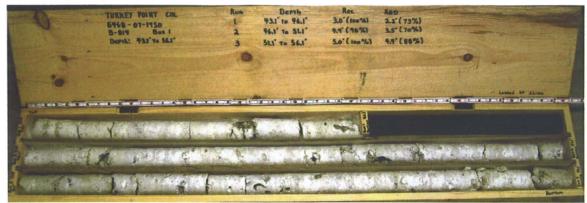


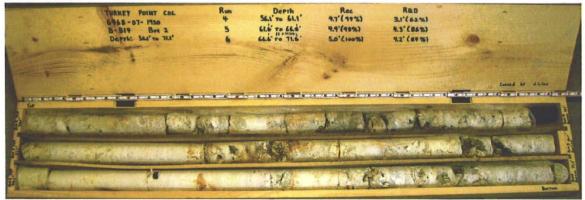
BECHT	ELFRO	JECT I				+				3-07-195				Miami-Da		OLOGIST: .		
SITE DESCRIPTION: Turkey Point COL						DRILL !	MACHIN	E: CM	E-550 (N	/liller)		DRILLI	ER: R. White/ J. Dugger/ C. White GROUND V					WATER (ft
BORING	G NO.:	B-814				DRILL I	NETHOE	: Mud	Rotary	Core		SAMPI	E M	ETHODS:	SPT/Core		0 HR.	NA
GROUN	ND ELEV	/.: 9.0	ft	(NAV	D88)	NORTH	ING: 3	99,139	US ft	(NAD83	3/90)	EASTI	NG:	877,405	US ft	(NAD83/90)	24 HR.	NA
	DEPTH			BORII	NG D	IAMETER	R: 4" to !	98.0', 3	" to 153	3.2' CA	SING	DEPTH	1: 4" 1	to 98.0'		HAMMER (	ID):140 lb. A	Auto (M06)
	STARTE		5/08	4		ETED: 5		<u> </u>		SIZE:					SED: 2 7/8	" Roller Con		
	DEPTH		ow cor		_		BLOWS F	PER FO				IP. <b>V</b>	1	<del>                                     </del>				
(ft)	(ft)	0.5ft	0.5ft	0.5ft	o o	20	40	60	80	100	1		O OI G		SOIL	AND ROCK D	ESCRIPTION	1
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140.6	_				- ,	Contin	ued from	previ	ous pag	e	+-		ļ.,					
142.7	151.7					1:::								i <u>l</u>	454 70 4			
}		4	4	5	<u> </u>	<b>4</b> 9	11	·			814-	20	_	-144.2	151.7ft: loc	minated at Ele	vation -144.2	1
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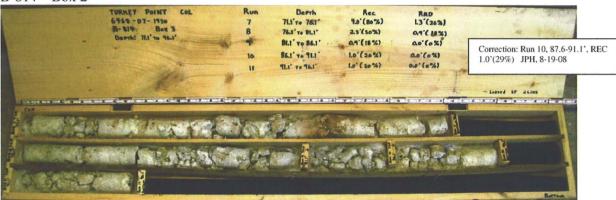
3-814 : 9.0 153.2 : 5/1!		(NAVE	DD88) N C C PLETE  JN RQD (#) (2.2) 73% (3.5) 70% (4.4) 88% (3.1)	PRILL ME NORTHIN LASING [ D: 5/18 SAMP. NO. RUN-1 RUN-2	STR REC. (ft)	: Mud 99,139 : 4" to	98.0 RE SI	O (Miller)  DRILLER: R. White/ J. Dugger/ C. White  GROUND WATER (  O HR. NA  S ft (NAD83/90)  EASTING: 877,405 US ft (NAD83/90)  HAMMER (ID): 140 Ib. Auto (M06)  SIZE: HQ3  CORE BARREL TYPE: Triple Tube Wireline (Split inner liners)  DESCRIPTION AND REMARKS  Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace vugs
: 9.0 153.2 : 5/1! RUN (ft) 3.0 5.0	1.53 1.05 0.48 1.07 1.07 1.07 1.07 1.07 1.18 1.24 1.24 1.24 1.24 1.21 1.24 1.21 1.24 1.21 1.24 1.21 1.23	(3.0) 100% (4.9) 98% (5.0) 100%	D88) N C PLETE RQD (ff) % (2.2) 73% (3.5) 70% (4.4) 88%	SAMP. NO.	OEPTH: /08 STR REC. (ft) %	99,139 : 4" to COF	98.0 RE SI	Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCI (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
153.2 : 5/1! RUN (ft) 3.0 5.0	1.53 1.05 0.48 1.07 1.07 1.07 1.07 1.07 1.18 1.24 1.24 1.24 1.24 1.21 1.24 1.21 1.24 1.21 1.24 1.21 1.23	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	SAMP. NO. RUN-2	08 STR REC. (ft) %	COF RATA RQD (ff)	98.0 RE SI	DESCRIPTION AND REMARKS  Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCI (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
RUN (ft)  3.0  5.0	5/08  DRILL RATE (Min/ft)  1:53 1:05 0:48 1:07 1:07 1:09 1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47 1:32	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	SAMP. NO. RUN-1	STR   REC.   (ft)   %	COF	L O G	DESCRIPTION AND REMARKS  Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
3.0 5.0 5.0	DRILL RATE (Min/ft)  1.53 1.05 0:48 1:07 1:07 1:07 1:09 1:117 1:18 1:24 1:26 1:21 1:07 1:09 1:128 1:21 1:07 1:09 1:128 1:21 1:07 1:09 1:09 1:09 1:09 1:09 1:09 1:09 1:09	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	RUN-1	STR REC. (ft) %	RATA RQD (ft) %	L O G	DESCRIPTION AND REMARKS  Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
3.0 5.0 5.0	RATE (Min/ft)  1.53 1.05 0.48 1.07 1.09 1.17 1.18 1.24 1.13 1.25 1.21 1.07 1.13 1.28 1.21 1.07 1.13	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	RUN-1 RUN-2 RUN-3	REC. (ft) %	RQD (ft) %	0	Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued)  43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
3.0 5.0 5.0	RATE (Min/ft)  1.53 1.05 0.48 1.07 1.09 1.17 1.18 1.24 1.13 1.25 1.21 1.07 1.13 1.28 1.21 1.07 1.13	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	RUN-1 RUN-2 RUN-3	REC. (ft) %	RQD (ft) %	0	Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued)  43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
5.0 5.0	(Min/ft)  1:53 1:05 0:48 1:07 1:07 1:07 1:17 1:18 1:24 1:11 0:54 1:13 1:28 1:21 1:07 1:07 1:07 1:08 1:07 1:09 1:07 1:09 1:07 1:09 1:07 1:09 1:09 1:09 1:09 1:09 1:09 1:09 1:09	(3.0) 100% (4.9) 98% (5.0) 100%	(2.2) 73% (3.5) 70% (4.4) 88%	RUN-1 RUN-2 RUN-3	(17.6)	(13.2)	G	Begin Coring @ 43.1 ft  LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued)  43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
5.0	1:05 0'48 1:07 1:07 1:09 1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47	(4.9) 98% (5.0) 100%	(3.5) 70% (4.4) 88%	RUN-2		(13.2) 73%		LIMESTONE, boundstone, pale yellow (2.5Y8/2), hard, wet, some coarse grained sand, strong HCl (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
5.0	1:05 0'48 1:07 1:07 1:09 1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47	(4.9) 98% (5.0) 100%	(3.5) 70% (4.4) 88%	RUN-2		(13.2) 73%		grained sand, strong HCl (Upper Fort Thompson Formation) (continued) 43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
5.0	1:07 1:07 1:07 1:09 1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47	(5.0) 100%	(4.4) 88%	RUN-3				43.1ft: medium hard to moderately hard, friable to moderately indurated, trace
5.0	1:07 1:09 1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47 1:32	(5.0) 100%	(4.4) 88%	RUN-3			I	1
5.0	1:17 1:18 1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47 1:32	(4.7)	(3.1)		1		r	- <del>-</del>
5.0	1:24 1:26 1:11 0:54 1:13 1:28 1:21 1:07 1:47 1:32	(4.7)	(3.1)			l	$\vdash$	<del>-</del>
	1:11 0:54 1:13 1:28 1:21 1:07 1:47 1:32	(4.7)	(3.1)				工	51.5ft: moderately hard to hard, moderately indurated to indurated
	1:13 1:28 1:21 1:07 1:47 1:32				i			<del>+</del> <del>-</del>
	1:21 1:07 1:47 1:32				1			‡
5.0	1:47 1:32		62%	RUN-4				56.1ft: few vugs, recrystallized calcite
5.0	1:32	'					I	<del>_</del>
5.5		(4.9)	(4.3)	RUN-5	(19.3)	(10.7)	-	-52.1 LIMESTONE, boundstone, white (2.5Y8/1), hard, indurated, trace vugs,
	2:00 2:10	98%	86%	110110	58%	32%	H	recrystallized calcite, strong HCI reaction (Lower Fort Thompson Formation)
	2:08 1:28						$\vdash$	<del> -</del> <del>-</del>
5.0	2:24	(5.0)	(4.2)	RUN-6				<del>-</del>
	1:42 1:24	100%	84%					<del>-</del> <del></del>
	1:04							_
5.0	0:51 1:02	(4.0) 80%	(1.3) 26%	RUN-7				71.1ft: few fine grained sand, few vugs
	0:51 2:21					1		_
5.0	1:54	(2.5)	(0.9)	RIIN-8	-		$\vdash$	76.1ft: moderately hard to hard, moderately indurated to indurated, trace vugs
3.0	0:24	50%	18%					+
	0:32						尸	77.0 to 99.0ft: interbedded sand layers
5.0	0:53	(0.9)	(0.0)	RUN-9	†		口	81.0ft: hard, indurated, some sand
	0:23	18%	0%				口	<del>-</del> -
	0:05						口	<del>1</del> -
25	N=0	(1.0)	(0.0)	814-13	-			86.1ft: Switch sampling method to SPT 86.1ft: interbedded sand, very loose, fine grained sand, wet, strong HCl reaction
3.3	0:11	29%	0%	1.014-10			口	87.6ft: Switch sampling method to coring 87.6 to 88.1ft: rod drop
5.0	1:02	(1.0)	(0.0)	RUN-11	-		口	88.1ft: moderately hard, moderately indurated
	0:09 0:06	20%	0%			-		1
	0:00	1	1	ł .	1			
	1:25							-T 
	5.0	1:12 1:04 5.0 0:51 1:02 0:51 2:21 1:54 5.0 0:24 0:06 0:32 1:37 5.0 0:53 0:50 0:23 0:22 0:05 N=0 3.5 WOR/0.5 0:11 0:27 1:02 0:09 0:06	1:12 1:04 5.0 0.51 1:02 0.51 2:21 1:54 5.0 1:50 0:24 0:06 0:32 1:37 5.0 0.53 0:53 0:50 0:23 0:22 0:05 N=0 3.5 WOR/0.5 0:11 0:27 1:02 0:06 0:11 0:27 1:02 0:06 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:23 0:22 0:05 0:40 0:50 0:40 0:50 0:23 0:22 0:05 0:50 0:40 0:50	1:12	1:12	1:12 1:04 5.0 0:51 1:02 80% 26% 1:54 5.0 1:50 1:54 5.0 1:50 0:24 0:06 0:32 1:37 5.0 0:53 0:50 0:50 0:22 0:05 N=0 N=0 N=0 N=0 1.02 0.05 0.02 0.05 N=0 0.02 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.05 0.02 0.00 0.00	1:12 1:04 5.0 0.51 1:02 0.51 2:21 1:54 5.0 1:50 0.24 0.06 0.32 1:37 5.0 0.53 0.53 0.50 0.50 0.50 0.50 0.50	1.12 1.04 5.0



B-814 - Box 1



B-814 - Box 2



B-814 - Box 3

# Back Hoe Test Pit Logs



GEOTECHNICAL BORING LOG

Prepared By 2007 Date 5-30.08

Checked By

SHEET 1 OF **BECHTEL PROJECT NO.: 25409** MACTEC PROJECT NO.: 6468-07-1950 COUNTY: Miami-Dade GEOLOGIST: S. Woodham DRILL MACHINE: Deere 310G DRILLER: Dan Rhodes SITE DESCRIPTION: Turkey Point COL **GROUND WATER (ft)** BORING NO.: TP-601 DRILL METHOD: Backhoe SAMPLE METHODS: Bulk 0 HR. 0.5 GROUND ELEV .: -1.4 ft (NAVD88) NORTHING: 397,106 US ft (NAD83/90) EASTING: 876,036 US ft (NAD83/90) 24 HR. NA TOTAL DEPTH: 5.2 ft **BORING DIAMETER: NA** CASING DEPTH: NA HAMMER (ID):NA DATE STARTED: 5/1/08 COMPLETED: 5/1/08 CORE SIZE: BITS USED: Backhoe bucket with steel rock teeth NA DEPTH ELEV. **BLOW COUNT BLOWS PER FOOT** SAMP 0 SOIL AND ROCK DESCRIPTION 20 100 60 80 (ft) (ft) 0.5ft 0.5ft 0.5ft NO MOI G -1.4 Ground Surface MUCK, some to mostly organics, clayey, organics increase with depth Not Sampled SEE LEGEND FOR ROCK HARDNESS CRITERIA BASED ON SPT DATA -4.6 3.2 TP-601-1 LIMESTONE, boundstone, white (10YR8/1), very soft to moderately hard, friable to moderately indurated, wet, oolitic, strong HCL reaction (Miami Formation) Samples Collected: Ten (10) 5-gallon buckets (TP-601-1, Buckets 1 to 10) Boring Terminated at Elevation -6.6 ft

TURKEY POINT COL BORE TURKEY POINT GPJ TURKEY POINT COL GDT 5/30/08



GEOTECHNICAL BORING LOG
Prepared By Date 3 - 30-08

Checked By

Date 9 20 06

SHEET 1 OF 1

COUNTY: Miami-Dade GEOLOGIST: S. Woodham **BECHTEL PROJECT NO.: 25409** MACTEC PROJECT NO.: 6468-07-1950 DRILL MACHINE: Deere 310G **DRILLER: Dan Rhodes GROUND WATER (ft)** SITE DESCRIPTION: Turkey Point COL SAMPLE METHODS: Bulk 0 HR. BORING NO.: TP-701 DRILL METHOD: Backhoe 0.0 GROUND ELEV .: -1.4 ft (NAVD88) NORTHING: 396,988 US ft (NAD83/90) **EASTING: 875,509** US ft (NAD83/90) 24 HR. NA BORING DIAMETER: NA **CASING DEPTH: NA** HAMMER (ID):NA TOTAL DEPTH: 5.0 ft BITS USED: Backhoe bucket with steel rock teeth DATE STARTED: 5/1/08 COMPLETED: 5/1/08 CORE SIZE: NA ELEV. DEPTH **BLOW COUNT BLOWS PER FOOT** SAMP 0 SOIL AND ROCK DESCRIPTION 20 40 60 100 0.5ft 0.5ft 0.5ft NO. (ft) (ft) MOI G -1.4 Ground Surface 0.0 MUCK, some to mostly organics, clayey, organics increase with depth Samples Collected: Two (2) 5-gallon buckets (TP-701-2, bucket 12; TP-701-3, bucket 11) SEE LEGEND FOR ROCK HARDNESS CRITERIA BASED ON SPT DATA -2.9 1.5 TP-701-2 -4.4 3.0 TP-701-1 LIMESTONE, boundstone, white (10YR8/1), very soft to moderately hard, friable to moderately indurated, wet, oolitic, some coarse sand, strong HCl reaction (Miami Formation) Samples Collected: Ten (10) 5-gallon buckets (TP-701-1, buckets 1 to 10) Boring Terminated at Elevation -6.4 ft

TURKEY POINT COL BORE TURKEY POINT GPJ TURKEY POINT COL GDT 5/30/08

# SPT Energy Measurement Reports



### engineering and constructing a better tomorrow

August 15, 2008

Memorandum to File From: Steve Kiser QU 8-15-00

Reviewed By: Tom McDaniel 8 1904

Subject:

Report of SPT Energy - MACTEC Raleigh CME 55LC

Hammer Serial No. MEC-02 Automatic Hammer

**WORK INSTRUCTION TUR-055** 

Turkey Point COL Project Dade County, Florida

MACTEC Project No. 6468-07-1950

Jay Cerceo, of MACTEC Engineering and Consulting, Inc. (MACTEC), performed energy measurements on the aim righa tub subject the per tub refered. Wark instructions: I ms memorandum summarizes the field testing activities and presents the results of the energy measurements.

#### **SPT Energy Field Measurements**

SPT energy measurements were made on March 25, 2008, during drilling of Borings B-615 at the referenced site. The testing was performed by Jay Cerceo from approximately 4:30 PM on March 25 to 9:10 AM on March 26 under clear skies and a temperature of about 70 degrees Fahrenheit. The boring was drilled with personnel and equipment from MACTEC. The drilling equipment consisted of a CME 55LC model drill rig with an SPT automatic hammer. The drilling tools consisted of AW-J-sized drilling rods and a 2-foot long split tube sampler. Mud rotary drilling techniques were used to advance the borings below the depth at which groundwater was encountered at the time of energy testing. The drill rig operator during sampling was Mr. Robert Banks. Energy measurements were recorded during sampling at the depth intervals shown in Table 1.

The energy measurements were performed with a Pile Driving Analyzer (PDA) model PAX (Serial No. 3622L), and calibrated accelerometers (Serial Nos. K1050 and P5992) and strain gages (Serial Nos. AW #75/1 and AW#75/2). A steel drill rod, 2 feet long and instrumented with dedicated strain gages, was inserted at the top of the drill rod string immediately below the SPT hammer. The inserted rod was also instrumented with two piezoresistive accelerometers that were bolted to the outside of the rod. The instrumented rod insert had a cross-sectional area of approximately 1.19 square inches and an outside diameter of approximately 1.75 inches at the gage location. The drill rods included in the drill rod string were hollow rods in 5 to 10 foot long sections, with an outside and inside diameter of approximately 1.75 and 1.375 inches, respectively. The recommended operation rate of the hammer is not known. Due to the closed hammer system, the hammer lubrication condition and anvil dimensions could not be observed.

#### Calibration Records

The calibration records for all the above are filed in DCN TUR054.

#### Calculations for EFV

The work was done in general accordance with ASTM D 4633-05. The strain and acceleration signals were converted to force and velocity by the PDA, and the data was interpreted by the PDA according to the Case Method equation. The maximum energy transmitted to the drill rod string (as measured at the location of the strain gages and accelerometers) was calculated by the PDA using the EFV method equation, as shown below:

$$EFV = \int F(t) * V(t) * dt$$

Where: EFV = Transferred energy (EFV equation), or Energy of FV

F(t) = Calculated force at time t

V(t) = Calculated velocity at time t

The EFV method of energy calculation is recommended in ASTM Standard D4633-05. The EFV equation, integrated over the complete wave event, measures the total energy content of the event using both force and velocity measurements. The EFV values associated with each blow analyzed are tabulated in the attached PDIPLOT tables and are also shown graphically in the PDIPLOT charts.

#### Calculations for ETR

The ratio of the incasured transferred energy (EFV) to the theoretical potential energy of the SPT system (140 lb weight with the specified 30 inch fall) is the ETR. The ETR values (as percent of the theoretical value) are shown in Table 1.

#### Comparison of ETR to Typical Energy Transfer Ratio Range

Based on a research report published by the Florida Department of Transportation (FDOT) (Report WPI No. 0510859, 1999), the average ETR measured for automatic hammers is 79.6%. The standard deviation was 7.9%; therefore, the range of ETRs within one standard deviation of the average was reported to be 71.7% to 87.5%. This range of ETRs was also consistent with other research that was cited in the FDOT research paper; however, maximum and minimum ETR values of up to 98% and 56%, respectively, were reported in the literature. The ETR values shown in Table 1 are generally within the range of typical values for automatic hammers as reported in the literature.

#### Discussion

Based on the field testing results, observations from the SPT energy measurements are summarized below:

• The data obtained by the PDA are consistent between individual hammer blows and between the sample depths tested. In general, the first and last one (and sometimes two) hammer blow records recorded by the PDA produced poor quality data (which is relatively common) and, as such, the record(s) was(were) not used in the data reduction.

- The average energy transferred from the hammer to the drill rods for each individual depth interval using the EFV method ranged from 286 foot-pounds to 303 foot-pounds. These average energy transfers correspond to energy transfer ratios (ETR) of 82% to 87% of the theoretical energy (350 foot-pounds) of the SPT hammer.
- The average at each depth interval was calculated as the transferred energy for each analyzed blow of the depth intervals divided by the total number of hammer blows analyzed. The overall average energy transfer of the SPT system (for all the depth intervals tested) was 292.8 foot-pounds, with an average ETR of 83.7%.

Attachments: Page 4 Table 1 - Summary of SPT Energy Measurements – 1 Page

Page 5 Work Instruction – DCN TUR-055 – 1 Page Pages 6 Record of SPT Energy Measurement – 1 Page

Pages 7 – 13 PDIPLOT Output – 7 Pages

## TABLE 1 SUMMARY OF SPT ENERGY MEASUREMENTS (ASTM D4633-05)

Turkey Point COL Project
Dade County, Florida
MACTEC Project No. 6468-07-1950

Hammer Serial No.	Rig Owner	Rig Operator	Boring No. Tested	Rod Size	Date Tested	Sample Depth (feet)	SPT Blow Count (blows. per six inches)	No. of Blows Analyzed	Average Measured Energy (Average EFV) (ft-lbs) <sup>a</sup>	Energy Transfer Ratio (%) <sup>b</sup> (Average ETR)
) (F.C. 02	MACTEC					117.3 - 118.8	27 - 22 - 31	82	287	82.0%
MEC-02	MACTEC Raleigh	Robert Banks	B-615	AW-J	3/25/2008	127.0 - 128.5	4 - 8 - 8	19	286	81.7%
(CME 55LC)	Kaleigu					139.1 - 140.6	27 - 24 - 16	59	303	86.6%
							Ave	rage for Rig:	292.8	83.7%

<sup>&</sup>lt;sup>a</sup>Measured Energy is energy based on the EFV method, as outlined in ASTM D4633-05, for each blow recorded by the PDA. In some cases, the initial and final one to two blows produced poor quality data, and were not used to calculate the Average Measured Energy.

EFV = EMX \* 1000 lbs/kip, where EMX equals the maximum transferred energy measured by the PDA (see attached PDA data).

The average ETR values may differ slightly and insignificantly from those in the PDIPLOT tables due to roundoff.

Prepared By:	Date: 8-15,08	Checked By:	Markell	Date: 🖇	19/08	/
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<sup>&</sup>lt;sup>b</sup>Energy Transfer Ratio is the Measured Energy divided by the theoretical SPT energy of 350 foot-pounds (140 pound hammer falling 2.5 feet).

#### Work Instruction No. 9

Turkey Point COL Project
MACTEC Engineering and Consulting, Inc.
MACTEC Project 6468-07-1950

Issued To: S	Steve Kiser and	Jay Cerceo		Rev. No.	1
Issued By:	Tom McDaniel			Date:_	3-24-08
Valid From:_	3-24-08		To:	4-30-08	

**Task Description:** Perform SPT Energy Measurements

<u>Applicable Technical Procedures or Plans, or other reference:</u> Geotechnical Work Plan (current revision; available at Site Office), Bechtel Specification 25409-102-3PS-CY00-00001, Rev. 000 or later revision, section 4.3, ASTM D 4633-05 (copy attached.).

Specific Instructions (note attachments where necessary): Perform energy measurements for each drill rig on site in accordance with ASTM D-4633-05. Consult with Site Coordinator as to schedule for rigs that may be planned for use that are not yet present. Hammer weights have been checked by site personnel, and records will be available on site. All rigs are using automatic hammer systems. Confirm that automatic hammer system is being operated within manufacturer's recommendations or in a typical operating fashion as observed from watching one or two SPT measurements prior to measuring energy. Be sure to check each drill rig using all hammer/rod combinations that it will be using. Depths for measurements should be coordinated with the Site Coordinator, and can be directed by Becthel in accordance with the specification. Site profile consists of very soft soils to about 5 feet followed by high-N-value soft rock to about 20 feet where coring begins. Sands are present below about 100 to 125 feet. Energy measurements should be made in the deeper sand zone as often as can be done, consistent with the drilling depths at the time of the measurements. See Site Coordinator for current boring logs of holes drilled and use these to plan most effective field measurement program.

Submit copies of calibration records for equipment to Project Principal for review prior to beginning work on site.

<u>Special Instructions</u> (note attachments where necessary): Confirm with Site Manager that approval of equipment calibration records has been received prior to beginning field testing. If unexpected conditions are encountered that affect measurements, contact Site Coordinator, Project Principal (Tom McDaniel) or Sr. Project Principal (Al Tice) immediately.

**Report Format:** Standard report in accordance with ASTM D 4633 requirements.

Specific Quality Assurance Procedures Applicable: QAP 20-1; QAP 25-1; QAP for Reporting Nuclear-Related Defects, or Noncompliances, per Federal Regulation 10CFR21 and Section 306 of the Energy Reorganization Act of 1974. Current revisions apply.

#### Hold Points or Witness Points: None

**Records:** All records generated shall be considered QA Records.

Reviewed and Approved by: (No	ote: Only one signature is required fo	r issuance)
Project Manager:	MATHO	Date:
Project Principal Engineer:	14.11110	Date:
Site Manager/Coordinator:	// // ( )	Date:
Pages: 1 plus attachment		DCN: TUR-055
Attachments: ASTM D 4633-05		



2801 YORKMONT ROAD, SUITE 100 ☐ CHARLOTTE, NC 28208 Telephone: (704) 357-8600 / Facsimile: (704) 357-8638

### RECORD OF SPT ENERGY MEASUREMENT

	GENERA	L INFORM	ATION		<del>"</del>	<u> </u>		DR	ILL RIG DA	\TA					
PROJECT:	Turkey Po	int COL Pro	oject			MAKE:		CME				<del></del>			
LOCATION:	Florida Cit				· ·	MODEL:		5510	· · · · · · · · · · · · · · · · · · ·		<del> </del>				
PROJECT NO.:	6468-07-1					SERIAL NO.:		33114			·				
DATE:	3-25-		···			HAMMER TYPE: Automatic									
WEATHER:		70'S W	indu			ROPE CONDITION: N/A									
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DRILLING COMPANY:	MAC					NO. OF SHE	AVES:	N/A							
					BORING	DATA									
BORING NUMBER:	B-61	5				<del></del>	***	***		···	<del></del>	<del></del>			
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TIME DRIVEN:	5:40	om o													
RIG OPERATOR:	R.B	anks													
HAMMER OPERATOR:	J.R.	sse(									,,,,, <u></u> ,,,				
PDA PAK SERIAL NO.:		36	22L			362	22L			362	2L				
INSTR. ROD AREA:	1.19	'nz													
ACCEL, SERIAL NOS.:	K1050	d 1	25992												
STRAIN SERIAL NOS.:	75 N	W-1 a	- 75 Air	1-2											
	SAMPLE	SPT	- DEPTH	C 3/25/0	SAMPLE	SPT	DEPTH	SPT	SAMPLE	SPT	DEPTH	SPT			
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