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Robert J. Murillo Licensing Manager Waterford 3

W3F1-2010-0012

February 25, 2010

U.S. Nuclear Regulatory Commission Attn: Document Control Desk Washington, DC 20555-0001

Subject:

Licensee Event Report 2009-006-00 Waterford Steam Electric Station, Unit 3 (Waterford 3) Docket No. 50-382 License No. NPF-38

Dear Sir or Madam:

Entergy is hereby submitting Licensee Event Report (LER) 2009-006-00 for Waterford Steam Electric Station Unit 3. This report provides details associated with the Main Feedwater Isolation Valves failing their timed stroke tests during Inservice Testing.

Based on these failures, it was determined that Waterford 3 operated in a condition prohibited by the Limiting Condition for Operation (LCO) delineated in Technical Specification 3.7.1.6, which requires that each Main Feedwater Isolation Valve (MFIV) shall be operable in modes 1 through 4. Additionally, it was determined that this condition could have prevented the fulfillment of a safety function that is needed to mitigate the consequences of an accident, and that a single cause led to the inoperability of two independent trains. The condition is reported herein as required by 10 CFR 50.73(a)(2)(i)(B), 10 CFR 50.73(a)(2)(v)(D), and 10 CFR 50.73(a)(2)(vii).

This report contains no new commitments. Please contact Robert J. Murillo at (504) 739-6715 if you have questions regarding this information.

Sincerely; $1n\Lambda$. Im RJM/RJP

Attachment:

Licensee Event Report 2009-006-00



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cc:

Mr. Elmo E. Collins, Jr. Regional Administrator U. S. Nuclear Regulatory Commission Region IV 612 E. Lamar Blvd., Suite 400 Arlington, TX 76011-4125

NRC Senior Resident Inspector Waterford Steam Electric Station Unit 3 P.O. Box 822 Killona, LA 70066-0751

U. S. Nuclear Regulatory Commission Attn: Mr. N. Kalyanam Mail Stop O-07D1 Washington, DC 20555-0001

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Louisiana Department of Environmental Quality Office of Environmental Compliance Surveillance Division P. O. Box 4312 Baton Rouge, LA 70821-4312

R.K. West, lerevents@inpo.org - INPO Records Center

Attachment

W3F1-2010-0012

Licensee Event Report 2009-006-00

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	5		20.2	201(d)		20.2203	(a)(3)(ii)	50.73(a)(2)(ii)(A)).73(a)(2)(viii)(/	۹)
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			20.2	203(a)(2)(Vi) 12	2. LICE	50.73(a))(2)(1)(B ONTAC) T FOR T	HIS LER	/)(D)		RC FORM 366A	\
ACILITY NAME				· · ·					TELEPHONE NUM	BER (Inc	ude Area	a Code)	
Vaterford	3 Steam	n Electi	ric Stat	ion Robe	ert J.	Murillo				(50	4) 739	9-6715	
0.1105	OVOTE			MANU-							REPU	MANU-	REPORTABLE
CAUSE	SYSTEM			FACTURER	1			CAUSE	SYSTEM	COMPC	NEN I	FACTURER	TO EPIX
E	SJ	ν	/OP	A391		YES							
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On 1'	T 2/28/200	Q it wa	ae aeta	blichad th	nat in	sonvice	a tast		ailures that or	courro	d on 1	10/22/2000	on
both I	/20/200 /lain Fee	edwate	er Isola	tion Valve	es (M	FIVs)	nad a	comm	on cause and	t could	l have	prevented	the ·
) fulfilln	ent of t	he MFI	Vs saf	ety function	on ne	eded t	o miti	gate th	e consequer	nces of	an a	ccident. TI	ne
plant	operate	d in a c	conditic	n prohibi	ted b	y Tech	nical	Specifi	cation 3.7.1.6	6, whic	h req	uires both	MFIVs
to be	operable	e in Mo	odes 1	through 4	. Su	irveillar	nce re	quiren	ent 4.7.1.6 r	equire	s the	closure tim	e of
1622 (anore	qual lu	10 Sect	Jhus.									
Both	MFIVs u	se hvd	raulic a	actuators.	and	each d	contai	ns two	separate hvo	Iraulic	trains	s. An actua	ation
signa	results	in both	n trains	closing th	ne va	alve. W	/hile i	n Mode	e 5 with Read	tor Co	olant	System	
tempe	erature a	and pre	ssure	at approx	imate	ely 170	degr	ees F a	and 350 psia,	IST te	esting	using one	of
their l	ydraulio	c trains	result	ed in MFI		closing	in 12.	.6 seco	onds, and MF	IV B fa	ailing	to close. Ti	ne
maxir	num allo were sa	Wed Single	Iroke II orv. Th	me for the	e ISI Int Ca	IS 7.50 F Agus	o seco valua	tion de	ne MFIV test	is usin I moist	g thei	r otner nya trusion dur	raulic ring a
previo	us plan	t shutd	own lik	elv cause	ed ae	el to for	m, res	strictin	a flow in the a	affecte	d four	wav valve	s.
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		tion inc	luded	replacing	the I	nydraul	lic flui	d. Plar	ned correctiv	ve actio	on is t	o replace t	he
Corre	cuve ac												
Corre hydra	ctive ac ulic fluic	l prior t	o plant	t startup i	n whi	ich moi	isture	could	exist in the flu	uid.			1

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NRC FORM 366A					ULATOR		IISSION
(9-2007)	CONTINUATIO	N SHEET	(LER) [
1. FACILITY NAME	2. DOCKET		6. LER NUMBER	_		3. PAGE	
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		·	
Waterford 3 Steam Electric Sta	tion 05000382	2009	- 006 -	00	· 2	OF	6
NARRATIVE	· · · · · · · · · · · · · · · · · · ·						
REPORTABLE OCCURREN	CE						
This condition meets three re	porting criteria:						

10CFR50.73(a)(2)(i)(B), 10CFR50.73(a)(2)(v)(D), and 10CFR50.73(a)(2)(vii).

10CFR50.73(a)(2)(i)(B):

Waterford 3 operated in a condition prohibited by the limiting condition for operation (LCO) delineated in Technical Specification 3.7.1.6, which requires that each Main Feedwater Isolation Valve (MFIV) [SJ] shall be OPERABLE in MODES 1, 2, 3, and 4. The MFIVs were not recognized as inoperable in cycle 16. The requirement was not met to close and deactivate, or isolate the inoperable valve within 72 hours and verify inoperable valve closed and deactivated or isolated once every 7 days; otherwise, be in at least HOT STANDBY within the next 6 hours and in COLD SHUTDOWN within the following 30 hours.

10CFR50.73(a)(2)(v)(D):

A condition existed that could have prevented the fulfillment of a safety function of a system that is needed to mitigate the consequences of an accident. Specifically, the condition could have prevented the ability to isolate Main Feedwater flow to the Steam Generators within the time limit allowed by design.

10CFR50.73(a)(2)(vii):

A condition existed where single cause led to inoperability of two independent trains. Specifically, the M and M1 4-way valves for both the A MFIV and B MFIV respectively experienced moisture induced gelling of its Fyrquel hydraulic fluid. The M1 and M 4-way valves for both the A MFIV and B MFIV respectively functioned properly. This single cause resulted in a reasonable expectation that both trains of the MFIVs were not functional at some time during operating cycle 16.

The event date is 10/22/2009 based on failure of the MFIVs to successfully pass Inservice Testing performed on 10/22/2009. Following an evaluation of information provided in the associated condition report's apparent cause and additional information obtained from engineering, it was established on 12/28/2009 that the MFIVs did not meet their design closure time. The cause was due to gelling that likely occurred over a period of time during operating cycle 16. The 60 day report due date was determined to be 2/26/2010.

INITIAL CONDITIONS

During the period of inservice testing on the MFIVs, the plant was in cold shutdown (Mode 5) conducting refueling operations for refueling outage 16. Reactor Coolant System [AB] temperature was approximately 170 degrees F and Reactor Coolant System pressure was at approximately 350 psia. There was no requirement for the MFIVs to be operable in this plant condition. This plant condition did not contribute to this event. There were no other structures, systems, or components inoperable at the start of the event that contributed to the event.

NRC FORM 366A (9-2007) LICENSE	EE EVENT R	EPORT (U.S. NUC (LER)	LEAR REG	ULATOR	COMMIS	SSION
1. FACILITY NAME	2. DOCKET		LER NUMBER			3. PAGE	
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		:	
Waterford 3 Steam Electric Station	05000382	2009	- 006 -	00	⁻ 3	OF	6 ,
NARRATIVE INITIAL CONDITIONS (continued)					2		•
The main feed water isolation valves isola generators and isolate the non-safety rela of the system. The MFIVs close on recei either low steam generator pressure or h actuated manually from the control room.	ate main feed ated main feed pt of a Main S igh containme	water flow Iwater sup team Isola nt pressur	to the secon oply from the ation Signal (re. The MFIN	idary side safety-re MSIS), g /s may a	e of the elated p enerate lso be	steam ortion ed by	
The MFIV hydraulic actuator consists of t system. The pneumatic system supplies pump and supplies motive air to position the piston actuator and the hydraulic accu an associated pump providing hydraulic f 'M' and 'M1') that feed the MFIV's accum operator requires both of its accumulators closure stroke time. That is, both the 'M' accumulators operate simultaneously. F achieve its design closure time.	wo systems: to the motive for the 4-way hyd umulators. Ea fluid to two in- julators and va s to supply the and 'M1' 4-wa ailure of any c	he pneum ce to ope raulic valv ch MFIV to arallel 4-v live actual motive fo ay valves r ne 4-way	atic system a rate the air m ves that direct train has a hy way hydrauli tor. The des prce needed must function valve results	and the h notor of th ydraulic r c valves (ign of each to achiev n in order in an MF	ydrauli ne hydr ic fluid eservoi (design ch MFI) e its de to have FIV not	c aulic flow to ir with ated as V valve esigned e both able to	2
The hydraulic fluid used in the MFIVs is F fluid can undergo hydrolysis producing an breather cap is used to minimize moistur	Fyrquel 220 M n acid which c e in the reserv	LT. Wate an result i oirs.	r or moisture n gel formati	in this ty on. A de	pe of h siccant	ydraulio	•
When the valve is first opened for plant s accumulator through the 'M' and 'M1' val The fluid in the reservoirs is sampled on- However, the hydraulic fluid within each on- on-line.	tart up, the hy ves where it is line monthly a 4-way valve is	draulic flu locked in nd change trapped a	id (Fyrquel) i place by the ed approxima ind not samp	s drawn i e 'M' and ately ever lled or ch	nto the 'M1' va y 3 mo anged y	lves. nths. while	. ·
The plant was shutdown in preparation for for this shut down, and the hydraulic fluid During the hurricane force winds and rair breather. Upon reopening of the MFIVs a moisture) was drawn back into the accun above, the hydraulic fluid within each 4-w on-line. Thus, for approximately 13 mon 'M1' 4-way valves, creating the condition actuated by the IST train A tests.	or Hurricane G I from the actu n, moisture int after several d nulator throug vay valve is tra ths, Fyrquel w s for gel forma	ators was rusion like ays, the hy n the 'M' a upped and ith moistu ation withir	8/31/2008. T discharged ly occurred t ydraulic fluid and 'M1' 4-wa is not sampl re was captu n the 4-way w	The MFIV to the res hrough th (that was ay valves led or cha red inside valves wh	s were ervoirs e desid s expos . As no anged v e the 'N ich are	closed ccant ed to oted while 1' and	
	* .						

		PEPORT	U.S. NUCLE	AR REGULA	ATORY COMMI	SSION
	CONTINUATIO	N SHEET		X		
1. FACILITY NAME	2. DOCKET		6. LER NUMBER		3. PAGE	
		YEAR	SEQUENTIAL R			
Waterford 3 Steam Electric Station	05000382	2000	006	00	4 05	6
	0000002	2009	- 006 -	00	-+ UF	<u> </u>
EVENT DESCRIPTION						
FW-184A (Steam Generator No. 1 MF hydraulic train. Inservice Tests (IST) a only one hydraulic train in service per allowed closed stroke time of less that calculation EC-M00-006 is a maximum test used the "M" 4-way valve to close the A train test circuit	FIV) [SJ] closed in are performed at procedure OP-9 n 6.6 seconds. T n allowed closed the valve. This	n 12.6 sec no feedwa 03-033. T The design stroke tim was the in	-service testing onds using the ater flow or pres he IST procedu analysis limit p he of less than 7 hitial as-found te	A accum ssure con re limit is per Water 2.56 secon est of FW	ed valve ulator and ditions with a maximur ford 3 nds. The -184A using	n
At approximately 20:28 hours on 10/2 stroke time tested per procedure OP-9 used the "M1" 4-way valve to close the as-found test of FW-184A using the B	2/2009, FW-184/ 903-033 using the e valve. The valv train test circuit.	A (Steam) e B accum ve closed	Generator No. 1 nulator and hydi in 6.4 seconds.	MFIV) w aulic trair This was	vas close n. The test s the initial	
At approximately 21:40 hours on 10/2 time tested per OP-903-033 using the way valve to close the valve. The valve This was the initial as-found test of FV At approximately 21:48 hours on 10/2 time tested per OP-903-033 using the valve to close the valve. The valve clo acceptance criteria but was within the	2/2009, FW-184 B accumulator a ve did not move V-184B using the 2/2009, FW-184 A accumulator a osed in 6.7 secon design analysis	B (Steam) and hydrau off the full A train te B (Steam) and hydrau nds, which limit of 7.5	Generator No. 2 ulic train. The te open position (est circuit. Generator No. 2 ulic train. The te did not meet th 56 seconds. Thi	2 MFIV) w est used t did not str 2 MFIV) w est used t ne proced s was the	vas stroke he "M1" 4- roke closed vas stroke he "M" 4-wa ure initial as-). ,
found test of FW-184B using the B tra It is a reasonable expectation that the during design basis conditions based	in test circuit. MFIVs could ha on the IST train /	ve failed to A closure :	o meet their req stroke times.	uired stro	ke times	
The last successful test of MFIV closu Outage 15 on April 29, 2008.	ire was complete	d when th	e plant was shu	ıtdown in	Refueling	
When discovered, this event did not a release of radioactive material, or miti maintain Mode 5 were available and o Specifications.	ffect the systems gate the conseque operating as requ	s needed t Jences of Ired by pla	o remove resid an accident. T ant conditions a	ual heat, he syster nd the Te	control the ns needed chnical	to
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Veak Scienting NUMBER NUMBER Waterford 3 Steam Electric Station 05000382 2009 006 00 5 0F 6 VarRATIVE CAUSAL FACTORS The cause analysis determined the most probable cause is that the four way hydraulic valve was sluggish during the first stroke due to gelled hydraulic fluid that developed over time. When sitting static, Fryquel fluid has a known history of gelling. This localized gelling caused the four way hydraulic 'M' and 'M1' valves on the 'A' and 'B' MFIV's respectively to have sluggish operation. This sluggish operation delayed the porting of fluid to the main hydraulic piston to cause a delay on the MFIV A and failure to stroke on the MFIV B. A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic fluid uring refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	1. FACILITY NAME	2. DOCKET		6. LER NUMBER			3. PAGE	
Waterford 3 Steam Electric Station 05000382 2009 0.06 0.0 5 0F 6 VARRATIVE CAUSAL FACTORS The cause analysis determined the most probable cause is that the four way hydraulic valve was sluggish during the first stroke due to gelied hydraulic fluid that developed over time. When sitting static, Fyrquel fluid has a known history of gelling. This localized gelling caused the four way hydraulic IV and M1 valves on the 'A' and 'B' MFIV's respectively to have sluggish operation. This sluggish operation delayed the porting of fluid to the main hydraulic piston to cause a delay on the MFIV A and failure to stroke on the MFIV B. A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueing outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.			YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		,	
 VARRATIVE CAUSAL FACTORS The cause analysis determined the most probable cause is that the four way hydraulic valve was sluggish during the first stroke due to gelled hydraulic fluid that developed over time. When sitting static, Fyrquel fluid has a known history of gelling. This localized gelling caused the four way hydraulic 'M' and 'M1' valves on the 'A' and 'B' MFIV's respectively to have sluggish operation. This sluggish operation delayed the porting of fluid to the main hydraulic piston to cause a delay on the MFIV A and failure to stroke on the MFIV B. A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition. 	Waterford 3 Steam Electric Station	05000382	2009	- 006 -	00	5	OF	6
CAUSAL FACTORS The cause analysis determined the most probable cause is that the four way hydraulic valve was sluggish during the first stroke due to gelled hydraulic fluid that developed over time. When sitting static, Fyrquel fluid has a known history of gelling. This localized gelling caused the four way hydraulic fw and M1' valves on the 'A' and 'B' MFIVs respectively to have sluggish operation. This sluggish operation delayed the porting of fluid to the main hydraulic piston to cause a delay on the MFIV A and failure to stroke on the MFIV B. A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	ARRATIVE		1					
The cause analysis determined the most probable cause is that the four way hydraulic valve was sluggish during the first stroke due to gelled hydraulic fluid that developed over time. When sitting static, Fyrquel fluid has a known history of gelling. This localized gelling caused the four way hydraulic fil fund that a developed over time. When sitting static, Fyrque fluid has a known history of gelling. This localized gelling caused the four way hydraulic fil fund that developed over time. When sitting static, Fyrque fluid has a known history of gelling. This localized gelling caused the four way hydraulic fil fund the 'A and ff' MFIVs respectively to have sluggish operation. This sluggish operation delayed the porting of fluid to the main hydraulic piston to cause a delay on the MFIV A and failure to stroke on the MFIV B. A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	CAUSAL FACTORS							
A contributing cause was that plant processes did not direct replacement of the hydraulic fluid during outages that did not involve a refueling outage. CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic, components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	The cause analysis determined the m sluggish during the first stroke due to static, Fyrquel fluid has a known histo hydraulic 'M' and 'M1' valves on the 'A sluggish operation delayed the porting MFIV A and failure to stroke on the M	ost probable cau gelled hydraulic f ry of gelling. Thi A' and 'B' MFIVs g of fluid to the m FIV B.	se is that f fluid that d s localized respective ain hydrau	the four way leveloped ove d gelling caus ly to have slu ulic piston to	hydraulic er time. V ed the fo uggish op cause a c	valve Vhen ur way eration lelay c	was sitting / n. This on the	
CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	A contributing cause was that plant p outages that did not involve a refuelin	rocesses did not g outage.	direct rep	lacement of t	he hydra	ulic flu	id during	9
CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic. components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.				· · ·	•			
CORRECTIVE ACTIONS During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.								, .
During maintenance on MFIV A, the valve hydraulic fluid was replaced, the valve hydraulic components were flushed, and the valve was successfully stroked. The entire hydraulic actuator on MFIV B was replaced. The hydraulic fluid was replaced during the refueling outage as part of a preplanned replacement of the actuator. Planned corrective action is to revise the preventative maintenance task to replace the hydraulic fluid in MFIV A and MFIV B with new oil prior to plant startup (including forced outages) in which moisture could exist in the reservoir or actuator to ensure oil is not in a degraded condition.	CORRECTIVE ACTIONS							
	The entire hydraulic actuator on MFIV	B was replaced.	. The hydr	raulic fluid wa	as replace	ed dur	ing the	
	The entire hydraulic actuator on MFIV refueling outage as part of a preplann Planned corrective action is to revise in MFIV A and MFIV B with new oil pr could exist in the reservoir or actuator	B was replaced ed replacement of the preventative ior to plant startu	The hydion of the actur maintenar p (includir not in a de	raulic fluid wa lator. nce task to re ng forced outa graded condi	as replace place the ages) in v tion.	ed dur hydra vhich r	ing the aulic fluid moisture	d e
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NARRATIVE

SAFETY SIGNIFICANCE

The as found condition supports that the MFIVs would have closed upon demand at a rate slower than called for in their design. The risk associated with the 10/22/09 failure of the MFIVs (FW-184A and FW-184B) [SJ] to meet their OP-903-033 stroke time requirements for maximum closing time was bounded by a conservative risk assessment using the current Waterford 3 PSA model. Since in one of the MFIV tests (FW-184B with the ESFAS-A test circuit) the valve did not close at all, and there was a hydraulic fluid problem common to both valves, it was conservatively assumed in the risk assessment that both MFIVs failed to close. Failure to close of the MFIVs does not adversely affect the core damage risk, since availability of feedwater (i.e., the valves being open) maintains decay heat removal and contributes to prevention of core damage; the potential risk impact of failure to close of the MFIVs is in terms of failure to isolate in a core damage sequence, measured by the Large Early Release Frequency (LERF). The impact of MFIV closure on large early release risk was assessed by modeling a feedwater line break with failure of the feedwater line to isolate. In order for a large release from containment following a core damage event to occur through the ruptured feedwater line, failure of the MFIV to close would require, in addition, failure to close of the upstream check valve (FW-181A or B) and failure to close of either the main feedwater regulating valve (FW-173A or B) or the startup feedwater regulating valve (FW-166A or B). The probability of these failures was estimated using the W3 PSA model and combined with the CDF for a feedwater line break. The large early release risk impact (change in large early release frequency, delta-LERF) for both MFIVs failing to close was estimated to be an increase of 3.8E-14 per reactor year, which is very small (the generally accepted LERF threshold for risk significance is 1E-7; see for example Regulatory Guide 1.174.). Therefore, since the LERF increase was estimated to be extremely small, there is no risk significance to the condition of the MFIVs failing to meet their OP-903-033 stroke time requirements for maximum closing time.

There were no safety consequences due to this occurrence. When discovered, this event did not affect the systems needed to remove residual heat, control the release of radioactive material, or mitigate the consequences of an accident. The systems needed to maintain Mode 5 were available and operating as required by plant conditions and the Technical Specifications. The main feedwater regulating valves (FW-173A and B) and the startup feedwater regulating valves (FW-166A and B) are credited as backups to the MFIVs upon a failure of its associated MFIV to close. These backup valves also close on receipt of an MSIS and were available to provide the backup function. Thus, if a design basis accident would have occurred, redundant equipment was available to meet the design function.

SIMILAR EVENTS

There have been no previous, similar events associated with IST failure of the MFIVs due to degradation of the hydraulic fluid.

ADDITIONAL INFORMATION

Energy industry identification system (EIIS) codes are identified in the text within brackets [].