ATTACHMENT II TO IPN-97-173

REFUELING OUTAGE 9

STEAM GENERATOR INSPECTION SUMMARY REPORT

New York Power Authority
Indian Point 3 Nuclear Power Plant
Docket No. 50-286
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New York Power Authority

Indian Point Unit 3 Nuclear Power Plant

Refueling Outage 9
Steam Generator Inspection Summary Report

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1.0 SUMMARY

Indian Point Unit 3 is a Westinghouse designed four (4) loop unit having Model 44F steam generators. These steam generators each have 3214 tubes fabricated from Alloy 690 Thermally Treated Seamless Tubing, having a nominal wall thickness of 0.050 inches and an outside diameter of 0.875 inches. The tubes are full depth hydraulic expanded into the tubesheet and welded to the cladding on the primary side.

The tubes are supported by six support plates made from ASME SA-240 stainless steel which have broached quatrefoil (concave) holes on a 1.2344" square pitch. Below the first support plate is a flow distribution baffle that has octafoil shaped broached holes.

During Indian Point's Refueling Outage 9, the Steam Generator Field Services Group of the Westinghouse Nuclear Services Division (W NSD) provided services that included primary manway removal/installation, nozzle cover installation/removal, eddy current tube inspection, primary and secondary eddy current data analysis, handhole removal/installation, inspection port removal/installation, tubesheet cleaning, secondary manway removal/installation, foreign object search (FOS) and retrieval, support plate inspection (SID), in-bundle inspection service (IBIS), upper support plate inspection, steam drum inspection and assessment, feedring visual inspection, wrapper support inspection, and an upper girth weld inspection. The visual inspections were informational to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. The criteria used for these visual inspection assessments were not of an ISI non-destructive examination nature.

Primary side steam generator activities followed defueling in the outage schedule and were not critical path activities. The eddy current inspection program consisted of 61.17 and 64.25 percent full-length bobbin in steam generators 33 and 34 consisting of 1966 and 2065 tubes respectively. An augmented inspection was also performed which included a 20% and 21.17% random sampling of the top of the tubesheet (643 and 681 tubes respectively) 20% random sampling of row 1 and 2 u-bend areas (37 tubes in each S/G) and a sampling of dents in each steam generator, Reference Table 2.3.1.

There were no pluggable indications identified during this program and no tubes were repaired.

2.0 STEAM GENERATOR PRIMARY SIDE ACTIVITIES

Steam generator primary side activities included manway cover removal and installation, installation of nozzle covers, eddy current inspection, primary and secondary data analysis, and channelhead video scans. Contingencies for mechanical tube plugging, tube mouth rework, bolt hole repair, and gasket seating surface repair were planned but not required.

Steam generators 33 and 34 were inspected during Refuel Outage 9. This was the third in-service inspection program for these steam generators since their installation in 1989. Prior inspections were two - 20% bobbin probe inspections of all four steam generators performed in September

1990 and May 1992. The inspections performed in steam generators 33 and 34, respectively, during the current outage included a 61.17% and 64.25% full length bobbin inspection, a 20% and 21.17% random pattern hot leg top-of-tubesheet plus point program, and a 20% random pattern of row 1 and row 2 plus point U-bend inspection program. The bobbin inspection program was augmented by adding to it all tubes that had any prior history of dent identification, tubes surrounding previously identified loose parts (reference NYPA Nuclear Safety Evaluations NSE-92-03-124 SG and 90-03-305-SG), and tubes that did not have full length inspections from prior outages. Thus steam generators 33 and 34 now have 100% of their tubes in-service inspected with bobbin probes. Also based on the results of the current bobbin inspection program, all tubes having tube support plate dents were inspected with a rotating pancake coil probe.

2.1 Eddy Current Inspection

Eddy current inspection was performed in steam generators 33 and 34 using Westinghouse's ROSA III positioning system. ROSA III was operated using a 3400 feet fiber optic cable from the Mechanical/Electrical Annex room in the Theodore Hill training building. Data collection, resolutions, and data management was performed at site in the training building. Primary and secondary analysis was performed independently in separate bays at the Westinghouse Waltz Mill Site (RDAC), located in Madison Pennsylvania. During primary and secondary data analysis, surveillance was performed by NYPA Quality Assurance (QA) to ensure independence .

A generalized system configuration is shown in Figure 2.3.1.

ROSA was installed and operated using procedure NSD-FP-1997-7994 Revision 0, ROSA III Operating Procedure, Indian Point 3. Eddy current data acquisition was performed using the following procedures:

- NSD-FP-1997-7956 Revision 2, Eddy Current Inspection of Inservice Heat Exchanger Tubing, Indian Point 3.
- ACTS INT-01-197, Revision 3, - Full Length Bobbin.
- ACTS INT-02-197, Revision 3, - TSH and Special Interest Plus Point RPC.
- ACTS INT-03-197, Revision 3, - Special Interest 3 Coil RPC.
- ACTS INT-04-197, Revision 3, - Low Row U-Bend Bobbin Inspection.
- ACTS INT-05-197, Revision 3, - U-Bend RPC.
- ACTS INT-06-197, Revision 3, - Locations masked by permeability.

Eddy current analysis and Site Specific Performance Demonstration (SSPD) Testing was performed in Madison, PA via a dedicated high speed transmission line (T-1) connection in the Mechanical/Electrical Annex room on site. Ten (10) analysts were used per shift; five primary reviewers and five secondary reviewers. One analyst handled the data from each bobbin probe and one analyst handled +Point data. Results of the analysis were returned to site via the T-1 line and compared by on-site resolution analysts. Discrepancies between primary and secondary analysis were reviewed daily. The following procedures were used for analysis;

- NSD-FP-1997-7971 Revision 3, Steam Generator Eddy Current Data Analysis, Indian Point 3.
- ANTS INT-A-197, Revision 3 & 4, - Bobbin.
- ANTS INT-B-197, Revision 3 & 4, - Plus Point RPC.
- ANTS INT-C-197, Revision 3 & 4, - 3 Coil RPC.

- ANTS INT-D-197, Revision 3 & 5, U-Bend Plus Point RPC.

Copies of the Acquisition Technique Specification Sheet (ACTS), Analysis Technique Specification Sheet (ANTS), data analysts resolution reports, data analysts sheets showing review of ANT revisions during the job, Probe Authorization Letter, and the probe usage log have been included in the appropriate work package.

The 9th Refueling Outage eddy current inspection scope consisted of 61.17% and 64.25% full length bobbin, 20% and 21.17% top of tubesheet plus point RPC, and 20% of row 1 and 2 u-bend magnetic-bias plus point RPC in S/G's 33 and 34, respectively. A special interest program, which included all dents at tube support plates, was established upon completion of the bobbin probe inspection program.

The inspection was performed utilizing the Westinghouse ROSA III robot and TC-6700 tester. The techniques performed during the inspection were qualified in accordance with Appendix H of EPRI's "PWR Examination Guidelines". The Westinghouse long life probe, EB-720-LLMC, was used for the bulk of the bobbin inspections. The EB-680-BJFM-UF probe was used for the low row u-bends. The top of tubesheet RPC program was performed using the Zetec, 720-115-+PT-36S8052PH, plus point probe. This probe contains a 115 mil mid-range pancake coil, a plus point coil, and an 80 mil high-frequency pancake coil. The row 1 and 2 u-bend RPC program utilized the Zetec, M+PT-680MRPCFH52PH, magnetically biased plus point probe. The special interest program utilized the Zetec, 720/680-115-+PT-36S8052PH, plus point and the Zetec, M-720-115-+PT-36S8052PH, magnetically biased plus point probe.

The inspection programs are described in the volume "Supertubin™ data summary "New York Power Authority, Indian Point Unit 3 Refuel 9, June 1997, Steam Generator Eddy Current Inspection Results INT-33 and INT-34 (Volume 4 of Westinghouse Field Service Report INT-20). That report contains color maps of the inspection plans and specific types of indications. For reference, the final inspection plan maps are included in this summary as Figures 2.3.2, 2.3.3, 2.3.4, 2.3.5, 2.3.6, 2.3.7, 2.3.8, 2.3.10, and 2.3.11.

Table 2.3.1 summarizes the inspection program:

Table 2.3.1 Summary of Inspection Program Scope

Inspection Program	Steam Generator 33 Tube Count	Steam Generator 34 Tube Count
Full Length Bobbin	1966	2065
Hot Leg top-of-tubesheet +Point RPC	643	681
U-bend +Point RPC	37	37
Hot Leg Dent + Point Inspection	0	5
Cold Leg Dent + Point Inspection	0	28
Hot Leg Post Loose Object Removal	0	4

There were no pluggable indications identified during this inspection. The following indications were identified during this inspection:

Table 2.3.2 Indications: Steam Generator 33

Call	Code	Quantity
Manufacturing Buff Mark	MBM	7
Ding	DNG	1
Free Span Differential Signal	FSD	3

Table 2.3.3 Indications: Steam Generator 34

Call	Code	Quantity
Manufacturing Buff Mark	MBM	21
Ding	DNG	3
Dent	DNT	49
Free Span Differential Signal	FSD	7
Free Span - Non-confirmed	FSN	1
Possible Loose Part	PLP	10

As mandated by NYPA procedures, NSD-FP-1997-7971 Revision 3, Steam Generator Eddy Current Data Analysis, Indian Point 3, Appendix A (Free Span Disposition Flow Chart), FSDs (free span differential signal) required a history review to monitor change of signal phase and voltage. If change occurred, the code was altered to a FSI (free span indication) code and required further dispositioning. One tube (R8 C21) in S/G - 34 exhibited a bobbin signal that changed from baseline and was identified as a FSI. This signal was reported in the tangent area 2.8 inches above the 6th hot leg support plate ("G"). The FSI was later inspected with the plus point RPC probe which revealed a small ding at this location. The FSI code was then changed to a FSN (free span non-confirmed) and is currently considered a non-repairable condition.

MBMs (manufacturing burnish mark) also require a history review of baseline data. All MBMs that were reported had a history review performed on them and showed no change since the baseline data was taken.

There were no new dents reported during the bobbin inspection that were not present in baseline data. In addition, all dents reported by bobbin at support plates were inspected by the plus point RPC probe which detected no degradation or cracking. One tube in steam generator 34 was identified as having a dent present at an AVB location. This location is approximately 36 inches above the top support plate in the u-bend. A history review showed no change at this location since the baseline data was taken.

There were 10 tubes identified during the top of tubesheet RPC program in steam generator 34 (see Figure 2.3.12 Tubesheet map showing Eddy Current Identification of Potential Loose Parts) as possibly having a loose part (PLP). Four of these were caused by a piece of wire that was later removed. These 4 tubes were retested after the wire was removed and exhibited no degradation

nor any loose parts signals. The remaining tubes identified as PLPs had a visual examination performed which revealed small amounts of sludge/scale and no foreign objects.

During the plus point RPC top of tubesheet program, one tube (R21 C10) in steam generator 34 was found to have a dent at the transition area of the top of tubesheet. This location was inspected three times with the 0.720 diameter plus point probe and once with a 0.680 diameter plus point probe. All inspections showed a dent response with no detectable degradation.

There were several tubes tested that were not on the inspection program due to operator error. None of these tubes exhibited any degradation.

Detailed reports of the inspections, inspection results, analysis records, summary information related to this outage is contained in the steam generator field service report, INT-20, Volumes 1 through 4. **A listing of the indications for number 33 and 34 steam generators is provided in Attachment 2.**

Subsequent to the removal of ROSA from the steam generator channelheads, but prior to channelhead closure, a videoscan of both channelheads of steam generator 33 and 34 was performed. No anomalous conditions were noted during the scan. These scans also included an engineering assessment of the condition of the two factory weld plugs in steam generator 34 (R44C57 and R45C52); no anomalous conditions were noted.

3.0 STEAM GENERATOR SECONDARY SIDE ACTIVITIES

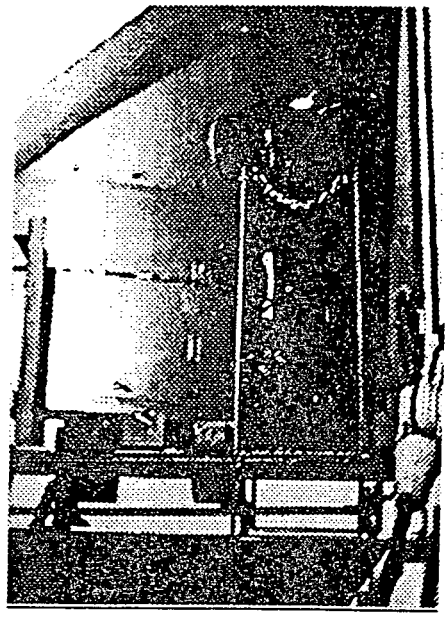
Handhole removal and installation, flow distribution baffle and tubesheet cleaning, FOS, and an In-Bundle Inspection (IBIS) were performed in steam generators 31, 32, 33, and 34. A Support Plate Inspection (SID) was planned for steam generators 33 and 34, but only completed in steam generator 34 due to equipment interferences encountered in steam generator 33. Subsequent to tubesheet cleaning in the first steam generator, 34, a cleanliness inspection was performed to characterized the existing sludge condition. This inspection was video taped .

In steam generator 33 and 34 the inspection port was removed and the "G" support plate inspected. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. This assessment was not of an ISI non-destructive examination nature but a visual evaluation performed by Westinghouse Engineering. This inspection was performed to inspect the support plate for evidence of cracking as identified in NRC Information Notice 96-09 and supplement.

In steam generator 34 the steam drum was inspected. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. This assessment was performed by a visual exam but was not of an ISI non-destructive examination nature. The visual inspections covered a number of areas; "G" support plate inspection through swirl vanes to look for evidence of support plate cracking at attachment points, AVB inspection through the swirl vanes to look for evidence of deposits, the transition cone to shell weld for evidence of pitting during wet lay up, inspection of the moisture separator for mechanical damage, inspection of selected J-nozzle and feedring welds, inspection of the upper wrapper supports, anti-rotation keys, and lower support

keys for evidence of mechanical damage or gross cracking of the wrapper, and inspection of the wrapper weld seam for gross mechanical features. This inspection was video taped.

3.1 Visual Inspections at Handholes



Following tubesheet cleaning cleanliness, foreign object searches, and in-bundle inspections were performed on all steam generators using procedure NSD-FP-1997-7965 Revision 2, Remote Examination and Removal of Foreign Objects from Steam Generator Secondary Side, Indian Point 3. For the foreign object search, the annulus and tube lane were inspected. For the in-bundle inspection approximately every 5th column was inspected in each quadrant of the steam generator. Additional in-bundle inspections were performed in steam generator 34 to examine areas where eddy current examination indicated the locations of several potential foreign objects. These inspections were videotaped.

In steam generator 34 a support plate inspection was performed with SID (Support plate Inspection Device); the SID inspection planned for steam generator 33 was aborted when the SID would not fit properly. The SID inspection was performed using procedure NSD-FP-1997-7965 Revision 2, Remote Examination and Removal of Foreign Objects from Steam Generator Secondary Side, Indian Point 3. This inspection was videotaped.

During the eddy current inspection several tubes were identified as having potential loose parts. These were all loca. . in steam generator 34 and were identified during the hot leg +Point probe inspection program. There were a total of 10 tubes in 5 specific areas (Figure 3.3.1) All five areas were examined by videoprobe and 4 of the 5 were identified as hard sludge deposits contacting the tube. The fifth, located in the hot leg near row 2 column 30 was a piece of wire. Following the removal of the object the tubes surrounding this location were inspected again with ECT and did not exhibit damage.

Retrieval of some other foreign objects was performed in steam generators 31, 32, 33, and 34. Some objects were not/could not be retrieved and a safety analysis (NSE 97-3-318-RCS) was performed to address operation without removal of the objects.

3.2 Visual Inspections through the Inspection Port

Procedure NSD-FP-1997-7966 Revision 1, Steam Generator Secondary Side Inspection , Indian Point 3, was used to perform the inspections of the upper, 6th or "G" support plate. This was an informational gathering procedure to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. This assessment was not of an ISI non-destructive examination nature but a visual evaluation performed by Westinghouse Engineering. A tubelane inspection was performed to assess sludge buildup on the "G" support plate. Additionally an in-bundle inspection was performed on selected columns

corresponding to attachment points of the "G" plate to the wrapper. This in-bundle was performed to address concerns identified in NRC Information Notice 96-09 and supplement regarding support plate cracking in some foreign plants. No indications of cracking being present in the "G" support plate were observed. The inspection was videotaped.

3.2.1 Inspection Port / Top Tube Support Plate "G" Inspections:

Steam Generator No. 33:

This inspection was an assessment of the top support plate to provide an indication of sludge buildup or for anomalous conditions. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. Entry was made through the steam generator lower shell upper inspection port and a video probe was traversed along the tube lane passing over the stay rod upper nut. This was a subjective examination with respect to sludge and will be compared to future inspections for evidence of heavy accumulation rates. In addition, the top support plate and its attachment to the wrapper were examined for gross cracking, missing segments, or anomalous conditions.

The initial examinations were in the tube lane region, which included scanning the top surface of the "G" tube support plate (top tube support plate), the tube support plate supports at each end of the tube lane, the bottom of the tube U-bends (Row 1), and looking into the tube rows. All support hardware reference numbers listed below are as specified in procedure NSD-FP-1997-7966 (page 25). This inspection was videotaped.

Wrapper/tube support plate support block #23 at the opposite end of the tube lane was assessed and no signs of deterioration were observed with the support wedges and their welds, and to the local tube support plate (limited views available).

- Tube support plate /Tubelane: No sludge deposits were seen in the tubelane, other than what appeared to be a thin magnetite coating with a powdery surface. The flow holes (i.e., two rows of 90 flow holes within the Row 1 U-bend) all looked clear on the top side, and occasional limited views into a few flow holes revealed that original machining marks were still visible and there was no apparent sludge build-up. All viewed row 1 tubes and a few row 2 tubes looked clean, with very little if any scale buildup. The tubes observed showed no marks on their outer diameter surface that could result from tube support plate movement upward. Viewing of the stay rod and nut in the center of the tube lane revealed no apparent weld (3 welds) cracking.
- At the inspection port end of the tubelane, tube bundle periphery, stamped letters in the tube support plate "G" top surface could be seen indicating a very thin, if any, magnetite coating at that position. All wrapper block #24 tube support plate support wedges looked clean and in good condition with no cracks observed in the welds (limited view available).
- During a second pass through the tubelane to view the bottom of the Row 1- U-bends, all the tube surfaces looked to be clean and in good condition.

The final examinations were in-bundle along the tube columns out to the tube support plate-to-wrapper junctions. These inspections included scanning the top surface of the "G" tube support plate, and the tube support plate supports at each end of the tube columns inspected (hot leg and cold leg). Again, all support reference numbers listed below are as specified in Procedure NSD-FP-1997-7966 (page 25). Observations from the videotape are as follows:

- This summary is for the upper "back-up bars" (the lower "back-up bars" could not be seen) which rest against the top surface of the tube support plate (without tube support plate welding) and prevent the tube support plate vertical movement. An assessment has been made of these back-up bars; the following observations were made for the hot leg side junctions at columns 91, 80, 63, 29, 10 and 1, and for the cold leg side junctions at columns 1, 10, 29, 63, and 80, as examined. All upper back-up bars appeared to be in good condition and are resting on the tube support plate top surface, with no observed cracks in the bar-to-wrapper welds (limited coverage). In addition, at these back-up bar locations, no gross cracking, missing segments, or anomalous conditions were observed in the tube support plate (limited views available).

- This summary is for the wrapper-to-tube support plate wedge groups that bear against the backside of the wrapper anti-rotation keys (4) and the "U" shaped tapered block attachments (6 of 8 total). An assessment has been made of the upper portion (the lower portion could not be seen) of the wedges and their wrapper attachment welds; the following observations were made for the hot leg side junctions at columns 88, 65, 48, 20, and 4, and for the cold leg side junctions at columns 4, 20, 48, 65, and 88, as examined. All wrapper-to-tube support plate wedge groups (upper portion) appeared to be in good condition and bearing against the tube support plate top surface, with no observed cracks in the attachment welds (limited coverage). In addition, at these wedge group locations, no gross cracking, missing segments, or anomalous conditions were observed in the tube support plate (very limited views available).

- For all the above assessments, the tube support plate was examined for the full traverse of the tube column from the wrapper to the tube lane. It was assessed that no gross tube support plate cracking, missing segments, or significant anomalous conditions were observed in the upper "G" tube support plate quatrefoil holes (limited views available - only those columns traversed and the top half of the tube support plate holes). For most of the tube support plate examined, a limited sludge/magnetite coating was present on the top surface and in the tube support plate tube holes. However, in a few locations as noted below, some tube scale was building up between the tube and tube support plate tube hole quatrefoil "lands." This tube scale seemed to be limited to the "land" locations and just above the "lands" on the tube, and in most cases has broken free of the "land" (scale was cracked). Where this tube hole scale existed, generally a little more sludge was present on the tube support plate top surface. These observations of slightly higher sludge concentrations were made for the hot leg side column 29, and for the cold leg side columns 4, 10, 48, 63, 65 and 80, as examined

Additional observations for the inspection port / top tube support plate "G" inspections are as follow:

- No foreign objects were observed during the above inspection port inspections.

- There were limited views available of the tube support plate at the wedge groups (contact points), where the highest tube support plate stresses exist, during the above inspection port inspections. It was recommended that the additional (optional) inspections of the tube support plate with a video probes probe from the primary separator entry points be performed in order to get a full picture of these bearing areas. See results of these additional (optional) inspections below (Section 3.3.1.5).

3.2.2 Inspection Port / Top Tube Support Plate "G" Inspections:

Steam Generator No. 34:

This inspection was identical to the inspection performed for the top support plate of SG 33 in section 3.2.1, and was to provide an indication of sludge buildup or for anomalous conditions. Entry was made through the steam generator 34 lower shell upper inspection port and a video probe was traversed along the tube lane passing over the stay rod upper nut. This was intended to be a subjective examination with respect to sludge and will be compared to future inspections for evidence of heavy accumulation rates. In addition, by using an in-bundle style guide tube, the top support plate and its attachment to the wrapper were examined for gross cracking, missing segments, or anomalous conditions.

SG 34 inspection port inspection produced results no different from those observed and reviewed by Westinghouse for SG 33. The SG 34 top tube support plate was inspected by video probe from the swirl vanes and the results of these additional inspection are described later in section 3.3.1.5.

3.3 Steam Drum Inspections

In support of normal maintenance and operation, as well as to address issues identified in the NRC Information Notice 96-09 and supplement, a steam drum and wrapper inspection plan was developed prior to the outage and performed using procedure NSD-FP-1997-7966 Revision 1, Steam Generator Secondary Side Inspection, Indian Point 3. This is an informational gathering procedure to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. Entry to the steam drum was made through a temporary scaffold which was erected at the "B" or outboard manway. This scaffold, which was larger than the permanent scaffold on the reactor cavity side, allowed for staging of equipment and personnel.

Westinghouse NSD Engineering, under contract with NYPA, provided a review and assessment of the steam drum and support plate inspections. These information gathering were of the top support plate accessed through the transition cone inspection port (on steam generators 33 and 34), and of the complete steam drum including remote inspections of the wrapper supports (upper and lower), top tube support plate and supports, and the tube bundle U-bend region, all performed by manned entry into the secondary side of steam generator 34.

From the collective observations which follow, these steam generators, to the extent inspected during this outage by procedure NSD-FP-1997-7966, do not exhibit any advance degradation, and only exhibit the possible initiation of some deterioration modes that should be observed in the future to establish the rate of progression. These possible initiations of deterioration include:

(1) Upper tube support plate "G" tube hole blockage in select areas that are only now beginning to show as scale build-up between the tube support plate quatrefoil hole lands and the tube.

(2) Feedwater ring J-tube discharge impingement on the feedring pipe outer diameter surface and/or on the primary separator riser barrels, now observed as only a "washed" areas void of magnetite build-up and having no discernible depth of base material.

(3) J-tube to feedwater ring inner diameter surface joint erosion-corrosion of the feedwater pipe base material, only identified during this outage as possibly starting for the J-tube closest to the feedwater nozzle and "T" section.

(4) Sludge collection on the lower deck plate where washing off is prevented by the lower deck skirt attached at the periphery of the deck; now showing as a uniform sludge depth of approximately 1/16 inch and a few local piles up to ½ inch deep.

3.3.1 Steam Generator 34 Upper Steam Drum Inspections

3.3.1.1 Primary Separator/Swirl Vane Inspection:

The criteria for this engineering assessment was to look for gross misplacement or misalignment, gross cracking of welds, discontinuities of weld surfaces, distinct corrosion or erosion patterns, excessive buildup of deposits, or other anomalous conditions.

Visual inspections of a random selection of primary separators and swirl vane assemblies were performed. The inspection results are reported in the Procedure NSD-FP-1997-7966 data package, and no internal deterioration of the primary separator units was observed. A Westinghouse engineer also viewed the interior of approximately 12 primary separators. He observed that all the primary separator swirl vane assemblies were intact, with the swirl vanes not showing any obvious signs of an erosion-corrosion condition. The swirl vane to riser barrel welds all appeared to be intact and showed no signs of erosion-corrosion attack. The riser barrels to which the swirl vanes are mounted, and the perforated riser barrels above the swirl vanes also appeared to be in good condition, with no obvious signs of initiation of erosion-corrosion of the inner diameter surfaces. The perforated riser barrel holes all appear to still be square edged and show no obvious signs of blockage. With an inspection by touch, the trailing edge of the perforated riser barrels and the leading edge of the primary separator orifice ring (primary separator exit pipe at the mid-deck) were confirmed to still have the original manufactured combination square and beveled cut edge therefore indicating that no erosion-corrosion of these pipe sections is currently taking place. In summary, no deterioration of the primary separators was observed. During the remote inspections of the top tube support plate and AVB assemblies through the primary separators, although the video was not a formal inspection of the primary separator riser barrels, no evidence of deterioration of these riser barrels and swirl vanes and welds, was observed (limited view).

3.3.1.2 Transition Cone to Upper Shell Weld:

The criteria for this assessment are to look for pitting or gross cracks in this circumferential weld seam area. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity.

Westinghouse identified for the inspection team the location of the transition cone to upper shell circumferential weld seam, at approximately six (6) inches above the shell inner diameter surface slope transition. Inspections of this area at six different locations around the shell inner diameter surface did not identify a distinct weld seam. This is understandable because the weld inner diameter surface was ground nearly flush with the surrounding base material, and without surface preparation this surface may not exhibit any visible signs of the weld boundary. It can be concluded that because the inspection

was performed in the correct area, but was unable to visually identify the weld seam, that no large scale pitting or gross cracking in the weld exists.

3.3.1.3 **Secondary Separator Inspection**:

The criteria for this engineering assessment was to look for gross misplacement or misalignment, gross cracking of welds, discontinuities of weld surfaces, distinct corrosion or erosion patterns, excessive buildup of deposits, or other anomalous conditions.

Visual inspections of all eight secondary separator banks were performed The inspection results are reported in the Procedure NSD-FP-1997-7966 data package, and no deterioration of the secondary separator structures was observed. The Westinghouse engineer assessed the external condition of 6 or the 8 secondary separators visually. He observed that all the secondary separator structural welds were intact, with no obvious signs of weld cracking. This included the secondary assembly welds and the welds which attach the perforated plate assemblies to the separator banks (A - H). The secondary separator perforated plates attached to the separator bank entrances all appeared to show no signs of erosion-corrosion attack and the holes remain square cut. The perforated plate holes had very little to no sludge accumulation/blockage. The only exception to this is that the lowermost row of holes on the upper separator banks had initiation of flow hole blockage(~ 10%); this is a lower flow area. An attempt to view the secondary separator demister vanes through the perforated plate holes was difficult, but no internal sludge build-up was observed (limited views available). In summary, no deterioration of the secondary separators was observed.

3.3.1.4 **J-Nozzle and Feedwater Ring Inspection**:

The criteria for this engineering assessment was to look for gross misplacement of misalignment, gross cracking of welds, discontinuities of weld surfaces, distinct corrosion or erosion patterns, excessive buildup of deposits, or other anomalous conditions.

Remote video probe inspection was performed on five selected J-tubes to feedwater ring joint inner diameter surfaces in order to assess the interface condition of the feedring base metal and the J-tube inside edge. Inspection of the two J-tube to feedring joints closest to the feedwater nozzle and "T" section, i.e , J-tubes numbers 1 and 36, was inconclusive. Video inspection of these two J-tube joints indicates possible initiation of erosion-corrosion at these joints. The level of erosion-corrosion, if present, is not significant at this time and should not pose a concern for feedring through-wall wastage for a number of cycles. However, these J-tubes will be re-inspected at a later outage to determine if erosion-corrosion is progressing and at what rate. The other three J-tube to feedring joints inspected, J-tubes numbers 9, 18, and 28, did not show any sign of erosion-corrosion. The joints all have square-cut edges on the feedring inner diameter surface and acceptable fit-ups with the J-tubes. All five J-tubes inspected have square cut leading edges showing no apparent damage to the J-tube material.

All inspected feedwater pipe weld seams internal to the feedring, and inspected by video probe insertion through J-tubes numbered 1 and 36, do not show any signs of deterioration. No weld feedwater ring backing rings were observed (as expected), thus, the potential for loose parts originating from the interior of the feedring is remote. All feedring inner diameter surface pipe welds appear to have a smooth finished look with no signs of significant weld or feedring base metal erosion-corrosion. However, some flow

induced surface scouring patterns were faintly visible in this video tape inspection of the feedring inner diameter surfaces.

Viewed from the outside, the feedring and J-Tubes looked to be in good condition. No J-tubes were found to be loose (as expected) and there were no apparent signs of any flow-induced erosion-corrosion holes through the feedring (as expected). The only observation identified at this time is the effect that the J-tube discharge is having as it impinges the feedring and the primary separator riser barrels. It was observed for some (approximately 30%) of the 36 J-tubes, the discharge flow is impinging on (in a glancing manner) the feedring outer diameter pipe surface. This impingement was distinctly observed for J-tubes numbers 20, 22 and 26. This impingement has washed the local pipe surface clean of all magnetite allowing the flow to directly impinge on the feedring base metal. At this time the smoothed surface of the washed feedring does not appear to have any base material loss. If any material loss due to erosion-corrosion action has occurred, it is estimated to be limited to approximately 1-3 mils depth. By feel (tactile), no erosion-corrosion material loss could be detected on the feedring outer diameter surface.

Other J-tubes' discharge flow appears to be impinging on the primary separator riser barrels. This impingement has washed the local riser barrel pipe surface partially clean of the magnetite coating, allowing the flow to directly impinge on some of the riser barrel base metal. At this time the smoothed surface of the washed riser barrel does not appear to have any base material loss. By feel (tactile), no erosion-corrosion material loss could be detected on the riser barrel outer diameter surfaces.

3.3.1.5 Top Support Plate Ligament Cracking Inspection:

The intent of this engineering assessment was to examine the top tube support plate "G" for evidence of gross cracking or missing segments at certain areas, in particular where the tube support plate is attached to the wrapper adjacent to the wrapper longitudinal seam. The remote video inspection performed was insertion of a video probe down the 25 most outward located primary separator riser barrels around the complete periphery of the mid-deck plate. Of these 25 attempts, 21 probe insertions made it to the top support plate periphery. The other 4 attempts inspected the AVBs only and did not proceed to the tube support plate for concern of jamming the probe. The video quality at the tube support plate was very good.

For the 21 areas inspected, no signs of tube support plate cracking were observed. All tube support plate areas examined showed fully intact quatrefoil tube hole ligaments, there were no missing tube support plate sections, tube support plate surfaces were clean of significant sludge deposits, all machined edges were square and well defined, and the tube holes observed (limited) exhibited no apparent flow blockage. In addition, to the extent inspected, all wrapper to tube support plate supports, i.e., wedge groups and back-up bars (vertical supports) showed no deterioration in the form of crack welds or loose hardware. The only exception to this was an approximate ½" of wedge side weld appeared to have separated from the shell, but the wedge was fully captured by the top weld and tube support plate. This inspection was complimented by the inspection port - top support plate inspections (Procedure NSD-FP-1997-7966 - Section 9.0, also see above) that also resulted in similar observations.

3.3.1.6 AVB Visual Inspection:

The intent of this engineering assessment was to examine the top of the Anti-Vibration Bars (AVBs) for evidence of gross misplacement and missing parts. Quantification of AVB-to-Tube wear or anomalies in the tube bundle are addressed by the eddy current examination. The remote video inspection performed was insertion of a video probe down the 25 most outward located primary separator riser barrels around the complete periphery of the mid-deck plate. Of these 25 attempts, 13 probe insertions made it to the AVBs, the others missed the AVBs and preceded to the top support plate periphery. The video quality at the AVBs was fair to good.

For the 13 areas inspected, there was no evidence of gross misplacement and missing parts. For those portions of the AVBs observed, the AVB assemblies were intact and preceded into the tube bundle with an apparent tight fit-up, and all AVB assemblies were captured by the retaining ring, i.e., all attachment welds were in-place and no cracked welds were observed.

3.3.1.7 Upper Wrapper Support Inspections:

The upper end of the wrapper (near the top support plate, "G") is supported vertically by eight (8) "U" shaped tapered blocks which are welded to the wrapper and bear against the transition cone. These supports allow the wrapper to expand vertically upward relative to the shell. There is no guidance or anti-rotation function associated with these supports.

The intent of this engineering assessment was to examine the upper wrapper support block for evidence of gross misplacement, gross cracking of the weld, and gross cracking of the wrapper in the area of attachment. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. The transition cone will be examined in the area of the block for gross scoring or spalling.

For the eight (8) areas inspected, all upper wrapper "U" shaped tapered blocks were clearly viewed by the inspections video probe with good detail shown. For all 8 tapered support blocks, there was no evidence of gross misalignment, and no evidence of any deterioration of the block or shell bearing surfaces. The backside (wrapper outer diameter side) of the support block welds were observed from the wrapper/shell annulus. These welds appeared to have a straight uniform gap in some cases, to a ragged gap with scale deposits in other cases. However, for all cases, the weld appeared to be the unimproved backside of the root pass of a penetration weld. In all eight case the upper wrapper "U" shaped tapered blocks appeared to be in acceptable condition with no signs of deterioration.

3.3.1.8 Upper Wrapper Support Anti-rotation Keys and Wedges:

The upper end of the wrapper (near the top support plate, "G") has four (4) tapered wedges which bear on anti-rotation keys which are affixed to the steam generator shell. These keys do not permit rotation of the wrapper but allow vertical expansion and contraction of the wrapper relative to the shell.

The intent of this engineering assessment was to examine the upper wrapper anti-rotation wedges for evidence of gross misplacement, gross cracking of the weld, and gross

cracking of the wrapper in the area of attachment. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. The transition cone was examined in the area of the key for gross cracking of the weld or gross deformation of the key.

For the four (4) areas inspected, all upper wrapper wedges which bear on anti-rotation keys were clearly viewed by the inspections video probe with good detail shown. For all 4 wedges, there was no evidence of gross misalignment, and no evidence of any deterioration of the wedge or shell anti-rotation keys. The backside (wrapper outer diameter side) of the support wedge block welds were observed from the wrapper/shell annulus. This weld appeared to have a straight uniform gap in some cases, to a ragged gap with scale deposits in other cases. However, for all cases, the weld appeared to be the unimproved backside of the root pass of a penetration weld. In all four cases the upper wrapper wedges appeared to be in acceptable condition with no signs of deterioration. The transition cone has been examined in the area of the keys and no gross cracking of the weld or gross deformation of the key was observed.

3.3.1.9 Lower Wrapper Support Keys:

The lower end of the wrapper (nearest the first support plate above the flow distribution baffle) is supported vertically by six (6) - 12 inch long blocks which are welded to the wrapper and bear against the shell via two - 2.25 inch diameter jacking studs. A 1.75 inch thick horizontally oriented key on the shell fits into a groove in these blocks, fixing the wrapper vertically. There is no anti-rotation function associated with these supports.

The intent of this engineering assessment was to examine the lower wrapper support block for evidence of gross misplacement, gross cracking of the weld, and gross cracking of the wrapper in the area of attachment. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. The shell was examined in the area of the block for gross deformation of the key. The inspection was performed by lowering a video probe down through the shell-wrapper annulus.

This inspection covered all six (6) of the lower wrapper support keys. It showed that there appears to be no evidence of gross misplacement or gross deformation of these support assemblies. All wrapper jacking bolts observed, were in good condition and remain in contact with the shell indicating that the wrapper-to-support block junctions have not deformed. No cracks in the wrapper plate around the support blocks [1] were observed (best effort basis). Viewing of the wrapper plate was limited and partially obscured by the weld backing bar (360° around the support block). In addition, all six of the shell keys were observed to be in-place and properly positioned in the wrapper blocks. The shell key welds (to the shell pressure boundary) were intact in all cases, with no deformation and no cracks observed in these welds.

[1] The 44F steam generator has round lower support blocks; the blocks in some foreign plants reporting initiation of cracking from the corners are rectangular.

3.3.1.10 **Wrapper Weld Seam**:

Three separate attempts were made by to find and identify the wrapper vertical weld seam. This was an informational gathering inspection to collect data for an engineering assessment of the secondary side structural condition, including erosion, corrosion, and structural weld integrity. This weld seam could not be distinctly identified in either of four anticipated locations, approximately 15° to either side and either end of the tubelane. During each of the inspection attempts, the remote observers were unable to visually identify this weld seam, which is likely to have been ground smooth[2] to the wrapper outer diameter surface and obscured by the magnetite film on the wrapper. However, by the process of searching for the wrapper weld seam, no observation was made of any gross cracking or pitting of the wrapper outer diameter that could be indicative of the possible loss of integrity present in this weld seam.

4.0 CONDITION MONITORING AND OPERATIONAL ASSESSMENT

Draft Regulatory Guide X.XX, "Steam Generator Tube Integrity", states that "each holder of an operating license .....shall develop and implement a program that provides reasonable assurance that pressurized water reactor (PWR) steam generator (SG) tubes remain capable of fulfilling their intended safety functions". The safety function of the steam generator tubing includes the ability to maintain reactor coolant inventory and pressure, as well as service as a medium for heat transfer to ensure the capability to shutdown the reactor.

The program strategy begins with the steam generator tube NDE following plant shutdown. Tube NDE is followed by assessments of tube integrity performance relative to currently accepted performance criteria provided in draft Regulatory Guide X.XX, to draft Regulatory Guide 1.121, PWR Steam Generator Tube Plugging Limits. Tube integrity performance is subject to two different types of assessments in the proposed Regulatory Guide; a condition monitoring assessment, which is a "backward looking" assessment intended to confirm that adequate tube integrity has been maintained since the last inspection, and an operational assessment, which is a "forward looking" assessment intended to demonstrate reasonable assurance that the tube integrity performance criteria will be met throughout the next operating cycle until the next scheduled tube inspection.

This evaluation presents a condition monitoring and operational assessment of the Indian Point Unit 3 steam generator tubing structural and leakage integrity conditions for the observed end of cycle (EOC) 09 condition, the recently completed cycle, as well as for the expected EOC 10 condition. By establishing EOC 09 structural and leakage integrity conditions, projected EOC 10 conditions can be assessed, based on planned operational cycle lengths, efficacy of the EOC 09 inspections performed, and Cycle 10 operational conditions. Results of these assessments can be used to establish steam generator tube intended safety functions as suggested by draft RG X.XX.

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[2] Foreign plants reporting wrapper weld seam cracking have a "U" shaped channel which was used to secure the seam together. The 44F wrapper has a full penetration weld where the rolled wrapper joins.

EOC 09 eddy current and secondary side visual inspections are used to establish the structural and leakage integrity conditions of the Indian Point Unit 3 steam generator tubing for EOC 09 as well as overall tube bundle integrity issues raised by NRC Information Notice 96-09 and supplement. Scope and results of these inspections are provided in appropriate sections of this report. The results of these inspections are used to establish the expected structural and leakage integrity conditions of the Indian Point Unit 3 SG tubing at EOC 10.

4.1 Cycle 9 Condition Monitoring Assessment

As suggested by draft RG X.XX, STEAM Generator Tube Integrity, the condition monitoring assessment is "backward Looking", and is intended to establish the structural and leakage integrity characteristics of the SG tube at the end of the operating cycle, against the current minimum NRC performance criteria These performance criteria include burst capability of 3 times the normal operating condition pressure differential for freespan indications and leakage integrity such that the current licensing basis remains valid. Establishment of these conditions is provided using the eddy current testing results, in-situ testing results (if performed), and any other tube integrity evaluations for detected flaws

4.1.1 Development of Limiting Axial and Circumferential Flaw In-situ Testing Screening Parameters for Indian Point Unit 3

Prior to the EOC 09 outage, axial and circumferential flow screening parameters were developed specifically for Indian Point Unit 3 using lower tolerance limit (LTL) material properties for 7/8" OD x 0.050" wall thickness thermally treated Alloy 690 tube material at a bounding normal operating condition pressure value of 1480 psi. While in-situ testing was not performed in the Spring 1997 outage, these values remain valid for future evaluations up to a pressure differential of 1480 psi across the steam generator tubes.

Axial Indications:

The first in-situ screening parameter threshold for pressure testing of axial indications in the straight leg freespan region and U-bend regions, developed for Indian Point 3 is 0.43". This model assumes the flaw is throughwall (TW) over the entire reported length. Even though the Indian Point Unit 3 replacement steam generator low row U-bends received a supplemental thermal treatment following bending, the material properties in the U-bend regions are expected to be slightly higher than the straight leg region. The axial length based limits for the U-bends at Indian Point Unit 3 are conservatively calculated using straight leg material properties, and are therefore, conservative. Axial indications would subsequently be screened based on peak depth and average depth as a function of the total flow length. The peak depth screen uses the uniform flaw depth for a 1.5" long flaw as the screening parameter. As axial flaws typically contain localized areas with significantly deeper flaw penetration compared to the average flaw depth, this screen eliminates such flaws. The final screen provides specific average depth structural limits for a specific flaw length, extending from the uniform TW flaw limiting length to a flaw length such that the limiting average depth becomes independent of the total flaw length. Indications, which do not exceed all, three of the screening parameters are judged not to represent a burst potential less than 3 times the normal operating condition primary to secondary pressure differential.

Leakage screening of axial indications is performed using indicated maximum voltage, maximum depth, and depth exceeding the leakage threshold of 80% throughwall over a minimum axial length. The parameters are based on an assessment of recorded voltages of leaking and non-leaking tubes and on threshold TW lengths required to support a leakage potential.

Circumferential Indications:

Circumferential indications are similarly screened to provide burst integrity of 3 times normal operating pressure differential and to provide a likelihood of SLB leakage potential. Using the latest EPRI burst correlation for circumferential indications, a single, throughwall circumferential flaw angle of 256° is established for Indian Point Unit 3. Circumferential indications are subsequently screened based on the average voltage taken from the multiscan mode (voltage integral) and percent degraded area (PDA).

Leakage screening of circumferential indications is similarly performed as for axial indications in that the maximum voltage threshold, maximum depth and minimum length to support leakage at the maximum depth threshold must be provided in order to represent a leakage potential.

4.1.2 Condition Monitoring Assessment based on EOC 09 Eddy Current Results

As stated previously, no active tube degradation mechanism indications were detected in the Spring1997 eddy current inspection of SGs 33 and 34. The scope of the inspection far exceeded the Technical Specification requirements and is virtually in line with EPRI's inspection scope guidelines for specific tube locations such as the top of tubesheet and low Row U-bend region. As stated previously, a number of non-reportable signals were noted by the production analysts. These signals were subsequently determined not flaw-like. MBM signals were also noted and determined not to be flaw-like. Several dent or ding signals were detected by bobbin inspection. These signals were determined to be manufacturing related and were found to exist in prior or baseline inspection data.

SGs 33 and 34 were last inspected at EOC 08 (March 1992). The extensive bobbin inspection in 1997 indicates that with a high degree of confidence, no degradation has occurred since the last eddy current inspection in 1992. Since no tube degradation was found, tube integrity recommendations were satisfied at EOC 09.

At the EOC 10 inspection, eddy current inspection will be performed in SGs 31 and 32.

4.1.3 Steam Generator 33 and 34 Secondary Side Visual Inspection

The results of the steam generator 33 and 34 secondary side visual inspections indicated that no evidence of sludge buildup on the quatrefoil hole design tube support plates was observed.

In SG 34, no evidence of wrapper lower support block degradation or wrapper structural degradation was noted. Sludge lancing was performed in all four steam generators. A total of 223 lbs. of sludge were removed. The total removed sludge weights, combined with the TSP visual inspection indicates that sludge deposition in the upper bundle region or the top of tubesheet is not occurring at a rapid rate.

4.2 Cycle 10 Operational Assessment

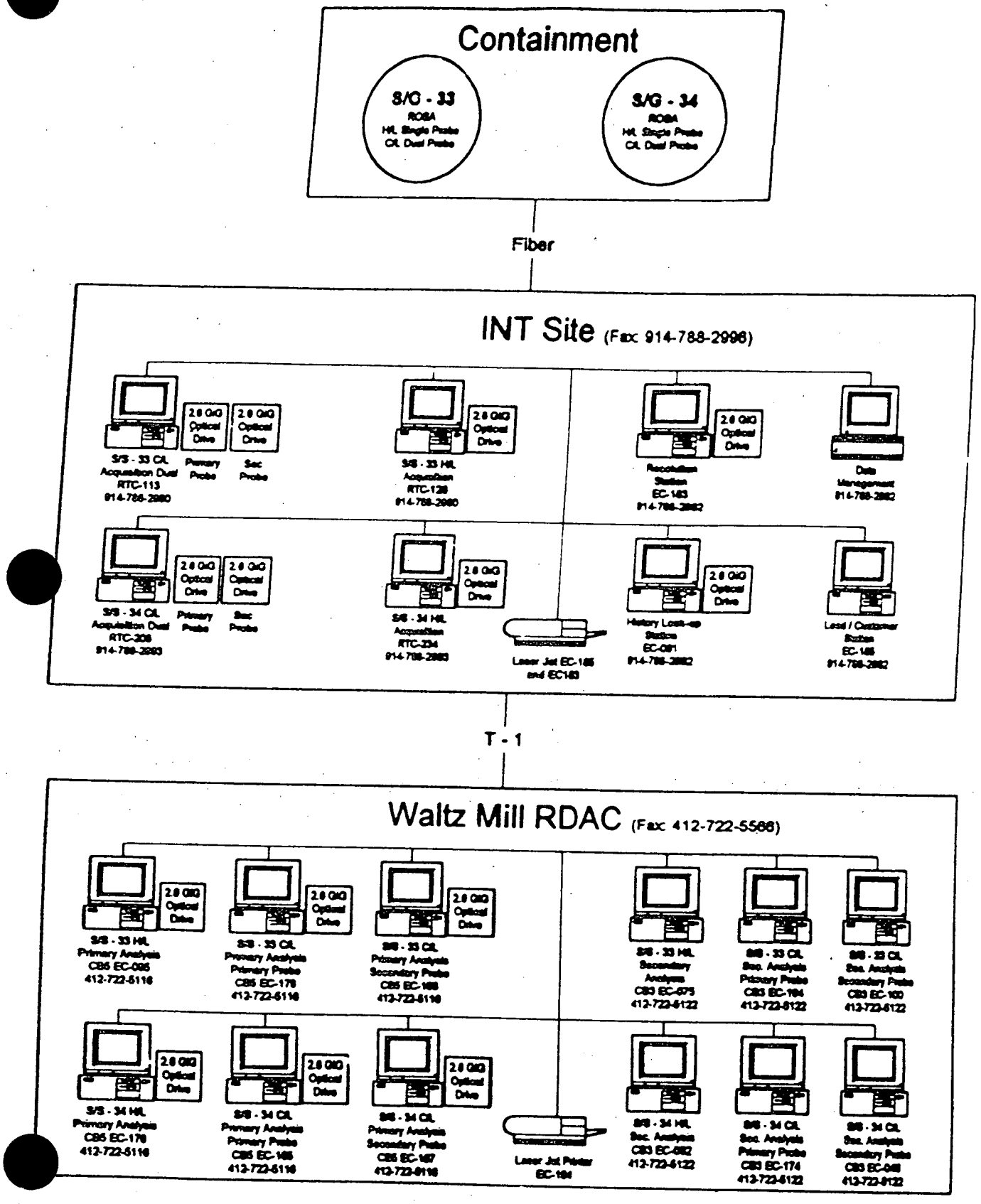
The expected condition of the Indian Point Unit 3 steam generator tubing at EOC 10 can be expected to be entirely consistent with the EOC 09 inspection results, that is, individual tube structural and leakage integrity will be maintained.

Several factors influence this judgment. First, the historical performance of thermally treated Alloy 600 tubing material in replacement steam generators has indicated little evidence of stress corrosion degradation in nearly 17 calendar years of operational experience. The Indian Point Unit 3 tubing (thermally treated Alloy 690) is expected to perform similarly as or better than other replacements, which use Alloy 600 thermally treated tubing. Second, the reactor vessel outlet temperature at Indian Point Unit 3 of approximately 600.4° is several degrees less than other plants with similar replacement steam generators which have operated since 1980 with no evidence of tube degradation. As PWSCC is particularly dependent upon temperature, no instances of PWSCC are expected at the next inspection of steam generators 33 and 34. Visual examination of the secondary sides of SGs 33 and 34 indicated no scale buildup on the tube OD surfaces and tube ODSCC due to elevated contaminant levels in secondary side sludge or scale is unlikely. The quatrefoil tube hole design limits the potential for corrosive elements to collect in the tube to tube support plate crevice. The TSP material, stainless steel, prevents the progression of tube deformation due to denting. In the EOC 08 inspections, 20% of all four steam generators were inspected. The inspection results from SGs 33 and 34 at EOC 09 indicate that the extended non-operational period from 1993 to 1996 did not have an adverse impact upon the overall maintenance of steam generator structural or leakage integrity. SGs 31 and 32 will be inspected at EOC 10 after two successive cycles of operation and approximately 3 EFPY prior to the last inspection. In conclusion, inspection results for steam generators 31 and 32 supporting tube structural and leakage integrity are expected to be entirely consistent with the inspection results for steam generators 33 and 34 from the Spring 1997 outage.

ATTACHMENT 1

FIGURES

Figure 2.3.1 Generalized Schematic of Indian Point 3 Analysis Network



INT-33 BOBBIN INSPECTION PROGRAM

COLD LEG REVISION 0
Indiun Point 3 R09 INT-33 SERIES 44F

06-27-1997 16:24 HRS. SUPERTUBIN

ACTS # INT-01-197
X : 1966 TEST FULL LENGTH

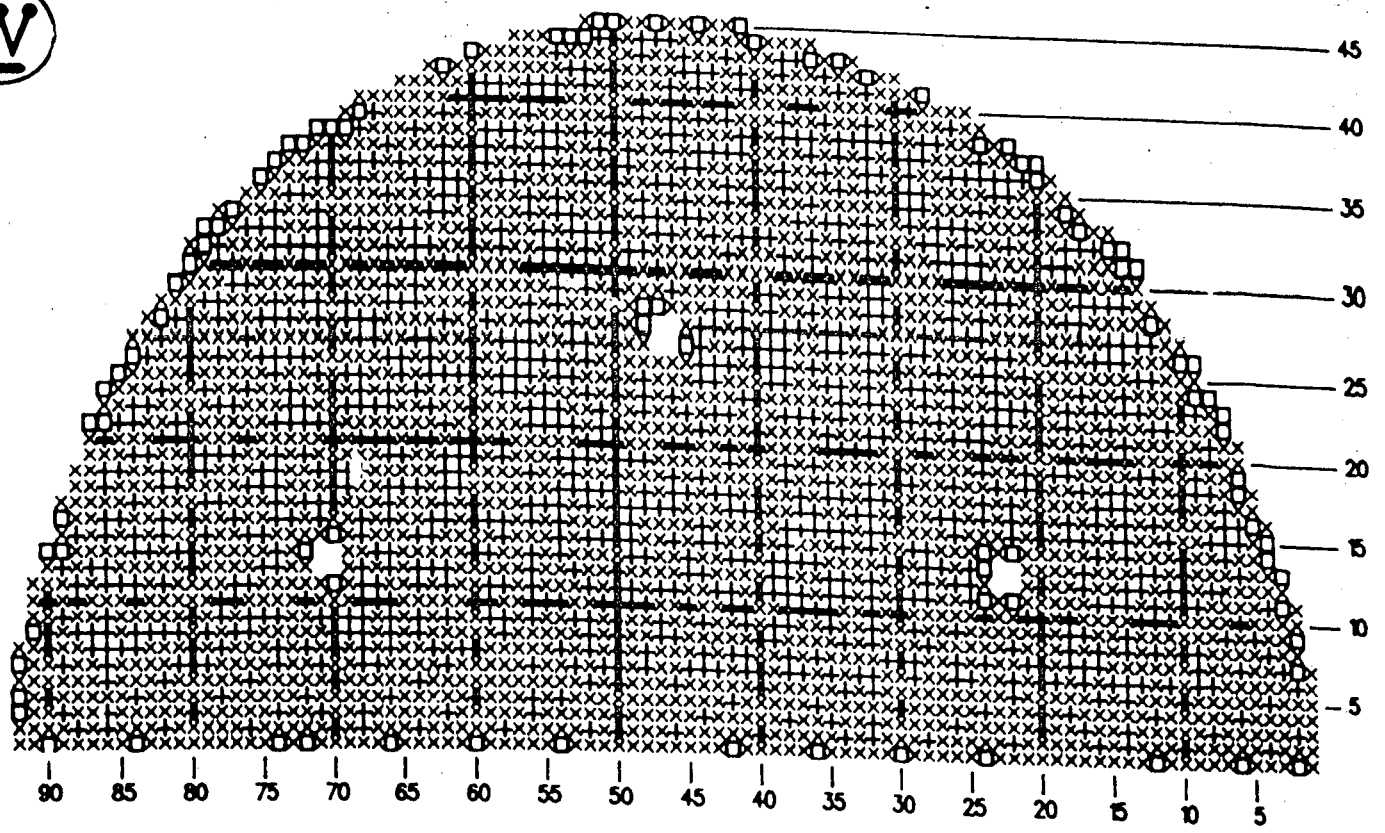


Figure 2.3.2, Steam Generator 33 Bobbin Inspection Program

INT-33 HOT LEG TOP OF TUBESHEET PROGRAM

REVISION 0

Indian Point 3 R09 INT-33 SERIES 44F

06-27-1997 12:37 HRS. SUPERTUBIN

ACTS # INT-02-197

X .: 643 TEST TSH -3 / +2 INCHES

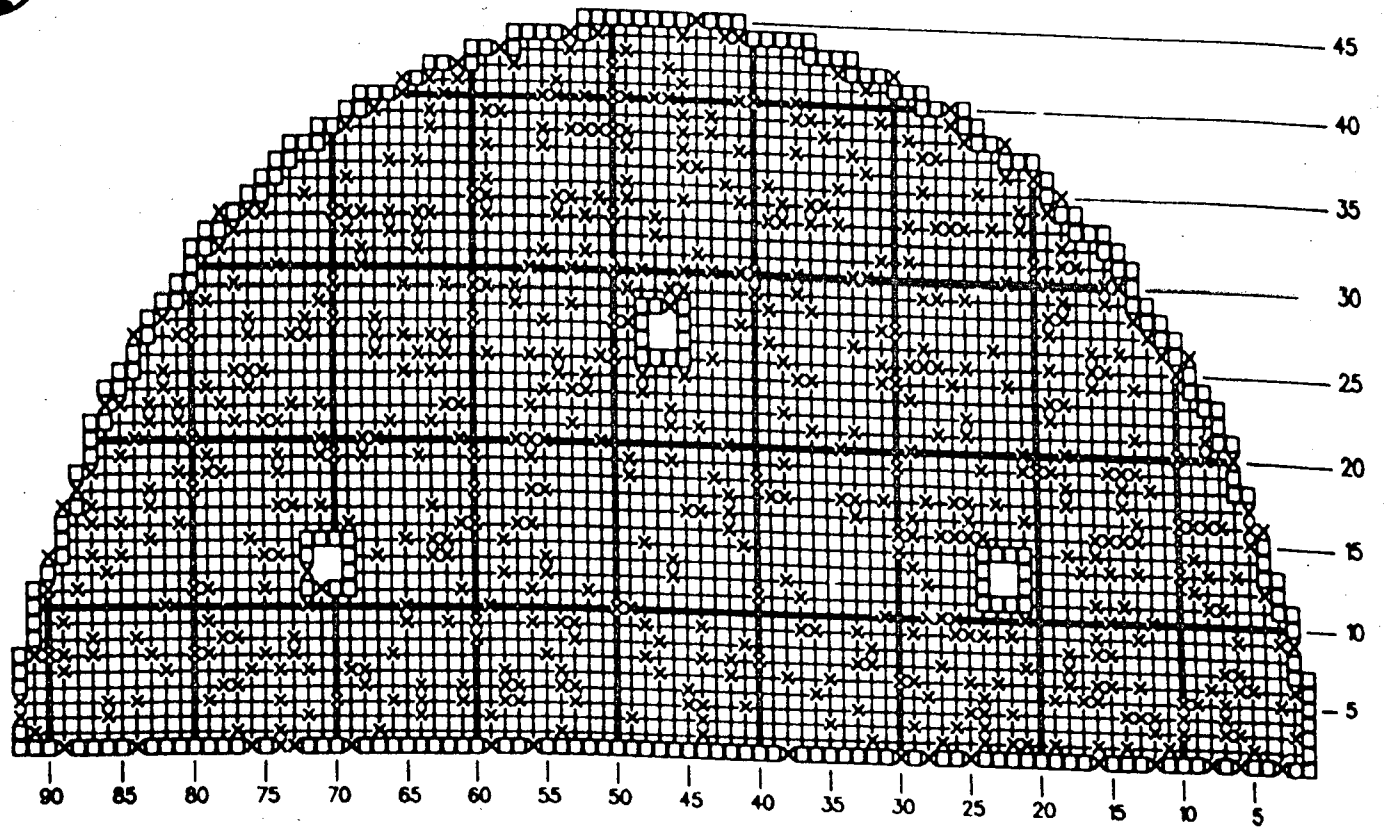


Figure 2.3.3-Steam Generator 33 Hot Leg Top of Tubesheet +Point Program

INT-33 U-BEND +POINT RPC PROGRAM

HOT LEG REVISION 0

Indian Point 3 R09 INT-33 SERIES 44F

06-27-1997 12:39 HRS. SUPERTUBIN

ACTS # INT-05-197

X : 37 TEST 6C THROUGH 6H

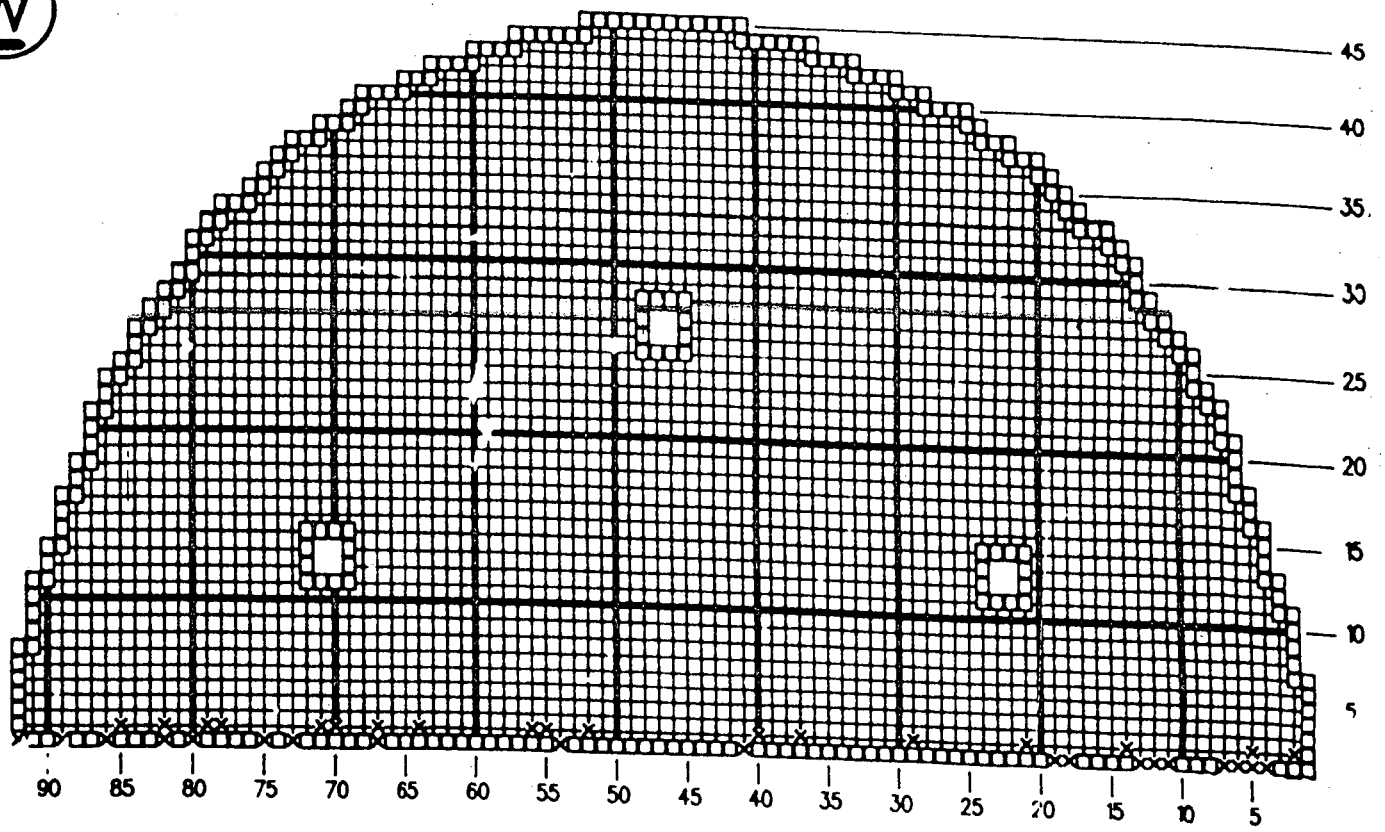


Figure 2.3.4, Steam Generator 33 U-Bend +Point RPC Program

INT-34 BOBBIN INSPECTION PROGRAM

COLD LEG REVISION 0
Indian Point 3 R09 INT-34 SERIES 44F

06-28-1997 15:32 HRS. SUPERTUBIN

ACTS # INT-01-197
X : 2065 TEST FULL LENGTH
□ : 2 PLUGGED TUBE

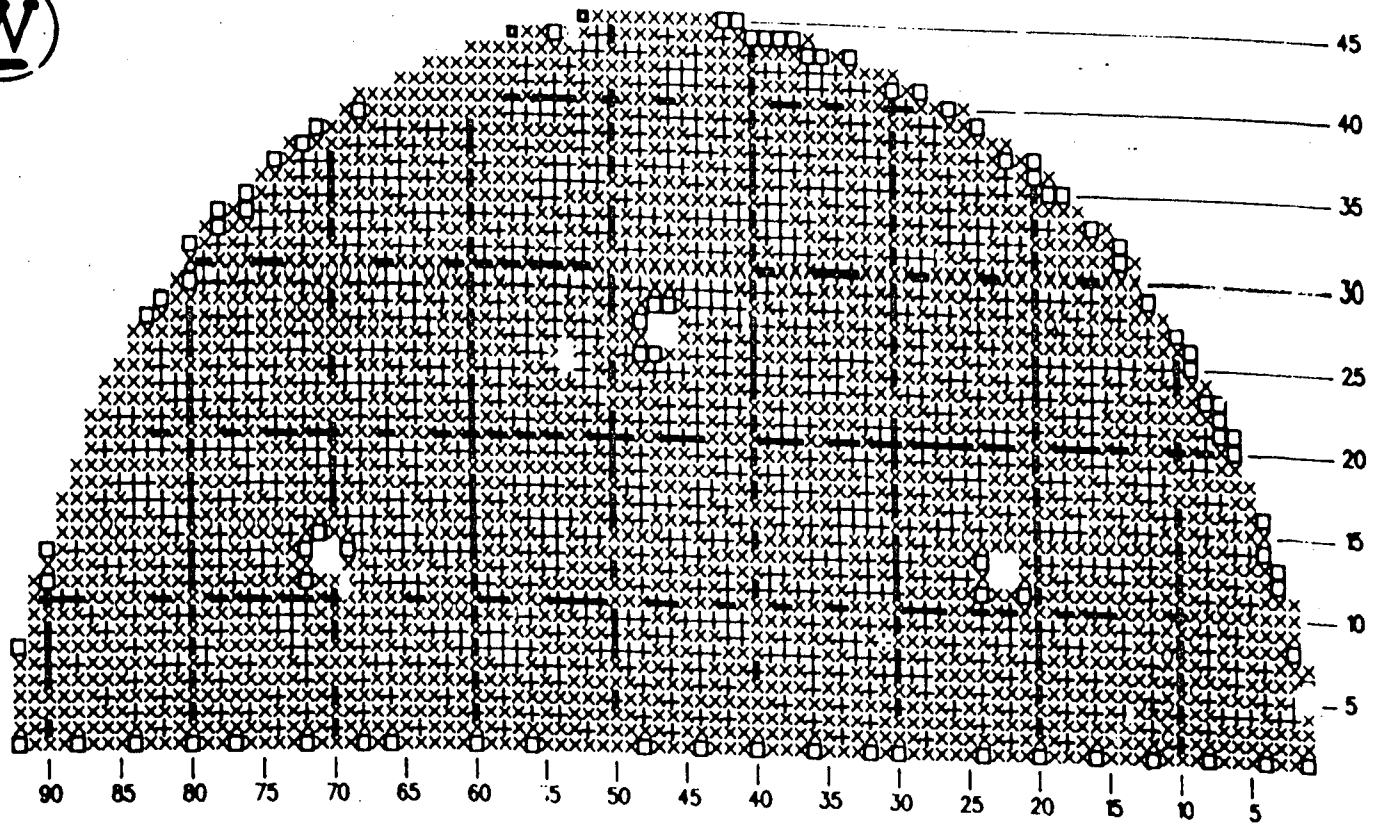


Figure 2.3.5, Steam Generator 34 Bobbin Inspection Program

INT-34 ; HOT LEG TOP OF TUBESHEET PROGRAM
REVISION 1
Indian Point 3 R09 INT-34 SERIES 44F
06-27-1997 14:51 HRS. SUPERTUBIN

ACTS # INT-02-197

X : 643 TEST TSH -3 / +2 INCHES

\ : 38 TUBE ADDED TO PROGRAM TO ENCOMPASS POSSIBLE LOOSE PART TEST TSH -3 / +2 INCHES

▫ : 2 PLUGGED TUBE

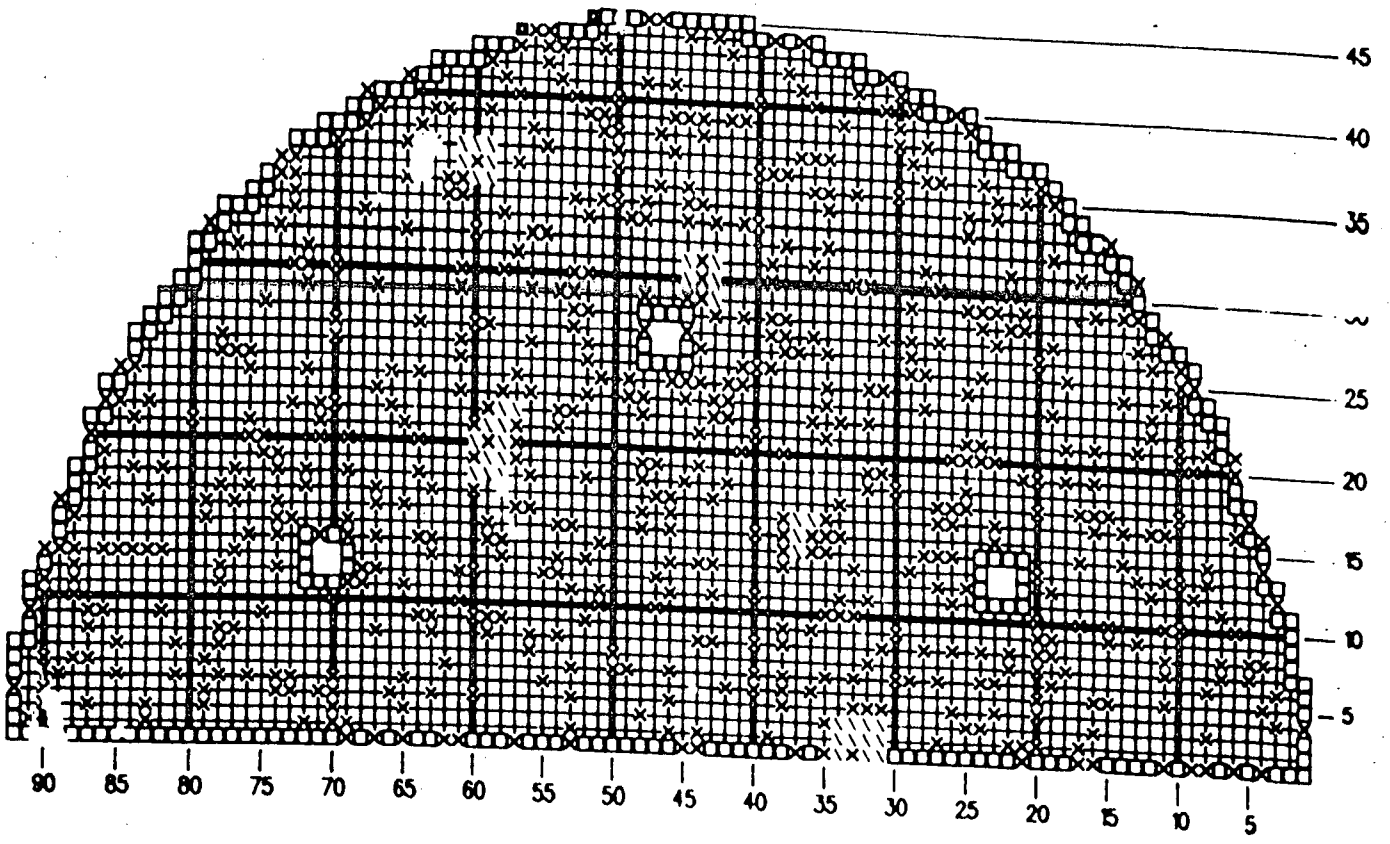


Figure 2.3.6, Steam Generator 34 Hot Leg Top-of-Tubesheet +Point Program

INT-34 U-BEND +POINT RPC PROGRAM

HOT LEG REVISION 0

Indian Point 3 R09 INT-34 SERIES 44F

06-27-1997 14:58 HRS. SUPERTUBIN

ACTS # INT-05-197

X : 37 TEST 6C THROUGH 6H

□ : 2 PLUGGED TUBE

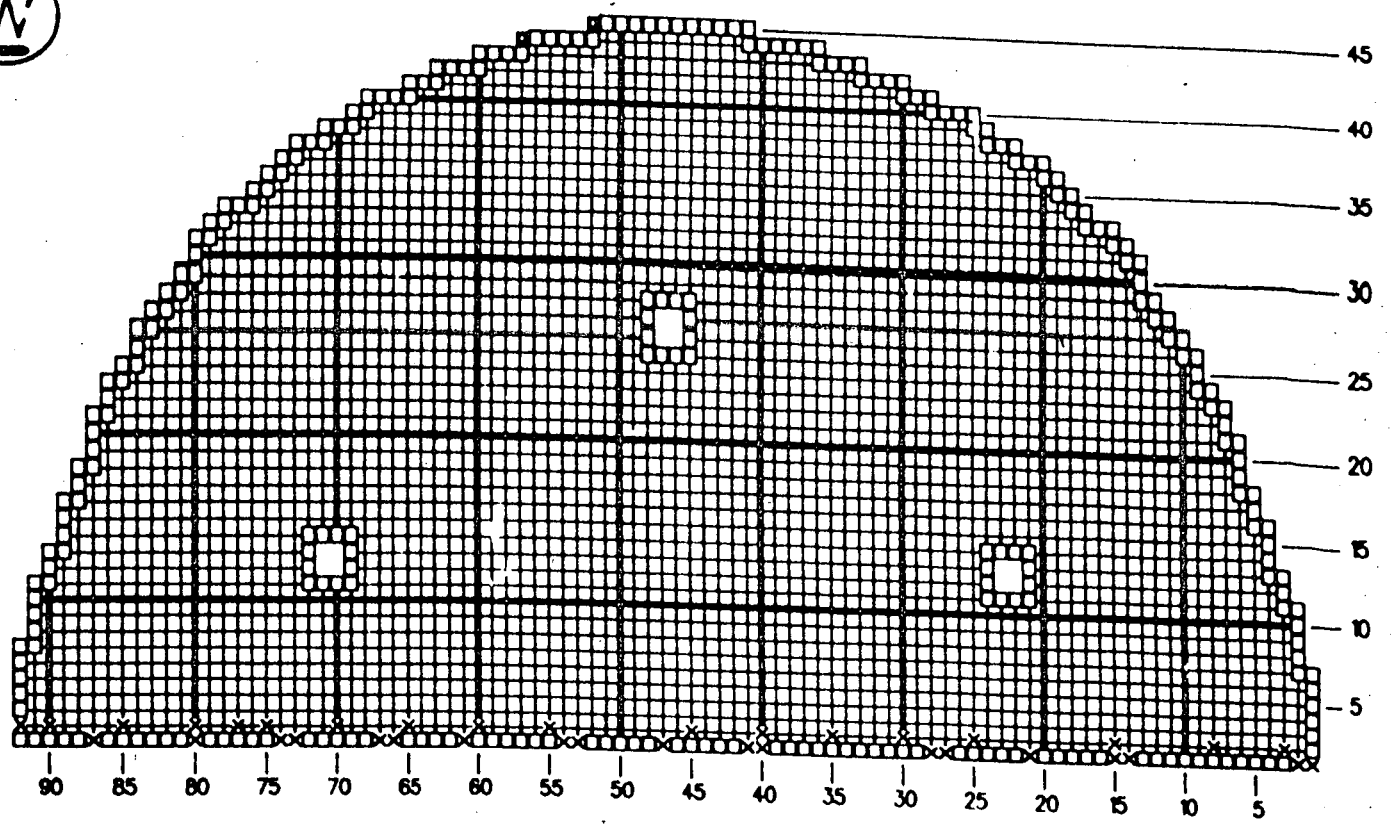


Figure 2.3.7, Steam Generator 34 U-Bend +Point RPC Program

INT-34 HOT LEG DENT +POINT PROGRAM

Indian Point 3 R09 INT-34 SERIES 44F

06-28-1997 15:49 HRS. SUPERTUBIN

6 : 5 TEST 6H +/- 2"

◘ : 2 PLUGGED TUB

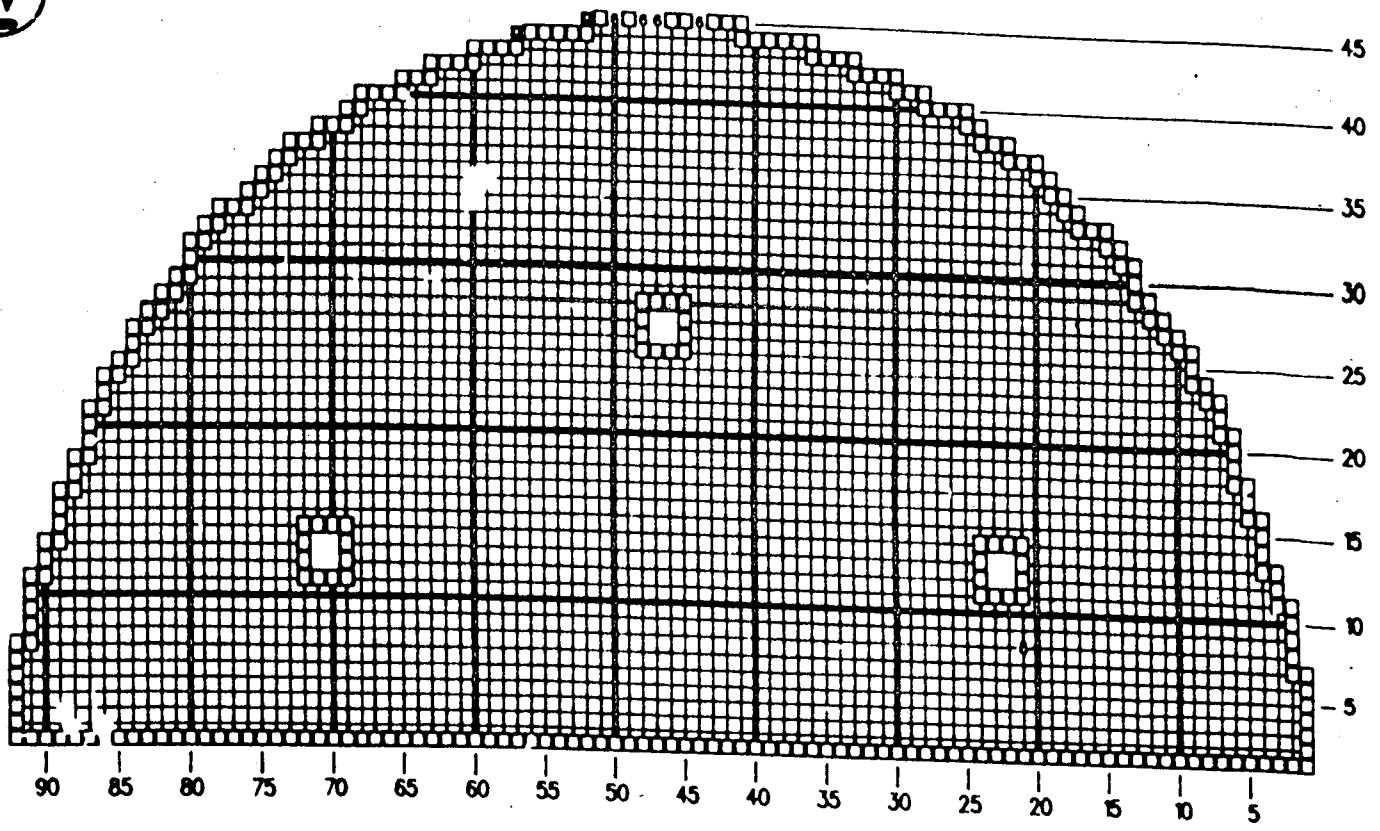


Figure 2.3.8, Steam Generator 34 Hot Leg +Point Dent Inspection Program

INT-34 COLD LEG DENT +POINT PROGRAM

Indiun Point 3 R09 INT-34 SERIES 44F

06-28-1997 15:50 HRS. SUPERTUBIN

6 : 2 TEST 6C +/-2 INCHES

5 : 26 TEST 5C +/- 2 INCHES

□ : 2 PLUGGED TUBE

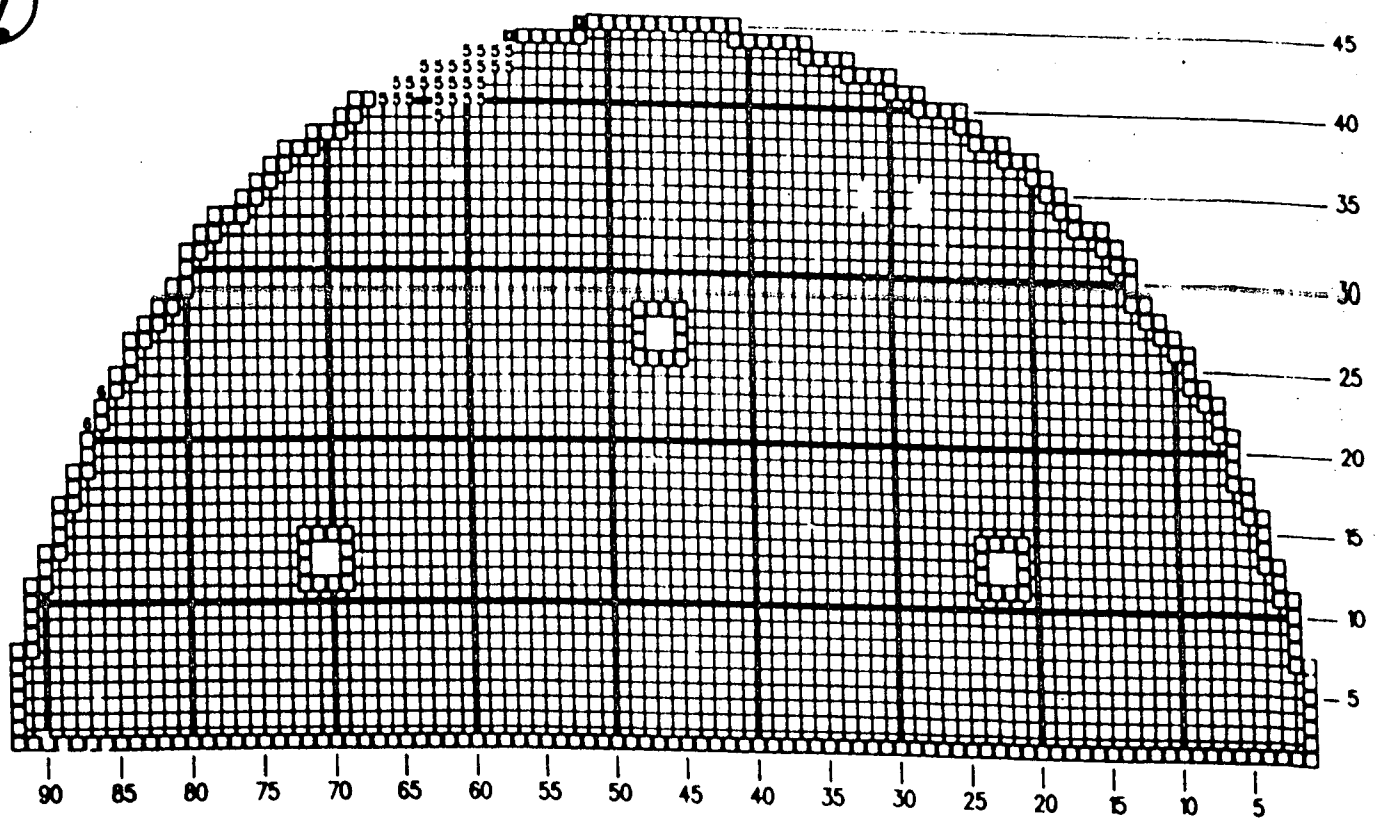


Figure 2.3.10, Steam Generator 3-4 Cold Leg +Point Dent Inspection Program

INT-34 POST FOSAR LOOSE PART PROGRAM

HOT LEG
Indian Point 3 R09 INT-34 SERIES 44F

06-28-1997 15:52 HRS. SUPERTUBIN

ACTS #INT--02-197
X : 4 TEST TSH -3/+2"
□ : 2 PLUGGED TUBE

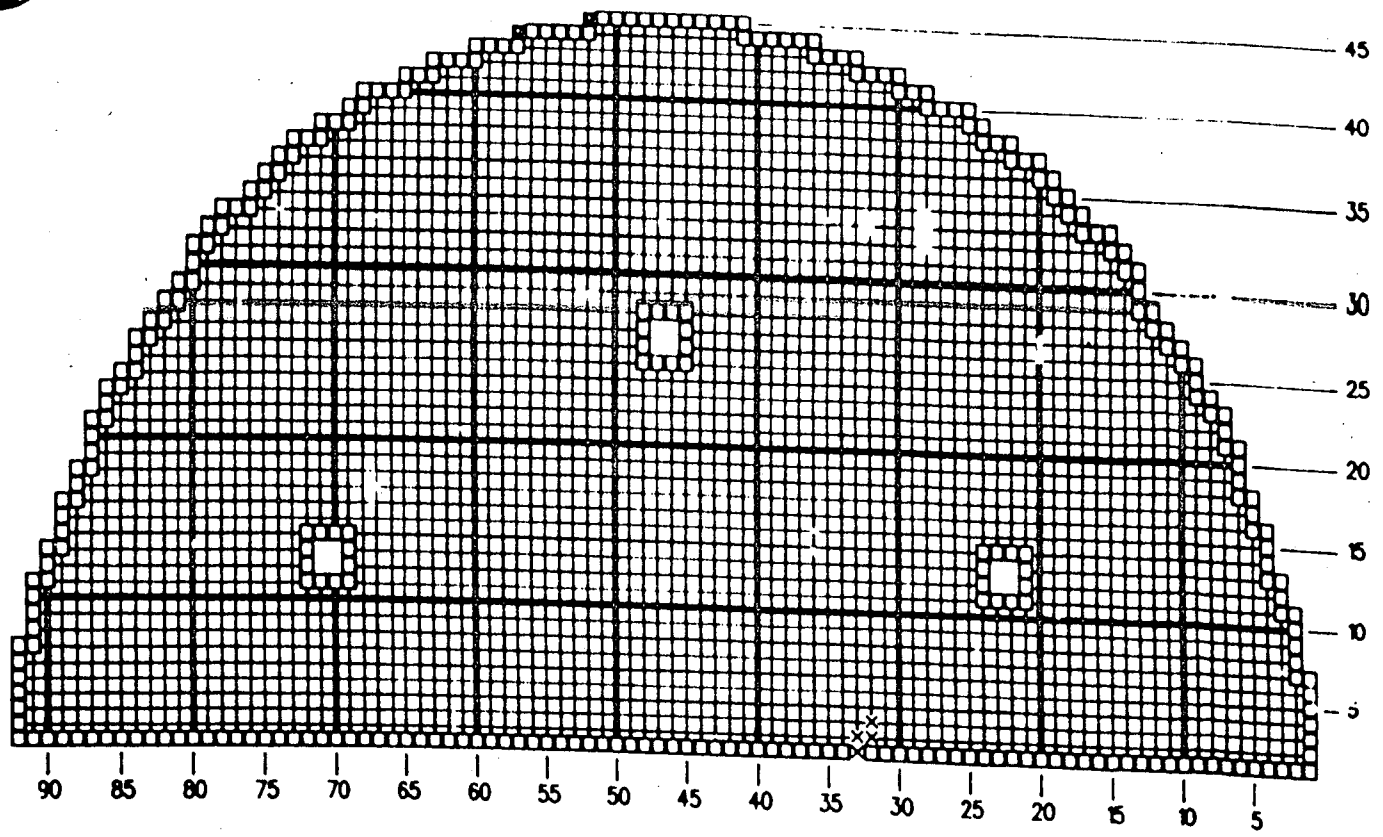


Figure 2.3.11, Steam Generator 34 Hot Leg +Point Post FOSAR Program

INT-34 POSSIBLE LOOSE PARTS

× : 10 TUBE WITH POSSIBLE LOOSE PART

◘ : 2 PLUGGED TUBE

Indian Point 3 R09 INT-34 SERIES 44F

06-28-1997 16:28 HRS. SUPER1 3IN

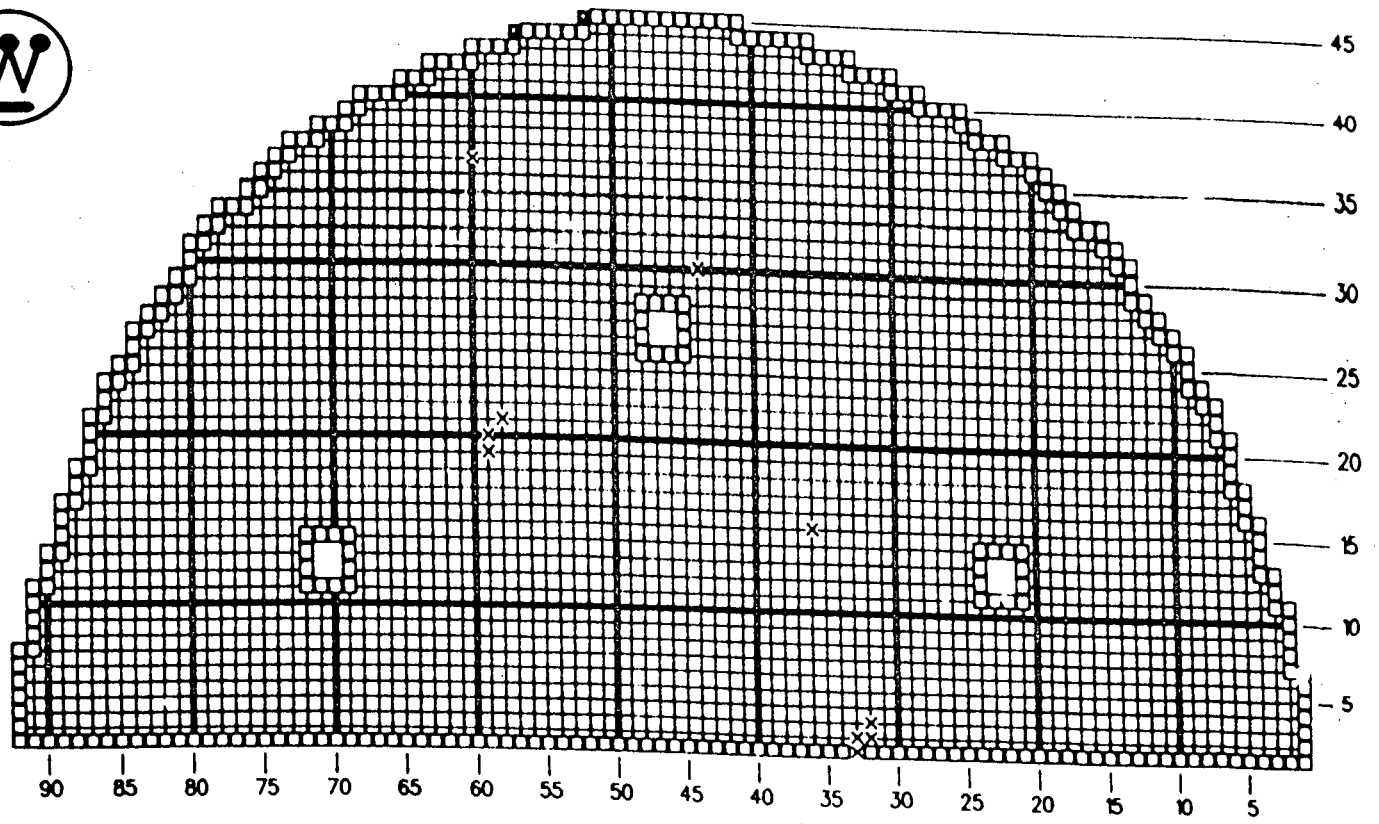


Figure 2.3.12-Tubesheet Map Showing Eddy Current Identification of Potential Loose Parts

ATTACHMENT 2

USER'S GUIDE AND LETTER CODES

INDICATION LISTING – STEAM GENERATOR 33

INDICATION LISTING – STEAM GENERATOR 34

USER'S GUIDE AND LETTER CODES

The following explains the format of the data as displayed in the Supertubin Report hard copies.

ROW and COL (COLUMN)

Tube identifier numbers - an X-Y coordinate system.

CE-B - COMPLETED BEGIN TEST

Tube location where the test actually began.

CE-E - COMPLETED END TEST

Tube location where the test actually ended.

PROBE

Diameter of probe used for the test.

TYPE

Characters representing the type of probe used. See the table in this report for probe descriptors used for this inspection.

IND - INDICATION

Character codes and numerics that represent the analysis results of the data for the tube. Please refererence the Analysis Guidelines for three letter code descriptions.

LOCN - LOCATION

The location in the tube where the indication is referenced from.

INCH1

Distance in inches above or below the location where the indication is referenced from.

INCH2

Typically the distance above or below INCH1 that a particular indication extends, such as a permeability variation extending along a length of a tube.

CHAN - CHANNEL

Describes the data channel used in reporting the indication.

VOLTS

The voltage reported by the analyst as referenced to a standard.

DEG - DEGREES

The angle of the indication as reported by the analyst.

TAPE

The data set where the raw eddy current data was collected to.

COMMENTS

Additional remarks which enhance the information contained in the other fields of the record.

LOCATION TERMS DESCRIPTION

Please reference the Analysis Guidelines for descriptions of locations referenced during this inspection.

Table Of Probes Used This Inspection

Probe	Designator	ACTS Reference
EL720LLMC Bobbin	720-EL	INT-01-197
ZP720115+PT36S80 RPC	720-ZP	INT-02-197
EF680BJFM'JF Bobbin	680-EF	INT-04-197
ZU680+PTMRPCFH	680-ZU	INT-05-197
ZB72u115+PT36S80	720-ZB	INT-06-197

9.5 Bobbin Coil Codes

A. ADR - "Absolute Drift Response" Used when the analyst detects a positive "Y" and negative "X" component on an absolute OD mix elimination signal. Considered an unquantifiable signal flagged for future monitoring. Has been determined under laboratory examination of S/G tube samples to signify a possible "IGA" condition; however, it is not confined to such a phenomenon. Requires location and range if applicable and channel. GRAPHICS PLOT REQUIRED

B. ANF - "Anomaly Not Found" Used by an analyst when a previously reported anomaly cannot be located within 0.50" of the previously called anomaly.

C. ANR - "Anomaly Not Reportable" Used by an analyst when a previously reported anomaly does not meet the present reporting criteria.

D. BDA - "Bad Data" requires retest.

E. BLG - "Bulged" tube Requires location, volts, phase angle, and channel.

F. CUD - Indicates the presence of "Copper" deposits. Requires location and range if applicable, volts, phase angle and channel.

G. DNG - Localized tube deformation on the free span tubing. 3

H. DNT - Indicates "Dent" in the tubing. This is a service induced tube deformation coincident with support plate, tubesheet, AVB, etc. 3

I. DI - Indicates "Distorted Indication" to be used in lieu of a percent (%) through wall value on a signal that is reportable but too distorted to quantify. Further clarification with RPC is required.

This code is only used instead of NQI, DSI, and DTI if site specifics requires. This code is changed to DIN if subsequent RPC test does not confirm. GRAPHICS PLOT REQUIRED.

J. DRI - Indicates a Distorted Roll Transition Indication". This is a special case "I-code" used to define suspect roll transitions occurring at the top of tubesheet, or in partially expanded tubes near the tube end. This indication is too distorted to quantify but is reportable and requires RPC for further clarification. This code is changed to DRN if subsequent RPC test does not confirm the indication. GRAPHICS PLOT REQUIRED.

K. DSI - Indicates "Distorted Support Indication" - An I-code used in lieu of a (%) through wall value on a signal located within or extending out from a support structure which is reportable but too distorted to quantity. This indication requires RPC for further clarification. This code is changed to DSN if subsequent RPC does not confirm the indication. GRAPHICS PLOT REQUIRED

L. DTI - Indicates "Distorted Tubesheet Indication" - I-code used in lieu of a (%) through wall value on a signal starting within 0.5" of the top of tubesheet and extending out from or down into the tubesheet which the analyst believes to be an indication but too distorted to quantify. This indication is too distorted to quantify but reportable and requires RPC for further clarification. This code is changed to DTN if subsequent RPC does not confirm the indication. GRAPHICS PLOT REQUIRED.

M. FSD - Free Span Differential Signal which behaves like a flaw. This signal should be addressed by review of previous history.

N. FSI - Free Span Indication indicates a signal with a meaningful change from history or which did not exist in history or historical data is considered to have poor signal-to-noise correlation. This indication is treated the same as all other I-codes in the database and requires RPC for further clarification. This code is changed to

FSN if subsequent RPC does not confirm the indication. GRAPHICS PLOT REQUIRED.

O. INF - Indicates "Indication Not Found". Used by an analyst when a previously reported indication cannot be detected within 0.50" of the previously reported indication.

P. INR - Indicates "Indication Not Reportable". Similar to "INF" except signal is present; however, current analysis results do not meet pre-established guidelines on signal reporting.

Q. LAR - "Lead Analyst Review"

R. MBI - Indicates "Manufacturing Buff Mark Indication". This code indicates change since preservice data. This indication is treated the same as all I-Codes in the data base and requires RPC for further clarification. This code is changed to MBN if subsequent RPC does not confirm the indication. GRAPHICS PLOT REQUIRED.

S. MBM - Indicates "Manufacturing Buff Mark". Reference Appendix B for suggested disposition techniques.

T. MMB - Indicates "Multiple Manufacturing Buff Marks", usually over a range. Reference Appendix B for suggested disposition techniques.

U. NDD - "No Detectable Degradation".

V. NQI - Indicates "Non Quantifiable Indication" - An I-code used in lieu of a (%) through wall value on a signal located in free span area of the tube which is reportable but too distorted to quantify. This indication is treated the same as all other I-codes in the database and requires RPC for further clarification. This code is changed to NQN if subsequent RPC does not confirm the indication. GRAPHICS PLOT REQUIRED.

W. NT - "NO TEST"

X. NTE - "No Tubesheet Expansion"

Y. PDS -"Pilger Drift Signal" - A drift in the absolute signals that occur at random elevations and generally only in one leg of a tube. These signals have been determined to be a result of the tube pilgering process (stopping the process) that results in a minor change in the tube ID (approximately 1 to 1.5 mils on the diameter) and thus a change in the tube wall thickness when the OD is surface ground. The signals always show an increase in the wall thickness (negative drift) but may exhibit a positive drift (thinner wall) at the offset of the signal. The signals are always long from several inches to several feet, depending on how long it takes the pilger process to return to the nominal ID. These signals are only addressed at baseline.

Z. PI - "Possible Indication" - Possible AVB or wear indication that requires to be retested with a wear standard in line.

aa. PID - "Positive ID Established". GRAPHICS PLOT REQUIRED

bb. PLG - "Plugged Tube"

cc. PLP - "Possible Loose Part"

dd. PTE - "Partial Tube Expansion"

ee. PVN - Indicates the presence of a "Permeability Variation". Requires location, and range if applicable, volts, phase angle and channel.

ff. RST - "Restricted Tube"

gg. SCM - "See Comment"

hh. SLG - Indicates "Sludge". Used in measuring or quantifying deposits which lie on the O.D. of the tubing.

ii. SPA - Indicates "Shot Peen Anomaly". Located either at start point or throughout shot peened region. This region is typically from inside tubesheet to about 3 inches above tubesheet. Signal resembles a bulge but rotates closer to the flaw plane on differential channels.

jj. TIU - Indicates "Tube ID Uncertain". The tube will be retested for ID verification.

kk. TTH - " \Transition to High"

ll. TTL - "Transition to Low"

mm. UDS - Indicates "Undefinable Signal". To be used when an analyst detects a signal that cannot be classified as tube degradation, however, it is recommended that during future examinations this particular signal should be monitored. Can best be described as a means of establishing a data base on unclassifiable signals to better understand their meaning from future analysis. GRAPHICS PLOT REQUIRED.

10.0 GENERAL ROTATING PROBE GUIDELINES

This section will address the basic setups, evaluation, and reporting criteria for rotating probes. Specific instructions and additional requirements for a particular rotating probe type can be found in the ANTS Sheet.

10.1 Types of Rotating Probes & Coils

The following coil types for rotating probes currently exist in the industry today and are commonly used in industry today:

A. .080" midrange pancake coil

10.5.2 The graphics plots shall include one page containing an isometric plot of the most suitable channel (and coil) which shows the indication most clearly along with the corresponding lissajous window showing the largest or clearest representative lissajous signal with properly placed measurement dots.

10.5.3 The Overall Lead Analyst shall designate any additional graphics requirements as needed.

10.6 Letter Codes (RPC)

The following letter codes apply to crack-like indications only.

A. SCI - "Single Circumferentially Oriented Indication" This term is to be used when the isometric plot depicts a crack-like indication whose axial extent is usually less than its circumferential extent. This type of indication is normally located within transition areas or dented support plate edges.

B. MCI - "Multiple Circumferentially Oriented Indications" Same definition as SCI except more than one SCI is present. Requires LIG measurements.

C. SAI - "Single Axial Indication" When displayed in an isometric plot, this indication will usually have an axial extent which is greater than its circumferential extent. This indication may be found immediately adjacent to transitions (or dents) and may run into or through the transition (or dent), in free length tubing, e.g., in sludge pile areas, as well as in small radius u-bends.

D. MAI - "Multiple Axial Indications" Same definition as SAI except more than one SAI except more than one SAI is present. Requires LIG measurements.

E. LIG - "Ligament" Used as an additional measurement where multiple crack-like indications are present in the same axial location are called. "LIG" denotes the "clean" space between the indications. LIG is measured in circumferential degrees and extends from null return of one indication to null departure of the immediately adjacent indication. All ligaments must be measured and in combination with the indications, should total approximately 360 degrees when all circumferential degree measurements are added.

F. PIT - A localized corrosion attack on the tubing related to oxygen ingress through continuous condenser inleakage and the presence of copper on the secondary side.

G. VOL - Volumetric indication that can be associated with thinning, manufacturing or service induced. This indication will present approximate amplitude response from the 3-coil RPC. This signal will normally present a shallow and large amplitude response from the bobbin coil.

Other letter codes which may be used with RPC are:

H. BDA - "Bad Data"

I. DEP - Deposit(s)

J. DNG - Localized tube deformation on the free span tubing.

K. DNT - Indicates "Dent" in the tubing. This is a service induced tube deformation coincident with support plate, tubesheet, AVB, etc. 3

L. MBM - "Manufacturing Buff Mark"

M. NDD - "No Detectable Degradation"

N. NT - "No Test"

O. PID - "Positive I.D."

P. PLP - "Possible Loose Part"

Q. PVN - "Permeability Variation"

R. RST - "Restricted"

S. SCM - "See Comment"

T. TIU - "Tube I.D. Uncertain"

U. UDS - "Undefinable Signal" This indication is used to identify a signal which the analyst cannot characterize as a crack-like indication but believes should be brought to the attention of the utility and Overall Lead Analyst for further discussion and a potential decision to either continue calling and track on subsequent inspections, investigate further by other techniques (e.g., UT or tube pull), and/or repair actions on the basis of conservatism.

INDICATION LISTING – STEAM GENERATOR 33

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	2	1	6C	TEC	720-EL	ANF	TSC	.00	.00	M1			14	RESULT OF LAR
	2	1												RESULT OF BASELINE DATA REVIEW
88-Nov	2	1	TEH	TEC	720-ED	BLG	TSC	.00	.00	2	791.52	72	59	
	2	6	6H	TEH	720-EL	ANF	TSH	.00	.00	2			25	RESULT OF LAR
	2	6												RESULT OF BASELINE DATA REVIEW
88-Nov	2	6	6H	TEH	740-EC	BLG	TSH	.00	.00	2	790.94	50	65	
	21	6	TEH	TEC	720-EL	INR	2H	28.92	.00	6			8	
88-Nov	21	6	TEH	TEC	740-ED	MBM	2H	28.90	.00	6	.60	113	45	
	2	7	6H	TEH	720-EL	ANF	TSH	.06	.00	M1			25	RESULT OF LAR
	2	7												RESULT OF BASELINE DATA REVIEW
92-May	2	7	6H	TEH	720-ZM	RST	UB	.00	.00	1			10	
92-May	2	7	6C	SH	700-ZS	NOD				1			11	
88-Nov	2	7	6H	TEH	740-EC	BLG	TSH	.00	.00	2	791.90	56	65	
	22	8	TEH	TEC	720-EL	ANR	1H	40.66	.00	1			10	
88-Nov	22	8	TEH	TEC	740-ED	DNT	1H	40.81	.00	M1	3.43	186	42	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	8												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	3	10	6C	TEC	720-EL	INR	3C	13.16	.00	6			14	
[illegible]v	3	10	TEH	TEC	720-ED	MBM	3C	13.17	.00	6	.52	86	59	RESULT OF DISCREPANCY RESOLUTION
	7	12	TEH	TEC	720-EL	ANF	4C	33.70	.00	1			12	RESULT OF LAR
	7	12												RESULT OF BASELINE DATA REVIEW
	7	12	TEH	TEC	720-EL	ANF	4C	33.71	.00	1			16	RESULT OF DISCREPANCY RESOLUTION
90-Sep	7	12	TEC	TEH	720-EB	NOD				1			9	
88-Nov	7	12	TEH	TEC	740-EC	DNT	4C	33.70	.00	M1	3.22	181	63	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	21	12	TEH	TEC	720-EL	ANR	3H	47.72	.00	1			10	
88-Nov	21	12	TEH	TEC	740-ED	DNT	3H	48.23	.00	M1	4.44	183	45	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	1	13	6H	TEH	720-EL	INR	BPH	4.19	.00	6			25	
88-Nov	1	13	6H	TEH	740-ED	MBM	BPH	4.19	.00	5	.51	66	54	
88-Nov	1	13	6H	5C	720-ED	NOD				1			62	
	2	13	6H	TEH	720-EL	INR	3H	10.03	.00	6			25	
92-May	2	13	6H	TEH	740-ZM	NOD				1			1	
88-Nov	2	13	6H	TEH	740-EC	MBM	3H	10.02	.00	5	.41	65	65	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	22	16	TEH	TEC	720-EL	INR	1C	47.41	.00	6			6	
88-Nov	22	16	TEH	TEC	740-ED	MBM	1C	47.40	.00	6	.44	83	42	RESULT OF DISCREPANCY RESOLUTION
	32	19	TEH	TEC	720-EL	INR	BPC	17.15	.00	6			40	RESULT OF DISCREPANCY RESOLUTION
88-Nov	32	19	TEH	TEC	740-ED	MBM	BPC	17.60	.00	6	.44	68	28	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	35	20	TEH	TEC	720-EL	INR	4H	48.44	.00	6			12	
88-Nov	35	20	TEH	TEC	740-ED	MBM	4H	48.01	.00	6	.41	66	34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	35	20												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	14	21	TEH	TEC	720-EL	INR	5H	2.64	.00	6			2	RESULT OF DISCREPANCY RESOLUTION
88-Nov	14	21	TEH	TEC	740-ED	MBM	5H	2.69	.00	6	.40	95	55	
	20	21	TEH	TEC	720-EL	INR	3H	28.43	.00	6			2	RESULT OF DISCREPANCY RESOLUTION
88-Nov	20	21	TEH	TEC	740-ED	MBM	3H	28.66	.00	6	.58	106	50	RESULT OF DISCREPANCY RESOLUTION
	10	22	TEH	TEC	720-EL	INR	TSH	14.06	.00	6			2	RESULT OF DISCREPANCY RESOLUTION
88-Nov	10	22	TEH	TEC	740-ED	MBM	TSH	14.15	.00	6	.54	92	16	RESULT OF DISCREPANCY RESOLUTION
	34	22	TEH	TEC	720-EL	INR	3H	30.17	.00	6			12	RESULT OF DISCREPANCY RESOLUTION
88-Nov	34	22	TEH	TEC	740-ED	MBM	3H	30.27	.00	6	.46	95	32	RESULT OF DISCREPANCY RESOLUTION
	28	25	TEH	TEC	720-EL	INR	4H	26.73	.00	6			12	RESULT OF DISCREPANCY RESOLUTION
88-Nov	28	25	TEH	TEC	740-ED	MBM	4H	26.73	.00	6	.72	99	36	
	37	25	TEH	TEC	720-EL	ANR	3H	48.33	.00	M1			12	RESULT OF DISCREPANCY RESOLUTION
88-Nov	37	25	TEH	TEC	740-ED	DNT	3H	48.23	.00	M1	3.39	185	22	
	9	27	TEH	TEC	720-EL	ANF	3H	46.55	.00	1			12	RESULT OF DISCREPANCY RESOLUTION
	9	27	TEH	TEC	720-EL	ANR	3H	40.95	.00	M1			12	RESULT OF DISCREPANCY RESOLUTION
88-Nov	9	27	TEH	TEC	740-ED	DNT	3H	46.56	.00	M1	4.17	188	16	RESULT OF DISCREPANCY RESOLUTION
	23	27	TEH	TEC	720-EL	ANR	3H	18.23	.00	1			14	
88-Nov	23	27	TEH	TEC	740-ED	DNT	3H	18.33	.00	M1	4.76	189	42	RESULT OF DISCREPANCY RESOLUTION
	30	28	TEH	TEC	720-EL	INR	1H	19.75	.00	6			18	
88-Nov	30	28	TEH	TEC	740-ED	MBM	1H	19.75	.00	6	.49	256	37	
	29	29	TEH	TEC	720-EL	INR	2H	8.44	.00	6			6	
88-Nov	29	29	TEH	TEC	740-ED	MBM	2H	8.46	.00	6	.51	102	36	
	36	30	TEH	TEC	720-EL	INR	1C	7.76	.00	6			16	
88-Nov	36	30	TEH	TEC	740-ED	MBM	1C	8.18	.00	6	.40	252	20	
	8	31	TEH	TEC	720-EL	INR	1H	43.12	.00	6			16	
88-Nov	8	31	TEH	TEC	740-ED	MBM	1H	42.85	.00	6	.46	91	13	
	11	31	TEH	TEC	720-EL	ANR	BPC	7.47	.00	1			16	
88-Nov	11	31	TEH	TEC	740-ED	DNT	BPC	7.63	.00	M1	3.48	3	52	
	34	31	TEH	TEC	720-EL	INR	2C	26.69	.00	6			16	
88-Nov	34	31	TEH	TEC	740-ED	MBM	2C	26.78	.00	6	.49	107	32	
	42	31	TEH	TEC	720-EL	INR	1C	23.28	.00	6			18	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	42	31	TEH	TEC	740-ED	MBM	1C	23.28	.00	6	.40	115	18	
	7	33	TEH	TEC	720-EL	DNG	6H	4.25	.00	1	5.38	188	42	RESULT OF DISCREPANCY RESOLUTION
	7	33												RESULT OF BASELINE DATA REVIEW
	41	33	TEH	TEC	720-EL	INR	AV1	10.15	.00	6			16	
88-Nov	41	33	TEH	TEC	740-ED	MBM	AV1	10.14	.00	6	.48	80	18	RESULT OF DISCREPANCY RESOLUTION
	12	36	TEH	TEC	720-EL	INR	4H	45.70	.00	6			40	
88-Nov	12	36	TEH	TEC	740-ED	MBM	4H	45.88	.00	6	.44	57	40	RESULT OF DISCREPANCY RESOLUTION
	20	37	TEH	TEC	720-EL	FSD	1C	7.18	.00	3	.29	26	24	RESULT OF DISCREPANCY RESOLUTION
	20	37												RESULT OF BASELINE DATA REVIEW
	20	38	TEH	TEC	720-EL	MBM	3H	35.55	.00	6	2.06	89	24	RESULT OF DISCREPANCY RESOLUTION
88-Nov	20	38	TEH	TEC	740-ED	MBM	3H	35.50	.00	6	.61	85	23	RESULT OF BASELINE DATA REVIEW
	32	38	TEH	TEC	720-EL	INR	2C	5.76	.00	6			16	
88-Nov	32	38	TEH	TEC	740-ED	MBM	2C	5.78	.00	6	.47	83	28	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	40	38	TEH	TEC	720-EL	ANR	3H	22.00	.00	1			16	
	40	38	TEH	TEC	720-EL	INR	AV6	21.00	.00	6			16	
[illegible]	40	38	TEH	TEC	740-ED	DNT	3H	21.82	.00	M1	6.49	185	24	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
[illegible]	40	38	TEH	TEC	740-ED	MBM	AV6	21.07	.00	6	.55	84	24	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	7	40	TEH	TEC	720-EL	ANR	4H	8.03	.00	1			46	RESULT OF DISCREPANCY RESOLUTION
88-Nov	7	40	TEH	TEC	740-ED	DNT	4H	8.03	.00	M1	3.38	190	13	RESULT OF DISCREPANCY RESOLUTION
	13	40	TEH	TEC	720-EL	FSD	TSH	12.85	244.00	3	.29	85	26	RESULT OF DISCREPANCY RESOLUTION
	13	40												RESULT OF BASELINE DATA REVIEW
	30	40	TEH	TEC	720-EL	ANR	4H	41.93	.00	1			20	
88-Nov	30	40	TEH	TEC	740-ED	DNT	4H	41.93	.00	M1	4.26	190	37	RESULT OF DISCREPANCY RESOLUTION
	22	41	TEH	TEC	720-EL	INR	BPC	1.72	.00	6			24	
	22	41	TEH	TEC	720-EL	INR	TSC	20.08	.00	6			24	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	41	TEH	1C	740-ED	INC				1			50	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	41												RETEST - TEST FROM 1CL TO TEC
88-Nov	22	41	TEH	1C	740-ED	MBM	BPC	1.74	.00	6	.41	69	50	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	41												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	22	41	TEH	1C	740-ED	MBM	TSC	20.08	.00	6	.46	75	50	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	41												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	22	41		2C	TEC	720-ED	MBM	BPC	1.74	.00	6	.41	69	62 RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	29	41	TEH	TEC	720-EL	ANR	AV1	4.06	.00	1			24	
88-Nov	29	41	TEH	TEC	740-ED	DNT	AV1	4.25	.00	M1	3.21	188	39	RESULT OF DISCREPANCY RESOLUTION
88-Nov	29	41												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	30	42	TEH	TEC	720-EL	INR	4H	27.43	.00	6			20	RESULT OF DISCREPANCY RESOLUTION
88-Nov	30	42	TEH	TEC	740-ED	MBM	4H	27.38	.00	6	.81	91	37	RESULT OF DISCREPANCY RESOLUTION
	38	42	TEH	TEC	720-EL	FSD	1H	49.08	.00	3	.65	91	20	RESULT OF BASELINE DATA REVIEW
88-Nov	38	42	TEH	TEC	740-ED	MBM	1H	48.98	.00	6	.42	76	24	RESULT OF DISCREPANCY RESOLUTION
88-Nov	38	42												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	42	42	TEH	TEC	720-EL	INR	3H	49.27	.00	6			16	RESULT OF DISCREPANCY RESOLUTION
88-Nov	42	42	TEH	TEC	740-ED	MBM	3H	49.02	.00	6	.57	99	20	
	33	43	TEH	TEC	720-EL	INR	TSH	14.75	.00	6			20	RESULT OF DISCREPANCY RESOLUTION
88-Nov	33	43	TEH	TEC	740-ED	MBM	TSH	14.94	.00	6	.83	93	6	RESULT OF DISCREPANCY RESOLUTION
	38	43	TEH	TEC	720-EL	INR	4H	3.45	.00	6			20	
88-Nov	38	43	TEH	TEC	740-ED	MBM	4H	3.02	.00	6	.47	73	24	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	32	44	TEH	TEC	720-EL	INR	BPC	17.15	.00	6			22	
88-Nov	32	44	TEH	TEC	740-ED	MBM	BPC	17.16	.00	6	.42	75	6	RESULT OF DISCREPANCY RESOLUTION
	15	45	TEH	TEC	720-EL	ANR	1H	30.03	.00	1			24	RESULT OF LAR
	15	45												RESULT OF BASELINE DATA REVIEW
May	15	45	TEC	TEH	740-ZM	NOD				1			4	
ov	15	45	TEH	TEC	740-ED	DNT	1H	30.48	.00	M1	3.54	185	35	RESULT OF DISCREPANCY RESOLUTION
	33	46	TEH	TEC	720-EL	INR	BPH	12.73	.00	6			16	
88-Nov	33	46	TEH	TEC	740-ED	MBM	BPH	12.83	.00	6	.42	97	6	RESULT OF DISCREPANCY RESOLUTION
	4	48	TEH	TEC	720-EL	ANR	[illegible]	25.16	.00	M1			46	
90-Sep	4	48	6H	TEH	740-EB	NOD				1			11	
90-Sep	4	48	5C	TEH	680-EB	NOD				1			12	
90-Sep	4	48	4C	TEC	740-EB	NOD				1			16	
90-Sep	4	48	6C	TEC	700-EC	NOD				1			17	
88-Nov	4	48	TEH	TEC	740-ED	DNT	4H	25.15	.00	M1	3.23	185	9	RESULT OF DISCREPANCY RESOLUTION
88-Nov	4	48												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	8	48	TEH	TEC	720-EL	INR	TSC	14.65	.00	6			46	RESULT OF DISCREPANCY RESOLUTION
88-Nov	8	48	TEH	TEC	740-ED	MBM	TSC	14.65	.00	6	.40	105	53	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	15	48	TEH	TEC	720-EL	ANR	TSC	-.12	.00	M1			40	RESULT OF LAR
	15	48												RESULT OF BASELINE DATA REVIEW
88-Nov	15	48	TEH	TEC	740-ED	BLG	TSC	.00	.00	2	792.61	55	35	
	20	48	TEH	TEC	720-EL	INR	3C	40.42	.00	6			24	
88-Nov	20	48	TEH	TEC	740-ED	MBM	3C	40.42	.00	6	.49	278	23	RESULT OF DISCREPANCY RESOLUTION
	29	49	TEH	TEC	720-EL	INR	BPC	4.00	.00	6			20	RESULT OF DISCREPANCY RESOLUTION
88-Nov	29	49	TEH	TEC	740-ED	MBM	BPC	3.52	9.69	6	.48	284	37	RESULT OF DISCREPANCY RESOLUTION

| DATE | ROW | COL | CEB | CEE | PROBE | IND | LOC | INCH1 | INCH2 | CHAN | VOLTS | DEG | TAPE | COMMENTS |

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	29	49												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	3	51	6H	TEH	720-EL	INR	2H	4.12	.00	5			23	
92-May	3	51	6H	TEH	740-ZM	NDD				1			9	
88-Nov	3	51	TEH	TEC	720-ED	MBM	2H	4.12	.00	6	.69	97	59	RESULT OF DISCREPANCY RESOLUTION
	8	54	TEH	TEC	720-EL	INR	3H	25.85	.00	6			44	
88-Nov	8	54	TEH	TEC	740-ED	MBM	3H	26.00	.00	6	.53	88	46	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	32	54	TEH	TEC	720-EL	ANR	BPC	26.88	.00	M1			28	RESULT OF DISCREPANCY RESOLUTION
88-Nov	32	54	TEH	TEC	740-ED	DNT	BPC	26.80	.00	M1	6.23	183	10	
	1	55	6C	TEC	720-EL	INR	3C	31.38	.00	6			40	
92-May	1	55	6H	TEH	720-ZM	RST	UB	.00	.00	1			10	
92-May	1	55	6C	5H	700-ZS	NDD				1			11	
88-Nov	1	55	6C	TEC	740-ED	MBM	3C	31.51	.00	6	.40	267	53	
88-Nov	1	55	6H	5C	720-ED	NDD				1			62	
	17	56	TEH	TEC	720-EL	ANR	TEH	6.56	.00	2			32	
88-Nov	17	56	TEH	TEC	740-ED	BLG	TEH	6.56	.00	2	793.01	54	25	
	27	58	TEH	TEC	720-EL	ANR	5C	26.92	.00	M1			28	RESULT OF DISCREPANCY RESOLUTION
May	27	58	TEC	TEH	740-ZM	NDD				1			6	
ep	27	58	TEC	TEH	740-EB	NDD				1			13	
Nov	27	58	TEH	TEC	740-ED	DNT	5C	26.90	.00	M1	4.96	188	12	RESULT OF DISCREPANCY RESOLUTION
	4	59	TEH	TEC	720-EL	ANR	3C	48.59	.00	M1			42	
88-Nov	4	59	TEH	TEC	740-ED	DNT	3C	48.55	.00	M1	3.01	180	9	RESULT OF DISCREPANCY RESOLUTION
	16	59	TEH	TEC	720-EL	MBM	1H	36.66	.00	6	3.28	24	34	RESULT OF DISCREPANCY RESOLUTION
	16	59												RESULT OF BASELINE DATA REVIEW
	1	61	6C	TEC	720-EL	MBM	1C	6.30	.00	6	2.16	84	40	RESULT OF BASELINE DATA REVIEW
88-Nov	1	61	6C	TEC	740-ED	MBM	1C	5.76	.00	6	.68	92	53	
88-Nov	1	61	6H	5C	720-ED	NDD				1			62	
	32	61	TEH	TEC	720-EL	INR	5C	4.04	.00	6			30	RESULT OF DISCREPANCY RESOLUTION
88-Nov	32	61	TEH	TEC	740-ED	MBM	5C	4.02	.00	6	.54	114	8	
	7	62	TEH	TEC	720-EL	INR	2C	2.30	.00	3			36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	7	62	TEH	TEC	740-ED	MBM	2C	2.29	.00	6	1.06	97	43	
	39	64	TEH	TEC	720-EL	MBM	4H	33.18	.00	6	7.43	43	28	RESULT OF DISCREPANCY RESOLUTION
	39	64												RESULT OF BASELINE DATA REVIEW
92-May	39	64	TEC	TEH	740-ZM	NDD				1			6	
	21	66	TEH	TEC	720-EL	MBM	1H	2.26	.00	6	2.06	89	28	RESULT OF BASELINE DATA REVIEW
88-Nov	21	66	TEH	TEC	740-ED	MBM	1H	2.21	.00	6	.75	97	17	RESULT OF DISCREPANCY RESOLUTION

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	4	67	TEH	TEC	720-EL	INR	4C	5.02	.00	3			42	RESULT OF DISCREPANCY RESOLUTION
88-Nov	4	67	TEH	TEC	740-ED	MBM	4C	5.05	.00	6	.76	78	5	
	6	69	TEH	TEC	720-EL	INR	3H	4.28	.00	6			36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	6	69	TEH	TEC	740-ED	MBM	3H	4.27	.00	6	.44	92	43	
	11	69	TEH	TEC	720-EL	ANR	2C	47.96	.00	M1			36	
88-Nov	11	69	TEH	TEC	740-ED	DNT	2C	47.93	.00	M1	3.37	183	35	RESULT OF DISCREPANCY RESOLUTION
	21	69	TEH	TEC	720-EL	MBM	4H	29.86	.00	6	5.32	47	30	RESULT OF BASELINE DATA REVIEW
	23	69	TEH	TEC	720-EL	INR	3H	15.38	.00	6			30	
88-Nov	23	69	TEH	TEC	740-ED	MBM	3H	15.58	.00	6	.41	103	51	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	27	72	TEH	TEC	720-EL	INR	3H	28.62	.00	6			28	
88-Nov	27	72	TEH	TEC	740-ED	MBM	3H	28.64	.00	6	.50	89	14	
	3	73	6H	TEH	720-EL	INR	1H	33.00	.00	6			23	
92-May	3	73	6C	TEH	720-ZM	NDD				1			10	
88-Nov	3	73	TEH	TEC	720-ED	MBM	1H	33.00	.00	6	.40	82	1	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	18	73	TEH	TEC	720-EL	INR	1H	7.37	.00	6			34	RESULT OF DISCREPANCY RESOLUTION
-Nov	18	73	TEH	TEC	740-ED	MBM	1H	7.37	.00	6	.40	269	21	
	11	75	TEH	TEC	720-EL	MBM	2H	6.78	.00	6	3.28	85	36	RESULT OF BASELINE DATA REVIEW
88-Nov	11	75	TEH	TEC	740-ED	MBM	2H	6.78	12.07	6	1.04	100	33	RESULT OF DISCREPANCY RESOLUTION
	15	75	TEH	TEC	720-EL	INR	TSC	15.05	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	15	75	TEH	TEC	740-ED	MBM	TSC	15.00	.00	6	.40	84	31	
	4	77	TEH	TEC	720-EL	INR	TSH	7.25	.00	6			42	RESULT OF DISCREPANCY RESOLUTION
88-Nov	4	77	TEH	TEC	740-ED	MBM	TSH	7.25	.00	6	.32	269	5	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	18	78	TEH	TEC	720-EL	INR	1C	44.25	.00	6			34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	18	78	TEH	TEC	740-ED	MBM	1C	44.25	.00	6	.40	279	21	
	1	80	6H	TEH	720-EL	ANR	5H	19.34	.00	1			23	
	1	80	6C	4H	680-EF	ANR	5H	19.34	.00	1			27	RESULT OF DISCREPANCY RESOLUTION
92-May	1	80	6H	TEH	740-ZM	NDD				1			9	
88-Nov	1	80	6H	TEH	740-ED	DNT	5H	19.34	.00	M1	4.36	5	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	1	80	6H	5C	720-ED	NDD				1			62	
	6	87	TEH	TEC	720-EL	INR	BPH	21.85	.00	6			36	
88-Nov	6	87	TEH	TEC	740-ED	MBM	BPH	21.87	.00	6	.56	99	58	

INDICATION LISTING – STEAM GENERATOR 34

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	9	4	TEH	TEC	720-EL	DNG	6H	16.99	.00	M1	5.52	180	22	RESULT OF LAR
	9	4												RESULT OF BASELINE DATA REVIEW
88-Nov	9	4	TEH	TEC	740-ED	DNT	6H	17.00	.00	M1	6.60	181	37	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	1	5	6C	TEC	720-EL	INR	2C	27.40	.00	6			28	
92-May	1	5	6H	TEH	740-ZM	NOD				1			1	
88-Nov	1	5	6C	TEC	740-ED	MBM	2C	27.40	.00	6	.47	120	18	RESULT OF DISCREPANCY RESOLUTION
	9	7	TEH	TEC	720-EL	INR	4C	26.85	.00	6			22	
88-Nov	9	7	TEH	TEC	740-ED	MBM	4C	26.86	.00	6	.44	94	37	RESULT OF DISCREPANCY RESOLUTION
	1	10	6C	TEC	720-EL	INR	4C	11.01	.00	6			28	
92-May	1	10	6H	TEH	740-ZM	NOD				1			2	
88-Nov	1	10	6C	TEC	740-ED	MBM	4C	11.00	.00	6	.44	270	18	RESULT OF DISCREPANCY RESOLUTION
	21	10	TSH	TSH	720-ZP	DNT	TSH	.00	.00	3	20.88	3	7	RESULT OF LAR
	21	10	TSH	TSH	680-ZP	DNT	TSH	-.01	.00	2	16.09	14	31	RESULT OF LAR
	25	12	TEH	TEC	720-EL	ANR	4H	9.40	.00	M1			12	
90-Sep	25	12	TEH	TEC	740-EB	NOD				1			2	
88-Nov	25	12	TEH	TEC	740-ED	DNT	4H	9.39	.00	M1	3.23	186	22	RESULT OF DISCREPANCY RESOLUTION
Nov	25	12												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	3	13	6C	TEC	720-EL	INR	2C	3.21	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
92-May	3	13	6H	TEH	740-ZM	NOD				1			2	
88-Nov	3	13	TEH	TEC	740-ED	MBM	2C	3.20	.00	6	.43	99	18	RESULT OF DISCREPANCY RESOLUTION
	7	13	TEH	TEC	720-EL	INR	3C	41.87	49.60	6			22	RESULT OF DISCREPANCY RESOLUTION
88-Nov	7	13	TEH	TEC	740-ED	MMB	3C	41.85	49.69	6	.47	249	39	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	18	14	TEH	TEC	720-EL	MBM	AV6	16.10	.00	6	6.99	89	12	RESULT OF BASELINE DATA REVIEW
88-Nov	18	14	TEH	TEC	740-EC	MBM	AV6	16.10	.00	6	1.32	66	28	RESULT OF DISCREPANCY RESOLUTION
	26	15	TEH	TEC	720-EL	FSD	1H	21.36	.00	3	.31	66	10	RESULT OF DISCREPANCY RESOLUTION
	26	15												RESULT OF BASELINE DATA REVIEW
88-Nov	26	15	TEH	TEC	740-EC	MBM	1H	21.40	.00	6	.43	263	28	RESULT OF DISCREPANCY RESOLUTION
	32	17	TEH	TEC	720-EL	INR	2C	40.12	.00	6			10	RESULT OF DISCREPANCY RESOLUTION
88-Nov	32	17	TEH	TEC	740-EC	MBM	2C	39.79	.00	6	.46	81	36	RESULT OF DISCREPANCY RESOLUTION
	5	18	TEH	TEC	720-EL	INR	2H	19.05	.00	6			22	RESULT OF DISCREPANCY RESOLUTION
88-Nov	5	18	TEH	TEC	740-ED	MBM	2H	19.00	.00	6	.53	135	16	RESULT OF DISCREPANCY RESOLUTION
	28	18	TEH	TEC	720-EL	INR	2H	5.43	.00	6			16	RESULT OF DISCREPANCY RESOLUTION
88-Nov	28	18	TEH	TEC	740-EC	MBM	2H	5.50	.00	6	.68	96	31	RESULT OF DISCREPANCY RESOLUTION
	34	20	TEH	TEC	720-EL	ANR	1C	24.00	.00	1			16	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
92-May	34	20	TEC	TEH	740-ZM	NDD				1			3	
88-Nov	34	20	TEH	TEC	740-EC	DNT	1C	23.70	.00	M1	3.28	185	38	RESULT OF DISCREPANCY RESOLUTION
	8	21	TEH	TEC	720-EL	FSN	6H	2.88	.00	3	1.11	65	18	RESULT OF LAR
	8	21												RESULT OF BASELINE DATA REVIEW
	8	21	6H	6H	680-ZP	DNG	6H	2.88	.00	2	5.17	12	31	
	22	21	TEH	TEC	720-EL	ANR	BPH	21.07	.00	M1			14	
88-Nov	22	21	TEH	TEC	740-ED	DNT	BPH	21.00	.00	M1	3.55	180	19	RESULT OF DISCREPANCY RESOLUTION
	37	21	TEH	TEC	720-EL	ANR	AV1	11.02	.00	M1			14	
88-Nov	37	21	TEH	TEC	740-ED	DNT	AV1	10.99	.00	M1	3.57	186	7	RESULT OF DISCREPANCY RESOLUTION
	1	22	6H	TEH	720-EL	INR	3H	16.56	.00	6			23	
	1	22	6C	TEC	720-EL	INR	2C	31.80	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
92-May	1	22	6H	TEH	720-ZM	NDD				1			12	
92-May	1	22	6C	5H	700-ZM	NDD				1			13	
88-Nov	1	22	6C	TEC	740-ED	MBM	2C	31.80	.00	6	.41	105	18	RESULT OF DISCREPANCY RESOLUTION
88-Nov	1	22	6C	TEH	720-ED	MBM	3H	16.56	.00	6	.50	38	57	RESULT OF DISCREPANCY RESOLUTION
	7	22	TEH	TEC	720-EL	INR	3C	3.50	.00	6			20	
88-Nov	7	22	TEH	TEC	740-ED	MBM	3C	3.49	.00	6	.44	71	39	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	5	23	TEH	TEC	720-EL	INR	1C	17.41	.00	3			22	RESULT OF LAR
88-Nov	5	23	TEH	TEC	740-ED	MBM	1C	17.40	.00	6	.51	90	16	RESULT OF DISCREPANCY RESOLUTION
	27	23	TEH	TEC	720-EL	MBM	3C	43.25	.00	6	3.43	86	14	RESULT OF BASELINE DATA REVIEW
88-Nov	27	23	TEH	TEC	740-EC	MBM	3C	43.26	.00	6	.82	88	31	
	16	24	TEH	TEC	720-EL	FSD	TSH	7.24	.00	3	.14	81	16	RESULT OF DISCREPANCY RESOLUTION
	16	24												RESULT OF BASELINE DATA REVIEW
	37	25	TEH	TEC	720-EL	INR	2C	4.76	.00	6			6	
88-Nov	37	25	TEH	TEC	740-ED	MBM	2C	4.84	.00	6	.51	85	7	RESULT OF DISCREPANCY RESOLUTION
	23	27	TEH	TEC	720-EL	INR	1H	34.10	.00	6			14	
88-Nov	23	27	TEH	TEC	740-ED	MBM	1H	34.10	.00	6	.52	90	24	RESULT OF DISCREPANCY RESOLUTION
88-Nov	23	27												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	29	27	TEH	TEC	720-EL	INR	2H	10.31	.00	6			14	
88-Nov	29	27	TEH	TEC	740-EC	MBM	2H	10.31	.00	6	.33	87	34	
	11	28	TEH	TEC	720-EL	INR	3C	36.17	41.99	6			16	RESULT OF DISCREPANCY RESOLUTION
88-Nov	11	28	TEH	TEC	740-EC	MBM	3C	36.17	42.02	6	.68	85	50	RESULT OF DISCREPANCY RESOLUTION
	15	28	TEH	TEC	720-EL	INR	2C	16.41	.00	6			16	
88-Nov	15	28	TEH	TEC	740-EC	MBM	2C	16.41	.00	6	.58	92	48	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	16	29	TEH	TEC	720-EL	INR	1H	17.89	.00	6			14	
88-Nov	16	29	TEH	TEC	740-ED	MBM	1H	17.90	.00	6	.42	85	24	RESULT OF DISCREPANCY RESOLUTION
	37	29	TEH	TEC	720-EL	INR	BPC	8.02	.00	6			6	RESULT OF DISCREPANCY RESOLUTION
88-Nov	37	29	TEH	TEC	740-ED	MBM	BPC	8.00	.00	6	.40	83	5	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	41	29	TEH	TEC	720-EL	ANR	5C	.51	.00	M1			6	RESULT OF DISCREPANCY RESOLUTION
92-May	41	29	TEC	TEH	740-ZM	NDD				1			3	
88-Nov	41	29	TEH	TEC	740-ED	DNT	5C	.46	.00	M1	4.08	178	5	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	42	30	TEH	TEC	720-EL	ANR	5C	.00	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
90-Sep	42	30	TEH	TEC	740-EB	NDD				1			3	
88-Nov	42	30	TEH	TEC	740-ED	DNT	5C	.00	.00	M1	5.28	2	1	
	41	31	TEH	TEC	720-EL	DNT	5C	.45	.00	M1	3.54	176	6	RESULT OF DISCREPANCY RESOLUTION
92-May	41	31	TEC	TEH	740-ZM	NDD				1			3	
88-Nov	41	31	TEH	TEC	740-ED	DNT	5C	.45	.00	M1	4.98	177	5	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	32	TSH	TSH	720-ZP	PLP	TSH	.29	.00	10	.71	270	7	
92-May	2	32	6H	TEH	720-ZM	NDD				1			12	
92-May	2	32	6C	5H	700-ZM	NDD				1			13	
	3	32	TSH	TSH	720-ZP	PLP	TSH	.00	.00	10	.27	87	7	RESULT OF DISCREPANCY RESOLUTION
	3	32	6C	TEC	740-EB	NDD				1			3	
90-Sep	3	32	TEH	TEC	740-ZS	NDD				1			10	
	30	32	TEH	TEC	720-EL	ANR	5C	10.65	.00	M1			14	
88-Nov	30	32	TEH	TEC	740-EC	DNT	5C	10.65	.00	M1	3.51	186	34	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	42	32	TEH	TEC	720-EL	ANR	5C	.00	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
88-Nov	42	32	TEH	TEC	740-ED	DNT	5C	.00	.00	M1	4.82	2	1	
	1	33	TSH	TSH	720-ZP	PLP	TSH	.82	.00	10	.77	94	5	
	2	33	TSH	TSH	720-ZP	PLP	TSH	.50	.00	10	.71	89	7	RESULT OF DISCREPANCY RESOLUTION
	2	33	TSH	TSH	720-ZP	DNT	TSH	-.12	.00	2	3.30		7	RESULT OF DISCREPANCY RESOLUTION
	43	34	TEH	TEC	720-EL	ANR	5C	.57	.00	M1			2	
88-Nov	43	34	TEH	TEC	740-ED	DNT	5C	.52	.00	M1	3.43	185	1	
	18	35	TEH	TEC	720-EL	MBM	6H	12.69	.00	6	3.48	88	18	RESULT OF BASELINE DATA REVIEW
88-Nov	18	35	TEH	TEC	740-ED	MBM	6H	12.68	.00	6	.75	83	9	RESULT OF DISCREPANCY RESOLUTION
	15	36	TSH	TSH	720-ZP	PLP	TSH	.22	.00	10	.30	79	7	
90-Sep	15	36	TEH	TEC	740-EB	NDD				1			4	
	44	36	TEH	TEC	720-EL	ANR	5C	.51	.00	M1			2	
92-May	44	36	TEC	TEH	740-ZM	NDD				1			3	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	44	36	TEH	TEC	740-ED	DNT	5C	.50	.00	M1	3.12	182	1	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	6	37	TEH	TEC	720-EL	ANR	6H	27.12	.00	M1			26	RESULT OF DISCREPANCY RESOLUTION
	6	37	TEH	TEC	720-EL	DNG	6H	4.44	.00	1	13.51	189	26	RESULT OF DISCREPANCY RESOLUTION
	6	37	----------											RESULT OF BASELINE DATA REVIEW
88-Nov	6	37	TEH	TEC	740-ED	DNT	6C	4.95	.00	M1	15.82	186	41	RESULT OF DISCREPANCY RESOLUTION
	25	38	TEH	TEC	720-EL	INR	TSC	15.00	.00	6			18	
88-Nov	25	38	TEH	TEC	740-EC	MBM	TSC	15.00	.00	6	.49	73	44	RESULT OF DISCREPANCY RESOLUTION
	8	40	TEH	TEC	720-EL	DNG	6H	38.10	.00	1	5.51	188	28	RESULT OF DISCREPANCY RESOLUTION
	8	40	----------											RESULT OF BASELINE DATA REVIEW
	11	40	TSH	TSH	720-ZP	PVN	TSH	.00	.00	2	8.23	105	7	RESULT OF DISCREPANCY RESOLUTION
	11	40	----------											RETEST WITH MAG BIAS PROBE
90-Sep	11	40	TEH	TEC	740-EB	NOD				1			4	
	15	42	TEH	TEC	720-EL	INR	2C	2.36	.00	6			20	
88-Nov	15	42	TEH	TEC	740-ED	MBM	2C	2.71	.00	6	.56	103	8	RESULT OF DISCREPANCY RESOLUTION
	40	42	TEH	TEC	720-EL	ANR	5H	18.47	.00	M1			6	
92-May	40	42	TEC	TEH	740-ZM	NOD				1			4	
[redacted]Nov	40	42	TEH	TEC	740-ED	DNT	5H	18.63	.00	M1	4.71	178	17	
	20	43	TEH	TEC	720-EL	MBM	5C	3.53	.00	6	2.31	75	20	RESULT OF BASELINE DATA REVIEW
88-Nov	20	43	TEH	TEC	740-ED	MBM	5C	3.92	.00	6	.59	83	8	
	45	43	TEH	TEC	720-EL	ANR	6H	-.06	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
92-May	45	43	TEC	TEH	740-ZM	NOD				1			4	
88-Nov	45	43	TEH	TEC	740-ED	DNT	6H	.00	.00	M1	3.94	6	1	
	30	44	TSH	TSH	720-ZP	PLP	TSH	.11	.00	10	.24	75	7	RESULT OF DISCREPANCY RESOLUTION
	40	44	TEH	TEC	720-EL	INR	5C	42.48	.00	6			6	
	40	44	TEH	TEC	720-EL	INR	5C	38.01	.00	6			6	
88-Nov	40	44	TEH	TEC	740-ED	MBM	5C	38.40	.00	6	.50	79	17	RESULT OF DISCREPANCY RESOLUTION
88-Nov	40	44	TEH	TEC	740-ED	MBM	5C	42.30	.00	6	.64	90	17	RESULT OF DISCREPANCY RESOLUTION
	45	44	TEH	TEC	720-EL	DNT	6H	.57	.00	M1	9.87	180	2	
	45	44	6H	6H	720-ZP	DNT	6H	.65	.00	2	14.02	194	15	
90-Sep	45	44	TEH	TEC	740-EB	NOD				1			4	
88-Nov	45	44	TEH	TEC	740-ED	DNT	6H	.57	.00	M1	12.29	185	1	RESULT OF DISCREPANCY RESOLUTION
	45	45	TEH	TEC	720-EL	ANR	6H	-.57	.00	M1			2	
	45	45	TEH	TEC	720-EL	ANR	6H	.37	.00	M1			2	
92-May	45	45	TEC	TEH	740-ZM	DNT	6H	.63	.00	M1	6.53	181	4	
88-Nov	45	45	TEH	TEC	740-ED	DNT	6H	.51	.00	M1	6.50	5	1	
88-Nov	45	45	TEH	TEC	740-ED	DNT	6H	-.62	.00	M1	4.84	186	1	RESULT OF DISCREPANCY RESOLUTION

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	7	46	TEC	TEH	720-EL	MBM	1H	34.13	.00	6	2.54	80	35	RESULT OF BASELINE DATA REVIEW
88-Nov	7	46	TEH	TEC	740-ED	MBM	1H	34.62	.00	4	1.05	121	43	
	38	46	TEH	TEC	720-EL	FSD	6H	10.79	.00	3	.50	84	6	RESULT OF DISCREPANCY RESOLUTION
	38	46	----------											RESULT OF BASELINE DATA REVIEW
88-Nov	38	46	TEH	TEC	740-ED	MBM	6H	9.77	.00	6	1.31	89	7	RESULT OF DISCREPANCY RESOLUTION
	45	46	TEH	TEC	720-EL	ANR	6H	-.54	.00	M1			2	
	45	46	TEH	TEC	720-EL	ANR	6H	.49	.00	M1			2	
88-Nov	45	46	TEH	TEC	740-ED	DNT	6H	-.33	.00	M1	4.10	185	1	RESULT OF DISCREPANCY RESOLUTION
88-Nov	45	46	TEH	TEC	740-ED	DNT	6H	.73	.00	M1	5.59	186	1	RESULT OF DISCREPANCY RESOLUTION
	1	47	6C	TEC	720-EL	FSD	3C	16.34	.00	3	.35	83	54	RESULT OF BASELINE DATA REVIEW
92-May	1	47	6C	TEH	700-ZM	NDD				1			11	
92-May	1	47	6H	TEH	720-ZM	NDD				1			12	
88-Nov	1	47	6C	TEC	740-ED	MBM	3C	16.34	.00	6	.30	65	35	
	22	47	TEH	TEC	720-EL	FSD	1H	39.57	.00	3	.26	63	20	RESULT OF DISCREPANCY RESOLUTION
	22	47	----------											RESULT OF BASELINE DATA REVIEW
	35	47	TEH	TEC	720-EL	INR	2H	36.60	.00	6			6	RESULT OF DISCREPANCY RESOLUTION
[illegible]v	35	47	TEH	TEC	740-EC	MBM	2H	35.82	.00	6	.66	88	40	
	45	47	TEH	TEC	720-EL	DNT	6H	.51	.00	M1	5.21	178	2	
	45	47	6H	6H	720-ZP	DNT	6H	.71	.00	2	7.01	13	15	
88-Nov	45	47	TEH	TEC	740-ED	DNT	6H	.60	.00	M1	8.60	178	32	
	30	48	TEH	TEC	720-EL	INR	[illegible]	12.35	.00	M1			8	
88-Nov	30	48	TEH	TEC	740-EC	MBM	2C	12.32	.00	6	.48	91	40	
	45	48	TEH	TEC	720-EL	ANR	6H	-.60	.00	M1			2	
	45	48	TEH	TEC	720-EL	DNT	6H	.54	.00	M1	5.42	178	2	
	45	48	6H	6H	720-ZP	DNT	6H	.54	.00	2	7.60	196	15	
	45	48	6H	6H	720-ZP	DNT	6H	-.69	.00	2	6.01	14	15	
90-Sep	45	48	TEH	TEC	740-EB	NDD				1			5	
88-Nov	45	48	TEH	TEC	740-ED	DNT	6H	.60	.00	M1	8.76	178	32	
88-Nov	45	48	TEH	TEC	740-ED	DNT	6H	-.40	.00	M1	4.18	178	32	
	18	49	TEH	TEC	720-EL	INR	4C	24.56	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
	18	49	TEH	TEC	720-EL	INF	4C	21.65	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
88-Nov	18	49	TEH	TEC	740-ED	MBM	4C	21.65	29.06	6	.67	98	9	RESULT OF DISCREPANCY RESOLUTION
	27	49	TEH	TEC	720-EL	ANR	2C	46.19	.00	1			20	
88-Nov	27	49	TEH	TEC	740-EC	DNT	2C	46.40	.00	M1	3.01	183	42	RESULT OF DISCREPANCY RESOLUTION
	45	49	TEH	TEC	720-EL	ANR	6H	-.63	.00	M1			2	
	45	49	TEH	TEC	720-EL	ANR	6H	.51	.00	M1			2	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	45	49	TEH	TEC	740-ED	DNT	6H	-.50	.00	M1	4.07	178	32	
88-Nov	45	49	TEH	TEC	740-ED	DNT	6H	.60	.00	M1	8.16	178	32	
	2	50	6C	TEC	720-EL	INR	2C	17.00	.00	6			54	
88-Nov	2	50	TEH	TEC	740-ED	MBM	2C	17.00	.00	6	.48	77	35	RESULT OF DISCREPANCY RESOLUTION
	3	50	6C	TEC	720-EL	MBM	2C	22.58	.00	6	3.69	79	54	RESULT OF BASELINE DATA REVIEW
92-May	3	50	6H	TEH	740-ZM	NOD				1			7	
88-Nov	3	50	TEH	TEC	740-ED	MBM	2C	22.63	.00	6	1.47	95	35	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	10	50	TEC	TEH	720-EL	INR	1C	35.56	.00	6			35	
	10	50	TEC	TEH	720-EL	INR	1C	38.13	.00	6			35	
88-Nov	10	50	TEH	TEC	740-ED	MBM	1C	38.13	.00	6	.45	58	45	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	10	50	TEH	TEC	740-ED	MBM	1C	35.65	.00	6	.42	108	45	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	45	50	TEH	TEC	720-EL	DNT	6H	.46	.00	M1	5.95	179	2	
	45	50	6H	6H	720-ZP	DNT	6H	.70	.00	2	7.56	13	15	
88-Nov	45	50	TEH	TEC	740-ED	DNT	6H	.30	.00	M1	9.66	180	32	
	1	51	6C	TEC	720-EL	INF	TSC	42.00	.00	6			54	RESULT OF DISCREPANCY RESOLUTION
	1	51	6C	TEC	720-EL	INR	TSC	33.53	.00	6			54	RESULT OF LAR
	1	51	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	RESULT OF BASELINE DATA REVIEW
[illegible]y	1	51	6H	TEH	740-ZM	NOD				1			7	
[illegible]v	1	51	6C	TEC	740-ED	MBM	TSC	42.00	.00	6	.39		35	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	45	51	TEH	TEC	720-EL	ANR	6H	.59	.00	M1			2	
90-Sep	45	51	TEH	TEC	740-EB	NOD				1			5	
88-Nov	45	51	TEH	TEC	740-ED	DNT	6H	.32	.00	M1	5.81	178	32	
	44	52	TEH	TEC	720-EL	DNT	AV1	-.43	.00	M1	5.37	177	2	RESULT OF DISCREPANCY RESOLUTION
	44	52	TEH	TEC	720-EL	ANR	AV3	.00	.00	M1			2	
88-Nov	44	52	TEH	TEC	740-ED	DNT	6H	31.45	.00	M1	6.01	180	32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	44	52	TEH	TEC	740-ED	DNT	AV2	23.00	.00	M1	6.87	180	32	RESULT OF DISCREPANCY RESOLUTION
	3	53	6H	TEH	720-EL	INR	1H	29.50	.00	6			23	
92-May	3	53	6H	TEH	740-ZM	NOD				1			7	
88-Nov	3	53	TEH	TEC	740-ED	MBM	1H	29.49	.00	6	.28	83	35	
	19	53	TEH	TEC	720-EL	MBM	4H	20.63	.00	6	2.76	81	26	RESULT OF BASELINE DATA REVIEW
88-Nov	19	53	TEH	TEC	740-ED	MBM	4H	20.15	.00	6	.86	92	9	RESULT OF DISCREPANCY RESOLUTION
	4	54	TEH	TEC	720-EL	INR	TSC	36.98	.00	6			38	
92-May	4	54	6C	TEH	720-ZM	NOD				1			10	
88-Nov	4	54	TEH	TEC	740-ED	MBM	TSC	36.97	.00	6	.44	83	33	
	11	54	TEH	TEC	720-EL	MBM	AV1	5.51	.00	6	2.26	81	38	RESULT OF LAR
	11	54	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	RESULT OF BASELINE DATA REVIEW
88-Nov	11	54	TEH	TEC	740-ED	MBM	AV1	5.50	.00	6	.87	62	8	RESULT OF LAR

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	1	55	6C	TEC	720-EL	INR	4C	29.28	.00	6			36	
88-Nov	1	55	6C	TEC	740-ED	MBM	4C	29.28	.00	6	.39	94	35	
	5	55	TEH	TEC	720-EL	INR	4H	4.01	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
88-Nov	5	55	TEH	TEC	740-ED	MBM	4H	4.00	.00	6	.54	95	33	RESULT OF DISCREPANCY RESOLUTION
	43	55	TEH	TEC	720-EL	ANR	5C	.76	.00	M1			2	
88-Nov	43	55	TEH	TEC	740-ED	DNT	5C	.58	.00	M1	3.11	184	32	
	44	55	TEH	TEC	720-EL	ANR	5C	.71	.00	M1			2	
88-Nov	44	55	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	6.09	183	32	
	2	56	6C	TEC	720-EL	MBM	3C	5.85	.00	6	5.03	84	38	RESULT OF BASELINE DATA REVIEW
92-May	2	56	6H	TEH	740-ZM	NOD				1			7	
88-Nov	2	56	TEH	TEC	740-ED	MBM	3C	5.84	.00	6	1.32	95	35	
	32	56	TEH	TEC	720-EL	MBM	3H	20.55	.00	6	2.68	79	8	RESULT OF LAR
	32	56	----------											RESULT OF BASELINE DATA REVIEW
88-Nov	32	56	TEH	TEC	740-ED	MBM	3H	21.28	.00	6	.73	92	25	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	43	56	TEH	TEC	720-EL	ANR	5C	.85	.00	M1			2	
[illegible]p	43	56	TEH	TEC	740-ZS	NOD				1			6	
[illegible]v	43	56	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	4.56	183	32	
	44	56	TEH	TEC	720-EL	ANR	5C	.76	.00	M1			2	
	44	56	TEH	TEC	720-EL	ANR	5C	-.42	.00	M1			2	
88-Nov	44	56	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	4.82	182	32	
86-Nov	44	56	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	4.04	183	32	
	1	57	6C	TEC	720-EL	INR	4C	7.00	.00	6			36	
88-Nov	1	57	6C	TEC	740-ED	MBM	4C	7.00	.00	6	.39		35	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	57	6H	TEH	720-EL	INR	1H	13.77	.00	6			23	
	2	57	6C	TEC	720-EL	INR	5C	-1.94	.00	1			38	RESULT OF DISCREPANCY RESOLUTION
	2	57	6H	5C	680-EF	INR	5C	-1.88	.00	6			48	RESULT OF DISCREPANCY RESOLUTION
92-May	2	57	6H	TEH	740-ZM	NOD				1			7	
88-Nov	2	57	TEH	TEC	740-ED	MBM	1H	13.70	.00	6	.45	81	35	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	57	TEH	TEC	740-ED	MBM	4C	50.80	.00	6	.61	103	35	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	57	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	3	57	6H	TEH	720-EL	INR	1H	48.64	.00	6			23	RESULT OF DISCREPANCY RESOLUTION
92-May	3	57	6C	TEH	720-ZM	NOD				1			10	
88-Nov	3	57	TEH	TEC	740-ED	MBM	1H	48.64	.00	6	.62	114	35	RESULT OF DISCREPANCY RESOLUTION
	4	57	TEH	TEC	720-EL	INR	2H	1.61	.00	6			26	RESULT OF DISCREPANCY RESOLUTION
88-Nov	4	57	TEH	TEC	740-ED	MBM	2H	1.60	.00	6	.47	100	33	RESULT OF DISCREPANCY RESOLUTION

| DATE | ROW | COL | CEB | CEE | PROBE | IND | LOC | INCH1 | INCH2 | CHAN | VOLTS | DEG | TAPE | COMMENTS |

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	32	57	TEH	TEC	720-EL	INR	4H	13.05	.00	6			8	
88-Nov	32	57	TEH	TEC	740-ED	MBM	4H	13.52	.00	6	.49	264	25	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	42	57	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	5.07	177	2	
	42	57	5C	5C	720-ZP	DNT	5C	.60	.00	2	7.C5	184	56	
88-Nov	42	57	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	6.33	182	32	
	43	57	TEH	TEC	720-EL	DNT	5C	.79	.00	M1	6.81	178	2	
	43	57	TEH	TEC	720-EL	ANR	5C	-.31	.00	M1			2	
	43	57	5C	5C	720-ZP	DNT	5C	.65	.00	2	8.44	183	56	
88-Nov	43	57	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	8.63	183	32	
88-Nov	43	57	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	3.27	182	32	
	1	58	6C	TEC	720-EL	INR	5C	8.21	.00	6			36	RESULT OF DISCREPANCY RESOLUTION
	1	58	6H	5C	680-EF	INR	5C	8.21	.00	6			48	
92-May	1	58	6H	TEH	740-ZM	NOD				1			7	
88-Nov	1	58	6C	TEC	740-ED	MBM	5C	8.22	.00	6	.48	73	35	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	17	58	TEH	TEC	720-EL	INR	2C	43.05	.00	6			28	RESULT OF DISCREPANCY RESOLUTION
88-Nov	17	58	TEH	TEC	740-ED	MBM	2C	43.04	.00	6	.43	88	10	
	21	58	TSH	TSH	720-ZP	PLP	TSH	.03	.00	10	.26	84	15	
	34	58	TEH	TEC	720-EL	INR	3H	33.68	.00	6			8	
88-Nov	34	58	TEH	TEC	740-ED	MBM	3H	33.60	.00	6	.43	92	23	
	40	58	TEH	TEC	720-EL	ANR	4H	.91	.00	M1			6	
90-Sep	40	58	TEH	TEC	740-ZS	NOD				1			6	
88-Nov	40	58	TEH	TEC	740-ED	DNT	4H	-.12	.00	M1	5.61	184	30	
	41	58	TEH	TEC	720-EL	ANR	5C	.62	.00	M1			2	
88-Nov	41	58	TEH	TEC	740-ED	DNT	5C	.58	.00	M1	4.33	182	30	
	42	58	TEH	TEC	720-EL	DNT	5C	.79	.00	M1	6.54	177	2	
	42	58	TEH	TEC	720-EL	ANR	5C	-.31	.00	M1			2	
	42	58	5C	5C	720-ZP	DNT	5C	.69	.00	2	10.58	182	56	
88-Nov	42	58	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	8.37	182	32	
88-Nov	42	58	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	4.78	182	32	
	43	58	TEH	TEC	720-EL	ANR	5H	.75	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
	43	58	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	8.92	178	2	
	43	58	TEH	TEC	720-EL	ANR	5C	-.48	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
	43	58	5C	5C	720-ZP	DNT	5C	.63	.00	2	14.04	183	56	
88-Nov	43	58	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	3.48	182	32	
88-Nov	43	58	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	11.54	183	32	
88-Nov	43	58	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	6.60	182	32	
	14	59	TEH	TEC	720-EL	INR	TSC	4.81	.00	6			30	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	14	59	TEH	TEC	740-ED	MBM	TSC	4.80	.00	6	.60	86	4	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	19	59	TSH	TSH	720-ZP	PLP	TSH	.13	.00	10	.40	84	15	
	20	59	TSH	TSH	720-ZP	PLP	TSH	.10	.00	10	.41	81	9	
	25	59	TEH	TEC	720-EL	INR	TSC	7.72	.00	6			30	
88-Nov	25	59	TEH	TEC	740-ED	MBM	TSC	7.73	.00	6	.56	91	15	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	40	59	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	5.09	177	6	
	40	59	5C	5C	720-ZP	DNT	5C	.60	.00	2	8.76	183	56	
92-May	40	59	TEC	TEH	740-ZM	DNT	5C	.39	.00	M1	5.82	184	5	
88-Nov	40	59	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	5.69	183	30	
	41	59	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	6.27	178	2	
	41	59	TEH	TEC	720-EL	ANR	5C	-.40	.00	M1			2	RESULT OF DISCREPANCY RESOLUTION
	41	59	5C	5C	720-ZP	DNT	5C	.66	.00	2	9.53	182	56	
88-Nov	41	59	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	7.95	184	30	
88-Nov	41	59	TEH	TEC	740-ED	DNT	5C	-.53	.00	M1	4.08	182	30	
	42	59	TEH	TEC	720-EL	DNT	5C	.93	.00	M1	8.23	178	2	
	42	59	TEH	TEC	720-EL	DNT	5C	-.28	.00	M1	7.01	179	2	
	42	59	5C	5C	720-ZP	DNT	5C	-.32	.00	2	9.99	187	56	
	42	59	5C	5C	720-ZP	DNT	5C	.63	.00	2	11.97	183	56	
92-May	42	59	TEC	TEH	740-ZM	DNT	5C	.72	.00	M1	9.20	186	5	RESULT OF LAR
92-May	42	59	TEC	TEH	740-ZM	DNT	5C	-.46	.00	M1	6.92	188	5	RESULT OF LAR
88-Nov	42	59	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	10.83	182	32	
88-Nov	42	59	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	8.85	182	32	
	43	59	TEH	TEC	720-EL	DNT	5C	.76	.00	M1	10.64	178	2	
	43	59	TEH	TEC	720-EL	DNT	5C	-.40	.00	M1	7.84	178	2	
	43	59	5C	5C	720-ZP	DNT	5C	-.39	.00	2	4.81	189	56	
	43	59	5C	5C	720-ZP	DNT	5C	.64	.00	2	15.25	183	56	
88-Nov	43	59	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	13.07	183	32	
88-Nov	43	59	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	9.79	183	32	
	2	60	6C	TEC	720-EL	MBM	4C	13.88	.00	6	2.55	85	38	
	2	60	6C	TEC	720-EL	MBM	TSC	17.20	.00	6	4.10	75	38	RESULT OF DISCREPANCY RESOLUTION
	2	60	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	RESULT OF BASELINE DATA REVIEW
88-Nov	2	60	TEH	TEC	740-ED	MBM	4C	13.92	.00	6	.66	90	35	
88-Nov	2	60	TEH	TEC	740-ED	MBM	TSC	17.82	.00	6	1.12	85	35	
	36	60	TSH	TSH	720-ZP	PLP	TSH	.12	.00	10	.37	89	9	RESULT OF DISCREPANCY RESOLUTION
	39	60	TEH	TEC	720-EL	ANR	5C	.71	.00	M1			6	
90-Sep	39	60	TEH	TEC	740-ZS	NDD				1			7	
88-Nov	39	60	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	3.75	183	30	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	40	60	TEH	TEC	720-EL	DNT	5C	.62	.00	M1	6.62	178	6	
	40	60	TEH	TEC	720-EL	ANR	5C	-.34	.00	M1			6	RESULT OF DISCREPANCY RESOLUTION
	40	60	5C	5C	720-ZP	DNT	5C	.60	.00	2	11.06	183	56	
92-May	40	60	TEC	TEH	740-ZM	DNT	5C	.39	.00	M1	6.98	184	5	
88-Nov	40	60	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	7.60	183	30	
88-Nov	40	60	TEH	TEC	740-ED	DNT	5C	-.51	.00	M1	4.37	182	30	
	41	60	TEH	TEC	720-EL	DNT	5C	.68	.00	M1	9.44	178	2	
	41	60	TEH	TEC	720-EL	DNT	5C	-.42	.00	M1	6.96	178	2	
	41	60	5C	5C	720-ZP	DNT	5C	-.40	.00	2	10.34	185	56	
	41	60	5C	5C	720-ZP	DNT	5C	.62	.00	2	13.54	188	56	
90-Sep	41	60	TEH	TEC	740-ZS	DNT	5C	.56	.00	M1	10.29	180	7	
90-Sep	41	60	TEH	TEC	740-ZS	DNT	5C	-.53	.00	M1	7.20	178	7	
88-Nov	41	60	TEH	TEC	740-ED	DNT	5C	.57	.00	M1	11.93	182	32	
88-Nov	41	60	TEH	TEC	740-ED	DNT	5C	-.52	.00	M1	9.11	181	32	
	42	60	TEH	TEC	720-EL	ANR	5H	.69	.00	M1			2	
	42	60	TEH	TEC	720-EL	DNT	5C	.77	.00	M1	9.53	179	2	
	42	60	TEH	TEC	720-EL	DNT	5C	-.40	.00	M1	8.46	178	2	
	42	60	5C	5C	720-ZP	DNT	5C	-.40	.00	2	12.42	185	56	
	42	60	5C	5C	720-ZP	DNT	5C	.68	.00	2	14.79	190	56	
88-Nov	42	60	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	4.57	180	32	
[illegible]ov	42	60	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	12.79	182	32	
[illegible]ov	42	60	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	10.34	182	32	
	43	60	TEH	TEC	720-EL	ANR	5H	.77	.00	M1			2	
	43	60	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	10.50	178	2	
	43	60	TEH	TEC	720-EL	DNT	5C	-.40	.00	M1	9.88	179	2	
	43	60	5C	5C	720-ZP	DNT	5C	-.34	.00	2	16.17	189	56	
	43	60	5C	5C	720-ZP	DNT	5C	.71	.00	2	16.40	186	56	
90-Sep	43	60	TEH	TEC	740-ZS	NOD				1			7	
88-Nov	43	60	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	3.55	182	32	
88-Nov	43	60	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	13.44	182	32	
88-Nov	43	60	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	12.26	184	32	
	1	61	6C	TEC	720-EL	INR	3C	30.58	.00	6			36	RESULT OF LAR
92-May	1	61	6C	TEH	700-ZM	NOD				1			11	
92-May	1	61	6H	TEH	720-ZM	NOD				1			12	
88-Nov	1	61	6C	TEC	740-ED	MBM	3C	30.34	.00	6	.61	93	35	
	4	61	TEH	TEC	720-EL	INR	1H	43.15	.00	6			30	RESULT OF DISCREPANCY RESOLUTION
	4	61	TEH	TEC	720-EL	MBM	2H	27.37	.00	6	2.02	84	30	RESULT OF DISCREPANCY RESOLUTION
	4	61	----------											RESULT OF BASELINE DATA REVIEW
	4	61	TEH	TEC	720-EL	INR	2H	48.13	.00	6			30	RESULT OF LAR
	4	61	TEH	TEC	720-EL	INR	3C	23.29	.00	6			30	
88-Nov	4	61	TEH	TEC	740-ED	MBM	1H	43.65	.00	6	.52	86	33	
88-Nov	4	61	TEH	TEC	740-ED	MBM	2H	27.48	.00	6	.62	89	33	
88-Nov	4	61	TEH	TEC	740-ED	MBM	2H	48.12	.00	6	.41	75	33	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	4	61	TEH	TEC	740-ED	MBM	3C	23.30	.00	6	.41	84	33	RESULT OF DISCREPANCY RESOLUTION
88-Nov	4	61												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	9	61	TEH	TEC	720-EL	FSD	BPH	23.83	.00	3	.21	69	30	RESULT OF DISCREPANCY RESOLUTION
	9	61												RESULT OF BASELINE DATA REVIEW
	21	61	TEH	TEC	720-EL	INR	2H	40.82	.00	6			30	
	21	61	TEH	TEC	720-EL	INR	1C	43.17	.00	6			30	
88-Nov	21	61	TEH	TEC	740-ED	MBM	2H	40.82	.00	6	.51	82	13	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	21	61	TEH	TEC	740-ED	MBM	1C	43.16	.00	6	.37	101	13	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	29	61	TEH	TEC	720-EL	INR	2C	10.60	.00	6			30	
	29	61	TEH	TEC	720-EL	INR	2C	13.19	.00	6			30	
88-Nov	29	61	TEH	TEC	740-ED	MBM	2C	10.60	.00	6	.42	72	21	RESULT OF DISCREPANCY RESOLUTION
88-Nov	29	61												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	29	61	TEH	TEC	740-ED	MBM	2C	13.20	.00	6	.49	71	21	RESULT OF DISCREPANCY RESOLUTION
88-Nov	29	61												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	39	61	TEH	TEC	720-EL	ANR	5C	.82	.00	M1			6	
88-Nov	39	61	TEH	TEC	740-ED	DNT	5C	.58	.00	M1	3.89	183	30	RESULT OF DISCREPANCY RESOLUTION
	40	61	TEH	TEC	720-EL	DNT	5C	.88	.00	M1	8.37	177	6	
	40	61	TEH	TEC	720-EL	ANR	5C	-.37	.00	M1			6	
	40	61	5C	5C	720-ZP	DNT	5C	.84	.00	2	14.32	187	56	
92-May	40	61	TEC	TEH	740-ZM	DNT	5C	.79	.00	M1	8.64	186	5	RESULT OF LAR
88-Nov	40	61	TEH	TEC	740-ED	DNT	5C	.59	.00	M1	9.65	183	30	
88-Nov	40	61	TEH	TEC	740-ED	DNT	5C	-.51	.00	M1	4.89	183	30	
	41	61	TEH	TEC	720-EL	DNT	5C	.68	.00	M1	12.49	177	8	
	41	61	TEH	TEC	720-EL	DNT	5C	-.34	.00	M1	9.32	178	8	
	41	61	5C	5C	720-ZP	DNT	5C	-.34	.00	2	15.00	185	56	
	41	61	5C	5C	720-ZP	DNT	5C	.59	.00	2	17.88	189	56	
88-Nov	41	61	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	15.53	182	32	
88-Nov	41	61	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	13.39	183	32	
	42	61	TEH	TEC	720-EL	ANR	5H	.77	.00	M1			8	
	42	61	TEH	TEC	720-EL	DNT	5C	.94	.00	M1	14.32	179	8	
	42	61	TEH	TEC	720-EL	DNT	5C	-.23	.00	M1	7.39	177	8	
	42	61	5C	5C	720-ZP	DNT	5C	-.24	.00	2	11.78	185	56	
	42	61	5C	5C	720-ZP	DNT	5C	.71	.00	2	19.80	188	56	
88-Nov	42	61	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	3.97	180	32	
88-Nov	42	61	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	16.80	183	32	
88-Nov	42	61	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	10.36	182	32	
	21	62	TEH	TEC	720-EL	INR	BPC	14.81	.00	4			30	
88-Nov	21	62	TEH	TEC	740-ED	MBM	BPC	14.82	.00	6	.35	76	13	
	39	62	TEH	TEC	720-EL	DNT	5C	.62	.00	M1	5.59	176	6	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	39	62	TEH	TEC	720-EL	ANR	5C	-.59	.00	M1			6	
	39	62	5C	5C	720-ZP	DNT	5C	.67	.00	2	10.69	194	56	
88-Nov	39	62	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	6.31	182	30	
88-Nov	39	62	TEH	TEC	740-ED	DNT	5C	-.53	.00	M1	3.36	183	30	
	40	62	TEH	TEC	720-EL	DNT	5C	.85	.00	M1	11.13	177	6	
	40	62	TEH	TEC	720-EL	DNT	5C	-.45	.00	M1	5.31	179	6	
	40	62	5C	5C	720-ZP	DNT	5C	-.47	.00	2	8.85	185	56	
	40	62	5C	5C	720-ZP	DNT	5C	.73	.00	2	16.17	187	56	
90-Sep	40	62	TEH	TEC	740-ZS	DNT	5C	.54	.00	M1	11.12	178	7	
90-Sep	40	62	TEH	TEC	740-ZS	DNT	5C	-.40	.00	M1	5.86	178	7	
88-Nov	40	62	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	12.46	183	30	
88-Nov	40	62	TEH	TEC	740-ED	DNT	5C	-.53	.00	M1	6.88	183	30	
	41	62	TEH	TEC	720-EL	ANR	5H	.54	.00	M1			8	
	41	62	TEH	TEC	720-EL	DNT	5C	.80	.00	M1	13.19	179	8	
	41	62	TEH	TEC	720-EL	DNT	5C	-.37	.00	M1	7.72	180	8	
	41	62	5C	5C	720-ZP	DNT	5C	-.43	.00	2	14.13	186	56	
	41	62	5C	5C	720-ZP	DNT	5C	.76	.00	2	17.92	188	56	
88-Nov	41	62	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	4.10	181	32	
88-Nov	41	62	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	15.76	183	32	
88-Nov	41	62	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	10.57	182	32	
	42	62	TEH	TEC	720-EL	ANR	5H	.60	.00	M1			8	
	42	62	TEH	TEC	720-EL	DNT	5C	.79	.00	M1	11.90	177	8	
	42	62	TEH	TEC	720-EL	DNT	5C	-.25	.00	M1	9.40	178	8	
	42	62	5C	5C	720-ZP	DNT	5C	-.41	.00	2	15.59	186	56	
	42	62	5C	5C	720-ZP	DNT	5C	.68	.00	2	17.85	187	56	
92-May	42	62	TEC	TEH	740-ZM	DNT	[illegible]	-.38	.00	M2	10.56	185	7	
92-May	42	62	TEC	TEH	740-ZM	DNT	5C	.70	.00	M2	13.05	184	7	
88-Nov	42	62	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	6.41	181	32	
88-Nov	42	62	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	14.65	183	32	
88-Nov	42	62	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	13.05	182	32	
	23	63	TEH	TEC	720-EL	INR	5H	2.91	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	23	63	TEH	TEC	740-ED	MBM	5H	2.91	.00	6	.62	81	14	
	39	63	TEH	TEC	720-EL	ANR	5C	.65	.00	M1			6	
88-Nov	39	63	TEH	TEC	740-ED	DNT	5C	.53	.00	M1	5.21	183	30	
	40	63	TEH	TEC	720-EL	ANR	5C	-.25	.00	M1			6	RESULT OF DISCREPANCY RESOLUTION
92-May	40	63	TEC	TEH	740-ZM	NDD	[illegible]	[illegible]	[illegible]	1			5	
88-Nov	40	63	TEH	TEC	740-ED	DNT	5C	-.40	.00	M1	3.08	182	30	RESULT OF DISCREPANCY RESOLUTION
	41	63	TEH	TEC	720-EL	ANR	5H	.55	.00	M1			8	
	41	63	TEH	TEC	720-EL	DNT	5C	.77	.00	M1	11.51	179	8	
	41	63	TEH	TEC	720-EL	DNT	5C	-.37	.00	M1	6.84	180	8	
	41	63	5C	5C	720-ZP	DNT	5C	-.34	.00	2	13.32	185	56	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	41	63	5C	5C	72[illegible]-ZP	DNT	5C	.69	.00	2	19.07	190	56	
88-Nov	41	63	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	3.57	181	32	
88-Nov	41	63	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	14.48	183	32	
88-Nov	41	63	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	9.62	183	32	
	42	63	TEH	TEC	720-EL	ANR	5H	.69	.00	M1			8	
	42	63	TEH	TEC	720-EL	DNT	5C	1.02	.00	M1	15.04	177	8	
	42	63	TEH	TEC	720-EL	DNT	5C	-.37	.00	M1	8.55	180	8	
	42	63	5C	5C	720-ZP	DNT	5C	-.35	.00	2	14.16	185	56	
	42	63	5C	5C	720-ZP	DNT	5C	.72	.00	2	21.22	192	56	
88-Nov	42	63	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	6.32	182	32	
88-Nov	42	63	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	17.24	183	32	
88-Nov	42	63	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	11.64	183	32	
	1	64	6C	TEC	720-EL	INF	5C	42.64	.00	6			36	RESULT OF LAR
	1	64	6C	TEC	720-EL	MBM	5C	45.63	.00	6	2.08	57	36	RESULT OF LAR
	1	64	----------											RESULT OF BASELINE DATA REVIEW
	1	64	6H	5C	680-EF	MBM	5C	45.63	.00	6	2.58	70	48	RESULT OF BASELINE DATA REVIEW
	1	64	6H	5C	680-EF	INF	5C	42.85	.00	3			48	RESULT OF DISCREPANCY RESOLUTION
88-Nov	1	64	6C	TEC	740-ED	MBM	5C	42.84	.00	6	.50	80	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	35	64	TEH	TEC	720-EL	ANR	6H	17.13	.00	M1			6	
[illegible]p	35	64	TEH	TEC	740-ZS	NDD				1			7	
[illegible]v	35	64	TEH	TEC	740-ED	DNT	6H	17.10	.00	M1	3.96	189	23	RESULT OF DISCREPANCY RESOLUTION
88-Nov	35	64	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	39	64	TEH	TEC	720-EL	ANR	5C	.71	.00	M1			6	RESULT OF DISCREPANCY RESOLUTION
90-Sep	39	64	TEH	TEC	740-ZS	NDD				1			7	
88-Nov	39	64	TEH	TEC	740-ED	DNT	[illegible]	.53	.00	M1	5.37	183	30	
	40	64	TEH	TEC	720-EL	DNT	5C	.62	.00	M1	9.38	179	6	
	40	64	TEH	TEC	720-EL	DNT	5C	-.17	.00	M1	5.98	179	6	
	40	64	5C	5C	720-ZP	DNT	5C	-.28	.00	2	8.25	188	56	
	40	64	5C	5C	720-ZP	DNT	5C	.61	.00	2	16.61	185	56	
92-May	40	64	TEC	TEH	740-ZM	DNT	5C	.00	.00	M1	9.30	186	5	
88-Nov	40	64	TEH	TEC	740-ED	DNT	5C	.59	.00	M1	10.74	184	30	
88-Nov	40	64	TEH	TEC	740-ED	DNT	5C	-.56	.00	M1	7.62	183	30	
	41	64	TEH	TEC	720-EL	ANR	5H	.86	.00	M1			8	
	41	64	TEH	TEC	720-EL	DNT	5C	.85	.00	M1	10.45	177	8	
	41	64	TEH	TEC	720-EL	DNT	5C	-.26	.00	M1	6.89	178	8	
	41	64	5C	5C	720-ZP	DNT	5C	-.37	.00	2	13.52	185	56	
	41	64	5C	5C	720-ZP	DNT	5C	.68	.00	2	16.69	189	56	
90-Sep	41	64	TEH	TEC	740-ZS	DNT	5C	.68	.00	M1	10.29	180	7	
90-Sep	41	64	TEH	TEC	740-ZS	DNT	5C	-.51	.00	M1	7.66	179	7	
88-Nov	41	64	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	4.46	181	32	
88-Nov	41	64	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	13.49	183	32	
88-Nov	41	64	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	9.23	182	32	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	28	65	TEH	TEC	720-EL	INR	BPH	9.55	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
	28	65	TEH	TEC	720-EL	INR	1H	13.50	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	28	65	TEH	TEC	740-ED	MBM	BPH	9.70	.00	6	.40	90	20	RESULT OF DISCREPANCY RESOLUTION
88-Nov	28	65	TEH	TEC	740-ED	MBM	1H	13.10	.00	6	.44	100	20	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	39	65	TEH	TEC	720-EL	ANR	5C	.59	.00	M1			8	RESULT OF DISCREPANCY RESOLUTION
92-May	39	65	TEC	TEH	740-ZM	NOD				1			5	
88-Nov	39	65	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	3.71	185	30	
	40	65	TEH	TEC	720-EL	DNT	5C	.63	.00	M1	6.40	177	8	
	40	65	TEH	TEC	720-EL	ANR	5C	-.28	.00	M1			8	RESULT OF DISCREPANCY RESOLUTION
	40	65	5C	5C	720-ZP	DNT	5C	72	.00	2	11.40	188	56	
92-May	40	65	TEC	TEH	740-ZM	DNT	5C	.80	.00	M1	6.94	185	5	
88-Nov	40	65	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	7.68	183	30	
88-Nov	40	65	TEH	TEC	740-ED	DNT	5C	-.56	.00	M1	5.88	183	30	
	41	65	TEH	TEC	720-EL	ANR	5H	.77	.00	M1			8	
	41	65	TEH	TEC	720-EL	DNT	5C	.71	.00	M1	8.13	179	8	
	41	65	TEH	TEC	720-EL	DNT	5C	-.37	.00	M1	6.40	179	8	
	41	65	5C	5C	720-ZP	DNT	5C	-.36	.00	2	13.49	185	56	
	41	65	5C	5C	720-ZP	DNT	5C	.66	.00	2	13.32	185	56	
[illegible]ay	41	65	TEC	TEH	740-ZM	DNT	5C	-.47	.00	M1	6.92	189	5	
[illegible]ay	41	65	TEC	TEH	740-ZM	DNT	5C	.66	.00	M1	8.59	187	5	
88-Nov	41	65	TEH	TEC	740-ED	DNT	5H	.56	.00	M1	5.00	180	32	
88-Nov	41	65	TEH	TEC	740-ED	DNT	5C	.56	.00	M1	11.46	182	32	
88-Nov	41	65	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	9.24	183	32	
	5	66	TEH	TEC	720-EL	MBM	TSH	1.90	.00	6	2.16	82	34	RESULT OF BASELINE DATA REVIEW
92-May	5	66	6H	TEH	740-ZM	NOD				1			7	
88-Nov	5	66	TEH	TEC	740-ED	MBM	TSH	1.90	.00	6	.64	85	53	RESULT OF DISCREPANCY RESOLUTION
88-Nov	5	66	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	14	66	TEH	TEC	720-EL	MBM	4C	46.33	.00	6	3.16	79	32	RESULT OF BASELINE DATA REVIEW
88-Nov	14	66	TEH	TEC	740-ED	MBM	4C	45.51	.00	6	.83	90	3	
	22	66	TEH	TEC	720-EL	INR	4C	15.24	.00	6			34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	66	TEH	TEC	740-ED	MBM	4C	15.70	.00	6	.40	67	54	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	66	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	40	66	TEH	TEC	720-EL	DNT	5C	.94	.00	M1	6.40	178	8	RESULT OF DISCREPANCY RESOLUTION
	40	66	TEH	TEC	720-EL	ANR	5C	-.43	.00	M1			8	RESULT OF DISCREPANCY RESOLUTION
	40	66	5C	5C	720-ZP	DNT	5C	.70	.00	2	14.28	189	56	
90-Sep	40	66	TEH	TEC	740-ZS	DNT	5C	.57	.00	M1	6.82	178	7	
88-Nov	40	66	TEH	TEC	740-ED	DNT	5C	.59	.00	M1	7.71	184	30	
88-Nov	40	66	TEH	TEC	740-ED	DNT	5C	-.50	.00	M1	5.54	182	30	
	8	67	TEH	TEC	720-EL	INR	1H	6.68	.00	6			34	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
92-May	8	67	6C	TEH	720-ZM	NDD				1			9	
88-Nov	8	67	TEH	TEC	740-ED	MBM	1H	6.67	.00	6	.40	83	47	RESULT OF DISCREPANCY RESOLUTION
	37	67	TEH	TEC	720-EL	INR	2H	1.20	.00	6			8	RESULT OF DISCREPANCY RESOLUTION
88-Nov	37	67	TEH	TEC	740-ED	MBM	2H	1.67	.00	6	.48	78	29	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	40	67	TEH	TEC	720-EL	ANR	5C	.99	.00	M1			8	
92-May	40	67	TEC	TEH	740-ZM	DNT	5C	.83	.00	M1	5.16	184	5	
88-Nov	40	67	TEH	TEC	740-ED	DNT	5C	.61	.00	M1	5.11	183	30	
	10	68	TEH	TEC	720-EL	INR	TSC	17.70	.00	6			32	
88-Nov	10	68	TEH	TEC	740-ED	MBM	TSC	17.74	.00	6	.61	111	45	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	16	68	TEH	TEC	720-EL	INR	AV6	11.81	.00	6			32	
88-Nov	16	68	TEH	TEC	740-ED	MBM	AV6	11.84	.00	6	.52	121	11	RESULT OF DISCREPANCY RESOLUTION
	40	68	TEH	TEC	720-EL	ANR	AV3	26.00	.00	M1			8	
	40	68	TEH	TEC	720-EL	ANR	5C	.68	.00	M1			8	
88-Nov	40	68	6H	TEC	740-ED	DNT	AV3	26.00	.00	M1	6.13	178	0	
88-Nov	40	68	6H	TEC	740-ED	DNT	5C	.64	.00	M1	3.31	183	0	RESULT OF DISCREPANCY RESOLUTION
88-Nov	40	68	TEH	TEC	740-ED	DNT	AV3	26.22	.00	M1	5.63	180	30	RESULT OF DISCREPANCY RESOLUTION
Nov	40	68												RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	27	70	TEH	TEC	720-EL	ANR	AV6	1.44	.00	1			34	RESULT OF DISCREPANCY RESOLUTION
	27	70	TEH	TEC	720-EL	ANF	6C	23.85	.00	1			34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	27	70	TEH	TEC	740-ED	DNT	6C	23.85	.00	M1	3.21	182	20	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	71	6C	TEC	720-EL	INR	4C	13.93	.00	5			38	RESULT OF DISCREPANCY RESOLUTION
92-May	2	71	6C	TEH	720-ZM	NDD				1			10	
88-Nov	2	71	TEH	TEC	740-ED	MBM	4C	13.20	.00	6	.27	61	51	
	9	71	TEH	TEC	720-EL	INR	2C	29.75	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	9	71	TEH	TEC	740-ED	MBM	2C	29.60	.00	6	.51	108	47	RESULT OF DISCREPANCY RESOLUTION
	10	71	TEH	TEC	720-EL	INR	BPH	2.46	.00	6			34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	10	71	TEH	TEC	740-ED	MBM	BPH	2.52	.00	6	.51	64	45	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	27	72	TEH	TEC	720-EL	ANR	AV6	1.42	.00	M1			34	RESULT OF DISCREPANCY RESOLUTION
	27	72	TEH	TEC	720-EL	ANF	6C	24.00	.00	1			34	RESULT OF DISCREPANCY RESOLUTION
90-Sep	27	72	TEH	TEC	740-ZS	NDD				1			8	
88-Nov	27	72	TEH	TEC	740-ED	DNT	6C	24.00	.00	M1	3.18	184	20	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	73	6C	TEC	720-EL	INR	1C	20.15	.00	6			38	
92-May	2	73	6C	TEH	720-ZM	NDD				1			10	
88-Nov	2	73	TEH	TEC	740-ED	MBM	1C	20.19	.00	6	.32	95	51	
	18	73	TEH	TEC	720-EL	INR	4C	26.62	.00	6			34	
88-Nov	18	73	TEH	TEC	740-ED	MBM	4C	26.63	.00	6	.41	105	12	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	27	73	TEH	TEC	720-EL	ANR	AV6	1.58	.00	M1			34	RESULT OF DISCREPANCY RESOLUTION
	27	73	TEH	TEC	720-EL	ANF	6C	23.74	.00	1			34	RESULT OF DISCREPANCY RESOLUTION
88-Nov	27	73	TEH	TEC	740-ED	DNT	6C	23.75	.00	M1	3.45	183	20	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	37	73	TEH	TEC	720-EL	ANR	3C	28.40	.00	M1			8	RESULT OF DISCREPANCY RESOLUTION
92-May	37	73	TEC	TEH	740-ZM	NDD				1			5	
88-Nov	37	73	TEH	TEC	740-ED	DNT	3C	28.68	.00	M1	4.35	185	29	
	7	74	TEH	TEC	720-EL	INR	2C	3.26	.00	6			34	
88-Nov	7	74	TEH	TEC	740-ED	MBM	2C	3.27	.00	6	.37	89	49	
	16	75	TEH	TEC	720-EL	INR	4H	44.30	.00	6			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	16	75	TEH	TEC	740-ED	MBM	4H	44.28	.00	6	.73	82	54	RESULT OF DISCREPANCY RESOLUTION
88-Nov	16	75	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	24	75	TEH	TEC	720-EL	ANR	BPH	5.13	.00	1			32	RESULT OF DISCREPANCY RESOLUTION
92-May	24	75	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	24	75	TEH	TEC	740-ED	DNT	BPH	5.10	.00	M1	3.92	187	15	RESULT OF DISCREPANCY RESOLUTION
	27	75	TEH	TEC	720-EL	ANR	6C	23.58	.00	1			32	RESULT OF DISCREPANCY RESOLUTION
88-Nov	27	75	TEH	TEC	740-ED	DNT	6C	23.58	.00	M1	3.12	182	20	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	35	75	TEH	TEC	720-EL	ANR	6H	6.12	.00	M1			8	
[illegible]-Nov	35	75	TEH	TEC	740-ED	DNT	6H	5.80	.00	M1	3.25	185	23	RESULT OF DISCREPANCY RESOLUTION
	2	76	6H	TEH	720-EL	INR	5H	22.57	.00	6			23	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	76	TEH	TEC	740-ED	MBM	5H	22.57	.00	6	.65	110	5[illegible]	
	16	76	TEH	TEC	720-EL	MBM	2H	11.91	.00	6	2.04	68	34	RESULT OF BASELINE DATA REVIEW
	16	76	TEH	TEC	720-EL	INR	3H	34.83	.00	6			34	
88-Nov	16	76	TEH	TEC	740-ED	MBM	2H	11.90	.00	6	.61	77	11	RESULT OF DISCREPANCY RESOLUTION
88-Nov	16	76	TEH	TEC	740-ED	MBM	3H	34.82	.00	6	.42	290	11	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	7	77	TEH	TEC	720-EL	INR	5H	6.72	.00	6			32	
88-Nov	7	77	TEH	TEC	740-ED	MBM	5H	6.72	.00	6	.40	97	49	
	26	77	TEH	TEC	720-EL	MBM	3H	41.65	.00	6	2.66	70	34	RESULT OF BASELINE DATA REVIEW
	26	77	TEH	TEC	720-EL	INR	4H	17.19	.00	6			34	
88-Nov	26	77	TEH	TEC	740-ED	MBM	3H	41.65	.00	6	.75	77	20	
88-Nov	26	77	TEH	TEC	740-ED	MBM	4H	17.20	.00	6	.41	265	20	RESULT OF DISCREPANCY RESOLUTION
	27	77	TEH	TEC	720-EL	INR	1H	12.39	.00	6			34	
88-Nov	27	77	TEH	TEC	740-ED	MBM	1H	12.40	.00	6	.47	107	20	RESULT OF DISCREPANCY RESOLUTION
	6	78	TEH	TEC	720-EL	INR	2C	23.75	.00	6			34	
88-Nov	6	78	TEH	TEC	740-ED	MBM	2C	23.77	.00	6	.39	91	49	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	17	78	TEH	TEC	720-EL	INR	TSH	.00	.00	6			44	RESULT OF DISCREPANCY RESOLUTION
	17	78	TEH	TEC	720-EL	INR	1H	31.94	.00	6			44	RESULT OF DISCREPANCY RESOLUTION
88-Nov	17	78	TEH	TEC	740-ED	MBM	1H	31.93	.00	6	.49	283	11	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	17	78	TEH	TEC	740-ED	MMB	TSH	.00	709.19	6	.40	96	54	RESULT OF DISCREPANCY RESOLUTION
	16	79	TEH	TEC	720-EL	MBM	BPH	15.85	.00	6	2.32	71	38	RESULT OF BASELINE DATA REVIEW
88-Nov	16	79	TEH	TEC	740-ED	MBM	BPH	15.63	.00	6	.67	84	54	
	27	79	TEH	TEC	720-EL	INR	3H	47.88	.00	6			38	RESULT OF LAR
88-Nov	27	79	TEH	TEC	740-ED	MBM	3H	47.89	.00	6	1.49	82	20	
	32	79	TEH	TEC	720-EL	ANR	2C	21.78	.00	1			38	RESULT OF DISCREPANCY RESOLUTION
92-May	32	79	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	32	79	TEH	TEC	740-ED	DNT	2C	21.78	.00	M1	3.30	183	27	RESULT OF DISCREPANCY RESOLUTION
88-Nov	32	79	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	10	81	TEH	TEC	720-EL	INR	BPC	5.82	.00	6			42	
88-Nov	10	81	TEH	TEC	740-ED	MBM	BPC	5.82	14.68	6	.53	72	47	RESULT OF DISCREPANCY RESOLUTION
	16	81	TEH	TEC	720-EL	INR	BPH	17.56	.00	6			36	
88-Nov	16	81	TEH	TEC	740-ED	MBM	BPH	17.58	.00	6	.69	87	11	RESULT OF DISCREPANCY RESOLUTION
	13	83	TEH	TEC	720-EL	ANR	5H	42.39	.00	1			38	RESULT OF DISCREPANCY RESOLUTION
	13	83	TEH	TEC	720-EL	INR	5H	41.48	.00	6			38	RESULT OF DISCREPANCY RESOLUTION
88-Nov	13	83	TEH	TEC	740-ED	DNT	5H	42.35	.00	M1	4.01	184	2	RESULT OF DISCREPANCY RESOLUTION
88-Nov	13	83	TEH	TEC	740-ED	MBM	5H	41.48	.00	6	.37	83	2	
	24	83	TEH	TEC	720-EL	INR	2H	21.97	.00	6			36	
88-Nov	24	83	TEH	TEC	740-ED	MBM	2H	22.20	.00	6	.40	95	15	
	24	84	TEH	TEC	720-EL	ANR	6H	9.88	.00	M1			38	
88-Nov	24	84	TEH	TEC	740-ED	DNT	6H	9.90	.00	M1	4.25	189	15	RESULT OF DISCREPANCY RESOLUTION
	25	84	TEH	TEC	720-EL	ANR	6C	.63	.00	M1			38	
90-Sep	25	84	TEH	TEC	740-ZS	NDD				1			9	
88-Nov	25	84	TEH	TEC	740-ED	DNT	6C	.59	.00	M1	4.30	180	15	
	26	84	TEH	TEC	720-EL	ANR	6C	.00	.00	M1			38	RESULT OF DISCREPANCY RESOLUTION
92-May	26	84	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	26	84	TEH	TEC	740-ED	DNT	6C	.00	.00	M1	6.24	178	20	
	8	85	TEH	TEC	720-EL	INR	BPC	14.02	.00	6			40	
88-Nov	8	85	TEH	TEC	740-ED	MBM	BPC	13.99	.00	6	.32	103	47	
	22	85	TEH	TEC	720-EL	ANR	6C	.57	.00	M1			44	
92-May	22	85	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	22	85	TEH	TEC	740-ED	DNT	6C	.57	.00	M1	3.02	182	13	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	85	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	23	85	TEH	TEC	720-EL	ANR	6C	.63	.00	M1			40	
88-Nov	23	85	TEH	TEC	740-ED	DNT	6C	.63	.00	M1	4.74	183	14	RESULT OF DISCREPANCY RESOLUTION
88-Nov	23	85	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	24	85	TEH	TEC	720-EL	ANR	6C	.62	.00	M1				
	24	85	TEH	TEC	720-EL	ANR	6C	-.42	.00	M1			42	
88-Nov	24	85	TEH	TEC	740-ED	DNT	6C	.62	.00	M1	5.11	183	42	
88-Nov	24	85	TEH	TEC	740-ED	DNT	6C	-.42	.00	M1	3.29	181	15	
	1	86	6C	TEC	720-EL	FSO	TSC	19.89	.00	3	1.15	19	15	
92-May	1	86	6C	TEH	700-ZM	NOD				1			40	RESULT OF BASELINE DATA REVIEW
92-May	1	86	6H	TEH	720-ZM	NOD				1			11	
88-Nov	1	86	6C	TEC	740-ED	MBM	TSC	19.88	.00	6	.44	213	12	
	10	86	TEH	TEC	720-EL	INR	3H	1.71	.00	6			54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	10	86	TEH	TEC	740-ED	MBM	3H	1.71	.00	6			32	
	20	86	TEH	TEC	720-EL	ANR	2H	39.13	.00	1	.47	250	47	RESULT OF DISCREPANCY RESOLUTION
	20	86	TEH	TEC	720-EL	ANR	6C	-.17	.00	M1			36	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	20	86	TEH	TEC	720-EL	ANR	6C	.62	.00	M1			36	
	20	86	TEH	TEC	720-EL	ANR	2H	39.13	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
	20	86	TEH	TEC	720-EL	ANR	6C	.60	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
	20	86	TEH	TEC	720-EL	ANR	6C	-.37	.00	M1			40	
90-Sep	20	86	TEH	TEC	740-ZS	NOD				1			40	
88-Nov	20	86	TEH	TEC	740-ED	DNT	2H	39.14	.00	M1	3.02	190	9	
88-Nov	20	86	----------											RESULT OF DISCREPANCY RESOLUTION
88-Nov	20	86	TEH	TEC	740-ED	DNT	6C	.66	.00	M1	4.91	186	12	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	20	86	----------											RESULT OF DISCREPANCY RESOLUTION
88-Nov	20	86	TEH	TEC	740-ED	DNT	6C	-.36	.00	M1	3.03	184	12	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	21	86	TEH	TEC	720-EL	ANR	6C	.71	.00	M1			12	RESULT OF DISCREPANCY RESOLUTION
	21	86	TEH	TEC	720-EL	ANR	6C	-.31	.00	M1			36	
88-Nov	21	86	TEH	TEC	740-ED	DNT	6C	.63	.00	M1	6.24	183	36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	21	86	TEH	TEC	740-ED	DNT	6C	-.53	.00	M1	4.14	182	13	RESULT OF DISCREPANCY RESOLUTION
	22	86	TEH	TEC	720-EL	ANR	6C	.65	.00	M1			13	
	22	86	TEH	TEC	720-EL	ANR	6C	-.37	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	86	TEH	TEC	740-ED	DNT	6C	.65	.00	M1	6.17	182	36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	22	86	TEH	TEC	740-ED	DNT	6C	-.50	.00	M1	4.62	183	13	
	23	86	TEH	TEC	720-EL	DNT	6C	.68	.00	M1	5.69	177	13	
	23	86	TEH	TEC	720-EL	ANR	6C	-.43	.00	M1			40	
	23	86	6C	6C	720-ZP	DNT	6C	.65	.00	2	9.33	186	40	
90-Sep	23	86	TEH	TEC	740-ZS	DNT	6C	.68	.00	M1	6.36	175	56	
88-Nov	23	86	TEH	TEC	740-ED	DNT	6C	.63	.00	M1	8.20	182	9	
88-Nov	23	86	TEH	TEC	740-ED	DNT	6C	-.44	.00	M1	4.60	182	15	

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
	1	87	6C	TEC	720-EL	INR	1C	23.46	.00	6			40	
88-Nov	1	87	6C	TEC	740-ED	MBM	1C	23.34	.00	6	.51	87	54	
	2	87	6H	TEH	720-EL	INR	BPH	12.40	.00	6			23	
	2	87	6H	TEH	720-EL	INR	2H	33.30	.00	6			23	
	2	87	6H	TEH	720-EL	INR	2H	44.00	.00	6			23	
	2	87	6H	TEH	720-EL	INR	4H	23.20	.00	6			23	
88-Nov	2	87	TEH	TEC	740-ED	MBM	BPH	12.40	.00	6	.44	66	49	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	87	TEH	TEC	740-ED	MBM	2H	33.30	.00	6	.42	74	49	
88-Nov	2	87	TEH	TEC	740-ED	MBM	2H	44.00	.00	6	.45	75	49	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	87	TEH	TEC	740-ED	MBM	4H	23.20	.00	6	.52	63	49	RESULT OF DISCREPANCY RESOLUTION
	6	87	TEH	TEC	720-EL	MBM	3C	45.93	.00	6	2.55	75	40	
88-Nov	6	87	TEH	TEC	740-ED	MBM	3C	45.96	.00	6	.72	84	49	RESULT OF BASELINE DATA REVIEW
	18	87	TEH	TEC	720-EL	ANR	6C	-.34	.00	M1			36	
88-Nov	18	87	TEH	TEC	740-ED	DNT	6C	-.50	.00	M1	3.36	179	11	RESULT OF DISCREPANCY RESOLUTION
	19	87	TEH	TEC	720-EL	ANR	6C	.71	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
	19	87	TEH	TEC	720-EL	ANR	6C	-.34	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
92-May	19	87	TEC	TEH	740-ZM	NOD				1			6	
88-Nov	19	87	TEH	TEC	740-ED	DNT	6C	.66	.00	M1	5.62	186	12	RESULT OF DISCREPANCY RESOLUTION
[illegible]Nov	19	87	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
[illegible]v	19	87	TEH	TEC	740-ED	DNT	6C	-.36	.00	M1	3.69	184	12	RESULT OF DISCREPANCY RESOLUTION
[illegible]Nov	19	87	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	20	87	TEH	TEC	720-EL	ANR	6C	.68	.00	M1			38	
	20	87	TEH	TEC	720-EL	ANR	6C	-.37	.00	M1			38	
88-Nov	20	87	TEH	TEC	740-ED	DNT	6C	.69	.00	M1	6.66	186	12	RESULT OF DISCREPANCY RESOLUTION
88-Nov	20	87	TEH	TEC	740-ED	DNT	6C	-.38	.00	M1	4.75	185	12	RESULT OF DISCREPANCY RESOLUTION
	21	87	TEH	TEC	720-EL	DNT	6C	.68	.00	M1	5.73	178	38	
	21	87	TEH	TEC	720-EL	ANR	6C	-.34	.00	M1			38	
	21	87	6C	6C	720-ZP	DNT	6C	.69	.00	2	11.89	185	56	
88-Nov	21	87	TEH	TEC	740-ED	DNT	6C	.68	.00	M1	8.16	182	13	
88-Nov	21	87	TEH	TEC	740-ED	DNT	6C	-.55	.00	M1	5.18	182	13	
	14	88	TEH	TEC	720-EL	ANR	6C	.00	.00	M1			36	
90-Sep	14	88	TEH	TEC	740-ZS	NOD				1			9	
88-Nov	14	88	TEH	TEC	740-ED	DNT	6C	.00	.00	M1	4.23	178	3	RESULT OF DISCREPANCY RESOLUTION
	15	88	TEH	TEC	720-EL	ANR	6C	-.37	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
	15	88	----------											RESULT OF LAR
	15	88	----------											RESULT OF BASELINE DATA REVIEW
	15	88	TEH	TEC	720-EL	ANR	5C	.68	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
	15	88	----------											RESULT OF LAR
	15	88	----------											RESULT OF BASELINE DATA REVIEW
88-Nov	15	88	TEH	TEC	740-ED	DNT	5C	48.05	.00	M1	3.59	180	3	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
88-Nov	15	88	TEH	TEC	740-ED	DNT	5C	.64	.00	M1	3.55	183	3	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	16	88	TEH	TEC	720-EL	ANR	6C	.71	.00	M1			36	
	16	88	TEH	TEC	720-EL	ANR	6C	-.25	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	16	88	TEH	TEC	740-ED	DNT	6C	.38	.00	M1	5.27	185	11	
88-Nov	16	88	TEH	TEC	740-ED	DNT	6C	-.50	.00	M1	4.57	182	11	RESULT OF DISCREPANCY RESOLUTION
	17	88	TEH	TEC	720-EL	ANR	6C	.88	.00	M1			36	
	17	88	TEH	TEC	720-EL	ANR	6C	-.34	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
90-Sep	17	88	TEH	TEC	740-ZS	NDD				:			9	
88-Nov	17	88	TEH	TEC	740-ED	DNT	5C	52.00	.00	M1	3.56	180	11	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
88-Nov	17	88	TEH	TEC	740-ED	DNT	6C	.70	.00	M1	3.00	180	53	RESULT OF DISCREPANCY RESOLUTION
88-Nov	17	88	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	18	88	TEH	TEC	720-EL	ANR	6C	.68	.00	M1			38	
92-May	18	88	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	18	88	TEH	TEC	740-ED	DNT	6C	.64	.00	M1	4.04	181	53	RESULT OF DISCREPANCY RESOLUTION
88-Nov	18	88	----------											RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	1	89	6C	TEC	720-EL	INR	1C	18.79	.00	6			40	
92-May	1	89	6C	TEH	700-ZM	NDD				1			11	
92-May	1	89	6H	TEH	720-ZM	NDD				1			12	
[illegible]ov	1	89	6C	TEC	740-ED	MBM	1C	18.78	.00	6	.51	2[illegible]7	54	
	15	89	TEH	TEC	720-EL	ANR	6C	.00	.00	M1			38	RESULT OF DISCREPANCY RESOLUTION
92-May	15	89	TEC	TEH	740-ZM	NDD				1			6	
88-Nov	15	89	TEH	TEC	740-ED	DNT	6C	.00	.00	M1	5.22	178	3	RESULT OF DISCREPANCY RESOLUTION
	16	89	TEH	TEC	720-EL	ANR		.46	.00	M1			38	RESULT OF DISCREPANCY RESOLUTION
	16	89	TEH	TEC	720-EL	ANR	6C	-.31	.00	M1			38	RESULT OF DISCREPANCY RESOLUTION
88-Nov	16	89	TEH	TEC	740-ED	DNT	6C	.38	.00	M1	5.32	184	11	
88-Nov	16	89	TEH	TEC	740-ED	DNT	6C	-.50	.00	M1	3.96	181	11	RESULT OF DISCREPANCY RESOLUTION
	12	90	TEH	TEC	720-EL	ANR	5H	.00	.00	M1			36	RESULT OF DISCREPANCY RESOLUTION
88-Nov	12	90	TEH	TEC	740-ED	DNT	5H	.00	.00	M1	3.19	177	3	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	91	6C	TEC	720-EL	MBM	4C	24.46	.00	6	2.58	76	42	RESULT OF BASELINE DATA REVIEW
	2	91	6C	TEC	720-EL	INF	4C	23.88	.00	6			42	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	91	6H	TEC	720-ED	MBM	4C	23.88	.00	6	.73	109	58	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	2	92	6C	6H	680-ZU	DNG	6C	.93	.00	2	.73	196	21	RESULT OF DISCREPANCY RESOLUTION
	2	92	6C	TEC	720-EL	ANR	6C	.45	.00	M1			42	
	2	92	6H	5C	680-EF	ANR	6C	.71	.00	M1			48	RESULT OF DISCREPANCY RESOLUTION
88-Nov	2	92	6H	TEC	740-ED	DNT	6C	.71	.00	M1	5.23	183	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	3	92	6C	TEC	720-EL	ANR	6C	.59	.00	M1			42	
	3	92	6H	5C	680-EF	ANR	6C	.66	.00	M1			48	RESULT OF DISCREPANCY RESOLUTION
90-Sep	3	92	6C	TEC	740-ZS	NDD				1			9	

DATE ROW COL CEB CEE PROBE IND LOC INCH1 INCH2 CHAN VOLTS DEG TAPE COMMENTS

DATE	ROW	COL	CEB	CEE	PROBE	IND	LOC	INCH1	INCH2	CHAN	VOLTS	DEG	TAPE	COMMENTS
90-Sep	3	92	TEH	TEC	720-ZS	NDD				1			11	
88-Nov	3	92	6H	TEC	740-ED	DNT	6C	.66	.00	M1	4.93	183	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	4	92	TEH	TEC	720-EL	ANR	6C	.66	.00	M1			42	
88-Nov	4	92	TEH	TEC	740-ED	DNT	6C	.68	.00	M1	5.03	183	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION
	5	92	TEH	TEC	720-EL	ANR	6C	.80	.00	M1			42	
90-Sep	5	92	TEH	TEC	740-ZS	NDD				1			9	
88-Nov	5	92	TEH	TEC	740-ED	DNT	6C	.61	.00	M1	3.29	185	54	RESULT OF 3RD PARTY DISCREPANCY RESOLUTION

| DATE | ROW | COL | CEB | CEE | PROBE | IND | LOC | INCH1 | INCH2 | CHAN | VOLTS | DEG | TAPE | COMMENTS |