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PLANT OPERATIONS & BETTERMENT SERVICES

INDIAN POINT NO. 3
NUCLEAR POWER PLANT
BUCHANAN, NEW YORK

DOCKET NUMBER 50-286

REACTOR CONTAINMENT BUILDING
INTEGRATED LEAK RATE TEST

FINAL REPORT

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I. INTRODUCTION

A periodic Type "A" Integrated Leakage Rate Test (ILRT) was performed on the containment structure of the Power Authority of the State of New York, Indian Point Nuclear Power Plant Unit No. 3 pressurized water reactor. The "Absolute Method" of testing was used in accordance with the Code of Federal Regulations, Title 10, Part 50, Appendix J - Primary Reactor Containment Leakage Testing for Water-cooled Power Reactors; and in accordance with ANSI N45.4-1972, American National Standard, Leakage-Rate Testing of Containment Structures for Nuclear Reactors. This test was performed at a pressure in excess of the calculated peak containment internal pressure (Pa) related to the design basis accident and specified in the Technical Specifications.

This report describes and presents the results of this periodic Type "A" Leakage Rate Test including the supplemental test method utilized for verification.

II. SUMMARY

Since conducting the last Integrated Leak Rate Test (ILRT), three sets of Type "B" and "C" local leakage rate tests were performed by Power Authority of the State of New York station personnel. The tests were performed at pressures equal to or in excess of the required minimum test pressure delineated in the unit's Technical Specifications. In all cases the influent method of testing was used. Whenever the leakage measured was less than the lowest calibrated point of the flow instrument the value of the lowest calibrated point was used. Therefore, the total type B&C worst case measured leakage could not exceed those values as indicated on the individual summary sheets. (Refer to the Local Leakage Type B&C Testing attachment).

At the start of the Type "A" ILRT test, all valves were in their normal position for accident conditions with exception of those valves required to maintain the plant in a safe condition.

The reactor containment was pressurized to slightly above Pa with dry air supplied by eight industrial compressors. After allowing the reactor containment temperature to stabilize (refer to Appendix A.3), the mass of air within the reactor containment was calculated every fifteen minutes. A straight line least squares analysis was then calculated to measure the leakage rate (Lam). An upper limit of the 95 percent confidence level (UCL) was then calculated to estimate the uncertainty in Lam.

Lam was calculated to be 0.034 percent per day and the UCL was calculated to be 0.035 percent per day. The supplementary Verification Test (CLRT) results verified the measured leakage within the allowable acceptance band.

III. TEST DISCUSSION

A. Description of Containment

The reactor containment structure completely encloses the entire reactor and reactor coolant system to ensure no leakage of radioactive materials to the environment in the unlikely event of a loss of coolant accident.

The containment vessel is a reinforced concrete vertical right cylinder with a hemispherical dome and a generally flat base supported on rock. A welded steel liner with a minimum thickness of 1/4 inch is attached to the inside face of the concrete to ensure a high degree of leak tightness. Small steel channels are welded over all joints in the containment vessel liner forming leaktight air chambers. These chambers are continuously pressurized with air to serve as a leak prevention system. These channels also serve to identify any liner plate weld leakage.

The containment has side walls measuring 148 feet from the liner on the base to the spring line of the dome and has an inside diameter of 135 feet. The side walls of the cylinder and the dome are 4-1/2 feet and 3-1/2 feet thick, respectively. The inside radius of the dome is equal to the inside radius of the cylinder so that the discontinuity at the spring line due to the change in thickness is on the outer surface. The flat concrete base mat is 9 feet thick with the bottom liner plate located on top of this mat. The bottom liner plate is covered with 3 feet of concrete, the top of which forms the floor of the containment.

All penetrations made in the containment vessel were considered as potential leak sources and as such were designed with double barriers and treated by a leak prevention system. There are approximately 60 electrical penetration cannisters, 80 process piping penetrations, one personnel access airlock, one airlock/equipment hatch and one fuel transfer tube penetration.

Each process piping system which penetrates the containment vessel is designed to maintain the leak integrity of the containment vessel through the use of double leaktight barriers. The design of process piping isolation barriers is such that no single active failure degrades the leak tightness of the containment vessel. An Isolation Valve Seal Water System is provided as a leak prevention system.

The containment vessel, penetrations and isolation valves are aligned to simulate accident conditions for the performance of the Integrated Leak Rate Test. An extra degree of conservatism in testing is provided by not using the Isolation Valve Seal Water or the Channel Weld and Penetration Pressurizing Systems during the Integrated Leak Rate Test.

The containment vessel and all associated isolation valves, penetrations and support systems have been designed to limit leakage to 0.1 percent by weight of the contained air per day at 47 PSIG. The calculated peak accident pressure is 40.6 PSIG with a calculated temperature of 247°F. The containment free volume is 2.61×10^6 cubic feet.

B. Description of Instrumentation

A "state-of-the-art" ILRT instrumentation package was utilized to allow leakage rate determination by the "Absolute Method." The primary measurement variables include containment pressure, humidity and temperature as a function of time. Ancillary measurements include ambient outside pressure and temperature. During the supplemental CLRT, containment bleed-off flow is also measured. Instrument readings were output at 15-minute intervals automatically via a data logger and printer.

1. Temperature Instrumentation

Thirty precision Resistance Temperature Detectors (RTDs) were located throughout the containment to allow measurement of the volumetrically weighted average temperature. The location of the temperature detectors in the containment is depicted in Figure 1. The calibrated accuracy of the RTDs is ± 0.1°F. The sensitivity of the sensor is quoted as 0.01°F.

2. Humidity Instrumentation

Ten Resistance Humidity Detectors (RHDs) were located throughout the containment to allow measurement of the volumetrically weighted average containment vapor pressure. The location of the RHDs in the containment is depicted in Figure 2. The calibrated accuracy of the RHDs is ± 2.5 percent RH. The sensitivity of the sensor is quoted as ± 0.1 percent RH.

3. Pressure Instrumentation

Two precision quartz bourdon tube pressure indicators were supplied in the instrumentation package for the determination of containment absolute pressure. One precision pressure indicator was used as the primary sensor while the second indicator was considered as a backup. The calibrated accuracy of the precision pressure indicators is ± 0.015 PSIA. The sensitivity of the instrument is quoted as ± 0.001 PSIA.

4. Flow Instrumentation

One float-type meter was used to superimpose the leakage for the verification test. The accuracy of the instrument is ± 0.1 scfm which is equivalent to ± 0.0014 precent per day and the repeatability is ± 0.05 scfm which is equivalent to ± 0.0007 percent per day.

5. Ancillary Instrumentation

The ambient outside temperature at the site was measured using a precision RTD with the same specifications as RTD's above. The ambient barometric pressure was measured with a pressure indicator with an accuracy of ± 0.07 PSIA. The repeatability of the instrument is quoted as ± 0.03 PSIA.

Sensor data was recorded through a data acquisition system that scanned sensor channels every 15 minutes and used an 18-column digital printer to record sensor indications. The printed data was then manually entered into the computer program via a computer terminal.

C. Description of the Computer Program

The Ebasco ILRT computer program is an interactive Fortran IV program written specifically for fast, easy utilization during all phases of the ILRT and CLRT. Data entry and modifications, if necessary, are readily accomplished by the data acquisition team. In addition to extensive data verification routines, the program calculates, on demand, total time and mass point leak rates as well as the 95 percent Upper Confidence Level for these leakage rate calculations.

Data rejection based upon the Chauvenet criterion may be utilized in the analysis, if required.

Data evaluations are enhanced by the flexible display of either sensor variables or various computed values in tabular or graphical form on the computer terminal. Data is recorded on tape to prevent loss during the testing. All data is stored on the computer systems in use with retrieval capability to any desired data base throughout the testing.

Temperature, pressure and humidity data are entered interactively via the computer terminal at 15-minute intervals. Computer verification and checking routines supplement data verification by the data acquisition team. Modifications are promptly made when errors are detected. Prior to issuance of this report, further extensive data verification was performed.

D. Description of the Integrated Leakage Rate Test (ILRT)

On July 27, 1982 an inspection of the reactor containment was made listing those items that needed removal or correcting prior to pressurization. This included the removal of fire extinguishers, excess wood, deenergizing the welding machines, venting tanks and oil reservoirs, etc. These items were accomplished and a final inspection was made. In addition to the containment inspection, sensor response checks were made to ensure proper operation of all sensors and associated equipment.

Eight oil-free industrial compressors were used to produce the needed 10,000 SCFM to pressurize the reactor containment. These compressors were placed in service at 0045 hours July 30, 1982 to purge the containment in final preparation for pressurization. At 0239 July 30, 1982 pressurization commenced.

At 1600 hours July 30, 1982 an air leak was found in the main steam line of steam generator number 32. Containment pressure was 40 psia. The decision was made to continue pressurizing and the target containment pressure of 60.61 PSIA was reached at 1835 hours. A search was conducted to identify any additional leaks. The measured leakage rate during this time was 2.24 percent per day.

At 0319 hours August 1, 1982 the measured leakage rate fell to 0.033 percent per day. This was achieved by using auxiliary boiler feed water and air to pressurize steam generator number 32 to a pressure close to containment pressure. The reduction of measured leakage rate verified that steam generator number 32 was the source of excessive leakage. It was decided to depresssurize the containment and inspect the steam generator to determine the source of leakage.

After inspecting steam generator number 32 it was discovered that the upper manway cover and a temporary plug installed in a hand hole were leaking. Both items were repaired and pressurization was restarted at 0600 hours August 2, 1982.

A new target pressure of 60.31 PSIA was reached at 0037 hours August 3, 1982 and containment temperature stabilization was achieved at 0515 hours. After eight hours of data entry the calculated leakage rate was 0.036 percent per day and the containment showed good signs of stability. The remainder of the test was uneventful.

Two humidity sensor systems failed which necessitated the deletion of these sensors from the calculation of mean humidity. All other sensors performed as expected and data acquisition was normal. The last data sample for the main portion of the test was taken at 0515 hours August 4, 1982 and the measured leakage rate was 0.034 percent per day with an Upper Confidence Level of 0.035 percent per day.

E. Description of the Verification Test

The rotameter was set to an indicated 74 percent to achieve a superimposed airflow of approximately 0.10 percent per day. The average rotameter indication through the remainder of the verification test was 73.98 percent. This average is equivalent to 7.142 SCFM or 0.0986 percent per day. Data entry began at 0700 hours August 4, 1982 and the verification test was complete at 1130 hours. The computed leakage rate was 0.136 percent per day. Depressurization was then initiated and preparations began to conduct the post-test debriefing.

IV. ANALYSIS AND INTERPRETATION

The Type A Integrated Leakage Rate for the Indian Point No. 3 Nuclear Power Plant was successfully completed on August 4, 1982. The final measured Leakage Rate was 0.034 percent per day with a 95 percent Upper Confidence Level of 0.035 percent per day. The acceptance criteria (0.75 La) is 0.075 percent per day. The verification test which followed induced a 0.0986 percent per day superimposed leakage. The measured leakage rate was then calculated to be 0.136 percent per day; well within the verification criteria band of 0.107 percent per day and 0.157 percent per day. (Refer to Appendix A.1 & A.2)

The first pressurization had detected a leakage of 2.24 percent per day, above the acceptance criteria of 0.075 percent per day. The suspected leakage in steam generator number 32 was confirmed when the isolation of this system drastically lowered the measured leakage rate to 0.033 percent per day. After repairs were made the second pressurization proved the success of the steam generator repairs.

The leakage in steam generator number 32 was identified to be an improperly installed steam side access manway and a temporary plug on a steam side hand hole.

The leakage found on steam generator number 32 was induced during maintenance in the refueling outage and in no means is an indication of containment leakage during prior and subsequent power operation. The steam generator would have received leak tests subsequent to maintenance and the improperly installed equipment would have been discovered prior to power operation. Excess leakage measured during the period of steam generator number 32 leakage is not considered a failed ILRT.

The Instrumentation Selection Guide (ISG) was calculated to be 0.00272 percent before the test and the acceptance critieria for the ISG is .25 La or 0.025 percent. This clearly indicated that the ISG was acceptable to begin the ILRT.

During the test, number 1 and 7 humidity sensor systems failed which necessitated the deletion of these sensors in the calculation of mean humidity. These two failures were immediate and total failures, not a slow degradation of indications. The post test ISG was calculated to be 0.00284 percent and the ISG continued to remain below the acceptance criteria.

After the second pressurization, temperature was monitored closely and the reactor containment reached temperature stabilization at 0515 hours August 3, 1982 (refer to Appendix A.3). At that time the ILRT officially commenced.

The main test continued until 0515 hours August 4, 1982 allowing 24 hours of data and 97 samples to be used as the bases for leakage rate calculation. Appendix (A.1) shows in table and graphic form the sensor values and resultant calculations. The plot titled "Containment Air Masses" shows a smooth straight line trend in containment mass and possessed no unusual outlying points. The slope of the regression line of these mass points is the leakage rate. The "Computed Leak Rate" plot displays the fitted mass point calculation of leakage rate and its relationship to simple mass point (total time) calculations as the test progressed. It is easy to see that these two calculations became closer in value as the test progressed. The next plot, "Computed Leak Rates Relative to Limits" shows the relationship between computed leakage rates and the acceptance criteria. This plot depicts the measured leakage rate and the UCL as it progressed through the test and notably well below established limits.

The Verification Test (CLRT) tables and plots in Appendix (A.2) show that the CLRT progressed smoothly and the results fell well within acceptance limits.

Once the steam generator leaks were repaired, the test progressed very nicely. The data was stable and the instrumentation worked as expected enabling accurate analysis. The test results clearly show that the reactor containment leakage rate was markedly below maximum limitations.

FIGURES

POWER AUTHORITY OF THE STATE OF NEW YORK
INDIAN POINT UNIT NO. 3 ILRT
RTD LOCATION/VOLUME

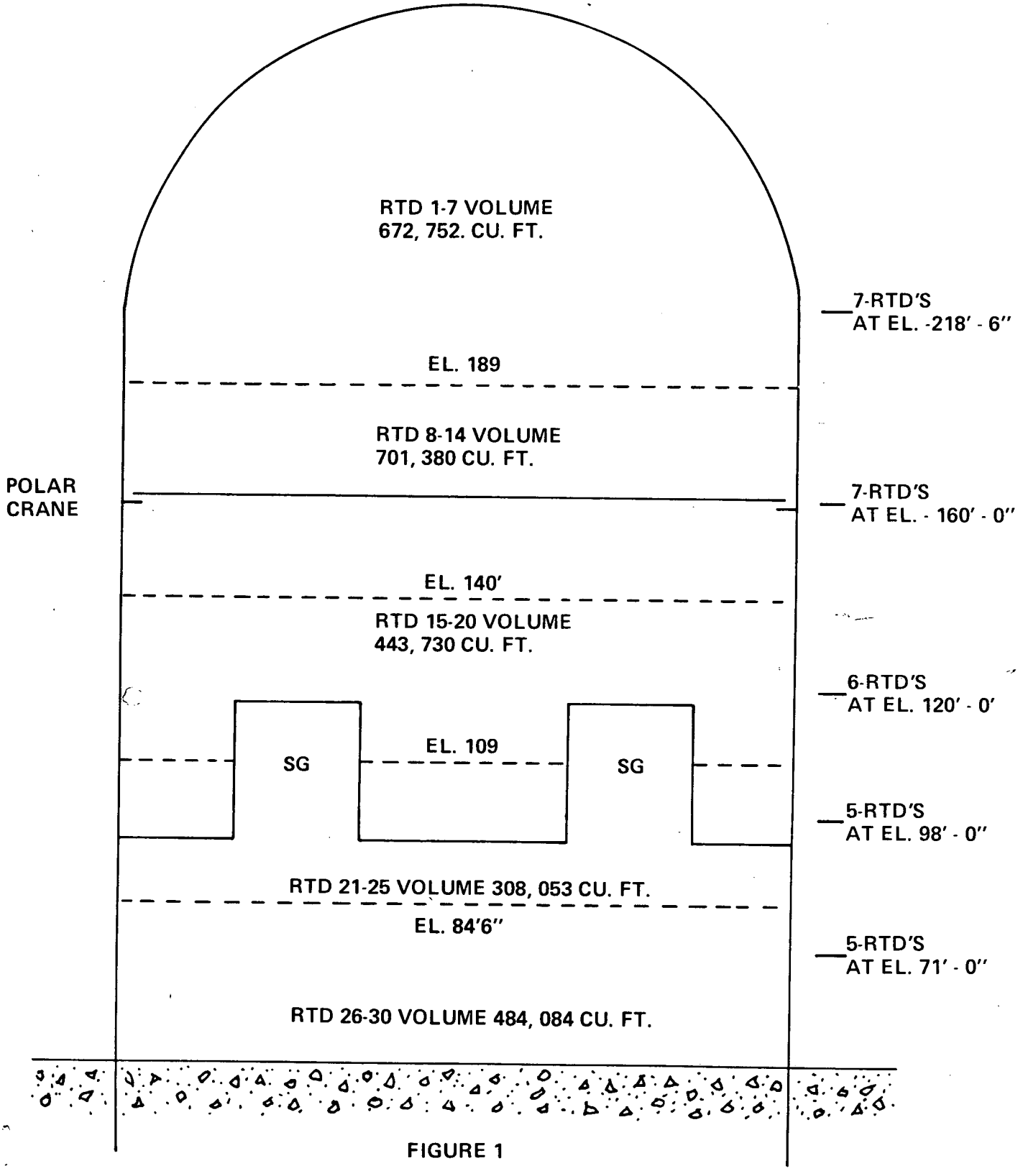


FIGURE 1

POWER AUTHORITY OF THE STATE OF NEW YORK
INDIAN POINT UNIT NO. 3 ILRT
RHD LOCATION/VOLUME

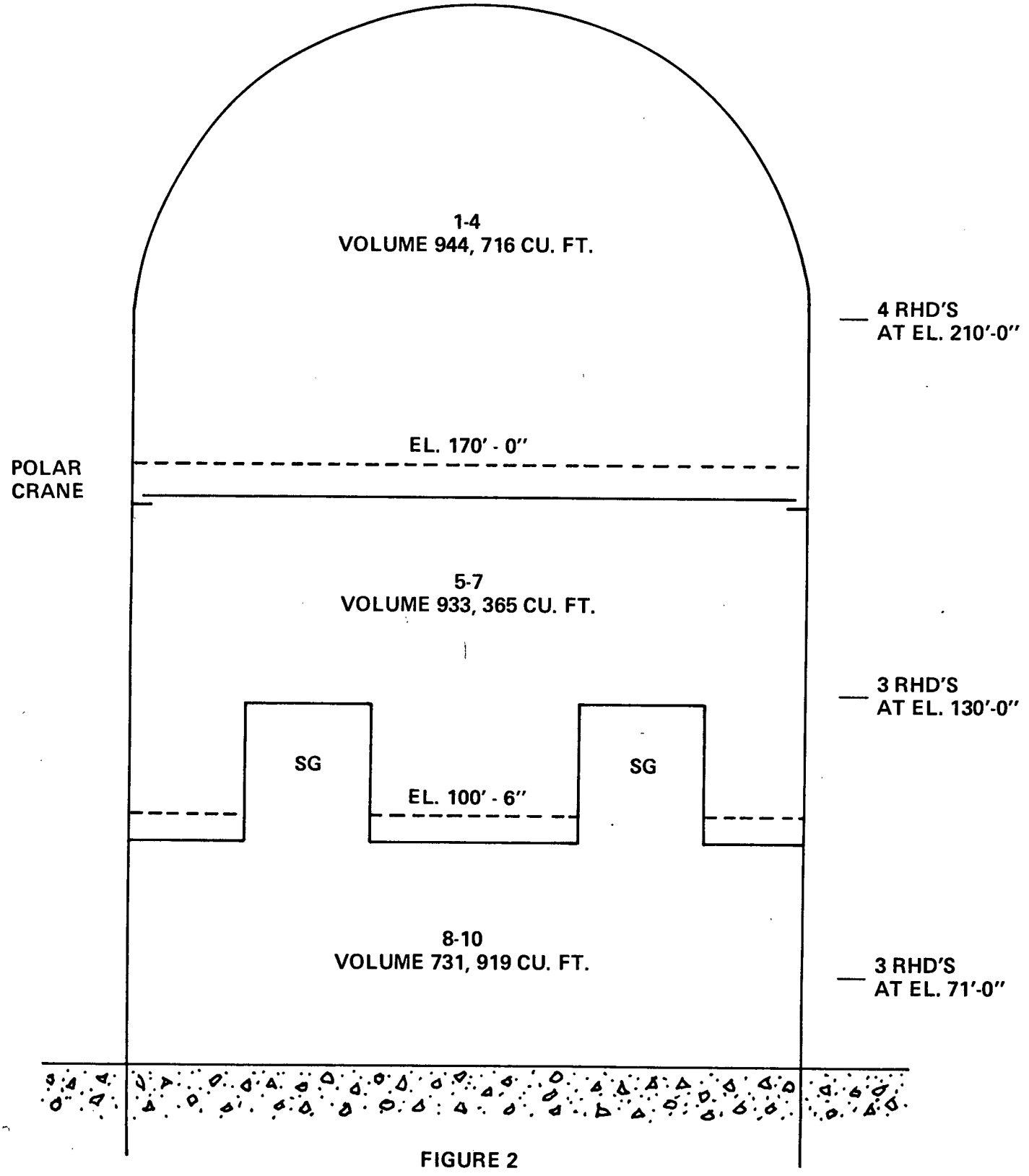


FIGURE 2

POWER AUTHORITY OF THE STATE OF NEW YORK
INDIAN POINT UNIT NO. 3 ILRT
CONTAINMENT PRESSURIZATION SYSTEM

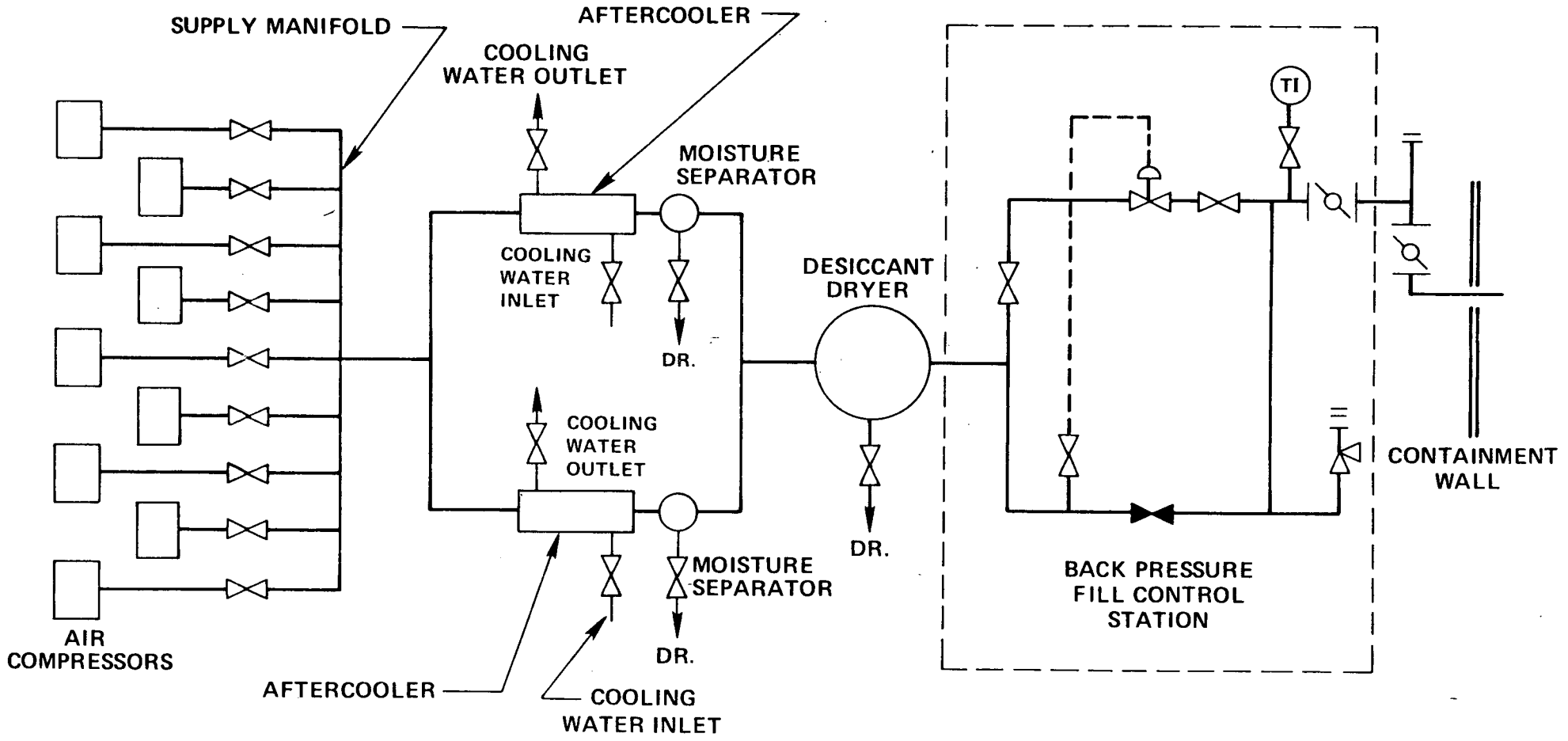


FIGURE 3

APPENDIX A.1

COMPUTER GENERATED REPORT

INTEGRATED LEAK RATE TEST (ILRT)

POWER AUTHORITY STATE OF NEW YORK
ILRT INDIAN POINT 3

CONTAINMENT INTEGRATED LEAKAGE RATE TEST
LEAKAGE RATE MEASURED USING THE ABSOLUTE METHOD
LEAKAGE RATE COMPUTED USING THE MASS POINT METHOD

TEST PERIOD STARTED AT 515 HOURS ON AUGUST 3,1982
TEST CONDUCTED FOR 24.00 HOURS

FREE SPACE VOLUME OF CONTAINMENT IS 2610000 CU FT
CONTAINMENT WAS PRESSURIZED TO 59.63 PSIA

INITIAL CONTAINMENT AIR WEIGHT 754320.7 LBS
FINAL CONTAINMENT AIR WEIGHT 754054.4 LBS
FITTED MASS POINT LEAKAGE RATE IS 0.034 % PER DAY
UPPER LIMIT OF 95% CONFIDENCE LEVEL IS 0.035 % PER DAY
NRC MAXIMUM ALLOWABLE LEAKAGE RATE IS 0.100 % PER DAY

DESCRIPTION OF VARIABLES

AVG. TEM - CONTAINMENT MEAN TEMPERATURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RTD SENSOR INDICATIONS.
AVE. PRE - PRIMARY CONTAINMENT PRESSURE INDICATION.
VAP. PRE - CONTAINMENT VAPOR PRESSURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RHD SENSOR INDICATIONS.
LEAK SIM - SIMPLE TOTAL TIME LEAKAGE RATE.
LEAK MAS - LEAKAGE RATE COMPUTED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.
AIR MASS - CONTAINMENT AIR MASS.

NOTE FOR TABULAR DATA -
TABLE VALUES OF ZERO SIGNIFY EITHER.

1. DATA IS NOT APPLICABLE TO THE CALCULATION OR
2. SENSOR HAS BEEN DELETED FROM THE SCAN.

NOTE FOR CURVES -

1. TOP ABSCISSA SCALE REPRESENTS SAMPLE NUMBERS.
2. AIR MASS IS THE CALCULATED CONTAINMENT AIR MASS AND FITTED AIR MASS IS THE LINEAR LEAST SQUARE FIT OF THE AIR MASSES.
3. SIMPLE MASS POINT IS THE TOTAL TIME LEAKAGE RATE AND FITTED MASS POINT IS THE LEAKAGE RATE COMPUTED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.
4. UCL IS THE UPPER LIMIT OF THE 95% CONFIDENCE LEVEL OF AIR MASS DATA.

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	AVG. TEM DEG. F	AVG. PRE PSIA	VAP. PRE PSIA	LEAK SIM PER CENT	LEAK MAS PER CENT	AIR MASS POUNDS
1	0	92.966	59.6349	0.4556	0.000	0.000	754321
2	15	92.873	59.6238	0.4552	0.104	0.000	754313
3	30	92.783	59.6147	0.4562	0.084	0.084	754307
4	45	92.701	59.6056	0.4560	0.069	0.068	754304
5	60	92.625	59.5975	0.4562	0.056	0.055	754303
6	75	92.557	59.5895	0.4567	0.083	0.071	754288
7	90	92.476	59.5814	0.4567	0.055	0.060	754295
8	105	92.403	59.5743	0.4576	0.050	0.052	754293
9	120	92.344	59.5673	0.4574	0.055	0.051	754286
10	135	92.282	59.5602	0.4579	0.066	0.056	754274
11	150	92.211	59.5542	0.4568	0.016	0.036	754308
12	165	92.151	59.5481	0.4574	0.018	0.025	754305
13	180	92.105	59.5421	0.4572	0.030	0.023	754293
14	195	92.056	59.5350	0.4580	0.060	0.033	754260
15	210	92.003	59.5300	0.4563	0.028	0.028	754290
16	225	91.958	59.5249	0.4573	0.039	0.029	754274
17	240	91.908	59.5199	0.4579	0.040	0.031	754270
18	255	91.869	59.5148	0.4570	0.037	0.031	754271
19	270	91.826	59.5098	0.4573	0.042	0.032	754261
20	285	91.781	59.5058	0.4571	0.031	0.031	754274
21	300	91.740	59.5017	0.4566	0.023	0.027	754285
22	315	91.708	59.4967	0.4575	0.041	0.029	754253
23	330	91.663	59.4926	0.4571	0.031	0.028	754267
24	345	91.635	59.4896	0.4568	0.028	0.027	754271
25	360	91.599	59.4856	0.4571	0.029	0.026	754265
26	375	91.574	59.4815	0.4571	0.038	0.028	754247
27	390	91.533	59.4785	0.4574	0.029	0.027	754261
28	405	91.515	59.4745	0.4577	0.042	0.029	754231
29	420	91.480	59.4715	0.4580	0.039	0.030	754236
30	435	91.457	59.4684	0.4579	0.040	0.031	754230
31	450	91.428	59.4644	0.4579	0.043	0.033	754219
32	465	91.403	59.4614	0.4584	0.047	0.035	754207
33	480	91.369	59.4583	0.4588	0.044	0.036	754210
34	495	91.344	59.4553	0.4580	0.041	0.037	754216
35	510	91.321	59.4523	0.4588	0.046	0.038	754198
36	525	91.306	59.4493	0.4586	0.050	0.040	754182
37	540	91.270	59.4472	0.4581	0.038	0.040	754213
38	555	91.252	59.4432	0.4583	0.048	0.041	754182
39	570	91.213	59.4412	0.4579	0.035	0.040	754215
40	585	91.195	59.4392	0.4579	0.035	0.039	754215
41	600	91.171	59.4361	0.4578	0.036	0.039	754209
42	615	91.152	59.4331	0.4580	0.039	0.039	754196
43	630	91.134	59.4301	0.4586	0.045	0.039	754174
44	645	91.108	59.4281	0.4587	0.041	0.040	754181
45	660	91.085	59.4271	0.4588	0.035	0.039	754198
46	675	91.064	59.4240	0.4587	0.037	0.039	754191
47	690	91.049	59.4220	0.4588	0.038	0.039	754183
48	705	91.027	59.4200	0.4594	0.038	0.038	754181
49	720	91.004	59.4180	0.4595	0.036	0.038	754184
50	735	90.984	59.4150	0.4598	0.039	0.038	754170

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	AVG. TEM DEG. F	AVG. PRE PSIA	VAP. PRE PSIA	LEAK SIM PER CENT	LEAK MAS PER CENT	AIR MASS POUNDS
51	750	90.970	59.4140	0.4599	0.037	0.038	754174
52	765	90.949	59.4119	0.4601	0.036	0.038	754176
53	780	90.928	59.4099	0.4603	0.036	0.037	754175
54	795	90.917	59.4089	0.4607	0.036	0.037	754171
55	810	90.895	59.4069	0.4608	0.034	0.037	754175
56	825	90.866	59.4059	0.4610	0.028	0.036	754200
57	840	90.858	59.4049	0.4616	0.030	0.035	754189
58	855	90.846	59.4029	0.4617	0.032	0.035	754179
59	870	90.827	59.4008	0.4620	0.032	0.034	754176
60	885	90.812	59.3988	0.4621	0.033	0.034	754169
61	900	90.802	59.3968	0.4620	0.034	0.034	754158
62	915	90.785	59.3958	0.4622	0.032	0.033	754166
63	930	90.768	59.3938	0.4629	0.034	0.033	754155
64	945	90.761	59.3918	0.4629	0.037	0.033	754139
65	960	90.741	59.3908	0.4630	0.034	0.033	754151
66	975	90.730	59.3887	0.4633	0.036	0.033	754137
67	990	90.716	59.3877	0.4636	0.035	0.033	754139
68	1005	90.701	59.3867	0.4639	0.034	0.033	754144
69	1020	90.697	59.3847	0.4644	0.038	0.034	754118
70	1035	90.678	59.3837	0.4650	0.037	0.034	754122
71	1050	90.666	59.3827	0.4654	0.036	0.034	754121
72	1065	90.650	59.3817	0.4649	0.033	0.034	754136
73	1080	90.638	59.3807	0.4656	0.034	0.033	754130
74	1095	90.629	59.3797	0.4655	0.033	0.033	754131
75	1110	90.613	59.3776	0.4664	0.035	0.033	754117
76	1125	90.597	59.3766	0.4664	0.033	0.033	754126
77	1140	90.598	59.3756	0.4670	0.036	0.033	754103
78	1155	90.575	59.3746	0.4666	0.032	0.033	754126
79	1170	90.566	59.3736	0.4674	0.033	0.033	754116
80	1185	90.559	59.3726	0.4679	0.035	0.033	754105
81	1200	90.542	59.3716	0.4679	0.032	0.033	754117
82	1215	90.535	59.3706	0.4681	0.033	0.033	754110
83	1230	90.529	59.3686	0.4686	0.036	0.033	754087
84	1245	90.512	59.3676	0.4689	0.035	0.033	754094
85	1260	90.502	59.3666	0.4691	0.035	0.033	754091
86	1275	90.492	59.3655	0.4694	0.035	0.033	754089
87	1290	90.479	59.3645	0.4694	0.034	0.033	754092
88	1305	90.473	59.3625	0.4700	0.037	0.033	754068
89	1320	90.460	59.3625	0.4702	0.034	0.033	754084
90	1335	90.456	59.3615	0.4705	0.036	0.033	754072
91	1350	90.443	59.3595	0.4706	0.037	0.033	754062
92	1365	90.440	59.3595	0.4711	0.036	0.033	754060
93	1380	90.429	59.3575	0.4712	0.038	0.034	754048
94	1395	90.428	59.3575	0.4710	0.037	0.034	754052
95	1410	90.415	59.3555	0.4716	0.039	0.034	754036
96	1425	90.399	59.3555	0.4712	0.035	0.034	754063
97	1440	90.390	59.3544	0.4719	0.035	0.034	754054

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 1 DEG. F	TEMP 2 DEG. F	TEMP 3 DEG. F	TEMP 4 DEG. F	TEMP 5 DEG. F	TEMP 6 DEG. F
1	0	97.580	97.260	97.160	97.000	97.000	97.150
2	15	97.470	97.100	97.040	96.850	96.890	97.030
3	30	97.330	96.980	96.930	96.750	96.750	96.900
4	45	97.200	96.860	96.770	96.610	96.650	96.770
5	60	97.090	96.740	96.660	96.460	96.550	96.660
6	75	97.000	96.620	96.550	96.340	96.430	96.570
7	90	96.850	96.480	96.470	96.230	96.340	96.470
8	105	96.790	96.420	96.360	96.120	96.200	96.370
9	120	96.670	96.330	96.240	96.020	96.130	96.280
10	135	96.600	96.280	96.150	95.950	96.050	96.190
11	150	96.510	96.180	96.090	95.880	95.950	96.110
12	165	96.460	96.070	95.980	95.770	95.880	96.000
13	180	96.350	96.050	95.910	95.700	95.790	95.930
14	195	96.330	95.940	95.820	95.610	95.720	95.850
15	210	96.190	95.840	95.770	95.570	95.640	95.770
16	225	96.110	95.790	95.700	95.500	95.590	95.720
17	240	96.070	95.760	95.610	95.410	95.510	95.640
18	255	96.020	95.590	95.560	95.360	95.450	95.600
19	270	95.940	95.630	95.490	95.290	95.400	95.530
20	285	95.890	95.520	95.430	95.220	95.340	95.440
21	300	95.770	95.530	95.370	95.150	95.280	95.400
22	315	95.760	95.430	95.330	95.130	95.230	95.350
23	330	95.610	95.400	95.270	95.090	95.220	95.270
24	345	95.610	95.350	95.200	95.010	95.110	95.250
25	360	95.540	95.270	95.190	94.950	95.090	95.200
26	375	95.560	95.240	95.130	94.930	95.050	95.150
27	390	95.450	95.140	95.050	94.890	95.010	95.110
28	405	95.450	95.120	95.030	94.850	94.980	95.050
29	420	95.370	95.050	94.990	94.780	94.920	94.980
30	435	95.370	95.040	94.920	94.790	94.880	94.950
31	450	95.250	94.960	94.910	94.760	94.810	94.880
32	465	95.310	94.920	94.870	94.700	94.780	94.860
33	480	95.210	94.880	94.790	94.660	94.740	94.850
34	495	95.180	94.840	94.770	94.590	94.700	94.780
35	510	95.180	94.750	94.700	94.520	94.670	94.760
36	525	95.120	94.810	94.650	94.540	94.640	94.730
37	540	95.090	94.780	94.640	94.420	94.580	94.680
38	555	95.070	94.710	94.580	94.420	94.570	94.650
39	570	95.010	94.670	94.570	94.330	94.480	94.620
40	585	94.970	94.640	94.520	94.330	94.490	94.530
41	600	94.950	94.610	94.470	94.270	94.430	94.530
42	615	94.910	94.600	94.450	94.250	94.430	94.490
43	630	94.890	94.580	94.420	94.220	94.340	94.450
44	645	94.870	94.540	94.390	94.160	94.330	94.430
45	660	94.790	94.430	94.340	94.140	94.300	94.410
46	675	94.760	94.400	94.310	94.090	94.260	94.380
47	690	94.760	94.390	94.300	94.070	94.230	94.330
48	705	94.720	94.350	94.250	94.060	94.220	94.330
49	720	94.660	94.340	94.210	93.990	94.180	94.250
50	735	94.640	94.300	94.200	93.990	94.120	94.250

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	TEMP 1 DEG. F	TEMP 2 DEG. F	TEMP 3 DEG. F	TEMP 4 DEG. F	TEMP 5 DEG. F	TEMP 6 DEG. F
51	750	94.610	94.290	94.170	93.970	94.130	94.240
52	765	94.560	94.300	94.130	93.910	94.080	94.160
53	780	94.510	94.220	94.120	93.900	94.070	94.150
54	795	94.520	94.200	94.080	93.880	94.070	94.130
55	810	94.490	94.170	94.040	93.850	94.010	94.100
56	825	94.480	94.110	94.000	93.810	93.990	94.050
57	840	94.400	94.140	93.960	93.730	93.950	94.020
58	855	94.430	94.120	93.940	93.710	93.940	93.990
59	870	94.360	94.110	93.920	93.710	93.890	93.960
60	885	94.340	94.050	93.890	93.700	93.880	93.940
61	900	94.330	94.060	93.880	93.670	93.850	93.910
62	915	94.330	94.040	93.850	93.650	93.840	93.880
63	930	94.290	94.010	93.820	93.600	93.830	93.860
64	945	94.270	93.950	93.820	93.630	93.780	93.820
65	960	94.240	93.910	93.780	93.600	93.770	93.800
66	975	94.220	93.910	93.750	93.540	93.720	93.800
67	990	94.190	93.890	93.750	93.530	93.700	93.770
68	1005	94.170	93.870	93.720	93.520	93.670	93.730
69	1020	94.150	93.820	93.710	93.520	93.700	93.740
70	1035	94.140	93.820	93.670	93.480	93.650	93.710
71	1050	94.120	93.790	93.660	93.460	93.630	93.690
72	1065	94.090	93.780	93.630	93.430	93.600	93.680
73	1080	94.070	93.760	93.620	93.400	93.580	93.640
74	1095	94.050	93.750	93.590	93.390	93.560	93.610
75	1110	94.040	93.710	93.570	93.360	93.570	93.590
76	1125	94.020	93.710	93.580	93.350	93.530	93.610
77	1140	94.020	93.690	93.560	93.330	93.500	93.590
78	1155	93.990	93.670	93.540	93.340	93.480	93.550
79	1170	93.970	93.650	93.500	93.290	93.490	93.530
80	1185	93.960	93.670	93.490	93.280	93.480	93.520
81	1200	93.930	93.600	93.450	93.270	93.440	93.510
82	1215	93.950	93.570	93.450	93.220	93.430	93.480
83	1230	93.890	93.590	93.430	93.270	93.420	93.460
84	1245	93.880	93.550	93.400	93.190	93.420	93.440
85	1260	93.850	93.530	93.400	93.160	93.370	93.430
86	1275	93.830	93.520	93.380	93.170	93.350	93.380
87	1290	93.840	93.500	93.360	93.120	93.320	93.360
88	1305	93.830	93.500	93.350	93.130	93.330	93.360
89	1320	93.800	93.490	93.310	93.130	93.320	93.360
90	1335	93.790	93.480	93.330	93.100	93.290	93.350
91	1350	93.750	93.430	93.300	93.100	93.280	93.330
92	1365	93.750	93.410	93.280	93.080	93.260	93.310
93	1380	93.720	93.400	93.270	93.070	93.270	93.300
94	1395	93.740	93.400	93.240	93.060	93.230	93.290
95	1410	93.700	93.370	93.230	93.040	93.230	93.260
96	1425	93.680	93.340	93.200	93.030	93.200	93.260
97	1440	93.660	93.330	93.190	93.010	93.210	93.240

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 7 DEG. F	TEMP 8 DEG. F	TEMP 9 DEG. F	TEMP 10 DEG. F	TEMP 11 DEG. F	TEMP 12 DEG. F
1	0	97.480	97.030	96.890	94.580	95.830	95.900
2	15	97.350	96.890	96.780	94.440	95.660	95.750
3	30	97.200	96.770	96.620	94.340	95.560	95.640
4	45	97.110	96.630	96.530	94.200	95.420	95.490
5	60	97.010	96.530	96.410	94.100	95.360	95.410
6	75	96.870	96.410	96.290	94.000	95.240	95.300
7	90	96.770	96.310	96.200	93.870	95.140	95.190
8	105	96.690	96.200	96.090	93.790	95.000	95.050
9	120	96.600	96.090	96.010	93.710	94.920	95.000
10	135	96.500	96.000	95.920	93.610	94.840	94.880
11	150	96.420	95.930	95.800	93.520	94.740	94.770
12	165	96.310	95.830	95.740	93.420	94.650	94.720
13	180	96.260	95.770	95.650	93.330	94.570	94.660
14	195	96.190	95.650	95.570	93.300	94.490	94.530
15	210	96.110	95.590	95.480	93.200	94.430	94.460
16	225	96.040	95.500	95.440	93.130	94.360	94.400
17	240	96.000	95.460	95.370	93.050	94.310	94.350
18	255	95.910	95.390	95.300	93.010	94.220	94.270
19	270	95.870	95.320	95.220	92.930	94.170	94.200
20	285	95.810	95.240	95.160	92.890	94.090	94.160
21	300	95.730	95.170	95.120	92.810	94.020	94.060
22	315	95.670	95.100	95.060	92.760	93.930	94.050
23	330	95.620	95.080	94.970	92.710	93.920	93.950
24	345	95.550	95.040	94.910	92.660	93.890	93.920
25	360	95.500	94.970	94.870	92.600	93.790	93.870
26	375	95.480	94.890	94.820	92.540	93.760	93.830
27	390	95.370	94.860	94.760	92.470	93.690	93.780
28	405	95.360	94.810	94.710	92.440	93.670	93.710
29	420	95.280	94.760	94.680	92.420	93.620	93.680
30	435	95.250	94.700	94.610	92.340	93.540	93.630
31	450	95.220	94.680	94.590	92.310	93.520	93.580
32	465	95.200	94.630	94.540	92.250	93.470	93.540
33	480	95.130	94.580	94.490	92.200	93.440	93.450
34	495	95.090	94.530	94.430	92.150	93.390	93.470
35	510	95.070	94.480	94.410	92.110	93.360	93.430
36	525	95.050	94.460	94.370	92.090	93.330	93.390
37	540	95.020	94.420	94.340	92.050	93.270	93.310
38	555	94.980	94.380	94.290	92.020	93.260	93.320
39	570	94.910	94.310	94.240	91.980	93.210	93.280
40	585	94.870	94.310	94.220	91.920	93.190	93.250
41	600	94.860	94.260	94.180	91.890	93.140	93.210
42	615	94.800	94.230	94.140	91.870	93.110	93.180
43	630	94.780	94.180	94.120	91.840	93.080	93.160
44	645	94.770	94.150	94.070	91.800	93.040	93.130
45	660	94.710	94.130	94.040	91.760	93.010	93.100
46	675	94.660	94.090	94.020	91.730	92.990	93.060
47	690	94.650	94.070	93.990	91.680	92.940	93.030
48	705	94.620	94.030	93.940	91.640	92.920	93.010
49	720	94.590	94.000	93.920	91.600	92.880	92.960
50	735	94.570	93.970	93.900	91.590	92.860	92.930

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	TEMP 7 DEG. F	TEMP 8 DEG. F	TEMP 9 DEG. F	TEMP 10 DEG. F	TEMP 11 DEG. F	TEMP 12 DEG. F
51	750	94.510	93.950	93.860	91.560	92.840	92.900
52	765	94.490	93.900	93.840	91.540	92.800	92.860
53	780	94.470	93.880	93.800	91.520	92.770	92.830
54	795	94.440	93.860	93.770	91.470	92.750	92.810
55	810	94.430	93.830	93.750	91.420	92.730	92.790
56	825	94.380	93.810	93.690	91.390	92.670	92.720
57	840	94.370	93.770	93.650	91.370	92.650	92.690
58	855	94.320	93.750	93.630	91.360	92.620	92.680
59	870	94.290	93.700	93.610	91.340	92.580	92.650
60	885	94.280	93.710	93.580	91.310	92.560	92.620
61	900	94.240	93.650	93.550	91.270	92.550	92.570
62	915	94.230	93.640	93.530	91.230	92.530	92.560
63	930	94.210	93.610	93.500	91.200	92.500	92.540
64	945	94.200	93.590	93.500	91.200	92.480	92.510
65	960	94.140	93.580	93.450	91.160	92.460	92.490
66	975	94.130	93.580	93.450	91.180	92.440	92.470
67	990	94.070	93.560	93.420	91.150	92.430	92.440
68	1005	94.060	93.520	93.430	91.120	92.410	92.390
69	1020	94.020	93.530	93.380	91.090	92.390	92.390
70	1035	94.020	93.520	93.350	91.090	92.350	92.370
71	1050	94.010	93.470	93.360	91.050	92.270	92.370
72	1065	93.970	93.460	93.310	91.040	92.250	92.310
73	1080	93.930	93.440	93.300	91.020	92.210	92.300
74	1095	93.920	93.430	93.300	91.020	92.220	92.270
75	1110	93.930	93.400	93.290	90.990	92.160	92.270
76	1125	93.890	93.370	93.220	90.930	92.150	92.230
77	1140	93.900	93.370	93.240	90.960	92.150	92.220
78	1155	93.850	93.320	93.190	90.920	92.120	92.230
79	1170	93.830	93.310	93.190	90.900	92.110	92.170
80	1185	93.810	93.300	93.170	90.860	92.090	92.160
81	1200	93.810	93.310	93.160	90.870	92.070	92.130
82	1215	93.810	93.280	93.120	90.900	92.070	92.100
83	1230	93.780	93.250	93.120	90.850	92.060	92.100
84	1245	93.750	93.230	93.080	90.840	92.040	92.080
85	1260	93.730	93.220	93.090	90.860	92.030	92.070
86	1275	93.730	93.170	93.090	90.790	92.030	92.050
87	1290	93.700	93.170	93.080	90.810	92.020	92.040
88	1305	93.700	93.150	93.060	90.820	92.000	92.040
89	1320	93.670	93.130	93.070	90.740	91.990	92.000
90	1335	93.650	93.130	93.030	90.770	91.990	92.000
91	1350	93.630	93.110	93.030	90.770	91.970	92.000
92	1365	93.630	93.080	92.980	90.720	91.990	91.980
93	1380	93.620	93.090	93.020	90.720	91.970	91.950
94	1395	93.620	93.100	92.980	90.740	91.970	91.960
95	1410	93.580	93.070	92.980	90.730	91.970	91.930
96	1425	93.560	93.040	92.980	90.720	91.940	91.920
97	1440	93.540	93.030	92.910	90.670	91.950	91.910

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 13 DEG. F	TEMP 14 DEG. F	TEMP 15 DEG. F	TEMP 16 DEG. F	TEMP 17 DEG. F	TEMP 18 DEG. F
1	0	96.030	96.360	94.060	94.480	97.210	94.960
2	15	95.880	96.230	94.020	94.340	97.140	94.880
3	30	95.780	96.080	93.890	94.310	97.040	94.810
4	45	95.660	95.990	93.900	94.170	96.930	94.680
5	60	95.530	95.890	93.770	94.140	96.810	94.600
6	75	95.440	95.780	93.760	94.120	96.770	94.560
7	90	95.340	95.650	93.680	94.020	96.650	94.500
8	105	95.230	95.570	93.580	93.970	96.580	94.420
9	120	95.120	95.480	93.530	93.890	96.460	94.340
10	135	95.040	95.390	93.500	93.810	96.470	94.300
11	150	94.930	95.280	93.440	93.770	96.390	94.190
12	165	94.840	95.180	93.350	93.730	96.380	94.200
13	180	94.790	95.110	93.340	93.700	96.340	94.130
14	195	94.730	95.040	93.330	93.670	96.270	94.020
15	210	94.630	94.960	93.270	93.580	96.150	93.980
16	225	94.570	94.890	93.270	93.590	96.120	93.970
17	240	94.510	94.800	93.180	93.510	96.100	93.870
18	255	94.430	94.750	93.190	93.500	96.050	93.920
19	270	94.360	94.680	93.170	93.460	96.030	93.930
20	285	94.300	94.620	93.120	93.460	95.990	93.850
21	300	94.210	94.570	93.100	93.420	95.970	93.850
22	315	94.180	94.510	93.070	93.400	95.940	93.810
23	330	94.120	94.440	93.010	93.310	95.890	93.770
24	345	94.040	94.390	92.970	93.360	95.860	93.750
25	360	94.010	94.350	92.980	93.340	95.840	93.720
26	375	93.950	94.300	92.980	93.330	95.840	93.730
27	390	93.910	94.190	92.940	93.290	95.800	93.700
28	405	93.860	94.180	92.930	93.260	95.780	93.660
29	420	93.800	94.140	92.910	93.280	95.790	93.650
30	435	93.770	94.080	92.890	93.260	95.760	93.620
31	450	93.730	94.020	92.880	93.240	95.760	93.610
32	465	93.670	93.990	92.890	93.210	95.740	93.620
33	480	93.650	93.930	92.850	93.220	95.680	93.550
34	495	93.610	93.920	92.870	93.220	95.680	93.540
35	510	93.570	93.860	92.880	93.210	95.650	93.510
36	525	93.520	93.800	92.870	93.180	95.620	93.530
37	540	93.490	93.770	92.850	93.170	95.580	93.500
38	555	93.470	93.760	92.860	93.170	95.520	93.500
39	570	93.390	93.700	92.850	93.120	95.450	93.450
40	585	93.360	93.660	92.800	93.120	95.460	93.450
41	600	93.340	93.630	92.780	93.110	95.450	93.420
42	615	93.290	93.610	92.790	93.040	95.430	93.370
43	630	93.260	93.570	92.780	93.060	95.420	93.400
44	645	93.220	93.540	92.780	93.040	95.420	93.350
45	660	93.200	93.480	92.760	93.030	95.380	93.310
46	675	93.170	93.450	92.720	93.040	95.370	93.360
47	690	93.140	93.410	92.760	93.000	95.360	93.340
48	705	93.110	93.390	92.720	92.970	95.350	93.280
49	720	93.060	93.360	92.730	92.990	95.360	93.280
50	735	93.040	93.320	92.690	92.940	95.330	93.260

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	TEMP 13 DEG. F	TEMP 14 DEG. F	TEMP 15 DEG. F	TEMP 16 DEG. F	TEMP 17 DEG. F	TEMP 18 DEG. F
51	750	93.000	93.270	92.700	92.920	95.350	93.270
52	765	92.990	93.250	92.670	92.910	95.320	93.250
53	780	92.940	93.210	92.660	92.900	95.300	93.220
54	795	92.920	93.200	92.620	92.870	95.290	93.220
55	810	92.890	93.160	92.620	92.850	95.290	93.240
56	825	92.850	93.110	92.570	92.830	95.340	93.180
57	840	92.830	93.070	92.590	92.810	95.380	93.210
58	855	92.790	93.070	92.540	92.820	95.430	93.180
59	870	92.770	93.030	92.520	92.810	95.430	93.170
60	885	92.730	93.010	92.520	92.820	95.420	93.140
61	900	92.720	92.990	92.470	92.850	95.440	93.150
62	915	92.690	92.950	92.490	92.790	95.410	93.160
63	930	92.650	92.950	92.440	92.780	95.400	93.130
64	945	92.640	92.930	92.470	92.800	95.400	93.130
65	960	92.640	92.890	92.430	92.780	95.370	93.130
66	975	92.620	92.880	92.450	92.770	95.370	93.080
67	990	92.600	92.840	92.440	92.750	95.350	93.130
68	1005	92.580	92.840	92.440	92.750	95.370	93.080
69	1020	92.550	92.820	92.450	92.760	95.320	93.090
70	1035	92.510	92.800	92.410	92.750	95.320	93.070
71	1050	92.470	92.780	92.410	92.750	95.310	93.090
72	1065	92.460	92.750	92.420	92.750	95.330	93.050
73	1080	92.420	92.740	92.420	92.730	95.290	93.060
74	1095	92.400	92.740	92.410	92.720	95.300	93.070
75	1110	92.370	92.730	92.440	92.790	95.260	93.060
76	1125	92.350	92.730	92.410	92.720	95.250	93.000
77	1140	92.340	92.710	92.410	92.730	95.250	93.060
78	1155	92.320	92.690	92.430	92.710	95.210	93.020
79	1170	92.300	92.680	92.410	92.720	95.220	92.990
80	1185	92.290	92.660	92.410	92.720	95.220	93.010
81	1200	92.250	92.630	92.380	92.690	95.210	92.970
82	1215	92.240	92.620	92.350	92.710	95.230	93.000
83	1230	92.230	92.590	92.400	92.670	95.220	93.010
84	1245	92.210	92.580	92.390	92.670	95.220	92.980
85	1260	92.200	92.540	92.370	92.660	95.220	92.970
86	1275	92.200	92.530	92.350	92.700	95.210	92.920
87	1290	92.180	92.550	92.350	92.660	95.230	92.970
88	1305	92.150	92.500	92.360	92.670	95.210	92.960
89	1320	92.150	92.490	92.360	92.670	95.170	92.920
90	1335	92.160	92.450	92.350	92.650	95.200	92.930
91	1350	92.150	92.460	92.360	92.640	95.190	92.880
92	1365	92.170	92.460	92.340	92.660	95.190	92.940
93	1380	92.150	92.440	92.330	92.670	95.190	92.900
94	1395	92.120	92.440	92.340	92.670	95.160	92.940
95	1410	92.120	92.430	92.310	92.630	95.160	92.870
96	1425	92.130	92.400	92.320	92.620	95.170	92.850
97	1440	92.090	92.350	92.300	92.630	95.160	92.900

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 19 DEG. F	TEMP 20 DEG. F	TEMP 21 DEG. F	TEMP 22 DEG. F	TEMP 23 DEG. F	TEMP 24 DEG. F
1	0	95.080	94.400	85.630	85.600	85.310	85.700
2	15	94.970	94.310	85.550	85.560	85.310	85.680
3	30	94.890	94.290	85.540	85.490	85.280	85.650
4	45	94.790	94.190	85.470	85.490	85.260	85.640
5	60	94.710	94.100	85.410	85.450	85.240	85.610
6	75	94.610	94.050	85.470	85.460	85.210	85.580
7	90	94.550	93.970	85.420	85.400	85.210	85.570
8	105	94.480	93.900	85.350	85.350	85.160	85.540
9	120	94.330	93.860	85.330	85.390	85.170	85.550
10	135	94.310	93.820	85.240	85.370	85.140	85.530
11	150	94.270	93.730	85.320	85.290	85.120	85.490
12	165	94.220	93.680	85.290	85.300	85.110	85.460
13	180	94.160	93.650	85.210	85.260	85.090	85.440
14	195	94.100	93.580	85.260	85.280	85.080	85.440
15	210	94.050	93.590	85.240	85.250	85.090	85.440
16	225	93.920	93.540	85.220	85.250	85.070	85.430
17	240	93.900	93.510	85.170	85.190	85.030	85.400
18	255	93.860	93.480	85.100	85.200	85.050	85.380
19	270	93.840	93.430	85.080	85.150	85.010	85.390
20	285	93.770	93.400	85.190	85.160	85.000	85.360
21	300	93.720	93.380	85.040	85.170	85.000	85.360
22	315	93.730	93.390	85.180	85.180	84.980	85.320
23	330	93.660	93.320	85.200	85.110	84.950	85.320
24	345	93.630	93.360	85.140	85.080	84.970	85.310
25	360	93.580	93.290	85.080	85.110	84.930	85.290
26	375	93.580	93.320	85.040	85.100	84.970	85.310
27	390	93.510	93.290	85.120	85.070	84.960	85.280
28	405	93.530	93.290	85.100	85.090	84.960	85.300
29	420	93.480	93.260	85.040	85.090	84.950	85.290
30	435	93.480	93.260	85.110	85.080	84.960	85.270
31	450	93.420	93.250	85.040	85.070	84.960	85.260
32	465	93.390	93.220	85.040	85.060	84.950	85.260
33	480	93.360	93.240	85.070	85.060	84.940	85.250
34	495	93.310	93.240	85.070	85.100	84.930	85.240
35	510	93.290	93.230	85.010	85.070	84.940	85.240
36	525	93.250	93.200	85.040	85.070	84.940	85.230
37	540	93.220	93.130	84.930	85.070	84.930	85.210
38	555	93.210	93.160	84.990	85.060	84.940	85.240
39	570	93.200	93.110	85.020	85.070	84.890	85.240
40	585	93.160	93.140	85.030	85.030	84.890	85.210
41	600	93.160	93.130	85.030	85.050	84.910	85.220
42	615	93.140	93.100	84.980	85.030	84.920	85.210
43	630	93.150	93.110	85.010	85.010	84.890	85.250
44	645	93.110	93.050	84.980	85.010	84.880	85.210
45	660	93.110	93.040	84.970	85.020	84.860	85.210
46	675	93.090	93.010	84.910	84.970	84.880	85.180
47	690	93.110	93.010	84.870	84.960	84.880	85.180
48	705	93.060	92.990	84.880	84.970	84.860	85.180
49	720	93.060	92.950	84.880	84.990	84.880	85.180
50	735	93.080	92.980	84.940	84.960	84.860	85.180

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	TEMP 19 DEG. F	TEMP 20 DEG. F	TEMP 21 DEG. F	TEMP 22 DEG. F	TEMP 23 DEG. F	TEMP 24 DEG. F
51	750	93.080	92.960	84.940	85.000	84.850	85.160
52	765	93.040	92.950	84.970	84.970	84.860	85.150
53	780	93.030	92.920	84.850	84.980	84.850	85.140
54	795	93.000	92.930	84.920	84.960	84.850	85.140
55	810	92.990	92.930	84.840	84.960	84.830	85.150
56	825	92.990	92.900	84.860	84.960	84.830	85.130
57	840	92.990	92.920	84.910	84.920	84.820	85.140
58	855	92.980	92.920	84.870	84.930	84.810	85.130
59	870	92.970	92.880	84.880	84.970	84.790	85.120
60	885	92.960	92.830	84.860	84.930	84.800	85.130
61	900	92.970	92.880	84.860	84.920	84.810	85.110
62	915	92.950	92.810	84.840	84.960	84.790	85.120
63	930	92.930	92.890	84.820	84.910	84.800	85.110
64	945	92.950	92.870	84.830	84.900	84.810	85.110
65	960	92.970	92.840	84.870	84.940	84.790	85.110
66	975	92.900	92.820	84.890	84.890	84.790	85.100
67	990	92.920	92.810	84.850	84.920	84.760	85.070
68	1005	92.930	92.780	84.770	84.870	84.790	85.090
69	1020	92.910	92.810	84.860	84.870	84.790	85.090
70	1035	92.910	92.820	84.810	84.900	84.770	85.070
71	1050	92.910	92.790	84.840	84.920	84.770	85.080
72	1065	92.880	92.780	84.780	84.870	84.750	85.070
73	1080	92.910	92.800	84.800	84.890	84.760	85.060
74	1095	92.870	92.770	84.860	84.880	84.760	85.070
75	1110	92.850	92.740	84.850	84.870	84.740	85.050
76	1125	92.880	92.750	84.830	84.880	84.760	85.040
77	1140	92.880	92.740	84.900	84.870	84.740	85.040
78	1155	92.850	92.780	84.800	84.910	84.730	85.040
79	1170	92.830	92.730	84.840	84.870	84.760	85.030
80	1185	92.800	92.770	84.860	84.860	84.720	85.050
81	1200	92.810	92.730	84.780	84.880	84.740	85.040
82	1215	92.850	92.690	84.810	84.850	84.720	85.030
83	1230	92.800	92.720	84.870	84.860	84.750	85.030
84	1245	92.810	92.720	84.770	84.820	84.720	85.020
85	1260	92.800	92.690	84.800	84.820	84.710	85.030
86	1275	92.820	92.710	84.870	84.860	84.680	85.010
87	1290	92.770	92.690	84.800	84.830	84.670	84.990
88	1305	92.810	92.630	84.780	84.840	84.710	84.990
89	1320	92.770	92.660	84.720	84.810	84.700	85.010
90	1335	92.760	92.660	84.840	84.800	84.710	85.010
91	1350	92.750	92.630	84.760	84.790	84.710	84.990
92	1365	92.760	92.730	84.740	84.800	84.650	84.990
93	1380	92.690	92.670	84.780	84.780	84.690	84.970
94	1395	92.720	92.640	84.760	84.770	84.700	84.990
95	1410	92.690	92.670	84.800	84.770	84.690	84.980
96	1425	92.660	92.610	84.740	84.800	84.660	84.960
97	1440	92.720	92.680	84.720	84.770	84.650	84.960

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 25 DEG. F	TEMP 26 DEG. F	TEMP 27 DEG. F	TEMP 28 DEG. F	TEMP 29 DEG. F	TEMP 30 DEG. F
1	0	85.560	84.400	85.610	85.700	85.970	84.960
2	15	85.530	84.380	85.600	85.680	85.960	84.930
3	30	85.510	84.370	85.410	85.650	85.930	84.940
4	45	85.470	84.350	85.600	85.630	85.910	84.900
5	60	85.460	84.360	85.560	85.640	85.900	84.910
6	75	85.450	84.350	85.560	85.600	85.890	84.890
7	90	85.420	84.340	85.510	85.590	85.850	84.850
8	105	85.390	84.330	85.490	85.600	85.840	84.860
9	120	85.390	84.300	85.640	85.570	85.820	84.860
10	135	85.360	84.320	85.500	85.560	85.820	84.810
11	150	85.350	84.300	85.310	85.550	85.790	84.820
12	165	85.340	84.270	85.290	85.520	85.790	84.790
13	180	85.300	84.270	85.350	85.510	85.780	84.810
14	195	85.300	84.240	85.490	85.500	85.750	84.770
15	210	85.280	84.260	85.470	85.490	85.760	84.780
16	225	85.260	84.230	85.460	85.480	85.720	84.770
17	240	85.250	84.230	85.390	85.470	85.730	84.770
18	255	85.210	84.230	85.480	85.460	85.740	84.750
19	270	85.200	84.230	85.410	85.450	85.720	84.730
20	285	85.190	84.240	85.320	85.450	85.690	84.720
21	300	85.170	84.210	85.370	85.430	85.710	84.730
22	315	85.100	84.210	85.330	85.430	85.670	84.730
23	330	85.100	84.210	85.290	85.440	85.660	84.730
24	345	85.150	84.210	85.250	85.460	85.730	84.720
25	360	85.110	84.190	85.350	85.430	85.670	84.720
26	375	85.120	84.220	85.200	85.420	85.690	84.710
27	390	85.120	84.210	85.260	85.420	85.700	84.690
28	405	85.130	84.200	85.280	85.410	85.700	84.700
29	420	85.140	84.210	85.270	85.400	85.650	84.690
30	435	85.110	84.200	85.330	85.400	85.660	84.680
31	450	85.130	84.170	85.350	85.410	85.650	84.680
32	465	85.120	84.180	85.280	85.410	85.660	84.670
33	480	85.110	84.190	85.240	85.390	85.630	84.680
34	495	85.100	84.200	85.120	85.400	85.640	84.680
35	510	85.100	84.170	85.300	85.390	85.620	84.660
36	525	85.090	84.200	85.280	85.400	85.640	84.670
37	540	85.080	84.190	85.270	85.370	85.620	84.660
38	555	85.080	84.190	85.130	85.390	85.620	84.660
39	570	85.060	84.160	85.140	85.350	85.610	84.670
40	585	85.050	84.190	85.140	85.380	85.610	84.650
41	600	85.050	84.170	85.070	85.370	85.620	84.630
42	615	85.040	84.170	85.160	85.370	85.590	84.640
43	630	85.040	84.160	85.110	85.350	85.600	84.650
44	645	85.020	84.130	85.100	85.360	85.590	84.660
45	660	85.020	84.170	85.180	85.350	85.580	84.640
46	675	85.010	84.150	85.220	85.340	85.580	84.650
47	690	84.990	84.160	85.270	85.350	85.580	84.630
48	705	84.990	84.150	85.250	85.320	85.590	84.630
49	720	84.980	84.150	85.240	85.340	85.580	84.610
50	735	84.970	84.160	85.030	85.340	85.590	84.640

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	TEMP 25 DEG. F	TEMP 26 DEG. F	TEMP 27 DEG. F	TEMP 28 DEG. F	TEMP 29 DEG. F	TEMP 30 DEG. F
51	750	84.970	84.150	85.060	85.350	85.560	84.640
52	765	84.970	84.150	85.120	85.330	85.560	84.630
53	780	84.970	84.140	85.180	85.330	85.570	84.620
54	795	84.960	84.140	85.210	85.340	85.580	84.620
55	810	84.960	84.140	85.180	85.310	85.560	84.610
56	825	84.930	84.120	85.120	85.320	85.550	84.610
57	840	84.920	84.150	85.310	85.290	85.580	84.590
58	855	84.910	84.130	85.350	85.300	85.550	84.580
59	870	84.900	84.130	85.360	85.270	85.550	84.570
60	885	84.920	84.110	85.370	85.280	85.540	84.590
61	900	84.910	84.130	85.380	85.290	85.560	84.590
62	915	84.900	84.120	85.400	85.280	85.530	84.580
63	930	84.900	84.120	85.390	85.270	85.530	84.580
64	945	84.910	84.110	85.420	85.270	85.530	84.580
65	960	84.890	84.130	85.380	85.260	85.510	84.570
66	975	84.880	84.120	85.420	85.270	85.540	84.560
67	990	84.880	84.130	85.430	85.270	85.520	84.570
68	1005	84.880	84.100	85.440	85.270	85.520	84.570
69	1020	84.870	84.120	85.480	85.270	85.530	84.570
70	1035	84.860	84.120	85.420	85.290	85.520	84.550
71	1050	84.850	84.120	85.430	85.280	85.520	84.560
72	1065	84.860	84.120	85.470	85.280	85.530	84.570
73	1080	84.880	84.130	85.440	85.290	85.530	84.560
74	1095	84.860	84.120	85.460	85.270	85.500	84.560
75	1110	84.840	84.130	85.350	85.260	85.520	84.540
76	1125	84.850	84.130	85.320	85.270	85.500	84.560
77	1140	84.860	84.130	85.390	85.260	85.500	84.540
78	1155	84.830	84.100	85.310	85.260	85.490	84.540
79	1170	84.820	84.130	85.350	85.290	85.500	84.540
80	1185	84.840	84.120	85.370	85.260	85.500	84.550
81	1200	84.840	84.110	85.360	85.270	85.490	84.540
82	1215	84.800	84.130	85.400	85.270	85.470	84.540
83	1230	84.810	84.110	85.380	85.260	85.480	84.540
84	1245	84.800	84.120	85.390	85.270	85.470	84.560
85	1260	84.810	84.110	85.370	85.260	85.500	84.550
86	1275	84.780	84.120	85.350	85.260	85.490	84.540
87	1290	84.780	84.100	85.380	85.240	85.460	84.530
88	1305	84.760	84.120	85.330	85.240	85.470	84.530
89	1320	84.750	84.110	85.370	85.240	85.480	84.530
90	1335	84.760	84.110	85.340	85.240	85.460	84.540
91	1350	84.740	84.100	85.340	85.250	85.470	84.540
92	1365	84.760	84.100	85.390	85.250	85.480	84.520
93	1380	84.740	84.110	85.350	85.230	85.450	84.530
94	1395	84.740	84.120	85.360	85.240	85.460	84.540
95	1410	84.740	84.120	85.400	85.230	85.450	84.530
96	1425	84.730	84.110	85.350	85.220	85.470	84.520
97	1440	84.720	84.090	85.350	85.220	85.450	84.540

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	PRES 1 PSIA	HUM 1 FRACTION	HUM 2 FRACTION	HUM 3 FRACTION	HUM 4 FRACTION	HUM 5 FRACTION
1	0	59.635	DELETED	0.652	0.648	0.639	0.628
2	15	59.624	DELETED	0.654	0.649	0.642	0.630
3	30	59.615	DELETED	0.657	0.652	0.644	0.632
4	45	59.606	DELETED	0.658	0.654	0.646	0.631
5	60	59.598	DELETED	0.660	0.656	0.648	0.630
6	75	59.589	DELETED	0.661	0.657	0.650	0.631
7	90	59.581	DELETED	0.663	0.658	0.651	0.630
8	105	59.574	DELETED	0.664	0.661	0.653	0.630
9	120	59.567	DELETED	0.666	0.663	0.655	0.627
10	135	59.560	DELETED	0.667	0.664	0.656	0.627
11	150	59.554	DELETED	0.668	0.666	0.657	0.625
12	165	59.548	DELETED	0.669	0.667	0.658	0.629
13	180	59.542	DELETED	0.670	0.667	0.660	0.626
14	195	59.535	DELETED	0.671	0.670	0.661	0.628
15	210	59.530	DELETED	0.672	0.670	0.662	0.620
16	225	59.525	DELETED	0.673	0.672	0.664	0.624
17	240	59.520	DELETED	0.674	0.673	0.665	0.621
18	255	59.515	DELETED	0.675	0.672	0.665	0.622
19	270	59.510	DELETED	0.675	0.674	0.666	0.624
20	285	59.506	DELETED	0.676	0.675	0.667	0.617
21	300	59.502	DELETED	0.677	0.675	0.667	0.619
22	315	59.497	DELETED	0.678	0.678	0.668	0.620
23	330	59.493	DELETED	0.679	0.677	0.668	0.620
24	345	59.490	DELETED	0.680	0.678	0.669	0.617
25	360	59.486	DELETED	0.680	0.677	0.669	0.619
26	375	59.482	DELETED	0.681	0.678	0.670	0.619
27	390	59.479	DELETED	0.681	0.680	0.671	0.618
28	405	59.474	DELETED	0.682	0.680	0.671	0.618
29	420	59.471	DELETED	0.682	0.682	0.672	0.621
30	435	59.468	DELETED	0.683	0.681	0.672	0.620
31	450	59.464	DELETED	0.684	0.680	0.674	0.622
32	465	59.461	DELETED	0.684	0.681	0.674	0.623
33	480	59.458	DELETED	0.685	0.682	0.675	0.622
34	495	59.455	DELETED	0.685	0.682	0.675	0.620
35	510	59.452	DELETED	0.686	0.684	0.676	0.621
36	525	59.449	DELETED	0.686	0.684	0.676	0.620
37	540	59.447	DELETED	0.686	0.683	0.677	0.619
38	555	59.443	DELETED	0.686	0.683	0.677	0.618
39	570	59.441	DELETED	0.686	0.681	0.677	0.618
40	585	59.439	DELETED	0.686	0.681	0.677	0.617
41	600	59.436	DELETED	0.687	0.681	0.678	0.616
42	615	59.433	DELETED	0.687	0.682	0.678	0.615
43	630	59.430	DELETED	0.688	0.685	0.679	0.614
44	645	59.428	DELETED	0.689	0.686	0.680	0.615
45	660	59.427	DELETED	0.690	0.687	0.680	0.613
46	675	59.424	DELETED	0.689	0.684	0.680	0.614
47	690	59.422	DELETED	0.689	0.684	0.680	0.612
48	705	59.420	DELETED	0.691	0.688	0.682	0.612
49	720	59.418	DELETED	0.690	0.690	0.682	0.612
50	735	59.415	DELETED	0.692	0.689	0.682	0.612

VARIABLE TABLE SUMMARY (CONTINUED)

SAMPLE NUMBER	DELTA MINS	PRES 1 PSIA	HUM 1 FRACTION	HUM 2 FRACTION	HUM 3 FRACTION	HUM 4 FRACTION	HUM 5 FRACTION
51	750	59.414	DELETED	0.692	0.689	0.683	0.613
52	765	59.412	DELETED	0.692	0.689	0.683	0.613
53	780	59.410	DELETED	0.692	0.690	0.684	0.613
54	795	59.409	DELETED	0.693	0.691	0.684	0.614
55	810	59.407	DELETED	0.693	0.690	0.684	0.615
56	825	59.406	DELETED	0.694	0.691	0.684	0.616
57	840	59.405	DELETED	0.694	0.693	0.685	0.616
58	855	59.403	DELETED	0.694	0.691	0.685	0.617
59	870	59.401	DELETED	0.694	0.692	0.685	0.618
60	885	59.399	DELETED	0.695	0.692	0.686	0.618
61	900	59.397	DELETED	0.694	0.689	0.685	0.618
62	915	59.396	DELETED	0.694	0.690	0.685	0.618
63	930	59.394	DELETED	0.695	0.693	0.686	0.620
64	945	59.392	DELETED	0.695	0.690	0.686	0.620
65	960	59.391	DELETED	0.695	0.690	0.686	0.621
66	975	59.389	DELETED	0.695	0.690	0.686	0.621
67	990	59.388	DELETED	0.696	0.690	0.687	0.622
68	1005	59.387	DELETED	0.696	0.691	0.687	0.623
69	1020	59.385	DELETED	0.696	0.691	0.687	0.624
70	1035	59.384	DELETED	0.697	0.695	0.688	0.625
71	1050	59.383	DELETED	0.697	0.696	0.689	0.626
72	1065	59.382	DELETED	0.696	0.691	0.688	0.626
73	1080	59.381	DELETED	0.698	0.694	0.689	0.627
74	1095	59.380	DELETED	0.697	0.692	0.688	0.628
75	1110	59.378	DELETED	0.698	0.696	0.689	0.629
76	1125	59.377	DELETED	0.698	0.695	0.690	0.629
77	1140	59.376	DELETED	0.698	0.697	0.690	0.630
78	1155	59.375	DELETED	0.698	0.693	0.689	0.630
79	1170	59.374	DELETED	0.699	0.697	0.690	0.632
80	1185	59.373	DELETED	0.699	0.697	0.690	0.633
81	1200	59.372	DELETED	0.699	0.697	0.690	0.633
82	1215	59.371	DELETED	0.699	0.696	0.690	0.634
83	1230	59.369	DELETED	0.700	0.697	0.690	0.635
84	1245	59.368	DELETED	0.700	0.698	0.690	0.636
85	1260	59.367	DELETED	0.700	0.698	0.690	0.636
86	1275	59.366	DELETED	0.700	0.697	0.691	0.637
87	1290	59.365	DELETED	0.700	0.697	0.691	0.637
88	1305	59.363	DELETED	0.700	0.699	0.691	0.638
89	1320	59.363	DELETED	0.701	0.698	0.691	0.639
90	1335	59.362	DELETED	0.701	0.698	0.692	0.640
91	1350	59.359	DELETED	0.701	0.697	0.691	0.640
92	1365	59.359	DELETED	0.701	0.699	0.691	0.641
93	1380	59.357	DELETED	0.701	0.699	0.692	0.641
94	1395	59.357	DELETED	0.701	0.694	0.691	0.642
95	1410	59.355	DELETED	0.701	0.697	0.691	0.642
96	1425	59.355	DELETED	0.700	0.694	0.691	0.643
97	1440	59.354	DELETED	0.702	0.698	0.692	0.643

END OF TABLE

VARIABLE TABLE SUMMARY

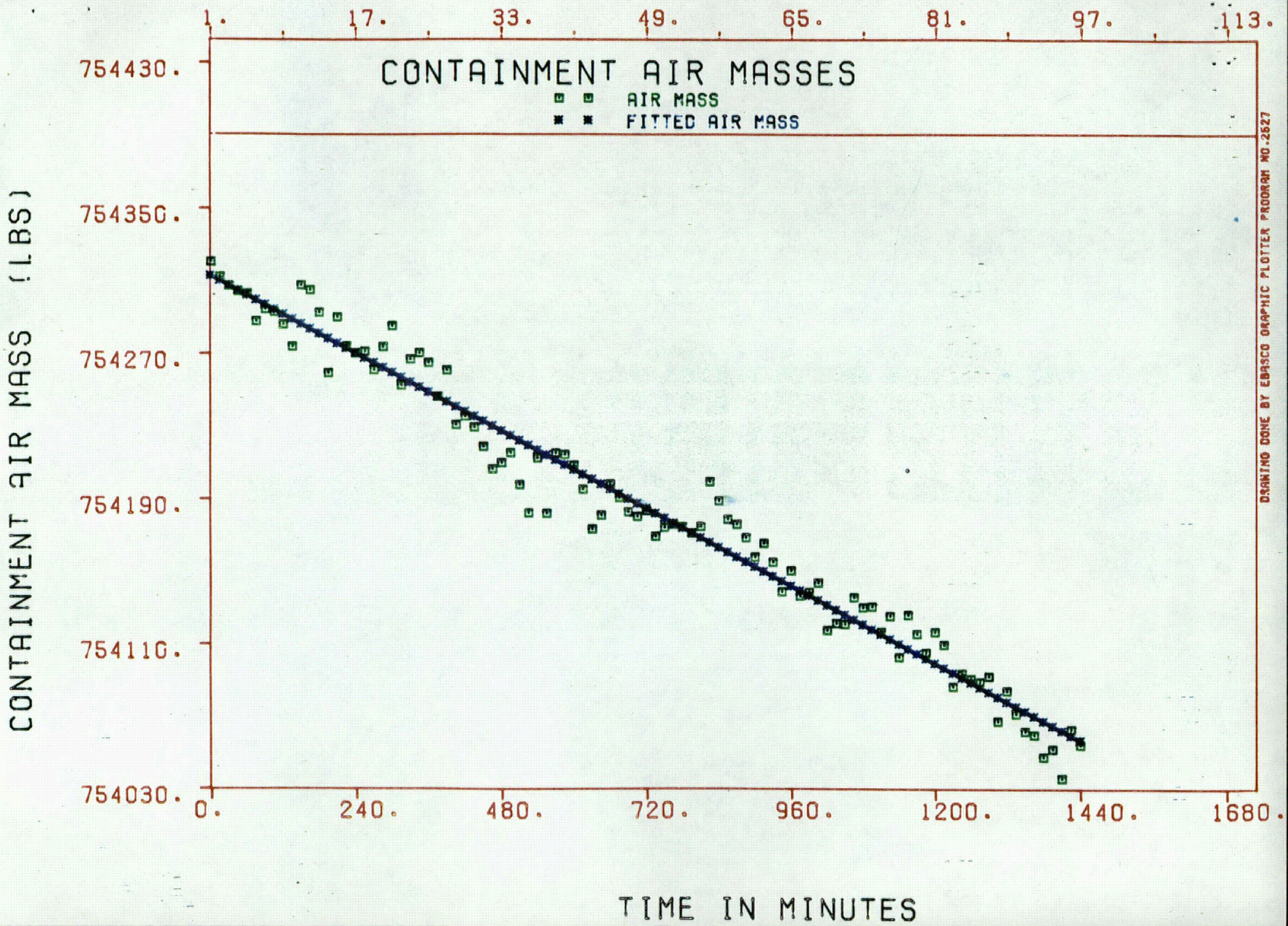
SAMPLE NUMBER	DELTA MINS	HUM 6 FRACTION	HUM 7 FRACTION	HUM 8 FRACTION	HUM 9 FRACTION	HUM 10 FRACTION
1	0	0.608	DELETED	0.510	0.491	0.496
2	15	0.603	DELETED	0.513	0.495	0.499
3	30	0.607	DELETED	0.517	0.498	0.503
4	45	0.606	DELETED	0.521	0.502	0.507
5	60	0.607	DELETED	0.523	0.505	0.511
6	75	0.608	DELETED	0.526	0.508	0.514
7	90	0.609	DELETED	0.529	0.511	0.519
8	105	0.615	DELETED	0.533	0.515	0.522
9	120	0.614	DELETED	0.536	0.517	0.524
10	135	0.618	DELETED	0.539	0.520	0.528
11	150	0.612	DELETED	0.542	0.523	0.531
12	165	0.612	DELETED	0.544	0.526	0.534
13	180	0.613	DELETED	0.547	0.529	0.537
14	195	0.616	DELETED	0.549	0.531	0.539
15	210	0.611	DELETED	0.552	0.534	0.541
16	225	0.613	DELETED	0.554	0.536	0.543
17	240	0.619	DELETED	0.557	0.539	0.546
18	255	0.611	DELETED	0.559	0.541	0.548
19	270	0.611	DELETED	0.561	0.543	0.550
20	285	0.615	DELETED	0.563	0.546	0.551
21	300	0.610	DELETED	0.565	0.548	0.553
22	315	0.614	DELETED	0.567	0.549	0.556
23	330	0.613	DELETED	0.569	0.552	0.556
24	345	0.612	DELETED	0.571	0.554	0.559
25	360	0.613	DELETED	0.573	0.556	0.560
26	375	0.612	DELETED	0.575	0.557	0.562
27	390	0.613	DELETED	0.578	0.559	0.565
28	405	0.613	DELETED	0.581	0.561	0.567
29	420	0.611	DELETED	0.583	0.563	0.568
30	435	0.611	DELETED	0.586	0.564	0.571
31	450	0.607	DELETED	0.588	0.566	0.574
32	465	0.607	DELETED	0.590	0.569	0.577
33	480	0.610	DELETED	0.592	0.571	0.578
34	495	0.605	DELETED	0.594	0.573	0.582
35	510	0.607	DELETED	0.596	0.575	0.584
36	525	0.605	DELETED	0.598	0.577	0.586
37	540	0.602	DELETED	0.600	0.579	0.588
38	555	0.604	DELETED	0.602	0.582	0.590
39	570	0.603	DELETED	0.604	0.583	0.592
40	585	0.603	DELETED	0.606	0.585	0.594
41	600	0.603	DELETED	0.607	0.587	0.596
42	615	0.604	DELETED	0.609	0.589	0.597
43	630	0.605	DELETED	0.611	0.591	0.599
44	645	0.604	DELETED	0.612	0.592	0.600
45	660	0.605	DELETED	0.614	0.594	0.602
46	675	0.605	DELETED	0.616	0.595	0.604
47	690	0.608	DELETED	0.617	0.597	0.604
48	705	0.608	DELETED	0.619	0.598	0.606
49	720	0.608	DELETED	0.620	0.600	0.607
50	735	0.609	DELETED	0.622	0.602	0.609

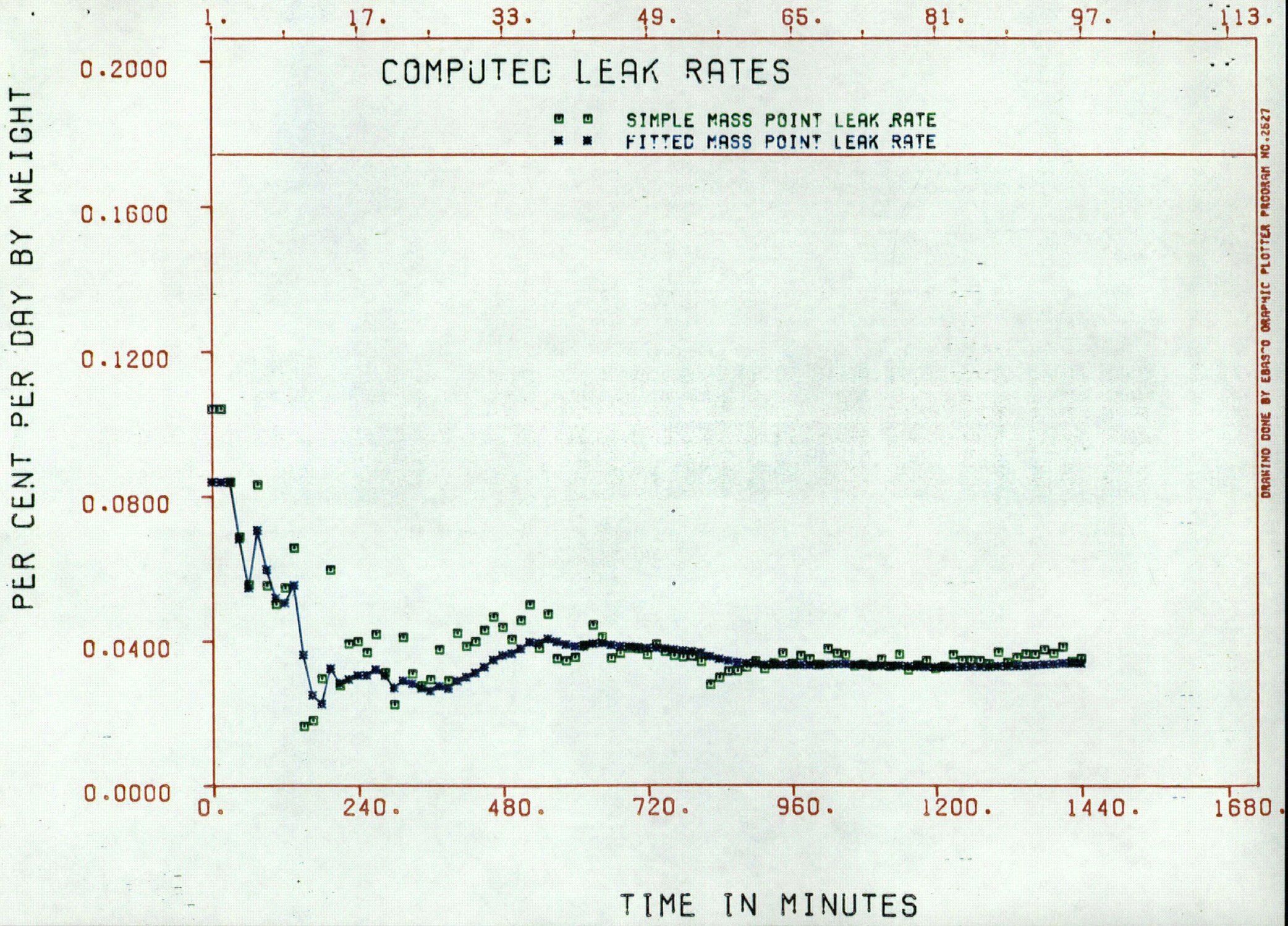
VARIABLE TABLE SUMMARY (CONTINUED)

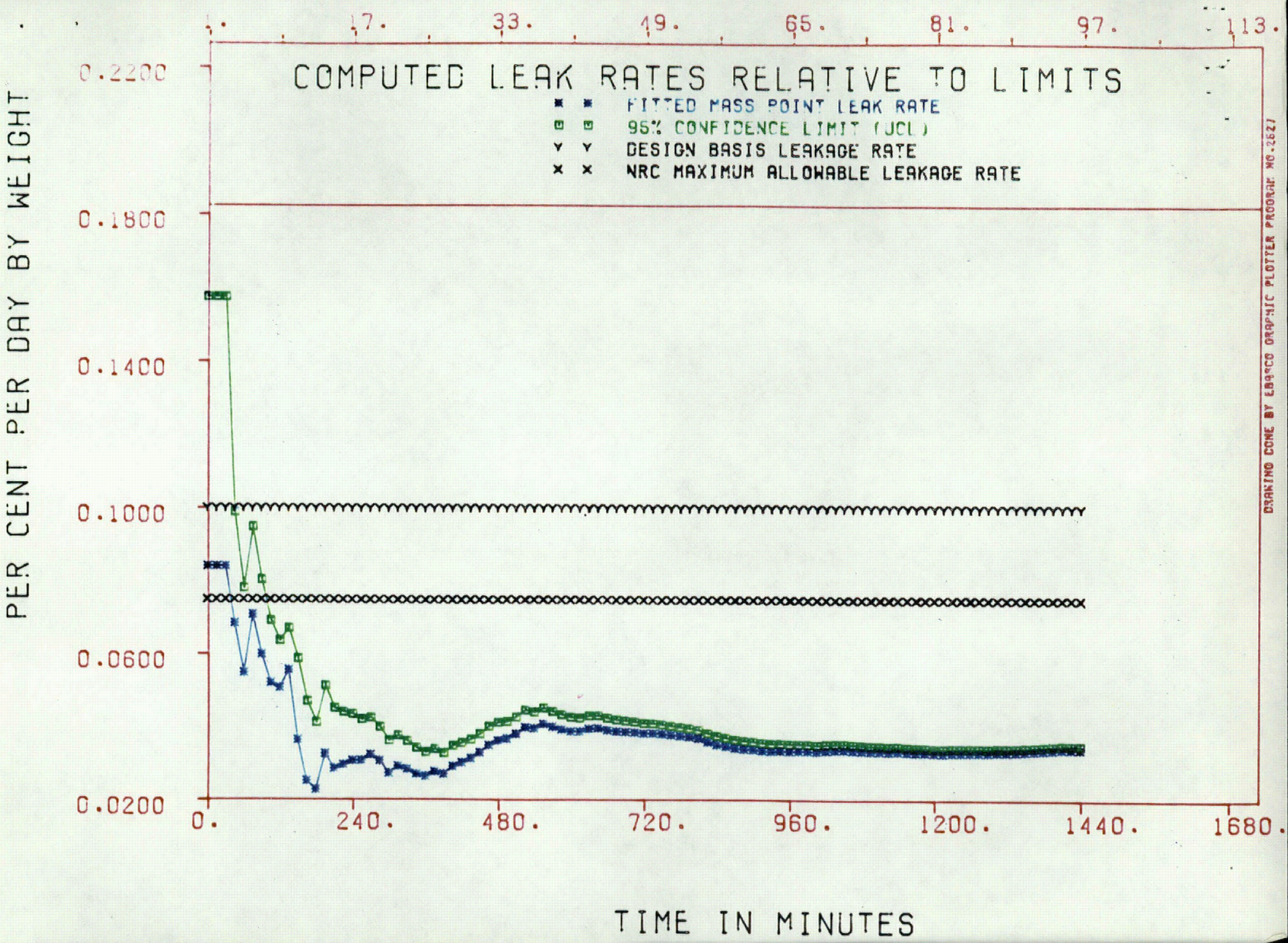
SAMPLE NUMBER	DELTA MINS	HUM 6 FRACTION	HUM 7 FRACTION	HUM 8 FRACTION	HUM 9 FRACTION	HUM 10 FRACTION
51	750	0.609	DELETED	0.623	0.603	0.610
52	765	0.610	DELETED	0.625	0.604	0.611
53	780	0.610	DELETED	0.626	0.606	0.612
54	795	0.611	DELETED	0.627	0.607	0.613
55	810	0.612	DELETED	0.628	0.608	0.615
56	825	0.612	DELETED	0.630	0.610	0.616
57	840	0.613	DELETED	0.631	0.611	0.617
58	855	0.614	DELETED	0.632	0.612	0.618
59	870	0.615	DELETED	0.633	0.613	0.619
60	885	0.615	DELETED	0.634	0.614	0.620
61	900	0.616	DELETED	0.635	0.616	0.621
62	915	0.617	DELETED	0.636	0.617	0.622
63	930	0.618	DELETED	0.637	0.618	0.623
64	945	0.619	DELETED	0.638	0.619	0.625
65	960	0.619	DELETED	0.639	0.620	0.626
66	975	0.620	DELETED	0.640	0.621	0.627
67	990	0.621	DELETED	0.642	0.623	0.628
68	1005	0.622	DELETED	0.643	0.624	0.629
69	1020	0.623	DELETED	0.644	0.625	0.630
70	1035	0.624	DELETED	0.645	0.626	0.631
71	1050	0.624	DELETED	0.645	0.627	0.632
72	1065	0.625	DELETED	0.646	0.628	0.633
73	1080	0.626	DELETED	0.647	0.629	0.634
74	1095	0.627	DELETED	0.648	0.630	0.635
75	1110	0.628	DELETED	0.649	0.631	0.636
76	1125	0.629	DELETED	0.650	0.632	0.637
77	1140	0.630	DELETED	0.651	0.633	0.638
78	1155	0.631	DELETED	0.652	0.634	0.639
79	1170	0.631	DELETED	0.653	0.635	0.640
80	1185	0.633	DELETED	0.654	0.636	0.641
81	1200	0.633	DELETED	0.655	0.637	0.642
82	1215	0.634	DELETED	0.655	0.638	0.642
83	1230	0.635	DELETED	0.657	0.639	0.643
84	1245	0.636	DELETED	0.657	0.640	0.644
85	1260	0.637	DELETED	0.658	0.641	0.645
86	1275	0.638	DELETED	0.659	0.642	0.646
87	1290	0.639	DELETED	0.660	0.643	0.647
88	1305	0.640	DELETED	0.661	0.644	0.648
89	1320	0.640	DELETED	0.661	0.645	0.649
90	1335	0.641	DELETED	0.663	0.646	0.649
91	1350	0.642	DELETED	0.664	0.647	0.650
92	1365	0.643	DELETED	0.664	0.648	0.651
93	1380	0.644	DELETED	0.665	0.649	0.652
94	1395	0.645	DELETED	0.666	0.649	0.653
95	1410	0.646	DELETED	0.667	0.650	0.653
96	1425	0.647	DELETED	0.667	0.651	0.654
97	1440	0.647	DELETED	0.668	0.652	0.654

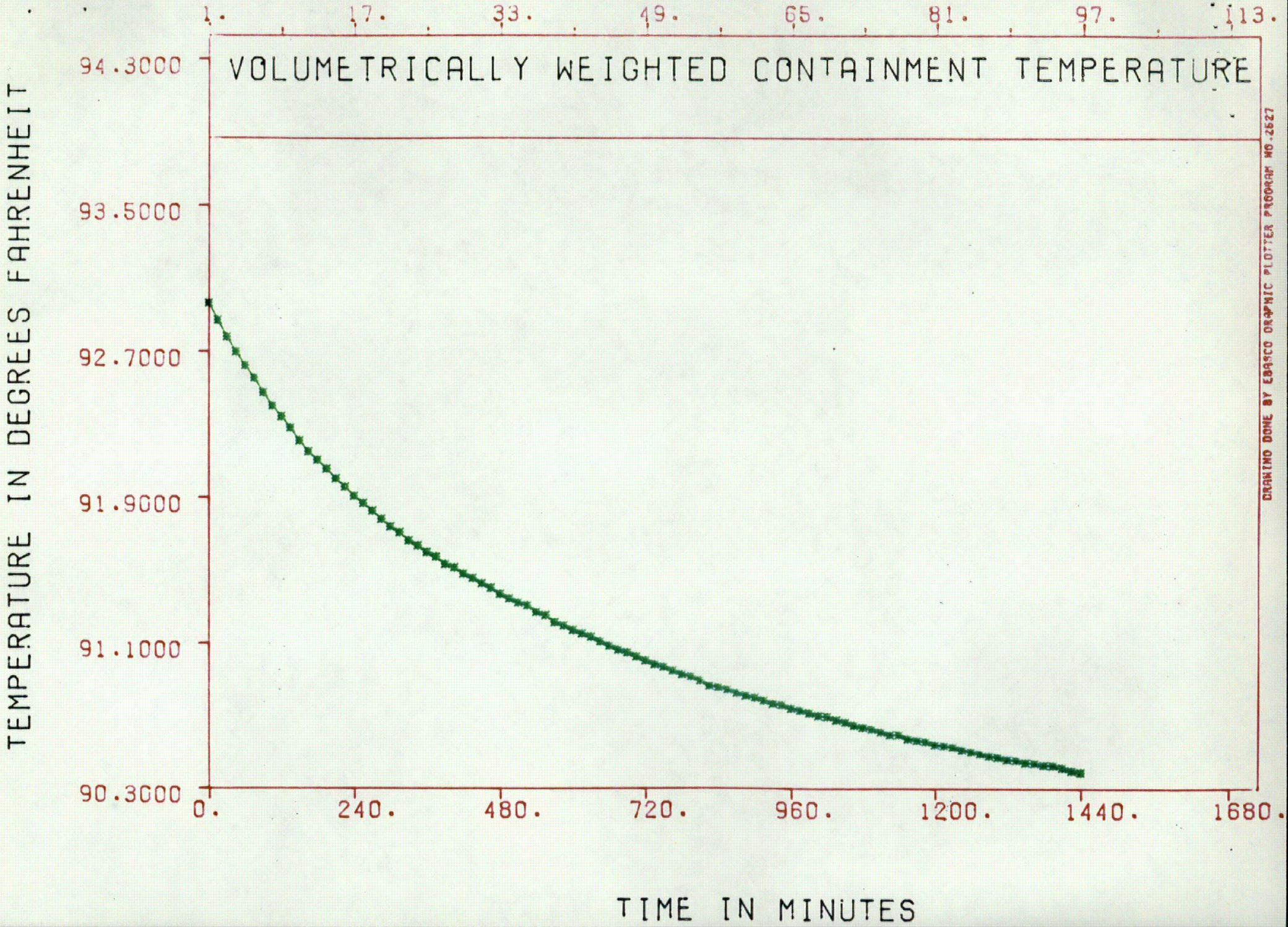
END OF TABLE

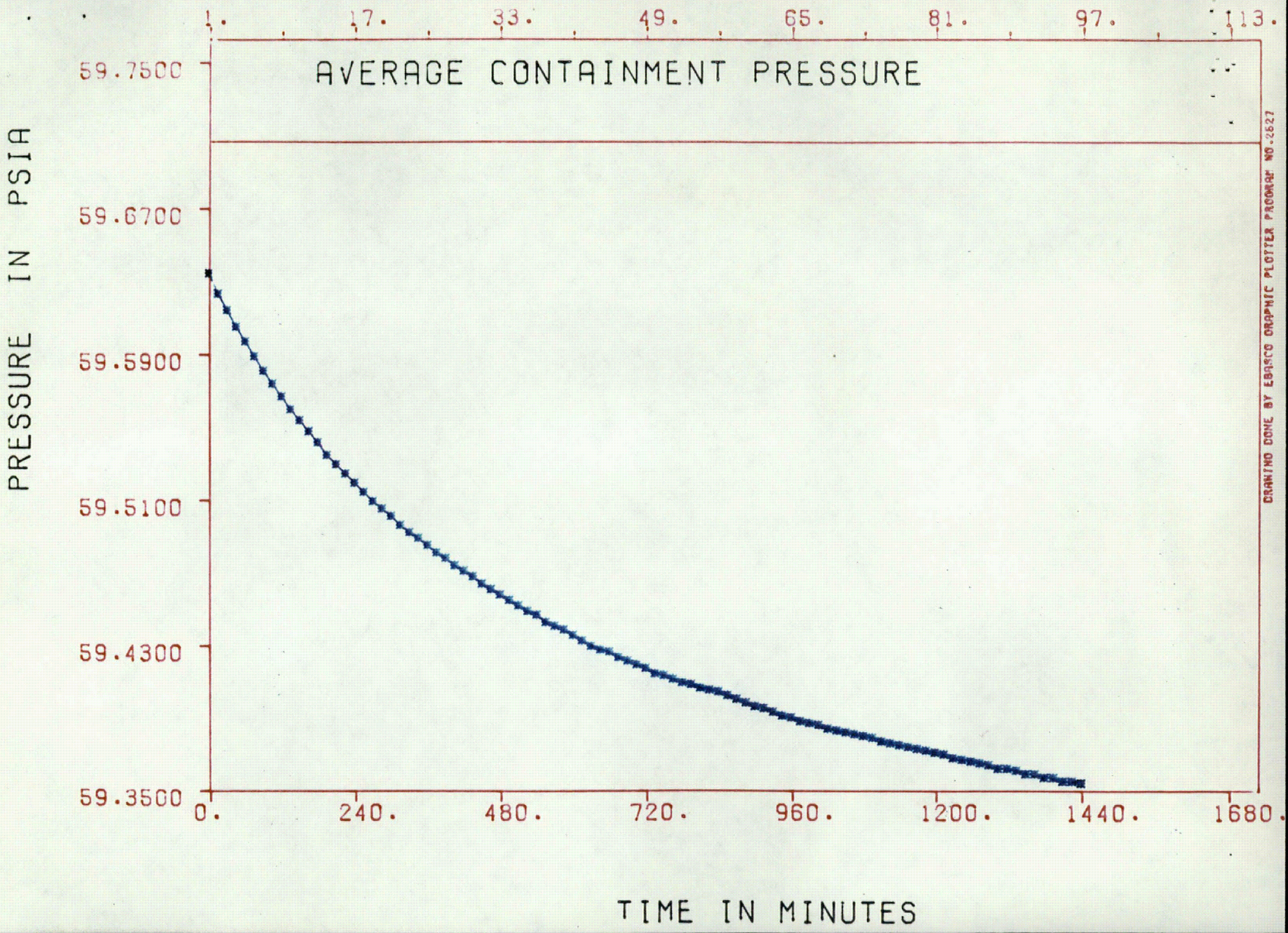
EBASCO SERVICES INCORPORATED

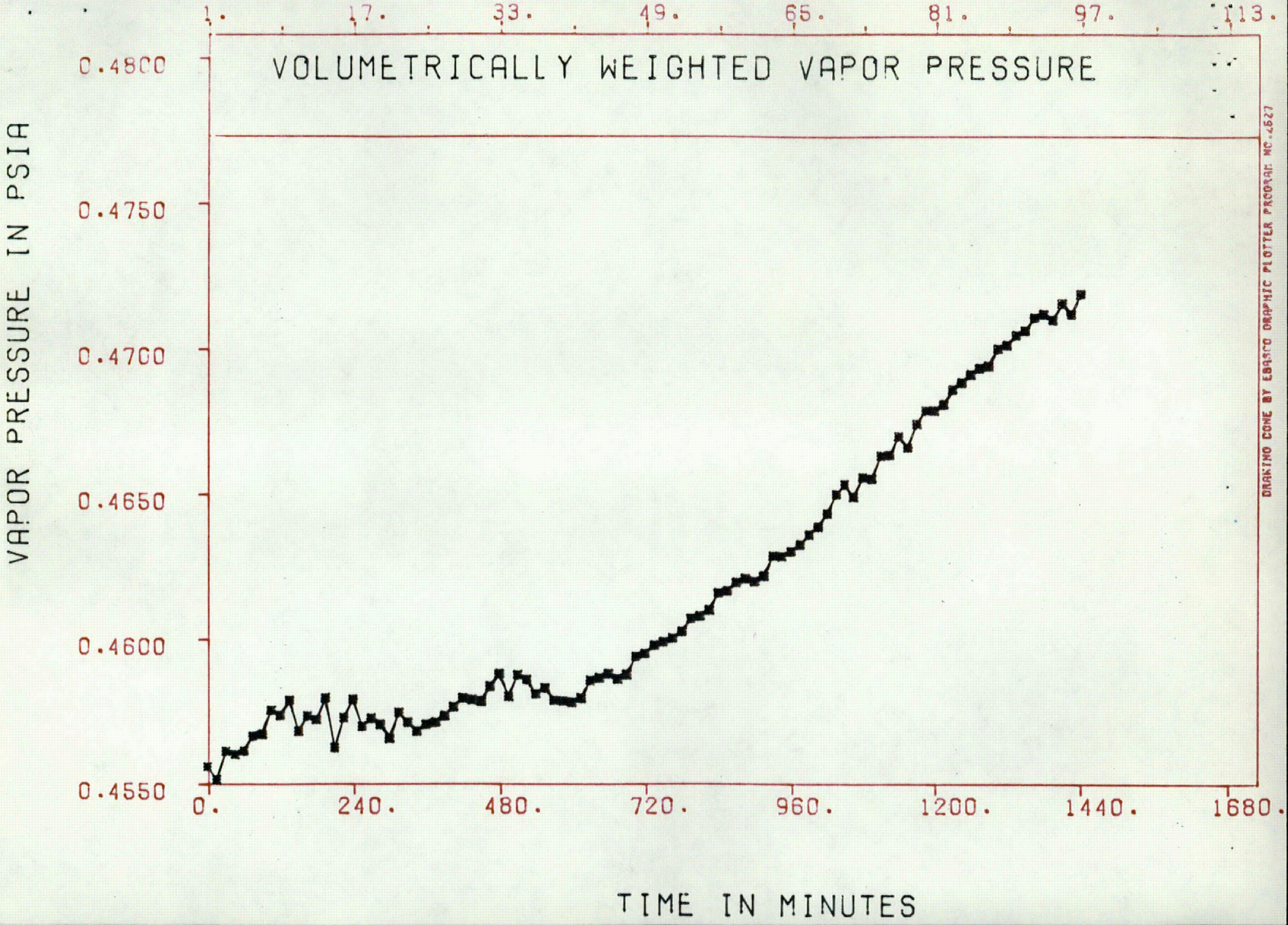



COMPUTED LEAK RATES
SIMPLE MASS POINT LEAK RATE
FITTED MASS POINT LEAK RATE
PER CENT PER DAY BY WEIGHT
0.2000
0.1600
0.1200
0.0800
0.0400
0.0000
1.
17.
33.
49.
65.
81.
97.
113.
0.
240.
480.
720.
960.
1200.
1440.
1680.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


COMPUTED LEAK RATES RELATIVE TO LIMITS
FITTED MASS POINT LEAK RATE
95% CONFIDENCE LIMIT (UCL)
DESIGN BASIS LEAKAGE RATE
NRC MAXIMUM ALLOWABLE LEAKAGE RATE
PER CENT PER DAY BY WEIGHT
0.2200
0.1800
0.1400
0.1000
0.0600
0.0200
1.
17.
33.
49.
65.
81.
97.
113.
0.
240.
480.
720.
960.
1200.
1440.
1680.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


VOLUMETRICALLY WEIGHTED CONTAINMENT TEMPERATURE
TEMPERATURE IN DEGREES FAHRENHEIT
94.3000
93.5000
92.7000
91.9000
91.1000
90.3000
1.
17.
33.
49.
65.
81.
97.
113.
0.
240.
480.
720.
960.
1200.
1440.
1680.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


AVERAGE CONTAINMENT PRESSURE
PRESSURE IN PSIA
59.7500
59.6700
59.5900
59.5100
59.4300
59.3500
1.
17.
33.
49.
65.
81.
97.
113.
0.
240.
480.
720.
960.
1200.
1440.
1680.
TIME IN MINUTES
DRAWING DONE BY EDASCO GRAPHIC PLOTTER PROGRAM NO.2627


VOLUMETRICALLY WEIGHTED VAPOR PRESSURE
VAPOR PRESSURE IN PSIA
0.4800
0.4750
0.4700
0.4650
0.4600
0.4550
1.
17.
33.
49.
65.
81.
97.
113.
0.
240.
480.
720.
960.
1200.
1440.
1680.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.4627

APPENDIX A.2

COMPUTER GENERATED REPORT

VERIFICATION CONTROLLED LEAK RATE TEST (CLRT)

EBASCO SERVICES
INCORPORATED

POWER AUTHORITY STATE OF NEW YORK
ILRT INDIAN POINT 3

CONTAINMENT INTEGRATED LEAKAGE RATE TEST
SUPPLEMENTAL VERIFICATION TEST
LEAKAGE RATE MEASURED USING THE ABSOLUTE METHOD
LEAKAGE RATE COMPUTED USING THE MASS POINT METHOD

TEST PERIOD STARTED AT 700 HOURS ON AUGUST 4,1982
TEST CONDUCTED FOR 4.50 HOURS

FREE SPACE VOLUME OF CONTAINMENT IS 2610000 CU FT
CONTAINMENT WAS PRESSURIZED TO 59.35 PSIA

INITIAL VERIFICATION AIR WEIGHT 754018.6 LBS
FINAL VERIFICATION AIR WEIGHT 753815.3 LBS
FITTED MASS POINT LEAKAGE RATE IS 0.136 % PER DAY

LC = 0.136 LAM = 0.034 LO = 0.099

$$LO + LAM - .025\ LA \leq LC \leq LO + LAM + 0.25\ LA$$

$$0.099 + 0.034 - 0.025 \leq 0.136 \leq 0.099 + 0.034 + 0.025$$

$$0.108 \leq 0.136 \leq 0.158$$

LC =FITTED CLRT MASS POINT LEAKAGE RATE
LAM =FITTED ILRT MASS POINT LEAKAGE RATE
LO =SUPERIMPOSED LEAKAGE DURING VERIFICATION TEST
LA =NRC MAXIMUM ALLOWABLE LEAKAGE RATE

DESCRIPTION OF VARIABLES

AVG. TEM - CONTAINMENT MEAN TEMPERATURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RTD SENSOR INDICATIONS.

AVE. PRE - PRIMARY CONTAINMENT PRESSURE INDICATION.

VAP. PRE - CONTAINMENT VAPOR PRESSURE CALCULATED FROM VOLUMETRICALLY WEIGHTED RHD SENSOR INDICATIONS.

LEAK SIM - SIMPLE TOTAL TIME LEAKAGE RATE.

LEAK MAS - LEAKAGE RATE COMPUTED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.

AIR MASS - CONTAINMENT AIR MASS.

NOTE FOR TABULAR DATA -

TABLE VALUES OF ZERO SIGNIFY EITHER.

1. DATA IS NOT APPLICABLE TO THE CALCULATION OR
2. SENSOR HAS BEEN DELETED FROM THE SCAN.

NOTE FOR CURVES -

1. TOP ABSCISSA SCALE REPRESENTS SAMPLE NUMBERS.
2. AIR MASS IS THE CALCULATED CONTAINMENT AIR MASS AND FITTED AIR MASS IS THE LINEAR LEAST SQUARE FIT OF THE AIR MASSES.
3. SIMPLE MASS POINT IS THE TOTAL TIME LEAKAGE RATE AND FITTED MASS POINT IS THE LEAKAGE RATE COMPUTED FROM FIRST ORDER REGRESSION OF AIR MASS DATA.
4. UCL IS THE UPPER LIMIT OF THE 95% CONFIDENCE LEVEL OF AIR MASS DATA.

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	AVG. TEM DEG. F	AVG. PRE PSIA	VAP. PRE PSIA	LEAK SIM PER CENT	LEAK MAS PER CENT	AIR MASS POUNDS
1	0	90.319	59.3454	0.4732	0.000	0.000	754019
2	15	90.312	59.3444	0.4734	0.079	0.000	754012
3	30	90.305	59.3413	0.4735	0.230	0.230	753982
4	45	90.299	59.3403	0.4737	0.185	0.204	753975
5	60	90.290	59.3383	0.4739	0.189	0.199	753959
6	75	90.280	59.3373	0.4742	0.159	0.174	753956
7	90	90.271	59.3363	0.4737	0.123	0.141	753961
8	105	90.265	59.3343	0.4745	0.154	0.143	753934
9	120	90.252	59.3323	0.4746	0.151	0.143	753924
10	135	90.251	59.3312	0.4745	0.148	0.143	753914
11	150	90.234	59.3292	0.4745	0.135	0.137	753912
12	165	90.228	59.3282	0.4747	0.131	0.132	753905
13	180	90.223	59.3262	0.4754	0.151	0.136	753876
14	195	90.218	59.3252	0.4752	0.143	0.137	753872
15	210	90.208	59.3242	0.4757	0.138	0.135	753867
16	225	90.205	59.3222	0.4756	0.146	0.137	753847
17	240	90.193	59.3212	0.4763	0.141	0.137	753842
18	255	90.189	59.3202	0.4760	0.135	0.135	753839
19	270	90.181	59.3181	0.4766	0.144	0.136	753815

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 1 DEG. F	TEMP 2 DEG. F	TEMP 3 DEG. F	TEMP 4 DEG. F	TEMP 5 DEG. F	TEMP 6 DEG. F
1	0	93.540	93.210	93.080	92.870	93.070	93.120
2	15	93.530	93.210	93.070	92.880	93.080	93.100
3	30	93.520	93.190	93.080	92.890	93.070	93.100
4	45	93.500	93.180	93.040	92.840	93.050	93.090
5	60	93.480	93.150	93.030	92.860	93.050	93.050
6	75	93.440	93.150	93.040	92.840	93.040	93.030
7	90	93.440	93.100	93.000	92.810	93.010	93.030
8	105	93.430	93.140	93.020	92.810	93.030	93.000
9	120	93.400	93.090	93.000	92.820	93.000	93.000
10	135	93.410	93.100	92.990	92.770	92.990	93.000
11	150	93.390	93.070	92.960	92.760	92.990	92.960
12	165	93.390	93.040	92.950	92.730	92.950	92.950
13	180	93.380	93.040	92.950	92.760	92.960	92.960
14	195	93.370	93.020	92.930	92.740	92.930	92.940
15	210	93.340	93.000	92.890	92.700	92.920	92.940
16	225	93.330	93.020	92.890	92.710	92.910	92.920
17	240	93.310	93.000	92.890	92.700	92.890	92.900
18	255	93.310	92.990	92.870	92.670	92.890	92.900
19	270	93.290	92.980	92.860	92.670	92.870	92.880

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 7 DEG. F	TEMP 8 DEG. F	TEMP 9 DEG. F	TEMP 10 DEG. F	TEMP 11 DEG. F	TEMP 12 DEG. F
1	0	93.410	92.950	92.850	90.480	91.840	91.840
2	15	93.400	92.930	92.810	90.500	91.850	91.810
3	30	93.390	92.920	92.750	90.460	91.820	91.810
4	45	93.380	92.920	92.800	90.500	91.790	91.790
5	60	93.350	92.900	92.780	90.460	91.800	91.790
6	75	93.350	92.900	92.750	90.450	91.800	91.790
7	90	93.310	92.880	92.760	90.400	91.790	91.770
8	105	93.300	92.870	92.660	90.420	91.770	91.770
9	120	93.300	92.840	92.700	90.400	91.760	91.760
10	135	93.290	92.860	92.720	90.420	91.750	91.730
11	150	93.280	92.840	92.690	90.370	91.730	91.740
12	165	93.280	92.810	92.680	90.360	91.740	91.740
13	180	93.260	92.800	92.700	90.380	91.710	91.720
14	195	93.210	92.810	92.650	90.380	91.740	91.730
15	210	93.210	92.810	92.630	90.360	91.710	91.700
16	225	93.170	92.790	92.700	90.340	91.680	91.730
17	240	93.190	92.790	92.620	90.330	91.660	91.700
18	255	93.170	92.730	92.690	90.360	91.700	91.690
19	270	93.160	92.750	92.640	90.300	91.680	91.690

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 13 DEG. F	TEMP 14 DEG. F	TEMP 15 DEG. F	TEMP 16 DEG. F	TEMP 17 DEG. F	TEMP 18 DEG. F
1	0	92.020	92.300	92.280	92.570	95.130	92.820
2	15	92.030	92.300	92.280	92.560	95.130	92.840
3	30	92.030	92.300	92.260	92.540	95.140	92.790
4	45	92.020	92.270	92.270	92.550	95.130	92.770
5	60	92.010	92.240	92.240	92.560	95.150	92.830
6	75	91.990	92.270	92.240	92.540	95.130	92.760
7	90	91.990	92.250	92.260	92.540	95.140	92.810
8	105	91.970	92.240	92.250	92.520	95.140	92.790
9	120	91.960	92.250	92.220	92.510	95.110	92.780
10	135	91.970	92.250	92.230	92.520	95.110	92.760
11	150	91.930	92.240	92.200	92.510	95.090	92.710
12	165	91.950	92.220	92.210	92.500	95.090	92.760
13	180	91.940	92.210	92.200	92.530	95.070	92.730
14	195	91.900	92.190	92.200	92.510	95.060	92.710
15	210	91.940	92.210	92.190	92.500	95.060	92.740
16	225	91.900	92.180	92.180	92.510	95.070	92.720
17	240	91.890	92.170	92.170	92.490	95.080	92.740
18	255	91.880	92.170	92.170	92.510	95.040	92.720
19	270	91.880	92.150	92.150	92.500	95.060	92.710

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 19 DEG. F	TEMP 20 DEG. F	TEMP 21 DEG. F	TEMP 22 DEG. F	TEMP 23 DEG. F	TEMP 24 DEG. F
1	0	92.640	92.560	84.770	84.740	84.640	84.920
2	15	92.620	92.560	84.720	84.750	84.600	84.930
3	30	92.640	92.580	84.720	84.760	84.630	84.930
4	45	92.600	92.570	84.800	84.730	84.620	84.900
5	60	92.660	92.540	84.770	84.720	84.620	84.920
6	75	92.600	92.530	84.730	84.740	84.620	84.920
7	90	92.620	92.530	84.740	84.720	84.610	84.910
8	105	92.590	92.540	84.770	84.700	84.600	84.910
9	120	92.610	92.530	84.720	84.700	84.580	84.850
10	135	92.550	92.510	84.780	84.700	84.570	84.890
11	150	92.570	92.510	84.730	84.710	84.590	84.890
12	165	92.550	92.540	84.760	84.680	84.590	84.850
13	180	92.550	92.490	84.710	84.680	84.550	84.890
14	195	92.550	92.530	84.730	84.710	84.570	84.870
15	210	92.550	92.490	84.750	84.690	84.550	84.870
16	225	92.540	92.500	84.760	84.700	84.580	84.870
17	240	92.510	92.480	84.710	84.700	84.540	84.860
18	255	92.520	92.480	84.700	84.690	84.530	84.840
19	270	92.540	92.450	84.720	84.680	84.550	84.840

END OF TABLE

VARIABLE TABLE SUMMARY

SAMPLE NUMBER	DELTA MINS	TEMP 25 DEG. F	TEMP 26 DEG. F	TEMP 27 DEG. F	TEMP 28 DEG. F	TEMP 29 DEG. F	TEMP 30 DEG. F
1	0	84.680	84.110	85.380	85.190	85.430	84.510
2	15	84.690	84.060	85.380	85.190	85.440	84.490
3	30	84.670	84.080	85.400	85.180	85.400	84.500
4	45	84.640	84.080	85.430	85.190	85.410	84.500
5	60	84.670	84.070	85.380	85.180	85.400	84.490
6	75	84.640	84.080	85.400	85.150	85.420	84.480
7	90	84.640	84.080	85.410	85.150	85.400	84.500
8	105	84.640	84.060	85.420	85.150	85.410	84.490
9	120	84.640	84.070	85.370	85.140	85.400	84.490
10	135	84.650	84.070	85.380	85.150	85.400	84.480
11	150	84.620	84.050	85.360	85.150	85.380	84.480
12	165	84.580	84.050	85.350	85.140	85.380	84.490
13	180	84.590	84.050	85.340	85.130	85.400	84.470
14	195	84.600	84.070	85.370	85.150	85.390	84.480
15	210	84.600	84.060	85.350	85.150	85.380	84.470
16	225	84.600	84.050	85.370	85.140	85.360	84.480
17	240	84.580	84.040	85.400	85.130	85.370	84.470
18	255	84.570	84.060	85.350	85.130	85.370	84.470
19	270	84.560	84.050	85.380	85.130	85.380	84.480

END OF TABLE

VARIABLE TABLE SUMMARY

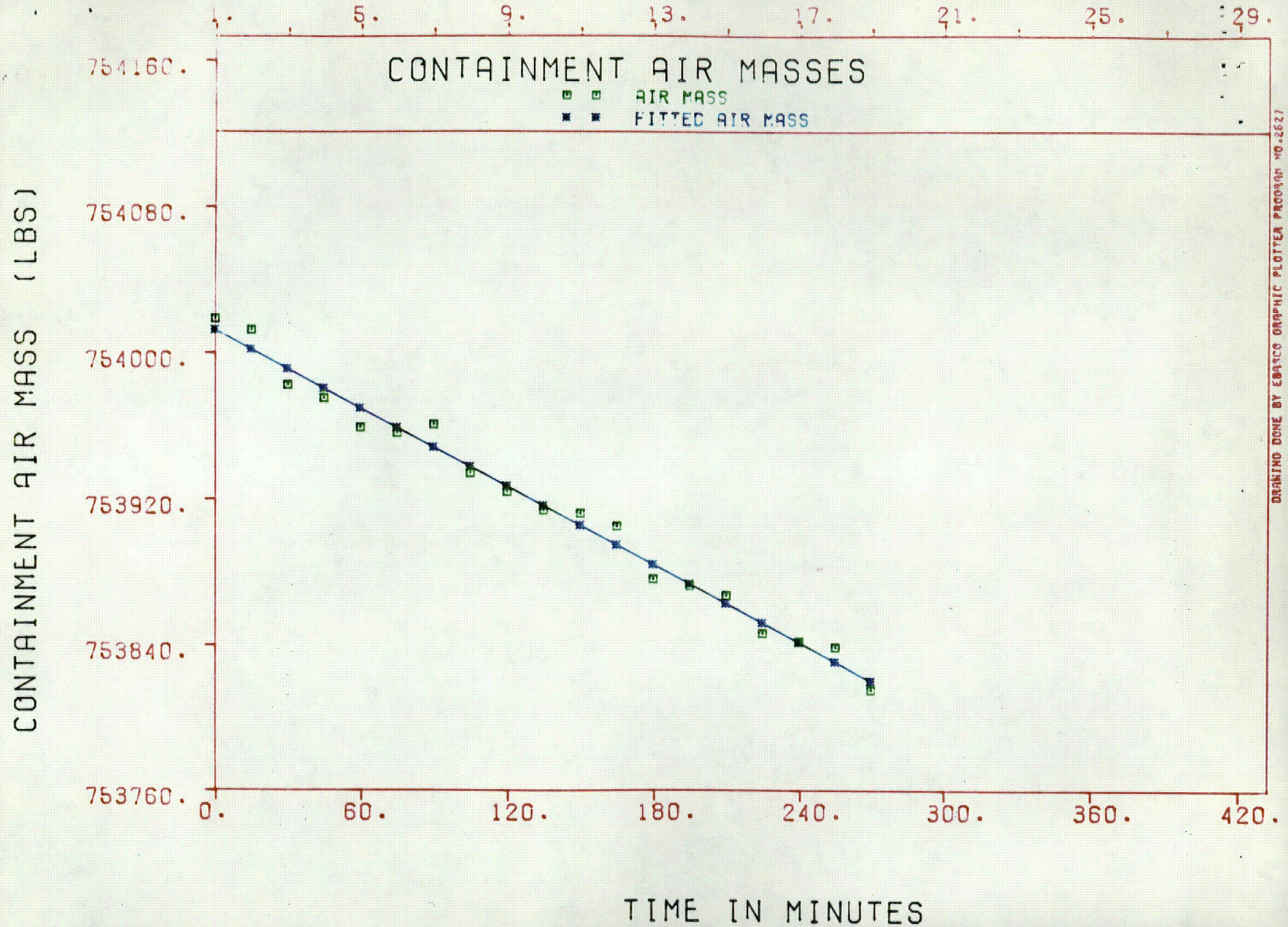
SAMPLE NUMBER	DELTA MINS	PRES 1 PSIA	HUM 1 FRACTION	HUM 2 FRACTION	HUM 3 FRACTION	HUM 4 FRACTION	HUM 5 FRACTION
1	0	59.345	DELETED	0.702	0.700	0.693	0.648
2	15	59.344	DELETED	0.702	0.701	0.692	0.648
3	30	59.341	DELETED	0.703	0.699	0.693	0.648
4	45	59.340	DELETED	0.703	0.700	0.693	0.649
5	60	59.338	DELETED	0.702	0.700	0.693	0.650
6	75	59.337	DELETED	0.703	0.700	0.694	0.651
7	90	59.336	DELETED	0.702	0.697	0.693	0.650
8	105	59.334	DELETED	0.703	0.701	0.694	0.652
9	120	59.332	DELETED	0.704	0.700	0.694	0.652
10	135	59.331	DELETED	0.703	0.697	0.694	0.653
11	150	59.329	DELETED	0.702	0.697	0.693	0.653
12	165	59.328	DELETED	0.703	0.698	0.693	0.654
13	180	59.326	DELETED	0.704	0.702	0.694	0.654
14	195	59.325	DELETED	0.703	0.699	0.694	0.655
15	210	59.324	DELETED	0.704	0.701	0.694	0.655
16	225	59.322	DELETED	0.704	0.698	0.694	0.656
17	240	59.321	DELETED	0.705	0.703	0.695	0.657
18	255	59.320	DELETED	0.704	0.699	0.694	0.657
19	270	59.318	DELETED	0.704	0.702	0.695	0.658

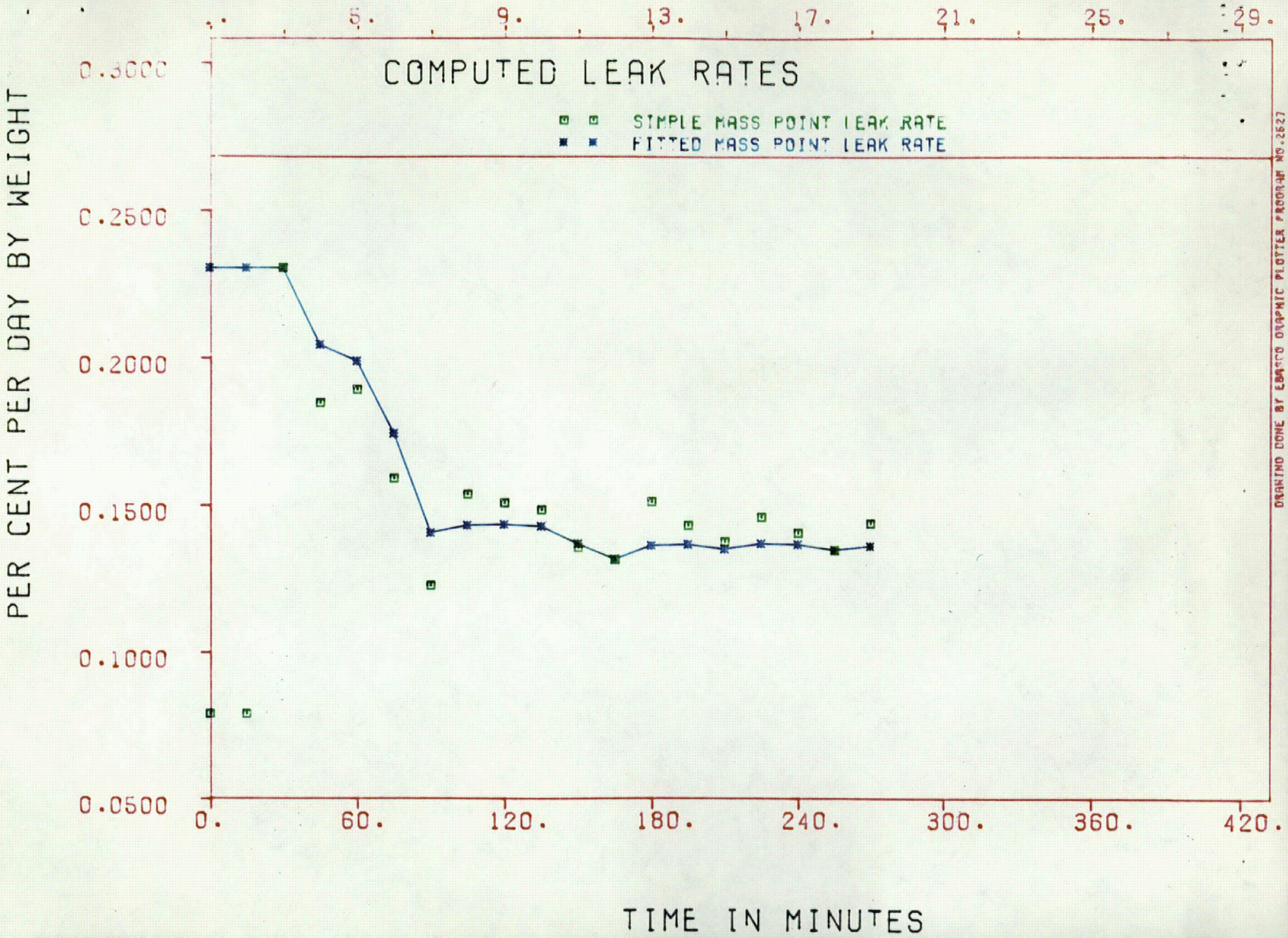
END OF TABLE

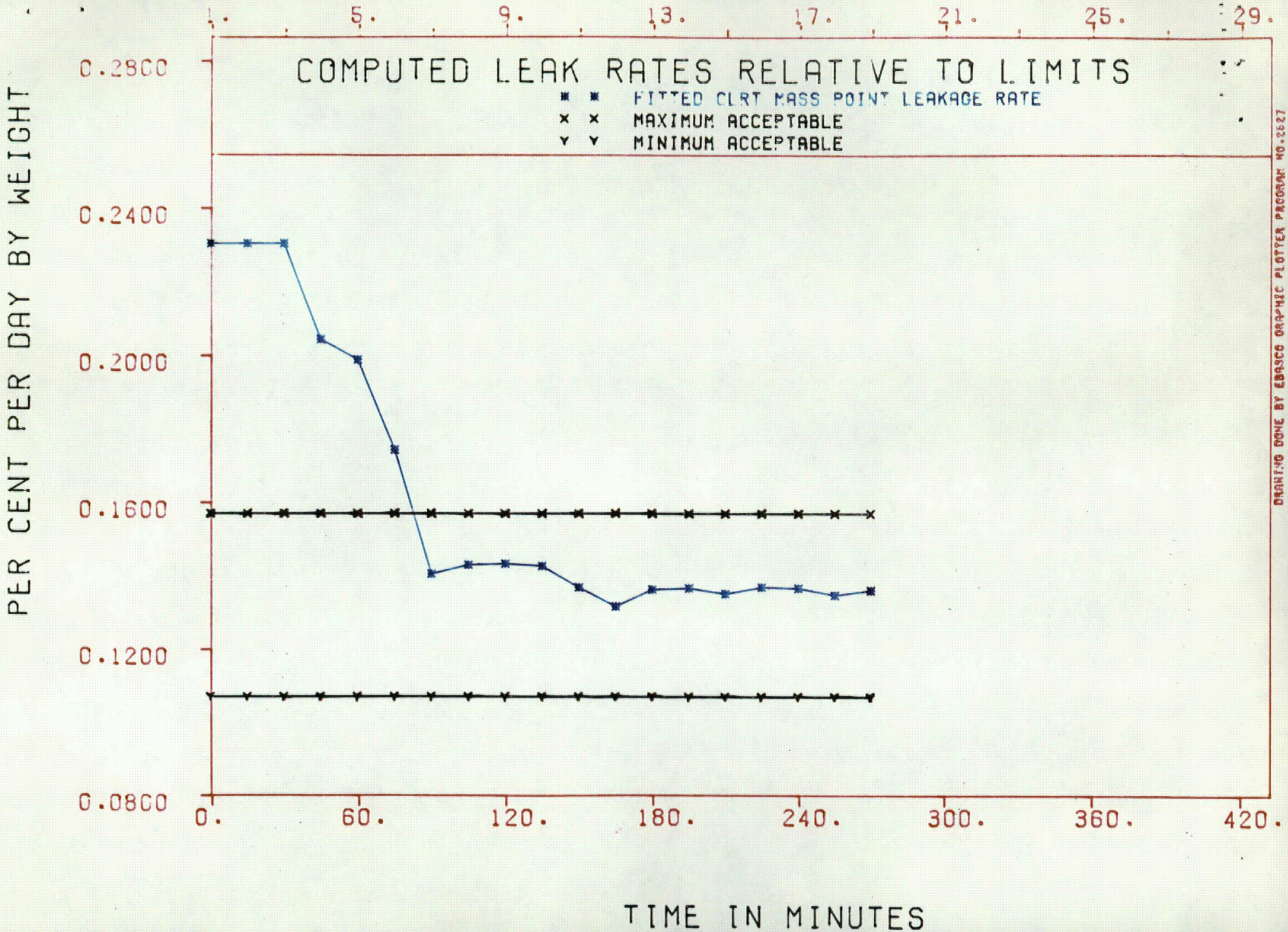
VARIABLE TABLE SUMMARY

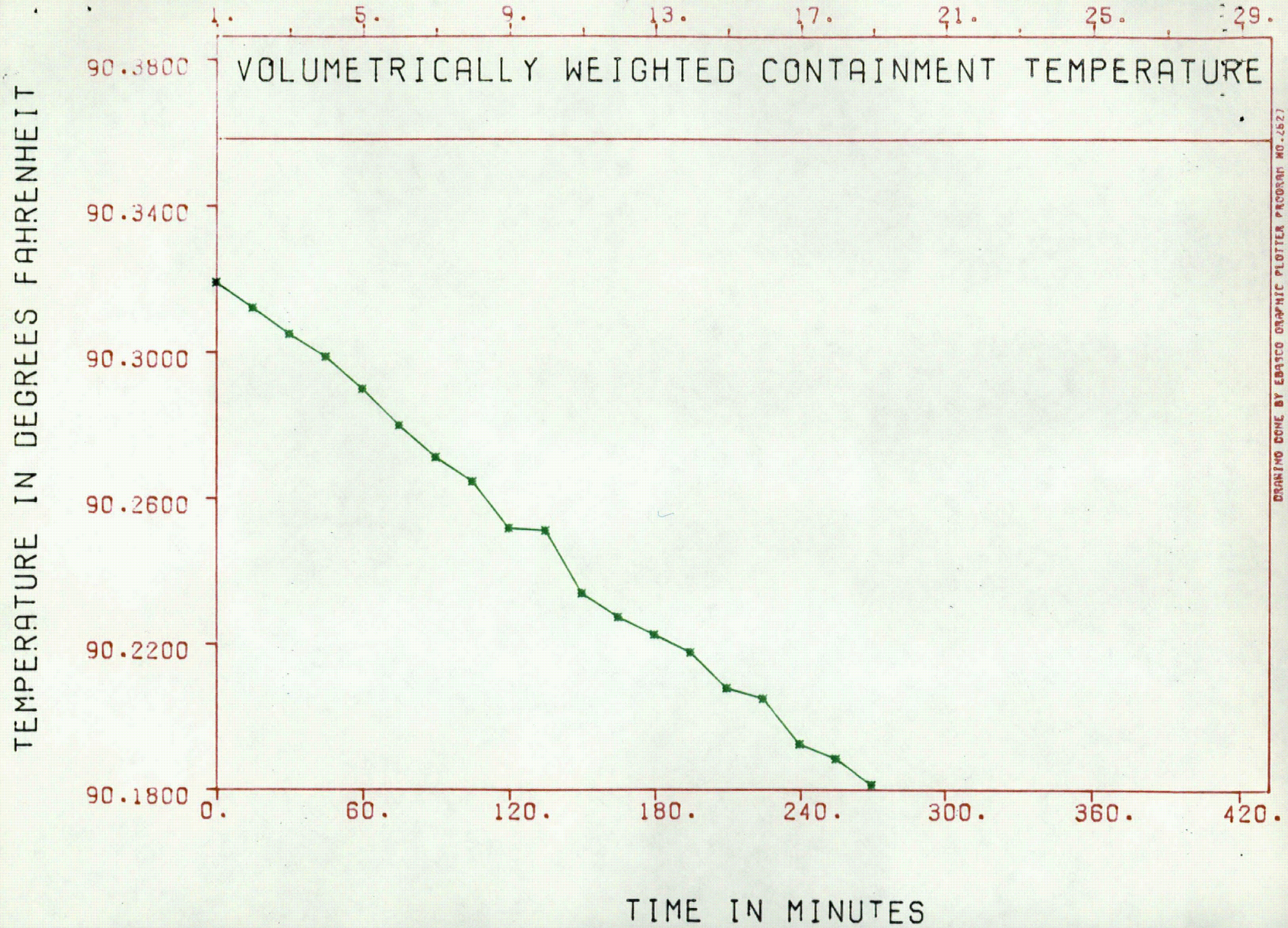
SAMPLE NUMBER	DELTA MINS	HUM 6 FRACTION	HUM 7 FRACTION	HUM 8 FRACTION	HUM 9 FRACTION	HUM 10 FRACTION
1	0	0.652	DELETED	0.672	0.657	0.659
2	15	0.653	DELETED	0.673	0.657	0.659
3	30	0.653	DELETED	0.674	0.658	0.660
4	45	0.654	DELETED	0.674	0.658	0.661
5	60	0.655	DELETED	0.675	0.659	0.661
6	75	0.655	DELETED	0.675	0.660	0.661
7	90	0.656	DELETED	0.675	0.660	0.662
8	105	0.656	DELETED	0.676	0.661	0.663
9	120	0.658	DELETED	0.677	0.662	0.663
10	135	0.658	DELETED	0.677	0.662	0.664
11	150	0.658	DELETED	0.678	0.663	0.664
12	165	0.659	DELETED	0.679	0.663	0.665
13	180	0.660	DELETED	0.679	0.664	0.665
14	195	0.661	DELETED	0.680	0.665	0.666
15	210	0.661	DELETED	0.680	0.666	0.667
16	225	0.662	DELETED	0.681	0.666	0.667
17	240	0.663	DELETED	0.682	0.667	0.668
18	255	0.663	DELETED	0.682	0.667	0.668
19	270	0.664	DELETED	0.682	0.668	0.669

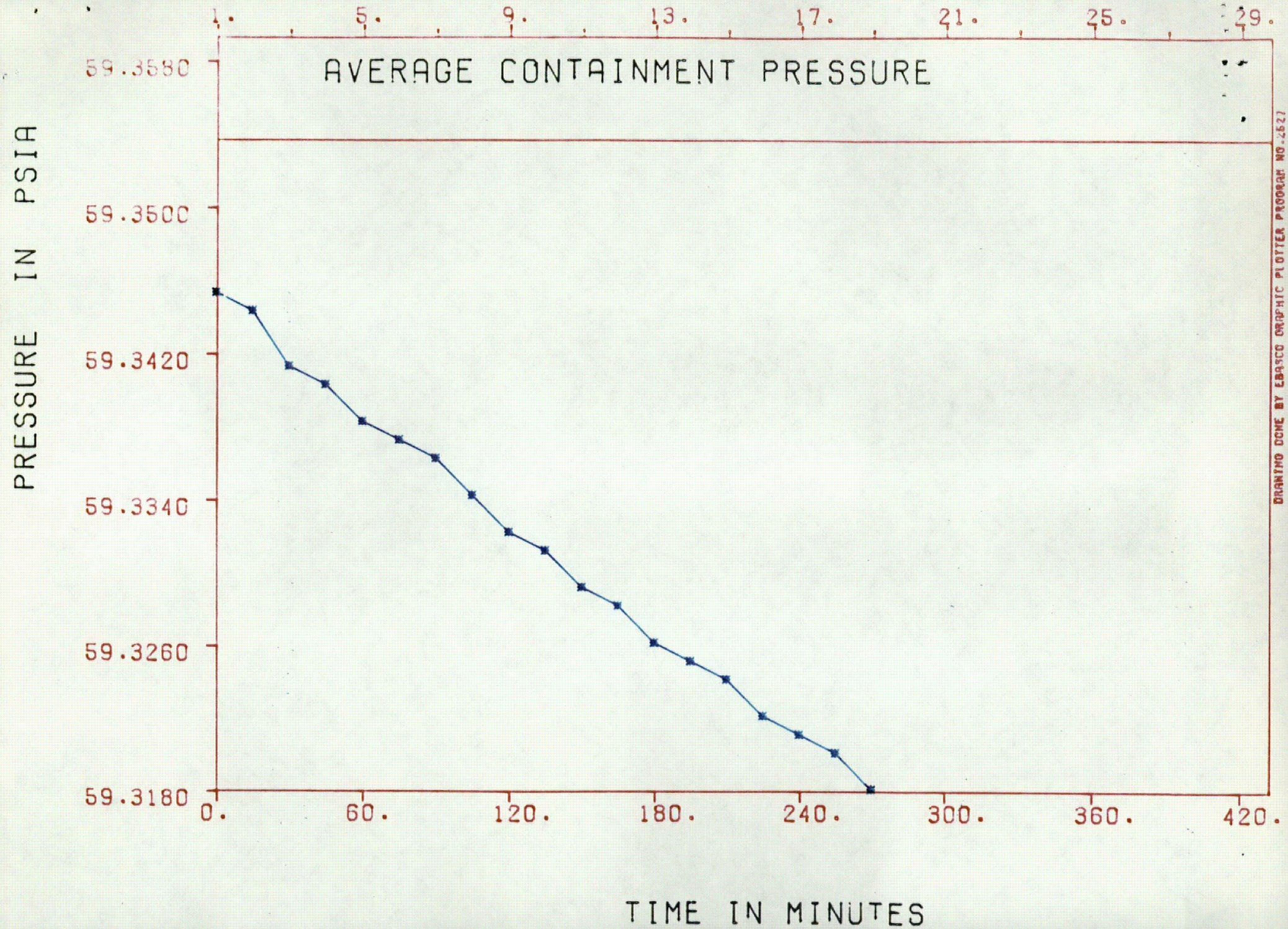
END OF TABLE

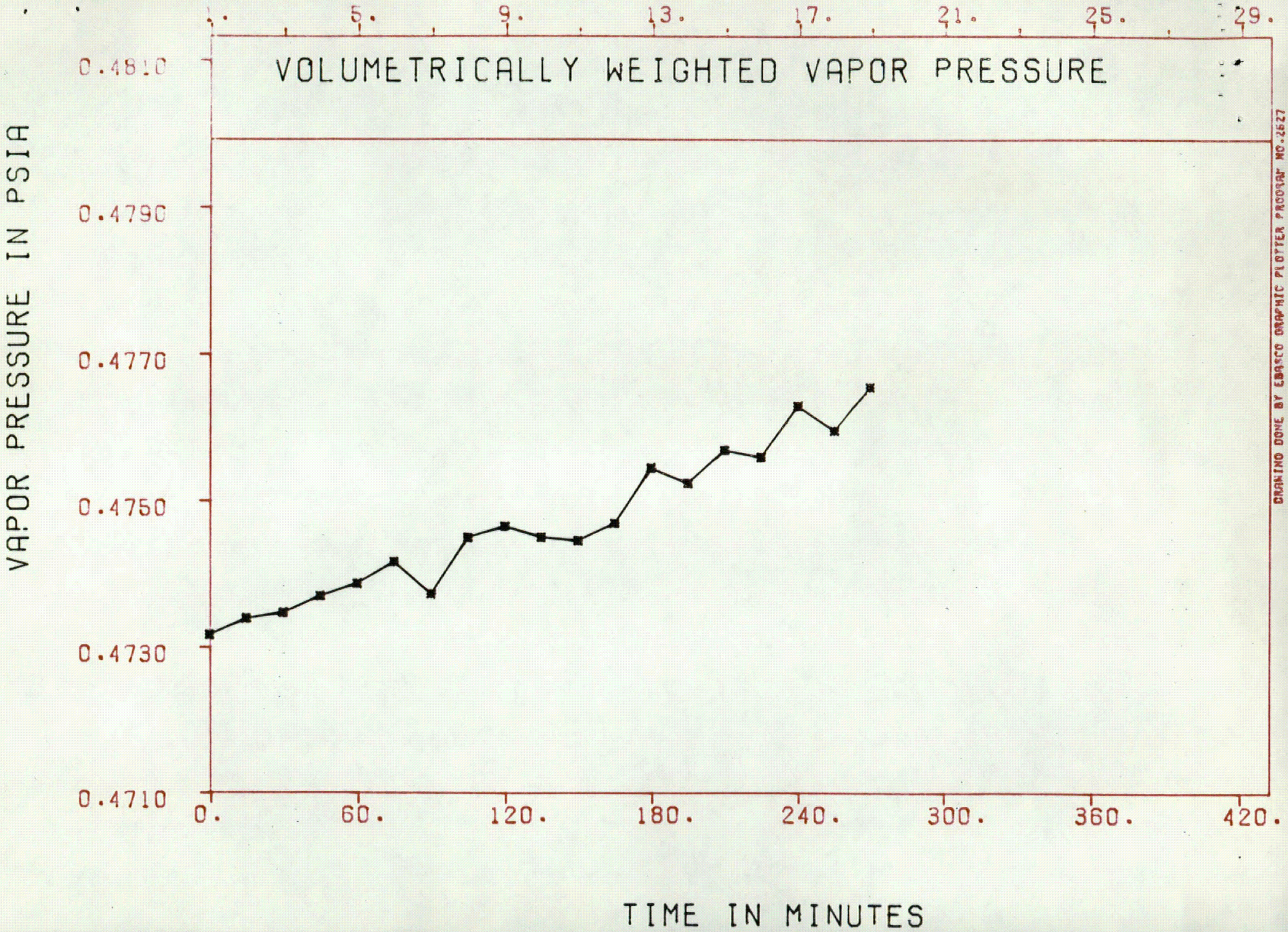

CONTAINMENT AIR MASSES
AIR MASS
FITTED AIR MASS
CONTAINMENT AIR MASS (LBS)
754160.
754080.
754000.
753920.
753840.
753760.
1.
5.
9.
13.
17.
21.
25.
29.
0.
60.
120.
180.
240.
300.
360.
420.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


COMPUTED LEAK RATES
SIMPLE MASS POINT LEAK RATE
FITTED MASS POINT LEAK RATE
PER CENT PER DAY BY WEIGHT
0.3000
0.2500
0.2000
0.1500
0.1000
0.0500
0.
60.
120.
180.
240.
300.
360.
420.
5.
9.
13.
17.
21.
25.
29.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


COMPUTED LEAK RATES RELATIVE TO LIMITS
FITTED CLRT MASS POINT LEAKAGE RATE
MAXIMUM ACCEPTABLE
MINIMUM ACCEPTABLE
PER CENT PER DAY BY WEIGHT
0.2800
0.2400
0.2000
0.1600
0.1200
0.0800
1.
5.
9.
13.
17.
21.
25.
29.
0.
60.
120.
180.
240.
300.
360.
420.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


VOLUMETRICALLY WEIGHTED CONTAINMENT TEMPERATURE
TEMPERATURE IN DEGREES FAHRENHEIT
90.3800
90.3400
90.3000
90.2600
90.2200
90.1800
1.
5.
9.
13.
17.
21.
25.
29.
0.
60.
120.
180.
240.
300.
360.
420.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627


AVERAGE CONTAINMENT PRESSURE
PRESSURE IN PSIA
59.3580
59.3500
59.3420
59.3340
59.3260
59.3180
1.
5.
9.
13.
17.
21.
25.
29.
0.
60.
120.
180.
240.
300.
360.
420.
TIME IN MINUTES
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2527


VOLUMETRICALLY WEIGHTED VAPOR PRESSURE
VAPOR PRESSURE IN PSIA
0.4810
0.4790
0.4770
0.4750
0.4730
0.4710
1.
5.
9.
13.
17.
21.
25.
29.
0.
60.
120.
180.
240.
300.
360.
420.
TIME IN MINUTES
GRAPHING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627

APPENDIX A.3

COMPUTER GENERATED REPORT

TEMPERATURE STABILIZATION

EBASCO SERVICES
INCORPORATED

TEMPERATURE STABILIZATION

A	B	C	D	E
0045	98.390			
0100	97.465			
0115	96.711			
0130	96.130			
0145	95.669			
0200	95.273			
0215	94.948			
0230	94.671			
0245	94.427			
0300	94.209			
0315	94.015			
0330	93.850			
0345	93.679			
0400	93.551			
0415	93.411			
0430	93.283			
0445	93.175	1.304	0.504	0.800
0500	93.071	1.100	0.480	0.620
0515	92.966	0.936	0.445	0.491
0545	92.783	0.722	0.392	0.330
0600	92.701	0.643	0.370	0.273
0615	92.625	0.581	0.341	0.240
0630	92.557	0.549	0.316	0.233
0645	92.476	0.488	0.307	0.181
0700	92.403	0.452	0.298	0.154
0715	92.344	0.418	0.281	0.137
0730	92.282	0.392	0.275	0.117
0745	92.211	0.367	0.265	0.102
0800	92.151	0.350	0.252	0.098

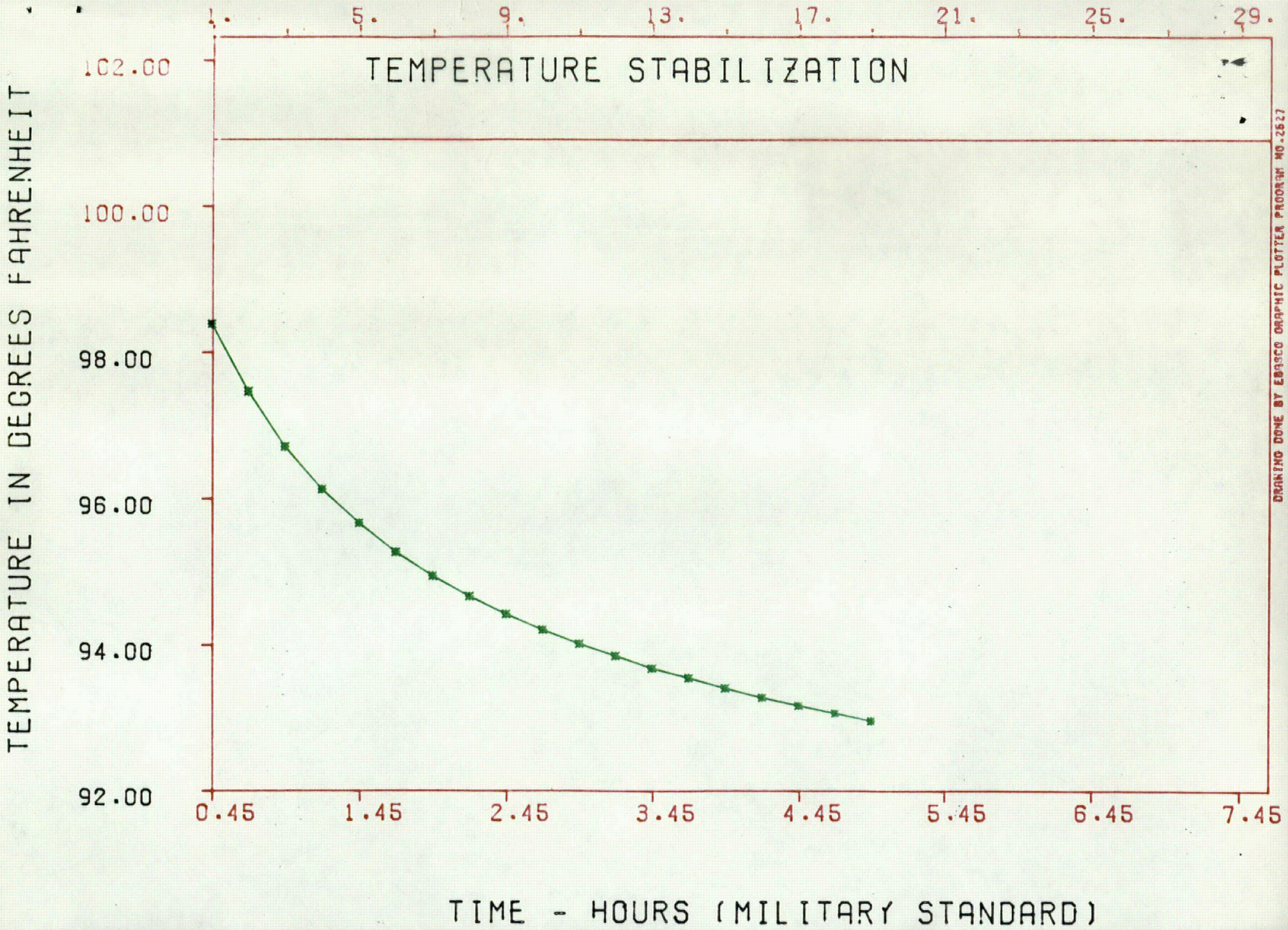
A = TIME OF DAY IN MILITARY STANDARD

B = AVERAGE CONTAINMENT TEMPERATURE F

C = AVERAGE DIFFERENCE IN TEMP. OVER LAST 4 HOURS

D = AVERAGE DIFFERENCE IN TEMP. OVER LAST 1 HOUR

E = C - D


TEMPERATURE STABILIZATION
TEMPERATURE IN DEGREES FAHRENHEIT
102.00
100.00
98.00
96.00
94.00
92.00
1.
5.
9.
13.
17.
21.
25.
29.
0.45
1.45
2.45
3.45
4.45
5.45
6.45
7.45
TIME - HOURS (MILITARY STANDARD)
DRAWING DONE BY EBASCO GRAPHIC PLOTTER PROGRAM NO.2627